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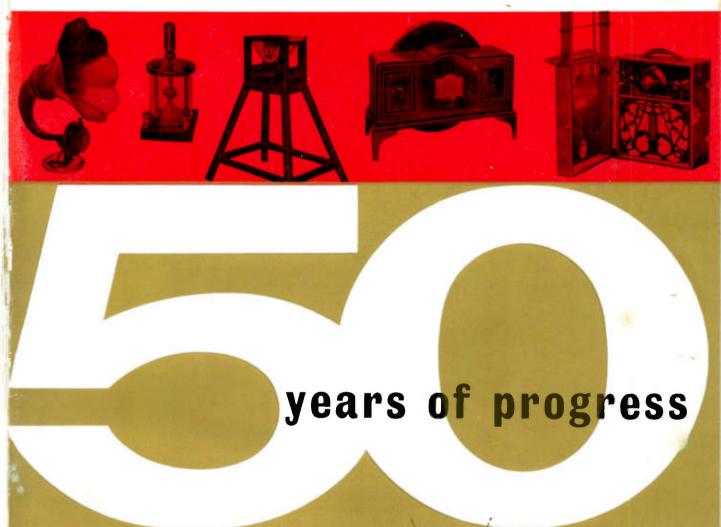
APRIL 1961

TWO SHILLINGS

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Electronics

Television







We make three germanium NPN alloy high speed switching transistors, each one an ace in its own class, and if you don't think that's something to write home about, just look at these brief specifications:

	Maximum	Maximum	Maximum	Minimum
	Vcb (Volts)	Vceo (Volts)	I _c (mA)	fα (Mc's)
XA701	25	15	200	3
XA702	25	15	400	5
XA703	25	12	400	10

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| Example of Collector Voltage: 1.SV to 10.SV (up to 150V using excernal supplies)
| Example of Collector Voltage of C

0-1 mA, 0-40 mA 0-1A 0-25, 0-250 measured at 1 Kc/s Collector Current:

Beta: Noise Measurement: 1-20, 21-40 dB

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Service Spec. KII4.

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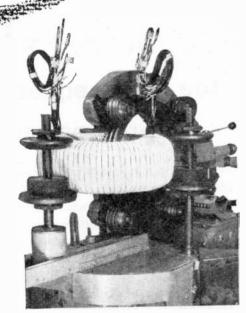
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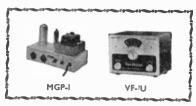
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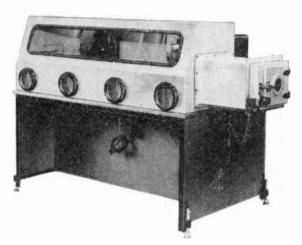
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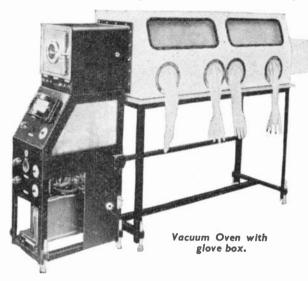
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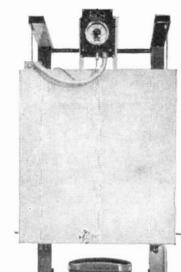


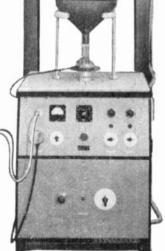
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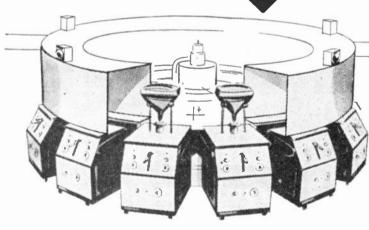




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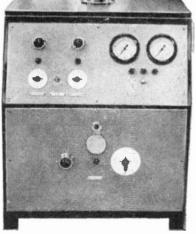
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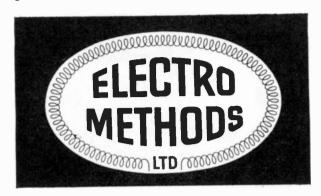
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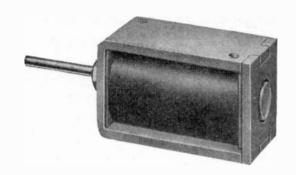
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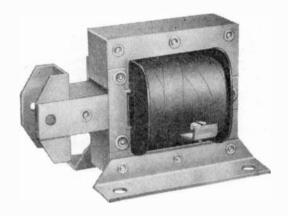




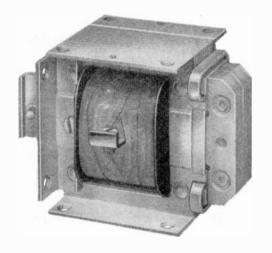


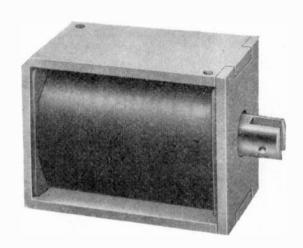














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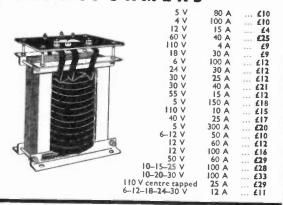
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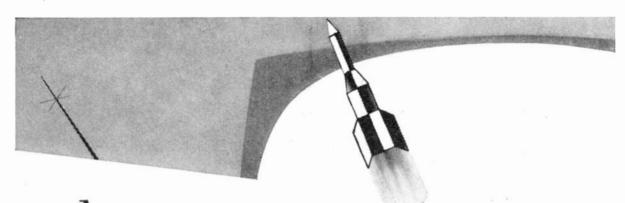
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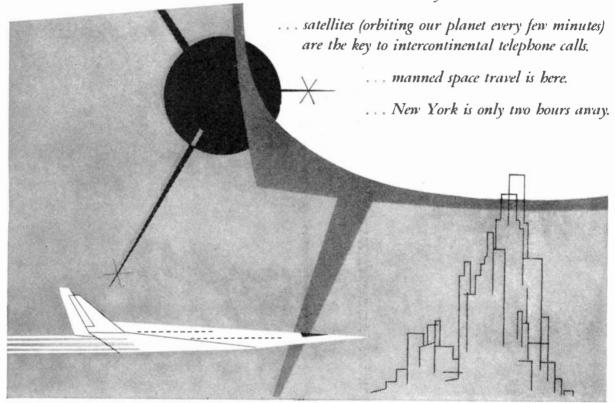
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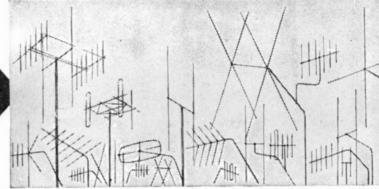
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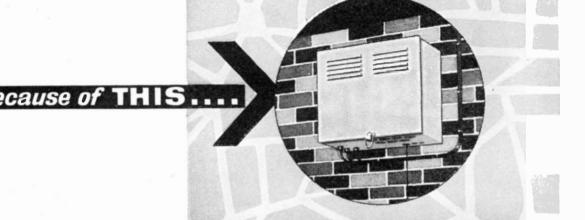
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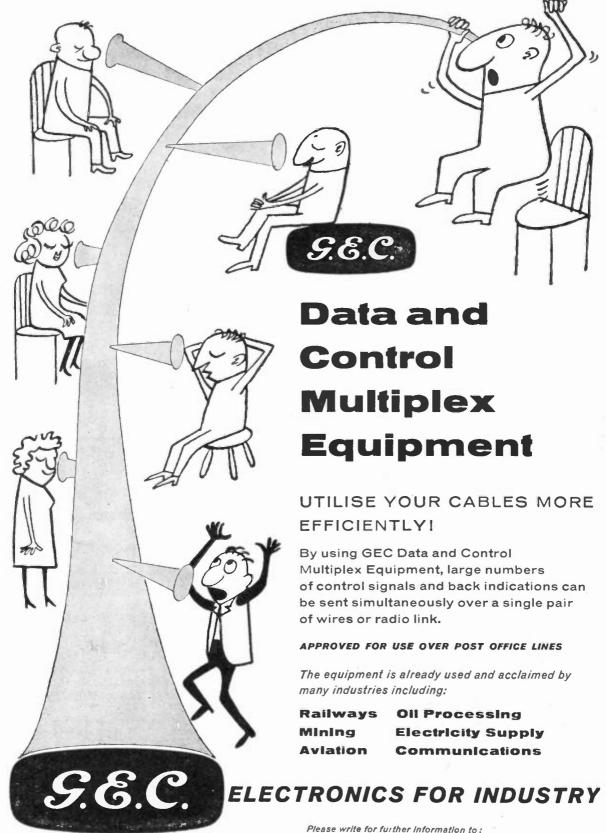
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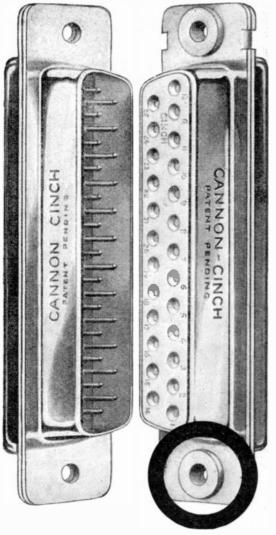
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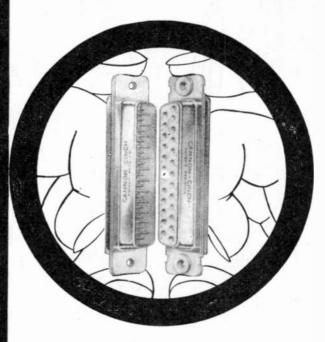


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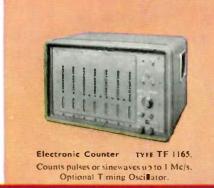
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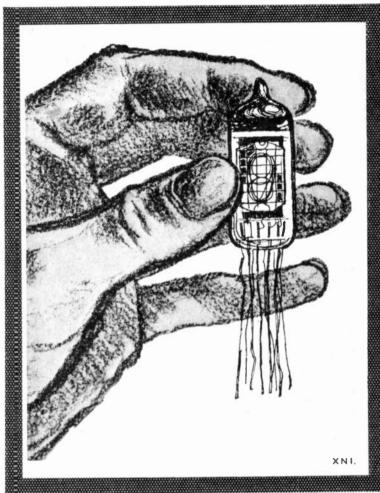
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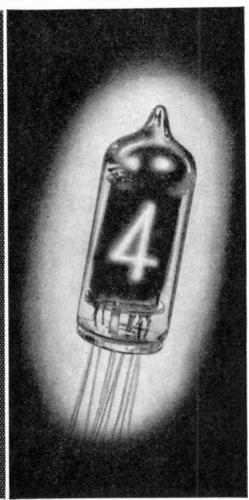
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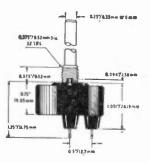
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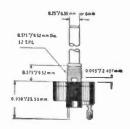
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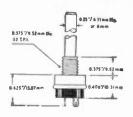
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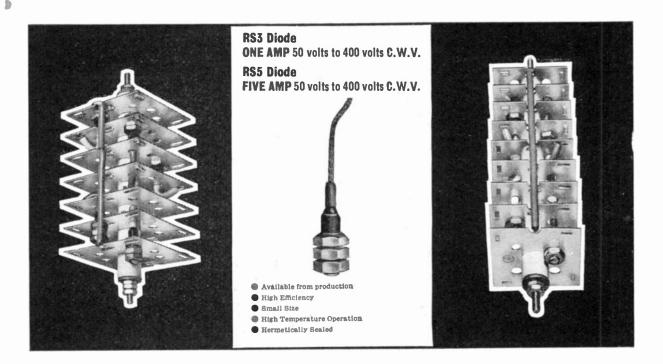


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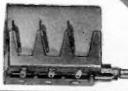
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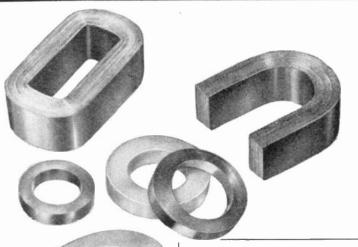
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Maximum permeability #max	15 000 to 40 800	50 008 to 158 000	12 000 to 20 000	200 008 10 400 000	3 000 to 6 000
Magnetising force for #max-cersteds	0.20 to 0.40	8.825 te 0.84	0.2 te 0.5	0.03 to 0.10	2.0 te 5.0
Maximum flux density-gauss	16 000	8 000	13 000	14 000	24 080
Geercive ferce in eersteds for B _{max} = 5 800 gauss	0.15	0.03	0-15	0.05*	2.3†
Remanence in gauss for B _{max} — 5 000 gauss	4 000	3 500	3 500	13 000°	16 000†
Rysteresis loss in ergs/cc/ cycle for 0 _{max} - 5 000 gauss	160	40	200	220*	12 500 t
Total Toss In watts/lb for 0 max = 5 000 gauss 50 c/s 0.015 in, sheet	0.11	0.04	0.2	0.3*	41

* for \$ max - 14 000 gauss

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SECONDARY (b): An H.T. winding is provided on certain models for stabilised circuits and this is tapped at each 50V. from 0-250 volts.

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	SECONDARY (A)			SECONDARY (B)		
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140.	R.M.S.	R.M.S. OR D.C. CHOKE	D.C. COND.	R.M.S.	R.M.S. CURRENT	
P-2945	1 to 24V.	1-6 A ,	1-0A.	_	_	
P-2946	2 to 46V.	1·6 A .	1-0A.	_	_	
P-2947	1 to 24V.	3·2A.	2-0A.	_	_	
P-2948	1 to 24V.	1-6A.	1-0A.	0-250V. (50V. 5teps)	40 mA	
P-2949	2 to 48V.	1-6A.	1-0A.	0-250V. (50V. Steps)	40mA	
P-2950	1 to 24V.	3·2A.	2·0A.	0-250V. (50V. Steps)	40mA	
P-2951	2 to 48V.	3-2A.	2-0A.	0-250V. (50V. Steps)	40mA	
P-2952	1 to 24V.	5-0A.	3·2A.	0-250V. (50V. Steps)	40mA	
P-2953	2 to 48V.	5-0A.	3-2A.	0-250V. (50V. Steps)	40mA	

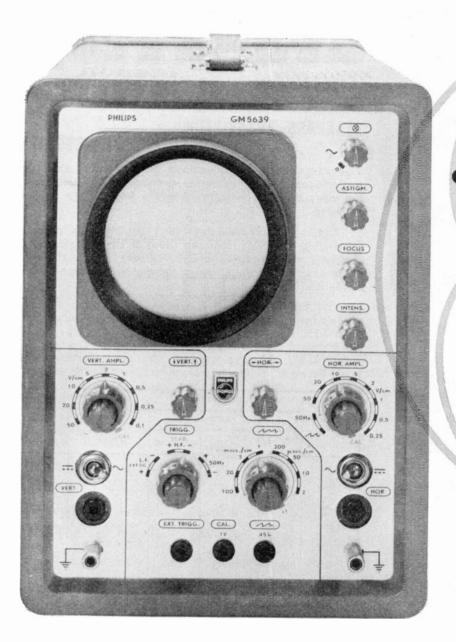
A table showing method of connection is supplied with each transformer.

STANDARD SMOOTHING CHOKES

Catalogue Number	D.C. Current	Inductance	Approx. D.C. Resis. Ohms.	Model Size	Termina Positions
P-2954	1-6A	40mH	0-62	9000/49	2-3
P-2955	1-6A	60mH	0.90	9000/57	9–10
P-2956	3-2A	15mH	0-31	9000/49	2-3
P-2957	3-2A	35mH	0-39	9000/65	9-10
P-2958	5-0A	9mH	0-15	9000/57	9-10
P-2959	5-0A	25mH	0-16	9000/73	9–10
P-2959	5-0A	25mH	0.16	9000/73	I

The Atlantic Series can accommodate transformer designs rated up to 650VA at 50 c.p.s. We shall be pleased to quote for your specific requirements.

PARMEKO LTD · PERCY ROAD · LEICESTER · ENGLAND

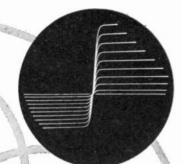


X-Y oscilloscope

GM 5639

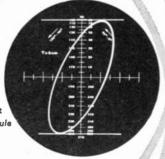
PHILIPS electronic measuring

Sold and serviced by Philips Organizations all over the world Sole Distributors in the U.K.: Research & Control Instruments Ltd., 207 King's Cross Road, London W.C. I Overseas enquiries please, to the manufacturers, N.V. Philips, EMA-Department, Eindhoven, the Netherlands.

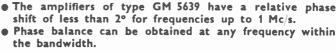


Ic - Vc curves of a transistor

with exactly identical amplifiers



Phase measurement with special graticule



Due to these features curve tracing without any distortion as well as accurate phase measurements can be carried out.

The time base with its sensitive and stable triggering permits of the oscilloscope also being used as a general purpose instrument.

Thus it is suitable for a wide range of applications in industry and research, especially in semiconductor and power-current techniques.

Characteristic Features

Both amplifiers

: 0-1 Mc/s Bandwidth

Sensitivity

Y-amplifier 100 mV/cm, X-amplifier 200 mV/cm Attenuation up to 50 V/cm adjustable in 9 calibrated steps (accuracy

 \pm 3%) and continuous 1:3

Relative phase shift less than 20 for frequencies up to 1 Mc/s.

Time base

Sweep speeds: 2 µs/cm- 100 ms/cm adjustable in 8 calibrated steps (accuracy

 \pm 50/0) or continuously up to 600 ms/cm.

Triggering facilities: internal or from an external source for pulse repetition frequencies up to 1 Mc/s.

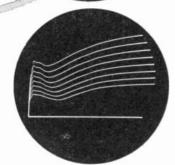
Adjustable triggerstability.

C.R.T.

10 cm flat-faced tube with 2 kV acceleration voltage.

Different graticules for curve tracing and phase measurements are supplied.





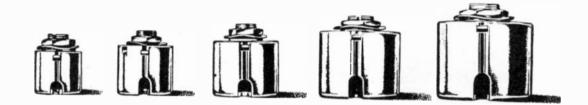
la - Va curves of a tetrode

instruments: quality tools for industry and research



NEW VINKOR SERIES

Covers frequencies from 100 Kc/s to Mc/s



A new series of Vinkor adjustable pot cores has now been developed by Mullard for use in the frequency range 100 kc/s to 2 Mc/s. This series is in addition to the highly successful group already widely used for frequencies between 1 kc/s and 200 kc/s.

The world's most efficient pot core assembly, the Mullard Vinkor gives a choice of 3 permeabilities and has exceptionally high performance and stability.

Write today for full details of the wide range of Vinkors now available.

Mullard VINKOR

ADJUSTABLE POT CORE ASSEMBLIES



SMA COUNTS selects indicates

Here is a tube which can be used either as a counter and indicator, or selector and indicator—just as you require. It's the Mullard Z504S—a 4kc/s tube of all-glass construction. Modern techniques make economically possible these functions in one envelope. The Z504S brings you economies from every angle. It is a remarkably inexpensive tube . . . and achieves some really welcome economies in equipment space. Moreover it is made to close mechanical tolerances and so avoids the need for post-assembly adjustments. If you would like to know more about the new multi-purpose tube, just write to Mullard quoting reference M4104.



MULLARD LIMITED · Mullard House · Torrington Place · London W.C.1

Telephone: LANgham 6633



This advertisement invites YOU to contact HP RADIO for **EDDYSTONE**



EDDYSTONE 680/X

A 15 valve communication receiver with many refinements, including crystal filter, variable selectivity "5" meter, push-pull output and stabilized supply to oscillator stages. 1110 kc/s to 480 kc/s and 2.5 to 30 mc/s in 5 switched bands. Electrical performance, sensitivity for 50 milliwatts, 15 db signal/noise ratio, 4 microvolts on all ranges.



EDDYSTONE 840/A

Communication receiver at a moderate price. 7 B8A valves in a straightforward superheterodyne circuit. 4 wave bands 30.6–10.5 mc/s, 10.6–3.7 mc/s, 3.8 mc/s-1.4 mc/s, 205–620 metres. Sensitivity better than 10 microvolts. Selectivity 30 db down 10 kc/s off resonance. AC/DC, Internal speaker. (55.0.0.)

EDDYSTONE 880

The Eddystone 880 high stability The Eddystone 880 high stability communications receiver has been designed expressly for use in professional communications systems. Tuning range is from 500 kc/s to 30.5 mc/s. Please write for technical specification. £380.0.0.



RADIO RECEIVERS

EDDYSTONE 888/A

A 12 valve receiver designed for A 12 valve receiver designed for the amateur bands, giving full bandspread. Double superhetero-dyne with high selectivity and excellent signal to noise charac-teristics. Crystal calibrator audio filter, separate gain controls, nter, separate gain controls, oscillator trimmer. Frequency 1,800–2,000 kc/s, 3,500–4,000 kc/s, 7,000–7,300 kc/s, 14,000–14,350 kc/s, 21,000–21,500 kc/s, 28,000–30,000 kc/s. £110.0.0



EDDYSTONE 870/A

A compact, precision built receiver for the home, giving news and entertainment from the whole world. 5 wavebands, vernier device. AC/DC operation, built-in mains filter and loud speaker. Two tone metal cabinet. (33.0.0





51. COUNTY ROAD LIVERPOOL, 4

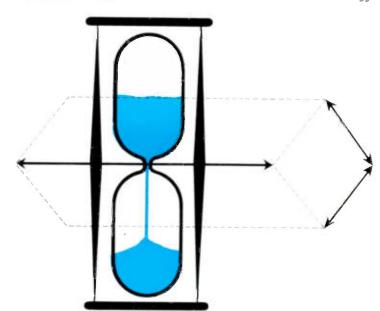
To:	H.P.	RADIO	SERVICES	LTD.,	51	COUNTY	RD.,	LIVERPOOL,	4
	P	lease sen	d particular	s of the	ED	DYSTONE E	RADIO	RANGE	

Address

THIS COUPON

STC

and the fourth dimension—



RELIABILITY...

The fourth dimension, time—invisible and intangible, but in the case of STC components, definable in terms of sustained, faultless performance—is a very definite factor incorporated in their design and manufacture.

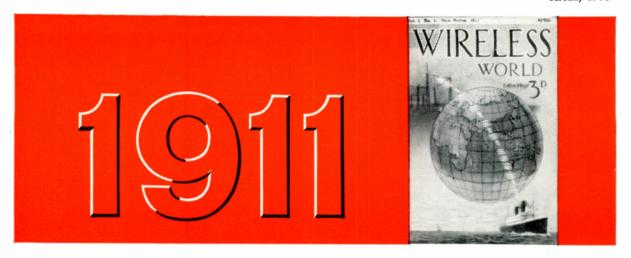
Such dependability is very necessary in view of the vital functions that STC components have to perform—in equipment for communications, navigation and remote control; and it is the reason why STC components are trusted implicitly by manufacturers of electronic equipment all over the world.

Capacitors Crystal Filters **Ferrites** Germanium Diodes Germanium Photocells Hermetic Seals High Stability Resistors Infra-red Filters Ionisation Gauges Magnetic Materials Quartz Crystals Selenium Rectifiers Silicon Rectifiers Silistors Suppressors Thermal Delay Switches **Thermistors** Thermocouples **Transformers Transistors** Tunnel Diodes Vacuum Capacitors Valves Zener Diodes



Standard Telephones and Cables Limited

Registered Office: Connaught House, Aldwych, London W.C.2.



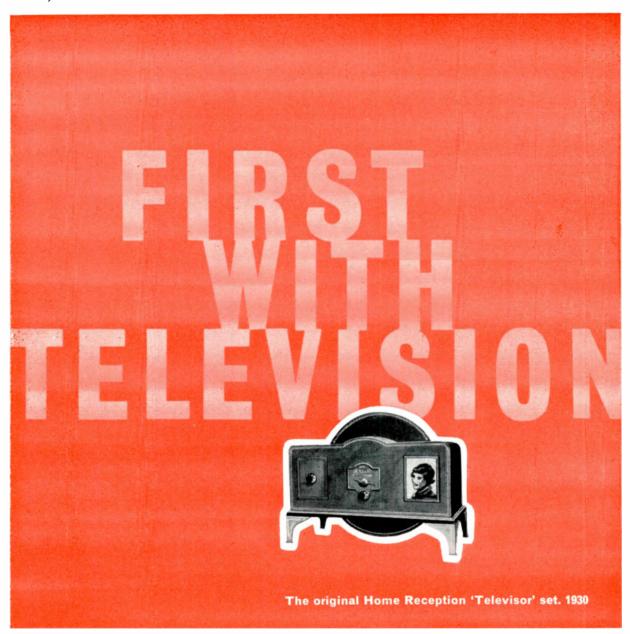
For the past fifty years "The Wireless World" has constantly performed an unfailing and vital service to the Radio Industry of Great Britain.

Within the half century there can have been no really worth-while development or technical achievement by British radio engineers which has not been accurately reviewed in the columns of "The Wireless World".

Bush Radio Limited take the opportunity to express their appreciation of this service and offer their congratulations in this Golden Jubilee edition









Rank Cintel have a direct link with the very beginning of Television. To emphasize the physical aspects of this connection, portions of the fabric of John L. Baird's original Research Laboratory has been incorporated in the modern premises that have grown, over the years, on this historic site. Here, where Television history was made, Electronic history is still being made. Frontiers have widened, techniques changed but the spirit of leadership is still with RANK CINTEL.

Announcing the

6th INTERNATIONAL INSTRUMENT SHOW

The Polarad Microwave Receiver Model R-BI with RW-T Tuning Head is a triple conversion Superheterodyne Receives, covering the frequency range from 2 to 75 kmc/s in one unit.

The Polarad CSG Electronic Sweep Generator has five interchangeable heads covering 1.0 to 16.0 kmc/s with wide range of sweep rates and continuously variable sweep width.

The Precision π magnetic recorder/reproducer is an advanced instrumentation tape recorder, fully transistorized and truly portable.

Interchangeable components and a c c e s s o r i e s provide maximum versatility.

The F.S. 300 series instrumentation tape recorder measures only 5" x 4" x 2". It incorporates the Precision unique coaxially stacked reel system and provides facilities for multi-tracked recording up to 160 kc/s for 3 minutes or 10 kc/s for 56 minutes.

minutes.
The entire electronics package includes record and reproduce channels, oscillator and timing reference.

Type 2305A Level Recorder is designed for the accurate recording of signal levels in the frequency range from 10 c/s to 200 kc/s is well as for DC signals. Levels may be recorded as a function of time or of frequency when the recorder is used in conjunction with one of the B & K Beat Frequency Oscillators or Frequency Analyzers.



The Polarad Model SA-84W Spectrum Analyzer is a portable instrument covering the range from 10 to 40880 mc/s in a single unit. It provides a spectrum analysis display for precise measurements of wide and narrow pulses, F.M. characteristics, and harmonic and spurious content of signals.

The 1961 INTERNATIONAL INSTRUMENT SHOW, once again sponsored by B & K Laboratories Limited, will be larger and more varied than ever. Over 50 manufacturers representing 10 countries will be exhibiting the world's most advanced instrumentation and electronic apparatus.

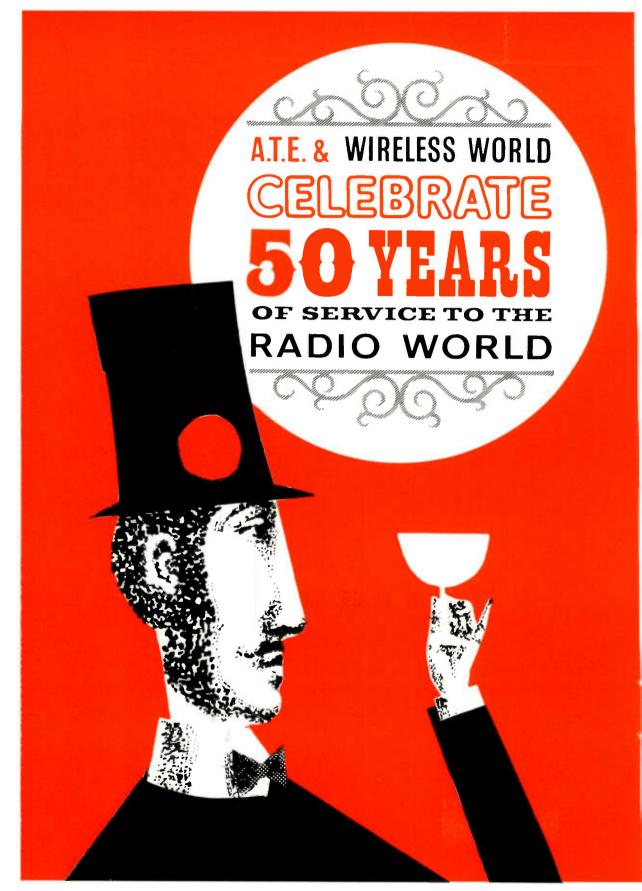
Illustrated opposite are but a few of the hundreds of exciting exhibits. For further details of these, or complimentary tickets for the show, contact:—



B & K LABORATORIES LTD.

Telephone: GROsvenor 4567

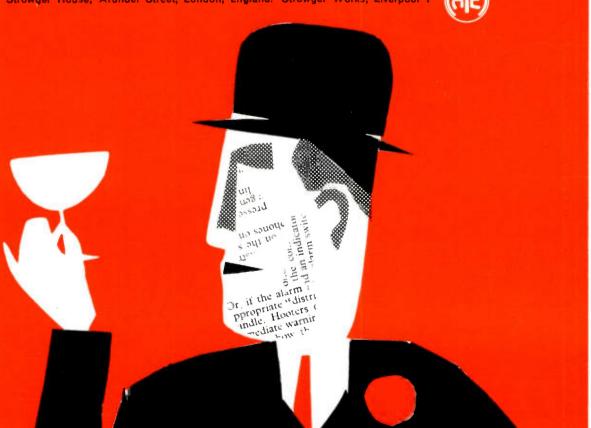
4 Tilney St.,Park Lane, London W. 1. June 19th – June 23rd 1961



A.T.E. congratulates the Wireless World on its Golden Jubilee, an event which coincides with the fiftieth anniversary of the Company's own experiments in radio. These led naturally to it entering the domestic market in the 1920's with the "Claritone" headphones and loudspeakers which were to earn a world-wide reputation for their quality. Investigations in radio telephony, particularly in channelling equipment for micro-wave transmission systems, have been continuous. A.T.E. supplied the world's first single channel v.h.f. harbour radio system to Liverpool Mersey Docks and Harbour Board in 1950 and have since supplied single and multichannel v.h.f. radio systems for telephone subscribers in all parts of the world. A.T.E.'s activities at present are concerned with the applications of electronics in tele-communication with particular reference to telephony, telegraphy, telemetry and computer design.

AUTOMATIC TELEPHONE & ELECTRIC CO. LTD.

Strowger House, Arundel Street, London, England. Strowger Works, Liverpool 7





LOW FORCE 'UNITOR' PLUG & SOCKET

The Ferranti Unitor has been designed to satisfy the need for a reliable multi-pole plug and socket with a low insertion and withdrawal force suitable for use with rack-mounted electronic equipment, where electrical connections are required at the rear of the sub-units. It is also entirely suitable for use with either free plug or free socket



FORTH SERIES TRANSFORMERS

The Ferranti Forth Series Resin Cast Transformers and Chokes have been extensively adopted for airborne and missile applications in view of the significant saving of weight and volume which can be achieved over conventional types. The range is designed to meet inter-service specifications.



PRECISION POTENTIOMETERS

The Ferranti range of Precision Potentiometers is designed to provide analogue conversion from mechanical rotation to an electrical signal. They have a wide range of uses in flight simulators, flight trainers, airborne flight instruments, computers and similar applications.

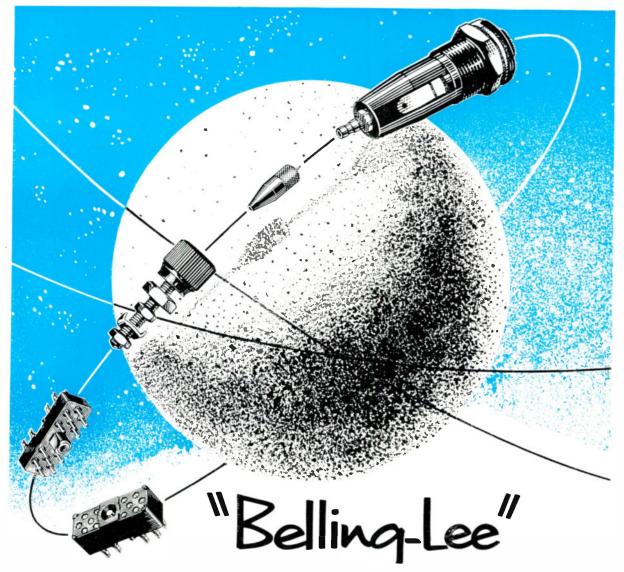


DIGITAL VOLTMETER

The use of digital instruments for the measurement of voltages has now become established in many fields such as production testing, calibration, data handling and quality control. Ferranti are now able to offer a 4 digit voltmeter which, while retaining all the features of the previous 3 digit model, will enable a greater accuracy to be obtained.



FERRANTI LTD · FERRY ROAD · EDINBURGH 5 · SCOTLAND Telephone : DEAn 1211



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As one of their oldest regular advertisers* of components,

Belling & Lee Ltd. offer warmest congratulations to the

"Wireless World" on the occasion of their Golden

Jubilee. We are proud to share with them such a fine

tradition in the annals of wireless history, a tradition to which
intregrity, quality, and forward looking have been the major
factors which have contributed to the joint success of each.

* The first advertisement appeared on February 18, 1925.



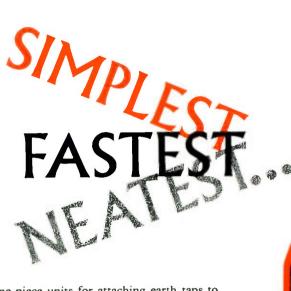
PLUGS & SOCKETS · GLASS SEALS · TERMINALS

CIRCUIT PROTECTION DEVICES

INTERFERENCE FILTERS · RECEIVING AERIALS



Telephone: Enfield 5393 - Telegrams: Radiobel, Enfield



A-MP Termashield ferrules are one-piece units for attaching earth taps to screened wiring. One operation of the A-MP crimping tool permanently attaches the ferrule to the screen and one or two earth taps. The ferrule is only slightly larger in diameter than the screened lead. Attachment is speedy, electrical characteristics are excellent, and the attachment strong and permanent. As the system is solderless, there is no risk of dry joints and burnt insulation. Snap-on insulating caps, colourcoded, simply slide over the ferrules and are self-locking.

··· AND MOST ECONOMICAL







on the insulation



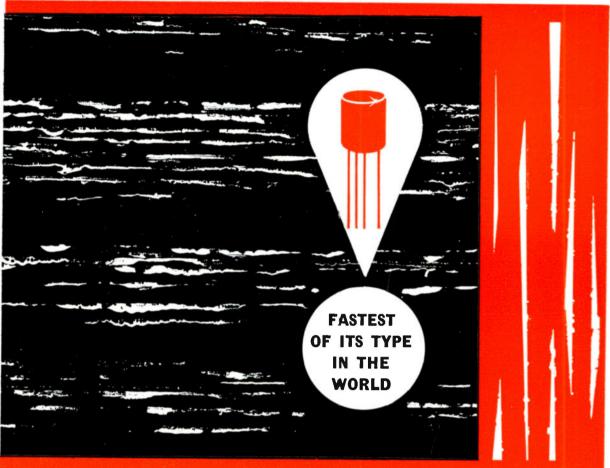
* Trade Mark of AMP Incorporated, U.S.A.

TRADE MARK

AIRCRAFT-MARINE PRODUCTS (GT. BRITAIN) LTD.

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SOUTH AFRICA: DISTRIBUTOR: E. S. MOWAT & SONS (PTY) LTD., \$1-57 MILNE STREET, P.O. BOX 437, DURBAN, NATAL, SOUTH AFRICA. ASSOCIATED COMPANIES IN: AUSTRALIA, U.S.A., CANADA, HOLLAND, FRANCE, GERMANY, ITALY, JAPAN, PUERTO RICO AND MEXICO



NEW MULLARD AVALANCHE TRANSISTOR

Today you can specify a truly dependable avalanche junction transistor, for use in very high speed circuits. It is the Mullard ASZ23—a new purpose-made transistor that is manufactured by the Mullard alloy diffusion technique to give complete reliability of the avalanche mode. Mullard experience in the development of alloy diffused transistors has made possible the production of this high avalanche performance p-n-p junction transistor at a realistic price.

Here is a transistor to give the designer tremendous scope. The ASZ23 opens up a new field of nanosecond pulse techniques. A typical application is in the sampling oscilloscope circuit shown alongside.

Supplies of the ASZ23 are immediately available.

ASZ23 ALLOY DIFFUSION p-n-p JUNCTION TRANSISTOR

· · · · · · · · · · · · · · · · · · ·
Absolute Maximum Ratings
Collector currents ic (pk) max100mA
Reverse emitter-base voltage Veb max
Temperature Ratings
Storage temperature limits
Maximum junction temperature 75°C
Junction temperature rise above ambient 0.6°C/mW
Junction temperature rise above case

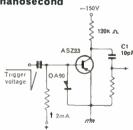
If you would like more detailed information, please write to the address below:

another ALLOY DIFFUSION transistor

Mullard Limited · Semiconductor Division · Mullard House · Torrington Place · London WC1

ASZ 23

60mA pulse with rise time of 1 nanosecond

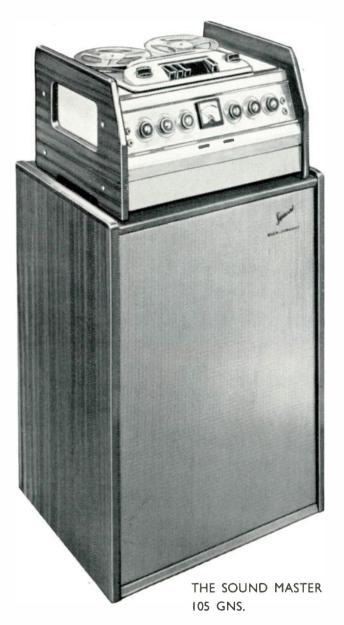


A typical method of obtaining a predetermined sampling by means of the ASZ23





SOUND TAPE RECORDERS



A decade of manufacturing experience

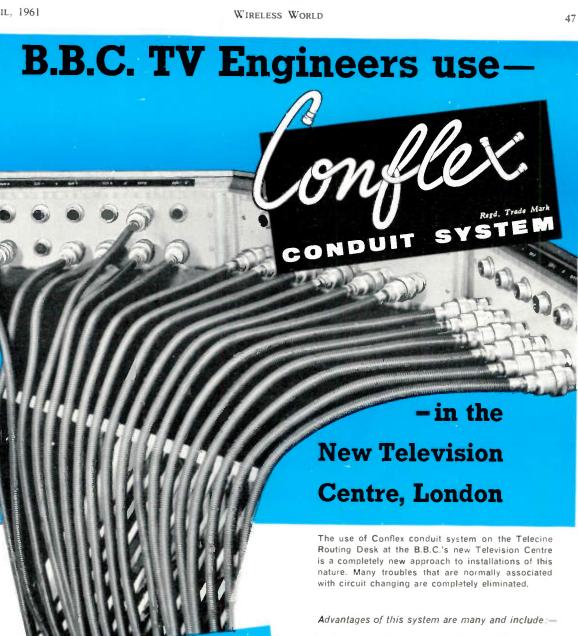
With ten year's tape recorder manufacturing experience Tape Recorders (Electronics) Ltd., makers of Sound Tape Recorders, have a background knowledge which enables them to produce fine, reliable equipment. Ten year's experience lie behind the new Sound Master, a precision instrument engineered to professional standards of performance and reliability. It is a four track, three speed machine with separate recording and replay amplifiers. There are full facilities for mixing, monitoring and multiple superimposition, and 10 watts output, through the acoustically designed reflex loudspeaker system. The Master is, in fact, a complete magnetic recording system offering studio quality performance. Sound Tape Recorders are available in a range of models to suit every pocket. All are handsomely styled, and precision engineered for long, trouble-free life.

SOUND

TAPE RECORDERS (ELECTRONICS) LTD.

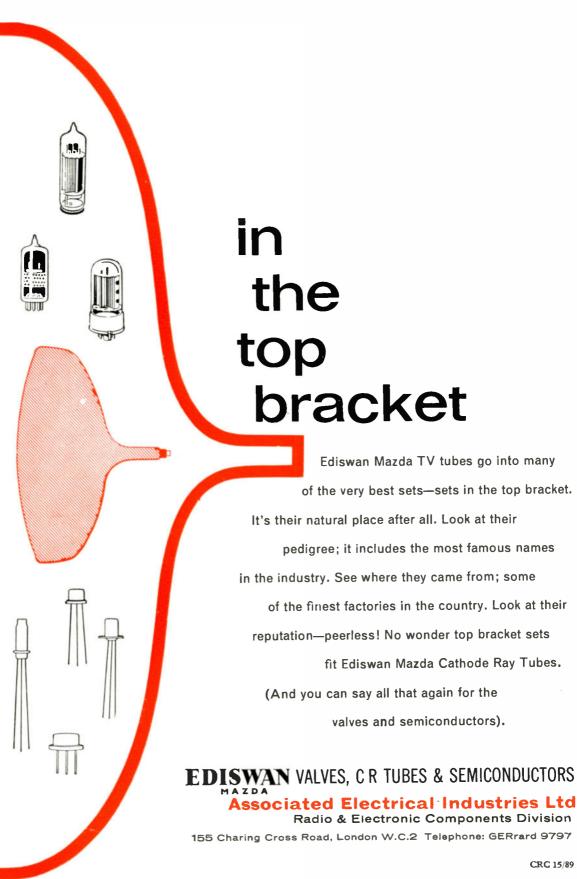
784-788, High Road, Tottenham, London, N.17.

Telephone: TOTtenham 0811



- A high degree of flexibility no metal fatigue.
- Terminations that fit British and American connecters, junction boxes, etc.
- Eliminations of special cable lays, moulded harnesses and problems involved in encapsulation.
- Simplification of connecter wiring and easier conductor changes.
- In situ assembly that requires no special tools.
- Provision for double-screening on R.F. circuits.
- * Write for technical details.

The Telecina Control Desk



CRC 15/89

AN IMPORTANT NEW DEVELOPMENT

the Airedale free-standing speaker assembly

For many years the Wharfedale Omni-directional 3-speaker Corner System has been recognised as a superbly natural reproducer. It has been demonstrated in the major concert halls of many countries and has frequently stood the difficult test of comparison with live musical performances.

The AIREDALE is the latest version of this famous speaker presented for the first time in a one-piece free-standing assembly suitable for corner or along-thewall location.

The smooth, clean bass is characteristic of the high flux 15in, unit which is now fitted with roll surround.

The 8in. mid-range and 3in. treble units face upwards for omni-directional treble, and are arranged in a manner which imparts a natural airiness to the reproduction.

Cabinet resonance is avoided by loading the larger panels with ceramic tiles. Some idea of the solid construction is given by the fact that the total weight exceeds \frac{3}{2} cwt.

UNITS:

W15/RS fitted with heavy cone and impregnated cloth roll surround for minimum distortion.

Half-section three-way separator unit with crossover frequencies at 400 c/s and 5,000 c/s.

 $39 \times 28\frac{1}{2} \times 14$ in.

WEIGHT:

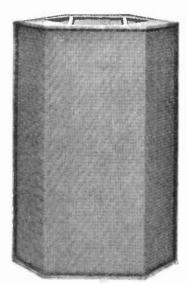
91 lb complete.

IMPEDANCE: 12/15 ohms only.

MAX. INPUT: 15 watts.

Individual controls for middle and trebie response are located in the rear panel.





PRICE £65-0-0

Available in whitewood or fully finished with a choice of walnut, oak or mahogany veneers. Tropical model also available at extra cost.

Fully descriptive literature free on request.

IDLE, BRADFORD, Yorkshire

Tel : Idle 123516.

Grams: Wharfdel, Idle, Bradford.



A tape recorder is only as good as its deck. This is where precision in manufacture and assembly is vital for professional standards of recording and reproduction. In the Brenell Mark 5 deck there's a rare combination of advanced technology and an almost-forgotten kind of craftsmanship.

The Mark 5 deck has a remarkable, new main motor of a type widely regarded as the most efficient to be used in tape recording. The HYSTE-RESIS SYNCHRONOUS MOTOR, with a balanced outer rotor and a heavy, statically and dynamically balanced flywheel. It brings 'wow and flutter' down to below .1% at 7½ ips!

This and the other components providing the specification shown below are assembled with fanatical care. Brenell Mark 5 (and all other equipment) production is an individual task which is repeatedly checked and tested. Nothing less than mechanical and electrical perfection will do.

At 28 gns., you'd be missing a great deal to pay less and there's no need to pay more.

Abridged specification
3 INDEPENDENT MOTORS
4 RECORDING SPEEDS
FAST REWIND in either direction. 1,200ft. reel rewound in 45

SELECTIVE FREQUENCY CORRECTION at 15, 7½ and 3½ ips. ACCEPTS 8½ in. REELS, PAUSE CONTROL, DIGITAL REV. COUNTER, PROVISION FOR EXTRA HEADS.



TAPE RECORDERS:

3 STAR: 58 GNS. MK.5: 64 GNS. 3 STAR. R/P STEREO: 89 GNS. MK.5 R/P STEREO: £99.12.0

track available with 3 Star models

Full details and the address of your nearest stockist from the Sole Manufacturers

BRENELL ENGINEERING CO. LTD. · 1a DOUGHTY STREET · LONDON WC1





CONTROL DESK—CABINETWORK BY LOCKWOOD

Central Apparatus Room, British Broadcasting Corporation, Television Centre, London, W.12 Manufactured in conjunction with the Planning & Installation Dept., B.B.C.

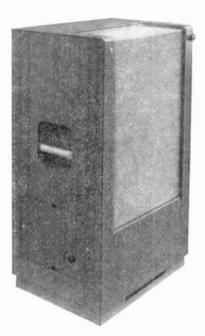
Wireless World

CONGRATULATIONS

on your

GOLDEN JUBILEE

It has given us pleasure to have been associated with you for nearly 30 years



Lockwood Studio Monitoring Loudspeaker

LOCKWOOD

ACOUSTIC AND ELECTRONIC EQUIPMENT

LOWLANDS ROAD . HARROW . MIDDX . BYRON 3704

WIRELESS WORLD



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PRODUCTS FOR PRODUCTION

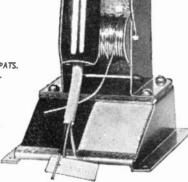


ALL BRITISH MANUFACTURE

ILLUSTRATED

SOLDERING INSTRU-MENT, LIST No. 70 WITH COMBINED PROTECTIVE UNIT, LIST No. 700 SHOW-ING WIPER/ABRA-SION PAD AND SOLDER REEL.

BRITISH AND FOREIGN PATS. REG. DESIGNS ETC.



APPLY FULL PARTICULARS

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Plessey

SCAN COIL FOR EVERY TUEE

The new Plessey scan coil, designed for operation with the full range of 110° and 114° tubes, incorporates several novel features which improve performance and versatility.

- Polypropylene moulding to withstand elevated temperatures in service
- Smaller size to suit shortest tubes
- Frame and line coils available in wide range of Inductance values
- Ferrite loaded plastic shift rings remain permanently magnetised and do not absorb power from the frame coils
- Three methods of picture correction available.

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Components Group, Tuners and Wound Components Division · Ilford · Essex · Telephone 3040

Overseas Sales Organisation: Plessey International Limited, Ilford, Essex

Arcolectric

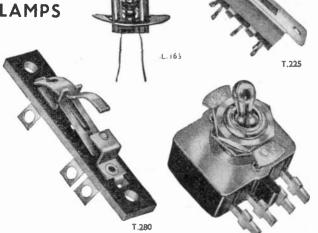
SWITCHES & SIGNAL LAMPS

T.225: Miniature Slide Switch D.P. change-over switch

S.L.166: Very small low cost mains neon indicator

T.280: Sensitive Snap Action Switch Popular switch for tape recorders

T.626: Double pole 3-AMP switch with tags to fit printed circuit boards



T.626

Write for Catalogue No. 132

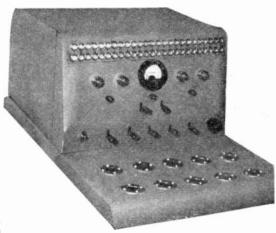
ARCOLECTRIC

CENTRAL AVENUE, WEST MOLESEY, SURREY. TEL.: MOLESEY 32 32

AUTOMATIC CONTINUITY & INSULATOR TESTER (A.C.I.T.)

for the FASTEST-EVER

TESTING OF MULTI-CORE CABLES



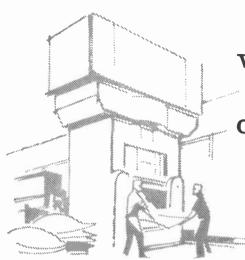
Example of testing speed 25 pt cable tested:—
625 insulation tests, 25 leakage to screen, 25 continuity tests—all in 25 seconds.

Insulation faults are shown and faulty circuits indicated by lamps. Cross connected circuit leakages to screen are discovered, also involved circuits indicated.

Continuity tests are carried out with low voltage, insulation tests 500 v. A.C.I.T. stops automatically after discovering any fault or when the test is finished.

Brass type Plessey Mk. IV sockets and plugs are used, also an aluminium version Mk. IV is available if required. A.C.I.T. is built for 25, 50 or to order for more circuits. Fully descriptive leaflet on request.

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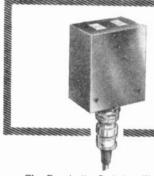


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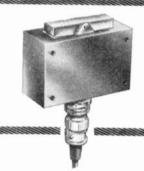
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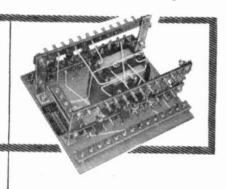
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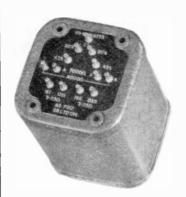
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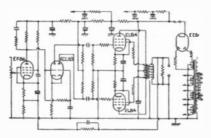
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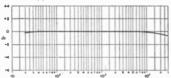
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Below is reproduced the response curve of the AS 7012 which is typical of the whole of the Solent Series.



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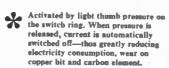
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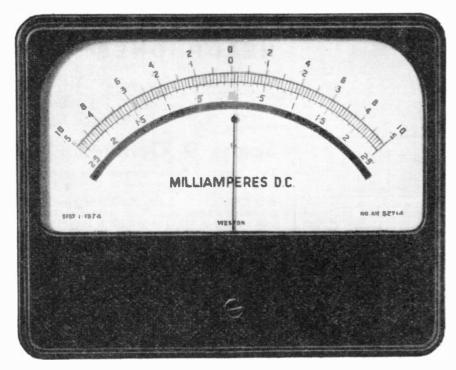
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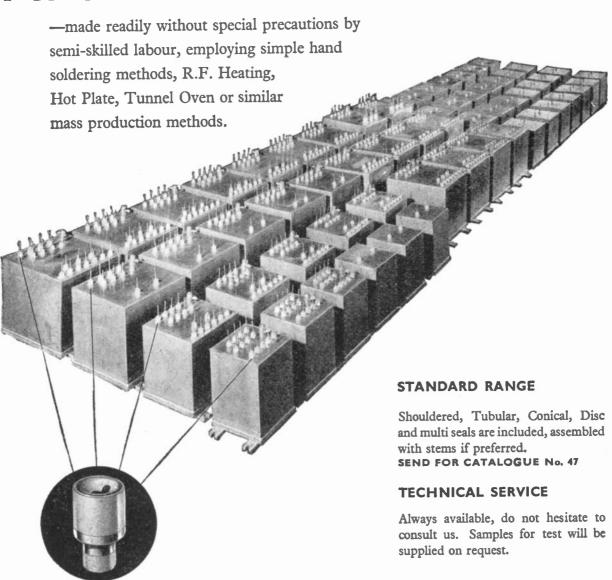
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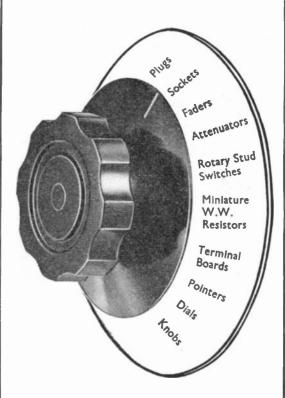
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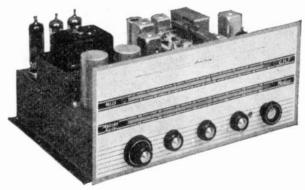
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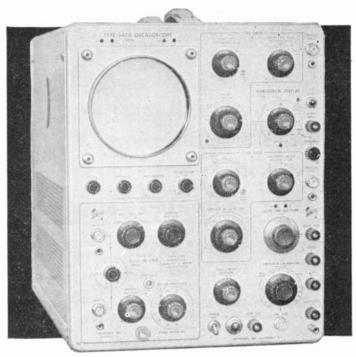
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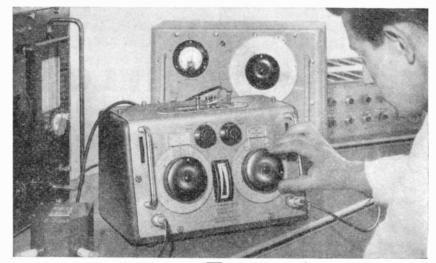


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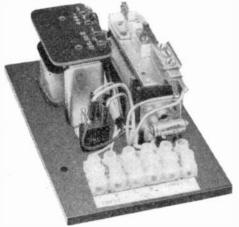
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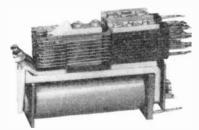
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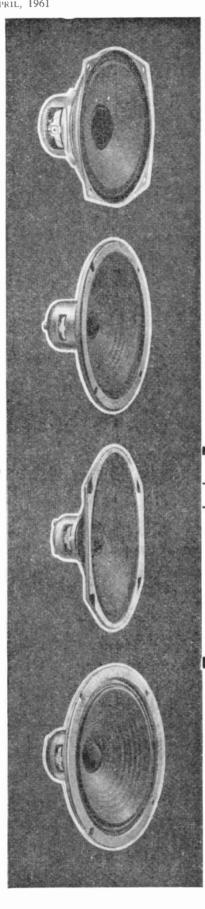
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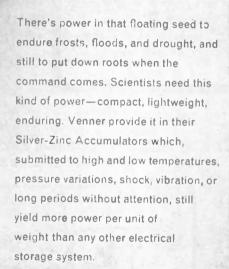
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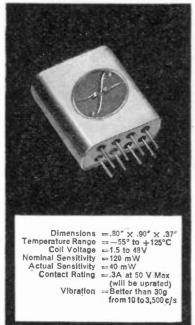
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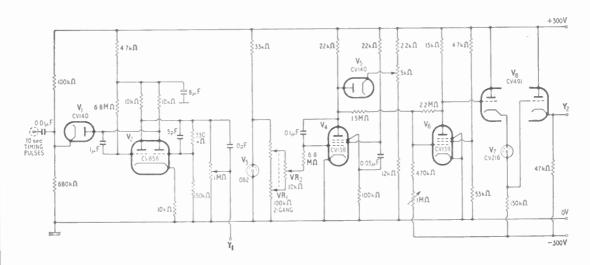
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Telemetry Signals from Sputnik III



This article in the current March issue of ELECTRONIC TECHNOLOGY describes equipment used for transcribing te'emetry signals from the Russian satellite Sputnik III from magnetic tape on to 35 mm. photographic film. The resultant record, samples of which are shown, is in raster form showing successive keying cycles one under another. The telemetry encoding system used in the satellite is also described and the results of the analysis of two transits are included and briefly discussed.

ARTICLES

IN THE APRIL ISSUE

INCLUDE:

A CURRENT REGULATOR AND SWEEP MECHANISM

A simple regulator and sweep mechanism for controlling the output of a d.c. generator is described in this article. The regulator uses a single-ended error-signa, amplifier and no reference battery is required. The sweep mechanism can vary the output current automatically over a wide range, and the arrangement, which has a stability 1 in 4,000, has been used as an electromagnet current supply in paramagnetic resonance experiments.

THE ROUND-TRAVIS DISCRIMINATOR

In this article the conditions for minimum non-linearity distortion in the Round-Travis discriminator are derived. The application considered is for the frequency-amplitude conversion of a frequency-modulated signal.

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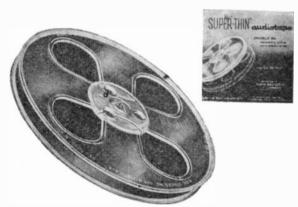


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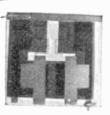
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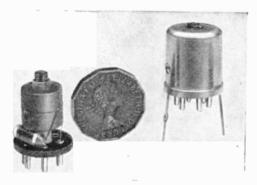
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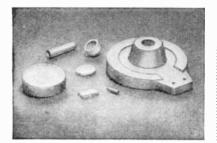
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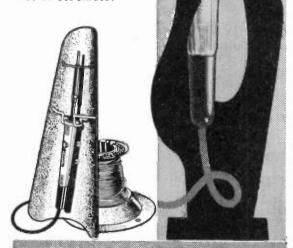
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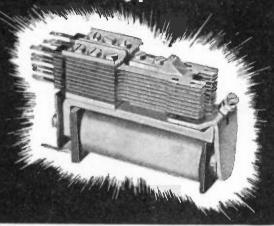


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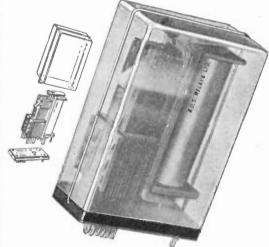


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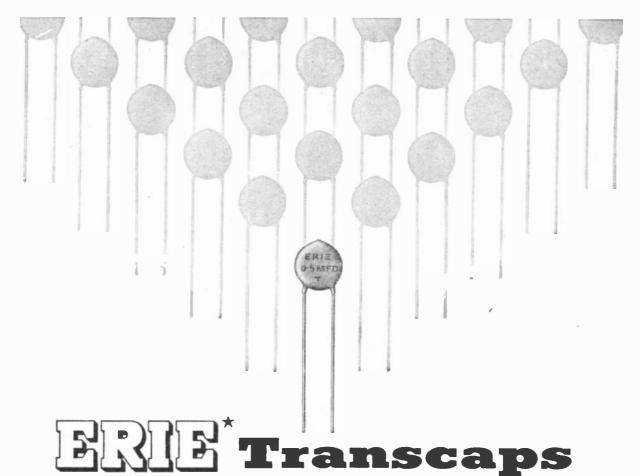
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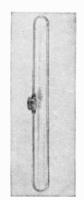
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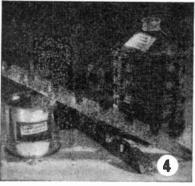


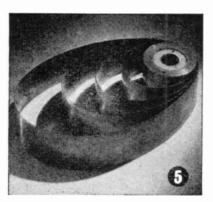
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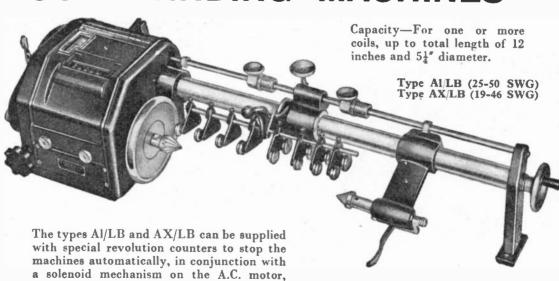
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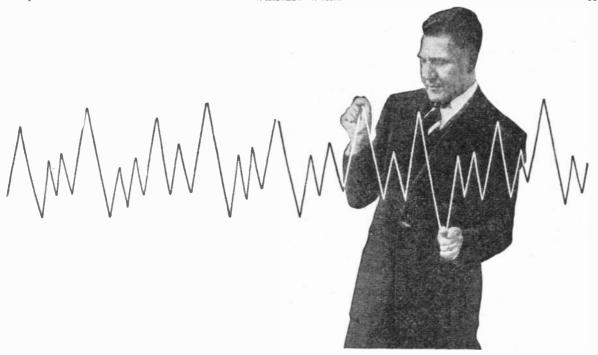
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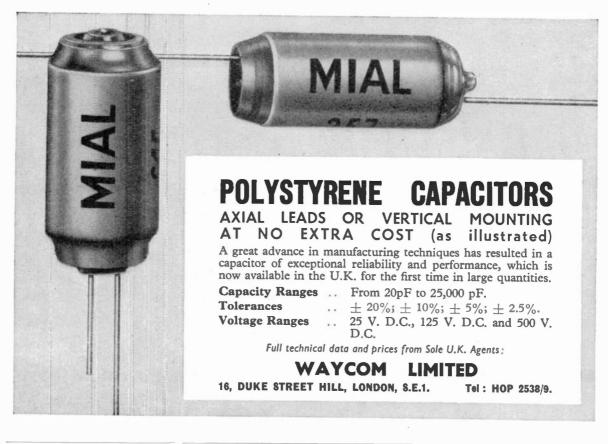


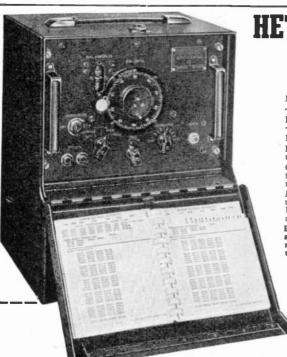
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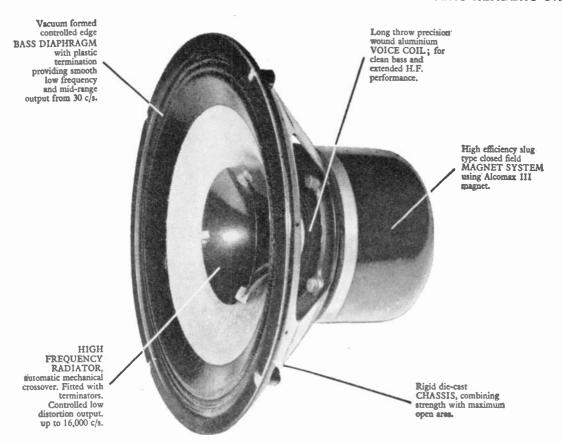
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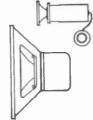
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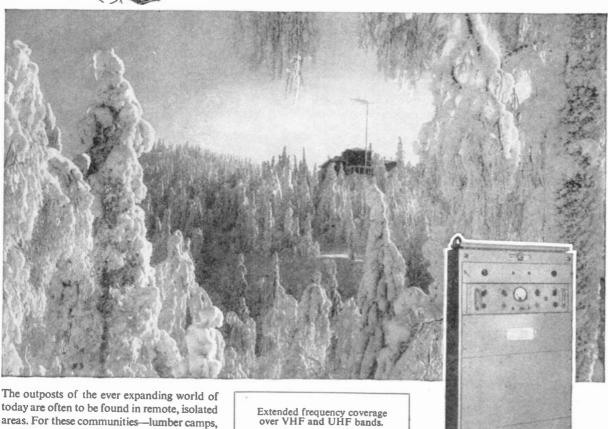
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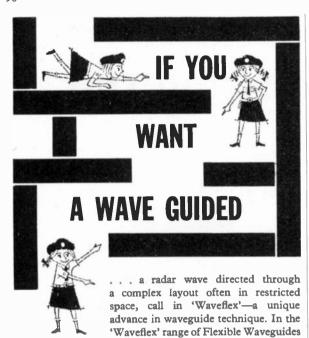
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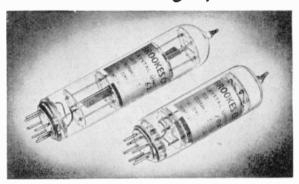
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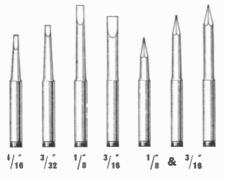
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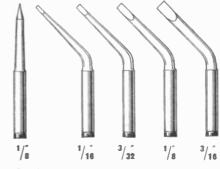
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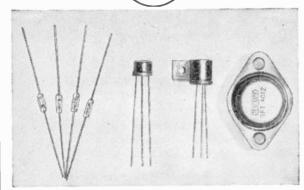
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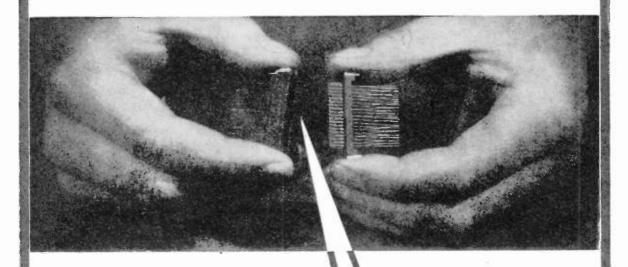
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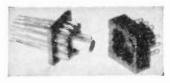
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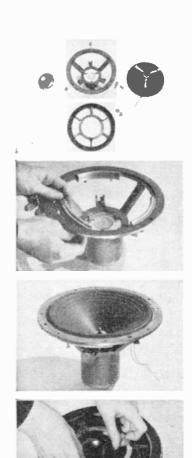
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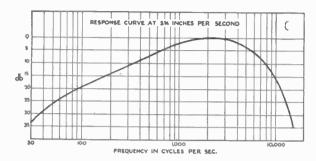
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DEPTH #"

WIDTH #

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RECORD/PLAYBACK HEADS

HEIGHT #"

Track width				***			0.043 in
Inductance	***	***	***	***	***	***	400mH at 1 Kc/s.
Bias Current	***	***	***	***	***	***	0.0001 in
Record Current		•••	***	***	***	***	0.45–0.8mA 30–80µA
Output				i.4-	2.5mV.	(at	
Recorded Crossta	lk			***	***		Better than-70 dB
Playback Crosstall	ic.	***	***	***	***	***	Not measurable

ERASE HEADS

Track widt Gap	h	***		***						0.0	56 In.
Impedance	***	***	***	***	***	***	Double	Gap	each o	0.0	04 in.
Volts		***	***	***	***	***	***		200Ω a	ε 50	Kc/s.
Current	***	***	***	***	***	***	***		10 V a	t 50	Kc/s.
Current	***	***	***	***		***	***		5	0-60	mA.

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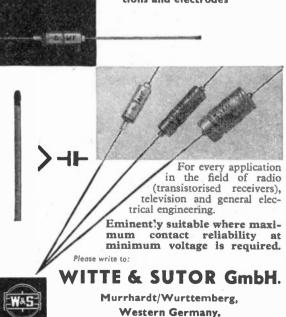
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Screen Area	8 x 10	6 × 10	4×10	4×10	6 x 10	5 x 8	5 x 8	5 x 6
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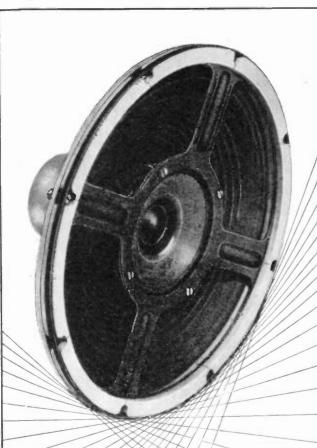
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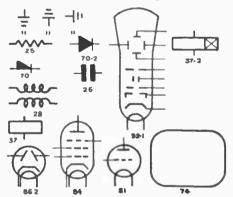


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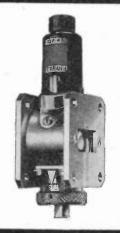
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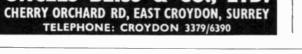
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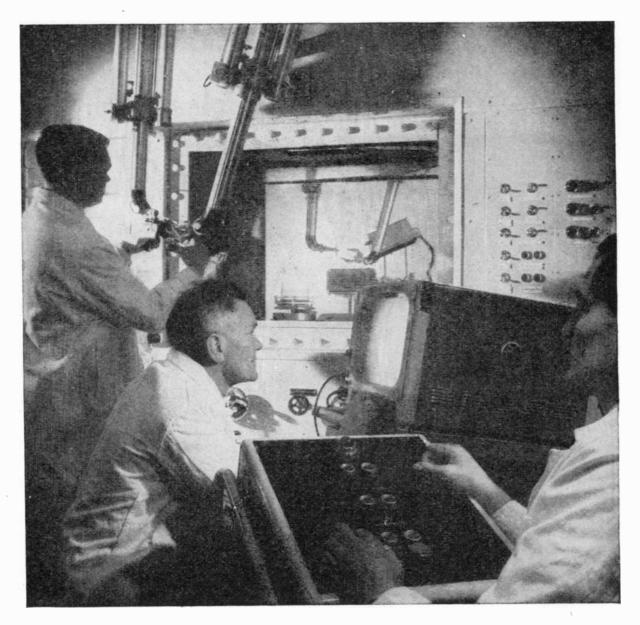
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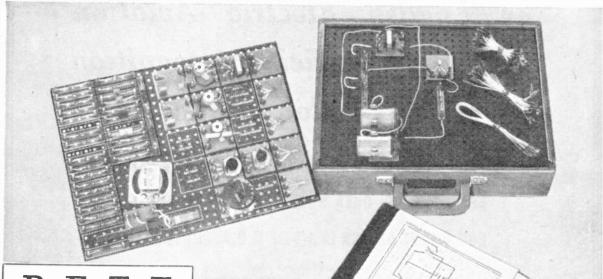
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ELECTRONICS, RADIO, TELEVISION

APRIL 1961

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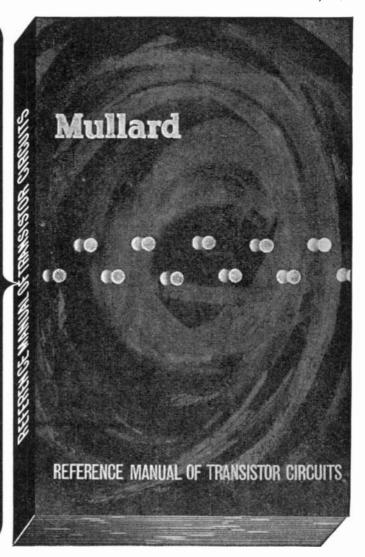
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Wireless World

VOL 67 NO 4 APRIL 1961

HALF A CENTURY

IN 1911 the business and profession of wireless communication was already established, but as yet it had made little impact on the daily lives of most people. There was a certain novelty in sending a telegram "via Marconi" and a few amateurs dabbling with spark coils and crystal and electrolytic detectors made a welcome diversion from lantern lectures and microscopy at the local literary and scientific society. But the seeds of future developments had germinated. Every day more ships were being fitted with wireless, and more amateurs were proudly passing their headphones to admiring friends to listen to the musical morse of Clifden or the growl of Eiffel Tower and Poldhu.

Until then technical information had been scattered in occasional articles in the electrical journals and in one or two papers read before the learned societies. Now it was decided that there was sufficient interest to support a journal "the aim of which will be to acquaint the reader with the latest possibilities of this most marvellous invention." Such was the success of the Marconigraph that two years later it was decided to give it a new format and a new title in keeping with its wider circulation. In the first editorial of the new series we said, "The Wireless World will still be the medium, as was the Marconigraph, for the interchange of ideas concerning the further scientific and commercial development of wireless telegraphy, with its bearing upon national and economic interests. But these long words do not mean that we intend to take up the standpoint of a dry and educational science. Our Magazine is to be popular, and while the information we shall print will compel the attention of the scientist, it will not be beyond the scope of the general public."

If at times we seem to have become more complex it is because we reflect the growth of our subject, which even in its beginnings called for more than a little application to gain mastery. We invite those who doubt this to turn up some of our earliest issues (e.g., the series on aerial capacitance

by Professor G. W. O. Howe in 1915). While many of our articles have been addressed exclusively to the professional quite as many have been prepared specially for the beginner who may be at the start of his career as a radio engineer or technician or just interested in the subject as an amateur. The dividing line, if indeed one exists, is hard to draw. Many of our readers who earn their living by research on semiconductors or development on microwaves find relaxation as amateur transmitters or high-quality sound enthusiasts. We welcome them all as readers and take this opportunity of thanking them for their sustained interest, which as our recent questionnaire has shown, more often than not is of long standing.

The entity and character of a journal is something which is difficult to define in words. It transcends all outward forms of print and styling; it cannot be detected in the contents of individual articles; it exists as like-minded thought and a community of interests between readers and staff. We are all of different ages, have divergent personal interests and while retaining our independence are prepared to argue, to listen and to learn—all with one object: as far as this journal is concerned to keep the record straight.

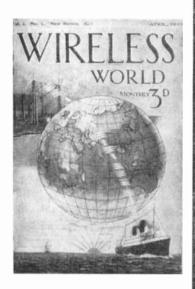
Looking back we pay tribute to our predecessors in office, to past members of the staff, to our contributors and to all those whose ability and loyalty have laid the foundations upon which we build. Looking to the future we shall strive to improve our journal as the medium of communication between all whose vocation or interest lies with radio and electronics, to serve as a forum for discussion, as a medium for enlightenment and exposition, and as a bulletin for news of the world of wireless.

