# Wireless World 

# RLECTRONICS 

Radio . Television


F(IBTY-NINTH YEAR OF IPUBLICATION

# ONE THOUSAND FEET UP 

## AT MENDLESHAM!

On the 27th October High Power Transmission from the Mendlesham mast commenced. Over one million televiewers will now be able to receive a first-class service from the I.T.A. Station.

A thousand feet high, this mast is the tallest structure in Great Britain, yet it is only 8 ft . 6 in . across each side of its triangular framework.

It was built in ten weeks to the requirements of I.T.A. and their main contractors, E.M.I. Electronics Ltd. The design and erection were undertaken by BIC Construction Company and the steelwork was fabricated and galvanised by Painter Bros. of Hereford-both members of the BICC Group.

Other transmitting masts and towers supplied by BICC include those at:-

CRYSTAL PALACE (London)
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## BICG GROUP

Note: Our artist's impression of the Mendlesham mast shows it flying the Union fack. This in fact was only, flown dwing "Topping Out",-an informal ceremony held by evectors on combletion. of large-scale construcrion jobs.

Tightening one of the steel wire supporting stays.

BLACK MOUNTAIN (Belfast)
KIRK O' SHOTTS (Lanarkshire) DOVER (Kent)
BLACK HILL (Lanarkshire)
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[^1]
# CRAME GBID valves 

 for televisionThe second advertisement in this series described the EF183, which is a variable-mu r.f. pentode, and discussed its use in the i.f. stages of television receivers.
When little or no control is required, a straight r.f. pentode, the EF184, is available. This valve is particularly suitable for use in uncontrolled final i.f. amplifiers, or in television systems using f.m. sound.
The EF184, in common with the other types in the Mullard frame grid range, has about twice the slope of its conventional counterpart. Under comparable conditions, the conventional EF80 has a slope of $7.4 \mathrm{~mA} / \mathrm{V}$, as against $15 \cdot 5 \mathrm{~mA} / \mathrm{V}$ for the EF184. This doubling of the slope provides a substantially improved gain per stage, of the order of 2 or $2 \frac{1}{2}$ times.


Under cathode bias conditions the EF184 shows an advantage in gain of 6 dB over the EF80. If grid current bias is used, the advantage can be increased to 8 dB . It should be noted that it is good practice to include a certain amount of cathode bias for these high slope valves, even when they are working under grid current bias conditions, and when a large value of sliding screen resistor is used. A suitable value for the EF184 under these conditions is about $10 \Omega$. This value is also sufficient for input capacitance compensation with small amounts of a.g.c., or with variations in bias that might be caused by changes in signal level with large signals.
It was said above that the EF184 is suitable for use when little or no control is required. This should be interpreted to mean a control of not more than 2 or 3 times. If a
greater control ratio is required, the variablemu EF183 should be used instead, since the variations of its tail from valve to valve are kept within narrow limits.
Typical anodecurrent and mutual conductance characteristics under cathode bias and grid current bias conditions are shown in the graph.


MULLARD LIMITED
MULLARD HOUSE, TORRINGTON PLACE, LONDÓN, W.C.I

## Writing il Down

THE stimulating and exemplary article on the use of words by P. P. Eckersley in our November 1959 issue and the corollary advanced by R. A. Waldron on page 22 of this issue must serve as pretexts for referring on this occasion to ourselves and to our chosen medium-the written and printed word.

To us it is axiomatic that printing is the best medium for the communication of technical knowledge. It is cheap and it is permanent. No time factor is involved. The reader can skim or study at leisure. There is no obligation to keep up with the pace of the thought processes of an author, as there may be with the spoken thoughts of a lecturer or broadcaster.

The benefits of good writing to the reader are obvious. What may not be quite so apparent, except to those who have tried it, is the value of writing for its own sake, as an exercise, as a discipline and as means of finding out how much (more often how little) one knows about a subject. The act of writing is a clarifying and very often a scarifying experience. Many people fight shy of writing because they think that a special gift or specific training is necessary, that writing is an esoteric craft to be learned by hard and long apprenticeship, for which they cannot spare the time. It may be true that special training is necessary for the writing-up of technical specifications and instructional manuals (as distinct from the writing down of levitating facts and ideas) and we would not deny that there are general precepts of which a conscious knowledge is sometimes advantageous. Certainly the techniques of preparation for press and of printing production are the province of specialists. Many excellent textbooks ${ }^{\star}$ and training courses exist for the guidance of those who wish to take up technical writing as a profession, but for the beginner essaying his first article for submission to a journal the less he knows about these things the better. The recipe for good writing is quite simple and involves only two processes; first, making up one's mind what to say, and then saying it. As in painting and decorating it is the preparation that takes the time. Putting on the paint is the easy part, but it will soon have to be done all over again if the preparation has been less than thorough.

In a technical journal like ours the content of an article is of greater importance than the style in which it is written; matter is more important than manner. But that is not to say that style is unimportant. It may help or hinder the reader in getting to grips with the subject. It is even more significant in revealing the writer's mental make-up and capacity. As Buffon has put it (rather more succinctly), "Le style est l'homme même." And if a turgid and
obscure first draft, full of irrelevant digressions is turned by the author into a simple and direct exposition of a single central theme, the struggle will not have been made without leaving its mark on the man.

In writing there is no substitute for practice, but one should not despair if there seems to be too slow a gain in facility; remember the dictum that "easy writing makes hard reading."

If the matter seems worthy of a wider readership and it is decided to send the article to a journal, it should be typed or legibly written on one side of the paper with space between the lines for printers' instructions (and, who knows, spelling corrections). Time spent by the author on beautifully inked-in diagrams, and lettering on photographs is usually wasted, as most journals like to prepare illustrations themselves. There are many technical reasons why this should be so, and in this journal all we ask is legibility, and, if there is any doubt about size or quality of photographs, the loan of the negatives to make our own enlargements. It is not safe to assume that there will always be time to send proofs to authors for reading. Do not count, therefore, on having an opportunity for second thoughts, but make sure that the manuscript is in a finished state before it is submitted. We will then see that the printer has properly interpreted the author's intentions, and it goes without saying that no major alterations will be made without consultation (pace Mr. Waldron).

There can be no doubt that a well-written article gains wide recognition for its author, not only from his compeers but also from his employers. The Radio Industry Council and the Electronic Engineering Association have acknowledged this by making a number of premium awards annually for technical writing, and on the occasion of the last prize distribution L. T. Hinton, Chairman of the E.E.A., had this to say :
"I can tell you that we look upon [these awards] as of the utmost importance in so far as they encourage technical authors to give of their best.
"These articles are not only helpful to British industry, but the prestige and standing of British research and engineering in the countries of the world can be greatly enhanced by the standard of technical writing. The product we sell is highly technical. we sell it to technical customers and good, authoritative, well presented and well distributed technical writing does more to help our vital exports than all the glossy brochures put together."

[^2]
# THE SMITHE CHRRT 

Survey of Transmission Line Phenomena : Derivation and Uses of the Chart

By R. A. HICKSON*

THE Smith chart ${ }^{1}$ is a transmission-line chart which facilitates the solution of almost all problems arising in the use of coaxial or balanced transmission lines, and some related problems, such as the design of lumped-element matching networks. However, its forbidding appearance, and the severely mathematical tone of most references to it in the literature ${ }^{\text {a. }}{ }^{\text {s. }}$. ${ }^{\text {a }}$ have given it a reputation for difficulty which is not merited. The Smith chart is no more difficult than the slide rule and saves a comparable amount of time and effort in its own field. In addition, its use is of great assistance in understanding transmission-line behaviour at very high frequencies. Transmission-line Phenomena.-If a radio-frequency generator is connected to one end of an infinitely long transmission line the power supplied to the line will travel along it towards the remote end and will gradually be dissipated in the line. There will be no power travelling in the opposite direction. If now the line is cut, a certain load can be connected to the cut end which will simulate the missing portion of the line by absorbing all the power reaching it; the impedance of this load is the same as the characteristic impedance of the line ( $\mathrm{Z}_{\mathrm{o}}$ ). This is for practical purposes equal to a pure resistance of value $\sqrt{\mathrm{L} / \mathrm{C}}$ where L is the inductance and C the capacitance of equal lengths of line. This formula is an approximation which assumes that the loop resistance is negligible in comparison with the inductive loop reactance and that the conductance between the two conductors is negligible in comparison with the capacitive susceptance between them. In other words it assumes good conductors and a good dielectric, and operation at a reasonably high frequency.

Any load other than the characteristic impedance will not absorb all the power travelling from the generator. (The power may be dissipated directly as heat at radio frequency, or rectified and used to operate, e.g., a meter, or radiated, as in the case of an aerial). The power which is not absorbed by the load is reflected by it and travels back along the line towards the generator. It will be assumed for the moment that the generator has the same impedance as the line and so absorbs all the reflected power. A load or generator having the same impedance as the line is said to be matched to the line.
The extent to which a load is matched to a line can be expressed by stating the voltage reflection coefficient or the return loss of the load. The value of the concept of return loss has been discussed recently ${ }^{5}$ and we will mention only the definition at this point. Return loss is the attenuation between the incident power and the reflected power. A

[^3]related concept is reflection loss, which is the attenuation between the incident power and the power absorbed by the load. Formulae for both these losses, which are customarily expressed in decibels, will be derived later.
The voltage reflection coefficient K is the ratio of the reflected wave voltage $\mathrm{E}_{r}$ to the incident wave voltage $\mathrm{E}_{i}$. The best possible match, given by a load of impedance equal to $Z_{o}$ will produce a voltage reflection coefficient of zero. The worst possible match, given by a loss-free load, i.e. an ideal open circuit, an ideal short-circuit, an ideal capacitor or an ideal inductor, will produce a voltage reflection coefficient of unity. The phase of the reflected wave with respect to the incident wave will depend on the nature of the load, and may have any value from $0^{\circ}$ (in-phase) to $\pm 180^{\circ}$ (exactly out-of-phase). As the incident and reflected waves are being propagated along the line in opposite directions the phase angle will vary with the distance from the load. In a distance in which each wave alters in phase by $180^{\circ}$, that is, in a half wavelength, the total change in phase between the two waves will be $360^{\circ}$.

The phase angle of the voltage reflection coefficient will therefore have the same value at halfwavelength intervals along the line. For a frequency of $\mathrm{F} \mathrm{Mc} / \mathrm{s}$, one wavelength in air is approximately equal to $300 / \mathrm{F}$ metres. For other dielectrics the wavelength in air is divided by the square root of the effective permittivity of the dielectric, or multiplied by the velocity factor of the line.

The reflection coefficient may be plotted on a polar chart showing the phase angle as the angle from an arbitrary direction and the magnitude $\mathrm{E}_{r} / \mathrm{E}_{i}$ as distance from the centre. Movement along a transmission line will then correspond to movement round a circle of constant radius on the chart, assuming that line losses are negligible. In cases where the line losses are not negligible the magnitude of the reflection coefficient will decrease as distance from the load increases. If the attenuation between two points is N dB each voltage will change by antilog $\mathrm{N} / 20$, so that their ratio $\mathrm{E}_{r} / \mathrm{E}_{i}$ will change by antilog N/10.
Movement along a line having attenuation will therefore be represented by movement along a spiral on the chart, the radius of the spiral decreasing as distance from the load increases. Fig. 1 shows the change in reflection coefficient entailed in moving along loss-free and lossy lines through a distance of one half-wavelength from a load giving a voltage reflection coefficient of $0.8\left(180^{\circ}\right)$. The loss of 2.5 dB per wavelength is greater than will normally be encountered. For example, a typical cellular polythene feeder in Band III would have a loss of only about 0.25 dB per wavelength. The choice
of the clockwise direction to represent movement away from the load is the accepted convention.
Effect of Type of Load on Reflection Coeffi-cient.-The nature of the voltage reflection coefficient produced by various types of load will now be considered. Considering the current and voltage relationships in the incident wave, the reflected wave and the load, we may write:-

$$
\begin{aligned}
& \mathrm{E}_{i}=\mathrm{Z}_{o} \mathrm{I}_{i} \\
& \mathrm{E}_{r}=-\mathrm{Z}_{0} \mathrm{I}_{r} \\
& \mathrm{E}_{\boldsymbol{l}}=\mathrm{Z}_{l} \mathrm{I}_{l}
\end{aligned}
$$

The minus sign in the second equation expresses


Ag. I. Polar diagram of voltage reflection coefficient. Effect of movement along loss-free and lossy lines.

Fig. 2. Voltage reflection coefficients produced at the load by five specific loods.

the fact that the reflected power is propagated in the reverse direction.
Applying Kirchoff's laws to the junction of line and load:-

$$
\begin{aligned}
& E_{i}+E_{T}=E_{l} \\
& I_{i}+I_{r}=I_{l}
\end{aligned}
$$

Simultaneous solution of these five equations gives:-

$$
\frac{E_{r}}{E_{i}}=\frac{Z_{l}-Z_{o}}{Z_{i}+Z_{o}}
$$

As stated above, $\mathrm{Z}_{o}$ may be considered as a pure resistance, which we may call $\mathrm{R}_{0}$, so that:-

$$
\frac{\mathrm{E}_{r}}{\mathrm{E}_{i}}=\frac{\mathrm{Z}_{l}-\mathrm{R}_{0}}{\mathrm{Z}_{l}+\mathrm{R}_{0}}
$$

Writing K for $\mathrm{E}_{\mathrm{r}} / \mathrm{E}_{i}$

$$
\mathrm{K}=\frac{\mathrm{Z}_{l}-\mathrm{R}_{0}}{\mathrm{Z}_{l}+\mathrm{R}_{0}}
$$

(a) Characteristic impedance $R_{0}$.-By definition, see above, this will produce a voltage reflection coefficient of $0\left(0^{\circ}\right)$.
(b) Short circuit.-As this cannot absorb any power, $\mathrm{E}_{r}=\mathrm{E}_{t}$ and, as no voltage can exist across a short circuit, $\mathrm{E}_{r}$ and $\mathrm{E}_{i}$ must be exactly out of phase. The voltage reflection coefficient is $1\left(180^{\circ}\right)$. Mathematically

$$
K=\left(0-\mathbf{R}_{0}\right) /\left(0+R_{0}\right)=-1 .
$$

This is equivalent to $+1\left(180^{\circ}\right)$ as can be seen by considering that the positive direction along the $0^{\circ}$ line is from the centre of the chart towards the edge,
(c) Open circuit.-As with the short circuit no power is absorbed and $E_{r}=E_{i}$. Since no current can flow across an open circuit the current due to $\mathrm{E}_{i}$ must be exactly out of phase with that due to $\mathrm{E}_{r}$, that is, $\mathrm{I}_{i}=-\mathrm{I}_{r}$.
As $\left(\mathrm{E}_{i} / \mathrm{I}_{i}\right)=\mathrm{Z}_{o}=-\left(\mathrm{E}_{\mathrm{r}} / \mathrm{I}_{r}\right), \mathrm{E}_{i}=\mathrm{E}_{r}$, that is, they are in phase and the voltage reflection coefficient is $1\left(0^{\circ}\right)$.
$\mathrm{K}=\left(\infty+\mathrm{R}_{\rho}\right) /\left(\infty-\mathrm{R}_{o}\right)=1$
(d) Capacitor.-A loss-free capacitor whose reaotance at the operating frequency is numerically equal to the line impedance will be considered-

$$
\mathrm{Z}_{l}=0-j \mathrm{R}_{o}
$$

$$
\begin{aligned}
\mathrm{K} & =\frac{0-j \mathbf{R}_{o}-\mathrm{R}_{o}}{0-j \mathbf{R}_{o}+\mathrm{R}_{o}}=\frac{-j 1-1}{-j 1+1} \\
& =\frac{(-j 1-1)(+j 1+1)}{(-j 1+1)(+j 1+1)} \\
& =\frac{-j^{2}-j 2-1}{-j^{2}+1}=-j 1
\end{aligned}
$$

In polar notation, $\mathrm{K}=1\left(-90^{\circ}\right)$.
(e) Inductor.-For a loss-free inductor whose reastance at the operating frequency is numerically equal to the line impedance, $Z_{l}=0+j \mathbf{R}_{\infty}$ A calculation on the same lines as that for the capacitor, above, shows that $\mathrm{K}=1\left(90^{\circ}\right)$.
We are now ready to derive the Smith chart. Derivation of the Smith Chart.-The five points corresponding to loads of $\mathrm{R}_{o}, 0, \infty, 0+j \mathrm{R}_{o}$ and $0-j \mathrm{R}_{0}$, as determined previously, are indicated in Fig. 2, which shows the voltage reflection coeffcient produced at the load itself; as discussed in connection with Fig. 1, the reflection coefficient will change as we move along the line away from the load. Further calculations on the same basis will show that the reflection coefficients produced by the five possible types of load are as shown in Fig. 3. It will be appreciated that infinite reactance is, like infinite resistance, an open circuit; similarly
zero reactance is, like zero resistance, a short circuit, so that the points $\infty$ and 0 are common to the resistance and reactance axes.

Since in any particular problem the characteristic impedance of the transmission line is a constant,


Fig. 3. Voltoge reflection coefficients produced at the load by the five possible types of lood. Magnitude of the reflection coefficient is shown on an auxiliary scale.

Fig. 4. Voltage reflection coefficients produced at the load by various normalized loads.

it is customary to normalize the load impedance by expressing it as a multiple of the line impedance. Fig. 4 shows the same loads as Fig. 2, now normalized, together with certain intermediate points obtainable by means of similar calculations.


Fig. 5. Voltoge reflection coefficients produced by loads having the same normalized resistive component of load impedance lie on a circle.
Fig. 6. Voltage reflection coefficients produced by loods hoving the same normalized reactive component of load impedance lie on an arc of a circle.


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It is found that all loads having the same normalized resistive component of load impedance $\mathrm{R}_{l} / \mathrm{R}_{o}$ produce reflection coefficients which lie on a circle. A mathematical demonstration of this is given in Appendix I. The centre of the circle lies on the resistance axis and the circle passes through the point of reflection coefficient $1\left(0^{\circ}\right)$. Some of these circles of constant ratio $\mathrm{R}_{l} / \mathrm{R}_{o}$ are shown in Fig. 5.

Similarly it is found that all loads having the same normalized reactive component of load impedance $\pm j \mathrm{X}_{l} / \mathrm{R}_{o}$ produce reflection coefficients which lie on an arc of a circle. Each circle again passes through the point of reflection coefficient $1\left(^{\circ}\right)$ and the centre of each circle lies on the line through this point at right angles to the resistance axis. Some of these arcs of circles of constant ratio



FIg. 8. Auxiliary scoles are provided for rodially-scoled parameters to avoid additional circles on the chart.
$\pm j \mathrm{X}_{l} / \mathrm{R}_{0}$ are shown in Fig. 6. The portions lying outside the circle defined by a reflection coefficient of unity have no physical significance here, as we are considering only passive loads, which cannot reflect a voltage greater than the incident voltage.
The Smith chart, Fig. 7, is a reflection coefficient chart drawn in terms of these circles of constant normalized load resistance and reactance.
The underlying circles of constant magnitude of voltage reflection coefficient and the radial lines of constant phase angle of voltage reflection coefficient are not shown on the chart, to avoid confusion. Instead, a separate auxiliary scale is provided for the magnitude, and a scale of phase angles is provided round the perimeter of the chart.
In addition to the phase-angle scale, scales for "Wavelengths towards Generator" and "Wavelengths towards Load " are normally provided round the outside of the chart. As shown earlier, a complete circle round the centre of the chart represents a distance of one half-wavelength: movement clockwise represents movement towards the generator and vice versa. These scales are customarily shown with their zeros at the point of minimum impedance (phase angle $180^{\circ}$ ). This is, of course, an arbitrary choice, and in practical problems one may wish to start at any phase angle. In one commercially available Smith chart calculator the wavelength scales are movable and the zeros can be set to any phase angle.
Returning now to radially scaled parameters, Fig. 8, these may include, in addition to voltage reflection coefficient:-
(a) Voltage standing-wave ratio.
(b) Return loss.
(c) Reflection loss.
(d) Effect of line attenuation.
(a) Voltage standing-wave ratio.-The v.s.w.r. scale is the same as the resistive component scale along the pure resistance axis. This is demonstrated in the later section "Voltage Variations along a Mismatched Line," where it is also shown that, writing $S$ for v.s.w.r., $S=(1+K) /$ ( $1-\mathrm{K}$ ).
(b) Return loss.-This is the attenuation between the incident wave and the reflected wave, so that it is equal to the square of the reciprocal of the voltage reflection coefficient. It is usually expressed in decibels so that:-
Return loss $=20 \log 1 / \mathrm{K} . \mathrm{dB}$.
(c) Reflection loss.-This is the attenuation between the incident wave and the power absorbed by
the load. As the power absorbed $P_{0}$ is that which is not reflected $P_{r}$ the reflection toss is complementary to the return loss:-

$$
\begin{aligned}
& P_{a}=P_{i}-P_{r} \\
& \frac{P_{a}}{P_{i}}=1-\frac{P_{r}}{P_{i}}=1-\left(\frac{E_{r}}{E_{i}}\right)^{2}=1-K^{2} \\
& \frac{P_{i}}{P_{a}}=\frac{1}{1-K^{2}} \\
& \text { Reflection loss }=10 \log \left(\frac{1}{1-K^{2}}\right) \ldots \mathrm{dB}
\end{aligned}
$$

(d) Effect of Line Attenuation.-This effect on the voltage reflection coefficient was discussed in the first section, where it was shown that if there is an attenuation of N dB between two points the ratio of the voltage reflection coefficients at the two points is antilog N/10. The effect of line attenuation on the v.s.w.r., return loss and reflection loss can be arrived at by use of the radial scales. As with the wavelength scales round the perimeter of the chart, the line attenuation scale may be entered at any point and the graduations, shown here as $1-\mathrm{dB}$ steps, are not normally numbered. This makes interpolation rather difficult at the open end of the scale. However, the difficulty may be eased by use of the "Return Loss" scale. Steps of 2 dB on this scale are mathematically equivalent to steps of 1 dB on the "Effect of Line Attenuation" scale. The two scales are placed side by side to facilitate this use. It should be pointed out that the equivalence is purely mathematical and it is meaningless to say that, for example, a return loss of $4 d B$ corresponds to a line attenuation of 2 dB . The "Return Loss" scale is an absolute one, in the sense that any point on the scale has a definite significance. The "Effect of Line Attenuation" scale is a relative one, and a point on this scale has no significance in itself; only distances along this scale are of interest.
Impedance Variations Along a Mismatched Line.-Comparing Fig. 1 with Fig. 7 it will be seen that the impedance looking towards the load will vary at different points along a mismatched transmission line. The Smith chart shows directly the effect of the length of line on its input impedance.

Taking the example of Fig. 1, in which the load is resistive and less then the characteristic line impedance, the input impedance, moving away from the load, is inductive for the first quarter-wavelength, then, at $\lambda / 4$ from the load, a resistance
greater than the characteristic line impedance, then capacitive for a quarter-wavelength, then, at $\lambda / 2$ from the load, again becomes resistive and less than the line impedance. If it is permissible to neglect line losses, then the line input impedance is the same at half-wavelength intervals. Thus a half-wavelength section of line may be said to repeat the load: the impedance of the line itself does not enter into this result. This is not the case for any shorter length. At quarter-wavelength intervals, for example, the impedances are such that, when multiplied together, the result is equal to the square of the characteristic impedance.

This result is easily verified in the case of resistive impedances; for example, the point $2+j 0$ is on the same voltage reflection coefficient circle as the point $\frac{1}{2}+j 0$. Similarly, an open-circuit at the end of a line will appear as a short circuit a quarterwavelength away from the end, and vice versa. A quarter-wavelength section of line is said to invert the load. In the case of loads which are not purely resistive, the impedance is inverted and the phase angle is changed by $180^{\circ}$, so that a capacitive load is transformed into an inductive load, and vice versa, by a quarter-wavelength section of line. For example a load of impedance $3+j 4$, i.e., $Z_{l}=5$, is transformed into ( $0.12-j 0.16$ ), i.e., $\mathbf{Z}_{\mathbf{t}}=0.2$. This can be seen by starting from the point $3+j 4$ and moving through $180^{\circ}$ round a circle centred on the centre of the chart; as stated in connecrion with Fig. 1, this angle corresponds to a movement along the line of one quarter wavelength. The apparent impedance is $0.12-j 0.16$ after this movement, and the phase angle of the reflection coefficient has changed from $+18^{\circ}$ to - $162^{\circ}$, i.e., from inductive to capacitive.
Voltage Variations Along a Mismatched Line.The instantaneous voltage along the line is varying sinusoidally at the operating frequency, and it is not this voltage, but the peak value which it attains, that is referred to here. Neglecting line losses, the power flowing along a line under steady conditions does not change. As $P=E^{2} / R$, the maximum total voltage $E_{i}+E_{r}$ will occur at points of high impedance. As $\mathrm{E}_{i}$ and $\mathrm{E}_{\mathrm{p}}$ are vector quantities, this implies that they are in phase at these points. Fig. 7 indicates that the phase angle of the reflection coefficient (i.e., the vector difference between $E_{r}$ and $E_{r}$ ) is zero for a load of infinite impedance. Similarly, at points of low impedance the resultant voltage will have a minimum value, and $\mathrm{E}_{i}$ will be exactly out of phase with $\mathrm{E}_{r}$. This is again in agreement with Fig. 7, which indicates a phase angle of $\pm 180^{\circ}$ for a load of zero impedance. The maximum and minimum points do not move along the line with time, and the resultant pattern of peak voltage distribution is referred to as a quasistationary or standing-wave pattern. The ratio between the maximum and minimum peak voltages is called the voltage standing-wave ratio, S .

$$
\begin{aligned}
\mathrm{S} & =\frac{\mathrm{E}_{\max }}{\mathrm{E}_{\text {min }}}=\frac{\mathrm{E}_{i}+\mathrm{E}_{r}}{\mathrm{E}_{i}-\mathrm{E}_{r}} \\
& =\frac{1+\left(\mathrm{E}_{r} / \mathrm{E}_{i}\right)}{1-\left(\mathrm{E}_{r} / \mathrm{E}_{i}\right)}=\frac{1+\mathrm{K}}{1-\mathrm{K}}
\end{aligned}
$$

A number of British workers define v.s.w.r. as ( $\mathrm{E}_{m+n} / \mathrm{E}_{m a a}$ ) but the American practice, followed here, is becoming more common. As the v.s.w.r. is never greater than unity in the one system, and
never less than unity in the other, there is no possibility of confusion.

For loads other than resistive, the v.s.w.r. will bear the same relation to $K$. The only difference in the v.s.w.r. pattern produced by resistive and reactive loads of the same voltage reflection coefficient will be in the positions of the maxima and minima with respect to the load. The whole standing-wave patters will be displaced along the line according to the phase angle of the reflection coefficient at the load.

It is interesting to note that the v.s.w.r, is simply related to the load impedance.

$$
\mathrm{S}=\frac{1+\mathrm{K}}{1-\mathrm{K}} \text { and } \mathrm{K}=\frac{\mathrm{Z}_{l}-\mathrm{R}_{\mathrm{o}}}{\mathrm{Z}_{l}+\mathrm{R}_{o}}
$$

Writing $z$ for $\frac{\mathrm{Z}_{I}}{\mathrm{R}_{0}}, \mathrm{~K}=\frac{z-1}{z+1}$

$$
\mathrm{S}=\frac{1-\left(\frac{z-1}{z+1}\right)}{1+\left(\frac{z-1}{z+1}\right)}=\frac{z+1+z-1}{z+1-z+1}=z
$$

In words, the v.s.w.r. is equal to the normalized load impedance, or to its reciprocal if this is greater than unity.

The importance of the $\nabla . s . w . r$. is that it can be measured with comparatively simple equipment, and from the result useful deductions can be made. It is clear that movement along a line having attenuation will result in a change in v.s.w.r., as it does in voltage reflection coefficient. The change can be evaluated with the aid of the auxiliary line attenuation scale of the Smith chart.

A quantity sometimes encountered in the literature is the so-called power standing-wave ratio. In fact, of course, there are no standing waves of power. The power flowing along a transmission line can only vary gradually, by attenuation, or once-for-all, by reflection, not in the cyclic manner in which the voltage varies when reflection occurs. The term arises when a square-law indicator is used in the measurement of v.s.w.r. The readings obtained are proportional to the square of the voltage and so their ratio represents the power ratio which would correspond to the voltage ratio if both voltages were developed across the same impedance. As they are not, the term is meaningless. Some workers, to avoid the possibility of confusion, convert their standing-wave ratios to decibels. This cure is worse then the disease, as the decibel is a power ratio, and may only be used for voltages when the voltages are developed across identical impedances.
Representation of Admittance of the Smith Chart.-In certain applications, such as the addition of a matching stub in parallel with a load impedance, the use of normalized admittance is convenient. This is because admittances add when placed in parallel. The normalized admittance $y$ is the reciprocal of the normalized impedance $z$.

$$
\begin{aligned}
y & =\frac{1}{z} \\
z & =\frac{1-k}{1+k} \\
y & =\frac{1+k}{1-k} \\
& =\frac{1-(-k)}{1+(-k)}
\end{aligned}
$$

Thus the relation of $y$ to $-k$ is the same as that
of $z$ to $k$. The Smith chart may therefore be used for admittance calculations with the scale for reflection coefficient angle rotated through $180^{\circ}$.
, When it is necessary to change from an admittance to an impedance basis during the course of a calculation, all that is necessary is to rotate the point representing the value through $180^{\circ}$ round a circle of constant K. This operation amounts to finding the reciprocal of a complex number.

Some Smith charts are provided with a circle of unity conductance to facilitate operations. This is the circle of unity resistance rotated bodily through $180^{\circ}$ about the point $(1+j 0)$.
Loads expressed as admittances, conductances or susceptances are normalized by dividing the values by the characteristic admittance of the line, that is, by multiplying the values by the characteristic impedance. For example, a load of $0.02-j 0.01$ mhos on a 75 -ohm line would have a normalized value of $1.5-j 0.75$.

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## APPENDIX I.

Construction of the Smith Chart. -The voltage reflection coefficient is shown in Fig. 1 in polar co-ordinates. However, it may also be expressed in rectangular coordinates, and this will be done here, as it leads to easier mathematics.
The use of $u+j v$ does not imply that the reflection coefficient has resistive and reactive components. It is merely a mathematical device for describing the location


Fig. 9. Use of rectangular co-ordinates for voltage reflection coefficient.


Fig. 10. The Smith chart is geometrically reloted to the Cartesian impedance diagram.
on the chart of the point representing the reflection $\mathbf{c o}-$ efficient. For example, point A in Fig. 9 represents a reflection coefficient of $0.75\left(30^{\circ}\right)$ : using the $u+j v$ notation it would become $0.65+j 0.375$.
Let $\mathrm{K}=u+j v$

$$
\begin{aligned}
\frac{\mathrm{R}_{t}}{\mathrm{Z}_{o}} & =r \\
\frac{\mathrm{X}_{t}}{\mathrm{Z}_{o}} & =x \\
\text { Then } \frac{\mathrm{Z}_{2}}{\mathrm{Z}_{o}} & =r+j x=\frac{1+\mathrm{K}}{1-\mathrm{K}} \\
r+j x & =\frac{1+u+j v}{1-u-j v}
\end{aligned}
$$

Rationalizing

$$
\begin{equation*}
r+i x=\frac{1-u^{2}-v^{2}+i 2 v}{(1-u)^{2}+v^{2}} \tag{1}
\end{equation*}
$$

Equating the real parts of (1)

$$
\begin{gathered}
r=\frac{1-u^{2}-v^{2}}{(1-u)^{2}+v^{2}} \\
r(1-u)^{2}-r v^{2}=1-u^{2}-v^{2} \\
r+r u^{2}-2 r u+u^{2}=1-v^{2}-r v^{2} \\
u^{2}(1+r)-2 r u+r=1-v^{2}(1+r) \\
u^{2}-\frac{2 r u}{1+r}-\frac{r}{1+r}=\frac{1}{1+r}-v^{2}
\end{gathered}
$$

Subtracting $\frac{r}{(1+r)^{2}}$ from both sides

$$
u^{2}-\frac{2 r u}{1+r}-\frac{r^{2}}{(1+r)^{2}}=\frac{1}{(1+r)^{2}}-0^{2}
$$

$$
\begin{equation*}
\left(u-\frac{r}{1+r}\right)^{2}+v^{2}=\frac{1}{(1+r)^{2}} \tag{2}
\end{equation*}
$$

This is the equation of a circle in the $u, v$ plane with centre at the point $\frac{r}{1+r}+j 0$ and with radius $\frac{1}{1+r}$.
Substitution of the value of $r$ in these formulae will give the circle of constant normalized resistance equal to $r$.

Similarly, equating the imaginary parts of (1)

$$
\begin{gathered}
j x=j \frac{2 v}{(1-u)^{2}+v^{2}} \\
x-2 u x+x u^{2}+x v^{2}=2 v \\
u^{2}-2 u+1+v^{2}-\frac{2 v}{x}=0
\end{gathered}
$$

Adding $\frac{1}{x^{2}}$ to both sides

$$
\begin{align*}
& u^{2}-2 u+1+v^{2}-\frac{2 v}{x}+\frac{1}{x^{2}}=\frac{1}{x^{2}} \\
& (u-1)^{2}+\left(v-\frac{1}{x}\right)^{2}=\frac{1}{x^{2}} \quad \cdots \cdots \cdot \tag{3}
\end{align*}
$$

This is the equation of a circle in the $u, v$ plane with centreat the point $\left(1 \pm j \frac{1}{x}\right)$ and with radius $\frac{1}{x}$. Substitution of the value of $x$ in these formulae will give circles of constant normalized reactance equal to $x$. For a given arithmetical value of $x, j x$ may be positive or negative.

Equations (2) and (3) give the basis for the construction of the chart itself. The auxiliary radial scales are constructed on the basis of the equations given earlier.

## APPENDIX II.

Original Derivation of the Smith Chart.-The Smith chart can be obtained from the Cartesian impedance diagram by means of a conformal transformation. This is the method originally used by Smith (1) and is referred to in the standard texts ${ }^{2,3,4}$. However, it is less satisfying from the physical standpoint than the approach presented above. The Cartesian diagram is the normalized form of the Argand diagram of impedance; the negative resistance axis is omitted, as only passive loads are considered. To accommodate an open circuit this diagram would require extension to infinity, and so it is not in common use. Another, related, defect of this diagram is that the voltage reflection coefficient cannot be represented on it in the skeleton form used in the Smith chart, but must be shown in full.

A suitable conformal transformation distorts the straight constant-resistance and constant-reactance axes into circles, but preserves the orthogonality of their intersections. Details are given in references 1,2 and 3. The geometrical equivalent of the transformation is shown in Fig. 10.

The Cartesian chart is inverted about the point ( $-1+j 0$ ), which becomes the infinity point on the Smith chart. Corresponding points in the two charts lie on the same straight line and the distances of the points from ( $-1+j 0$ ) are reciprocally related. Derivation for the Argand diagram is the reason why the Smith chart is often shown with the resistance axis horizontal, although the chart itself is more readily handled with the resistance axis vertical.

# Radio Hobbies Exhibition 

SINGLE-SIDEBAND EQUIPMENT ON SHOW

THIS year, two awards for outstanding design and construction were made. Both took the form of silver plaques; one, as in previous years, being awarded for the most outstanding home-constructed piece of equipment and, an innovation, one for the piece of commercial equipment of the greatest value to the amateur.
W. J. Colclough, G3XC, gained the amateur award with his transistor communications receiver, which uses 14 transistors, covers 1.9 to $29.5 \mathrm{Mc} / \mathrm{s}$ in six bands and operates from an internal 6-V dry battery. The receiver is a double superhet with an r.f. amplifier using OC170 transistors for this stage, the first mixer and the oscillator: the first i.f. is $1 \mathrm{Mc} / \mathrm{s}$ and the second, is $500 \mathrm{kc} / \mathrm{s}$. A" Q-multiplier" operates on the $500 \mathrm{kc} / \mathrm{s}$ i.f. stage and a.g.c. is derived from a two-stage amplifier.

The Minimitter Company won the commercial award with their MR44 communications receiver. This is an 11-valve set-again a double superhet-covering six amateur bands between 1.8 and $30 \mathrm{Mc} / \mathrm{s}$, each band being represented by 8 -in of tuning scale. The MR44 is designed for reception of a.m. R/T, s.s.b. and c.w. signals; for s.s.b. it uses a half-lattice crystal filter and a product detector. This, though, was not the only commercial equipment offering single-sideband facilities but all the apparatus seen used the filter system for generation or demodulation of s.s.b. signals.

The recent relaxation of dollar-import regulations resulted in the appearance of two well-known American names at the show-Collins and Hallicrafters-both with equipment which, in appearance and performance specification, is of the highest quality. James H. Scott, representing Hallicrafters, were showing an extensive range of receivers and transmitters, notable among which was the SX-101A-a 15 -valve double superhet giving
a.m., c.w. or s.s.b. reception on the amateur bands between 160 m and 10 m ; it has a sensitivity of better than $1 \mu \mathrm{~V}$ for a signal-to-noise ratio of 10 dB . On show was the Collins KWM-2 which, in a cabinet $8 \times 15 \times 13$ in, combines a five-band s.s.b./c.w. transmitter of 100 W p.e.p. output and a receiver of sensitivity $0.5 \mu \mathrm{~V}$ (for 10dB-s.n. ratio). The power supply is separate and two versions are available; one is a straight-forward a.c.-mains unit and the other is a low-voltage transistor convertor so that the KWM-2 may be used as a mobile station. Two interesting features of Collins equipment are their s.s.b. filters, and a noise suppression circuit which, in contrast to more common arrangements, uses the slow response of the narrow-band main receiver as an advantage. The noise-blanking unit receives electrical interference on a separate wide-band receiver

## W. J. Colclough's amateur-oword-winning receiver.


( $\pm 0.5 \mathrm{Mc} / \mathrm{s}$ ) operating at about $40 \mathrm{Mc} / \mathrm{s}$ and produces from the noise a pulse which is used to cut off the main receiver. Due to the difference in speed of travel of the noise through the two receivers (slow in the main set, fast in the wide-band receiver) this blanking action can occur before the noise has completed its transit through the main receiver. For s.s.b. generation and detection Collins use a "mechanical filter" which consists of a set of resonant discs coupled together mechanically and excited by a magnetostrictive transducer.

Another s.s.b. transmitter, using an exciter unit based on a design by G2NH, comes from K. W. Electronics. The basic output of the exciter is in the $80-\mathrm{m}$ band and for operation on other bands crystal beat oscillators are switched in by the band switch. Provision is made for normal a.m. and c.w. transmission and the s.s.b. output is 180 W p.e.p. from the class-AB1 push-pull stage.

Printed-circuit panels are used for the exciter and modulator of the Labgear LG50 50-W and "Topbander" $160-\mathrm{m}$, $10-\mathrm{W}$ transmitters. These employ screen-grid modulation and they have a "power control" which varies the power-amplifier screen-grid potentials, allowing the maximum power to be reduced to 7 W and 3 W respectively, whilst preserving a reasonably linear modulation characteristic.

Often the problem of coupling $300-\Omega$ or $80-\Omega$ twin feeder to a coaxial $80-\Omega$ transmitter output, or vice versa is encountered. Whilst it is relatively easy to make up a balance-to-unbalance transformer-with, if necessary an impedance adjustment-for one band, a wide-band device is rather more of a problem. Heathkit, however, now offer a "balun". unit consisting of two bifilar transformers in a screening box. These have one pair of windings connected in parallel to a coaxial socket,


Hallicrafters SX-IOIA receiver.
and the other windings may be joined in series or parallel to give either a $300-\Omega$ or $80-\Omega$ balanced feeder connection. Minimitter were showing an aerial rotator with a beam-direction indicator consisting of a sector of light of included angle equivalent to the beam width shining through a great-circle map centred on London. This is rotated in synchronism with the aerial (not the drive motor) by a selsyn system. Labgear have produced a three-band "quad" design ( 14,21 and $28 \mathrm{Mc} / \mathrm{s}$ ) consisting of three separate "quad" aerials, which are supported concentrically on eight bamboo poles radiating from castings at the ends of the boom. These poles are angled so that correct parasitic-element spacing from the driven elements avoids the need for tuning stubs.

To the R.S.G.B. credit is due for another innovation -a most successful one, too. Entitled "Communications Receivers of the World," this exhibit comprised thirteen "famous name" receivers of British and foreign manufacture. In all except one case, the receivers were working and visitors to the exhibition were invited to put the sets through their paces. This they did, most enthusiastically!

The items in the display of R.S.G.B.-members' work again reached a very high standard, both in ingenuity of approach to electrical design and in the mechanical execution of the design idea. Here mention must be made of J. D. Heyes' (G3BDQ) mains-powered communications receiver, which has one of the most comprehensive specifications any "DX-hound" could want. Using 18 valves, this set provides for s.s.b., a.m. and c.w. reception on the 14,21 and $28 \mathrm{Mc} / \mathrm{s}$ bands in four ranges, the $28-\mathrm{Mc} / \mathrm{s}$ band being split into two parts. Using a grounded-grid buffer first stage followed by a tuned r.f. amplifier, the double-superhet design urilizes a wide-band first i.f. amplifier which is followed by a fixed-frequency second i.f. section at $460 \mathrm{kc} / \mathrm{s}$. The oscillator for the first frequency-changer is crystal controlled: the second is tunable to give band-spread.

Mullard were demonstrating, for classroom use, a simple method of displaying the properties of magnetic materials using an oscilloscope.* Two coils with a large number of turns (about 3,000 ) are used and one coil is fed with $50 \mathrm{c} / \mathrm{s}$ a.c. which provides the horizontal deflection for the c.r.o. The output from the second coil, when a magnetic core is used to couple the pair, represents the rate of change of flux density. Integration of this by an R-C combination provides the vertical-deflection voltage for the oscilloscope, which then displays the hysteresis loop.
A new item of rest equipment from Jason is the W11 "wobbulator." This gives a frequency-modulated output from 0 to $85 \mathrm{Mc} / \mathrm{s}$ on fundamentals, in three ranges (0-2, 0-40 and $35-85 \mathrm{Mc} / \mathrm{s}$ ), using only two double valves and a rectifier. The basic oscillator operates at $150 \mathrm{Mc} / \mathrm{s}$
Wireless World, Vol. 64, p. 433 (September, 1958) (oscil. loscope), and "Demonstrations and Experiments in Electronics No. 9.'' Mullard Educational Service (hysteresis demonstration).


Wireless World, January 1960


G2UK's f.s.k. teleprinter terminal unit.
and is frequency modulated by a back-biased junction diode. The output from this oscillator beats with another oscillator whose frequency is varied by the manual controls, the beat being detected and amplified for use as the generator output. In this way a maximum sweep of about $8 \mathrm{Mc} / \mathrm{s}$ is achieved, but the relation between frequency and back-bias voltage for a semi-conductor-diode-controlled oscillator is not linear. Thus, to provide a linear sweep, the $50 \mathrm{c} / \mathrm{s}$ sweep voltage is fed through a non-linear amplifier, whose non-linearity is the inverse of the bias/frequency characteristic.
Amateur television activity was represented, as usual, by the British Amateur Television Club. Right up to the minute, one of the items on this stand was a working display of slow-scan television equipment, similar in principle to the method used recently by the B.B.C. over the transatlantic cable $\dagger$. Chemical processing of quantities of film was regarded as ruling out this means of storing the pictures, so they were recorded on magnetic tape running at $7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$. Two systems were represented; one, developed by WA2BCW of the U.S.A., uses an amplitude-modulated $2 \mathrm{kc} / \mathrm{s}$ sub-carrier, whilst J. A. Plowman (G3AST) uses a composite a.m./ f.m. system. A recording made by WA2BCW was played back at the exhibition on Plowman's equipment, which uses a VCR517 long-persistence c.r.t. to build up the picture: the line-scan frequency was $20 \mathrm{c} / \mathrm{s}$, resulting in a read-out time of 6 sec for the complete 120 -line picture.
Mobile radio is another facet of the amateur's interests and a recently formed group-the Amateur Radio Mobile Society-caters for enthusiasts. The transistor has done much to ease both the physical and electrical loads on cars-some examples of both British and American transistor power convertors were shown on this stand. One, available as a kit of parts or "ready made" from Transipack, provides an output of 115W high-voltage d.c. at the seemingly incredible efficiency of $95 \%$. This is achieved by the use of a toroidallywound transformer, silicon-junction bridge rectification of the transformer output and a diode circuit which recovers the energy stored in the transformer core.
Teletype is not often thought of as a means of communication between radio amateurs; but it has for some years been gaining ground in the U.S.A. and it has now gained a foothold in the U.K., with the formation of the British Amateur Radio Teletype Group. Due to a purchase of some G.P.O.-surplus machines, several amateurs now have the basic facilities for generating and receiving teleprinter signals. These are used with frequency-shift keying (the normal form for teletype transmission) transmitter exciters in which the shift is usually achieved by "pulling" the v.f.o. by the required amount. Reception is effected by a unit which, fed

[^4]
"Communications Receivers of the World ". Visitors put one of the working receivers through its paces.


Untouched reproduction of 120 -line picture from slowscan television (British Amateur Television Club).
from the receiver, converts the $860 \mathrm{c} / \mathrm{s}$ frequency shift back into $\pm 80 \mathrm{~V}$ signals for the machine. These convertors are usually specialized discriminators, and A. C. Gee's (G2UK) unit, using modified TV width-control coils for the tuned circuits, was on show, together with some "copy" from several contacts with the U.S.A. and Australia, made over radio "circuits." The great advantage of f.s.k. is, of course, the small bandwith required; but a side issue of the work of this group is that the identity of commercial operators who infringe the amateur band allocations can now be established without the necessity for professional help.

## WORLID OF WIREILESS

## Sound Broadcasting

IN view of the recent discussion both in Parliament and the lay Press on the subject of commercial broadcasting and especially its potentialities as a local broadcasting service, the B.B.C. has stated that "Any major extension of the existing services, particularly for local broadcasting, depends in the first instance on the allocation of additional frequencies in the v.h.f. band."

The B.B.C. has already made known to the Post Office its desire to use further frequencies to fill gaps in its present v.h.f. coverage and for local broadcasting, and the statement adds "These frequencies, which are allocated internationally for broadcasting, are at present used in this country by other services, and their release for broadcasting is problematical. Until this question is resolved it is not possible to proceed with detailed plans."

The frequencies referred to are those between 95 and $100 \mathrm{Mc} / \mathrm{s}$. Although the $88-100 \mathrm{Mc} / \mathrm{s}$ band is allocated throughout the world for broadcasting, the Atlantic City allocation table does include a provision that the top $5 \mathrm{Mc} / \mathrm{s}$ may be used in the U.K. for fixed and land mobile services. There is also a provision that the meteorological aids service in the U.K., France and India may be operated between 94.5 and $95 \mathrm{Mc} / \mathrm{s}$.
It remains to be seen what changes in these allocations will be made at the Geneva Conference.

## Government Radio Research

WITH the announcement of the appointment of J. A. Ratcliffe as successor to Dr. R. L. Smith-Rose (see "Personalitics") as director of the D.S.I.R. Radio Research Station, the Council for Scientific and Industrial Research has also announced changes in the terms of reference of the Station.
The Radio Research Station at Slough, which has an international reputation for its detailed studies of ionospheric and tropospheric radio propagation, is to extend its programme to take advantage of the techniques provided by rockets and earth satellites.

Under its new terms of reference the Station, which has a staff of about 160 scientists and assistants, will undertake investigations of the upper atmosphere and outėr space by both radio and nonradio methods. At the invitation of the present director, Mr. Ratcliffe will assist in planning the future research programme before taking up his appointment in October.

## Broadcasting in Italy

ITALY'S network of v.h.f. transmitters is by far the largest in Europe and possibly in the world. At the beginning of December she had 235 stations and as each station radiates three programmes, the total number of f.m. transmitters in use was over 700.
Television stations in Italy now total some 340. They are all accommodated in eight $7-\mathrm{Mc} / \mathrm{s}$ channels in Bands I and III. Only about $10 \%$ of them have an e.r.p. of over 1 kW and some are as low as 0.4 W .

The majority of both the television and v.h.f. sound broadcasting stations are operated as satellites of main transmitters. Italy also operates 116 transmitters in the medium-wave band, more than half of which are low-power. A total of about 7.5 M licences, including well over 1 M for television, are now in force.

International Conferences.-In our comment on page 421 of the October, 1959, issue we suggested the desirability of a Conference on conferences to anticipate congestion. We now learn that the 1st Congress of International Congress Organizers and Technicians was, in fact, held in Düsseldorf in February, 1959, and that the 2nd Congress is already arranged for March 15th-18th, 1960, in Lausanne. It will be held under the auspices of the Union of International Associations whose U.K. representative is E. S. Tew, 91, Lyndhurst Gardens, London, N.3. Other participating bodies include the International Association of Congress Palaces and the International Association of Conference Interpreters.

Medical Electronics Conference.-The third international conference on medical electronics is to be held at Olympia, London, from July 21st to 27 th , $1 \subseteq 60$. It is being organized by the Electronics and Communications Section of the I.E.E. in association with the International Federation for Medical Electronics, which was set up at the Paris conference a few months ago. Those requiring registration forms and further particulars or who are interested in submitting a paper should write to the secretary, I.E.E., for further information. The I.E.E. is also promoting an international scientific exhibition which will be run concurrently with the conference. The exhibition organizers are Industrial Exhibitions Ltd., 9 Argyll Street, London, W.l.

Vibration.-The Acoustics Group of the Physical Society will hold a symposium on the subject of "Vibration" in the Physics Department, Imperial College, Imperial Institute Road, London, S.W.7, at 2.30 on January 20th. Papers will be read on the analysis of noiseexcited vibrations in aircraft, on vibration-isolation, on ground vibrations and on the influence of vibration, including that from small power tools, on the human body. Speakers will include Prof. E. J. Richards and Dr. B. L. Clarkson, of Southampton University, P. H. Allaway, of Absorbit, Dr. N. Ambraseys, of Imperial College, Dr. J. N. Agate, formerly of the London Hospital, and Flt. Lt. Guignard, of the R.A.F. Institute of Aviation Medicine.

The College of Technologists, established by the National Council for Technological Awards last May to administer "an award higher than the Diploma in Technology," to be known as M.C.T. (Membership of the College of Technologists), has issued a memorandum giving guidance to applicants for registration. It outlines the qualifications required, the procedure for the submission of an application and the fees payable. The eight-page leaflet is available from the National Council for Technological Awards, 9 Cavendish Square, London, W.1.

Correspondence Courses.-Approval has now been given by the Royal Navy, the Army and the Royal Air Force for the acceptance of the C.R.E.I. (Capitol Radio Engineering Institute) courses in electronic engineering as qualifying for part refund of fees for external correspondence courses used by members of the Armed Services. The value of the concession may amount to up to $50 \%$ of the cost of the course.
V.H.F. radio-telephone service to ships, which is already provided on the Clyde and from the North Foreland, Niton (Isle of Wight) and Humber coast radio stations, will soon be available from the Land's End station also. All these stations operate on frequencies around $160 \mathrm{Mc} / \mathrm{s}$. The charge for a three-minute call to a vessel within the 40 to 50 mile service area of a station is 6 s 6 d plus a land line charge of from 6 d to 2s $6 d$, depending on the distance the inland telephone subscriber is from the coast station.

Orkney Television Station. - The permanent installation at the B.B.C.'s Orkuey television station, replacing the temporary low-power equipment which has been in use for the past year, was brought into service on December 17 th. The station radiates in channel 5 (vision $66.75 \mathrm{Mc} / \mathrm{s}$, sound $63.25 \mathrm{Mc} / \mathrm{s}$ ) and its directional aerial provides an e.r.p. of from 4 to 14 kW , depending on direction. Transmissions are vertically polarized. The station serves the whole of the Orkney Islands and a large part of Caithness.
E.B.U. Station Lists.-Revised lists of television and v.h.f. sound broadcasting stations in Europe have been prepared by the European Broadcasting Union. These show the situation at July lst last year. The next edition will give the position on January 1st, 1960 , and in future only one edition will be published each year, but supplements will be issued every two months. The price for each of the lists plus the supplements is 50 Belgian francs. They are obtainable from the E.B.U. Technical Centre, 32 avenue Albert Lancaster, Brussels 18, Belgium.

Televis'on Society.-In an endeavour to attract more student members into the Television Society, the Council has decided to waive the entrance fee, which is 30 s . Student membership, for which the annual fee is $£ 1$, is open to those over 16 but under 21, but students over 21 who are taking a recognized college course in television are also eligible. Details of membership are obtainable from the secretary, Television Society, 166, Shaftesbury Avenue, London, W.C.2.

Provincial Centres.-Readers in South Wales may be interested to know that a Centre of the Television Society has been formed in the area. The secretary is D. M. Thomas, 39 Gron Ffordd, Wenallt Road, Rhiwbina, Cardiff. The Society also announces the reformation of the Leicester Centre (secretary E. F. Dawson, 28 Clumber Street, Melton Mowbray) and plans to revive the Manchester and Birmingham centres.
"Engineering Education in the Region" is the title of a booklet produced by the London and Home Counties Regional Advisory Council for Technological Education to assist those who wish to follow a recognized course in some branch of engineering in the region. The courses, grouped under some 50 subjects, are also classified under "grades," ranging from degree and diploma courses to those for craftsmen. The 38 -page booklet costs 3s 6 d from the Council at Tavistock House South, Tavistock Square, London, W.C.1.

Control Engineering.-A course of ten evening lectures on the principles of control engineering. covering both linear and non-linear servo systems, will be given at the South East London Technical College. Lewisham Way, S.E.4, on Wednesdays, from January 20th. Fee £1.

The Technical Publications Association is donating two $£ 10$ awards annually to the City and Guilds of London Institute for the top students in the final grade in the two recently introduced training courses in technical authorship and technical illustration.

Norwood Technical College, London, S.E.27, celebrated its centenary by holding in December a two-day exhibition. It included demonstrations showing some aspects of the work of the various departments and also equipment lent by manufacturers.

Swedish Television.-In the three years since Sweden opened her television service, the number of stations has grown to 23 and half a million television receiving licences are now in force. Although the present stations cover only about $60 \%$ of the 7.4 M population, the present number of licences represents a television density of 66 sets per 1,000 inhabitants. It is planned to open a further 19 stations before July 1 st this year. Sweden employs the $625-\mathrm{line} 7-\mathrm{Mc} / \mathrm{s}$ standard with f.m. sound and all the present transmitters operate in Bands I and III.

Receiving Licences.--October's total of 9,844,365 combined sound and television licences in the U.K. was 125,893 up on the previous month. Sound-only licences totalled $5,084,380$ including 410,372 for car radio.

West German TV.-The number of television licences issued in the German Federal Republic and West Berlin increased by 102,000 in September, and the total is now well past the three million mark.
U.S.S.R.-Television sets in the U.S.S.R. are stated to be among the consumer goods in short supply. Steps are therefore being taken to increase the output from the 1958 total of 979,300 to $1,926,000$ in 1961.

Soviet Radio Telescope.-The first Soviet steerable radio telescope was recently completed at the scientific station of the Lebedev Physics Institute near Moscow. It has a 22-metre (over 72 -feet) paraboloid with a focal length of 9.5 metres. The parabolic mirror weighs 65 tons and the overall weight of the telescope is 380 tons. The paraboloid of the Jodrell Bank radio telescope has a diameter of 250 feet.

For Yachtsmen.-Details of radio beacons and coast radio stations, a map showing the weather forecasting areas and details of the B.B.C.'s transmissions of time signals are included in the 52 -page reference section of the Yachting World Diary, 1960. It costs 6s 3d (with leather cloth cover) or 9 s 9 d (Morocco leather).

## CLUB NEWS

A.R.M.S.-A meeting of the Amateur Radio Mobile Society will be held on January 30 th at 3.0 in the Small Hall of the St. Bride Foundation Institute, Bride Lane, Fleet Street, London, E.C.4. The programme will inciude a lecture and films. Details are available from the secretary, G. E. Storey, 10 Avon Road, Sunbury-on-Thames, Middx, from whom information on the mobile rally planned for April or May is obtainable.

Birmingham.-The January programme of the Midland Amateur Radio Society includes a talk on the 7th by R. Rew on the construction of a $70-\mathrm{cm}$ transmitter and on the 19 th a talk by H. Buckley, of Bradmatic, on sound recording and reproduction. Meetings are held at 7.0 at the Birmingham Midland Institute, Paradise Street.

Calcot-A lecture-demonstration will be given by a representative of Dynatron Radio to members of the Calcot Radio Society on January 21 st at 7.45 in the St. Birinus Church Hall, Calcot, neär Reading.

Cleckheaton.-A representative of Philips is giving a talk on tape recorders to members of the Spen Valley and Leeds Amateur Radio Societies at the George Hotel, Cleckheaton, at 7.30 on January 20th.

Halifax.-A talk on television interference is to be given by H. Swift (G3ADG) to the Halifax and District Amateur Radio Society on January 5th at the Sportsman Inn, Ogden.
Mitcham.-Meetings of the Mitcham and District Radio Society are held every Friday at 8.0 at "The Cannons," Madeira Road, Mitcham. Lecture meetings alternate with instruction classes. On January 8 th a member of the G.P.O. engineering department will give a talk on cable link systems.

Wellingborough.-"Transistors" is the title of the talk to be given by F . Manning at the January 21 st meeting of the Wellingborough and District Radio and Television Society. Meetings are held every Thursday at 7.30 at Silver Street Club Room.

## Personalities

Brigadier Sir Lionel Harris, K.B.E., T.D., M.Sc., F.C.G.I. M.I.E.E., who is 62 , is retiring at the end of January from the position of Engincer-in-Chief of the Post Office. He joined the Post Office research branch at Dollis Hill in 1922 having previously spent four years with signals in the Australian Imperial Forces. During the 1939-45 war he successively commanded G.H.Q. Signals; was Chief Signal Officer, Lines of Communication; and for two years chief of General Bisenhower's Telecommunications Section. From 1949 until his appointment in 1954 as engineer-in-chief he was controller of research.


Sir LIONEL HARRIS.

A. H. MUMFORD.
A. H. Mumford, O.B.E., B.Sc.(Eng.), M.I.E.E., deputy engineer-in-chief of the Post Office for the past six years, succeeds Sir Lionel Harris as Engineer-inChief. He joined the Post Office as a probationary assistant engineer in 1924 and after a short period at headquarters went to Dollis Hill laboratory. He was in charge of the Radio Branch during much of the war. Mr. Mumford was a member of the Post Office team which first recorded aircraft reflections of radio waves in June, 1932. He is 56.

The Postmaster-General has also appointed two deputy engineers-in-chief-Capt. C. F. Booth, O.B.E., M1.E.E, and D. A. Barron, M.Sc., M.I.E.E. Both have been assistant e.-in-c. since 1954. Capt. Booth, who is 59, joined the Post Office in 1923 and was for twenty-five years at Dollis Hill. He led the U.K. delegation to the recent I.T.U. Conference at Geneva. Mr. Barron entered the Post Office engineering departmemt as a probationary assistant engineer in 1927 at the age of 20 . In 1947 he was placed in charge of a working party which examined problems of subscriber trunk dialling.
A. H. M. Arnold, Ph.D., D.Eng., has had the title of Professor of Electrical Engineering conferred upon him by the University of London in respect of his post at King's College, where he has been reader in electrical engineering since 1955. Professor Arnold, who is 59 , graduated at Liverpool University in 1923. He spent a year with Metropolitan-Vickers before going to the National Physical Laboratory in 1926 where he was head of the electronics section of the Electricity Division when he left in 1955 to join the staff at King's College.
R. G. Kenwright has rejoined the Plessey Co. as chief engineer, Television Components Division, Ilford. He was a radio design engineer with the company prior to 1940 when he joined Pilot Radio of which he became chicf engineer in 1946. For ten years Mr. Kenwright was a member of the B.R.E.M.A. technical committee.
R. Hanbury Brown, B.Sc.(Eng.), who has been I.C.I. Research Fellow at the Jodrell Bank Research Station, Manchester University, since 1949 has been granted the status of professor with the title of Professor of Radio Astronomy from January 1st. This chair is a personal appointment and is additional to that held by Professor A. C. B. Lovell, F.R.S. Professor Brown, who received a monetary award from the Royal Commission on Awards to Inventors for his contribution to the development of radar-especially metre-wave AI and ASV--ioined the staff of the Bawdsey Research Station in 1936. He participated in the early experimental flying with night-fighter equipment (AI) and ship and submarine detection gear (ASV). With Dr. E. G. Bowen he detected the first submarine by radar in 1939. From 1942 to 1945 Professor Brown was in the Naval Research Laboratory, Washington, D.C., as assistant head of the combined research group working on the development of radar equipment. "He is 43.
V. J. Cooper, B.Sc., A.C.G.I., M.I.E.E., M.Brit.I.R.E., since 1956 Marconi's chief television engineer (an office which, under a reorganization, no longer exists), has been appointed manager and chief engineer of the company's new Closed Circuit Television Division. He joined Marconi's in 1936 and was chief engineer, advance development, from 1954 to 1956. Mr. Cooper is a member of the technical sub-committee of the P.M.G.'s Television Advisory Committee.
J. E. H. Brace, B.Sc., who joined Marconi's Broadcasting Division in 1954 when a specialist industrial TV unit was established, has been appointed deputy manager and chief of sales and contracts of the Closed Circuit Television Division. Since 1956 he has been chief of the industrial television group with headquarters at the company's Basildon works.
N. N. Parker-Smith, B.Sc., A.M.I.E.E., is appointed chief development engineer of Marconi's Closed Circuit Television Division. He has been with the company since 1947 and for most of the time has been engaged in television development work. From 1953 to 1956 he headed the section of the advance development group handling colour television.