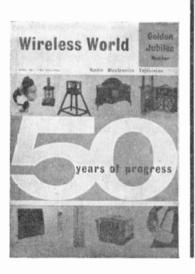
"This then is our policy: to be of use and interest to our readers, and through them to be a factor for progress." These words are quoted from Volume 1, No. 1 of Wireless World and we can find no reason for altering them today.



SINCE THE

Years of Progress As Seen Through Our Pages





THE STATE OF THE ART IN 1911

HE Edwardian age into which The Marconigraph was launched was less prone than is the Neo-Elizabethan to the unquestioning acceptance of scientific marvels.

Many people still looked upon wireless telegraphy as "against Nature"; as something akin to a music-hall trick. That attitude of mind was certainly not discouraged by wire telegraphy and submarine cable interests, with whom we were to remain in bitter competition for many years. By way of counterattack, we made great play of the fact that the so-called "KR factor," which limited the speed of cable transmission, did not apply to us. High-speed wireless transmissionwhich then meant about 60 words per minute-had already been demonstrated experimentally, but the volume of traffic on offer was generally not great enough to encourage its commercial use.

Whatever the reason may have been, wireless telegraphy had hardly made spectacular progress during the first dozen years of its existence. When we began publication there were, according to official figures published later, a mere 1,740 licensed land and ship stations in the whole world.

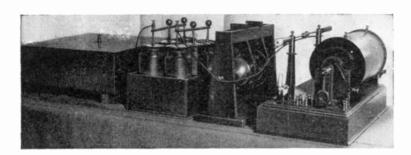
But that understates the position rather seriously. The United States had not ratified the International Convention and had no licensing system; thus the true number of her stations cannot be ascertained. For once, America had made a slow start in taking up a scientific innovation; when the first wirelessequipped ships sailed from Europe to the New World there were no coastal stations in the North American continent with which they could communicate. But America was soon to catch up, and by 1911 probably had a greater number of stations than any other single country. Going by the few figures available and working backwards from the time when licensing came in, it is fairly safe to guess at a round 1,000, or something not far short of it. Thus the world total of stations in 1911 was over 2,500. The total number of people gaining their livelihood in wireless, from Mr. Marconi himself down to the humblest messenger boy, could hardly have exceeded 8,000.

Though the commercial growth of wireless may have been disappointingly slow, technical progress had been quite impressive. An old-timer dating back to 1911 might make out some sort of case for claiming that the effectiveness of the gear of his period had increased as much since 1897 as it has done between 1911 and the present day. Be that as it may, he would be on

Wireless World BEGAN

Wireless World, the first radio journal, appeared in April, 1911, as The Marconigraph. The present title was assumed two years later. We were originally published by the Marconi Company and circulated largely among engineers and operators, though from the start there was a public readership. We became an independent journal 36 years ago. This review traces the significant advances in radio and electronics since we began. Except in the introductory section, the material is taken entirely from our own pages. In the introduction an attempt is made to give the reader a glimpse of "what everybody knew " in 1911.





A "coil set"; the kind of transmitter that was going out as we came in. Right to left: induction coil, spark gap, "battery" of Leyden jar condensers, "jigger."

pretty sure grounds in going on to claim that by 1911 the foundations of nearly all modern techniques had been laid and the majority of the great basic inventions had been made. Practitioners of the art certainly did not look on themselves as being in the Dark Ages. They had already seen great technical progress and were full of confidence for the future. To them, it was a kind of Elizabethan age, when everything was bright, new and exciting.

Many of the inventions that had been made were waiting-and some had to wait for many years-for the means to put them usefully into practice. Christian Hülsmeyer's radar pulses, first suggested by him in 1904, had to wait 30 years for the means of generating them and usefully detecting their reflections. Oliver Lodge's moving-coil loudspeaker looks, in the patent specification drawing of 1898, surprisingly like the instrument of today, even if the "hi-fi" enthusiast would hardly approve of his diaphragm or its suspension. But valve amplifiers capable of working moving-coil speakers did not appear until 20 years later.

Fleming's diode, which we used to call, rather confusingly, an oscillation valve, was already ancient history, and was not especially esteemed as a signal rectifier. De Forest had added a grid in 1907, but his triode had made no impact. Probably fewer than five per cent of our early readers had ever heard of it and there was no mention of triodes in our pages for the first two or three years. The triode remained in obscurity until the discovery of regeneration caused many workers to concentrate their efforts on its improvement. Those efforts were probably triggered off by von Lieben's work on the amplifying triode in 1910-11.

"Tele-vision" (generally

printed) was a word that appeared surprisingly early. Nipkow had enunciated the basic principles of scanning in the nineteenth century, but few seemed seriously to expect that "moving pictures by wireless" would be achieved. One of the exceptions was Campbell Swinton, a versatile engineer and wireless enthusiast who had already forecast that, if the difficulties were ever to be overcome, it would be by means of "the weightless cathode rays" of the Braun tube, the forerunner of the c.r. tube of today. Magnetic recording-on wire, not coated tape -was already known and had been used for the recording of high-speed signals.

Transistors? Well, hardly. But oscillating crystal circuits had been devised by Dr. W. H. Eccles, one

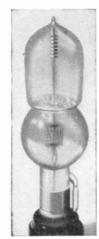


Photo: Deutsches Museum, München.

An historic valve the Lieben-Reisz triode of 1911.

of the "founder members" of wireless technology whose name recurred constantly in our pages for many years. In another sphere, he was one of the first to accept and interpret Heaviside's theory of a conductive layer in the upper atmosphere as an explanation of observed phenomena in long-distance wave propagation. For a long time to come there was a tendency to ignore or even to scoff at Heaviside's theory; his American co-worker Kennelly had even less recognition on this side of the Atlantic.

In Britain the art we practised was always called "wireless." The official international word "radio" had been introduced some years earlier but had had a chilly reception. It did not trip easily off English tongues; worse, to use it was considered "non-U" and aping the foreigner. In fact, though, most nationalities still preferred their own versions of "wireless": sans fil, drahtlose, sin hilos. But in Germany they soon began to show a preference for the word Funk (spark) which still survives strongly in Rundfunk (broadcasting).

Naturally enough, wireless had already produced its own jargon. Equally naturally, many of the earlier examples have now disappeared, some of them frozen out by changing techniques. One of the queer words was "jigger" (r.f. transformer for coupling the closed circuit, transmitting or receiving, to the open aerial). The derivation of this term is obscure and has apparently been lost in the mists of time. Maurice Child, in a historical lecture in the early 20s, admitted his inability to trace it. "Billi" is easier; it was a small variable condenser reputed to have a capacitance measured in billionths of a farad. Though by international agreement wavelengths were measured in metres, the foot still served occasion-

ally as the unit. It had not been so long ago that only two wavelengths were in use, officially for merchant ship communication, but in fact for other purposes as well: Tune A. 1,000ft and Tune B, 2,000ft-quite near enough to 300 and 600 metres for the order of accuracy then prevailing. Whether chosen by luck or judgment, Tune B, the more popular, was in fact an excellent generalpurpose wavelength for the techniques of the times. The foot (length of wire used in winding a coil) sometimes served also as a unit of inductancel

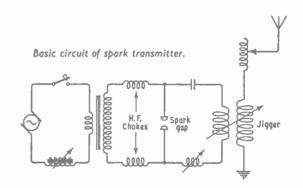
The Postmaster-General's control of all wireless activities in Britain had been firmly established by the Wireless Telegraphy Act of 1904. Even before that date the Post Office had quietly assumed power over us by virtue of the monopoly in telegraphy conferred on it by Disraeli in Victorian times. This control may at times have seemed somewhat heavy-handed; indeed, Wireless World has on many occasions throughout its life been at odds with the Post Office over allegedly restrictive practices or other departures from rectitude. But we must remember that the Post Office, as one of its historians has said, "is not just another Department." It functions under a long-established tradition of providing a public service, first in carrying the mails, then in transmitting telegrams and later in running a telephone service. In return, Parliament has granted certain monopolies and privileges, which have always been jealously guarded. Each successive development in wireless must have seemed to the official mind to threaten serious encroachment on these monopolies and it is small wonder there have been occasional bunglings and examples of over-cautiousness. However, it is a pleasant thought that Post Office control has generally been benevolent and beneficent.

Apart from the exercise of his monopolistic powers, it was (and is) the duty of the Postmaster-General to ensure the observance of international regulations. In 1911 we were governed by the Convention of 1906, to which nearly all nations had adhered. The United States was an exception; neither had she ratified the Convention (was that a manifestation of the Monroe Doctrine?) nor had Congress as yet passed any law to regulate or control wireless communication. America was indeed the land of the free. But, according to stories-perhaps exaggerated-filtering across the Atlantic,

jungle law prevailed. Deliberate jamming of competing stations was commonplace and powerful stations shouted down the weaker. And there was nothing to protect the secrecy of messages. According to the folklore of the time, submarine cable interests intercepted telegrams sent by the Marconi transatlantic station at Glace Bay, Nova Scotia, and published a selection of themreputedly the most scandalous-as advertisements in New York newspapers. They are also said to have published intercepted messages relating to interruptions in communication, such as "stand by for three hours; atmospherics too bad," thus hoping further to discourage potential users of the new and then struggling wireless service. This latter

Both arc transmitters and rotary r.f. generators capable of producing continuous waves had been developed, but in the absence of valves the problem of modulation was indeed difficult. Water-cooled and liquid jet microphones, inserted directly in the aerial circuit had been used in some of the experiments.

For telegraphy, spark transmitters were almost universal. A big station of the period was an impressive affair; the sight, and still more the sound, of tens of kilowatts being dissipated in a crashing oscillatory discharge was something not easily forgotten. There was even a strong characteristic smell, generally referred to as "ozone". All the so-called "systems" were basically similar; the circuit arrangement,



kind of interception was eventually circumvented by the use of code words for inter-station messages relating to interruptions and similar matters.

Some support for the truth of these stories comes from the fact that American legislation, when it eventually came, was not particularly onerous in most respects but imposed severe penalties for deliberate jamming and failure to observe secrecy. As things turned out, the American free-for-all had worked remarkably well in the early stages. No doubt most of the stations did in fact establish a tacit modus vivendi with their competitors. But control was bound to come sooner or later; in the event, it came sooner than expected, and for a reason that nobody could have foreseen.

Wireless telephony had already been accomplished experimentally when we began publication, but was as yet of no practical significance.

shown in the accompanying diagram, was simple enough. The a.c. supply, of 50 or 60c/s, was stepped up to 15 or 20kV, an iron-cored choke being inserted in the transformer primary circuit to bring it into resonance with the alternator frequency. The condenser of the closed oscillatory circuit, charged through protective h.f. chokes, discharged itself through a spark gap, the electrodes of which, in all but the most up-to-date sets, were stationary, though adjustable as to The closed circuit was distance. coupled to the open aerial through a double-wound "jigger" or an autotransformer.

These fixed-gap sets gave a lowpitched, irregular tone distinguishable with difficulty from atmospherics and radiated heavily-damped wave trains, due to interaction between closed and aerial circuits. The "rotary discharger" sets which were just being introduced were a great improvement in both these respects. In the most highly developed form the rotary electrode, mounted on an extension of the alternator shaft, carried a number of projecting studs arranged to give a spark for each half-cycle of the supply frequency; this had now been increased to several hundred cycles per second. Thus a clear high-pitched note was produced, and, as the primary circuit was opened after a very short interval of time, interaction was reduced and there were more persistent oscillations in the aerial circuit.

Transmitters fed from alternators were known as "power sets" and were mostly fairly up-to-date. But there were in 1911 many relics of the not-so-distant past with induction coils drawing their supply from accumulators or d.c. mains. These were mostly fitted in merchant ships but the British Post Office station at Malin Head in the remote North-West of Ireland is thought to have had at this time a coil set worked from an accumulator battery charged from banks of primary cells.

Input power of the typical and more modern transmitters of the period for ships and coastal stations was generally between one and three kilowatts; anything more was considered high power. A fair number of point-to-point and special-service stations used as much as 30kW; anything more was quite exceptional. The lower-powered stations seldom achieved a daylight range of much over 300 miles, depending on their aerial height.

The most common type of receiver used the Marconi magnetic detector, a rugged and reliable but relatively rather insensitive device. depended for its action on hysteresis changes in an endless soft-iron-wire band moved by clockwork through a coil carrying the received signal current. A magnetic field was provided by a pair of permanent magnets and a secondary winding, concentric with the r.f. coil, was connected to a pair of telephones. Unlike other detectors, the magnetic was a current-operated device and

the associated three-circuit tuner had circuits with a low L/C ratio.

The only other kind of detector in widespread use was the crystal rectifier, the combinations most favoured being carborundum-steel, zincitebornite and silicon-gold. Crystals were almost always used with two-circuit tuners having variable coupling between primary and secondary. A few stations had Fleming diodes.

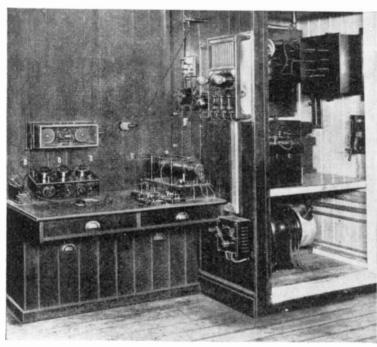
Work on rotary r.f. generators had been going on for some years, but they had barely reached the stage of commercial use. The fact that an electric arc, shunted by a tuned circuit, could produce continuous oscillations had been known for some time. This had been turned to practical use by enclosing the arc in a chamber filled with hydrogen or alcohol vapour and subjecting it to a strong magnetic field. A small number of arc stations were in operation, mostly in America, but efficiency was low and continuous waves had little advantage until heterodyne reception became possible. The mechanical interrupters ("tickers") used in early c.w. receivers did not allow aural discrimination between signals and atmospherics.

Constructionally, the gear of the period tended to follow contemporary scientific instrument practice. with lacquered brasswork much in evidence, especially in Britain. Nickel-plated finish was more popular on the Continent and in the U.S.A., where ceramic insulants tended to be more widely used. Ebonite was, however, the most favoured material; plastic mouldings were virtually unknown. The concept of a "packaged" station had not arrived; the majority of transmitters and receivers consisted of a collection of units mounted where convenient and then wired together. But complete single-unit receivers were fairly common.

Some of the older stations used tinfoil-coated Leyden jars as transmitter condensers (the "jar" still did occasional duty as a unit of capacitance, but not in our pages). There were more modern tubular versions with sputtered or electrically deposited metal coatings on superior glass. Oil-filled condensers with metal plates and sheet-glass dielectric were perhaps the most common. Receiving variable condensers often had ebonite dielectric.

By far the most important applicainfinitellimi





Typical Marconi ship's wireless installation of the period showing (left) receiving tuner with magnetic detector on bulkhead above it; (centre) eme. gency spark-coil transmitter and (right) $1\frac{1}{2}$ kW rotary converter and spark gap of the main transmitter with (above) boxed coils of ''jigger'' and aerial tuning inductances.



Log cabin station typical of those used by North American miners, trappers and fishermen to keep in touch with civilization.

both in merchant ships and the navies of the world. Next came coastal stations for working with the ships. These were often sited on prominent headlands; a relic of the days when ranges were even shorter than in 1911. A few strategic naval and military stations, mostly of relatively high power, had been erected.

With the exception of the transatlantic service (of which more later). wireless had so far made little progress in its competition with landline and cable for point-to-point work. There were, however, a certain number of stations providing a telegraph service for isolated communities in cases where a wire connection was uneconomic. particular, the so-called log-cabin stations on the North American continent allowed local miners, trappers or fishermen to keep in touch with the outside world. A few of the early point-to-point stations, working at distances well beyond normal daylight range, provided a rather erratic service by taking advantage of night-time propagation conditions. Indeed, what might be called the "Heaviside bonus" was extremely valuable in the early days, particularly to ships. With its help, extraordinary ranges were attained with some consistency, especially outside the equatorial atmospherics belt. Atmospherics, or X's, were the great enemy. X-stoppers, optimistically so-called, had already appeared, but no real solution was in sight. About the best that could be done was to use pairs of crystal detectors working in opposition as limiters.

Special-purpose equipment for military and similar uses was already being designed and wireless had managed to stagger into the air in both lighter- and heavier-than-air machines.

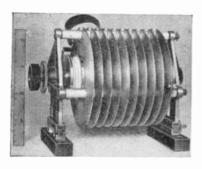
Prominent among the handful of famous stations of the time was Poldhu, in Cornwall, whose main task, together with its counterpart Cape Cod, U.S.A., was to provide a Press Service for the big liners which already printed daily newspapers on board. Poldhu was the first a.c.operated "power set," as distinct from an instrument-maker's job powered from an induction coil. It had been used by Marconi just after the turn of the century for the first transatlantic experiments. Dr. J. A. (afterwards Sir Ambrose) Fleming had been called in to do the original engineering design. Fleming is mainly remembered for his invention of the dlode, but he has an equalperhaps even greater-claim to fame as the first of the wireless engineers. Incidentally, he was the author of the first severely technical article (on r.f. resistance measurement) ever to be published in The Marconigraph.

The French military station on the Eiffel Tower, with its fixed spark gap and 25-c/s a.c. supply ("one spark for a dot and three for a dash") was known throughout Europe for its time-signal service. Thanks to the exceptional height of aerial, very long ranges were achieved, though the signals were often quite difficult to read through X's. The German stations of Nauen and Norddeich were also well known. Most of the high-power transmitters worked on wavelengths around 2,000 metres but the transatlantic station Clifden and Glace Bay were on about 6,000m.

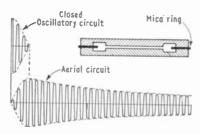
Commercially, the Marconi Company and its associates throughout the world were in a dominant position, if only by virtue of the patent position. In our very first issue we reported a successful action for patent infringement against the British Radio Telegraph and Telephone Company which did much to consolidate that position. Marconi's personal claims as the originator of wireless telegraphy had been hotly challenged for a dozen years or more. But, now the smoke has cleared away, it is not difficult to see that those claims were fully justified. He may not have contributed any great fundamental invention but, put in the simplest possible way, he had "made it work." The last word in the controversy had in reality been said as long ago as 1897, when the Editor of the Electrical Review, in answer to the rhetorical question "What did Marconi invent?" said, quite simply, "the elevated electrode." A prolonged subsequent correspondence in the pages of the journal failed to establish any valid claim to the anticipation of Marconi's invention of the aerial. It is clear enough now that an elevated aerial, plus an earth connection, was all that was basically necessary to turn Hertz's transmitting oscillator and Branly's receiving coherer at one step into a communication system with a useful beyond-the-horizon range. Subsequent detail improvements were not so difficult, but especial credit should be given to Lodge, whose "syntonic jars" experiment of 1889 had paved the way for syntony or tuning, without which wireless could never have got very

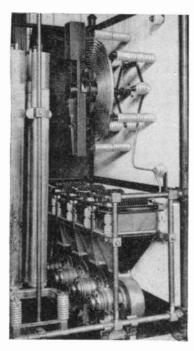
The race for priority had been close run and several rivals were breathing hard down Marconi's neck for the golden prize. And golden it turned out to be. When the young Marconi, in his early 20's, formed his company in 1897 he received £15,000—in golden sover-

SINCE THE WIRELESS WORLD BEGAN-Continued



Construction and electrical characteristics of the Telefunken quenched spark gap (based on Figs. 8, 10, 11, page 155 of Telefunken Zeitung, Vol. 26, No. 100





Air-blast cooling of multiple quenched spark gaps in a Telefunkon high-powered transmitter.

eigns, not depreciated paper pounds—and £60,000 in shares, which gave him a controlling interest. He was no guinea-pig director; at the time we began he was playing a dominant part in technical development.

At that time Marconi had no significant competition in England but his American company had to struggle against the United Wireless Company which controlled some 500 stations. But, in a year's time United Wireless was to be absorbed after admitting the validity of the Marconi patents. The real and most serious competitor, both commercially and technically, was the Telefunken Company in Germany, an amalgamation of several German wireless interests.

Telefunken had produced a distinctive and extremely effective spark transmitter of which the main feature was a multiple spark gap made up of a number of silver-faced copper discs with deep cooling flanges separated by thin mica rings. In the standard 2½kW set there were eight series-connected gaps. Thanks to the rapid dissipation of heat, excellent quenching of the primary circuit oscillations was secured, with wave-trains of high persistence in the aerial circuit. An alternator frequency of 500c/s gave a spark frequency of 1,000; the high-pitched note of Telefunken transmitters was quite distinctive. Efficiency was high; probably over 60%.

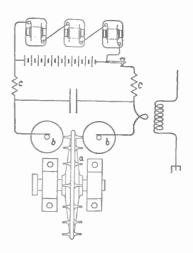
The Telefunken receiver had a tuned aerial circuit variably coupled to a semi-aperiodic secondary shunted by a crystal detector and headphones. An alternative type of set, giving higher selectivity, had an intermediate tuned circuit. Clip-in interchangeable coils were used. The detector, a sealed cartridge usually with a silicon-gold combination, was interesting as a kind of forerunner of the modern crystal diode.

Germany's contribution to wireless development had been acknowledged when Ferdinand Braun shared with Marconi the Nobel Prize for physics in 1909.

In the early days the transatlantic station at Clifden, in the wilds of Connemara, was the wonder of the world of wireless. And rightly so; there was nothing remotely approaching it, either in technology or performance, except its communicating station at Glace Bay, Nova Scotia, which, being more remote, was less in the limelight. Marconi himself gave a detailed description of Clif-

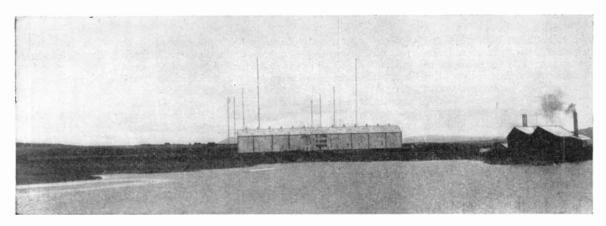
den, which had recently been rebuilt, in a lecture to the Royal Institution, reported in our first volume. fantastic station was unique in being powered by d.c., drawing 300kW from a 6,000-cell accumulator battery, "the largest of its kind in existence," which, when fully charged, gave a voltage of 15,000. Charging of the battery was by three seriesconnected high-voltage generators, the prime mover being a steam engine. The six boilers were fired with peat, brought by a light railway from the adjacent bog. Still more fantastic was the closed circuit airdielectric condenser; the metal plates were spaced a foot apart and this component-the first to which the term "low-loss" was appliedneeded an enormous shed to house it. The rotary spark gap was run at a speed giving a sparking rate of 500 p.s. As the rate was independent of load, the note was exceptionally pure.

For the year to April, 1911, it was proudly claimed that 812,200 words of paid traffic had been pumped across the Atlantic. That would sound pitifully small to the manager of a modern communication circuit, but



DISC DISCHARGER
CONTINUOUS CURRENT

Circuit diagram of the Clifden "d.c." transmitter.



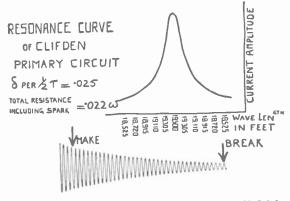
General view of the transatlantic high-power spark station at Clifden, Connemara. On the right is the peat-burning power house.

was probably a great improvement over that achieved with earlier apparatus. Detailed records are lacking, but in the Marconi archives there are some figures relating to the period beginning October, 1907, when a limited public service had been opened. Traffic was then running at the rate of a mere 300,000 words a year and average delays ranged from $2\frac{1}{2}$ hours at best to over 14 hours.

And—supreme humiliation to wireless men—well over 7,000 words had to be handed over for transmission by cable. Apart from the humiliation, that involved a dead financial loss of 4d a word: the "via Marconi" service was cut-price.

We do not know what were the delays and "cablings," as they were called, in 1910/11, but it seems certain that the new apparatus just

described had brought about a great improvement in communication. Independent testimony given a year or two later suggested that average delays did not exceed those of the cable. But highly detailed signal-strength curves shown in Marconi's 1911 lecture make it appear that communication was liable to fail for a few hours nightly at times when X's were prevalent. Still, it is fair to



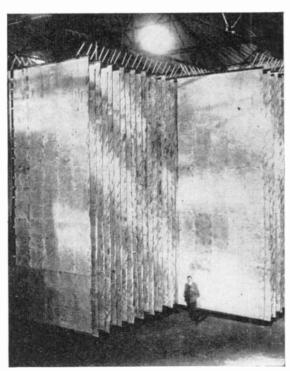
OSCILLATIONS CORRESPONDING TO ABOVE RESONANCE CURVE



SERIES OF WAVE TRAINS RADIATED FROM CLIFDEN AERIAL SPARK FREQUENCY 500 PER SEC.

Characteristics of the Clifden transmitter. (From Marconi's Royal Institution Lecture, June 2nd, 1911.)

Air-dielectric condenser of the closed circuit at Clifden.



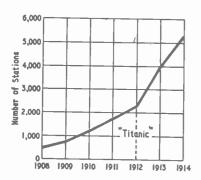
say the Atlantic had been conquered at last after many failures and disappointments. The epic struggle to get consistent signals across had started from the Canadian end* eight years earlier, at a time when nothing was known about long-distance propagation; the engineers did not even know on what wavelength they transmitting! were Countless changes in circuitry, power and aerial arrangement had been made. Glace Bay station had even been shifted to a different site.

Clifden came to a sad end in "The Troubles" of 1922, when the station buildings were burned to the ground. Still, it had nearly served its time and a radically new long-distance technique was soon to emerge. The station has no memorial, though, by a strange coincidence, near the site is a commemoration stone to the flyers Alcock and Brown, who crashlanded there after conquering the Atlantic through a different medium.

* The Canadian government had subsidized the Glace Bay station to the extent of \$80,000.

1912

A CATASTROPHE which stirred the minds of men—and still does so—was the sinking of the *Titanic*. That great liner, believed to be unsinkable, struck an iceberg on her maiden voyage and sank in a few hours. Over 1,500 lives were lost, but some 700 were saved by ships summoned by wireless.



Increase in the number of the world's licensed stations between 1903 and 1914. (Based on data from the International Radiotelegraphic Bureau, Berne.)

That "epic tragedy of the sea," as we called it, was to have far-reaching effects. In earlier shipwrecks lives had been saved by wireless, but the part it had played in the Titanic disaster fired the public imagination: no longer did anyone doubt its America quickly passed a value. law to regulate wireless communication and, at long last, ratified the International Convention. Wireless men had become benefactors of humanity and, if our pages can be taken as reflecting their attitude, felt they "had never had it so good." Indeed, over-confidence began to creep in.

A grandiose, and what now seems over-optimistic, "Imperial Wireless Scheme" for linking the units of the British Empire was planned and a contract between the Postmaster-General and the Marconi Company was signed in July. A few extracts from the specification will give some idea of the giant spark stations proposed: "Capable of transmitting to the distant station at any time of day or night. . . . Wavelengths as great as possible within the limits of 17,000 and 50 000ft. . . . Aerials over 3,000ft to 8,000ft long, supported by tubular masts 300ft high. . . . Prime mover to be a steam turbine of between 1,300 and 2,500 h.p."

A name that has constantly recurred in our pages since the beginning—and happily still recurs—is that of H. J. Round, one of Marconi's engineers. In an article on the strength of atmospherics in relation to signals, Round described the use of a Fleming diode as a valve voltmeter to measure voltages set up by the X's—certainly our first mention of what we would now call electronics. Round has played a prominent part in many important developments.

High-speed automatic telegraphy was discussed. The transmitter was keyed by a Wheatstone machine and, for reception, there was the choice of photographic or phonographic methods. The phonograph, which allowed better discrimination between signals and X's, seems to have won the day; before long, speeds of 100 words per minute were demonstrated.

Heaviside's theory of wave propagation, enunciated some ten years earlier and now expanded and championed by Eccles, became the subject of quite violent controversy. It is pleasing to record that we came down editorially on the right side—but very cautiously: "at the moment there is a disposition to accept the hypothesis

put forward by Dr. W. H. Eccles as yielding the best explanation of the observed phenomena."

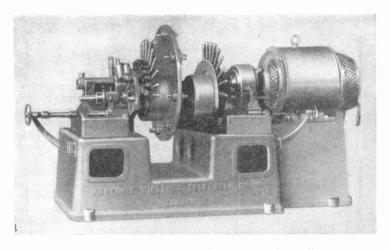
Direction finding, a brand-new application of wireless, now appeared. Thanks to the large size of the pair of fixed loops used in the original d.f. gear, sufficient signal pick-up was obtained to give fairly useful ranges without amplifying valves.

Throughout the early period wireless was bedevilled by patent litigation. During this year some sort of agreement seems to have been reached between Marconi's and their rivals Telefunken; actions and counter-actions with Siemens, who exploited the German system in Britain, were called off.

1913

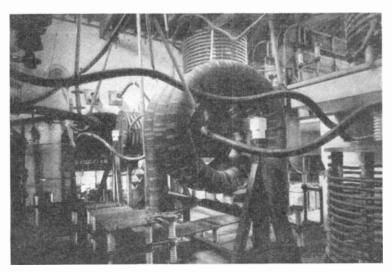
EVER since the Imperial wireless scheme had been announced the Government had been constantly under criticism, mainly on the grounds that the contract had not been thrown open to tender. A technical committee was now appointed "to report on the merits of the existing systems of long-distance wireless telegraphy." The distinguished members, all Fellows of the Royal Society, included the Director of the N.P.L. and the President of the I.E.E. They obviously did a conscientious job and produced a report providing a valuable and unbiased commentary on the state of the art in 1913. The systems examined were Marconi and Telefunken (spark), Poulsen (arc) and Goldschmidt (alternator), which used a rotary r.f. generator with contrarotating field and armature, frequency multiplication being obtained by feedback. Those responsible for these systems were invited to give practical demonstrations "if possible over distances of 2,000 miles and upwards."

According to the committee's report "Except in the case of the Marconi system we did not, however, obtain any demonstrations over a distance of even 1,000 miles". Of Telefunken, it was said that experiments were being made between Nauen and Togoland (4,000 miles) and that communication seemed possible at night. Results of the Poulsen arc system working between San Francisco and Honolulu (2,100 miles) "do not appear to have been very satisfactory". The Goldschmidt machine being set up at Hannover "was ad-



Disc discharger for the 75kW Marconi spark installation.

The huge primary winding of one of the "jiggers" (aerial coupling transformers) far the 300kW synchronous spark transmitter at Caernarvon.



mirable both in design and workmanship" and expected to be capable of communicating across the Atlantic.

The Clifden transatlantic station was visited by the committee members, to whom high-speed and duplex working were successfully demonstrated. Of the general performance, it was said "Communication is practically continuous, though there are, no doubt, periods when the signals become very weak and even occasional periods when no signals can get through". But a note of warning was wisely sounded about the possibilities of atmospheric interference in the tropics.

In spite of this favourable report, the Imperial wireless scheme was not to have a smooth passage. Criticism of the Government continued and a political scandal had developed. To cut a long story short, although the contract was eventually ratified by Parliament, the scheme never came to fruition. It ended with the conferring of the G.C.V.O. on Marconi and the award to his company, many years later, of £590,000 damages against the Postmaster-General for breach of contract.

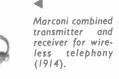
Thanks to the attention focused on wireless by the *Titanic* disaster the amateur movement had begun, and we were already publishing instructional articles for the benefit of amateur readers. We showed them it was quite easy to make a start: "An old motor-cycle ignition coil will do for the transmitter and a simple crystal set for the receiver". American amateurs were now controlled, being restricted to wavelengths below 200m and input powers of not more than 1kW.

1914

THIS year was marked by the most momentous advance so far described in our pages—the practical introduction of the triode, which had got off to a false start in 1907. This

Man Sup S

The Round-Marconi triode, one of the early practical amplifying valves.



ism of the Government continued иншиниципиници

was used in "a practical standard set for wireless telephony" developed by Marconi. This transmitter took 10-12mA from a 500-V dry battery and was stated to have a range up to 45 miles. Hardly any details were given.

The Marconi transatlantic station at Caernarvon was opened, working on the "timed spark" system in which more-or-less continuous waves were produced by overlapping spark discharges in appropriate phase. The "tone wheel", a mechanical beatfrequency generator for c.w. reception was introduced in Germany.

THE FIRST WORLD WAR

DURING the war our activities were severely circumscribed by what we called "the heavy hand of censorship" and, in particular, we were prevented from writing anything about the rapidly increasing use of valves for war purposes. In fact, the only "safe" technical news was that coming from neutral America. David Sarnoff, then in Marconi's W.T. Co. of America, and later to become President of the Radio Corporation of America, was for a time our New York correspondent.

Without any doubt, the most important news coming from the U.S.A. concerned the development of the triode: in particular "the simultaneous use of a single bulb as rectifier, amplifier and oscillator has already produced startling results". That may raise a smile nowadays but, at the time, it was difficult to believe that anything more sensitive and selective than a good singlevalve regenerative receiver would ever be devised. The importance of heterodyne reception was fully realized, thus giving continuous wave systems a new lease of life.

Towards the end of the war there was some relaxation by the censor and theoretical articles on valves were printed. Among the authors of these were two distinguished founder-members of Phase II of wireless technology: Dr. R. L. Smith-Rose and E. V. (later Sir Edward) Appleton. Smith-Rose wrote a long series of articles, starting with elementary thermionics, while Appleton's contribution gave our first mathematical treatment of valve characteristics. Valve manufacture was advancing rapidly and as early as 1916 transatlantic wireless telephone tests were made, using 300



Police wireless car in New York (1918).



Dame Nellie Melba giving her famous broadcast concert from Chelmsford long-wave station on June 15th, 1920.

receiving-type valves in parallel in the transmitter.

In the early days most wireless stations were designed empirically but by 1917 it was thought possible to design a complete station of specified performance by applying accepted formulæ; to "fly 'em straight off the drawing board", as they say in aviation circles.

theoretical exercise of this kind was now offered to readers in a series of articles.

The end of the spark transmitter era was now drawing nearer, thanks to improvements in continuous-wave gear and still more to heterodyne valve reception. The last of the great spark stations were those built for spanning the Pacific in two hops; from San Francisco to Honolulu (2,100 miles) and from Honolulu to Funabashi, Japan (3,350 miles).

British amateur activities had been entirely suspended since the outbreak of war but in the U.S.A. the movement steadily gained strength until America's entry into the war in 1917; by that time the supply of amateur equipment had become big business.

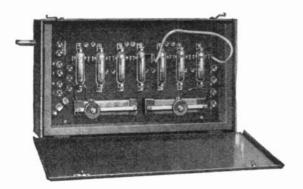
Television; a contributor's prophesy that went wrong: "The idea of wireless television is . . . absurdly improbable. . . . To construct wireless apparatus capable of receiving 40,000 signals in one-tenth of a second and arranging them in their correct order [would be beyond] the limit of human ingenuity."

WITH the end of the war, articles of the "it-can-now-be-revealed" type were printed. One of the developments disclosed was the multi-stage r.f. amplifier with semi-aperiodic couplings.

Valves were now being produced by improved processes and the "soft" kind was fast disappearing. The generation of oscillations (by van der Pol) on a wavelength as short as 3.65m was considered a notable advance. Eccles suggested the modern valve nomenclature; diode, triode, tetrode and pentode. We were not quite at our best in editorially stigmatizing these now-universal terms as "too academic and refined to become familiar." High-power transmitting valves were now being made, allowing Marconi to span the Atlantic by telephony in daylight.

Amateur transmitting licences were not restored by the Post Office until a year after the war had ended; this delay caused much complaint.

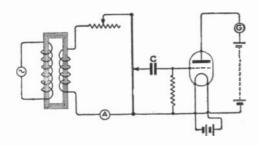
THIS was the heyday or tne great long-wave stations with arcs or r.f. machine generators, operating on



A famous r.f. amplifier-detector—the Marconi 55A with V24 type valves.



A group of passengers about to embark for Paris on the first commercial machine (Handley Page) to be equipped with radiotelephony (1920).



Circuit diagram of the Moullin valve voltmeter (1922) showing method of calibration.

wavelengths most conveniently measured in miles; the longest (Bordeaux) was 14 miles. Powers were up to 1,000kW or even more. In spite of improvements, the arcs radiated a rich assortment of harmonics and "arc hash."

Continuous-wave sets for ships, wireless gear (including telephony) for the new airlines and commercially available direction finders were new developments.

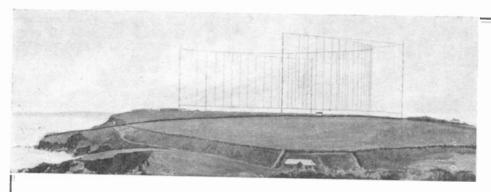
The Wireless Society of London, suspended during the war, had now resumed full activity. Though by constitution an amateur body, this unique institution did in fact represent a happy mingling of amateurism and professionalism. Many of the "eminent wireless telemost graphists," as we used to call them in our earliest days, lectured before the Society. The first five Presidents-Campbell Swinton, Erskine Murray, Admiral of the Fleet Sir Henry Jackson, Eccles and Sir Oliver Lodge-had all from before the turn of the century played distinguished parts in wireless development. The Society changed its name to Radio Society of Great Britain in 1922.

1921

THERE had by now been several casual mentions in our pages of what is now called "electronics"; Appleton, in a tailpiece to a book review, referred to the valve as "an invaluable laboratory instrument" to the general physicist. The use of amplifying valves in conjunction with photoelectric cells for measuring light intensities had also been mentioned. Now came our first full-dress electronics article in a report of a paper read before the Wireless Society of London by Prof. R. Whiddington on the measurement of physical quantities. He described the measurement of short distances by capacitance variation using the beat-note method with two oscillating valves. Sensitivity claimed was 50 to 100 times greater than that of the optical interferometer.

Broadcasting in America was already under way and regular "Dutch concerts" from The Hague were started. The Marconi Company's transmissions from Writte were licensed by the Post Office early next year. With increased interest in telephony loudspeakers became important. Most of them consisted essentially of a telephone earpiece with a horn, but the American Mag-

SINCE THE WIRELESS WORLD BEGAN-Continued



Above: The parabolic aerial reflector at Poldhu used in early short-wave beam experiments.

Right: A floating laboratory— Marconi's yacht Elettra.



navox moving coil and the Western Electric balanced-armature types had appeared.

1922

AMATEUR transatlantic tests were successfully carried out on 200 metres, Wireless World organizing the arrangements on this side. Moullin described his valve voltmeter, the first widely used electronic device. Dull-emitter valves

with a filament wattage about 1/15th that of earlier types were introduced and news of Armstrong's superregenerative receiver came from America.

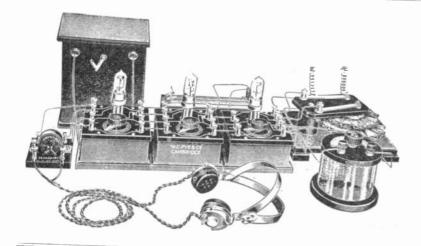
C. S. Franklin of Marconi's described an important development—the use of highly directional aerial arrays on wavelengths below 20m. But so far there was no suggestion that such waves were usable over very great distances.

Towards the end of the year the British Broadcasting Company, fore-

runner of the Corporation, began official transmissions. Wireless World started weekly publication.

1923

WITH broadcasting in full swing, the biggest do-it-yourself boom of all time got under way; a high proportion of receivers were homeassembled The typical valve set of the period had a regenerative de-



"Messrs. W. G. Pye & Co. (Makers of Physical and Electrical Apparatus) beg to announce that they have opened a Wireless Dept. at their works" (Advertisement from W.W. May 27th, 1922).

The unit receiver was popular in the early broadcasting era.

tector with two transformer-coupled a.f. stages and sometimes a rather ineffective r.f. stage, stabilized by aerial loading or positive grid bias. Neutralizing of anode-grid capacitance was already known, but its use did not become widespread for several years. Cost of valve receivers was high, so many listeners used crystal sets with headphones.

The superheterodyne principle of reception was first described; this was one of the great basic inventions which got off to a slow start.

"Electromagnetic Screening," the subject of an article by R. A. (later Sir Robert) Watson Watt, seems a far cry from the author's future work in radar. More in character was his R.S.G.B. lecture "Observations on Atmospherics" (using recording gear and direction-finding) reported later in the year. "The greatest unsolved problem in radiotelegraphy is interference by X's."

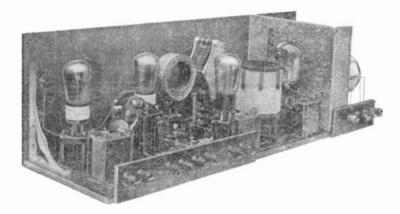
THIS was the year of the "wavelength revolution," a distinct landmark of the half-century. Marconi exploded his "beam wireless bombshell" by disclosing how, in the spring of 1923, he had conducted short-wave receiving tests on 93m while cruising in his yacht Elettra in the S. Atlantic. The transmitting station was at Poldhu, where Franklin had erected a parabolic reflector array. The British Government hastily revised their scheme of expensive mile-wavelength stations for Imperial communications and the Marconi Company undertook a contract to erect beam transmitters on a strict "no play, no pay" basis. That was probably one of the boldest commercial enterprises ever undertaken; nothing was known about short-wave propagation theory and the phased multiple "grid" aerials which were to replace the parabolic reflector system existed only on the drawing board. But fortune had favoured the brave; we now know 1923 was a sunspot minimum year; the frequencies chosen for the early experiments, though on the low side, were not so low as to be unworkable; on the other hand, they were not so nearly correct for prevailing conditions as to give an over-optimistic impression of the potentialities of short waves.

Short-wave working had by now become widespread, particularly among amateurs, and s.w. broadcasting had started in America. Other highlights of the year: Campbell Swinton's detailed pronouncement on the possibilities of cathode-ray television and Baird's first article on his mechanical system.

SOMETHING approaching the modern theory of short-wave propagation was now put forward by Appleton; Round wrote our first article on second-channel interference and other troubles to which the superheterodyne, now becoming of practical significance, is prone. Baird wrote on television by reflected light (as opposed to shadowgraphs) and that versatile genius, A. D. Blumlein, in collaboration with N. V. Kipping, discussed valve

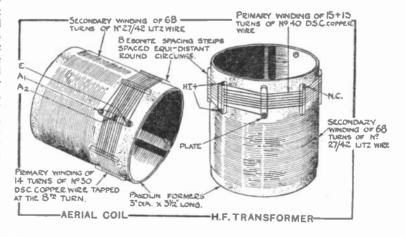
theory. Electrical recording and reproduction of gramophone records was introduced and the quartz oscillator and piezoelectric effect were described.

The amateurs' position had, we considered, been steadily undermined by the Post Office and, feeling diplomatic methods would no longer suffice, we publicly offered £500 towards the cost of fighting a test case against the Postmaster-General. It so happened the Marconi Company (then our publisher) was at the time engaged in delicate negotiations with the Post Office: an embarrassing situation seemed likely to arise, so the obvious course was to get rid of Wireless World as quickly as possible. Thus the transfer to our present publishers came about. That, needless to say, is a story which did not appear in Wireless World.



Wireless World "Everyman 4" receiver (1926) set a new standard in range and selectivity for broadcast receivers.

Details of the low-loss tuning coils used in the "Everyman 4."



1926

SO far as we were concerned, the event of the year was the introduction of the "Everyman Four," a receiver design of outstanding performance produced by us for home constructors. The feature of the set, which survived for many years in various modifications, was a highgain neutralized r.f. stage with coils of exceptional "goodness," based on the classical work of Butterworth and on tests of coils submitted by readers.

The first mains-operated broadcast set (Gambrell) made its appearance. The series-connected 60-mA valve filaments were heated with rectified current from the h.t. supply source. Battery eliminators were now commonplace.

1927

AT last, Heaviside's theory of a conductive layer in the upper atmosphere was experimentally verified. Amplifying work done in the previous year, Appleton wrote an article showing how, by a method of distinguishing between waves travelling horizontally and those arriving in a downward direction, he had concluded the height of the layer of ionized air at night was 80-100km.

The first public transatlantic telephone service was opened and we conducted a campaign for Empire broadcasting on short waves.

1928

A MORE scientific approach to many problems, particularly to the details of receiver design, now becomes evident. It had already been shown (by M. G. Scroggie) that even a very low value of impedance common to several anode circuits could completely spoil the performance of an a.f. amplifier. This trouble was overcome by "decoupling" individual circuits, a method originated by Ferranti. The isolation of circuits by "scientific wiring" was also descr.bed.

By now, the neutralized triode was being replaced by the screened tetrode for r.f. amplification. Output pentodes, fed directly from the detector, helped to simplify and cheapen broadcast receivers: the three-valve set was becoming the most popular.

Detection of signal echoes "from the depth of space," with a time delay of 15 sec, gave a foretaste of extra-terrestrial communication.

1929

BAIRD'S 30-line mechanical television system, with flying spot scanning, was now sufficiently developed for the B.B.C. to give experimental transmissions of it for half-an-hour a day; these were continued until 1935. The broadcasting of "still" pictures by the Fultograph system by the B.B.C. and many European countries enjoyed a short-lived vogue.

Spark transmission for ships and coast stations was slowly giving way to i.c.w. (interrupted continuous wave); for long-distance point-to-point communication short waves had almost entirely replaced long-waves except on the N. Atlantic circuit

Broadcast receivers were now built more or less in the modern manner, with metal chassis and, quite often, built-in speakers. Mains sets with the recently introduced indirectly-heated valves were commonplace. But there were still few sets with ganged tuning. Efforts were being made to provide greater selectivity in preparation for the "Regional" broadcasting plan, which was to offer listeners a choice of two programmes. The architect of the scheme, of which many traces remain in the present B.B.C. distribution system, was P. P. Eckersley, then chief engineer, who for many years has projected his ebullient personality and original thoughts through occasional Wireless World articles.

1930

A LIVELY controversy arose over the so-called "Stenode" receiving system, in which sidebands lost by extremely sharp tuning were restored by tone correction. The crucial question: "was interference put back equally with the sidebands?" A related controversy concerned the physical reality of s'debands; there were several notable "heretics."

The susceptibility to cross-modulation of screen-grid valves brought about a wave of interest in bandpass as a corollary, ganged single knob tuning was widely adopted for broadcast and other receivers. Per-

manent-magnet moving coil loudspeakers were now in general use.

Our funny man "Free Grid," shrugging off an Editorial footnote threatening imminent "earthing" soon after starting his whimsical writings in September, 1930, has carried on ever since with his task of preventing us all from taking ourselves too seriously. One of his outstanding contributions (in our issue of March 10th, 1933) contained a remarkable anticipation by 16 years of Orwell's "1984." "Free Grid" went one better than Orwell in giving his Big Brother an electronic "thoughterime" detector.

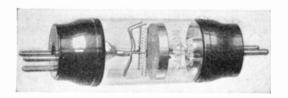
1931

PAVING the way for a better understanding of short-wave propagation, Appleton showed for the first time in our pages that there was more than one reflecting layer in the upper atmosphere. He had earlier sought the help of our readers in reporting distortion of the Baird 30-line television picture brought about by multipath propagation and reproduced a reader's sketch of a picture which clearly showed the effect.

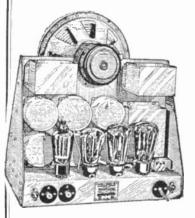
Short-wave telegraph and telephone services had by now linked many, if not most, of the more advanced countries of the world and lack of secrecy, a handicap of wireless since the earliest days, was overcome by "scrambling."

The N.P.L. was taking steps to develop a standardized form of test for the sensitivity, selectivity and fidelity of receivers. The decibel scale began to come into general use in place of such expressions as "times amplification," etc.

So far as receivers were concerned, the introduction of the variable-mu valve with linear characteristics largely overcoming the difficulties of cross-modulation, was an important development. "Straight versus superhet" became a burning issue, but the outcome was not in much doubt. Realizing that ganged tuning with "potted" coils would soon become universal, we commissioned a special investigation of the characteristics of coils. Moving-coil speakers, now generally built into the receiver, were almost universal: during this and the preceding year the finer points of their design were discussed in a long series of important articles by Dr. N. W. McLachlan.



The introduction of the screened-grid valve in 1927 enabled higher r.f. gains to be achieved with stability.

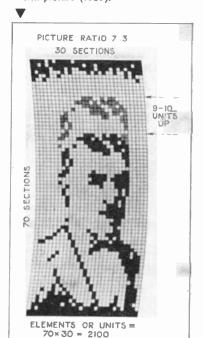


A highly-developed broadcast receiver of the late "straight-set" period: the Murphy A3 (1931).

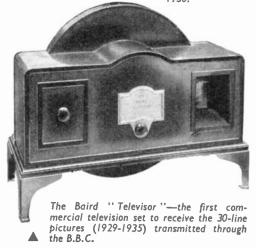


A. A. Campbell Swinton, F.R.S., the prophet of television as we know it today, who died in 1930.

Sketch by a reader (W. B. Weber) showing observed effect of multipath propagation on a 30-line television picture (1931).



A turn of this kind, giving wide contrasts of light and shade, was thought to provide "genuine entertainment value" on 30-line television.





SINCE THE WIRELESS WORLD BEGAN-Continued

1932

THOUGH many ships still had spark transmitters, marine wireless had by now made considerable progress. Short-wave equipment for telegraphy was commonplace and some 15 transatlantic liners provided a radio-

telephone service for passengers. The G.P.O.'s long-distance station for working to ships had been much improved and now had a rotating beam array with an electrically-interconnected receiving beam turning in unison at the remote controlling station.

The cathode-ray tube had by now

become a regular article of commerce and its applications were no longer restricted to research work; it was being used for routine factory testing.

A stir was caused by the introduction (from Germany) of coils with powder-iron cores; inductors of this type were soon to be widely used in receivers in place of bulky air-cored windings.

A B.B.C. service of official "Empire" broadcasting, for which we had campaigned for some six years, was at last started. Wire and wireless were linked by a five-metre Post Office telephone link across the Bristol channel.

1022

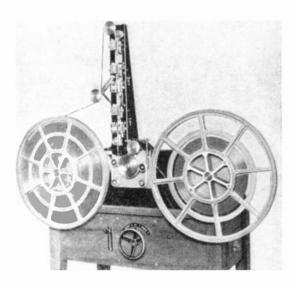
WITH the increase in sensitivity of receivers and the growing electrification of the country, man-made interference had become a serious problem. Following suggestions made in Wireless World the I.E.E. had set up a committee to consider the possibility of legislation and interference complaint questionnaire forms could be had from post offices. This service is still available to the public.

The "small superheterodyne" was soon to become Britain's standard broadcast receiver: early versions had bandpass input, single-valve frequency-changer, one i.f. stage and a second detector feeding a pentode output valve. R.F. pentodes were by now widely used and the electroncoupled frequency-changer had appeared. Refinements like automatic gain control, noise-suppression switches and, occasionally, "quiet" a.g.c., were coming in. For battery sets, economy circuits with push-pull output valves biased to cut-off were being used. Built-in car sets had arrived, so we described methods of suppressing ignition interference.

S.T.C. put up for the Air Ministry a decimetre-wave (17.5 cm) link working across the English Channel.

1934

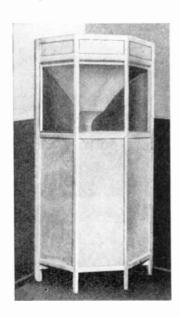
SEVERAL high-definition television systems were now being described and Zworykin's "Iconoscope" camera tube was announced. Apparently the audience of the Baird 30-line broadcasts was greater than we had thought; publication of a proposal to suspend the transmissions brought,

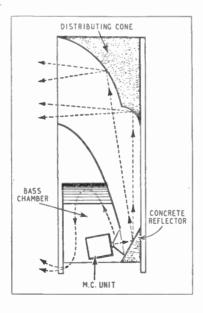


Marconi-Stille steel tape recorder.

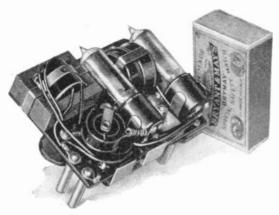
ARRIGED PROFESSORE STREET THE PROFESSORE AND A PROFESSORE

An historic high-quality loudspeaker: the Voigt domestic corner horn in its original form (1934).





DESIGNOCESTATUDADE DE REPUESTRO DE DE LA COMPANIO DEL COMPANIO DE LA COMPANIO DE LA COMPANIO DE LA COMPANIO DE LA COMPANIO DEL COMPANIO DE LA COMPANIO DEL COMPANIO DE LA COMPANIO DE LA COMPANIO DE LA COMPANIO DE LA COMPANIO DEL COMPANIO DE LA COMPANIO DE LA COMPANIO DE LA COMPANIO DE LA COMPANIO DEL COMPANIO DEL COMPANIO DE LA COMPANIO DE LA COMPANIO DEL COMPANIO DEL COMPANION DEL COMPANION



Forerunner of the (transistor) pocket portable: chassis of a super - regenerative valve set (1935).

within the week, protests from a large number of readers. No doubt the transmissions on this system, crude as it was, did a great deal to stimulate work on television; some correspondents were now using cathode-ray receivers.

The introduction of suitable valves

now made practicable the "universal" a.c./d.c. receiver, without a transformer.

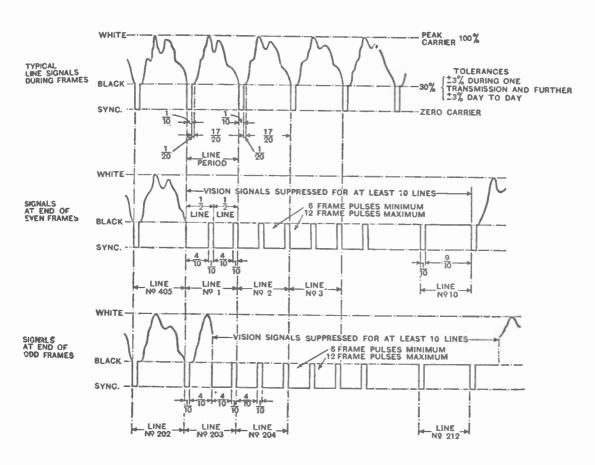
Our contributor "Cathode Ray" started his inimitable series of expository articles in 1934. Apart from his services as a talented and sympathetic expositor of the trickier aspects of

technology he has been a doughty fighter against the many irrational and confusing technical terms which make life so difficult for the student and beginner. And "Cathode Ray" has won many of his battles: few of us now dare to speak of "non-linear distortion" unless we really mean it is the distortion which is non-linear!

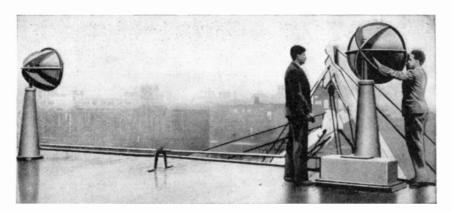
Other innovations of the year: investigations of the effect of sunspots on h.f. propagation: the Marconi-Stille magnetic wire recorder: highnote speakers (tweeters): the Wireless World Quality Amplifier, with resistance-coupled push-pull, which set a standard for high-quality reproduction for many years: the Voigt domestic corner horn loudspeaker.

1935

THE scene was now set for the start of a regular British television service



Characteristics of the Marconi-E.M.I. television system as first issued in 1935.



Radar: S.F.R. "obstacle detector" fitted in the liner Normandie (1936).

next year and it was decided that alternative test transmissions should be made on the Marconi-E.M.I. system (405 lines interlaced; characteristics basically as at present) and a new Baird system (240 lines with sequential scanning; 25 frames per second). One of the television systems much discussed was the "intermediate film," with a time delay of

about half a minute; it was easier to scan the film image than the direct scene.

Our "Diallist" now started his

non-stop radiations of his random

and highly individualistic comment-

ary on the happenings of the times. Some developments of the year: Armstrong's frequency modulation in America: the electron multiplier: "all-wave" tuning and refinements like contrast expansion and automatic selectivity control in broadcast receivers: public address became important.

1936

THIS year marks the end of our first quarter-century and it is time for a backward glance. And a very appropriate time, as it happens: technical development was moving rapidly into Phase III, the era of high-definition television, industrial electronics, microwaves, radar and pulse techniques. Phase I had been the evolution of spark telegraphy on medium and long waves. Phase II, coming to an end in 1936, had began with the practical development of the amplifying and oscillating valve in 1911-1913, followed by radio-telephony, broadcasting, the full exploitation of the multi-mile wavelengths and then of those rich bonanzas the h.f. and v.h.f. frequency bands; also

the start of electronics for scientific purposes. Most of this progress had been made possible by valve improvements; our contributor, "Cathode Ray," produced detailed support for the assertion that 92 valves of the 1921 type would be needed to provide the performance of the typical five-valve broadcast receiver of 1936. And a resourceful designer, well primed with the accumulated knowledge of 1936, would have been needed to achieve that performance.

A quick glance through our 1936 volume shows how fast radio technology was then moving into modern times: The B.B.C.'s London television station started the world's first regular high-definition service; the French S.F.R. company introduced the "obstacle detector," a non-pulse radar device; "plumbing" was coming in and waveguide theory was treated; there was a number of articles on electronics; an editorial plea was made for the abolition of spark transmission.

A quarter-century's progress in wireless telegraphy; the Queen Mary on her maiden voyage handled as many words of traffic in the few days of the crossing as the great transatlantic station Clifden had averaged in two months in 1910/1911.

1937

NOW that regular transmissions had started, television became the centre of interest and was much discussed both in theory and practice. The first 405-line commercial receiver to be reviewed was an H.M.V. model giving a picture 10in by 8in viewed indirectly in an inclined mirror. The vision unit had a "straight" six-

stage r.f. amplifier, the sound receiver being a superheterodyne. Deflection was magnetic and the set, complete with aerial, cost 95gns. After a few weeks' trial the Baird 240-line transmissions were discontinued, leaving the 405-line system, basically as it is today, as the British standard. One of the first television outside broadcasts was that of the coronation procession of King George VI.

Designs for the home construction of ordinary broadcast receivers were now seldom offered in our pages; the readership was undergoing a change, as was shown by a questionnaire. About half our readers were now professionally concerned with radio.

The "all-wave" broadcast receiver, often with three short-wave bands, was now firmly established and the complicated switching required had made the wafer switch almost universal.



Guglielmo Marconi who died in July 1937, aged 63.

1938

THE days were long past when the vagaries of short-wave propagation had been stoically accepted as something to be endured, like the weather. Diversity reception was now well established; a description of the B.B.C.'s highly developed receiving station at Tatsfield was published. And the minor deficiencies of equipment generally were less readily tolerated. Now came a determined effort to overcome tuning drift by more basic and cheaper means than automatic frequency control; much attention was given to temperaturecompensated components.

The public demand for television receivers had so far been disappointing. Now, in an attempt to attract buyers, cheap sets with small 5-in, 6-in or 7-in tubes were introduced. One example, costing 29gns, had a 5-in tube giving a picture 4½in by 4in.

Push-button tuning became the vogue in sound broadcast receivers. There were three main methods: mechanical location of the condenser; motor drive of the condenser; separate pre-tuned circuits for each station.

In brief: electronic techniques used for neurological research and Grey Walter's electro-encephalograph produced; improved electron microscope announced; "wobbulator" and Cossor double-beam oscilloscope introduced.

1939

EVER-INCREASING interest in sound reproduction was further stimulated by B.B.C. experimental transmissions of high quality on 45Mc/s; this was Britain's first taste of v.h.f. broadcasting, though f.m. had already started in America.

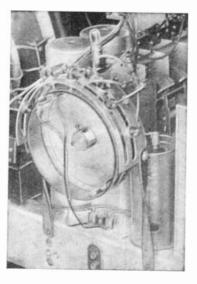
The Western Electric "radio altimeter" for aircraft, an f.m. device working on frequency differences between the emitted wave and reflections received from the ground, was described.

In television, the public had not taken kindly to the small "peephole" sets introduced last year and there was a reversion to larger tubes, the 12-in size being most favoured. Ignition interference was being discussed and voluntary suppression was suggested.

Some new introductions: the cathode follower; "all-glass" valves with short, well-spaced internal leads;



Cossor Model 54 with 6-in tube (1938).



Drum-type commutator of the H.M.V. motor-driven tuning mechanism (1938).

forced air cooling for high-power transmitting valves; short-wave therapy.

With the threat of imminent war, Wireless World had, with official approval and collaboration, instituted early in the year a "National Wireless Register" through which readers were able, without any liability, to have a record of their technical qualifications made available to the appropriate authorities. The Register was later to prove a valuable source of technical man-power for war-time radar as well as for communications.

1940-44 THE SECOND WORLD WAR

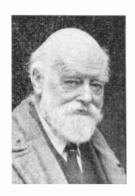
AMONG the immediate results of the outbreak of war in September 1939 was the closing down of the television service and of amateur transmission; car radio was banned later. B.B.C. headquarters "moved into the country" and a single-programme service was transmitted from synchronized stations to avoid giving direction-finding help to the enemy. There was a short-lived boom in receivers, especially in the recentlyintroduced "semi-communications" models, which offered an exceptionally good performance on short waves. This was mainly wanted for the reception of news bulletins from overseas, and especially from neutral sources. Information on short-wave receiving conditions was also wanted: for some time we published ionosphere forecasts provided by Cable and Wireless, but these were eventually stopped by the censor. However, no objection was raised against "doit-yourself" forecasting and general articles on propagation by T. W. Bennington were continued.

One of the popular "semi-communications" receivers of the early days of the war: the Pye "International" with band-spreading on six short-wave ranges.



SINCE THE WIRELESS WORLD BEGAN-Continued

So far as Wireless World was concerned, the war brought an abrupt change from weekly to monthly publication and, with a depleted staff, we did our best to meet the changing needs of readers, especially in producing instructional articles on new subjects: morse telegraphy was



Sir Oliver Lodge, the pioneer of "syntony" (tuning), died in August 1940, aged 89.

now important. And a rather unexpected demand arose for the treatment of topics bearing no relation to the grim realities of the times—for maintaining the journal, as a correspondent put it, as "one of the few remaining links with normality." Escapism also manifested itself in lively discussions by contributors and correspondents of the changes in radio and electronics they hoped to see in the brave new post-war world. The phrase "after the war" recurred constantly.

Maintenance of interest in highquality sound reproduction was probably another manifestation of escapism. In this sphere an important war-time article was "The Acoustics of Small Rooms," by J. Moir. The kind of acoustics discussed by Moir had hitherto been studied mainly in relation to halls and large rooms.

In spite of restrictions, readers were kept fairly well-informed on the underlying reasons why valves were working better and better on everhigher frequencies by a series of articles by Dr. Martin Johnson.

Though censorship was quite different from that prevailing in World War I, it did in fact bear quite heavily on the contents of the journal, as most of the developments now emerging were being applied to purposes of war. Radar and everything

connected with it, especially pulse techniques, were completely banned. The authorities had taken us into their confidence about radar before the outbreak of war, so we knew what to avoid. There was a transient lifting of the veil of radar secrecy in 1941, mainly as an aid to the recruitment of civilian technicians, especially from America, but we were allowed to print only a few dozen words of basic description. One of the few electronics developments which could be treated at length was radio-frequency heating.

The fusion of the Institute of Wireless Technology with the British Institute of Radio Engineers and the deaths of Sir Oliver Lodge, of the German pioneer von Arco, and of Nipkow, the originator of television scanning were reported.



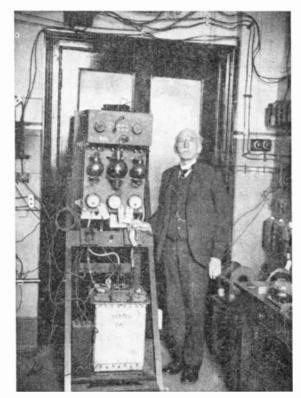
WITH the end of the war in sight, we were able to publish the first full article on the fundamental principles of radar. Appropriately enough, the



John Logie Baird, the pioneer of practical television, who died in 1946, aged 57.

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author was Smith-Rose, who, towards the end of World War I, had given our first detailed exposition of the amplifying valve. Pulse modulation, an offshoot of radar, was described later, as was the proximity fuse, "a radio station in a shell



Sir Ambrose Fleming, who died in 1945, aged 95.

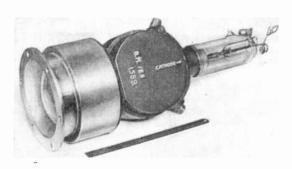
nose-cap," which made use of the Doppler effect. The fuse marked the start of the trend towards miniaturization of components, one of the features of the coming decade.

What may well turn out to be a strikingly accurate forecast of things to come was given in Arthur Clarke's article "Extra-Terrestrial Relays." Clarke contended that artificial earth satellites would provide the most effective and economical means for inter-continental telegraph and telephone communications and for distributing world-wide television. His proposals were described in considerable detail; their essential practicability has not been controverted.

1946

MUCH new information on radar was now published, but Wircless World considered it had come too late. Many of the devices, including some of essentially British origin, had already been described in American journals, and subsequently repeated in the technical Press of the world without emphasis on the country of origin. It was thought that British prestige

"The greatest invention of the war": cavity magnetron with a peak output of 2,500kW, photograph alongside a 6-in rule.



had suffered through these delays. The cavity magnetron, produced by Randall, Boot and Sayers was considered the most important single development.

Parts of the inner story of radar development were still coming out as late as 1952, when Government awards were made to the pioneers: £50,000 to Watson-Watt "for the initiation of radar" and other awards ranging from £12,000 to £250 to twenty others.

The Physical Society's first postwar exhibition in 1946 showed in an impressive manner how deeply radio techniques had infiltrated into most

branches of applied physics during the war years.

In brief: London television station re-opened; the Decca navigational system described; death of Baird, aged 57; the German Magnetophon tape recorder described.

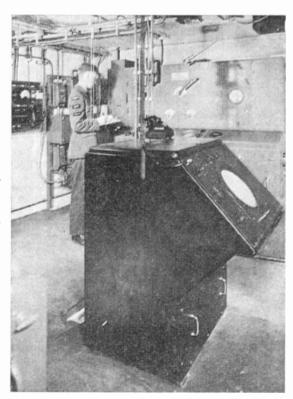
1947

THE first post-war Radio Exhibition gave a clear indication of how the industry had progressed during the past seven years. Equipment of every kind was better designed and better

The proximity fuse, "a radio station (sending and receiving) in the nose of a shell."



One of the first photographs of radar equipment to be released: an underground station for location of enemy aircraft and fighter control.



SINCE THE WIRELESS WORLD BEGAN—Continued

made, while the uses of radio and radio-like devices had been vastly extended, partly thanks to miniaturization and tropicalization. In communications, the greatest advance had been in pulse modulation techniques and in the attainment of a high degree of secrecy by the use of centimetric waves in narrow beams.

The Williamson amplifier design, published this year, seemed to satisfy the most exacting requirements of the "high-fidelity" enthusiasts and soon variants of it were to appear in many countries. It was the first design for home construction to exploit the use of direct coupling and meticulous design in the output transformer to reduce phase shifts and to enable a high degree of negative feedback to be used with stability.

The Marconi Company celebrated its 50th anniversary.



Sir Edward Appleton, whose pioneer scientific work paved the way for radar.



Sir Robert Watson-Watt who directed the initial investigations into the use of radio wave reflections for the location of aircraft.

1948

THE transistor, probably one of the half-dozen most significant radio devices of the half-century, was announced. What was now briefly described was the original point transistor produced by Shockley, Bardeen and Brattain in the Bell Telephone Laboratories.

The International Radio Convention, the first to be held since 1938, issued its decisions. Since the previous Convention in 1938, the highest frequency allotted had risen from 200Mc/s to 10,500Mc/s.

In brief: Appleton awarded the Nobel Prize for ionosphere researches; British sub-miniature valves, 10mm diameter, 25-mA filaments introduced by Mullard; frequency-shift keying now widely used for high-speed telegraphy; mobile radio licences granted more freely by the G.P.O.



AROUND this time there was much discussion of television standards. In the previous year the Postmaster-General had decided the 405-line British system was to be retained "for a number of years": later, an international study was made to decide upon the standards for the continent of Europe. Wireless World now decided the British system was even better than had been originally thought, being economical in both bandwidth and receiver cost. general adoption was therefore advocated and much information was published on line standards in relation to true definition in both horizontal and vertical planes.

In brief: commercial radar began to make spectacular progress; printed circuits were coming into the limelight; a new Wireless Telegraphy Act, extending the P.M.G.'s powers and allowing him to control interference, was passed.

1950

TELEVISION was now beginning to spread over the country and, as a result, the tunable receiver appeared. It was more usual, though, to provide interchangeable tuning units for the various channels. In anticipation of v.h.f. sound broadcasting, the provincial television stations were fitted



"There may possibly be a sufficiently conducting layer in the upper air...". Oliver Heaviside, the centenary of whose birth was celebrated in 1950.

with a superstructure carrying a slot aerial.

At the British Sound Recording Association's exhibition 33\frac{1}{2}-r.p.m. records (which had been exported for some time) made a first appearance. In addition to longer playing time they offered, thanks to the use of improved moulding material, lower surface noise, increased dynamic range and longer life.

In brief: centenary of Heaviside's birth; television boom in America (2½ million sets sold in 1949).

1951

WHAT amounted virtually to a new use of radio technique was now coming into prominence. As long ago as 1932 it had been known that radio waves were reaching this planet from outer space; in 1948, localized sources of emission, since known as radio stars, had been detected. Now radio astronomy-the use of the socalled radio telescope-was made possible by improved low-noise receiving techniques. The famous station at Jodrell Bank, with its huge steerable "dish," had already begun probing into space at distances far beyond the range of optical telescopes.

In brief: Interest in electronic computers began to widen; much discussion on frequency versus amplitude modulation for v.h.f. broadcasting; marked growth of mobile radio telephony, including installations in London taxicabs; tape recorders the centre of interest in sound reproduction.

1952

SOME of the exhibits at the Physical Society's annual exhibition showed how widely electronic techniques had now been adopted for "run-ofthe-mill" industrial processes, as opposed to their original laboratory uses. In the textile industry it was being used for measuring the tension of yarn and for showing irregularities in its weight per unit length. Supersonic waves were being used as a matter of routine for the detection of flaws and for determining thicknesses with high accuracy. Perhaps the most important of all was the growing use of electronic controls in the chemical industry.

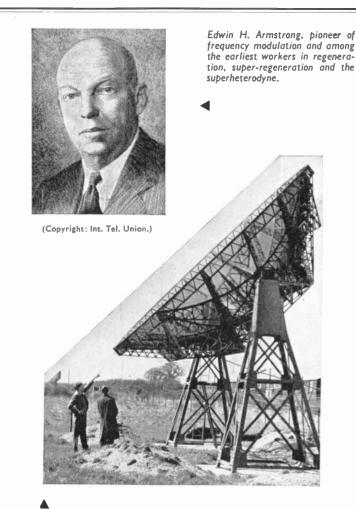
Detailed information came from the U.S. Bureau of Standards on "a new kind of v.h.f. propagation," later to be known as "ionospheric scatter." Weak but consistent signals on a frequency of 50Mc/s had been received over a period of many months at a distance of 774 miles. The power used was 23kW, the signals being radiated from a high-gain aerial set at an elevation angle of seven degrees.

1953

FOR nearly a quarter of a century there had been agitation for control by law of man-made interference with radio reception. In 1933 a committee had been set up at the suggestion of Wireless World to investigate the possibilities but the labours of that committee and of various successors had failed to produce an agreed basis for legislation. Now, at last, the Postmaster-General, using powers conferred on him by the Wireless Telegraphy Act of 1949, made a start by issuing regulations for the compulsory suppression of interference from newly-built internal combustion engines.

A minor difficulty in presenting information on a rapidly growing science is that the terminology, sometimes hastily and arbitrarily chosen, is often quickly out-dated by developments. One of the words about which ambiguity had long existed was "electronics." Transistors were now coming into general use and the fact was recognized by the addition of the words "and semiconductors" to the official definition.

In brief: The Coronation broadcast, the B.B.C.'s most ambitious undertaking, relayed on television to the Continent; 50th anniversary of the first international radio conference.



Radio-astronomy: two spaced paraboloids for producing a multi-lobed interference pattern (Cambridge University).



Interest in sound reproduction: G. A. Briggs' demonstration of comparisons between reproduced and "live" musical performances filled the Royal Festival Hall, London.

SINCE THE WIRELESS WORLD BEGAN-Continued

1954

WE had the sad duty of recording the death, by his own hand, of Edwin Armstrong, one of America's most distinguished radio pioneers. His most important work had been in the fields of valve regeneration, the superheterodyne receiver, super-regeneration and frequency modulation. He had been involved in much patent litigation. Only a few weeks before his c'eath Armstrong had written a lette for our correspondence columns 'to keep the history

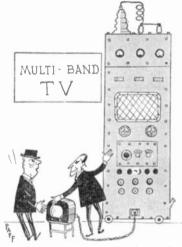
1955

NARROW-BAND ionospheric "scatter" transmission, first reported some years earlier, had now been tested up to ranges of 1,250 miles on the v.h.f. band. This year attention was turned to tropospheric u.h.f. scatter, offering ranges up to 200 miles with a much wider bandwidth. Both systems called for highly directional aerials and, between them, were thought to have a useful future for communication at ranges too long for normal v.h.f. and too short for

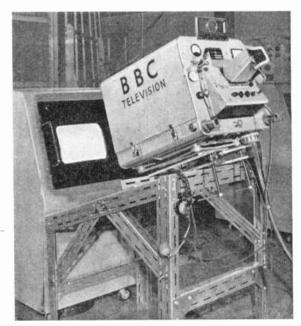
reliable high-frequency working. Electrostatic loudspeakers had hitherto been considered incapable of reproducing low notes. The description (by P. J. Walker) of a wide-range electrostatic speaker, working from 40c/s upwards, caused great interest.