Consequent upon the formation of the new division by Marconi's, the following appointments have been made in the Broadcasting Division: G. E. Partington, B.Sc., A.M.I.E.E., becomes chief engineer and J. F. James, B.Sc., M.I.E.E., chief development engineer. Mr. Partington joined Marconi's in 1938 when he attended a course of advanced training for postgraduate engineers at the Marconi College. In 1949 he was appointed chief of the television studio development group and in 1956 became deputy chief television engineer. Mr. James went to Marconi's from the Ministry of Supply (where he was a senior scientific officer) in 1949. He became deputy to the chief of the radar development group in 1952 and for the past four years has been in charge of this group.
R. E. Burnett, M.A.(Oxon.), A.M.I.E.E., A.Inst.P., general manager of Marconi Instruments since 1956, has been elected to the board and appointed managing director of the company. Mr. Burnett, who is 44, joined the Marconi organization in 1950 when he was appointed principal of Marconi College and manager of the Technical Personnel and Education Department. In 1954 he became assistant to the general manager of Marconi's W/T Co., and a year later transferred to Marconi Instruments as deputy general manager.
A. J. Young, B.Sc.(Eng.), M.I.E.E., general manager of the English Electric Valve Co. since 1956, has been elected to the board and appointed managing director of the company. He joined Marconi's W/T Co., as a valve engineer in 1934 and in 1947 transferred to the English Electric Valve Co . as assistant general manager. He is 51. F. N. Sutherland, C.B.E., M.A., M.I.E.E., managing director of Marconi's W/T Co., has also been elected to the board of the English Electric Valve Co.

Dr. R. L. Smith-Rose, C.B.E., is to retire from the directorship of the Radio Research Station of the D.S.I.R. at the end of September and is to be succeeded by J. A. Ratcliffe, C.B.E., F.R.S., who is head of the radio section of the Cavendish Laboratory, Cambridge. Dr. Smith-Rose, who is 65, has been in the Scientific Civil Service since 1919 and was from 1939 until 1947 superintendent of the Radio Division of the National Physical Laboratory. In 1948 he was appointed as the first Director of Radio Research when the post was created by the D.S.I.R. Dr. Smith-Rose, who has served on many national and international scientific committees, is a member of the technical sub-committee of the Television Advisory Committee and also of the P.M.G.'s Frequency Advisory Committee. Mr. Ratcliffe joined the Cavendish Laboratory in 1924 and worked with E. V. Appleton (now Sir Edward) on his researches on the ionosphere. He founded the Army radar school at Petersham and he later built up the "Post-Design Service" for the R.A.F. which was concerned with the study of radar equipment under Service conditions. During the latter part of the war he was superintendent of T.R.E. He is 57.

J. A. RATCLIFFE.


Prof. E. B. MOULLIN.

Professor E. B. Moullin, M.A., Sc.D., M.I.E.E., is to retire next October from the chair of electrical engineering at Cambridge University, which he has occupied since it was established in 1945. He is 66. Dr. Moullin, who is a Fellow of both King's College, Cambridge, and Magdalen College, Oxford, was a lecturer at Cambridge from 1920 until 1929 when he was appointed Donald Pollock reader in engineering science at Oxford where he stayed until 1945. He is author of a number of books including "Principles of Electromagnetism" and "Radio Aerials", and his research studies have covered a very wide range of radio subjects. Professor Moullin is a member of the Editorial Advisory Board of our sister journal, Electronic Technology (previously Electronic $\mathcal{E}$ Radio Engineer).
C. Collaro, O.B.E., has resigned from the board and chairmanship of Hartley Baird, Ltd. A. W. M. Hartley has succeeded him as chairman and simultaneously has resigned as managing director. H. J. D. L. Walmsley and J. Symonds have been appointed joint managing directors. Mr. Collaro has also resigned from the board of Camp Bird, Ltd., and from Camp Bird Industries, of which he was managing director. He joined the Camp Bird Group in 1957 following his resignation from the chairmanship and managing directorship of Collaro, Ltd.
E. R. Lewis, chairman of the Decca Group of Companies, and Group Captain E. Fennessy, C.B.E., managing director of Decca Radar, Ltd., have joined the board of General Precision Systems, Ltd. (formerly Air Trainers Link, Ltd.), following the acquisition by Decca Radar of a $25 \%$ interest in that company. The two companies are to co-operate in the development of air traffic control systems.

## OUR AUTHORS

Dr. Manfred von Ardenne, a pioneer in the development of the cathode-ray tube for television, writes in this issue on the evolution of the c.r.t. Dr. von Ardenne, who is now head of a research institute in Dresden, East Germany, first wrote for Wireless World over thirty years ago and has made many notable contributions to the development of television. Sydney Moseley and H. J. Barton Chapple in their book "Television Today and Tomorrow" wrote of von Ardenne "he commenced his researches on television in 1930. within a year he earned the distinction of being the first to demonstrate publicly cathode ray reception comparable with that produced by mechanical means."
A. R. Bailey, M.Sc.(Eng.), author of the article on page 25, took his London B.Sc. degree in 1953 at Bradford Technical College (now Bradford Institute of Technology) where he stayed to undertake research into precision three-phase a.c. voltage stabilizers under a D.S.I.R. grant. He went into industry for a short while but returned to the college where he is now a lecturer.
A. E. Falkus, B.Sc.(Eng.), M.I.E.E., who writes in this issue on loudspeaker magnet design, was chief loudspeaker designer of the Plessey Company for eight years until 1958 when with D. A. Newbold he formed Fane Acoustics Ltd. He obtained his degree at London University in 1925 and was at one time chief engineer of Reproducers and Amplifiers Ltd.

Robert Hickson, whose article on the Smith Chart is on page 2, is technical librarian of Belling and Lee, Ltd. During his national service in the Royal Navy (1945-47) he was a radio mechanic and before joining Belling and Lee he had been a technical writer on the staffs of Marconi Instruments and S.T.C
J. M. Waddell, M.A., A.M.I.E.E., who with D. R. Coleman discusses Zener diodes in an article on page 17, spent a little over two years in R.E.M.E., after leaving Cambridge where he read physics. From 1949 to 1958 he worked in the Rectifier Division of Standard Telephones and Cables and from 1956 was responsible for the development and applications of silicon rectifiers. For the past year he has been with Texas Instruments, Ltd., Bedford.
D. R. Coleman, B.Sc.(Eng.), A.M.I.E.E., co-author of the article on Zener diodes, joined S.T.C.'s rectifier division in 1956 and is now in charge of the group concerned with the evaluation and applications of semiconductor devices. After three years in the Royal Engineers he studied at the Regent Street Polytechnic and then spent five years (1951-56) on the development of aircraft electrical equipment.

## OBITUARY

Hilary F. C. Wiliiams, B.Sc., chief electronics engineer of Andec, Ltd., for the past 12 months, died suddenly on November 11 th at the age of 45 . After graduating at London University in 1935 he became a schoolmaster and during the war was at the Royal Aircraft Establishment where he held an honorary commission in the Royal Air Force. He was with Cossor's for nine years after the war as a development engineer and later assistant chief engineer of Racal Engineering.

Joseph Poliakoff, founder of the Multitone Electric Co. in 1931, died on November 24th at the age of 86. Mr. Poliakoff, who established the Telephone Construction Co. in Russia (it was nationalized in 1921), came to this country in 1924. He was managing director of Multitone until 1938 when owing to ill-health he resigned in favour of his son, but continued on the board and took an active part in the day-to-day affairs of the company. Although his life-work was devoted to the alleviation of deafness, he was an engineer of wide interests-he had a patent for recording sound on film in 1894.

# News from the Industry 

A.E.I. Reorganization.-On January 1st the British Thomson-Houston Co., Metropolitan-Vickers Electrical Co. and Siemens Edison Swan changed their names to Associated Electrical Industries (Rugby) Ltd., Associated Electrical Industries (Manchester) Ltd., and Associated Electrical Industries (Woolwich) Ltd., respectively. At the same time five new Product Divisions of A.E.I. (making 12 in all) come into operation. They are: Cable Division and Construction Division combining the interests of the S.E.S. Cables Division with those of W. T. Henley's Telegraph Works Co. and Liverpool Electric Cables; Telecommunications Division, hitherto a Product Division of Siemens Edison Swan; and a Radio and Electronic Components Division. These four Divisions will be managed by Associated Electrical Industries (Woolwich) Ltd. The fifth is the Instrumentation Division combining the interests of Sunvic Controls with the instrument and meter, X-ray, and scientific apparatus departments of Metropolitan-Vickers and will be managed by Associated Electrical Industries (Manchester).
G.E.C.-Plessey Co-operation.-An arrangement has been entered into by the Semiconductor Division of the G.E.C. and Semiconductors L.td., of the Plessey Group, whereby each will handle information on the products of both organizations.

Plessey's trading profit for the year ended in June was $£ 2.206 \mathrm{M}$ compared with $£ 1.350 \mathrm{M}$ the previous year. The net profit after rax deduction was $£ 1,194,499$ as against $£ 561,991$ last year.

Gresham Automation Ltd. has been formed to handle the Gresham Unit Sequencing System. The directors are John P. Coleman (chairman of Gresham Transformers Ltd. and of the Gresham Lion Group) and R. M. Campbell, a director of Gresham Transformers. Dr. D. B. Foster is appointed as consultant to the board. The offices of the new company are at Gresham House, Twickenham Road, Hanworth, Middx. (Tel.: Feltham 2271.)

Marconi's W/T Co. have received a contract from the B.B.C. for the supply of a considerable quantity of equipment, valued at approximately $£ 115,000$, to extend the coverage of the television and v.h.f. sound broadcasting services to "difficult" areas. The order includes 10 television translators (for picking up sound and vision signals from one station, and re-transmitting them on other frequencies); 4 television transmitters and 30 f.m. translators-all of 10 watts output. The associated amplifiers for the equipments vary in power from 100 watts to 1 kW .
E.M.I. apprentices with Clifford Metcalfe, C.B.E., managing director of E.M.I. Electronics, who presented them with prizes for obtaining their Higher National Diploma in electrical engineering with three or more distinctions. The recipients (from left to right) are David Jackson, George East and James Jordan, who were among thirteen E.M.I. apprentices who enrolled for the first four-year sandwich course at Southall Technical College in 1956. All thirteen have obtained their H.N.D. and are taking the fourth year of the course to qualify as Grad. I.E.E.

Electronic Associates Ltd., with offices and works at Victoria Road, Burgess Hill, Sussex, have been formed by Electronic Associates Inc., of Long Branch, N.J., U.S.A., manufacturers of Precision Analog Computing Equipment (PACE). The Burgess Hill works will be managed by H . Turner, a director of the new company and a graduate of Manchester University, who has been with the parent company for several years. The managing director is Dr. B. Murphy, who is also general manager of the European branch of Electronic Associates Inc, set up in Brussels in 1957.

Pye Telecommunications Ltd., have moved their London sales and service headquarters to 1 Carrol Place, Highgate Road, N.W.5 (Tel.: Gulliver 8771), where Brigadier E. J. H. Moppett, the London-based director, has an office.

Datum Metal Products Ltd. (formerly Davis and Thompson), members of the J. Langham Thompson Group, have moved into a new factory on the Colne Way Trading Estate, Watford By-Pass, Herts (Tel.: Watford 22351). These new premises have trebled the production area of the company.

Aircraft-Marine Products (G.B.) Ltd., who market the range of A-MP solderless terminations, have moved from Regent Street to Amplo House, 87-89 Saffron Hill, London, E.C. 1 (Tel.: Chancery 2902). The building houses the head office, the research laboratory (formerly at Bournemouth), the sales and engineering departments, and the international trade division (previously at Bedford Row).

Lasky's Radio have opened new premises at 207 Edgware Road, London, W. 2 (Tel.: Paddington 3271), in addition to their branch at 42 Tottenham Court Road, London, W.1.

Pye have supplied the equipment for the inter-branch television network recently introduced by the Westminster Bank in Manchester. The cable system linking two branches with the central book-keeping department in the main city office, is provided by the G.P.O. The 625 -line system is employed.

Smiths.-Examples of many of the products manufactured at the twenty factories in the Smiths Group, which includes Kelvin-Hughes and Radiomobile, are displayed at the Smiths Centre, Cricklewood, which was officially opened by H.R.H. the Duke of Edinburgh on November 19th.


By J. M. WADDELL,* M.A., A.M.I.E.E., AND D. R. COLEMAN, $\dagger$ B.Sc. (Eng.), A.M.I.E.E.

AMONG the many new components now appearing in electronic equipment as a result of the intensive work which has been done on semiconductors in the last few years is a useful group usually known as "Zener" diodes. What are these "Zener" diodes, and what do they do?

If we examine the reverse characteristic of a typical silicon junction rectifier, shown in Fig. 1, we can see that the reverse current remains extremely small at all voltages below a certain value, the "Zener voltage." Then, as the voltage is raised slightly above this value, the current increases very rapidly indeed into the so-called "breakdown" region. For power rectifiers, the manufacturer arranges that this breakdown region occurs well above the normal reverse operating voltage, in order to avoid excessive power dissipation in the reverse direction and consequent failure due to overheating.

It should be noted that this phenomenon is not a breakdown in the ordinary sense of the word (in the sense in which a dielectric breaks down), but is a completely reversible process which of itself causes no damage to the rectifier. However, if the rectifier were run continuously in this region it is probable that the maximum allowable dissipation of the device would be exceeded and the rectifier damaged; but if excessive dissipation is avoided the diode can be run in the "broken down" condition indefinitely. A diode used deliberately in this way for any purpose is called a "Zener diode."

The term "Zener diode" was coined when this


Fig. 1 Reverse characteristic of a typical silicon junction rectifier.
breakdown was first observed' because it was thought that the mechanism responsible was that proposed by C. Zener in 1934 to account for the breakdown of solid dielectrics ${ }^{2}$. It turns out that this "Zener breakdown" is responsible where the breakdown occurs at low voltages (below 5 volts in silicon), but that at higher voltages breakdown is

[^5]

A group of typical Zener diodes.
due to another mechanism, "avalanche multiplication," similar to the breakdown process in gaseous dielectrics described by Townsend. ${ }^{3}$ Thus the higher voltage Zener diodes should really be called avalanche diodes. While one of the purposes of this article is to draw attention to the different behaviour of Zener and avalanche diodes-for example, the "knee" of the breakdown characteristic is more rounded in a Zener diode and so the slope resistance of such diodes is higher than that of the corresponding avalanche diodes-it is convenient to have a generic term to cover all such devices, and the term "Zener diode" has received widespread acceptance.

It is possible to use a term denoting the application, e.g., " reference diode," "regulator diode," but the range of use of these devices is so vast that no one application can be singled out for such special mention. We recommend the continued use of "Zener diode" as the most useful general term.
One of the great advantages of these devices over previously available voltage stabilizing devices, such as gas discharge tubes, is that the breakdown voltage can be controlled during manufacture to any value from about two volts to several hundred volts. In addition the transition from "off " to "on" takes place smoothly, without the discontinuity associated with gas discharge tubes. No special arrangements are needed for starting, and the absence of negative resistance means that shunt capacitance can be added without causing oscillation. Under appropriate conditions, substantially zero temperature coefficients of voltage may be obtained. Furthermore, Zener diodes are smaller and more robust than gas tubes or batteries, and by comparison they have an almost indefinite life.

Fig. 2 shows typical characteristics of some diodes specially made for use in this way. It will be noted that here the breakdown voltages are quite low, from about 4 to 9 volts. From this graph the important parameters which define the properties

[^6]

Fig. 2 Typical characteristics of diodes specially made for Zener operation.
current as that at which the nominal voltage is measured. The lower the slope resistance the more constant is the operating voltage with changes in current. As will be seen from the curves, the operating voltage at a given current changes with working temperature, and so for many applications the temperature coefficient of voltage is also important. Finally, since these devices, like most components, are given a maximum operating temperature, the maximum dissipation limits the maximum continuous working current.
Operating Mechanism.-In order to understand the way in which these various parameters change for different values of working voltage, it is helpful to have some understanding of the alternative mechanisms involved in the breakdown region. In a silicon rectifier biased in
of a particular Zener diode can be clearly seen. The first and most important is the voltage in the breakdown region. This is not a unique and fixed value, but increases with the operating current; thus the current at which the voltage is measured must be specified. Usually the manufacturer chooses a particular value of current and quotes the voltages of a complete range of diodes at this particular current.

The next most important parameter is the "slope resistance," or the dynamic resistance of the diode in the "breakdown" region. This again is measured at a particular current, usually the same


Fig. 3 Variation of slope resistance with reverse current for a typical range of Zener diodes.
the reverse direction almost all the applied voltage appears across the narrow depletion layer located immediately on either side of the junction, and the remaining volume of the silicon is essentially field free. For a given applied voltage the field in the depletion layer depends on the width of this layer, being a function of the centre region resistivity of the diode. This resistivity is controlled during manufacture so that the field in the finished diode can be made to have any desired value for a given voltage across the diode : the higher the resistivity, the wider the depletion layer and the smaller the field per unit of applied voltage. The depletion layer is normally quite narrow, so that fields of the order of several hundred thousand volts per cm . are readily reached.

With fields of this order in the depletion layer the current carriers which constitute the reverse current are accelerated to considerable energies between each collision with the stationary silicon atoms of the


Fig. 4 Temperature coefficient of voltage for a typical range of Zener diodes.


Fig. 5 Variation of forward slope resistance for a typical Zener diode.
lattice. As the voltage across the diode is raised, the field increases, and when it reaches a critical value the energy obtained by each electron or hole between collisions is sufficient to eject an additional electron from the atom with which it collides, thus creating a hole-electron pair. These additional free carriers are also accelerated in their turn, and produce yet more free carriers which all add to the total reverse current. Thus the reverse current, initially no larger than the saturation reverse current present at low voltages, is multiplied to a much larger value by this "avalanche" process, in a manner analogous to the Townsend mechanism in gas discharge tubes.

Zener Effect.-In order to produce low breakdown voltage diodes, the depletion layer must be made very narrow. Under these conditions the current carriers are accelerated through the barrier without ever striking an atom of the lattice, and so the avalanche effect does not occur. In these circumstances, as the voltage across the diode is increased the field can rise until it reaches a higher critical value at which true Zener effect occurs. This is a quantum mechanical effect in which holeelectron pairs are generated directly from the energy of the electrical field. The resultant current increases rapidly with voltage, but not quite as rapidly, as with the avalanche effect, so that the "knee" of the curve is more rounded.

For silicon junction diodes the changeover occurs in the region of 5-8 volts, those diodes below 5 volts exhibiting Zener breakdown, while those above 8 volts exhibit avalanche breakdown. The breakdown of diodes between 5 and 8 volts is due to a combination of the two mechanisms. An important difference between these two mechanisms is that the temperature coefficient of voltage or the Zener process is negative, whereas that for the avalanche process is positive.

Characteristics.-As a result of the above, it is customary to present the characteristics of a particular series of Zener diodes (that is, a range manufactured to the same physical dimensions and differing only in breakdown voltage) in the form of curves showing the various parameters plotted against the breakdown voltage at which the diode under consideration actually operates. Since the characteristics of Zener diodes are related to their operating temperature, it is important to distinguish between a " convection-cooled" (such as a wire-ended) diode for which the immediate ambient temperature is considered, and a "conduction-cooled" (such as a stud-ended) diode for which the characteristics are


Fig. 6 Change of reverse voltage (ot constant current) for a typical range of Zener diodes.


Fig. 7 Change of forward voltage for a typical Zener diode.
quoted in terms of the stud temperature. The following data may, for simplicity, be considered applicable to wire-ended diodes at the stated ambient temperatures.

Fig. 3 shows, for example, the variation of slope resistance with voltage for typical Zener diodes from a particular range. Since the slope resistance is also a function of the operating current, curves for several currents are given. The higher current curves are limited in voltage excursion by the allowable dissipation in the diodes. The slope resistance shows a minimum in the changeover region around 7 volts and rises steeply on the low voltage side of this point, but less steeply on the high voltage side. On the high voltage side, however, the slope resistance increases more rapidly than the voltage, so that if slope resistance is important better results can be obtained by using, say, five 7 -volt diodes in series, instead of one 35 -volt diode.

The variation of temperature coefficient of voltage against working voltage is shown in Fig. 4. It will be seen that diodes with breakdown voltages in the region of 5 volts are the most attractive from this point of view. However, approximately zero temperature coefficients can also be obtained by connecting a diode having a positive coefficient in series with one having a negative coefficient, although this


Fig. 8 Applicotion as a voltoge regulator or reference source.

Fig. 9 Surge limiting circuit using a Zener diode.


Fig. 10 Balanced clipping circuit using back-toback diodes.
arrangement will probably give a higher slope resistance. In a similar way the negative temperature coefficient of the forward characteristic of a diode may be used to cancel a positive temperature coefficient of reverse breakdown voltage. The slope resistance in the forward direction is low (Fig. 5).

In making up series chains of Zener diodes to achieve approximately zero temperature coefficient, it should be noted that the calculations require curves showing actual change in voltage per ${ }^{\circ} \mathrm{C}$ (as in Figs. 6 and 7), and not the conventional values of temperature coefficient of voltage expressed as percentage change of voltage per ${ }^{\circ} \mathrm{C}$.

The exact value of the temperature coefficient of a given diode is a function of the operating current, and of the precise temperature range over which the change in voltage is measured. Consequently, zero temperature coefficient of voltage will only be possible at one value of current for any one diode, and only over a limited temperature range. Where the very best performance as a voltage reference is required, care should be taken to keep the current constant, and if possible at that value which gives zero temperature coefficient.

As explained above, the manufacturer can design diodes to operate at any given voltage by adjustment


Fig. II Zener diodes used for coupling elements and cathode bias in a d.c. amplifier.

Fig. 12 Application as a voltage-sensitive relay.

of the resistivity of the base region of the diode; but this can only be done with limited accuracy. A given batch of diodes as manufactured has a certain spread of voltage values. Of the many varied uses of Zener diodes, some applications may call for the diode to have an accurately specified working voltage with a tolerance of, say, $\pm 1 \%$, while others may merely require a breakdown voltage between, say, 15 and 20 volts. In an application as a source of reference voltage, the working voltage of the diode may be quite unimportant; but extreme stability, coupled with low slope resistance and low temperature coefficient, will be desirable. As a result, if care is not exercised, there will grow up a vast proliferation of types, each differing only slightly from the next, and the manufacturer and the user will be faced with the problem of stocking reasonable numbers of each type, while the small demands for any one type will result in uneconomic manufacturing runs.

To deal with this problem, manufacturers in this, country are at present marketing "general purpose" Zener diodes, which are available in $\pm 5 \%, \pm 10 \%$, and $\pm 20 \%$ tolerances, using the same preferred numbers for nominal breakdown voltage which are familiar to users of resistors and capacitors, e.g. 3.3, 3.6, 3.9, 4.3, 4.7V, etc.

Applications.-The number of possible applications for these diodes appears to be extremely large. The most obvious applications are as voltage regulators and voltage reference sources (Fig. 8). For regulator application a low slope resistance and high power handling capacity are desirable features, while for reference purposes, stability of reference voltage with time and a low temperature coefficient are the most important factors. Suitably chosen voltage reference Zener diodes appear at this moment to be comparable with industrial standard cells in their voltage stability.

Another large field of application lies in the use of Zener diodes for surge limiting and waveform clipping, etc. Fig. 9 shows a circuit which gives both top and bottom clipping using only one diode. This circuit makes use of the fact that Zener diodes, being in other respects normal silicon rectifiers, have a forward characteristic which may be used on many occasions. The same circuit may also be used for protecting transistor circuits from line surges. If a balanced clipping action is required, two Zener diodes should be used, connected back to back (Fig.


Fig. 13 Characteristic of an experimental high-bower shunt regulator Zener diode for the region 2-20 amperes.


Fig. 14 Capacitance effect over a range of Zener diodes.
10). Some manufacturers now make special clipper diodes for this purpose.
Zener diodes have a much lower a.c. resistance than d.c. resistance (i.e. $\frac{\mathrm{dV}}{\mathrm{dI}} \ll \frac{\mathrm{V} \text { ) }}{\mathrm{I}}$ which means that they behave rather like a capacitor or battery. They are particularly useful for coupling and decoupling elements in d.c. amplifiers, where capacitors cannot be used because of the rise in impedance at low frequencies. Even in a.c. circuits at low frequencies the Zener diode may be more economical than a large capacitor, especially in space. Fig. 11 shows the use of a Zener diode as a coupling element and for fixed cathode bias in a d.c. amplifier.
Fig. 12 shows a method of obtaining a robust and inexpensive voltage sensitive relay; the relay should operate with a low voltage across it and thus the Zener diode used must be capable of passing a reasonably large current. Zener diodes can be made capable of handling quite large powers. Fig. 13 shows the characteristic of an experimental $150-$ watt unit intended for shunt regulation of power supplies, to operate between 2 and 20 amps .

A further useful property of silicon junction diodes (such as Zener diodes) is their "self capacitance." In addition to the electrostatic capacitance between the diode leads, or between the leads and metal case, there is a "self capacitance" associated with the junction itself; because the depletion layer is extremely narrow in a Zener diode, the junction capacitance is usually much greater than the case capacitance. This "self capacitance" is seen when the diode is biased in the reverse direction below the breakdown voltage. Fig. 14 shows the variation over a range of Zener diodes, the capacitances being measured at the same low voltage for all diodes in the range.

In addition, for any one diode, the capacitance depends upon the bias voltage applied. Increase of bias voltage up to the breakdown value causes a reduction of capacitance, as illustrated in Fig. 15. The voltage-dependent capacitance has applications in automatic frequency control. With an f.m. tuner, for example, the diode may be used as part of the tuning capacitance, whose value is controlled by the output from the discriminator.


Fig. 15 Typical values of capacitance for reverse bias voltages before the breakdown region (at $25^{\circ} \mathrm{C}$ ).

It is hoped that sufficient has been said about these new components to stimulate interest in their application and to give some guidance in their use. Much remains to be learnt of their characteristics and possible applications. Perhaps this article will help to speed the process.


Semiconductor Production ot the G.E.C. Semiconductor Division factory at Hazel Grove, Stockport, Cheshire, is now about 70,000 transistors and diodes per week. This automatic wafer measuring machine sorts germanium and silicon wafers according to thickness at the rate of 1,200 per hour. Another interesting technique uses a centrifuge to ensure good glass-to-metal seals in the housings. The glass and metal components are placed in jigs in an annular-shaped boat which is rotated and heated in an inert atmosphere, so that centrifugal force throws the molten glass into intimate contact with the metal parts. The method of operation, including control of temperature and cooling, is completely automatic. Using such methods the firm claims to have achieved an average yield of between $70 \%$ and $80 \%$.

## LEETTERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

## Single-channel Stereo

HASN'T "Free Grid" (in the October issue) gone a bit wild over his one amplifier, two channels. If you sample (with rectangular wave) at $50 \mathrm{c} / \mathrm{s}$ you get every frequency in the spectrum modulated by $50,100,150$, etc., and that's a nasty noise. You should sample at something over twice the highest frequency in the wanted spectrum and put in a low-pass filter to get rid of higher-frequency unwanted modulator products. But the low-pass filters you would need have a reaction component in their impedances; they store energy and so forbid the clean cut that is essential for sampling as
"Free Grid" wants it.
London, S.W.3. P. P. ECKERSLEY.

## Editors and Editing

IN his article "Words, Words, Words" in the November "Wireless World," Mr. Eckersley very rightly calls for an improvement in the standard of writing of technical articles and papers. Victorian scientists, he says, wrote well, even excellently; many of them could be described as cultured. Nowadays, it is of no help to a scientist to be cultured and to write well, because the editors won't let him publish a paper as he writes it. Editors quite rightly tidy up ${ }^{1}$ a badly-written piece of work, but when a paper is well written, they should leave it alone ${ }^{2}$.

The interference frequently consists in making alterations to the style to bring it into line with editorial policy ${ }^{4}$. People who believe that it is possible to make small alterations in the style of a well-written piece of prose without ruining its effect-an effect that the author has probably worked hard to achieve-ought not to sit in editorial chairs. One famous Learned Society ${ }^{1}$ will never allow an author of a paper to refer to that paper as "this paper," always substituting "the paper," to which a reader of any sensibility ${ }^{5}$ reacts by asking "' what paper?". The same Learned Society" recently allowed
one of its vice-presidents to use the phrase "a whole diversity of new materials $\%$. If it is willing to allow such a phrase to appear in its Proceedings, by what right does it sit in judgment on the work of other authors? The Chairman of the Editorial Board of another Learned Society ${ }^{4}$ is the author of several books from which it is clear that he does not know how to punctuate. Yet this Learned Society, like many others, dares to have an editorial policy on style-as if style can ever be a matter of policy.
May I therefore make a plea that writers be allowed to publish their papers and articles in the language in which they were originally conceived? While the various Learned Societies ${ }^{4}$ should do all they can to improve standards of writing, they should refrain from interference with a piece of work, once it is written, except on technical grounds-and even then, any alterations called for should be made by the author'. Let the cditors confine their activities to editing-that is, to deciding the arrangement of the material on the printed page, to interpreting the author's intentions to the typographers, to correcting obvious errors, and to adding footnotes, e.g. "continued on page. ..."s And, critics, please be a little more charitable to the author ${ }^{9}$. Why should he take all the blame, when things are done to his work over which he has no control, and of which he may even have no knowledge until his alleged work appears in print? ${ }^{10}$

## Chelmsford.

## R. A. WALDRON.

## [1 Or decline to publish.

${ }_{2}$ Being busy men they are usually happy to do so.

- This journal welcomes diversity of style.
- Capitals for a common noun and its adjective?
s Sense is shorter than sensibility and does not involve the emotions.
© What is wrong with this? Collectively the materials are finitc and although diverse can be comprehended as a whole.
, Who will then permit the editor's name to appear as co-author?
- This is the dull mechanic trade of sub-editing.
-Touché!
${ }^{10} \mathrm{Mr}$. Waldron's letter is printed as received with the exception of the interpolation of reference numbers to the rejoinders which the Editor feels compelled to make in defence of his vocation. He is nevertheless glad to publish this letter if only to show that he is mindful of the feelings of his contributors-present and future.]


G.M.T.

.......... FREQUENCY BELOW WHICH COMMUNICATION SHOULD BE POSSIBLE
FOR $25 \%$ OF THE TOTAL TIME
— - - predicted median standard maximum usable frequency
frequency below which communication should be possible
ON ALL UNDISTURBED DAYS

Speed-Change Drive for magnetic tape data recording equipment has been devised by E.M.I. Electronics for applications where it is necessary to play back the data for analysis at a different speed from that at which it was recorded. It is a simple device giving a wide-ratio change of speed without mechanical complexity. Power is applied to one shaft carrying a stepped plain pulley A, and the output drive is taken from another shaft carrying flywheel $B$ which also has two working surfaces of different radii, one external and the other internal. An idler carriage E is mounted on a plain bearing on the input shaft, so that it is dragged round by friction as far as it is free to move in whichever direction the input shaft is turned. If, in the diagrams, the drive shaft is turned anti-clockwise (State 1), the resulting anticlockwise motion of the idler carriage will draw the idler wheel $F$, supported on E by the swinging arm H , into engagement with the larger diameter (C) of pulley $A$ and the smaller diameter ' $d$ ' of the flywheel B. B will move anti-clockwise, and

as in the figure $C$ and ' $d$ ' are approximately equal, there is no change of angular velocity in the mechanism. If the direction of the drive shaft is reversed (State 2), the carriage E will move clockwise until the alternative idler $G$ engages between the smaller diameter (' $c$ ') of $A$ and the larger diameter (D) of B. When this occurs the flywheel B will move anticlockwise as before, but with a speed reduction determined by the ratio

of $D$ to ' $c$.' In the case drawn this ratio is about 1 to 30 . Thus it will be seen that by reversing the direction of the input shaft a large speed reduction may be obtained-the output shaft always revolving in the same direction. A large number of speed ratios may be obtained by suitable selection of diameters and positioning of components.

Magnetless Masers are possible according to an article by G. S. Bogle and H. F. Symmons in the Australian fournal of Physics for March 1959 (p. 1). Normally in the three level type of maser, three suitable spin quantum levels between which transitions are possible can only be obtained in certain paramagnetic salts in a magnetic field. The authors point out, however, that certain paramagnetic salts possess three suitable energy levels between which transitions are possible even in the absence of a magnetic field. Unfortunately, unlike ordinary masers, magnetless masers will not be tuneable over a wide frequency range. On the other hand, magnetless masers possess a number of compensating advantages over ordinary masers. For example, exacting requirements of magnetic field uniformity and stability are avoided and, since crystal orientation is no longer necessary, a single crystal is not required for a magnetless maser.

Directly Printed Circuits, as distinct from the usual etched variety, are made possible by a new copperbearing paste developed by Bell Telephone Laboratories in the U.S.A. The paste is applied in the required circuit pattern to a ceramic base and the process is completed by heat treatment. The main advantage of the new system is the strong adhesion of the copper coating to the base material, compared with conventional etched circuits. Failure of bonding does not occur, it is claimed, until the pulling strength exceeds 2,000 $\mathrm{lbs} / \mathrm{sq}$. in. In preparation a paste is made from a finely ground mixture of copper oxide and a special glass "frit" (a term from glass-making), blended with a standard silk-screen printing material. After the pattern of paste is printed on the ceramic, the circuit card is dried to remove solvents. The card is then fired in
air at $750^{\circ} \mathrm{C}$ for twenty minutes to burn off the screen-printing material. This operation leaves a non-conducting copper oxide pattern, ready to be reduced to metallic copper. The second firing operation is conducted at $850^{\circ} \mathrm{C}$ for thirty minutes, in an atmosphere containing hydrogen, nitrogen and oxygen. The hydrogen reduces the copper oxide to metallic copper, while the oxygen prevents reduction of other oxides in the system and promotes good wetting of the glass frit and the ceramic. Without the oxygen present, a poor bond results. Printed wiring cards prepared this way can be dip-soldered without bond failure, and without the use of corrosive fluxes. Resistivity of the copper film is said to be well within requirements for typical printed wiring applications. The process is suitable for automatic production techniques, and is expected to be competitive with other printed wiring methods in cost. Another possible application is in making metal-to-ceramic bonds.

Distortion Reduction in class-B amplifiers using biased diodes to switch in different signal potential dividing resistors at different signal levels to compensate for non-linearities in the class-B input/output characteristic is described in an article by B. Sklar in Electronics for May 22, 1959 (p. 54). One arm of the signal potential divider consists of a fixed resistor, and the other a number of branches in parallel, each branch containing a fixed resistor in series with a diode and biasing battery. Thus, at a signal voltage determined by the biasing battery voltage, the diode switches the fixed resistor into one arm of the potential divider. The resultant resistance in this arm thus varies with the signal level, and the consequent changes in the signal potential dividing ratio with the signal level can be used to compensate for non-linearities in the class-B input/output characteristic. A graphical method of determining from the input/output characteristic the resistance required in series with each diode for a given biasing voltage is described in the article. In a practical case the total harmonic distortion in a push-pull amplifier (mainly third harmonic) was reduced from 13 to $2 \cdot 6 \%$.

# Physical Society Exhibition 

Manufacturers and Research Establishments Exhibiting

ON the majority of the 140 stands at the 44th exhibitoon of scientific instruments and apparatus arranged by the Physical Society there will be equipment of interest to zadio and electronic engineers. The exhibition will be held from January 18th to 22nd in both the Old and New Halls of the Royal Horticultural Society, at Westminster, London, S.W.1.

The opening ceremony will be performed by J. A. Ratcliffe, C.B.E., F.R.S., president of the Physical

Society, at 11.0 on January 18th. On the opening day admission will be limited to members of the Society and the Press until 2.0. The times of opening are: $18 \mathrm{th}, 10.30$ to 7.0 ; 19th, 10.0 to $9.0 ; 20 \mathrm{th}$ and $21 \mathrm{st}, 10.0$ t. 7.0 ; and $22 \mathrm{nd}, 10.0$ to 1.0 .

Tickets of admission are obtainable free from exhibitors or from the Society, 1, Lowther Gardens, Prince Consort Road, London, S.W.7.

A feature of the Society's exhibition each year has been the series of
demonstration lectures. This year the lectures will be given on each of the first three days at 5.45. On the 18th the subject will be "Some reactions of the human body to the stresses of high performance flight" and the lecturer, Flt. Lt. J. Billingham (R.A.F. Institute of Aviation Medicine); on the 19th "Atomic Time" by Dr. L. Essen (N.P.L.); and on the 20th "Recent developments in solid state physics" by Dr D. A. Wright (G.E.C. Research).

Name
Stand

Harrison, W
Hatfield Instruments
Hilger \& Watts

## Imperial College

Infra Red Development Co.
Institute of Physics
Isotype Developments
Johnson, Matthey \& Co.
Joyce, Loebl \& Co.
Kelvin \& Hughes
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Physical Society Acoustics Group 140
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ARTHUR R. BAILEY*,
M.Sc.(Eng.), B.Sc.(Eng.)

# Economical High-Gain A.F. Amplification 

MICROPHONE AND TAPE-REPLAY AMPLIFIERS USING UNUSUAL CIRCUIT

FOR many years engineers have been trying to obtain the maximum amplification from the minimum number of components. During research into precision three-phase a.v. stabilizers, the author came across a somewhat unorthodox phase-splitter which gave an unusually large gain for the valves and components used. This circuit, which is shown in Fig. 1, utilizes the high input impedance of a concertina phase-splitter to provide a very high load impedance to the anode of a pentode amplifier. As the amplification factor for an r.f. pentode can be over 10,000 at low values of anode current ( 0.1 mA ) and the anode slope resistance may then be as high as $20 \mathrm{M} \Omega$, then it can be seen from the formula


Fig. 1. Theoretical circuit of high-gain phase-splitter.
$A=\mu R_{L} /\left(r_{a}+R_{L}\right)$ that if the load resistance can be made greater than $r_{a}$ then the amplification will be greater than $\mu / 2$.

In the high-gain phase-splitter circuit the maximum amplification obtained is about 1,000 times. This compares favourably with the normal overall gain for a pentode amplifier (and "concertina" phase-splitter) of 100 to 300 times. Providing that a push-pull output is required, it is difficult to see how this circuit can be improved. If, however, a single-ended output is desired, then the circuit can be modified with advantage.

The first obvious step is to remove the anode load resistor $R_{4}$ of the triode valve: this is unnecessary as it merely provides the phase-inverted output. It will now be noted that the cathode load of the cathode-follower so formed consists of the pentode valve and its load resistor $R_{1}$ (in series) in parallel with the h.t.-feed resistor $R_{3}$ and the cathode resistor $\mathrm{R}_{\mathrm{s}}$ (in parallel). If the circuit is now re-
arranged, as shown in Fig. 2, it will be seen that the pentode valve now obtains its anode supply through the triode valve and the loading effects of resistors $R_{3}$ and $R_{5}$ (Fig. 1) are removed. The cathode-follower has now a very high effective load in its cathode circuit; thus it will generate a cathode-to-earth voltage of very nearly $\mu$ times the grid-tocathode input voltage ${ }^{2}$. This grid-to-cathode input is developed across the anode-load resistor $\mathrm{R}_{1}$ of the pentode valve. Hence for $1 V$ of signal developed across this resistor there will be approximately $\mu_{\mathrm{t}} \mathrm{V}$ (where $\mu_{t}$ is the amplification factor of the triode) developed at the cathode of the triode. This means that the signal voltage on the pentode anode will be approximately $(1+\mu) \mathrm{V}$. As 1 V is developed across the pentode anode-load resistor $R_{1}$, the triode must therefore be acting as an additional a.c. load of approximately $\mu_{t} R_{1}$. To be accurate, both $R_{1}$ and $R_{2}$ should be considered; but as $R_{2}$ is over 10 times larger in value than $R_{1}$ its effect is very small.
The voltage drop in the triode valve need not exceed about 75 V and so the triode will only slightly reduce the dynamic mutual conductance of the pentode valve. The triode therefore acts as a low resistance to d.c., but as a very high anode-load resistance. The pentode will give a very large gain due to this high anode load and the gain may approach the pentode amplification factor. For some pentodes this may be 10,000 times, and under these conditions the effective anode load may rise as high a value as $100 \mathrm{M} \Omega$. The effect of stray capacitances is then extremely serious and care has to be taken if a useful a.f. bandwidth is to be obtained.
Providing that the pentode anode-circuit components are physically small and sensibly arranged, the main capacitances in shunt with the pentode-anode circuit are the anode-to-grid capacitance of the

Fig. 2. High-gain amplifier derived from phase-splitter shown in Fig. 1.


[^7]

Fig. 3. High-gain amplifier used as microphone pre-amplifier. Preset gain switch positions: 1, low gain; 2, high gain.
triode and the output capacitance of the pentode. The anode-to-grid capacitance of a 12 AT 7 is only 1.5 pF and is therefore hardly worth ncutralising. The output capacitance of a 6 BW 7 is 3.5 pF which is also quite small. The effect of these capacitances could be reduced somewhat by the "Cathoguard" circuit ${ }^{3}$. If the response is to be maintained up to $10 \mathrm{kc} / \mathrm{s}$ with a maximum of 3 dB fall in responsc, then the total capacitance of 5 pF (ignoring stray and valve-base capacitances) will limit the effective anode output impedance to $10 / \pi \mathrm{M} \Omega$. This value is composed of the anode load of the pentode in parallel with the anode slope resistance of the pentode valve. Assuming a dynamic anode-slope resistance for the pentode of 5 MO , this gives a maximum pentode anode load in the order of 8 MS ? . This was halved to allow for the stray capacitances that were ignored; thus a value of $4 \mathrm{M} \Omega$ was obtained. With a 12 AT 7 valve a voltage amplification of 40 would be expected, hence a value of $4 \times 10^{6} /(40+1)$, or approximately $100 \mathrm{k} \Omega$, for the pentode load resistor $R_{1}$ was obtained.

The circuit has been used in a tape-recorder built by the author and has given very satisfactory results. The microphone amplifier of the recorder is shown in Fig. 3. This can be used at either high or low gain to allow for a wide range of input signals. In the high-gain position the circuit operates as previously described; in the low-gain position the pentode is re-connected as a "straight" amplifier driving a cathodefollower. The gain of the circuit is approximately 200 in the low-gain position and 3,500 in the high-gain position. The output is at low impedance, and providing that the outputvoltage swing is restricted to several volts, loads of as little


Fig. 4. Tape-playback pre-amplifier providing equalizotion facilities. Switch positions: 1, $3 \frac{3}{4} \mathrm{in} / \mathrm{sec} ; 2,7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$.
tage of a relatively low amplification factor. When using a 6BR7 in place of the 6BW7 the value of the cathode-bias resistor must be decreased to 4.7 k : for the tape-replay amplifier and to $1 \mathrm{k} \Omega$ for the microphone amplifier.

Summing up, the advantages of the circuit are that few components are required and that all the amplification is obtained from the pentode valve. Due to this and the low output impedance of the circuit, the hum and noise introduced by the second valve is negligible, whatever valve type is used. The one disadvantage is that it is difficult to maintain a high amplification at supersonic frequencies; but this is not normally important.

Acknowledgement.- The author wishes to acknowledge the facilities provided by the Bradford Institute of Technology where most of the work on this circuit has been carried out.

## REFERENCES

${ }^{1}$ Push-Pull Phase-splitter, by E. Jeffery, Wireless World, Vol. 53, p. 274 (August 1947), also "Amplifiers" (Ist Edition) p. 101, by G. A. Briggs and H. H. Garner, Wharfedale Wireless Works.
${ }^{2}$ Radio Engineering (3rd Edition) by F. E. Terman, p. 308, McGraw-Hill Publishing Co., Ltd.
${ }^{3}$ The "Cathoguard" by L. G. White, Wireless World, Vol. 64, p. 312 (July 1958).

## JANUARY MEETINGS

Tickets are required for some meetings; readers are advised therefore to communicate with the secietary' of the Society concerned.

## LONDON

6th. Brit.I.R.E.-" Some new possibilities in civil underwater echo-rang-ing-current research at the University of Birmingham" by Professor D. G. Tucker at 6.30 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C.1.

8th. I.E.E-Discussion on electrical and electronic techniques in respiratory research at 6.0 at Savoy Place, W.C.2.

8th. Television Society.-" Problems of u.h.f. television: transmission, propagation and reception" by T. M. J. Jaskolsky (E.M.I), R. A. Rowden (B.B.C.) and K. Moulding (Mullard) at 7.0 at the Cinematograph Exthibitors' Association, 164, Shaftesbury Avenue, W.C. 2.
11th. I.E.E.-" A quadrature network for generating vestigial-sideband signals" by G. G. Gouriet and G. F. Newell; "The input impedance of rectifier modulators" by Professor D. G. Tucker; and "Rectifier modulators with frequency-selective terminations, with particular reference to the effect of evenorder modulation products" by D. P. Howson and Professor D. G. Tucker at 5.30 at Savoy Place, W.C.2.

13th. Brit.I.R.E.-"A proposal for a space-charge-linited dielectric triode" by Dr. G. T. Wright at 6.30 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C. 1.

15th. B.S.R.A. - "Stereophonic hearing" by Professor Colin Cherry at 7.15 at the Royal Society of Arts, John Adam Street, W.C.2.
20th. Physical Society Acoustics Group.-Symposium on "vibration" at 2.30 in the Physics Dept., Imperial College, Imperial Institute Road, S.W. 7.

21st. Television Society.-Fleming Memorial Lecture on "Crystal Imperfections" by Professor R. King at 7.0 at the Royal Institution, Albemarle Street, W. 1 .
22nd. R.S.G.B.-Presidential address by W. R. Metcalfe (G3DQ) at 6.30 at the I.E.E., Savoy Place, W.C.2.

25th. I.E.E. Graduate and Student Section.-"Transistors in switching circuits" by M. Paskins at 6.30 at Savoy Place, W.C.2.

25th.-Radar and Electronics Asso-
ciation.-"The problems of technical reviewing" by J. C. G. Gilbert and R. S. Roberts at 7.30 at the Royal Society of Arts, John Adam Street, W.C. 2 .

27th. British Computer Society."Storage elements for very-high-speed computers" by Dr. G. G. Macfarlane (R.R.E.) at 2.30 at Northampton College of Advanced Technology, St. John Street, E.C. 1 .

27th. I.E.E.-" The oral presentation of scientific material " by Dr. A. Clow at 5.30 at Savoy Place, W.C.2.

27th. Brit.I.R.E.-"Training for operating and maintaining television broadcasting equipment" by Dr. K. R. Sturley and A. E. Robertson at 6.30 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C. 1.

28th I.E.E.-"Radio communications by means of satellites" by Dr. A. W. Lines at 5.30 at Savoy Place, W.C.2.

29th. I.E.E.-"Beam-type parametric amplifiers: some aspects of design and use" by R. B. Dyott and C. R. Russell at 5.30 at Savoy Place, W.C.2.

## BIRMINGHAM

19th. I.E.E.-Faraday Lecture on "Electrical machines" by Professor M. G. Say at 6.30 at the Town Hall.

25th. I.E.E.-" Long-distance waveguide communication" by F. J. D. Taylor at 6.0 at the James Watt Institute

## BRISTOL

27th. Brit.I.R.E.-"An equipment for automatically processing time multiplexed telemetry data (Timtape)" by I. H. Russell, N. Purnell and T. Walters at 7.0 at the School of Management Studies, Unity Street.

## BROADSTAIRS

26th. Association of Supervising Electrical Enginecrs.--" The Decca navigational system" by B. A. A. SmyeRumsby at 8.0 at the Clarendon Hotel.

## CARDIFF

21st. I.E.E.-Faraday Lecture on "Electrical machines" by Professor M. G. Say at 6.0 at Sophia Gardens Pavilion.

28th. British Compurer Socicty. "Basic principles of programmine" by Dr. R. J. Ord-Smith (S.T.C.) at 6.30 at University College.

## CHESTER

25th. I.E.E.-" The characteristics and protection of semiconductor rectifiers" by D. E. Corbyn and N. L. Potter at 6.30 at the Town Hall.

## LEICESTER

19th. Television Society.-."The electrical synthesis of music" by A Douglas at 7.30 at the Collcge of Technology and Commerce.

## LEEDS

4th. Association of Supervising Elcctrical Enginecrs.- "Radio control" by E. B. Hill at 7.30 at the Great Northern Hotel.

## LIVERPOOL

1lth. Brit.I.R.E.-" High frequency propagation-its present and future use for communication purposes" by A. F. Wilkins at 7.0 at the University Club.

14th. Institute of Physics.-"Electronic applications of superconductivity," by Dr. E. Mendoza at 7.0 at the University.

18th. I.E.E-" Radio aspects of the International Geophysical Year" by Dr. R. L. Smith-Rose at 6.30 at the Donnan Laboratories, Vine Street.

## MANCHESTER

18th. Institute of Physics.-" Recent developments in scintillation counting" by Dr. J. B. Birks at 7.0 at the University.

## NEWCASTRE-UPON-TYNE

13th. Brit.I.R.E.-"Data processing machines" by J. Allen and I. Keating at 6.0 at the Institution of Mining and Mechanical Engineers, Neville Hall, Westgate Road.

## TREFOREST

13th. Brit.I.R.E. - "Television broadcasting methods" by H. J. M. Hockley at 6.30 at the Glamorgan College of Technology

## WOLVERHAMPTON

13th. Brit.I.R.E.--"Electronics in medicine" by P. Styles at 7.15 at the Wolverhampton and Staffordshire College of Technology, Wulfruna Street

# Evolution of the Cathode-Ray Tube 

A Survey of Developments over Three Decades

By MANFRED VON ARDENNE*

UNTIL the year 1928 the cathode-ray tube devised in 1897 by Ferdinand Braun only found application on rare occasions, despite the fact that Wehnelt (in 1905) and Westphal (in 1908) had already improved it considerably by the introduction of the incandescent cathode. In 1928 the cathode-ray tube emerged from its latent existence and rapidly gained in importance in two directions of development:

1. About this time the high-tension cathode-ray oscillograph with cold cathode and continuous


Fig. 1. The electron gun developed in 1928 with negativelybiased control electrode and beam cross-over. This gun, which is used in most present-day electron beam appliances, is shown here in an oscillograph tube for anode voltages above 1 kV , introduced by Leybold of Cologne in 1929.
evacuation made its appearance for the investigation of transient waves. The development of this instrument is linked with the names of Rogowski, Gabor, Dufour, MacGregor-Morris, von Borries and Binder.
2. The cathode-ray tube of modern design, which today plays important roles in the fields of oscillography, radar, and television, made its appearance.

A kindly fate has made it possible for me to collaborate actively in this second direction of development over a period of more than three decades. Today, perhaps, I may be permitted to look back over the field of my personal experience in this work.

## Looking Back

The devclopment of the modern cathode-ray tube received a decisive impetus in 1928 when it became possible, in my laboratory at Lichterfelde, to produce a fine electron beam with a current density of about $100 \mu \mathrm{~A}$ and an acceleration of up to 3,000 volts as a result of a three-electrode system with

[^8]a hot cathode and a control electrode with a negative bias. This electron gun was not only characterised by its construction from a thermal small-area cathode, a control electrode with negative bias and an anode, as well as by the geometry employed. Its most significant feature was the formation of an electron beam cross-over of small cross-sectional area and high current density. This emitting system differed from all earlier methods of operation of similar electrode arrangements in that the negative bias of the control electrode had a definite value somewhat below the initial voltage of the cathoderay current. So far as can be seen from the literature available, these features were combined for the first time in the oscillograph tube ${ }^{1}$ developed by me in 1928 and put on the market in 1929 by E. Leybold's Nachfolger of Cologne. Fig. 1 shows the structure of this tube with the type of electron gun characterised by the cross-over formation, as is used today in a great many electron devices.

Another branch of oscillograph technology which was making strides at that time, and which was later to achieve great significance in television engincering, radar engineering and high-frequency carrier telecommunications, was the wide-band amplifier or, as we called it in those days, the "aperiodic high-frequency amplifier." Together with Siegmund Loewe, we had begun in 1925 to combine several valve systems with their low-capacitance coupling units in a single evacuated glass envelope. In this way the Loewe dual valve, shown in Fig. 2, which had a space-charge grid system with a steep slope, was able to achieve a bandwidth of $1 \mathrm{Mc} / \mathrm{s}^{2}$.

In order to change over from timebase deflection by mechanical/optical means (rotating mirror) to deflection by low-inertia electrical methods, relaxation oscillator devices were devised in that particular year in the

Fig. 2. The Loewe dual tube, developed in 1925, was in fact the first wideband amplifier, in the modern sense of the term, and had a bandwidth of $1 \mathrm{Mc} / \mathrm{s}$. This was obtained by the combination of a particularly low-capacitance circuit with highslope valve systems.


Lichterfelde laboratory, on the basis of publications by B. van der Pol and H. Frühauf ${ }^{3}$ with the collaboration of I. Kammerloher. These gave triangular waveforms which could be synchronised by means of a cold-cathode thyraton with external control from the signal.

In the year 1930 there were available, in my laboratory in Lichterfelde, electron beam tubes with intensity modulation electrodes and high focal point brightness ${ }^{4}$, relaxation oscillator devices to suit these and wide-band amplifiers in large numbers ready for operation. At that moment it was only a short step to the realisation of television on a purely electronic basis. The technical prerequisites for this purpose were so favourable as a result of the fact that the three basic elements were standing ready in one building, that this realisation, from the time of making the decision to the time of succeeding in an experiment, required hardly more than one day's wiring operations and experimental effort.

The stimulus for starting this work came in the main from outside. Since 1924 I had been following with great interest the reports of the pionoer experiments by J. L. Baird in England using mechanical scanning of the picture by means of a Nipkow disc ${ }^{5}$. This interest was considerably increased when D. von Mihaly demonstrated practical experiments at the Berlin Radio Exhibition of 1928, using an arrangement which was somewhat similar to a Baird televisor, and the demonstrations of mechanical television continued at the Radio Exhibitions of 1929 and 1930 with increasing quality. Finally, I received a particularly powerful stimulus to carry out this work from the experience of a personal meeting with Baird himself, and from the detailed discussions with him regarding the limits of the mechanical methods employed at that time.

Despite repeated indications of the advantages of the electronic method by Fritz Schröter and myself, in lectures and articles, television experiments continued to be conducted with mechanical scanning only. The time had become ripe for some experiments of our own. These experiments led to the achievement, on the 14th of December, 1930, of the first television pictures obtained on a purely electronic basis. One of the pictures, obtained in the year 1930, is shown in Fig. 3(a). A few months later the quality of the pictures had already been increased to the stage shown in Fig. 3(b).

An important factor in carrying out the television transmission experiment so quickly with electron ray tubes both at the transmitter and at the receiver, was the conception of the flying spot scanner ${ }^{6}$. Since then the flying spot scanner has been further developed for the scanning of colour films, for facsimile transmission of over 1 million words per minute (Ultrafax), for counting and sorting of particles on microscope slides, for optical auto-correlation measurements and many other purposes. As is known, this scanner works by deflecting a light spot over the screen of a cathode-ray tube with short after-glow so as to produce a bright raster which is focused by an object lens on the slide or film to be transmitted. The beam of light passing through the slide or film is then fed to a photoelectric cell. According to the optical density of the picture points encountered by the scanning spot a greater or lesser quantity of light is absorbed, so that the electron current emitted by the photoelectric cell is proportional to the brightness values of the picture points.

(a)

(b)

Fig. 3. Electron beam television pictures produced (a) in the year 1930 and (b) in 1931.

Soon after the first experiments with slides, the device used at that time was converted for the scanning of cinematographic films. The first public demonstration of the equipment as a whole was made in the autumn of 1931 at the Berlin Radio Exhibition. It had already been demonstrated to most of the leading technicians of the various European development centres. Because of the simplicity of the arrangement and the brightness of the pictures obtained, these demonstrations turned out to be such effective propaganda for the electronic method that, one year later at the Radio Exhibition of 1932, television receivers with cathode-ray tubes were exhibited by several radio firms. Today I still regard one of the great events of those days to be a visit to the Lichterfelde laboratory, of J. L. Baird, who unfortunately is no longer with us (see Fig. 4). During these demonstrations there had already been a display of the projection of television pictures from a cathode-ray tube on to a large screen of about 1 square metre, using a special optical system ${ }^{\text {. }}$.
In the efforts to increase still further the brightness of the picture, and to increase the number of picture elements which could be transmitted for a given frequency band of the transmission channel, experiments were carried out in the Lichterfelde laboratory in 1932, partly with the collaboration of Kurt


Fig. 4. The British television pioneer J. L. Baird (left) on a visit to our television laboratory in Berlin-Lichterfelde.

Schlesinger, using the so-called "variable speed scanning method" proposed shortly before by Richard Thun'. As is known, in this method the control of the brightness of the picture elements is effected by changing the speed of deflection of the light spot, so that at the receiving end the picture is reproduced always with the maximum possible spot brightness. Against this, in the modern television method only a mean spot brightness is effective.

In view of the advantages offered by the variable speed scanning process it is surprising that, up to the present time, nobody has tried out this process in industrial television, where there are no television standards which have to be observed. At that time, in 1932, our efforts with a system of television picture reproduction using variable speed scanning very soon found powerful support in the London laboratories of Cossor in the work of Bedford and Puckle ${ }^{8}$. These workers improved the quality of the picture by controlling the brightness not only by varying the line deflection speed, but also by using a certain amount of intensity control of the light spot.

In the year 1933 the demand for electron ray tubes began to increase at a tremendous rate. One of the largest customers in those days was the development centre at Slough in charge of R. A. (now Sir Robert) Watson-Watt, which of ten required deliveries of from 50 to 100 cathode-ray tubes. At the same time there arose an ever-increasing demand for the construction of complete cathode-ray oscillographs with builtin power packs and timebase units. It could be foreseen that the production possibilities of our small Lichterfelde laboratory would rapidly be exhausted. For this reason, working in collaboration with Leybold, the "Leybold-von Ardenne-OszillographenGesellschaft" was founded which grew extremely rapidly in the years which followed. Even this company was no longer able to cope with the tremendous increase in the requirement for oscillographs, and shortly before the outbreak of the second world war it was taken over by the firm of Siemens and Halske of Berlin.

As a result of the development in Lichterfelde, the Leybold - von Ardenne company brought out the polar co-ordinate electron beam oscillograph in the year $1936^{\circ}$. In this apparatus, which made use of some of the radar techniques being introduced at that time, the timebase was described by an exactly circular movement of the light spot and the measur-
ing deflection was carried out in a radial direction.
Already the transition from the gas-filled to the high-vacuum cathode-ray tube with beam concentration by electron-optical methods had been completed. Already, in the television tubes of 1930 and 1931, electrode arrangements had been used in the Lichterfelde laboratory ${ }^{4}$ which are known today as electrostatic focusing lenses, and the control knob on the receiver for adjusting the voltage to these lenses was marked "Focusing." Based on the work of Busch "", the electron-optical mode of operation had been developed by Calbrick-Davisson, Brüche, Knoll, Recknagel, Scherzer and others ${ }^{11}$. It was therefore soon possible in Lichterfelde, with comparatively few stages of experimentation, to develop high-vacuum cathode-ray tubes with a long cathode life and with anode voltages of up to more than 8 kV for mass production ${ }^{\prime 2}$.

A parallel idea to my electron raster microscope came into being in 1938 in the form of the closely related electron-optical ray path of the electron micro-oscillograph ${ }^{13}$. In this type of oscillograph,


Fig. 5. (a) The electron micro-oscillograph devised in 1939 became well known, particularly through the equipment developed by Lee shown here. At (b) is a "one-shot" oscillogram of a wave with a frequency of $3,000 \mathrm{Mc} / \mathrm{s}$, traced with a 10 -micron scanning spot.
which was developed for Siemens with three or four scanning systems, the scanning spot was focused by means of a magnetic lens with a short focal length and a comparatively large beam aperture. In this way a scanning spot having a diameter of only about 10 microns was obtained, which gave an extraordinarily high current density at the anode voltage of 50 kV . This feature made it possible for the oscillograph to have an unusually high scanning speed. Since the deflection plates were also produced in "micro" construction and consequently the transit time effects were reduced, the instrument opened up possibilities of oscillographical investigation of transient phenomena at very high frequencies. This oscillograph principle has become known particularly through the Lee ${ }^{14}$ equipment in Fig 5.

Very often certain inventive ideas occur quite independently of one another, and almost simultaneously, when the time for their conception is ripe. As an example of this I would like to recount here an incident from the early part of the second world war. H. E. Hollmann, a radio physicist also working in Lichterfelde, and I had decided in 1940 to work jointly on the development of a panoramic
(Continued on page. 31)
radar apparatus with decimetric waves ${ }^{18}$. The basic concept was already pretty obvious to us as a result of the polar co-ordinate oscillograph I have already mentioned. We foresaw the tremendous importance of the panoramic radar principle for the future, and so the development proposal was taken direct to the German government minister, Goering, who was at that time responsible for aviation research. Goering's answer, that the war was already won and consequently there was no longer any need for a development which would not bear fruit for one or two years, characterizes the mental capacity of the system of government ruling in Germany at that time. Approximately at the same time as ourselves, Wat-son-Watt had begun the development of his panoramic radar system which found its way into the history of the second world war and, encouraged by the farsightedness of his Government, was brought to such a successful conclusion during the years which followed.

At the end of the war, the Lichterfelde laboratory, which had remained completely intact, was transferred, together with its staff, to the south of the Soviet Union. Here, in 1952, was the first opportunity for re-commencing our work in the field of electron beam devices. The result was the precision electron beam oscillograph with a scanning spot of about 3 microns diameter and a scanning area of almost $9 \times 12$ centimetres. Fig. 6 shows the apparatus $^{16}$ which was further perfected after the return to Dresden from the Soviet Union. The fine focusing of the scanning spot was carried out with the help of a grainless luminous screen, which was observed through an optical microscope. The photograph in the vacuum camera is taken on a $9 \mathrm{~cm} \times$ 12 cm photographic plate with a fine-grain thin emulsion layer.
This oscillograph differs from the micro-oscillograph mentioned earlier in respect of the increased length of the deflected beam and the extreme sharpness of the spot. By virtue of the large deflected beam length and the extremely small convergence angle of the writing beam, the deflection errors with this system are reduced to the extent that nearly $10^{9}$ image points can be accommodated on an oscillograph screen of the size mentioned. This figure is about four orders of magnitude higher than in the case of the usual cathode-ray oscillograph. Consequently, as a result of the smallness of the beam convergence angle
( $2 \alpha_{L} \approx 3 \times 10^{-0}$ ), the photographic scanning speed of this type of oscillograph (as also the scanning speed in relation to the diameter of the scanning spot) is necessarily small. Furthermore, as a result of the smallness of the scanning spot the oscillograms are not visible to the naked eye, so that in order to observe them it is necessary to use an optical microscope.

By means of this type of oscillograph, which is only at the beginning of its applications in research work, the fine structure of oscillograms is opened up to direct observation. Two sections of an oscillogram obtained with this apparatus, one highly magnified and the other very highly magnified, are shown in Fig. 7. These will perhaps serve to give an idea of the properties of this latest child of the electron beam oscillograph family. By recording the fine structure of characteristics in plasma investigations (characterizing the stability of the plasma), by making visible details of curves produced by the Barkhausen effect, by plotting fine details of transistor characteristics, the precision electron beam oscillograph has already introduced a new era in the graphical recording of electrical phenomena. The first results of this type of oscillographic recording have already shown great promise, particularly in studying the fine structure of electro-encephalograms, electro-cardiograms and nerve action potentials.

## Looking Forward

It is perhaps a comforting thought for the younger generation that there are still many important problems in the science and technology of electron beam 1 devices which remain to be solved in the future. Some of these problems can be clearly seen already, or are delaying the introduction of apparatus into practical use. Perhaps I may be permitted to conclude this article with a few remarks regarding such fields which so far have hardly been broached.

As far back as 1955 H. E. Kallmann ${ }^{17}$ had mentioned a new deflection system by means of which the deflection sensitivity in the $Y$ direction can be increased by about one order of magnitude. It is worthy of note that this system has found no application up to the present. A start was made at testing it out in conjunction with the precision electron beam oscillograph, because the new deflection principle could be a great step forward in this technique, where there is a very small beam cross-section in the deflection space. The relative deflection sensitivity of the precision oscillograph in terms of the diameter of the scanning spot is already more than one order of magnitude higher than that of the cathode-ray oscillograph tubes available on the market. One should therefore expect that this combination, at present in the development stage, should provide a total increase of more than two orders of magnitude of Y deflection sensitivity.

With very many measuring problems this advance would make it possible to manage completely without a deflection amplifier. This prospect is particularly valu-

Fig. 6. Layout of the precision electron beam oscillograph developed during the period 1952-55. In this apparatus, built by VEB Vakutronik of Dresden, the scanning spot is only 3 to 5 microns and the scanning area is about $9 \mathrm{~cm} \times 12 \mathrm{~cm}$.


Wtreless World, January 1960


Fig. 7. Highly-magnified sections from o precision oscilogram of a music waveform at the output of a radio receiver: (a), section magnified 15 times (approx. 1/900 of the area of the $9 \mathrm{~cm} \times 12 \mathrm{~cm}$ photographic plate); (b), section magnified 56 times, showing velocity modulation of the scanning line by residual i.f. signal from the receiver. (Approx. 1/4000 of the surface area of the $9 \mathrm{~cm} \times 12 \mathrm{~cm}$ photographic plate!)
able in the case of the precision oscillograph, because the fine structure of the oscillogram would no longer be restricted by fluctuations in the deflection amplifier, and only the fine structure of the waveform under investigation would be made visible.
Closely related to the questions I have just touched upon is another line of development, in which low-noise amplifiers are used as deflection voltage amplifiers for oscillographs, especially for precision instruments. The future use of low-noise amplifiers in conjunction with precision oscillographs, for example, in the field of action-potential oscillography in medicine and physiology (observing the details of electro-cardiograms, electro-encephalograms and so on) should lead to interesting results.

Some of the tasks which face the precision oscillograph today will perhaps also be carried out by means of a special oscillograph tube with a very high spot sharpness (e.g. 5 to 10 microns), equipped with a suitable electron lens, with a grainless cemented luminous screen and with an anode voltage of 10 to 30 kV .

A wide field of application, especially in the field
of medical electronics, should be claimed by the single-gun multiple oscillograph with television tube bulb, of which individual examples have already been constructed. With this 4 to 6 waveforms can be traced simultaneously on an after-glow screen with the help of an electronic switch.
Far greater efforts will be made than in the past to achieve the direct recording of oscillograms in single processes. Going beyond the recording tubes which have already been developed so far there should be wide use in practice for tubes with the facility of storing traces and also for instruments with xerographic recording of oscillograms developed from the old idea of Selényi ${ }^{18}$.

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# Subjective Colour Tests 

MEASUREMENTS ON A REDISCOVERED "TWO-COLOUR" SYSTEM

TELEVISION engineers have recently been showing a good deal of interest in a system for reproducing pictures in colour which has the unusual feature of using white as one "colour" component and, say, red as the other. This phenomenon has been known for some time, but about a year ago was rediscovered and studied in detail by E. H. Land in the U.S.A.-as a result of which it has become popularly known as "Land colour." The feature of Land colour which would seem attractive for possible use in colour television is that it would only be necessary to transmit two simple signals carrying colour information. In the established N.T.S.C. colour television system it is necessary to transmit a luminance signal plus two colour-difference signals which, in a very complex way, contain information on the three primarycolour components of the picture. Even if Land colour did not offer an advantage in bandwidth economy it would apparently make things much simpler for the engineer.
Unfortunately, Land colour has a big drawback in that it depends on subjective effects to convey some of the colour information to the mind of the observer. And the extent to which the observer "sees" these colours, which are not presented physically to his eyes, depends very much on their positions and areas in the colour picture. At a recent meeting of the Physical Society's Colour Group some very fine examples of Land colour

> Results of the B.B.C. tests plotted on the C.I.E. chromaticity diagram, which also shows the N.T.S.C. red, green and blue primaries for colour television. The figures around the spectrum locus are wavelengths in millimicrons $\left(10^{-9} \mathrm{~m}\right)$. (a) and (b) are two different results for one colour.

pictures were presented by M. H. Wilson and R. W. Brocklebank of the Goethean Science Foundation, Stourbridge. These, to most people, would have certainly passed muster as genuine three-colour reproductions, but it was pointed out that their success was very much a result of the careful composition of the coloured objects in the pictures. The effectiveness of the subjective colours cannot easily be determined, of course, but one speaker at the meeting, W. N. Sproson, described some subjective measurements for this purpose which had been conducted at the B.B.C. Research Department, using colour-matching procedures. Before giving details of the B.B.C. tests, however, it may be as well to recapitulate the basic method of producing Land colour pictures, for the benefit of those readers who may not be able to consult the relevant literature. ${ }^{\star}$
Two photographs are taken of the scene to be reproduced; one through an optical filter passing only light of wavelengths longer than about 590 $\times 10^{-9} \mathrm{~m}$ (appears red when viewed by transmitted light) and the other is taken through a filter passing wavelengths shorter than this figure: this filter appears green or bluish-green. Processing to produce positive black-and-white images is then carried out-images in which the amount of light passed at any point represents the brightness of the scene at that point, within the pass-band of the filters used. These two records are thrown together on to a screen by two projectors, or otherwise superimposed additively (i.e., taking the electrical analogue, the images are in parallel, not series), the long-wavelength record being illuminated by light of a "longer" wavelength and the short record by light of the "shorter" wavelengths. The point on the wavelength scale about which the terms "longer" and "shorter" apply does not seem to be critical as the result is a picture in colour, even if two similar filters, such as orange and yellow, are used in projection. Also one positive may be illuminated by white light and the other by coloured light: Land concentrated on this latter method, using red light for the long record and white for the short.
"Simultaneous contrast" effects, in which the apparent colour of an area is influenced by its surroundings, have been known (and exploited) for a long time, especially in fields such as stage lighting. $\dagger$ However, the only result one would expect from the use of red and white lights would be the appearance of "minus red" (blue-green, the complementary colour to red). As Land's claims went far beyond this, Wireless World decided, as did many others, to repeat Land's experiments. Photographs of a test piece containing coloured cloths, china,

[^9]truit and fiowers were taken through Ilford filters Nos. 204 and 404 and these were processed to form positive transparencies for projection with red and white light. The colour rendering varied over the scene, being fair on small areas, such as the fruit, good on one or two points of fine detail such as the yellow centre of a white daisy, and poor in large areas. Another interesting point was that a suggestion of blues appeared in the right places in the reproduction, but, in fact, little blue light could have been registered on the film, for the pair of filters used were the red and green from a set of three designed to split the spectrum into three parts centred on the three primary colours in light; red, green and blue. Also, Wireless World was invited to view some work being done by J. P. Wilson, of the Information Systems Group, King's College, London, where similar effects were noted. An interesting side-issue of this visit was a demonstration which seemed to indicate that the simultaneouscontrast effects occur not in the retina, but in the brain. The experiment consisted of displaying one positive transparency to each eye, the long record having also the appropriate filter included in the light-path. In this way, each retina was presented with only one picture, but the result was still a Land-colour rendering of the scene.

In the B.B.C. tests the object was to form an estinate of the range of chromaticities given by Land colour reproduction, and the results were plotted on the standard C.I.E. chromaticity diagram $\ddagger$ as shown in Fig. 1. A triple projector was used. Two-colour and three-colour versions of the same slide were shown to the observers individually. The threecolour version used red, green and blue positive separations projected through the same coloured filters. The two-colour version used the red and green separations projected in red and white lights.

A colour-naming technique was used to assess the accuracy of the two-colour version in terms of the three-colour version. Specific areas of a given picture were named by the observer; no restriction was placed on the actual colour names to be used by the observers but consistency of naming was requested. The same areas were named in both a two-colour and a three-colour reproduction. The colour namings were then analysed into the three classes: "identical," "similar" and "different." Chromaticities of the colours were estimated by comparison with the Munsell Colour Atlas.
On the C.I.E. chromaticity diagram in Fig. 1 are shown the results of the colour namings. The numbers at specific chromaticities are the percentages of observers giving "identical and similar" namings to the two-colour and three-colour versions. On the basis of these few results a central area has been shaded in, over which $50 \%$ or more of the observers gave "identical" and "similar" namings. The diagram shows a straight line CR (joining Illuminant C standard white to red) which represents the "objective" range of colours produced. A further, outer area is also shaded in, and over this there is little or no similarity in the colours produced by a two-colour and a three-colour reproduction.

The cffect of the size of colour patch is important, and the C.I.E. diagram gives the results for fairly

[^10]large colour patches. The tests have shown that the range produced by this two-colour process is definitely greater when the colour patch is somewhat smaller. Yellows, greens and blues have been reported in small areas, although the C.I.E. diagram indicates, correctly, that in larger areas these colours are not accurately reproduced. This fact has been confirmed by the Wireless World experiments.

Thus, in view of the subjective nature of the colours and the fact that they depend a great deal on the composition of the pictures, it does not seem that Land colour has much to offer for a practical system of colour television. One has only to compare the limited range of chromaticities indicated by the central area in Fig. 1 with the wide range enclosed by the N.T.S.C. primaries to see the disadvantage of Land colour for large-area reproduction. It has been suggested that the phenomenon might be valuable in prompting us to revise our orthodox ideas on colour vision, but at the abovementioned meeting Professor W. D. Wright, the eminent authority on optics, expressed the view that the established theories are not likely to be affected by it.

## Doctors' Hohbies Exhibition

DIVIDED into 22 classes covering activities ranging from the collection of antiques to photography, this exhibition included an Electrical Class in which the winning entry was a small television receiver described on the accompanying card by its maker, Dr. M. J. Ball, as ". . . suitable for the invalid's bedside or the bureaucrat's desk". The set is housed in a cabinet made by resin-bonding Formica to a wooden frame and it uses a 5 -in magnetically deflected and focused c.r.t. (Type 5FP7). The long-persistence afterglow of the screen phosphors had been partly destroyed by exposure to ultraviolet light. Providing for the reception of both B.B.C. and I.T.A. programmes on its attached 16 -in rod aerial, the receiver consists, in the main, of sections of commercial receivers modified and adapted to suit the 5 -in tube. In all, 17 valves of various heater-current ratings are used and these are interconnected in a series-parallel configuration to provide a $0.3-\mathrm{A}$ heater chain.

As the receiver is made up from units and components of normal size, their close packing inside the case caused difficulties due to deflection of the c.r.t. beam by stray magnetic fields and the heat produced by the 120 W or so of mains power consumed. The use of Mumetal screening and careful orientation of iron-cored components overcame the first problem, whilst ventilation through the loudspeaker grille in the top of the cabinet, coupled with the use of an aluminium deflector assisted in the removal of heat.

The exhibition was oganized by Benger Laboratories, Ltd., and held at the London headquarters of the British Medical Association.


Small television receiver seen at recent exhibition.

# Electromechanical Analogies 

By<br>"CATHODE RAY"

Some Further Details of How to Represent
Mechanical "Works" as Electrical Circuits

UAST month we agreed that developing the analogy between electrical circuits and mechanical (and acoustical) devices was a very nice idea, and most instructive and useful if correctly handled. But it was casier to go wrong with it than might seem at first sight.

On the electrical side, we all understand how to represent a piece of equipment as a circuit diagram, made up of standardized graphic symbols joined up by lines representing wires. Our difficulties begin when we try to represent a piece of mechanical equipment by an analogous type of diagram. Even when that part of the job is done for us in a book, we may not be quite clear how the various components are "connected." Not clear enough, anyway, to apply a foolproof rule for translating the diagram into its equivalent electrical circuit.

That was the part of the problem we dealt with last time. Before going on let us recapitulate.

The analogy we considered was the familiar "direct" one in which force is represented by e.m.f., velocity by current, mass by inductance, compliance by capacitance and resistance, reactance, impedance, etc., are terms common to both. Mechanical links such as rods (assumed massless, or their masses represented separately in lumps) correspond roughly with wiring, but if we treat them in the same way as electrical connections we can hardly fail to go wrong. In particular, the order in which they are connected-unimportant in electrical circuits-makes all the difference. If an applied " a.c." force gives two mechanical elements the same linear vibratory velocities, reckoned between their "terminals," they are by definition analogous to corresponding electrical elements in series, though visually they are " in parallel." Whereas the two "terminals" of a mechanical resistance (represented conventionally by two flat surfaces sliding across one another frictionally, or by the piston and cylinder of a dashpot) and of a compliance (represented by a coil spring) can easily be located, a mass has only one connection to the force. But it


R Fig. 1. Mechanical "circuit", in which on alternating force $F$ is applied to two springs, to one of which is connected a frictional damper.

Bloch* suggested the term "co-resistive" for both it and an electrical series circuit. And because the analogue of an electrical parallel circuit is one in which the same force comes across each mechanical element equally, which happens when they arc apparently in series, he uses the description "co-

Fig. 2. Direct electrical analogue of Fig. I.

yielding " for both. So to transform a mechanical system into its equivalent electrical circuit in accordance with the direct analogy, first draw it as a mechanical "circuit" by the foregoing conventions, to bring out the points of application of forces and to show whether elements are connected in what we electrical people would call series or parallel; then convert it to the "dual" arrangement (in which series and parallel are all interchanged), and at the same time-or as a separate step if we aren't sufficiently adept-exchange the mechanical symbols for the corresponding electrical ones.

If you are new to all this, not having read the last instalment, you may have found its condensation into a single paragraph rather bewildering. If so, a simple example should make it clearer. We might at the same time make some progress towards the practical side by working in numerical values.

Fig. 1, then, shows a mechanical system consisting of two springs with a frictional damper across one of them. When the springs are tested separately, a 1 -kg. weight (about $2 \frac{1}{4} \mathrm{lbs}$.) compresses $\mathrm{C}_{\mathrm{M1}} 0.4 \mathrm{~cm}$. and $\mathrm{C}_{\mathrm{M} 2} 2.15 \mathrm{~cm}$. The same force applied between the ends of the damper arms makes the distance between them change steadily at $3.3 \mathrm{~cm} / \mathrm{sec}$. We shall assume that this velocity varies exactly in proportion to the applied force. (In practice it probably wouldn't, but we don't want to involve ourselves in non-linear resistances right at the start.) The masses of these parts are supposed to be negligible. We can now calculate the compliances and mechanical resistance, and if we do so in m.k.s. units they will be in mechanical farads and ohms, which will at least make us feel partly at home straight away. Capacitance is equal to charge/voltage, so compliance is displacement/force; and mechanical resistance is force/velocity. The m.k.s. unit of force is the newton, which is enough to give a mass of 1 kg . an acceleration of $1 \mathrm{metre} / \mathrm{sec} .{ }^{2}$. The force of gravity at sea-level gives a mass of 1 kg . an accelera-

[^11]tion of $9.81 \mathrm{~m} / \mathrm{s}^{2}$ (" $g$ "), so 1 kg . weight is equal to 9.81 newtons. Therefore
\[

$$
\begin{aligned}
\mathrm{C}_{\mathrm{M} 1} & =\frac{0.004}{9.81}=0.00041 \text { mech. farad }=410 \text { mech. } \mu \mathrm{F} \\
\mathrm{C}_{\mathrm{M} 2} & =\frac{0.0215}{9.81}=0.0022 \text { mech. farad }=2,200 \text { mech } . \mu \mathrm{F} \\
\mathrm{R}_{\mathrm{M}} & =\frac{9.81}{0.033}=300 \text { mech. ohms. }
\end{aligned}
$$
\]

With such a simple arrangement there is really no need to draw a separate diagram to show the " circuit "; the only thing to remember is that in order to impart the force $F$ to the springs the source of the force must be rigidly attached to the framework or " earth" to which the bottom spring is anchored. So we have to imagine, if we don't dot in, this completion of the circuit.

There should be no difficulty in arriving in one stride at the equivalent electrical circuit. Capacitances take the place of compliances, and resistance the place of mechanical resistance. $C_{m 1}$ being (visually) in series with F and the combination of $\mathrm{C}_{M_{2}}$ and $\mathrm{R}_{\mathrm{M}}$, its analogue $\mathrm{C}_{1}$ in Fig. 2 must be in parallel with them. And the analogues of the parallel pair $\mathrm{C}_{\mathrm{M} 2}$ and $\mathrm{R}_{M 1}$ appear in series with one another. The translation into electrical units consists simply in deleting the prefix " mechanical."

Note that frequency hasn't come into this at all. So Fig. 2 should be valid for any waveform. But we must not forget that such conclusions are true only so far as our assumptions are true. For instance, we neglected the mechanical masses entirely. While that might be justifiable at very low frequencies, it could hardly be so at high. A rough way of deciding whether it was significant or not would be to suppose that something of the order of half the total mass was concentrated at the junction of the three mechanical elements. This, being subjected to the same velocity as $\mathrm{C}_{\mathrm{M} 2}$ and $\mathrm{R}_{\mathrm{M}}$, would appear in Fig. 2 as an inductance of 1 henry per kg. in the $\mathrm{C}_{2} \mathrm{R}$ branch. The resonant frequency of this branch could then easily be calculated.

Confining ourselves to the simple Fig. 2, we can find the frequency at which the impedance of $\mathrm{C}_{2}$ equals that of $R$ :

$$
\therefore f=\frac{1}{2 \pi} \frac{1}{2 \pi f \mathrm{C}_{2}}=\mathbf{R}, \frac{1}{2 \pi \times 0.0022 \times 300}=0.24 \mathrm{c} / \mathrm{s}
$$

At this frequency, the impedance of $C_{1}$ would be several times greater than that of $\mathrm{C}_{2}$ and R combined, so would take that much less


Fig. 3. Inverse electrical analogue of Fig. 1 and dual of Fig. 2.
being important) the impedance of $\mathrm{C}_{\mathrm{M} 1}$ is relatively low, so it flexes most.

If the exercise is confined to paper, the question of rate of exchange between mechanical and electrical quantities need hardly arise. So far we have made it one-to-one in every case, and because we have worked in a single system of units throughout (m.k.s.) we can be sure the analogy can be relied upon throughout. For instance, the amount of power needed to make a point on the machine vibrate with an r.m.s. velocity of $0.01 \mathrm{~m} / \mathrm{s}$ would be the same as that needed to make 0.01 amp r.m.s. flow through the corresponding part of the circuit at the same frequency.

With mechanical systems complicated enough to make this sort of study worth while, however-and expecially when distributed masses, etc., are involved -it may be more convenient to measure the performance of the electrical circuit than to calculate it. If so, you may ask, why not measure the performance of the mechanical system direct and save all the trouble of translation? The answer is that it is usually easier and more accurate to measure electrically, and much easier to vary circuit quantities continuously during test than machine quantities.

When it comes to building actual electrical models, the $1: 1$ scale may be awkward. We may not have a $2,200 \mu \mathrm{~F}$ fixed capacitor, for example; much less a variable one for trying other values. The solution is to use some other scale, but we must take care to keep it consistent.

We can decide to represent a velocity of 1 metre/sec by $a$ amps, and a force of 1 newton by $b$ volts. That is to say

$$
\begin{array}{r}
\mathrm{I}=a \text { and } \frac{\mathrm{E}}{\mathrm{~F}}=b \quad \ldots \\
\text { Therefore } \quad \frac{\mathrm{R}}{\mathrm{R}_{\mathrm{M}}}=\frac{\mathrm{E}}{\mathrm{I}} \cdot \frac{\mathrm{~V}}{\mathrm{~F}}=\frac{b}{a} \quad \ldots \tag{2}
\end{array}
$$

and similarly for impedance and reactance. So, as inductive reactance is proportional to inductance and mass reactance to mass,

$$
\begin{equation*}
\frac{\mathrm{L}}{\mathrm{M}}=\frac{b}{a} \tag{3}
\end{equation*}
$$

and inversely

$$
\begin{equation*}
\frac{\mathrm{C}}{\mathrm{C}_{\mathrm{M}}}=\frac{a}{b} \tag{4}
\end{equation*}
$$

Frequency of resonance is proportional to $1 / \sqrt{\text { LC }}$ and therefore to $1 / \sqrt{M C}_{M}$, so the analogue works in " real time."

Power is proportional to EI and FV, and

$$
\begin{equation*}
\frac{\mathrm{EI}}{\mathrm{FV}}=a b \tag{5}
\end{equation*}
$$

so 1 mechanical watt is represented by $a b$ electrical watts, and the same for energy. If you want watts to be the same size in both domains, you must choose $b=1 / a$.

If it would suit us to make $\mathrm{C}_{2}$ in Fig. $22.2 \mu \mathrm{~F}$, then from eqn. (4) $b / a=1,000$, and if we make $b=1 / a$ we have $b^{2}=1 / a^{2}=1,000$. Substituting these in eqns (1)-(5) we find our scale factors to be:

1 newton is represented by $\sqrt{1000}$ volts
1 metre $/ \mathrm{sec}$ is represented by $1 / \sqrt{1000} \mathrm{amp}$.
1 mech. watt ", " 1 electrical watt
1 mech. c/s $\quad " \quad " \quad 1$ electrical $\mathrm{c} / \mathrm{s}$
1 mech. ohm ", ", 1000 electrical ohms
1 kg . mass
" ", 1000 henries
1 mech. farad ", ", by 0.001 farad


Fig. 4. Use of an ideal 1:I transformer (PS) to enable a circuit to be drown without crossing wires. This brings such exceptional circuits within the scope of the rules for drawing dual circuits.

It would be advisable to make a table like this whenever the model is not life-size throughout.

Having (let me optimistically assume) made the effort of mastering this electromechanical analogy chiefly for the sake of avoiding the sweat of learning mechanics, making double use instead of our knowledge of electrical circuits, you may feel very strongly that it is superfluous, not to say positively confusing, to add to it another type of analogy in which everything is upside down and clean contrary to all our technical upbringing. If you add " and common sense" I can hardly blame you, as that was how I used to feel. Now, as Bloch's latest disciple, I am going to try to put across what I was at first extremely, rcluctant to buy from him, narr ely the " inverse", analogy (which is the same as the " mobility" analogy invented by F. A. Firestone in 1933). I fear I lack the masterly salesmanship with which he converted my hostility into enthusiasm, but here goes.
In the inverse analogy, force is represented by current and velocity by voltage. I need hardly explain that this necessitates everything else being upside down; mass is represented by capacitance, compliance by inductance, mechanical resistance by conductance, mechanical impedance by electrical admittance, etc. It follows that co-resistive mechanical arrangement is represented by co-yielding electrical arrang $\epsilon m \geq n t$. In fact, the inverse electrical analogue is the "dual" of the direct electrical analogue. And if you don't know what "dual " means in this context and haven't got last month's Wireless World or "Second Thoughts on Radio Theory" (Chap. 35) handy for looking up, it means the whole upside-down relationship between the two electrical analogues of any mechanical system.
Before you say rash things about not listening a moment longer to such nonsense as making voltage analogous to velocity and inductance to compliance, may I point out that in the first case they both begin with a " v " and in the second both are shown in diagrams as a curl. Small points, but quite useful for a taxed brain to hang on to.

More important is the fact that in translating from mechanical to electrical circuit diagram the arrangement is the same-there is no interchanging of series and parallel, which can be quite tricky with complicated systems. The translation of symbols is relatively easy, especially as they are much more like one another than in the inverse analogy. Thus instead of Fig., 2 to represent Fig. 1 we would have Fig. 3. (" G " is the symbol for conductance.)

So far, then, all is well. The disdavantage is that when one comes to study the mechanical behaviour on a basis of familiarity with circuit behaviour, one's familiarity is found to be of the wrong kind. It may
be hard at first to interpret the increase in voltage across $L_{1}$ with rise in frequency as an increase in vibrational velocity of the upper spring in Fig. 1. But a little practice soon gets one into the way of it. If it doesn't, there is always the alternative of converting Fig. 3 into its complete electrical dual, as explained last month. The result is Fig. 2.

When Bloch advocated the inverse analogy he did so with the argument that just as in some situations a current can be regarded as the cause of a voltage (e.g., in the anode circuit of a line-scan pentode) so a velocity can be regarded as the cause of a force. While this is quite true, it seems to me that the question of cause and effect confuses the issue of direct versus inverse analogies. As we have just seen, it is possible to use either, according to one's whim, without any interchange of cause and effect.

But I am particularly grateful to him for unconsciously putting the finishing touch to the system of vector diagrams I praised so conceitedly only a month or two ago. Hitherto I had to admit one little flawthat as regards current vectors it broke down if the circuit diagram couldn't be drawn without crossing wires. Actually there are very few practical circuits, for which one might want to draw vector diagrams, where this difficulty arises. I have never come across any, but the possibility irked me. The same difficulty occurs when drawing the dual of such a circuit, as one may want to do when changing over between inverse and direct analogies. Bloch showed that this difficulty can be overcome by bringing in an ideal 1:1 transformer.

One of the "impossible" circuits, though not

Fig. 5. Diagram of a simple lever. One of the forces $F_{1}$ - $F_{3}$ represents the support given by the fulcrum.

of much interest to most of us, is a 3-phase source connected to two loads, Fig. 4. There is always one lead that can't be run without crossing; in this case, the one from 3 to 9 . But there is no rule against an invisible magnetic field crossing, so the transformer PS solves the problem. This enables a vector diagram to be drawn according to my rules (Wireless World, August 1954, p.383), and enables the dual circuit diagram to be drawn according to the rules given last month.
Some things still remain to be said in favour of the inverse analogy, and as space is running out I won't go into detail again about units and scale factors for it; the principles are the same as for the direct analogy.
One much-used mechanical component which I have held back until now is the lever, because (notwithstanding what Dr. Bloch seems to say to the contrary) it needs the inverse analogy to link it with its electrical counterpart-the transformer. Ideally, a lever is perfectly rigid and without mass, so is incapable of storing mechanical energy in itself, and it has a frictionless fulcrum, so dissipates no energy. What it does do is vary the ratio of force to velocity (mechanical impedance), gaining say force at the expense of velocity. In the same way, an ideal transformer stores and dissipates no energy, but changes the voltage/current ratio.

A lever must have at least three forces acting on it, as for example in Fig. 5. The sum of the three
$\left(F_{1}+F_{2}+F_{3}\right)$ must be zero, otherwise it would go flying off. Also to conform to the ideal conditions mentioned, the total power going into it ( $F_{1} V_{1}+$ $\mathrm{F}_{2} \mathrm{~V}_{2}+\mathrm{F}_{3} \mathrm{~V}_{3}$ ) must be zero. Finally, and obviously the angular velocity $\frac{(\mathrm{d} \phi)}{\mathrm{d} t}$ of both parts of it $\left(d_{12}\right.$ and $d_{23}$ ) must be the same:

$$
\frac{\mathrm{d} \phi}{\mathrm{~d} t}=\frac{\mathrm{V}_{1}-\mathrm{V}_{2}}{d_{12}}=\frac{\mathrm{V}_{2}-\mathrm{V}_{3}}{d_{23}}
$$

Compare this with an auto-transformer, Fig. 6. The clearest analogue of lever length is number of turns, N. To this, voltage is proportional. Voltage per turn is proportional to the rate at which the magnetic flux in the core (also denoted by $\phi$ ) is changing:

$$
\frac{\mathrm{d} \phi}{\mathrm{~d} t}=\frac{\mathrm{E}_{1}-\mathrm{E}_{2}}{\mathrm{~N}_{12}}=\frac{\mathrm{E}_{2}-\mathbf{E}_{3}}{\mathrm{~N}_{23}}
$$

So voltage is analogous to velocity. This fits the other conditions too. Suppose $\mathrm{F}_{3}$ in Fig. 5 is an upward (positive) force of 10 kg ., and the lever is hinged at the $F_{1}$ end. Then, if $d_{23}=2 d_{12}, F_{3}$ can lift 30 kg . at $\mathrm{F}_{2}$ (which is therefore negative). To balance these two, the upward pressure $\mathrm{F}_{1}$ must be 20 kg . If forces were represented by voltages, as in the direct analogy, the transformer figures would be wrong. But if force is analogous to current we

have as the first condition $\mathrm{I}_{1}+\mathrm{I}_{2}+\mathrm{I}_{3}=0$, which is true. The second condition would be true either way.
Our interest in all this is likely to be in connection with " transducers" which are partly electrical and partly mechanical, such as loudspeakers, microphones, pickups, motors, and relays. In early treatises, separate circuit diagrams were shown for the electrical and mechanical portions of these. The reaction of the mechanical portion on the electrical circuit was represented in the electrical circuit diagram as a single element called " motional impedance ". One can go further than this, however, and make a single circuit diagram in which all the mechanical elements are separately represented along with the purely electrical. The thing can then be studied as a whole.
You will probably foresee that in order to do this we must accept some restrictions on choice of scale factors. Otherwise the mechanical and electrical portions won't join up properly. For one thing, the law of conservation of energy must be observed. It may be less obvious that there is no longer freedom to choose between the direct an inverse analogies. Bloch deals with this, but unfortunately I couldn't follow his proof and had to satisfy myself on the following lines.
Suppose first we have a device, such as a movingcoil loudspeaker, in which the cause of the mechanical force on a wire is the reaction of a magnetic field on current flowing through the wire. (This is sometimes known as the electric motor effect.) Assuming the wire carrying current I is at right angles to the field of flux density $B$, and the length of the wire is $l$, the fundamental equation is:

$$
\begin{equation*}
\mathrm{F}=\mathrm{B} l \mathrm{I} . \tag{6}
\end{equation*}
$$

If the wire is free to move, this force will move it
and cause an e.m.f. to be generated in it (dynamo effect):

$$
\begin{equation*}
\mathrm{E}=\mathrm{B} / \mathrm{V} \tag{7}
\end{equation*}
$$ where V is the velocity of the wire, assumed to be at right angles to the field and current.

If the electrical impedance of the wire is either negligible or separately represented, its only impedance is due to the back e.m.f. generated by its motion, so is called the motional impedance, $\mathrm{Z}_{\mathrm{EM}}$ It can be derived from equations (6) and (7):

$$
Z_{\mathrm{FM}}=\frac{\mathrm{E}}{\mathrm{I}}=(\mathrm{B} l)^{2} \frac{\mathrm{~V}}{\mathrm{~F}}
$$

(B $l)^{2}$ is a constant, and force/velocity ( $\mathrm{F} / \mathrm{V}$ ) is a mechanical impedance-in this case the mechanical impedance of the wire and all that moves with it. So the electrical impedance is inversely proportional to the mechanical impedance, and consequently we are bound to use the inverse analogy. And the scale factor is also fixed for us-(B $l)^{2}$.

The same result, except for the details of the constant, emerges from corresponding calculations of other magnetic types of electromechanical transducer.

But now compare the electrostatic type. (I don't like the term "electrostatic" for something that moves, but it will probably be better understood than just "electric".) Suppose we have a pair of parallel plates, each of area A, separated by a dielectric of thickness $d$ and permittivity $\epsilon$, and supplied with a fixed polarizing voltage $\mathrm{E}_{0}$. Then if E is a relatively very small "signal" voltage, the force caused by it can be shown to be

$$
\begin{equation*}
\mathrm{F}=\frac{\mathrm{E}_{0} \in \mathrm{AE}}{d^{2}} . \tag{8}
\end{equation*}
$$

If free to move as a result of this incremental force, with velocity $V$, the capacitance will vary. If at the same time $\mathrm{E}_{0}$ is kept constant, the charge must vary, giving rise to a current

$$
\begin{equation*}
\mathbf{I}=\frac{\mathbf{E}_{\mathbf{0}} \in \mathrm{AV}}{d} \tag{9}
\end{equation*}
$$

Deriving the motional impedance from (8) and (9) we get

$$
Z_{\mathrm{S} M}=\frac{\mathrm{E}}{\mathrm{I}}=\left(\frac{d^{2}}{\mathrm{E}_{0} \in \mathrm{~A}}\right)^{2} \frac{\mathrm{~F}}{\mathrm{~V}}
$$

so it is directly proportional to the mechanical impedance, and we must use the direct analogy, and of course the scale factor specified.

This, of course, is only the beginning of the subject. So far it has been idealized to make the basic principles clear. Extending the thing to distributed masses, etc., is more or less routine stuff, like extending r.f. theory to microwaves.

Since writing these two articles I have had my attention drawn to "Notes on Electro-Mechanical Equivalents" by H. Jefferson in Wireless Engineer, December 1944. He deals throughout with both "direct" and "inverse" analogies, which he calls " $b$-equivalent" and " $a$-equivalent" respectively; and shows that the "wrong " equivalent can be made to fit a lever or an electro-mechanical transducer by use of an " inverting transformer" with a ratio of $1: \sqrt{ }-n^{2}$. While this is mathematically feasible, it does rather spoil one main purpose of these analogies -to assist easy visualization-and he naturally recommends the other equivalents.

# MIDCETS AND FIDGETS 

## -Or Biiocals Anyone?

By JACK DARR^

1MONG the many unpleasantnesses the American radio-TV repairmen have to put up with is the increasing tendency of the setmakers toward miniaturization of their products. These gentry are evidently firmly convinced of the truth of the old saw about "Good Things Coming In Small Packages!". While this might conceivably be quite useful in the small transistor portable radio field, where we have already seen a 4-transistor set reduced to the size of a packet of cigarettes, to fit into the shirt pocket, it can lead to uncounted confusion in others! Not too much trouble is encountered, always providing you have a good supply of very high-powered jeweller's loupes, a soldering-iron with a very small bit, and immeasurably good eyesight. (If you do, cherish it: it won't last long!)
The poets sigh for "the halycon days of yore. So, too, do some of us "old gaffers" who remember the radio business "away back when." In this instance the phrase refers to the early 1930s, when the radio business was only beginning to grow into the giant of today. This was the period which saw the biggest home radios ever built. Housed in cabinets faintly reminiscent of grand pianos, in both size and construction, they were filled with masses of chasses (Sorry! Shan't do it again) which were separate power supplies, audio amplifiers, tuners, and so on.
This decade also witnessed the birth of the first "midget" radio. This happy event took place about 1931, with the advent of the Model 6 "Echophone." It was about $12 \times 14$ inches, and about 15 inches high. It had a round-topped cabinet of veneer plywood, a 6 -valve circuit, and was famed far and wide as being the only radio set made that one could pick up with only one hand! These sold like hot cakes, and soon every major manufacturer had his finger in the pie, making "midgets."

The classic example was the original Majestic Company (Grigsby-Grunow) who built the immortal Model 50. This was classified as a midget, although there were many who expressed doubt as to the validity of the classification. It was about the same size as the "Echophone," although a bit taller, rather square-topped, with a sort of Corrupt Gothic pilaster effect on the front of the cabinet. Its principal feature, though, was its weight. This hefty little giant was so heavy that servicemen with ordinary sized feet often found themselves sinking hock-deep into lawns, and asphalt paving in midsummer, while attempting to carry it to their trucks! The cabinet, while not too large, was reputed to be filled with solid iron. This was a base canard; there were a few air-spaces left here and there, albeit not too many! The heft was accounted for by some of the design practices common to that period; massive mains transformers, input and output transformers, and a 10 -inch electrodynamic loudspeaker with a tremendous field coil furnished a goodly share of it. A large cast-iron-framed tuning condenser and
large components did the rest. Even the i.f. transformers were about 2 inches square, 3 high, and filled solidly with tar! True! Each i.f. can weighed about two pounds! Incidentally, these were not tunable!
For a final touch, these sets were sold with a "matching table," to which they were somewhat insecurely fastened. This consisted of a heavy framework ( $1 \times 2$-in lumber!) at the top, and slender, tapered legs; from a scant inch at the top, they wound up less than a half-inch diameter at the bottom! Much to our surprise these tables, despite their decidedly unsafe appearance, never collapsed under their tremendous load. Of course, we did find, now and then, the tiny ends of the legs sunk completely through the lino, or into a soft pine floor, but somehow or other they never did quite completely let go, like the proverbial One-Hoss Shay.
Modern science has once again leaped into the breach, though. From "midgets" that were so heavy we couldn't lift 'em, they have given us radios that are so tiny we can't see 'em! The customer now comes into the shop, saying, "Can you fix my radio?" Upon receiving an affirmative reply (although with certain unspoken reservations), he begins frantically searching his person. Claiming that he certainly had it when he left home, he finally digs it out of his shirt pocket, where it has gone to earth behind a packet of Pall Malls. The difficulty, of course, is occasioned by the fact that the radio is smaller than the fags!

## The Tool Kit

Our brave technician gingerly accepts it, turns on a very bright light over his bench, and rounds up a group of tools filched from local jewellers, surgeons, and the like: tiny tweezers, hæmostats, picks, screwdrivers, and that essential appendage, a jeweller's loupe of at least four power. Screwing this firmly into his eye, he at last attacks the plastic case. Opening this, he discloses a mess of miniaturized components which would be far more at home in the nose of a proximity-fused anti-aircraft shell. (This is where most of them came from, and at the moment he fervently wishes they were back!) At one end is a wee battery. Hopefully, he measures its voltage, in the faint thought that it might be low. No luck; he must work on the thing!

Printed circuits? Oh, definitely, old boy. There isn't room inside the thing for a normal wire! One couldn't close the case! By cleverly mounting all the transistors and parts on one side of the board, and printing the wiring on the other, the designer has managed to render the gadget almost immune from normal maintenance: procedures. However, our braw laddie removes a few minute screws, about the size of those securing the balance-staff in a

[^12]medium-sized pocket-watch, and gets the thing out into the light. Now, by holding it up between his eyes and the powerful light, he can sce througin the translucent board. (In the process, he also manages to acquire a mild sunburn on the tip of his nose from the actinic rays, but this is quite incidental.)

A standard test-prod looks rather like a telegraph pole beside the space available for insertion of same. By contrast, the older radios and TV sets had enough space to park a good-sized lorry between components! Nevertheless, Our Hero finally manages to pick up a voltage here, a resistance reading there, and, after a while, he locates the trouble: it is, as usual, a minuscule break in the printed wiring. (Due, no doubt, to the mistress dropping it off the dresser the night before, or bunging it at the master's head!) Flowing solder over this with his special needle-nose bit, it works! He reassembles it and hands it back to the customer, who, as is customary in such cases, has left his wallet in his other coat. Now, in America, would be the ideal time for a coffee break (a "cuppa" in England?).

We were getting by with these Minute Marvels until the setmakers decided that too much of a good thing was not enough, and began their shrinking techniques upon TV receivers! Now, the average TV set, even some of our mail-order marvels, need quite a few more parts than a 4 -transistor radio. Still, these electronic Jivaros seem to be making an earnest effort to cram all of them into a space of about the same size! This has some quite ridiculous results, at times. Upon opening the back of a modern portable TV, which by this time measures some eight inches in depth, one finds a wee blobby object sticking out in the centre: this is the neck of the picture tube. Upon a perfectly flat wall of glass is apparently pasted some peculiar-looking coils, etc.: these comprise the deflection yoke! Upon looking up the spec's for the picture tube, he finds that it has a deflection angle of 110 degrees! Wondering how long it will be until someone succeeds in making tubes with deflection angles greater than 180 degrees, so that the tubes could be built in the shape of inverted ice-cream cones, he begins to look for the chassis. Here the words "look for" are used advisedly. Of the chassis as we knew it, there ain't no such no more. Scattered here and there about the case are odd bits of metal, with valves sticking out at odd angles. A few resistors and capacitors may be seen, and from this evidence, he deduces that this weird assembly is intended to be "the works".

The printed circuits, which were the subject of an earlier diatribe**, abound in these little monsters. Because of their space-saving characteristics, they have been seized upon with glee by the sadists who are in charge of Design. In some cases, they have been cleverly arranged in the form of a box, enclosing the picture tube. This enables the designer to enclose almost totally all parts and valves (Oh, didn't I tell you? The valves are on the inside of the box, with their sockets indecently exposed on the outside!) rendering the whole thing something like $89 \%$ inaccessible for normal maintenance work! The edges of the PC boards comprising the major part of the assembly are firmly tied together by the wiring and interconnecting leads. To get it out of

[^13]the "box" so that it can be checked, it is necessary to spend at least half an hour totally disabling the set, by disconnecting the major part of these. Of course, if the technician has unlimited time on his hands, he may make the set operative in this odd condition by reconnecting the edges with scraps of flex, test leads, etc. This, of course, induces some strange and wonderful feedback lops, aiding no end in the diagnosis of the original defect!

Be that as it may, we are learning to live with them, in a resigned sort of way. Patience and fortitude can do wonders when applied to such instances. Really, some of the PC boards are not too difficult to work on, provided the maker has not rendered things too hard, by concealing one side of the board completely with a heavy steel plate, as has been the case in some recent models. Practice will do wonders!

As to radios, one never knows what will come up next. With hearing-aids fitted into the bows of a pair of eyeglasses, one can scarcely blame the unfortunate technician involved in this incident. A customer came into the shop, and said, "Could you fix my radio?" Upon receiving the usual affirmative answer, he began trying to remove a large ornate ring from his finger. The technician turned, saw this, and swooned! When revived, the customer explained that he only wanted one of the prongs of the ring resoldered: the radio was still out in his car! The technician, remembering the article he had just read about future trends in micro-miniaturization, had been under a completely wrong impression!


This crystal-pulling furnace is mode by Nash and Thompson, Ltd., Chessington, Surrey, to the design of the Services Electronics Research Laboratory, Baldock. The temperature of the molten semiconductor material in the crucible, which is heated by a graphite element, is judged by looking into the vocuum chamber (left) at the liquid surfoce. The meniscus formed is an extremely sensitive indicator as it depends on surface tension which changes widely with temperoture near the melting point of the moterial. The equipment rack contains the pumps, instrumentation and control apparatus for the heater and pulling motors.

# Loudspeaker Magnet Design 

## With Special Reference to Capped Cylindrical Slugs of

Alcomax III<br>By A. E. FALKUS ${ }^{\star}$, b.Sc. (Eng), M.I.E.E.

THE development of a process for making production quantities of Alcomax magnets with a semi-columnar structure has placed in the hands of loudspeaker designers a material which, while having a better performance than any used hitherto, yet has certain limitations of shape.
The figure of merit of a permanent magnet material is the maximum value of the product BH , where B is the flux density in the magnet and $H$ the magnetomotive force per unit of length that the magnet can exert when carrying B in a magnetic circuit. The BH (Max.) value for semicolumnar Alcomax III is 5.8 mega-gauss-oersteds whereas for normal cast Alcomax III the value is 5 . Thus the process whereby longitudinal crystal growth, i.e., semi-columnar structure, is induced increases the performance of a given weight of alloy by $16 \%$ for a small extra process cost.

There is, however, a limitation on the shape of the magnet in that the semi-columnar structure can only be obtained when the magnet consists of a solid cylinder.

However, this feature of semi-columnar material, the limitation of the shape to a plain cylinder,


Fig. 1 Dimensions and stray fields in the capped cylindrical-slug magnet design.
leads to a simplified method of design. It will be shown later that for a given load (i.e., mass of cone to be driven) a given input impedance, and given weight of magnetic alloy, there is one optimum value for the pole diameter and depth of gap.

Although semi-columnar Alcomax III is the magnet material considered, the design methods suggested can be applied to any magnet material by using the appropriate values of the magnetic constants.
Basic Design. - The best basic design for a loudspeaker magnet of semi-columnar material is that of a capped slug. The magnet consists of a cylindrical slug of a diameter equal to the inside diameter of the voice coil less the working clearances. This slug is capped by a disc of mild steel which forms the pole piece. This disc is of the same diameter as the magnet and of a thickness equal to the desired depth of air gap.

The design is shown diagrammatically in Fig. 1, where the magnet slug has a diameter D and length L. It is capped by a disc of mild steel also of dia-

[^14]meter D and thickness T . The radia' width of the air gap is G.

Since the magnet slug may not have a central hole, it is best fixed to the yoke and pole piece by some form of adhesive, such as Araldite, which will provide a satisfactory bond.

The capped slug design is well known as an efficient design for small sizes of magnet. It will be shown that it may be used for any weight of magnet and, when the proportions are correct, will give high magnetic efficiencies.
Gap Flux.- To design a loudspeaker magnet satisfactorily it is necessary to be able to calculate what proportion of the total flux carried by the magnet passes usefully through the air gap and what proportion leaks across above and below the gap.

Referring to Fig. 1 and assuming that the magnet is working at its BH (Max.) point, the magnetomotive force across the gap, neglecting losses in the yoke, will be LH. The flux density in the air gap will therefore be LH/G. Now the gap cross-sectional area is $\pi \mathrm{DT}$.
The total useful gap flux is therefore $\mathrm{LH} \pi \mathrm{DT} / \mathrm{G}$ (1) Leakage Flux.- The leakage flux is also driven by the magnetomotive force LH. The total admittance of the leakage paths will be proportional to a factor which depends on the configuration of the magnet, multiplied by the circumference of the pole piece. That is, the total leakage flux may be expressed as $\mathrm{LHC} \pi \mathrm{D}$.

The factor C will be constant for all capped slug designs. Measurements of a number of different capped slug magnet designs all give a value for C of 3.5 when $L$ and $D$ are measured in cm and H in gauss.
The total leakage flux is therefore $3.5 \mathrm{LH} \pi \mathrm{D}$. . (2)
It should be noted that the value for C of 3.5 takes into account only the leakage flux in the vicinity of the gap.

The top leakage between the flat end face of the pole picce and the front plate near the gap will be a constant for a given pole diameter and a given magnetomotive force across the gap. It will be the same for all types of magnet construction, i.e., capped slug, skirted pole piece, ring magnet, etc. It will be a little greater where the front plate is chamfered down in thickness at the gap so that the leakage surfaces are at less than $180^{\circ}$ to each other. In general, however, the effect of a chamfer may be neglected.

The internal leakage between the cylindrical surface of the pole piece or magnet below the gap and the under side of the front plate will always be greater than the top leakage because the average leakage path is approximately halved as the surfaces are only at $90^{\circ}$ to each other. In the case of the capped slug design, however, the leakage falls off rapidly with increasing distance from the gap. This is
because not only is the leakage path increasing, but the magnetomotive force operating is decreasing because the flux is coming from a point below the top of the magnet.
In the case of the skirted pole piece construction of Fig. 2, the magnetomotive force driving the internal leakage increases with increasing distance below the gap due to the drop of magnetomotive potential


Fig. 2 Skirted pole piece magnet construction showing stray fields.
in the cylindrical portion of the pole piece which is usually working near saturation point. Further, the conical surface of the skirt, which is running nearly parallel to the under side of the front plate, adds considerably to the total leakage. The leakage factor C will thus be considerably greater than 3.5 for this design and will also depend on the ratio of the skirt diameter to the pole diameter and on the length of the nearly parallel portion of the pole piece.
Magnetic Efficiency.-The ratio of useful gap flux to leakage flux may be found from equations (1) and (2) as:

$$
\begin{equation*}
\frac{\mathrm{LH} \pi \mathrm{DT} / \mathrm{G}}{3.5 \mathrm{LH} \pi \mathrm{D}} \tag{3}
\end{equation*}
$$

This simplifies to $\mathrm{T} / 3.5 \mathrm{G}$
It is interesting to note that the ratio of gap flux to leakage flux is directly proportional to the depth of the air gap and inversely proportional to its width.

The magnetic efficiency of a loudspeaker magnet system may be defined as the percentage of the total flux supplied by the magnet which passes usefully through the air gap. This may be written as:

$$
\frac{\text { Gap flux }}{\text { Gap flux }+ \text { Leakage flux }} \times 100 \%
$$

From equations (1) and (2) this becomes:

$$
\frac{\mathrm{LH} \pi \mathrm{DT} / \mathrm{G}}{\mathrm{LH} \pi \mathrm{DT} / \mathrm{G}+3.5 \mathrm{LH} \pi \mathrm{D}} \times 100 \%
$$

This simplifies to

$$
\begin{equation*}
\frac{\mathrm{T}}{\mathrm{~T}+3.5 \mathrm{G}} \times 100 \% \tag{4}
\end{equation*}
$$

Magnet Diameter.-The total flux in the magnet
is B times the cross sectional area, i.e., $\mathrm{B} \pi \mathrm{D}^{2} / 4$. This must equal the sum of the gap flux and leakage flux. Thus, from equations (1) and (2):-

$$
\mathrm{B}_{\pi} \mathrm{D}^{2} / 4=\mathrm{LH}_{\pi} \mathrm{DT} / \mathrm{G}+3.5 \mathrm{LH}_{\pi} \mathrm{D}
$$

Dividing out by $\pi \mathrm{D}$, this becomes:-
$\mathrm{BD} / 4=\mathrm{LHT} / \mathrm{G}+3.5 \mathrm{LH}$

$$
\text { Hence, } \begin{align*}
\mathrm{D} & =\frac{4 \mathrm{LHT}}{\mathrm{BG}}+\frac{14 \mathrm{LH}}{\mathrm{~B}} \\
& =\mathrm{L}\left(\frac{4 \mathrm{HT}}{\mathrm{BG}}+\frac{14 \mathrm{H}}{\mathrm{~B}}\right) \ldots \tag{5}
\end{align*}
$$

If the volume of the magnet slug is V , then:-
$\mathrm{V}=\pi \mathrm{D}^{2} \mathrm{~L} / 4$
Hence $\quad \mathrm{L}=4 \mathrm{~V} / \pi \mathrm{D}^{2}$
Substituting for L in equation (5) we have:-

$$
\mathrm{D}=\frac{4 \mathrm{~V}}{\pi \mathrm{D}^{2}}\left(\frac{4 \mathrm{HT}}{\mathrm{BG}}+\frac{14 \mathrm{H}}{\mathrm{~B}}\right)
$$

Multiplying out by $\mathrm{D}^{2}$ this becomes:-

$$
\begin{equation*}
D^{3}=\frac{4 \mathrm{~V}}{\pi}\left(\frac{4 \mathrm{HT}}{\mathrm{BG}}+\frac{14 \mathrm{H}}{\mathrm{~B}}\right) \tag{6}
\end{equation*}
$$

Air Gap Required to Accommodate the Voice Coil.-For optimum acoustic response, the voice coil weight must bear a certain relation to the weight of the cone that it drives.

The required impedance of the voice coil is determined by the matching load of the output circuit to which the speaker will be connected. Assuming the impedance to be $10 \%$ higher than the d.c. resistance, which it normally is over the middlefrequency range, the required d.c. resistance of the coil may be found.

Knowing the weight and resistance of the voice coil winding, the wire diameter and its total length can be found with the aid of standard wire tables. Let this diameter be $d$ and the total length of wire be $w$.

Then the number of turns in the coil will be $w / \pi \mathrm{D}$ and the total length of the winding, assuming two layers, will be $w d / 2 \pi \mathrm{D}$.

This neglects the slight increase of the coil diameter over the magnet diameter.

For maximum sensitivity, particularly where large excursions of the coil are not expected, the voice coil winding may be made equal in length to the depth of the air gap, i.e., $\mathrm{T}=w d / 2 \pi \mathrm{D}$.
Hence $\mathrm{D}=w d / 2 \pi \mathrm{~T}$
In the case of a speaker required to handle considerable power, particularly at low frequencies, the coil should be longer than the gap to reduce harmonic distortion at large amplitudes. In this case T will be less than the coil length by twice the over-hang and equation (7) must be modified accordingly.
Magnet Dimensions.-It will be seen from equations (6) and (7) that we have two expressions for

TABLE 1: Magnet Designs For Small Commercial Loudspeakers

| Weight of magnet | Diameter of pole and magnet |  | Depth of gap |  | Length of magnet |  | Flux density in gap | Magnetic efficiency |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| oz | cm | in | cm | in | cm | in | gauss | \% |
|  | 1.742 | 0.686 | 0.445 | 0.175 | 0.810 | 0.319 | 6,080 | 62.2 |
| 1 | 2.112 | 0.832 | 0.367 | 0.144 | 1.102 | 0.434 | 8,270 | 57.6 |
| 2 | 2.565 | 1.011 | 0.302 | 0.119 | 1.494 | 0.588 | 11,220 | 52.8 |
| 4 | 3.127 | 1.232 | 0.248 | 0.098 | 2.008 | 0.791 | 15,070 | 47.9 |

D in terms of T for a given volume of magnet material of known characteristics and a given cone and input impedance.

The gap width $G$ which occurs in equation (6) may be calculated as $2 d$ plus the thickness of the voice coil former plus twice the working clearance between voice coil and pole piece.
B and H for semi-columnar Alcomax III may be taken as 10,000 and 580 respectively when the magnet is working at its BH (max.) point. The specific gravity of Alcomax III may be taken as 7.35 . The value of V will therefore be its weight in gm divided by 7.35 .
By substituting numerical values for V, H, B, G, $w$, and $d$ in equations (6) and (7), we are left with two simultaneous equations involving D and T which may then be evaluated.
To illustrate the design methods outlined above, a range of designs have been worked out:-
(A) For a small commercial speaker which is to have maximum sensitivity for small power handling and magnet weights of $\frac{1}{2} \mathrm{oz}$ to 4 oz .
(B) For a 12 -in speaker to handle 20 W at low frequencies and with magnet weights of $\frac{1}{2} \mathrm{lb}$ to $1 \frac{1}{2} \mathrm{lb}$. These two series of speakers have been chosen as being near the extremes likely to be met in practice. Design of Small Commercial Speakers: Voice Coil.-It has become standard for this type of loudspeaker to have an input impedance of $3 \Omega$. The d.c. resistance of the voice coil may therefore be taken as $2.7 \Omega$.
Experience has shown that the average $5 \mathrm{in}, 6 \mathrm{in} \times$ 4 in , or 7 in $\times 4$ in cone requires a voice coil weight of about $\frac{1}{2} \mathrm{gm}$ to provide a good tonal balance.
From the standard wire tables we find that the wire gauge which most nearly meets this is 38 s.w.g. which has $2570 \Omega$ per lb; since $2.7 \Omega$ will weigh $2.7 \times 454 / 2570=0.48 \mathrm{gm}$.
Now, 38 s.w.g. copper wire has $864 \Omega$ per 1000 yd. The length for $2.7 \Omega$ is therefore $2.7 \times 1000 \times$ $91.4 / 864=286 \mathrm{~cm}=w$.
The overall diameter of 38 s.w.g. wire, enamelled, is $0.0067 \mathrm{in}=0.01703 \mathrm{~cm}=d$.

Substituting for $w$ and $d$ in equation (7), we have:-

$$
\begin{equation*}
\mathrm{D}=\frac{286 \times 0.01703}{2 \pi \mathrm{~T}}=\frac{0.775}{\mathrm{~T}} \tag{8}
\end{equation*}
$$

Magnet.-The values for $\mathbf{B}$ and H for semicolumnar Alcomax III are 10,000 and 580 respectively.

The voice coil wire diameter, $d$, is 0.0067 in . If we assume a thickness for the former of 0.003 in and gap clearances of 0.007 in , we arrive at a gap width G of $2 \times 0.0067+0.003+2 \times 0.007$ in $=0.0304$ in $=0.0772 \mathrm{~cm}$.

Substituting these values of $\mathrm{B}, \mathrm{H}$, and G in equation (6), we have:-

$$
\begin{align*}
\mathrm{D}^{3} & =1.273 \mathrm{~V}\left(\frac{4 \times 580 \mathrm{~T}}{10,000 \times 0.0772}+\frac{14 \times 580}{10,000}\right) \\
& =\mathrm{V}(3.83 \mathrm{~T}+1.034) \quad . \quad . . \quad(9) \tag{9}
\end{align*}
$$

Now, the specific gravity of Alcomax III is 7.35 and $10 z$ is equal to 28.4 gm . Then, if $W$ is the weight of the magnet slug in oz:-

$$
\mathrm{V}=\mathrm{W} \times 28.4 / 7.35=3.86 \mathrm{~W}
$$

Substituting this value of V in equation (9), we have:-

$$
\begin{equation*}
\mathrm{D}^{3}=3.86 \mathrm{~W}(3.83 \mathrm{~T}+1.034) . \tag{10}
\end{equation*}
$$

From equation (8) we have $T=0.775 / \mathrm{D}$. Substitut-
ing this value of $T$ in equation (10), we have:$\mathrm{D}^{3}=3.86 \mathrm{~W}(2.97 / \mathrm{D}+1.034)$
Multiplying both sides by D and simplifying, this becomes:-
$\mathrm{D}^{4}-3.99 \mathrm{WD}=11.44 \mathrm{~W}$
We may now insert any required value for $W$ in equation (11) and solve for D by trial and error.

When $D$ is known, the values of $T, L$, the gap flux density and the magnetic efficiency may be found from the various equations given previously.
These operations have been carried out for magnet weights of $\frac{1}{2}, 1,2$, and 4 oz and the results are given in Table 1. The dimensions are given in the table in inches as well as in centimetres.
It should be noted that in these calculations no allowance has been made for the magnetomotive force required to drive the flux through the iron circuit between the bottom of the magnet and the air gap. This may be allowed for by adopting a value for $\mathbf{H}$ some 5 or $10 \%$ less than that given by the magnet manufacturers.
In this country, there are no standard sizes for loudspeaker magnets and one weight of slug may be purchased as easily as another. It will therefore probably be preferred to make the pole diameter a standard size of steel rod for ease of production, rather than to have the magnet an exact number of ounces. For this reason curves are given in Fig. 3 showing pole diameter, gap depth, magnet length and gap flux density in terms of magnet weight. From these curves, for instance, it will be seen that a 1 -in pole may be used with a 1.95 oz magnet to give a flux density of 11,100 gauss in a gap of $0.120-\mathrm{in}$ depth.