"Automation," the witch-word of the year, enjoyed a short-lived vogue. Though there was some uncertainty as to its precise meaning it did clearly signify more work for industrial electronic control devices.

In brief: Atlantic telephone cable laid; B.B.C. started f.m. broadcast service.



No, Sir! This is the set and that is the converter. (Misgivings were being expressed about the technical difficulties of adapting existing television receivers for reception of the projected Band III service.)



B.B.C. equipment for converting the French 819-line pictures to the British standard.

straight" on the early development of the triode. Nobody, he contended, had made a serious study of how it worked until six years after it had been introduced.

Parliament passed an Act setting up the Independent Television Authority. As a result, there was a minor revolution in the design of television receivers, which in future would have to work on Bands I and III.

In brief: Printed circuit techniques now widely used; ferrite rod aerials in portable receivers; permanent "Eurovision" television links set up on the Continent; interest in highquality sound reproduction reached new heights.



Doppler navigation equipment (Marconi) in a Viking aircraft.

1956

BY now transistors had ousted valves in hearing aids and some all-transistor "personal portables" had appeared. But the transistor was still incapable of equalling valve performance at the higher frequencies and some of these sets had valves in the r.f. and i.f. stages, with transistors in the a.f. section.

For point-to-point radio-telegraphy the teleprinter had been steadily replacing older methods. Accuracy and speed had been progressively improved by refined and highly developed methods of "clean-

1957

THE terms psycho-acoustics and psycho-optics were by now becoming fairly familiar and it was real zed increasingly that the "classical mechanistic approach" d'd not provide solutions to all the problems of electrical communication. As Dr. Colin Cherry pointed out in an important article, that approach often ignores the real purpose, which is to transmit information from person to person. Chains of communication should sometimes be modified to suit psychological needs.

An exciting event was the recep-

World has through the years stuck closely to its last and, except when our specialized interests are directly affected, has taken little notice of the great social, economic and political changes of the half-century. We have, though, commented on the fact that the emancipation of women has had curlously little effect in technical radio, which remains an almost exclusively male preserve. This year we reported that Kathleen A. Gough had the distinction of being the first woman in nearly sixty years to be elected to full corporate membership of the I.E.E.

In brief: 1½ milion licensed stations in U.S.A. (against under 1,000 when we started in 1911), stereophonic reproduction commercially established.



Experimental tropospheric scatter station at Start Point: frequency 858Mc/s, power 10kW.

ing up" the received wave form. tion at many places in Britain of

We were able to take our courage in both hands and assert that the British television receiver was virtually standardized at last. "For the first time it is possible to put forward a general description of a receiver which will apply with remarkable accuracy to the great majority of modern sets." The "straight" r.f. amplifier had disappeared some years earlier and tubes were getting bigger; 17-in was now the most popular.

In br'ef: Decca introduced "truemotion" radar, Ampex television tape recorder announced; Shockley, Bardeen and Brattain awarded Nobel Prize for work on transistors. tion at many places in Britain of signals from the 1-watt transmitter in the first of the Russian artificial satellites.

In brief: Marconi Doppler nav gation system for aircraft described first British all-trans stor digital computer (Metropolitan Vickers).

1958

THE introduction of an experimental all-trans stor television receiver gave an indication of the notable advances in transistors, which could now work at v.h.f. and also deal with considerable power.

Generally speaking Wireless

1959

AN article on automatic error correction in multiplex teleprinter working showed in an impressive way how radio-telegraphy had been improved and refined during recent years. It was suggested that, on a poor "unprotected" circuit producing one error per hundred characters, the introduction of automatic repetition of detected errors might well reduce the error rate to one character in 10,000.

Within the short space of ten years the digital electronic computer had grown from a university or Government laboratory curiosity into a fully developed and engineered commercial product. So far most of them had been "scientific" computers, but machines for business data processing were rapidly emerging.

Two "quiet" microwave amplifiers, the maser and the parametric amplifier, were described. Both offered a solution of one of the most basic problems of radio—how to improve signal/noise ratio.

In brief: much discussion of stereophonic reproduction; B.B.C. serving 98.7% of population with television and 96.4% with v.h.f. sound.

1960

THE idea of radio communication via artificial earth satellites, which seemed little more than "a pleasant exercise in speculation" when first put forward by Arthur Clarke in our pages 15 years earlier, now began to look much nearer realization. The practical possibilities of using both

SINCE THE WIRELESS WORLD BEGAN-Continued



A. D. Blumlein whose early and thorough investigations of stereophonic recording and reproduction were "re-discovered" in 1958.

That and the control of the control

passive (reflecting) and active (retransmitting) satellites were discussed in an article by R. J. Hitchcock, who drew attention to the need for early international agreement on the allocation of suitable frequencies for the purpose, preferably in the band 2,000-6,000Mc/s.

Tribute was paid in an article by M. G. Scroggie to the memory of A. D. Blumlein, one of the most talented, versatile and prolific of British electronics technologists. During his tragically short working life of 17 years Blumlein was granted 132 patents—one every 46 days! "It is significant that the E.M.I. equipment of the Alexandra Palace [tele-

vision] station, almost every part of which owed something to Blumlein, made straight up from drawings to begin the world's first public high-definition service in 1936, was still in use in 1950."

The death of Dr. G. W. O. Howe severed a link with our earliest days, since when he had been prominent in academic wireless circles. For 30 years he had been Technical Editor of our associated journal Wireless Engineer (now Electronic Technology).

1961

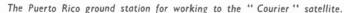
IT is easy enough to see in proper perspective the progress made during the first quarter-century covered by this survey and to say with confidence that at the end of it electronics technology was rapidly moving into Phase III, the era of highdefinition television, industrial electronics, microwaves and radar. Enormous advances have been made during our second quarter-century, but have we in fact moved into a distinctly new phase of development during the period? If so, when and why? Has anything been introduced to compare with such far-reaching developments of the 1911-1936 period as the amplifying/oscillating valve, the exploitation of the h.f. and v.h.f. bands, telephony, sound broadcasting and scientific electronics?

All those questions are more appropriate to a debating society

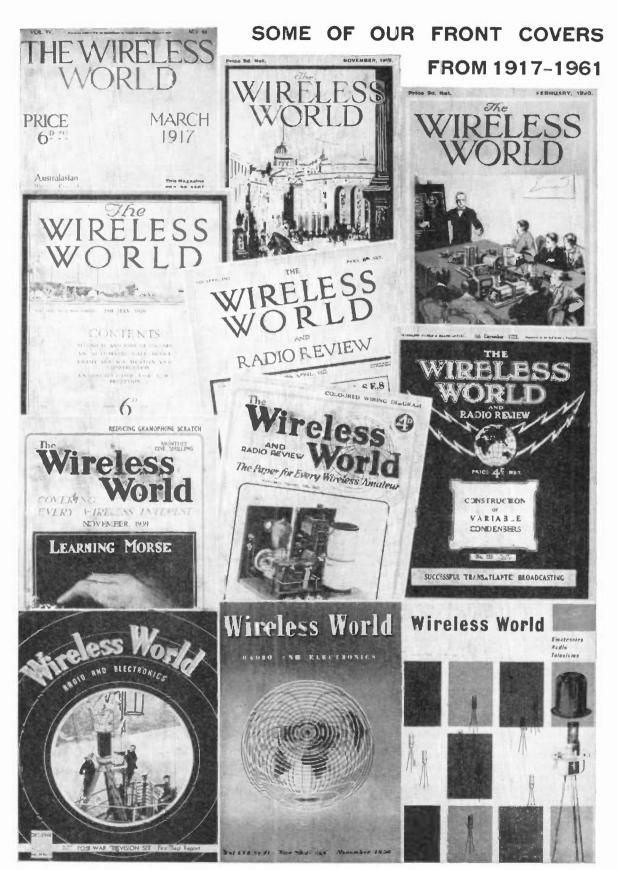
meeting than subjects for dogmatic pronouncements. It would be ridiculous to deny, though, that most of the techniques of 1936 have been refined almost beyond recognition and that many basically new things have come in. Of these, outstanding examples are transistors and masers, both of which depend on recent extensions of man's knowledge of the nature of matter.

Looking back over the longer term, it seems impossible to find a yardstick to measure the tremendous progress of the full half-century. Nearly all the activities with which we and our readers are now concerned had not even started when we began in 1911. A Rip van Winkle from our Volume I, resuming his readership during the past few months, would find most of our present contents entirely beyond his comprehension.

But our Rip Van Winkle of 1911 would discover one thing to seize upon. In his day, range of communication was the simple yardstick and the main criterion of progress; since wireless began each successive increase of distance had been a landmark. Remembering that Clifden, the wonder-station of his time, had just managed to achieve a dependable range of 2,000 miles, he would read with amazement of "successful communication out to a distance of 23 million miles" with a space vehicle. And would he be far from the truth in thinking that increase in range gives a fair measure of the achievements of the half-century?









Tape Cassette for the Blind

NEW "TALKING BOOK" MACHINE

Tape cassette in position on its playing deck.

AFTER a thorough field trial in one hundred blind person's homes, a new "talking book" tape cassette reproducer will be introduced in a few months by the Royal National Institute for the Blind. It is hoped that this new tape reproducer will completely replace the present talking-book long-playing record reproducers within the next few years.

Apart from the usual advantages that tape has over disc of being more durable and less easily damaged, for this particular application tape has the additional advantage of enabling the recording and copying to be carried out by the Institute itself rather than by an outside company, so that there is less delay in providing "readers" with their choice.

In the new tape reproducer the speech is recorded on 1-in tape using 18 tracks. Up to 1,500ft of tape can be used in one "book," giving a maximum total playing time of 20 hours. The tape, the take-up and supply spools as well as the replay head are all housed in a cassette. In use this cassette is simply placed on the deck so that it engages with the tape drive spindle and is connected via a jack plug to the replay amplifier and

The size of the whole cassette is kept down to only 8½in by 10½in by 2in by mounting the supply spool on top of the take-up spool. The tape passes from one side of the supply spool to the other side of the take up spool so that the tape which is momentarily on neither spool is slightly inclined to the horizontal. The tape is driven solely by the take-up spool which engages with the driving spindle when the cassette is placed on the deck: the supply spool is pulled round by the winding of the tape on to the take-up spool, the tape speed thus varies from about 3 to 7in/sec. This speed change does not alter the speech pitch since the recording is made with an equally-varying speed on the same cassette. The changing tape replay frequency response due to the same speed variation is compensated for by an opposite response when recording.

A recorded announcement indicates the end of each

A recorded announcement indicates the end of each track. The listener then simply stops the drive mechanism, turns the cassette over so that the full take-up spool becomes the new supply spool, and then restarts the drive to replay and the next tape track.

Two safety devices operate should the listener not switch off at the end of the track. First, the track end recorded announcement is followed by a high-pitch whistle. The replay head output produced by this whistle is rectified and then used to cut off a valve whose anode current flows through the hold-on solenoid of the motor supply switch. When the valve is cut off this switch thus opens and stops the tape drive motor. The second safety device operates in the unlikely event of this whistle switch-off arrangement failing. It consists

simply of a slipping clutch on the take-up spool which prevents the tape from being pulled off the supply spool. Spring-loaded pads bear on the tape on the spools to prevent tape spillage if the spools are inadvertently hand wound in the wrong direction.

A portion of speech can be repeated by turning the cassette over, playing a portion of the next track (which is equivalent to winding back a portion of the first track) and then turning the cassette over again to replay the desired portion.

The tape replay head is mounted near the middle of a lever which is pivoted at one end and fitted with cogged teeth at the other. These teeth engage a spring-loaded ratchet wheel so that, when a button is depressed, the wheel advances one step and the head is moved opposite to the adjacent track. This must be done every second time the cassette is turned over on the deck. The head can be returned opposite to the first track by a relatively simple adjustment which does not entail opening the cassette. This would normally be done when the "book" is returned to the library, but could be carried out by a skilled user.

This tape reproducer is a development of the model described on page 32 of the January 1954 issue of "Wireless World."

Novel Hearing Aid

USING A "WIRELESS" EARPIECE

TELEX in the United States have recently developed a new type of hearing aid, called "Telex Radiant," that is actually a transmitter and receiver built into a pair of spectacles. A miniaturized transmitter located in the temple bows accepts sound waves, converts them into electrical energy and transmits them through the air to the receiver located in the ear. The receiver picks up the signal, amplifies it, and converts it back to sound waves in the ear canal. The "Telex Radiant" uses six miniature transistors.



Pair of spectacles equipped with the "Telex Radiant" hearing aid. At the bottom left is shown the receiving unit: this is normally fitted inside the ear.

ENGLISH ELECTRIC' announce the first

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E.E.V. type	Approx linear capacitance sange (pF)	Shaft turns in linear capacitance range	Max peak r.f. voltage (kV)	Max r.f. current (r.m.s.) (A)	Max length (in)	Max dia. (in)
U30/15 U50/15 U80/15 U200/8 U200/10	5—30 8—50 16—80 5.5—206 5.5—206	10.4 10.4 10.4 17	15 15 15 8 10	10* 15* 20* 20- 20-	6.5 6.5 6.5 9.5 9.5	2.13 2.75 3.30 2.49 3.50

* Up to 30 Mc/s † Up to 20 Mc/s

ENGLISH ELECTRIC VALVE CO.

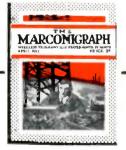
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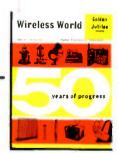
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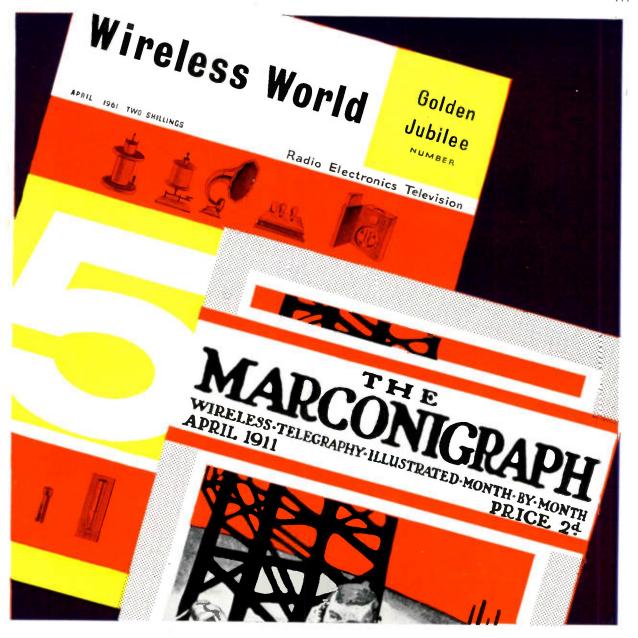
and the world of wireless were founded by

MARCONI

WORLD LEADERS IN EVERY BRANCH
OF RADIO AND ELECTRONICS







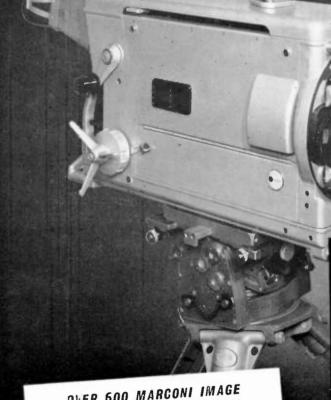
In April 1911, Marconi's Wireless Telegraph Company published the first edition of the 'Marconigraph'. In 1913 its name was changed to 'Wireless World' and its publishers to the Marconi Press Agency, which had been founded in 1910 to provide a fast news service by wireless telegraphy. In 1914 the agency's name was changed to Wireless Press Limited and in 1924 the Company's interest in 'Wireless World' was acquired by the present proprietors.

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THE MARK IV CAMERA CHAIN

EXPERIENCE COUNTS

Marconi's pioneered the use of the $4\frac{1}{2}$ inch Image Orthicon Camera using the tube developed by their associates, the English Electric Valve Company. Marconi's have amassed more 'know-how' on the use of the $4\frac{1}{2}$ inch Image Orthicon than any other manufacturer.



OVER 600 MARCONI IMAGE ORTHICON CAMERA CHAINS HAVE BEEN SOLD THROUGHOUT THE WORLD

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The 4½ inch Image Orthicon tube gives a picture quality substantially better than any other type or size.

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By reducing and simplifying the camera electronics its weight has been held below 100 lb. and its size made correspondingly small. 1. - BASIC DESIGN CONSIDERATIONS CIRCUIT DETAILS AND **PERFORMANCE**

By E. JEFFERY, A.M.I.E.E.

LOW-COST STEREO AMPLIFIER

OME years ago the writer published in this journal a design for a high-gain phase-splitting circuit which, using only two valve stages, provided a gain to either output terminal of approximately 1,000. As an illustration of the principles described an amplifier design was also given using KT.66's as triodes in the output stage. Although intended essentially to be a design article many readers chose to regard the amplifier as a high-quality system (we didn't use the term "high fidelity" much in those days*) as it gave a distortion harmonic content of less than 0.5%.

The phase-splitting circuit was later used fairly widely in commercial amplifiers, e.g. the R.C.A. Orthophonic, and has also been used in the design of industrial equipment. Mullard have published a "starvation" version of the circuit, whilst more recently in this journal³ and in Electronic Technology^{4,7} A. R. Bailey has evolved single-ended versions of the circuit for special purposes.

Principle of the High-gain Circuit.—G. W. Short has recently surveyed, very exhaustively, this and circuits of a similar nature, and it will only be necessary to restate the principles involved very

briefly.

Let us first consider the circuit to the right of A-B in Fig. 1; the stage V2 has the general configuration of a divided load phase-splitter, the anode load is R₃ and the effective cathode load consists of R₂ in parallel with R₁; since h.t.+ and h.t.- are at the same a.c. potential, it is immaterial from the point of view of V2 whether the point C of R_1 is returned to the positive or to the negative rail. Consequently, if the value of R₁ and R₂ in parallel is made equal to R_3 then, for a given impressed voltage between A and B, the output voltages V_{o1} and V_{o2} will be equal. There is no a priori reason why R_1 and R_2 should be made equal but the author chooses to make them so to make the sums easier because then $R_1 = R_2$ =2R₃ for equality of output.

From our general knowledge of such circuits we know that V_{o1} (= V_{o2}) will be slightly less than V_{AB}

since the grid-cathode voltage of V2 will be such that

 $V_{o2} = V_{AB} - V_g$.

If we choose a triode of the following characteristics for V2; $g_m = 8.5 \text{ mA/V}$, $\mu = 40$, $r_a = 5 \text{k} \Omega$ and make $R_1 = R_2 = 100 \text{k} \Omega$ and $R_4 = 50 \text{k} \Omega$, then V_{o1}/V_{AB} will be about 10 or V_g will be about 1/11 of V_{AB} . Now R_4 and R_5 are in parallel so that the effective

grid—cathode impedance $R_{\mathfrak{g}^{'}}=\frac{R_4.R_5}{R_4+R_5}$. The current

flowing through this impedance will be $i_{in} = \frac{\mathbf{v}_{g}}{\mathbf{R}'}$

and this current is supplied from the anode circuit of V1. Viewed from A-B, the input impedance will be V_{AB}/V_g or, in terms of V_g , this impedance will be $\frac{V_{AB}}{V_g}$. R'_g. We have already seen that $\frac{V_{AB}}{V_g}$ may be

about 10 (actually 11 in our calculated case) so that the effective impedance presented to the anode circuit of V1 is some 10 times the physical gridcathode impedance of V2.

The d.c. required for the anode of V1 sets a limit to the maximum permissible value of R4 and these d.c. considerations will usually fix R4 at a value from

 $100k\Omega$ to about $1M\Omega$.

In our practical case $R_4{=}\,820k\,\Omega$ and $R_5=2.2M\,\Omega$ so that $R'_g=598k\,\Omega.$ We have also seen that $V_{_{AB}}/$ V_a may be about 10 so that the apparent input impedance to the right of AB becomes of the order 10×598 k $\Omega = 6M\Omega$. As we have seen, this appears as the anode load to the pentode V1 and the value is in the same world as the a.c. resistance of the pentode. By this means we can realize a substantial proportion of the μ of the pentode as gain and since this μ may be very high (frequently of the order of × 5000) it is possible to achieve a gain of the order of 3000 to either output point, without much difficulty.

Even with separate valve envelopes for V1 and V2, the circuit offers substantial benefits of gain over any other similar arrangement: the recent introduc-

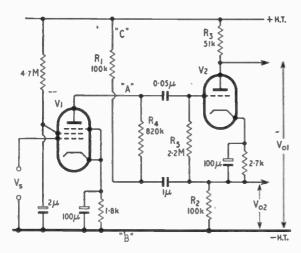


Fig. 1. Basic circuit of high-gain phase splitter.

tion of a suitable audio-frequency triode-pentode, the Brimar 6BR8, enables these benefits to be achieved in a single envelope. The values shown on the circuit of Fig. 1 do, in fact, relate to a 6BR8; with an h.t. supply of 300V the values shown give a gain of over 3000 times (to either output V_{o1} or V_{o2}). At 10V r.m.s. output the measured distortion was 0.6%. This distortion was almost entirely second harmonic in content. The a.c. and d.c. loads on V1 are very different and the circuit component values were therefore finally determined experimentally to give a reasonable compromise between the somewhat conflicting factors of gain and available output.

It will be seen that the circuit operates in a semistarvation condition which has the effect of raising the available μ considerably above the value given in the relevant application report; the makers characteristics for the pentode portion are quoted as $g_m = 5.25$ mA/V and $r_a = 500$ k Ω for a bias resistor of 80 ohms and a cathode current of 12.8mA. This gives a computed value of $\mu = 2600$, which is less than the gain which we can realize; it follows therefore that by operating the pentode stage in a lower current régime the available μ is significantly increased, in fact the anode current under our chosen condition of operation is less than 0.25mA. A circuit virtuoso could probably soar to even greater heights of gain in a cadenza on this theme.

In the practical application of this circuit some of the gain is deliberately thrown away in the interests of low frequency stability when negative feedback is applied over the whole amplifier, thus in the applied

version the bypass capacitor on V2 bias resistor is omitted.

Advantages of the Circuit.—It is, of course, easy to achieve the same total gain by other means using more stages but in addition to the obvious economy in valves and components there are substantial advantages to be obtained in achieving a large gain in as few stages as possible since this gain is thereby associated with a correspondingly smaller number of phase-shifting networks. This greatly simplifies the application of negative feedback over a whole amplifier system; in fact the real virtue of the circuit resides in this property and it is this which makes it most suitable for inclusion in a design which has to be constructed by readers who, for all I know, may not possess wide-range oscillators, phase-sensitive valve voltmeters, long persistence oscilloscopes or even transfer function analysers!

Comparison with Other Two-valve Phase-splitter Arrangements.—There are, of course, many other methods of connecting two (similar or dissimilar) valves in a phase-splitting arrangement; we must of course regard any two-valve combination in a single envelope as two valves for the purpose of the act.

The following table sets out the gains available with different valve combinations, for comparison purposes.

It is seen therefore that the circuit of Fig. 1 offers very substantial advantages of gain over any comparable arrangement.

Advantages of the Circuit for Stereo Use.—We have already seen that the circuit of Fig. 1 can save a complete valve compared with other methods of phase splitting, for equivalent gain; the saving of one valve has not tended to be a matter of prime importance in recent years but with the advent of stereo a possible saving of two valves becomes well worth having. It must be a matter of regret to manufacturers that only two channels were adopted for stereo but even so the ark-like need for two of everything is a strain on most pockets.

The high gain permits another substantial benefit, however. As designed, a gain of well over 2,000 is obtained from the phase splitter; if we use the circuit to drive EL84s which requires 8V r.m.s. grid drive, the input signal without negative feedback is some 3mV; when overall feedback of 20dB is applied the overall sensitivity is better than 40mV. This enables the relatively insensitive ceramic type of pickup to be fed directly into the main amplifier and, if desired, it is possible to dispense entirely with a pre-amplifier.

The author is of the opinion—and will no doubt live to regret it in the correspondence columns—

Valve Combination	Triode + Triode	Triode + Triode	Triode + Triode	Pentode + Triode	Pentode + Triode
Typical Valves	ECC83 (both sections)	ECC83 (both sections)	ECC83 (both sections)	EF86+ EF86 (as triode)	6BR8 (both sections)
Method of Connection	Triode amplifier + divided load splitter	See-saw	Schmitt (long- tailed pair) or cathode-coupled	Pentode ampli- fier+ divided load splitter	As in Fig. 1
Gain	54	62	27	200	3500

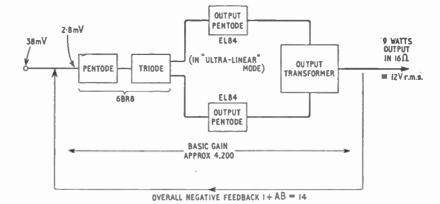


Fig. 2. Block diogram of either channel of stereo power amplifier.

that with a good pickup and loudspeaker system the modern pre-amplifier with its multiplicity of possible settings is more trouble than it is worth. One example has 14 panel controls alone, if we assume that a 2dB change of level is just discernible on the tone controls then there are some 1,200 possible combinations of tonal quality alone for a given volume, and the probability of the domestic user selecting the optimum setting is low. If any reader doubts this suggestion let him play the same record on different days and on the two occasions let him set the controls with his eyes shut; the comparison, even of volume setting, will be a little daunting. We also have it on the excellent authority of Mr. P. J. Walker that "With a very good loudspeaker it should seldom be possible to improve the balance professionally achieved at the transmitting studio." Even the impressive unit referred to earlier, which aims to be all things to all men, is not really complete as no provision is made for equalizing Edison Bell cylindrical records.

For those who do wish to have auxiliary bass and treble controls the amplifier sensitivity is sufficient to permit the insertion of passive networks between a crystal or ceramic pickup and the amplifier.

One final advantage associated with the saving of two valves is, of course, the reduction in total size, which can significantly affect the cost of the cabinet or enclosure required.

Design of a 9W+9W Amplifier

The circuit has been applied to the design of a 9W + 9W Stereo power amplifier using EL84s in the "ultra-linear" mode as the output stage, a block schematic of either channel is given in Fig. 2.

Although the output valves are nominally rated for 11 watts output the author has the same trouble as a previous contributor, G. W. Short, for whom circuits never do what the manufacturers or designers claim, and has, therefore, deliberately down-rated the amplifier output. He also holds another heretical

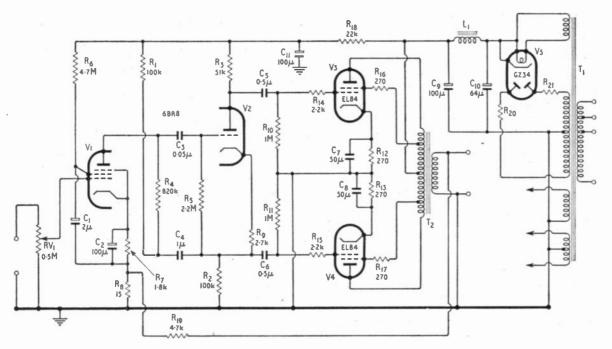
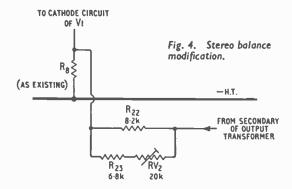


Fig. 3. Circuit diagram of either channel of power amplifier and power supply unit for both channels.

D



belief, that amplifiers should give something like the designed performance, even when only unmatched valves are available and without the need for setting phase-splitter balance controls.

The complete circuit for a single channel together with the power supply system required to serve

both channels is given in Fig. 3.

V1 and V2 constitute the pentode and triode sections respectively of a 6BR8 and as pointed out earlier the circuit differs slightly from Fig. 1 in that there is no bypass capacitor across the bias resistor of V2. In this form the gain of the phasesplitter from the V1 grid to either output grid, including the loading effect of the resistor R_{10} (or R₁₁) was measured to be 2,300, a number of prototypes produced values of gain within 10% of this value without any special precautions in the selection of components.

Overall negative feedback is derived from the secondary of the output transformer and applied through the feedback resistor R_{18} to resistor R_{8} in the cathode circuit of V1. The average overall gain of the system from V1 grid to the output transformer secondary load is some 4,200 so that, for a

feedback ratio
$$B = \frac{R_8}{R_8 + R_9} = \frac{15}{4,700 + 15} = \frac{1}{314}$$
, the

calculated feedback factor $1 + AB = 1 + \frac{4,200}{314}$ = 13.4 which is equivalent to 23dB. This compares very well with the measured value of 23dB.

Stereo Balance Arrangements.—A number of factors operate which can lead to an overall difference in the acoustical performance between the two channels, in particular:

(a) The ideal siting of loudspeakers may not be feasible in domestic surroundings.

(b) It is quite usual to create a stereo system from existing "bricks" and this may lead to the employment of loudspeakers which have different characteristics.

(c) There may be differences in the basic sensitivity of the pickup between the two channels. It is usual therefore to provide some method of

adjusting, on a pre-set basis, the balance, or relative,

gains of the two channels.

The best method of achieving this depends on the overall system chosen and therefore two alternatives are offered.

If no pre-amplifier is used.—In this case the control RV₁ and its counterpart in the RH channel will be two sections of a ganged volume control, and this control will be the main volume adjustment of the system. The balance control can then take the form of an adjustment of one of the channel amplifier feedback resistors. Since the range of adjustment is small (about 41dB) and since there is a generous margin of stability in the amplifier the adjustment needed makes no significant difference to the designed performance.

To provide the variation required the feedback resistor R19 on one of the amplifiers is replaced

by the arrangement of Fig. 4.

If a pre-amplifier is used the main volume control will normally be associated with the preamplifier so that the input volume control RV of Fig. 3, and its related component in the RH channel, will be redundant. Two methods of providing the stereo balance adjustment are, therefore, available:

- (a) An adjustment of one channel can be provided as shown in Fig. 4, in which case the input volume controls can be replaced by fixed resistors of say $1M\Omega$,
- the input volume controls can be replaced or (b) ganged logarithmic/antilogarithmic potentiometers following the 10% law. In this system the LH channel is connected to a logarithmic potentiometer reversed, and the RH channel is connected normally to antilogarithmic potentiometer as shown in Fig. 5. This method has the advantage that no internal modification to either amplifier is required and the insertion loss of the balance circuit at the midposition is less than 1dB.

The gain adjustment is then differential over the whole range of maximum to minimum, but in practice this wide range of adjustment can sometimes be an embarrassment and of course the cost of this type of control is considerably higher than the simpler arrangement of Fig. 4.

Power Supply Unit

The power supply unit is common to both amplifiers and consists of a standard mains transformer feeding a GZ34 rectifier operating in the capacitorinput condition.

Although in recent years there has been a tendency to adopt resistor-capacitor smoothing for small amplifiers, in this instance choke-capacitor smoothing has been adopted for the following reasons:

(a) The combined current of the two amplifiers is quite high (approximately 180mA) and common resistive smoothing would not be practicable.

(b) The regulation of the h.t. system is not significantly affected by drawing current for a pre-

amplifier or tuner unit.

A single heater supply has been provided to feed all valves in the main amplifiers (other than the rectifier). This supply is earthed on one side and there may be some further advantage, from a hum point of view, if a true or artificial centre tap were provided. A separate heater winding is provided for use with a pre-amplifier or tuner unit. If this supply is used alternatively for a pre-amplifier or tuner unit care should be taken to ensure that the earthing arrangements cannot lead to a short circuit, as some commercial f.m. tuners have internal earth connections to the heater circuit.

The h.t. circuit is capable of providing a current up to 20mA to a separate pre-amplifier or tuner. Any auxiliary unit should have its own adequate decoupling circuits to ensure that the overall system remains stable.

To simplify the construction of the amplifier all the smoothing electrolytic capacitors are provided in the form of two $64+100\mu F$ units. The $64\mu F$ portion of the can mounted in the LH portion of the chassis serves as the rectifier reservoir and the associated $100\mu F$ section acts as the choke filter capacitor. The other can provides the $64\mu F$ for smoothing to the early stages of the LH amplifier and the $100\mu F$ serves the same function to the RH channel. There is no significance in the difference in value, the selected components are combined in this particular way and there is no measurable difference in the 100-c/s hum level between the two channels of the amplifier.

Measured Performance of the Amplifier

The following measurements were taken on one channel of a representative prototype with the overall negative feedback applied.

Input Sensitivity.—38mV at 400c/s applied to the input produced 12V across a 16-ohm load connected at the output transformer secondary. Power Output.—With the conditions given in the foregoing paragraph, the 12V across a 16-ohm purely resistive load was equivalent to 9W power output. Distortion.—At 9W power output in the 16-ohm

Harmonic order	2nd	3rd	4th	5th	6th	7th	8th	9th
Distortion %	0.073	0.041	0.068	0.056	0.020	0.024	0.030	0.029

Total r.m.s. distortion 0.13%

load the following distortion products were measured (again at 400c/s input).

Gain Frequency Response.—The overall response was $\pm 1dB$ from 10c/s to 20,000c/s.

Hum Level.—The total r.m.s. hum level was 80dB down on maximum output.

Channel-to-Channel Crosstalk.—When measured with the input to each channel short-circuited, the channel-to-channel crosstalk at 400c/s was better than 74dB. At 1k/cs the crosstalk was 66dB whilst at 10kc/s a value of 48dB was measured.

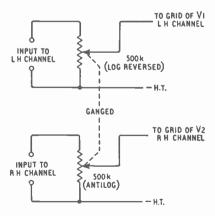


Fig. 5. Alternative stereo balance circuit.

Balance of Channel Gains.—The overall gains of the left-hand, right-hand channels with the gain controls at maximum were within ½dB of each other (this was also true when dissimilar transformers from different manufacturers were used in the two channels).

Additional Measured Data.—Other measurements taken, including internal measurements on the phase splitter and the overall loop gain characteristics, are given in Appendix I.

Comment on Measured Performance.—The measurements relate to a typical prototype; by selection of output valves and accurate adjustment of supply voltages it was possible to improve the distortion content to less than 0.1%, on the other hand the worst combination of available valves and output transformer gave 0.24% total distortion.

One of the most important features of any amplifier is its ability to perform adequately under conditions other than those obtaining in the closely controlled world of measurement. A. J. Kander suggests that all amplifiers should be stable under conditions ranging from half the nominal load impedance up to open circuit and also suggests that the amplifier should be stable with 0.1- μ F in shunt with the load. He finds, however, that many "amplifiers seen by the author have not been capable of meeting such a stability test." One famous amplifier at least is known to dislike

One famous amplifier at least is known to dislike the shunt capacitance of long loudspeaker leads and by the geographical limitations which stereo imposes it is often necessary for loudspeaker leads to run

considerable distances.

The present amplifier has, therefore, been checked for stability under the following load conditions:—

(a) A pure resistive load from zero to infinity (in fact the author uses an identical amplifier as part of a

power oscillator which is frequently fed into an open circuit).

(b) A number of loudspeakers of impedance from 3 ohms to 15 ohms, including units with built-in crossovers.

(c) A 15-ohm load shunted by a 0.5μF capacitor. The amplifier was found to be completely stable under all these test conditions. By using high-stability, close-tolerance resistors in the feedback circuits the gains of the two channels are very closely controlled (a maximum deviation of ½dB between prototypes was recorded). It is unlikely that the basic gains will need resetting as a 4dB change of internal gain results in an overall change of gain of only ½dB, such a change would normally be the symptom of some discernible catastrophic condition.

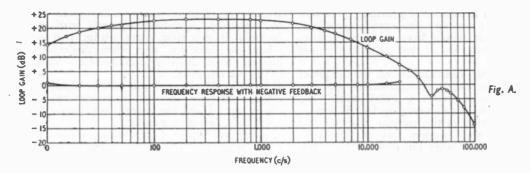
(To be continued.)

The next instalment will deal with constructional data, and will give guidance on various alternative input circuits including, where necessary, pickup equalizers and pre-amplifiers.

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- 1 "A New High-gain Push-pull Phase Splitter Circuit,"
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APPENDIX I

Additional Measurements on Stereo Amplifier.

- 1. The frequency response and loop gain characteristic of the amplifier are given in Fig. A.
- 2. Distortion before overall negative feedback is applied. Measured at 400 c/s with 12V r.m.s. across the 16- Ω output load.

Harmonic order	2nd	3rd	4th	5th	6th	7th	8th	9th
Distortion %	0.71	0.24	0.38	0.35	0.22	0.19	0.16	0.14

Total r.m.s. distortion = 0.98%

- 3. Sensitivity before negative feedback is applied. 1.09 mV input at 400 c/s gave 4.9V output. (i.e. overall gain at this frequency ≈ 4500).
- 4. Hum levels before negative feedback is applied.
 At 50 c/s 21mV or 55 dB below maximum output.
 At 100 c/s 7mV or 63 dB below maximum output. At 150 c/s 8.3mV or 63.5 dB below maximum output.
- Measurement of phase-splitter output.
 (a) Distortion at V3 grid with 12V output across $16-\Omega$ output load, at 400 c/s i.e. approx. 8 r.m.s. at grid.

4										
	Harmon order	i c	2nd	3rd	4th	5th	6th	7th	8th	9th
	Distortion	%	1.0	0.21	0.09	0.19	0.19	0.14	0.11	0.10

Total r.m.s. distortion 1.08%

(b) Distortion at V4 grid under conditions set out above.

4	Harmon order	i c	2nd	3rd	4th	5th	6th	7th	8th	9th
	Distortion	%	1.39	0.37	0.39	0.28	0.27	0.28	0.25	0.19

Total r.m.s. distortion 1.6%

(c) Grid-to-grid unbalance at 400c/s = 1.02%(This figure will inevitably depend on the resistor equality in the loads on V2.)

A note on a.c. voltage and harmonic distortion measurement. The author has noted a tendency to imply accuracies of a.c. measurement which are not realizable with commercial equipment, e.g., the excellent Avo Model 8 has an accuracy of $\pm 21\%$ of full scale on the a.c. voltage ranges and power measurements are therefore liable to a $\pm 5\%$

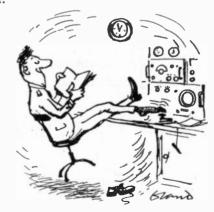
error. The best commercially available valve voltmeter claims an accuracy of \pm 1% (of full scale) although in fact the indicating meter fitted has itself this degree of inaccuracy. Elaborate precision laboratory equipment is needed to achieve better results than this. The author's distortion percentages are computed from ratios of fundamental and harmonic voltages and for this reason are liable to the errors of a.c. measurement.

"Wireless World" Books-New Editions

Principles of Transistor Circuits (2nd Edition) by S. W. Amos, B.Sc.(Hons.), A.M.I.E.E. The author, who is Editor of the Technical Instruction Section of the B.B.C. Engineering Department, has revised completely and brought up to date the first edition, incorporating six new chapters. Starting with a clear, simple exposition of the physical principles on which the operation of semi-conductor devices depends, a lucid and logical development leads to consideration of the factors affecting the use of transistors and other semiconductor components in equipment. Principles are illustrated by reference to typical circuit applications, including f.m. receivers and pulse techniques. The author's final chapter deals with some of the recently-developed devices such as the tecnetron, tunnel diode and controlled silicon rectifier. Pp. 211 with 125 diagrams; price 21s (by post 22s).

Learning Morse.—First published in 1939 and now in its 13th edition this guide to a mastery of the international telegraph code contains the Morse alphabet, numerals, punctuations and other commonly used signs. It explains how to hold and operate a telegraph key in the easiest way and contains a description of a simple transistor oscillator for practising and teaching the code. Included also is the revised "Q" code abbreviations approved at the 1959 International Radio Conference at Geneva. Pp. 20 with 7 illustrations. Price 1s 6d (1s 9d by post).

Both books are published for Wireless World by Iliffe Books Ltd., Dorset House, Stamford Street, London, S.E.1.



This method is not recommended in "Learning Morse."

International Semiconductor Symposium

Colloque International sur les Disposifs à Semiconducteurs-Paris, 20-25 February, 1961

RGANIZED by the Society of French Electronicians and Radioelectricians (S.F.E.R.) and under the patronage of the National Federation of Electronic Industries (F.N.I.E.) this colloquium followed the French Components Exhibition (in fact the two events overlapped by two days). More than 900 participants from all parts of the world attended. There were 140 lectures and discussions in three concurrent sessions, two in the UNESCO building and the third in the adjacent headquarters of the French P.T.T. Many supplementary discussion groups were organized spontaneously by specialists. The success of the symposium was proved by the attendance which was sustained to the end.

The main purpose of the conference was the exchange of ideas on the possibilities and limitations of semiconductor devices, and to promote a better undestanding of the ponts of view of manufacturers and users. To this end the papers were grouped under three main

this end the papers were grouped under three main headings, with various sub-divisions. (The figures in brackets indicate the number of papers in each section.)

Production. H.F. transistors (11); power transistors (6); miscellaneous transistors (6); p-n-p-n diode and triode switching devices (5); tunnel effect devices (7); parametric diodes (3); photo-diodes, solar cells (7); thermo elements (7); miscellaneous techniques (7); miscellaneous devices (8)

cellaneous devices (8).

Applications. Thyratrons (8); pulse circuits (9); amplifying and oscillating circuits (10); "equipments" (4); measurement (7); micro-electronics (4); tunnel diode applications (6); new devices (4).

Reliability. General (4); physical data and tech-

nology (7); methods of measurement (5).

Inevitably in such a rapidly developing subject as semiconductors, rigid classification was impossible and many papers seemed to sit uneasily in the sessions to which they had been assigned. The following notes are intended to give an impression of some of the highlights rather than a balanced survey of the conference, for which prolonged study of the published papers and discussions will be necessary.

All lectures containing any reference to mesa structures or to epitaxial techniques (the growth of very thin layers of high resistivity material by vapour deposition in which the new layer continues the crystalline alignment of the substrate) were well attended in the hope that something might be disclosed in the way of new manufacturing recipes and "cooking." Undoubtedly the customers learned much, but some of the "chefs" to whom we spoke did not think that their colleagues had been particularly communicative. Undoubtedly a lot of work is being done in gallium arsenide and other intermetallic compounds for use in transistors and diodes but much of this is clearly of an experimental nature and there are as yet no signs of their general adoption in production. Sintered semiconductor thermo-elements are not isotropic according to M. Alais and G. Fournet (Soc. Alsacienne de Constructions Mécanique) who showed that the figure of merit, as defined by thermo-electric power and thermal and electrical conductivity, is greatest at right angles to the direction of application of pressure during the forming process. Double-diffused transistors of the planar (as distinct from the mesa) type were reported by V. H. Grinich (Fairchild Semiconductor Corp.) in which the active base region is limited by masking with a film of silicon oxide using a photo-lithographic process to define the surfaces exposed for treatment. After diffusion all

the exposed surface is completely re-covered by a regrown SiO, layer which prevents contamination and gives mechanical protection when the transistor is en-capsulated in "micro" circuit elements. A comparable technique was described by Fromageot, Michelet and Saintesprit (Lignes Télégraphique et Téléphonique).

Among special-purpose junctions the most interesting were those designed for the detection of nuclear radia-These give rise to electron-hole pairs in the depletion layer and a ray counter junction of n-i-p type, described by Mme L. Koch and J. Messier (Centre d'Etudes Nucleaires de Saclay) has made possible the detection of individual gamma rays. Modification of the collector junction reverse current in l.f. transistors (e.g. OC72) due to flaws in the material has been used by J. Bok and R. Schuttler (Centre d'Etudes Nucleaires à Fontenay-aux-Roses) to measure neutron flux. Irradiated transistors of this type can be used to measure gamma radiation in the presence of neutron fluxes below that of the maximum irradiation.

Germanium grain boundary photocells of high sensitivity and extremely small size (smaller than a light spot can be focused) were described by Dr. H. A. Schell (Te-Ka-De), and field effect transistors utilizing grain boundaries and having a negligible temperature coefficient at low temperatures were discussed by H. F.

Matare of the same company.

The papers on micro-circuit techniques were well attended. A somewhat more sober approach, with a revision of early astronomical estimates of packing densities for components, was evident; no answer was forthcoming to the problem of interconnecting microunits in large and complex combinations. Research on the simulation of inductance by impedance inversion and multiplication by means of diode and transistor circuits was reported by Nishizawa, Kojima and Yoneyama (Tohoku University, Sandai) who have obtained stable impedances equivalent to 1H and 100 µF. The importance of these devices, which do not involve magnetic fields, and therefore unwanted couplings, in micro-circuits are obvious. The future of micro-circuits and indeed of the extension of semiconductor techniques in general towards higher frequencies and faster switching times seems now to rest with tunnel diodes which are cheap to produce, have fewer connections and are therefore more reliable, and are immune from surface effects and more suitable for encapsulation in microcircuit modules.

The symposium was honoured by the presidency of Prince Louis de Broglie who, in his opening address, traced the development of atomic physics and its bearing on semiconductor theory with the lucidity and simplicity which is characteristic of the greatest scientific minds. Cogent speeches were contributed to the opening session by M. R. Gueur (chairman of the organizing committee), M. Jeanneney (Minister for Industry) and General Guerin (chairman of the S.F.E.R.) who described the recent rate of development as "explosive," the result of a "chain reaction between research and application in industry." application in industry.

In the space available it has been possible to touch only on some of the highlights of the symposium, but the full proceedings will be printed and will be available to non-participants in two or three months' time from the Société Française des Electroniciens et des Radioélectriciens, 10 avenue Pierre Larousse, Malakoff (Siene), at a cost of about 150NF (£11).

LETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

Bootstrap Follower Amplifier

In the January issue of *Electronic Technology*, W. Tusting gives an interesting theoretical analysis of the low-frequency response of this type of circuit. If the lower coupling capacitor (C₃ in my Fig. 9, p. 79, February Wireless World) is very large compared with the upper one (C₂), then the l.f. response of a typical circuit is similar to that of a normal amplifier with one RC coupling. Mr. Tusting says that, generally speaking, it will suffice to choose the main coupling (C2R6) so that it alone will give the required response, and then make the lower capacitor about 50 times as big as the upper one. This looks like a useful rule of thumb. It may seem surprising that it is necessary to choose C2 and R_{δ} so that they will give the required response in the absence of any impedance multiplication. When C_3 is large enough R_{δ} is effectively returned to the cathode of V2, however, and because of this the time constant C2R6 is unaffected by feedback.

If the lower capacitor is appreciably less than 50 times as big as the upper, a step appears in the l.f. response. In the example given, the response levels out after an initial drop of about 7dB, remains level as the frequency is reduced, then falls again, at very low frequencies. This type of response is undesirable in a straightforward amplifier, but Mr. Tusting points out that it may be useful in a negative feedback amplifier because the l.f. phase shift is less than that of the ordinary

RC coupling (C_2R_b) alone. The writer has confirmed the existence of the step in the l.f. response by experiment.

G. W. SHORT. Croydon.

THIS circuit has received considerable attention from the technical press this year, and additional analytical treatment appears in *Electronic Technology* (January 1961), as well as in the January and February issues of this journal. However, I find it difficult to accept certain explanations of its behaviour.

First, a.c. coupling to the cathode follower is not essential. Secondly, the high input impedance of the cathode follower is not primarily responsible for the substantial increase in gain of the pentode. I would suggest that the bootstrapping is merely a form of positive feedback, or servo assistance.

It is well known that if the anode load of a pentode

valve be progressively increased the gain ceases to rise appreciably because of the fall in anode current, and mutual conductance. The h.t. supply has to be progressively increased to avoid this effect which is frequently uneconomical, and moreover the valve ratings may be exceeded. In the bootstrap circuit the cathode follower regulates the h.t. supply to the pentode (junction of R_{LP} and R_{LC}) at signal frequency and in phase with the output of the pentode. This may be regarded as positive feedback, and the cathode follower is able to do this because of its low output impedance.

The accompanying circuits illustrate these points and a circuit which I have used for some time. It yields a gain of 2,500 with complete reliability. Other readers may be interested to know that this type of circuit has also been discussed by Mr. A. W. Keen in a paper entitled "Bootstrap Technique" (Electronic & Radio Engineer,

Sept. 1958).

An EF86 and half a 12AT7 in one envelope would be very useful in low level audio circuits because the signal-to-hum ratio would be superior to the 6BR8.

It has, like the cascode amplifier, the advantage of high gain with a single phase inversion, but in contrast a lower output impedance. For this reason the circuit may also find application as a time base or shunt amplifier circuit in an h.t. stabilizer.

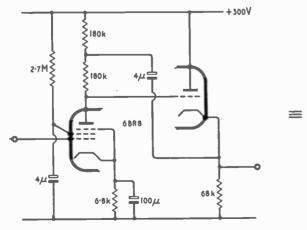
I. R. OGILVIE. Sevenoaks.

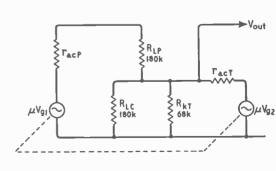
The author replies:

It is certainly possible to regard the bootstrap follower as an amplifier containing a positive feedback loop. This does not clash with the approach used in my article: it leads to precisely the same results for the overall performance of the circuit.

Personally I prefer not to stress the positive feedback, because there is also a negative feedback loop, and, with resistive circuit components, the negative feedback always predominates. It is impossible for the positive feedback to make the circuit unstable, because the most it can do is to counteract the negative.

It seems simpler to treat the circuit just as a "circuit," without harbouring any preconceived notions about it, than to begin with the assumption that the triode is a true cathode-follower with 100% negative feedback, and then allow for the effect of the reduction of this negative feedback by the potential divider in the triode grid circuit. (Or, taking Mr. Ogilvie's standpoint, to allow





WIRELESS WORLD, APRIL 1961

for the application of positive feedback by the same means.)

Mr. Ogilvie's circuit uses the same type of interstage coupling as my experimental phase-splitter (February issue, p. 82, Fig. 17). It is gratifying to learn that he has found it completely reliable. He does not, however, say anything about the frequency response of his single-ended high gain circuit. The amplification factor of the 6BR8 pentode is 2080 (with $I_n = 10$ mA) so his circuit must be operating near the performance limit!

G. W. SHORT.

Aerial Models

IN his article entitled "Practical Aerial Measurements" in the December, 1960 issue, Mr. F. C. Judd includes many useful points of practical nature. It may be helpful to add certain others which have arisen during the installation of a similar aerial model table at the Royal

Military College of Science.

The reciprocity principle implies that the radiation pattern of an aerial system is the same for transmission and for reception. One may, therefore, use the model aerial either as a transmitter or as a receiver. The first alternative demands and r.f. coupling between klystron and aerial to permit continuous rotation through 360°; whereas if the model aerial is used as receiver, the crystal diode may be built into its base and simple slip rings may be used to pass the a.f. modulation to the subsequent amplifying stages.

When the author refers to "the use of scale models... for determining performance under working conditions," his definitions of "model" includes not only the correct scaling of the aerial under test, but equally faithful reproduction of site obstacles, as shown in the photograph at the foot of page 581. Three points arise in this context, which must be borne in mind in determining the construction and the dimensions of the "V" frame carrying (in Mr. Judd's case) the receiving aerial:

(i) The use of a nearby receiver implies spherical-wave rather than plane-wave geometry, and if the resulting phase discrepancies are to be kept below 45°, the receiving aerial must be at a distance greater than a^2/λ from the nearest point on the model, where a is the width of the complete model (i.e., the test aerial together with the site obstructions).

(ii) The receiving aerial must itself have a radiation pattern sufficiently uniform to "see" the complete model; otherwise reflections from site obstructions near the extremities of the model will be unduly

attenuated.

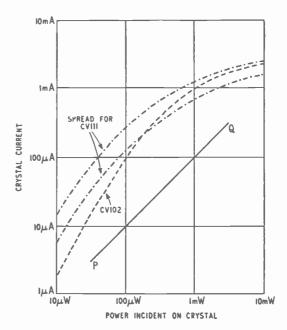
(iii) The "V" frame itself should be constructed in such a way as to minimize additional reflections from its legs. We have used legs of triangular cross-section and have coated their inclined surfaces with Aquadag; thus reflection from the frame legs is not only cut down in amplitude but is also directed away from the receiving aerial.

For his receiver, the author uses a simple crystal-audio system, but we have found this technique to be inadequate for a very fundamental reason. One normally assumes square-law operation for the receiver crystal and, therefore, regards the crystal current reading (after appropriate amplification and demodulation) as a direct measure of received power. Unfortunately crystal performance checks show that this law does not hold good over the 20dB range which is essential if one is to evaluate satisfactorily the side lobes of many practical aerials.

The accompanying figure shows readings taken on a batch of five CV 111 crystals newly drawn from store. The scales are logarithmic, so that a square law would appear as a straight line parallel to the line PQ. Even greater departure from square law behaviour was found in the case of CV 102 crystals which had been in use for

several months.

Errors arising from this cause may be avoided by operating the crystals at a fixed power level, and two methods have been widely used to accomplish this. In



the first, a piston attenuator adjusts the transmitter output so that the received power always remains at a fixed level. Such an attenuator may, indeed, be servo-controlled from the receiver, the driving shaft being coupled to a pen recorder to facilitate automatic operation. Alternatively, normal superheterodyne techniques may be used, with a second klystron serving as receiver local oscillator.

The power incident on the crystal remains effectively constant, provided the local oscillator delivers a signal substantially greater than that picked up by the receiving aerial. One may either feed the receiver output to a normal p.p.i. display to permit inspection or photographic recordings, or one may meter and record receiver output in the normal way.

Frincipal Lecturer,
Principal Lecturer,
Radar & Telecommunications Branch,
Royal Military College of Science.
Shrivenham, Wilts.

Transatlantic Radio Telegraphy

NO doubt A. M. Humby is right in saying (March issue) that the long-distance l.f. stations, even when at their zenith in 1924, never managed to carry more than a very small proportion of world traffic. But I think he does rather less than justice to the pioneer stations Clifden and Glace Bay which, 50 years ago, maintained what appears to have been remarkably consistent transatlantic communication.

A tribute to the service was paid in 1912 by an apparently satisfied user, the New York Times, which was then receiving its European news telegrams, running at about 25,000 words weekly, by the Clifden—Glace Bay route. Refuting allegations by a cable company that the news was so much delayed as to be no longer "live," the New York Times issued a table showing average delays of under two hours*. Much of that delay was ascribed to the long and indirect landlines but, even so, results compared well with the cable service.

The Clifden circuit was still without a long-range rival in 1913, when the Government-appointed Parker Committee reported "practically continuous" communication.

Chichester, Sussex.

H. F. SMITH.

^{*} See The Marconigraph, April, 1912, p.23.

Paris International Sound Exhibition

NEW LOUDSPEAKER DEVELOPMENTS

NE of the characteristics of the third International Sound Festival held recently in Paris was the considerable support given to the organization of stereo and other demonstrations by Radiodiffusion-Télévision Française. Foreign radio organizations from Italy, Holland and Switzerland also took part

and Switzerland also took part.

"Foreigners" were also well represented among the exhibitors, although in this case the "foreigners" were mainly British. In fact, of the total of forty-three stands, eleven formed a joint British section organized by the Audio Manufacturers Group of B.R.E.M.A. and paid for by the Board of Trade. British equipment was also shown in several cases by its French distributors.

As it happened, almost all the unusual items we noted were in the fields of loudspeakers or amplifiers, and so we are confining this report almost entirely to these two fields.

Mention should however be made of the Frei "Echolette"—a compact device for producing artificial reverberation effects which was shown by Lyrec. This device uses an endless band of magnetic tape in association with three record and two replay heads. These may be used to produce single echos with several delay values lying between about 0.05 and 1 sec. By combining a number of such echoes at various levels, artificial reverberation effects may be produced.

LOUDSPEAKERS

Perhaps the most interesting exhibit was the Orthophase loudspeaker shown by Ge-Go. This might be described as a modernized version of the Blatthaller loudspeaker developed in the nineteen twenties. In both cases a number of long magnets placed side by side are used. In the long magnet gaps lie corresponding long driving conductors: adjacent conductor ends are joined so as to form a single zig-zig shaped conductor. This driving conductor is distributed over the diaphragm so that this latter (as in electrostatic speak-

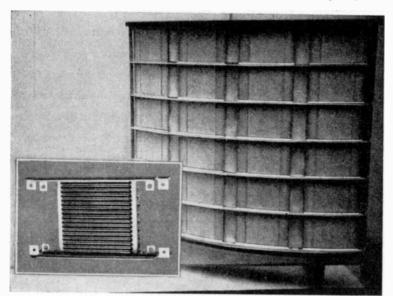
ers) is driven over the whole of its area. The Orthophase loudspeaker uses a foam plastic diaphragm which is flat on one side and ridged on the other. To the ridges are attached the light-metal ribbon driving conductors and these lie between the pole pieces of a set of ferrite magnets (see diagram).

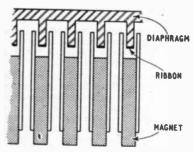
Seventeen magnets and driving ribbons distributed evenly over an area of four by five inches form a single cell unit, and any number of such units may be combined as required. The high-frequency res-

ponse of each cell extends within 2dB to 25kc/s—the low-frequency response extends (also within 2dB) to 1kc/s or lower, depending on the total cell area in use and how the cells are loaded acoustically. intermodulation distortion is claimed to be less than 2% at 5 watts output (for each cell). A square wave reproduced by this loudspeaker bears a considerable resemblance to the original: readers who have seen oscillograms of square waves as reproduced even by high-quality conventional moving-coil loudspeakers will know that this is a remarkable achievement. Each cell has a directional characteristic covering an angle of 30° at 15kc/s (for 6dB down). The fundamental resonance is at 40c/s and the diaphragm can move up to one quarter of an inch. The efficiency is somewhat below that of a conventional moving-coil loudspeaker and the impedance of each cell is 0.35Ω .

A private demonstration was given of a 24-cell full-range free-standing version of this loudspeaker. 30in/sec master tapes (with obviously a very-close microphone recording technique) produced some of the most "immediate" sound your reporter has ever heard. No distortion could be detected, and the bassdrum appeared to be reproduced accurately in that it was partly heard and partly felt.

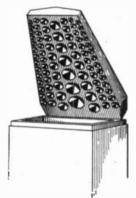
Another unusual type of loudspeaker was introduced by Philco International. This used "exploded"





Free standing 24-element Orthophase loudspeaker with (inset) rear view of a single element and (above) diagram showing the construction of one element.

polystyrene as a diaphragm material in order to achieve a high stiffnessto-weight ratio and thus reduce breakup. Although driven normally by a centrally attached voice coil, the diaphragm was unconventionally shaped-convex rather than concave and saucer- rather than cone-shaped. The diaphragm thickness also varied considerably from about 4in at its centre to only about 0.2in at its rim. This rim was suspended by means of special rubberized linen so as to eliminate reflections at the diaphragm edge. The diaphragm was also suspended in various other places, not disclosed. The resonant frequency of this loudspeaker is only about 10c/s in free air: when mounted in its totally enclosed cabinet, the enclosed air stiffness increases this frequency to about 40c/s. The cabinet volume is less than 2 cu. ft. It



Reflector used in one of the Andre-Radio "Clevox" range of loudspeakers. The conical indentations resonate at different frequencies to correct for deficiencies in the treble response of the loudspeakers.

is claimed that this diaphragm does not break up below about 2000c/s frequencies above this value are reproduced by a capacitive-fed conventional pressure-driven tweeter.

A high stiffness-to-weight ratio can also be obtained for the diaphragm by making it in sandwich form with the skin material denser and stronger than the filler, as described by D. A. Barlow in our December 1958 issue. The production version of a sandwich cone loudspeaker was shown by Leak. Unlike the prototype first shown at the 1959 Northern Audio Fair, this is associated with a conventional 3-in cone tweeter loudspeaker (crossing over at 1kc/s) rather than an electrostatic unit. Cabinet resonances are, it is claimed, almost completely eliminated by means of a new damping material.

A range of unusual column-shaped loudspeaker systems—the Clevox was shown by Andre-Radio. Each column contains a number of irregularly positioned flat baffles proFrei artificial reverberation device using an endless loop of magnetic tape (shown by Lyrec).



truding from the interior of its walls. These baffles both increase the effective column length (by forcing the sound to follow a longer path) and, it is claimed, effectively provide a number of pipes of different lengths and thus produce resonant loading over a considerable frequency range. An unusual reflector is also mounted

above the speaker at the top of each of these columns. The surface of each such reflector is indented with a number of conical depressions of different sizes. These depressions resonate at different frequencies to compensate for deficiencies in the high-frequency response of the loudspeaker.

AMPLIFIERS AND PRE-AMPLIFIERS

Two unusual features noted in Gaillard equipment were, in their "Europe" amplifier, a separate ECL82 output stage for feeding an electrostatic loudspeaker with frequencies above 10kc/s and, in their Himalaya amplifier, a voltage-stabilizing circuit (using a 6BQ7A double-triode) for counteracting mains supply variations (these are proportionately greater in France than England).

The Ribet Desjardins "Mozart" stereo radio-gram is unusual in that a single power amplifier is used for frequencies below 300c/s, and two separate power amplifiers for frequencies above 300c/s.

A fully transistorized pre-amplifier and 2×5-watt amplifier formed part of the S.P.E.S. "Monteverdi" stereo sound reproducing system. The amplifier response is claimed to be

within 2dB from 20c/s to 50kc/s with overall feedback of 28dB.

The Innovation demonstration featured a number of American units which, so far as we know, have not vet been exhibited in England. This enabled one to get an idea of some of the more unusual (dare we say exotic) facilities often available in American equipment. For example, a Marantz pre-amplifier could compensate for five different low-frequency and (independently) five high-frequency different record characteristics. In the corresponding power amplifier, the bias of the output stage as well as its d.c. and a.c. balance could be monitored and adjusted. The output valves could be operated either as triodes or in an "ultra-linear" connection and the damping factor of this amplifier could also be varied.

Digital Computer Kit

The Nash and Thompson transistorized kit shown in the photograph enables complete computers to be built directly from schematic diagrams and is suitable for educational or training purposes. The individual sub-unit "brickettes", which are also available separately, include AND gates, OR gates, inverters, delay units, flipflops and power packs. The majority af the units have emitter-follower outputs so that several units can be connected directly to one output.



Elements of Electronic Circuits

24.—Delay Circuits

By J. M. PETERS, B.Sc. (Eng.), A.M.I.E.E., A.M.Brit.I.R.E.

DELAY circuit is one which is arranged to allow the passage of a period of time after the application of an input before an output appears. This property enables it to be used in a variety of roles which are principally:-

(1) To act as a delay or store for pulses in computers so that slow-acting circuits can be permitted to operate.

(2) To generate rectangular pulses.

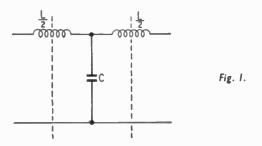
(3) To duplicate an existing pulse at a later time. Naturally, trigger circuits can be used to produce delays; however the output from these is synthesized and not the original input delayed: in a true delay circuit the input re-appears as the output after the passage of time.

Various forms and modifications of transmission lines are commonly used as delay circuits and an explanation of the properties of transmission lines will assist the reader in following and understanding

their operation.

Properties of Transmission Lines

We will assume that L, R, C and G represent the inductance, resistance, capacitance and leakance* of the line per unit length (metre). If the line is uniform and lossless i.e. $\omega L \gg R$ and $\omega C \gg G$



then a travelling wave of any shape will move along the line at a uniform velocity without change of shape: if this line is infinite the input impedance is constant and is not affected by the type of waveform applied. Also if the line is of finite length, but properly terminated, the line will appear to the generator to be infinite and the properties of the infinite line will still obtain. An improper termination will cause a reflection and the interaction between incident and reflected waves will create a change in input condition; this effect is used in the generation of rectangular pulses.

Characteristic Impedance.—Still assuming that the line is uniform and lossless, for a travelling wave at any point in the line the ratio (change in voltage)/ (change in current) is constant and is equal to

*Leakance, a term meaning shunt conductance, i.e. the reciprocal of the insulation resistance of the line.

 $\sqrt{(L/C)\Omega}$ which is known as the "characteristic impedance" of the line (this ratio implies that the voltage and current are in phase with each other). For our hypothetical ideal line the characteristic impedance is a pure resistance denoted by R₀; but for the general case of a line which is not loss-free, the expression for characteristic impedance is complex and introduces the terms R and G: this is usually referred to as Z_0 . Another name is the "surge impedance" of the line.

Parallel-Wire Line.-For a balanced line, that is, one formed of two parallel wires, L and C depend on the dimensions of the conductors, their separation and the characteristics of the material between them. If we embed the conductors in a material which has a dielectric constant, «, different from air this will alter the characteristic impedance, the formula for which can be reduced to:-

 $Z_0 \approx (276/\sqrt{\kappa}) \log_{10} (d/r) \Omega$ where r = radius of the conductor, d = spacing between conductors and $d \gg r$.

Coaxial Cable.—The coaxial or unbalanced line is made up of a central conductor surrounded by dielectric sheathed by an outer earthed screen. The expression for Z_0 is of similar form and can be reduced to:-

 $Z_0 \approx (138/\sqrt{\kappa}) \log_{10} (r_2/r_1) \Omega$ where r_2 is the internal radius of the outer conductor and r_1 is the radius of the inner conductor.

Losses.—As the frequency is raised both the resistive (R) and dielectric (G) losses increase. It may seem odd that the resistance of a piece of wire can vary with frequency; but a phenomenon known as the "skin effect" occurs. This, as its name suggests, is the confining of the current to a thin layer at the surface of the conductor. The "inside" of the wire carries no current and can even be removed, leaving a tube.

Transmission Delay

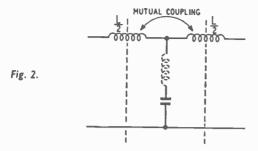
The velocity of propagation along the loss-free line is $1/\sqrt{LC}$ representing a delay of \sqrt{LC} sec/metre. For a uniform open-wire line in free space (strictly, in a vacuum) which does not dissipate energy, L and C are so related that their product is equal to the speed of light $\approx 3 \times 10^8$ metres/sec so that the time delay on an ideal line of this sort is $1/(3 \times 10^8)$ $0.003\mu sec/m$.

In practice the conductors are usually separated by a dielectric other than air. The general expression for the speed of an electro-magnetic plane wave

 $v = c/\sqrt{\kappa\mu}$

where c = velocity of light, $\kappa =$ dielectric constant, μ = magnetic permeability of the dielectric which in practice can be taken as unity.

The time delay is therefore $0.003\sqrt{\kappa(\mu\text{sec/metre})}$.



A characteristic often quoted by cable manufacturers is "velocity factor"—this is the ratio between transmission speed in free space and in the cable.

Delay Times and Types of Line

For delays as short as $0.005\mu\text{sec}$ it is usual to use coaxial lines where $\kappa \approx 2.5$ (e.g. $0.003\sqrt{2.5} \approx 0.005\mu\text{sec/m}$). Longer delays entail what is usually an unacceptably long coaxial line; however by increasing the length of the inner conductor (by winding it into a spiral) it is possible to obtain delays of the order of $1\mu\text{sec/metre}$. Some special cables use a magnetic material to further slow progress of the wave. The characteristic impedance of these modified lines is usually high and for time delays of this order it is often necessary to resort to artificial lines.

Lumped-Constant Lines.—Artificial lines comprise a number of low-pass filters connected in series. The filter section possesses a delaying characteristic; hence it is possible, by suitable choice of capacitors and inductors, to simulate the true line as the transmission line itself can be regarded as comprising an infinite number of filters in series. One of the difficulties, especially when it is desired to delay steep waveforms, is the preservation of the wave shape. All the frequency components of the pulse (and for an ideal rectangular pulse these extend to infinite frequency) must lie within the filter pass band. In other words the frequency components of the pulse must pass through the section with a constant time delay and amplitude. This is impossible to achieve in practice but a compromise is reached in which the filter possesses amplitude and time delay characteristics independent of frequency over a fairly wide band of frequencies. With a line comprising simple filter sections ("constant k") (see Fig. 1), it is necessary for the cut-off frequency to be very much higher than the frequencies to be passed, if distortion is to be avoided. If more complex sections with mutual coupling between the coils are resorted to ("M-derived") (Fig. 2), then it is possible to pass, without distortion, frequencies which are a much higher percentage of the cut-off frequency. In other words, the Mderived section possesses a flatter characteristic with a sharper fall at the cut-off point.

Mechanical Lines.—Lumped-constant lines can give long delays, but even these constructions become cumbersome and it is usually necessary to resort to the use of "mechanical", rather than electrical, transmission. Mechanical lines are diverse in form; but three common types are considered here:

Mercury Tubes: The electrical pulse is converted into a supersonic compression wave by means of a quartz or magnetostriction transducer. The

wave is applied to a tube of mercury through which it passes at a relatively low velocity.

 $v = \sqrt{(E/\rho)}$

where E is Young's modulus of the medium and ρ = density of the medium.

Another transducer reconverts the acoustic wave to an electro-magnetic wave. It is necessary to maintain the medium at a controlled temperature since the velocity of the supersonic wave varies with temperature. Special precautions are also necessary to prevent unwanted reflections.

Torsion Wire: The mercury tube is long and can be inconvenient. A simpler form of delay line makes use of the transmission of a "twist" applied to a length of wire, which can be coiled up and supported on a compliant suspension without deleterious effects. The "twist" is usually applied by magnetic means

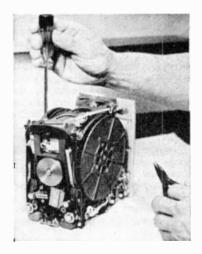
Quartz Plate: Another form of mechanical line uses a many-sided plate of quartz arranged so that a wave fed in at one side is reflected internally from the other sides in turn until it either returns to the input or reaches an output transducer.

Satellite Tape Recorder

FIVE tape recorders like the one shown in the photograph are in use in the U.S. Army's Courier 1B "delayed-repeater" communications satellite. When in range of the Puerto Rican or Fort Monmouth (New Jersey) ground station, the satellite can either receive and record or replay and transmit 340,000 words in a five-minute period. Four of the tape recorders are used for transmitting and receiving digital data at a rate of 55kilobits per second, and the remaining one for analogue signals from 300 to 50,000c/s (the tape speed is 30in/sec).

As it is hoped that the satellite will remain in orbit for at least a year, a tape was required which could withstand at least 10,000 passes across the heads. The tape selected was "Scotch" Brand No. 199, a heavyduty instrumentation tape made by the Minnesota Mining and Manufacturing Company. To produce the low wear required, the same binder is used as is normally employed with videotape. The tape must also be capable of withstanding extremes of temperature: this binder showed no deterioration when tested from -40 up to +250°F.

Tape recorder used in the Courier IB "delayed-repeater" communication's satellite.



WORLD OF WIRELESS

German TV Chaos

THE opening date for West Germany's u.h.f. television network, originally planned for January 1st, is again postponed; this time for a further two or three months. This decision was taken by the West German Federal Court, who ruled that the Federal Government is not allowed to set up and operate a television network of its own as, according to the Constitution, all broadcasting activities must be conducted by the Länder Governments.

The thirty u.h.f. transmitters constructed by the German Post Office in readiness for the government network have so far had to confine themselves to test transmissions. It is not yet known whether or not these stations will be used by the Länder. Another problem is what will happen to the private company, Freies Fernsehen G.m.b.H., which was designated sole programme contractor to the government u.h.f. network. The company has a library full of recorded TV programmes and no transmitters to broadcast them.

West German set manufacturers who have been advertising and producing u.h.f. sets for more than six months are facing trouble, too. The uncertainty about the start of the u.h.f. network has made the public reluctant to buy u.h.f.-equipped sets and stocks of old models (without u.h.f.) are mounting despite price cutting.

It is still not known whether the Länder u.h.f. network will operate on a commercial basis (the government u.h.f. plans were for commercial broadcasts) or whether it will follow the pattern set in the v.h.f. bands by local stations which are non-profitmaking but have up to 15 minutes of commercial time per day.

Tape Recorder Import Duty

TWO consolidated actions were recently brought by Grundig (Great Britain) against the Commissioners of Customs & Excise to recover part of the 20% ad valorem duty charged on tape recorders imported from Germany in 1958 and 1959; their claim being that they should have come under the category of dictating machines and subject to only 10% duty. In a reserved judgment Mr. Justice Barry granted Grundig a declaration that recorders imported between June and November, 1958, were dictating machines liable for only 10% duty and were not musical instruments. He dismissed their claim for a similar declaration on other recorders and found that they were "combined recorders and reproducers" suitable for reproducing music and were liable for 20% duty.

It was stated that on instructions from Grundig, the German makers had removed small resistors from the machines to reduce their frequency response, but similar resistors were installed after the machines arrived in Britain. Plaintiffs had frankly admitted that the sole purpose for the machines being "maimed" in Germany was to attract the lower import duty rate and they had not attempted to conceal what they had done from the Com-

missioners.

Stockholm Broadcasting Conference

AT the invitation of the Swedish Government, the European VHF/UHF Broadcasting Conference, convened by the International Telecommunication Union, is to be held in Stockholm from May 26th to June 22nd. The delegations, representing the telecommunication administrations of Europe, will have two principal tasks. First, to examine the present situation of v.h.f. sound and television broadcasting in the European Broadcasting Area (which includes North Africa and part of Asia Minor). The Conference will therefore have to consider whether experience has brought to light any serious defects in the 1952 Stockholm Plans and, if so, to decide what remedies might be applied.