The suggestion of using a $1-$ in. pole or larger for a small commercial speaker may seem strange at first. Provided a non-perforated dome is used for an internal dust cover, however, there will be no acoustic disadvantage. In fact, there is an improvement in response to be obtained by partially filling the apex of the cone. The gain in sensitivity and


Fig. 3 Magnet designs for small commercial loudspeakers showing diameter of pole, flux density in gap, length of magnet, and depth of gap in terms of weight of magnet.

TABLE 2: Magnet Designs for 12-in Low-frequency Loudspeakers

| Weight <br> of <br> magnet | Diameter of pole and <br> magnet | Depth of gap | Length of magnet | Flux density <br> in gap | Magnetic <br> efficiency |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| oz | cm | in | cm | in | cm | in | gauss |
|  |  |  |  |  |  |  |  |
| 8 | 4.663 | 1.837 | 0.872 | 0.343 | 1.786 | 0.703 | 9,050 |
| 16 | 5.500 | 2.165 | 0.644 | 0.253 | 2.598 | 1.023 | 13,180 |
| 32 | 6.478 | 2.505 | 0.452 | 0.178 | 3.748 | 1.477 | 19,000 |

reduction in overall depth of the speaker as compared with a skirted pole or ring magnet design for magnet weights of 2 or 3 oz is considerable.
Design of 12 -in Low-frequency Speakers:
Voice Coil.-For speakers for public address or high-fidelity reproduction it has become standard to use an input impedance of $15 \Omega$. For a speaker to be used as the bass unit of a multi-speaker combination the most important region is that part of the range below $100 \mathrm{c} / \mathrm{s}$ because, since the cone diameter is much smaller than the sound wavelength in air at the lowest frequencies, everything possible must be done to off-set the drop in radiation efficiency.

Below $100 \mathrm{c} / \mathrm{s}$ the impedance will depend on the method of loading and will be considerably more than the d.c. resistance, so that the best compromise is to make the voice coil 8 to $10 \Omega$ rather than $15 \Omega$ less $10 \%$. For this design we shall take $9 \Omega$.
Again, in order to obtain the best 'performance below $100 \mathrm{c} / \mathrm{s}$, it is best to use a voice-coil weight heavier in proportion to the cone than for a small general purpose speaker. For a 12 -in. bass speaker the best coil weight is 6 to 7 gm .
From the wire tables we find the nearest gauge is 35 s.w.g. of which $9 \Omega$ has a weight of 6.1 gm . This gauge has also $441 \Omega$ per $1,000 \mathrm{yd}$. The length for $9 \Omega$ is thus $1000 \times 91.4 \times 9 / 441=1840 \mathrm{~cm}=w$. The overall diameter of 35 s.w.g. enamelled wire is $0.0094 \mathrm{in}=0.0239 \mathrm{~cm} .=d$.

A speaker to have a good low-frequency perfor-


Fig. 4 Magnet designs for 12-in low-frequency loudspeakers showing diameter of pole, flux density in gap, length of magnet, and depth of gap in terms of weight of magnet.
mance must be capable of considerable voice-coil excursion without undue distortion due to the coil moving out of the gap. This is achieved by making the coil longer than the gap depth. For a 12 -in. speaker to be used primarily as a bass unit it is desirable for the coil to extend some $\frac{1}{8} \mathrm{in}$. above and below the gap. Thus the coil will not commence to leave the gap until the amplitude of movement exceeds $\frac{1}{4}$ in.
The gap depth may therefore be taken as $\frac{4}{}$ in or 0.625 cm less than the coil length. Thus

$$
\begin{align*}
\mathrm{T} & =w d / 2 \pi \mathrm{D}-0.625 . \\
\text { Whence } \mathrm{D} & =\frac{w d d}{2 \pi(\mathrm{~T}+0.625)} . \tag{12}
\end{align*}
$$

Substituting for $w$ and $d$ in equation (12), we have:-

$$
\begin{align*}
\mathrm{D} & =\frac{1840 \times 0.0239}{2 \pi(\mathrm{~T}+0.625)} \\
& =\frac{6.98}{\mathrm{~T}+0.625} \ldots \tag{13}
\end{align*}
$$

Magnet.-The voice coil wire diameter, $d$, $=0.0094 \mathrm{in}$. If we assume a thickness for the former of 0.0045 in and gap clearances of 0.011 in , we arrive at a gap width, $G$, of $2 \times 0.0094+0.0045+2 \times 0.011$ in $=0.045 \mathrm{in}=0.1143 \mathrm{~cm}$.
Substituting for $B, H$, and $G$ in equation (6) we have:-

$$
\begin{align*}
\mathrm{D}^{3} & =1.273 \mathrm{~V}\left(\frac{4 \times 580 \mathrm{~T}}{10,000 \times 0.1143}+\frac{14 \times 580}{10,000}\right) \\
& =\mathrm{V}(2.58 \mathrm{~T}+1.034) \tag{14}
\end{align*}
$$

Substituting 3.86 W for V we have:$\mathrm{D}^{3}=3.86 \mathrm{~W}(2.58 \mathrm{~T}+1.034)$
From equation (13), $T=6.98 / \mathrm{D}-0.625$
Substituting this value of $T$ in equation (14) we have:-

$$
\begin{aligned}
\mathrm{D}^{3} & =3.86 \mathrm{~W}(2.58[6.98 / \mathrm{D}-0.625]+1.034) \\
& =69.6 \mathrm{~W} / \mathrm{D}-2.24 \mathrm{~W}
\end{aligned}
$$

Thus $\mathrm{D}^{4}=69.6 \mathrm{~W}-2.24 \mathrm{WD}$
Or, $\mathrm{D}^{4}+2.24 \mathrm{WD}=69.6 \mathrm{~W}$
We may now insert various values for $W$ and solve for D . This has been done for magnet weights of $\frac{1}{2} \mathrm{lb}, 1 \mathrm{lb}$, and 2 lb and the various details of the design worked out. The figures are given in Table 2.
As for the previous examples, the results are presented graphically in Fig. 4.

In considering these designs, it must be remembered that one requirement was that the voice coil must extend for $\frac{1}{8}$-in above and below the gap. A result of this is that, as the pole diameter increases with increasing magnet weight, a smaller proportion of the coil is within the gap. For magnet weights above $1 \frac{1}{2} \mathrm{lb}$ therefore, it is considered that it would be better to increase the wire gauge and thus the length of wire for $9 \Omega$.

# Elements of Electronic Circuits 

9.-TRIGGERED TWO-STATE CIRCUITS

By J. M. PETERS, B.Sc. (Eng.), A.M.I.E.E., A.M.Brit.I.R.E.

THE freely running multivibrator, as described last month, can be locked on to an applied wave of fixed repetition frequency as shown in Fig. 1. Conditions for an asymmetrical multivibrator are illustrated here. The frequency of oscillation will


Fig. I.


Fig. 2.
increase until it becomes a multiple or a sub-multiple of the frequency of the injected signal.

Positive-going synchronizing pulses are applied to the grid of one valve of the circuit-say $\mathrm{V}_{1}$ in Fig. 1 of last month. Let us assume that the repetition frequency of these pulses is greater than that of the freely running multivibrator and let us consider a single pulse. It will be seen that when the pulse arrives at the grid of $V_{1}$ the potential of the grid, discharging to zero with time constant $\mathrm{C}_{2} \mathrm{R}_{3}$, has not quite reached the valve cut-off voltage. The application of the positive pulse carries it over this level, so accelerating the transition of $\mathrm{V}_{1}$ to its conducting state. In effect it causes $\mathrm{V}_{1}$ to conduct before it would have done under normal $\mathrm{C}_{2} \mathrm{R}_{3}$ discharging conditions (shown by the dotted line in Fig. 1). As each positive input pulse causes this to happen, the multivibrator becomes synchronized to the input wave.

Instead of making every synchronizing pulse trigger the multivibrator, it is possible to arrange for the circuit to be triggered by each $n^{\text {th }}$ pulse.

This will mean that the multivibrator frequency is then $\frac{1}{n}$ th of the input frequency. For example, an input with a repetition frequency of 500 pulses per second can cause the multivibrator to oscillate at 125 pulses per second by arranging for it to be triggered by every 4th pulse; this is shown in Fig. 2. Frequency division therefore takes place, and it is possible to make $n=10$ or more by careful choice of component values. It will be noted that the amplitude of the sync pulse will to a large extent govern the frequency of oscillation of the multivibrator.
In the example shown, only the duration of the positive portion of the anode voltage waveform is affected by the triggering action. If the duration of both positive and negative portions of the waveform are to be controlled, it will be necessary for both valves to be triggered. A convenient method is by applying negative trigger pulses between the common cathode and earth.
On account of the possibility of the multivibrator grid voltage changes reacting back on the source of sync voltage, it is often necessary to isolate the oscillator from the source by means of a buffer amplifier stage, as shown in Fig. 3. Sync amplitude can be controlled at the amplifier grid as indicated.
Fig. 4 shows a development of the basic multivibrator in which two pentodes, $\mathrm{V}_{1}$ and $\mathrm{V}_{2}$, are used instead of triodes, and a further refinement is the incorporation of a diode clamp $\mathrm{V}_{3}$.

From Fig. 5 we will assume that $V_{1}$ is conducting and $V_{2}$ is cut off. A negative sync pulse applied to the control grid of $\mathrm{V}_{1}$ becomes an amplified positive pulse on the control grid of $\mathrm{V}_{2}$, and $\mathrm{V}_{2}$ conducts. This results in a fall in voltage on $\mathrm{V}_{2}^{2}$ screen grid, which is transferred to the suppressor of $V_{1}$ by $C_{2}$. As $C_{2}$ discharges through $R_{3}$ and $V_{2}$, the $g_{3}$ of $V_{1}$ rises through the suppressor cut-off


Fig. 4.
voltage, causing anode current in $\mathrm{V}_{1}$ to flow again and the anode volts of $\mathrm{V}_{1}$ to fall. This fall in voltage is transferred to $V_{2}$ control grid by $C_{1}$, causing $V_{2}$ to be cut off. As $C_{1}$ discharges through $\mathrm{R}_{4}$ the voltage on $\mathrm{V}_{2}$ control grid rises through cut-off, $\mathrm{V}_{2}$ conducts again and the cycle continues on similar lines, as has been described previously.
It is important to note the advantages gained by making the circuit connection in this manner:-

First, since $V_{1}$ control grid is isolated from the
operation of the circuit there is no need for a buffer amplifier, i.e. the sync input is decoupled from the oscillator. Secondly, $\mathrm{V}_{2}$ anode is unaffected by the charging of $\mathrm{C}_{2}$ as is the case in the simple multivibrator. A squarer output waveform therefore


Fig. 5.
results. A further improvement is the incorporation of diode $V_{3}$, the function of which is to clamp the voltage on $\mathrm{V}_{1}$ suppressor to zero.

## Speedier Component Assembly

SHOWN in the illustration is one of the new rotary dispensing machines for small components, known as the Rotasembler. It consists of 19 vertical hoppers, each divided longitudinally to provide two compartments each 3 in wide and $1 \frac{1}{2}$ in deep. The front one is 20 in and the rear one 24 in high, the difference being accounted for by the adjacent positions of the two feed lips, as shown


One of several Rotasembler component dispensing mochines in use in the Regentone factory at Romford, Essex.
in the illustration. Up to 38 different parts can be accommodated in one machine, and about 2,000 small components in each of the 38 hoppers.

The Rotasembler is rotated by compressed air being operated by a foot-controlled valve. As the hopper next in sequence always stops in exactly the same place as the previous one operator time and fatigue in identifying and selecting the next part for assembly is reduced, and it is claimed that the assembly work is considerably speeded up with assembly errors reduced to a minimum.

The machine, which costs $£ 87$ 10s, is made by Work Study Equipments, 4, Montalt Road, Woodford Green, Essex, from whom further details can be obtained.

## Printed Wiring Practice

IN order to make known as widely as possible the current practice in designing and producing printed circuits the Electronic Engineering Association has issued a report covering design considerations, general standards (materials, conductor sizes, etc.), production practices and special components. The object of this document is -" (a) To promote the adoption of such design and production practices as have proved to date to be justified as a result of common experience. (b) To make a contribution to any national standards that may be prepared on the subjects covered. Such national standards are considered urgently desirable in order to coordinate the numerous documents already in preparation by various sectional interests." Copies may be obtained from the Secretary, E.E.A., 11 Green Street, London, W.l.

CONFERENCES AND EXHIBITIONS
Latest information on forthcoming events both in the U.K. and abroad is given below. Further details are obtainable from the addresses in parenthesis.

## UNITED KINGDOM

Physical Society Exhibition, Royal Horticultural Society's Halls, Victorias London, S.W.I Jan. 18-22
(Physical Society, I Lowther Gardens, Prince Consort Road, London, S.W.7),
Managerial and Engineering Aspects of Reliability and Maintenance of Digital Computer Systems (Conference), I.E.E., Savoy Place, London W.C.2.

Jan. 20-21
(British Conference on Automation and Computation, c/o I.E.E.,)
Engineering Materials and Design Exhibition and Conference, Earls Court, London, S . 5 .
(Industrial \& Trade Fairs Ltd., Drury House, Russell Street, London, W.C.2.)
Electrical Engineers Exhibition, Earls Court, London, S.W.5 . ..... April 5-9
(A.S.E.E. Exhibition, Museum House, Museum Street, London, W.C.1).

Solid State Microwave Amplifiers (Conference), University of Nottingham
(Institute of Physics, 47 Belgrave Square, London, S.W.1). April 6-8
Audio Fair, Hotel Russell, Russell Square, London, W.C.1........... . April 21-24 (Audio Fairs Ltd., 22, Orchard Street, London, W.1.)
Production Exhibition and Conference, Olympia, London, W.14 .. April 25-30 (The Production Exhibition, 11 Manchester Square, London, W.1).
Mechanical Handling Exhibition, Earls Court, London, S.W.5 .... May 3-13 (Mechanical Handling, Dorset House, Stamford Street, London, S.E.1).
Instruments, Electronics and Automation Exhibition, Olympia, London, W. 14.
May 23-28
(Industrial Exhibitions Lid., 9 Argyll Street, London, W.1.)
Medical Electronics Conference and Exhibition, Olympia, London, W. 14. July 21-27
(I.E.E., Savoy Place, London, W.C.2.)

National Radio and Television Show, Earls Court, London, S.W.5.
Aug. 24-Sept. 3
(Radio Industry Exhibitions Ltd., 49 Russell Square, London, W.C.1.)

## Farnborough Air Show

Sept. 5-12 (Society of British Aircraft Constructors, 29 King Street, London, S.W.1.)
Industrial Photographic and Television Exhibition, Earls Court, London, S.W. 5.

Nov. 21-25
(Industrial and Trade Fairs Ltd., Drury House, Russeli Street, London, W.C.2.)
Radio Hobbies Exhibition, R.H.S. Old Hall Victoria, London, S.W.1. Nov. 23-26 (P. A. Thorogood, 35 Gibbs Green, Edgware, Middx.)

## OVERSEAS

Reliability and Quality Control in Electronics (Symposium), Washington, D.C. (R. Brewer, G.E.C. Research Laboratories, Wembley, Middx.)

Instrument-Automation Conference and Exhibition, Houston.
Feb. 2-4
(Instrument Society of America, 313, Sixth Avenue, Pittsburgh 22, Pa., U.S.A.)
Solid-State Circuits Conference, Philadelphia Feb. 10-12 (Tudor R. Finch, Bell Telephone Laboratories, Murray Hill, N.J., U.S.A.)
French Components Show (Salon International de la Pièce Détachée Electronique), Paris Feb 19-23 (Féderation Nationale des Industries Electroniques, 23 rue de Lubeck, Paris 16e).
Non-Destructive Testing (Conference), Tokyo ..................... Mar. 15-21 (Secretary, British National Committee for Non-Destructive Testing, c/o the Institution of Mechanical Engineers, 1 Birdcage Walk, London, S.W.1.)
I.R.E. National Convention, New York (E. K. Gannett, I.R.E., 1 East 79th Street, N.Y.21.)

German Industries Fair, Hanover..
Mar. 21-24 (Schenkers Ltd., 13, Finsbury Square, London, E.C.3.)
Instrument-Automation Conference and Exhibition, San Francisco May 10-12 (Instrument Socicty of America, 313, Sixth Avenue, Pittsburgh 22, Pa., U.S.A.)
International Congress on Microwave Tubes, Munich
June 7-11 (Prof. Dr. W. Kleen, Balanstrasse 73, Munich 8.)
British Exhibition, New York
June 10-26 (British Overseas Fairs Ltd., 21 Tothill Street, London, s.w.i.)
Nuclear and Electronic Congress and Exhibition, Rome
. .June 15-29 (Fairs and Exhibitions Ltd., 2, Dunraven Street, London W.1.)
Automatic Control Congress, Moscow
June 27-July 6 (British Conference on Automation and Computation, c/o I.E.E., Savoy Place, London, W.C.2.)
Physics of Semiconductors (Conference), Prague
Aug. 29-Sept. 2 (International Union of Pure and Applied Physics, 3 Boulevard Pasteur, Paris 15)
Instrument-Automation Conference and Exhibition, New York Sept. 26-30 (Instrument Society of America, 313, Sixth Avenue, Pittsburgh 22, Pa., U.S.A.)
Firato-International Radio Show, Amsterdam ...................September (Firato Secretariat, Emmalaan 20. Amsterdam, 2).
General and Applied Phonetics Congress, Hamburg
September (Dr. H.-H. Wängler, Alsterદ lacis 3, Hamburg 36, Germany).
Interkama-International Congress and Exhibition for Measuring Techniques and Automation, Dusseldorf (Nordwestdeutsche Ausstellungs-Gesellischaft m.b.H., Ehrenhof 4, Dusseldorf)


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Model G7823 is complete with screened connector plug and locking ring and beautifully finished in satin chrome. A silent switch adaptor G7819 is also available.


## RANIDOM RADIAIIONS

## By " DIALLIST"

## The Tenth Million

BY this time the total of British television receiving licences must have reached the ten million mark. The latest figures available at the time of writing were those for the end of October. There were then $9,844,365$ licensed TV receivers and there's always a big increase at the end of the year. And to help things on new transmitters and small local boosters have been coming into action. An astonishing businessisn't it?-that progress should have been so rapid since the restart of television in 1946. Ten years ago there were only half a million sets. It's bound to continue and one wonders what the saturation point will be. I'd put it at well over fifteen million, for that's the present number of homes with either sound or television sets in them. As TV coverage increases and improves many -maybe most-of the homes that are now equipped for sound only are bound to go in for television. New homes, too, are being built apace in TV service areas and it looks as if television manufacturers will be kept busy for a long time to come both in supplying the needs of new viewers and in providing sets to replace old ones.

## International

## Standardization

SOMETHING very badly needed, particularly now that the import restrictions on various kinds of electrical gear have been relaxed, is the adoption of an international colour code for three-wire flex mains leads. A dealer to whom I was talking not long ago told me that he'd seen appliances of foreign origin with mains leads with green covered phase wires! As green is now the colour for the earth lead here, this could have unfortunate consequences should a serviceman not look before he leaps and test carefully before wiring up a 3 -pin plug. Another bit of international, or at any rate N.A.T.O., standardization I'd like to see is in the screws, bolts and nuts used in things electrical. During the war the fact that American sizes and threads weren't the same as ours cost this country a pretty penny. You couldn't get An erican replace-
ments for any which were lost or suffered from stripped threads. The quickest method of replacement we found in radar was to re-drill and re-tap screw holes so that they'd take our own sizes. The loss of a nut usually meant replacing a bolt. Now that the world is growing more and more metric in outlook, the answer might be for everyone gradually to adopt metric sizes and threads.

## Do You Crane?

SHOULD people whose sight is normal or who wear correct glasses find it tiring to the eyes to watch television? That's a question often asked and to me the answer seems to be something like this: No, provided your set is properly adjusted, that the signal is good, that you sit at the proper viewing distance, that you don't switch off the room lighting and that you don't keep your eyes glued to the screen for hours on end. This summarizes the seven simple rules laid down by the Association of Optical Practitioners to avoid eyestrain when viewing. Neglect all or any of these provisions and you needn't be surprised if in time you find watching TV a trying business. Our 405 -line system probably gives the best balance between horizontal and vertical
definition that can be obtained on the $5-\mathrm{Mc} / \mathrm{s}$ channels now used in this country; but it has one drawback which, to my mind, is a serious one. That is that to avoid lininess you must sit quite a way from the screen. As I've mentioned before, a useful rule of thumb is: minimum viewing distance (feet) =half the screen diameter or diagonal (inches). Now, at $8 \frac{1}{2}$-feet from a 17 -in screen, or $10 \frac{1}{2}$-feet from one of 21 in it's difficult to feel that you aren't missing something. That's why people watching TV have a tendency to crane forward, thus reducing the effective viewing distance and so increasing the effects of lininess.

## Let's Have The Best

That's the reason why I've always been so keen that when u.h.f. channels are assigned to TV we should use them for transmissions of much higher definition. Eugène Aisberg, editor of Toute la Radio, after seeing television here, in the U.S.A. and in other Continental countries than his own, wrote that he was indeed thankful that he lived in France with its 819 -line system. Any readers who have had the chance of comparing French television pictures with ours will, I am sure, bear me out when I say that they are enormously better than our

own. You can view them, for instance, at a much smaller distance, without being conscious of the lines. I don't just want our new system to be as good as the French; I want it to be better still. We'll soon have the chance to snake our u.h.f. telcvision the best in the world and it's a chance that may not come again.

## Bewitched?

HAVE you ever come across a receiver of first-rate make which seemed to have a hoodoo on it? They're rare, as you'd expect them to be; but just once in a blue moon one of these turns up which seems to be bewitched. A friend was so delighted with the appearance and the performance of a particular set which he'd seen and heard in another house and so impressed by the enthusiastic reports that other owners gave of its utter freedom from trouble of any kind that he promptly ordered one for himself. It came; it was installed; all went well on the first evening; but on the second it just faded into silence. His dealer, who employs first-class servicemen, had it attended to at once. But hardly was the man out of the house when a valve went phut and all was silence again. And so it went on week after week-a day or perhaps two days of perfect listening, and then something always went wrong. At length, he wrote to the makers, adding that he knew from experience how good their sets of that type were-with the unhappy exception of his own. At once, they sent down one of their engineers who having seen this particular set's record in the dealer's files, fitted a new chassis free of charge. The set has been in regular use for nearly a year now and there's been not the slightest sign of any trouble. Queer, isn't it?

## Good Work

IT'S good news that C.R.T., Ltd., of Baldock, who specialize in rebuilding c.r. tubes, are now giving an eighteen month's guarantee on all their products. To my way of thinking every bit and piece in sound and television sets should be covered in the same way. I'm glad to see that Siemens Edison Swan have made a move in the right direction, by giving a twelve month's guarantee on their transistors used in any proprietary set of which it is a standardized part. By the time this note appears other makers may have followed suit. There should, after all, be nothing to go wrong in a properly sealed transistor orovided that it isn't badly overloaded.


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## UNBIASTED

## Pedagogic Pedantries

IN his interesting article entitled "Words, Words, Words" in the November issue, P. P. Eckersley, as one of the old guard of the B.B.C., naturally tries to continue the almost hopeless task of educating us, which the B.B.C. started nearly forty years ago when it tried to get us to use the pedantically pedagogic plural violincelli.

I do, however, heartily endorse most of what P. P. Eckersley says but I was a bit surprised that a writer, who rightly chides those who speak of "spectrums" when they mean " spectra," should have used the barbaric adjactive "ionic" when he ought to have tried to lead us to better things. The pedantically correct word is, of course, "iontic" as we were all reminded by D. J. Bataimis, of Athens, in a letter published in Wireless World of Septem-

Of course, the real culprit in this " ionic" business is Faraday, who in 1839 coined the word "ion" in connection with electrolysis and made its plural "ions" instead of "ionta." I have a sneaking sympathy with him, but regret that he spoke of "cations" and not "cathions." In any case, it would be a pedagogic pedantry to try to do anything about it now, and so we shall have to put up with it; it ain't possible to do otherwise.

## Hypnagogic Hum

IN pre-war years I frequently used to chide the B.B.C. for the duil and feeble programmes it put out, especially on Sunday afternoons. They usually resulted in sending me into a profound sleep. Some of the B.B.C. programmes were particutarly feeble, and I recollect one occasion when I hadpened to be chatting with a water diviner. We were standing rather near to my loudsp:aker when suddeniy his dowsing rod flew into the air owing to the programme being even more wet than usual.

But I was very puzzled when sometimes I found my head nodding even in the middle of a bright and breezy programme. The mystery is explained now. I recollect that the receiver I was using then had a low-pitched hum which seemed incurable no matter how many times I juggled with the smoothing circuits of the power pack and, I learn now, it was this hum which was causing me to fall asleep, and not the B.B.C. programmes. It appears that this mains hum is so strongly hypnagogic that it is now being used theraber, 1954. We must, at least, credit Mr. Bataimis with knowing his own language.

It is true that the word "ionic" has an ancient history dating back as it does to the issue of Nature for October 9th, 1890, but so also has the word "ain't." But antiquity doesn't make ain't correct unless used with its proper meaning of "am not" as Queen Victoria used it. Similarly the word "ionic" has its proper usage in a phrase like "ionic capitals" such as are to be found on the supporting columns of certain public buildings of classical architecture.

As for the Ionians being wanderers, this may well have been so but they took thoir name from the Greek god Ion from whom they are said to be descended; incidentally, many scholars have tried to identify Ion with Noah's grandson Javan whose sons certainly did a bit of colonizing after the flood (Gen. X 4, 5).

## Peak for Pain

WAY back in 1890 when the electric chair was first installed in Sing Sing there were two rival companies supplying electric power to New York according to a book written by a retired warder of the famous prison. Naturally a.c. was chosen for the chair as it was an easy matter to step up the e.m.f. to provide the necessary 2,000 volts.

This fact was immediately seized upon by the d.c. supply company who pointed out to potential users of electricity that the very fact that a.c. was chosen for the chair proved the product of the rival company to be highly dangerous and unsuitable for domestic use. This ingenious bit of propaganda had a very profound effect on electricity users of that time, and I sometimes wonder if it doesn't do so to a small extent even today.

The reason I say this is because recently when I was going over a house with a friend who was its potential purchaser I said I hoped for his sake that the electricity supply was a.c., otherwise a lot of appliances like synchronous clocks and fan heaters would be denied him. To my surprise he immediately switched on a light, removed the bulb and stuck his thumb in the socket. With scarcely a moment's pause he announced triumphantly that it was a.c. When I asked how he knew, he at once replied cryptically "Peak for Pain ", and went on to explain that with a.c. the shock was considerably greater, as one received the benefit of the peak voltage.

## Dr. Crippen

THIS issue of Wireless World ushers in the year 1960 and this reminds me of the unique event of 50 years ago which first put wireless on the map in the eyes of the general public. I refer, of course, to the arrest in July, 1910, of Dr. Crippen as a result of a radio message sent by Captain Kendall of s.s. Montrose saying he believed the doctor was on board in the guise of a Mr. Robinson. As a result of the message Inspector Dew sailed in late July on the Laurentic which overtook the Montrose in midAtlantic.

I have always thought we radio people have been rather remiss in not putting up a monument to Dr. Crippen to acknowledge his undoubted great service in publicizing radio.

Those who would acclaim Jack Binns, wireless operator of s.s. Republic, as the one who first demonstrated the value of wireless when his vessel was in collision with s.s. Florida in January, 1909, must remember that his name is unknown today whereas everybody has heard of Dr. Crippen.
 modest price, suitable for use on modern electronic apparatus as well as for radio and television receivers, motor vebicles, and all kinds of

## 19 Ranges

| D.C. Voltage | A.C. Voltage |
| :---: | :---: |
| $0-100 \mathrm{mV}$. | $0-10 \mathrm{~V}$. |
| $0-2.5 \mathrm{~V}$. | $0-25$ V. |
| $0-10 \mathrm{~V}$. | $0-100 \mathrm{~V}$. |
| $0-25 \mathrm{~V}$. | $0-250 \mathrm{~V}$. |
| $0-100 \mathrm{~V}$. | $0-1000 \mathrm{~V}$. |
| $0-250 \mathrm{~V}$. |  |
| 0-1000 V. |  |
|  | D.C. Current |
|  | $0-100 \mu \mathrm{~A}$ |
| Resistance | $0 \rightarrow 1 \mathrm{~mA}$ |
| 0-20,000. 7 | $0=100 \mathrm{~mA}$ |
| $0-2 M . i$ | $0 \rightarrow$ I A |

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1,000 . . A.C. . .

Accuracy:
$3 \%$ of full scale value on D.C. 4\% .. .. . . . . A.C.
To meet special requirements, instruments can be supplied to a higher degree of accuracy for a small additional charge.

Lus Picke: $£ 9 / 10$ s. complete with Test Leads and Clips Size: $51 \times 3$. $\times 1 \frac{1}{8}$ inches Weight: | lb. approx.

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## MULLARD GENERAL PURPOSE SILICON ALLOY TRANSISTORS ...THE FIRST THREE TYPES

Transistor OC203, the most recent of the first three types in the Mullard series of 50 mA general purpose silicon alloy transistors, is now fully available. This new transistor has a collector hold-off voltage of -60 V and is intended for high voltage applications.

Like the OC200 and OC201 announced earlier, the OC203 has a low bottoming voltage and all the advantages of the well-known OC71 germanium series. The equipment design considerations are basically the same for both the silicon and germanium series, and designers can gain the maximum benefit from their
experience with germanium when using the silicon transistors.

All three silicon transistors feature a low collector leakage current and reduced noise figure. Their wide junction temperature range makes them suitable for use at low and high temperatures in aircraft, guided weapons and industrial equipment.

These silicon 50 mA transistors express the Mullard philosophy for both germanium and silicon devices . . . thorough development followed by extremely large scale production to provide the user with practical and reliable transistors at very favourable prices.

Your enquiries are invited on the OC200 series and orher semiconductor devices in the
Mullard range of over sixty types. Please write or telephone the address below.

## OC200

The basic type in the series. Average current gain 20 and minimum $f_{\alpha} 0.3 \mathrm{Mc} / \mathrm{s}$. Maximum collector voltage is -25 V , but the low bottoming point allows operation from supplies as low as 1.2 V .

## OC2OI

A similar transistor to the OC200, but with average current gain increased to 30 and minimum $f_{\alpha}$ increased to $2 \mathbf{M c} / \mathrm{s}$.

## $0 C 203$

This, the most recent transistor in the series, fulfils the requirements of applications needing higher voltage ratings. Maximum collector voltage, d.c. or peak, is -60 V .

| TYPE No. | OC 200 | OC 201 | OC 203 |
| :---: | :---: | :---: | :---: |
| Minimum operating ambient temperature |  |  |  |
| ( ${ }^{\circ} \mathrm{C}$ ) | -50 | -50 | -50 |
| Maximum junction temperature | $+150$ | +150 | $+150$ |
| Abridged data (at Tamb $25^{\circ} \mathrm{C}$ ) |  |  |  |
| ${ }^{\text {cbb }}$ (pk) max. (V) | -25 | -25 | -60 |
| $V_{\text {cb max }}$ (avor d.c.) (V) | -25 | -25 | -60 |
| $i_{c}(p k) \max$. (mA) | 50 | 50 | 50 |
| $I_{c}$ max. (mA) | 50 | 50 | 50 |
| $\alpha^{\prime}$ (or $\beta$ ) spread | 15 to 60 | 20 to 80 | 10 to 60 |
| $V_{\text {ce }}\left(I_{c}=7 \mathrm{~mA}\right.$ 。 |  |  |  |
| $\left.\mathrm{lb}_{\mathrm{b}}=1 \mathrm{~mA}\right)(\mathrm{mV})$ | $-130$ | -100 | -130 |
| rbb ${ }^{\circ}$ ( $)^{\text {a }}$ | 125 | 125 | 125 |

THE FIRST THREE TYPES ARE NOW
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## Mullard



## from alrpoots

By far the largest number of hospital and industrial installations of the pocket receiver type in this country, and overseas, are Multitone. Our selective induction system " Personal Call" is saving time, money and worry in well over 100 different types of industrial concerns from airports to zymurgists. (We are looking for a Quill Manufacturer to complete the alphabet.)
The new MULTI-CHANNEL equipment provides over 400 individual channels using the new flat Receiver (as illustrated).

Additional Facilities

## ELECTRONIC TRUNCHEON

The Electronic Truncheon is no bigger than standard equipment carried by guards and serves the same purpose, but inside there is a transmitter which, when the button is pressed, sends out a signal. This is picked up by the loop of wire around the area to be protected. The pulse is used to operate a small receiver, which automatically switches on any form of electrical alarm. It can be operated from any point in the area.

INTERNAL TRANSPORT COMMUNICATION
The Multitone "Personal Call" loudspeakerreceiver has been designed to solve the problem of conveying verbal instructions to transport vehicles used for handling loads inside a given area. Messages can be conveyed to all or selected vehicles from the central transmitter.

MULTITONE INDUCTION SYSTEMS CAN SOLVE YOUR STAFF LOCATION PROBLEMS:

* Equally suitable for large and small areas or concerns
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(the 'peep-peep' in the pocket), the only staff location system worth installing Write or 'phone for further particulars. We can be found in 10 seconds.


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50kc/s Read-out Scaler
1Mc/s Read-out Scaler
4 Channel Output Unit
Read-out Unit
Meter Display Unit
Lamp Display Unit
Numerical Indicator Tube
Shift Register Stage
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[^15]

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- Switched tone controls for accurate matching between channels, with true " flat" position.
- Separate tone controls for each channel to enable the response of the separate channels to be controlled on monaural sound.
- Separate inputs for pickups, tape decks and radio.
- Recording characteristic correction for 78 and L.P. records.
- Long switch spindles and separate escutcheons to enable amplifier to be built into customers' cabinets.
- Power available to drive tape deck or radio feeder unit.


# 300 Popular Models 

(1958-1959) in one volume

672
pages
of wanted DATA

TELEVISION, RADIO, RECORD AND TAPE SERVICING DATA-
Covering many of the newer models sow in use all over the country, this volume fillis an urgent need for technical data.
It contains the circuits, component and chassis layout diagrams for 300 Masteradio, Murphy, Pageant, Pam, Perdio, Peto Scott, Philco, Philips, Pilot, Portadyne, Pye, Pye Telecommunications, Raymond, Regentone, R.G.D., Roberts' Radio, Sobell, Spencer - West, Stella, Ultra, Vidor, Walter.

## RECENT DEVELOPMENTS

Sections include: Picture Tube Repair, Car Radio Interference Suppression, Valve and Plcture Tube Data, Heater Ratings, Base Connections. Equivalents.

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## Includes the 300 models

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＂More than repaid the cost in a short period．＂ Says E．J．S．（Wolvercote）． of its worth，＂writes J．F．B．（Leicester）． ＂A boon and a must＂，
＂J．S．（Manchester）
Never at a loss now no matter which set I
ave to deal with．＂－S B．D．（Croydon）．
WILL PAY YOU TO EYAM．（ ＂Never at a los now no matter which have to deal with．－S B．D．（Croyd Address


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# CEIESION moon out//300  <br>  

## LOUDSPEAKER SYSTEM

The complete answer to the demand for a reasonably priced high quality speaker system for the reproduction of stereophonic recordings in the home.
Utilising two very small pressure type direct radiator units for the higher frequencies and two 12 in . reproducers for the lower, the equipment covers a response which is substantially level from $35-15,000 \mathrm{c} / \mathrm{s}$. with true stereophonic effect.


## HIGH-NOTE PRESSURE TYPE UNITS

The price for two HF. 1300
and two G. 44 units, complete
Designed and developed in CELESTION Laboratories this class of unit has been manufactured for special purposes over the past five years. A new unit, Model HF.1300, has been introduced for the new stereophonic system and its smooth response and wide dispersion ensure an exceptionally high standard of reproduction of the higher frequencies.

## LOW-NOTE REPRODUCER G-44

This new 12 in . Loudspeaker has been designed specially to work in conjunction with the HF.1300. A skilfully balanced voice coil and cone assembly with correct cone edge

## \&18:10:0

 termination result in a level and clean low frequency response.
## COMPLETE SYSTEM

The system uses only one enclosure, 15 in . high $\times 42 \mathrm{in}$. wide $\times 18 \mathrm{in}$. deep, having a central dividing partition with one G. 44 unit mounted at each end. The enclosure should then be positioned near the centre and against one wall so that the speakers are facing outwards and are about 2 ft . 6 in . from the floor.
The two HF. 1300 units should then be placed near the corners of the room, one on each side of the enclosure and approximately 4 feet above the floor. The width of sound will very nearly correspond to the distance between these two units. No elaborate cross-over networks are required and the system is completed by a 12 Mfd . capacitor in series with each high note unit.

## Designed and developed by

## For details of a NEW range of

## d.c.



ELECTRO METHODS LTD. General Products Division, CAXTON WAY, STEVENAGE, HERTS. Phone: Stevenage $2110-7$

## Five years ago THE WINSTON

 SEMI-DECADE OSCILLATOR
#### Abstract

was designed for use in the development laboratories and test department at our works. it was found to be such a useful instrument that it was decided to produce it in quantity. By advanced production techniques we are able to offer this instrument at most competitive price.


## DESCRIPTION

The oscillator uses an R.C. Wien bridge circuit with a thermistor controlling amplltude stability. It produces independent sine and square wave outputs.
It is attractively styled in smoke grey cabinet with dove grey front panel.

## SPECIFICATION

Frequency Range: 10 c.s. to 100 Kcs . in four main ranges with slow-motion vernier dial for setting a continuously variable frequency within the main ranges. The dial is engraved with both direct reading and vernier, for more accurate resetting. Calibration accuracy $1 \%$.
Output: Sine wave variable from $0-10 \mathrm{v}$ peak. adjustable with a high impedance variable attenuator and divider switch giving
ratios of $\times 1, \times 0.1, \times 0.01, \times 0.001$ atteñuation. Total content of harmonics and hum is less than $1 \%$. Square wave of fixed amplitude of $10 \mathrm{v} \pm 5 \%$ maximum drop at 10 cps. is $2 \%$. The rise and fall time at 100 Kcs . is 1 microsec.
Amplitude Stability: Output stability, $\pm 1 \%$ at any frequency.
Frequency Stability: Better than 1\%
Power Supply: 100-120v 200-250v50-60 cycles.
Terminals: Concentric sockets for sine and square wave outputs.
Accessories supplied: Mains lead. Coaxial Output Plug.
Dimensions (overall): Width 15 in . ( 37.5 cm .). Helght $10 \frac{1}{8} \mathrm{in}$. ( 25 cm .). Depth 83ain. ( 22 cm .). Weight 18 lb . ( 8 Kg .).

Facsimile of stability checks on the oscillators using a Berkeley Universal Counter/| Timer Type 7360 and a Berkeley Digital Recorder Type 1452. Checked at 100 Kcs., 10 Kcs., and I Kc. over a period of 24 hours.


## WINSTON

 SHEPPERTON MIDDLESEXWalton-on-Thames 26321

# Voltage Amplifiers 

MODEL 1439 WIDE-BAND AMPLIFIER
for TV and VHF distribution systems.
The Amplifier is designed to provide simultaneous distribution of signals anywhere in Bands I, II and III, enabling a common aerial to be used for a number of television or VHF radio receivers or other applications requiring a wide band voltage amplifier.
Voltage gain: 20 dB at $60 \mathrm{Mc} / \mathrm{s}$.
Bandwidth : better than $40 \mathrm{Mc} / \mathrm{s}-220 \mathrm{Mc}$, s .
Output voltage: 3 V pk-pk max.
Input and output impedance : $72 \Omega$ (matched coaxial).


## MODEL 1440 PRE-AMPLIFIER

This instrument is a directly coupled pre-amplifier of high stability which has been designed for use in cascade with a further amplifier or with a recording device.
Frequency response : d.c. : $0-50 \mathrm{kc} / \mathrm{s}$, a.c. : $5 \mathrm{c} / \mathrm{s}-50 \mathrm{kc} / \mathrm{s}$. Gain: continuously variable $10-55$ (d.c.), 165 (a.c.) Input: balanced or unbalanced, impedance $11.2 \mathrm{M} \Omega$ (grid-grid.)
Output: balanced or unbalanced, impedance 2000 2
(output 1-output 2).
Output voltage: 5 V pk-pk max. (output 1-output 2)
Calibration signal: 1 mV or 10 mV .


## MODEL I442 LABORATORY

 HIGH-GAIN AMPLIFIERModel 1442 has been designed for use in the Laboratory and is suitable for voltage amplification in the low frequency ranges. It can be used for special applications in Industry, Nuclear Physics Laboratories, neuro- and myo-graphic investigations and similar purposes.
Frequency response: $5 \mathrm{c} / \mathrm{s}-5 \mathrm{kc} / \mathrm{s}$ (gain $10^{4}$ and $10^{5}$ ) $25 \mathrm{c} / \mathrm{s}-3 \mathrm{kc} / \mathrm{s}$ (gain $10^{6}$ ).
Gain: $10^{6}$ Max. Switched and variable controte provide continuous variation.
Input: balanced or unbalanced, impedance $20 \mathrm{M} \Omega$ (grid-grid).
Output: balanced or unbalanced.
Output voltage: 400 V pk-pk max.
Calibration signal: $0.1 \mathrm{mV}, 1 \mathrm{mV}$ or 10 mV .
Write for the latest Cossor catalogue or ask for a representative to

## call and discuss your special requirements.




## CATHODE-RAY TUBE

Cossor 4 in. ( 10 cm .) double-beam, p.d.a., type 93D with green fluorescence, operating with overall accelerating potential of 3 kV or 6 kV .

## YI AMPLIFIER

$1 \mathrm{c} / \mathrm{s}$ to $10 \mathrm{Mc} / \mathrm{s}(30 \%$ down). Rise-time : $0.04 \mu \mathrm{sec}$.
Output deflection: $6 \mathrm{~cm}(4 \mathrm{~cm}$ at $10 \mathrm{Mc} / \mathrm{s})$. Sensitivity: calibrated $100 \mathrm{mV} / \mathrm{cm}$ to $10 \mathrm{~V} / \mathrm{cm}$. Sensitivity control: in steps $3: 1$ and $10: 1$ with continuously variable intermediate control. Input Attenuator impedance: $1.2 \mathrm{M} \Omega$ and 65 pF .

## Y2 AMPLIFIER

Identical with YI amplifier.

## SIGNAL DELAY

$200 \mathrm{~m} \mu \mathrm{sec}$ approximately. Not more than $10 \mathrm{~m} \mu \mathrm{sec}$ differential between channels.

## PRE-AMPLIFIER (2)

Gain 10. $5 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}(30 \%$ down). Input Resistance: $3 \mathrm{M} \Omega$.
One for Al amplifier, the other for A2 or $\mathbf{X}$ amplifier.

## PROBES (OPTIONAL EXTRA)

Frequency-compensated "L" attenuator., Input impedance: $6 \mathrm{M} \Omega$ and 15 pF . Insertion loss: 10:1.

## TIME-BASE

## Triggered.

Range: $0.03 \mu \mathrm{sec} / \mathrm{cm}$ to $15 \mathrm{msec} / \mathrm{cm}$ in eleven steps. Triggered from positive or negative signals derived externally or from Yl amplifier.
Sensitivity: pulse -1 cm . deflection or 2 V external. Sine wave -2 cm deflection or 2 V r.m.s. external at frequencies up to $5 \mathrm{Mc} / \mathrm{s}$. Expansion amplifier, continuously variable gain up to 5 times. Time-base output available at front panel on slow speed ranges. Delayed time-base: continuously variable delay $2 \mu \mathrm{sec}$ to $150 \mu \mathrm{sec}$. Delay jitter not greater than 1 part in 1,000 . Sensitivity pulse -1 cm deflection or 2 V external.

## X AMPLIFIER

$10 \mathrm{c} / \mathrm{s}$ to $750 \mathrm{kc} / \mathrm{s}$ ( $30 \%$ down).
As time-base amplifier: continuously variable expansion up to 5 times.
As independent $X$ amplifier: sensitivity variable from $1 \mathrm{~V} / \mathrm{cm}$ to $100 \mathrm{~V} / \mathrm{cm}$ in 5 ranges.

## CALIBRATION

Voltage measurement: internal calibrating voltage (square wave) referred through sensitivity control of the amplifiers. Accuracy $\pm 3 \%$. Time measurement: by directly calibrated $X$ shift control ( $\pm 5 \%$ ) and/or by $20 \mathrm{musec}( \pm 3 \%)$ black-out pips (for accurate measurement of rise-time).

## POWER SUPPLY

Mains: 100 V to 130 V and 200 V to 250 V . Frequency: $50 \mathrm{c} / \mathrm{s}$ to $100 \mathrm{c} / \mathrm{s}$.
Consumption: 550 W .
Internal supplies are stabilized where necessary.

## SIZE AND WEIGHT

| Height | $17 \frac{1}{2} \mathrm{in}$. | $(43.2 \mathrm{~cm})$. |
| :--- | :--- | :--- |
| Width | $12 \mathrm{in}$. | $(30.5 \mathrm{~cm})$. |
| Depth | 244 in. | $(62.9 \mathrm{~cm})$. |
| Weight | 80 lb. | $(36.3 \mathrm{~kg})$. |

## ACCESSORY

Camera Model 1428.

# COSSOR instruments ito 

The Instrument Company of the Cossor Group

## FERRANTI T.R. CELLS for Marine Radar

The QF 41 Cell already used throughout the world has been chosen for the D7 Series of Decca Marine Radar



# Fly-Wheel Magnetos 

Advertisements in this series deal with general design considerations. If you require more specific information on the use of permanent magnets, please send your enquiry to the address below, mentioning the Design Advisory Service.

The improved performance required from modern small petrol engines has resulted in higher specifications for the performance of magnetos to meet both ignition and lighting requirements.

The problems involved in magnetos have been solved in the fly-wheel design by the use of improved materials and in particular, the use of ceramic permanent magnets. An example of the type of design which is being adopted by a number of users is described and illustrated below.

In this magneto the magnetic circuit is designed to have the highest practical efficiency. The rotor consists essentially of four 'Magnadur' 2 segments with mild steel pole pieces equally spaced inside a cupshaped steel shell. The rotor/stator clearance is nominally 0.02 " and the 'Magnadur' magnets maintain a fleld of 2500 oersteds across this gap. The four pole stator conacross this gap. The four pole stator conparallel, each having a coil to produce the power output required for both ignition and lighting circuits.


The fly-wheel generator illustrated has an outside diameter of $5^{\prime \prime}$ with an overall depth of $24^{\prime \prime}$. The rotor is designed to be magnetised on a special magnetising fixture after assembly and will withstand removal and replacement for maintenance purposes without impairing the magnetic or electrical performance. Previously, one of the major disadvantages of magnetos was the loss of performance resulting from stripping down for maintenance or overhaul.

The power generated at 3000 r.p.m. is in excess of 24 watts, but when regulated to 12 volts, the maximum output decreases to approximately 20 watts.

A typical voltage output/speed curve for this design of fly-wheel magneto is shown for both regulated and unregulated conditions.


This example referred to, represents a typical design of a fly-wheel generator now going into general use, where the designer has taken full advantage of the unique properties of 'Magnadur' magnets with their exceptionally high coercive force and favourable length-to-section ratio.

If you wish to recelve reprints of this advertisement and others in this series write to the address below.



## SINGLE SIDEBAND

## Communications system

Over 4000 RCA single sideband equipments are in use the world over as fixed and mobile stations.

- Eight Channels.
- Instant Selection of Upper or Lower sideband.
- Compatibility with double sideband systems.
- Remote aerial tuning facility for SSB-L1.
- Mechanical Filter giving outstandingly High Selectivity.
- Exceptionally Stable and Reliable Operation.
- Rugged construction for naval and military use.


SSB-L30M Mobile Station. 30 watt ( 250 watt double sideband equivalent) eight channels $3-15 \mathrm{mc} / \mathrm{s}$.


## SONOTONE 8T

## Ceramics <br> bring reliability and

## high performance

## stereophonic reproduction

The new 8T ceramic pick-up cartritge is already accepted in all five continets as the most efficient means of obtaining stereophonic reproduction: it is impervious to all climatic conditions and has proved equally popular both at home and abroad. Intense development and accurate manufacture ensure that this exceptional cartridge provides among other advantages:-

- Response, $40-12,000 \mathrm{c} / \mathrm{s} \pm 1.5 \mathrm{~dB}$
- Sensitivity, 200 mV at $1 \mathrm{kc} / \mathrm{s}$ on stereo
- Compliance $2.4 \times 10^{-6} \mathrm{~cm} / d y n$
- Separation, 20 dB between channels
- Tracking Weight 6 grams on record changers, 4 grams on transcriptor arms
- Inbuilt vertical rumble filter
- Completely compatable for 331, 45 and 78 r.p.m., fits most popular arms
- Stylus weight less than 11 mg ., diamond or sapphire stylus (easily replaceable)

Performance data is freely available to those interested in fitting this outstanding TCL product.

Technical Ceramics Limited Wood Burcote Way Towcester Northants

Tel: Towcester 337


A whole range of PB and PK switches is provided by Plessey to meet the contemporary requirement in TV, radio and audio equipment design. And whether you plan to employ the one or the other, you will find a suitable Plessey switch with the shape of key or button you prefer - in the colour of your choice.

By the use of Plessey switches you can give your equipment the advantage of self-cleaning, positive contact switching with low contact resistance. All Plessey switches are free from electrical noise, due to their unique 'Wedgelock' riveted construction-which represents a great advance over conventional eyeleted methods. Standard or printed circuit contacts.


## MINIATURE PIANO KEY SWITCHES

Among the many universally employed ranges of Plessey switches is featured a miniature piano key series, available with either standard or printed circuit contacts.

* May we suggest that you talk to a
Plessey Technical Repı eschtative about your switch requirements.


## Plessey

## range of

## Mullard

## adjustable pot cores gives you

## outstanding

advantages

- Wide range of sizes
- Easily assembled
- Close tolerance permeability
- Precise and easy inductance adjustment
- Stability
- Single hole chassis mounting

Mullard Vinkors are the most efflclent adjustable pot core assemblies commercially avaitable. In addition to high performance, they have the distinct advantage of close tolerance permeabllity, thus enablling designers to precalculate to within $\pm 3 \%$ the Inductance of the core when wound. Final adjustment, taking into account normal capacitor tolerance, can be easlly effected to an accuracy of better than $0.02 \%$, by means of a simple self-locking device bullt into the core.
Write today for full detalls of the wide range of Vinkors currently avallable.

## Mullard

TINIOR POT CORIS


$5^{\prime \prime}$

## ELECTRO ACOUSTIC INDUSTRIES LTD., Stamford Works, Broad Lane, Tottenham, N. 15

Tel: Tottenham 0505/9 (5 lines)


## * Simet "AS" type Silicon Rectifiers

* and this isn't all.

Simet "AS" type Silicon Rectifiers cost less than Selenium and valve types for a great many thicitions, operate at higher tempesatumos than both Selenium or Germanium (up to $150^{\circ} \mathrm{C}$ ), do not age, and show savings in weight, bulk and total cost.
The range is extended to 800 P.I.V. Engineers and Designers who would like to know more are invited to write for complete data . . . and . . . deliveries, remember, are immediate.

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## THE PLESSEY COMPANY LIMITED

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DUST
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BASE ?

## GAN NOW BE SUPPLIED AS FOLLOWS:-

## A.I.D.

## ADMIRALTY APPROVED

3000 \& 600 TYPE RELAYS

6 CHANGE-OVERS LIGHT DUTY. 6 MAKES OR 6 BREAYS HEAVY DUTY. 2 CHANGE-OVERS HEAVY DUTY AND 2 CHANGE-OVERS LIGHT DUTY. -
TRANSISTORISED TO OPERATE AS LOW AS 3 MICRO-AMPS.
A.C. OPERATION FOR 6V, 12V, 24V, 50V, 110 V AND 250 V A.C.

DOUBLE WOUND COILS. P.T.F.E. INSULATION. OPERATE AND DELAY UP TO 5 SECONDS.

## A.D.S. RELAYS LTD

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The
Electronic
Lung

A member of the Pye Instrument Group W. Watson \& Sons Ltd. has produced an electronic lung which is capable of replacing an iron lung. The Barnet Ventilator, as the instrument is called, is transistorised and is easily portable in cases of emergency. It is shown here in its application in an operating theatre for the administration of anæsthetics.

The Pye Instruments Group Consists of:


TRANSISTOR PORTABLE KIT Model UXR-I


Presented in elegant real hide case with tasteful gold relief. Can be assembled in 4 to 6 hours and you have a set in the top flight of the 20-23 guinea class. Prealigned I.F. eransformers, printed circuit and a $7 \mathrm{in}, \times 4 \mathrm{in}$. high-flux speaker.
\&15.18.6
HI-FI STEREO AMPLIFIER KIT Model S-88


Gives $16 w$. output ( 8 per channel with 0.1 per cent. distortion at 6 w . per channel). It has ganged controls, STEREO/MONAURAL gram, radio and tape recorder inputs and push-button selection as well as many other first class leatures well above its price range. In two-tone grey metal cabinet with a golden surround and fittings. Also
£25.5.6 ultra-linear push-pull outpus. Basic sensitivity 10 mV . ( 2 mV , available, $30 /-$ extra).

## VARIABLE FREQUENCY OSCILLATOR KIT

 Model VFIU

For all Amateur Bands, 160-10 metres. Ideal for Heathkit DX-40U and similar transmitters Price less valves $88 / 19 / 6$ \&10.12.0

## DUAL-WAVE TRANSISTOR RADIO KIT Model UJR-I

This sensitive headphone set is a fine introduction to eleceronics for any youngster. (Not illustrated)
£2.16.6

- Deferred Terms available on all orders
above $\mathbf{E l} \mathbf{O}$.

ELECTRONIC SWITCH KIT
(Oscilloscope Trace Doubler)

## Model S-3U

This extremely useful, low priced device will extend the use of your single-beam oscilloscope for duties otherwise only in the province of the double-beam tube.
In short, at a nominal cost, the Heathkit model S-3U will give you the advantages of a double (or other muttiple) beam 'scope, while retaining all the advantages of your present single-beam instrumene.
Hitherto an electronic switch of this nature, permitting the simultaneous observation of two signals on the screen of a single-beam C.R.T. oscilloscope, has cost nearly as much as the scope itself.
£9.18.6

## RESISTANCE-CAPACITANCE BRIDGE

## KIT Model C-3U

Measures capacity 10 pF . to $1,000 \mu \mathrm{~F}$, resistance $100 \Omega$ to 5 megohms and power factor. $5-450$ y. tes voltages. Safety switch provided.
27.19 .6

## Technically



6 WATTS STEREO AMPLIFIER KIT Model S-33 A versatile high-quality self-contained
STEREO/MONAURAL Amplifier with adequate outpur for a living room-or with quate output for a living room-or with which to convert a favourite (monaural) per channel; $0.3 \%$ distortion at $2.5 \mathrm{w} / \mathrm{chnl}$.; 20 dB N.F.B., inputs for Radio (or Tape) and Gram., Stereo-or Monaural: Ganged controls.
Sensitivity 100 mV .
£11.8.0

||||"||||||||||||||||||

## VALVE VOLTMETER KIT Model V-7A

The world's most popular valve voltmeter, with printed sircuit and I per cent. precision rasistors to ensure consistent laboratory performance. it has 7 voltage ranges measuring respectively d.c. voits to 1,500 and a.e. to 1,500 r.m...s. and 4,000 peak to peak. Resistance measurements from 0.1 ohm to 1.000 M ohms with internal battery. D.C. input impedance is 14 Megohms and dB measurement has a centre-zero scale. Comp'ete with test prods, leads
and standardising battery... $\mathbf{\$ 1 3 , 0 , 0}$
R.F. PROBE KIT Model 309-CU

This complete probe kit will extend the frequency range of the V-7A Valve Volemerer to $100 \mathrm{Mc} / \mathrm{s}$. and will enable useful voltage indication ro be obrained up to $300 \mathrm{Me} / \mathrm{s}$.

Feathkit
=DAYSTROM
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AMATEUR TRANSMITTER KIT Model DX-I00U
The world's most popular "Ham" TX Kit

- Completely self-coníained, compact "Ham" Transmitter.
- Built-in, highly stable VFO and all Power Supplies. - TVI: Careful design has reduced TVI to a minimum by use of effe:tively screened frequency-generating. stages and pi tuned circuits at the input and output of the PA stage, and by 11 chokes and pi network filters to all outiets from the cabinet. No fewer than 35 disc seramic- by-pass capacitors help to achieve the exceptional stability and high-performanse for which this Transmitter is noted.
- The KT88 high-level anode and screen modulator stage gives over 105 watts of audio from less than 1.5 mV . input.
- Adiustable drive and clamp control ensure that valves are only driven sufficiently to maintain the required output.
- Keying on CW is via the VFO and buffer amplifier cathodes; the other RF valves are blased beyond cutoff. When zero-beating the TX with incoming signals, the exciter stages only may be run without the final amplifier being switched on.
- Provision has been made for remote control operation.
- VFO slow-motion drive is very smooth and back-lash free.
- Covers all Amateur bands up to $30 \mathrm{Mc} / \mathrm{s}$. phone or CW.
- VFO or Crystal control.
£78.10.0


## MATCHED HI-FI STEREO KIT

4-speed Transcription Record Player
Model RP-IU
612100
6 w. HI-Fi Amplifier, Model S-33
Ell 80
Twin Stereo Speakers System Model SSU-1 $E 20110$ Total cost if purchased separately. $\qquad$ 64490 YOURS for 642/10/- if all ordered together or 68/8/deposit and 9 monthly payments of $64 / 3 /$. Pedestal deposit and 9 monthly payments
speaker legs $\mathbf{E 2} / 14 /$ - optional extra.

## excellent



## TRANSCRIPTION RECORD

 PLAYER Model RP-IUWith 4-speed A.C. motor unit and Stereophonic Pick-up completely assembled on plinth.
High performance at low cost.
This attractive Transcription Record Player incorporates many new features which make it suitable for all types of recordings on dises. It has the new Collaro RP. 594 unit with the Ronette Stereo Pick-up and gives excellent results on stereo or mono (33, 45 L.P. or 78 r.p.m.)
gramophone records
£12.10.0

"HAM" TRANSMITTER KIT Model DX-40U
Covers all amateur bands from 80 to 10 metres. Power input 75 watts C.W. 60 watts peak controlled carrier phone. Output 40 watts to aerial. Provision for V.F.O. Fitters minimise T.V. inter
ference.
$£ 29.10 .0$

Our Technical Consultation and Service Departments are always ready to help in Departments are always ready to help in the unlikely event of your experiencing any difficulty.
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## a superbly designed stereo cabinet kit



Specially developed to meet the varying needs of different homes. It will house Tape Deck anj/or Record Player, F.M. Tuner and Stereo Amplifier. In addition for the convenience of those to whom space is an overriding consideration, it is possible to house speaker systems at each end. For this purpose a loudspeaker kit, comprising two 4 in . plus 8 in . speaker systems, balance unit, speaker grille, cutting template, padsaw and mounting details is also available. Neutral hardwoods have carefully been selected so that the finished product can be stained and polished to Individual choice. There is storage space for records, capes, etc., also for power amplifiers. Mk. I for Tape Deck or Record Player ......... $\subset 15$ is 6 Mk. II for boch T/D and R/P 61786


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## thoroughly

## $\underline{\underline{\text { ² }}}$



## COTSWOLD SPEAKER SYSTEM KIT

This acoustically designed enclosure measures $26 \times 23 \times 15 \frac{1}{\mathrm{i}} \mathrm{in}$. and houses a special 12 in . bass speaker with 2 in speech coil, elliptical middle speaker together with a pressure unit to cover the full frequency range of $30-20,000 \mathrm{c} / \mathrm{s}$. Ies polar distribution makes it ideal for really $\mathrm{Hi}-\mathrm{Fi}$ Stereo. Delivered complete with speakers, cross-over unit, level control. Tygan grille cloth, etc. Left " in the white " for finish to personal taste, all parts are precut and drilled for ease of assembly.
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$10 \mathrm{c} / \mathrm{s}$. to $100 \mathrm{Kc} / \mathrm{s}$., switch selected. Distortion less than $0.1 \%$. 10 v . sine wave output metred in volts and dB 's


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£14.10.0 tion



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Ducted-port bass reflex cabinet, $"$ in the white." Frequency response to $40-16,000 \mathrm{c} / \mathrm{s}$. Power rating 25 warts. Matched speaker unizs 8in. high flux ( 12,000 lines) with hyperbolic cone and 4in. wide angle dispersion type tor higher frequancies. \&10.5.6


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$400 \mathrm{k} \Omega \ldots 50 \mathrm{M} \Omega \cdot / / 7 \mathrm{pF} \ldots 2 \mathrm{pF}$ Overall accuracy: $3 \%$ with no respect to variations in the frequency repose curve. which variations are limited within $5 \%$ of the gain at the calibration frequency.
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About 56 million television sets were available in the world in 1957. By 1958 for every hundred inhabitants in England 17.4 sets were counted. In Belgium this figure amounted to 3.8 and in France to 2.5. The further growth shows a rapid rate of increase. It is predicted that in 10 years' time about $50 \%$ of all families in Europe will be in possession of a television set.
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Since the scientist K. F. Braun developed the cathode-ray valve 61 years have passed. That denotes six decades of technical progress since then and tremendous achievement in the field of electronic engineering.
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# A FURTHER IMPORTANT ANNOUNCEMENT 

## by <br>  METAL PRODUCTS LTD

A. B. Metal Products Ltd. proudly announce that they have been granted by the Trolex Corporation of Illinois, U.S.A., the sole manufacturing rights of the new "TROLEX" range of switches.