The second and, perhaps, most important task will be in the field of u.h.f. television for which no allocations were made at the 1952 Conference.

To undertake the technical preparatory work for the Conference, a meeting of experts organized by the C.C.I.R. was held in Cannes early in March. Four committees were constituted, dealing respectively with propagation, sound broadcasting, television broadcasting and planning methods for Bands IV and V.

The question of planning methods is a more delicate one in Bands IV and V, compared with Bands I and III, because the u.h.f. bands represent an almost continuous region of the spectrum from 470 to 960 Mc/s, which means that second-channel and receiver-oscillator interference have also to be taken into account when assigning frequencies to stations. It is consequently rather doubtful whether the arbitrary methods adopted at earlier conferences can be applied successfully. The European Broadcasting Union has proposed the use of computers; the problem being the large number of variables in each case and the repercussions of any particular assignment on many other channels.

All the European administrations have adopted 8 Mc/s channel spacing and all Continental European administrations have agreed to utilize a 625-line standard for u.h.f. television.

In the field of sound broadcasting, the experts have come to the conclusion that as yet insufficient data exist to take the special requirements of stereophonic broadcasting into account and it is, therefore, probable that the Conference will plan Band II for "mono" only.

Electronics Review

AN ever-increasing proportion of the cost of "military" aircraft is for the electronic equipment installed. Whereas in the Scimitar it was 5% and in the Sea Vixen 14%, in the new NA39 it is 20%. These figures were given by C. I. Orr-Ewing, Civil Lord of the Board of Admiralty, who was guest of honour at the annual luncheon of the Electronic Engineering Association. He also stated that 21% of the cost of a Leander frigate was for the electronic content.

The Association has again issued a well-illustrated

annual review, "British Electronics Engineering," which in its 28 pages outlines the various fields for which its members manufacture capital equipment. The British radio and electronics industry as a whole is now producing some £500M worth of equipment a year (increasing at the rate of 10%) and £175M of this total is manufactured by the capital goods division of the industry.

E.E.A. Council.—The new Council of the Electronic Engineering Association consists of the following member firms, whose representatives' names are in

parenthesis:-

parenthesis:—
A.E.I. (V. M. Roberts); Decca Radar (C. H. T. Johnson); E.M.I. Electronics (C. Metcalfe); Elliott Brothers (W. R. Thomas); Ferranti (W. D. H. Gregson, vice-chairman); G.E.C. (Dr. D. N. Truscott, chairman); Kelvin & Hughes (C. G. White); Marconi's W/T (F. S. Mockford); Mullard Equipment (R. R. C. Rankin); Murphy Radio (K. S. Davies); Plessey Co. (P. D. Canning); Pye Telecommunications (J. R. Brinkley); Redifon (A.V.-M. E. B. Addison); and S.T.C. (L. T. Hinton). Hinton).

Association of Public Address A.P.A.E.—The Engineers is negotiating with the Post Office for the allocation of a frequency for radio microphones which are being marketed by some of its members. At the Association's recent exhibition two of these, one from West Germany and another from Japan, were shown. The new president of the association is J. Maurice, managing director of Lustraphone Ltd.

B.M.E.W.S.—In order to "protect operating personnel from the extremely high r.f. radiated power. and to ensure interference-free conditions for the varied electronic equipment" used on the B.M.E.W.S. site at Fylingdales, Yorks, extensive screening is necessary. Belling and Lee announce that they have been engaged to assist in the design and implementation of r.f. shielding and interference suppression.

Via the Moon.—The first England-Australia radio link using the moon as a reflector was made on February 24 by Pye engineers working in co-operation with the staffs manning the radio telescopes at Jodrell Bank and Sydney. A Pye 1-kW double-sideband a.m. transmitter was used to feed the signals from voice-frequency teleprinter equipment into the 250ft paraboloid at Jodrell Bank. At Sydney a new 60ft radiotelescope was used.

VOR/DME.—A plan for the provision of the short-range navigation aids VOR and DME in the European-Mediterranean area has been prepared by an International Civil Aviation Organization regional meeting recently held in Paris. The plan, which will now be submitted to the Air Navigation Commission and the Council of I.C.A.O. for approval, involves over 550 facilities at approximately 380 locations.

Tape Recording.—Over 1,300 tapes were submitted for a competition for 2½-minute tape recordings sponsored by Curry's, the radio and electrical dealers, in a Radio Luxembourg programme.

Receiving Licences.—January's increase in the number of combined TV/sound licences was 72,459, bringing the total to 11,148,463. Domestic sound-only licences totalled 3,532,922 and the number of licensed sets fitted in cars was 464,226.

Training schemes operated by the Ultra group of companies are outlined in the booklet "Guide to Training Schemes" available from the company's head office at Western Avenue, Acton, London, W.3.

Another Jubilee.-The 50th anniversary of the establishment of the British Electrical and Allied Manufacturers' Association this year will be marked by a number of special events, including the issue of a new Electrical Export Directory with a reference section in five languages, including Russian. Reference is made in the 50th annual report of the Association to its two latest sections—"Semiconductor Devices" and "Industrial Electronics." The latter has been established "to provide the means of closer discussions with other associations and help towards the wider examination of general policy questions affecting the industrial electronics industry as a whole."

Higher Technological Education.—The reasons for comparatively fewer students electing to read for technological qualifications in this country than in the U.S.A. and Russia are to be investigated by the University of Oxford's Department of Education led by its director, A. D. C. Peterson. The research, which will continue for two years, has been made possible by a grant of £2,500 from the Capitol Radio Engineering Institute, of Washington, through its International Division, C.R.E.I. (London).

Dip.Tech. and M.C.T .- A revised edition of the booklet giving details of the two awards (Dip.Tech. and Membership of the College of Technologists) conferred by the National Council for Technological Awards, is now available from the Council at 9, Cavendish Square, London, W.1.

Technical Authorship.—The results of the first examination in technical authorship conducted by the City and Guilds of London Institute will be discussed by W. Hazel, of the Ministry of Aviation, at a meeting of the Technical Publications Association at 7.0 on April 20th at Monotype House, Fetter Lane, London, E.C.4. The meeting is not confined to members of the

Audio Centre.—On May 17th a Centre of Sound for both industrial and amateur "devotees of the science of sound" will open at 12, Archer Street, London, W.1. It is sponsored by the newly formed Audio Industries Club Ltd. in association with the British Recording Club. The centre will incorporate an exhibition of sound equipment, a demonstration theatre for both sound and vision, an information bureau and a restaurant.

Maurice Child, the well-known radio amateur, has presented to the Radio Society of Great Britain a collection of antique radio equipment. The collection of 26 items is almost entirely of pre-1914/18 vintage. Mr. Child is a vice-president of the Society and was for many years principal of the London Telegraph Training College.

Demonstrations of loudspeakers (both domestic and monitoring) and professional recording equipment are being given by Lockwood and Co. in collaboration with other manufacturers at the I.B.C. Recording Studios, 35, Portland Place, London, W.1, on April 6th and 7th from 6 to 9.30 p.m. and on April 8th and 9th from 9.30 a.m. to 9.30 p.m.

Westward TV.-Full-power trade tests have been radiated since March 20th from both the I.T.A. transmitters which will serve S.W. England. They are transmitted daily (except Sundays) from 10 a.m. to The programme contractors for both transmitters, Stockland Hill, Devon (Channel 9) and Caradon Hill, Cornwall (Channel 12), are Westward Television who plan to start their service on April 29th.

"Applications of Frequency-Sweep Oscillators."-Unfortunately, due to pressure on space, the concluding part of R. Brown's article has had to be held over until our next issue.

News from Industry

Marconi's.—The 63rd annual report of Marconi's W/T Company and its subsidiaries shows a group profit for 1960 of £57,892 compared with £411,470 for the previous year. This decline has resulted from the writing off of a loss of £670,000 incurred during the year by Marconi Italiana S.p.A. The company became a wholly owned subsidiary in September 1959, and Lord Nelson of Stafford in his reference to this at the Marconi annual general meeting said that investigation had disclosed that inadequate provision had been made for losses incurred by the Italian company prior to 1960. The 61st annual report of the Marconi International Marine Communication Company shows a net profit of £304,276 against £264,624 for 1959.

Relay Exchanges Ltd. and its subsidiary companies announced a group trading profit for 1960 of £3,949,892, almost £600,000 above the 1959 figure. After allowing for taxation and £2.75M for depreciation the net group profit was just over £1M.

Radio Rentals have changed the name of their setmanufacturing subsidiary from Mains Radio Gramophones Ltd. to Baird Television Ltd. It will be recalled that they recently acquired the trade name from Hartley Baird Ltd. The chairman's annual report records a record trading profit of £5.95M which is some £850,000 above the previous year. After charging £3.44M for depreciation and allowing for taxation the net group profit showed an increase of nearly £500,000.

T.C.C.—A trading profit of £701,737 for 1960, compared with £770,679 for the previous year, is announced by the Telegraph Condenser Company.

Packaged television stations, costing under £10,000, are being marketed by E.M.I. Electronics Ltd. to provide a low-cost, uncomplicated television system for mass education and instruction by television. In a region with flat terrain, good reception should be obtained within 15 miles radius of the transmitter. A number of receivers is supplied with each transmitter.

Power System Computers Ltd., of Team Valley, Gateshead-on-Tyne, 11, have undertaken to manufacture the analogue computers developed in the Department of Electrical Engineering at Sunderland Technical College.

EMIFAIR—an exhibition of medical, musical and scientific developments of the E.M.I. family of companies—will shortly commence a tour of the country. The exhibition contains 16 stands. The major emphasis is on Ardente hearing aid equipment, but included among the other exhibits are records and record reproducers, and tape recorders for sound reproduction and dictation.

Anglo-Czechoslovak trade agreement for 1961 provides for about £5.6M worth of U.K. goods to go to Czechoslovakia and about £8M worth in the reverse direction. The quota includes Czech valves and transistors to the value £60,000 (not more than a fifth of which may be transistors) and gramophone records and tapes to the value of £20,000. The quota of U.K. exports under the agreement lists £50,000 worth of electronic and communication equipment including sound and television receivers.

Anglo-French co-operation in the field of communication earth satellites is provided for in a joint study to be undertaken by the Hawker Siddeley group and SEREB (Société pour l'Etude et la Realisation d'Engins Ballistiques) of Paris. SEREB was set up two years ago by the French government to act as systems managers for all ballistic weapon development to be undertaken in France or in association with other countries.

Computer appreciation courses for executives are conducted from time to time by Leo Computers Ltd. The week's course "providing a sound introduction to data processing in general," is non-residential and costs 25 gn. Particulars of the next series of courses, which will be held on April 10th to 14th, July 10th to 14th and September 11th to 15th, are obtainable from Leo Computers Ltd., 151A-159A Queensway, London, W.2.

Rank Precision Industries have been granted exclusive selling rights in the U.K. and many overseas territories for the Dage range of closed-circuit television equipment manufactured by Thompson Ramo Wooldridge, of Michigan City, Indiana. The Dage range of cameras includes one of only 7½" long and weighing only 4lb. It is "completely transistorised" and is available with a three-lens turret.

B & K Laboratories, of 4 Tilney Street, London, W.1, are to market in this country two new spectrum analysers developed by the Polarad Electronics Corp., of New York. One (type WSA) covers 10-40,000Mc/s in 20 bands and the other (type DA70) 50-100Gc/s in three bands.

Vicsteels Ltd., of Craven House, 16, Northumberland Avenue, London, W.C.2, have been appointed U.K. agents of Lumalampan AB, of Stockholm, manufacturers of tungsten and molybdenum wire and the Luma wire cutting, stripping and twisting machine.

Ultra Electronics are to supply 40 sets of their UA60 intercom, equipment for the Westland P.531 aircraft being supplied to the Army Air Corps. The value of the contract is approximately £21,000.

W.S. Electronics Ltd., a member of the K.G. (Holdings) Group, has been awarded a contract for a further 300 u.h.f. airborne emergency transmitter-receivers, (Type D103) for the Royal Air Force.

Livingston Laboratories Ltd. are moving to new premises at 31, Camden Road, London, N.W.1 (Tel.: Gulliver 8501) on April 4th.

EXPORTS

Rhodesian police are to be equipped with Cossor packset transmitter-receivers. These v.h.f. sets, which weigh only 5 lb, will be used for ground and ground-to-air communications.

Signal generators to the value of approximately \$160,000 have been ordered from Marconi Instruments for the Royal Canadian Air Force. The instruments, which cover the 10-470Mc/s frequency range, are amplitude molulated.

A Continental tour to promote the next International Instruments, Electronics and Automation Exhibition, to be held in London in May, 1962, is being undertaken by the organizing committee. They have already visited several cities and from April to June will visit Milan, Brussels, Amsterdam, Paris, Stockholm and Frankfurt.

Sweden has placed a further contract with Marconi's (following substantial orders in 1959) for the supply of "secret electronic equipment" for her air defence system. The contract is valued at over £1.7M.

Personalities

Lord Nelson of Stafford, LL.D., chairman of the English Electric group of companies, has been elected to honorary membership of the Institution of Electrical Engineers "in recognition of his outstanding contribution to the development of electrical science and engineering, and for his many services to The Institution." Lord Nelson, who was a post-graduate student with the Brush Electrical Company, Loughborough, became their chief outside engineer at the age of 22. He later joined the British Westinghouse Company (which became Metropolitan-Vickers). His association with the English Electric Company started in 1930 when he was appointed managing director. Lord Nelson was created a Baronet in 1959 and raised to the peerage in 1960.

Julius A. Stratton, Sc.D., LL.D., president of the Massachusetts Institute of Technology, is the 39th recipient of the Faraday Medal of the I.E.E., which he is awarded for "his notable contributions in the fields of technological education and research in radio communication." Dr. Stratton, who will be 60 in May, has been on the staff of M.I.T. since 1924 when he joined as a research associate. He was in the radiation laboratory from 1940 until 1945 when he became director of the research laboratory (electronics). He remained in that post until his appointment as president in 1959. Dr. Stratton has made "an outstanding contribution to the theory of transmission line, waveguide and antenna systems in relation to the wartime development of centimetre-wave radar."

D. N. Truscott, O.B.E., A.C.G.I., D.I.C., B.Sc., Ph.D., Sc.D., general manager of the electronics division of the G.E.C., which he joined ten years ago, has been elected chairman of the Electronic Engineering Association in succession to L. T. Hinton (Standard Telephones and Cables). Dr. Truscott was for four years in the engineering department of Murphy Radio which he left in 1939 to join the Ministry of Aircraft Production where he was an assistant director from 1944 to 1945. He then spent six years in the Ministry of Supply as an assistant secretary.

N. McAdam, B.Sc., has been appointed chief engineer of the industrial valves and cathode-ray tubes department of the A.E.I. Radio and Electronic Components Division. After spending five years with A. Reyrolle and Company as a student apprentice he graduated in electrical engineering in 1933. In 1934 he joined Mullards and a year later went to the Edison Swan Electric Company as a junior development engineer. In 1947

he went to the company's valve factory at Sunderland as chief factory engineer. He became divisional chief inspector for the Edison Swan group of factories in 1955.

Clifford Metcalfe, C.B.E., will, at his own request, relinquish the managing directorship of E.M.I. Electronics Ltd., on July 1st. He will remain a full-time director of Electric & Musical Industries Ltd., and will devote his main attention to initiating technical and development policy for new products. He will be succeeded as managing director of E.M.I. Electronics Ltd. by Percy A. Allaway who has been his deputy since 1957. Mr. Metcalfe spent his early years with Bristol Aeroplane Company on engine design. He joined the Gramophone Company in 1930 as a mechanical designer and was appointed a director of E.M.I. Engineering Development Ltd. in 1946. Mr. Allaway also joined the Gramophone Company in 1930. He spent the war years designing equipment for radar and similar electronic devices. He was appointed general manager of E.M.I. Engineering Development Ltd. in 1953, and works director in 1956.

Charles Bovill, A.M.I.E.E., M.Brit.I.R.E., A.F.R.Ae.S., has joined Multisignals Ltd. as executive engineer. He had previously been with the Decca group since 1946, first with the Navigator Company and since 1954 with Decca Radar as overseas technical representative working mainly in France. Trained at the University of Grenoble, France, and the Regent Street Polytechnic, he joined the development department of the Gramophone Company in 1933. From 1936 to 1937 he was with the Air Ministry, and in 1938 joined the air division of Marconi's, later becoming liaison engineer with R.A.F. Bomber and Coastal Commands. Mr. Bovill was commissioned in the R.A.F.V.R. in 1942 and was appointed officer in charge of the Air Operational Research Group of the Inter-Services Research Bureau.

D. Edmundson, general manager of the Rugby works of A.E.I. since January last year, is appointed manufacturing manager, A.E.I. Electronic Apparatus Division in succession to the late E. T. W. Barnes. Mr. Edmundson served an engineering apprenticeship with B.T.H. In 1940 he was appointed head of the electrical laboratory, and in 1946 test engineer, Rugby works, eventually becoming superintendent, test department. G. P. Thompson, who becomes manager of the Rugby works of A.E.I., joined B.T.H., Rugby, as a student apprentice in 1930.



Dr. D. N. Truscott



N. McAdam



P. A. Allaway



C. Bovill

E. A. W. Spreadbury, M.Brit.I.R.E., associate editor of the Wireless & Electrical Trader, has been elected chairman of the Radio Trades Examination Board for a second term of office. He has been associated with the work of the Board since its inception in 1944 and was for many years an examiner in both sound radio and television servicing. He joined the laboratory staff of Wireless Trader in 1937 where he was responsible for the preparation of the service sheets issued by the journal.

Three appointments to the directorate are announced by the Solartron group. R. Catherall, B.Sc., who joined Solartron Laboratory Instruments as a development engineer in 1952 and since 1957 has been a director of Solartron Research and Development, joins the group board as director of research and development. After graduating at Manchester University he joined Rotol Ltd. where he was concerned with the development of electronic equipment for vibration measurements in aircraft propellers. In 1948 he went to S. Smith and Sons on automatic pilot design. Soon after joining Solartron





R. Catherall

H. D. Binyon

in 1952 he became responsible for the development of their transfer function analyser. H. D. Binyon has joined the group board as director of product sales. He joined Solartron Laboratory Instruments in 1952. After coming down from Magdalen College in 1940 he joined the R.A.F. Signals Branch and in 1947 went to the Cavendish Laboratory, Cambridge, for two years. L. Malec, M.B.E., who joined the group two years ago as managing director of Solartron Radar Simulators is appointed director of systems sales to the group. After war service in the R.A.F. he joined British European Airways. From 1948 to 1959 he was with Air Trainers Ltd., of which he subsequently became managing director.

- J. Reekie, B.Sc., Ph.D., M.I.E.E., who joined Semiconductors Ltd., the Plessey-Philco company, in 1957 as chief engineer and subsequently became executive director and general manager, is being detached for special duties by the board of the Plessey company, and will shortly be visiting a number of overseas territories on behalf of the company. G. W. Pratt has been seconded by the Philco Corporation of America to act as general manager of Semiconductors Ltd.
- J. W. Haig-Ferguson, M.A., A.M.I.E.E., has recently been appointed managing director of R. & J. Beck Ltd., one of the Griffin & George group of companies. Mr. Haig-Ferguson, who was born in 1923 and is a graduate of Queen's College, Cambridge, was in R.E.M.E. in the latter part of the war. He was until recently divisional director (electronics) of Bruce Peebles & Co. Ltd., Edinburgh.

- K. A. Robinson, A.M.Brit.I.R.E., who joined Lancashire Dynamo Electronic Products in 1948 as chief development engineer, has been appointed to the board of the company, which is a member of the Metal Industries group. Mr. Robinson, who is 34, was appointed chief engineer in 1959. Before joining the company he was concerned with the development of industrial electronic equipment with the English Electric Company.
- A. S. D. Barrett, B.Sc.(Eng.), M.I.Mech.E., M.I.Chem.E., has been appointed consultant to Research and Control Instruments Ltd., and has joined the board of directors. Prior to setting up in private practice as an industrial consultant at the beginning of this year Mr. Barrett was technical director of Edwards High Vacuum Ltd. He is a vice-chairman of the Scientific Instrument Research Association and secretary of the International Organisation for Vacuum Science and Technology.

The board of Livingston Laboratories has been enlarged and now includes F. Livingston Hogg as chairman and joint managing director, D. C. Rennie (joint managing director), M. R. Hogg, H. Sellers, S. W. Urry and F. R. G. Webb.

OUR AUTHORS

Richard C. Foss, B.Sc., Grad.I.E.E., joint author of the article on multivibrator design in this issue, joined E.M.I. Electronics on leaving school in 1952. During four years' training he spent two years working on digital computers. He studied at Southall Technical College and won an I.E.E. prize and a Technical State Scholarship, going to King's College, Newcastle-upon-Tyne, in the University of Durham, where in 1959 he graduated with first class honours in electronics. He is now carrying on research on second-harmonic magnetic modulators and some applications using ferrites, having been awarded the Oliver Lodge Scholarship of the I.E.E. (made honorary by the financial support of E.M.I. Electronics). His co-author, Malcolm F. Sizmur, B.Sc., also joined E.M.I. Electronics in 1952. He took his H.N.C. at Slough Technical College and won an I.E.E. prize and Technical State Scholarship. He spent two years in the digital computer division of the company and he too went to King's College, Newcastle-upon-Tyne, where he obtained a general degree in electrical engineering.

E. Jeffery, A.M.I.E.E., the first part of whose article on a low-cost stereo amplifier appears in this issue, has been an engineering superintendent at the Bracknell Division of the Sperry Gyroscope Co. since 1956. He entered the Post Office Engineering Dept. in 1936 and during the war was an officer instructor at the Army Radio School at Petersham. At the end of the war he took a regular commission in R.E.M.E. and was for some years Major Chief Instructor (first in telecommunications and later in radar and control equipment) at the R.E.M.E. Training Centre, Arborfield, Berks. He was at one time in charge of the electronics branch of R.E.M.E. Base Workshops, Singapore. After resigning from R.E.M.E. he was technical executive to Modern Telephones Ltd. until joining Sperry. His present article derives from his personal interests and is not related to his work at Sperry.

Arthur C. Gee, who reviews on page 231 the growing interest among amateurs in the use of teleprinters, is a doctor by profession and, "believing that hobbies are essential for the well-being of mankind," has been a radio amateur for many years. Dr. Gee is chairman of the Radio Amateur Emergency Network committee of the R.S.G.B.

"BELLING-LEE" NOTES No. 27 of a Series Power Factor

When a steady e.m.f. is applied to an inductor, a current flows, its steady value being determined by the resistance of the winding, and this current creates a magnetic field surrounding the inductor. If the current varies, the field varies and, as is well known, when a field surrounding a coil varies an e.m.f. is created across its terminals; this is the principle of generation. self-generated or induced e.m.f. is in opposition to the applied e.m.f., and its effect is therefore to impede the current producing it. Other things being equal, the magnitude of the induced e.m.f. is dependent upon the rate of change of the field.

If the applied e.m.f. is alternating, the maximum value of the induced e.m.f. occurs every half cycle at the instant when the current changes direction, for although its value is then zero, this is when the rate of change is greatest. The induced e.m.f. is therefore completely out of step (90° out of phase) with the current and, since it is opposing the applied e.m.f., the latter must already be in the opposite phase. This means that the current is lagging behind the applied e.m.f. by an amount depending on the characteristics of the inductor.

Looked at another way, it is obvious that while the current is increasing, the magnetic field is being built up, and as soon as the current starts diminishing, the field begins to collapse. Energy is therefore alternately stored up in the inductor and returned to the circuit, and if there were no losses, the net power consumed would be nil. If this could occur, it would mean that the current and the applied e.m.f. would be completely out of phase, zero current occurring at the instant of maximum voltage, and vice versa, the product (power) being zero. In practice, however, some energy is always dissipated, e.g. the inductor has some resistance and becomes hot, so the current is never completely out of phase with the applied e.m.f.; the power taken, then, is given by the product of the voltage and the in-phase component of the current. It can be demonstrated that the in-phase component of the current is the actual current value multiplied by the cosine of the angle of lag. Thus, if the angle of lag is 90°, the power is nil (cos $90^{\circ} = 0$) and, at the other extreme, if there is no

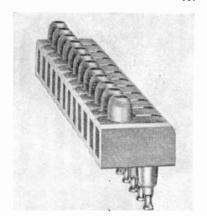
angle of lag the power taken is the product of voltage and current since $\cos 0^\circ = 1$ (this is the familiar relationship applying to D.C. circuits, and all circuits which are entirely resistive).

The ratio of power dissipated to the apparent power (the direct product of volts and amps) is known as the "Power Factor," and it can be seen that it is the same thing as the cosine of the angle of phase lag between current and applied e.m.f. Similarly, in the case of a capacitor it can be shown that the current leads an applied e.m.f., and its power factor is given by the cosine of the angle of lead. The power factor of an inductor or a capacitor is therefore an index of its quality, and should ideally be zero.

However, when we consider the goodness of a power converting device, e.g. a motor, fed from an A.C. supply, preferably none of the current passing through it should be wasted. But any out-of-phase component of the current in a circuit contributes nothing to the power output of the device, and is termed "wattless," although it heats up the conductors and the generator, embarrassing the supply authority. From the point of view of circuit efficiency the e.m.f. and current should be in phase, i.e. the power factor should ideally be unity, although values down to 0.8 are generally considered satisfactory. Domestic consumers, who are charged for the power used, are not normally very interested in wattless current, but industrial users who are supplied on a maximum demand tariff are vitally concerned since their maximum demand meters register volt-amps. In all cases where the power factor is less than 0.8 it is desirable to improve matters and, since most circuits which have a poor power factor are mainly inductive, with the current lagging behind the voltage, by connecting a capacitor of appropriate value across them a wattless leading current is taken, which reduces the net wattless current to a reasonable value.

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Fifty Years' Research in

RADIO WAVE PROPAGATION

By R. L. SMITH-ROSE,* C.B.E., D.Sc., F.C.G.I., F.I.R.E., M.I.E.E.

WHILE in 1911 great achievements had been attained in the practical developments of wireless telegraphy, there was little understanding of the manner in which the electromagnetic or radio waves involved travelled over the earth's surface; and particularly as to how it came about that these waves, which normally travel in straight lines, could bend round the spherical earth.

This was brought out very clearly in a lecture given by G. Marconi before the Royal Institution on 2nd June, 1911. The following extract is taken from the report of this lecture in the July, 1911, issue of the Marconigraph, a journal which was incorporated in the Wireless World less than two years later (April, 1913).

"Although we have—or believe we have—all the data necessary for the satisfactory production and reception of electric waves, we are yet far from possessing any very exact knowledge concerning the conditions governing the transmission of these waves through space—especially over what may be termed long distances. Although it is now easy to design, construct and operate stations capable of satisfactory commercial working over distances up to 2,500 miles, no clear explanation has yet been given of many absolutely authenticated facts concerning these waves."

Later on in the same lecture, Marconi said:

"Although the mathematical theory of electric wave propagation through space was worked out by Clerk Maxwell more than fifty years ago, and notwithstanding all the experimental evidence obtained in laboratories concerning these waves, yet so far we understand but incompletely the true fundamental principles concerning the manner of propagation of the waves on which wireless telegraph transmission is based."

Such statements, based on experimental measurements, aroused great interest since it had hitherto been considered that the electromagnetic waves involved travelled over the surface of the earth. The attenuation of the waves was less over sea than over land owing to the much greater electrical conductivity of salt water. W. Duddell and J. E. Taylor had shown in 1905 that for distances up to about 60 miles, the signal strength of radio waves was nearly inversely proportional to the distance between transmitter and receiver. But for distances beyond 100 or 200 miles, it was found by other investigators that signal strength decreased more rapidly; and L. W. Austin and L. Cohen obtained better agreement between calculated and measured signal strength by adding an exponential factor, involving both distance and wavelength, to the inverse distance relationship. Although this "Austin-Cohen formula" was used for several years by radio design engineers as a convenient practical guide, it was soon found to have serious limitations. The most important of these was the discovery that at distances greater than a few hundred miles, the strength of received signals varied from day to night: for the wavelengths and conditions then in use, the signal strength was usually greater, but more variable, by night than by day.

The first systematic discussion of these phenomena is also recorded in the issues of the *Marconigraph* for September to November, 1912, particularly by Drs. W. H. Eccles and J. A. Fleming, both of whom were closely associated with Marconi in his pioneer development of wireless communication. What was termed "The Effect of Daylight upon Radiotelegraphic Waves" became an active subject of discussion; and H. J. Round was the leading Marconi engineer who, with K. W. Tremellen, made many systematic measurements of the changes in signal strength over short and long distances due to the passage of the sunrise and sunset boundaries across the path. (See Fig. 1.)

At the 1912 Dundee meeting of the British Association Professor Fleming opened a discussion on the subject of "Unsolved Problems of Wireless Telegraphy," which was published in the *Marconigraph* for October, 1912. From the theoretical contributions made by Professors J. W. Nicholson and A. Somerfield, it became clear that diffraction alone could not account for the transmission of waves round the surface of the earth to the extent that had

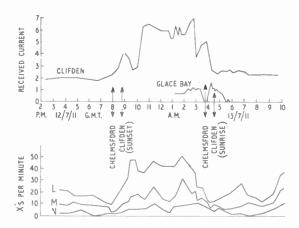


Fig. 1. Measurements of strength of signals and atmospheric noise made at Chelmsford in July 1911. (a) The upper curves relate to the reception of signals from Clifden and Glace Bay. (b) Observations of the number of atmospherics per minute which produced peak voltages of 3(L), 6(M) and 12(N) respectively. Note the effect of day and night conditions on both signals and atmospherics.

^{*} President of the International Scientific Radio Union (U.R.S.I.).

already been demonstrated. Having regard to the long waves used, however, 6 km or more, and the difference in conductivity between land and sea, it was still necessary to consider the ground wave propagation phenomena up to moderate distances.

It was in the course of this discussion that the effect of sunlight on the propagation of radio waves was emphasized by Dr. Eccles; and he described in some detail his study of the possibilities of an ionized layer in the atmosphere acting as a reflector of radio waves as first suggested by Oliver Heaviside in 1900. With a further contribution from Professor A. E. Kennelly at the British Association discussion, the foundations were laid of an understanding of the characteristics of an ionospheric shell surrounding the earth and which, subject to variations in time and place due to the influence of solar radiation, could reflect upgoing radio waves back towards the earth's surface.

International Collaboration

It was clear from this meeting (in 1912) that progress in investigating the complex phenomena involved could best be achieved by forming a committee or similar body comprising both theoretical and practical workers in the subject. It is therefore significant that in the following year a meeting was held in Brussels to discuss the formation of an international committee to organize and conduct scientific experiments in wireless telegraphy. A reunion was held in Brussels in April, 1914, at which a programme of scientific measurements was drawn up and discussed in some detail. This included observations of the variations in signal strength received in different directions and at various distances from the transmitter; and also simultaneous measurements of the strength of atmospheric disturbances in different places.

This body became the International Scientific Radio Union (U.R.S.I.), which held its first meeting in Brussels in 1922, and its XIIIth General Assembly† in London in September, 1960. During its nearly forty years of existence, the work of U.R.S.I. has covered a range of scientific subjects, such as standards of radio measurements and their application to wave propagation and radio noise, for the study of which on a world-wide scale, international co-operation is not only a great advantage, but indeed a necessity. In addition to pursuing scientific research on radio matters, U.R.S.I. has, for the past thirty years or more, collaborated with the International Radio Consultative Committee (C.C.I.R.) on many problems of mutual interest, particularly those concerned with the design and operation of long-distance communication circuits. It is natural to find that this co-operation is actively continuing in connection with the more recent problems of radio astronomy and communication to and from vehicles in space.

The Ionosphere and Round-the-world Transmission

It was not until 1925 that the first experiments which demonstrated the existence of the Kennelly-Heaviside layer were made by Sir Edward Appleton and his co-workers using the Bournemouth trans-

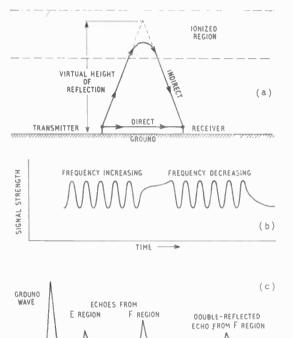


Fig. 2. (a) Paths of direct and indirect waves from transmitter to receiver; and the measured—or virtual-height of reflection of the indirect wave. (b) Interference fringes in received signal due to ground and ionospheric waves, as the frequency of the transmitter is varied over a small range. The ratio of the number of signal maxima to the change of frequency gives the difference in time of arrival of the two signals, and so the height of reflection of the indirect wave. (c) Echoes of transmitted pulses after reflection from the lower (E) and upper (F) ionized regions: and also of an echo of a pulse which has been twice reflected from F with an intermediate reflection at the ground.

TIME

mitter of the B.B.C. By changing the frequency of this station, the strength of the received signal was found to vary, indicating an interference pattern such as would be produced by two sets of arriving waves, one travelling along the ground and another coming down after reflection at the ionized layer. (See Fig. 2 (a) and (b).) Confirmatory evidence was found by comparing the signal variations obtained when receiving on a loop and vertical aerial. An alternative method was used by R. L. Smith-Rose and R. H. Barfield, who compared the strength of signal from a transmitting station received simultaneously on a loop and vertical aerial. All these experiments indicated that the radio waves usedabout 300m in wavelength—were reflected from an ionized layer at a height of about 100 km. Almost concurrently with this work G. Breit and M. A. Tuve used a pulse technique to measure directly the time interval between the arrival of the pulses travelling along the ground and those which arrived later after travelling up to the ionized layer and down to the receiving station. (See Fig. 2 (c).) A year or two later, by using shorter wavelengths, Appleton and his co-workers showed that at certain times the radio waves could penetrate the first reflecting (or E) region and be reflected from an upper region, termed F, at a height of some 400 or 500 km.

[†] A brief account of this meeting was given in Wireless World, January 1961, p. 10.

These pioneer experiments and discoveries provided, first the complete explanation of the manner in which radio waves can travel right round the earth by successive reflections between the earth and the upper atmosphere; and, secondly, the basis of the subsequent exploration of the physical characteristics of our upper atmosphere which has been in progress for the past thirty years or more. Ionospheric observatories have come into operation for measuring the height and density of ionization of the various reflecting regions, and the manner in which these change from day to night and from summer to winter. The installation of such observatories has gradually spread throughout the world, to over 250 which were in operation on a regular and systematic basis during the International Geophysical Year of 1957-58.

As a result of the international collaboration obtained under the auspices of U.R.S.I. observations made in different parts of the world are freely exchanged, so that national laboratories can prepare charts showing the state of ionization in the upper atmosphere all over the world. Based on data accumulated in this way, over one or more solar cycles of 11 years duration, accurate forecasts can now be made of the ionospheric conditions to be

expected up to six months in advance.

Concurrently with this observatory work on conditions at vertical incidence, continuous studies have been made on the transmission of radio waves over oblique incidence paths at distances from a few hundred up to several thousand miles between sending and receiving stations. In this way, a detailed and fairly accurate knowledge has become available for use in the design and operation of long-distance radio communication services throughout the world. The frequencies or wavelengths to be used for such services can be selected in advance according to the time and geographical location of operation, and systematic planning can take place to deal with the diurnal fluctuations in ionospheric conditions as well as with the longer-term variations which follow the solar cycle.

Radar Technique and Back-scatter

It is well known that the use of pulse transmission and receiving technique formed the basis of the development of radar for detecting and locating ships, aircraft and geographical features. It seemed only just, therefore, that research workers concerned with the exploration of the ionosphere should take advantage of advanced and powerful radar techniques for their continued investigations. Following earlier work by T. L. Eckersley on the scattering -as distinct from reflection-of radio waves from ionospheric clouds or regions, E. D. R. Shearman used a high-power radar transmitter to direct a beam of waves horizontally. The waves after reflection from the ionosphere reached the earth's surface at some one or two thousand miles from the transmitter. Some of the energy of the waves was scattered backwards, and after a second reflection at the ionosphere was detected at a receiver alongside or incorporated with the transmitter. From a measurement of the time taken for the pulses of radio waves to travel to and from the sending station, the path of the waves was determined. Furthermore observations made on various frequencies soon showed the characteristics of the ionosphere at the distant

reflecting region. By suitably rotating the aerial system, the beam of waves was made to scan the horizon, and in this way the conditions in the ionosphere all round the observing station could be explored at ranges up to 7,000 miles or so. This technique has proved to be a powerful tool not only for the scientist investigating the ionosphere all round him, but it also enables the radio operator of a long-distance circuit to determine from time to time the best and most suitable frequencies to use in the prevailing circumstances.

Propagation at V.H.F.

In general, radio communication services which make use of ionospheric propagation are confined to frequencies below 30 Mc/s (wavelengths above 10 metres): although it has long been known that under appropriate conditions the density of ionization in the ionosphere is at times sufficient to support the transmission of radio waves within the band 30 to 50 Mc/s. But experience has shown that this type of transmission is comparatively rare and inefficient with normal transmitter powers and receiver sensitivities. To obtain anything approaching a regular service, it is necessary to use the scattering of the waves at the ionosphere which, on account of the weakness of the resulting signals, entails the use of very high power and concentrated beams of radiation. This technique is, however, used in certain "ionospheric scatter" services where the utmost reliability is necessary at all times, irrespective of economy and efficiency.

The main use of the v.h.f. band between 30 and 300 Mc/s (wavelengths 1 to 10 m) is, however, for the localized services involved in broadcasting, television, police and private mobile services, and certain types of beacon and navigational aids mainly perhaps, for aircraft services. These services as used today, are based on the knowledge obtained in research on the propagation of such waves over the past thirty years or so. The subject here is broadly divisible into two parts. First, a study of the electrical characteristics and the physical features of the earth's surface, which mainly determine the trans-mission of the waves to short distances broadly within the horizon as seen from the sending aerial. Secondly, and particularly at the longer distances beyond the horizon, the strength of the waves arriving at the receiver may be affected to a varying extent by the bending of the waves due to the refractive index gradient in the atmosphere. This refractive index gradient is determined by the temperature, pressure, and more especially, the humidity of the atmosphere, and so the extent to which the waves are bent is very dependent on the weather conditions prevailing over the transmission path.

But considering the shorter-range phenomena first, in order to extend the horizon and so the service of a transmitting station, it is usual to elevate the aerial of the latter as much as possible. It then becomes clear that there are two paths by which the waves can travel towards the receiver. One of these is directly through the air from transmitting to receiving aerial: while the other path involves reflection from the ground, the inverse of reflection from the upper atmosphere. The resulting signal at the receiver is the combination of these two sets of waves, which are usually out-of-phase in practice, and result in the signal strength being inversely propor-

tional to the square of the distance between sending and receiving stations. There are, of course, wide variations in practice from this simple law, mainly due to the effect of obstacles such as hills and buildings in the path of the ground reflected waves.

Next, as already suggested, the direct waves which travel through the air may be subject to bending which may result in their being propagated appreciably beyond the horizon. As a result the vice area" of such a transmitting station is increased beyond the limits of the optical horizon, albeit the extended range is variable and dependent upon the prevailing atmospheric conditions. For practical purposes, in such cases as broadcasting and television services, measurements are made over long periods of time and in various parts of the world to obtain sufficient data to express the results on a statistical basis. An example of the application of this type of study is shown in Fig. 3 which is reproduced from a recommendation of the C.C.I.R. in 1959, setting out the field strengths likely to be received at various distances beyond the horizon for typical proportions of the time of observation. Such information is of direct importance to designers of broadcasting services, and assists them to determine the minimum separation in distance necessary between stations operating in the same frequency channel to secure comparative freedom from any specified degree of mutual interference.

Future Research in Radio Wave Propagation

A general view of the trend of future scientific research in this subject of radio wave propagation can be obtained from the conclusions and recommendations of the various Commissions of U.R.S.I. concerned with this subject. In the first place interest in the propagation of waves through the lower atmosphere is not confined to those concerned with communications. As Commission I indicated, the measurement of standards of frequency and time has become so precise that it is very important to know what changes in phase of both low and very low frequency waves occur over various transmission paths. Furthermore, since both light and radio waves are used in geodetic surveying, it is important to standardize the formulæ used for calculating the re-

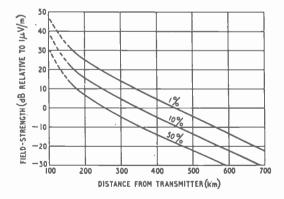


Fig. 3. Frequency range: 40 to 600Mc/s. Values of field-strength for 50% of locations for IkW radiated power by a half-wave dipole with vertical or horizontal polarization exceeded for 1%, 10%, and 50% of the time. (The dashed portions of the curves are less reliable than the portions shown in full lines.)

fractive index of the air at the working frequencies.

Commission II, dealing with propagation through the troposphere, pointed out that, while further quantitative studies were required to elucidate the statistical facts of propagation beyond the horizon, it was also important to investigate the fine structure of irregularities in the atmosphere. The latter become of increasing importance in connection with the absorption and scattering in the atmosphere at centimetre and millimetre wavelengths. Also, since many of the frequencies likely to be used in space research are susceptible to tropospheric influences, the importance of the effects of these should be examined.

With regard to the propagation of waves through the ionosphere, a subject concern to Commission III, the great co-operative work carried out during the International Geophysical Year (1957-58) has been described in previous publications. At last year's General Assembly of U.R.S.I. it was noted that several scientific unions, including the International Committee on Geophysics, were organizing a Sunspot Minimum Programme to be conducted during 1964-65 as a companion enterprise to the I.G.Y. which, as is well known, took place during a period of maximum solar activity. The results of this international effort should do much to elucidate some of the outstanding features in our knowledge of the ionosphere, which by 1965 will have been the subject of study by radio scientists for over forty years. By this date also, it may be anticipated that the use of rockets and artificial earth satellites will also have appreciably added to our knowledge of the upper reaches of the ionosphere, which it has so far been difficult to explore by radio waves sent up from ground stations.

Fifty years ago, Marconi engineers and others were recording the number of atmospherics—or X's as they were then termed—which produced a certain voltage across the receiver terminals (see Fig. 1). This study of "Radio Noise of Terrestrial Origin"to use the present title of Commission IV of U.R.S.I. -has continued ever since on a continually increasing scale all over the world. The number and variety of the various types of noise which produce an audible or detectable response on modern sensitive receivers is now so great that it was decided at the recent General Assembly of U.R.S.I. to draw up an agreed terminology of the subject. Terrestrial Noise comprises those natural electromagnetic disturbances which originate in the earth's atmosphere, and there appear to be four recognizable classes of such noise:

(i) Atmospheric noise which originates in natural electrical discharges below the ionosphere, and which travels to the receiver by the normal paths of propagation between the earth and the lower boundary of the ionosphere.

(ii) Ionospheric noise which originates in the ionosphere and is usually associated with magnetic disturbances.

(iii) Whistlers which are a form of terrestrial noise, originating in electrical discharges in the lower atmosphere, and which are propagated through the ionosphere along dispersive paths. The whistler type of noise when heard at a receiver is characterized by one or more components of the nature of gliding tones, which descend in frequency through the audible range in a period ranging from a fraction of a second to several seconds.

See, for example, Wireless World, February 1960, pp. 52-58.

(iv) Finally, composite noises are recognized as having the combined characteristics of whistlers and ionospheric noise. Such "interactions," as they are termed, may be initiated by lightning discharges and are often associated with magnetic disturbances.

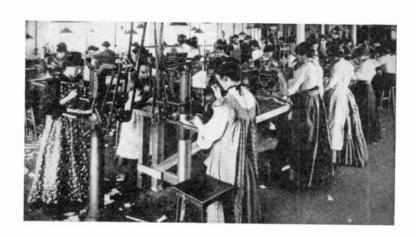
The continued study of this subject is helping to elucidate some outstanding problems on the nature of the earth's magnetism as well as on the physical characteristics of the upper atmosphere.

In this article, an attempt has been made to describe briefly some of the advances made, during the past fifty years, in the study of the propagation of radio waves around our earth and also through its atmosphere.

Much has been learnt and understood about the physical processes and conditions involved: much more remains to be discovered; and interest in future research will be greatly quickened by the possibilities of the new tools available to the radio scientist in the form of rockets and artificial satellites and the associated measuring techniques and instruments.

INDUSTRIAL GROUPS-VI

The Victorian origin of the wireless industry in this country is apparent from this photograph taken in the Marconi works over 60 years ago.



THE history of the Marconi company, and therefore that of the radio industry, started with the formation on July 20th 1897 of the Wireless Telegraph and Signal Company (soon afterwards renamed Marconi's Wireless Telegraph Company). Two years later the company established its first factory in Chelmsford, Essex. Since 1946 Marconi's W/T Company, together with its subsidiaries and associated companies has been part of the English Electric Group.

As will be seen from the following list the group.

English Electric Co. Ltd. D. Napier & Son and its subsidiaries Marconi's Wireless Telegraph Co and its overseas subsidiaries Marconi Instruments Ltd. Marconi International Code Co. Marconi International Marine Communication Co. and subsidiaries Marconi Radio Sounding Device Co. Marconi Television Co. Radio Communication Co. Scanners Vulcan Foundry Robert Stephenson & Hawthorns Ltd. English Electric Valve Co. English Electric Export and Trading Co. Canadian Marconi Co. John Inglis Co., Toronto. English Electric Canada English Electric Company of South Africa (Pty.) Ltd. English Electric Company (Central Africa) Ltd. English Electric de Venezuela English Electric Company of India (Pty.) Ltd. English Electric Company of Australia Pty. Ltd. English Electric Company of New Zealand Ltd. English Electric Espanola English Electrica de Portugal English Electric Marconi Argentina Associated Transistors Ltd.

English Electric, Babcock & Wilcox and Taylor Woodrow Atomic Power Construction Co.

ment of electronic computers and, jointly with the Automatic Telephone and Electric Company, operates Associated Transistors Ltd., manufacturers of semi-conductors. Also the English Electric Valve Company produces the "glassware" which is the very heart of duced by Marconi's.

the transmitters, radars, television cameras, etc., pro-The English Electric group profit for 1960 of £3,142,580 (after providing nearly £3M for taxation) is slightly above the previous year's figure. The group has an issued share capital of nearly £33M, fixed assets of nearly £44M and current assets of £48M.

of which Lord Nelson of Stafford is chairman, now com-

prises over 30 allied and associated companies. It employs 84,000 people in its 24 principal works in this country and abroad. The group's interests are too diverse to be covered adequately in a short survey, but they range from aviation to atomic power plant, electrical generation to electric cookers, traction equipment to

transistors, marine engines to marine radio, transmitters

to turbines, and klystrons to computers. Its radio and

electronics interests are not, however, concentrated in the Marconi section of the group, for the English Electric Company itself has been in the forefront of the develop-

Reactance Calculator

A SLIDE-RULE Calculator measuring 83×31in providing a simplified means of calculating resonance frequency of tuned circuits, reactance of inductors and capacitors, Q of coils and dissipation factor, all over a wide range of values, has been introduced by Shure Brothers Inc. of Evanston, Illinois, U.S.A. It is, how-ever, obtainable in the U.K. from J. W. Maunder, 22 Orchard Street, London, W.1, at the modest price of 12s 6d.

Kingsway Housing Association Power Traction Finance Co.

British Aircraft Corporation and its subsidiaries

MANUFACTURERS' PRODUCTS

NEW ELECTRONIC EQUIPMENT AND ACCESSORIES

Fast Pulse Generator

WITH the American Du Mont Type 404 pulse generator the pulse width can be continuously varied from 0.05 to 100µsec and the pulse repetition rate can be continuously varied from as high as 100,000 down to 10 pulses/sec with internal triggering or, with external triggering, even down to a single pulse. The maximum allowable duty cycle is 10%, and a warning cut-out prevents higher duty cycle pulse trains from being generated. The pulse rise and fall times are at most 0.02 and 0.025µsec respectively and the overshoot less



Du Mont Type 404 fast pulse generator (Aveley Electric).

than 3%. The maximum peak pulse output is $50V\pm10\%$ (into 50Ω) and this can be attenuated in $\frac{1}{2}dB$ steps up to 59.5dB to an accuracy of $\pm3\%$. The leading pulse can be delayed from 3 to $125\mu \rm{sec}$ relative to an external 2V trigger with a jitter of less than $4m\mu \rm{sec} + 0.1\,^{\circ}_{o}$ of the delay time. This generator costs £280 and is imported into this country by Aveley Electric Ltd., of Ayron Road, Aveley Industrial Estate, South Ockendon, Essex.

Vacuum Switch

SHOWN in the illustration is the B. & R. Relays new Type 85 vacuum switch, a moderate-sized, single-pole make and break unit capable of switching loads of up to 2kW at voltages up to 3kV. The contacts are enclosed in an evacuated glass capsule fitted with metal end-caps and these provide the external electrical connections.

It is mechanically operated by means of the small rod seen projecting from the larger-diameter end-cap. This actuating rod is attached to a flexible diaphragm to which is fixed also the internal moving switch contact.

Although rated for relatively heavy loads a switch of this kind has many applications in radio and electronic equipments, especially where only very infrequent operation is required or highly inductive loads have to be switched. As the contacts are in vacuum they are protected against all forms of contamination.

The switch capsule is available separately as Type 183, and enclosed in the plastic housing shown in the illustration it becomes Type 85. Up to four Type 85 switches may be fitted to either an a.c. or a d.c. relay which will provide change-over or make and break facilities as required. These relays (Type C12 d.c., or C62 a.c. operated) consume about 6W (20VA a.c.) and are fitted with coils of 12kt? nominal resistance. Further details can be obtained from B. & R. Relays Ltd., Temple Fields, Harlow, Essex.

Wide Range Communications Receiver

A COMPLETELY new communications receiver, the Type 51S-1, offering extreme frequency accuracy and operational simplicity has been introduced by the Collins Radio Company. Continuous coverage of the 2 to 30Mc/s range is provided in 1-Mc/s bands with 1-kc/s increments on the main tuning dial. Additional coverage from 0.2 to 2.0Mc/s permits broadcast monitoring or laboratory use. Reception of upper sideband, lower sideband, a.m. or c.w. signals is provided at any frequency within the tuning range.

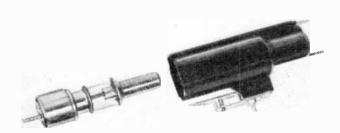
A.G.C. characteristics and a separate product detector

A.G.C. characteristics and a separate product detector contribute to optimum s.s.b. performance. A rejection notch tuning feature provides at least 40dB attenuation of unwanted signals and a level meter may be switched to indicate either r.f. signal or audio output levels. Turret construction of the r.f. section results in increased efficiency and the R.F. gain may be remotely controlled, if required, by simplexing on the audio output line.

The 51S-1 receiver is fitted with a gray simulated leather panel and housed in a gray enamel cabinet. As

The 51S-1 receiver is fitted with a gray simulated leather panel and housed in a gray enamel cabinet. As the illustration shows the set not only has an attractive appearance but the controls are neatly and conveniently arranged. Operation is from either a 115 or 230V, 50 to 400c/s power supply. A 28V, d.c. model is also available. The receiver may be mounted in the standard 19in rack and a special fittings kit is available for this purpose.

It is understood that the price of the 51S-1 receiver



B. & R. Relays vacuum switch withdrawn from its plastic housing.



Collins new communication receiver, Type 515-1 which has a very comprehensive specification.

is of the order of 1,920 dollars f.o.b. U.S.A. Further details can be obtained from Collins Radio Co. of Fngland Ltd., 242 London Road, Staines, Middx.

Low Torque Precision Potentiometer

SPECIAL features of a new precision wire-wound potentionneter introduced recently by Miles Electronics are: low rotational torque, not exceeding 7gm/cm for any resistance value; multi-contact wiper assembly of



Miles Electronics precision potentiometer.

precious metal alloy; spindle carried in a miniature ball-race; intermediate tappings up to 33 in number and ganging of up to 6 units normally, and to 8 if specially required.

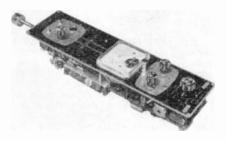
Resistance range is $0.5k\Omega$ to $100k\Omega$ in 8 standard values with a normal tolerance of 5%, but 1% can be supplied if necessary. The rating is 4.5W and the dimensions are $2\frac{4}{3}$ in diameter \times lin deep.

Linear resistance elements are fitted wound normally with enamelled nickel-chrome or cupreous-nickel wire, but windings of precious alloy wire, such as silver-palladium, can be fitted if specially required.

Further details can be obtained from Miles Electronics Ltd., Shoreham Airport, Sussex.

Sound Spectrometer

WITH the new Advance Type SPM1 battery sound spectrometer sounds at frequencies between 20 and 12,000c/s and at levels between 20 and 150dB (referred to 2×10⁻¹ dynes/cm²) can have their levels measured and can also be analysed by making use of the eight alternative filters provided. These filters consist of a low-pass filter covering up to 90c/s, six band-pass octave filters covering in all from 90c/s to 5,600c/s, and a high-pass filter covering upwards from 5,600c/s. The attenuations produced by these filters outside their nominal pass bands are, for the low-pass filter, 40dB at 450c/s; for the band-pass filters, 30dB at one half and twice the lower and upper cut-off frequencies respectively and 50dB at one quarter of and four times these



Advance battery sound spectrometer Type SPMI with cover removed.

frequencies (except for the lowest octave (90-175c/s) filter for which these attenuations are somewhat less); and, for the high-pass filter, at least 40dB at 1,200c/s. This spectrometer costs £210 and is manufactured by Advance Components Ltd., of Roebuck Road, Hainault. Essex

Transistor Analyser

RAPID and convenient measurement of many of the parameters of both p.n.p. and n.p.n. transistors is made possible by the Microcell Transistor Analyser type 440. The measurements are carried out in common-emitter configuration, and include current-gain, cut-off frequency, leakage current and turnover voltage. Diode characteristics may also be determined.

The signal source is a Wien-bridge oscillator which covers the range 1kc/s-10Mc/s, and which is amplitude stabilized to within ±1.5dB. Current gain up to a maximum of 200 is measured by a differential-input, wide band valve voltmeter, while collector voltage and



Microcell Transistor Analyser Type 440.

current are continuously adjustable up to 100V and 3A respectively, and are monitored by edge reading meters. External adaptors may be used to determine "h" parameters.

The instrument is obtainable from Microcell Electronics Division, Blackwater, Camberley, Surrey.

Tape Revolution Counter

SUITABLE for use with Scotch Boy 53 in and 7in and Emitape 7in reels, the "Call-Boy" revolution counter is attached to the supply spool by a three-pronged rubber clip. The three-digit resettable counter is driven

Colton "Call Boy" tape revolution counter.



from this clip via a flexible shaft, and can be attached to any smooth surface by means of a suction cup. The "Call-Boy" costs 42s 6d, and is manufactured by Colton & Co. (Lapidaries) Ltd., of The Crescent, Wimbledon, London, S.W.19.

TECHNICAL NOTEBOOK

Radio Star Survey recently reported by Ryle showed that, per unit angular area of sky, the number of radio stars increases rapidly as their intensity decreases. Even when the many possible modifying factors are allowed for, this result corresponds to an increase in the density of radio sources with increasing distance. Bearing in mind the time taken for the radio noise to travel from its source, this result thus also corresponds to an increase in the density of radio sources at increasing times in the past. It is this final deduction which appears to support theories in which the mean density of matter in the universe decreases with time (evolutionary theories) rather than theories in which this density remains constant (steady-state theories). (In steady-state theories, in order to nullify the decrease in density which would otherwise be produced by the expansion of the universe, continuous creation of matter must be postulated.) Most of the ratio sources are vastly more intense than their optical counterparts and so can be observed to far greater distances. The increase in density in fact only becomes noticeable beyond the limit reached by presentday optical telescopes.

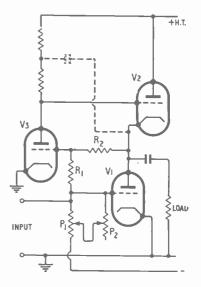
C.W. Optical Maser has been recently developed at the Bell Telephone Laboratories. Unlike the pulsed optical maser which was also recently developed by Bell and which was described in the Technical Notebook section of our December 1960 issue, the new maser uses a gas (a mixture of helium and neon) rather than a solid (ruby) as its active material. An ordinary low-power (≈ 10 W) electrical discharge is used to excite the helium atoms. These atoms collide with the neon atoms and in the process excite them in

turn to one of four upper energy levels. Transitions of the neon atoms to one of ten intermediate energy levels can then be stimulated, continuous radiation (at a level of the order of 0.01W) being emitted as the transitions take place. Thirty dif-ferent transitions are in fact possible, so that there are thirty possible maser emission wavelengths. These all lie in the infra-red between 9,000 and 17,000A: operation at five of them (between 11,000 and 12,000.4) has at present been observed. As in the Bell ruby optical maser, semireflecting accurately-parallel endplates are used to reflect the stimulated radiation back and forth along the gas-filled tube and thus to increase its intensity. Some of the stimulated radiation passes through the end plates forming a beam whose spread is less than a minute of arc in the case of the new gas maser. The spectral line width of this new maser is more than one hundred thousand times narrower than that of the ruby maser, and more than one thousand times narrower even than the narrowest hitherto-obtainable optical lines. This very narrow line width has already permitted the first observation of difference signals at radio frequencies between two optical lines. Broadband modulation of the beam at frequencies up to 60kc/s has also been accomplished using a Kerr cell

Piezoelectric Ignition is used in the U.S. Clinton industrial engine shown by Trojan at the recent Smithfield Show. This ignition system utilizes the voltage developed by compressing a piezoelectric material—in this case PZT (the trade name for the lead zirconate titanate group of ceramics). In the ignition unit the PZT is enclosed in a plastic container which is squeezed by a lever mechanism driven off the

crankshaft or camshaft. The generated voltage is fed to the sparking plug via a timing switch which can be operated from the flywheel. Thus no capacitor or spark coil is required. With this ignition system the voltage generated is nearly independent of the engine speed so that starting is made easier. The voltage rate of rise can also be made fast enough (\approx 105V/usec) to fire sparking plugs which seem to be fouled when used with ordinary ignition systems. These units can be made very small (occupying only 3½cu in) and light (weighing only 802). In this country, PZT is manufactured under licence, by Brush.)

Very-Low Distortion single-ended push-pull audio output stage is described by C. T. Murray in the March 1960 issue of Proc.I.R.E. Australia. The basic circuit is shown in the diagram. From this it can be seen that, whereas one of the two output valves, VI, is fed directly



from the input, the other output valve, V2, is fed from an amplifier, V3, which is itself fed both from the output and from the input. The low distortion results from the fact that any distortion in the output is amplified and phase reversed by V3, and then fed back to V2 so as to oppose the distortion produced in the load by V1. V3 must be fed with the correct fraction (determined by R₁, R₂, P₁, P₂) of the input and output voltages to produce a signal input to V2 equal to that to V1 and thus to correctly balance the push-pull stage. The negative supply is used to back off the positive voltage at the cathode of V2 and thus produce the correct voltage at the grid of V3. The dotted capacitive "bootstrap" connection shown both ensures that V3 can provide sufficient drive for V2 and effectively increases the gain of V3 and thus still further reduces the distortion. With this type of circuit at full output a total harmonic distortion of only 0.02% was achieved without applying any overall feedback.



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Available free on request, unique calculator providing full relay specifications.

This relay incor-15 porates amp. Micro Switch; amp. Mercury Switch and standard 0.3 to 8 amp. contacts.

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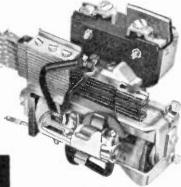


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Behind this achievement are the extensive prototype and quality manufacturing resources of the Telecommunications Division, inspired by the work of a unique research and development organisation. The Company recognises the need to segregate advanced thinking from the hustle and distraction of the factory. Accordingly, in addition to the Group Research Laboratories at Roke Manor and other specialised research centres already existing in the U.K., extremely well equipped laboratories have recently been established at West Leigh for

> advanced Telecommunications studies. In these establishments, the next generation of telecommunications equipment is already taking shape.

> In close support at all times are the complete resources of the Plessey Group of Companies which include unrivalled tool making and machining facilities, a full range of environmental testing and production laboratories, and the service of the metallurgical and chemical laboratories at Caswell.



INTERNATIONAL **ELECTRONIC** COMPONENTS SHOW



Salon International des Composants Electronique. Tubes et Accessoires Electronique Paris, 17-21 February, 1961

ALTHOUGH this annual exhibition has for the past four years been open to foreign exhibitors it still retains much of the character of the old French Components Show which started in 1934. Of the total of 435 stands about three-quarters were taken by French exhibitors, the remaining quarter by firms from eight other countries among which Germany (28), United States (27) and Great Britain (21) predominated. As in recent years the décor of the stands was uniform and the width of the allées ample, allowing those who wished, to saunter without impeding the movement of any with more urgent business (e.g., journalists?). To look at every stand it was necessary to walk at least a mile—two if both sides of each avenue were examined in detail.

Electronic accessories and measuring instruments are admitted, but

the show remains predominantly one of pièces détachées. The fact that most of the products had been seen in previous years can be taken as indicating their general acceptability, but there were enough nouveautés (so marked by stick-on labels) to keep interest alive. A wide range of very small components for printed wiring and of tuner, i.f. and a.f. "modules for incorporation in small portables were shown by Orega (a subsidiary of C.S.F.). Both Orega and S.E.C.R.E. (Soc. d'Études et de Constructions Electroniques) were showing fixed inductances, with end wires resembling fixed resistors, for use in filters and similar applications. S.E.C.R.E. here also introduced, in addition to their lumped-constant delay lines, a range of distributed-constant lines in moulded form with end wires for suspension in circuit wiring.

For test and measurement a num-

OS601 (7 to 11kMc/s). A special stabilized power supply (SCF 300) is available for these klystron oscillators. Solartron were showing their decade pulse generator (GO1005) which has a p.r.f. range of 10c/s to 1Mc/s and pulse width variable from 250mµsec to 100msec ±5%. A lightweight transistor a.f. generator shown by S.E.C.R.E. working in conjunction with a transistor frequency meter with direct-reading, 6decade luminous display were recent additions to their range of measuring instruments. Quartz-controlled transistor oscillators with self-contained 9-V battery in cylindrical cans 22mm in diameter and from 600 to 100mm high have been produced by Quartz et Electronique. Frequencies be-tween 1kc/s and 1Mc/s are available and typical characteristics (for the 1Mc/s oscillator) are: output 700mV (impedance 1500 Ω); distortion <5%;

stability 18c/s (-60° to +90°C).

Powers in excess of 5mW at a frequency of 2.2kMc/s are provided by an all-solid-state generator shown by Philco and developed in the Lansdale Division. Improve-ments in efficiency of up to two orders of magnitude, compared with klystrons, are claimed and the power supply is four 4-volt mercury cells. The total volume of the equipment is about 100 cubic inches and the weight 4lb. A crystal-controlled 110Mc/s oscillator (2N1158) is followed by a "field flow" (L5437) transistor amplifier which raises the signal level to 100mW. This is then applied to a varactor (L4105) harmonic generator and the fourth harmonic selected. After passing through a bandpass filter the 440-Mc/s signal is applied to a further varactor (L4102) and the fifth harmonic (2.2kMc/s) selected. It is claimed that the unit is particularly

Right: Encapsulated fixed inductors (Orega).

Below: Pair of i.f. coupling transformers for transistor printed circuits. Q>160; dimensions 20 x 13 x 13mm (Orega).



ber of new signal sources made their first appearance. Metrix were showing a response curve tracer for v.h.f. covering a frequency range of 5 to 220Mc/s and comprising an assembly of wobbulator, marker and c.r. oscilloscope units which can be used separately. Férisol have added two new high-level (40mW) oscillators to their

range of microwave signal generators:

Type OS501 (4 to 8kMc/s) and Type





Transistor a.f. generator and transistor frequency meter (0 to I Mc/s) shown by S.E.C.R.E.



Test instrument for routine measurement of carrier lifetime in semiconductors (J. L. Amiot).

suitable for airborne and space applications (rechargeable nickel-cadmium batteries can be used if the duration—100 hours—of the mercury batteries is inadequate). The frequency stability is suitable for a Doppler system local standard, and amplitude modulation can be applied through variation of the varactor

Ribet-Desigrations were showing a new signal generator (428A) with a

Response curve tracer for v.h.f. (Metrix).

constant-level output ±2% over the frequency range of 100kc/s to 30Mc/s and a laboratory type wobbulator and oscilloscope (411A) covering 0 to 320Mc/s in three ranges. Modulation is ±10Mc/s for the middle range (80-160Mc/s) and ±20Mc/s for the upper and lower ranges. Solartron were showing a double-beam oscilloscope (CD1016) for rack mounting, covering 0 to 5Mc/s and also a portable double - beam oscilloscope (CD1014). Another interesting Solartron portable instrument shown at this exhibition for the first time was a transistor direct-reading frequency and capacitance meter covering 0 to 10(k2/s in seven ranges and 0 to 0.3µF in six ranges.

Equipment for the routine testing of carrier lifetime in semiconductor specimens has been developed by J. L. Amiot. It makes use of the fact that intense illumination can be used to produce minority carriers. The



Above: Transistor noise level meter for hand or stand (L.E.A.).



specimen under test is placed over a hole in a horizontal shelf on the front of the instrument and connected in series with a resistance to a d.c. source. Light from a flash tube with a pulse duration of, typically, 10-7sec is concentrated by a mirror and lens system on the underside of the specimen. The output signal from the specimen triggers a sawtooth time base which runs until the signal falls to 1/e of its initial value, when the time-base voltage rise is stopped and the time-base returns to zero. sawtooth maximum is read by a peak voltmeter which is calibrated to give direct readings of carrier lifetime.

Incidentally, a small portable flash stroboscope was chosen by Ferranti as an example of an application of their four-layer p-n-p-n switching diodes.

diodes.

Sound level meters were shown by several firms. Many of these are transistor instruments, e.g., the "Minophon" pocket instrument made by the Swiss firm of Ing. Heinrich Spyri S.A. which measures only 125 × 85 × 40mm; and the Sonometre S.S.T.1 made by Laboratoire Electro-Acoustique (LEA) which incorporates checking facilities for battery voltage and amplifier gain.

voltage and amplifier gain.

A "wireless" microphone demonstrated by Sennheiser made use of a transistor pocket f.m. transmitter work ng on 35Mc/s and was effective at considerable distances from the stand under adverse exhibition conditions, showing no signs of interference pick-up.

Sonocolor mounted an effective demonstration of magnetic recordings as revealed by the Bitter technique, of applying colloidal iron oxide and then viewing the patterns produced on the screen of a projection microscope.

Many interesting audio exhibits were seen, but as these were also shown at the Festival of Sound in the Palais d'Orsay in March they are described elsewhere in this issue.

Response Curves and Tone Quality

By M. G. SCROGGIE, B.Sc., M.I.E.E.

AMPLITUDE/FREQUENCY response curves have had their ups and downs, in more senses than one. Until about 1925 the reception of programmes by radio was considered so wonderful that it would have seemed churlish to criticize the quality of reproduction. Effort was still being concentrated mainly on the feat of being able to hear them at all. But as the art of amplification reached the stage of ensuring adequate volume, people began to get quality-conscious. Technical enthusiasts, then as now, were unimpressed by the inevitable slogans—"Perfect Tone," "Reproduction Absolutely Indistinguishable from the Original Performance," etc.—and wanted scientific evidence. This first came in the form of amplitude/frequency response curves, hereinafter to be called just "response curves."

The typical a.f. amplifier of the period comprised two transformer-coupled stages (sometimes more than two!), the response curve of which consisted mainly of a fairly sharp peak somewhere in the range 1-3 kc/s. Clearly such curves were commercially unpublishable, but may have had something to do with the rapidity with which amplifier design began to progress. What the amplifier was doing below 300 c/s—or not doing, more likely—was at first concealed by the linear frequency scale (Fig. 1).

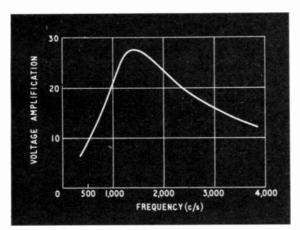


Fig. 1. Response curve of a single-stage transformercoupled amplifier dated 1925.

Ferranti deserve remembrance for their pioneering of level-response a.f. transformers and publication of logarithmic frequency curves (if they could be called curves in their casel) with which to commend them factually. Soon, however, the development of r.f. tetrodes was to render a.f. transformer coupling unnecessary, and resistance coupling gradually superseded it. By about 1927, a.f. amplifiers had so much improved that even overall response curves began to be worth advertising. And so the passion

for high-quality sound reproduction gained momentum. Loudspeakers were still extras, however, externally connected and not included in the price of a broadcast receiver, so naturally they did not come within the scope of the response curves—which was fortunate for the advertisers.

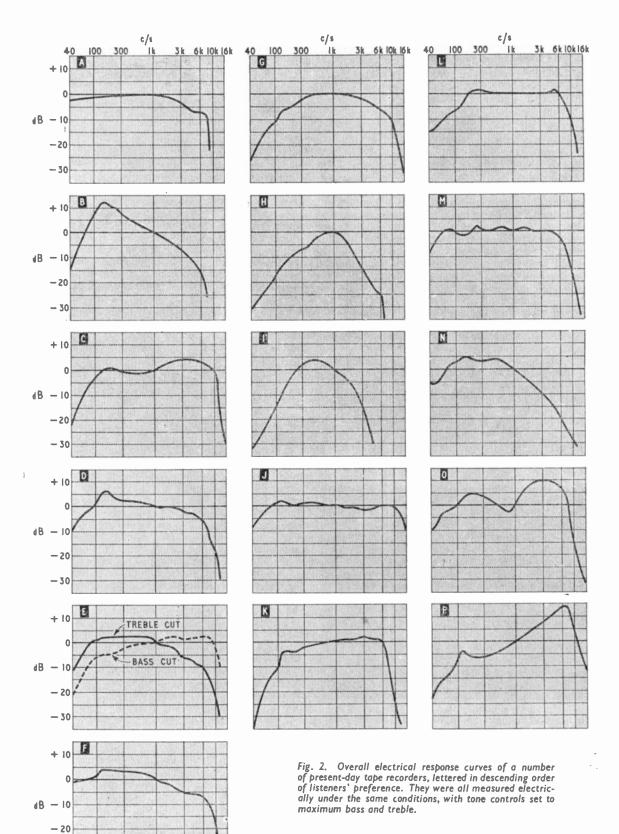
For some years a response curve was almost the only available objective index of tone quality, and enthusiasts attached great importance to ironing out every fraction of a decibel departure from perfect horizontality, regardless of what the loudspeaker and listening room were doing—a striking example of straining at a gnat and swallowing a camel. Some attention was beginning to be given to non-linearity, but mainly among the technical avant-garde. Outstanding was an article by J. H. O. Harries¹ in which he brought forward experimental evidence that the largely third-harmonic distortion generated by pentodes sounded worse than the same amount of triode distortion (mainly second-harmonic).

As the frequency range of a.f. amplifiers—and to a lesser degree other equipment such as pickups and loudspeakers-continued to be extended, a controversy arose as to the desirability or otherwise of such development, especially at the top end of the scale. Some held uncompromisingly that the higher the fi-er; others, while generally conceding this as an ideal, argued that noise, interference, and (dare one whisper it?) distortion made it expedient to cut off everything above, say, 5,000 c/s. Capt. P. P. Eckersley had, as usual, a memorably picturesque way of putting it—"The wider the window is opened, the more dirt comes in." This controversy, challenging the validity of the response curve as a measure of fidelity, reached a peak of intensity in the correspondence columns of Wireless World during 1932, and continued indecisively until smothered by the outbreak of war.

The end of the war released a greatly augmented number of enthusiasts, amateur and professional, to pursue the search for perfect sound reproduction. Almost at once the "flat from 20 to 20,000" school of thought—and with it the prestige of the response curve—received a severe blow by the publication of experiments by Chinn and Eisenberg² which produced an impressive mass of evidence to show that few listeners had any use for reproduction of frequencies outside 70-6,500 c/s, and many chose to be restricted to 150-4,000 c/s. This was what a lot of people, including the more successful manufacturers, had believed for a long time, but it was no doubt comforting for them to find that their heresy had suddenly become respectable.

As was to be expected, the orthodox reacted vigorously, and many attempts were made to discredit the findings of Chinn and Eisenberg. The

[&]quot;Amplitude Distortion," Wireless Engineer, Feb. 1937, p. 63.
"Tonal-range and Sound Intensity Preferences of Broadcast Listeners," Proc. 1.R.E., Sept. 1945, p. 571.



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-30

main weight of the attack was launched against their statement that distortion from the equipment used for the experiments was imperceptible to the most highly critical listener. Clearly (it was said) the lack of enthusiasm for the widest window must have been due to harmonic and intermodulation dirt too fine to be detected as such but nevertheless spoiling the reproduction. Otherwise—and this was their trump card—the original sounds themselves would be unacceptable if heard with their full natural frequency range.

Direct Hearing

Not long afterwards H. F. Olson³ took them up on this point by testing listeners' preferences in the same room with the original sounds, no electrical apparatus being used. It was something of a shock to read that about a third of the listeners preferred to hear the music and speech restricted to a top frequency of 4,000 c/s by means of an acoustical filter. The shock was considerably allayed when one read on and learned that from overhearing the comments made afterwards by the listeners it could be concluded that those who voted for the restricted hearing were mainly those who disliked the programmes anyway, so would naturally be glad to hear as little of them as possible. That even a small minority should prefer sounds to be muffled—especially speech, which is so often heard naturally that nobody would regard loudspeaker reproduction as the standard-does, however, seem to call for some explanation by the authorities who insist that anything less than 15,000 or even 20,000 c/s is not good enough.

The difference between the results of the two sets of experiments-especially if allowance is made for those who were merely using the only means open to them to protect themselves from Mr. Olsen's programmes—is sufficiently marked to give possible or even probable support to the unmeasurable-distortion theory. It seems that many listeners who prefer to hear original sounds with all their crispness would reach for the "top cut" control if they were presented with even the highest-fi reproductions of them. Complete proof is lacking, however, because Chinn and Eisenberg's reproductions were monophonic, and it can be argued that the difference between this and direct (or stereophonic) hearing may affect the preferred frequency range. So far from stopping to straighten out this tangle, I am pausing, just long enough to add the observation that members of my family consistently tolerate much more "modern" symphonic music when they hear it direct than via hi-fi. But that may be merely because their attention is diverted by the antics of the executants.

The last decade seems to have brought forth little to aid interpretation of response curves or restore confidence in them. Nevertheless, and in spite of the obstinate refusal of the ordinary listener to prefer what he ought to prefer—full frequency range reproduction—there is still a tendency to assume that the higher the top frequency that can be advertised the higher the "fi" it implies. Recently I had occasion to see some frequency response measurements on tape recorders which were also judged by

systematic listening tests, and thought a comparison might be instructive. The tests were carried out under the auspices of the Consumers' Association Ltd.

Measurements and tests were made under like conditions on all models, and (with exceptions to be mentioned) the listening tests were under conditions similar to those for the response measurements. All were at 3½ in/sec tape speed.

The measurements were made by recording sinusoidal signals at 27 frequencies from 40 c/s to 16 kc/s, the a.f. source being connected to the microphone input. The tape was then played back and the power output into rated load was measured. The ratio of output to input overall was expressed in dB relative to that at 1 kc/s. Tone controls were set to give maximum bass and treble, except Model E, in which there was only a single tone control, which was set at its extremes and two separate curves taken.

The listening tests likewise embraced recording and replay, and also the microphone and loudspeaker included in or prescribed for the recorder; this of course was a significant difference in conditions. Another difference was that the tone controls were adjusted by the panel of three listeners to what they judged to be optimum settings. In each case one male and one female speaker were recorded "live," and also some piano playing. The tone quality for each was separately assessed by each of the listeners, who awarded marks out of 100. They were not aware of the names of the machines being heard, or of their measured characteristics. Scores were weighted in the ratio 2 to 1 for piano and speech respectively. The results quoted here are the overall averages for the panel. In most cases the three listeners' scores were reasonably similar, but a minority showed a wider spread from average.

The response curves are arranged in Fig. 2 in descending order of listener preference. The corresponding average scores are as follows:

Model	Score	Model	Score
Α	58		35
В	57	J	34
C	51	K	34
D	51	L	32
Ē	48	M	32
F	47	N	30
G	38	0	29
H	37	Р	16

To forestall one query that might be made on comparing the curves with this table, mention should be made that harmonic distortion measurements were also carried out, but do not shed any certain light on the matter. For listening, the output level was kept low, in a room of average domestic size.

One's first conclusion, especially after noting the widely different placings of B and N despite the similarity of their curves, might well be that response curves couldn't matter less. More mature consideration is likely to reduce this to some such statement as that response curves are not an entirely safe index of tone quality. With regard to B and N in particular, it should be mentioned that they were about the least consistently judged, and also that the excessive bass

^{3 6} Frequency Range Preference for Speech and Music," J. Acous. Soc. Amer., July 1947, p. 549.

in B could be and probably was reduced by the listeners' tone adjustments. A more damaging comparison is that between the exemplary curve of M

and its mediocre placing.

The first definite conclusion could be one in harmony with Chinn and Eisenberg—that response above 7 kc/s is not essential for pleasing reproduction (note A and B). Furthermore, an excess of very high frequencies is particularly distasteful (P). A more puzzling conclusion is that a very narrow response, so long as it comes well in the middle (H and I), is not wholly unacceptable to listeners; it can in fact be preferred to more level curves (J, K, L and M). An interesting point is that in general the machines with the most level curves were the most consistently judged by the listeners.

Almost certainly the picture would have differed somewhat if the overall response tests had been really overall, including microphone and loudspeaker, and been measured at the listeners' tone control settings; but since most of the response curves presented by manufacturers are obtained under conditions similar to those shown here, the general conclusions stand. It is doubtful whether they would have been far out even if the conditions had been

identical to those for listening.

Audio Festival Exhibitors

MANUFACTURERS from the Continent, Japan and the U.S.A. are among the 72 exhibitors at the International Audio Festival, which opens at the Hotel Russell, London, W.C.1, on April 6th, for four days. In addition to the usual demonstration room for each of

AKG Acoustical Allied Records Ampex Armstrong Audio Fidelity Aveley Electric

BASF Brenell Engineering British Ferrograph

Challen Instrument Co. Chapman (Ultrasonics) Chitnis Electronic A.G. Ciné Accessories Clarke & Smith Collel Cosmocord

E.M.I. Records E.M.I. Sales & Service

Faraday Electronic Insts. Fi-Cord (Distribution) Field, N. S. B.

Garrard Gevaert Photo-Reproduction Goodmans Gramophone Co. Grampian Grundig

Leak Lowther Lustraphone

M.S.S. Recording Magnavox

Minnesota Mining & Mfg. Mullard Multimusic

Orr Industries

Pamphonic Philharmonic Records Philips Projection

Radford Electronics Robuck Electrical Industries Rogers Developments Rola Celestion

S.M.E. S.T.C. Schwarzalder Uhrwerke-Fabrik Burger Shure Simon Sound Equipment Sony Sony Sugden

Tannoy Tape Recorders Telefunken Teppaz

Veritone Vitavox Vortexion

Wellington Acoustic Labs. Wharfedale Whiteley Electrical Wyndsor Recording Co.

Zonal Films

the manufacturers listed there will be an audio theatre, seating 200, in which frequent lecture-demonstrations will be given.

Tickets for the Festival, which is open from 11.0 to 9.0 each day, are obtainable from manufacturers, audio dealers or from Wireless World. Until 4.0 on the first two days admission is restricted to the trade.

CLUB NEWS

Barnet.—H, W. Pope (G3HT) will speak about d.f. gear to members of the Barnet & District Radio Club on April 28th. The club meets on the last Tuesday of each month at 8.0 at the Red Lion Hotel.

Birmingham.—April meetings of the Slade Radio Society include a talk on the 7th on transistors by N. B. Simmonds and another on the 21st on 2-metre amateur gear. The club's first d.f. contest of the year will be held on April 23rd. Slade Radio Society meets at 7.45 at Church House, High Street, Erdington.

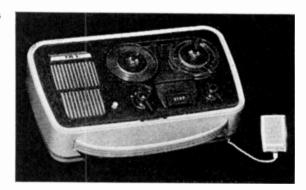
Bury.—Future meetings of the Bury Radio Society will be held at 8.0 at The Knowsley Hotel, Kay Gardens. At the April 11th meeting K. Taylor (G3NNW) will talk on "My First Eighteen Months."

Derby.—Meetings of the Derby & District Amateur Radio Society, which incorporates the Derby Wireless Club formed in 1911, are held each Wednesday at 7.30 at 119 Green Lane.

Guildford.—Maurice Child will speak on "The Early Development of Radio" at the April 13th meeting of the Guildford and District Radio Society, which meets on the 2nd Thursday and 4th Friday of each month at 7.30 at the City Cafe, Onslow Street.

Halifax.—At the April 4th meeting of the Halifax & District Amateur Radio Society H. Swift (G3ADG), the club's chairman, will speak on efficiency modulation. The society meets on alternate Tuesdays at 7.30 at the Sportsman Inn, Ogden.

Leeds.—Mobile equipment is the topic of the talk to be given to H. Brooks (G3GJV) at the April 12th meeting of the Leeds Amateur Radio Society. Meetings are normally held at 7.45 each Wednesday at Swarthmore Education Centre, 3 Woodhouse Square, but on April 26th members are visiting the Batley Works of Fane Acoustics.



Transistor Battery Tape Recorder recently introduced by Grundig, the TK1, is shown in the photograph. At the operating speed of $3\frac{3}{2}$ in/sec the frequency response is 80 to 8.000 c/s \pm 3dB and the total wow and flutter 1%. The output power is 250mW. High-frequency bias is used and permanent-magnet erase. The weight of this recorder is 8lb and its dimensions $11\frac{3}{4}$ in by 7in by $4\frac{1}{2}$ in.

Aspects of design

This is No. 33 in the series of articles dealing with advanced problems in circuit design published by The Ediswan Mazda Applications Laboratory. No. 34 will appear next month. We shall be pleased to answer queries arising from this or other articles. Reprints of the first twenty-four articles, in booklet form, are available on request.

RF TETRODE FOR TELEVISION **TUNERS**

The use of a tetrode valve in the RF stage of a television tuner offers certain advantages over the more conventional double-triode cascode arrangement. With the tetrode the number of circuit components required is smaller, the layout is simpler and for valves having comparable mutual conductance the single

cathode type valve can be manufactured more economically.

A serious disadvantage of the multi-electrode valve as an RF amplifier for television has been its inferior noise performance compared with a triode. This is due to the presence of an additional noise source in the tetrode arising from the random division of the electron stream passing through the screen grid, the added noise, referred to as partition noise, increasing with screen current. This subject has been dealt with more fully in "Aspects of Design No. 32."

It follows that if the ratio of screen current to anode current can be kept as low as possible the effect of partition noise will be minimised and the noise of a tetrode then becomes low enough for this type of valve to be worthy of consideration as an RF amplifier for television. While it is possible to design tetrode valves in which the screen current is less than 10% of the anode current; must be remembered that the primary purpose of the current it must be remembered that the primary purpose of the screen grid is, in fact, to screen the input or control grid from the anode and thus reduce the g₁-a capacitance. Therefore although the screen current to anode current ratio can be made extremely low, with a corresponding reduction in tetrode noise, there is a

limit to the extent to which this can be taken.

This limit is reached when any further reduction of screen current brought about by opening the winding pitch of the screen grid electrode increases the g₁-a capacitance to such an

extent that instability may occur in operation.

It has been found that in the case of a high slope tetrode, an acceptable compromise between low partition noise and good screening can be obtained by designing a valve in which the g₁-a capacitance does not exceed 0.05 pF, giving a screen to anode current ratio of about 12%. It is then possible to use the tetrode successfully without any form of circuit neutralisation and obtain an acceptable performance. With frame grid techand obtain an acceptable performance. With frame grid techniques, a valve to the above specification can be manufactured with a high slope per milliamp of anode current resulting in a high gain stable RF valve with a noise performance much superior to that of a conventional pentode and nearly equal to that of a double triode cascode amplifier such as the 30L15.

The Ediswan Mazda tetrode that has been designed along these lines is the frame grid type 30F27 which is a VHF tetrode having variable any characteristics for reducing cross-modulation.

having variable-mu characteristics for reducing cross-modulation effects and a nominal mutual conductance of 15 mA,V at an anode current of 13.5 mA and a screen current of 1.7 mA.

CIRCUIT RECOMMENDATIONS FOR THE 30F27

The chassis layout for the 30F27 should follow the normal pattern for a VHF amplifier. It should have a well-fitting screen, going across the valveholder between grid and anode circuits and it is essential that the valveholder has a central earthed spigot.

The 30F27 can be used in a circuit with either grid current bias or cathode self bias, the latter giving the greater degree of anode current stabilisation with a normal spread of valve characanode current stabilisation with a normal spread of valve characteristics. However, stabilisation is satisfactory with grid current bias providing the screen supply is obtained from the lower potential end of the anode decoupling resistor (Fig. 1). This ensures that the screen voltage is controlled largely by the total current instead of being controlled only by the screen current. The high value of screen dropping resistor (33 k Ω) prevents the screen dissipation being exceeded should the valve be run without anode voltage. This can occur, for example, in a turret tuner when no band-pass segment is engaged. Moreover with grid current bias a further simplification of the circuit is obtained and a greater economy in the use of components can be effected. and a greater economy in the use of components can be effected.

The circuit recommended for the 30F27 when using grid

current bias is shown in Fig. 1, with decoupling resistors suitable

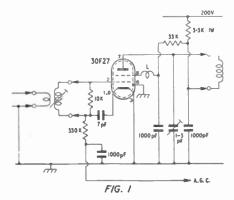
Associated Electrical Industries Ltd

Radio and Electronic Components Division Technical Service Department 155 Charing Cross Road, London, W.C.2 Tel: GERrard 9797 * Grams: Sleswan Westcent London for a 200 V high tension supply. The following points should be noted:-

 The screen voltage is dropped to 105 V to give an anode current of 14.0 mA with the relatively low bias voltage obtained from grid current which is of the order of 2 µA.

ii. To minimise feedback due to cathode lead inductance the cathode of the 30F27 is brought out on three separate pins, 1, 3 and 9. For this circuit pins 1 and 9 are strapped externally and taken to the grid circuit while pin 3 is taken to chassis.

iii. A low value inductance (about 20 muH) is placed between g₂ (pin 8) and its decoupling capacitor to provide a small amount of regeneration on Band 1II.



ECONOMY IN CIRCUIT COMPONENTS WITH THE 30F27

Compared to the double-triode cascode circuit the use of the tetrode with cathode bias results in the saving of the following components:

(a) One resistor, previously required as part of the grounded grid potentiometer.
(b) Neutralising capacitor, usually 2 pF.

When using the tetrode under grid current bias conditions as shown in Fig. 1 there is a further saving, in that the cathode circuit decoupling capacitor (1000 pF) is not required. No cathode resistor is used but this is offset by the need for an additional resistor in the grid circuit.

COMPARATIVE PERFORMANCE OF THE 30F27, 30L1 and 30L15

The typical performance to be expected from a television tuner using the 30F27 and 30C15 is given in Table 1 with comparative figures for the 30L1 and 30L15 in place of the

TABLE 1

Channel		301	F27	30L1 30L1		L15	
	Chamic	Gain dB	Noise dB	Gain dB	Noise dB	Gain dB	Noise dB
	2	51	5.0	46	4.0	50	3.3
	11	48	7.8	41	8.2	48	6.5

Gain figures are for open-circuit calibration (generator emf) Tuner mixer valve: 30C15

Transfer impedance of 1F transformer: 2200 ohms.
The 30F27 will handle a larger input signal without cross modulation than either the 30L1 or 30L15 and it provides an economical, high gain, stable RF amplifier for a tuner, with a noise performance that is found to be acceptable except for the most exacting requirements.

141

- 35

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8 H 8 VOLTS =

FAIR . p 2

TV TUNER HIGH SLOPE VHF TETRODE

EDISWAN MAZDA 30F27

The 30F27 is a frame grid VHF tetrode having a mutual

The 30F27 is a frame grid VHF tetrode having a mutual conductance of 15 mA.V at an anode current of 13.5 mA and a screen current of 1.7 mA with variable-mu characteristics to reduce cross-modulation effects at high signal levels.

This tetrode used in the RF stage of a television tuner offers certain advantages over the more conventional double triode cascode arrangement. For instance, the number of circuit components required is smaller, the layout is simpler and for valves having comparable slopes the single cathode type valve can be manufactured more economically.

Normally the noise performance of a tetrode is inferior to that

Normally the noise performance of a tetrode is inferior to that of a triode due to the presence of partition noise arising from the screen current. However the 30F27 has been specially designed to provide a low ratio of screen to anode current to minimise the effect of partition noise while still retaining good screening between control grid and anode. When this is used in conjunction with frame-grid techniques a high slope per milliamp of anode current can be obtained resulting in a high gain RF valve with a noise performance much superior to that of a conventional pentode and equal to that of a double triode cascode amplifier such as the 301.1.

Heater Current (amps) Heater Voltage (volts) 3.7

TENTATIVE RATINGS AND DATA

Maximum Design Centre	: Kati	ngs		
Anode Dissipation (watts)			pa(max)	2.5
Screen Dissipation (watts)			Pg2(max)	0.4
Anode Voltage (volts)			Va(max)	250
Screen Voltage (volts)			$V_{g2(max)}$	230
Heater to Cathode Voltage	(volts	rms)	$V_{h-k}(max)$	rms 90*
Cashada Cumana (A)	٠		Ik(max)	18
* From cathode to	higher	noten	tial heater r	nio.

Inter-electrode Capacitances (pF)† Input Capacitance
Output Capacitance 6.3 Cin 1.8 Cout

Grid 1 to Anode Grid 1 to Grid 2 0.027 C_{E1-8} . . Cg1-g2 2.0 Grid 1 to Cathode 4.0 Cg 1-k † Measured in fully shielded socket, without can.

22.2

Maximum Dimensions (mm) Overall Length Seated Height 49 . .

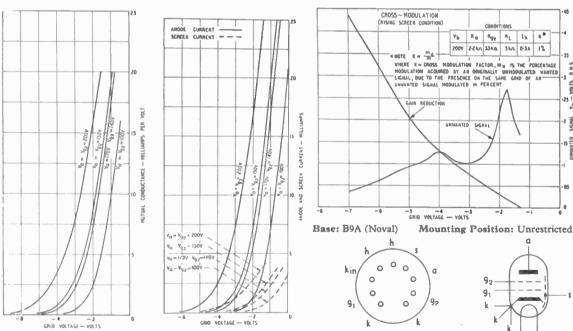
Diameter

TYPICAL OPERATION					
		Cathode Self Bias Circuit	Grid Current Bias Circuit		
Supply Voltage (volts)	$V_{\rm b}$	200	200		
Anode Voltage (volts)	V a	170	150		
Screen Voltage (Initial) (volts)	Vgc	140	105		
Anode & Screen Common	. 10.00				
Decoupling Resistor $(k\Omega)$		many	3.3		
Anode Decoupling Resistor (kΩ)		2.2			
Screen Decoupling Resistor (kΩ)		33	33		
Cathode Bias Resistor (Ω)	Rk	82			
Grid Current Bias Resistor (kΩ)	R_{g1}	_	330		
Grid Bias Voltage approx. (volts)	Vgi	- 1.25			
Anode Current (mA)	I a	13.5	14		
Screen Current (mA)	Îg2	1.7	1.4		
Mutual Conductance (mA/V)	g m	15	15.5		
Inner Amplification	g m	1.7	13,3		
Factor (g ₁ to g ₂)	4-10	60	_		
Equivalent Grid Noise	7 E 1 - E 2	00			
Resistance (Ω)	R	450			
Input Loss at 50 Mc/s (k Ω)					
Input Capacity Working (pF)	FRI-K(W)	10.3¶§			
Change in Input Capacity produce	od by	10.598	_		
biasing valve to cut-off (nF)	Ac. ()	2.0#	_		
biasing valve to cut-off (pF)	7 cin(w)	2.9¶			

Measured at 50 Mc/s with the three cathodes strapped and taken directly to earth.

§ Inter-electrode capacity with holder capacity balanced out.

Tentative Characteristic Curves of Ediswan Mazda Valve Type 30F27



Associated Electrical Industries Ltd

Radio and Electronic Components Division Technical Service Department 155 Charing Cross Road, London, W.C.2 97 Grams: Sieswan Westcent London Tel: GERrard 9797



VIEW OF FREE END

SOME THOUGHTS ON INDUCTANCE

HENRYS OR VOLT-SECONDS?

By THOMAS RODDAM

N recent months I have been constrained to think about a variety of devices in which a coil is wound on a piece of ferromagnetic material and a current is passed through the coil. The practice of my temperate youth was to restrict the current so that this system remained linear, or fairly linear anyway, air gaps and extra iron being added whenever it became necessary to avoid the unwanted non-linearities. The characteristic property of such an arrangement is, of course, its inductance and it has become a matter of habit to assume that a thing having this sort of construction will also have associated with it the inductance-property, the idea of an inductance, the pure characteristic to which in this imperfect world we can only approximate.

There are now, however, a number of what appear to be inductance-devices which seems to have lost this old, this familiar, inductance property. Clearly the essential characteristics of a coil wound on a ferromagnetic core are unaltered by the circuit in which it is connected and the desect must therefore be one of understanding. One great aid to clarity of thought is freedom from reference books: it is therefore my practice annually to abandon my library and retire to some inexpensive retreat where the gentle susurration of the rain and the heavier patter of the boots of a large but inefficient hotel staff can encourage the search for comprehension.

What, then, is an iron-cored coil? Digging into memory I recall that the passage of a current produces in the core a magnetomotive force, H, which is proportional to the current and to the number of turns and which is the same sort of thing as an

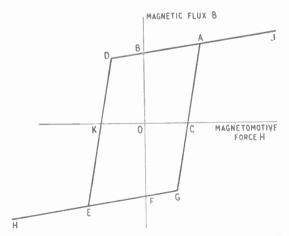


Fig. 1. Idealized B-H characteristic of a "square-loop" ferromagnetic material.

electric field in that it is proportionately diluted by the length over which the current acts. In fact

$$H = 4\pi NI/10l$$

The effect of this magnetomotive force H is to produce a magnetic flux. This is where the energy is stored in the magnetic system. We commonly write the simple equation

$$B = \mu H$$

to express the connection between the flux and the m.m.f. but although I quote this highly memorable equation further exploration shows that its use is attended with some danger.

A safer approach is based on the fact that when we change the flux which links the turns of a coil we produce a voltage across the terminals. The equation connecting these factors is

$$V = NA \cdot 10^{-8} \cdot dB/dt$$

where A is the area.

From these two equations we can go on to consider the very important term dI/dt. Since

$$I = (10l/4 \pi N) H$$

$$\frac{dI}{dt} = (10l/4 \pi N) \frac{dH}{dt}$$

Now let us define the inductance by the equation

$$LdI/dt = V$$

and we find that

$$L = \frac{NA \cdot 10^{-8}}{(10l/4\pi N)} \cdot \frac{dB/dt}{dH/dt}$$

$$= \frac{4\pi N^2 A \cdot 10^{-9}}{l} \cdot \frac{dB/dt}{dH/dt}$$

$$= \frac{4\pi N^2 A \cdot 10^{-9}}{l} \cdot \frac{dB}{dH}$$

When $B = \mu H$ we obviously have $dB/dH = \mu$ and the expression for the inductance has a similar form. When, however, this simple proportionality between B and H no longer holds the expression for inductance in terms of dB/dH is still true. The only trouble with it is that it depends on this differential term, which in strictness we must remember is actually (dB/dt)(dH/dt). This is by no means a pedantic distinction, as we shall see at a later stage. It retains in our equations the very important element of time. For engineering purposes you cannot put the clocks back and any expression containing time has built into it an arrow showing which way you are going.

Let us now look at the sort of relationship which we may encounter between B and H with some of the specially prepared ferromagnetic materials. The typical form is shown in Fig. 1, and it will easily be appreciated why materials which give a close approximation to this are called "square-loop" materials. First of all note that there is no indication in this diagram of what happens near the origin. This is rather a consequence of the way in which the square-loop materials are used than of their properties. In the region of the origin there is, in fact, a fairly conventional high-permeability loop. When used in this way a coil wound on such a core has an inductance of conventional meaning. One material which is of value in both modes is Mumetal.

In considering the square-loop behaviour of a core of this kind it is most convenient to start off by passing a very large current through the coil so that the flux is brought up to the point J. We now reduce the current without reversal to zero and after passing through A we follow along the line AB to the point B. Here the magnetomotive force H, and equally the current, is zero, so that we can disconnect the circuit. The core, however, remains magnetized with a stored flux B.

Connected back in circuit we apply a small current in the reverse direction along the path BD. The change in flux is very small so that the inductance, as we have defined it, is also very small. As we continue to increase the current we reach the point D. Quite suddenly dB/dH changes to a very large value, for the jump in flux from D to E involves only a small change in magnetomotive force. The inductance for this region traversed in this direction is very high. When we reach E we turn sharply again towards H and the inductance is again low since EH is almost parallel to the magnetomotive force axis.

The description of the changes in inductance in the last paragraph depends on our definition of inductance in terms of the volts per ampere per second, the tendency of inductance to prevent changes in current. We could also consider inductance in its energy storage character: if a current is flowing through an inductive element the stored energy is LI2. It is this property which makes inductance such an important element in filter theory, where the network elements must hold the energy introduced at stop-band frequencies and then force it back to the generator. I would remind you that a filter using only inductance and capacitance cannot actually attenuate a signal passing through it as there is nowhere for the energy to be dissipated. Such filters operate by presenting a reactive load to the generator in the stop band so that the energy is all flung back.

In this sense of inductance the word seems to have practically no meaning when the device is operated

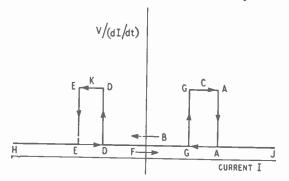


Fig. 2. Measured properties of two-terminal device with current drive.

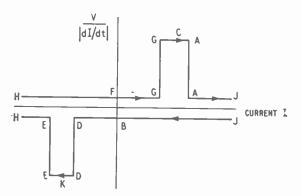


Fig. 3. An alternative way of drawing Fig. 2.

round the loop shown in Fig. 1. The stored energy has become virtually inaccessible and certainly unpredictable for any pattern of current other than a regular full excursion from H to J and back again. The energy which we force in up the path GCA is locked up in the remanent flux at the point B when we try to get it back: to move from C to A we find we are putting energy into a high inductance device and the small current (and m.m.f.) change takes a good deal of energy but when we try to get it out again the device decides to be a low-inductance one. It is all rather like the operations of a bucket shop or some new fairy story in which the princess when kissed turns into a frog, though these columns are no place for comments on marriage.

By now, no doubt, several familiar figures are reaching for their reference books, their slates and pencils. How many readers, I wonder, traced their first faltering characters, to the accompaniment of excruciating squeaks, on the economical slate: how long before their children complain that electric typewriters have not been provided for every infant in the village school? But s.f.f. are on my track with the revelation that if I consult Ezekiel Spanheim I shall find a clear definition of inductance which will dispose of all these difficulties. This I do not doubt, but neither do I doubt that the trick of producing such a clear definition is to restrict one's thought to ideal linear systems. Once we do this it is not really important which definition we adopt, since the alternatives can be easily and unambiguously derived.

What is the circuit designer to do? He is not concerned with magnetic flux and magnetomotive force: he has a black box with two terminals and has to define its properties in terms of voltage and current at these terminals. As a user of this black box it is merely vulgar curiosity which excites him to enquire why the behaviour is as he finds it. There are two experiments which he can profitably conduct. These will define the properties of his two-terminal device in a form which he can use.

In the first experiment a source of current is required. This, of course, is a circuit which produces a specified current no matter what the impedance through which the current must be driven may be. There are a number of ways of approximating to this: the simplest is a sufficiently high voltage source in series with a sufficiently high resistance, while in more sophisticated versions the high slope resistance at a pentode anode or a transistor collector can offer the wanted approximation with economy

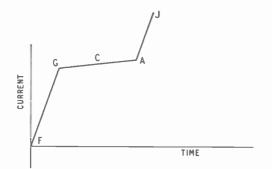


Fig. 4. Measured properties of two-terminal device with voltage drive.

of voltage. I do not think we need to explore the details of a suitable circuit here.

We set the current at a substantial negative value, corresponding to the point H and then increase it. "Increase" is used here in a strictly formal way to mean that dI/dt is positive: numerically the current shown on a meter, which is |I|, will fall to zero and then rise in the opposite direction. We measure the voltage across the terminals and we also measure, or fix in advance, the rate of change of current with time. Let us assume that we have arranged matters so that dI/dt is constant. Then, equally, as we allow (and what else can we do, indeed) the passage of time, H increases steadily, with dH/dt also constant. (Again, since dH/dt is positive, I use "increase" From H through E, F to G we have dB/dt which is constant and small, so that we observe a small and constant voltage across the terminals. At G there is a sudden change. As we go along G, C to A the terminals voltage becomes very high but at A, and as we progress towards J it drops again. The voltages we observe are proportional to dB/dt, and thus proportional to dI/dt. We can therefore plot the diagram of Fig. 2. This may be more familiar to some readers in the form shown in Fig. 3 which takes account of the fact that to traverse the system from right to left we must have dI/dt negative and we shall therefore observe a negative voltage across the terminals. This effect is slightly obscured in Fig. 2.

In a second experiment we apply a constant voltage to the terminals and observe the current. We shall assume that initially we are at the point F of Fig. 1. As we have already said, the rate of change of magnetic flux is proportional to voltage and since the voltage is constant the flux must be changing at a constant rate. The projection of the working point on the B axis moves steadily upwards. There is a rapid transition from F to G, associated with a rapid rise in current but then as we move along G, C to A the current changes very little. Once A is reached only a short time is occupied by the run along AJ towards unlimited current. This is the pattern shown in Fig. 4.

The important feature of the current-time characteristic at constant voltage is the plateau GCA. Since we have $V = NA.10^{-8}dB/dt$ and V is constant we can integrate this very easily to get

$$Vt = NA.10^{-8} (B_1 - B_0)$$

where B_1 and B_0 are the values of flux corresponding to the points A and G respectively. (B_1-B_0) is equal

to the spacing between points B and F, or twice the remanent flux B_{r-1} A coil of N turns of area A on a material having a remanent flux B_r has therefore a characteristic

It may be useful to notice the sort of values to be expected. A coil of 1,000 turns will give volts-seconds products in the region of 1-10 volt milliseconds while draining away only milliamperes. Thus such a coil might take an almost constant current of a few milliamps for perhaps 10 milliseconds and then allow some hundreds of milliamps to flow. With only a few turns the characteristic will be a few volts-microseconds and the current required to reach the point G will be some hundreds of milliamps.

For many practical applications we do not operate with ideal voltage or current sources but with sources of finite (which means in practice comparable with the load) impedance. Let us consider a source of voltage V₀ and resistance R₀. Now in Fig. 4 the step from F to G is very short and we can therefore get a quick picture of the sequence of events by assuming that there is somehow a jump to a constant current Io which is the value for the whole GCA plateau. When the generator is first connected the full voltage V₀ appears across the coil but as soon as the current I₀ is established the voltage across the coil falls to (V_0-I_0R) . This value remains constant for a time $(2NAB_r.10^{-8})/(V_0-I_0R)$ and then the current through the coil increases rapidly and, if the coil resistance can be neglected the current rises to V₀/R and the voltage drop across the coil is zero. This is shown in Fig. 5. The idealized characteristic shown in Fig. 5(b) can be turned into a closer approximation by replacing the three linear segments by the exponential which would be calculated using the appropriate values of inductance, defined in terms of the value of dB/dH for the corresponding segment.

It is this property of square-loop materials which has led to their widespread use in transistor squarewave oscillators which are now becoming popular as inverters for producing an a.c. supply from a battery source and, by extension, producing high

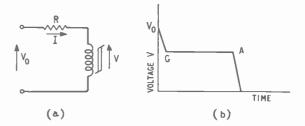


Fig. 5. The voltage with a finite source resistance.

voltages by the subsequent transformation and rectification. In these circuits the duration of each half-cycle is fixed by the plateau A Fig. 5(b). Another way of looking at these circuits is to consider them to be LR multivibrators, with a very large inductance corresponding to the steep slope of GCA in Fig. 1. The half-cycle time, which depends upon L/R has barely begun, and the characteristic sag is only just discernible, when the core reaches its limit at A. The inductance changes to a very small

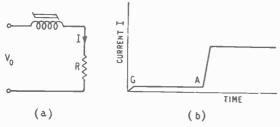


Fig. 6. The current into a finite resistance fed from a fixed voltage through a saturable choke.

value and the remainder of the half-cycle is performed with a very small L/R value.

Another application is, of course, the memory core. We have seen that with no current applied we must be at B or F, depending on whether the last active point was J or H. Suppose we are at B. A current pulse, with positive current, will run up the track BAJ. The change of flux will not be very great so that the voltage generated in a winding on the core, which depends on dB/dt, will be small. But if the last state were F, this current pulse would traverse the path FGCAJAB and we can see from Fig. 2 or Fig. 3 a substantial voltage pulse would be produced. By setting the core to either B or F we can thus "write in" one bit of information, a yes or no, a 1 or 0, and can extract it at our leisure. Moreover, since a current, or more exactly ampere-turns, which does not carry us to G will not affect the setting at F but will let the core fall back again we can use several windings which must be simultaneously pulled to bring the information out. It is in structures of this kind that we encounter the cores switched in times measured in microseconds, perhaps using only single turns.

The memory cores are perhaps a couple of millimetres in diameter, the inverter cores the size familiar in ordinary low-frequency amplifier design. In yet another application, magnetic amplifiers, which find application in a wide field from aircraft

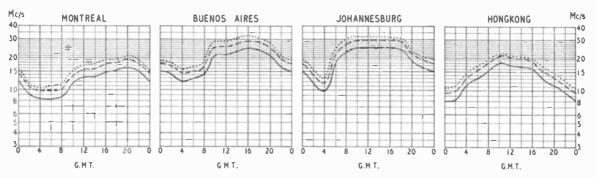
controls to the regulation of the supplies to large furnaces, the sizes range upwards from a few ounces into the hundredweights. Fig. 6 is merely a rearrangement of Fig. 5 with attention focused on the current through the resistor R. It will be seen that until A is reached there is only a small current in the load resistor. Suppose, then, that just as we reach A we reverse the voltage: we shall then traverse the path ABDKE with a similar, but oppositely sensed, current. At E we again reverse the voltage and this alternating voltage drives only a small alternating current through the load. Now let us, by means of another winding carrying a steady current, bring the starting point to C. To move from C to A under the influence of V₀ takes only one-half the time for the movement from G to A and so for the remainder of the time before the reversal the full current of V₀/R will flow in the load.

Having regard to the space I have already filled I do not propose to describe how the core is reset and how this second winding is disposed of so that, in fact, by the use of several windings on separate lines, it is protected from having excessive voltages induced in it. These matters of ingenuity are used to make practicable the magnetic amplifiers in which relatively small control currents affect the discharge of large powers into the loads by altering the fraction of a cycle during which the current is free to flow.

I had hoped that at some point in this study the idea of inductance would have forced itself in. It has not done so except as a means for improving some of the approximations and even then I am sure we could have managed without it. In its place we find a factor which has no name but which we might call endurance, the volts-seconds product before collapse. This is a very real characteristic of a square-loop cored coil and a much less sharply defined characteristic of a coil with a silicon iron core or with a small air-gap. It is a characteristic to which I fear we must all become accustomed. But how I wish it had a name.

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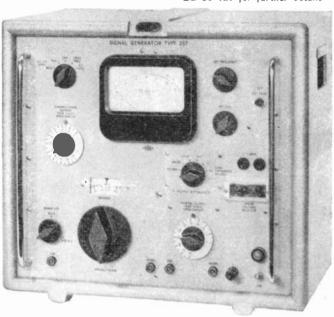
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Multivibrator Design

USE OF CONSTANT-CURRENT PRINCIPLE

By R. C. FOSS, B.Sc., Grad.I.E.E., and M. F. SIZMUR, B.Sc.

An engineer designing electronic circuits has a number of special problems which are not commonly met in other branches of engineering. One such problem arises from the use of valves and transistors, which have unavoidably wide tolerances on their characteristics. Steam engines manufactured with a tolerance of $\pm 50\%$ on piston diameter would hardly be expected to perform well or even work at all! However, it is often necessary to make electronic circuits perform reliably with tolerances of this order on transistor parameters. Evidently to achieve this aim, the performance of the circuit must be made as far as possible independent of the precise values of such parameters. The designer must use techniques which ensure that the behaviour of the circuit depends upon those components whose values are

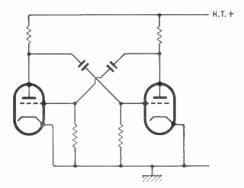


Fig. 1. Abraham and Bloch multivibrator circuit.

under his control, such as capacitors, resistors and inductors.

Because it is a comparatively easy task to assemble and modify a prototype, there is often a strong temptation to "design" circuits by cut and try This temptation should be resisted as this method has numerous drawbacks. there is no reason why the performance of a circuit arrived at by cut and try should be governed by the values of passive components and not depend critically upon valve or transistor parameters. The circuit may have this desirable property but most likely it will not. The second drawback is that the circuit can only be developed into a form suitable for production by an experimental investigation in which the effects of all tolerance changes are explored in a systematic manner. This may well turn out to be a lengthy process and there is always the possibility that at some late stage the circuit may be found unsuitable for production, necessitating a fresh start. Another drawback is that it will be purely fortuitous

if an optimum design is achieved at the first attempt, and it is impossible to tell how far away from the optimum the design is without experimental investigation. Lastly, the lack of a quantitative understanding of the way in which the circuit works may well complicate maintenance because of the difficulty in deciding whether it is operating correctly or not.

These difficulties may all be avoided if circuits can be designed which are not critical as to the precise values of valve or transistor parameters and whose behaviour is determined by the values of passive components. Experience shows that the design procedures for such circuits are often quite simple; the amount of effort needed may be reduced to little more than an exercise in Ohm's Law and the solution of the transient response of an R-C circuit!

The way to achieve this state of affairs is to use the valve or transistor as a switch with "on" and "off" states determined by passive components, the transition between states being governed by R-C timing circuits. The characteristics of the active element are thus involved only in the transition from one state to the other.

Because the multivibrator is one of the most useful and most widely known of waveform-generating circuits, it has been taken as an example to illustrate these techniques. Fig. 1 shows the Abraham and Bloch multivibrator circuit. Neglecting the time taken for change of state, the periodic time for this arrangement is the sum of the "off" periods for both valves. Fig. 2 shows the exponential waveform appearing on each grid in turn during its "off" period, E_0 being the initial value, E_1 the value at which the circuit changes state and T the circuit time constant. If the "off" period, t_1 , is to be accurately specified, it is necessary to fix E_0 and E_1 or at least the ratio of these voltages.

The appendix describes a simple method of finding

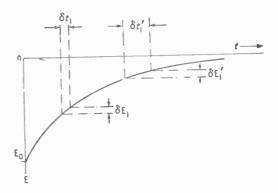


Fig. 2. Exponential waveform appearing in turn at each grid in Fig. 1 during its "off" period.

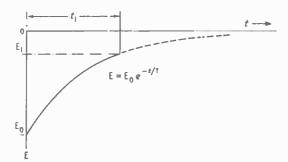


Fig. 3. Illustration of the important design point that E_1 should not be made too small relative to E_0 so that a small change in E_1 does not produce too large a change in t_1 .

 t_1 in terms of this ratio and the circuit time constant. It should be noted that if E_1 is made small with respect to E_0 , then small changes in the value of E_1 will produce disproportionately large changes in t_1 and hence in the periodic time of the circuit. Fig. 3 illustrates this point and it should be emphasized that this is most important in practice when E_1 is dependent on valve or transistor characteristics.

The basic multivibrator of Fig. 1 is not a "designable" circuit as it stands because the "on" state of the triode valve is made dependent on its characteristics, including the grid current/grid voltage relationship. Thus the change in anode potential between cut-off and cut-on and therefore the output amplitude and the starting point of the grid timing exponential are poorly defined. Furthermore, in this particular circuit the value of grid voltage, E₁, at which the transition occurs is small compared with the initial value, E₀, and is likely to change as the valves age or are replaced.

It has been shown by Williams (Ref. 1) that these unsound features of the circuit can be avoided by the use of "bottoming" pentodes to give a well-defined anode swing, and by returning the grid leaks to the h.t. positive rail to make changes in the effective grid base have little effect.

The circuit known as the long-tailed pair (Ref. 2) can be used to achieve equal case and soundness of design in a wide range of waveform circuits, while retaining the economic advantage of the triode, particularly the double triode. Although circuits employing feedback in a common-cathode resistor are fairly well known, it does not seem to be so well appreciated that it is possible to use this resistor to largely define the total cathode current, or "tail current" of the pair. The tail current in the circuit of Fig. 4 is given by:—

$$I_{T} = \frac{E_{T} + v_{k}}{R_{T}} \dots (1)$$

where the cathode voltage v_k is determined by the values of v_{y1} , v_{y2} , and the valve bias. Provided that these quantities, and changes in them, are made appreciably less than the fixed "tail voltage" E_T , say up to 20% of E_T , it will often be possible to take the tail current as constant.

$$I_{\rm T} \approx \frac{E_{\rm T}}{R_{\rm T}} \dots$$
 (2)

For waveform-generating circuits, this current is normally arranged to flow entirely in one or other of the pair, and this current is switched from one to the other by a differential voltage applied to the grids. To estimate the value of differential grid voltage necessary to produce this switching action, suppose that the valve characteristics of each of the pair are identical. Suppose also that a value of grid-cathode bias $-e_b$ is necessary for the valve to draw current I_T , and that a value $-e_c$ just cuts off the valve. As changes in anode voltage are not normally large, the effective grid base, defined as $(e_c - e_b)$, may be assumed constant. Considering again the circuit of Fig. 4; if v_{g1} is made zero and v_{g2} very negative, V2 will be cut off, and V1 will be conducting. By the assumption, the cathode potential is $+e_b$. If v_{a2} is now allowed to rise, then when it passes a value $-e_c$ relative to the common cathode, that is $-(e_c-e_b)$ relative to earth, V2 starts to conduct. With v_{g2} continuing to rise the cathode voltage increases until it reaches a value $+e_c$ when V1 will be completely cut off. The value of v_{g2} at this point is $(e_c - e_b)$, and it is seen that a differential change in grid voltage of two effective grid bases is required to switch I_T. This thermionic equivalent of the two-way switch has been very successfully used in the design of digital computors (Ref. 3).

The multivibrator about to be described, due originally to E. L. C. White (Ref. 4), can be thought of as just such a switch actuated by positive feedback through a timing network from one anode to the opposite grid (see Fig. 5). With this circuit the freerunning repetition rate is not well-defined, since it is very dependent upon the valve cut-off bias as shown in Fig. 3. However, this is an excellent circuit for use where a square wave synchronized to an external waveform is required. As it is the differential grid voltage which actuates the "switch", the synchronizing waveform is applied to the "free" grid (with acknowledgements to a well-known contributor to Wireless World!). This grid takes no part in the regenerative action, so it will not inject any signal back into the synchronizing circuit.

The anode of V2 also plays no part in the regenerative action, and from this anode an output can be taken without affecting the operation of the circuit, a feature which may eliminate the necessity for a buffer stage.

To analyse the operation of the circuit, a few

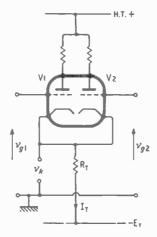


Fig. 4. Long-tailed pair circuit.

additional assumptions will be helpful. These are:-

 That R₃ is large relative to R₁ so that the grid circuit loading on the anode of V1 may be neglected.

(ii) That stray capacitances may be neglected.

(iii) That neither valve is forced to draw grid current.

(iv) The circuit is free-running, the grid of V1

being at earth potential.

To begin the analysis, suppose that I_T has just started to flow through V1, the valve having previously been cut off. The fall in anode voltage, $E = I_T R_1$, will have been coupled to the grid of V2 by the capacitor C, as shown in the waveform diagram Fig. 6. This fall cuts off V2 and drives the current into V1 as postulated. C will now discharge through R_3 and R_1 and the grid voltage waveform will be an exponential rise towards earth. Meanwhile the cathode is at e_b , held by the grid of V1. When the grid of V2 reaches a point one effective grid base below earth, V2 can start to conduct just as was considered in the case of the circuit of Fig. 4. The current in V1 falls and this rapidly turns V2 on and V1 completely off, transmitting a positive swing of E to the grid of V2. The cathode follows this rise, and also the ensuing fall towards earth. Finally, when the grid has reached a point one effective grid base above earth, V1 can start to conduct and the cycle recommences.

From the analysis, it can be seen that the mark and space times are equal, and are governed by an exponential curve from $E-(e_c-e_b)$ to (e_c-e_b) , relative to earth, on a time constant of CR_3 seconds approximately. The free-running period can thus be estimated using log tables, or graphically as shown

in the appendix.

Some practical design points arising from the assumptions made for the analysis can now be

considered.

The designer must ensure that neither valve is forced to draw grid current. In the case of V2 this would alter the effective time constant in an unpredictable way on one half cycle only, giving unequal mark and space times. The most critical instant in the cycle is t_1 , Fig. 6, when the anode-to-cathode voltage of V2 has its minimum value. This must be sufficient to enable the valve to pass current I_T with negative grid bias.

During the transitions R_3 is effectively in parallel with R_1 , and if R_3 is made comparable with R_1 , the anode and grid swings will be reduced to $I_TR_1R_3/(R_1+R_3)$. Also the time constant of the exponential grid voltage should be taken as $C(R_1+R_3)$.

Stray capacitances cannot be neglected in practice. At an anode, stray capacitance C₈ will turn the theoretically instantaneous rise and fall into exponentials of time constant C₈ times the anode load. The effect of stray capacitance at the grid of V2 will depend upon the value chosen for the coupling capacitor C. Should the two be comparable then only an unknown proportion of the anode swing appears at the grid of V2.

To show how easy the design procedure is in practice, suppose a synchronized multivibrator is required, using a 12AT7 valve to give two antiphase outputs of 100 volts. Although the design would be easier if a negative supply were available for the "tail", it will be assumed that only a 300 volts supply is available. Of this 300 volts, 100 are used

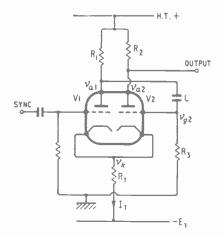


Fig. 5. White's mu'tivibrotor circuit.

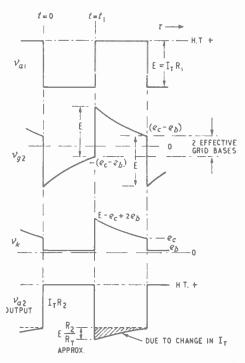


Fig. 6. Waveforms appearing at various points in the multivibratar circuit of Fig. 5.

for the tail. This leaves only 100 volts for the conducting valve, and to avoid driving it into grid current, a small value of tail current, 2mA, is chosen, making $R_T\!=\!47$ kilohms. For two 100 volt outputs, both anode loads are 47 kilohms also. If the whole 100-volt swing is coupled to the grid of V2, the assumption of constant I_T will fail miserably, and V2 will be left with no anode voltage. The circuit of Fig. 7 shows how this is overcome by transferring only 20 volts of the swing. The approximate freerunning half-period will be governed by (20-4) volts decaying to 4 volts, the effective grid base. As shown in the appendix, this decay to 0.25 of the initial value takes 1.4CR3 seconds, CR3 being the

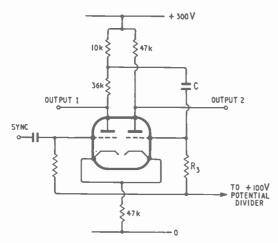


Fig. 7. Illustrative multivibrator design.

time constant. Finally the rise and fall times with $C_s{=}20 pF$ at each anode will be about $3 \mu sec$, with anode time constants of $1 \mu sec$. This figure compares favourably with the rise time obtainable from a circuit of the type shown in Fig. 1; at a repetition frequency of 500 c/s values of the order of $100 \mu sec$ are more typical.

For many purposes, the measured performance of the circuit will correspond sufficiently closely to these design figures. The negative swing at the anode of V2 is about 20% greater than 100 volts due to the increase in I_T at time t_1 in Fig. 6. The only other major discrepancy likely to arise is in the free-running half-period, as this depends on the grid base as previously mentioned.

In the concluding part of this article, a similar circuit will be described in which the free-running period of oscillation can be defined to within a few per cent, the circuit being particularly suitable for use with transistors.

APPENDIX

Graphical Solution of the Exponential Equation.

The solution to expressions of the form

 $E_1 = E_0 e^{-t/T}$

where E_0 and E_1 are known, and it is required to find t in terms of the time constant T, can be obtained by taking logs or by log-log slide-rule scales. A quick alternative method, which is usually sufficiently accurate, is to use a graph of the function $e^{-t/T}$

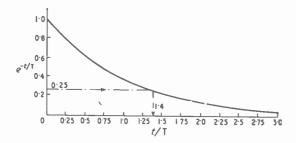


Fig. 8. Graph of exp(-t/T) plotted against t/T.

plotted against t/T, Fig. 8. Taking the example of a decay from 16 volts to 4 volts, that is $E_1/E_0=0.25$, this corresponds to a time of 1.4 T. Because this graph is, in effect, a scale drawing of the circuit waveshape, gross errors in calculation are valikely and the effects of small changes of E_1 on the timing of a circuit are more easily seen.

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Ref. 4. White, E. L. C., British Patent No. 535,778 (1941).

Commercial Literature

Sheet Insulation may be adversely affected by discharges taking place on or near its surface. Eight plastics materials and silicone rubber, Perspex and synthetic-resin-bonded laminates have been tested tor the resistance to surface discharges by the Electrical Research Association Laboratory. Copies of the 42-page report entitled "The Resistance of Sheet Insulation to Surface Discharges" by J. H. Mason may be obtained from Publication Sales Department, Electrical Research Association, Thorncroft Manor, Dorking Road, Leatherhead, Surrey. Price 15s or 15s 8d by post.

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Demonstration Servo System made by Feedback Ltd., of Crowborough, Sussex, uses part "bread-board," part unit construction to make clear the functioning of d.c. closed- and open-loop position control. The front panel of the control unit carries a simplified diagram fitted with terminals for interconnecting links.

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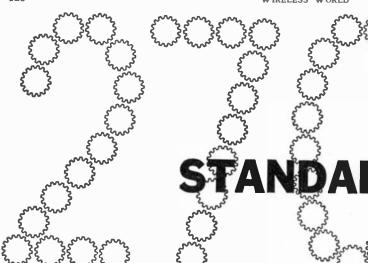
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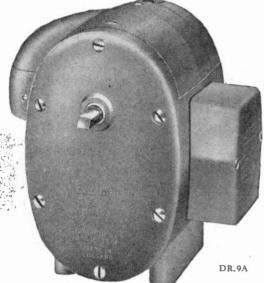






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Negative Feedback and Non-Linearity

By "CATHODE RAY"

T is commonly believed that negative feedback reduces undesirable things, such as distortion, to the same extent as it reduces amplification. This belief is not without some foundation, but like many others it is an over-simplification and ought not to be

applied indiscriminately.

For instance, one of the undesirable things (in a.c.-driven equipment) is hum. So far from invariably reducing it in the same ratio as amplification, negative feedback sometimes reduces it less than that, or not at all, or even considerably increases it.* Another of the undesirable things is the random noise we were considering only a month or two ago. It is certainly possible to reduce such noise by negative feedback, but, since the wanted signals are likewise reduced, the signal-to-noise ratio (which is what matters) is in no way improved. Increasing the overall amplification to make good the loss due to feedback increases the noise too.

By this time some may be beginning to wonder what advantage negative feedback ever does give. What about distortion? Might not the necessary extra amplification re-introduce it and leave one no

better off?

Well, of course, there are several different kinds of distortion, and one can't cover them all at once with a simple Yes or No. There is non-linearity, which alters the shape of even a single pure sine-wave signal. This it can be regarded as doing by introducing signal frequencies that were not present in the original. Then there is amplitude/frequency distortion, which alters the shape of signals only when they include more than one frequency, and upsets the balance of tone in sound programmes. Phase distortion makes no perceptible difference to sound, but it alters the shape of multiple-frequency signals, so it affects the appearance of television pictures.

Reducing non-linearity is usually the main object of negative feedback, because that is the most unpleasant form of distortion where sound is concerned. No amplifier with any claim to be suitable for high-quality reproduction would be without negative feedback. So presumably it does do some good. The question is whether it does as much good

as is commonly believed.

Readers who were born, so to speak, with Nyquist diagrams on their bibs, and who are merely following my plough on the off-chance of its unearthing some stray fragment of novelty, must be prepared to show forbearance while for the next few paragraphs I recapitulate the basic principles of negative feedback for their juniors in the art.

The box in Fig. 1(a) represents an amplifier; its voltage amplification or gain is customarily denoted by A, which means that for every signal volt (or millivolt, more likely) applied between the input

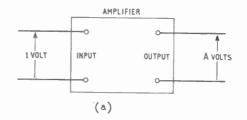
terminals it gives A volts (etc.) between the output terminals.

If now we take some fraction B of this output voltage and introduce it in series with the input voltage, as at (b), the gain of the amplifier, reckoned between its own two pairs of terminals, is still A. But for practical purposes the feedback connection becomes part of the amplifier, so the input terminals become those marked XX. The net gain between them and the output terminals is called A'. If we try to calculate A' in terms of A and B by supposing (for simplicity) that the signal source delivers 1 volt to the new input terminals, we get stuck. The thing to do is to work from the fact that 1 volt at the old input terminals gives A volts at the output. The voltage fed back is then AB.

Now this is where we have to be careful about signs. Negative feedback, represented by a negative value of AB, is defined as feedback that opposes the input voltage to XX, requiring it to be greater than I volt in order to maintain the I volt at the input to the amplifier itself. A positive value of AB therefore means an XX input less than I. So in either case it must be 1 — AB volts. The corresponding output being A volts, the overall gain is

$$A' = \frac{\text{output}}{\text{input}} = \frac{A}{1 - AB}$$

This is the "Ohm's law" or ABC of feedback.



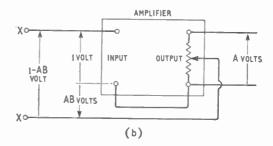


Fig. 1 (a) represents an amplifier without feedback, and (b) the same amplifier with feedback, a fraction B of the output voltage being tapped off and returned to the input. The arrows show the relative polarities for positive values of all instantaneous voltages. If the feedback is negative, the minus sign in 1-AB is cancelled out.

^{*}My last treatise on this was 15 years ago, and as it is unlikely that many readers present ever saw it or could remember it if they did, a return to the subject may be nearly due.

Although for simplicity we assumed 1 volt at the original or internal input, the above result would have been just the same if it had been any other

amount, say V.

One of the first things usually pointed out about this equation is that if the negative voltage fed back is made much larger than the internal input, an approximate formula for A' can be obtained by neglecting the relatively small 1 in the denominator, the result being

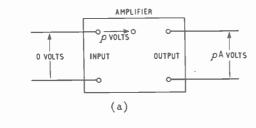
$$A' = \frac{1}{-B}$$

which means that the overall gain is almost independent of the internal gain, A, and is decided mainly by B. In other words, ample quantities of negative feedback prevent the gain of an amplifier from being much affected by the usual uncertainties such as ageing valves and fluctuating supply

voltages.

By the way, newcomers may have been wondering why we take the trouble to put a minus in these formulae, only to cancel it with another minus by making the feedback negative. Why not define AB as the negative voltage fed back, making the denominator 1 + AB? That would be quite sensible if in a negative-feedback amplifier the feedback were always negative, but in all but the simplest circuits (such as cathode followers) there are some frequencies at which a 180° phase shift makes the feedback positive, and the risk of confusion might be even greater if we decided to denote this by a negative value of AB. Nevertheless, it is sometimes done (in case Mr. D. L. Clay is reading this, I hasten to point out that I did it myself in Feb. 1946) so one must be prepared for either.

The recapitulation is now over and those who were dozing off may wake up. We were saying that the belief that negative feedback reduces non-linearity distortion in the same ratio as it



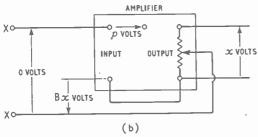


Fig. 2. These diagrams correspond to Fig. 1, with the same signal voltages present but not shown. Instead, the voltages shown refer to distortion products created by the nonlinearity of the amplifier at that particular signal level. They enable the apparent reduction of distortion by feedback to be calculated.

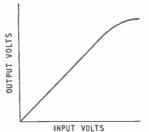


Fig. 3. This is one kind of output/input graph, in which the voltages are peak or r.m.s. values.

reduces the gain of an amplifier may need to be

looked at again.

The basis for the belief can be explained simply as follows. Suppose we still have our 1 volt of signal at the input of the amplifier itself, yielding A volts of signal at the output. But owing to non-linearity the amplifier generates harmonics and intermodulation products. Suppose the amplitude of any or all of these, relative to the signal output, is p. Then the distortion output (without feedback) is pA volts. This can be regarded as due to a distortion signal 1A/ as large (i.e., p volts) at the input, but to make clear that this is an internal signal, not applied from without, it can be shown as in Fig. 2(a), which takes account of distortion only. The corresponding state of affairs with feedback is shown at (b), and as we don't know how much distortion is emerging we call it x volts. The voltage fed back is of course Bx, so the total input is Bx + p. When multiplied by the gain of the amplifier, A, this must amount to x:

$$A(Bx + p) = x$$

$$Ap = x(1 - AB)$$

$$\frac{x}{Ap} = \frac{1}{1 - AB} = \frac{A'}{A}$$

proving that feedback affects the amount of distortion emerging from the amplifier in the same ratio as it affects the overall gain of the amplifier.

In this calculation we quietly assumed that the signal output (not shown) was the same in both (a) and (b), for that is what determines the amount of distortion generated internally, as is represented in both diagrams by the same "p volts." This means that the input (to XX) must have been increased to the same extent as the internal gain was reduced by negative feedback. And of course that could cause serious distortion in the pre-amplifier. But even with the increased signal level at XX it is generally easy to keep it negligible. However, if the use of feedback raises the level there so much that it is not easy, the feedback should be taken to an earlier stage, or A increased with perhaps a reduction in B. That is all part of routine feedback technique.

The basis of belief having been proved, we may think we can all go home. But actually this is just where we begin. For a start, what precisely do we mean by A? We defined it—or, to be quite fair to you, I defined it—as the number of signal volts received at the output for every volt applied at the input. (To silence any objectors who might claim that even 1 volt at the input of their amplifier would hopelessly overload it, I offered a choice of millivolts, or indeed any appropriate unit.) Nothing was said about the sort of volts—peak, r.m.s. or

instantaneous-but whatever was in mind it must have been assumed that A was constant, not depending on the signal voltage, at least within the working limits of the amplifier. In other words, it was assumed that the amplifier was linear. That being so, it wasn't very clever to use it in a calculation concerning amplifier non-linearity. We did, of course, guard against complete absurdity by stipulating that the signal voltage must be the same in both diagrams in Fig. 2. But if the non-linearity is considerable, so that the distortion is a substantial part of the total output, that safeguard isn't good enough. For, if feedback has any effect on the amount of distortion, the total output will be different and A will almost certainly be different.

So much for the general principle. The belief is undermined. The next thing is to see how it might work out in practice. The correct procedure, of course, would be to embark on a comprehensive and rigorous mathematical analysis that would cover every case (for those who could see the wood for the trees). But you know me too well to expect that

The "line" in "linearity" is the graph of output against input. There are two sorts of these graphs: one could be plotted by connecting a calibrated a.f. signal generator to the input of the amplifier and varying the signal strength there while measuring the corresponding r.m.s. or peak voltages at the output. The curve might look something like Fig. 3. There would be no point in reversing the connections with the idea of extending the curve into the negative

region, for its shape would necessarily be the same in reverse. The other kind, which is the one we are going to study, is to be seen by substituting the Y plates of a cathode-ray oscilloscope for the output voltmeter, and connecting the X plates (with suitable distortionless amplification) across the input. The positive and negative half-cycles obviously swing the curve in both directions from the origin as their instantaneous values are shown on the screen, and their shapes are not necessarily the same.

A perfectly linear amplifier would yield a perfectly straight "curve," as in Fig. 4(a). In the case of a power amplifier this would merely show that it was being uneconomically under-driven. In a commercial world it is necessary to work up to some distortion, even though it be limited to as little as 0.1%. Most amplifiers, so long as they are not over-driven, tend to show curves of two main shapes (or combinations of both), as in Fig. 4(b) and (c). The first has a square-law term in its output/input equation, which generates a second harmonic of the signal, and second-order intermodulation. The second has a cubic term and generates third-order distortion, which sounds worse.

Now A (being output/input) is represented on these Fig. 4 diagrams by the slope of the curve. In (a) the slope is the same throughout, so A is constant and (assuming, as we usually can, that B is likewise) there need be no question as to exactly what 1—AB means. In (b) and (c), A is varying all the time, so one doesn't know what figure to insert for it when using the formulae. We can say that Fig. 4(b)

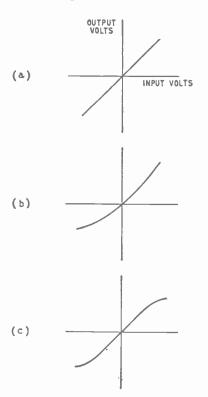


Fig. 4. In this kind of output/input graph, instantaneous voltages are plotted. (a) is a linear (distortionless) characteristic: (b) and (c) are non-linear curves, representing second and third order distortion respectively.

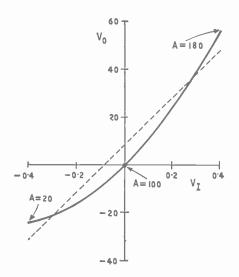


Fig. 5. The full line is a graph of the Fig. 4(b) type. The dotted line shows its fundamental part: the full-line variations from this cause second-harmonic distortion, as shown in Fig. 6.

indicates a smaller A at the negative peaks than at the positive, so presumably the negative part of the curve is straightened out less by negative feedback than the positive part, but the effect on the distortion is difficult to assess without a large-scale mathematical operation. Let us see what we can do without that.

Our example is an amplifier having a Fig. 4(b) type characteristic, which appears quantitatively as Fig. 5.

To make sure that the only distortion is secondharmonic, I have plotted it from the equation

 $V_0 = 100V_1 + 100V_1$ where V₀ is the instantaneous output voltage and V₁ the input voltage. This gives the amplifier a gain of

100 as regards the fundamental.

A simple calculation shows that with a peak V₁ of 0.4V the 100V₁² term is the cause of 20% secondharmonic distortion. We can do it graphically by drawing a straight line joining the tips of the curve, noting how far up the Vo axis it comes (16 volts in this case) and lowering the line half that distance. It is then the linear characteristic responsible for the fundamental, shown as a pure sine wave in Fig. 6(a). The actual curve we have plotted is 8 volts lower at zero V₁ and 8 volts higher at positive and negative peaks; these points can be transferred to Fig. 6(a), and when joined up by the full line show what comes out of the amplifier when \pm 0.4V peak is put in. The difference between this and the fundamental has been plotted below, (b), and is clearly a second harmonic. Both Fig. 5 and Fig. 6 show that its peak value is 8V, which in relation to the fundamental's 40V is 20%.

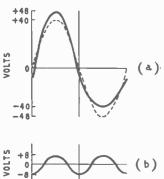


Fig. 6. (a) the full line shows the output of an amplifier with the characteristic given in Fig. 5, when the input is a pure sine-wave. The dotted line is the fundamental part, corresponding to the dotted line in Fig. 5. The difference between the two, shown by itself at (b), is a second harmonic.

Readers who hitherto may have been rather hazy about the connection between the output/input curve and the waveforms seen on a linear time base are now, I hope, feeling more confident.

Anyone with the most elementary knowledge of the differential calculus will realize that the easiest way of finding the slope (which is A) at any point on the Fig. 5 curve is to differentiate its equation, thus:

$$A = \frac{dV_0}{dV_1} = 100 + 200V_1$$

 $A = \frac{dV_0}{dV_1} = 100 + 200V_1$ So at zero V_1 it is 100, which is what one would expect, since an input confined to very small values of V₁ would yield negligible distortion, and 100 is the slope of the fundamental line. At the positive peak it is 100 + 80 = 180 and at the negative peak 100 - 80 or only 20. So 20% distortion, which isn't so horrible as you might expect, if it is all second-harmonic, is associated with no less than a 9 to 1 variation in amplification over each cycle of signal. We can hardly be surprised, then, if we find that negative feedback doesn't work entirely according to plan.

Perhaps the best way of seeing how it does work is to plot a with-feedback curve to compare with Fig. 5, which can be done by making a table to calculate some points. Remember, the voltage fed back at any point is equal to $-BV_0$, and this added to V_1 gives V_1 , the with-feedback input required.

To make it easy to compare the two curves, the

 V'_1 scale of the new one should be the V_1 scale of the

old, multiplied by as many times as V'1 must be greater than V_I to maintain the same output. convenient figure for this, which is also typical of feedback practice, is 10. 1 -AB being 10, -AB is 9 and - B is 0.09. (This is sometimes called 9% feedback.)

(I)	(2)	(3)	(4)
V ₁	V _o	0.09V _o	V'1
0.1 0.2 0.3 0.4 -0.1 -0.2 -0.3 -0.4	11 24 39 56 - 9 - 16 - 210 - 240	0.99 2.16 3.51 5.04 	1.09 2.36 3.81 5.44 — 0.91 — 1.64 — 2.19 — 2.56

Column (1) contains a few selected points covering the peak-to-peak swing of V_I. Column (2) contains the corresponding output voltages calculated from the equation, which were needed for plotting Fig. 5. Column (3) shows the voltage fed back, equal to 0.09V₀. Lastly column (4), which is got by adding (3) to (1), shows the input required at XX to maintain the same output (2) as before.

Plotting Fig. 7 from columns (2) and (4), we are at once impressed by the success of negative feedback in straightening out the amplifier curve. It is now hardly distinguishable from a straight line, especially

on the positive side.

Becoming a little more critical, we note that we need considerably more than 10 times the former positive peak input; to be exact, 13.6 times. But 10 was calculated on the basis of A = 100, whereas we have already noted on Fig. 5 that A varies from 100 to 180 during the positive half-cycle, and if we recalculate the average multiplier for these values of A we find it is 13.6. Rather than find fault here, we might thank feedback for raising the positive fundamental peak output from 40V with 20% distortion (Continued on page 229)

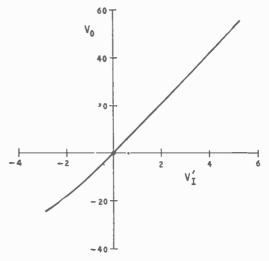


Fig. 7. This, for comparison with Fig. 5, is the result of reducing the small-signal gain 10-fold by negative feedback, and correspondingly increasing the overall input (V'_1) to yield the same net input (V_1) as before.

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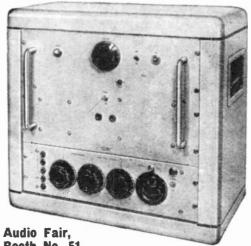
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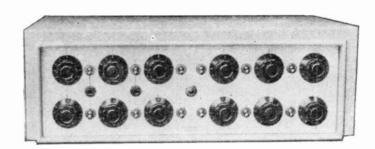
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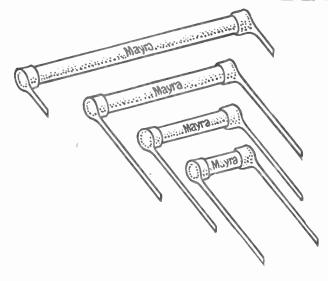
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to 55V with about 1½% distortion, and it looks as if it could be increased indefinitely by increasing V'₁.

On the other hand, any satisfaction that might at first be derived from seeing that the input needed for the negative peak has been increased only 6.4 times is damped by the unfortunate accompanying fact that the fundamental negative peak has been reduced from 40V to about 25V. And of course a 55V positive peak is no good with a 25V negative peak—unless use of the amplifier is to be confined to rather unusual waveforms.

No; if at least our original \pm 40V peak sine-wave output is to be maintained, it will clearly be necessary to bring up the negative input, as we should be able to do, seeing that we were prepared to find at least \pm 4V.

To see what we get we shall have to extend our plots in the negative direction. If we do, we find that beyond $V_1 = -0.5V$ a complication sets in: increasing V_1 reduces V_0 , making the curve bend up. (This could have been foreseen from the equation for A, which becomes negative directly V_1 becomes more negative than -0.5V). Now it is true that something like this can occur in some amplifiers, but a more likely explanation of zero A with a Fig. 4(b) type of curve is that a valve has cut off. It of course stays cut off if V_1 is made still more negative, so a more realistic procedure would be to continue the curve horizontally to the left:

Vı	V _o	0.09V ₀	V '1
-0.5	25	-2.25	- 2.75
-0.6	25	-2.25	- 2.85
-0.7	25	-2.25	- 2.95

At this rate it is obviously going to take us a long time to reach $V'_1 = -4$, but we can see which way the wind is blowing and—although such impatience is often risky with graphs—in this case we are justified in boldly writing " $V'_1 = -4.00$; $V_0 = -25$ "

Continuing beyond our original \pm 4V (comparable with the \pm 0.4V in Fig. 5) is clearly not going to make the picture look any prettier, so in Fig. 8 I have kept within those limits. Now at least we see the truth about negative feedback, and it doesn't look so good. And if anyone is thinking I've fiddled it to look worse by arbitrarily departing from the simple quadratic equation at the negative end, I invite him to stick to the equation. The result will be far more ghastly than Fig. 8.

That is bad enough, for on analysing Fig. 8* I find that the fundamental output is only just over 30V peak, compared with 40V in Fig. 5 (a power reduction of 44%), and in exchange for our 20% second harmonic we have received the following mixed bag:

and bag:
2nd harmonic: 13.2 %
3rd ,, 7.4 %
4th ,, 3.3 %
5th ,, 1.24 %
6th ,, 0.16 %
7th ,, 0.83 %

plus uncounted amounts of higher harmonics, which,

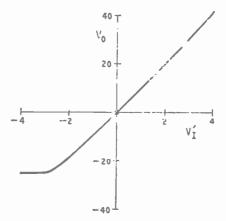


Fig. 8. The result of further adjusting the input V_1 to 10 times V_1 , positive and negative, is shown here. Audi-Ny, the distortion would be worse than without feedbark (Fig. 5).

judging from the sharpness of the bend in Fig. 8, and the magnitude of the 7th harmonic, are likely to be very significant, aurally if not numerically. It is true that the total harmonic distortion, found by taking the square root of the sum of the squares of the above lot, is 15.6%, which compares favourably with the 20% total harmonic distortion without feedback. But if anyone thinks he is thereby getting a bargain, he oughtn't to be allowed out alone in the hi-fi market. He will be an easy prey to the merchants, whose motive in quoting total distortion figures is only too clear to those who have compared actual sound reproduction with the harmonics present. Though such authorities differ as to the precise factors by which percentages of harmonics higher than the second should be multiplied to give some idea of their relative unpleasantness, the most conservative of them advocate (without necessarily admitting that it is adequate) a weighting factor equal to half the harmonic order; and D.E.L. Shorter of the B.B.C. considers the square of this factor is not excessive*. For instance, the 7th harmonic would have a weighting factor of $(7/2)^2$ 12.2, raising the above 0.83% to over 10%.

At this point a red herring labelled "Intermodulation" is almost certain to be seen trailing across our path. But I advise that if any benefit is to be derived from the time so self-sacrificingly spent in following me thus far, we must firmly ignore it. No doubt we know that the products of intermodulation, being in general not harmonically related to the tones present in the original sounds, are more conspicuously unpleasant than at least the lower harmonics, which are; but it does not follow that one must insist on intermodulation data and refuse harmonics as worthless substitutes. For, when measured under comparable conditions, harmonic percentages are more or less proportional to intermodulation percentages. And anyway, in this case we are getting the higher harmonics, which are discordant in their own right.

Continuing our uneasy contemplation of Fig. 8, we see that there is nothing for it, if we have regard for the feelings of listeners, but to reduce our input signal until the sharp bend is cleared; say 2.5V peak.

^{*}By the method described in M. G. Scroggie's "Radio Laboratory Handbook" (now temporarily out of print). 6th edition, Sec. 11.14.

^{*&}quot; The Influence of high-order products in non-linear distortion." Electronic Engineering, April 1950, p.152.

The output, which by then is nearly all pure fundamental, is barely 25V, or less than § of the power we got in Fig. 5, admittedly with lots of second harmonic too. But if we reduce the fundamental output without feedback to the same level, the second harmonic comes down to 12½%, which on paper is certainly not hi-fi, but wouldn't offend as many listeners as you might think.

It is now about time to sum up with a few con-

- (1) The "common belief" (that negative feedback reduces non-linearity distortion in the same ratio as it reduces amplification) is true in the simple sense only if there is no non-linearity to reduce.
- (2) However, provided that the original non-linearity is not so bad that the slope of the output/input curve (which is the amplification) falls seriously below the nominal value at any point within the maximum signal amplitude, the common belief is fair enough.
- (3) It follows from (1) and (2) that any idea that one can sling an amplifier together any old how and pull it straight with liberal supplies of negative feedback is unsound—even apart from the practical difficulties of this treatment.
- (4) While negative feedback works like a charm on amplifiers with *moderate* non-linearity, run well within their powers, it doesn't necessarily increase

the amount of power that can be drawn; on the contrary, it may well reduce it.

- (5) In any case, once the signal amplitude runs past the nearly-undistorted limits, it abruptly becomes very distorted, not only as regards quantity but even more as regards quality. In other words, even a moderately overloaded set sounds a lot worse with feedback than without.
- (6) The fact that hi-fi fans, to whom negative feedback is a sine qua non, also insist (especially in America) on vast numbers of output watts being available, in spite of the surprisingly small average power required even for quite loud reproduction, is thus explained.