The Trolex method of switch manufacture incorporates a technique which is completely revolutionary and will enable A. B. Metal Products Ltd. to make available shortly in this country a range of multi-pole, multi-way switches which will be unique in design, size and performance. Samples will be available very shortly.


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| CAPACITANCE $\mu \mathrm{F}$ | VOLTAGE RATINGS |  |  | DIMENSIONS |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{aligned} & \text { d.c. Whg. at }-40^{\circ} \mathrm{C} \\ & \text { to }+125^{\circ} \mathrm{C} \end{aligned}$ | d.c. Test at $20^{\circ} \mathrm{C}$ | $\begin{array}{\|l} \text { a.c. Wkg. r.m.s. at } \\ -40^{\circ} \mathrm{C} \text { to }+70^{\circ} \mathrm{C} \\ \text { and up to } 60 \mathrm{c} / \mathrm{s} \\ \hline \end{array}$ | $\begin{gathered} \text { Diameter } \\ +0.020^{\circ} \\ -0 \end{gathered}$ | $\begin{aligned} & \text { Length } \\ & \pm 0.040^{\circ} \end{aligned}$ |
| 0.001 | 1,000 | 2,500 | 250 | $t$ | 1 |
| 0.002 | 1,000 | 2,500 | 250 | 1 | 1 |
| 0.005 | 1,000 | 2,500 | 250 | 1 | 1 |
| 0.01 | 1,000 | 2,500 | 250 | $\frac{1}{8}$ | 12 |
| 0.02 | 750 | 2,250 | 250 | 7 | 18 |
| 0.05 | 500 | 1.500 | 250 | 1 | $1 \frac{18}{8}$ |
| 0.1 | 350 | 1,000 | 180 | $\frac{1}{1}$ | $1{ }^{18}$ |
| 0.1 | 500 | 1,500 | 250 | $\frac{1}{2}$ | $1{ }^{\text {H }}$ |

If you have a problem that can be solved by using digital techniques-then Venner packaged circuits can help. Their versatility can solve your development or test set problems, because either you or we can build the equipment from fully developed circuit elements.

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on punched tape, in I" figures or in print.

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1 In-line readout frequency and time measuring equipment.
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10 Frequency source providing . $0 \mathrm{kc} / \mathrm{s}, 1 \mathrm{kc} / \mathrm{s}, 100 \mathrm{c} / \mathrm{s}$, and $10 \mathrm{c} / \mathrm{s}$.
11 Reaction time indicator.

As a general rule we can give you delivery in 6 to 8 weeks of special items built in this way. Alternatively, if you "do-it-yourself", we will give advice and provide the majority of plug-in stages within $7 / 10$ days of receiving your order.

If you are not familiar with our circuit blocks, please send for leaflet WW/IO4.


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## 

## COMPONENTS

## C7402 Condenser

For applications requiring larger capacity values than C7802. A cut oscillator vane is available for an I.F. of $470 \mathrm{Kc} / \mathrm{s}$. Capacity swing 196 pfs aerial and 110 pfs oscillator or 196 pfs in each section. Either slow motion or direct drive types are offered with trimmers if required.

## Sl204 Trimmer

A popular and well proved Compression Trimmer available in $1,2,3,4,5$ and 6 Bank Units with fixed screwed adjusting stem ensuring high stability. Cap. 3-33pf. and 25-50 pf.


## C7802 Condenser

A miniature 2-gang less than I" in length. Can be provided with trimmers and either direct or slow motion drive. Capacity swing 118 pfs each section or 153 pfs and 82 pfs.

## WINGROVE \& ROGERS LIMITED



3 WATTS The Hand Portable Electronic Megaphone weighs only 5 lb . The transistor amplifier gives more than 3 watts output. It uses standard torch batteries which last. about six months.
The Portable Electronic Megaphone with adjustable stand and separate microphone

Pye Portable Public Address equipment is transistorised for maximum portability and minimum current consumption. It is the perfect answer to all situations where mobility, temporary use or lack of power supplies make it impractical to use more conventional systems.
Ideal for police, fire services, political meetings and electioneering vehicles, garden fetes and sports meetings, touring coaches and all types of ships, passenger and freight control on railways, building operations and many others too numerous to mention. Intrinsically safe versions of this equipment are available which have been certified as suitable for use in methane and pentane atmospheres by the Ministry of Power and the Ministry of Labour Factory Inspectorate.


10 WATTS The Portable Transistor Amplifier weighs only $5 \frac{1}{2} \mathrm{lb}$. and measures $8^{\prime \prime} \times 3 \frac{z^{\prime \prime}}{} \times 6^{\prime \prime}$. It will deliver 10 watts output for a consumption of 1.8 amps from a 12 volt battery. It is ideal for use in moving vehicles or on sites where a mains supply is not available. A comprehensive selection of microphones and loudspeakers is available.


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## "Ranger" v.h.f. boot-mounting Radiotelephone

Brief Specification: PTC 8201/2: 20 watt F.M. PTC 2201/2: 15 watt A.M. PTC 8101/2: 10 watt F.M. PTC 2101/2: 5 watt A.M. Available from $25-174 \mathrm{Mc} / \mathrm{s}$. Simplex or Duplex operation "Split-channel" selectivity Up to 6 switch-selected channels Power supply: Models for 6,12 or -24 रolts operation.

The Pye "Ranger" radiotelephone has been designed to meet the specifications of the American F.C.C. and the British G.P.O. It is suitable for use under all climatic conditions and is vibration proofed. Its features include light weight, low battery drain and low cost of installation and maintenance. Optional features are alternative channel spacing; public address and rebroadcast facility on A.M. types; and a choice of fist microphone or telephone handset. The models listed here form part of a complete series which include dash mounting types and fixed stations.

## PYE TELECOMMUNICATIONS LIMITED <br> NEWMARKET ROAD - CAMBRIDGE



FEATURING PYE TELECOMMUNICATIONS EQUIPMENT

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The Pye PTC 8710 Fixed Station has been designed to provide reliable communications in the $450-470 \mathrm{Mc} / \mathrm{s}$ band. Both the transmitter and receiver are fitted with temperature-controlled crystal units to ensure an exceedingly high frequency stability over a wide temperature range. All the materials used have been chosen to ensure reliable operation under a wide range of climatic conditions.
Additional control equipment is available for operating the Station at distances of up to 200 feet or, via telephone lines, over greater distances.
A switchboard Termination Unit is also available for working the Station into a manual or automatic telephone switchboard.

## PYE TELECOMMUNICATIONS LIMITED

NEWMARKET ROAD • CAMBRIDGE



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Inside and out . . . the expertly designed Brenell tape recording equipment establishes a lasting impression of quality at its best. How true this is of its performance too! Superb sound reproduction that the discerning ear of the connoissur will find highly commendable and its versatility in application of immense advantage.
Small wonder when you consider over 10 years of engineering development and production experience by Brenell-the sole manufacurers-are behind every machine produced. You'll be missing hi-fi at its finest if you fail to see and hear a Brenell in action before you make your choice.

Three recording speeds $1 \frac{7}{8}, 3 \frac{3}{4}, 7 \frac{1}{2}$ i.p.s. Frequency compensation at all speeds: Push button operation (interlocked): printed circuit amplifier: separate bass and treble controls: .high quality speaker (8in. $X$ 5in.) : takes spools up to 7 in .: pause control: digital rev. counter: contemporary style wooden cabinet for improved acoustic performance. Approved by the Council of Industrial Design. Price Includ-

## Irenell

 ing 1200 ft . tape, spool and quality microphone, 58 GNS. 3 Star Stereo rec/playback model now available 89 GNS. or with two microphones 95 GNS. Send now for complete detalls.BRENELL PERFORMANCE IS TRUE-TO-LIfE PERFORMANCE

## ALPHASIL- the modern core material

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Alphasil $013^{\prime \prime}$ thick is produced in coil 30 inches wide, and can be supplied slit to narrower widths by arrangement.


ABOVE-A $4.000-1 \mathrm{~b}$, coil of $30^{\circ}$ wide X. $013^{\prime \prime}$ thick,

ALPHASIL 44
ALPHASIL 40
ALPHASIL 37
ALPHASIL 33
Thin Alphasil for high frequency work is also available in coil in $.004^{\prime \prime}$ thick in widths up to $5 \frac{1}{2}$ inches, and in -002" thick, in widths up to $4 \frac{1}{2}$ inches.

|  | frequency cycles/second | Guaronteed max. zotal losses |
| :---: | :---: | :---: |
| ALPHASIL -004HF | 400 | 8000 wates/lb. at B. Max is Kilogauss |
| ALPHASIL O02HF | 8.000 | 9.50 wates/lb. at B. Max 2 Kilogauss |

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The TYPE DI/D v.h.f. SIGNAL GENERATOR

## $\varepsilon 97$

Both the DI/D and DIP/2 are now available with an output impedance of 50 ahms.

## Advance

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This model is a special version of the D1/D designed for the alignment of narrow band communication receivers, and incorporates:-
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(9)


The possibility of a component change - due to shortage of supplies, increased costs or failure to meet specific conditions - is a problem facing every designer of electronic equipment. However, one basic component can be 'tailor-made' from the start, for LAB will supply the precise type of Resistor required, ex stock and at the right price. Write for full technical data, prototype samples and price schedules to:-

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Abridged data for the 3AZPl is given herefor full information please use the coupon below.

## ABRIDGED DATA

Diameter 94 mm max. Length 310 mm max.
Heater $6.3 \mathrm{~V}, \mathrm{I} .25 \mathrm{~A}$ max.

$S_{x}$ (each gun)................................ . . $23 \mathrm{~V} / \mathrm{cm}$.
$\mathrm{S}_{\mathrm{y}}$ (each gun)................................ $16 \mathrm{~V} / \mathrm{cm}$.
Trace overlap.............................. 5 cm. min.
$c_{y l-y 2}$ (each gun)............................. 2.0 pF



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JANUARY 1960

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# Tirimbl 



The second advertisement in this series described the EF183, which is a variable-mu r.f. pentode, and discussed its use in the i.f. stages of television receivers.
When little or no control is required, a straight r.f. pentode, the EF184, is available. This valve is particularly suitable for use in uncontrolled final i.f. amplifiers, or in television systems using f.m. sound.
The EF184, in common with the other types in the Mullard frame grid range, has about twice the slope of its conventional counterpart. Under comparable conditions, the conventional EF80 has a slope of $7 \cdot 4 \mathrm{~mA} / \mathrm{V}$, as against $15 \cdot 5 \mathrm{~mA} / \mathrm{V}$ for the EF184. This doubling of the slope provides a substantially improved gain per stage, of the order of 2 or $2 \frac{1}{2}$ times.


Under cathode bias conditions the EF184 shows an advantage in gain of 6 dB over the EF80. If grid current bias is used, the advantage can be increased to 8 dB . It should be noted that it is good practice to include a certain amount of cathode bias for these high slope valves, even when they are working under grid current bias conditions, and when a large value of sliding screen resistor is used. A suitable value for the EF184 under these conditions is about $10 \Omega$. This value is also sufficient for input capacitance compensation with small amounts of a.g.c., or with variations in bias that might be caused by changes in signal level with large signals.
It was said above that the EF184 is suitable for use when little or no control is required. This should be interpreted to mean a control of not more than 2 or 3 times. If a
greater control ratio is required, the variablemu EF183 should be used instead, since the variations of its tail from valve to valve are kept within narrow limits.
Typical anode current and mutual conductance characteristics under cathode bias and grid current bias conditions are shown in the graph.


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## "BELLING-LEE" NOTES

## No. 12 of a Series

Recently we have been fortunate in engaging the services of a very experienced electronic instrument maker who has worked with one of the bigger equipment makers. When watching him at work on our distribution amplifiers and talking to him, he volunteered the information that the quality of the printed circuit we used was very much better than anything he had experienced elsewhere. Knowing the feelings of a considerable cross-section of the industry, we became inquisitive, Why? How? Well, he said, lots of circuit boards he had used had so little copper on them and stuck so badly that it lifted if touched with a soldering iron. Open circuit occurred through invisible fractures occurring due to flexing of the board. He was emphatic that he had not come


This photograph shows the interior of a printed circuit triplexer, L.1411. The cable connections are made through terminals which are mounted directly onto the printed circuit.
across any of the old trouble he was used to, and had quite changed his mind about printed circuitry, provided the boards were as good as used by us. We then visited Research and asked some more questions. There are two main ways of making printed circuit boards, one, by the deposition of copper on a laminated board where it is required. The other starts with a copper clad board, and the unwanted copper is etched away. It is this last method that we use, and let it be said here and now that the gauge or thickness of the copper cladding is an important part of the specification, as is the minimum width of the conductors. We are also very interested in the adhesion of the metal to the board.

There are three accepted ways of testing for this characteristic:-
(1) Float a small square of the board face downwards in molten solder for a predetermined period.
(2) A copper disc is etched on the face of the board to the centre of which a copper wire is butt soldered. It is then pulled off and the required force measured.
(3) A one einch strip of cladded board has the copper peeled from it by a pull perpendicular to the board, and the pull monitored.
It will be seen that in a good quality board, little is left to chance.
In some boards considered by us to be unsuitable, the copper is so thinly deposited that it is only useful as a key to solder, and the whole board must be dipped to ensure a satisfactory result. With the board we use the adhesion of the cladding is so good that we can, with safety and confidence, solder to the copper, or rivet right through.
This facility will be appreciated by those who may have to change a faulty capacitor or resistor. From correspondence published in some technical journals, the inability to do just this thing is cited against printed circuits, but please do not condemn the technique because it has been used to save a few pence, without regard to its limitations.

Samples of the board we use are constantly subjected to the Admiralty test salt spray chamber where they are given the full forty-day test. At the end of that time, they are in a sorry state but still serviceable, but such a test represents a very hard life under conditions rarely met with in practice.

It will probably interest many to learn that the conditions met with in salt spray test is more severe than those experienced in areas considered to be bad through industrial air pollution, such as sulphurous fumes found in some towns.

There is no doubt that the technique of printed circuits has suffered by the use of unsuitable materials.


The interior of an L. 1360 TV/FM diplexer is shown in this photograph. The continuity of the outer braid is maintained through the metal body to which the board is secured.

We at "Belling-Lee" have a wonderful reputation to keep up which we are certainly not going to jeopardise by offering poor quality printed circuits, when good ones are available at a slightly higher cost.

Advertisement of
BELLING \& LEE LTD.
Great Cambridge Rd., Enfield, Middx. Written 12th November, 1959
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L. $1370 / \mathrm{Au}$ or Ag .

12-pole, $0.15^{\prime \prime}$ Module
L.I372/Au. or Ag.

18-pole, 0.15 " Module L.I380. Guide for printed circuit
panels
This range of connectors enables the printed circuit board to be easily removed from equipment, but ensures that when the board is inserted, reliable electrical contact is made in the various circuits.
The connectors can be used with conventional or printed wiring at the solder spills. When used with printed wiring the base printed circuit can be drilled or punched with holes on a 0.1 in . grid in the case of L. 1355 and on a 0.05 in. grid with the other connectors.
The plug-in board for use with these connectors should have a thickness of $0.0625 \mathrm{in} . \pm 0.005 \mathrm{in}$. and can be single or double sided.
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Most "Belling-Lee" products
are covered by patents or registered designs, or applications.


## HQUALITY • QUANTITY • QUIGKIY G.E.C. SEMICONIJUGTORS

[^21]
## Aspects of design <br> 18 <br> "BRIGHT SPOT " SUPPRESSION in television RECEIVERS <br> This is the eighteenth of a series of special features dealing with advanced problems in television and radio circuit design to be published by The Ediswan Mazda Applications Laboratory. We will be pleased to deal with any questions arising from this or other articles, the Nineteenth of which will appear in the February 1960 issue.

The primary concern in designing a television receiver is to provide good reproduction of picture and sound with reliability. In addition to ensuring that valves and components are operating within their published ratings under normal viewing conditions, consideration must also be given to transient conditions occurring when the receiver is switched on or off which may be liable to cause damage or reduction of life in valves or cathode ray tubes.

One such transient effect which may occur on switching off the receiver is the appearance of a bright spot in the centre of the screen. If the spot is sharply focused and too bright, the screen can suffer permanent damage and a burn mark appear after a number of such switching operations. This tendency has become more apparent with recent types of cathode ray tube using a unipotential electrostatic beam focusing system without an ion trap. The sharpness of focus of these guns is not critically dependent on focus electrode voltage.


Associated Electrical Industries Ltd
Radio and Electronic Components Division
Technlcal Servlce Department
155 Charing Cross Road, London, W.C. 2
Tel: GERrard 8660. Grams: Sleswan, Westcent, London

Factors controlling the intensity of the spot are:
(a) Receiver control settings

The spot brightness is generally greater if no picture is visible before switching off. Thus it is not desirable to gang the mains switch with the brilliance control.
(b) Time decay characteristics of voltage sources

The rates of fall of the voltages on the various electrodes of the cathode ray tube are controlled by the rate of fall of the H.T. line voltage on switch-off, together with the time constants of the circuits supplying the electrodes. Figure 1 shows, on logarithmic scales for both voltage and time, the decay of voltages in a typical receiver using no time constants other than the usual H.T. smoothing circuit. Initially the tube grid voltage potentiometer is assumed to have been set just below beam cut-off with no picture modulation signal, the tube cathode being directly connected to the anode of the video amplifier valve. After the initial rapid fall of H.T. voltage before the valve cathodes cool, a few volts remain and decay very slowly.

## (c) Cathode ray tube characteristics

The grid to cathode voltage required to cut off the beam current decreases in proportion to the first anode to cathode voltage and in normal conditions is insensitive to second anode voltage changes. However, with zero first anode voltage and a second anode voltage of $10-15$ kilovolts, a negative bias of a few volts between grid and cathode is still required to cut off the beam current. This effect is due to penetration of the electrostatic field of the second anode into the gap between first anode and grid. In Figure 1, the dashed curve shows an estimation for a typical tube of the cathode voltage required at any instant to cut off the beam current. The actual cathode voltage is seen to fall below this line about three seconds after switching off, when scanning has completely ceased. As the tube cathode can still emit due to its relatively high thermal capacity, a bright spot appears on the screen and may persist for one or two minutes as the E.H.T. capacity is gradually discharged.

## PREVENTION OF SWITCH-OFF SPOT

One method is to maintain beam cut-off until tube cathode emission ceases. This, however, is difficult as sufficient emission is maintained for at least a minute and has the disadvantage from a servicing point of view that the E.H.T. capacity is left in a charged condition.

The alternative approach is to ensure rapid discharge of the E.H.T. capacity to a comparatively low voltage before scanning entirely ceases. Three methods are generally used to effect this as follows:
(1) A time constant of $\frac{1}{2}-1 \mathrm{sec}$. may be connected in series with the first anode voltage supply to delay the decay of this voltage. The series resistance component is limited to a maximum of 2.2 Megohms from leakage considerations. Figure 2 shows similar curves to Figure 1 modified to incorporate this change. The cathode ray tube passes beam current in the shaded area which now occurs before the scanning has ceased. Thus a bright collapsing raster is seen which will not cause any damage to the screen.
(2) A long time constant may be connected in series with the tube grid bias supply. This has a similar effect to the first method but a compromise must generally be made to avoid a slow-reacting brilliance control.
(3) The E.H.T. capacity may be discharged by a bleed resistance to chassis. A convenient method which also improves E.H.T. regulation is to use a nonlinear voltage sensitive resistance such as "Metrosil". In this case, the E.H.T. voltage falls sufficiently rapidly for no more than a defocused moving spot to be briefly seen.

## EDISWAN MAZDA 10C14

The 10 C 14 is a Triode Heptode valve combination, with separate electrode structures, for use in broadcast radio a.c./d.c. receivers. The valve is intended to be used as a frequency changer for amplitude modulated signals with the triode as local oscillator. In combined AM/FM receivers, the heptode may be switched to operate at $10.7 \mathrm{Mc} / \mathrm{s}$. as an IF amplifier for frequency modulated signals.

$$
\begin{array}{lll}
\text { Heater Current (amps) } & \mathrm{I}_{\mathrm{b}} & 0.1 \\
\text { Heater Voltage (volts) } & \mathrm{V}_{\mathrm{b}} & 19
\end{array}
$$

## Preliminary Ratings and Characteristics.

## MAXIMUM DESIGN CENTRE RATINGS

| Anode Dissipation (watts) |  | $1.7{ }^{\text {tode }}$ | Triod |
| :---: | :---: | :---: | :---: |
| Screen Dissipation (watts) |  | $\begin{array}{r} 1.7 \\ 1.0 \end{array}$ |  |
| Anode Voltage (volts) | $\mathrm{V}_{\mathrm{a} \text { (mas) }}$ | 250 | 25 |
| $\underset{\text { (volts) }}{\text { Screen }}$ Voltage $\left(\mathrm{I}_{\mathrm{a}}<1 \mathrm{~mA}\right)$ | $\mathrm{V}_{\mathrm{E}^{2}}$ | 250 |  |
| $\underset{\text { (volts) }}{\text { Screen }}$ Voltage ( $\mathrm{I}_{\mathrm{a}}{ }^{\circ}=7.6 \mathrm{~mA}$ | $\left.V_{\mathrm{B} 2}+{ }_{\mathrm{B}} \mathrm{t}_{\text {(max }}\right)$ | 125 | - |

Heater to Cathode Voltage (volts rms)
${ }^{5}{ }^{1} 4_{(\max )}$
125
volts rms) $\quad \therefore \quad \therefore V_{b-k(m a x)}$ rms
12.5

100
Mean Cathode Current (mA) $I_{\text {(av max }}$
INTER-ELECTRODE CAPACITANCES ( pF )

|  |  |  | Heptode | Triode |  |
| :--- | :--- | :--- | :---: | :---: | :---: |
| Anode to Earth | $\ldots$ | $\ldots$ | $c_{a-E}$ | 7.9 | 2.1 |
| Anode to Grid 1 |  | $\ldots$ | $c_{a-g 1}$ | $<0.006$ | 1.0 |
| Grid 1 to Earth | $\ldots$ | $\ldots$ | $c_{g 1-E}$ | 4.8 | $2.6:$ |
| Grid 3 to Earth | $\ldots$ | $\ldots$ | $c_{g 3-E}$ | 6.0 | - |

Inter-electrode capacitances measured in fully shielded socket.

## CHARACTERISTICS

Anode Voltage (volts)

| HARACTERISTICS | Heptode | riode |
| :---: | :---: | :---: |
| Anode Voltage (volts) .. V $\mathrm{V}_{*}$ | 170 | 100 |
|  | 102 |  |
| Grid No. 3 to Cathode Voltage (volts) $\qquad$ | 0 |  |
| Grid No. 1 to Cathode Voltage (volts) | -2.2 | 0 |
| Anode Current (mA) . . $\mathrm{I}_{3}$ | 6.2 | 13.5 |
| Screen Current (mA) $\quad \ldots \mathrm{I}_{\mathrm{g} 2}+\mathrm{g}^{4}$ | 3.8 |  |
| Mutual Conductance (mA/V) gm | 2.3 | 3.7 |
| Amplification Factor (Hep- | 0 | 2 |

## TYPICAL OPERATION

## AS AM FREQUENCY CHANGER

## Heptode



Base: B9A
(Nuval)


VIEW OF FREE END


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Radio and Electronic Components Division 155 Charing Cross Road Lechnical Service Department Tel: GERrard BGGO. Grams: Sleswan, Westcent, London


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$$
\begin{array}{llll}
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\text { Third overtone } & \ddots & 15-40 \mathrm{Mc} / \mathrm{s} .
\end{array}
$$

and wlll operate within the specified actlvity and frequency limits when subiected to the bump and vibration tests stipulated by Defence Specification DEF 527I.

## TECHNICAL DETAILS

furthermore, the units continue to conform to the perating conditions of DEF 5271, even under more stringent test conditions during which the applied vibraion is swept from $30 \mathrm{c} . \mathrm{p} . \mathrm{s}$. to $2,000 \mathrm{c.p.s}$. , at a rate not exceeding two octaves per minute, and the peak acceleraexceeding two octaves per minute, and the peak acceleration is maintained at 20 g . Thitually perpendicular planes.
The graph illustrates the more rigorous nature of this The graph illustrates the more rigorous nature of this test in comparison with that specified in DEF 5271 . The extended frequency range and general increase in the amplitude of vibration, particularly at the lower frequencies, are readily apparent.


QC 327
STYLE D
HC - $6 / \mathrm{U}$
QC 193 STYLE E
 ans $0.40^{\circ} \mathrm{inn}$



## DRIVE LEVEL

All units are designed to operate at the drive levels specified in DEF 5271 as follows :-
(a) Fundamental Oscillators

| Skrie | Prequency nance |  |  |  | Orive heref(milliwate |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Mininum |  | Maximum |  |  |
| B | $\begin{aligned} & 100 \\ & 100 \\ & 100 \end{aligned}$ | $\mathrm{K} \mathrm{K} / \mathrm{a}$ $\mathrm{Ms}_{\mathrm{s} / \mathrm{a}}$ | $\begin{gathered} 308 \\ \text { F90. } \\ 20 \end{gathered}$ |  | ${ }_{18}^{18}$ |
| C\& | $\begin{aligned} & 2000 \\ & \\ & \hline 10 \end{aligned}$ | $\mathrm{K}_{\mathrm{K}} \mathrm{l} / \mathrm{b}$ $\begin{aligned} & \mathrm{Kc} / \mathrm{m}, \\ & \mathrm{me} / \mathrm{a} \end{aligned}$ $\mathrm{me}_{1 / x}$ | $\sin _{20}^{\sin }$ |  | ${ }_{5}^{18}$ |
| - | $\begin{aligned} & 176 \\ & 100 \\ & 10 \end{aligned}$ |  K4/6 $\mathrm{m} / \mathrm{L}$ | $\begin{gathered} 500 \\ \substack{501 ., 20} \end{gathered}$ |  | $i^{84}$ |

(b) Overtone Oscllators-All Styles

| Prapuancy Range |  |  | Drive Laval in minisation |  |
| :---: | :---: | :---: | :---: | :---: |
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|  | ${ }_{18}^{2490099}$ | $\mathrm{Mc}_{\mathrm{Mc} / \mathrm{L}}$ | i | 1 |

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\begin{aligned}
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\end{aligned}
$$

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\begin{aligned}
& \text { T 143 } 1 \text { в., 34)=. P./P. 2/9. }
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Plays at 7lin. Der sec.
Other speeds if desired.
Other speeds if desired.

- Erase head. Fast motor re-wind or hand re-wind.
- Instantly plays back through gramophone or radio.

MADE BY. THE FIRM THAT MAKES MICROWAVE WAVE-GUIDES FOR VISCOUNTS AND BRITANNIAS


## Gramdeck

GRAMOPHONE TAPE RECORDER
(Dept. WW/805), 29 WRIGHT'S LANE, LONDON, W. 8


| TV AERIALS |  |
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| labgear spiral combi band III TV AERIALS. |  |
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| PL81 ¢olled, amazing 6/- |  |
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| CRMP1, CRM92, MWZ2-7, M W22-14, MW22-14C, MW28-17, MW22-18, | £2/15 | - | - |
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 coramic condensers. $3-10,000 \mathrm{PF}$. List value over 55 .

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A magnificent assortment. Standari carboh

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| 3 ohm. |
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Tested top makes-performance giaranteed. 6 in., $8 \mathrm{in} ., 7 / 6 ; 5 \mathrm{~m} ., 7 \times 4 \mathrm{in}$. $12 / \mathrm{m} ; 10 \mathrm{in}$.

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4 TRANSISTOR AMPLIFIERS, 1 WATT From single 6 v . all-dry battery. Latest
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| 145 CT T 6 | 6BJA | 6L6G | 76 | 10 C 2 | $12 / 6$ | ${ }^{25 L 6 G T}$ |  | ${ }^{836}$ | 16 | EBL31. . $16 /$ | EL3 | LN152 | 8 |  | UCL82. | 121- |
| 1A7GT . - 12/6 | 6BR7 . . 10/6 | 6L7M | 8- | 10 Cl 4 | $9 / 3$ | 25 Y 5 C . |  | B65 |  | EC52 .. $3 / 9$ | EL38 .. 12/6 | I.7319 | 719 | -. $2 / 6$ | UC | 13/6 |
| 1C5GT. . 108 | 6BW8 .. $7 / 9$ | 6L18 | 6 | 10Fl |  | $25 \mathrm{Z4G}$ | 7 | CBL31 | $24 / 4$ | EC90 .. 3/8 | EL41 .. $9 / 3$ | MU14 | 81. | SP61 | UP41 |  |
| 1D6... 9/6 | $\mathrm{6BW7}^{68 \mathrm{C}}$. 616 | ${ }_{6119}^{619}$ | 11/6 | $10 \mathrm{F9} 9$ | 1016 | 2573 | 9/6 | ССН3 | \% | $\text { EC91 } \because 4 / 6$ | ELA2 $\cdot .9816$ |  |  | 8U25 . 12 | UF42 | 16 |
| $1 \mathrm{H5GT}$ 8/9 | $6 \mathrm{Bx8}$.. $5 / 9$ | 6LD3 | 8/9 | $10 \mathrm{L14}$ |  | 25780 | 916 | CL33 | 14)- | $\text { ECC31.. } 9^{\prime} 8$ | FL84 $\quad 813$ | N7 |  | SU2150A 4/6 | UF80 |  |
| 1 L 4 | $6 C 4 \cdots 3 / 6$ | $6 \mathrm{LD12}$ | $7 / 8$ | 10LD3 | 3 | ${ }^{2780}$ | 16/ | CY31 | 9/6 | ECC32.. $3 / 9$ | $\frac{\text { ELS5 }}{\text { GL91 }} \times 11$ | N10 | 11/- | $1 \ldots . .7 / 6$ | UF88 | 816 |
| 1N5C | 6CJ .. 516 | ${ }^{6} \mathrm{LDD} 20$ | $8 / 6$ | 10LD12 |  | 30 Cl | 719 | D63 | $1 / 6$ | ECC33.. $7 / 6$ | EL91 .. $4 / 9$ | N15 | $10 / 6$ | TH30C. . 12/8 | UF86 | 16/ |
| 1R6 | $6 \mathrm{CC6}$.. $4 / 3$ | ${ }^{6 P 15}$ | $8 / 3$ | 10P13. | $2 /$. | 30F5 | $7 / 8$ | D7 |  | ECC34 .. 9/- | EL,95 .. 9 | P41 | 4/6 | U14.... 8)= | UFR9 |  |
| $184 . .$. 8/ | $6 \mathrm{C} 9 \quad \cdots \quad 9 / 8$ | 6P25 |  | 10 P 14 |  | 30FL1 | 916 | D152 | $6 / 6$ | ECC35.. 6/9 | EM34 | P61 |  | U18.... 9 9/ | UL41 |  |
| $185 . . .{ }^{6 / 6}$ | $\mathrm{BClO}^{810} 8 / 8$ | ${ }^{81} 28$ |  | 10 P 18 | $8 / 3$ | 30 Ll | 719 | DA30 | $2 / 6$ | ECC81.: 6/9 | EM80 | PABC80* | $8 / 6$ | $022 . . .$. | ULA4 |  |
| 1T4 $\ldots 5 /$ | 6CD6G.. 18/6 | 697a | $7 / 6$ | 12A6 |  | 30P4 | $12 / 6$ | D100 | $5 /$ | ECC82.. $6 / 6$ | EM81 | PCC84. | 719 | $\text { U24... } 8 / 8$ | UL46 |  |
|  |  | 6Q7GT 8SA7 | 9/3 | 12ATT7 |  | $30 \mathrm{Pl2}$ 30 P 16 | $11 / 8$ | $\begin{aligned} & \text { DACB2 } \\ & \text { DAF91 } \end{aligned}$ | 9/9 | ECC83.. $7 / 6$ | EM84 | PCCS | $9 / 6$ | $\mathrm{U} 28 \text {.... 12/ }$ | UL84 <br> UM80 |  |
| 3A4 ... 61- | 6D2 .... 4 | 6SA7 | 6/0 | 12AT7 |  | 30P16 30 PL | 1318 | DAF91 | 6 | ECC84.. $8 / 9$ | E485 EN31 $\cdots \frac{10 / 6}{18 / \%}$ | PCC89 | $41^{\circ}$ | U26 .... 12/ | UM80 UU6 |  |
| 305 CT 819 | ${ }_{6}^{6 D 3}$ | ${ }_{\text {R }}^{6807}$ |  | $12 \mathrm{AU7.}$ |  | $\begin{aligned} & 30 \mathrm{PLI} \\ & 35 \mathrm{~L} 6 \mathrm{O} \end{aligned}$ | 1316 $9 / 6$ | $\begin{aligned} & \text { DAP98 } \\ & \text { DF33 } \end{aligned}$ |  | ECC85 . . $8 / 3$ | $\begin{aligned} & \text { EN31 } \\ & \text { EYY1 } \end{aligned}$ | PCP80 | 719 | U33.... 11/ | $\begin{aligned} & \text { UU6 } \\ & \text { UUZ } \end{aligned}$ |  |
| 3Q5GT. . 8 | ${ }_{6 F 1}^{6 D}$ | $\begin{aligned} & 68 \mathrm{S7} \\ & 6 \mathrm{SH7} \end{aligned}$ |  | $\begin{aligned} & 12 A X 7 \\ & 12 B A B \text {. } \end{aligned}$ | $7 / 6$ | $\begin{aligned} & 35 \mathrm{LGO} \\ & \mathbf{3 5 W} 4 \end{aligned}$ | , | $\begin{aligned} & \text { DF33 } \\ & \text { DF91 } \end{aligned}$ | . | ECC81 .. $4 / 6$ | EY51 | PCF82 | 919 | U35 .... 8,6 | $\begin{aligned} & \text { UU7 } \\ & \text { UU8 } \end{aligned}$ |  |
| 3v4.... 8 | 6F6G ... $8 / 8$ | 68J7 |  | 12BE6. |  | 35 Z | $61-$ | DF9\% | 13 | ECP80.. ${ }^{\text {E }}$ 10/6 ECP82 10/6 | EY86 .. $8 / 9$ |  |  |  | पU9 | 7\% |
| 5R4G .. 8'6 | 6F6M .- 7 | 68 C 7 |  | 12BH7 |  | 357 | 6 | DH63 | 716 | ECH42.. 819 | EZ35 .. 8/6 | PCL4 | $2 / 6$ |  | UY41 | 6 |
| 5049 . 5/9 | $6 \mathrm{Fl2}$-. $4 /-$ | 68L7CT | 19 | 12 C 8 | ${ }^{6} 6$ | 42 | 76 | DH77 | 716 | ECH81 ... 813 | E240 | PEN25 |  | U52 .... 8/3 | UY85 | 713 |
| 5 F 4 C . . 1016 | 6F13 -- $5 / 9$ | 68N7GT | 51 | 12 EL | 126 | 5005 | $10 \cdot 6$ | DK91 | 8 | ECL80.. 816 | E241 E280 |  |  |  | VR150/30 | 7\% |
| 5Y3G ${ }_{\text {ch }}$ | 6F14 | 68 S 7 | $6 / 6$ | 12J5GT | $3 / 6$ | 50LAG |  | DK92 |  | ECLÅ2. . 11 | E28 | PEN 48 | 5/ | U78 | W ${ }^{\text {W }} 17$ | 13 |
| $\text { 5Y } 3 \text { G }$ | $6 \mathrm{~F} 15$ |  |  | 12 K 7 GT 12 KgTT | 12/- | 54 |  | DL35 |  | F35 .. 2/6 | GT10 | PEN383 | $12 / 6$ | U191 .. 9/8 |  |  |
| SZHGT... 11/ | 6F19 ... $7 / 6$ | 6V60t | $6 / 8$ | $12 \mathrm{Q} \mathrm{GTT}^{\text {d }}$ | 61- | 61 BT | 1.6 | DL82 | 716 | EF37 .. 6/6 | Gz32 ... 9/- | PL33 | \% | U281 $\cdots$.. $8 / 6$ | W77 |  |
| 647.... $8 / 8$ | 6F33 | 6X 4 | - | 12897. | 6/ | 618PT | 11. | DL92 |  | EF39 $\quad . .13 / 6$ | 9234 ${ }^{\text {a }}$ 12/6 | PL38 | $13 / 6$ | $\begin{array}{lll} \text { U282 } & . . & 22 / 7 \\ \text { U301 } \end{array}$ | W81 |  |
| 6A8 ${ }^{\text {cht }}$ | $6 \mathrm{H6}$.... 21- | 6x50 | 5/ | 128.57 |  |  | $4{ }^{\prime} 6$ | DL94 |  | EF41 | $\begin{array}{lll}\text { az37 } & . & 10 / 6 \\ \text { HABCs0 } & \\ \text { 9/6 }\end{array}$ | ${ }^{\text {PLL38 }}$ | $\begin{aligned} & 14 / 6 \\ & 10 / 6 \end{aligned}$ | $\begin{array}{lll} \mathrm{U} 301 & \cdots / 6 \\ \text { V329 } & \cdots & 12 / 6 \end{array}$ | - 61 M | $6$ |
| 6AB8 .. 8/6 | 6J5 $\ldots . .43$ | 6X5at | 66 | $12 s \mathrm{~K}^{2}$ |  | $\begin{aligned} & 78 \\ & 8 \end{aligned}$ | I | $\begin{aligned} & \text { DLD6 } \\ & \text { EA50 } \end{aligned}$ |  | EF42 |  | ${ }^{\text {PL818 }}$ | $\begin{array}{r} 10 / 6 \\ 7 / 8 \end{array}$ | $\begin{array}{rrr} \text { U329 } & \ldots & 12 / 6 \\ \text { U403 } & \ldots & 9 / 6 \end{array}$ | $\begin{aligned} & \mathrm{X} 63 \\ & \mathrm{X} 65 \end{aligned}$ | $18$ |
| $\begin{array}{lll}\text { 6AC7 } & . . & 4 / 8 \\ 6 A K 5 & \\ 6 / 8\end{array}$ | ${ }_{6}^{6 J 5 G}$ |  | $11 / 6$ | SSN7OT |  | $\begin{array}{\|l\|} 80 \\ 83 \end{array}$ | 6 | $\begin{aligned} & \text { EA50 } \\ & \text { EABC80 } \end{aligned}$ | $9 \mathrm{9d}$. | EF50-BR $1 / 6$ | $\begin{array}{ll}\text { HLHDD } & 9 / 6 \\ \text { HVR2.. } & 6 / 6\end{array}$ | PL83 | $7 / 8$ | $\begin{array}{lll} \mathbf{U 4 0 3} & \therefore & 9 \\ \mathbf{U 4 0 4} & \therefore & 9 \end{array}$ | $\begin{aligned} & \times 65 \\ & \times 66 \end{aligned}$ |  |
| 6AK5 .. 8/6 | J59 | 783 |  | $\begin{aligned} & 1487 \\ & 19 \mathrm{AC} \end{aligned}$ | / 6 | $\begin{aligned} & 83 \\ & 90 \mathrm{Av} \end{aligned}$ | 916 $4 / 6$ | EABC80 | 7/6 | EF50RED 2 \% | HVR2 KT32 | PX25 | $8 / 6$ |  | $\begin{array}{r} \times 66 \\ \times 76 \end{array}$ |  |
| 6AM5 .. 48 | 6J7M | 787 | 16 | 19BG6G | 18\% | 185BT | $16 \%$ | EAP42 |  | EF50 USA 2/8 | KT330 | PY31 | 8 | UAF42. | X78 |  |
| ВАМО .. 4/\% | 6J7G .. 5l= | 7 BS | 12/ | 20D1 | 816 | 323A | $15^{\prime}$ | EB34 | $1 / 6$ | EF54 .. 316 | KT88.. 9/ | PY32 | 12/6 | UB41 | $\times 79$ |  |
| 6AT6 .. 7/6 | 0.179T $7 / 8$ | $7 \mathrm{7c5}$ | 7/8 | $20 \mathrm{~F}^{2}$ | 916 | 723A | 351 | EB41 | $7 /$ | EF80 .. 5/8 | KT44 | PY80 | 7 | UBC41... 81 | Y83 |  |
| 6AD6 .. 9/6 | 6 K 6 GT b/ | 7 Ca | 76 | 20 Ll | 12/6 | 807 BR | $4 / 6$ | E891 | 4/- | EFA5 .. 76 | KT45 .. 818 | PY81 | 71- | UBC81.. $12 /$ | 214 | 19 |
| 6B7 | 6K7 | 7 FF | 6 | 20P1 |  | 907U8 | 8/ | EBC3 | $8 /-$ | KP88 .. 11/0 | KT01 - ${ }^{\text {8/- }}$ | PY82 |  | UBF80.. 86 | 283 |  |
| ${ }^{\text {B B }}$ B | 8K70T | 7 7 7 |  | 20 P 3 |  | 808 |  | EBC33 |  | EF89 $\quad \cdots \quad 8 / 6$ | KTaA . 15/* | PY83 |  | UBF89.. | 286 | 6 |
| 6BA6 6BE6 | $\begin{aligned} & 6 \mathrm{KSG} \\ & 6 \mathrm{~K} 8 \mathrm{OT} \end{aligned}$ | 787 |  | $20 \mathrm{P3}$ |  | $\begin{aligned} & 818 \\ & 8050 \end{aligned}$ |  | EBC41 |  | EF92 $\quad . .418$ | KTW61 $5 / 6$ <br> KTW63 $5 / 6$ | $\begin{aligned} & \text { P230 } \\ & \text { R18 } \end{aligned}$ | $816$ | UCC85.. 88 UCFSo. . 16/- | $297$ $\bar{Z} 152$ |  |
|  | $\begin{aligned} & 6 \mathrm{~K} 80 \\ & 6 K 25 \end{aligned}$ | $7 \times 4$ |  | 20 P |  | 7198 | 6 |  |  | EF92 .. 48 | KTze3. |  |  | Cr |  |  |

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WHEATSTONE BRIDGE in a beautiful pak case centre zerogalvanometer 2.5 mA .
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HEAVY DUTY SLIDING RESISTORS. $26 \Omega$ 6a., Double Tube Slider Control, 45/$73 \Omega$ i-3a. Completely enclosed. SIngle Tube Slider, 35/a $120 \Omega$ 1.75-0.9a. Completely Enclosed. Single Tube Slider Control, 30/$70 \Omega$ 2.9-0.65a. Double Tube Geared Drive Control, 32/6. $1.25 \Omega, 25 \mathrm{a}$. Geared Drive Control, 27/6. $0.4 \Omega 25$ a, Geared Drive Concrol, $17 / 6$. II $\Omega$ 4.5a., $12 / 6$. $3 \Omega$, 10 a ., $12 / \mathrm{b}$. $1.2 \Omega 15 \mathrm{a}$. $10 / 6$. $1 \Omega$ i2a., $8 / 6$. All single Tube Sider Control. $5.3 \Omega$ 8a. Fixed $10 /-605 \Omega$ $2.8-0.452$. Fixed, $10 /-$. Carr. on all Resistors, 3 -
AMERICAN CAPACITORS. 4 mfd , 4,000 . wkg., $17 / 60.1 \mathrm{mid} .7,500$ v. wkg., 6 mid . $330 \mathrm{v} . \mathrm{A} . \mathrm{C}$. wkg., 8/6 Pyranol 8 mid .300 v . wkg., tubular, 8/6. British types 8 mfd .400 v . wkg. at 71 deg. C., 5/6. Nitrogol, $8 \mathrm{mfd}, 750 \mathrm{v}$. wkg. at 71 deg. $\mathrm{C}, 8 / 6.8 \mathrm{mfd} .250 \mathrm{v}$. wkg. at 71 deg. C $4 / 6.4 \mathrm{mfd} .800 \mathrm{v} . w \mathrm{~kg}$. at 160 deg . F., $3 / 6$. $0.5 \mathrm{mfd} 2,000$ V. wkg. at $50 \mathrm{deg} . \mathrm{C} ., 2 /-$. All
VENNER EIGHT-DAY CLOCK-WORK TIME SWITCHES. One make and one Break every 24 hours. 5 amp. 230 volt switch contacts. Complete with Key and Mounting Bracket in Perfect Condition, 29/6, P.P. 1/6. SPECIAL OFFER OF B.A. SCREWS, STEEL. 4 BA $\frac{1}{6 i n}$. C.S., 15 gross 27/6. P.P. 3/Or $2 / 6$ per gross. Post free. 4 BA fin. stee C.S., 20 gross cartons, 32/6. P.P. 3/-. Or $2 / 6$ per gross, Post free. 2 BA brass lin. C.S., 5 gross cartons 15/-. P.P. 21-, 4 BA steel R.H. It in 5 gross cartons $15 /-$ - P.P. 2/-. NUTS, VÖLTS, WASHERS. Special bargain offer. $5 /$ carton 2, 4,6 BA nuts, bolts and washers.
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HEAVY DUTY AUTO TRANSFORMERS. Tropically rated at 5 kVA Tapped 250, 240, 230, 220, 120, 115, 110,105 volts. Compietely enclosed in metal case. Size $23 \times 14 \times 1 /$ inches. Weight approx. 2 ewt. Brand new E15/0/0 ex Warehouse.
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A.C. input 100. 260 voles 45-65 $\mathrm{C} / \mathrm{s}$. output 24 volts
10 amps. at max. ambient $t \in m$ pera $131^{\circ} \mathrm{F}$. buart
guaran$t$
$m a x$
$m$ output
of 20
amps. All components turers an this current. The charger is fitsed with 20 amp . fuses on the D.C. output, 10 amp . luses on the A.C. input. 2 tin. 0-20 M.C. D.C. ammeter. On/off full charge/trickle chargeswitch. Heavy duty outpuc terminals and mains neon indicator lamp. Behind control panel are mounted full charge ballast and triekle charge resistances.
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purpose L.T. supply unit.
Supplied brand newat a fraction of maker's price. Size: 2 ft . $\times 1 \mathrm{ft}$. $3 \frac{1}{2} \mathrm{in}$. $\times 2 \mathrm{ft} 8 \mathrm{in}$ Weight: 141 lbs .
E22-10-0 Ex warehouse.


WESTINGHOUSE L.T. SUPPLY UNITS. Type No. 139. A.C. input, $200-250$ voles. D.C. output, 36 volts, 18 amps. Continuous Rating at 50 deg. C. Fitted with Input and Ourput Fuses and Mains On/Off Switch. Size of cabinet, $26 \times 19 \times 14 \mathrm{in}$., $\mathrm{E} / 7 / 10 / \mathrm{F}$. Ex ware. house

L.T. SUPPLY UNIT No. 19 YA 8087 A.C. input $100-250$ v. D.C. output tapped 12/24 voles, continuous eropical rating, 3 amps. Buile-in metal case $17 \times 7 \times 6 \frac{1}{2}$ in., with 保es Buite-in metal case $17 \times 7 \times 6 \frac{1}{2}$ in.
and with iteh. An ideal L.T. supply unit for and switeh. An conting relays, contactors, battery charging operating relays, contactors, battery charging
etc. In perfect condition. $\mathbf{6 3 / 1 / 7 / 6 . ~ C a r r . ~} 7 / 6$. G.E.C. L.T. SUPPLY UNITS TYPE O.S. 1773 G.A. A.C. input 200-240v. D.C. outpur 24 voles 10 smps. Tropically rated. Built-in metal case size $20 \times 15 \frac{1}{5} \times$ loins. Supplied Brand new in Maker's cases, $\{13 / 10 / \%$, ex

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We deaign and manutacture MANS AND O/P TRANSFORMERS to Individual apec ONLY A FEW ITEMS ARE LISTED FROM OUR COMPREHEN SIVE STOCK. WRITE NOW FOR FULL BARGAIN LISTS, 3d. Terms: C.W.O. or C.O.D. post and pocking up to \(1 / \mathrm{lb}\). 7 d .: 1/b. \(1 / 1 ; 3 / \mathrm{b} .1 / 6: 5 / \mathrm{b} .2 / \mathrm{-} ; 10 \mathrm{lb} .2 / 9\).
\(T S\) RADIO COMPONENT SPECIALISTS
70 BRIGSTOCK RD.,THORNTON HEATH, SURREY Established 1946. Tel: THO 2188 Hours: 9 o.m. -6 p.m. 1 D.m. Wednesday


Made for the Ministry by leading manufacturers (e.g., Erskine \& Hartley Electromotives) this fine instrument is suitable for the examination of waveforms from two cycles to ten megacycles. It is extremely well designed and incorporates such desirable features of construction as potted " C " core transformers and paper smoothing capacitors for complete reliability. No electrolytic condensors are used.

> TIME BASE
> Y PLATE AMPS. CAL. MARKERS SIZE \& WEIGHT EXTERNAL PROBE POWER SUPPLIES

2 cps. to 750 Kcs . \(5 \mathrm{Mc} / \mathrm{s}\). bandwidth ( 3 dB ). \(1 \mu \mathrm{sec}\). and \(10 \mu \mathrm{sec}\). 13 in. \(\times 10 \mathrm{in} . \times 22 \mathrm{in} .58 \mathrm{lbs}\). For RF measurements Internal (AC mains)
All instruments are in first class condition and are carefully checked and tested before despatch. Mains connector, test leads, probe and circuit diagram are neatly contained in the detachable front cover.

\section*{\(£ 25\) 운}

\section*{VIDEO OSCILLATOR TF885A}


Frequency coverage in two ranges: 25 cps . to 30 \(\mathrm{Kc} / \mathrm{s}\). and \(30 \mathrm{Kc} / \mathrm{s}\). to \(5 \mathrm{Mc} / \mathrm{s}\). (sinewave) and 50 cps . to \(150 \mathrm{Kc} / \mathrm{s}\). (squarewave). Output 1 watt into \(1000 \Omega\) (sinewave) and 64 volt peak to peak (squarewave). Operates from A.C. mains. MODERN equipment in first class electrical and mechanical condition. \(\$ 100\) carr. paid.

\section*{MARCONI VIDEO OSCILLATOR TF410C}

An earlier design of video oscillator having the same frequency coverage as the TF 885. The output meter is a circular \(3 \frac{1}{2} \mathrm{in}\). instrument. For AC mains operation. In good condition and working order. \&35. Carriage paid.


Lmpedance from \(2.5 \Omega\) to 20,0000 in 40 ateps. 100 W . to 5 watts. Four ranges 0.5 mW ., \(0-50 \mathrm{~mW}\)., \(0-500 \mathrm{~mW}\), and \(0=5\) Watte. First clana condition. Tested. \(89 / 19 / 6\). Cartiage \(7 / 6\).
\begin{tabular}{|c|c|c|c|}
\hline D.c. Volts & A.c. Volts & D.c. Current & A.C. Current \\
\hline 150 mV . & 7.5 V . & \(15 \mathrm{~m} / \mathrm{A}\). & \(75 \mathrm{~m} / \mathrm{A}\). \\
\hline 300 mV . & 15 V . & \(30 \mathrm{~m} / \mathrm{A}\). & \(150 \mathrm{~m} / \mathrm{A}\). \\
\hline 1.57 . & 75. & \(150 \mathrm{~m} / \mathrm{A}\). & \(750 \mathrm{~m} / \mathrm{A}\). \\
\hline 3 V . & 150 V. & \(300 \mathrm{~m} / \mathrm{A}\). & 1.5 Ampa. \\
\hline 15 V . & 300 V . & 1.5 Ampu. & 7.5 Arnpe. \\
\hline 30 V . & 600 V. & 3 Amps. & 15 Ampar. \\
\hline 130 V . & 730 V . & 15 Amps. & \\
\hline 300 V . & 1.5 KV & 30 Ахррs. & Resistance \\
\hline 730 V . & & & 0-1000 ohms. \\
\hline 1.5 KV & & & 0.10 K ohms. \\
\hline
\end{tabular}

\section*{SPECTRUM ANALYSER TF984/1}

For viewing the spectra of " \(S\) " band transmitters in the range \(2,900-3,150 \mathrm{Mc} / \mathrm{s}\). These are in virtually new condition but are NOT tested. Operation is from 180 volts 500 cps . power supplies. £30 carriage paid.

\section*{MARCONI B.F.O. TF602A}

Frequency range 10 cps . to \(12,000 \mathrm{cps}\). Operation is from AC mains. Output indication by magic eye Incorporates 50 cycles check. A reasonably compact instrument useful for general audio testing. Fair condition, tested and working perfectly, £6/19/6. Carriage 10/6.

\section*{FERRANTI TESTMETER TYPE Q}

Volts 0 to \(30,150,600\) A.C./D.C. with additional \(0-3\) V. D.C. and \(0-15 \mathrm{~V}\). A.C. ranges; milliamps 0 to \(7.5,30,150\) and \(750 \mathrm{D} . \mathrm{C}\).; ohms \(0-25 \mathrm{~K}\). Accuracy BSS 1st grade. 500 ohms per volt. With leads, prods, battery and instructions. In velvet lined \(4 \times 7 \times 3\) in. case. Brand new condition, perfect working order \(52 / 6\). Post \(2 / 6\).
G.E.C. SELECTEST DIII


This teatmeter haa exactly the same ranges as the Avo "D." The scale is even targer. Those we offer are is first class condition, completely overhauled and carefully tested prior io despatch. Complete pith battery, teat leads and instructions. \(\mathbf{\varepsilon 7 / 1 0 / \%} \boldsymbol{P}\) : \(\boldsymbol{P}\).
\(3 / 6\).


CRYSTAL CALIBRATOR No. 10 A crystal controlled heterodyne wave--
meter covering \(500 \mathrm{Ke} / \mathrm{s}\) to \(10 \mathrm{Mc} / \mathrm{s}\). meter covering \(500 \mathrm{Kc} / \mathrm{s}\) to \(10 \mathrm{Mc} / \mathrm{s}\).
( Harmon .
R \(15 \mathrm{~m} / \mathrm{a}\). and 12 v .0 .3 A . d.c. but can be easily modified for 120 v . and 1.4 v . working. Size \(7 \times 7 \frac{1}{2} \times 4 \mathrm{in}\). First class condialon, \begin{tabular}{l} 
59/6. Post \(3 / 6\). \\
ind \\
\\
\hline
\end{tabular}

CHOKES. Parmeko 5 H. \(200 \mathrm{~m} / \mathrm{amps}\)., 6/6. HRO chokes, \(17 \mathrm{H} ., 80 \mathrm{~m} / \mathrm{mpss} ., 7 / 6\). AR-88 chokes, 15 H., 90 m/amps., \(8 / 6\). Parmeko \(8 \mathrm{H} ., 100 \mathrm{~m} / \mathrm{amps} ., 7 / 6\). Postage any type, 1/6.

\section*{Q'5ER (BC-453)}

This Command Receiver covers 190-550 \(\mathrm{Ke} / \mathrm{s}\).-(1.F. \(85 \mathrm{Kc} / \mathrm{s}\).) and is ideal for double superhet conversion erc. Supplied
BRAND NEW in original cartons, with BRAND NEW in original cartons, with
all 6 valves and CIRCUIT. \(89 / 6\). Post \(3 / 6\). SELENIUM BRIDGE RECTIFIERS. Funnel cooled. A.C. input 45 v. RMS. D.C. output 30 v .10 amps. BRAND NEW. Boxed. 45/\%. Post \(3 / 6\).
HEAVY DUTY L.T. TRANSFORMERS. (Gresham.) Latest type potted. oil filled, Pri. \(230 \mathrm{r} .50 \mathrm{c} / \mathrm{s}\). Sec. 0-70-7580 v. 4 amps. Size \(5 t \times 4 \frac{1}{2} \times 6 / \frac{1}{2}\) in. high. Gardner's Transformer. Tapped mains input. Secondary 12 volts RMS (C.T.). 30 amps. Housed in sheet metal case \(9 \frac{1}{2} \times\) \(8 \downarrow \times 6 \frac{1}{i n}\), high. BRAND NEW. 72/6,
carr. \(7 / 6\).

DUAL PURPOSE TRANSFORMERS (Gresham.). Pri. 230/250 v. Secs. 240-
 \(0-240 \mathrm{v}\). 1.5 amps., 5 V . 12.5 amps.0 5 V . FORMER, to obtain TWO 240 V 360 watt lines. Potted, oil-filled, \(7 \times 7 \frac{1}{2} \times 10 \frac{1}{2} \mathrm{in}\). high. Wt. 50 lb . BRAND NEW. E3/10/-, Carr. 10/-.
ADVANCE CONSTANT VOLTAGE TRANSFORMERS. Input 190-260 \(50 \mathrm{c} / \mathrm{s}\). A.C. mains. Output 230
150 watrs. \(88 / 10 /=\) Carr, \(5 /-\) 150 watts. E8/10/-. Carr. 5/-

\section*{STANDARD TRANSFORMERS}

Vacuum impregnated, interleaved, E.S screen, universal mounting. Sizo \(4 \times 3 \frac{1}{2} \times\) \(2 \frac{1}{2} \mathrm{in}\). ALL BRAND NEW. \(18 / 6\) cach Pose \(1 / 6\).
Type 1. \(250-0-250 \mathrm{v} .80 \mathrm{~m} / \mathrm{a} .6 .3 \mathrm{v} .3\) A., tapped at 4 v .4 A., 6.3 v .1 A. tepped at Type 2 . 5 V. 2 A.
Type 2. As above, but \(350-0-350\) \(80 \mathrm{~m} / \mathrm{a}\).
Type 3. 30 v. 2 A., tapped at 12,15, 20 and 24 v ., to give 3-4-5-6-8-9-10 v. etc. Ideal for models, trains, ete
6-VOLT VIBRATOR PACKS. HRO type, 180 v . D.C., \(65 \mathrm{~m} / \mathrm{mmps}\). BRAND NEW. 29/6, post 3/6. Type PU2, 2CO V. D.C. \(100 \mathrm{~m} /\) amps, , with OZ4 rectifier.
BRAND NEW. \(25 /\). Post FREE. BRAND NEW. \(25 /\)-. Pose FREE. CRYSTALS \(200 \mathrm{Kc} / \mathrm{s}\). American GEC,
\(10 /\) each. \(100 \mathrm{Kc} / \mathrm{s}\). RCA bars. \(15 / \mathrm{m}\). ADMIRALTY HT TRANSFORMERS

 m/amps., 375 .. \(250 \mathrm{~m} / \mathrm{amps}\).). plus two 5 V. \({ }^{3}\) Amp. Vrectifier windings. We 25 tb . Made 1953. BRAND NEW. Original boxes. 45/-. Carr. 5/-.
INSTRUMENT TRANSFORMERS. 230 v. A.C. input. Ourpurs 0-65-130-195 . \(85 \mathrm{~m} / \mathrm{amps} ., 6.3\) v. \(5 \mathrm{amps} ., 6.3\) v. 0.3 amps. Shrouded. Size \(3 t \times 3 \ddagger \times 3\) itin. high. \(15 /-\), post FREE.
ARB8D MAINS TRANSFORMERS. Input 110-240 v. Oucput 345-0-345 v \(125 \mathrm{~m} / \mathrm{amps}, 6.4 \mathrm{v}, 0.4 \mathrm{amps} ., 5 \mathrm{v} .2 \mathrm{amps}\). \(4 \frac{3}{3} \times 4 \frac{1}{2} \times 5 \frac{1}{2}\) in. high. We. 12 Ib . Porred. Tag ends. RCA BRAND NEW. Boxed.

\section*{MARCONI CRI00}

Completely overhauled. In perfect working order. LOOK LIKE NEW. E21.
Later model with Noise Limiter, 25.
Carr. Eng, and Wales \(30 /\)-. Send S.A.E. for full detalls.