(7) The fact that demonstrations of "hi-fi", unless conducted by masters of the art such as Gilbert Briggs, are usually such painful experiences, is also explained. The demonstrator of an X-watt amplifier so often doesn't reckon he is doing his job if the output falls below the maximum rating.

During the whole of this investigation we have assumed that the feedback is precisely negative. That is never true at relatively high frequencies, even with the simple cathode follower, and the picture is then far worse than I have drawn. This is why sharp-cornered waveforms, which contain high-frequency components, may become horribly distorted. Perhaps it will be worth enlarging on the matter next time.

BOOKS RECEIVED

Radio, Television, Industrial Tube, Diode and Transistor Equivalents Manual, by B. B. Babani. A comprehensive equivalents list of over 20,000 devices, giving commercial equivalents, C.V. types, Service-to-civilian equivalents, and U.S.A.-to-British commercial equivalents. A replacements list is given for television picture tubes. Pp. 208. Bernards (Publishers) Ltd., The Grampians, Western Gate, London, W.6. Price 9s 6d.

Reception of Sound and Television Broadcasting, British Standard Code of Practice CP327.201 (1960). Recommendations for good practice in installation of broadcast receiving apparatus. Reference is made to relay services, individual-set installations, communal-aerial systems, provisions for maintenance personnel. Pp. 52; Figs. 8. Price 12s 6d. The Council for Codes of Practice, British Standards Institution, British Standards House, 2, Park Street, London, W.1.

Radio Stations—Installation, Design and Practice, by G. A. Chappel. Deals fully with all the aspects of highand low-power radio transmitting-station design, installation and servicing. Includes chapters on the electrical and mechanical design of transmission lines and aerial systems. Pp. 248; Figs. 148; plates 31. Pergamon Press, Headington Hill Hall, Oxford. Price 50s.

Electrical Noise: Fundamentals and Physical Mechanism, by D. A. Bell. A complete reference and text-book on the subject of noise in electronic and physical devices. The author approaches present-day knowledge in the light of historical theories and controversies. The Nyquist theory of voltage fluctuations across resistors is dealt with exhaustively, and there is a chapter on v.h.f. valves, travelling-wave tubes, parametric amplifiers and masers; noise in metal films is also discussed. Information on measurements is included, and each chapter is followed by an extensive list

of references. Pp. 342; Figs. 98. D. Van Nostrand Company, Ltd., 358, Kensington High Street, London, W.14. Price 50s.

Beam and Wave Electronics in Microwave Tubes, by R. G. E. Hutter. A mathematical treatise on the basic principles of the family of microwave tubes. Small-signal effects only are considered, and as this is a discussion of principles, no design information is given. The author does not attempt a physical description, but confines himself to the mathematics of operation. Such microwave circuitry as is closely associated with the tubes under discussion is described, and the concept of d.c.-to-a.c. energy conversion is discussed. A chapter is devoted to noise phenomena. Pp. 378; Figs. 158. D. Van Nostrand Company, Ltd., 358 Kensington High Street, London, W.14. Price 73s 6d.

Hochfrequenz-Messtechnik, by O. Zinke and H. Brunswig. This third revised and enlarged edition is a reference book of measurements at high frequencies. The range of frequency covered is from just above the audio band to the microwave region. Instruments and their operation are described, together with methods of determining many parameters such as frequency, phase, power and impedance. Throughout, reference is made to commercial instruments relevant to the measurement under discussion, and also to the equipment specifications in the companion book, Hochfrequenz-Messgeräte. Pp. 234, Figs. 258. S. Hirzel Verlag, Stuttgart N., Birkenwaldstrasse 185. Price DM 24,80.

Hochfrequenz-Messgeräte, by O. Zinke and H. Brunswig. Abbreviated specifications of commercial instruments and devices for the measurement and generation of high-frequencies. Complementary to the companion work, Hochfrequenz-Messtechnik. Pp. 60. S. Hirzel Verlag, Stuttgart N., Birkenwaldstrasse 185. Price DM 9,60.



The outhor's station at Lowestoft, Suffolk, showing his Creed teleprinter.

ON the Saturday evening of the week in which the recent Radio Hobbies Exhibition was held, the British Amateur Radio Teleprinter Group held its first dinner, celebrating in doing so its first year of activity.

Amateur radio teleprinting is a very new mode of communication for the British radio amateur, for whilst this mode has been followed in the U.S.A. and Canada for a number of years, its exploitation by radio amateurs in Europe was held up by a number of difficulties. These difficulties included a certain prejudice amongst some amateurs to this method of communication, lack of information on sources of suitable equipment and uncertainty as to the licence conditions regulating this aspect of amateur radio transmission.

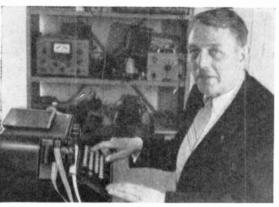
The group was formed in the middle of 1959 to investigate these problems and endeavour to get "RTTY," as it is designated in radio circles, introduced into the field of amateur radio activity in this country. Enquiry from the G.P.O. revealed that teleprinting by means of frequency shift keying was, in fact, permitted by the terms of the licence controlling amateur radio transmitting activities in this country. A source of suitable teleprinters was found at a price the amateur enthusiast could afford, viz., around £3 to £4! Admittedly these were pretty obsolete by modern commercial standards, but they proved eminently satisfactory for the particular characteristics of amateur radio communication. The group produced and distributed news sheets. information leaflets and data so that almost imperceptibly old prejudices were broken down and knowledge of the system was disseminated throughout the amateur fraternity.

The first amateur radio teleprinting in this country took place towards the end of 1959 between Peter Carnochan's station (G3IAO) in Lowestoft, that of the author, also in Lowestoft, and that of W.M. Brennan (G3CQE) in Norwich. Transmissions were in the 80-metre band (850c/s) using f.s.k. At the 1959 Radio Hobbies Exhibition, a demonstration of amateur radio teleprinting was put on and the

AMATEUR TELEPRINTING

GROWING INTEREST IN EUROPE

By ARTHUR C. GEE* (G2UK)



Jan Adama (PAØFB) of The Hague, operating his Siemens teleprinter with autohead reperforator.

f.s.k. convertor unit used by the author for these first tests was shown working and it was briefly described and illustrated in a subsequent issue of Wireless World.

This demonstration was seen by Jan Adama, a prominent Dutch amateur (PAØFB), who wrote to the author early in 1960 saying he had assembled radio teleprinting gear and was ready for tests. These were soon successfully carried out with the author's station. In the meantime Mr. Brennan had been making successful contacts with RTTY stations in the U.S.A., Canada, Australia and other distant countries, and we soon learnt that Hans H. Horn, of Flensburg, W. Germany, was equipped for RTTY operation from his station DL1GP.

During 1960 there was a rapid growth of both membership of the Group and activity on the air and at the end of the year about twenty radio amateurs in this country, Holland and Germany were regularly using this mode of transmission. There is much yet to be done in popularizing RTTY amongst the European amateur radio fraternity; in extending its use to other countries; in developing equipment more suited to amateur requirements than the surplus commercial material which is at the moment widely used; and by disseminating technical information to those wishing to use this type of communication. RTTY has, without doubt, come to stay and is for the c.w. man what s.s.b. has become for the 'phone enthusiast.

^{*}Hon. Sec. British Amateur Radio Teleprinter Group

By "FREE GRID"

WIRELESS WORLD has always been noted for its meticulous accuracy, and I recollect being very greatly impressed in 1936, when the 25th birthday number was published, by the fact that the word jubilee was strictly avoided, the obvious ground for such avoidance being that the word can only properly be applied to a fiftieth anniversary, it being ultimately derived, of course, from the Hebrew festival of emancipation held every 50th year, as is described in such detail in the 25th chapter of Leviticus. This festival was always initiated by a blast from a trumpet made out of a ram's horn (Heb. Yobel).

Incidentally, the correct spelling of the word is "jubile," as the A.V. translations of Leviticus make abundantly clear (Lev. XXV, 9, et seq) and I have often wondered how the extra "e" got stuck on to it. I suppose it is all part of the centuries-old craze for using French feminine past participles, such as "employee," which finally gave us the offensive word "evacuee," which can only be correctly used to describe a child who has received the attentions of a nurse armed with Mr. Higginson's remarkably effective invention.

Coherer to Crystal

However, to get back to our own jubilee, Wireless World was undoubtedly the first journal catering solely for radio interests, but it was by no means the first to publish details of how to rig up a wireless

receiver at home. That honour belongs, I believe, to *The Model Engineer*, which gave such information over 63 years ago, in January, 1898, as I pointed out in the May, 1951, issue of *Wireless World* when I also reproduced the circuit diagram.

I certainly cannot claim to have been reading *The Model Engineer* in 1898 but, curiously enough, I did write my first technical article in one of its sister journals in the early days of the First World War. But I don't think what I wrote—nor yet the 5s I received for the article—had anything to do with the journal's subsequent decease.

It is a strange coincidence, but in 1911, when Wireless World was born, I built my first wireless set from a design in The Boys Own Paper, the idea being to receive the time signals from the Eiffel Tower. On the outbreak of war I had to surrender the set to the police, but I never reclaimed it afterwards. Judging by the primitive apparatus used at Scotland Yard in the early post-war years, as shown in the photograph on this page, I think I can see what the police did with some, at any rate, of my components.

Operation Helen

My other photograph, an instructional class of girl morse learners, was taken in the early part of the First World War when there was such a desperate shortage of manpower at sea that it was decided to put female auxiliaries aboard ship, a start being made in the wireless

room. This enterprise was appropriately enough named "Operation Helen," as it was hoped that the prospect of having beautiful girls in the ship's company would do far more than "launch a thousand ships"; it was hoped that it would also attract men eager to serve in their crews. Had I not been serving in Kitchener's army I should certainly have been an eager recruit.

In the First World War, of course, there was no direction of labour and, indeed, no conscription for the fighting forces until March 2nd, 1916. Many of my older readers in the U.K. will recall the caption of the final pre-conscription recruiting poster, "Will you march too, or wait till March Two."

Do you notice how astonishingly reminiscent of my own features are those of the portly instructress standing on the starboard side of the class. She is, at least, becomingly dressed, which is more than can be said for the girls in her charge, whose dress was considered rather daring in those days, as their ankles were visible, and in the case of one girl, several inches of leg above them. As the old music-hall song of the times said, "Who cares a damn, for Mary's little lamb, now you can see her calves?"

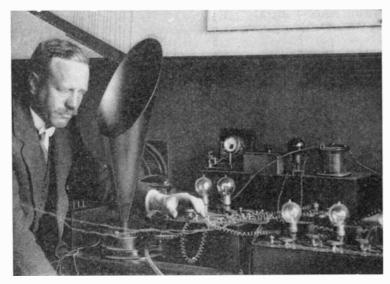
However, with the coming of conscription, "Operation Helen" was abandoned, with the result that sailors were deprived of many home comforts with which the girls might have eased their hard lot in their watch below.

A.D. 1971, 1986, 2011

Another 50 years will have to pass before Wireless World can publish another jubilee number, and that will be the centenary number of April, A.D. 2011. However, it is customary to celebrate 60th and 75th anniversaries of things. I shall be very surprised if by the 60th anniversary in 1971 we do not have coloured television and by the 75th anniversary in 1986 stereoscopic coloured TV.

By 1971 our television sets will probably have a scanning unit so that we can show our coloured slides and also our home ciné films on the c.r.t., and by 1986 our home ciné films will be returned to us from the processing station in the form of magnetic tapes holding both sound and vision recordings.

By 1986 every set will, of course, have a built-in multi-channel tape recorder for vision and sound so that while we are watching one programme we can simultaneously bottle one or more of the several alternative



"Primitive apparatus used at Scotland Yard in the early post-war years"



"Prospect of having beautiful girls in the ship's company"

programmes which will be available. Built-in time switches will enable programmes to be bottled in our absence. There is not the slightest reason why these built-in recording facilities should not be available to-day in the case of our sound receivers.

Gynarchy

Long before our centenary year, the growing menace of gynarchy will have reached its logical conclusion, and all positions now sacred to the male will have been taken over by women. I have tried to imagine what the Wireless World editress of 2011 will probably be like. I think she will be a ravishingly beautiful blonde, but rather brainless, as is only natural since the Wireless World office will be fully "automationized" ("What a word!" as A.P.H. would say) and all articles will be written and sub-edited by electronic devices.

Some of you who are a bit lacking in imagination may wonder what need there will be of an editress, brainless or otherwise, in the days of full automation. Her function will, of course, be the purely psychological one of imbuing the male machine minders with a false sense of euphoria so that they give of their best; even today, some men work themselves to death just to provide dumb blondes with mink coats and Cadillacs, their sole reward being to win their soulless toothpaste smiles of approval. The blondes are not so dumb as some people think.

In the case of Wireless World readers of 2011, the psychological effect of the face of the glamorous editress on the cover, "in glorious Technicolor," will be to get them to accept, without complaint, articles which would otherwise cause them to

send letters of carping criticism to the editorial boudoir. Even hardfaced business-men like advertisers will be induced to buy more space than they intended.

Fettered by Physics

I will now leave the domestic scene of Wireless World's office and venture to glance into the future of the world of electronics, but I am definitely not going to inflict on you any of the unimaginative and rather obvious ideas which most science-fiction writers present to their readers; I except Poe, Conan Doyle and H. G. Wells. Who can doubt that the interplanetary flights of which they wrote will one day take place? Mr. Kruschev may well be on his way to Mars as you read these words. It is equally obvious that interstellar and even intergalactic flights will eventually take place; not I think by the year 2011 nor even by the year 2011²⁰¹¹.

The reason for their unimaginative stories is that writers of sciencefiction allow their minds to be fettered by physics, or, more accurately, by our contemporary knowledge of The sciction scribes, as I physics. call them, write fantastic storiesdoubtless accurate by contemporary scientific knowledge—about travel to distant worlds while overlooking the possibility of travel to another kind of world which is right under their noses. The world to which I refer is the extra-spatial and extra-temporal one which I discussed fully in the March, 1959, issue of this journal. I am greatly indebted to "Cathode Ray" for my ideas and gladly Ray" for my ideas and gladly acknowledge it. As I explained in my original thesis on the sub-iect, it was he who set me think-

ing by his article in the November, 1958, issue. In that article he gave us a very vivid picture of electrons as being "waves of which nobody knows" which it is usual to call ψ waves. As a result of reading this I expressed the view that if we could manage to alter one of the properties of the ψ waves such, for instance, as their λ , we should probably find that these metamorphosed electrons vanished, like H. G. Wells's Time Machine, out of our world of time and space into that extra-spatial and extra-temporal "world" inhabited by ghosts, fairies, poltergeists, and other seemingly shadowy and clammy entities who seem to pass through brick walls, to be able to be in two places simultaneously and, in general, to ignore many if not all the laws of physics.

In actual fact I don't believe they do ignore them; they merely seem to ignore physical laws because our knowledge of physics today is very limited in comparison with what it will be in the year 2011. After all, our present-day achievements in radio communications would have seemed incredible to the physicists

of a century ago.

I am reluctant to call this spaceless and timeless place the metaphysical world because I don't think it is "beyond physics" as the name would imply. I will, therefore, call it the psychotronic world which simply means that it is built of metamorphosed electrons or, in other words, psychotrons, a word which I coined in the May, 1960, issue to describe these extra-spatial and extra-temporal electrons or ψ waves which had had their wavelength or other property changed or metamorphosed, and had, therefore, become μ ψ waves.

Electrovision

I will venture only one prophecy on more ordinary lines. Over a quarter of a century ago in the issue of July 20th, 1934, I described in these columns the automatic camera with selfadjusting stops and shutter speeds as I reminded you last October. This type of camera has become all the rage since last year. I wonder if I can repeat my success of 1934 by suggesting that before 2011, our electronic experts and ophthalmic surgeons will have got together to do something very drastic for people like myself suffering from failing sight.

I have in mind the development of something like the special kind of cathode-ray tube used for transmission but in very miniature form so that it would actually take the place of an eye and convert vision into pulses along the optic nerve, as the natural eye does now. It sounds nonsense. But so would a simple breadand-butter job like an appendectomy have sounded if it had been suggested in the days of the Crimean War, or even very much la'er.

reflections RANDOM RADIATI

By "DIALLIST"

A Wonderful Occasion

AND so Wireless World reaches its jubilee after a wonderful record. I'm sure that congratulations and birthday "many happies" will pour in from all parts of the world and I'm glad to make my own small contribution. May it go on from strength to strength. Myself, I've been one of its readers for over forty years and have been a regular contributor for over 26 years, radiating at random in every issue since that of January 18th, 1935. Before me is a letter from H. S. Pocock dated December 28th, 1934. In it he agrees to give the feature a twelve months' trial, agrees, too, to adopt my suggestion that the title should be "Random Radiations" and that my penname should be "Diallist." It's my proud boast that I've never missed an issue, though some of the copy was written in pretty difficult conditions -during the war, for instance, and in the course of two or three spells in hospital. Writing "Random Radiations" has been sheer pleasure, for it has brought me innumerable letters from all parts of the world.

Looking Back

WHAT amazing changes developments there have been since Wireless World was ushered into the world. Old hands will remember, as I do, fiddling with crystal and cats whisker to find the most sensitive spot. The triode valve didn't become available to amateurs until after World War I. The early ones were all hand made and for that reason they were expensive. If I remember aright the price of the "R" valve, the only one on the market after the First War, was 27s 6d, though this came down a bit as the demand grew. Then the whole position was altered by the appearance of the Mullard "Ora" valve (Oscillator, Rectifier, Amplifier), which was priced at 15s, and a little later by the coming of the Cossor "tin hat" valve, which got its name from the shape of its anode, and sold at the same price. There were few power valves in

those early days and I remember that The Set-building Boom my first 4-valve set (home made, of course) consisted of four "R" type ceiver and a horn. What it must have sounded like I can't think, but people were enthusiastic about the quality of its reproduction!

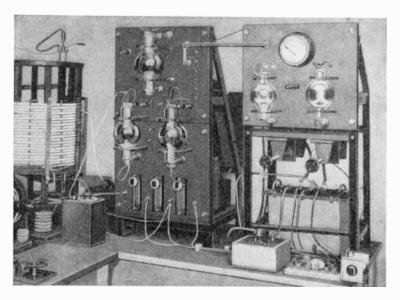
Before the B.B.C.

UNTIL the British Broadcasting Company, afterwards to become the British Broadcasting Corporation, started transmitting there were only two sound broadcasting stations we could listen to in this country. One was The Hague (PCGG), which transmitted for short periods three days a week; the other was the Marconi station, 2MT, at Writtle, Chelmsford, which was on the air for about half an hour on Tuesday evenings. Its presiding genius was P. P. Eckersley, who not only ran the station but also provided much of the programme himself. Then in November 1922 2LO made its welcome appearance with programmes every THE triode with a 6-volt filament

EVERYBODY who was, or thought triodes, the output going to a loud- he was, in the service area of 2LO. speaker consisting of a telephone re- or the other B.B.C. stations as they came along in quick succession, was determined to have a wireless set. Many receivers were bought ready made but far more were probably home made. We wound our own coils, built our variable condensers (they weren't called capacitors then) and even made up our own a.f. transformers. If you're a Londoner do you remember Mrs. Raymond of Lisle Street? By that time a good few wireless weeklies of the popular kind had come into being and each of them contained every week instructions for building one or more receivers. As ready-made sets became cheaper and more plentiful the home building boom began to wane a little, though tens of thousands of receivers continued to be made by amateur enthusiasts.

Valves

gave way to 4-volt types and later to



Pre-B.B.C. broadcasting station. The transmitter at 2MT, Writtle.

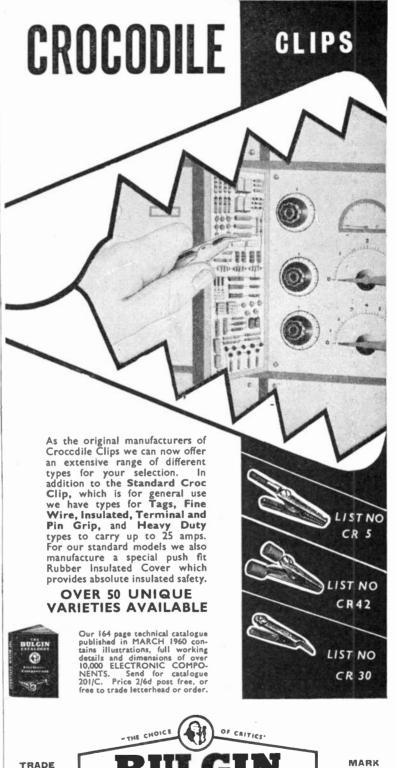
2-volt dull emitters. All were battery valves (you had your filament accumulator and your dry h.t.b.) for quite a time until the mains valve with its indirectly heated cathode burst on to an astonished world. All mains sets had transformers and in my humble opinion it's a thousand pities that transformerless valve chains were ever permitted. power valve came on to the market and a sensation was caused by the appearance of the screen-grid valve and the pentode. Then all sorts of complex valves were developedhexode, triode-hexode and a whole range, some of which are now almost forgotten.

Receiving Sets

RUMMAGING in a drawer a few days before this was written, I came across the supplement to Wireless World of December 9th, 1932. It's entitled "Buyers' Guide to 1933 Receivers and Radiograms" and lists the products of some eighty firms. It was a little before that that perhaps the most hideous of all receivers were made: it was usual then to mount the loudspeaker above the chassis of the set and this led to the development of cabinets with straight sides and rounded tops. They were, in fact, exactly like tombstones! The earliest sets were all single-valve or two-valve with grid-leak and condenser detectors and reaction. Reaction, misused as it so often was, could cause interference at considerable distances. A frequent item in B.B.C. news bulletins was: "Complaints of interference in the neighbourhood of X-road, Y-borough are being received. Will listeners living in that area please look to their sets.

Television

THE first television broadcasts by the B.B.C. were made on the medium waves and were received on J. L. Baird's 30-line scanning disc televisor. The pictures were tiny, though you viewed them through a lens, and therefore of very limited entertainment value by present-day standards. Bearing in mind the present-day craze for bigger and bigger screens it is interesting to recall that at the last pre-war radio show several manufacturers introduced sets with small tubes (some as small as 5in) in order to reduce the prices of sets. Even so there weren't a lot of television receivers in existence when World War II caused the Alexandra Palace to close down its transmissions.



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APRIL MEETINGS

Tickets are required for some meetings; readers are advised, therefore, to communicate with the secretary of the society concerned.

LONDON

6th. Brit.I.R.E. — Discussion on "Transistorized television receivers" at 6.0 at the London School of Hygiene, Keppel Street, W.C.1. 7th. I.E.E.—Discussion on "The

Conversion of biological data into electrical signals" at 6.0 at Savoy Place,

10th. I.E.E.-Discussion on "Applications of electrical phenomena at liquid helium temperatures" at 5.30 at Savoy Place, W.C.2.

11th. I.E.E.—" Precision instruments for coaxial line measurements up to 4Gc/s" by D. Woods at 5.30 at Savoy Place, W.C.2.

12th. Brit.I.R.E. — "Vibration

12th. Brit.I.R.E. — "Vibration analysis and testing" by D. E. Mullinger at 6.0 at the London School of Hygiene, Keppel Street, W.C.1.

12th. Society of Environmental Engineers. — "Climatic and high-vacuum environmental test chamber" by V. A. Austin at 6.0 at Imperial College.

14th. Television Society. — "Transparent phosphor screens" by Dr.

parent phosphor screens" by Dr. D E. N. King at 7.0 at the Cinematograph Exhibitors' Association, 164
Shaftesbury Avenue, W.C.2.

19th. Brit.I.R.E.—"Instrumentation

19th. Brit.I.R.E.—"Instrumentation in obstetrics" by Dr. C. N. Smyth at 6.0 at University College Medical School, University Street, W.C.1.
19th. Society of Instrument Technology.—"Electronic telephone exchanges" by T. H. Flowers at 7.0 at Manson House, 26 Portland Place, W.1.
20th. British Computer Society.—"The recording of time series and a 20th. British Computer Society.—
The recording of time series and a programme technique for handling these records on a computer" by Sir Edward Bullard at 6.15 at the North-

Edward Bullard at 6.15 at the North-ampton College of Advanced Techno-logy, St. John Street, E.C.1. 20th-21st. Television Society.—Con-vention on "Television and film tech-niques" at the I.E.E. Lecture Hall, Savoy Place, W.C.2.

Savoy Place, W.C.2.

21st. Institute of Navigation.—
"Marine radar presentation" by S. R.
Parsons and Capt. F. J. Wylie at 5.15
at the Royal Geographical Society, 1
Kensington Gore, S.W.7.

21st. B.S.R.A.—"Recording vision
signals on tape" by Dr. P. E. Axon at
7.15 at the Royal Society of Arts, John
Adam Street, W.C.2.

26th. I.E.E.—"Data transmission"
by R. H. Franklin and J. Rhodes at
5.30 at Savoy Place, W.C.2.

26th. Brit.I.R.E.—Symposium on
"Electronic counting techniques" at
6.0 at the London School of Hygiene,
Keppel Street, London, W.C.1.

Keppel Street, London, W.C.1.

27th. I.E.E.—Kelvin lecture on "Medical electronics" by Professor R. F. Woolmer at 5.30 at Savoy Place, W.C.2.

BIRMINGHAM

12th. Television Society.—"Television in nuclear science" by Dr. P. D. Whitaker at 7.0 in the New Physics Lecture Theatre, the University.

24th. I.E.E.—Annual general meeting at 6.0 followed by "A review of progress in ultrasonic inspection techniques" by A. C. Rankin at the James Watt Institute. Watt Institute.

P

BRISTOL
11th. Television Society,—"Deflection techniques for 110° picture tubes" by B. Eastwood at 7.30 in the Colston Room, Hawthorns Hotel, Road, Clifton. Woodland

19th. Brit.I.R.E.—"Colour television" by Dr. G. N. Patchett at 7.0 at the School of Management Studies, Unity Street.

CAMBRIDGE

20th. I.E.E.—"The potentialities of artificial earth satellites for radiocommunication" by W. J. Bray at 8.0 at the Cavendish Laboratory.

CHELTENHAM

21st. Brit.I.R.E.—Annual general meeting of the section followed by "The mesa transistor and its h.f. applications" by D. H. Mehrtens at 7.0 at Technical College.

EDINBURGH

18th. I.E.E.—"Radiocommunication in the power industry" by B. H. Cox and R. E. Martin at 7.0 at the Carlton

FARNBOROUGH
18th. I.E.E.—"The future of 'electrics' and 'electronics' in aircraft and guided missiles" by Viscount Caldecote at 6.15 at the Technical College.

LEICESTER

17th. Felevision Society.—"A novel approach to colour television" by A. P. H. Thomson at 7.30 in Room 104, the College of Technology & Commerce, The Newarke.

LIVERPOOL

13th. Society of Instrument Technology.—"Feedback" by R. S. Medlock at 7.0 at M.A.N.W.E.B. Industrial Development Centre.

19th. Brit.I.R.E.—"The history of radio" by G. R. M. Garratt at 7.0 at the Adelphi Hotel.

MANCHESTER

6th. Brit.I.R.E.—" Plant investigation and control using digital techniques" by K. J. McCarthy at 7.0 at the Reynolds Hall, College of Technology.

10th. Society of Instrument Technology.—" Industrial application of TV" at 6.45 at the Nags Head, Jacksons Row. 26th. I.P.R.E.—"Telecommunications" by British Railways at 7.30 at the Central Hall, Oldham Street.

NEWCASTLE-UPON-TYNE

NEWCASTLE-UPON-TYNE

10th. I.E.E.—Annual general meeting at 6.15 followed by "Some aspects of the application of electronics to medicine" by Dr. F. T. Farmer at the Rutherford College of Technology, Northumberland Road.

12th. Brit.I.R.E.—Annual general meeting of the section followed by "Colour television" by Dr. G. N. Patchett at 7.0 at the Institute of Mining and Mechanical Engineers, Neville Hall, Westgate Road.

NOTTINGHAM

11th. I.E.E.—"The power drive and control for Jodrell Bank radio telescope" by C. N. Kington, H. A. Prime and H. T Price at 6.30 in the Lecture Theatre, Portland Building, The University versity.

PORTSMOUTH

5th. I.E.E.—Annual general meeting at 6.30 followed by "The application of electronics to the electricity supply industry" by Dr. J. S. Forrest at the College of Technology.

SCUNTHORPE

SCUNTHORPE
19th. I.E.E.—"Silicon power rectifiers" by A. J. Blundell, A. E. Garside,
R. G. Hibberd and I. Williams at 6.30
at the North Lindsey Technical College.

SOUTHAMPTON

SOUTHAMPTON

11th. I.E.E.—"High-speed pulse techniques using transistors" by E. Wolfendale at 6.30 at the University.

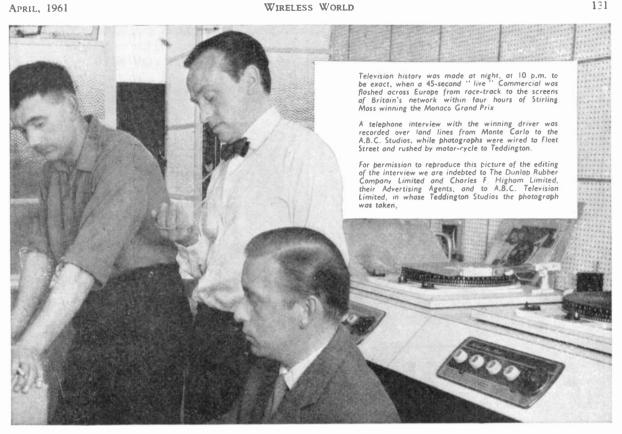
19th. Brit.I.R.E.—"The development

of an ammonia maser oscillator as a frequency standard" by A. Mitchell at 7.0 in the Lanchester Building, the University.

17th. I.E.E.—"The potentialities of artificial earth satellites for radiocommunication" by W. J. Bray at 7.0 at Duncan Hall.

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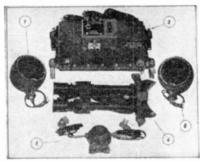
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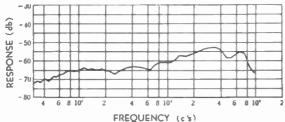
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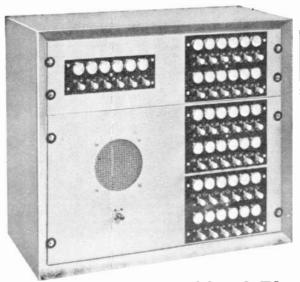
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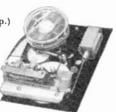
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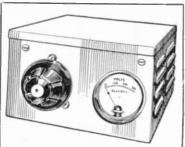
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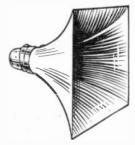
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Complete with twoway calling system
(buzzer), internal
battery. All ready
for simple two-wire
connection. Price
£3/2/6 each or £6/-/- the pair.
each handset.



/2/6 each or £6/-/- the pair. P. & P. 3/6 ch handset.

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100 YARD DRUMS GLASS BRAIDED FLEX. 10/.010. New. 10/6 per coil. P. & P. 2/-.

18-WAY P.V.C. COVERED 14/36 WIRE, screened overall, covered with P.V.C. all colour coded, 3/6 per yd.; £15 reel of 100 yds. Carriage paid.

LEATHER FLYING HELMETS. Used but in good condition. Complete with Harness, Jack Plug and brand new. No. 13466 Earpieces. Price 22/6. P. & P. 2/-.

NEW UNCHARGED UNFILLED 12 VOLT ACCUMULATOR 9 ampere in

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MINIATURE RELAYS 250 ohms. Two makes. For operation on 4.5-9 volt, ideal for transistor circuits. Weight just over 1 oz. Price 12/6 each.



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Type 5CW/3945, 4 pole changeover, 10 A contacts 24 v. operation. Brand new 13/6. P. & P. 1/6.

ELEPHONE HT O

CARPENTER'S TYPE POLARISED RELAYS. 2 x 9,500 turns at 1,685 ohms. Price 22/6 each. P. & P. I/-.



ohms each. New, 10/6 each. P. & P. I/-.



SIEMENS H.S. RELAY. Very latest type, sealed. H96E. 1,700 ohms plus 1,700 ohms, single C.O. contacts. Brand new with fixing clip. In maker's cartons. Price 16/6 each, plus 1/- P. & P. SIEMENS H.S. REL

Siemens sealed similar relay to above, but 2.2 ohms plus 2.2 ohms. Minus clips, 12/6 each. Plus I/- P. & P.

SUPERIOR BRAND NEW RELAY. 7,000 ohms coil. Will pull in at 750 microamps, and out at 450 microamp. Change-over, platinum contacts. Vacuum sealed, will therefore not be affected by oil, moisture or water and never needs adjusting. Weight 2½ oz. Price 18/6. needs adjusting. P. & P. I/-.

MINIATURE MOVING COIL DIFFER-ENTIAL RELAY. Two coils 350 ohms each. Operating current minimum 140 micro-



amp., nominal microamp, maximum 8 milliamp. way, o. Two pole two

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MINIATURE OPEN TYPE RELAY. 700 ohms coils. 24 volt. 2 C/O. Ex new equipment. Unused. 7/6. P. & P. I/-.

ROTARY RELAY. 12 volt. Heavy duty change-over contacts and one low current for external circuit, plus one break set. Price 7/6. P. & P. 1/6.



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MINIATURE UNISELECTOR SWITCH. Two banks of ten plus home contacts one bank continuous of normal. 30 ohm coil for 24 vols operation. Brand new, manufacturer's packing. Price 22/6 each. P. & P. 2/6. As illustrated.

CLASS D WAVE METER. Latest release of these famous Hetrodyne wave meters with directly calibrated illuminated dial, most suitable for amateur transmitters, covers two ranges 1.9-8.0 Mc/s.

and 4.0-8.0 Mc/s. Complete with reference crystals for zero settings, two valves, 2 x 6 volt vibrators, MAKER'S instruction book and matched set of headphones for monitoring. Designed for 6-volt D.C. operation, can easily be modified for mains and suitable transformer supplied for 7/6. In spot-on condition as tested by R.E.M.E. In transit case. Price 5 gns. each, plus 6/6 carriage.

SOUND POWER TELEPHONE HAND-SETS. Each couple connected by ordinary 2 core lighting flex will secure instant and reliable intercommunication. No batteries required. Price per set of 2 33/-, plus P.&P. 3/-.



MOULDED CAB-INET suitable for Transistor Set, Dual colour red/black. Size 51in. x 31in. x 11in. Gold metal dial. Price P. & P. 1/6. 7/6.

CONSTANT SPEED, PRECISION MADE, BATTERY DRIVEN D.C. GOVERNED MOTOR (Elliott Bros.). Commutator/brush (Elliott Bros.). Commutator/brush incorporating loading ballast resistor 2,470 r.p.m. ± 2% at 12 volt. Loss on 8.5 volt only 4%. Size 1.3 in. dia. x 23 in. long. Spindle .77 in. long x .15575 in. dia. Weight 4 oz. New. Price 25/-, plus 1/-. P. & P. Ideal for portable tape recorders.





NEW IMPORTED EX-TREMELY EFFICIENT MOTOR with tremendous power weight ratio. For 12 volt D.C. but very efficient on 6 volt. Three position switch. Weight 2.1 oz., size låin. x låin. dia. Speed 7,000 r.p.m. Self lubricating-15/-, plus 1/- P. & P.

PRECISION
MADE GEARED
MOTOR BY
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REGULATOR CO., for 230 volt 50 cycles A.C.

TYPE R.Q.R., reversible. 37 r.p.m., overall size 5in. x 4in. x 5½in. Weight 4½ lb. Ex brand new equipment. Unused. Price £3/17/6. P. & P. 3/-.





MAINS POWER SUPPLY UNITS. Potted and sealed transformer and choke by famous choke by famous maker. Mounted on metal chassis 6½ x 7½in., complete with 5Z4 rectifier valve and full smoothing.

Input tapped 220–230–240 volts.
Output: 300 V. D.C. at 100 mA.
6.3 V. A.C. at 4.5 amp.
6.3 V. A.C. at 2 amp.
Rectifier supply 5 V. A.C. at 3 amp. Very conservatively rated. Price 47/6 plus P. & P. 6/6.



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21 amp. D.C. M.I. 2in, fl. rnd,	7/6
5 amp. D.C. M.I. 2-in. fl. rnd	11/6
7± amp. D.C. M.I. 3±in. proj. rnd	12/6
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15 amp. D.C. M.C. 2in. rnd	10/6
30 amp. D.C. M.C. 2in. fl. sq	12/6
100 amp. A.C. M.I. 41in. fl. rnd	32/6
Voltmeters	
20 v. D.C. M.C. 2in. fl. sq	10/6
30 v. M.I. 3in. proj. rnd	10/6
300 v. A.C. M.C. 21 in. fl. rnd	27/6
300 v. A.C. M.I. 21in. fl. rnd	22/-
400 v. A.C. M.I. 41in. rnd.	35/-
90-180 v. A.C. M.I. 41in, fl. iron	25/-
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200 mA. M.C. 2\fin. fl. rnd	12/6
500 mA. M.C. 21in. fl. rnd	12/6
Microamp	

microamp., scaled 0-100, M.C. 24 in. fl. rnd. 00 microamp., M.C. 2in. rnd. F.L. scaled 15/600 volt. NEW.

Pastage an all meters 1/- each.

METERS GUARANTEED PERFECT

Miniature latest type moving coil 0-5 milliamp meter, lin. diameter, flush fitting, complete with fixing clip. Price 17/6. P. & P. I/-.



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controlled crystal 4-valve high-grade instrument same category as the famous B.C. 221. famous B.C. 221. Directly calibrated, does not require cross reference or charts — functions as follows:- (I) A crystal controlled

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Supplied complete with 3 spare valves, all leads and maker's instruction book in carryin haversack. The complete outfit is brand new-repeat NEW. Price £4/19/6. Carr. 3/-. in carrying

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50 mixed P.F. Condensors and 50 mixed Resistors. An assortment of useful valves. All popular sizes—all new—a must for the serviceman and constructor ONLY 10/-P. & P. 1/-.

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108K 10-inch. New and boxed, 15/-, plus 6/- P. & P. 75K 10-inch. New and boxed, 15/-, plus 6/- P. & P.

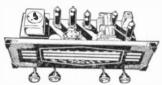
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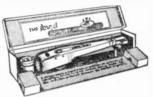
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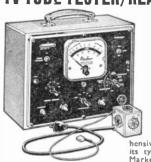
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Complete and ready for your cabinet, 4 valve superhet chassis. Complete with valves, ferrite aerial, dial and knobs. Valve line up—UCH81, UBF89, UCL83, UY8S. Long and Medium wave coverage.

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In response to numerous requests from delighted purchasers of our ''SUPER STEREO KIT" we have produced a "MONAURAL AMPLIFIER" on similar

- A UCL 82 valve provides a triode amplifying stage, and a pentode output stage (3 watts), enabling good amplification and sparkling reproduction to be combined with physical compactness (amplifier size, $7 \times 3\frac{1}{4} \times 6\frac{1}{4}$ in. high).
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5" loud speaker 14/6 extra.

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The product of a renowned maker, this stereo amplifier is composed of "ready-built" units, only requiring interconnection. This system has the advantage of being adaptable to fit any cabinet. Each unit is made from first-grade components, and valves used (ECL82, EZ80 range) are genuine Mullard. The comprehensive instructions supplied make the simple interconnection of units easy even for the novice

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TWO MIDGET AMPLIFIERS each of 3W output, good reproduction from both your stereo or monaural records. Both amplifiers complete with well-designed O.P transformers providing perfect matching 3-7 Ω speakers, and have remote bass, treble and volume controls. Size 5 x $2\frac{1}{2}$ x 3in. high (each amplifier).

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ISOLATED MAINS TRANFOR-MER of robust construction, may be mounted independently.

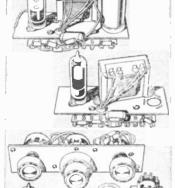
VOLTAGE SELECTION PANEL. Fitted with the "valve base" type of mains i/p selector and a channel out-

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CREAM DOUBLE PUSH BUT. TON SWITCH of neat design gives positive on/off switching.

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The ideal changer to suit the above amplifier

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4/6 | PX25 | 11/9 | U25 | 13/- | VP13C | 8/8 | 1H5CT 10/- 6AT6 | 6/2 | 6/2 | 11/9 | VP23 | 6/- 1L4 | 6/- 6AU6 | 6/2 | 6/2 | 11/9 | VP23 | 6/- 1L4 | 6/- 6AU6 | 6/2 | 6/2 | 6/2 | 11/9 | VP23 | 6/- 1L4 | 6/- 6AU6 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | 6/2 | ## CHAPANTZED VALVES ## CHAPAS | CHAPA GUARANTEED VALVES NEW and BOXED * PROMPT DESPATCH * POST 6d. per valve extra | Post 6d. ACHLODO 5/6 | 128G7 | 7/- | 35W4 | 7/- | 7/6 | 128H7 | 5/6 | 35Z4GT | 7/6 | 128H7 | 5/6 | 42 | 7/6 | 128K7 | 5/6 | 35Z3 | 15/6 | 8/6 | 128K7 | 7/6 | 35Z5GT | 8/6 | 6/6 | 128L7GT | 50C5 | 10/9 | 87-6 K6GT 6/6 7BS 5/8 979 6K7GT 5/6 7CS 7/6 979 6K7GT 5/6 7CS 7/6 979 6K7GT 5/6 7CS 7/6 970 6K26 18/6 7DS 12/6 12/6 14/6 7H7 8/6 12/6 14/6 7H7 8/6 12/6 14/6 7H7 8/6 12/6 14/6 7H7 8/7 11/9 6L18 19/8 81/2 2/6 8/6 6L19 19/9 19/2 2/6 8/7 6L19 19/1 19/2 2/6 8/7 6L19 8/7 19/2 2/6 8/7 6K10 19/8 19/9 14/6 8/7 6K10 19/8 19/9 10/1 19/6 8/7 6K10 19/8 10/1 19/8 8/8 6K10 19/8 10/1 18/7 18/7 6K17 7/6 12AT6 10/1 13/7 6K17 7/6 12AT6 10/1 13/7 6K17 7/7 12AT7 7/6 13/7 6K17 7/7 12AT7 7/6 13/7 6K17 19/8 12AU6 7/6 13/7 6K17 11/8 12AU7 7/6 13/7 6K17 6/7 8/9 12AU6 7/6 13/7 6K17 6/7 8/9 12AU7 7/6 13/7 6K17 8/7 8/9 12AU7 8/9 12AU7 7/6 13/7 6K17 8/7 8/9 12AU7 8 ACSPEN DD 25/9 ACSPEN 6/-14/-14/-8/-8/-50C5 10/9 50CD6G ACVP1/59/8 ATP4 3/8 28/6 AZI AZ3I 10/9 9/- 75 8/- 77 B36 14 -CBL31 22 9 CCH35 22 9 CL4 11 9 5/- 80 25- 142BT 25- 185BT 22/- 210DDT 25/- 210VPT 22- 83 6C31 7/- 6HA7 9/- 6CD6G 23/- 68G7 7/- 6D6 4/8 18 -15 9 CY31 99 9 89.77 9/- 10P14 18/- 2014 25/- 210V
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14/- 20A 9/- 12A 9/- 20A 9/- 30A
14/- 20A 9/- 12C 9/- 30P1 18/- 30A
14/- 20A 9/- 12C 9/- 30P1 19/- 30A
14/- 20A 9/- 12A77 10/- 30P1 11/- 30A
14/- 20A 9/- 3A0A 9/- 20A 9/- 3A0A
14/- 20A 9/- 3A0A 9/- 3A0A 9/- 3A DF96 8/6 DH 63 11/6 DH101 11/6 9/9 16/6 2/3 6U5G 2/3 6U7G 4/6 6V6G 9/3 EF508YL 6/6 HL23DD8-6/6 HL22 6-9/3 HL41 8/8 7/2 HN309 23-7 K40N 8 6 11/6 KF35 8-KF35 8-KK32 20 6 6/6 5/6 9 3 PCLN2 PCLN2 PCLN3 PL38 PL36 PL36 PLN1 1/9 1/8 EF55 40 8 6 EF80 EF85 3/3 1/9 EF86 10/9 8/-5/6

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5elf lubricating, capacity 60 g.p.h. at 30 lb./sq. in. Will operate O.K. on 12 v. ½ BSP inlet/outlet union. Only 15/6 each. P/P 2h6.

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Brand new moving iron instruments by famous manufacturer. Housed in polished teak case. 8in, mirror scale, 2 ranges, A.C or D.C. 0 to 160 v. and 0 to 320 v. Accuracy with-in 2%, £5/19/6 ea. P/P 3/6.



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Imported, brand new and imported, brand new and guaranteed. 1,000 ohm/ volt A.C./D.C. Volts D.C.: 10, 50, 250, 500, 1,000. Volts A.C.: 10, 50, 250, 500, 1,000.

Gurrent D.C. f mA., 100 mA., 500 mA. Resistance: 2,000 ohms and 200,000 ohms, Supplied complete with all instructions and

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VALVE VOLTMETERS No. 2. A laboratory instrument at a fraction of cost. Five ranges A.C. and D.C. 1.5 v., 5 v., 15 v., 50 v. and 150 volts. Operation 200/250 volts A.C. Supplied as new, fully tested and complete with internally mounted H.F. probe. £17/10/- each. P/P 10/-.



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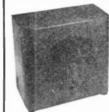
1961 model, 3 speeds 12, 32 or 71. Fitted with 3 separate motors, digital counter, press button switching, pro-vision for fitting vision ... extra steruc frond. Supplied with

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Frequency coverage 550 kc/s to 32 Mc/s supplied fully reconditioned and in perfect working order.

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115/230 volts. Brand new and boxed. ex-U.S.A. £15 each. P/P 10/-



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Will detect ferrous or non-ferrous metals. Complete, as new in transit cases. Supplied fully tested with instructions.

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Range 0/30 v. D.C. 1000 ohms per volt. Correct to B.S. 89 Pr. limits 6 inch mirror scale, £25 each. 3/6 P. & P.

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3 ranges covering 445-485 kc/s. Crystal controlled fitted with precision variable attenuators. Brand new, £15 each, 10/- carriage.

COLLINS TCS RECEIVERS



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Frequency coverage 1.5 to 12 Mc/s. Incorporates 7 valves, 1-125A7, I— 125Q7, 2— 12A6, 3— 1 2 5 K 7 . Power

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Senior model, table mounting. Supplied complete with full set of 9 coils covering 50 kc/s. to 30 mc/s. All re-

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Frequency coverage 95 kc/s to 40 mc/s. Ideal for all general radio work. Supplied fully tested and checked £7/19/6 each. P.P. 3/6. Operation is from 2 v. and 60 v. batteries but original Avo mains units can be supplied at 19/6 each extra.



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These special units contain a 1 microamp Tinsley galvonometer and a double selenium photo electric cell. Brand new £9/19/6 each. P/P 7/6

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Generator bell ringing, 2 line connection. Supplied fully tested, complete with batteries. 59/6 each. P/P 3/-.

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Perfect working condition. Thoroughly tested and realigned before despatch. Standard model B with new improved geared drive, £9/19/6 each. Carriage 7/6. Model L or N. These incorporate the trawler band 1.5/3 mc/s., £12/19/6 each. Carriage 7/6. Combined power pack and audio output stage operating from 200/250 volt A.C., to suit either model 85/- extra.

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Make simple inter com system. No batteries rebatteries re-quired. Just connect togother twin flex. Brand new only 15/- per new only 15/- per new only 15/- per new only 16. handset. P/P 1/6. Suitable twin flex 2½d. per yd.



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Perfect condition, 15/6 ea. P/P 2/6.

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B.S.R. Monarch UA8 4 speed record changers, £6/12/6 each.

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1,000 WATT MAINS ISOLATION TRANS-FORMERS. 230 volt primary, 230 volt secondary, Ex-Admiralty heavy duty type. New, boxed. 65 each. Carriage 10/-.

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125 kc/s to 20Mc/s As new condition. Supplied complete with valves, crystal and calibration charts.

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Also available less calibration charts only £9/10/- each.

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18 swg, four sided and with reinforced corners. 6 x 4 x 2½in. 3/6; 10 x 7½ x 2½in. 5/3; 7½ x 5½ x 2½in. 4/6; 11½ x 7½ x 2½in. 6/-; 13½ x 9 x 2½in. 6/9. Post extra.

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Covers 38 to 1,000 mc/s with 3 plug in R.F. units, TN16, 38-95 mc/s, TN17, 74-320 mc/s and TN18, 300-1,000 mc/s. Operation IIS volts A.C. 50-2,600 cps. Reconditioned as new to maker's spec., £75 each complete.

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Brand new. Incorporates a 6in. scale 3 amp. D.C. meter and variable rheostat for controlling current. Only 32/6 each. P/P 3/6.

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Twin 4 watt (or 8 watt monaural) employing two ECL82 and EZ80 rect., double-wound mains transformer, etc. Separate panel with bass, treble and volume controls. Indicator lamp, push-button on/off switch, elegant gold/cream knobs. Kit comprises two Amplifier Units and Power Unit, all 5in. x 2in. in size, fully assembled ready to be wired together. Kit is prised without Loudsneaders of that you can choose the type and Unit, all 5in. × 2in. in size, fully assembled ready to be wired together. Kit is priced without Loudspeaker so that you can choose the type and

LASKY'S PRICE Kit complete with new Mullard valves, full data, circuit diagram, assembly instructions and suggested layout 56/- Post 5/-.

SPECIAL OFFER OF SPEAKERS WITH THIS KIT

Two 5in. for 20/. Two 6×4 , 25/-. Suitable cabinets available to callers

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For 200-250 v. A.C. main. New and fully guaranteed. Few only

SAVILLE STEREO Pre-Amplifier and Control Unit. List £15. Lasky's Price 8 Gns. Post 3/6.

SPECIAL COMBINED OFFERS One Saville Twenty Amplifier and one Saville Pre-Amplifier 20 Gns. and Control Unit.

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Main Amplifier and Power Unit, 20 watts nominal, 30 watts, peak from "C" core distributed load stage. Freq. range: 34 c/s to 30,000 c/s±1dB at 20 watts. Distortion at 1,000 c/s and 20 watts. Distortion at 1,000 c/s and 20 watts <.0.1%. Mains transformer will sustain 100% overload continuously. Power supplies for Tuner: 300 v. 50 mA. 6.3 v. 2.5 amp. 4 valves: 2 EL34 push-pull, ECC81, GZ34. LIST £27

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Record level indicator. rewind. Facilities for recording from two inputs. Push-button controls. Plays for one hour on one reel of tape. Carrying Case with attractive rexine finish and detachable hinged lid. Size $104 \times 9 \times 6$ in.

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Complete Tape Recorder using Collaro Studio 3-speed deck, 1½, 3½, 7½ i.p.s. Twin track with pause control, rev. counter, latest type electronic recording indicator. Superimposing switch, volume and tone controls, 7×4 loudspeaker.

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LIMITED NUMBER ONLY The well-known MOTEK K10 Deck with push-button controls, 3 motors, 3-speed (12, 32, 7½ i.p.s.), rev. counter. Freq. response better than 40-12,000 c/s. at 7½ i.p.s. 2-tone grey finish. Listed at £22.

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Suitable case, callers only, 39/6.

COLLARO STUDIO TAPE TRANS-CRIPTOR. 3 motors, 3 speed 12, 32, 7½ i.p.s., takes 7in. spools. Push-button controls.

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HIGH FIDELITY TAPE RECORDER HEADS

Leading make, new and unused, or lower track. RECORD, PLAYBACK, high impedance. Double wound and will reproduce up to 12,000 c.p.c. at 7½ l.p.s. Azimuth adjustments. Output 5 millivolts at 1 Kc. at 7½ l.p.s. ERASE low

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lower track)

3in. 5in. 5lin. 7in. Slin 2/6 Post extra

COLLARO TAPE TRANSCRIPTOR Mk. 1V, fitted digital counter. List £25. Lasky's Price £16/19/6. Carr. & Ins. 12/6. Tape extra.

TAPE RECORDER PRE-AMPLI-TAPE RECORDER PRE-AMPLI-FIER. For use with any make of Tape Deck including Collaro, Motek, etc. Full recording facilities are provided for 7, 3½ and 1½ i.p.s. and multi-position switch gives automatic equalisation by negative feedback to each individual speed. 4 valves including magic eye level indicator. Overall dim.: 12×4×5in. Front panel: 12½×3½in. Sin. Front panel: 12½×3½in.
Attractive gold hammered finish.
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SPECIAL OFFER OF TAPE

Famous make plastic latest type plastic spools. Brand new, boxed and guaranteed. 1,200ft. on

7in. spool, 20/-1,800ft. (7in.) ...32/6 1,200ft. (5\)in.)

1,200ft. (5§in.) .21/-850ft. (5§in.) ...16/6 8COTCH PLASTIC TAPE 1,200ft. on 7in. spool....... 25/-

M.S.S. LONG PLAY TAPE 1,800ft. on 7in. spool...... 39/6 1,200ft. on 5%in. spool...... 29/6 25/6 7/11

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RADIO : TELEVISION : HI-FI : ELECTRONICS : RECORDERS

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" Diana," The high impedance moving coil mike with unique magnetised table base. Response 30-15,000 c.p.s. Response

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ACOS CRYSTAL STICK MIKE M.C.39/1, complete Listed at £5/5/--Lasky's Price 39/6

MINIATURE moving coil dynamic microphone, incorporating sw and complete with pocket clip-used for the "Fi-Cord." switch Post 1/6.

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B.S.R. type UA8	26	19	6
B.S.R. UA8, stcreo	£7	19	6
B.S.R. UA12, stereo	27	19	6
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COLLARO Conquest,			for
stereo, with monaural p.u	. £6	19	6
As above, stereo			
Post on all above			

GARRARD

Model	120		 82	8	0
Model					0
Model					
Model					
Model					nd
stere	eo head	ds	 £12	10	0
RC.88.			 £12	19	6
RC.88	stered		 £12	19	6
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SINGLE PLAYERS

Post on all above 5/

COLLARO JUNIOR 4-speed motor

PICK-UP CARTRIDGES

ACOS HGP.50 or HGP.37 turnover, crystal cartridge with L.P. and standard styli. List 39/7.

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AOCS 73-1A STEREO. List 52/6. Lasky's Price 29/6 post

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3½in, 4in, 5in, 6½in, 8in, 10in, 17/6 19/6 10/6 16/- 16/6 25/-2in 27/6 ELLIPTICAL

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DIATONIC "10-14 watts 12 Gns. CONCHORD" 30 watt 15 Gns. L45 4-5 watt Amplifier 25/19/6 LT45 Tape Deck Amplifier 12 Gns. 25/19/6 watt Amplifier ... 19 Gns. 50 L10 10-12 watt with pre-amplifier
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LS/3 Stereo Amplifier..... 7 Gns. LP.1, Tape Pre-amplifier... 9 Gns. All other types in stock.

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GARRARD 4HF, stereo or monaural, complete with plug-in head £18.19.0

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Also Lenco Connoisse	P117 6	etc.	



LASKY'S F.M. TUNER PRINTED CIRCUIT VERSION OF G.E.C. 912 "F.M. PLUS" TUNER FOR HOME CONSTRUCTION

Uses 5 valves, 2 germanium diodes and brand new T.C.C. condensers. The PRINTED CIRCUIT ensures that the I.F. and R.F. amplifiers are extremely stable at maximum gain and results are consistent on

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Details on request.

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200-250 v. A.C./D.C. Complete with 13 new Brimar valves, latest Fireball turner tuner covering all channels bands I and III (i.f. 33-38 Mc/s.). Ferroxcube line output transformer and wide angle 90° scanning coils, ion trap, latest electrostatic focus. All first quality components.

Overall dimensions 8×15½in.

Valve line-up: 3 PCF80, 1 PCC84, 3 B6W7, 1 PCL84, PCL82, PY82, PL81, PY83, EY51.

LASKY'S PRICE £18.19.6 Carr. & Ins. 7/6.

BRAND NEW BRIMAR 17in. C.R. TUBE, C17SM. 3-amp. heater, tatic focus. 12 months' guarantee.

LIST 10 gns. Lasky's Price \$6/19/6. Carr. & Ins. 12/6. electrostatic

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A few cabinets available to callers.

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TWO MATCHED SETS FOR STEREO 25 post paid.

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STEREO ADAPTOR CONVERTS ANY RADIOGRAM TO GIVE STEREOPHONIC

REPRODUCTION 2-valve Amplifier using EF80X and EL84 metal rectifier (full-wave bridge). Ma 50/60 c.p.s. Mains voltage 195-250, o.s. Ganged volume control and ganged tone control.
CAN ALSO BE USED AS A
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AMPLIFIER BARGAIN

6-watt, employing 4 EX80 rect., ECC83, feeding two E184 in push-pull. Separate con-trol unit with bass, treble and volume controls. Size of chassi 4½ × 4½ × 12in. Complete with new Mullard valves.

LASKY'S PRICE Post 4/6.

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Uses two valves, ECL82 and EZ80 and separate mains transformer to minimise hum. Incorporates Elac 8×5in. loudspeaker with output transformer mounted.
printed circuit 4×3×2¼in.
Lasky's Price 59/6 Size

Post 3/6.

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Large selection of various wellmakes at money-saving Call and select or write for known prices. Call and sell latest Bargain List.

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6 v. operation. For all L.P. and standard records. All components available separately.

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300 milliwatts push-pull output, using two OC71 and two OC72 transistors. Fully assembled, 79/8. Knobs 3/6 extra.

LOUDSPEAKER 30 ohms, 7 × 4in. elliptical, matched to amplifier, 25/-.

3-SPEED TURNTABLE

6 v., with rubber mat and speed adjustment, complete with t.o., adjustment, complete with t.o., crystal cartridge and two sapphire styli. 79/6.

CARRYING CASE

As illustrated, handsome two-tone finish. 17in. deep, 14in. wide, 54in. high. Well made and finished. 5\{\frac{1}{2}\]in. high. Well made \\
49/6. Batteries extra.

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49/6

LASKYS EVERYTHING FOR HOME CONSTRUCTOR & SERVICEMAN TEST METER IG.R. THE BARRAN RADIO

BARGAINS

NEW AND UNUSED

AN/20. Famous make pocket

AN/20. Famous make pocket size 18-range multi-test meter for amateur or service engineers. 5,000 ohms per volt A.C. and D.C. with accurate linear scales for the lower A.C. range. In black leatherette-covered case, 3\forall \times 2\forall 2\forall 1\forall in deep. LIST 9 gms.

Post 3/6. Leads 3/6 extra.

The KAPURA Mdl. U1. MULTI-RANGE TEST METER, incorporating 3in. rectangular meter.

Sensitivity: 1,000 ohms per volt A.C. and D.C. Ranges: (A.C. and D.C.) 0-10-50-250-500-1,000 v. D.C. current 0-100-500 m/a, 0-1 m/a. (used at 0-10 v. range).

Resistance: 1-2,000 ohms (centre 24 ohms) 100-200,000 ohms (centre 2.4 k.).

Size: 5in. × 3in. × 2\in. Weight: 22 ozs.

Fully guaranteed. LASKY'S PRICE 59/6 Complete with test leads. Post & Pkg. 3/6

Two



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Large selection, many by famous makers such as Cyldon, Brayhead, Plessey, Cossor, etc., all 1.F.s. New and unused. Let us quote you for the model required. Examples: 33-38 mc/s., 20/6, 6-9 mc/s., 59/6. 9-14 mc/s., 59/6, 14-25 mc/s., 59/6.

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P.N.P. Junction types.

AUDIO, suitable for high gain and low freq. amplifiers, and for output stages up to 250 milliwatts. Double spot—yellow and green.

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Type T81. Suitable for all audio Type Tal. applications.

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One dozen 35/- post free. Special prices quoted for large quantities. Enquiries invited.

OC44 15/-; OC45 15/-; OC70 8/6; OC71 8/6; OC78 15/-; (Matched Pair 30/-); OC73 14/-; OC16 54/-.

EDISWAN MAZDA TRANSISTORS. The very latest types: XB/102 7/6; XB/103 7/6; XC/101 10/- XA/101 12/6; XA/102 12/6.

SPECIAL OFFER. Set of 7 Ediswan Transistors: XA/101, XA/102, 2 XB/102 XB/103, 2 matched XC/101. Price 59/8.

CRYSTAL DIODES. General Purpos GEX00. each 1/-. Per doz. 9/-. All other type in stock.

" GOLTOP " POWER TRANSISTORS

All types in stock. Example: VIS/10P. Ideal for output stage of car-radio, will give approx. S watte operating from 12 v. Each 15/-, post free. Suitable Output Transformer for above, correct ratio, matched to 3 ohms, 9/6. Post 1/-, Driver Transformer, 9/6, Post 1/-,



FERRANTI. 12in. types T12/44 or 9in. type T9/8 4 v. heater.

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FERRANTI 17in. type TB17/10, 6.3 v.
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16in. METAL COME, famous make, type T901/A, 6.3 v., 0.3 amp. heater. £6.9.6

17in. 90 degrees C.R. TUBES

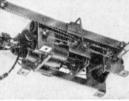
Seconds but in perfect working order and guaranteed.
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RE-GUNNED C.R. TUBES

GUABANTEE	D :	FOR	12	MONTES
15in. & 16 roun 17in. rect		25 10 25 19 25 19	0 6 6	Carr. & Ins. 12/6 12/6 12/6 12/6 12/6 21/•

CAR RADIO COIL PACK

(Superhet, I.F. 465 Kc/s)



As used in many famous makes car radios. A permeability tuned Coil Pack covering medium and long wavebands, with tuned R.F. stage wavebands, with tuned R.F. stage and complete with dial and pointer. Needs no ganged condenser. Its compact construction and small size, $7\frac{1}{2} \times 5 \times 1\frac{1}{2}$ in. enables it to be used in the smallest of car radios.

LASKY'S PRICE With circuit diagram and full data.

Post 2/6.

20,000 VALVES IN STOCK Mullard, Brimar, G.E.C., Mazda, Cossor, E.M.I., Philips, Pin-nacle, Telefunken, etc. Send for our latest Valve List.

SUB-MIN. RESISTORS, ith watt, most values available. Each 3id. Per doz. 2/6.

CONDENSERS, RESISTANCES. High stability Resistances, Electrolytics. All values and sizes stocked.

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CAN BE BUILT FOR ONLY 99/6

Post & Pkg. 5/-

contemporary design Handsome case, overall size 8½in. wide, 4½in. deep, 5in. high. 2 latest double-purpose valves EBF89 and ECL80, contact cooled rectifier. For A.C. mains 200-250 v. Med. and long wave, 5in. P.M. speaker. Plastic cabinet in cream, pastel green, pink, blue.

FULL DATA, instructions circuit diagram, shopping list 1/6. All components available separately.

LASKY'S CAR RADIO CAN NOW BE BUILT

ABSOLUTELY COMPLETE FOR £9.19.6



- ★ Small size. Will fit any car

- Transistor output New type Brimar valves
- ★ SIMMI SIZE. Will fit:

 ★ 12 volt operation

 ★ New Hybrid circuit

 ★ Transistor output

 ★ New type Brimar va

 ★ No Vibrator, 12 volt

 ★ T.C.C. Printed No Vibrator, 12 volt H.T. & L.T. T.C.C. Printed Circuit and ★ I.C.C. Finites
 Condensers
 ★ Tuned R.F. stage
 ★ Medium and long waves
 ★ Permeability tuning
 ★ 7in.×4in. elliptical speaker.

Instruction Booklet giving full details, illustrations, dimensions, circuit diagram and shopping list, price 2/6 post free (returned if you

watt watts, Accur-acy 5% and matched for 3, 15 and 600

25 milliwatte to 1 watt; 1 watt to 10 watts, Accurmilliwatts

ranges:

ohms. Ideal for constructors, hi-fi enthusiasts, engineers. COMPLETE KIT with full step-by-step instructions, circuit, data, \$9/8. Post free.

MINIATURE EARPHONES FOR POCKET TRANSISTOR RADIOS

High quality and remarkably High quality and remarkably sensitive, giving clear reproduction of music as well as speech. Complete with transparent ear-insert, 8ft. cord, sub-miniature jack and socket. Fully guaranteed.

Mdl. GR.5. Crystal
Earpiece, high imp.
Mdl. MR.4. Magnette
Earniece low imp.

10/-

10/-Earpiece, low imp. Post free.

SUB-MIN. COMPONENTS

As used in the smallest Japanese pocket transistor radios. Coils, Loudspeakers, I.F. transformers, Ganged Condensers, etc., now available from stock at lowest prices. Also in stock, all T.S.L. transistor-ised Miniature Units.

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Today may we congratulate Wireless World upon their Jubilee issue.



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THE CLYNE RADIO "DE LUXE" PRINTED CIRCUIT SUPERHET



(45

A may wave and band M) Superhet using latest miniavalves : ture valves EF85 and ECL80,

at (23) ECL80, plus contact cooled Rectifier. Incorporates Ferrite Rod Aerial and is of unit construction. Exceptional sensitivity and selectivity. Outstanding performance and quality T.C.C. condensers throughout. Easily constructed in one evening. Brown or ivory Bakelite cabinet. A.C. mains 200/250 v. All necessary components at special inclusive price of £7/19/6 plus 3/6 P. & P. Instruction Book with itemised price list available separately at 1/6 post free. Also available in De Luxe Cabinet (as illustrated) at 5/- extra.

ALL PARTS AVAILABLE SEPARATELY

THE "WAVEMASTER" 7-TRANSISTOR **LUXURY PORTABLE**

400 MILLIWATTS OUTPUT
To build yourself Medium and Long waves—Push-Pull Super-het A.V.C. Perfect Car Radio recention. Size 101- 11 (2)

To build yourself Medium and Long waves—Push-Pull Superhet A.V.C. Perfect Car Radio reception. Size 10in. x 63in. x 43in. at base tapering to 4in. at top.

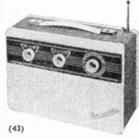
Very attractive two-tone grey Vynide covered cabinet with black and gold printed escutcheon plate, cream and gold knobs, handle and cabinet fittings. Weight—complete with long-life 7½ volt battery—1½1b. Mazda high-grade transistors throughout. Migh-Flux 7in. x 4in. Elliptical Speaker. Slow motion tuning. Co-axial socket at rear for direct connection to Car Radio Aerial Improved reception by use of seven-section plated telescopic aerial disappearing into Cabinet when closed, 34in. above Cabinet when fully extended.

Construction simplified by Bakelite chassis board with the following components already mounted: I.F. Transformers (3). Oscillator Coil, Trimmer Bank, Output Transformer, Interstage Transformer, Aerial Brackets and Earth Bar. SPECIAL INCLUSIVE PRICE for all required components full assembly instructions—nothing more to buy—is £10/19/6 plus 3/6 P. & P. Alignment service available. Full assembly instructions and individually priced parts list, all of which are available separately, 2/6, post free. available. Full assembly separately, 2/6, post free.

"OUR REPUTATION IS YOUR **GUARANTEE**"

All

required



Instruction

Book and

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6complete, post free

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STOP PRESS! All components available ex-stock for the "P.W. ROADFARER" TRANSISTORISED AM/FM RECEIVER, as described in "Practical Wireless," April issue. Send stamp for itemised price list. Usual components P itemised price list at special R. available inclusive P. special inclusive price available. separately price (I) New Look "RAMBLER" all dry s'het portable. NEW LOW "RAMBLER" Mains Unit (suits most portables)
"FAMILY FOUR" T.R.F. Mains Receiver
Standard JASON F.M. Tuner FMT1
Fringe area JASON F.M. Tuner FMF
JASON "MERCURY 2" Switched F.M. Tuner plus ITA/B.B.C. £2 7 2/6 2/6 1/6 2/-€7 15 0 Sound

JASON "ARGONAUT" AM/FM Chassis

JASON "ARGONAUT" AM/FM Tuner

F.M. Power Pack (suitable for most tuners)

R.C. 3/4 watt Amplifier (with Bass, Middle and Treble controls)

Zamp. Battery Chasses £10 10 €I 17 1/6 R.C. Jawatt Amplifier (with Bass, Friedre and Teorie College R.C. Transistor/Crystal Receiver ('phones extra)
R.E.P. I-valve Battery Receiver
"CRY-BABY" ALARM (Baby Alarm)
MULLARD SIO Amplifier (printed circuit) Ultra Linear Version £1 16 2/6 1/3 3d. 6 3d. 2/-9d. €3 12 1/6 ŏ (21) MULLARD SIO Ampliner (princed circuit, Otra Linear Visia)
(21) MULLARD SIO as above plus input selector and spare power supplies
(22) "DE-LUXE" With New Look Cabinet
(24) JASON J.T.V. 2 Tuner
(25) RADIO JACK 2/6 £11 10 1/6 €8 3/6 2/6 6d. 3/6 1/6 RADIO JACK
MULLARD TYPE "C" Tape pre-amp.

JASON W11 Wobbulator
JASON Valve Voltmeter EM10 (23 ranges)
NEW JASON F.M. TUNER FMT2 with built-in power supplies £12 9 2/6 3/6 2/6 €18 10 0 3/6 | JASON Valve Voltmeter ETIO (43 ranges) | STAND Valve Voltmeter ETIO (45 ranges) | STAND VALVE VOLTMET | STAND VALVE VOLTMET | STAND VALVE VALV 2/6 2/6 2/6 3/6 (35) 3/6 3/6 10/-(37 3/6 2/6 2/-3/6 (40i (42)

Instruction Books which contain full description, easy-to-follow practical wiring diagrams, theoretical diagrams, item-ised price lists, etc., are free of charge with all parcels but may be purchased separately as shown above.

PLEASE NOTE:—A selection of the above items are described more fully in this advertisement!!

NEW! "PAGEBOY" 2-TRANSISTOR
POCKET PORTABLE
Completely portable—NO EXTERNAL AERIAL
OR EARTH REQUIRED. This is an amazing
little receiver with built-in aerial and small
enough to be held in the
palm of the hand. Medium
wave reception at wonderful
volume. No fiddley tuning!
—condenser tuned! Supplied with drilled chassis
assembled with the
aid of the easy-tofollow assembly instructions provided.

Total cost of all necessary components, including transisters, wiring wire and even solder ONLY 32/6 plus 1/6 P. & P. Battery 3/- extra. Ardente type deaf-aid earpiece complete with cord and plugs extra at 12/6. Parts price list and East Lay-out Plans 2/- post free. Callers welcome to hear this set demonstrated at any of our branches. Our reputation is your guarantee.

SUPER PERSONAL POR-TABLE. A wonderful little set you can take any-where. Ideal for camping, etc. Detachable aerial rod supplied. Covers Medium waveband 200-500 metres. Can be band 200-500 metres. Can be built in approx. I hour. All necessary components available at the following SPECIAL INCLUSIVE PRICES: 1-valve version ONLY 35/- plus 2/-P. & P. Super 2-valve version ONLY 41/-. Plus 2/-P. & P. Send for point-report virtual statements with the send for point-report virtual statements.

Send for point-to-point wiring diagram and parts price list 2/- post free.
Extra for use with the above DLRS balanced
armature headphones, 7/6 pair.



Our supersensitive T.R.F. Receiver for home construction. Covers Long and Covers Long and Medium Wavebands, is housed in very smart plastic table



smart plastic table cabinet in Brown or Black. For A.C. mains 200/250 v. Comprehensive assembly instructions provided, including practical and theoretical diagrams, which are easy to follow and will enable you to complete this receiver which will be the envy of your friends. ALL NECESSARY COMPONENTS ONLY 79/6, plus 2/6 P. & P. Instruction book available separately if you wish to study before purchase at 1/6 post free.



(32)

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BY ALL LEADING MANUFACTURERS

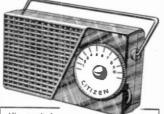
We stock equipment of Quality by all leading makers: i.e., Leak, Quad, Armstrong, Dulci, Ferrograph, Reflectograph, Vortexion, Tannoy, Linear, Wharfedale, Grundig, Goodmans, W.B., Rogers, Garrard, Lenco, B.T.H., Pamphonic, Simon, Brenell, Collaro, Telefunken, Fi-Cord, etc., etc. A full range of high qualicy cabinets to suit all purposes is on show, i.e., "RECORD HOUSING," "W.B." "A.D.," etc. Enquire about our interesting part-exchange scheme for personal callers. H.P. Available.

THE "CITIZEN"

Introducing our new Super-Sensitive 5-Stage (4 transistor plus diode) pocket transistor receiver—for full Medium Wave reception—with the following outstanding features.

- * Completely self-contained No external serial or earth required.
- * Gannine Siin, High Plux P.M. Spanker.
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- Geunine Ediswan transistors.
- Socket provided for personal listening.
- * Socket provided for connection to Car Aerial.
- Volume Control with on off switch-Condenser tuning.
- Easy assembly on colour coded pre-tagged circuit board.

(42)



All require! components including colder, etc. and battery full price of Plus 2/6 p. & p. ONLY 95/-

Yes, NINETY FIVE SHILLINGS ONLY! Nothing more to spend.

Suitable crystal deaf-aid type miniature ear-piece fitted with miniature jack plug at ONLY 7/8

Attractive polystyrene cabinet measures 5½ × 3 × 1½, chrome All parts available separately—Itemised list and full assembly instructions sent for 1/8 post free.

Hear this amazing little receiver working, at any of our branches.

SUPER I-VALVE SHORT-WAVE RADIO

World-wide coverage at most reasonable cost. Covers 40-100 metres with the coil supplied. Can be extended to cover 10-100 metres. Provision is also made 10-100 metres. Provision is also made for the addition of two extra valve stages. Employs the famous Acorn-type 954 valve.

All necessary components can be supplied complete with full assembly instructions at ONLY 35/- plus 2/-Send 2/- for point-to-point wiring diagram and price list.

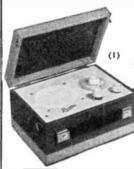
"POPULAR FOUR" NEW!

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PERFORMANCE I

A new three valve plus miniature contact-cooled restifier, mains T.R.F. Receiver is now available. New De Luxe Cabinet, polished walnut finish, cream trim, attractive horizontal dial (as illustrated). Quality Sin. P.M. speaker. Specially wound high gain super-sensitive Denco coils. Medium and Long Wavebands. Excellent Continental reception! Overall dimensions: 12in. x 6in. x 5in. A.C. 200/250 v. Simple construction with guaranteed results. Easy to follow practical and theoretical diagrams supplied. All necessary components, down to the last nut and bolt, are offered at a SPECIAL INCLUSIVE PRICE OF £5/5/6, plus 3/6 p. & p. Instruction book available separately 1/6, post free. ALL PARTS AVAILABLE SEPARATELY.

THE NEW LOOK RAMBLER PORTABLE



b

This wonderful little Medium and Long wave battery superhet incorporates IRS, IT4, IS5, 3V4 miniature valves, 5in. speaker and frame aerial. Housed in smart two-tone Red/Grey cabinet. All required components at the NEW All required components at the NEW LOW PRICE of £6/19/6, plus 2/6 p. & p. tow PRICE of £6/19/6, plus 2/6 p. & p. or with the latest low consumption "96 range" valves at the NEW LOW PRICE of £7/7/-, plus p. & p. Uses all-dry bacteries AD35 (1/6). B126 (9/-). Full descriptive instruction book, itemised price list, diagrams, etc., available separately at 1/6 post free.

(2) MAINS UNIT FOR ABOVE. This into battery compartment. A.C. 200/250 v. All required components at ONLY 47/6 plus 1/6 p. & p. or assembled and tested at £3/5-p plus p. & p. (Also suitable for many other portables.)

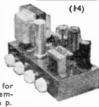
PRINTED CIRCUIT CAR RADIO

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(for Home Construction). We are proud to be able to offer this New type Car Radio employing up-to-the-minute circuitry, special 12 volt valves and transistorised output stage. The highest degree of sensitivity is assured by the incorporation of Permeability Tuning and a tuned R.F. Stage. Covers Medium and Long Wavebands. NO VIBRATOR PACK IS REQUIRED. This is a really compact receiver that will fit any car. Comprehensive assembly instructions are provided with all necessary components, including valves and transistor at a Special New Low inclusive Price of Only £11/19/6 plus 3/6 p. & p. Instruction booklet with itemised price list, full description dimensions, etc. available separately at 3/6 post free.

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Compare the advantages. Treble bass AND middle controls. For crystal or magnetic pickup. A.C. Mains 200/250 v. Valve line-up: 6V6GT, 6SG7 metal, 6X5GT. Negative feedback. Built on stove enamelled steel chassis, measuring only 8in. x 4in. x 13in. Four engraved cream knobs are included in the price of the complete kit with all necessary practical and theoretical diagrams at 4/5/s/- only, plus 2/6 p. & p. or Instruction Book fully illustrated for 1/- post free. This amplifier can be supplied assembled, tested and ready for use at £5/5/-. plus p. & p. 01 sp. 6. p. 01 sp. 6. p. bled, tested and ready for use at £5/5/-, plus p. & p.



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All required Components for the complete Osmor version as described in November issue of "Practical Wireless," now available at special inclusive price of £9/19/6 complete, including Printed Circuit and Osmor booklet. Overall size \$\frac{1}{2}\in, \times \frac{1}{2}\in, \times \frac{1}{2}\in \ti

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Covers local medium wave stations variably tuned. Compact self contained unit requiring only connection to aerial (no power supplies reed.) for 1st class reception when used in conjunction with your tape recorder or high gain amplifier. All necessary parts available at a special inclusive price of only 19/6. p. & p. 1/6.

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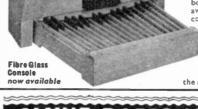
is simple to assemble, extremely sensitive and may be installed in a matter of minutes. Completely matter of minutes. Completely SAFE employing a double wound mains transformer. Attractively finished in Red and Grey (washable) "Lionide" with cream plastic escutcheon. Size only 7½in. x 3\frac{2}{3}in. x 6\frac{2}{3}in. Supplied in kit form complete with mike at ONLY 72/6 plus 2/6 p. & p. or assembled and tested 89/6 p. & p. 2/6. Suitable mike flex available at 3d. a yard. Instruction book and price list separately I/- post free. A.C. 200-250v.



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Readers will no doubt be pleased to know that our working model of this amazing organ for home construction, may be heard Showroom in Tottenham
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6 volt operation complete with pick-up £5/9/6, plus P. & P. 3/6. LATEST GARRARD MODEL 210. Four-speed manual or automatic, 10in. and 12in. records of matic. 10in. and 12in. records of same speed can be mixed in any order, wired for stereo, attractive white colour scheme. Price 10½ gns. plus 3/6 P. & P. LATEST B.S.R. UA14. 4-speed.

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These pocket-size multi-range test meters are of excellent quality and cover all the most useful ranges (A.C. Volts, D.C. Volts, resistance and current). Supplied complete with test prods, in-struction book and batteries. Model A.10 (2,000 ohms per volt) £4/17/6

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Only 12/6. P. & P. 1/-.
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SPEAKER. Size 13½in. x 8in. A
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3 ohm speech coil. 39/6 only,
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LOUDSPEAKER. 15 onns, 16 env. 64/10/-, P. & P. 3/6. 12in. RICHARD ALLAN P.M. LOUDSPEAKER. 3 ohm speech coil. Brand new. ONLY 32/6 plus

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Smallest yet available

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Two-pole two-way ONLY 2/6 EACH. P. & P. 6d.

Wholesale and manufacturer quantity enquiries invited on both of the above new items.

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TELEPHONE PICK-UP COIL. Designed to feed into the microphone input of either a tape recorder or any high gain amplifier. Easily attached to telephone by rubber suction attachment. The coil is electrostatically shielded to minimise hum pick-up. When positioned on telephone this model is more than adequate for a fully modulated tape recording. Brand new complete with Sft. shielded cable. on telephone tape recording. Brand

ONLY 14/-. P. & P. 1/6.

COLLARO TAPE PRE-AMPLIFIER AND BIAS OSCILLATOR.

Complete with power pack for use with Collaro Mk, 1V deck. 4 valve
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socket S m/v., auxiliary socket 500 m/v. Speed equalisation switch gives compensation at all 3 speeds. Full wiring instructions included. List price £21. Limited quantity only at £15/19/6. P. & P. 5/-.

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TAPERECORDER AMPLIFIER. Suitable for use with either of the above Tape Decks, and most other types. For A.C. mains, 4 watts output. 40–12,000 CP5 at 7½ i.p.s. ±3 db. Facilities for superimpose. Valves: 6BW6, ECL82, 12AX7, EM84, and contact cooled metal rectifier. valves: 50700, CLOS, 12AA7, ETION, and contract cooled metal rectiler. Radiogram input, microphone input, monitor facilities (can be used as straight through amplifler), volume control and separate treble and bass controls. Chassis measurement II½ x 3 x 4½in. Supplied complete with attractive grey/blue escutcheon plate finished in black and gold. Circuit diagram and connecting instructions included. Price £11/5- only, plus 3/6 P. & P. If purchased with either of the above decks, both items post free!

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Complete Elementary Course in French, Italian, German or Spanish. Phrase book supplied. 5" long play tape, 55 minutes at 3½ i.p.s. Price ONLY 29/6 per course, Post Free!

EXTRA SPECIAL OFFER!! A small three-valve PORTABLE RE-CORD PLAYER AMPLIFIER mounted on baffie 12 x 7in., with High Flux 61in, Loudspeaker. Valve line-up ECC83, EL84. Loudspeaker. Valve line-up ECC83, EL84, EZ80. Incorporates separate bass and treble controls. Max. output 3 watts. Will match all types of high impedance pick-up. Ready fo use, £5/12\dot6. P. & P. 3/6. NEW STYLE CABINET finished in two-tone Leatherette. Will accommodate above Amplifler and Baffle without modification, also most types of Ancillary Equipment. Overall size 18 x 13\frac{1}{2} x 8\frac{1}{2} n. Fitted with carrying handle, £3/9/6, plus 5/- P. & P. NOTE. If both items purchased together they will be supplied at a special inclusive price £8/7/6, plus 6/6 P. & P.

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A wonderful offer. This famous trans-No. 38 AFY WALFIELD AND A wonderful offer. This famous trans-receiver unit, with relay operated SEND/RECEIVE switch covering 7.4-9 Mc/s band, range approx. 5 miles. Good condition. ONLY 22/6, plus Good condition. ONLY 22/6, plus 2/6 P. & P. per unit (less accessories). Quantity export inquiries welcomed. AERIAL TUNING UNIT ZA0841 This well made ex-W.D. unit contains This well made ex-W.D. unit contains a host of useful components including: I mA. 2in. flush round M/C meter, I mA. Westinghouse full-wave meter rectifier. 5-pole 5-way heavy-duty silver plated wavechange switch. 3in. dia. silver plated rotary tuning indicator, 350 pF tuning condenser with invulsed coulers and 3iin. indicator, 350 pF tuning condenser with insulated coupler and 3½in. calibrated dial (0-180 deg.) etc., etc. Contained in strong metal carrying case 9in. × 9in. × 8in. with hinged lid. ONLY 27/6, plus 5/- C. & P. WIRING WIRE. 5 coils 10 yds., each coil, in different colours, contained in cellophane bag. 5/-, plus 9d.

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SOLDERING IRON with integral Stand and built-in Spot-light for illuminating work 200/250 v. ONLY 22/6. P. & P. 1/6. SOLDER. New boxed I lb. reels, 16 5.W.G. 50/50 at 8/6 only, plus 1/- P. & P. TRANESCONDERING INSTRUMENT

TRANSFORMER SPECIAL. Superior quality half-shrouded drop thro mains transformer. Input 200/250 v. Output 350-0-350 v. 80 mA.; 6.3 v. Output 350-0-350 V. 80 MA.; 6.5 V. 3 amps. 5 V. 2 amps. Ex-equipment but guaranteed O.K. ONLY 9/6, plus 1/- P. & P. R.F.26. Variable tuning. Brand new in sealed carton. ONLY 22/6, plus 2/- P. & P.

RCA AR88D RECEIVERS

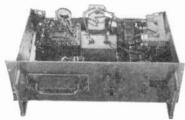
One of the most renowned American Communications Receivers ever manufactured. Widely used by all the Armed Services to maintain World-wide Communications and Monitoring Posts under all conditions. Employs 14 valves, and has 6 switched overlapping wave bands for complete coverage. Refinements include Mechanical Band Spread with Logging Scale, Automatic or Manual Volume Control, Automatic or Manual Noise Limiter, BFO with pitch control, RF and AF Gain Controls, Variable HF Tone Control, Variable Selectivity with Crystal Filter, Aerial Trimmer, Choice of Headphones or Speaker. Has internal mains power pack for nominal 115-230 volts A.C. In Black Crackled Case size 191in. W. x 11in. H. x 194in. D. Thoroughly reconditioned, immaculate in appearance, and in perfect working order. (Sovers 500 kc/s-32 Mc/s, price (add carriage 30)- and 50)- deposit on returnable transit case).

R1155 RECEIVERS

The famous Bomber Command Receiver known the world over to be supreme in its class. Covers 5 wave ranges: 18.5–7.5 Mc/s. 7.5–3.0 Mc/s. 1,500-600 kc/s., 500-200 kc/s., 200-75 kc/s. and is easily and simply adapted for normal mains use, ful: details being supplied. All sets thoroughly tested and in perfect working order before despatch, and on demonstration to callers. Fitted with latest type Super Slow Motion tuning assembly. Have had some use, but are in excellent condition. ONLY 29/19/6.

A.C. MAINS POWER PACK OUTPUT STAGE in black metal case to match receiver, enabling it to be operated immediately, by just plugging in, without any modification. Fitted with Sin. P.M. speaker 26/10/-. DEDUCT 10/- IF PURCHASING RE-CEIVER AND POWER PACK TOGETHER.
Send S.A.E. for illustrated leaflet, or 1/3 for 14-page booklet which gives technical information, circuits, etc., and is supplied free with each receiver. Add carriage 10/6 for Receiver, 5/- for Power Unit.

POWER UNITS TYPE 234



Primary 200/250 v. 50 cycles. Outputs of 250 v. 100 mA. and 6.3 v. 4 amps. Pitted double smoothing. For normal rack mounting (or bench use) having grey front panel size plin. x 7in. ONIY 59/6 (carriage, etc., 7/6). Or fitted with 24in. A.C. volts output meter, 79/6 (plus carr. as above).

CARRYING CASES, solid leather. SLIGHTLY USED, Internal dimensions 8\(\frac{1}{2}\)in. H. \times 8\(\frac{1}{2}\)in. W. \times 4\(\frac{1}{2}\)in. W. \times 4\(\frac{1}{2}\)in. W. \times 4\(\frac{1}{2}\)in. This is the solid property of the so

BC 342 RECEIVERS. A few only of these famous American sets covering 1.15-18.0 Mc/s. in six bands. Internal 115 v. A.C. Mains pack. A super receiver in first-class condition and perfect working order. ONLY 225 (carriage 15/-).

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12-WAY SCREENED CABLE. In 10ft, lengths, fitted with plugs, originally made for No. 19 Wireless Set. UNUSED. ONLY 15 - per lead.

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Frequency range 125-20,000 kc/s. in 2 bands. This is the United States Navy Model of the well-known BC.221 Frequency Meter, but has many additional features which increase its usefulness. Voltage stabilisation circuits and Crystal control ensure extreme securacy and in addition it is fitted with au Internal Modulation switch to allow use as a Signal Generator. Size only Sim. x Sin. x Sin. Pull information on request.

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Reads A.C, and D.C. Volts up to 1,000 in 5 ranges at 1,000 o.p.v., D.C. Current (3 ranges) to 500 mA. Resistance readings to 200 Kohms in 2 ranges, Basic movement 200µA sensitivity. Easily sensitivity. Easily read open scale. Dimensions 5½in. x 3½in. x 3½in. x 24in. Beautifully made, and fully guaranteed. Complete with leads, prods and internal battery. ONLY 59/6



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Similar specification to LM 14 Frequency Meter below, but does not have internal modulation or voltage stabilising circuits. Complete with original calibration book, crystal, valves, and instruction book. Used, but in very good condition. ONLY £16. Illustrated descriptive leaflet available on request.

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Type CV 1596 equivalent to Cossor O9D as used in cacilloscopes by Cossor (3:39 series). Hartley and Erskine (1:3 series). Listed at £12/10/s. Our price £2/19/6 (carriage 5/6). Brand new in makers' crates.

METERS

	F.S.D.	SI	ZEA	ND	TYPE	PRICE
50 50 00 1 00 20 40 5	microampe microampe microampe microampe miliamp miliamp miliamp ampe ampe voite voite	D.C. D.C. D.C. D.C. D.C. D.C. D.C. D.C.	2½in. 3½in. 2½in. 2½in. 2½in. 2in. 2in. 2in.	Proj. Flush Flush Flush Flush Plush Flush Proj. Proj. Plush Flush Flush	elreular circular circular circular circular circular circular circular circular circular circular	59/6 80/- 39/6 30/- 50/- 12/6 7/6 12/6 25/- 25/-
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HIGH FREQUENCY A.C. VOLTMETER

A First Grade Moving Iron Instrument with 6in. Mirror 8cale, reading up to 150 volts A.C. at 400 and 1,200-2,400 cycles. In aubstantial Oak case with removable lid, overall size 8½10. x8½10. x8½10. x8½10. Recently made for the Air Ministry. by Everett Edgrumbe, and in perfect order. Brand New & Unused, ONLY 27/10/-. Can also be suppiled for 50 cycles, use either 0-180 or 0-300 volts.



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18 VOLTS AMERICAN DYNAMOTOR. Delivers 220 volts at 100 mills. Size $\delta_j \times 3j$ in. diameter. Ideal for running Radio and Electric Shaver etc., from car battery ONLY 32/6.

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Utilises 4 valves I each 5Z4G, 6V6G, 6J7G, 6J5G and high quality components such as "C" Core Transformers and Block Paper Smoothing Condensers. AC Mains Pack for nominal 110 × 230 volts. Provision for 600 ohms on High Impedance Input. Output to 600 ohm Line. For normal use only requires changing Output Transformer. Output approximately 4 watta. Designed for Standard Rack Mounting having grey front panel size 19in. × 7in. All connections to rear panel, front having "On/On" Switch Gain Control Indicator Light. Puses and Valves Inspection Panel. BRAND NEW IN MAKER'S PACKING. ONLY £4/9/6 (carriage 10/6).

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Build a high quality recorder in the £70 class for only

Carr. 17/6.

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Can be assembled in | hour.

INCOEPORATING THE LATEST COLLARD STUDIO TAPE TRANSCRIPTOR, THE LITEST HOLLARD STUDIO TAPE TRANSCRIPTOR, THE LITEST HOLD TAPE AMPLIFIER. A RICH FLUX 4 (a). LOUDFEREER, Reed of Best Quality TAPE, Spart Tape Spool, a Portable Cabinet, size approx. 18 × 18 × 9in., insiabed in durable and stiractive due-tone Policerome, and connection diagram for wiring amplifier to transcriptor.

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WATTS * MAGIG EYE RECORDING LEVEL INDICATOR * 3 WOTORS

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FULL 7is. DIAMSTER REELS OF TAPE. * HEGLIGIBLE HUM. * ZETTERLY REFERETIVE AUTOMATIC ERASURE.

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Design of a high quality Radio Tuner Unit (specially suitable for use with any of our Amplifiers). A Triode Heptode Fichanger is used. Pantode I.P. and double Diode Second Detector delayed A.V.C. is arranged so that A.V.C. distriction is avoided. The W. Ch. 8w. incorporates Gramposition. Controls are Tuning, W. Ch. and Vol. Output will load most Amplifiers requiring 800 mV. input depending on Ae location. Only 250 v. 15 mA H.T. and L.T. of 6.3 v. 1 amp. required from amplifier. Size of unit approx. 9-6-7in. high, Send 8.A.E. for illustrated leaflet. Total building cost is \$\frac{24}{15}/-\text{.} - \text{.} Point-to-Point wirting diagrams and instructions \$\frac{2}{6}/6\text{.} - \text{.} Point-to-Point wirting diagrams

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SPEAKERS

IIF1012 10 watts, 15 ohm (or 3 ohm) speech coil. Where a really good quality speaker at a lw price is required, we highly recommend this untt with an amazing performance. 24/10/9. Please state whether 3 ohm or 15 ohm required. BASS EXPLEX CABINET. Specially designed for above specier. Acoustically lined and ported. Pollabed walnut veneer finish. Size 18 × 12 × 10 in. Strongly made. Handrome appearance. Ensure superb reproduction for only 23/18/6.

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or factory of outdoor use.

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Tannoy 7.5 ohms 8 watte
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Parmske horn type, highly efficient.

Handles up to
10 watta. 15 ohm, 200 ohm
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E.G.A. 20 watt rating, 3
ohm, 15 ohm, 200 ohm and
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ACOS HI-FI CRYSTAL 'MIKES' Mic 30 hand or Mic 30 hand or Desk type

27/9 (45/-)
39-1 Stick type

39/6 (5 Gns.) Limited number

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Type BM1. An all-dry battery eliminator, Size S\$\frac{1}{2} \times 2\$\frac{1}{2} \times 2\$\frac{1}{2}\$. Completely replaces batteries supply 1.4 v. and 90 v. where A.C. mains 200-350 v. 50 c/s is available. Buitable for all battery portable receivers requiring 1.4 v. This includes latest low consumption types. Complete kit with diagrams 39/9 or ready for use 48/9. Supplies 120 v. 90 v. and 60 v. 40 mA and 2 v. 0.4 s. to 1 sump. fully smoothed. THEREBY COMPLETELLY REPLACING BOTH H.T. BATTERIES AND L.T. 2 v. ACCURULATORS when connected to A.C. mains supply 200-220 v. 50 c/s. SUITABLE FOR ALL BATTERY EEECEIVERS normally using 2 v. accumulator. Complete kit with diagrams and instructions. 49/9 or ready for use 59/6 FOWER PAGK KITS. Only 19/11. Pully smoothed H.T. output of 250 v.

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RADIO DESIGN. Employing 2 Brimar R.F. Transistors, CABY A10 Basic meter, sensitivity 155 micro-ampa. 1 output Transistor, and crystal diode, Ferrite Rod Aerial, A.C. and D.C. ranges. 24.17/6, miniature Speaker unit. Handsome Piastic Case. Constructional Envelope 1/6. Total building cost 49/9.

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VALVES! Full range at really competitive prices.

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design of a 3 lve 200-250 v. A.C. mains L. and M. wave T.R.F. receiver with selen ium rectifier. ium rectifier. For inclusion in cabinet illustrated or wal-nut veneered type 1t employs valves 6K7, 8P61, 6P6

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Above ready for use with mains and output leads. Cases well ventilated and

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TRANSFORMERS 200-230-250 v. 50 c/s. 0-9-15 v. 1‡a. ...

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R.S.C. A12 STEREO AMPLIFIER KIT

4 GNS. + 3 watt (total 6 watt) Carr. and packing 7/6.

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R.S.C. STEREO/TEN HIGH QUALITY

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L.T. Types	H.T. Types H.W.
2/6 v. 1 a.h.w 1/9	190 v. 40 mA 3/9
8/12 v. 1 a.h.w 2/9	200 1. 00 mm G/11
Following F.W. (Bridge)	250 v. 60 mA 4/11
8/12 v. l a 3/11	250 v. 80 mA 6/11
8/12 v. 2 a 6/11	250 v. 250 mA 12/9
8/12 v. 3 a 9/9	Contact Cooled
8/12 v. 4 a 12/3	250 v. 80 mA 6 11
8/12 v. 5 a 14/6	250 v. 50 mA F.W.
8/12 v. 6 a 15/6	(Bridge) 8/11
8/12 v. 10 a 25/9	250 v. 75 mA F.W.
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6/12 v. variable charge rate up to 6 amps. Consisting of Mains Trans., F.W. (Bridge) Selenium Rectifier, 0-7 amp. meter, Rheostat with knob, fuses, fuse-holders, panels, plugs, and circuit. Only \$8/6. Post 4/16 Post 4/6.

EX. GOVT.

0-9-15 v. 21 a.

0-9-15 v. 3 a. 0-9-15 v. 3 a.

8/6.

Diameter 25in. approx. Scaled 0-100. 0-50 micro-amp. Dias Flush mounting, 29/6.

EX. GOVT. MAINS TRANSFORMERS

Pr. 0-110-200-230-250 v. 275-0-275 v. 100 mA, 6.3 7 a. 5 v. 3 a. 7 a. 5 v. 3 a.

Input 200-250 v. 50 c.p.s. 250 v. 60 mA 6.3 v. 2 a...

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100 mA Patead 22/9 10/11 27/9 watta, 0-110/120-230/250 v. ...

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Consisting of Mains Transformer, F.W. Bridge, Mctal Rectifier, well ventilated steel case. Fuses, fuse-holders, grommets, panels and circuit. Carr. 2/9 extra. panels

6 v. or 12 v. 1 amp	24/
As above, with ammeter	32/
6 v. 2 amps	25/
6 v. or 12 v. 2 amps	31/
6 v. or 12 v. 2 amps	42
(inclusive of ammeter)	
6/12 v. 4 amps	49/
6 v. or 12 v. 4 amps, with	
variable charge rate selector	

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Battery Chargers and Kits for 200-230-250 v. 50 c/s. A/C. Mains

6 v. or 12 v. 2 amps. Fitted Ammeter and selector plug for 6 v. or 12 v. Louvred metal case, finish tractive hammer Ready for mains blue. Ready ion use with mains and output leads. Double Only Carr. 3/9. 49/9

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6 Transistor Superhet Radio. Full constructional details etc. 1/8. All required parts including attractive plastic case and dial, printed circuit and first grade transistors. Only £9/19/6

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60 mA 10 h. 400 ohms 3/11
100 mA 7 h. 100 ohms 5/11
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100 mA 5-10 h. 100 ohms 10/9
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HIGH PILL UNITERPLOYING SIX VALVES, EP96, BOC38, 807, Tone EMPLOYING SIX
VALVES. EF96,
EF96, ECC38, 807,
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stages are incorporated. Sensitivity is
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Only 12 millivolt
minimum input is
required for full
output. THIS EMSURES THE SUITABILITY OF ANY
TYPE OR MAKE
OF MICROPHOME
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OR PICE-UP. Separate
Bass and Treble controls
give both "lift" and "cut"
with ample tone correction
for long playing records. An extra
input with associated vol. control
is provided so that two separate
inputs such as "mike" and
gram, etc., can be simultaneously is
with High Is INCLUIDED FOR A
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is provided so that two separate inputs such as "mike" and gram, etc., can be simultaneously applied for mixing purposes. AN OUTPUT SOCKET WITH PLUG IS INCLUDED FOR SUPPLY OF 300 v. 20 mA. and 6.3 v. 1.5 A. FOR A EADIO FREDER UNIT. Price in kit form with easy-to-follow wiring diagrams. Only 19 months' guarantee. 14 GMS. TERMS ON ASSERBLED UNITS. Cover as illustrated Type 807 output valves are used with High Quanity Sectionally 18/9 extra. Wire wound output transformer specially designed for Ultra Linear operation. Negative feedback of 20 D.B. in main loop. CERTIFIED PERFORMANCE FIGURES ARE EGUAL TO MOST EXPENSIVE UNITS AVAILABLE. Prequency response ± 3 D.B. 30-20,000 c/s. Tone Controls ± 12 D.B. at 50 c/cs. ± 12 D.B. to - 6 D.B. at 12,000 c/cs., hum and noise 70 D.B. down. Good quality reliable components used: Chassis finish blue hammer. Oversall size 13 v.9 v.9m. approv. Fower consumption 150 watts. For Ac. mains 200-220 v. 50 c.s. Outputs of 3 and 15 ohm speakers. EQUALLY SULKABLE FOR THE COMPONENT OF CO. SULVEY HALL, OUTS 50 C. TOTE DE ELECTROPIC DESAS. GUITAR, do. FOR DANCE HALL, OUTS 50 C. TOTE DE ELECTROPIC DESAS. GUITAR, do. FOR DANCE HALL, OUTS 50 C. TOTE DE ELECTROPIC DESAS. GUITAR, do. FOR DANCE HALL, OUTS 50 C. TOTE DE ELECTROPIC DESAS. GUITAR, do. FOR DANCE HALL, OUTS 50 C. TOTE DE ELECTROPIC DESAS. GUITAR, do. FOR DANCE HALL, OUTS 50 C. TOTE DE ELECTROPIC DESAS. GUITAR, do. FOR DANCE HALLS. OUTS 50 C. TOTE DE ELECTROPIC DESAS. GUITAR, do. FOR DANCE HALLS. OUTS 50 C. TOTE OF THE MIXED FIRST. EXPORT ENQUIRIES INVITED.

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For 200-250 v. 50 c.p.s. A.C. mains. Overall size only 11½ × 2½ × 2½m. Fitted Vol. and Tone Control with mains switch. Designed for use with any kind of single player or record changer unit. Output for 2-3 ohm speaker. Guaranteed 12 months. Only 59/6.

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PUSH-PULL ULTRA LINEAR OUTPUT "BUILT-IN" TONE CONTROL PRE-AMP **STAGES**

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JUNIOR 5 WATT, High Quality Output, Separate JUNION 5 WATT, High Quality Output, Separate Bass and Treble "cut" and "boost" controls. Sensitivity 15 mv. High Flux 8in. I/speaker. Input sockets for Radio/Tape or Gram Pick-up and Mike /Instrument Pick-up. Elandsome strongly made cabinet (size approx. 14×14×7in.). Finished in attractive and durable polychrome and fitted carrying handle.

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cut me. Two Loudspeakers are incorporated in 12in.
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12in, 20 WATT 15,000 line l'apeakers 15 ohms in Cabinet finished as above. Size $18 \times 16 \times 8$ in. £7/19/6 or Deposit 17/9 and 9 monthly payments of 17/9.



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(15 ohins), consisting of a high quality 12in.speaker of orthodox design support-ing a small elliptical speak-er ready wired with choke and condensers to act as tweeter. This high fidelity unit is highly recommended unit is highly recommended for use with our All or any similar amplifier. Rating is 10 watts. Gauss 12,000 lines. Price only £5,19/6. Or Deposit 13/9 and 9 monthly payments of 13/9.

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There are no "better value for money" Tape Recorders on the market—if you can't call and hear them send S.A.E. for fully call descriptive leaflets.



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- (d) COMPLETE KIT to build the HF/TR3 Amplifier, together with the COLLARO "STUDIO" DECK
- ASSEMBLED and TESTED above, but HF/TR3 (b)
- COMPLETE KIT to build the HF/TR3 AMPLIFIER with the BRENELL Mk. V TAPE DECK

29/6 Jointing Tape

## A LARGE PURCHASE OF BRAND NEW and FULLY GUARANTEED TRUVOX and GARRARD TAPE EQUIPMENT ENABLES THESE OUTSTANDING PRICE REDUCTIONS

THE "MODEL HF/G2R" PORTABLE TAPE RECORDER (Original Price #33.0.0)

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FOR 22 GNS. H.P. Dep. '24/14'. 12

ONLY CORNER on months 21/13/8. (Carriage and Ins. 10/- extra.)

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"MAGAZINE" TAPE DECK and MATCH

"MAGAZINE TAPE MAGAZINE and AND APPLIFIER. Based on the successful MULLARD TYPE "A" DESIGN and apecifically developed to operate the GARBARD DECK. PRICE INCLUDES THE GARRAND TAPE MAGAZINE and sin. SPOOL OF DOUBLE PLAY TAPE. A Twin Track Recorder operating at 3/11./

sec. providing up to 1 hour 10mins, playing time. The outstanding features being excellent performance and simplicity of operation. Incorporates RET. SPEARER SOCKET. also operates as independent amplifier for direct reproduction dio timer. Weighs only 22/h.

simplicity of operation. Incorporates RAT, SPRARGE SOURES, from P.U., mike or Radio tuner. Weighs only 22th.

WE ALSO OFFER DECK and AMPLIFIER OWNESTED, TESTED, FOR INMEDIATE OPERATION, 19 rms. H.P. Dep. 24 and 12 months 21/9/4. Carriage and Ina. 10/·ex.

INCLUDES SPEAKER. tape Magazine and 4in. Spool of Double Play Tape. Comprises a complete tape recorder chassis ready for easy fitting into cahinet.

"MODEL TK/Mk. IV" PORTABLE TAPE RECORDER Original Price 248/10/-

FOR \$36.10.0 PRICE INCLUDES A 7in.
ONLY
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INCORPORATES THE TRUVOX Mk. IV TAPE
DECK. ROLA/GELESTION 9 x 5in. LOUDSPEAKER and the Truvox Type "K" AMPLIFIER specifically developed by Truvox Ltd. tocorrectly operate their Mk. IV Tape Deck.
This combination affords first-class tape recording facilities.

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A Twin Track Two Speed model operating at 31 and 74 in./sec. Incorporates SAFETY BUTTON (prevents accidental erasure). Ext. Speaker.
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WE ALSO OFFEE THE DEUK and AMPLIFIER AS FOLLOWS: Mk. IV TAPE DECK, 216/10/-. H.P. Deposit 23/6/-. 12 months 21/4/3. TYPE "K" AMPLIFIER, 215. H.P. Deposit 23. 12 months 21/2/9. COMBINED ORDER FOR BOTH DECK AND AMPLIFIER, 230. H.P. Deposit 26. 12 months 22/4/-.

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OF PARTS

Designed by MULLARD-presented by STERNS strictly to specification
"5-10" MAIN AMPLIFIER MULLARD

Alternatively we supply ASSEMBLED AND TESTED..... £11.10.0

ABOVE INCORPORATING PARTRIDGE OUTPUT TRANSFORMER 21/6/- extra

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COMPLETE MULLARD A VERY HIGH QUALITY AMPLIFIER DE OPED FROM THE VERY POPULAR 3-V. 3-WATT AMPLIFIER DESIGNED IN MULLARD LABORATORIES.

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#### **MULLARD'S 2-VALVE** PRE-AMPLIFIER TONE CONTROL UNIT

Employing two EF86 valves and designed to operate with the Mullard MAIN AMPLIFIER but also perfectly suitable for other makes. Supplied strictly to MULLABD SPECIFICATION and incorporating:

• Equalisation for the latest B.I.A.A. characteristica.

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• Input (a) Direct from High Imp. Tape Head, (b) From a Tape Amplifier or Pr.

• Sensitive Microphone Channel.

• Wide range BASS and TREBLE Controls.

Price: COMPLETE KIT

OF PARTS

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ASSEMBLED AND TESTE

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COMPLETE MULLARD 5-10 AMPLIFIER
The popular and very successful complete "5-10" incorporating Control Unit
providing up to 10 watta high quality reproduction.
Specified components and new MULLARD VALVES are supplied including
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Self powered with Cathode follower output. Incorporates Two inputs for CRYSTAL MICROPHONES, one for CRYSTAL PICK-UPS and a Fourth for Radio or Tape. WIT OFFERS 10.88EMBLED \$10.0.0 Farms: Deposit AND TEMPEJ 10.0.0 Ferms: Deposit AND TEMPEJ 10.0.0 forms: Deposit AND TEMPEJ 10.0.0 forms: Deposit \$2 and 12 months at 15. Model I.L. one microphone input matched for moving coll or ribbon mike \$1/177- extra.



PRICE REDUCTIONS

both Assembled and Tested 218.18.1 H.P. TERMS: Deposit £3/16/- and 12 months of £1 7/8

MIXING UNIT

(a) The COMPLETE KIT OF PARTS to build both the "5-10" Main Amplifier and the 2-Stage Pre-Amplifier Control Unit

(b) The " 5-10" and the 2-Stage Pre-Amplifier

(c) The COMPLETE KIT OF PARTS to build the Dual Channel "3-3" Amplifier and the the Dual Channel "3-3" Amplifier and Dual Channel Pre-Amplifier Control Unit

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COMPLETE STEREO AMPLIFIER a low priced but good quality Stereophonic Amplifier. Out a for Crystal Pick-ups and Radio Tuner. put power is 4 watts. Inputs for

£8.10.0 KIT OF PARTS .... £10.10.0 or ASSEMBLED....

## STEREO DUAL CHANNEL PRE-AMPLIFIER

This model incorporates two 2-vaive Pre-Amplifiers (described above) combined into a Single Unit enabling it to be used for both STEREOPHONIC and MONAURAL operation. It is designed primarily to operate with our range of MULLARD MAIN AMPLIFIERS but will also operate equally well with any make of Amplifiers requiring an input of 250 m v.



£9.18.9

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£10.10.0 £9.10.0

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Price: COMPLETE £12.10.0 Alternatively ASSEMBL. RIT OF PARTS £12.10.1 ASSEMBL. and TESTED H.P. Terms on assembled unit: £3 Deposit and 12 months of £1/£1-Alternatively ASSEMBLED £15.0.0

# Mk. II "Fidelity" FM TUNING UNIT An attractively presented Unit incorporating MULLARD PERMEABILITY TUNING HEART and corresponding Mullard valve line-up. Very suitable to operate with our Mullard Amplifiers.

Our kit is complete to the MULLARD specification includ aponents, valves and PARMEKO OUTPUT TRANSFORMER disputs for 78 and L.P. records plus a Radio position. Extruming Unit is also available.

wo MULLABD 3-3 Main Amplifiers on one chassis. Operates with MULLARD RE-AMPLIFIER. Output power 6 watts. Inputs for Crystal Pick-up and 7. \$10.0.0 or ASSEMBLED. \$11.15.0

STEREO "3-3" MAIN AMPLIFIER

FOR THE CONSTRUCTOR ... £10.10.0 or ASSEMBLED £14.5.0

SPECIAL CASH ONLY OFFER!!

cified components.

STEREO PRE-AMPLIFIER.

KIT OF PARTS ....

The very attractive PORTABLE AMPLIFIER CASE together with a good quality GRAM AMPLIFIER and a matched P.M. SPEAKER, ALL FOR ONLY \$8.7.6 The Amplifier £8.7.6 macnee F.m. SPEARES. ALL FOR ONLY. (Plus 76 carr. and ins.). The Amplifier consists of a 2-stage design incorporating the 3 modern BVA valves and has separate BASS and TREBLE CONTROLS. The Portable Case will also accummodate almost any make of Autochanger and is attractively finished in Grey Colour Rexine—WE ALSO SUPPLY SEPARATELY:—

(a) The 2-stage (plus Rectifier) AMPLIFIER (b) The PORTABLE CARRYING CASE

(c) 6 in. P.M. SPEAKER ..... 23 17 6 (Carriage and 18 9 Insurance 4/- extra)



Hi-Fi" LOUDSPEAKERS WE HAVE IN STOCK A COMPLETE RANGE BY GOODMANS-WHARFEDALE-

ILLUSTRATED AND PRICED LEAFLETS ON REQUEST

"ADD - A - DECK" THE "ADD - A - DECK"
INCORPORATING GARRARD "MAGAZINE"
TAPE DECK and the MATCHED MODEL HF GEP
PREAMPLIFIER. Supplied on ONE CHASSIS
(as illustrated) READY FOR USE.
PRICE: Including GARRARD MAGAZINE
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TAPE (Carr. & Ins. 10/- extra).
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Provides complete tape recording facilities and
designed to operate through the plek-up socketa
of the providing up to 1 hour 10 mins. playing time.
Only needs connected to the Pre-amplifier and operates at 31in.
sec. speed, providing up to 1 hour 10 mins. playing time.
Only needs connecting to the mains supply and pick-up
socketa. Very simple to operate and easily installed in a cabinet only four fixing screws
being required.

being required.

H.P. TERMS ARE AVAILABLE ON ALL EQUIPMENT OVER \$9. FULLY DESCRIPTIVE LEAFLETS ARE AVAILABLE FOR ALL EQUIPMENT, BUT PLEASE SEND S.A.E.



THE EMI 4-speed single record player 4 gns. THE REU 4-speed single record player with separate crystal plok-up.

B.S.E. MONARCE UAS 4-spd, Mixer 26.19.6
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THE REW COLLARO "GOO" 4 speed autochanger unit with Studio "O" \$7.19.6

pickup.

The NEW COLLARO Model RP594, 4 speed Single Record Player, 

CHYSTAI PICK-UP.

THE NEW B.S.R. Model UA12 is in stock. A 4-"SPEED" MIXER AUTOUHANGER
UA12 is also available incorporating the B.S.R. STEREO Pick-up, plays L.P. and 78 records.

GABRARD EC209 4-speed Autochanger fitted with latest Crystal

The new GARRARD Model 4HF High Quality Single Record Player itted with the latest T.P.A. 12 Pick-up arm and G.C.S. Crystal Cartridge GARRARD Model TA, Milk. II Single Record Player litted with high output Crystal Pick-up, detachable head.

HIRE PURCHARE TERMS available on all units £8/19 6 and over Carriage and insurance on each above 5/- extra

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RANGE OF "EASY TO ASSEMBLE" PREFABRICATED CABINETS
Designed by the W.B. "STENTORIAN" COMPANY for "HI-FI" Loudspeaker systems
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Very special offer of compact 3 unit fixed frequency mobile Transmitter/Receiver equipments just out of service from a provincial police force.

● Transmitter 7in. wide × 12½in. high × 13½in. deep.

Xtal oscillator (xtal not supplied) 1st and 2nd Tripler, final and modulator stages. 3 Mullard miniature EF42, QVO4—7 and 3 x 2C34 all supplied. Cathodes and grids connected to metering jacks, with slots in side of case for tuning up each stage.

Receiver: 5in. wide, 11in. high,

♠ Receiver: 5in. wide, 11in. high, 12in. deep twin case.
Upper deck: 2 x EB34 and 4 x EF50 type valves. 6 pin power input two metering sockets.
Main chassis: 2 x EF39, 6K8, L63, 6V6, and 4 x EF50 type (Xtal not supplied).
3 1.F. coils in cast boxes.
Xtal frequencies 9.1 Mc/s. I.F. 2.9 Mc/s. Signal Frequency 79.1 Mc/s.

Power Unit 7in, wide 121in. high × 131in. deep.

12v. dynamotor giving 350v. DC at 180 m/A. Londex and 2 x GPO type Relays,

Offered in sets, at the "Job Lot" price of Carr. Paid. the three

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Type 75C, comprising RF Unit, RF Driver, RF Power Amplifier, Modulator, Modulator Power Unit, and Control Unit, all in 6 foot high 19 inch enclosed rack with full length rear access doors. This was the RAF ground station for operational communication with aircraft in the 100-150 Mc/s range and it is suggested that substitution of a suitable VFO for the existing RF Unit would provide the basis for an exceptional rig. Warehouse inspection invited.

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Highly sensitive device consisting of a ferrite encapsulated 160 kc/s coil with a moveable ferrite core attached to the free end of a single-disc aeronoid capsule so that it transmits a change in frequency equivait transmits a change in frequency equiva-lent to the change in atmospheric pressure with increasing altitude. Coil Q, 43. Capacitance 870 pf. Housed in a sin. square aluminium can on a lightweight 21/2 in. diameter plug-in unit. New, unused, 25/- post paid.

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200-250 volt 50 c/s. post paid

250-0-250 at 70mA. 6.3v. at 2A. 4v.

at 2A. 2, 300-0-300 at 70mA. 6.3v. at 2.5A. 5v.

3. 350-0-350 at 120 mA, 6,3v. at 3.5A. 5v. at 2A. 4. 350-0-350 at 300mA. 6.3v. at 8A. 5v. at 2A. plus 4v. at 2A. and 6.3v. at 2A. 5. Filament only: 6.3v. at 4A.

27/6

10/-

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## WALKIE-TALKIES Type 46

This is a later type than those previously available. A really serious job of sound design, crystal controlled, 10 mile range, transmitter and receiver covering any one frequency between 4125 and 7100 kcs in 25 kcs steps with standard crystal supplied—or any spot frequency between 3600 and 9000 kcs with special crystal supplied to order. Brand new, complete with headphones, throat mic., whip-antenna, plugs and leads. lb. £3/10/0 carriage paid

Size: 12 x 4 x 6‡in. Weight 8‡lb.

Price, with standard crystal

with chosen spot frequency

£7/15/0 carriage paid Crystal Carriage paid

Batteries required: 150, 15, and 3 volts. Transistorised converter to operate from 6v. or 12v. D.C.

ETCH - YOUR - OWN PRINTED CIRCUIT SETS 21 - Free

Each contains over 60 sq. in. of laminated board and sufficient chemicals to make dozens of printed circuits, plus comprehensive instruction book giving advice and examples on translating theoretical circuits into layouts ready for etching High-quality materials—completely safe to handle—carefully prepared to ensure fine definition and uniform results without laboratory control. laboratory control.

## Cathode Cold Trigger

A sub-miniature cold cathode valve developed by Ericsson primarily for computor work, these GTR.120W tubes have great possibilities in a number of experimental electronic automatic control cir-They have an Anode-Cathode cuits. running voltage of 95 to 140 at 4.5 mA. and at 290 anode volts require a trigger current of only 250 microamps to cause

the anode to take over the discharge. Typical ionization time=90 microseconds. They will withstand up to 310 v. with zero trigger voltage without self-igniting.

Supplied complete with full performance data in original packs of 100 at the Special Price of

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## TRANSISTOR AMPLIFIER

Printed circuit, 500 milliwatt push-pull output. High impedance input, 3 ohm output. Two OC71 and two OC72. Supplied with all components, condensers, resistors, volume control, transformers and printed circuit board. Input 6-9 v. D.C. Circuit diagram and component layout supplied with each kit. Size of board 21 x 51 in. 52/6 post paid.



## VENNER TIME SWITCHES

Type T.S.2, first grade precision time switches as supplied to G.P.O. Comprises absolutely silent, self starting, 250 volt 50 c/s synchronous clock mechanism totally enclosed in heavy gauge brass case. Central drive takes detachable dial that revolves to operate sensitive on and off trips for external mains operated circuit. Self contained clock is easily detachable from rear mounting panel (self starting down to 80 v. and keeps running down to 15 v.).

Brand new, in original packings, and with dial and adjustable stops.

37/6

adjustable stops.

post paid.

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Mullard OA.81 Diodes..... 



Release of a small quantity of the latest version of the well known APN-4 Indicator Unit from the American Loran Airborne radio navigation system. This provides a golden opportunity to

system. This provides a golden opportunity to make a serious television servicing and development tool as described in the Wireless World. This is a nice looking piece of equipment with a really business like inside. Steel, double-decked chassis with fully screened 5CP1 tube in the centre, all high-grade capacitors and resistors, separate tag boards and layout diagrams for individual sections, etc. Modern circuit technique centred around one type of valve (14 of 6SN7 double-troides and 8 of 6H6, plus three 6S7 and one 6SJ7), and RCA 100 kes. Crystal. Brand New, with W.W. Circuit £6.10.0

## TRANSMITTER/RECEIVER APN-I

This is the attractive lightweight American Radio Altimeter that superseded the British version. A complete 14-valve radar set covering 420-460 Mc/s ideal for conversion to radio control of models

TRANSMITTER

A push-pull feed-back oscillator tuneable either side of 445 Mc/s, frequency modulated at 100 c/s by a particularly robust moving coil transducer. Two 955 high frequency acorn valves. Case size only 3½ x 6½ x 2in. plus 2 x 2½in. dia. for transducer. RECEIVER

Tuneable to transmitter frequency. Size 3½ x 6½ x 2in. Two 900 acorn valves.

AUDIO AMPLIFIER

Self-contained RC coupled 12SH7, 12SH7 and 12SJ7. Size 3 x 5 x 1½in. Amplifies the received

signal which is passed to detector circuit giving a D.C. voltage proportional to the difference between the transmitted and received (reflected) signal to operate internal relays which pass appropriate correction signals to autopilot and supply external indicator (5 mA meter). MAIN CHASSIS

The main chassis carries the 3 sub-units and has a further three 12SH7, one 12SJ7, two 12H6 and one VR150 regulator, three 1% wire-wound resistors, one 4-pole changeover relay, two SPCO relays, three twin-ganged pre-set potentiometers, trimmers, fuses,

Power supply is derived from a 27-volt dynamotor (charging rate for 24 v. supply) delivery 285 v. at 75 mA. BRAND NEW, less dynamotor, a very useful buy

indeed at only **£2** plus 7/6 carriage.

#### ANTENNA INDICATOR

Remote indication to within 1° Remote indication to within 1° on precision instrument type flush fitting black crackle indicator with 3in. dial calibrated in 2° steps plus the four cardinals. Simple D.C. wiring (6-30 volt) from specially wound potentiometer in sealed diecast housing with 4in. drilled spindle transmits accurate signal of horizontal or vertical bearing. Brand new, post free.

35/\_

## BEAM-ECHO AVANTIC KITS

S.P.A.11 combined stereo control unit and power amplifier complete to the last nut and bolt, with specially prepared assembly instructions, full circuitry and wiring diagrams, plus a full copy of the handbook. ONLY A FEW LEFT. £11 plus 7/6 carriage.



## High Quality Power Pack

50'for only carriage paid.

## INVERTERS

28 Volt DC to 115v I phase AC

Self-contained motor generator unit with complementary carbon pile voltage regulator, contactor and associated rectifier in separate compartment on same base. Continuously rated for 25/28 volts D.C. input with 360 VA output at 115 volts single phase A.C. at 1,600 cycles with a power factor of 1.0. Fan cooled with end plate for blast or internal cooling as required. Type 200. Ref. SUB/5083.

In first class condition. 44.10.0 carriage 7/6

28 Volt DC to 115v 3 phase 400 c/s AC. Type 102A Output 625VA. Complete with suppressor, load compensating circuit and contactors. Brand new. £10 carriage 10/-

200/220 Volt DC to 200/250v I phase 50 c/s AC Output 260 Watts. New, in soundproof cabinet. carriage paid 49.10.0

24 Volt DC to 26v I phase 400 c/s AC

Output 6 VA. Size 2½in. dia. x 4in. long on 1½in. high pedestal base. Instrument quality As new. £1.10.0 carriage paid carriage paid

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This specially made oil-filled casing houses an hydraulic torque conversion unit originally precision made by Westinghouse from high quality materials for the U.S. Government at an acquisition cost exceeding £150 each. Highly suitable for lathe head drive, workshop variable speed power take-off, etc.

Basically the unit is a back-to-back mounted, oil submerged, variable displacement hydraulic pump (input shaft) feeding a reversible hydraulic motor (output shaft) so that variation of the pump dis-

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## ANTENNA INDICATOR

Remote indication to within 1° on precision instrument type flush fitting black crackle indicator with 3in. dial calibrated in 2° steps plus the four cardinals. Simple D.C. wiring (6-30 volt) from specially wound potentiometer in sealed die-cast housing with ½in. drilled spindle transmits accurate signal of horizontal or vertical bearing. Brand New, Post Free, 35/-.

## **B.C. 221 FREQUENCY METER**

125 kc/s to 20 Mc/s WITH CALIBRATION BOOK in first-class working order, £19 10s. carr. 10/-.

## POST FREE SNIPS

Double pole knife changeover switch on porcelain base. 2 for Pyrex Aerial Insulators. Four 3in. OR one 8in. U.S.A./British co-ax. adaptors. Four for Ncons. Ten 115 volt for 12/6; Six 80 volt for G.P.O. electro-mechanical counters. 0-9999
Bulgin Type M microswitches, new 4 for Moral Rectifiers. 7.6 Metal Rectifiers: 4 for 11 Metal Rectifiers: Selenium 6-12 v. 1½A., 6/6; 2¼A., 9/6; 4A., 16/6; 250 v. (twin 125 v. ), 60 mA. 5/6.

## CATHODE RAY TUBE

VCR139. (Cossor 23D Equiv.). 21in. dia. Tube. New in original cartons. 17/6 Post Paid.

200 amp WELDING

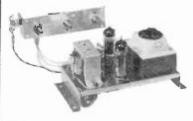
Relatively small but really heavy duty aircraft quality six-pole shunt-wound self-excited generator with six interpoles delivering 30

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tion according to position of changeover links. Are very successfully driven from tractor take-off pulley or the like. 13in. long, 7in. dia. Weight 57 lb. £6.15.0 Carriage paid (U.K. only).

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£5.10.0 plus 5/- Carriage

Separate control panel 6in. ×11in. Volume/On-Off switch, Bass and Treble Boost controls and Pilot light. Amplifier Chassis 3in. × 8in. × 4in. 2xECL82 in Push-Pull. Output transformer matched 3 and 15 ohms. 110-220-240V. A.C. with 6ft, mains lead.

All units guaranteed ready for installation

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LONDON'S GREATEST DEALERS IN RADIO AND ELECTRONIC EQUIPMENT



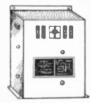
AMERICAN HIGH VOLTAGE CAPACI-TORS. 2 mfd. 10,000 volts wkg., £8/10/-. Carr. 7/6. 1 mfd. 20,000 volts wkg., £7/10/-Carr. 7/6. 0.25 mfd. 25,000 volts wkg., £6/10/-. 5-upplied brand new in maker's cartons at a Displied brand new in maker's cartons at a fraction of original price. 16 mfd. 400 v. wkg., 8/6. 10 mfd. 16 mfd. 660 v. wkg. A.C., 15/-10 mfd. 1,500 v. wkg., 15/-. 10 mfd. 600 v. wkg. 10/6. 8 mfd. 1,500 v. wkg., 12/6. 10 mfd. 300 v. wkg. A.C., 7/6. Please add 2/- postage on all capacitors.

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SPECIAL OFFER A.M. CAPACITORS. Tubular metal case size. Dia. 3½in., length 9in. 30 mfd. 400 v. wkg., 26 mfd. 500 v. wkg , 20 mfd. 500 v. wkg , 15/- each. P.P. 2/6.

WESTINGHOUSE HEAVY DUTY L.T. SIJPPLY UNITS TYPE 115. A.C. input 200–250 volts. D.C.

TYPE 115. A.C., 200–250 volts. D.C. 26 amps. into a 24 volt (nominal) battery. Rating continuous. Max. ambient temp. 35 deg. C. Completely smoothed and stabilised. Built in metal case approx. size 17 x 21 x 19 inches. With fitted fuses. On/



Off switch. Reconditioned as new. £32/10/- ex warehouse. Original maker's price over £100. ADMIRALTY HEAVY DUTY A.C. 230 v. 40 AMP. CONTACTORS D.P. Supplied Brand new in maker's cartons, 59/6, carr. 4/-. ADMIRALTY VOLTAGE REGULATORS. 1.000(2 0.59-0.16 amps. Rotary switch type 32 stud contacts. Brand new, 17/6, carr. 4/-. EQUIPMENT WIRE, P.V.C. 14(0076, 100 yard drums, 6/6. P.P. 1/6. Henley Rubber Covered Braided with cotton, 40(0076, 50 yd. drums, 7/6. P.P. 2/-. 110(0076 50 yd. drums, 7/6. P.P. 2/6. 162/0076 50 yd. drums, 10/6.

20 S.W.G. 100 yard coils 6/6. P.P. 1/6. Various colours. Transparent 14/36, 100 yard coils 7/6. P.P. 1/6.

TWIN 20 S.W.G. 100 yard coils 13/6. P.P.



Weight 2.1 oz. Motor dimensions 1\(\frac{1}{2}\)in. long, 1\(\frac{1}{2}\)in. dia. 5pindle 0.4in. long, 0.77in. dia. Consumption 0.72 watts off load. 7.68 watts on load. 5peed 7,000 r.p.m. 5witch. Centre off reverse by switching either side. General specification. These motors have a tremendous power-weight ratio, are extremely efficient. Can be used on 6 volts without great loss in power. Precision built in polythene housing. Self lubricating. With sintered bronze bearings. Easily mounted. Supplied brand new and guaranteed, 15/6. P.P. 1/6. Special price for quantities over 50. quantities over 50.



No. I. Pri. 240 v. 5ec, tapped 4, 6, 11 v. 200 (9/15/-, Carr. 7/6. £9/15/-Pri. 240 v. 5ec. 20 v. 30 amps., £6/15/-. Carr. 5/-Pri. 240 v. 5ec. 20 v. 20 amps., £4/5/-.

No. 3. P Carr. 5/-Carr. No. 4. Pr -r 7/6. Pri. 240 v. 5ec. 24 v. 30 amps., £8/10/-.

No. 3. - Fri. 240 v. Sec. 24 v. 30 amps., 169/10/2-Carr 7/6. No. 5. Pri. 200-240 v. Sec. 8.4 v. C.T. 10 amps., 27/6. Carr. 3/6. No. 6. Pri. 240 v. Sec. tapped 12 v.-18 v. 10 amps., 52/6. Carr. 4/-. No. 7. Pri. 240 v. Sec. tapped 6 v.-12 v. 20 amps., 69/6. Carr. 4/-. No. 8. Pri. 200-240 v. Sec. tapped 10 v.-17 v.-18 v. 10 amps., 57/6. Carr. 4/-. No. 9. Pri. 200-240 v. Sec. tapped 30 v.-32 v.-34 v.-36 v., 5 amps., 57/6. Carr. 4/-. No. 10. Pri. 240 v. Sec. 6 v.-12 v. 10 amps., 47/6. Carr. 4/-. No. 11. Pri. 230 v. Sec. 24 v. 7 amps. and 32-30 v. 2 amps., 52/6. Carr. 4/-. No. 11. Pri. 230 v. Sec. 24 v. 7 amps. and 32-30 v. 2 amps., 52/6. Carr. 4/-. No. 12. Pri. 200-240 v. Sec. tapped 48-56-60 v.,

No. 12. Pri. 200-240 v. 5ec. tapped. 48-56-60 v., t amp., 27/6. P.P. 3/6. No. 13. Pri. 200-240 v. 5ec. 12-20-24 v. 2 amps., 22/6. P.P. 3/6.

No. 14. Pri. 230 v. 6.3 v. 5 amps. and 6.3 v. 1 amp. and 65 v. 85 M.A., 15/-, P.P. 3/6. No. 15. Pri. 200-240 v. 5ec. tapped 3, 5, 12, 20, 30 v. 2 amps., 25/-, P.P. 3/6.

No. 16. Pri. 200-240 v. Sec. tapped 9-15 v. 4 amps., 22/6. P.P. 3/6.

No. 17, Pri. 230 v. 5ec. 6 v. 5 amp. 12/6, P.P. 2/6.

No. 18. Pri. 220-240 v. 5ec. four separate windings,  $3 \times 5$  v. CT 4 amp., 4 v. 4 amps, Potted type, 32/6. Carr. 4/-. No. 19. Pri. 200-240 v. Sec. tapped 3-60-66-70 v. 1.2 amps., 35/-. Carr. 4/-.

No. 20. Pri. 200-250 v. 5ec. 26 v., very conservatively rated at 36 amps., £9/10/-. Carr. 10/-.

SPECIAL OFFER: LATEST A.M. RE-LEASE. Isolation Transformers. Pri. tapped 100, 200, 220, 240 v. 5ec. 225 v. I.1 Amps. Tropically rated. Guaranteed £3/5/- Carr.

EXCLUSIVE PURCHASE OF A.M. HEAVY DUTY TRANSFORMERS. HEAVY DUTY TRANSFORMERS.

Tapped to give the following specifications:
Pri. 440-400 v. 5.P. 5ec. 220 v. or 110 v. 600 watts.

Pri. 220 v. 5ec. 220 v. or 110 v. 600 watts. Pri. 220 v. 5ec. 55 v. 10 amps. All winding. Double wound £5/19/6. Carr. 7/6.

OFFER. SPECIAL OFFER. BRAND NEW
PARMEKO SEALED TRANSFORMERS.
Pri. tapped 200-220-240 v. Sec. 4 volt C.T.
36 amps. Tropically rated. 25 kV. D.C.
insulation. Size 9 x 8 x 8 inches plus 4 inch
terminals. Offered at a fraction of maker's 69/10/-. Packing and carriage 15/-.

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o amps., runnel cooled, 59/6. Carr. 4/-.
No. 5. Max. A.C. input 18 v. D.C. output 15 amps., 45/-. Carr. 3/6.
No. 6. Max. A.C. input 36 v. D.C. output 36 amps., £8/10/-. Carr 4/-.
No. 7. Max. A.C. input 75 v. D.C. output 1.5 amps., 18/6. P.P. 1/6.

No. 8. Max. A.C. input 32 v. D.C. output 2 amps., 15/-. P.P. 2/-. No. 9. Max. A.C. input 40 v. D.C. output 0.75 amps., 10/6. P.P. 1/6.



 $0.4\Omega$  25 amp. geared drive,  $17/6,~P.P.~3/-.3\Omega$  10 amp. slider control,  $15/-.~P.P.~3/-.~1\Omega$  12 amp. slider control,  $10/6,~P.P.~2/6,~1.5\Omega$  15 amp slider control,  $12/6,~P.P.~2/6,~1.90\Omega$  0.1 amp. enclosed slider control,  $17/6,~P.P.~2/6,~70\Omega$  6-0.5 amp. enclosed slider control, equipment,  $15/-.~P.P.~3/6,~12,000\Omega$  3 mA. Double tube geared control, 35/-. P.P. 3/6.

HEAVY DUTY ADJUSTABLE RESISTORS.  $2\Omega$  6 amp., 7/6.  $1\Omega$  12 amp., 6/6. P.P. 2/-.

BERCO RHEOSTATS.  $3\frac{1}{2}$ in. dia.  $25\Omega$ , 200 watts, 15/-. P.P. 2/6.  $2\frac{1}{2}$ in. dia. 2001 50 watts, 8/6. P.P. 2/-. Ohmite  $1\frac{1}{2}$ in. dia.  $350\Omega$  25 watts, 5/6.  $25\Omega$  0.75 amp., 5/6.  $10\Omega$  1 amp., 6/6.



Manufactured by Crompton Parkinson MI 50 cycles, supplied new and guaranteed, 32/6. P.P. 3/6.

CROMPTON PARKINSON 41 in. A.C. MI AMMETERS. 0-30 amps, flush mounting, 27/6, P.P. 3/6.

FERRANTI A.C. VOLTMETERS. 0-300 v. 6 inch dial. Flush mounting. Supplied Brand New at a fraction of maker's price. £4/15/-. 5/- Carr.

A.M. LT SMOOTHING CHOKES. Resistance & ohm. Ideal for smoothing 12-24 v. D.C. 5 amps. Tropically rated, \$7/6. Carr. 4/-.

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COLVERN W.W. PRECISION POTENTIOMETER. 2\frac{1}{2}\text{in.} \text{dia.}, 3 \text{gang}, 2,000 + 5,000 + 5,000 \text{ohms.} 3 \text{gang} \text{200} + 500 + 500 \text{ohms.} 3 \text{gang} \text{200} + 500 + 500 \text{ohms.} 22/6. P.P. 2/6. 2 \text{gang} \text{40} \text{ k} \text{ohms.} \text{17/6}.

AMERICAN COMPRESSORS. 3 stage type. 32-R-500 24 volt D.C. C.F.M. 0.4 P.S.I. I,500. Supply brand new. Three only £45.

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PANTON ATTENUATORS, 3.000  $\Omega$  in 41 stud contact steps, 15/-. P.P. 1/6.  $500\Omega$  in 15 steps, 10/6. P.P. 1/6.

NON-KINKABLE TWIN CABLE. 23/0076 rubber covered braided with cotton. 25 yard coils 12/6. P.P. 1/6.

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DOUBLE READING, MOVING COIL. 0-3 v. and 0-30 v. D.C. Centre zero. Offered at a fraction of maker's price, 12/6. P.P. 2/-.

250-0-250 MICROAMMETERS. Latest design 2½in. square, flush. By Ernest Turner. Brand new and guaranteed, 42/6. P.P. 2/6.

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DECADE RESISTOR BOX  $100\Omega$ - $111,000\Omega$ , zero resistance  $0.006\Omega$ , accuracy 1%. Max. current  $10^\circ$ s decade 100 mA.  $100^\circ$ s decade 30 mA.  $1,000^\circ$ s decade 10 mA. Mounting. Metal case and panel size: H. 3in., W. 8in., D.  $3\frac{1}{2}\text{in.}$  Supplied brand new and guaranteed, £13/13/-. Further information on the above instruments will be sent on application.

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HIGH GRADE SLEEVING. 6 mm. 100 yd. coils, 10/6. P.P. 2/6. 2 mm. 1 gross yds., 5/-. P.P. 2/-. 2.S mm. 1 gross yds., 6/-. P.P. 2/-. Mixed bundle of sleeving over yard lengths, 1-4 mm., 5/-. P.P. 2/-.

AIRCRAFT 12-24 V. D.C. ACTUATORS. Size 8  $\times$  1½in. Plunger movement 1½in., 35/-. P.P. 2/6.

ADMIRALTY 24 VOLTS 3 A.H. ACCU-MULATORS. Suitable for low wattage lighting etc. Twelve 2 v. cells. crate and linked. Supplied new with charging instructions, 25/-. Carr. 5/-. Single cells supplied separately, 2/6. P.P. 1/6.

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A.C. 200-240 v. 20 amp, switch contacts, make and break once every 24 hours. Complete with mounting bracket, and earth strip. Supplied brand new at a fraction of maker's price, 69/6. P.P. 2/6.

VENNER 14 DAY CLOCKWORK TIME SWITCHES. 5 AMP. SWITCH CONTACTS. One make one break every 24 hours. Complete with two pin Mounting bracket and key, 32/6. P.P. 2/-.

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OIL FILLED H.D. L.T. TRANSFORMERS. P.R.I. 380/420 v. Single phase. 50 C.Y. Sec. 19 volt 3 kvA. £15 ex warehouse.

AMERICAN LEACH 2-POLE CONTACTORS. Res. 235 ohms.  $2\times2\times2$  inches. 7/6. P.P. 1/6. Just arrived G.P.O. 3000 type relays, twin coil, I 000 + 1,000 ohms. I CO 6 M 1 M before B. 12/6. P.P. 1/6.

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D.C. input, 230 v. A.C. output 230 v. 8.7 amps.
Complete with starter switch and fuse box.
Reconditioned as new £45. Ex-warehouse.

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HEAVY DUTY A.M. H.T. TRANS-FORMER. Tapped Pri. 200-250 v. Sec. 163 v. 2kVA. Double wound, one only. Brand new., £15. Ex warehouse.

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AMERICAN TYPE.  $235\Omega$  2 C.O., 7/6.  $400\Omega$  2 C.O. sealed, 10/6.  $10,000\Omega$  1 C.O., IM., sealed, 10/6. 1/- P.P. on all relays.

AMERICAN LEACH CONTACTORS. 110 v. A.C. 3 pole, 20 amp. 230 v. Contacts size 4½ x4 x 3in. Brand new in maker's cartons, 25/-. P.P. 3/6. A.M. Contactors, 12 v. D.C. 2 H.D.C.O., 1 C.O., 1 B. Brand new, 10/6. P.P. 2/-.

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FERRANTI L.F. CHOKE, 8 henries, 75 mA., 200 mA., 6/6. P.P. 2/6.

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24 v. 11 a.h. Size 8 x 8 x 8 inches. 62/6. Carriage 10/-.

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Five 1.2 v. cells crated and connected to give 6, v. Brand new and fully guaranteed. Size of crate  $15\frac{1}{2}$  in. × 12 in. ×  $6\frac{1}{2}$  in. £7/10/-. Carr. 15/-.



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Good output on 21 inch speaker.

OC44/OC45/OC45/OC72 Ist grade transistors.

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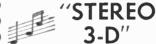
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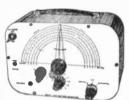
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"C" CORE TRANSFORMERS. Pri, 230 v. 50 c.p.s, 510-0-510 at 275 mA. 375-0-375 at 83 mA. 6.3 v. at 9 A. 6.3 v. at 2A. (twice), 6.3 v. at 1A. (twice), 6.3 v. at 1.5A. 6.3 v. at 0.5A, 5 v. at 3A. 6½ x 6 x 7½ in. high. Weight 25 lb. Removed from equipment but in perfect condition. 32/6. Carr. 5/6.

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CO-AXIAL RELAYS. Simultaneously switch two separate inputs to alternative outputs. 24 volt D.C. coils (can be hand operated). 5ize (approx.) 5 x 3 x 3in., operated). 6/6 post 2/-.



#### TRIPLETT **METER** MOVEMENT

This article consists of a basic 400 microamp meter movement mounted on a Bakelite panel 5½ x 2½. The dial is scaled as a 15 range Testmeter. A circuit and parts list of the original instrument is supplied.

BRAND NEW. Boxed. 35/-, post paid.

#### RECEIVERS AR-88D

A recent release enables us to offer thise superlative receivers at most advantageous prices. In addition to those which have been completely overhauled, re-aligned and recalibrated to our usual high standards, there will be some available to personal shoppers who may have their own facilities for overhaul. Prices will be very reasonable. Customers contemplating mail order purchase can obtain full details on request. (5.A.E. please.)

## **RCA AR-88 SPEAKERS**

A high quality 3 ohm unit fitted into heavy gauge black crackled steel cabinet, size 10½ x 11½ x 6in. Fitted with rubber feet and 6ft, lead. Ideal for extension speaker. CR 100, etc. In original cartons. BRAND NEW, 45/-. Post 3/6.

## R 1475 RECEIVERS

Also known as receiver Type 88 these exceedingly versatile ex R.A.F. It valve receivers cover 2-20 Mc/s in four bands. Many unusual features such as 600 Kc/s. Xtal reference oscillator. Xtal controlled BFO, voltage stabiliser and variable selectivity are incorporated. The dial is exceptionally large and readable and sensitivity is of the order of I microvolt. In very good condition, complete with power unit (A.C. and 12 v.) and in working order. £12/10/-, carr. 10/-.

#### CANADIAN RECEIVER No. 52

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1.75-16 Mc/s (19-170 m.) in three wavebands R.F., Mixer.
5ep. Osc. 2 I.F.'s, Det/A.V.C., Ist Audio, Output. BFO
(10 valves), plus a 3-valve dual Crystal Calibrator. Controls:
R.F. Gain, L.F. Gain, Crash Limiter, C.W. Filter, Variable
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Man. or A.V.C. BFO pitch control. Internal 3in. speaker and
valve check meter. Power supply required 160 v. H.T., 12 v.
L.T. Data and Circuit supplied. A really excellent receiver,
£8/19/6, carr. 15/6. Power supply Unit, 59/6, carr. 5/6.

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A first-class 10-valve Communications receiver, covering 75 Kc/s. to 18 Mc/s. (16.2-4,000 m.) in 5 bands. The large scale and superior dual ratio slow-motion drive make tuning easy and the R.F. stage and 2 I.F. stages ensure world-wide reception. All the receivers we sell have been thoroughly overhauled, completely realigned and are in first-class working order. ONLY £9/19/6.

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IDEAL POR CROWN CONTROL, FACTORIES, FETES, ETC. CON-SISTS OF 4 SPEAKER UNITS AND CONTROL UNIT. COMPLETE WITH MICROPHONE, HEADPHONE AND SPARES. OPERATES PROM 12 VOLTS D.C. (OR 6 VOLTS A.C. WITH SLIGHTLY REDUCED OUTPUT; CONSUMING ONLY 3 AMPS. OUTPUT POWER 8 WATTS, ALL TESTED AND WORKING, BUT SLIGHTLY SOLLED. A GENUINE BARGAIN. 24 19/6, CARRIAGE 25/8.

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Contains 100 § and 1 watt resistors, 50 Hi Stab resistors, wire wound resistors, carbon and W/W pots, 100 capacitors (mica, paper, Sprague, bina, variable, etc.), variebolders, tag strips, metal rectifiers, sleeving etc. All components are unused. GUARANTEED VALUE, 25 - plus etc. All 2 6 post.

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PVI-35 32/6, 2D21 7/6, OC3 6/-, PTI5 12/6, CV51 (Y65) 5/-, 6F33 5/-, 2050 W. 7/6, 5126 £10, 5670 5/-, FW4/500 7/6. BRAND NEW in individual cartons. Bulk enquiries invited.

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This crystal controlled heterodyne frequency meter is too well known to need further description. Those we offer are complete with correct individual calibration books and are carefully tested and guaranteed. Condition is very good.

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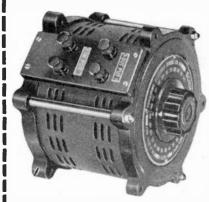
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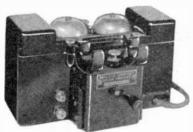
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RESISTORS. All preferred values. 20% 10 ohms to 10 meg., ½ w., 4d.; i w., 4d.; 1 w., 8d.; 1 w., 8d.; 2 w., 1/s. HIGH STABLIATY. j w., 1% ½/s. Preferred values 10 ohms to 10 meg. Ditto 5% 9d., 1000 to 5 meg. 5 watt WIRE-WOUND RESISTORS 3.10 watt 25 ohms—10,000 ohms.

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Cascode circuit using Valve ECC84. 17db
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Ready mounted on befile 12/n. × 7in., 3in. dece.
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I.F. 33/38 megs, complete with frame-grid valves. 30Cl and 30L15. (LT 16v. 3a.) With colls for channels 1 to 13. Includes F.M. Brand new, price 45/-, operating data and circuit supplied. Ideal for "P.T." Olympic.

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Midget size: Long spindle. Guarantee-l l year. All values.

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Semi air spaced, in, dia. Ideal Band III Losses cut 50% 6d. yd. FRINGE QUALITY AIRSPACED ...

COAXIAL PLUGS .. 1/- LEAD SOCKETS .. 2.
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BALANCED TWIN FEEDER per yd. 6d., 800 or 300 \( \Omega\$)
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ALUMINIUM CHASSIS, 18 s.w.g. Plain, undrilled, with 4 sides, riveled corners and lattice fixing holes with 2 $\mu$  in sides  $7 \times 10^{-3}$  m. 4 $(8^{\circ} \times 77 \text{m. 5}/9^{\circ} \times 11 \times 77 \text{m. 6}/9^{\circ} \times 12 \times 11 \times 11 \text{m. 10}/6^{\circ}$ ; 13×14 $\mu$ 1 m. 12/6 and 18×16×3 $\mu$ 1, 16/6.

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TAPE TRANSCRIPTOR 3 motors, 3 speeds: 12, 32, 71 i.p.s., take 7in. spool. Push-button conin. spool. Push-PRICE £12/12/-. trols. PRICE & Carr. & ins. 5/6. Tape extra.

#### **COLLARO Mk. IV TAPE** TRANSCRIPTOR

Four heads. Twin track operation. Pause control. Tape measuring and calibration device. Two motors. rause control. Tape measuring and calibration device. Two motors. Fast re-wind. 7in. tape spool. 3 speeds. 3\frac{3}{2}\text{in.}, 7\frac{1}{2}\text{in.} and 15\text{in.} per sec. Finish cream polystyrene cover plate with maroon control. Delivery from stock, £16/19/6.