\section*{RCA AR-88 SPEAKERS}

A high quality 3 ohm unit fitted into heavy gauge black crackled steel cabiner, size \(10 \frac{1}{2} \times 1 \frac{1}{2} \times 6 \mathrm{in}\). Fitted with rubber feet and 6ft. lead. Ideal for extension speaker, CR100, etc

CRI50 COMMUNICATIONS RECEIVERS Covers \(2-60 \mathrm{Mc} / \mathrm{s}\). in 5 ranges. Double superher, with 2 EF50 R.F. stages, \(500 \mathrm{Ke} / \mathrm{s}\). erystal calibrator H.T. stabiliser, "S" R.F. stages, \(500 \mathrm{Ke/s}\). erystal calibrator
and
valve-check meter, audio filter, etc. Vabiable selectivity, using TWO double-crystai band-pass filters. External power supply required, 300 v. D.C. \(65 \mathrm{~m} / \mathrm{Amps}\), and 6.3 v .3 .7 Amp . Size and appearance similar to CR100. In superb condition and working order, E45. Carr. 30/-

\section*{LOUD HAILER EQUIPMENT}

IDEAL FOR CROWD CONTROL, FACTORIES, FETES, ETC. CONIDEAL FOR CROWD CONTROL FACTORIES, EETES, ETC. CONWITH MICROPHONEE HEADPHONES AND SPARES, OPPRLATES WROM 12 VOLTS D.C. (OR 8 VOLTS D.C. WTYH SLIGHTLY REDUCED OUTPUT), CONSUMNG ONLY 3 AMPS: OUTPUT POWER 8 WATTS ALS TESTED AND WORKNG, BUT SLIGETLY SOLLED. A GENDINE bargain. fa/19/6. CARRIAGE 25/6.


MINIATURE 373 IF STRIPS. For FM tuner described in "Practical Wireless." Complete with 3 of EF91, 2 ol EF92 and I of EB9I. A rresh release enables us to offer these once again. BRAND NEW. Complete reprint of conversion instructions and circuit supplied free. 35/a OR less valves, 12/6. Post, either, \(2 / 6\).
T.C.C. VISCONOL.CONDENSERS. \(8 \mathrm{mFd}, 800\) D.C. wkg. at 71 deg. C. CPI52V. Size \(3 \times 17 \times 5 \mathrm{in}\). high. BRAND NEW. Boxed. \(8 / 6\) each post paid.

MINIATURE RELAYS (ALL BRAND NEW and BOXED) G.E.C. sealed, wire ends, \(670 \Omega, 2\) H/D makes, M 1099 … 15/G.E.C. sealed, wire ends, \(670 \Omega, 4\) C/overs, platinum, M1092 \(19 / 6\) G.E.C.sealed, wire ends, 5000 , 2 C/overs, platinum, MI \(05217 / 6\) Siemens High Speed, IK + IK \(\Omega\), I Clover.

\section*{HRO SENIOR RECEIVERS}


Complete with ALL NINE general coverage plug-in coilsets for \(50 \mathrm{Kc} / \mathrm{s}\), to \(30 \mathrm{Mc} / \mathrm{s}\). Instruction booklet, and círcuit, but less externai power supply unit. Table models, as new condition, 21 GNS. Rack mounting, 18 GNS. Packing and carriage 22/- extra. Send S.A.E. for further details. HRO POWER PACKS. \(115 / 230 \mathrm{v}\). A.C. mains input. Tested, and in good condition. Table or rack, 69/6. Post 4/-,

\section*{CHARLRS}
\(\|\) UPPER LONDON, W.C. 2
TEMple Bar 0545 BRITAIN
(Radio)
TTD.

One minure from Leicester Sq. Station (Up Cranbourne St,


\section*{SANGAMO.}

\section*{WESTON} VOLTMETERS S61. Dual range \(0-5\) and \(0-100 v\) D.C. FSD \(1 \mathrm{~m} / \mathrm{A}\) 3in. scale. Recent manufacture. Ideal for schools. Complete in superquality canvas carrying case, with test BRAND NEW. Boxed \(27 / 6\). Post \(2 / 6\).
ELECTROSTATIC METER Dia. \(6 \frac{1}{2}\) ins. reads \(5-18.5 \mathrm{Kv}\). Manufactured 1953. Contained in wooden case \(10 \times 10 \times 9\) ins. high. \(69 / 19 / 6\). Post paid.
SANGAMO - WESTON ANALYSER E772. A useful multi-range meter Thoroughly overhauled and in perfect working order. For full details see previous adverts. E7/10/=. Carr 4/6.
AVO LC \& R BRIDGES. Capacity 5 pFd to 50 mFd . Resistance 5 ohms to 50 megohms. Inductance can be measured against external scandard. Balance is indicated on a meter, which can be used as a valve voltmeter from 0.1 to 15 v . Leakage test and Power Factor scale. For use on A.C. mains. Tested and guaranteed €8/10/-. Post 3/6.

\section*{HICKOCK I-I77 VALVE TESTERS.} Checks dynamic murual conductance, shorts, emission, gas, and noise. For UX4, UX5, UX6, UX7, Octal, Loctal, B7G, and Acorn types. Portable, in wooden carrying case \(15 \frac{1}{2} \times 8 \times 5 \frac{1}{2}\) in. Wt. \(13 \frac{1}{2} 16\). BRAND NEW Complere with instruction book and valve testing charts. For 117 v. A.C. 10 gns. Carr. \(7 / 6\). Matching auto. transformers for 230 v. A.C. \(12 / 6\).

MARCONI SIGNAL GENERATORS \(85 \mathrm{Kc} / \mathrm{s}\). to \(25 \mathrm{Mc} / \mathrm{s}\). A.C. mains operation. In fair condition and good working order. TFI44F. €40, TFI44G. \(£ 50\).

RIIS5 RECEIVERS. With latest type super slow-motion drive. In good condition and perfect working order. redition and perfect working order. \({ }^{\text {aligned and air tested. Model " }}\) E7/19/6. Model "L" (covers trawler and shipping bands) ( \(12 / 19 / 6\). Carr. (either) 10/6. Send S.A.E. for detalis of sets and power units, or \(1 / 3\) for illustrated booklet.
SCR522 TRANSMITTER/RECEIVERS 100-150 Me/s. Comprises BC624A rec., and BC625 erans. with valves, and in good condition. BC624A, less relay 19/6. With relay, 25/-. BC625 22/6. These two, on rack 47/6. Carr. 7/6.
MOVING COIL PHONES. Finest quality Canadian, with chamois ear-muffs and leather-covered headband. Wich lead and jack plug. Noise excluding and supremely comfortable. 19/6. Post \(1 / 6\).

VITAVOX PRESSURE IJNITS TYPE N. 20 watts. P.M. Heavy ducy. BRAND NEW, boxed. 89/6. Carr. 5/6.

> RESISTORS

Morgan " T" ( \(\frac{1}{3}\) watt) and "R " (I watt) Latest sypes, all BRAND NEW. 100 - Post I/-

HEAVY DUTY SLIDER RESISTORS. \(1.25 \Omega 20\) A., \(12 / 4\), pose \(3 / 6\). I \(\Omega 12\) A., \(8 / 6\) ZENITH ÁDJUSTABLE \(25 \Omega\) 4 A., \(8 / 6\). Post 2/6.
PRECISION RESISTORS. I Megohm \(1 . \%\) I watt wire wound. Ex-U.S.A BRAND NEW. \(10 / 6\) per dazen.

\section*{DC/AC CONVERTERS. Input 12 v .} D.C. Output 230 v. \(50 \mathrm{c} / \mathrm{s} . \mathrm{A} . C_{\text {. as }}\) 135 watts. Fitted with \(0-300\) v. A.C. \(2 \frac{1}{2}\) in. meter and slider resistor for voltage adjustment. In stout wooden carrying case with lid. Perfect working order, 69/19/6. Carr. 10/6.
24 v. Input 230 v. A.C. \(50 \mathrm{c} / \mathrm{s} .100\) watts output. In grey metal case. BRAND output. In grey metal
NEW. 92/6. Carr. \(7 / 6\).
RADIATION METERS. Portable dose. rate meter, containing modern type rectangular 50 microAmp meter, CVX 494 lectromerer yalve, tec. BRAND NEW. In canvas carrying case. \(\mathbf{6} 3 / 19 / 6\). Post \(2 / 6\). For details of other equipment, see our previous adverts.

\section*{UNIVERSAL AVOMETER}


\section*{WESTON MODEL 772 TESTMETER}

\begin{tabular}{|c|c|c|}
\hline A.C. VOLTS & D.C. & A.C. CUR- \\
\hline 2.5 v . & CURRENT & RENT \\
\hline 10 v . & 100 microla. & 500 ma . \\
\hline 50 v . & 1 ma . & 1 amp . \\
\hline 250 v . & 10 ma . & 5 amp . \\
\hline 1,000 v. & 50 ma . & RESIST- \\
\hline D.C. VOLTS & 100 ma . & ANCE \\
\hline 2.5 v & 500 ma . & 100 ohms \\
\hline 10 v . & OUTPUT & 1,000 olims \\
\hline 50 v . & METER & 100k. ohms \\
\hline 250 v. & & 10 megohms \\
\hline
\end{tabular}

Supplied in perfect working order complete with internal batteries. \(\quad \mathbf{7 / 1 0 / F}\). P/P. 4/-.

FIELD TELEPHONES TYPE F. Generator bell ringing. Supplied complete with batteries, fully tested, and complete with wooden carrying case. \(59 / 6\) each. P/P. 3/6.
24 AMP. VARIAC TRANSFORMERS. 230 V input. Variable output \(185-250\) volts or \(185-250\) volts input, 230 voles out. \(61210 / \mathrm{e}\) each. P/P. \(10 \%\) MUIRHEAD PRECISION STUD SWITCHES. 4 bank, 4 pole, 24 positions. New, boxed, \(17 / 6\) each. P/P. \(1 / 3\).

OSCILLOSCOPES TYPE II. Compact little 'scope utilizing 3in. CRT with all standard controls, switched time base, etc 200/250 voles A.C. operation. Not brand new but In good condition, fully checked. These require no modification. E5/19/6 each. P/P. 7/6.
E.M.I. POTTED MIC. INPUT TRANSFORMERS. High quality. 50 : 1 ratio, \(4 / 6\) each. P/P. 9d.
LEACH 12 VOLT AERIAL CHANGEOVER RELAYS. Double pole, \(7 / 6\) each. P/P. 9 d AMERICAN H.T. BATTERIES. Tapped 90 v., \(67 \frac{1}{2}\) v., 45 v., \(22 \frac{1}{2} v\). New, \(5 /\) each. P/P.
\(\qquad\)
8 RANGE SUB-STANDARD D.C. AMMETERS. Ranges, 1.5 3, 7, 15, 30, 60,300 and 450 amps. Bin. mirror scale. Meter housed in polished teak case. Supplied complete with all shunts and leather carrying case. E/5 each. P/P. \(7 / 6\).

1,000 WATT MAINS ISOLATION TRANSFORMERS. 230 to 230 volts. Heavy duty, exAdmiralty. New boxed, 65 each. P/P, 10/-
750 WATT AUTO TRANSFORMERS. Tapped from 110 to 230 volts. Fine heavy duty type, \(69 / 6\) each. P/P. 5/-
DEAF-AID EAR-PIECES. 250 ohm imp. 4/6; 1,000 ohm imp. 7/6. P/P. 6d:
R.C.A. PLATE TRANSFORMERS. Input 200/250 volts 50 cycles. Output 2,000/1,500/0/ \(1,500 / 2,000\) volts \(500 \mathrm{~m} / \mathrm{a}\). Supplied brand new in transit cases, C6/10/- each. P/P. 10/-
R.II55 RECEIVERS MODEL B. Perfect working order, fully tested, \(£ 7 / 19 / 6\) each. P/P. 7/6. Combined power pack and output stage, 85/- extra.
AR. 88 WAVE CHANGE SWITCH ASSEM. BLY. Brand new with screens. 17/6 each. P.P. 2/6.
R.II55 N TYPE DRIVES. Improved geared version new, \(12 / 6\) each. P/P, \(1 / 6\).
POST OFFICE TELEPHONE HAND. SETS. Std. type, new boxed, \(12 / 6\) each. P/P. 1/6.

\section*{METER BARGAINS}
\({ }_{25}^{25}\) microamp D.C. M/C fluah rd. 21 in .
 50 microamp. D.C. M/C. proi. rd. 2 lm . 100 micrommp. D.C. ar C. fulh rd. 3 in. \(500 / 01500\) mucroamp. D. C. \(M / \mathrm{C}\). proj. rc . 2 m 1 milliamp. D.C. M/C. Aush aq. 2 in . 1 milliamp. D.C. \(\mathrm{m} / \mathrm{C}\). fuxsh rd. 24 in \({ }_{2}\) milliamp. D.C. M1/C. Gusb rd. 31 in . 200 milliamp D.C. M/C. Aush rd. 2lin 30 amF . D.C. M/C. flueh rol. 2 t in. \({ }_{25}\) volt D.C. M/C. flush rd. 1 in. 120 volt D.C. \(\mathrm{M} / \mathrm{C}\). flush pcl. 34 in .
300 voit A.C. M/L. Aubh rd. 2 hin.

CR. 100 SPARES KIT. Coneains 15 valves, resistors, pots, condensers, output trans., etc. All brand new, 59/6. P/P. \(3 / 6\).
DYNAMO EXPLODER UNITS. For deconating explosive charges. Hand generator operation. Brand new \(29 / 6\) each. P/P. 3/6. Hide leather cases \(19 / 6\) extra.

MARCONI TF. 428 B/I VALVE VOLTMETERS. 5 ranges A.C. and D.C. \(1.5,5\), 15,50 and 150 voles. Operation \(200 / 250\) voles A.C. Supplied brand new complete with incernal HF probe. \(\subset 17 / 10 /-\) each. P/P. \(10 / \mathrm{F}\).

EX-ADMIRALTY 12 VOLT D.C. MOBILE AMPLIFIERS. Std. mic. or gram. input. Push pull 10 watt, output matched to 3 or 15 ohms. Good working order. E8/19/6 each. P/P. 6/6.

\section*{MARCONI \\ BRIDGE TF-373 IMPEDANCE fication. \(1,000 \mathrm{c} / \mathrm{s}\). Ranges; 100 henry; 100 mid.; i megohm; 100 Q. 200/250 voles} A.C. operation. \(£ 35\) each.

CRYSTAL MICROPHONE INSERTS, 4/6 each. P/P. 6d.

\section*{MARCONI STANDARD SIGNAL GEN. ERATOR TF-144G. \(85 \mathrm{Kc} / \mathrm{s}\). to \(25 \mathrm{Mc} / \mathrm{s}\). Output 1 microvolt to 1 vole. \(200 / 250\) volts A.C. operation. Reconditioned to maker's specification. \(£ 55\) each.}

UNIVERSAL AVO METERS MODEL 1. Reconditioned perfect order, \(\leqslant 12 / 19 / 6\) each.
P/P. \(3 / 6\). P/P. \(3 / 6\).

\section*{FURZEHILL BEAT FREQUENCY AUD. 10 OSCILLATORS. Frequency range \(0-10,000\) c.p.s. Output 10 or 600 ohms. Separate 50 c.p.s. check. Set zero control. \(200 / 250\) volt A.C. operation. Supplied in perfect working order. \(£ 9 / 19 / 6\) each. P/P. 101.}
CV. 967 I IN. CR. TUBES. 4 volt heater suitable for 'scope, new. \(19 / 6\) each. P/P. \(1 / 6\).
230 VOLT A.C. MOTORS. Ideal for lan or blower. 15/6 each. P/P. 1/3.
R. 1294 V.H.F. COMMUNICATION RE. CEIVERS. 500 to \(3,000 \mathrm{mc} / \mathrm{s}\). Perfece condition wich handbook. E25. P/P. 10/-

\section*{MARCONI TF-329 " © " METERS. \(50 \mathrm{mc} / \mathrm{s}\). Re-conditioned to maker's specification. 200,250 voles A.C. operation. E65 each.}

GRESHAM POTTED L.T. TRANSFORMERS. 230 volts input. Secondary tapped 70. 75 and 80 volts 4 amps. New boxed, \(42 / 6\) each. P/P. 3/6.
FERRANTI FILAMENT TRANSFORMERS. Two eypes, both 200/250 volt input. Type I: 6.3 volt CT. \(5.6 \mathrm{amp}, 6.3\) volt CT. 4.8 amp, 6.3 volt CT., 1 amp. \(19 / 6\). Type 2: 6.3 volt CT. \(3.3 \mathrm{amp},{ }^{6.3}\) volt CT . I amp. 6.3 volt \(\mathrm{CT} . .9\)
amp., 6.3 vole CT. .6 amp . \(15 / 6\). P/P. \(2 /\).., both types.




\section*{UNREPEATABLE OFFER}

DUE TO LARGE PURCHASE FROM GOVERNMENT
COSSOR 339 DOUBLE BEAM OSCILLOSCOPES
PERFECT WORKING CONDITION WITH HANDBOOK ONLY \(£ 15 \mathrm{EACH}\)

Carriage 10\%-extra.

\section*{PORTABLE PRECISION VOLTMETERS}

Brand new and boxed instruments by famous manufacturer. Housed in polished teak case. Moving iron movement reading A.C. or D.C. voles on 2 ranges. \(0-160 \mathrm{v}\). and 0.320 v . 8in. mirror scale. Accuracy within \(2 \%\). Supplied at a fraction of original cost. Only \(\mathrm{E} / 19 / 6\) each. P/P. 3/6.


12 VOLT ROTARY CONVERTERS. Input 12 volt D.C. Output 230 volt A.C. 150 watts, 50 cycles. Housed In wooden case and fitted with voltage control slider resistance, switch, plugs and A.C. mains voltage output check meter. Supplied in perfect condition fully tested, \(£ 9 / 19 / 6\), each. P/P. 10/.

\section*{MARCONI TF410c VIDEO-OSCILLATORS.} Ranges \(20 \mathrm{c} / \mathrm{s}-30,000 \mathrm{c} / \mathrm{s}, 30 \mathrm{Kc} / \mathrm{s}-5 \mathrm{Mc} / \mathrm{s}\). Variable attenuator. \(200 / 250\) v. A.C.
AVO POWER PACKS. 230 volts input. Output \(67 \frac{1}{2}\) volts, \(5 \mathrm{~m} / \mathrm{a}\). and 1.5 voles \(250 \mathrm{~m} / \mathrm{a}\). Fully smoothed. New, boxed 19/6 each. P/P. 2/6.
FIELD TELEPHONES TYPEL. Generator bell ringing, light and very portable. Supplied complete with batteries. Fully tested. As new, 59/6 each. P/P. 3/-

POST OFFICE JUMPER LEADS. 4 ft fitted with two std. jack plugs. 3/- each. P/P. 9d. Standard jack sockets 9d. єach.
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Transformers. All primaries tapped 200/250 Transformers. Al primaries tapped \(200 / 250\)
volts. \(3.5,9\) or 17 volt 1 amp. \(9 / 9 ; 3.5\), 9 or voles. \(3.5,9\) or \(17 / \mathrm{volt}\) amp, \(9 / 9 ; 3.5\), 9 or
17 vole \(2 \mathrm{amp} .14 / 3 ; 3.5\), 9 or 17 volt 4 amp . \(16 / 6 ; 9\) or 17 volt 6 amp . 26/-; 3, 4, 5, 6, 8, \(10,12,15,18,20,24\) or 30 volt 2 amp . \(18 / 6\). Please add postage.

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Carriage 10/6 Complete equipment comprises Search Head, Rods for Search Head, Search Head Test Unitand Test Depth Measure and Haversack. Operation is from a standard \(60 \mathrm{v} . / 1.5 \mathrm{v}\). combined dry battery. The unit will detect ferrous or nonferrous metals to a depth of 24in. glving maximum outpur. Ideal for tracing underground pipes or cables and any hidden metallic objects.
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8 in ., 3 ahm Quality 5 peaker mounted in attractive black craekfe case to match AR88 Receivers, etc.

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45/- each. P/P. 3/6.
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In the f 70 class for only} incorporating the latest mk. iv collaro tape transcriptor. the linear ltas hog quality tape amplifieg. A high flux \(7 \times 4 i n\). LOUdSpeaker, Reel of Best Quality tape. Spare Tape 8 pool, a Portable Cablnot, size approi. \(18 \times 13 \times\) 9in., fished in ventered walnat or aspole, and connection diagram for wiring amplifier to transeriptor.

FEATURES INCLUDE
* 3 8PEEDS. * FREQUENCY RESPONSE 50-11,000 c.p.s. * SWITCYED NEGATIVE FEEDBACE EQUALIZATION FOR EACH SPEED. * OUTPUT 4 WATTS. \(\star\) MAGIC EYE RECORDING LEVEL INDICATOR. \(\star\) TWTN TRACE OPERATION. Both bottom and top tracks can be recorded or played baek without removing tape. \(\star\) INSTANTANEOUS CHANGES can be made from one track to another. Fast rewind in either direction. \(\star\) TAFE MEASORing and calibrating device. * takes full 7in. diameter reels Of TAPE. * NEGLIGIBLE HUM. * ENTIRELY EFFECTIVE ERASURE. Full descriptive leaflet supplied on receipt of S.A.E.

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THE SKY FOUR T.R.F. RECEVER

\(A\) desigu of
ralve 200.250 A.C. mains. \(L\). and M. wave T.R.F. recelver with selentum rectifier. Foi
Inclusion in cabinet Helusion in cabine uut veneered type. it employs valver 6K7, SP61. 6F6 and is epecially designed for slmplictty in wiring. Rensitivity and quality are well up to atandard. Polnt-to-Pnint wirtng diagram. Instructlons and parta list \(1 / 8\). This recelver can be built in brown or cream bakelite or reneered walnut.

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Type BMl. An all dry battery eliminator. Size \(5 \mathrm{f} \times\) if \(\times 2 \mathrm{in}\). approx. Com \(20 \mathrm{c} / \mathrm{s}\) repaces batteries supply \(1.4 v\), and 90 v , where A.C. maise \(2 \mathrm{ing} 1.4 \%\). and 90 a aliable. suitble for all battery poriable reoeivern requin with diat gram 3819 or ready for use 4819

Type Burz. Size \(8 \times 61 \times 2 \mathrm{kin}\). Supplies 120 v. 90 v. and 60 v., 40 mA . and 2 . n.4 a. to 1 amp. fully mmoothed. TBEREBY COMPLETELY REPLACING BOTH B.T. BATTERIES AND E.T 9 v. ACCDMULATORS when connerted to A.C. maing supply \(2011 \cdot 250\) v. \(\overline{0} 0 \mathrm{e} / \mathrm{s}\). SUITABLE FOR ALL BATTEBY RECEIVERS mormatly using of v . accuraulator.
Complete tit with diagrams end mistructions. \(48 / 8\) or ready for une \(58 / 6\)


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A fully assembled unit housed in attractive two tone rexine covered nortable cabinet.
\(\star\) Single Speed 3 in. per sec.
* Negative Feedback Tone Conpensation.
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Magic Eye Recording Level Indicator.

HI-FI 10 WATT AMPLIFIERS
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Uull.tro ACdish4 4 -speed aingle playern with hi-i tamover ir jakal plek-up head .26/12/6. Cart. 4/6.
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H.P. TERMS, DEPOSIT 2 Gns. \\
Twin Track. \\
Automatic Erasing. \\
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High Flux \(7 \times 4 \mathrm{in}\). P.M. Speaker. \\
Output 3 watts.
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A complete kit of parts to
contruct a good
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\(3+8\) watt (total 6 watt)

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\(33-1\) hand or Desk
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FULLY SEROUDED UPRIGHT MOUNTING \(350-5-250\) v. \(60 \mathrm{~mA} . .6 .3\) v. 2 a.. 5 v. 2 a.

\(300-0-300\) v. \(130 \mathrm{~mA}, 6.3\) v. 4 a., c.t., 6.3 v. 1 a
\(350-0-3.50 \mathrm{v} .150 \mathrm{~mA} ., 6.3 \mathrm{v} .4 \mathrm{a}, 5 \mathrm{~F}, 3 \mathrm{~A}\)
\(425.0-425\) v. 200 mA . 6.3 v. 4 a., o.t. \(5+. \mathrm{g}_{\text {々......... }} \quad 43 / 9\)
TOP SHROUDED DROP-TEROUGR TYPE

really life-like reprodcution. Suitable for use with all tereo ptck-up head. at preatht avaliable. Ganged volume
and tone controls. Preset bsance control. Outputs for matched 2-3 ohm speakers. For 200.250 v. A.C. main Astomahing value.
W.B. "STENTORIAN" HIGH FIDELITY P.M. SPEAKERS
HF1012, 10 watts 15 ohms (or 3 ohm) speech coil. Where a really good quality speaker at a low price is required, we highly recommend this unit with an amazing performance. \(\quad\) \&4/10/9. Please state whether 3 ohm or 15 ohm required


AM/FM RADIOGRAM CHASSIS, HIGH QUALITY PUSH-PULL. 6-8 WATT OUTPUT. Current manufacture. 12 months guarantee. For \(200-250 \mathrm{v}\) mains. Covers L. and M. wavebands plus F.M. Includes 8 latest type miniature B.V.A. valves Only 22 gns. plus \(7 / 6\) carr. Or deyosit \(82 / 12 /-\) and 9 monthly payments of \(£ 2 / 12 /\).
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GARRARD 4-8PEED AUTO-CHANGERS Type HO/1z0H. Limited number of 29/19/6 (approx. bin type Eq/izolis.
prlce). Carr. B/b. Brand uew.
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\section*{OTPPT TRANSFORMERS}

Hidget Battory Pentode 88:1 for 384. etc
Mandind Pentode \(5,000 \Omega^{3} \Omega\)
Itandsrd Pentode 8, 100 © to 30
Push-pull 8 watta 6 V8 to 3 ohms
Punh-pull 8 watts EIR4s to 15 ohms
Push-pull \(10-12\) wattas 6 V 8 to 30 or 15 a
Push-pull \(10-12\) watts to matoh \(6 v 6\) to \(3.5-8\) or 150 Push-pull 10-12 watts to matoh
Puah-pull ELSi to 3 or 15 ohms Push-pull Ultra Linear for Mullard 510
Pinh-pull 15-18 watta. sectionally wound, 6LB.
KT68, eto., or 3 or 15 ohms.........................
Push.pull 20 watt bigh-quality sectionally wound,
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If required louvred meral cover with 2 carrving handles can be gupplied to 18.9. TERM ON ASSEMBLED UNITS. DEPOSTT 181 , and 12 monthly payments o \(18 / 9\) send B.A.E. for tilustrated leaflet detailing
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Bass and Trebie cut and \({ }^{\text {boost }}\), ontrole Bass and Trebie cout and " boost, ontrols.
gensitivity 15 mv . High Flax gin. I/speaker. Input Genaitivity 15 mv . High Flux Min. L/apeaker. Input
sockecs for Radio/Tape or Gram Pick-up aud Miksockets for Radio/Tape or Gram Pick-up atid Mia
Instrumen Pick-up Handonme stronglv mad abinet (size spprox \(14 \times 14 \times 7\) in.). Finished in \(88 / 19 / 6\) Cari. 7/6. Or Deposit \(\& 1\) and nive 88/ 19,6 monthly payments \(\& 1\). Gend 8.A.E. for leatlet.
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For Record Players or Tape Recorders. Rexine
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Gauss 12.000 lines. Speech coll 3 chms or 15


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Above cabinet staar Chanker, Gram amplitier, and Bin. or Bin. \(\times 4 i n\).
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Or Conqueat changer in lieu of Conqueat changer in lieu ot
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(IB ohnus), consusting of 4 high quality 12 in . npeaiker of orthodor design aupport ling a small ellipticai spats er ready wired with choke
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We can quote speciai prices for quantlien of 12 to 10,000 of most types. Special troea musto
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\(6 / 12\) v. 4 a.
B/12 v. 5 a a
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v. 50 mA . \begin{tabular}{l}
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250 \\
V .60 mA. \\
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F. W. \\
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HIGH FLDELITY 10 watt PUSH-PULL AMPLIFIRRS Separato Bass and Treble controls. Inputs for Gram. and Mike. Mullard latest type vaves. Brand Now. Tery limited number efik/ Carr 7/8

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IDEAL FOR BATTERY CRAROER OR INGTRU. MENT OABE, COVER COULD BE USED FOR AMPLIFIER. Only \(0 / 9\), plus \(2 / 9\) poot.

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UNCTION TRANSISTORS. R.F. Type, \(12 / 8\) Audio type 6/9. Power type Goltop V18/10P 2 watts \(17 / 9\). OC71, \(\begin{array}{ll}10 /- & 0 C 72 \\ 0 C 44 & 22 / 6 .\end{array}\)

VIBRATORS. Oak and Wearlte, synchronous 7.pln, 2
2 v, 16 A.R. EX. GOVT. ACCUMULATORS. New Boxed Only \(5 / 6\) earh, 3 for \(15 / \%\), plua \(3 / 6\) carr.

All 200-250 Pr. \(0 \cdot 110-200 \cdot 230 \cdot 250\) v., \(275-0-275\) v. \(100 \mathrm{~mA}, 6.3\) \(250 \mathrm{v}, 60 \mathrm{~mA}, 6.3 \mathrm{v}, 2 \mathrm{~B} .\).
\(300.0-300\)
\(300 \cdot 0 \cdot 300\) ₹. \(60 \mathrm{~mA}, 6.3\) v. 2 a. ...................... 10/119


 ed with D.C. rating after rectification) 68/8. Carr. 15/-\(\begin{array}{lll}0-10-20-25 & \text { v. } 24 \mathrm{a} \text {. (Govt. rating) 79/6. Carr. 15/-. } \\ \text { AUTO } 500 \text { watts, } 0-215-220-225-230-235-240 & \text { v. } & 29 / 8\end{array}\) Carr. \(7 / 8 . \quad 50\) watts, \(0-110 / 120-230 / 250\) v. \(8 / 11\).

\section*{ARDENTE DEAF AID EARPIECES wth lead and plug.}

\section*{BATTERY CHARGING EQUIPMENT}

Trade supplied. Discounts according to quantity.

\section*{HEAVY DUTY CHARGER KIT}
\(6 / 12\) v. varlable charge rate up to 6 amps. Consisting of Mains Trans., F.W. (Bridge) Selenium Rectifier, 0.7 amp. meter, multiposition switch with knob, fuses, fuseholders, panels, plugs and circuit. Only 59/6 Post 4/6.

\section*{A8sEMBLED CHARGER9 BATTERY CHARGER KITS}

\section*{\(\begin{array}{ll}6 \\ 6 & \mathrm{y} .1 \\ 9 & \text { a. }\end{array}\) \\ 6 v .2 a .} \(6 / 12\) v. 1 a
\(6 / 12\) v.
6 \(8 / 12\) v. 4 a \(6 / 12\) v. 4 a. …......... \(38 / 9\) Above ready for use with mains and output leads. Cases well ventilated and finished in stoved blue hammer. Carr. \& pkg. 3/8,

CHARGER
TRANSFORMERS 200-230-250 v. \(50 \mathrm{c} / \mathrm{s}\). \(0-9-15 \mathrm{v} .1 \frac{1}{\text { a }}\) \(0-9-15\) v. \(2 \frac{1}{2}\) a \(0-9-15\)
0.9 .15
0.3
a \(0-9.15\) v. 5 a \(0-9-15\) v. 6 a.

\section*{Consisting of Mains Transformer} F.W. Bridge, Metal Rectifier, well ventilated steel case. Fuses, fuse-bolders, grommets, panels and circuit. Carr. 2/9 extra. 6 v . or 12 v .1 amp . As above, with ammeter 6 v .2 amps
6 v . or 12 v .2 amps
6 v. or 12 v. 2 amps.
(inclusive of ammeter)
6 r . or 12 v .4 amps .
6 v. or 12 v. 4 amp . with
variable charge rate selector
and ammeter
CHARGER AMMETERS
CHARGER AMMETERS
\(0.1 .5 \mathrm{amp}, 0,0-3 \mathrm{amp} ., 0-4 \mathrm{amp}\).
\(0.7 \mathrm{amp} ., 0.25 \mathrm{amp} ., 0.60 \mathrm{amp} 8 / 9\)

ASSEMBLED GHARGER

6 v. or 12 v. 2 amps. Fitted Ammeter \(24 / 9\) and selector plug \(32 / 9\) for 6 v . or 12 v 25/9 Louvred metal 31/6 case, finished at42/9 tractive hammer blue. Ready for \(3 / 9\) use with mains and output leads. Double Fused.
\(\begin{array}{ll}\text { Only } \\ \text { Cars. 3/9. } & \text { 49/9 }\end{array}\) Carr. 3/9. \(49 / 9\)
As above, but for As above, but for
3 amp. charging. 3 amp. charging.
Only \(59 / 6\). Carr. \(3 / 8\)

All for A.C. Mains 200-250 v. \(50 \mathrm{~s} / \mathrm{c}\) Guaranteed 12 months ASSEMBLED 6 v . or 12 v .

\section*{4 amps.}


ANOTHER SNIP OFFER SLIGHTLY SOILED AT THELOWPRICE 29/6 and \(4 /\) Surplus to manufacturSurplus to manufactur
er's requirements, well made 2 -tone colour made
portable player cabiportable player cabi-
nets, will take non-auto nets, wal Amplifier and in speaker. The above portable cabinet .S.R. T.V. 9 and Acos pick-up, 4 -speed player and 2 -watt amplifier and \(6 \times 4\) elliptical speaker making an ideal portable player, at the special price of \(\mathbf{c 8 / 5 / - \text { plus } 7 / 6 \text { Post and Pkg. }}\)
3 NEW RECEIVERSFOR CONSTRUCI TORS. One valve SW radio, 24-40 meeres All components, 35/-. P. \& P. 2/-
- Beginners' transistor pocket radio, miniature | components, 30/- complete. P. \& Pkg. 2/-. Personal portable radio. All parts, complete, 35/- P. \& Pkg. 2/-.

\section*{BUILD THIS YOURSELF}

The Transette Medium Wave, 2 transistor pocket portable. Nearly designed, using 2 pocket portable. Neatly designed, using 2 ransistors and diode. Simple to assemble Enlarged working diagram. All components colour coded. Ferrite wound aerial. WIII play indoors' and outside with self contained zerial All components and diagram complete, \(62 / 6\). Post \& Pkg. 1/6.
Plug-in ear piece
Single phone.
12/6
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All components available separately
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A GIFT FOR THE SERVICE MAN


\section*{BRAND NEW IN WOODEN} The Weston Model 772 Type 6 super sensitive analyser. This precision designed multi-range cest instrument has a large visible finely divided scale glving some of the range shown. Range: D.C. voles 20,000 ohms per volt or 1,000 per range 50,000 ohms. 10 volt tange 200,000 ohms, 50 vole range i megohm. 250 volt range 5 meg . ohms. 1,000 volt range 20 megohms. Ohms: \(0-3,000\) ohms, \(0-30,000\) ohms. 0.3 meg. 0.30 meg. D.C. milliamps: \(10,50,250 \mathrm{IM} / \mathrm{A}\) or 50 microamps. A.C. volts: 1,000 ohms per volt. ONLY E/2/10/-plus post and pkg. 7/6.

FOUR ASTOUNDING TV TUBE OFFERS All brand new in famous maker's cartons. (1) 17in. rectangular aluminized 6.3 HRTS. .3A current; max. anode voleage 16
Usual price E17/5)-
OUR PRICE E9/19/6. Crating
and carr. 15/-
(2) 14in. rectangular Tube, 6,3 heaters; . 3 amp current; max. anode 14 KV ; ion trap; external conducting coating; BI2A base. 68/I7/6: Crating and carriage \(12 / 6\)
(3) Ferranel T12/44 and T12/549 I2in. mag. netic white fluorescence; 4 v . heater: max anode 10 kV . As used in many TV receivers. Original price \(\mathrm{E} 17 / 15 /-\). OUR PRICE \(64 / 4 /\)-. Crating and carr. \(12 / 6\).
(4) Ferranti 9 in. Tube
(4) Ferranti 9in. Tube, round white flourescence, 4 v. heater, max. anode voltage 7 kV .
OUR PRICE \(£ 2 / 10 /-\). Crating and carr. \(11 / 6\).

SPECIAL OFFER IN TRANSISTORS Audio PNP transistors type TSI 5/- each Sensitive dlodes type GD3 \(\therefore . .\). 2/6 each Ediswan \(\times\) B104 …............................. \(9 / 6\) \(\times \mathrm{BlO3}\)
\[
\times \text { A104 ... }
\]
\(\qquad\)
General Purpose diodes ............. 10d. ea. Single ear' phones...... 4/6 ea., \(1 /-\) p. \& p. Crystal Ear pieces with lead and ear plugs. Low impedance. Our price 12/6. 1/-p. \& p. Transistor Condensers. Miniacure Electrolytic Capacitors. \(32 \mathrm{mfd} .3 \mathrm{v} ., 25 \mathrm{mfd} .25 \mathrm{v} .\), \(25 v ., 25 \mathrm{mfd} .6 \mathrm{v} ., 16 \mathrm{mfd} .12 \mathrm{v} ., 8 \mathrm{mfd} .6 \mathrm{v} .\), \(5 \mathrm{mid} .12 \mathrm{v},, 2.5 \mathrm{mfd} .25 \mathrm{v}, 1.6 \mathrm{mfd} .6 v_{\text {. }} 1 \mathrm{mfd}\). 12 v . All these types of condensers are \(2 / 6 \mathrm{ea}\).

\section*{BARGAINS IN MICROPHONES.}

Acos crystal stick mic., \(39 / 1\) complere with cable. Manufacturer's price \(84 /\). OUR . PRICE \(39 / 6\), post free.

\title{
MWhWWMWMNMATH Visit the City's popular accoustically designed HI-FI Centre
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COME AND HEAR THE LEADING MAKES IN AMPLIFIERS, TUNERS AND SPEAKER SYSTEMS

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Huge purchase of the world-famed RCA equipment enables us to offer the various units at enormous reductions.

\section*{THE NEW RCA ORTHOPHONIC AMPLIFIER}

12-20 watt output. Distortion: harmonic less than \(.1 \%\) at 10 watts/700 C.p.s. Noise Level: 85 D.B. below rated output. Frequency Response: within 2 D.B., 20/2,500 e.p.s., within .5 D.B., \(10 / 60,000\) c.p.s. Feed back: 40 D.B. total. Output Impedance: \(3-4\) ohms, 7 ohms and 15 ohms. Spare Power:
295 v. 145 M.A. and 6.3 v .2 .5 amps. for pre-amp. radio tuner and
tape amp. A.C. Input: \(100 / 150 \mathrm{v}\). and 200/250 v . Valve Line-up: two EF86, two KT66, one GZ32. Dimensions: \(16 \frac{1}{\frac{1}{2}} \times 8 \times 7\) tin. Weight: 321 b .

\section*{PRE-AMP.}

Input: Mic., radio/tape high and low level, crystal and magnetic p/ups. Tape and Record: output. Bass and Treble: lift and cut continuously variable. Mixing Facilities: mic. inpus output. Bass and \(\mathrm{Ceble:} \mathrm{lift} \mathrm{and} \mathrm{cut} \mathrm{continuously} \mathrm{variable} .\mathrm{Mixing} \mathrm{Facilities:} \mathrm{mic}\).input
with radio and tape, Iow and high pass filter. Valve Line-up: one EF86, two ECC8i. Dimenwith radio and tape, low and high pass f
sions: \(127 \times 6 \frac{1}{1} \times 3\) inin. Weight: 71 b .
THE COMPLETE EQUIPMENT AT 29 GNS. Carriage 15/-.
RCA F.M. TUNER
will match with the above amplifier or any other amplifier with radio input. Tuning range 87.5\(108 \mathrm{~m} / \mathrm{cs}\). The new RCA electronic ray tuning indicator is used, A.F.C., delayed A.G.C. Power required: \(230-390\) v. D.C. at 40 MA. H.T. 6.3 v. at 2.25 amps. Vaive Line-up: EF95, EF91, ECC81, three 6AU6, EB9I, 6AL7. Attractively finished. Dimensions: \(12 \frac{7}{\frac{7}{2}} \times 6 \frac{1}{2} \times 3 \frac{1}{8} \mathrm{in}\). Óriginai price \(£ 33 / 11 /\) OUR PRICE E18/19/6. Post and pkg. \(5 /-\)
RCA PANORAMIC MULTIPLE SPEAKER SYSTEM
Beautifully made in walnut finish using one 15 in . Hi-Fi speaker, response down to \(25 \mathrm{c} / \mathrm{s}\)., two \(2 \frac{1}{2}\) moving coil tweeters, response up to \(20,000 \mathrm{c} / \mathrm{s}\). crossoevr at \(2,000 \mathrm{c} / \mathrm{s}\)., cabinet, ported bass reflex and acoustically damped, 250 watt rating. FEW ONLY. Original price \(£ 56 / 11 /\) OUR PRICE \(£ 35\).
FOR THE CONSTRUCTOR
We can offer a limited number of RCA \(10-12\) watt amplifiers completely assembled. Just connect assembled amplifier chassis, control unit, power pack and attractive control panel together. Frequency response: \(25-20,000 \mathrm{c}\). p. s ., full 10 watt push/pull output, negative feedback. low hum level. 5 valves. Variable bass and treble controls and balanced loudness control which ensures true balance of sound from lowest bass to highest treble at both high and low listening levels. All this at the very low price of \(£ 7 / 19 / 6\), plus post. and pkg. \(4 / 6\).
AHERCA JUNIOR 5-B watt PUSH/P ULL AMPLIFIER
Completely assembled. Just connect assembled amplifier chiassis, power pack and attractive conCompletely assembled. Just connect assembled amplifier chassis, , power pack and ateractive con-
trol panel together. Frequency response \(40-20,000 \mathrm{c} . \mathrm{p} . \mathrm{s}\). Full 5 watt push/pull, negative feederol panel together. Frequency response \(40-20,000\) e.p.s. Full 5 watt push/pull, negative feed-
back, low hum level, 4 valves, variable bass and treble controls and balanced loudness control. back, low hum level, 4 valves, variab
ONLY \(£ 6 / 19 / 6\). Post. and pkg. \(4 / 6\).

\section*{RCA HIGH FIDELITY REPRODUCER}

Completely assembled quality equjpment in well styled and beautifully finished cabinet in wainut with contemporary style legs. - 5 -10 watt peak power, push/pull output, low hum level, 40-20,000 c/cs., separate bass and treble controls and balanced loudness control. 3-speaker system using \(10 \times 6\) elliptical speaker and two 4 in . tweeters for high frequencies dispersed through specially designed acoustic chamber. 4 -speed auto-changer playing ten 7,10 or 12 in . records. Monaural switch for hand operation of pick-up. 45 centre spindle for Continental records. Dimensions of cabinet: length 20 in ., height \(18 \frac{2}{2} \mathrm{in} .\), width \(11 \frac{3}{3} \mathrm{in} .\), legs 28 in .
OUR PRICE \(635 / /\)-., Post and pkg. \(25 /\) - for this remarkable player.
NOTE: This equipment has input socket for stereo and gram unit has stereo and monaural \(\mathrm{t} / \mathrm{o}\) cartridge.
THE RCA VARIABLE RELUCTANCE PICK-UP
A new deisgn variable reluctance pick-up. Cartridge completely protected from dust, damp and mechanical shock. Embodies an 8 -pole balanced design providing the adavntages of sersitivity and negligible hum with smooth and extended frequency response. Pick-up arm has simple tracking pressure selector and adjustable pedestal to suit all turntable heights. Fitted with dual
 sapphire stylus. Tracking pressure: micro-groove \(5-\)
f/3/9/6. OUR PRICE \(\mathbf{k} / 10 /-\). Post and pkg. I/6. 183/9/6. OHR PRICE
Brand new snip in manufacturer's carton. RCA 4-speed auto-changers in maroon finish incorporating auto. and manual control. Complete with Ronette Studio turnover crystal pick-up with sapphire styli for L.P.s and 78 r.p.m. records and including 45 cenere pose for large hole records. AT THE AMAZING PRICE OF E7/19/6, plus \(4 / 6\) pose. and pkg.

\section*{BUILD YOURSELF A HI-FI TAPE RECORDER AT HALF THE NORMAL PRICE LIMITED NUMBER AVAILABLE \\ BRAND NEW AND GUARANTEED}

The famous COLLARO Mk. 4 Transscriptor Tape Deck. Twin track, 2 record/ playback, 2 erase heads on 2 levels, pause control, digital counter, 3 speeds, 2 balanced motors of low wattage input, \(617110 /\) WHILE STOCKS LAST.

The Collaro pre-amp and bias oscillator complete with power pack for the above deck with instructions. Price \(£ 12 / 19 / 6\). Post and Pkg. \(7 / 6\).

The above two items at a special price of \(\mathbf{E 3 0}\). Carr. and pkg. 22/6 the two units.

The Linear Tape Deck Amplifier with power pack and oscillator incorporated. Switched for \(37,7 \frac{1}{2}\) and 15 in . per sce. Suitable for the Mk. 4 Deck, 12 gns . only. Post and pkg. \(3 / 6\).

\section*{HI-FIDELITY TAPE HEADS}

Made by famous manufacturer. Brand new. Upper or lower track, record/play-back, high impedance giving up to 12,000 c.p.s. at \(7 \frac{1}{2}\) I.P.S. output \(5 \mathrm{~m} /\) volts at 1 KC at \(7 \mathrm{t} 1 . \mathrm{P} . \mathrm{S}\). Erase heads low impedance.
Only \(39 / 6\) per pair. Post 1/-. State upper or lower track.

\section*{SNIPS IN TAPE ACCESSORIES}

Brand new E.M.I. Tin. take-up spools in polythene bag. \(3 / 9\) each post free, 6 for \(20 /-\). Brand new 5 in. Scotch Boy take-up spools \(3 / 3\) post free. 6 for 18/-.
1,200ft. P.V.C. rape on plastic spools made by famous manulacturer. 21/-reel. Post \& pkg. 1/-. \(1,200 \mathrm{ft}\). P.V.C. tape on \(5 \frac{3}{2}\) plastic spool. 22/6, plus \(1 /\)-post \& pkg:
The New American Audio Tape with plastic base Also supplied in green or blue at no extra cost.
\(3 i n\). reel 150 ft

4 in . reel 300 ft
in. reel 600 ft 18/
Post and packing, i/- per spooi.
KLENZATAPE, the new method for cleaning record and erase heads, 12/6. P. \& P. 1/-
special offers in tape by famous maker:
3 in . L.P. tape \(225 \mathrm{ft} ., 7 /-\) post free.
4 in . Std. tape \(300 \mathrm{ft} ., 10 / 6\) post free.
METROTABS for identifying recorded passages on tape, \(3 / 11\) plus postage.
THE NEW "INSTANT" BULK TAPE ERASER
Can erase a spool of magnetic tape in a lew seconds. Demagnetises oxide deposits on tape heads. Only 27/6 post free

Limited number Acos 73-1A stereo turnover cartridge, suitable for 78, microgroove and stereo records, will fit most modern pup heads. Mfrs. price 52/10. Our price 42/6, Post free.
Heavy magner \(9 \times 5\) Elliptical speaker by famous maker, 18/6. P. \& P. 1/6.

EVEIRYTHING we sell may be paid for weekly at no extra cost to yourself!

RADIO
super superior radio 5 /4

(plus carr. and ins.) initial payment and 19 weekly payments of \(4 / 2\). 4 waveband, 5 valve superhet radio, 2-tone covered metal cabinet. 4 control knobs. Positions for gram p.u. and extension speaker. A.C. only. Size \(241 \times 12 \times 10\) in. deep. Ins. Carr. \(8 / 6\).
HOME
RADIO 5'1
(plus carr. and ins.) initial payment and 19 weekly payments of \(3 / 11\).


Cash price 79/6. 3 waveband receiver can be adapted to gram p.u. In attractive wooden cabinet. \(9 \frac{1}{4} \times 18 \frac{1}{2} \times\) 11 inin. Ins. carr. 4/6.

* SUPER CHASSIS

5'1
(plus carr. and ins.) initial payment and 19 weekly payments of

\section*{Cash price 79/6.} \(3 / 11\).
5 -valve Superhet chassis including 8in. P.M. speaker and valves. Four control knobs (tone, volume, tuning, w/change switch). Four wavebands with position for gram p.u. and extension speaker. A.C. Ins. carr. \(\overline{5} / \beta\).

\section*{BAKELITE}

CABINETS 5/9
Brand new. Colour brown.
Attractive design. Size
\(12 \times 7 \times 5 \frac{1}{\mathrm{in}}\). Ideal for small receivers, con verters etc. P. \& P. \(3 / 9\).
SOUND/VISION and I.F. STRIP \(\quad\) //9 Plessey. I.F.'s \(10.5 \mathrm{Mc} / \mathrm{s}\). sound. \(14 \mathrm{Mc} / \mathrm{s}\). vision. 8 valve holders. Less valves. Size \(81 \times\) \(5 \times 4 \frac{1}{2}\). Circuit incl. The tuner unit plugs directly into the chassis. P. \& P. 2/6.
SOUND/VISION and I.F. STRIP
2/9
Salvaged. Complete sound and vision strip. 8 valve holders. Less valves. I.F.'s \(16-19.5 \mathrm{Mc} / \mathrm{s}\). Size \(8 \frac{1}{x} \times 4 \frac{1}{4} \times 4 \mathrm{in}\). Drawings free with order. TIMEBASE

2/9
Containing scanning coils, line transformer, etc. less valves. Drawings free with order. P. \& P. 2/6.

COLVERN PRESET POTENTIOMETERS
Brand new. 200 ohms. 10 K , and \(2 / 9\)
20K. P. \& P. 9d.
FOCUS MAGNET 9/9
Brand new. 38 mm . Incorporating picture shift control. P. \& P. 1/3.
SCANNING COILS
Low impedance. 38 mm . Brand new. P. \& P. 1/3.
SCANNING COILS \(15 / 9\)
Wide angle 90 deg. 38 mm . Low impedance. P. \& P. \(1 / 3\).

\section*{CHASSIS FOR 8 PARES
ALL THIS FOR ONLY}

58 Resis., 7 variable. Controls, conds., incl. electrolytics. Coils, 7 I.F. \& R.F. transformers. 14 v/holders. 4 trans., mains - O.P. - line \& frame. Chokes, metal rec., Fuse panel, scanning coil, focus magnet, plugs, sockets. etc.; 1.F. strip in separate power pack can be used without dismantling. 7 pages of circuits and instructions dshowing position of each component. Chassis showing position of each component. have been
Carr. \(10 / 6\).
catalogue free on request

\section*{* TELEVISION}

FOR AS LITTLE AS II/Id

per week this modern style 17" television set can grace your home!

Cash Price \(£ 19.19 .0\)
Details:-
* Beautiful latest finish cabinet in contemporary style. Covered and washable.
* Polished legs 18 in . optional extra for \(25 /\) -
* 17 in . Rectangular Tube. Guaranteed fully for 12 months.
\(\star 12\) channels. "Turret Tuned"-ITV/BBC. (Extra coils at only \(7 / 6\) a pair (with order)).
\(\star\) Chassis. 14 B.V.A. Valves-Salvaged but reconditioned and guaranteed 3 months. Cart. \& Ins. 30/-.
Due to overwhelming demands, some delay may occur. Please enquire when ordering.
TERM8: 36 weeks at 11/1 OR 20/7 and 19 weekly payments of 19/11.
( 4 weekly payments required in advance, plus carr. \& ins., on 36 weeks only).

\section*{* TELEVISION TUBES}

Pay as you view. Any size. Any type. Full allowance on your old tube.


NO EXTRA8. NO INTEREST. NO DEPOSIT.
Engineer available to fit. Express service same day as ordered. Write for detalls.
Completely rebuilt gun assembly, new cathode, heater, etc., giving the bigh standard required for long picture life, quality and value. Carr. \& Ins. \(15 / 6\).

\section*{SPARE PARTS \\ SOLO SOLDERING TOOL \\ 12'6 \\ 110 v ., 6 v ., or 12 v . (special adaptor for \(200 / 250 \quad \mathrm{v}\). \(10 /-\) extra). Automatic solder feed including \\  \\ \(60 / 40\) solder and spare parts. It is a tool for electronic soldering or car wiring. Revolutionary electronic soldering or car wiring. Revolutionary in design. Instantly ready for use and cannot
burn. In light metal case with full instructions forn. use. Post \(3 / 6\).}

\section*{TRANSFORMERS}

\section*{MAINS TRANSFORMER \\ 5/9}

Primary 200-250. Secondary 0-100-250. 150 mA . Suitable for small amplifier with .1 series valves. \(2!\times 1 \ddagger\) in. P. \& P. \(1 / 9\).
OUTPUT TRANSFORMER AND
SMOOTHING CHOKE COMBINED 4/9
\(2 \% \times 1 \frac{1}{2}\) in. Suitable for EL84s in single or push pull output. P. \& P. \(1 / 9\).
MAINS TRANSFORMER
Primary 200-250. Secondary \(300-0-300\). 6 v .
3.3 amps. P. \& P. \(1 / 9\).

MAINS TRANSFORMER 6/9
\(300-0-300\) volt at \(80 \mathrm{~m} . A\). Prim. 200/250v. 6.3v. @ 3a. 5v. @ 2a. P. \& P. 2/9.

FRAME OUTPUT TRANSFORMER \(1 / 9\) 500 ohms. primary. 18 ohms. secondary. P. \& P. 1/6.

SMOOTHING CHOKE 250 mA . \(5 / 9\) 2nd 40 ohms. D.C. Res. New. P. \& P. 1/6.
R.F. E.H.T. COIL \(\quad 7 / 9\)

7-10 Kv. R.F. frequency approx. \(22 \mathrm{Kc} / \mathrm{s}\). Uses 6V6 or P61 as osc., suitable for Ultra model V600, W700 and many other sets or replacing E.H.T. mains transformers. Ideal when using a larger tube. Size \(49 \times 2\) in. dia. Base \(4 \times 41 \mathrm{in}\). Circuit drawngs available with Base \(4 \times 4 \frac{1 i n}{}\) Cir
order. P. \(\&\) P. \(2 / 8\).
order. P. \&P. \({ }^{2 / 0}\)
7/9
17in. brand new. Latest pastel shades. Pink
and blue. Post \(2 / 3\).
T.V. MASKS

7/9
2lın. as above. Post \(2 / 3\).
T.V. MASKS

2/9
For \(15 i n\). tubes in gold plastic. Post \(1 / 3\).
T.V. AERIALS

23/6
For all I.T.A. channels. Outdoor or loft. 3 elements. P. \& P. 2/6.
AERIALS
B.B.C. Indoor type. Folded dipole with 12ft. co-ax cable fitted. Post \(1 / 9\).
CO-AX CABLE
6d. yd.
Good quality. Cut to any length. 1/6 postage on 20 yds .

\section*{MODERN 17" T.V. CHASSIS COMPLETE AND WORKING \\ 24 GNS. or Terms}

15/3 Initial Payment. Balance at \(14 / 3\) for 35 weeks.
29/6 Initial Payment. Balance at 25/6 for 19 weeks.
Ins., Carr. 25/- (must te paid with Initial Payment).
Latest chassis including 17 in . tube. Permanent magnet speaker. 13 channel Turret Tuner (any 2 selected channels fitted). Other channels supplied on request at \(7 / 6\) each. 13 valves. Chassis and valves guaranteed for three months. C.R.T. for 12 months' full guarantee. Sound I.F. \(19.5 \mathrm{Mc} / \mathrm{s}\). Vision \(16 \mathrm{Mc} / \mathrm{s}\). A.C. only. Ready and working to fit into your own cabinet. Carr. \& lns., 25/-.

As above with 14 in . Tube, complete and working £19.19.0.


FROM OUR EXCITING RANGE OF RECORD PLAYER CABINETS: -
T.W. 1
\(5 / 1\)

Initial payment. Balance over 19 weeks at \(3 / 11\).
Size 15 ? \(\times 198 \times 10\) in. Takes B.S.R. U.A. 84 speed autochanger. Twin speakers. 3 control amplifier. Carr. and ins. \(4 / 6\).

\section*{TAPE RECORDER CABINETS 19'6}


When goods are bought on our interest-free credit terms, the cost of carriage and insurance must be sent with the initial payment.


\section*{Cash Price}

69/6

\section*{Initial}

19 weekly payments of \(3 / 5\).
A beautifully styled cabinet. Made by a famous
manufacturer. In manufacturer. In with clipped lid and carrying handle. Size \(16 \times 14 \frac{1}{6} \times\) stin. deep. Wult take B.S.R. Monarch 4 speed autochanger and \(7 \times\) 4 in. elliptical speaker and most of the modern portable
R.P. 3 Cash price 69/6 A delightful looking cabinet \(149 \times 179 \times 83\) in. in 2 tone leatherette. Will take a Be.S.R. Monarch and speed autochanger and
\(6!\mathrm{in}\). round speaker.
 Initial payment 4/7 and 19 weekly payments of \(3 / 5\).

\section*{R.P. 6}

2916
Elegant cabinet, cloth covered in grey or red with sunken control panel and speaker fret. Size \(13 \times 17 \times 8\) in deep. Takes a B.S.R. Monarch 4 speed autochange; \(7 \times 4 \mathrm{in}\). elliptical speaker and most of the modern portable amplifiers. Carr. and Ins. 4/0.

\section*{B.S.R. FUL-FI CRYSTAL TURNOVER CARTRIDGES \\ 19/6}

Brand new. Including sapphire needles for L.P. and Standard, giving fullest range and finest tone obtainable for any player. Can be fitted to all standard pick-up amns. P. \& P. 9d.

\section*{AMPLIFIERS}

12 months' guarantee PORTABLE AMPLIFIER D.1. \(\quad 4 / 1\) initial payment and 19 weekly payments \(2 / 11\). Brand new. Latest design with printed circuit. Dimensions \(7 \times 21 \times 5 \mathrm{in}\). A.C. only. Mains isolated. \(2-3\) watts output. Incorporating EL84 as high gain output valve. Volume and tone controls. Knobs 2/6 extra. P. \& P. 3/6. Cash price 59/6.

PORTABLE AMPLIFIER MK.D.2. 5/1 initial payment and 19 weekly paymente \(3 / 11\). printed circuit. Latest design. Dimensions Printrd circuit. Latest design. Dimensions
\(7 \times 24 \times 5 \mathrm{n}\). A.C. only. Mains isolated \(3-4\) watts output. Incorporating the latest ECL 82 triode pentode output valve giving higher undistor ted output. Volume and tone controls. Knobs \(2 / 6\) extra. P. \& P. 3/6. Cash price 79/6.
PORTABLE AMPLIFIER MK.D.3. \(5 / 7\) initial payment and 19 woekly peyments \(4 / 5\).
De luxe model. Printed circuit. Latest design. Dimensions \(7 \times 2 \ddagger \times\) in. A.C. only. Mains isolated \(3-4\) watts output. Incorporating the latest ECL82 triode pentode output valve giving higher undistorted output. Volume, treble and bass control. Knobs \(3 / 6\) extra. P. \& P. 3/6. Cash price 89/6.

PORTABLE AMPLIFIER MK.D.5. \(3 / 1\) initial payment and 19 weekly payments \(1 / 11\).
Simple circuit employing ECL. 80 triode penSimple circuit employing ECL 8 triode pen-
tode output valve giving \(2-3 \mathrm{w}\) atts output. tode output vaive giving
A.C. only. Mains isolated. Single control for A.C. only. Mains isolated. Single control for
volume and on/off ;witch with knob. P. \& P. 3/6. Cash Price 39/6.

STEREOPHONIC AMPLIFIER \(9 / 1\) initial payment and 19 weekiy payments \(7 / 11\). Beautifully made for portable stereophonic record players. Latest design with printed circuit. Dimensions \(3 \times 5\} \times 9\) in. A.C. only. Mains isolated. Twin amplifiers each side giving \(3-4\) watts output. Incorporating ECL82 triode pentode valve. Full tone, volume and balance controls. Complete and ready to fit. Knobs \(3 / 6\) per sét extra. P. \(8: \mathbf{P}\). \(3 / 6\). Cash price \(£ 7 / 19 / 6\).

3 TRANSISTOR AMPLIFIER 79/6 9 volts. 1 control. P. \& P. 3/6.

621/3 ROMFORD RD., MANOR PK. E. 12 Tel. ILF 6001/3
U.A.8. B.S.R. MONARCH 4-SPEED AUTOCHANGER
8/1 Initial payment and 19 weekly payments of \(6 / 11\). Cash price \(£ 6 / 19 / 6\).
U.A.12. LATEST B.S.R. MONARCH 4-SPEED MIXER
9/7 Initial payment and 19 weokly payments of \(8 / 5\). Cash price \(£ 8 / 9 / 6\).

COLLARO CONQUEST 4-SPEED AUTOCHANGER
8/1 Initıal payment and 19 weekly payments of 6/11. Cash prise \(6 / 19 / 6\).

COLLARO CONQUEST STEREO AUTOCHANGER
\(12 / 6 \begin{gathered}\text { Initial } \\ \text { ments } \\ \text { pay ment and } \\ \text { of } \\ 11 / 6 \text {. } \\ \text { Carr. }\end{gathered}\) Cash price 11 gns.


\section*{EXTENSION \(19 / 9\) SPEAKERS}

Polished oak cabinet of attractive appearance. Fitted with 8in. P.M. speaker W.B. or Goodmans of the highest quality. Standard matching to any receiver. (2-5 ohms). Switch and flex included. Ins. carr. \(3 / 9\).

\section*{IDEAL FOR STEREOPHONIC SOUND}

8 in . P.M. Speakers \(8 / 9\). With O.P. trans. fitted 10/-. Post \(2 / 6\).
\(7 \times\) 4in. Elliptical speakers, 19/6.
\(9 \frac{1}{2} \times 4 \frac{1}{2} \mathrm{in}\). Elliptical speakers 22/6.
Post \(2 / 9\).
STURDY \(12 / 6\)
CASE
Covered in burgundy and grey washable rexine. washable rexine.



CABY MULTIRANGE TEST METER. Freshly Imported. Guaranteed Model A-10. A.C. D.C. Voltages, sensi rivity 2,000 ohms per volt. Ranges: 1000 v . Resistance 10K ohm and I megohm. D.C. Current: 0.5 mA ., 25 mA . 250 mA .' 25 Decibel 250 mA . Decibel range. Accuracy: \({ }^{2}\)
to \(3 \%\). Price \(£ 4 / 7 \%!6\). P. \& P. I/6. Ask for leaflet fully illustrating and describing this and other models.

SPARE CARRYING CASES FOR AVO MULTIMINOR WILL ALSO FIT MODEL A-10 ABOVE. NEW. Price \(10 / 6\) each. P\& \& P. I/-.

FRESHLY IMPORTED MINIATURE CONTACT COOLED RECTIFIERS Half.Wave Type
Max. A.C. In. 125 v. D.C. Out. 80 mA Max. A.C. In. 250 v. D.C. Out. 50 mA . Max. A.C. n. 250 v. D.C. Out. 50 mA .
Max. A.C. In. 250 v. D.C. Out. 85 mA . Max. A.C. In. 250 V
Television Type
Max. A.C. In. 250 v. D.C. Out. 300 mA .
18/6 Full-Wave Bridge Connected
Max. A.C. In. 250 y. D.C. Out. Max. A.C. In. 250 v. D.C. Out. 75 mA.
Max. A.C. In. 250 v. D.C. Out. 150 mA . 9/6 Max. A.C. In. 250 v. D.C. Out. 150 mA . \(15 / \mathrm{H}\)

SPECCIL OFFER. LIMITED Quantity.

\section*{GENERAL PURPOSE}

CATHODE RAY OSCILLOSCOPE The famous model 160-B C.R. 'Scope, manufactured by R.C.A. of U.S.A. Best general purpose instrument of its kind, complete purpose instrument of its kind, complete
with 6 in. cathode ray tube. Unused, guaranwith in. cathode ray rube. Unused, guaran-
teed perfect. For operation on 110 v. A.C. teed periect. For operation
Price \(£ 22 / 10 /\)-. Carr. \(10 /\) -
Price \(22 / 10 /\)-. Carr. to
Step-down transformer to enable the above Step-down transformer to enable
to operate on 230 v . Price \(19 / 6\).

SYNCHRONOUS MOTOR, one rev. every 24 hours. 110 v . or with resistor (supplied) 230 v . Price 27/6. P. \& P. 2/-.


WAVE GUIDE 3 cm . mounted on a carrying board consisting of: (1) directional coupler. (2) 90 degree bend. (3) co-ax to wave gulde adaptor type N. (4) British to W.916. (5) Co-ax to waye guide adaptor cir-
cular flange. cular flange. (6)
daptor.
Complete Circular to American adaptor. Complete in carrying case with coaxial cable. Price \(60 /\) -
Carr.

AERIAL AS ILLUSTRATED. Ideal for Car. Overall lengeh 33in., khaki, with flexible shaft which enables the aerial to be fixed firmly in any position. Price \(8 / 6\), plus P. \& P. \(1 / 6\).
NEW WIRE WOUND RHEOSTAT ON CERAMIC. 58 ohms, 50 watt, complete with instrument knob. Price 8/6. P. \& P. 1/6.
W. W. RHEOSTAT. New. 3.5K, 25 watts. Price 7/6. P. \& P. 1/6.
W. W. RHEOSTAT. New. 5K, 25 wates. Price 7/6. P. \& P. \(1 / 6\).
SLIDER RESISTANCE, 44 ohm, \(1 \frac{1}{2}\) amp. Price 18/6. P. \& P. 2/-.
EX P.O. MAGNETIC COUNTER 3 ohms type for \(4 \frac{1}{2} / 6\) volt D.C. operation. Price \(6 / 6\) each. P. \& P. \(1 /\).
AS ABOVE 500 ohm for \(24 / 36\) volt D.C operation. Price \(6 / 6\) each. P. \& P. I/-.


POTTED
TRANSFOR.
MERS. Type 2762 C Core: Input \(230 v .45 / 65\) cyeles.
Output \(350-0-350\) Output \(350-0-350\)
at 375 mA .25 v. at 1 amp., 21 v. at .5 amp ., 6.3 v . at it amp., 6.3 v . at
 Carr. \(6 / 6\).

Type 2759 C Core Input 230 v. \(45 / 65\) cycles. Output \(361-0-361\) at \(200 \mathrm{~mA} .361-0\) 361 at 65 mA . 5.16 v . at 4 amp ., 5.16 v . at \(3 \mathrm{amp} ., 3.25-0-3.25\) at \(2 \mathrm{amp} ., 6.5 \mathrm{v}\). at 5 amp . 3.25-0.3.25 at 5 amp . Price 65/-, Carr. \(6 / 6\).

Type 2669 Oil filled
Input 230 v. \(45 / 65\) cycles. Output 0.70 v. 75 v., 80 v., at 4 amp. Price 42/6. Carr. \(3 / 6\).


WHEATSTONE BRIDGE UNIT. 4 stud switches \(0-10,0-100\) ohms, galvanometer centre zero, F.S.D. 2.5 mA . In oak
 \(\begin{array}{ll}7 \frac{1}{2} \times 6 \text { in., } & 40 / 2 \\ \text { each. P. \& P. } 3 / 6 .\end{array}\)

EVERSHED AND VIGNOLES. Circuit testing Ohms
 "S" complete with testing prods, inst. book ges: 0-3 and \(0-30\) ohms.Brand new, guaranteed perfect, as illus. Offered as fracion of maker's price. eq \& \(17 / \mathrm{P}^{2}\) each.

\section*{BRIDGE}

MEGGER,
Evershed and
 II, 250 volt. Con
dition as new, guaranteed perfect. Price \(£ 22\). Carriage paid. Leather case available 20/- extra,

TRIPLE RANGE VOLTMETER. 0-5 25-250 r. D.C. M/C 3 tin. merer 3in. scale, mounted in bakelite carrying case \(7 \frac{1}{2}\) in \(x\) \(4 \frac{1}{2} \mathrm{in}\). \(\times 3\) in. complete with handle and test eads. 27/6 each. P. \& P. 2/-.

12 v. D.C. AMPLIFIER, as new, 12 operation on 12 v. car battery, 10 watts undistorted output, with 6L6 valves in push-pulf. Mike/

ped ourpur \(7 \frac{1}{2}, 15,62,100,250\) or 500 ohms E12/10/-each. Carr. 15/-.


MIDGET ROTARY TRANSFORMERS. 2 lin . dia, \(\times 4 \frac{1}{2} i n\). Input 11.5 volt. Output \(310 / 365\) volts at 30 mA . Brand new. \(12 / 6\) each. P. \& P. \(1 / 6\).


FRESHLY MANUFACTURED TRANS. FORMERS. Ideal for model makers. Input tapped 2001250 volt. Output multi-tapped from 3 to 30 volts at 2 ampere. Price \(19 / 6\). P. \& P. 2/-.

JACK PLUGS, cylindrical, bakelite, screw on covers, red or black as required, two contacts. Price \(2 /\) - each post free. Dozen lots 20/- post free. Three contacts same price.

MERCURY SWITCH, 10 amp. contacts, Single pole, New. Price 3/6. P. \& P. 6d.
\begin{tabular}{|c|c|}
\hline \multicolumn{2}{|l|}{METERS GUARANTEED PERFECT} \\
\hline Charging Types & \\
\hline 2 t amp. D.C. M.l. 2 in . fl. rnd. & 716 \\
\hline 5 amp D.C. M.I. 2 itin. fl. rnd. & \(11 / 6\) \\
\hline \(7 \frac{1}{2}\) amp. D.C. M.I. \(3 \frac{1}{2}\) In. proj. & \(12 / 6\) \\
\hline \multicolumn{2}{|l|}{9 amp D.C. Hot Wire W.R. \(2 \frac{1}{2} \mathrm{in}\). fi. rnd. \(6 / 6\)} \\
\hline \multicolumn{2}{|l|}{Voltmeters} \\
\hline 12 v.D.C. M.C. \(2 \frac{1}{2}\) in. & \(8 / 6\) \\
\hline 20 v. D.C. M.C. 2 in . fl. & \(9 / 6\) \\
\hline 25 v. D.C. M.C. 2 in . fl. rnd & \(7 / 6\) \\
\hline 30 v. M.I. 3in. proj. rnd. & \(10 / 6\) \\
\hline 40 v. M.C. 2 in. fl. sq & \(9 / 6\) \\
\hline 150 v. D.C. M.C. fl. rnd. \(2 \frac{1}{2} \mathrm{in}\). & 10/6 \\
\hline 250 v. A.C. rectified moving coillinear scale \(3 \frac{1}{\text { b }}\) in. fl. rad. & \\
\hline 300 v. A.C. M.1. \(2 \frac{1}{2} \mathrm{in}\). & 221- \\
\hline 400 v. A.C. M.I. \(4 \frac{1}{2} \mathrm{in}\). fl. rnd. & 35/- \\
\hline \multicolumn{2}{|l|}{Milliammeters} \\
\hline 2 mA . M.C. \(2 \frac{1}{2}\) in. fl. rnd & \(14 / 6\) \\
\hline 5 mA . M.C. 2 in . round & \(12 / 6\) \\
\hline 10 mA . M.C. \(3 \frac{1}{2} \mathrm{in} . \mathrm{fl}\). rn & 301- \\
\hline 30 mA . M.C. \(2 \frac{1}{2} \mathrm{in}\). fl. rn & \(9 / 6\) \\
\hline \(200 \mathrm{~mA}, \mathrm{M}, \mathrm{C} .2 \frac{1}{2} \mathrm{in} . \mathrm{fl}\). rnd & \(9 / 6\) \\
\hline 500 mA . M.C. \(2 \frac{1}{2} \mathrm{in}\), fl. r & \(9 / 6\) \\
\hline \multicolumn{2}{|l|}{Microamp} \\
\hline \multicolumn{2}{|l|}{50 microamp. sealed \(0-100\), M.C. \(2 \frac{1}{2}\) in. rnd. fl.} \\
\hline \multicolumn{2}{|l|}{200 microA. M. C. \(2 \frac{1}{2}\) in. rnd. fl. (cali-} \\
\hline 50 microA. \(2 \frac{1}{2} i n .5 q u a r e\), sidefieting 3 & \\
\hline scales ................. & 35/- \\
\hline 500 microA. M.C. 2 in . rnd. Postage on all meters 1/- each. & 16/6 \\
\hline
\end{tabular}

NEW UNCHARGED UNFILLED 12 VOLT ACCUMULATOR 9 ampere in unspillable plastic cases. Comprises cells connected by erminal strips. 6 \(\times 5 \frac{1}{2} \times 4 \frac{1}{2}\) in. over terminals. Price
19/-, plus P. \& P. 2/9. Wooden carrying case for same
 with lid and strap price \(3 / 6\).


MINIATURE P.M. MOTOR. 2/24 volt, reversible. Itin. dia. New. Price 9/6 each. P. \& P. I/-.

AIRCRAFT CINE CAMERA G45B Mk. III Fully modified, fitted with \(/ / 3.5\) triple anastigmatic lens, takes 25 tt . of 16 mm . film fitted with \(24 v\) motor. 16 exposures per see. Brand new, original packing, \(£ 4 / 10 /\) each. P. \& P. paid.


SIEMENS H.S. RELAY. Very latest type, sealed. H96E. 1,700 ohms plus 1,700 ohms, single C.O. contacts. Brand new with fixing clip. In maker's cartons Price \(16 / 6\) each, plus \(1 /-P\) \& \(P\).

NEW CAR. PENTER'S TYPE POLARISED RELAYS. \(2 \times 9,500\) turns \(2 \times 9,500\) turns
at 1,685 ohms. at 1,685 ohms.
Price \(22 / 6\) each. Price \& P. 1/-.


BRAND NEW SOUND POWER OPERATED EX ADMIRALTY HEAD AND BREAST SETS. Two such sets connected up will provide perfect intertomm., no batteries required. Will operate up to \(\frac{1}{2}\) mile. Original manufacturer's boxes. Price \(17 / 6\)
each, plus P. \& P. \(2 /\); or \(32 / 6\) per pair. P. \& P. \(3 /\).

\section*{AUTO TRANSFORMER}

Air cooled, very conservatively rated at 3 kVA . will handle 6 kVA . Tapped \(220 / 230 / 240 / 250\) volt, 12 amp . \(105 / 110 / 115 / 120\) volt, \(28,5 \mathrm{amp}\). Brand new. Each one shrouded in a metal case and packed in original manufacturer's wooden case. Price \(\mathbb{1 5}\). Carr. fI. Nett weight over 2 cwt.

MINIATURE MOVING COIL DIFFERENTIAL RELAY. Two coils 350 ohms each. \(<\) Operating current
 minimum 140 microamp, nominal 400 microamp, maximum 8 milliamp. One pole two way, or, centre stable. Two way contact current 100 mA , at 50 V . A.C. or D.C. Size \(14 \times \frac{3}{4} \times \frac{3}{4}\) in. Price \(22 / 6\) each.

HIGH SPEED RELAY. Siemens, two bobbins, 1,000 ohms each. New, 1016 each. P. \& P. I/-

SOLENOID OPERATED MAGNETIC RELAY. Type S. 5CW/3942 with 4 make, 4 break 25 Amp. contact D.C. coil resistance 160 ohms, 24 v . operation. Housed in metal screening can 2 itin. \(x\) lin. \(x\) litin. Brand new. \(7 / 6\) each. P. \& P. 6d.
U.S.A. 27-volt 4-pole CHANGE-OVER RELAYS. Brand new and boxed, \(5 / 6\) each. P. \& P. 6d.

ROTARY RELAY, 12 volt. Heavy duty change-over contacts and one low current for external circuit, plus one break set. Price \(7 / 6\). P. \& P. 1/6.

A VERY SUPERIOR BRAND NEW RELAY IDEAL FOR MODEL WORK. 7,000 ohms coil. Will pull in at 750 microamp and out at 450 microamp. Change-over, platinum contacts. Vacuum sealed, will therefore not be affected by oll, moisture or water and never needs adjusting. Weight \(2 \frac{1}{8}\) oz. Price 18/6. P. \& P. I/-.

MINIATURE TYPE SEALED SLAVE RELAY. 700 ohms coil. Will work on 12 v . D.C. Single pole change-over contact. Weight 2 ozs. Ex. new equipment. Price \(9 / 6\). P. \& P. 1/-.


20 WAY STRIP containing standard Post Office telephone Jack Sockets, overall size \(11 x\) \(3 \frac{1}{2} \times \frac{1}{2}\) in. New. Price 15/- each. P. \& P. 1/6. lo WAY STRIP standard Post Office rele\begin{tabular}{l} 
phone Jack Sockets, spacing allowing igranic \\
Jack Plugs New. Price \(10 /\) P \& P \\
\hline
\end{tabular} Jack Plugs. New. Price \(10 /\).. P. \& P. \(1 / 6\).
LATEST MOST MODERN TYPE OF EX W.D. MINIATURE HEADPHONES As illustrated. Brand new, low impedance. Price \(10 / 6\) plus P. \&
P. \(1 / 6\). NEW MOVING COIL HEAD. SETS. Complete
hand microphone, whth plug suitable for No 19 set. Price \(12 / 6\) each, plus P. \& P. 2/-.
AUTO TRANSFORMERS. Step up, stop down, \(110-200-220-240 v\). Fully shrouded. New. 300 watt type \(62 / 2 /\) each. P. \& P. 2/6. 500 watt type \(3 / 3 /-\) each. P. \& P. 3/9. 1,000 watt type \(44 / 4 /\) each. P. \& P. 6/6. Also 60 wates, \(19 / 6\) each. Plus P. \& P. \(2 /\) -
MARCHING COMPASS Mk. I. Brand new ex W.D. Price 14/6. P. \& P. I/-.

L.T. TRANSFORMER. Input
230 V. Output 50 V. 50 amp. Adjustable by regulator switch on primary. Steel case With mains switch overload. Welght 150 lb . Wound at 800 amps. per sq. nch. Brand new Price \&15. Carr. £ 1.

PLATE TRANSFORMER of very best U.S.A. make, brand new, original manufacturers cases. Input tapped at 190/210/230/250 V. Output 2250-0. 2250 centre tap. ped 400 mA . Nett ped 46 ib Net weight 76 lb., size \(13 i n . \times 9 i n . \times 6 \frac{1}{2} i n\).
Price \(66 / 10 /-\) each. plus carr. 10/.


BRAND NEW SELENIUM FULL WAVE BRIDGE TYPE RECTIFIERS, in manufacturer's original pack= ing. D.C. output 36 v. 10 amp., made up of \(12 \times 110 \mathrm{~mm}\). dia. plates. These fitted in cooling funnel (removable). Size \(11 \frac{1}{2}\) in. \(x^{8 i n} . x^{4} \frac{3}{4}\). \(3 / 3\).

\section*{TWELVE}

PLATE F.W. BRIDGE CON-
NECTED RECTINECTED RECTI-
FIER mounted on FIER mounted on
\(200 / 250\) volt A.C. input transformer. Output \(36 / 40\) volt D.C. at 1.2 amps . New, perfect. Price 16/6. P. \& P.. \(3 / 6\). SPRINGLOADED FUSED TEST PRODS, complete with wire leads and spade terminals. Price \(4 / 6\) per pair. P. \& P. 1/-.

MUIRHEAD VERNIER DRIVE. Scaled 0-180 degrees. ratio \(31 / 1\), dia. 3 in., as fited to R.F. 26 units. Complete with lampholder. In manufacturers' orig inal packing. New. 8/6 each. P. \& P. I/6.

\section*{NEW-The "CONTINENTAL-6" (Superseding the "TRANSISTOR-8") COMBINED TRANSISTOR PORTABLE/CAR RADIO SUPERHET}

\section*{SPECIFICATION}
t
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195 to 560 metres on medium wave. 1,150 to 1,800 metres on long wave. 400 mW . push-pull output. A.V.C. and Car radio. Standard Fitting Slow-motion tuning. \(\quad \star\) Size \(9 \frac{1}{2} \times 7 \times 3 \frac{1}{2}\) HI-FI SPEAKER. \(\quad \star\) Weight 4 lbs . 6 months' battery life. \(\star\) EASY TO BUILD Resistor \& Condenser leads pre-trimmed. Printed circuit board marked with component numbers.
* EDISWAN TRANSISTORS

XAIO2, 2-XAIOI, XBIO3, 2-XClO1. 2-DIODES.

TRANSISTOR "8"
STILL AVAILABLE AT \(£ 10-19-6\)

\section*{TOTAL COST OF ALL SPECIFIED COMPONENTS INCLUDING CABINET,BATTERY,ETC., ONLY Ell/10/-. P.P. 3/6.}

All components available separately. Send for descriptive leaflet and prices.

> A highly sensitive and selective portable fully tuneable on medium and long waves. Performs equally well as a car radio. Low running costs, good looks and ease of construction combine to produce a radio equal to any commercial receiver in the 20 gn . class.


2-WATT POWER STAGE For use with 'Continental.' Works from 12 -volt supply. Overall size \(4 \frac{1}{2} \times 3 \frac{1}{4} \times 2 \frac{1}{i n}\). All Overall size \(4 \frac{1}{2} \times 3 \frac{1}{4} \times 2\) in. All
parts with Power transistor, less parts with Power transistor, less
speaker. \(52 / 6 . ~ P . P . ~\)
2/.
Sin. speaker. \(52 / 6\). P.P. \(2 /-;\)
\(18 / 6 ; 7 \times 4,20 /-6 \frac{1}{2} \mathrm{in} ., 18 / 6\).


TOTAL 69/6 POST \(\star\) Personal phone
NEW BOOKLET FREE: All components sold separately
GOOD RECEPTION ANYWHERE

\section*{AUDIO GENERATOR}

Ideal for audio circuit checking or R.F. modulator. With \(\times 8104\) transistor. All components
+ Size \(2 \frac{1}{4} \times 1 \frac{1}{2} \times \operatorname{lin}\). \(\star\) Size \(2 \frac{1}{4} \times 1 \frac{1}{2} \times\) lin.

\section*{R.F., I.F. GENERATOR}
* Size \(2 \frac{1}{4} \times 1 \frac{1}{2} \times \operatorname{lin}\). Harmonic output \(450 \mathrm{kc} / \mathrm{s}\) to \(2 \mathrm{me} / \mathrm{s}\) or more. Ideal for complete receiver alignment. All components \(25 /=\) P.P. \(1 /\) -

AUDIO, R.F., I.F. SIGNAL TRACER
* 2 Ediswan transistors. \(\star\) Headphone output \(\star\) Size \(4 \frac{1}{2} \times 3 \times\) lim: All parts \(\quad 37 / 6\)

\section*{250mW "ADDON" STAGE}
\(\star 2\) Ediswan Transistors \(*\) Push-pull up to 250 \(\$ 2\) Ediswan ransistors \(\star\) Push-pull up to 250
mW . \(\star\) 3in. ELAC speaker. \(\star\) Cabinet \(5 \frac{1}{4} \times 3 \frac{1}{2}\) \(x\) itin. A unit for use with Major 2 and 3 or any earpiece pocker-portable to give full speaker output. Complete set of parts with cabinet \(59 / 6\)


TRANSISTORS GUARANTEED
Red Spot, audio 5/White Spot, RF \(7 / 6\) Photo-Trans....... 10/XB104, Audio ... 10/XCI21, 500 mW . P.P.. OC 71, Audio 17/SBO78. H F ... 14/SBO78, H.F. ...... 10/full list and

\footnotetext{
TRANSISTOR TRANSMITTER
* Top Band 150 to
} 160 metres.
\(\star\) Voice modulated. * 3-Transistor * Size \(4 \frac{1}{2} \times 3 \times 1 \mathrm{itin}\). Pocket size 1.8 to 2 Mc/s Transistor Transmitter, ideal for short range communication. All parts \(57 / 6\) P.P. I/6
Free Diagram and List

SB305, Rad. Control................... 15/SB23I, Rad. Con- \(22 / 6\) SB23IR, ose./ mixer, H.F. ... 30/OCi70, Power, HF . 35/VI5/10P, Power \(17 / 6\) data on réquest.

> CRYSTAL MICROPHONE INSERTS
\(\mathrm{A} C O S\) 23-4, lin. square ......... \(\operatorname{ACOS}\) 19-4, 1 iln .
round ..............

ACOS 14, \(1 \frac{1}{2} \mathrm{in}\). round.......... round............ \(12 / 6\) P.P. 6d, any type.


\section*{TRANSISTOR QUARTZ CRYSTAL OSCILLATOR}
* Uses crystal fundamentals between \(3 \mathrm{Mc} / \mathrm{s}\) and \(12 \mathrm{Mc} / \mathrm{s}\).
* New \(25 \mathrm{Mc} / \mathrm{s}\) Transistor
* Ideal Frequency Check.

All parts, less crystal and holder 22/6 P.P. I/Suitable Crystals from 5/-
Send for Free Diagram and Quarez Crystol List
CAR RADIO 2-watt Amplifier
* \(7 \times 4 \mathrm{in}\). high flux speaker

Y VI5/IOP power transisto
* Works off car 12 -vole battery

May be used with any battery portable with 15-ohm or 3-ohm output transformer
Complete set of parts ................. 65/-P. \& P. 2/6 Unit built-up and tested ............. 77/6 P. \& P. \(2 / 6\)
USE YOUR PORTABLE IN YOUR CAR!
"SUPER-SIX" TRANSISTOR PORTABLE SUPERHET \(\begin{aligned} & \text { size } 7 \frac{1}{2} \times 4 \frac{1}{2} \times 2 . \\ & \text { Weight } 20 \text { oz. }\end{aligned}\)
* MEDIUM AND LONG WAVES * MULLARD TRANSISTORS
* PRINTED CIRCUIT
* SENSITIVE AND SELECTIVE
Total cost of all components
E9. 10.0
P.P \(2 / 6\)
All parts sold separately


High sensitivity and selectivity combine ta give excellent reception on both medium and long waves this set is recommended as being one of the easiest to build transistor printed circuit sets ever offered

\section*{VALVE VOLTMETER}

\section*{R.C.A. Type 165-A}
D.C. ELECTRONIC VOLTMETER.
6-Ranges. \(0-3-10-30-100-300\) and 1,000 volts. Input res: 11 -meg. constant on all ranges. Sensicivity: \(3,666,666\) ohms per volt on 3 v . scale.
A.C. VOLTMETER.
5-Ranges: 0-10-30-100-300-1,000 volts. Sensi. tivity: 1,000 ohms per volt.
ELECTRONIC OHMMETER.
6-Ranges, from 0.1 ohms to 1,000 megohms.
Movernent. 200 microamperes. D.C. accuracy
COMPLETE WITH INSTRUCTION BOOK AND TEST PRODS, BRAND NEW.
Input \(110-250\) volts A.C.
ONLY \(\mathbb{L} \mid 2 / \| 0 /=\) P.P. \(3 / 6\)
SPECIAL PURCHASE - LIMITED STOCKS BUY NOW




MARCONI NO. 19 SET CRYSTAL CALIBRATOR
CRYSTAL CONTROLLED OSCILLATORS: 10 \(\mathrm{Kc} / \mathrm{s}\)., \(100 \mathrm{Kc} / \mathrm{s}\). and \(1 \mathrm{Mc} / \mathrm{s}\). On/Of MODULATOR. With handbook. Unused. ONLY 79/6. P.P. 2/6.

\section*{44 DYNAMOTORS}

24 volt D.C. 10230 V. A.C. \(50 \mathrm{c} / \mathrm{s}, 100\) watts.
E5/10/- P.P. 7/6.
28 volts D.C. to 250 voles \(60 \mathrm{~mA} .12 / 6\). P.P. 216 12 voles D.C. to 220 volts 165 mA . \(32 / 6\). post free.

\section*{AN/ARN-5D GLIDE PATH RECEIVER} 3-channel U.H.F. Receiver; uses plug-in crystals (not supplied): operating on 332.6; 333.8; \(335 \mathrm{Mc} / \mathrm{s}\). Unit contains 7-6AJ5; 28D7: 2-12SN7: I2SR7: Relays etc. BRAND NEW and boxed: a bargain at \(59 / 6\) P.P. 5/-.

\section*{QUARTZ CRYSTALS}

FROM 5/- EACH
From \(6 \mathrm{Kc} / \mathrm{s}-4 \mathrm{Mc} / \mathrm{s}\). FT243.
FT241, \(10 \times \mathrm{J}\) and B7G.
All types for all purposes. Send for free list.

\title{
RADIO CLEARANCE LTD.
}

\author{
TRADE \\ ENQUIRIES \\ INVITED \\ 27 TOTTENHAM COURT RD., LONDON, W.I \\ The oldest Component Specialists in the trade \\ Telephone: MUSEUM 9188 EST. 30 YRS
}

ELECTROLYTIC CONDENSERS-WE HOLD THE LARGEST STOCK OF ELECTROLYTICS IN ENGLAND ABBREVIATIONS:
C. Clip mounting tag ends. P. Prong mounting.
T. Tag ended. S. Sleeved.

PC. Printed Circuit. R. Reversible polarity.

\author{
M. Moulded with wire ends.
}
\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline & SIN & NGLES & & & Capacity (Mids.) & Wkg. Volts & \(81 z 0^{\circ}\) & Type & Price & Capacity (Mifds.) & Wkg. Volta & Size* & Typo & Price & Capacity (Mids.) & Wkg. Volt: & 8ize* & Type & Price \\
\hline Capacity & Wkg. & & & & (end & 350 & \(1 \times 3\) & \({ }^{\text {c }}\) & \(2 / 6\) & \(12+28\) & 275 & \(1 \times 2\) & & \(1 / 6\) & \(100+200\) & 250 & \(11 \times 4\) & c & \(2 / 6\) \\
\hline & & Size" & Type & Price & 75 & 12 & \(1 \times 11\) & c & & \(16+16\) & 150 & \({ }_{1 \times 1} \times 1\) & \({ }^{\text {T/8 }}\) & \(11-\) & \(100+200\) & 275 & \(11 \times 4\) & C & \\
\hline 1 & 275 & + \(\times 1\) & W/s & 1/- & 80 & 450 & \(1 \times 3\) & W/8 & \(2 / 6\) & \(18+16\) & 275 & \(1 \times 2\) & & \(2 /-\) & \(100+250\) & 275 & \(1{ }^{1} \times 4\). & C & - \\
\hline 2 & & \(13 / 32 \times 1\) & M & \(1 / 4\) & 100 & \({ }^{6}\) & \(13 / 32 \times 1\) & & 114 & \(18+16\) & 350 & \(1 \times 2\) & & \(31-\) & \(100+300\) & \({ }_{275}^{275}\) & \(11 \times 4\) & \({ }_{\text {c }}\) & 4 4- \\
\hline \(\stackrel{2}{4}\) & 275 & \(1 \times 1\) & \(\stackrel{\text { w }}{ }\) & 1/- & 100 & 12 & \(1 \times 18\) & W/B & & \(18+16\) & 450 & -1×2 & W/8 & 4/- & \(100+400\) & 275 & \({ }^{2} \times 14\) & C & 4,- \\
\hline 4 & 150 & \(1 \times 1\) & \({ }_{\mathbf{W}} / 8\) & 1-1- & 100 & \({ }_{25}^{25}\) & \(1 \times 18\) & T/8 & 1/3- & \(20+10\)
20 & 450 & +1×3 & P & 3/- & \(150+30\) & 350 & \(11 \times 4\) & c & 5- \\
\hline 5 & 150 & + \(\times 1\) & & 1/- & 100 & \({ }_{25}^{25}\) & \({ }^{1} \times 18\) & & \(1 / 3\) & 20+20 & 430 & - & & & & & & & \\
\hline \({ }_{8}^{5}\) & 250, & \(\pm \times 1\) & W/8 \({ }_{\text {W/ }}\) / & 181/3 & 100 & 25
270 & \(1 \times 2\) & \({ }^{\text {c }}\) & \(11 /\) & 20+20 & 450 & 1×3 & P & \(31 /\) & & RIPL & ES Et & & \\
\hline 8 & 150 & \(1 \times 1\) & & 10 d & 100 & 275 & \(1 \times 3\) & - & \(1 / 6\) & \(24+24\) & 350 & \(1 \times 2\) & c & & & & & & \\
\hline 8 & 200 & 1×1t & & & 100 & 275 & \(1 \times 3\) & P/S & 21- & \(25+25\) & 300 & \(1 \times 2\) & P & \(1 / 6\) & \(8+8+8\) & 350 & \(1 \times 2\) & P & \\
\hline 8 & 250
275 & \% \(\times 1\) & Worw/ & & 100
150 & \({ }_{23}^{350}\) & \(1 \times 3\) & \[
\stackrel{\mathrm{PC}}{\mathrm{w}}
\] & & 30
\(32+30\)
+32 & 150 & \({ }^{1 \times 1} \times\) & \({ }_{\text {W }}\) /8 & 1/- & \(18+8+4\)
\(16+16+4\) & \({ }_{275}^{275}\) & 1×2 & c & 2/6 \\
\hline 8 & 275
350 & - \(\times 1\) & & \(11 / 6\) & 150
150 & 25
150 & \(1 \times 19\)
\(1 \times 3\) & \({ }_{\text {w/ }}\) & 1/3 & \(32+32\)
\(32+32\) & 150 & - \(1 \times 2\) & \({ }_{\text {W/G }}^{\text {c }}\) & \(\stackrel{1 / 2}{1 /}\) & \(18+18+4\)
\(16+16+16\) & \({ }_{275}^{275}\) & 1×2 & & 2/8 \\
\hline 8 & 450 & + \(\times 1\) & \({ }_{\text {W }}\) /8 & \(1 / 11\) & 200 & 1 & \(1 \times 1\) & \(\mathrm{M}^{\text {m }}\) & 1/4 & \(32+32\) & 150 & \(1 \times 3\) & P & 10 d . & \(20+15+15\) & 450 & \(1 \times 3\) & P/8 & 3/6 \\
\hline 8 & 750 & \(11 \times 4\) & c & 5/6 & 200 & 12 & 1) \(\times 1\) & w & \(1 / 6\) & \(32+32\) & 250 & \(1 \times 2\}\) & PC & 1/6 & \(20+20+20\) & 250 & \(11 \times 2\) & P & 1/- \\
\hline 10 & & 13/32 \(\times 1\) & M & \(1 / 4\) & 200 & 25 & \(1 \times 12\) & T & 10 d. & & 275 & \(11 \times 2\) & & \(2 / 8\) & \(25+25+25\) & 23 & \(1 \times 2\) & \({ }_{\text {c/ }}\) & \\
\hline 10 & 15 & \(\pm \times 1 t\) & T/8/R & 116 & 200 & -35 & 1 \(1 \times 1\) & \({ }_{8}^{\text {c/8 }}\) & 10d. & \(32+32\)
\(32+32\) & \({ }_{350}^{275}\) & \({ }_{1 \times 2}^{1 \times 2}\) & \({ }^{\text {c/8 }}\) & \(2 / 6\) &  & \({ }_{275}^{275}\) & \(11 \times 2\) & \({ }_{\mathbf{P}}^{\mathbf{P}}\) & 2/6 \\
\hline 10 & \({ }^{23}\) & (xit & \({ }_{W}^{\text {T/7 }}\) & 1/3 & 200 & 275
6 & 11×3 & c/8 & 10d. & 32+32 & \({ }_{350}\) & +1×2 & \({ }_{P / 8}\) & 3/- & 3
\(32+8+8\)
\(32+16\) & \(200 / 25\) & \(1 \times 2\) & \({ }_{\text {P }}\) & \(\stackrel{2 /-}{1 /-}\) \\
\hline 10 & 450 & + \(\times 2\) & w & 1/9 & 250 & 12 & \(1 \times 1\) & W & 1/- & \(32+32\) & 450 & \(11 \times 3\) & W/8 & 4/6 & \(32+32+2\) & 275 & \(1 \times 2\) & c & \\
\hline 12 & 25 & \(13 / 32 \times 1\) & M/R & 1/6 & 250 & 25 & \(1 \times 1\) & T & 1- & \(40+20\) & 150 & \(1 \times 2\) & \({ }^{\text {P }}\) & 10 d. & \(32+32+6\) & 275 & \(11 \times 2\) & C & 6 \\
\hline 16 & 150 & 4 \(\times 14\) & T/8 & \({ }^{1 /-}\) & 250 & \({ }^{25}\) & \({ }^{3} \times 17\) & & \(1 / 3\) & \(40+40\) & 150 & \(1 \times 3\) & \(\stackrel{P}{P}\) & 10 d. & \(32+32+8\) & 250 & \(11 \times 2\) & c & \\
\hline \({ }^{16}\) & \({ }^{276}\) & \({ }^{1} \times 2\) & T & 10d. & 250 & 50 & \(1 \times 2\) & \({ }_{\text {c }}\) & \(1 / 6\) & \(40+40\)
\(40+40\) & 275
300 & 11×2 & & & \(32+32+25\)
\(32+32+32\) & 278/25 & 1×3 & C & \\
\hline \({ }_{20}^{18}\) & 350
6 & \(1 \times 2\) & P & 1/- & 250 & \({ }^{150}\) & +1103 & \({ }_{\mathbf{P} / \mathrm{R}}\) & 88. & \(40+40\)
\(40+40\) & 300
450 & \({ }_{11} \times 3 \times 8\) & \({ }_{\text {W }}{ }^{\text {PO/8 }}\) & 2/- & \(32+32+32\)
\(32+200+50\) & 330
275 & 11×2 & \(\stackrel{\text { c }}{ }\) & \(4{ }^{4}\) \\
\hline 20 & 12 & 13/32 \(\times 1\) & \(\mathrm{m}^{\text {r }}\) & 1/4 & 500 & 6 & | \(\times 1\) & & 10d. & \(50+50\) & 150 & \(1 \times 2\) & - & 1/- & \(32+300+70\) & 275 & 1 1 \(\times 4\) & c & \\
\hline 20 & 150 & \(1 \times 1\) & T & 10d. & 500 & 8 & \(1 \times 2\) & c & 8 d . & \(50+50\) & 200 & \(1 \times 3\) & \({ }_{P}\) & \(1 /\) & \(40+30+20\) & 150 & \(1 \times 2\) & P & \\
\hline 20 & 450 & \(1 \times 2\) & W/8 & 1/9 & 500 & 12 & \(1 \times 1\) & T & & \(50+50\) & 250 & \(11 \times 2\) & \({ }^{\text {P }}\) & \(1-\) & \(40+40+12\) & 275 & \(1 \times 2\) & C & 6 \\
\hline 25 & 12 & 13/32 \(\times 1\) & M/R & \(1 / 6\) & 500 & 12 & \(1 \times 11\) & W & 1/3 & \(50+50\) & 275 & \(14 \times 2\) & P & \(1 / 8\) & \(40+40+20\) & 275 & \(1 \times 2\) & P & 3/- \\
\hline 25 & 25 & 13/32 \(\times 1\) & M & & 500 & 12 & \(1 \times 2\) & - & 8 d. & \(50+50\) & 275 & \(11 \times 3\) & & \(1 / 6\) & \(40+40+20\) & 300 & \(1 \times 2\) & & \\
\hline 25 & 25 & \(1 \times 1\) & W & \(1 / 6\) & 500 & \({ }^{25}\) & \(1 \times 2\) & \[
\underset{0}{\mathbf{C}}
\] & 1/6 & \(50+50\)
80
80 & \({ }_{300}^{275}\) & \(1 \times 34\) & & 1/9 & \(40+40+32\)
\(40+80+20\) & \({ }_{450}^{275}\) & \({ }^{11} \times 2 \times 2{ }^{1}\) & PC & \\
\hline 25
25 & 50
50 & \(1 \times 1\) & \({ }_{\text {W }}^{\text {w }}\) & \(\frac{1 / 9}{1 / 9}\) & 5000
8000 & \({ }_{6}^{6}\) & 1182 & \({ }_{\text {d/8 }}\) & 3/6 & \(50+50\)
\(60+200\) & 375
275 & \(11 \times 2\)
\(1+\times 3\) & \(\stackrel{0}{0}\) & 846 & \(40+80+20\)
\(50+24+24\) & \({ }_{275}\) & \(11 \times 3\) & & \\
\hline 25 & 350 & \(1 \times 1\) & w & \(1 / 9\) & 8000 & 6 & \(1: \times 3\) & C/B & 4/- & \(60+100\) & 275 & \(1 \times 8\) & \(\stackrel{P}{P}\) & \(2 / 6\) & \(50+50+8\) & 275 & \(1 \times 3\) & \({ }^{P}\) & \\
\hline 32 & \({ }^{275}\) & \(1 \times 2\) & \({ }_{\mathbf{W} / 8}\) & \(1 / 6\) & & & & & & & 350
275 & & & & \(50+50+10\)
\(50+50\) & 150
350 & \(1 \times 2\) & & \\
\hline 40
40 & 150
350 & + \(\times 2\) & \[
\underset{\mathbf{P}}{\mathbf{W} / \mathbf{8}}
\] & \({ }_{1}^{6 d} 1\). & & DO & UBLE & & & \(60+200\)
\(80+250\) & 275 & \(11 \times 4\}\)
\(12 \times 4\) & \({ }_{C}\) & \(3 / 6\)
\(3 / 6\) & \(60+50+50\)
\(80+300+30\) & \(\begin{array}{r}350 \\ \hline 275\end{array}\) & 込 \(1 \times 3\) & \({ }_{\text {P }}^{\text {P }}\) & \\
\hline 50 & & \(13 / 32 \times 1\) & M & 1/4 & & & \(501 \times 2\) & c & 2/3 & \(80+300\) & 275 & \(1{ }^{1} \times 4\) & 0 & \(3 / 6\) & \(100+40+40\) & 450/50 & \(14 \times 4\) & P & \\
\hline 50
50 & 12 & \(13 / 32 \times 1\) & \({ }_{W}^{\mathrm{M} / \mathrm{R}}\) & 116 & 8+8 8 & & 50 & & 3/9 & \(100+65\)
\(100+100\) & 250 & \({ }^{1} \times 1 \times 3\) & & & \(100+100+5\) & \begin{tabular}{ll}
50 \\
& 300 \\
\hline 275
\end{tabular} & \(11 \times 3\) & P & 46 \\
\hline 50
50 & \({ }_{2}^{12}\) & 1 \(\times 1\) & W & \(1 / 6\)
\(1 / 6\) & \(8+8\)
\(8+16\) & & 50, \(1 \times 1+\) & W/8 \({ }_{\text {W/8 }}\) & \(3 / 6\) & \(100+100\)
\(100+100\) & \({ }_{2 / 12}^{12}\) & +1×2 & \(\stackrel{C}{\mathbf{P}}\) & 11- & \(100+100+2\)
\(100+250\) & 200275 & \(11 \times 4\) & \({ }_{0}^{\text {c }}\) & \\
\hline 50 & 50 & | \(\times 1\) & T & 116 & \(10+10\) & & \(501 \times 2\) & w/s & \(2 / 6\) & \(100+100\) & 275 & \(18 \times 3\) & & 2/6 & \(100+400+1\) & \(18{ }^{275}\) & 19x4 & c & 4 \\
\hline 60 & \({ }^{275}\) & \(1 \times 3\) & \({ }^{\mathbf{W}}\) & \(1 / 9\) & \(12+18\) & & \(751 \times 2\) & \(\stackrel{P}{1}\) & \(1 / 6\) & \(100+100\) & 300 & \(1 \times 3\) & \({ }_{\text {P }}\) & 31 & \(100+400+3\) & \(32 \quad 275\) & \(18 \times 4\) & - & 4-1 \\
\hline 60
64 & 350
275 & \(11 \times 2\)
\(1 \times 3\) & \({ }_{\mathbf{P}}{ }^{\text {P/8 }}\) & 1/6 & \(18+12\)
\(12+24\) & & 755 & \({ }_{0}\) & 1/6 & \(100+200\)
\(100+200\) & 25 & - & \({ }_{P}\) & 1/- & \(200+250+2\)
\(40+20+10\) & & 18 \(\times 1 \times 2\) & & 8)- \\
\hline
\end{tabular}

All voltages quoted are WORKING.

STAMPED AND ADDRESSED ENVELOPE with any enquiry please. please allow full postage and packing charges.
TERMS OF BUSINESS: CASH WITH ORDER OR C.O.D. ON ORDERS OVER IO/-.


\section*{Valve holders}

4 pin UX. Yd. 8 pin Brit. Pax. 2d. 7 pin Brit. Pax 3d. 7 pin Brit. Amp. 4d. Int. Octal Pax. 3d. Mazda Octa Pax. 3d. Loctals Amp. 6d. B7a Pax. 6d. B7G P.T.F.E. \({ }^{81}\) B8A Pax. 4 d . B8A Amp. Gd. B8A Cer. 8d. B9A Pax. \(\mathbf{B d}\). B9A Amp. Bd. BgA Cer. 10 d. B9A Cer, with maddle and
 B9A printed oircuit 10d. B7G Valve Cans 6d. EY86 Eigh woltage holders \(1 / 3\).

\section*{variable gang condensers}

Twin Gang 20 pF . Ideal for F.M. \(2 \mathrm{in} . \times 11 \mathrm{in} . \times 1 \mathrm{in} .2 / 0\) Twla Gang 0005 MFD. \(21 \mathrm{in} . \times 2 \mathrm{in} . \times 12 \mathrm{in}\). 8 pindle Min. Twing Gang. 0005 MFD. 2 tin. \({ }^{\circ} \times 1 \frac{1}{2} \mathrm{in} \times 11 \mathrm{in}\). Min. Twin Gang. 0005 MFD. 24 in . \(\times 1 \mathrm{fin} \times 1 \mathrm{in}\). Spindle in. with trimmers, 8/6.
Twla Gang 0005 MFD. Geared with 8.M., \(3 / 6\).
AMFM 2 RGang Condenvers, \(500+20 \mathrm{pF}\)., \(3 / 6\).

DISC CERAMIC CONDENSERS 500 v . Whg.
500 PF, .001 MFD. 0005 MPD., 002 MFD., .003 MFD. 005 MFD. 6d. each. . 01 MFD. 9 d .

\section*{TRANSISTOR COMPONENTS}

SUB MINIATURE ELECTROLYTIC CONDENSERS -SLEEVED-All at \(2 / 3\) each.
.1 Mfd. 12 г., \(2-6-8-10 \mathrm{Mfds}, 3\) \%., 2-6-8-10-12-16-3050 Mfds .6 . \(\quad 1 \mathrm{Mfd} .10 \mathrm{v}, 1,5 / 30 \mathrm{Mfds} .18 \mathrm{v}\). \(.25 \mathrm{Mdd} .12 \mathrm{Mids}, 8 \mathrm{Mfds}, 15 \mathrm{v} 8 \mathrm{Mids}, 16 \mathrm{Mfds}\).

SUB MINIATURE TRANSISTOR COILS Set of 3 I.F. Transformers \(470 \mathrm{Kc} / \mathrm{g}_{\mathrm{g}}\) plus Oscillator As specified for Mullard Circults \(23 / 6\) complete. As specified for Mazds Circuits \(23 / 6\) complete. WTC osclllator Coils for Jackson of Plessey Gang, 4/6 each. WTC \(470 \mathrm{kc} / \mathrm{s}\) I.F. Transformers, \(4 /\) each, 7/6 pair.

SUB MINIATURE CARBON POTS
\(5 \mathrm{~K},{ }^{50 K}, 220 \mathrm{~K}, 330 \mathrm{~K}, 1 \mathrm{M}, 2 / \mathrm{e}\) each. 5 M with switch, \(4 / 6.5 \mathrm{~K}, 1 / 6\). 500 K preset \(1 /\) - 1 M Tran siftor Pots, 2 \(/\) - 5K Transistor Pots, \(1 / 6\)

SUB MINIATURE METALLISED PAPER CONDENSERS \in. \(\times\) tin. 100 v. working. . 005 MFD. .0022 MFD., 002 MFD., 001 MFD., 8 d , each, . 01 MFD., 02 MFD. Price 9d. each.

TRANSISTOR GANO CONDENSERS With intermediate screen as opeclfied for MULLARD Transistor oircuits, \(9 / 6\). As above with switch for L.W. pre-selection, 11/-

MIN. POLYSTYRENE CONDENSERS 10 pF. 100 pF.. 500 pF., 1,000 DF. 125 v. 4 kg . 8d. each.

\section*{TY PRESET CONTROLS}

Knurled knoh and 6BA fising holes. Diam. 1in. \(5 \mathrm{~K}, 25 \mathrm{~K}\), \(50 \mathrm{~K}, 100 \mathrm{~K}, 250 \mathrm{~K}, 500 \mathrm{~K}, 2 \mathrm{M}, 1 / 3\) each 20 K , Firewound
\(1 / 6\).

\section*{SWITCHES BOTARY}

Size \(1 \frac{5}{16} \mathrm{in}\), dis,-2in, spindies. Price \(2 / 11\) esch. 1 pole 10 way. 1 pole 12 way. 2 pole 2 way. 2 pole 3 way. 2 pole 4 way. 2 pole 5 way. 2 pole 6 way. 3 pole 3 way

\section*{POTMETERS CARBON-HI-GRADE}

Moulded Tracks. Diam., 1 in ., 21 in . spindice, \(5 \mathrm{~K}, 10 \mathrm{~K}\), , Lor or Linear, less switch. \(2 / 6\) each. With switch, \(4 / 6\).

\section*{TRANSFORMERS}

Audio Output Types. 8,0000 to 30. 3/8. 10,0000 to 30, Universal ORT Boonters
Uni veras ORT Boosters with tapped primaries 2 v .6 .3 v 13 v., \(25 \%\) boust all taps, \(10 / 6\). Filament transformers, 916.

\section*{MODERN TV COMPONENTS}

Ferrox Line O/P transformers, 16 Kv . U25 19/6. Frame O/P transtormers to match 4/6. Scanning Coils to match Choke: 2 Ry \(250 \mathrm{~mA} 3 / 11\). 1.9 Ey 250 mA .9111 .3 Hy 250 mA . \(2 / 6\). Rectifier \(250 \mathrm{v}, 250 \mathrm{~mA} 10 / \mathrm{o}\), 34 Meg I F G.E.C. Metal Rectifier 250 v. \(250 \mathrm{~mA} 10 /-134 \mathrm{meg.i.F}\). 21in. 2/6, 3/6, 4/6 (plus 2/6 p.p.).

\section*{MISCELLANEOUS}

Cenuine 0C71 Transistors 6/6. Crocodile ellpe 4d. Coss Plugs and Sockets 2/2 per pair. Condenser clips 11 n. and 1 in. 6d. ea. Parmeko Smoothing Choke \(8 / 9 \mathrm{Hy} .100 \mathrm{~ms}\).
 Westector 6d. Elliptical Bpeakers \(71 \mathrm{n} . \times 4 \mathrm{in}\). \(12 / 6.100\) assorted first class Erie resiators 18/6. Translator twin gang condensers \(287+166 \mathrm{pF}\)., ex equip. \(4 / 6\). Vibrator
Has Chokes \(1 /\). Ext. Loudspeaker panel with switch \(1 /\).

We have an extenslve range of Waxed Paper Condeusere (avorage price 5 d . ea.). Mreallised Paper Condenserf (average price 11d. each) and Wirewound resistors 0/6/7
wate sypes (average price \(1 /=\) ea.).
\begin{tabular}{|c|c|}
\hline \multicolumn{2}{|r|}{\multirow[t]{5}{*}{}} \\
\hline & \\
\hline & \\
\hline & \\
\hline & \\
\hline
\end{tabular}

OUR LATEST SUPERIOR PROD High Quality. Low rapacity, \(10 / 15 \mathrm{pi}\). \(16 / 6\)
Optional boost \(25 \% .50 \% 75 \%\). Type B. Mains toput. Low capacity. Mult Output \(\left\lvert\, \begin{aligned} & 2,8 \% \\ & 50 \% \text {. Suftable for all Cathode Ray Tubee. } 21 /=\text {. }\end{aligned}\right.\) RESISTORS. All preferred values. \(20 \% 10\) ohms to 10
 to 10 meg. Dito \(5 \%, 9 \mathrm{~d}\), 100 o to 5 meg .
\(\left.\begin{array}{l}10 \text { watt } \\ 15 \text { watt }\end{array}\right\} \quad\) WIRE-WOUND RESISTORS
15 watt 25 ohms- 10,000 ohris
15,000 ohms- 50.000 ohms \(5 . W .1 / 9 ; 10 \mathrm{w}\).
WIRE-WOUND POTS. 3 w . WIRE
WIRE-WOUND POTS. 3 w .
Pre-set Min. T.V. type Pre-set Min. A. Gype
Knurled slotted knob.
An values 25 ohms to 25 K ., Al values 20 ohms to 25 K .,
\(3 /\) es., 30 K ., 50 K ., \(4 / \mathrm{m}\). standard sir POTs. \({ }^{2 / 3}\) Standard size Pots, long
Spladle High Grade. Spindle High Grade. All
valuea 100 ohma to 50 K ., \(6 / 6 ; 100 \mathrm{~K} .,{ }^{7} / 6\).
WIW EXT.
SPEAKER \begin{tabular}{l} 
CONTROL \(10 \Omega, 3 /-\) \\
Duty 50 mA ., \(4 / 6\). \\
\hline
\end{tabular} 30 K. to \({ }^{2}\) Meg-. \(3 / \%\). TRANSFORMERS. Heavy Duty 50 mA ., \(4 / 6\). Multi-
Of
 Push-pull 10 watts, 15/6. MULLAED CHOKES 15/10H 60/65 ma., \(5 /\) - 10 H 85 ma ., \(10 / 6\). 10 H 150 ma ., \(14 / \mathrm{F}\).

MAINS TRANSFORMERS \(200 / 250\) v. A.C
STANDARD \(250-0-250,80 \mathrm{~mA} .16 .3\) v. 3.5 a . tapped 4 v. 4 a. Reetifer 6.3 v. 1 a., tapped, 5

SMALL 250.0 .250 100 m 6
STANDARD, \(250-0-250,65 \mathrm{~mA} . \mathrm{m}^{6} 6.3\) v. 3.5 a HEATER TRANS., 6.3 \(r\). 11 A. \(7 / 6,3 \mathrm{amp}\). GENERAL PORPOSE LOW VOLTAGE. Outputs
\(6,8,9,10,12,15,18,24\) and 30 v. at 2 A. ALADDIN FORMERS and cores, tin., 8d.; Ith., 10d \(0.3 i \mathrm{n}\). FORMERS 5937 or 8 and Cans TV1 or 2 , 3 in . sq, \(x\)

SLOW MOTION DRIVES. Epicyclic ratio 6:1, \(2 / 3\).
TYANA, Midget Soldering Iron, 230 v. 40 w., \(16 / 8\). REMPLOT INSTRUMENT IRON. 230 v. 25 w., \(16 / 8 \%\) MADNS DROPPERS, \(3 \times 1 \frac{1}{2}\) n. Three Adj. Sliders, 3 amp . 750 ohms. \(4 / 3\). 2 amp., 1,000 ohrns, \(4 / 3\).
LINE CORD. 3 amp., 60 ohms per foot, 2 amp, 100 ohms per foot, 2 way, 6 d . per foot, 3 wry, 7 d . per foot.
CRYSTAL. MIKE INSERT by Acos \(6 / 6\)
Precision angineered. Size only \(\times 1 \frac{1 / 2}{6}\).
ACOS CRYSTAL DESK MIKE. Bargain. \(35 / \%\).

MTKE TRANSF. 50:1, \(3 / 8\) ea.; \(100: 1\) Potted, \(10 / 6\).
LOUDSPEAKERS P.M. 3 OHM. 5 tm , Bola, \(17 / 6\). \(6 \mathrm{in} . \times 4 \mathrm{in}\). Rota, 18 l-
10 in . \(\times\) 6in. Rala, \(27 / 6\) - Rola, 21/- 81 in . Plessey, \(19 / 6\).
 12 in . Baker 15 wt . 3 ohm and 15 ohm modele, \(105 /\) 12 in . Baker foam suspension 15 w
12 in . 15 ohm Plersey 10 wt., \(45 / \mathrm{F}\)

\section*{I.F. TRANSFORMERS \(7 / 6\) pa ir
465 k /s. slug tuning miniature ean \(21 \times 1 \times 1 \mathrm{n}\). High Q and good bandwidth. By Pye Radio. Data sheet supplied}
 Wearite 550 I.F. standard \(665 \mathrm{ke} / \mathrm{s} ., 12 / 6\) pai CRFSTAL DIODE G.E.O. \(2 / \omega\), GEX 34, 4/6. 40 Circults, \(3 /-\) H.R. HEADPEONES, 4luid, squirt spout, \(4 / 3 \mathrm{tin}\). SWITCH CLEANER FInd, \&quirt spout, \(4 / 3\) tin. 11 in . \(\times 1\) in. \(\times 11\) in. \(10 /-.0005\) Btandard with trimmers. \(9 /-\) less trimmers, \(8 /\)-. Midget. \(7 / 6\); Bingle 50 pf ., \(2 / 6\);
100 ph ., \(150 \mathrm{pf.}, \mathrm{7/-} \mathrm{Soud} \mathrm{dielectrie} 100,300,.500 \mathrm{pl}, 3 / 6\).

 9d. B7G with can, 1/B; B12A, 1/3. B0A with can, \(1 / 9\). SPEAKER FRET. Goid Cloth 17 in . \(x\) 25in., \(5 / \mathrm{m}_{-} 25 \mathrm{~m} \mathrm{~m}\) 35 in., 10/~. Ty
samples, 8.
WAVECHANOE SWITCHES.
2 p. 2-way, 3 p. 2 -way, short spindle
2 p. 6-way, 4 p. 2 -wxy, 4 p. 3-way, ong apindle 3 p. 4 -way. 1 p. 12 -way, long aplndie.
Wave change "MAKITs"
Wave change "WAKITS"" 1 wafer, 8/6; 2. wafer, \(12 / 6 ;\)
 MORSE KEYS, good quality, \(2 / 6\).
SUB-MNIATURE ELECTROLYTICS (15 v.), 1, 2, 4, 5, 8, 35, 50 mtd . 3/- each.

EDISWAN TRANSISTORS
JUNCTION TYPE P.N.P.
AUDIO XB102, for ampls- R.F. XA104 frequency fers and output stages up changer up to \(4 \mathrm{Mc} / \mathrm{f} .18 /=\)
to 250 millumatts in push. pull. PRICE \(10 /=\) XAl \(^{\text {X }} 2 \mathrm{IF}\) Mc/s. \(\quad 15 /-\) Goltop Power V15/10P, up to 10 W with heat sink, \(20 \%\)


SUPERIOR FM-AM MODEL Six Mullard Valves, ECC85, ECH81, EF89, EABC80, EL84 E280. Y.H.F. \(108-87\) Me/s. Med. \(180-550 \mathrm{~m}\). Long \(1000-\) 1800 m . Gram inpat. Ready for use. A.c. Mans 250 F . Isolated chassis. Outpat point for uze as \(\mathrm{Ei}-\mathrm{F}\) Tuner. 12 month guarantee. Cironit supplied.
£18. 19. 6. Carr. \(\mathrm{s} / \mathrm{\beta}\).
- GARRARD 4-SPEED RECORD HANGERS RC121/D MKI MODELS 大 Brand now and fully guaranteed 12 months. AUDIO PERFECTION

Desdgined to play 16, \(33,45,78\) r.p.m. Records 7 hn ., 10 in .
12in. With plug-in NORMAL HEAD. our price f10. 10.0 . Stereo head e2 extra

\section*{LATEST COLLARO AUTOCHANGER}


Or With Cabinet, Amplifier and Speaker £11.19.6. Carr. \(5 / 6\)
B.S.R. MONARCH UA8 4-SPEED AUTOMATIC RECORD CHANGERS

Brand new and fully gaaranteed 12 months.
OUR PRICE £6.19.6. post iree
sTEREO MODELS UA8. £7/19/6. UA12, £10/10/-.

\section*{AUTOCHANGER ACCESSORIES}

Suitable player cabinets (uncus boards)... 49/6 Amplifier player cabinets with cut boards 63/2 valve amplifier and \(6 \frac{1}{2} \mathrm{in}\). speaker for above \(79 / 6\) 3 valve amplifier and \(6 \frac{1}{2} \mathrm{in}\). speaker for above \(95 /-\) Wired and tested ready for use.
+
GARRARD 4-SPEED SINGLE AUDIO PERFECTION POST MODEL TA MK II \(\mathbf{E 8 / 1 0 \quad \text { Stereo Heads }}\) MODEL 4 HFEIB

E2 extra

\section*{BATTERY-MAINS POWER PACK}

Same size as batterís B126 and AD35, 90 v . H.T., 14 v . L.T. only 1/- a year to run on A.C. 200/250 v. Made by

THE HI-GAIN BAND 3 PRE-AMP Cascode circuit using Valve ECC84. 17db gain. Kit 29/6 less power power pack. Plans only 6 d.

LATEST "E.M.I." \({ }^{4}\) SPEED SINGLE Acos 73 Hi -fi Sterso and normal xtal pick-up for 7 in ., 10 in . and 12 in . records. Silent motor, heavy turntable.

Special offer C6/19/6. Post 3/6.
VOLUME CONTROLS
Midget size:
Long spindle. Guaranked 1 year. An values 5 K . ohns up to 2 Meg.
No swlich
D.P. SFT. Lunear or Log
Traclks. Log Tracles. AIRSPACED .... 1/ yd. ANEL SOCKETS.. \(.1 \%\) LI\% LEAD SOCKETS .... 2\% PANEL SOCKETS … \(1 /\) OUTLET BOXES .... \(4 / 6\) BALANCED TWIN FEEDER per Yd.8d. 80 D or \(300 \Omega\) TWIN SCREENED BALANCED FEEDER \(1 / 6\) yd., 80 ohm with 4 sides, riveted cornera and
 and \(18 \times 3\) in., \(16 / 6\).
BLACK CRACKLE PAINT. AIr drying, 3/- tin. P.V.C. CONN. WIRE, 8 colours, ajagle or stranded, 2d. 5d.