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|----------|-------|-------|----------|-------|------|
| quality. |       |       |          |       |      |
| 5in. re  | el, 6 | 00ft. |          |       | 12/9 |

CLAROSTAT WIRE WOUND Potentiometers with single pole switch. Values available: 2.5Kohm, 25Kohm, 50Kohm, 100Kohm, 2/6 ea.

# 

max. primary current each half, 80 ma., 14 single-ended ratios, 11 push-pull. PRICE 23/-.

POTENTIOMETERS. Less switch POTENTIOMETERS. Less switch 500Kohms, 100Kohms, 100Kohms, 1-0 each. 5ingle pole switch, 5K, 10K, 25K, 50K, 10K, 25K, 25K, 256K, 2/6 each. Clarostat type 58, 3 watt wirewound, 50 ohms, 100 ohms, 250 ohms, 500 ohms, 1,000 ohms, 500 ohms, 1,000 ohms, 5,000 ohms, 7/6 each. HENLEY SOLON SOLDERING IRONS. 65 watt, with oval bit, 29/- each; 65 watt, with pencil bit, 30/8 each; 25 watt, instrument model, 24/- each.
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|                   | Stella 5T101            | 1/3   |  |  |  |  |
| SMD4              | Philips 290U and Stella |       |  |  |  |  |
|                   | 5T100                   | 1/3   |  |  |  |  |
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|                   | and DACII. Ekco U76,    |       |  |  |  |  |
| 0145              | U109                    | 5/3   |  |  |  |  |
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5T105U

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10 watt push-pull ultra linear Hi-Fi amplifier with pre-amp. control unit. Amplifier Valves EF86, ECC83, 2-EL84, EZ81. Sensitivity 40M/V for 10 watts, output impedance, 4, 8 and 16 ohms, spare supply for tuner, 200/250V, A.C. Pre-Amp. valve EF86. INPUTS Radio 100M/V, tape 100M/V, GRAM LP 50M/V, 78 60M/V, MIC 10M/V, output socket for recording direct to tape recorder Treble between —10D8 and +12D8 at 10KC/S. BASS between —10D8 and +12D8 at 20K/S. Finished in grey, green, stone enamel, controlognel Finished in grey, green, stone enamel, controlpanel in gold lettering, fully guaranteed. Original price 20 gns. OUR PRICE £14/19/6. P. & P. 7/6.

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IOin. wide, 20in. high, 7in. deep, with 8 x 5in. Hi-Flux speakers complete, price £13/19/6. Carr. and packing 7/6.

\( \times \) DECCA PORTABLE AMPLIFIER. As \( \times \) supplied in famous DECCAMATIC III. \( \times \) Complete with small cream knobs. Full \( \times \) range tone and volume controls. Employs \( \times \) range tone and volume controls. Employs \( \times \) reclast valve, Metal Rectifier. Size 3 x 3\( \times \) x 8\( \times \) in. Only 59/6 plus 2/6 P. & P.

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★ ECL82 valve, Metal Rectmer.

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# THE **NEW JASON** range for CONSTRUCTORS

JTV2 Tuner completely assembled ready for use £25/7/-.

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FMTI FM Tuner. In kit form for cabinet mounting. One of the most popular tuners. Up to 60 miles normal range. Including valves £6/15/-. Power pack kit £2/14/9.
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Consisting of:

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8in. × 2½in. Elliptical Speaker

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The SUPER 60

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MAY BE E9.15.0 Plus 4/6 P. & P. & P. & P.

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\$\frac{\text{Six}}{\text{six}}\$ lat grade Mullard Transistors and one Olode.
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\$\frac{\text{Si0}}{\text{mw}}\$ mW Push-pull Output.

\$\frac{\text{Poll medium and long waveband overage.}}{\text{Calibrated}}\$ Oirect Drive Dial Drive Assembly.

Assembly.

The Receiver is housed in an attractive contemporary mabogany finished cabinet trinimed with git, supported by gilt stands.

The Receiver will operate for months on one 9-volt long-life battery.

Instruction Book separately at 2/8 p.p.

28 Gns. 19 Gns.

SP21.

\*\*\*\*\*TAKE ADVANTAGE OF THESE\*\*\*\*\*

DRAMATIC PRICE

REDUCTIONS AVANTIC SPAII Stereophonic Amplifier.

Technical details: power output (each channel) 10 watts peak, L.S. impedance, 4, 8 and 16 ohms. 6-position input selector, bass, treble, volume on/off controls, stereo reverse switch, phase reverse switch, stereo balance control, P.U. balance control Dimensions 14½ x 8½ x 4in. Original price 28 Gns. P. & P. 7/6. OUR PRICE

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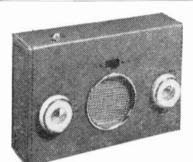
AVANTIC STEPII. Stereophonic Magnetic Pick-up Amplifier Unit. Price £4/4/-.

SP21. 0 inputs for each channel, class, treble, volume control, on/off stereo/3D/reverse stereo switch, stereo phase switch, low pass filter. Power requirements 6.3 v. at 1.3 A., A.C. 350 v. at 5 mA. D.C. dimensions 14½ x 9 x 4in. Original price £28/10/-.

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6 inputs for each channel, bas



## 6-TRANSISTOR POCKET SUPERHET

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PP3 Battery extra at 2/6.

This Receiver uses the most up-to-date printed circuit method and construction is simplicity itself with the aid of the point-to-point instructions supplied, using 6 Transistors and one Diode and internal Ferrite Rod Aerial, with provision for Car Radio Aerial. Full medium and long waveband coverage and when constructed the Receiver is housed in an attractive leatherette Case size 6½in. × 4½in. × 1½in.



P. & P. 51 on above units.

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- L.T. 1/6 (Type AD 35) or equivalent. High Q frame aerials.
- High sensitivity on both wavebands.
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An extremely reliable and
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switch, 4 speeds and off. Switch, 4 speeds and off. ivory finish with red T/T mat.



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BATTERY ELIMINATOR Housed in two con-Housed in two containers which are to replace AD 35 and B126 Batteries.

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Plus 2/- P. & P. Only suitable for use with DK96 Series

with DK96 Series valves.

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|---------------|----------|------|----|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|----|----|
| 1.200ft, on 8 | 5[in. 8] | looc |    |   |   | ٠ |   |   |   | ٠ |   |   |   |   |   |   |   |   |   | 25 | -  |
| 1.800ft. on 8 |          |      |    |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |    |    |
| 1,200ft. on 7 | 7in. Spc | ю    |    |   |   | ٠ |   |   |   |   |   |   | ٠ |   |   |   |   |   |   | 25 | /- |
| 1,800ft, on 7 |          |      |    |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   | 32 | /6 |
| Plus 17- per  | Spool 1  | P. & | Ρ, |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |   |    |    |
|               |          |      |    | _ | - | _ | _ | _ | _ | _ | _ | _ | _ | _ | _ | _ | _ | _ | _ |    | _  |

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The Kapura Model UI Multi-(complete with Test Leads). P. & P. 2 6.

A truly efficient Meter for the enthusiast: sensitivity 1,000 ohms per volt A.C. and D.C. ranges (AC/DC) 0-10-30-250-500-1/,000 v. D.C. current 0-100-500 mlm. 0-1 mlm, at D.C. 0-10 v.). Resistance 1:2,000 ohms (centre 24 ohms), 100-200 K. (centre 2,400 ohms.). Size 5in. x 3 in. x 2 in. Brand new in manufacturers' original boxes.





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A new circuit for the home constructor requiring a good quality medium-powered Amplifier for reproduction of Records or F.M. Broadcasts. Technical Specifications: separate bass and treble controls. Valve line-up EF86. EL84, EZ80. Voltage adjustment for A.C. mains from 200–250 volt. 3 or 15 ohms impedance. Negative feedback. Size  $7 \times 5 \times 2$ in, overall height 5 in, finished Chassis. Silver-hammered

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| Garrard 301               | £22 17 | 3 | Garrard 4HF (Stereo) Garrard 4HF (GCS) | £19 | 4 | 8 |
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£7.19.6

Compact designed 5 valve amplifier. Out-put 3.5 watts.

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Valves: ECL82, and metal rectifier. Tone and volume control panel on flying leads. P. & P. 3/6. P. & P. MK. D3

As above de luxe model, with separate tone controls for treble and bass boost. P. & P.

New circuit employing ECL80 triode pentode output valve giving 3 watts output. A.C. only. Mains isolated. Single control A.C. only. Mains isolated. Single control for volume and on/off switch with knob. Single control P. & P. 3/6.



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R.P.4. RECORD CABINET As above. Cloth covered in contrasting colours. Grilled front control panel. Size 15×19×8 in. deep.

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Exceptional offer. A lightweight portable player Cabinet in Rust or Cream. Famous manufacturer. Size 14½ × 11½ × 6in. Takes our single player; 2 control Amplifier; 5in. Speaker. Post, Packing and Insurance, 5/6.

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8in. P.M. Speakers fitted into polished cabinets. Standard matching to any receiver. (Complete.) Switch and flex included. P. & P. 3/9.





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60/- DOZ. 602, 6P28, 6V6, 6X5, 10P14, 12AT7, 20P1, ECC81, ECC82, ECC83, ECL80, EF80, PCC84, PCF80, PL81, PL82, PL33, PY80, PY81, UL46.

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| E.M.I. Type QD/051, 30<br>kc/s.·100 mc/s                                                                                                                                                                                                                                                                             | £22                                                             | 10          | 0         |
| ADVANCE Type D1,                                                                                                                                                                                                                                                                                                     | £45                                                             | 0           | 0         |
| R.C.A. Type 710, 370-<br>560 mc/s                                                                                                                                                                                                                                                                                    | £35                                                             | 0           | 0         |
| BOONTON Type 84, 300-1000 mc/s                                                                                                                                                                                                                                                                                       | £220                                                            | 0           | 0         |
| HEWLETT PACKAR Type ML-18738 Range 520-1300 mc/s. Accuracy 11 % Output voltage 11 1/4 Output voltage 12 1/4 to 100mV. Impedance 10 ohms. Reconditioned accuracy 17 me 20 A. G. Andis Oscillator, 20 c/s. 20 kc/s. in three bands. Output, 8 watts into 50, 200, 600, 5000 ohms. Retered input and output. Calibrated | RD<br>E125                                                      | 0           | 0         |
| 5000 ohms. Metered input<br>and output. Calibrated                                                                                                                                                                                                                                                                   |                                                                 |             |           |
| watts into 50, 200, 500, 500, 5000 ohms. Metered input and output. Calibrated attenuator Type 200A, 35 c/s35,000 c/s. 2 watts.                                                                                                                                                                                       | £85<br>£35                                                      | 0           | 0         |

**OSCILLOSCOPES** COSSOR Type 839 ....

DUMONT Type 241 ...

1085 1049 1052

| DUMONT                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |                          |                        |                                       |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------|------------------------|---------------------------------------|
| USM-32 Miniature Oscil-<br>loscope 115v. AC power<br>supply, 2lin2lin. tabe.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                          |                        |                                       |
| supply. 2lin2lin. tube.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |                          |                        |                                       |
| 0.1v. RMS volt/inch. 10<br>cps4 mc/s. ±2db freq.<br>response. 1 megohm, 28                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |                          |                        |                                       |
| response. 1 megohm, 28                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |                          |                        |                                       |
| μμ impedance, 16-200,000<br>μs timebase, 1-10,000 μs<br>marker, Calibrated ver-                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |                          |                        |                                       |
| tical amplifier. Trigger                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                          |                        |                                       |
| 1-2 μs, 45 cps—515 kc/s.<br>RPS. Attenuator, Cathode                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |                          |                        |                                       |
| follower, Detector probes.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | £125                     | 0                      | 0                                     |
| TS34/AP Portable Oscillo-                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                          | •                      |                                       |
| Tube with Magnifier. Time                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                          |                        |                                       |
| acope, 2in. Cathode Ray<br>Tube with Magnifier. Time<br>Base 10.50,000 c/s free<br>running, and 550 and 250                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                          |                        |                                       |
| m/cs. single-stroke sweep,<br>1 mc/s. internal calibrating                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |                          |                        |                                       |
| pulse input .1 to 1 voit for<br>lin. deflection maximum.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                          |                        |                                       |
| 115 A.C. complete with                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |                          |                        |                                       |
| probes FURZEHILL Laboratory                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | £45                      | 0                      | 0                                     |
| Type 1684D/2 3\in. screen.<br>Time base frequency 2 c/s.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                          |                        |                                       |
| to 150 kc/s., extendable to 00.2 c/s. Sensitivity .7                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |                          |                        |                                       |
| mm/mv, rms. modulation                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |                          |                        |                                       |
| available through A.C. coupling. Price                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | £60                      | 0                      | 0                                     |
| METROPOLITAN V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                          |                        |                                       |
| CT52, 2fin. screen. 10 cps.—40 kc/s. time base.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |                          |                        |                                       |
| cps.—40 kc/s. time base,<br>Y amplifier 0—5v/cm.<br>3db. 25 c/s.—150 kc/s.<br>1.8v/cm. 3db. 25 c/s-                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                          |                        |                                       |
| 1.6v/cm. 3db. 25 c/s-                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                          |                        |                                       |
| 1.6v/cm. 3db. 25 c/s-<br>1 mc/s. 0.5µs delay line.<br>AS NEW                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | £65                      | 0                      | 0                                     |
| ELLIOTT Single Pen 0-1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |                          |                        |                                       |
| m/amp. " Pen Recorder."                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |                          |                        |                                       |
| AS NEW.  ELLIOTT Single Pen 0-1 m/amp. "Pen Recorder."                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | £45                      | 0                      | 0                                     |
| MICROWAVE EQU                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | £45                      | -                      | -                                     |
| MICROWAVE EQU<br>S BAND<br>BG1277. Signal Generator                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | IPM                      | EN                     | IT                                    |
| MICROWAVE EQU<br>S BAND<br>BG1277. Signal Generator                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 1PM                      | -                      | 0                                     |
| MICROWAVE EQU<br>S BAND<br>BG1277. Signal Generator<br>2700-3400<br>T814. 3200-3370 mc/s                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250               | EN<br>0                | 0                                     |
| MICROWAVE EQU<br>S BAND<br>BG1277. Signal Generator<br>2700-3400<br>T814. 3200-3370 mc/s                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250               | EN<br>o                | 0                                     |
| MICROWAVE EQU<br>S BAND<br>B01277. 81gnal Generator<br>2700-3400.<br>T814. 3200-3370 mc/s<br>MARCONI 8pectrum An<br>alyser, TF984 2,900-3,150<br>Valves, type 707A, 728A,<br>from, each                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 295<br>250               | EN<br>0                | 0                                     |
| MICROWAVE EQU<br>S BAND<br>B01277. 81gnal Generator<br>2700-3400.<br>T814. 3200-3370 mc/s<br>MARCONI 8pectrum An<br>alyser, TF984 2,900-3,150<br>Valves, type 707A, 728A,<br>from, each                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 295<br>250<br>2100       | 0000                   | 000                                   |
| MICROWAVE EQU<br>S BAND<br>B01277. 81gnal Generator<br>2700-3400.<br>T814. 3200-3370 mc/s<br>MARCONI 8pectrum An<br>alyser, TF984 2,900-3,150<br>Valves, type 707A, 728A,<br>from, each                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 295<br>250<br>2100       | 0000                   | 000                                   |
| MICROWAVE EQU<br>S BAND<br>B01277. 81gnal Generator<br>2700-3400.<br>T814. 3200-3370 mc/s<br>MARCONI 8pectrum An<br>alyser, TF984 2,900-3,150<br>Valves, type 707A, 728A,<br>from, each                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 295<br>250<br>2100       | 0000                   | 000                                   |
| MICROWAVE EQU<br>S BAND<br>B01277. Signal Generator<br>2700-3400<br>T814. 3200-3370 mc/s<br>T814. 3200-3370 mc/s<br>Valves, type 707A, 2900-3,150<br>Valves, type 707A, 2900-3,150<br>Valves, type 707A, 7900-3,150<br>WAYNE KERR<br>8 Band Q Meter. Designed<br>to measure the time con-<br>stant, and therefore the<br>"Q" of any 8 band echo<br>box having a time constant,<br>between 1 and 3 µs. and                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 295<br>250<br>2100       | 0000                   | 000                                   |
| MIGROWAVE EQU S BAND BOLETT. Bignal Generator 2700-3400                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 295<br>250<br>2100<br>25 | 0000                   | 000                                   |
| MIGROWAVE EQU S BAND BOLETT. Bignal Generator 2700-3400. TB14. 3200-3370 mc/s  MARCONI Spectrum An alyser. TF964 2.900-3.150 Valves. type 707A, 726A, from, each  WAYNE KERR 8 Band Q Meter. Designed to measure the time constant, and therefore the "Q" of any 8 band echo box having a time constant between 1 and 3 µs. As NEW condition. Price and details on requee 726 Klystrons. Magne-726 Klystrons.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | 295<br>250<br>2100<br>25 | 0000                   | 000                                   |
| MIGROWAVE EQU S BAND BG1277. Bignal Generator 2700-3400. 370 mc/s MARCONI Spectrum An alyser. TP64 2,900-3,150 Valves. type 707A, 728A, from, each WAYNE KERR 8 Band Q Meter, Designed to measure the time constant, and therefore the "Q" of any 8 band echo box having a time constant between 1 and 3 µs. As NEW condition. Price and details on requered to many waveguide and Microwave components.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250<br>2100<br>25 | 0000                   | 000                                   |
| MIGROWAVE EQU S BAND BOLLETT. Signal Generator 2700-3400                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250<br>2100<br>25 | 0000                   | 000                                   |
| MIGROWAVE EQU S BAND BOLLETT. Signal Generator 2700-3400                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250<br>2100<br>25 | 0000                   | 00000                                 |
| MIGROWAVE EQU S BAND BOLLETT. Signal Generator 2700-3400                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250<br>2100<br>25 | 0000                   | 00000                                 |
| MIGROWAVE EQU S BAND BOLLETT. Signal Generator 2700-3400                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250<br>2100<br>25 | 0000                   | 00000                                 |
| MIGROWAVE EQU S BAND BOLLETT. Signal Generator 2700-3400                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250<br>2100<br>25 | EN<br>0<br>0<br>0      | 0<br>0<br>0<br>0                      |
| MIGROWAVE EQU S BAND BOLLETT. Signal Generator 2700-3400                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250<br>2100<br>25 | EN<br>0<br>0<br>0      | 0<br>0<br>0<br>0                      |
| MIGROWAVE EQU S BAND BOLLETT. Signal Generator 2700-3400                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 295<br>250<br>2100<br>25 | EN<br>0<br>0<br>0      | 0<br>0<br>0<br>0                      |
| MICROWAVE EQU S BAND B01977. 8ignal Generator 2007-3400. T814. 3200-3370 mc/s T814. 3200-3370 mc/s T814. 3200-3370 mc/s T814. 3200-3370 mc/s WAYNE KERR 8 Band Q Meter. Designed to measure the time constant, and therefore the Carlot of the Car | 295<br>250<br>2100<br>25 | EN<br>0<br>0<br>0<br>0 | 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 |

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| YLOR Model 20A.                                                                         | 214               | 0  | 0  | MARCONI CR100 220 C<br>CR150 250 O                                               | 0    |
| OA, Oscilloscope 2 c/s<br>DO c/s. with triggering                                       | £22<br>£50        |    | 0  | EDDYSTONE 640 222 10740 230 0                                                    | 0    |
| 5C, Mutual Conductance                                                                  | £35               | 0  | 0  | HAMMARLUND Super                                                                 | 0    |
| 5A, Valve Tester<br>5B Valve Tester<br>Iodal 77 Universal Meter.                        | £9<br>£25         |    | ŏ  | Pro £30 ()                                                                       | 0    |
| 0,000 opv                                                                               |                   |    | 0  | HALLICRAFTERS 8X28                                                               | 0    |
| 00 kc/s240 mc/s<br>AA, TV Waveform and                                                  | £27               | 0  | 0  | New 887, 30 mc/s140                                                              | 0    |
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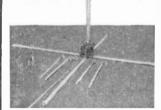
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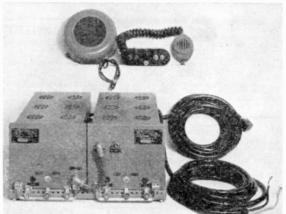
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| ERICSSON SEA              | LED. Hi    | chly se | nsitive. 700  | 00Ω 1 C.O  | . 24 v.  | 25/-  |
| Com                       | prehensive | range   | available fro | om stock.  |          |       |
|                           |            |         |               |            |          |       |



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Counting to 9999.

2-6 v. D.C., 15/- each, post 1/6. 75-230 v. D.C., 15/- each, post 1/6. HIGH SPEED TYPE No. 100c., 35/-, post 1/6.

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300\_000 available from stock now!
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| METERS             | GU      | ARANTEE          | D     |
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| F.8.D.             | 8ize    | Type             | Price |
| 100 Microamp       | 3lin.   | MC/FR            | 80/-  |
| 50 Microamp        | 2lin.   | MC/FR            | 70/-  |
| 250 Microamp       | 21 in.  | MC/PR            | 40/-  |
| 500 Microamp       | 2}in.   | MC/FR            | 37/6  |
| 1 Milliamp         | 2∏in.   | MC/FR            | 35/-  |
| 2 Milliamp         | 2§in.   | MC/FR            | 25/-  |
| 30 Milliamp        | 2∯in.   | MC/FR            | 15/-  |
| 100 Milliamp       | 2∦in.   | MC/FR            | 15/-  |
| 200 Milliamp       | 2∦in.   | MC/FR            | 15/-  |
| 1 Ampere           | 2 € in. | MC/FR            | 35/-  |
| 3 Ampere           | 2∦in.   | MC/FR            | 35/-  |
| 5 Ampere           | 2∦in.   | MC/FR            | 35/-  |
| 10 Ampere          | 2∮in    | MC/FR            | 35/-  |
| 20 Volts           | 2∦in.   | MC/FR            | 35/-  |
| 30 Volts           | 2∦in.   | MC/FR            | 35/-  |
| 40 Volts           | 2∦in    | MC/FR            | 35/-  |
| 500 Microamp       | 2ın.    | MC/FR            | 25/-  |
| 1 Milliamp         | 2ın.    | MC/FR            | 27/6  |
| 5 Milliamp         | 2in.    | MC/FR            | 27/6  |
| 10 Milliamp        | 2ın.    | MC/FR            | 27/6  |
| 20 Volts           | 2in.    | MC/FR            | 27/6  |
| 30 Volts           | 2ın.    | MC/FR            | 27/6  |
| 40 Volts           | 2in     | MC/FR            | 27/6  |
| 15 Amps            | 2in.    | MC/FR            | 12/6  |
| 3 Amps             | 2ın.    | MC/FS            | 27/6  |
| 5 Amps             | 2in.    | MC/FS            | 27/6  |
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| EDECHENCY MET      | FERS    | 45-55 cycles per | cecor |





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300 Volts A.C. 24 in. MI/FR 25/FREQUENCY METERS. 45.55 cycles per second 230 volts, 6 in. dia. Flush Round. Brand new in maker's box, £10/10/-, post 3/6. METER REGTIFIERS 250 µA 1 M.A., 5 M.A., F.W. bridge, \$/6\$, post 6d. AMMETER. 0-3 amp D.C., by Turner, MC/FR, 6in. 90/-, post 2/6. MIGROAMMETER. 250 F.S.D. 3 in. F.R. Sangamo Mod. S37. Scaled for valve voltmeter. Circuit available free, 55/-, post 1/6. UNI-PIVOT @ALVANOMETER, by Cambridge Instruments, 50-0-50 microamps, dia. 4 in. Knife pointer, mirror scale. Complete with leather carrying case. Ideal for laboratory use, £10, carriage 3/-.
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any distance. Two handsets are supplied as illustrated and the set is complete with Pushes, Buzzers, Battery, Plugs and Sockets. We can supply 4-core PVC cable at 10d. per yard or 2-core at 3d. per yard extra. Price 75/- set, post 3/6. TELEPHONE SET TYPE "K." The most compact telephone set available as the 4½ in. flat battery and buzzer is built-in to the hand instrument. Ringing and speaking both ways on twin wire, instrument is complete with 5ft. flex. Easily hangs on the wall. Set of two instruments, \$8/10/-, post 3/6.

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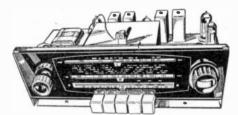
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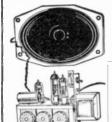
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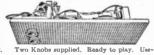
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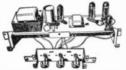
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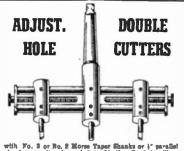
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£1,130 0 0-£1,367 10 0 per annum.

Applications giving details of experience and qualifications to:-Recruitment Manager, B.O.A.C., London Airport, Hounslow, Middlesex

#### **ELECTRONIC** INSTRUMENTATION

Small Electronics Consultant team, with wide knowledge of the applications field and with original ideas can now undertake an extra commission. Please reply Box 3668.

#### MOSCOW TRADE FAIR

Two Electronic Engineers/Technical Consultants visiting above Fair and with considerable knowledge, contacts and experience of Eastern Europe, are willing in return for sharing remaining expenses to represent firms interested in export. Box 3669.

#### RADIO TECHNICIANS IN **CIVIL AVIATION**

Men aged 19 or over for interesting work providing and maintaining aeronautical telecommunications and electronic navigational aids at aerodromes and radio stations in tronal ards at serodromes and radio scattors in the U.K. Fundamental knowledge of radio or radar with some practical experience essential; training provided on special types of equip-ment. Salary according to age and station, approx. £670 at age 25 rising to £795. Prospects approx. 6670 at age 25 rising to £795. Prospects of permanent pensionable posts. Good opportunities for those who obtain O.N.C. in Elec. Eng. or certain C. and G. Certificates for promotion to posts with maximum salaries of £7950, £1,085, £1,335. Apply to the Ministry of Aviation (Est. 5(a)/RT), Berkeley Square House, London, W.I., or to any Employment Exchange (quoting Order No. Westminster 3552).

#### PHILIPS ELECTRICAL LTD.

45 Nightingale Lane, 8.W.12

ENGINEERS

required for the service and installation of X-Ray equipment. Candidates with O.N.C. (electrical) or electronics experience would be considered. Also applicants with electronics experience as trainees.

Applications with full details should be addressed to the Personnel Officer, at the above address quoting reference SE2/61.

#### **ENGINEERS FOR RESEARCH & DEVELOPMENT** IN GOVERNMENT SERVICE

Following are examples of vacancies at SCIENTIFIC OFFICER (2738-61,329) or SRNIOE SCIENTIFIC OFFICER (21342-51,634) tevel now available—
FOST OFFICER RESEARCH STATION, Dollis Hill, London—research into DIRECTIONAL ARRIAL SYSTEMS suitable for long distance communications (scientific officer).

HATIONAL PHYSICAL LABORATORY, Tedding-to, Middlessy-muchanical suitables for long distance.

HATIONAL PRYENCAL LABORATORY, Teddington, Middleser-tenchanical engineer to lead a small team on HOVERGRAFT research. Practical research experience and knowledge of serodynamics and hydrodynamics required (sentior scientific officer).

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essential (senior scientific officer). ROYAL RADAR ESTABLISHMENT, Malvern, ROYAL RADAR ESTABLISHEEF, Malvern, Worcz---light electrical engineer for research in AIR TRAFFIC DATA HANDLING THOM: NIQUES involving data extraction, digital electronic computation and data transmission (scientific officer or senior scientific officer). There are many other vacancies for RESEARCH and DEVELOPMENT ENGINEERS and most acleatific disriplines. All posts carry a pension. Good promotion prospects. Full particulars from Civil Estrico Commission (Scientific Ernsch), 17 North Audier Street, London, W.1.

#### PHILIPS ELECTRICAL LIMITED 45 Nightingale Lane, Balham, 5.W.12

TEST ROOM ENGINEER

required for X-ray and Electro Medical apparatus. Applicants must be capable of carrying out final test and inspection. A minimum qualification of O.N.O. (electrical) is desirable or applicants with pravious experience would be considered. Write giving full details to the Fersonnel Officer at the above address quoting reference 22/61.

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HARPENDEN, HERTS

#### LABORATORY TECHNICIAN

required by Chemistry Department for maintenance and construction of nucleonic and other physical laboratory equipment and routine assay of radio-isotopes by conventional counting methods. H.N.C. or equivalent appropriate qualification. Pay on scale £786 by 7 increments to £1,082. Superannuation. Apply in writing to the Secretary.

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Aircraft Instrument Fitters and Ground and Air Radio/Radar **Fitters** 

Applications are invited from suitably qualified tradesmen for vacancies at a Flying Unit in North Wales, Canteen and Hostel facilities available.

Apply:

The Aerodrome, Llanbedr, Merioneth, N. Wales.



have vacancies for young men and women who wish to pursue an interesting and rewarding career in the field of

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The Company's activities are many and varied and the present vacancies are concerned with the preparation of publications associated with the "BLOODHOUND" Guided Weapon and the "ARGUS" Electronic Computer.

Applications are invited from men and women who either have experience of technical authorship or who wish to enter this field and possess:—

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Successful applicants will be offered a salary fully commensurate with qualifications and/or experience, and with the benefit of a Staff Pension Scheme and a Dependants Insurance Scheme.

The Publications Group is housed in a modern building, pleasantly situated on the Cheshire boundary with easy access to town and rural areas.

Forms of application can be obtained from:-

MEN: T. J. Lunt, Staff Manager, Ferranti Limited, Hollinwood, Lancs.

Please quote reference PC.

WOMEN: Women's Personnel
Officer,
Ferranti Limited,
Wythenshawe,
Manchester, 22.

# ENGLISH ELECTRIC VALVE COMPANY

# Microwave Research and Development

The Company has considerable effort engaged on research and development into very low noise microwave tubes.

Physicists and engineers are/required to assist in this programme and whilst we would prefer graduates with experience in this field of activity we would be pleased to hear from graduates with good honours degrees backed up with industrial experience in light electrical or electronic companies.

Employment would be at the Company's Works in Chelmsford, Essex.

Enquiries should be addressed to:-

Group Personnel Services, English Electric House, Strand, London, W.C.2. quoting reference WW 1506K.



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To: RADIOSTRUCTOR (Dept. G106) Reading, Berks, Please send Brochure without obligation to

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# ADMIRALTY REQUIRES EXPERIENCED MECHANICAL, ELECTRICAL AND **ELECTRONIC ENGINEERS**

Experienced Senior Production Engineers and Production Engineers required in various Admiralty Establishments, mainly in Bath, Portsmouth, Sheffield and Beith, (Ayrshire) Areas. Duties cover variously Marine, Mechanical and Electrical Electronic equipment including Guided Missiles and Radar. In particular, two Senior Production Engineers are required at Sheffield and one at Beith. At Sheffield, one post is in charge of the design of gauges, including electronic equipment for measuring and testing armament stores; the other post is in charge of manufacture of gauges and general factory production, including plant maintenance, etc. The post at Beith is to organise and advise staff engaged in testing and assembly of Guided Missiles, resolving technical problems, and designing special test equipment.

Qualifications. Candidates must be of British birth and have served a recognised apprenticeship or had equivalent training and possess University Degree, A.M.I. Mech. E., A.M.I.E.E. or exempting qualifications. Opportunities occur to gain establishment.

Salary (National Rates) Senior Production Engineers £1,456 to £1,950. Production Engineers £936 to £1,429.

Applications. Apply stating age, training, experience and qualifications to the Secretary of the Admiralty: C.E.II(88) Empire Hotel, Bath, quoting PE 6119.

# TRANSFORMER DESIGN ENGINEER

A further opening for a young man to design transformers for the Electronic and Allied Industries. Some previous experience essential.

The position offers excellent prospects in a firmly established expanding Company.

Write or phone:

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Telephone: Reading 81634.

#### **ELECTRONIC ENGINEER**

A Senior electronic engineer is required for the development of airborne electronic equipment (not communications).

Sound technical qualifications and experience in the use of solid state devices are essential.

This is a key post with very good prospects of advancement in an expanding organisation, for which a salary in excess of £1,600 per annum is envisaged.

Please reply, giving full details to Box No. 3603.

#### REMÔTE SUPERVISORY CONTROL

Serck Controls is an expanding organ-isation developing advanced systems of digital electronic equipment which are rapidly finding acceptance in the oil, gas, water and electricity industries both at home and abroad. Further staff are required to assist in the development of exciting projects.

**DEVELOPMENT ENGINEERS** 

These should be in the age group 23-35 with a degree or H.N.C. preferably with a knowledge of logical techniques using solid state devices.

#### CONTRACTS ENGINEERS

CONTRACTS ENGINEERS

These should be technically qualified and in the age group 25-35. Familiarity with instrumentation and/or communications and with an appreciation of an electronic approach together with an understanding of systems is essential. A facility for communicating ideas both personally and in writing is necessary. Opportunities for installation and commissioning work overseas may arise from time to time in the future.

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These should be in the age group 20-30 and of O.N.C. (electrical or electronic) standard and should have the potential to become Engineers in the near future.

These appointments will be of interest to those who are resulted.

These appointments will be of interest to those who are prepared to work hard towards the achievement of clearly defined objectives as members of a team. Success will be rewarded both financially and by additional responsibilities. sibility. Applications

ns to:
Serck Controls,
Parkfield House,
Dorridge,
Solihull,
Warwickshire.

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are invited to apply for two interesting appointments to prepare instruction manuals for a wide range of complex radio navigational equipment.

These posts which are permanent, and pensionable will be based at our New Malden research laboratories.

Please write, in confidence, with details of qualifications and experience, to Technical Publications Department, THE DECCA NAVIGATOR COMPANY LIMITED, 247 Burlington Road, New Malden, Surrey.

#### TECHNICIAN

Male, aged 20-40 required by

#### IBM UNITED KINGDOM LIMITED

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for their HARROW DEPOT.
Candidates with O.N.C. or
City and Guilds (Intermediate)
will be trained to maintain
electronic test apparatus employing pulse techniques.
Practical experience of radio
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Applications in writing to:
Mr. H. N. Taylor,
IBM United Kingdom Limited,
Stanley Road,
South Harrow,
quoting ref. GA/WW/300.



#### FIELD

Engineers are required by the Field Services Division of EMI Electronics Ltd. to engage in Trials in the Field of the complex prototype electronic equipments developed by EMI Electronics. Sound practical knowledge of the operation and maintenance of Radar or Communication equipments is necessary. Posts may involve periods away from base and a willingness to live away from home is essential. Starting salaries are based on qualifications and experience and it is Company practice to review salaries annually on the basis of ability and

Candidates should write initially, giving full details of qualifications and experience, and quoting Ref. Pa/8 22, to:-

Personnel Manager, EMIELECTRONICS LTD. HAYES, MIDDLESEX.

#### INTERNATIONAL COMPUTORS & TABULATORS LTD. HOLLERITH & POWERS SAMAS ACCOUNTING MACHINES **ELECTRONIC ENGINEERS**

are required

specialise on Calculators (a) to specialise on Calculators and Computers of all types manufactured by the Company and to be based on Field Engineering Headquarters, Luton, Beds. Successful applicants will be required to travel throughout the United Kingdom and occasionally abroad.

(b) to service Calculators and Computers of all types already installed in Greater London, the Home Counties, and the industrial Midlands.

in Greate Counties, Midlands.

The following training and experience is sought for both types of vacancies.

(i) Experience in the maintenance and

Experience in the maintenance and servicing of Electronic Equipment (Pulse Techniques) either in Industry or H.M. Forces and Radar; in addition the ability to handle bench tools and instruments, with an appreciation of the effect of electrical circuits or complete mechanisms. mechanisms.

mechanisms.

(ii) Qualifications ONC (Electrical) or equivalent Studies in Telecommunications. Applicants with experience on Radar in H.M. Forces will also be welcome.

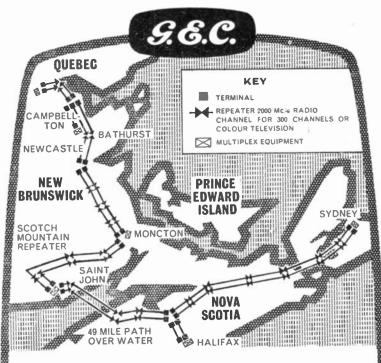
These are Salaried Positions which offer:—

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offer:—
(a) A progressive carreer.
(b) Retirement benefits.
(c) Excellent sick pay scheme.
(d) Holiday entitlement extended to three weeks after five years' service. Applicants who have this training and experience and who are aged 21-35 years are invited to write 1.

are invited to write to: E. J. Reeves, (Principal), Field Engineering Personnel

Section, 5-11 Holborn Bars, London, E.C.1.



The new microwave complex in Eastern Canada—now in service—marks another maior achievement by G.E.C. Consisting of 8 terminal and 18 both-way repeater stations, the link includes a path of 49 miles over water where space diversity reception is in use. The radio system operates in the 2000 Mc/s band and provides a main and standby channel on all routes. In the event of a failure or degradation of the working radio channel, changeover to standby is automatic. The capacity of each radio link is 300 speech circuits, and the standby channel can be used to carry television signals. Radio and multiplexing equipment for this vital link have been built by G.E.C., who have also teen responsible for its installation and commissioning.

Today at G.E.C. we require:

#### LABORATORY **ENGINEERS**

(qualified and preferably experienced)

to carry out development on more advanced transistorised multiplexing equipment using p.c.m. and f.d.m. techniques and radio operating in the U.H.F. and S.H.F. bands

#### LABORATORY ASSISTANTS.

These vacancies should prove attractive to the younger man or girl with a good G.E.C. at "O" level which includes Maths and Physics. Facilities for additional technical training are available.

To help us with the planning and installation of our current equipment which includes the 960-1,800 channel equipment working in the 6,000 Mc/s range. we require:

#### A SYSTEMS PLANNING ENGINEER

with wide experience.

#### COMMISSIONING AND INSTALLATION ENGINEERS

who are free to travel world wide.

If you are interested in any of these vacancies, please apply ta:

The Staff Officer. THE GENERAL ELECTRIC COMPANY LIMITED. Telephone Works, COVENTRY



Interesting vacancies have occurred in the inspection department at the Feltham laboratories of EMI Electronics Ltd., for the following:-

ENGINEER INSPECTORS to join a team carrying out electronic inspection of complex electronic equipment under development, and to conduct liaison with development teams and workshops. A strong engineering background with experience of similar work is necessary. Candidates should have H.N.C. (Electrical Engineering) or equivalent.

TEST ENGINEERS to carry out functional tests and to report on sub-units and complete systems in the radar and communications fields. Service or industrial experience in radar equipment is necessary, and an O.N.C. qualification would be an advantage.

ELECTRICAL INSPECTORS to carry out testing of sub-units to performance specifications. Some previous experience is essential.

Applications for these pensionable staff positions should be made, quoting Ref. Ia/1/X, to:-

> Personnel Manager. EMI ELECTRONICS LTD HAYES, MIDDLESEX

VACANCIES IN GOVERNMENT SERVICE A number of vacancies, offering good career prospects, exist for:—
RADIO OPERATORS MALE MALE CYPHER OPERATORS MALE TELEPRINTER OPERATORS MALE AND TELEPRINTER OPERATORS FEMALE Write, giving details of education, qualifications and experience, to:—

Personnel Officer, G.C.H.Q. (RCO/3)

Foreign Office,

53, Clarence Street, Cheltenham, Gles.

AGENCIES OFFERED
Technical Representatives offer agencies for the following:—
VIBRATING CONDENSERS (most advanced in the world).
Range of AUDIOMETERS and ELECTRO-ACOUSTICAL INSTRUMENTS (range somewhat similar to Bruel and Kjaer).
Other instruments subject to specific Other instruments subject to specific enquiry. Box 3670.

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A Company, well known and expanding in the electronic field, has established a group of engineers to develop Static Power Conversion devices, and requires a Project Leader to control and expand this team.

# electronics

Electronic engineers are invited to apply for this position, which demands ability to inspire and lead, together with technical competence of a very high order in this field.

The appointment carries senior staff status, and a salary of about £1,750 per year is envisaged.

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Principal: E. BAILEY, B.Sc., F.R.I.C., A.M.I.Chem.E.

MARINE RADIO OFFICERS' COURSES

The next Radar Maintenance Course will commence on 24th April, 1961.

The next First Class P.M.G. Conversion Course will commence on 10th April, 1961.

Applications should be sent direct to: The Registrar, Plymouth Technical College, Tavistock Road, Plymouth.

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CANDLER has taught MORSE CODE by correspondence for

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#### WIREMEN

- Due to a recent expansion in our Wiring Department, we have a
- number of vacancies for Components Wiremen for the complete wiring of memory stores •
- and systems. Excellent working conditions, 5-
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- Please apply to The Personnel Officer,
- The Plessey Company Ltd., Wood Burcote Way, Towcester

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# SERVICE ENGINEER

required by Northern electronics instrument manufacturer. Interesting work on all types of electronic testing instruments. Staff Pension Scheme and prospects of promotion. Applicants should state experience, qualifications, age and present salary. Box No. 3979 c/o "Wireless World."

#### DIGITAL COMPUTORS

Resulting from continued expansion in the computer field, a number of vacancies have arisen for Graduate Electronic Engineers and for Technicians of O.N.C. standard. The additional staff are needed for technical supervision and maintenance of Digital Computer Installa-

Vacancies exist in:

London, Birmingham and Sheffield.

Training will be provided for this interesting work and there are opportunities for rapid promotion to positions of responsibility. Salaries are generous and in proportion to ability. Pension Plan

Please write to Personnel Manager

THE NATIONAL CASH REGISTER COMPANY, LTD.,

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## SUPERVISOR

An excellent opportunity for a man aged 25-40 who will be required to lead a small team of wirers and assemblers producing electronic instruments.

Applicants must have undertaken electronic wiring and previous supervisory experience would be an advantage.

Ref. 451/WW.

Please apply to:

B. B. Lynch,
Personnel Officer,
Solartron Laboratory Instruments
Ltd.,
Queens Rd., Thames Ditton, Surrey.



#### MOULDED FIBRE DIVISION

A vacancy exists in this new and expanding Division for an

# **ELECTRONICS ENGINEER**

for development work on the manufacture of loud speaker cones. We are looking for a man interested in sound reproduction who is willing to transfer his interests from straightforward electronics to participate in this highly specialized project.

The work will involve the design and test of cones to specification, weight, resonance and acoustic response. The applicant will also be required to handle enquiries and new orders in this field.

A Higher National Certificate in Electronic Engineering or equivalent is desired, together with ability to work in close liaison with Mechanical Engineers and Paper Technologists.

A generous four figure salary will be paid in accordance with qualifications and experience, and there is an excellent Pension Scheme in being, together with Life Assurance benefits.

 Applications in writing, to Regional Personnel Manager, The Plessey Company Ltd., Kembrey Street, Swindon, Wilts, quoting reference No. MFD/8404/EE.

MATHEMATICIANS, PHYSICISTS, CHEMISTS, ELECTRONICISTS, ELECTRICAL, MECHANICAL and CIVIL ENGINEERS (Men and Women) required for War Dept. RESEARCH and DEVELOPMENT ESTABLISHMENTS at locations including Byfleet and Cherrsey, Surrey, Didcot and Shrivenham, Berks; Christchurch and Farnborough, Hants; Enfield and Feltham, Middlesex; S.E. London; Sevenoaks, Ken; Horsham, Sussex; Southend and Shoeburpress, Essex: as (a) EXPERIMENTAL OFFICER; (b) ASSISTANT EXPERIMENTAL OFFICER; (c) ASSISTANT EXPERIMENTAL OFFICER; (c) ASSISTANT (SCIENTIFIC). QUALS: (a) and (b) G.C.E. "O" level, or S.2/O.N.C. or equiv.: (c) G.C.E. "O" level, or S.2/O.N.C. or equiv. SALARIES: (a) (Min. age 27) £1,087-£1.336. (b) £45-£983. (c) £333—£723. Rates higher in London slightly lower in provinces. Opportunities for part-time further education and to compete for established (pensionable) posts. Forms from Ministry of Labour, Technical and Scientific Register (K), 26, King Street, London, S.W.1, quoting ref. A62/1A.

#### DESIGN/DEVELOPMENT **ENGINEER**

to work on Image Orthicon television project for X-Ray Image Intensification. Should have development experience on television equipment and graduate qualification although the latter is not essential for applicants with very extensive experience.

Apply: Dept. G.P.S., English Electric House, Strand, London, W.C.2, quoting reference WW 2976C.

# MINISTRY OF AVIATION E.I.D.

# **ELECTRONIC** INSPECTORS

required for

Radio, Radar, Components & Electrical Ancillaries at Bromley & Woolwich and eleswhere in London & the Home Counties.

Varied and interesting work with opportunities for gaining valuable experience and further training. Excellent Promotion Prospects.

Pay 266/- to 281/-. (with prospects of further progression to 306/-.) for a 5-day week. Skilled men apply, stating experience, to:-

ELECTRICAL INSPECTION DIRECTORATE (W.W.) AO/L

Aquila, Golf Road, Bromley, Kent

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THE FASTENER WITH ENDLESS APPLICATIONS - SIMPLE - POSITIVE SELF-LOCKING. MADE IN A
VARIETY OF TYPES AND SIZES.
SPECIAL FASTENERS TO SUIT
CUSTOMERS' REQUIREMENTS. WIDELY USED IN THE RADIO INDUSTRY.

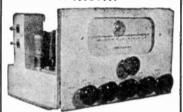
illustrated brochure and other information will gladly be sent on request

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Oddie, Bradbury & Cull Ltd., Southampton

Tel. 55883 Cables: Fasteners, Southampton

## Fidelia



Our present range includes: Fidelia Major AM/FM tuner unit with pre-amp, tone controls, etc. EF stage on all wavebands, variable selectivity. Price £30, or with the Major amplifier, £45.
Fidelia Emperial VHF tuner, Price £15/5/-, or with pre-amp and tone controls, £21.
Fidelia Presiton, switched VHF tuner, £16, or with pre-amplifier and tone controls, £21.
Fidelia Major amplifier, £18.

Full details willingly on request (4½d, for postage is appreciated).

2 AMHURST ROAD ELECTRO TELECOMBE CLIFFS -DEVELOPMENTS SUSSEX.

# 4 TRACK STEREO

and a genuine response from  $30-16,000 \ c/s \pm 3dB$ 

It becomes quickly apparent on listening that the performance characteristics claimed for AUDIOGRAPH recorders are demonstrably true. The re-markable thing is that such standards are achieved on quarter track at 3½ ips. Two stereo instruments (models 9/ S4K and KMS/66) are offered, differing principally in styling and speaker arrangement. Mechanically and electronically they offer similar facilities which permit very high standards of recording together with many elegant refinements. These include paired inputs, paired outputs (each tapped at 5 and 15 ohms plus one low level) stereo balance, etc., etc. Model KMS/ 33 includes a second speaker.

AUDIOGRAPH Recorders are sold by leading stockists. Leaflets on



With second speaker in lid 3½ ips. S/impose; pause, digital counter, etc.

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#### TEST ENGINEER

is required for the Test Department for fault finding and testing electronic instruments to specification.

In Solartron we believe that consideration for the individual is of prime importance. Our amenities and salaries match this philosophy.

Ref. 488/WW.

Please apply to:

Lynch, Personnel Officer, Solartron Laboratory Instruments Ltd., Ditton, Queens Road, Thames Surrey.

#### VACANCIES FOR RESEARCH AND DEVELOPMENT CRAPTSMEN IN GOVERNMENT SERVICE

one or more of the following:-ELECTRICAL (1) Maintenance of radio communica-

- (1) Mantenance of radio communica-tion receivers.
  (3) Sub-assembly lay out, wiring and testing of radio-type chassis.
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MECHANICAL Instrument makers and machinists with bench fit general fitting and

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29 18a. 2d. plus merit pay in the range of 10/- to 100/- per week. Merit pay will be assessed at interview, based on ability and the necessary basic qualifications. BASIC PAY

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Opportunities for eventual permanent and selonable posta. Five-day week; good work conditions; single accommodation available.

Apply in writing to: Personnel Officer, G.C.H.Q. (EDC/3), 53, Clarence Street, Cheltenham, Glo



#### THE AIRPORT, PORTSMOUTH

Are engaged in the development of a wide range of electronic and electro-mechanical projects. We have an immediate requirement for

# QUALIFIED **ENGINEERS**

particularly if they have experience in the design and development of transistorised circuitry.

This is a progressive establishment employing young men with advanced ideas.

Increasing commitments necessitate expansion of staff at all levels and promotion prospects are excellent.

Our senior technical staff will be pleased to have informal discussions, at weekends if desired.

Please write in confidence to the Personnel Officer.

# UNICAM INSTRUMENTS LIMITED

This Company specialises in the production of high quality optical instruments for use in spectrum analysis and has an international reputation as a leader in this field. At all stages of manufacture the best standards of workmanship are needed.

We have vacancies for men with electronic experience for testing. Radar and Radio Technicians with fault finding experience would be suitable.

If you have the kind of background which you think would fit you for this interesting work in a pleasant University City, please let us have full details of your qualifications and experience.

Write to:-The Works Manager, Instruments Limited. Arbury Works, Cambridge, quoting reference E.S.53.



#### IMPERIAL CHEMICAL INDUSTRIES LIMITED

#### A SCIENTIFIC INSTRUMENT MAKER

is required for the Instrument Laboratory of Fibres Division Research Department in which a very wide range of instruments for chemistry and physics is needed. A good all-round man is required, able to work from sketches or even verbal instructions. He should be able to produce a first-class instrument, the workmanship of which can be relied on and of which he can be proud.

This work should be of interest to a toolmaker or watchmaker.

This is a staff appointment and applications should be sent to: Division Staff Officer,

IMPERIAL CHEMICAL INDUSTRIES LIMITED.

Fibres Division, Hookstone Road, Harrogate, Yorkshire, quoting Kef. T.30/A.

#### UNITED KINGDOM ATOMIC ENERGY AUTHORITY

DOUNREAY EXPERIMENTAL



REACTOR ESTABLISHMENT

#### INSTRUMENT MECHANICS

(Physical and Electronic)

#### and INSTRUMENT ELECTRICIANS

There are vacancies in the Instrument Department for men with experience in the maintenance of instruments for the measurement of pressure, flow and temperature, electronic instruments, radar and television and for electricians with experience in the maintenance of temperature recorders and electromagnetic relays.

Applications are invited from men with experience of instruments in industry or with appropriate experience in H.M. Forces.

The rate of pay is £13 7 0d. for a 42 hour five day week and there is a superannuation scheme. Housing will be made available to married men and there is accommodation for single men and married men await-

Facilities are available for further education and promotion prospects are good.

Application forms and further information can be obtained from:

Recruitment Officer, Dounreay E.R.E., Thurso, Caithness, Scotland.

#### CITY OF LEIGESTER EDUCATION COMMITTEE

#### **COLLEGE OF TECHNOLOGY & COMMERCE**

Senior Laboratory Technician required in the School of Physics. It is desirable that applicants should be in possession of a Final City & Guilds Certificate or Higher National Certificate and have a good knowledge of electronics.

Salary on scale £685 to £760 per

Applications in writing should be addressed to the Registar at the College.

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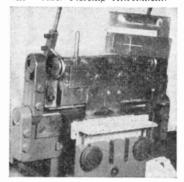
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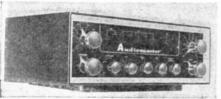
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| .1 MP at 2000V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | 6/-                                                                                 |
| LuF at 3000V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 7/-                                                                                 |
| .2 inF at 2000V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 5/-                                                                                 |
| .21µP at 3000V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | 7/6                                                                                 |
| .2 iuf at 4000V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 10/-                                                                                |
| .54F at 400V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 3/6                                                                                 |
| .5µP at 1000V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | 4/-                                                                                 |
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| LuP at 400V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 3/6                                                                                 |
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| LuF at 800V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | B/-                                                                                 |
| 14F at 1500V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 6/-                                                                                 |
| InF at 2000V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 17/6                                                                                |
| 1µF at 5000V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 25/-                                                                                |
| 2 x LttF at 300V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 5/-                                                                                 |
| 2µF at 600V Bathtub type                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 010                                                                                 |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 22/0                                                                                |
| LuF at 600V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 2/C                                                                                 |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                                                     |
| 1μF at 600V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 3/-                                                                                 |
| 1µF at 600V<br>2µF at 1000V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 3/-<br>6/-                                                                          |
| 1µF at 600V<br>2µF at 1000V<br>2µF at 1500V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 3/-<br>6/-<br>7/6                                                                   |
| λμF at 600V<br>2μF at 1000V<br>2μF at 1500V<br>3μF at 600V tubular.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 3/-<br>6/-<br>7/6<br>3/-                                                            |
| λμF at 600V<br>2μF at 1000V<br>2μF at 1500V<br>3μF at 600V tubular<br>1μF 220V AC                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 3/-<br>6/-<br>7/6<br>3/-<br>4/6                                                     |
| ΔμP at 600V 2μP at 1000V 2μP at 1500V 3μP at 1500V 3μP at 600V tubular 4μP 220V AC 4μP at 900V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | 3/-<br>7/6<br>3/-<br>4/6<br>5/6                                                     |
| ΔμP at 600V 2μP at 1000V 2μP at 1500V 3μP at 1500V 3μP at 600V tubular 4μP 220V AC 4μP at 900V                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | 3/-<br>7/6<br>3/-<br>4/6<br>5/6<br>25/-                                             |
| ### ### ##############################                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 3/-<br>7/6<br>3/-<br>4/6<br>5/6                                                     |
| \$\frac{\pmu}{\pmu} \text{ at 600V} \\ 2\pmu \text{ at 1500V} \\ 3\pmu \text{ at 1500V} \\ 3\pmu \text{ at 1500V} \\ 3\pmu \text{ at 600V tubular} \\ 4\pmu \text{ at 900V} \text{ ac} \\ 4\pmu \text{ at 900V} \\ 4\pmu \text{ at 900V} \\ 4\pmu \text{ at 4000V} \\ 6\pmu \text{ at 4000V} \\ 6\pmu \text{ at 900V} \\ 6\pmu \text{ at 90V} \\ 6\pm \text{ at 90V} | 3/-<br>7/6<br>3/-<br>4/6<br>5/6<br>7/6<br>25/-                                      |
| ### ### ##############################                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 3/-<br>6/-<br>7/8<br>3/-<br>4/6<br>5/6<br>7/6<br>15/-                               |
| \$\frac{\pmu}{\pmu} \text{ at 600V}\$ \$\frac{2\pmu}{\pmu} \text{ at 1500V}\$ \$\frac{2\pmu}{\pmu} \text{ at 1500V}\$ \$\frac{2\pmu}{\pmu} \text{ at 600V}\$ tubular \$\frac{4\pmu}{\pmu} \text{ at 800V}\$ \$\frac{4\pmu}{\pmu} \text{ at 800V}\$ \$\frac{4\pmu}{\pmu} \text{ at 4000V}\$ \$\frac{4\pmu}{\pmu} \text{ at 4000V}\$ \$\frac{6\pmu}{\pmu} \text{ at 3000V}\$ \$\frac{4\pmu}{\pmu} \text{ at 3000V}\$ \$\frac{4\pmu}{\pmu} \text{ at 3000V}\$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 3/-<br>6/-<br>7/6<br>3/-<br>4/6<br>5/6<br>7/6<br>25/-<br>7/6<br>15/-                |
| ### ### ##############################                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 3/-<br>6/-<br>7/8<br>3/-<br>4/6<br>5/6<br>25/-<br>7/6<br>15/-<br>6/6<br>10/-<br>8/- |
| \$\frac{\pmu}{\pmu} \text{ at 600V}\$ \$\frac{\pmu}{\pmu} \text{ at 1500V}\$ \$\frac{\pmu}{\pmu} \text{ at 1500V}\$ \$\frac{\pmu}{\pmu} \text{ at 900V}\$ \$\frac{\pmu}{\pmu} \text{ at 900V}\$ \$\frac{\pmu}{\pmu} \text{ at 900V}\$ \$\frac{\pmu}{\pmu} \text{ at 300V}\$ \$\frac{\pmu}{\pmu} \text{ at 300V}\$ \$\pmu \text{ at 300V}\$ \$\pmu \text{ at 300V}\$ \$\pmu \text{ at 1500V}\$ \$\pmu \text{ at 1500V}\$ \$\pmu \text{ at 1500V}\$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 3/-<br>6/-<br>7/6<br>3/-<br>4/6<br>5/6<br>7/6<br>25/-<br>7/6<br>15/-<br>6/6<br>10/- |

#### AN/AMT-II RADIO SONDE TRANSMITTERS

TRANSMITTERS

Complete transmitter designed to transmit signals in the range of 293-406 mo/a range sortio modulated at 10 to 200 c/a., modulation frequency depending on the magnitude measurest. Measuremente range: pressure 1.040 to 5 millibars; Belative Humidity 15 to 90%; Temperature -90 to +90%. Equipment incideds barometric switch and measuring device, humidity and temperature measuring elements, aerial and pressure calibration chart. Transmitter Circuit consists of Double Triode 3A6 with one half acting as modulating oscillator, the other as a buffer, and UHF Triode 5763.

17 6 Manual .....

#### METEROLOGICAL RADIO SO TRANSMITTERS AN/AMT-48 SONDE

Frequency Range Approx. 1,400 mo/s. Transmitter consists of modulator valve 5875 and EF Valve 5794. Operation from a battery 110V. 6.8V and 1.4V. Dissentions complete with serial: 2\text{in. dax \times in. long.} Weight 7 cas. less batteries. EF Output is pulse modulated with an audio frequency dependent on the value of resistors used in the 5875 circuit.

PRICE, new with circuit diagram (p.p. 3/6) . . . . 16/-

#### PEN RECORDERS

#### STRIP CHART PATTERN SWITCHBOARD MOUNTING.

| PEN RECORDERS:-                                                                                                                                                               |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 1 mA. D.7. F.S.D., Chart Speed Sin./min. 6in. Chart. Electrically driven                                                                                                      |
| mA. D.O. F.S.D., Chart Speed Sin./min. 6in. Chart. Electrically driven                                                                                                        |
| 2.5-0.25 mA, D.C. F.S.D. Chart Speed Sin./min., 6in.<br>Chart Electrically driven                                                                                             |
| RECORDING WATTMETER, three-phase, to record from 0 to 1,000 kW, when used with potential transformer 49400/110V, and current transformer 50/5 amps. Chart speed lin. per hour |
| All Recorders are supplied complete with suitable strip                                                                                                                       |

Other speeds and ranges are also available. Piesse write for full details.

#### LAE-2 HEWLETT PACKARD U.H.F. SIGNAL GENERATORS

Frequency range: 520-1300 me/s. E.F. or pulsed. Output: 1µV to 100mV into 50Q. Pulsed output: rectangular accusion.

Output: 1,47 to 100mV into 500.
Pulsed output: rectangular envelope 100% modulated, internally or externally synchronised. Fulse rate: 80-4,500 e/s; pulse with 2-50,0sec; pulse delay 3 to 300,sec. The instrument is supplied complete with set of calibration and correction charts. Power supplies 1157 &C.
PRICE: fully overhauled and guaranteed £135 0 0

Packing and carriage .....

# "MEASUREMENTS CORPORATION" TYPE 84 "STANDARD" SIGNAL GENERATOR



Range: 300-1,000 Mc/s. Direct Calibration. Accuracy: 0.5%.

Output Level:  $0.1 \mu V \cdot 100$  mV. continuously variable. Internal Modulation:—

Sinewaye—30% Max. at 400, 1,000 and 2,500 c/s. Pulse—1 to 50µsec., width delay variable from 0 to 50µsec. p.r.r. 60 to 100,000 c/s.

Output Impedance—50 ohms. Percentage Modulation Meter.

Packing and carriage....

# CT-82 NOISE GENERATOR AND RECEIVER NOISE FACTOR METER

Portable Mains operated instrument providing noise signal in the frequency range of 100 ko/s. to 160 mo/s and measuring the output of the receiver. 3-step input attenuator. Output impedance 43, 78 and 400 Q. 115/320V operation.

#### "MICOVAC" TYPE CT-54 VALVE VOLTMETER

Portable Battery operated instrument enclosed in a Portable Battery operated instrument enclosed in a watertight case.

Eanger 2.4—4.8—24—48—248—480V AC and DC full scole. Resetance: 0-1000Q with multipliers of 1, 10, 100, 1,000 and 10,000.

Dide probe for high frequency operation.

Dry Battery operation.

PRICE, fully overhauled and guaranteed.. 245 0 0 Packing and carriage \$1.

#### EMI TYPE 3794TA HIGH SPEED OSCILLOSCOPE

Time Base 1.5µaso. to 50 milliano. triggered or free-running. "Y — Amplifier provides sensitivity of 2 to 120 mm. per Volt with a frequency response flat within 2.3db from DC to 5 me/s. Time rise. 67µsec. minimum. Direct calibrated coals for time measurements permitting the measurements to be made down to 1,µsec. "Y" sift volturater in conjunction with range witch will measure voltages from 0 to 500V DC or RMS with a accuracy of 3%. Mounted on a rubber wheel trolley with power supply unit fixed below the main unit. 

#### AIRMEC TYPE 723 OSCILLOSCOPE

Time Base 1,µsec. to .5sec., free running or single sweep with repetition rate up to 30,000 per sec. 4in. Cathode ray Tube. Two-tage "Y "plate amplifier providing sensitivity from 30 to 900 mV/cm with a response from DC to 5 mc/s. Auxilliary amplifier. Automatic brilliano control. Adjustable E.H.T. voltage. 115/239V operation.

#### MAINS TRANSFORMERS

Parmsko ERT Filament Transformers. Input 100/128V. and 200/286V.; output 6.3V. at 3A and 4V. at 1.1A. Test Votte 1200; 4V. at 3A. Test Votte 4550; 4V. at 2A. and 4V. at 3A. Test Votte 2800 27/6

Pewer Transformer. Input 220V; output 310-0-310V. at 120mA. and 5V. at 3 Å.

Power Transformer. Input 100 to 250 V; output 375-9-275V. at 80mA., 6.3V. at .6A. and 6.3V. at 2.5A. 17/6 p.p. 2/6

Gardner or Parmako Power Transformers

Gardner or Parasko Power Transformers, Lupu: 300-250V; output 350-0-350V at 70mA.; 6.3V, at 1A.; 6.3V, CT at 3A. and 6.3V, at 3A. 25/-, p.p. 2/6 Gardner Power Transformers, Luput: 300-350V; 450-0-450V, at 250mA.DC; 6.3V, at 3.5A.; 6.3V, at 8A.; 6.3V, at 10A.; 6.0V, at 6A. The last three outputs have test voltage of 4000V, to earth, 80/-, p.p. 10/-. Gresham Power Transformers

Gresham Power Transformers
Input 110/200/230V.; output 6.3V. at 1A.; 6.3V. at 2.5A.; 480V. at 100mA. DC; 6.3V. at 2A.; 8V. at SA. 30/-, p.p. 4/6

#### STILL AVAILABLE-LIMITED QUAN-TITY ONLY

-chassis from SCR-522 4-channel transmitter-re

Sub-chassis from SCR-582 4-channel transmitter-receivers BC-624 Receiver Unit. Frequency range 190-156 mc/a. Valvea: 2003 RP stage, 9003 Mker. Three 12907 IF stages; 12G3 Det/AVC/Audio; 12 J5GT Second Audio; Coeilliator 9002; Harmonic Generator 9002; Harmonic Amplifider 9003. High and Low Impedarce Output. Amplifider 9003. High and Low Impedarce Output. PRICE, complete with valves, without squech relay, 25f.-, p.p. 5/Ditto without valves 7/6, p.p. 3/6
BC-625 Transmitter Unit. Valves: Speech Amplifier 6630; Fush-Pull Modulator—two 12A6; Oscillator 6630; Ist Harmonic Amplifier 12A6; 2nd Harmonic Amplifier 322; Power Output 322. Output 8 watts. PRICE, complete with valves 22.6, p.p. 5/Ditto without valves 7/6, p.p. 3/6
N.B.—The chassis are supplied complete and m good condition but neither valves nor components are guaranteed. Crystals are not included in price. Every unit is supplied with circuit diagram and description.

D.C. SOLENOIDS

Type 700-28 Peak-Pull Type, 24-28V, 1 Amp. holding force 12 lbe.; stroke 5/16m. Flange Mounting; Dimensions 2 jim. high x sin. x 2in. 6.6, p.p. 2/Type 137 Push-Pull Type: 26V. 12 Amp.; Holding Force approx. 40 lbs.; Stroke jim.; Dimensions 3 jin. high x 32 jim. x 2 jim. x 2 jim. x 3 jim. k 3 jim. k

#### RELAYS

EIGMA TYPE 4CI or ADVANUE TYPE G HIGH SPEED RELAYS. 1B contact. 5000 \( \text{Coll}, \text{Current} \) 4mA. \( \pm \).5mA. will operate with change of current of .2mA. 2mA. Second and of current of 5/6 STEVENS-ARNOLD "MILLISECOND 258" HIGH SPRED EELAYS. Sealed, Octab base, 1 CO contact, 24V. 1400 Q Coll 17/6 SIEMENS TYPE HIGH SPEED RELAYS. 1 CO 500mA. contact. Twin Coll 2X146 Q. Operating current 15mA. with coll in series and 20mA. with coll in parallel Second hand BALANCED ARMATURE MINIATURE STC RE-

 18:—
 11 Contact at 5A, 250 O Coll. Operating current
 40 mA. Release 15 mA. Second hand . 6/6
 2 CO Biturested Contacts at 500mA., 700 O
 COll. Operating current 16 mA; release 5 mA. Second hand
 7/-Second hand T/POST OFFICE BELAYS:—(Second hand)
Type 600, 600 n Coll acro 

#### TYPE 3 POWER UNITS

Mains operated rack mounted fully smoothed restifier power unitproviding adjustable H.T. voltage from 180 to 270 v. at 100 mA. and 6.3 V. A.C. at 4 amps. H.T. voltmeter and milliammeter are provided on the front

# WESTINGHOUSE SELENIUM RECTIFIER POWER UNITS

Input 116/230 V., fully smoothed and fused. Output adjustable from 80 to 140V. D.C. by means of fine and coarse tap switches in the secondary winding. Maximum current 400mA. continuous. Dimensions: 17½ im. x 10½in. deep x 3½in. high . . . . . p.p. 7/6 40/-



#### RATCHET MOTORS 12 v.

1 Amp. (Impulse Motors) . . 5.75 ohms ..... 3/6 each

Packing and postage .....1/6

# SUB-CHASSIS FROM TR-1985 AIRCRAFT CRYSTAL CONTROLLED 10-CHANNEL TRANSMITTER-RECEIVEER

TRANSMITTER-REGE.

Transmitter Chassis Type 81.

Frequency rance 100-125me's. Consists of 4.88mc/s. crystal oscillator (CV-136) coupled to Balanced Modulator (two CV-138) to which a signal at half the final receiver frequency is applied. After mixing the resulting frequency is doubled at CV136, A.F. modhlated at QV04-7 and finally amplifier at TT-15. PBIOE, complete but least values

3/6, p.p. 2/9 leas values

Modulator Chassis. Consists of microphone amplifier CV131, Telephone Amplifier CV-136, and push-pull audio amplifier—two CV-133. Leas valves 5/-, p.p. 2/-

Receiver Chassis type 114.
Frequency range 190-125mc/a. Consists of crystal oscillator tuned to the third harmonic, CV-136, trebier, CV-138 and doubler CV-138. Less valves 5-, p.p. 2/6

#### also available

#### AVO CR BRIDGES

Fortabe mains operated erviceman's component bridge providing the following range: — Capacity: from  $5\mu\nu$ F to  $80\mu$ F. Resistance from  $5\Omega$  to 80 megohms: Valve voltmeter from 0 to 18V RMS. Neon leakage indicator. Fower factor measurements in per centage. Portable mains

per centa.

BICE P. 4 P.

#### BRAND NEW EMISCOPE TV TUBES

Type 3-16; Aluminaed Iolin, dia. screen. 8V Heater. Final Anode 7.000V.. cut-off -34V. B7B Base. Complete with Deflection and Focussing Coils and rubber eacutcheon. 35-. P. P. 10/-.

|                                                                                                                                                     | · · · 0/0, p.p. 2/ •                                                                                                                                                                                                                                                                                                                                                                       | escutcheon,                                                     | 35/ P.P 10/                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
|-----------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| OAS 8/- 5U4G 5/- 7C7<br>OB2 6/- 5V4G 10/- 7E5<br>OB3 6/- 5Y5GT 6/- 7F7<br>OC3 5/6 5Z8 7/- 7Z4<br>OD3 5/6 5Z4 6/- 12A6<br>OZA 5/8 6A6 5/- 12AH       | TESTED and GUARANTEED V                                                                                                                                                                                                                                                                                                                                                                    | ALVES                                                           | _ 5829                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |
| 1A3 3/- 6AC7 3/-<br>1AH4 5/- 6AG5 3/6 12AT7<br>1B24 30/- 6AG7 7/- 12AU                                                                              | $\begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                       | Defl. Price                                                     | 5998 16/- EF22 10/- TT11 8/-<br>5998 15/- EF42 7/6 TT15 40/-<br>6005 9/- EF50 1/6 TT17 50/-<br>6064 10'- EF55 5/- TZ05-20 5/-                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |
| 1B32                                                                                                                                                | 3/- 3JF1 3 6.3 690 2000 90 green E8<br>3/- 3CCP1 5 8.3 578 2000 60 green E8<br>5/- 5FP7 5 6.3 250 7000 45 green/yell. E8<br>5/- 58P7° 5 6.3 430 1500 45 green/yell. E8                                                                                                                                                                                                                     | ES 25/-<br>ES 17/6<br>ES 15/-<br>ES 70/-<br>ES 40/-<br>ES 140/- | Section   Sect |
| 1LA6 6/- 6BB6 6/- 28D7<br>1LD5 6/- 6C4 2/6 32<br>1LN5 5/- 6C5G 7/- 39/44<br>1Q32 100/- 6C6 4/- 53A<br>1B4 6/- 6C8G 7/- 78                           | 78 7 78 7 7 6.3 250 7000 45 green/yell. E8 6/- DG7-5 2\$ 6.3 - 800 - green/white E8 25 6.3 - 800 - green white E8 25 6.3 - 800 - green white E8 25 6.3 - 800 - green white E8 25 6.3 - 800 - green E8                                                                                                                                                                                      | EM 60/-<br>ES 15/-<br>ES 55/-                                   | 9002   5/6   E9U150 89/-   VR31   3/6   VR30   3/6   9004   4/-   EY51   9/-   VR38   3/6   9006   2/6   EZ80   6/-   VR56   4/8   VR56   4/8   VR100   VR100   8/-   ARP3   3/-   FW4/800   VR107   6/-   WR107   WR107   6/-   WR107   W |
| 185                                                                                                                                                 | 10: - STARD SCHEMB FOR SM. TURES, 5/*, p.p. 9d.  9/- 9/- 7/- 7/- 8u/- 80/- 80/- Ref. W mW Mc/a.                                                                                                                                                                                                                                                                                            | D. O9J.  Base Price                                             | ARP4 8/6 8/6 VR10 <sup>2</sup> 3/6<br>ARP44 8/6 KT8 27/6 VR135 2/6<br>ARTH2 7/- KT35C 6/- VR136 4/-<br>ATR37 KT61 17/- VU33 3/-                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |
| 2A3 8/- 6J5 4/6 559<br>9C26A 5/- 6J5G 4/- 708A<br>9C34 4/- 6J6 3/6 705A<br>9C39A 90/- 6K7 4/- 717A<br>9C42 85/- 6L5G 8/- 907                        | 5/-   CV35   4.0 1,250 275   8.0 10 100 3,033 mean     80/-   KRN2A   CV129   4.0 1,650 420 - 10 75 9,375 mean     16/-   KRN3   CV217   4.0 1,350 255 7.4 10 15 9,738 mean     4/-   CV238   6.3 230 - 500 - 450 4,615 mean     6/6   KRN6/3   CV238   4.0 220 185 - 8 100 3,030 mean                                                                                                     | 1.0. £5<br>1.0. £4<br>1.0. £2<br>B7G £9<br>1.0. £5              | 70/- KTZ41 9/- VU39 7/- C3B14 15/- KTZ73 6/- VU111 4/- DAF96 7/6 L63 6/- VU120 4/6 DF93 9/- ML6 6/- X66 10/- DF91 5/- MZ05-20 6/- Z21 10/- DF92 3/6 NGT1 3/6 CV82 80/-                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |
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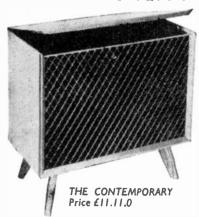
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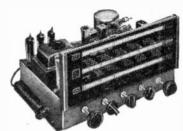
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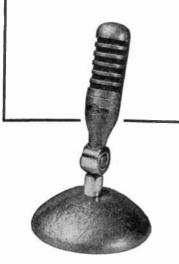
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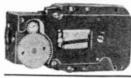
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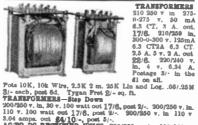
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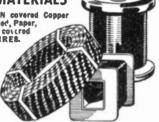
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