\section*{"GEVAERT GEVASONOR"}

50\% Extra Long Play Plastic Tape
1,7001t. 7in. Reel 35/-. 850tt. 5im. Reel 21/SUPERIOR 1,200tt. 7in. Plastic Tape 24/0 \(600 \mathrm{ft} .5 \mathrm{in} .15 /\) - All spare Reels \(3 /\) - each. LONG PLAY \(598 \mathrm{in} .1,200 \mathrm{ft} .28 / \mathrm{F}\). \(3 \mathrm{in} .225 \mathrm{ft} .7 / 6\). "INSTANT" Bulk Tape Eraser and Head Demagnetiser: 200/250 v. A.C. 27/6.
MAINS TYPE. RM1, \(125 \mathrm{v}, 60 \mathrm{~mA} ., 5 /-\) RM4, 100 mA . B/F: RM2, \(120 \mathrm{~mA}, 8 /\) - RMA, 250 v. \(275 \mathrm{~mA}, 16 / \mathrm{F}\) 50 mA . \(7 / 6 ; 60 \mathrm{~mA}, 8 / 6 ; 85 \mathrm{~mA}, 9 / 6 ; 200 \mathrm{~mA} ., 21\) 50 mA . 7/6; \(60 \mathrm{~mA}, 8 / 6 ; 85 \mathrm{~mA}\)., \(9 / 6 ; 200 \mathrm{~mA}\)., 21/-
\(300 \mathrm{~mA}, 27 / 6 ;\) Ful. Wave \(120 \mathrm{~mA}, 15 / \mathrm{l}\). colls. Wearite " \(\mathbf{P}\) " type, \(3 /-\) each. Osmor Midget " \(Q\) " type adj. dust core from \(4 /-\) each. All ranges.
 T.R.F. COMS. A/EF, 7/-pair. H.F. CHOKES, 2/6.

JASON F.M. TUNER COIL SET, 26/-. H.F. coll, aerlai coil, Oscillator coll, two I.F. transformers \(10.7 \mathrm{Mc} / \mathrm{s}\), ,
Detector transformer and heater, choke. Circult and component book using four 6AM6, 2/6. Complete bit with Jason Calibrated dinl and 4 valver, \(£ 6 / 15 /-\)
With new Jason Cablnet, \(20 \%\) extra.
CONDENSERS. New Stock. 001 mid 7 tV T CCC \(5 / 0\) \(20 \mathrm{kV} ., 8 / 6\). \(1 \mathrm{mfd}, 7 \mathrm{kV} ., 9 / 6\). 100 pf . to 500 pi . Mc.c. \(5 / 6\) Tubular 500 ₹. . 001 to .01 mfd ., \(9 \mathrm{~d} . ; .05 .1,1 /\); \(.2 \mathrm{ss}, 1 / 6\) \(.51 / 8 ; 1 / 350\) v., \(9 \mathrm{~d} . ; 1 / 1,000\) v., \(1 / 8 ; 0.1\) mid., 2,000 v. \(3 / 6 ; .001 \mathrm{~m} / \mathrm{d} .2,000\) v., \(1 / 9\).
CERAMIC CONDS. 500 pf. to .01 mfd ., 9 d
SILVER MICA CONDERSERS. \(10 \% .5\) ph, to 500 pf., 1/600 pf to \(3,000 \mathrm{pl}\)., \(1 / 3\).
CLOSE TOLERAANEE \(( \pm 1 \mathrm{pf}) 1.5 \mathrm{pt}\). to 47 pf ., \(1 / 6\). DITTO \(1 \% 50 \mathrm{pt}\). to 815 pt ., \(1 / 9 ; 1,000 \mathrm{pt}\). to \(5,000 \mathrm{pt}\)., \(2 /\).
 \(1 / 3.250\) pi, \(1 / 6\). 600 pf., 750 f., \(1 / 9\). Phllilp, \(1 /-\)
NEW ELECTROLYTIC8. FAMOUS MAKES

TUBULAR TUBULAR
 \(50 / 50\) v. \(2 /-32+32 / 350 \vee 4 / 6 / 100 \quad 200 / 275 * \cdot 12 / 6\)
 for charging TRAN for charging at 2.6 or 12 v. I 1 it.. \(15 / 6 ; 2 \mathrm{a} ., 17 / 8 ; 4\) a., \(22 / 6\).
Charger circuit free. A MPMETRES, 4 a. and 5 a., \(14 / 6\).
\begin{tabular}{|c|c|c|c|c|c|}
\hline NEW an & d bored & VALVES & \multicolumn{3}{|r|}{90-day guaranteo} \\
\hline 1R5 & 8/61618G & 10/6 & 1/6 & EY51 & 6 \\
\hline 185 & 816 6N7M & \(7 / 6\) EABC80 & 1016 & Ez81 & 818 \\
\hline 1T4 & 8166979 & 10/6 EB91 & & HABC80 & 12/6 \\
\hline 2X2 & \(2 / 66847 \mathrm{M}\) & \(10 / 6\) EBC33 & 816 & HVR2A & , \\
\hline 384 & \(8 / 6\) 6SJ7M & \(10 / 6\) EBC41 & 10/6 & MU14 & 10/6 \\
\hline 3 V 4 & 816. 68N7 & 8/6 EBF80 & 10/6 & P61 & 616 \\
\hline 5 54 & 8166 VgG & \(7 / 6\) ECC84 & 12/6 & PCC84 & 12 \\
\hline 5 EY 3 & \(8 / 66 \times 4\) & \(7 / 6\) ECF80 & 11/6 & PCP80 & \(11 / 6\) \\
\hline 524 & 10/6.685 & \(7 / 6\) ECH42 & \(10 / 6\) & PCF82 & 11/6 \\
\hline 6AM6 & 8/612A6 & 8/6 ECL80 & 12/6 & PCL84 & 11/6 \\
\hline 6BE6 & \(7 / 612 A T 7\) & 016 ECL8-2 & 126 & PEN25 & 6/6 \\
\hline 6BE6 & 10:612AU7 & 9/6 EF39 & \(7 / 6\) & PL82 & 10/6 \\
\hline 68W6 & 10/6/12AX7 & 9/6 EF41 & 10/6 & PY80 & \\
\hline \({ }^{68} \mathrm{DP}^{6}\) & \(7 / 612 \mathrm{BA6}\) & 8/6 EF50 & 5/6 & PY81 & \(10 / 6\) \\
\hline 6 FGG & \(7 / 6 \mid 12 \mathrm{BE} 6\) & Q/6 EF90 & 10/6 & \({ }_{\text {PY8 }}{ }^{\text {P }}\) & \\
\hline 6H6GT & \(3 / 612 \mathrm{~K} 7\) & 816 EF86 & \(14 / 6\) & SP61 & \\
\hline 6J5M & 6/61207 & \(8 / 6\) Erg2 & 5/6 & UBC41 & 10 \\
\hline 6J6 & 7/6 35La & \(9 / 6\) EL32 & 56 & UCH 42 & 10 \\
\hline 6.676 & \(8 / 63524\) & 916 ELA1 & \(10 / 6\) & UF41 & \(10 / 6\) \\
\hline \({ }_{6}^{6 K 6 G T}\) & 6.890 & 10/6 EL84 & 10/6 & U141 & \(10 / 6\) \\
\hline 6 K 7 G
6 K 8 G & \(5 / 6807\)
\(8 / 6954\) & \(6 / 6\)
\(1 / 6240\)
\(1 / 8280\) & \(8 / 6\)
\(8 / 6\) & UY41 & 8/6 \\
\hline
\end{tabular}

\section*{WIRELESS SET No. 19. MK. II.}


MULTI-METER 2,500 o.p.v. Multi 1,200 v. A.C diteo D.C. \(0.1 k . \mathrm{B}_{0} \mathrm{I}\) ditto ohm; 400 micro-A. ohm; 400 micro-A. 12 M.A., \({ }^{300}\) M.A.;
-00 to +64 -DB, \(-\infty\) to \(+64-D B\),
5 ranges \(3 \times 4 \frac{1}{2} x\) Itin. Large clear dial. Leads supplied. (List price \(\varepsilon 6 / 19 / 6\).) OUR PRICE E4/7/6. P. \& P. 2/6.

T.C.S. RECEIVER 1.5 to \(12 \mathrm{Mc} / \mathrm{s}\). 7-valve superhet, \(\begin{aligned} & \text { bullt like } \\ & \text { dream. } \\ & \\ & \text { l }\end{aligned} 2 \mathrm{SK7}-\) dream. \(12 S K 7-\)
RFI 12 SA 7 Mixer, RF, \(12 S A 7\) Mixer,
12A6 Oscillator, 12Q7 Detector, AVC - BFO - Ist AF, 12SK7-1.F.'S. The \(12 A 6\) final puts 1.4 watts into 500 ohms with an input modulated only \(30 \%\). Panel controls: R.F. Gain, A.F. Gain, C.W. Pitch, band-switch, mod.-C.W. switch, power switch, ground and aerial posts, M.O. or crystal frequency switch, speaker jack, card holder to log 30 stations, hand vernier tuning knob turning a large etched calibrated plate behind hair lined window, anti-backlash gears
 T.C.S. TRANSMITTER available at \(£ 9 / 10 / \%\), carriage 15/-
Note.-If both items purchased together, \(\& 17\). Carriage \(25 /\).
U.S.A. DYNAMOTORS


Manufactured by EICOR (as illus.). Input 12 v . output \(400 \vee\). at 180 ma . Size \(7 \times 4 \times 4 \frac{1}{2}\) in. Brand new 45/- D.M.34. 12 v .
in. with 220 v in. with 220 v. out. at \(\begin{array}{lll}80 \\ \mathrm{~mA} \\ \mathrm{P}, ~ \& ~ P, ~ & \text { ONLY } 35 / 6 \text { on each. }\end{array}\)
F.M. TRANS/RECEIVERS BC620
 Crystal controlled, operating on any two of 80 different \(100 \mathrm{Kc} / \mathrm{s}\). steps. Average range 5 10 milles. Contains 14 valves, filament plare alignment meter, volume control, mike and 'phone inputs. 6 and 12 volt supply unit and dry battery case. Complete Station only \(\mathbf{6} / 10 /=\). Carr \(20 \%\). U.S.A. hand set \(20 / \mathrm{e}\) extra

This most femous Army Trans/Receiver covers 2-8 Mc/s, \(1150-37\) metres) in two bands and \(230-240 \mathrm{Mc} / \mathrm{s}\). V.H.F. Has an intercom. amplifier. Designed for 12 and 24 volt operation. Uses a 6 valve superhet receiver, I.F. being \(465 \mathrm{Kc} / \mathrm{s}\)., and a 6 valve eransmitter designed for voice and C.W. operat on. Incorporates test and tuning meter for voltages, aerial loading and current tests. Panel Controls: Frequency tuning, P.A. tuning, Gain control, MCW, CW, R/T switch, Het-tone, netting, off-on, Quench, aerlal-AVC-LT-HT-Drive rests. Supplied complete with is valves and instruction book
Complete station (as illus.), comprising: 19 set, Supply Unit, Control box, Headphones, Microphone, Morse Key, Variometer, Short Wave and V.H.F.

MILITARY \& CIVIL ELECTRONICS

SWITCHBOARDS

\section*{Manual, fully portable, 10 line}

\section*{MOBILE}

TRANSMITTER/RECEIVERS Wireless Ser No. 19 2-8 Mc/s. Collins T.C.S. \(1.5-12 \mathrm{Mc} / \mathrm{s}\). Wireless Set No. 22 2-8 \(\mathrm{Mc} / \mathrm{s}\). Complete equipment.
Wireless Set B.C. \(62020-27.9 \mathrm{Mc} / \mathrm{s}\). F.M 80 Channels.

\section*{PORTABLE}

TRANSMITTER/RECEIVERS Wireless Set No. 46 3.6-9.4 Mc/s. Wireless Set No. 18 6-9 Mc/s. Wireless Set No. 38 7.4-9 Me/s. Complete equipment.

\section*{WALKIE-TALKIE}

TRANSMITTER/RECEIVERS
PRC-6 Handie Talkie 47-55 Mc/s. F.M. 43 channels.
V.H.F. STATIONS

Wireless Set 348 Trans/Receiver 100-124 \(\mathrm{Mc} / \mathrm{s}\).
COMMUNICATION RECEIVERS
B.C. 312 1.5-18 Mc/s. Tropicalised, 12 volts, R, \(107 \mathrm{I}, 2-17 \mathrm{Mc} / \mathrm{s}\). \(100-250 \mathrm{v}, \mathrm{A} . \mathrm{C}\). and 12 v. D.C.

\section*{HEADPHONES}
H.S.30, D.L.R.-5 D.L.R.-

No. I assembly, C.L.R.-I.

\section*{MICROPHONES}

No. 7, No. 8, No. 3, No. 4, T.S.30, No. 6 (Handset). Carbon and moving coil (Handset)

\section*{D.C. DYNAMOTORS}

Eicor Model, 12 voles in, 400 v . output at 180 M.A. Hoover Model 12, volts in, 490 v. output at 65 M.A. U.S.A. D.M.34, 12 voles in, 220 v. output at 80 M.A. Delco Model, 12 and 24 v . in, 265 v . output at 120 M.A. and 540 v . at 26 M.A.

\section*{ACCUMULATORS}

2 volt 16 A.H. Unspillable Model. Oldham, Exide, etc.
All equipment ex-stock and fully guaranteed.

BRAND NEW VARIABLE TRANSFORMERS. Input 230 volts. Outpur 0.240 volts, 5 amps. Brand new, only EB . \(0-240\) volt
Carr, \(12 / 6\).

MINE DETECTOR No. 3. Complere equipment comprising 2 search heads, amplifier, headser, control box, haversack. Operates from standard batteries. Will detect all ferrous and non-ferrous metals. Fully portable and sensitive. New in original transit case, \(65 /-\). Carr. 15/-

AMERICAN LIGHTWEIGHT HEAD SET They're High and Low impedance! the ema.S. 30 phones are US Air Force 2500 the .s Aing for \(250 \Omega\) mp. using solt rubber minia mum music and voice reproduction of the finest quality. Supplied free is a small transformer unit with cord and plug which steps impedance up to \(4,000 \Omega\). ONLY \(15 /-\). P. \& P. 2/6.

\section*{ONVERT TO} V.H.F. Within minutes you can extend the irequency of your reby using our brand new. by using our brand new V.H.F. Convertors. R.F. 26 covers 50-65 Mc/s, vernier calibrated
tuning, 20/., R.F. 25 covers \(40-50 \mathrm{Mc} / \mathrm{s}\), switched tuning, 8/6. Circuits supplied. P. \& P. 3/6 on each.

COMPLETE TRAINING UNIT Complete Code Set, Complete Code Ser, contains key, buzzer, headphones, pitch con-
trol, operating internal trol, operating internai
battery, housed in battery, housed in portable wooden case. Brand new, only 12/6.
Carr. \(5 /-\). Battery \(1 / 6\) extra.

INSTANT VALVE FILAMENT MODEL VT-AI Pocket-size battery operated CHECK OF: CHECK OF:
- All Radio

Valves.
All T.V. Valves.*
- AllT.V. Radio Fuses.
- Circuit Continuity.
- All Pilot Lamps.

- Has built-in minia-

cure 7- and 9-pin

valve straighteners and battery test.
- International Octal, B.8, B.9, B7 Battery and Mains types.
Beautifully styled-precision made. Supplied


\section*{NEW 1960 \\ \(\begin{array}{ll}\text { ILLUSTRATED } \\ \text { CATALOGUE } & 1 / 3\end{array}\)}

\section*{PORTABLE TRANSMITTER RECEIVER No. 18}

Entirely self-contained 6-valve Transmitter Receiver for voice and C.W. Frequency; 6-9 Mc/s. (50-33 metres). The Transmitter signal is generated by a master oscillator circuit followed by a power amplifier. The aerial is auto-coupled to the power amplifier by aerial taps to a parallel tuned output circuit. The Receiver is a 4-valve superhet, comprising signal frequency amplifier, frequency changer, If amplifier, 2nd det.-A.V.C.-A.F. Stage. Selectivity: The resonance curve of the If amplifier has a width of \(7 \mathrm{Kc} / \mathrm{s}\). with an average cut-off of \(5 \mathrm{db} / \mathrm{kc} / \mathrm{s}\). Full netting facilities, circuit set for full modulation, operated by standard dry batteries, range approximately 10 miles. Incorporates Test Meter for aerial loading, H.T. \& L.T. readings. Supplied Brand New complete with Power Microphone, Headphones, Morse Key, Aerials, Webbing and full instruction book all for only \(80 /\), carriage \(10 / \mathrm{F}\). 18 Set as above less attachments \(60 \%\), carriage \(10 \%\).

\section*{Kedracte.}

Callers: 87 TOTTENHAM COURT ROAD, LONDON, W.I
Mail orders: (DEPT. W.) 32a COPTIC ST., LONDON, W.C.I. MUs. 9607 WOT! You don't own a Relda catalogue! It's terrific and fully lllus. Only \(1 / 3\)


\section*{25,000 OHMS PER VOLT TESTMETER}

Made by TRIPLETT of Amerles. Bize \(7 f \times 6\} \times 6\{i n\)., and incorporates \(n\) nnlque tliting bakelite contaliner size \(5 \frac{1}{2} \times 31 \mathrm{in}\)., which has two meters, a 25,000 ohrms per Volt moving coll for D.C. measurements, and a firat grade moving iron for A.C. Reads Realstance up to 40 Megohms, A.C. \& D.C. Volte to 1,0 O, D.C. Current to 230 mA ., and nlso has 0.50 Microamps range. Facilities for measuring Condenser Capacity, etc., and Audio Output. Completely portable, with protective tace cover. Complete with leads, batteries, and instrictions. Fully re-conditioned. ONLY £10/10/- (post. etc., s/6).

\section*{UNIVERSAL AVOMETER 34} RANGE MODEL D
Ex-Air Miniatry, but thoroughly re-conditioned and checked. Supplied with interpal batteries and In. atructlons. Covers ranger as follows:

\author{
\(\begin{array}{lll}\text { D.C. A.C. } & \text { D.C. } \\ \text { VoLT } & \text { VoLits } & \text { Current }\end{array}\) \(150 \mathrm{mv} . \quad 7.5 \mathrm{~F} . \quad 15 \mathrm{~mA}\). \(\begin{array}{lll}300 \mathrm{mv} . & 15 \\ 15 \mathrm{v} . & 30 \mathrm{mLA} \\ & 75 \mathrm{v} . & 150 \mathrm{~mA}\end{array}\) \(\begin{array}{lll}1.5 \mathrm{v} . & 75 \mathrm{v} . & 150 \mathrm{~mA} . \\ 3 \mathrm{\nabla} . & 150 \mathrm{\nabla}, & 300 \mathrm{~mA}\end{array}\) \\ \begin{tabular}{lll}
\(18 \%\) & 300 & F. \\
\(30 \%\) & 1.5 amp \\
150 & 7 amp \\
\hline
\end{tabular} \\ \(\begin{array}{lll}50 \mathrm{v} & 750 \mathrm{\%} & 15 \mathrm{amp} \\ 300 \mathrm{v}, & 1,500 \mathrm{v} . & 30 \mathrm{amp}\end{array}\) \\ 300 v . \\ ,500 \\ ONLY £8/19/6 (Portage, etc. 3 \\ A.C.
Current
78 mA
150 mA
750 mA
1.5 mmp.
7.5 smp.
15 amp.
Resistance
1.000 n
\(10.000 \Omega\)
}


Frequency range \(125-20,000 \mathrm{kc} / \mathrm{f} \ln 2\) bands. This la the Uniced States Navy Model of the well-known BC.?21 Prequency Meter, but have many udditlonal featurea which Increase thelr usefulness. Voitage stabilisation clrcuith and Crystal control ensure extreme accuracy, and in
addition they are fitted with an Internal Modulation addition they are htted with an Internal Modulation sritch to nlow use ga a Signal Genarator, size only
8tin. \(\times 8 \mathrm{in} \times 8 \mathrm{in}\). Full information on requeat.

\section*{TRAWLER BAND R 1155 s}

The latest version of this famous Communications Recelver to be released by the Air Minitiry. Coverm \(1.5 \mathrm{Mc} / \mathrm{s}, \mathrm{a}, 600 \mathrm{kc} / \mathrm{s}, 500-200 \mathrm{kc} / \mathrm{s}\). As used by Coastal Command, Atr-sea Rescue Laupchen, etc. All sets thoroughly teated and in perfect working order before despatch, and on demonstration to callers. Have had slight use, but are in excclent condition. ONLY \&12/19/6. 3.0.1.5 Mc/a also avalable. An above but instead of 3.0-1.5 Mc/s. band hus \(200-75 \mathrm{kc} / \mathrm{s}\), coverage. ONLY A.C. MAINS POWER PACK OUTPUT STAGE, in black metal case to match receiver, enabling it to be operated immediately, by just plugging in. rithout any modifica-

RCA 9in. P.M. SPEAKER, to beavy black crackled metal came, desirned for use with AR 88 Recelver, or MAKERS CARTONR. ONLY 45I- (PORE 9/6).


OSCILLOSCOPE No. II
Made by A. C. Consor. Incorporates Hard Vaive TIme converted to produce \(\mathbf{3}\) cycles per second \(2030 \mathrm{tr} / \mathrm{s}\). Controls include Fine and Coarse Gain, Brighireas, Focus, \(X\) and \(Y\) shifta. Has Power Pack for nominal 115 :. and 230 v. A.C., with adequate fuae protectlon. Empluys
atin. tube type ACR10. Grev and black engraved front panel, size \(19 i n . \times 7 \mathrm{in}\). For'standard rack use if regulred depth of unit being 12 tn . In steel transtt case as illustrated. Complete with leads and sugreated modifiocation data. BRAND NEW. ONLY E12/10/- (carriage 15!-). "Q FTVER" COM MAND RECEIVER. The famous American \({ }_{550} \mathbf{8 5 3}\) covering 190 \(\begin{array}{lll}850 & \mathrm{kc} / \mathrm{s} . & \text { I. Fs being } \\ 85 & \mathrm{kc} / \mathrm{s}, & \text { Complete }\end{array}\) with all 6 valres and circuit. Rize \(11 \times 5 \$ \times\) 5 in GRAND NEW IN MAXERE CAR TONS ONLY 89/6 (Post 3/6).


\section*{TCS RECEIVERS}

The renowned American ret designed by Collins for static or mobile use. Coverage \(1.5-12.0\) Mc's in 3 bands. Complete with all 7 palves. Power regulred 12 \%. LT
and 225 . HTT \(81 z e\) and 225 . HT. \(81 z e ~ 11 \mathrm{in} . \times 13 \mathrm{in} . \times 11 \mathrm{in}\)., in black crackled case. IN NEW CONDITION. ONLI \&10/10/We can still a
Frequency coverage and fize the TC8 TRANS ITTTER. all vaives, new condition internall but externally with on Hed ONLY \(\mathrm{e}^{2} / 19^{\prime} 6\) (carriage \(15 \%\) ).

\section*{10,000 OHMS PER VOLT TESTMETER}

This latest Caby model is a handy pocket sized
 2Jin. Read
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\hline 082.. & \(17 / 6\) & 6A & 8/6 & 6LD20 15/ & 124 & 7/16 \\
\hline 7.4.. & 81. & 6AT & 816 & 6N7.. 8/- & & \\
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\hline 1 C 5 & 12/8 & 6B8G & 4/6 & 697G 8/- & 12AV & 12/7 \\
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\hline , & 5 & 9RJ6 & \(7 \%\) & 68Q7GT 9/- & 12 J & 10 \\
\hline N6 & o)- & BQ7 & 15/- & 6U4GT 12/6 & 125 & 7/ \\
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\hline U5 & 101- & 6CD6 & 36/8 & 786 .. 21/8 & 1487 & 27120 \\
\hline 2 & 4/8 & 6 CH 6 & 12/6 & 787.. 8/6 & 19A0 & 18 \\
\hline 4 & 71 & 6 Fl & 26/6 & 7C5 .. 81 & 19B & 88/3 \\
\hline & 10/8 & 6 FBG & 71- & \(7 \mathrm{C6}\)-. 8/- & 20 D & 15/3 \\
\hline & 12/8 & 8F12 & 5/6 & 787. . 8!- & 20F2 & 26/6 \\
\hline 36 & \(5 /-\) & 6 Fl 3 & 11/6 & 787 .. 1016 & 20 LI & \(28 / 6\) \\
\hline 24 & 718 & 6 F 32 & 10/6 & 7Y4... 81- & 20 Pl & \\
\hline S & \(9 / 6\) & 6P38 & 7/8 & \(8 \mathrm{~B} 3 \ldots 8\) & 20 P & \\
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\hline 3Z3.. & 12/8 & 6K6GT & 81 & D11 & 78 L & 9/11 \\
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\hline & 8 & 6L7GT & 12/6 & 12AD6 \(17 / 3\) & \(30 \mathrm{Pl2}\) & 8 - \\
\hline & - & 6 Ll 18 & 131- & 12AF6 \(13 / 1\) & 30 P 1 & \\
\hline
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\hline PRN46 & 7 \\
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\hline & \(10 / 6\) & 6BJ6 & 91/ & 6SH7 & 6/6 \\
\hline & 91- & 6BR7 & 12/6 & 6SJ7 & 816 \\
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\hline & \(7 / 6\) & 6BW7 & 8/6 & 6SL7GT & 81- \\
\hline & 3/6 & 6C4 & 51- & 6SN7GT & 7/6 \\
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\hline & 5/6 & 6L19 & 2313 & 12A6 & 616 \\
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\hline G & 23/3 & \(165 A 7 G T\) & 8/- & |12E| & 35/- \\
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\begin{tabular}{|c|c|c|c|c|}
\hline \(7 / 6\) & \(112 \mathrm{H6}\) & 3/6 & 80 & 8/6 \\
\hline 6/6 & 1215GT & 31- & 142BT & 3/6 \\
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\hline 61- & 20 LI & \(26 / 6\) & & \\
\hline 8/- & 20P1 & \(26 / 6\) & OA70 & \\
\hline 8/- & 20P3 & 23,3 & \[
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& \text { OA70 } \\
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\hline 13/6 & 20P5 & 23/3 & OA79 & 4/- \\
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& \text { CG12E }
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\hline \(9 / 6\) & 25Z4 & \(9 / 6\) & & \\
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\hline 15/3 & 30 PI 2 & \(12 / 6\) & \(\times 8104\) & 10/- \\
\hline 15/11 & 30P16 & 9/6 & & \\
\hline 15/11 & 30PLI & 12/6 & & \\
\hline 23/3 & 30 PLI 13 & \(21 / 11\) & \multicolumn{2}{|l|}{\multirow[t]{2}{*}{Catalogue is}} \\
\hline 17/6 & 35L6GT & 10\% & & \\
\hline 19/3 & 25 Y5 & \(9 / 9\) & now r & ready, \\
\hline 616 & \(35 W 4\) & \(7 / 6\) & please sen & end 1/- \\
\hline \(10 / 6\) & 35Z4GT & 8/- & in stamp & ps 0 \\
\hline 7/6 & 42 & 8/- & cover co & ost. \\
\hline Bi/ & 35Z3 & 16/7 & & \\
\hline 8/- & 35Z5GT & 9/- & Trade & Cata- \\
\hline & \(50 \mathrm{C5}\) & \(11 / 6\) & logue als & lso av- \\
\hline \(9{ }^{9} 1\) & 50CD6G & 29/10 & ailable, & apply \\
\hline 91- & 50L6GT & 8/6 & on Bu & usiness \\
\hline 91. & 75 & \(11 / 6\) & Letter & Head- \\
\hline 35/- & & 7/6 & ing. & \\
\hline
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\section*{LOUDSPEAKER UNITS}

All Brand New, Note the Special Prices. All Permanent Magnet, 3 ohms Impedance.
2 tin. square Celestion
3 in. Square Celestion \(18 / 6\)
\(18 / 6\)
3 tin. Square Elac
Celestion and Plessey Goom, 6tin. Round Celestion \(6 \frac{1}{2}\) in. Round Celestion
IOin. Round Elac and Celestion
2in. Round Plessey ............ \(32 / 6\) 6 in. \(\times 4\) in. Plessey \& Go.......... \(19 / 6\) \(7 \mathrm{in} . \times 4\) in. Plessey \& Good.
min. \(x\) sin. Allen (Golden)... \(25 / 6\) IOin. x 6in. Goodman \& Celestion
Special Offer: 8in. Golden Eight
15 ohms Speech coil
42/6

\section*{MAINS TRANSFORMERS} 3-WAY MOUNTING TYPE MTI Primary 200/250 v., Secondaries \(250-0-250 \mathrm{v} .80 \mathrm{~mA}\). 0-6.3 v. 4 A. 0.4 v. 2 A., both tapped at 4 v., \(21 / 9\) each.
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MT3' Primary 200/250 v., Secondary 30 v. 2 A. Taps at 3 v. \(4 v_{0}, 6 v_{0}\)
 \(21 / 9\) each.
Postage and Packing please add \(2 /\) per transformer.


RECTIFIERS FOR BATTERY CHARGERS
\begin{tabular}{lll}
12 & v. 1 & amp. \\
12 & v. 2 & 2 amp. \\
12 & v. 3 amp. \\
12 v. 4 amp. \\
12 v. 5 amp.
\end{tabular}

\section*{RECORD PLAYER UNITS}

BSR Monarch Model UAB, 4 speed, 10 record capacity, Ful-Fi surnover crystal cartridge, \(£ 6 / 19 / 6\).
Collaro Conquest, fully mixing changer on 7 in ., 10 in . and 12 in . Crystal Cartridge, \(47 / 19 / 6\).
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Collaro AC \(4 / 564,4\) speed single player, with automatic stop, fitted Studio 'O' Crystal Cartridge, 66/19/6.
Pifco All-in-One Radiometer, for all practical testing, \(32 / 6\).
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Acos Mie 39-I. Crystal Stick Microphone for use as a hand, desk or floor stand unit for high quality recording, broadcasting and public address work. LIST
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1 Milliamp 30 Milliamps 100 Milliamps 200 Milliamps 500 Milliamps
5 Amperes 15 Amperes \({ }_{25}\) Amperes D. \(50-0-50 \mathrm{Amp}\). \(30^{\circ} 0.30 \mathrm{Amp}\). 30 Volts
20.30 Amp 20 Volts 300 Volts
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\hline Size & Type \\
\hline 2 in. & MC/FR \\
\hline \(3 \frac{1}{2}\). & MC/FR \\
\hline 2 in . & MC/FR \\
\hline 21 in . & MC/FR \\
\hline \(2 \mathrm{in}\). & MC/FS \\
\hline \(2 \frac{1}{2} \mathrm{in}\). & MC/FR \\
\hline 2hin. & MC/FR \\
\hline 2 l in. & MC/FR \\
\hline 2 in . & MC/FR \\
\hline \(3 \frac{1}{2} \mathrm{in}\). & MI/FR \\
\hline 2 in . & MC/FS \\
\hline 2 in. & MC/FR \\
\hline 21 in . & MI/FR \\
\hline 2 in. & MC/FS \\
\hline 2 in. & MC/FR \\
\hline 2 in. & MC/FS \\
\hline 2 in. & MC/FS \\
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\hline \multicolumn{7}{|l|}{Siemens High Speed Sealed.} \\
\hline \(2.2 \Omega+2.2 \Omega\) & H90A & 15/6 & \(2 \Omega\) & 2 CO & 4184GA & 18/6 \\
\hline \(145 \Omega+145 \Omega\) & H98C & 19/6 & \(700 \Omega\) & 2 CO & 418GD & 19/6 \\
\hline \(500 \Omega+500 \Omega\) & H96D & 22/6 & \(2500 \Omega\) & 1 mak & HD¢186EE & 22/6 \\
\hline \(1700 \Omega+1700 \Omega\) & H96E & 25/- & \(2700 \Omega\) & 2 CO & 4184GE & 21/6 \\
\hline Siemens High Sp & O Open & & \(180 \Omega\) & 2 m 2 b & - M1087 & 19/6 \\
\hline \(100 \Omega+100 \Omega\) & H85N & 15/- & \(670 \Omega\) & 4 CO & M1002 & 21/6 \\
\hline \(1000 \Omega+1000 \Omega\) & H95A & 17/6 & \(2500 \Omega\) & 1 CO & M1022 & 22/6 \\
\hline \(1700 \Omega+1700 \Omega\) & H85L & 17/6 & \(6000 \Omega\) & 2 CO & M1052 & 25/- \\
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Comprehensive range available from stock.
1 hole fixing, 3 amp. 250 volt.
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mounting bracket, \(85 / 10 /-\) carr. \(10 \%\).
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HERE IS YOUR CHANGE TO PURCHASE A BRAND NEW UNIT WORTH \&40! FOR OUR SPECIAL PRICE

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Input 200/250 V. A.C. 50 cy . Output 10 amps ., 22 volts D.C. Controlled by two 4 -position switches for fine and coarse control which enables 6 to 24 volt batts. to be charged. Brand new with \(0 / 12\) ammeter. Fused A.C./D.C.
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\hline \multicolumn{4}{|l|}{Discounts for quantities of above charging rectifiers.} \\
\hline MAIN8 TRAN8F & MER8 to suit abo & rectifiers & \\
\hline 12 Volts 1 Am & 12/6 each & 12 Volts 4 Amps MT5 & 25/-each \\
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\hline Amp & 22/-each MT5B & 24 Volts 3 Amps & 25/- ea \\
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COUNTING UP TO 9899
Type 16A
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SHROUDED FULLY VARIABLE TRANSFORMER
FOR BENCH OR PANEL MOUNTING. SIZE:-Approximately \(8 \frac{1}{2}\) inches Cube. WEIGHT:-Approximately 30 lb .
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3 KVA Air Co oled ( \(100 \%\) under-rated) GUARANTEED \(230 / 250\) tapped, 12 amps. 6 KVA \(105 / 120\) tapped, 28.5 amps . Made by well-known manufacturer and housed in strong metal case. Weight: 2 cwt . Brand new, in original maker's cases. PRICE \&15.0.0

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Complete with amplifier unit, 4 speakers, microphone, headphones and all spares packed in wooden cases. 6 or 12 volt D.C. handling capacity 8 watts. Ideal for cars, boats, factories, etc
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BRIDGE Meggers Evershed
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EVERSHED AND VIGNOLES WEE MEGGERS. Good condition. 500 v . \(£ 12 / 10 \%\). P. \& P. 3/. Ditto 250 v. \(£ 10 / 10 /-\) P. \& P. \(3 /\)-.
 CI R CUGER TESTER (low reading ohm \(m\) eter)
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ranges. \(0-3,0-30\) ranges. 0-3, 0-30 ohms. The perfect meter for concinuity and polarity testing. complete with test leads and Brand new. Only \& \(4 / 17 / 6\). P \& \& P. \(3 \%\)

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Type GM. 4140/1. Mains operated from \(100-250 \mathrm{v}\). A.C. Will test resistances from 0.1 ohm to 10 megohms and condensers 10 mfd Good condition and complete with inseruc. tion booklet. t6/19/6. P. \& P. 2/6.


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and Unused \(£ 18 / 10 /\). Carr. \(10 /\).
HEAYY DUTYLT TRANSFORMERS. 230 v 50 cycles pri. 17 v . sec. at \(35 \mathrm{amps} .\), capable of carrying \(\mathbf{2 5} \%\) over actual rating. Perfect condition. ONLY \(\| 5 /\) each, either type. Carr. 5/\(6 \mathrm{kV} / \mathrm{A}\) AUTO-TRANSFORMER. \(230 / 110 \mathrm{v}\). 50 cycles (fully tapped primary and secondary). Capable of 25 \% and unused. \(f 18\). Carr. 20/\%. Also \(3 \mathrm{kV} / \mathrm{A}\) as above. f \(12 / 10 /\). Carr. 20/.
\(20 \mathrm{kV} / \mathrm{A}\) AUTO-TRANSFORMER. 230/115 50-60 cycles, by Jefferies Transformer Co., U.S.A Perfect condition, E20. Carr. fl .
CONSTANT VOLTAGE TRANSFORMER \(190-260\)-v, primary, sec. 115 v . at \(1 \frac{1}{3}\), kW/A (listed at \(2 \mathrm{kV} / \mathrm{A}\) ). Brand new and unused. \(£ 25\) or \(£ 45\) per pair. Carr. 10/- each.
MARCONI SIGNAL GENERATOR. TYPE TF5I7-F/I. Covering \(10-18 \mathrm{Mc} / \mathrm{s}\). \(33-58 \mathrm{Mc} / \mathrm{s}\). \(150-300 \mathrm{Mc} / \mathrm{s}\). Used but in very good condition. Complete with full technical data and instructions. Limited quantity. Unrepeatable at only \(\mathbf{f} / \mathbf{2} / \mathbf{1 0 / F}\). Carr. 20/-.
ALSO MARCONI SIGNAL GENERATOR TYPE TF390G for \(200-250\) v. A.C. mains input. Frequency range \(4-16 \mathrm{Mc} / \mathrm{s}\). and \(32-100 \mathrm{Mc} / \mathrm{s}\). indirect calibration. Output I \(\mu \mathrm{V}\) to \(100 \mathrm{M} / \mathrm{V}\). \(400 \mathrm{c} / \mathrm{s}\) internal modulation. In good order. Only ¢ \(12 / 10 /\). Carr. 20/.
VALVE TESTER. TYPE 4. 200/230 v. A.C. input. Ex Govt., in good condition, with descriptive book containing circuit diagram of instrument and how to test valves from 1.4 v . to 40 v . With valve holders for Brit. 4, 5, 7 pin and Octal, U.S., 5 and 7 pln. 1/Octal, side contact large Brit., 4 and 9 pin. Acorn and diode. Housed in substantial 9 pin. Acorn and diode. Housed in substantial A.C.-D.C. RECTIFIER POWER SUPPLY UNITS
\(110-230\) v. A.C. 50 eycles input, \(100 / 110\) v. D.C output max. \(2 \frac{1}{2}\) amp. Brand new and unused. 64/10/-. Carr. 7/6.
230 v. A.C. 50 eycles Input, \(200 / 220\) v. D.C. output at \(3 / 4\) amps. approx. Good condition. 610. Carr. 10/-
\(200 / 250\) v. A.C. 50 cycles input, secondary 24 v. at 26 amps. D.C. Capable of \(25 \%\) over actual rating. Brand New and unused. \(£ 12 / 10 /\). Carr 20/.
\(200 / 250\) v. pri., 110 v. sec, at 4 amps. max. Brand New and unused. \(68 / 10 /\). Carr. \(10 /\).
TRUYOX TANNOY LOUD-HAILERS. With 180 ohm line eransformer and condenser. Impedance \(7 \frac{1}{2}\) ohms, handling capaciry 8 wates. Complete in slope-front wooden case. In good condition 18/6. P. \& P. 3/6. Brand new \(25 /\) P. \& P. 3/6.

AIRBORNE TRANSMITTER RECEIVER. TYPE 1986. A mobile 10 -channel crystal controlled V.H.F. Tx. \(/ \mathrm{Rx}\). covering \(124.5 / 156 \mathrm{Mc} / \mathrm{s}\). 1.F. band width \(23 \mathrm{kc} / \mathrm{s}\). Complete (less external attachments) In metal case, with all valves and 24 v. rotary power unit. Used, but in first-class condition. ONLY \&8/10/-. Carr. paid. Also, complete with control box and all necossary con necting leads, \(\mathbf{t} 12\), carr. paid.
RESISTORS. Mixed parcel of \(\frac{t}{4}, \frac{1}{2}, 1\) and 2 watt sizes. Good assortment. \(7 / 6\) per 100 . Post 6d. CONDENSERS. Mixed parcel, good assort ment of types and values, 50 for \(10 /\).. P. \& P. \(1 / /\) a TELEPHONE DIALS. Standard (G.P.O.). Pattern. 0-9. Brand new. 30/., P. \& P. I/..


ACCUMULATORS 12 v. 25 A.H. New and unused. Housed in strong wooden case for extra protection, 45/*. Carr.
\(7 / 6.2\) v. 100 A.H. 75 actual. Ex Gove. New and unused. Complete with carrying handle. Size \(6 \frac{1}{2} \times 6 \frac{1}{2} \times 3 \frac{1}{2} i_{n}\).
\(15 /-\) each. Carr. \(3 / 6\). 3 sent for \(50 / \mathrm{F}\), or 6 for 45, carr, paid. Ditto 16 A.H., 5/-. P. \& P. 2/-; 6 for 24/.. P. \& P. 10/-. Dicto 14 A.H., less handle, 5/-. P. \& P. 2/-; 6 for 24/\%. P. \& P. 10/-

\section*{RECORDING TAPE. Send S.A.E. for} money-saving price list.
TELESCOPIC AERIAL MAST. 20ft, sections of 5ft. each. Independently locking at any height. Tapering from 2 in , to \(\frac{3}{4} \mathrm{in}\). (less accessories). \(50 /\)-, carr. \(5 /\)-.


HEAVY DUTY-ALL STEEL TRIPOD STANDS. Adjustable every 6in. to approx 9 ft . 6 in . when fully extended. (Folds up to only 4 ft . 6 in. for storage.) Suitable for outdoor speakers public address systems, floodlighting, etc., etc (as illus. Dec.). OUR PRICE \(\mathbf{4} 3 / 10 / \%\). Carr. 5/.

> BAKER'S SELHURST SPEAKERS
> 12in. P.M. 15 ohms 15 watts, \(30-14,000\) c.p.s. Our price \(4 / 10 /-\).
> "AUDITORIUM" 12 in. 15 ohms 12 watts, \(35-16,000\) c.p.s. Flux density 14,500 . OUR PRIC, £7/IO/.
> "SUPER-HI-FI 25 " 12 in., 15 ohms, 25 watts \(25-20,000\) c.p.s. Flux density. 17,600 OUR PRICE, E9/9/. Allthe abovespeakersareBrand new and full descriptive specification is available.
G.P.O. RACKS. I9in. Heavy duty, all steel. Standard drilling. Two types: 5fr. 6in. angle uprighes. \(3 / 10 /\) carr. 10/. 6ft. channel uprights, 65, carr. 10/-

19in. x 14in. PANEL SHELF in 14 s.w.g. steel. Sultable for above racks. 15/, P. \& P. 5/-.


\section*{EDDY'S (поттм) LTD \\ 172 ALFRETON ROAD NOTTINGHAM}

SURPLUS NEW AND GUARANTEED
\begin{tabular}{|c|c|c|c|c|c|}
\hline AZI & 12/6 & P61 & 2/3 & 6816 & 6/6 \\
\hline CY31 & 12/6 & 'PCC84 & \(9 /-\) & 6 C 4 & 3/6 \\
\hline DAF96 & \(8 / 6\) & PCF80 & 8/6 & 6 C 5 & 5/6 \\
\hline DF96 & 8/6 & PCL82 & 10/- & \(6 F 33\) & 5/6 \\
\hline DL96 & \(8 / 6\) & PEN25 & 5/- & 615 M & 4/3 \\
\hline DM70 & \(7 / 6\) & PEN36C & 9/6 & 6 J GT & 3/11 \\
\hline EB91 & 4/- & PL33 & \(9 /-\) & \(6 J 5 \mathrm{G}\) & \(2 / 6\) \\
\hline ECC81 & 6/- & PL81 & 10/6 & 956 & \(2 / 11\) \\
\hline ECC82 & 7/- & PL83 & \(8 / 9\) & \(6 \mathrm{K7G}\) & \(2 / 3\) \\
\hline ECC83 & 716 & PY31 & 8/6 & 6 P 28 & \(9 / 6\) \\
\hline ECC84 & \(91-\) & PY80 & 7/- & 6Q7G & \(7 / 9\) \\
\hline ECC85 & \(8 / 6\) & PY81 & 7/- & 6SA7M & 6/- \\
\hline ECF80 & 10/6 & PY82 & \(7 / 6\) & 6SG7M & 5/- \\
\hline ECH42 & \(8 / 9\) & U25 & 121- & 6SK7GT & 5/- \\
\hline ECH81 & 8/3 & U35 & 8/6 & 6SN7GT & 419 \\
\hline ECL80 & \(9 / 6\) & U31 & \(7 / 9\) & 6V6G & 5/9 \\
\hline ECL82 & 11/- & 955 & \(3 / 11\) & 6V6GT & \\
\hline EF36 & 216 & UAF42 & 91- & 6X64 & 6/6 \\
\hline EF37 & 4/- & UBC41 & 8/3 & \(6 \times 5 \mathrm{GT}\) & \(6 / 6\) \\
\hline EF41 & \(8 / 9\) & UCH41 & \(81-\) & \({ }_{7} \mathbf{6 \times 5} 5\) & 6/6 \\
\hline EF42 & \(8 / 6\) & UF41 & \(8 / 9\) & \(7 \mathrm{C6}\) & \(7 / 6\) \\
\hline EF50 & 1/9 & UL84 & 8/3 & 757 & 916 \\
\hline EF80 & \(6 / 6\) & UY41 & \(6 / 6\) & 757 & \(9 / 6\) \\
\hline EF86 & 11/- & 105 & 916 & \(7{ }^{7} 4\) & \(7 / 6\) \\
\hline EF89 & \(8 / 6\) & 114 & 319 & \(12 \mathrm{K7}\) & \(7 / 6\) \\
\hline 954 & 1/6 & IRS & 71- & \(12 \mathrm{C7}\) & \(7 / 6\) \\
\hline EF91 & 4/- & is5 & \(6 / 6\) & 20 DI & 9/6 \\
\hline EL4! & 9/3 & IT4 & 4/9 & 25A6G & 8 8- \\
\hline EL84 & 8/3 & 354 & 7 - & 25L6GT & 9/- \\
\hline EY51 & \(9 / 6\) & \(3 \vee 4\) & 7/9 & 25Z4G & 7/9 \\
\hline EY86 & 8/6 & 5U4G & 5/9 & 35L6GT & 9/6 \\
\hline EZ40 & 7/- & 5Z4G & 5/9 & 35 W 4 & 6/9 \\
\hline EZ80 & \(6 / 9\) & 6AG5 & 5/- & 35Z3 & 12/6 \\
\hline GTIC & 7/6 & 6B8G & \(2 / 11\) & 35Z4 & \(7 / 6\) \\
\hline MU14 & 8/- & 6BA6 & 6/6 & 807B & 3/9 \\
\hline
\end{tabular}

RI585 RECEIVER. 12 valves, 6 preset positions, Medium waves, 19/1I. P. \& P. \(2 / 6\).
RECTIFIER/STABILISER for 1.4 volt valves, Midget, 3/-. Post 6d.
2000 mfd . CO NDENSERS, 6 volts working, \(1 / 6\). Post 6d.
NIFE ACCUMULATORS, Midget single unit size \(3 \times 2 \frac{3}{4}, 7 \mathrm{amp}\). hours, \(1 / 11\). Post \(1 / 6\), DYNAMOTORS. 200 volt D.C. 1012 volt D.C. ideal for train sets on D.C. main, \(19 / 1\) I. Post \(2 / 6\). GERMANIUM DIODES, \(1 /\) e each, \(9 / 6\) dozen. Post 4d.
ACOS CRYSTAL PICK-UPS. (Turnover 2 sapphire styli), 29/11. Post 2/-.
DIMMER SWITCHES. Ideal for train speed regulators, \(1 / 11\). Post 6d.
NEON MAINS TESTER/SCREWDRIVERS, 3/II. Past \(6 d\).
RECTIFIERS. Contact cooled miniature 200 v . \(60 \mathrm{~mA} ., 7 / 6\); RMI, 4/9; RM2 6/6; RM3, 7/6; RM4, 15/6; RM5, \(19 / 6\). Post 1/-.
CONDENSERS. Tubular Wire End (not ex Gove.), \(8 \mathrm{mfd} ., 450 \mathrm{v} .11 / 9 ; 8-8 \mathrm{mfd} .450 \mathrm{v} ., 2 / 6\); \(16 \mathrm{mfd} ., 450 \mathrm{v} ., 2 / 9 ; 16-8 \mathrm{mfd} ., 450\) v.. \(4 / \mathrm{F}\); 16 -16 mid., \(450 \mathrm{v} ., 3 / 9 ; 32 \mathrm{mfd} ., 450 \mathrm{v} ., 3 / 9 ; 32-32 \mathrm{mfd}\). 350 v., 4/-. Pose 1/-
VIBRATORS. 12 v., 4 pin, 4/II. Post I/-
MORSE TAPPERS. Plated contacts, adjustable gaps, Heavy Duty, 3/6. Post 9d.
RELAYS. Siemens High Speed suitable for mode control, 8/II. P.O. 3,000 type assorted values, 5/11 each. Post 1/-
SPEAKER GOLD GRILL. \(6 \frac{1}{2} \times 4 \mathrm{in}\)., \(1 /\). each. Post 6d,
HEADPHONE CORDS. Git. I/II pair. Post \(6 d\).
JACK PLUGS. Standard Type, I/II. Post 6d, GRAM AMPLIFIERS. High sensisivicy 3 watcs output. Separate volume and tone conerols. Printed circuit. 59/1I. Post \(4 /\). Fully guaranteed. Size \(8 \times 2\) in in . Max, height, 5 inches.
CAR RADIO KITS. 7 transistors, long and medium waves, 2 watts output. R.F. scage and automatic gain control, 6 or 12 volts. Completo kit with cabinet, 10 gns . Post \(5 /\).

\section*{ALL ABOVE ARE NEW AND GUARANTEED}

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Any parcel insured agalnst damage in transit for only \(6 d\). extra per order. All uninsured parcels at cuscomers risk. Postage and Packing 6d. per valve extra. Over 63 Free. C.O.D. or C.W.O. only. C.O.D. charge 3/- extra. S.A.E. with enquiries.
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A year of pleasure lies ahead for all who own Duodes already. We wish them not only personal happiness and good health, but that special enjoyment which comes from listening to Natural Sound-true, clear cut, full range sound which brings the nearest approach to reality.
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Act NOW. Send for detalls of the new I2D and I2E-

The finest long term investment in good sound.

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TO BE SURE OF REAL SATISFACTION FIT A TUBE WITH ALL THE LATEST DEVELOPMENTS.

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12in., 14 in . sizes \(£ 6 / 10 /\)-.
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> SOUTHERN RADIO'S SPECIAL BARGAINS \(\downarrow\) TRANSMITTER - RECEIVER

TYPE 38 MK II * WALKIE-TALKIE *


Complete in Mecal Carrying Case. 9in. \(x\)
6?in. \(x 4\) in. Weight \(61 b\). Frequency 7.3 to 6atin. \(x 4\) in. Weight \(61 b\). Frequency 7.3 to \(9 \mathrm{Mc} / \mathrm{s}\). Five valves, \(\mathrm{f} / \mathbf{2} / 6\). Post paid.

These TX-Rs are in NEW CONDITION, but owing to demand they are not tested by us and carry no guarantee, but should prove SERVICEABLE. ATTACHMENTS for Type "38" Transreceivers. ALL BRAND NEW. Headphones 15/6; Throat Microphones 4/6; Junction Boxes 2/6; Aerials, No, \(12 / 6\); No. 2 5/:: Webbing 4/-: Haversacks 5/-i Valves-A,R.P. 12 4/6; A.T.P. \(43 / 6\); Set of FIVE VALVES 19/- the set. SPECIAL OFFER No, 2:
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Transmitter-Receiver " 38 " Mk, II. Brand new with complete set of external attachments including Webbing, Haversacks and Valves. including Webbing, Haversacks
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QUARTZ CRYSTALS. Types F.T. 241 and F.T.243, 2-pln, tin, spacing. Frequencies beF. T. \(243,12-\mathrm{pin}\), \(\frac{1}{2}\) in, spacing.
tween \(5.675 \mathrm{kc} / \mathrm{s}\), and \(8.650 \mathrm{kc} / \mathrm{s}\). (F.T.243), 20 cween \(5.675 \mathrm{kc} / \mathrm{s}\), and \(8.650 \mathrm{kc} / \mathrm{s}\), (F. T. 243 ), 20 , \(38.8 \mathrm{Mc} / \mathrm{s}\) (F.T.241, 54th Harmonic), \(\mathrm{Mc} / \mathrm{s}\) and \(38.8 \mathrm{Mc} / \mathrm{s}\) (F.T. 241 . 54th Harmonic),
\(4 /-\) each. ALL BRAND NEW. TWELVE ASSORTED CRYSTALS, 45/-. Holders for both types, 1/- each. Customers ordering 12 erystals can be supplied with lists of frequencies available for their choice.
RECORDING BLANKS. Brand new. "Emidisc." Ready for cutting. \(13 \mathrm{in}, 6 \%\) each or 15 complete in metal case \(£ 4\).
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A.C. MAINA, \(200 / 250\) volts. Provides:-
"WOBBULATOR"
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4 -speed plays 10 records 12 in ., 10 in . or 7 in . at 16, 33 , 45 or \(78 \mathrm{r} . \mathrm{p} . \mathrm{m}\). Intermixes 7 in ., 10 im . and 12 in . records of the same speed. Has manual play position; colour above baseboard \(4!\) in., below haseboard 2 yin. Fitted with Ful-Fl turnover crystal head. £6/19/6. Plus \(5 / *\)

8TEREO HEAD 8\%/19/6 Plus 5/. P. \& P.


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Fuished in 2 -tone leatherette, will take B.S.R. UA, with room for amplifier and 7 in . \(X\) in. speaker

Stmilar to the above in POLISHED WALNUT, will
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Will tune to all Band I and Band III stations. BRAND NEW by famous manufacturer. Complete with P.C.C. 84 and P.C.F. 80 valves (in serries). I.F. 18-18 or \(33-38\). Albo can be modised as an
Complete with knobs.

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22/6

AC/DC POCKET MULTI-METER KIT


Comprising 2in. moving coll meter, scale callbrated in A.C./D.C. volts, ohms and milliampe. Toltage range A.O.ID.C. \(0-50,0-100,0-250,0-500\) Milliamps. \(0.10,0-100\). Ohms range, \(0-10,000\) Front panel, range switch, wire-wound po (for ohms zero setting), toggle switch, resistor and rectifier. Basle movement, 2 mA . In grey hammer inish case.
19/6 p. \& P. Plus. Built and tested Point-to-point wiring diagram \(1 /\) - free with kit

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All with tapped primaries \(200-250\) volts.
 8 ₹., 2 amp., 10/6. 280-0-280, 80 ma., 6.3 v., 2 amp., 8.3 ₹., 1 amp., 10/6. Postage nd packing on the above \(3 /\) -

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Covering \(100 \mathrm{Kc} / \mathrm{s}-100 \mathrm{Mc} / \mathrm{s}\). on fundamen. tals and \(100 \mathrm{Mc} / \mathrm{a}\) to \(200 \mathrm{Mc} / \mathrm{s}\), on harmonics. Metal case 10 in . \(\times 6\) in. \(\times 5\) in., grey ham mer finish. Incorporating three miniature valves and Metal Rectifler. A.C. Mains 200 250 v . Internal Modulation of \(400 \mathrm{c} . \mathrm{p} . \mathrm{s}\). to a depth of \(30 \%\). Modulated or unmodolated R.F., output contnuously variable 100 millivolts C.W. and mod, switeh, varias ontput ind leator. Accuracy plus or minus

Or 25/- depasit and 6 monthly paymenta of \(21 / 6\)
Poat \& Packing \(5 /\) - extra. £6/19/6

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Coveraze \(120 \mathrm{Kc} / \mathrm{s}-\mathbf{2 3 0} \mathrm{Kc} / \mathrm{a}\)., \(300 \mathrm{Kc} / \mathrm{B},-\) \(900 \mathrm{Kc} / \mathrm{sc}, 900 \mathrm{Ko} / \mathrm{s} .-2.75 \mathrm{Kc} / \mathrm{s}, 2,2.75 \mathrm{Mc} / \mathrm{s}\). \(\mathrm{M} / \mathrm{cs}_{\mathrm{s}}, 24 \mathrm{Mc} / \mathrm{s}\). \(-84 \mathrm{Mc} / \mathrm{s}\). Metal \(16 \mathrm{Mc} / \mathrm{s},-56\)
 valves and rectifier A.C. mains 230.250 c. Internal modulation of 400 c.p.s. to a depth of 30 per cent. modulated or unmodulated R.F. Output continuously variable 100 millivolts C.W. and mod-swltch variable A.F. output
and moving coil output meter. Grey hammer finish case and white panel. S4/19/6


Or 251- deposit and 4 monthly
SIGNAL \& PATTERN GENERATOR 66/19/6
Or 25/- deposit. P. \& P. 5f and 6 monthly payments of \(21 / 6\). Coverage 7.6 Mcjs.-210 \(\mathrm{Mc} / \mathrm{s}\). in tive bands. ull on fundamentale, slow motion tuning audio output. 8 vertical and horizontal bars, log ging scale. In grey hammer tinished case with carrying handle. Accuracy \(\pm 1 \%\) A.C. maine \(200-250 \mathrm{\nabla}\)


\section*{F.M. TUNER UNIT}

Permeability tuned by famous German Manufacturer. Coverage \(88-100 \mathrm{Mc}\) g. Com plete with ECC85. Size \(4 \mathrm{in} . \times 2 \mathrm{in} . \times 2 \mathrm{in}\).

25/- Plus P. P . I/6 10.7 Mos . I.F. and Discriminator Coill \(2 / 6 \mathrm{pair}\).


\section*{8 WATT PUSH. AMPLIFIER}

COMPLETE WITH CRYSTAL MIKE AND 8in. LOUDSPEAKER
A.C. mains \(200 / 250\) v. Size 10 仵. \(\times 6\) itn. \(\times\) \(2 \jmath_{2}\). Incorporatlog 6 valves, H.F. pen., 2 triodes, 2 output pens, and rectifier. For use with sil makes and types of pick-up and mike. Negative feed-back. Two inputs, mike sind gram., and
controly for same. Beparate controls for Bass and Treble lift. Reaponse flat from 40 cycles to \(15 \mathrm{Kc} / \mathrm{s}, \pm 2 \mathrm{db} ; 4 \mathrm{db}\) down at \(20 \mathrm{Kc} / \mathrm{s}\). Output 8 watts at \(5 \%\), total distortion. Noise level 40 db down, all hum. Output transformer tapped for 3 and 15 ohm speech coils. For use with 8 td. or L.P. records, musical instruments such as Guitars,

Or \(£ 1\) deposit, plus \(\mathbf{P}, \& \mathbf{P} .7 / 6\) and 4 monthly paymente of \(23 /-\)

\section*{LINE E.H.T. TRANSFORMER}

With built-in line and width control and winding for EY81. 14 KV . Scan coll, \(90^{\circ}\) deflection, on ferrite yokes. Frame O.P. transformer 500 pf . 18 KV . smoothing condenser. Can be used for 14 in ., 17 in , or 21 in . tubes. Complete with circult diagram. 29/6 \({ }_{41 \text { Plius }}^{\text {Pit }}\)
Focus Magnet suitable for the above (state tubo). \(10 /-\) Plus \(2 / 6 \bar{P}\). \& \(P\).
17in. PERSPEX MASK 8/6 Plus 2/6 P. \& \(\mathbf{P}^{2}\)

\section*{2-TRANSISTOR POCKET RADIO}

Plus Germanium diode, fully tuneable over medium and-long waves. Size 31 in . \(4 \mathrm{ln} . \times 1\) in. Complete set of componenta includtag case, 2 transistory and earpiece (less batteries). Point to point wiring diagram 1/6, (Free with kit.)
\[
19 / 6 \quad \begin{gathered}
\text { P. Plus. } \& \text { P. } / 6 .
\end{gathered}
\]

\section*{PUSH-PULL OUTPUT STAGE}

Incluslve of transistors with input and output transformers to match 3 ohm epeech coil, sultable for use with the above kit. Complete kit of parts including transistore, Point to point wiring diagram 1/6. (Free with kit.)

RADIO AND T.V. COMPONENTS (ACTON) LTD.
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GOODS NOT DESPATCHED OUTSIDE U.K. ALL ENQUIRIES S.A.E. TERMS OF BUSINESS C.W.O.

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Electric-Methods Ltd
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Electronics (Ruislip), Ltd.
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Foyle, \(W\).
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Samsons Surplus Stores Lit.
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[^2]:    * For example "The Technical Writer" by J. W. Godfrey and G. Parr (Chapman \& Hall).

[^3]:    * Belling and Lee Ltd.

[^4]:    $\dagger$ High-speed Facsimile, Wireless World, Vol. 65, pp. 314 and 362 (July/August, 1959).

[^5]:    *Texas Instruments, Led., formerly with Standard Telephones \& Cables, Ltd.
    TStandard Telephones \& Cables, Ltd.
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[^7]:    * Bradford Institute of Technology.

[^8]:    * Forschungs Institut Manfred von Ardenne, Dresden, E. Germany.

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    $\dagger$ See, for instance, "The Technique of Stage-Lighting", (2nd Edn.), p. 151, by R.' G. Williams. Pitman, 1958.

[^10]:    $\ddagger$ For an explanation of the C.I.E. (Commission Internationale de l'Eclairage) chromaticity diagram and its $x$ and $y$ co-ordinates, see "Colour Fundamentals," by H. Henderson, Wireless World, August 1956.

[^11]:    * "Electromechanical Analogies and their Use for the Analysis of Mechanical and Electromechanical Systems", fournal I.E.E.. Part I, April 1945, pp. 157-169.

[^12]:    * Ouachita Radio-TV Service, Mena, Arkansas, U.S.A.

[^13]:    ** Wireless World, November 1957.

[^14]:    * Fane Acoustics, Ltd.

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