# Wireless World 

## ELECTRONICS

Radio • Television



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## We Were About to Say

THE hiatus in the publication of this journal caused by the slow-down and eventual stoppage in the printing industry is very much regretted. Although the June issue was eventually dispatched it was very late, and there was no possibility of producing anything in July. However, the present enlarged issue will help to bridge the gap and bring readers up to date with information of some of the interesting things to be seen at the Radio Show at Earls Court.

Throughout the "rest period," as some of our facetious friends have called it, the editorial staff have continued their normal duties, which include the assessment of events at home and abroad, and the present issue contains first-hand reports of the International Transistor Convention and Exhibition at Earls Court, the Brit.I.R.E. Television Convention in Cambridge, the "Automath" Computer Exhibition and Information Processing Conference in Paris and the French Air Show. Another International Congress on Medical Electronics was also held in Paris, but the full report on this will be held over until our next issue as we feel that any attempt at further condensation would do less than justice to its importance.

Our next issue, due for publication in mid-September will contain a full stand-to-stand report of the National Radio Show (for the benefit primarily of those who are unable to see for themselves, but useful also as a record for future reference), while the October issue will carry a technical review of the Show in retrospect which will look more closely at any new developments and assess the general trend of progress. In these issues we hope to give also some first-hand impressions of developments on the Continent as exemplified by the German Radio Show in Frankfurt, the Dutch Firato in Amsterdam and the International ElectroAcoustics Congress in Stuttgart.

The present spate of conventions and exhibitions, interesting as it is, will not be allowed to take more than its fair share of our space, and we shall continue to provide balanced issues with articles catering for a wide variety of interests and at different levels of technical understanding. While maintaining the standard of articles addressed to the professional we hope to extend our service to the student and the amateur experimenter by more articles of an expository and constructional nature. And there will be occasions when we shall take time
off to look at ourselves and perhaps discover that there is a less serious side to what must often appear the grim business of radio and electronics.

Finally, a word of reassurance to our subscribers. To compensate for the loss of an issue in July, subscription periods will be extended by one month.

## Eurovision-Five Years

ON June 6th the European Broadcasting Union celebrated the fifth anniversary of Eurovision, for it was on that day in 1954 that eight countrics collaborated to bring to their viewers the first of a memorable series of live programme exchanges which have set the pattern for subsequent expansion and improvement. True, there had been earlier pioneer work by the B.B.C. and the French R.T.F. but the "Lille Experiment" of June 1954 marked the establishment of a flexible network which superseded what was until then merely a chain.
The history of the technical development of the system is admirably recorded by E. L. E. Pawley (Chairman, E.B.U. Technical Committee) and M. J. L. P'ulling (Chairman, E.B.U. Working Party L) in No. 55a of the E.B.U. Review (June 1959). At the present time sixteen television services in twelve countries are abl 233 share programmes, and in 1958 no fewer than 233 exchanges were handled by the co-ordination centre in Brussels.
The sole justification of the Eurovision network is immediacy and this has brought many production problems, particularly in arranging multilingual commentaries. Furthermore, the picture itself is not necessarily an international language. As Jean d'Arcy (Vice-chairman, E.B.U. Programme Committee) writing in No. 56b of the E.B.U. Review points out, people of different races "simply don't see the same thing when looking at the same picture. . . . A brilliant theme for a broadcast that seems lively and attractive to the Latin is quite unbearable to the English person; a programme that is thought highly of in one place is forbidden in another. Eurovision became a school for us where we learned tolerance and understanding of others."

Looking to the future, world-wide television is already feasible. Using an airborne relay station the French have already linked Europe with Africa. Transatlantic television by such a method or by satellites would be prohibitively expensive, but by exploiting the principle of redundancy and transmitting only new information in each frame it might be possible to reduce bandwidth and so come within the capacity of the transatlantic telephone cable.

## National Radio Show

THIS year's National Radio Show opens to the public at Earls Court on August 26th. Last year's innovation of a section devoted exclusively to audio equipment was such a marked success that the area allocated to this section is this year enlarged. There are nearly 150 exhibitors at the show and of this number 38 are in the audio hall; some are in both sections. Seventy-five per cent of the exhibitors are manufacturers of domestic receiving equipment, the remainder being either users
(such as the Services, B.B.C. and I.T.A.), publishers and those providing services for the radio and electronics industry. The manufacturing and retailing sides of the industry have joined forces to provide a comprehensive display and information centre (Stand 401) devoted to careers in the radio and electronics industry.

In the following few pages will be found a selection of highlights from the information made available by exhibitors at the time of going to press.

## ALPHABETICAL LIST OF EXHIBITORS




## NATIONAL RADIO EXHIBITION

## Highlights of the Show

The innovation of an Audio Hall, combined with the surge of activity in stereophony, made sound, rather than vision, the predominating interest at last year's Radio Show. This year the pattern seems to be repeated, although the following selection of items will show that there has been no lack of development in other branches of the industry.

[^0]

Tape Magazine is provided for the new Garrard "Bichette" deck to make the tape easier to handle. The magazine contains two 4 -in diameter spools of double-play tape giving about 35 minutes playing time for each track at the tape speed used $\left(3{ }_{3}^{3} \mathrm{in} / \mathrm{sec}\right)$. The spools are so arranged in the magazine that, when the magazine is slotted into its correct position on the tape deck, the tape is already in the correct position for recording or playback.

Low-tracking Weight crystal pickup heads shown by Cosmocord include a stereo model which will track at about 2 gm and, tracking at 0.3 gm , an improved version of the singlechannel pickup described by J. Walton in our April issue. These pickup heads are fitted to the lowfriction vibration-stabilized X286
arm which was described in our Junc issue. An inexpensive low sidethrust arm designed expressly for use with stereo pickup heads is also on show.

Stereo Balance with dissimilar response loudspeakers is simplified in the Tripletone Stereo 5-5 and 12-12 amplifiers and pre-amplifiers by provision of concentric twin middlefrequency as well as bass and treble controls. Conversion to stereo of the Tripletone "Convertible" singlechannel amplifier and pre-amplifier is made easier by extending the control spindles on both sides of the potentiometers," so that, if two "Convertibles" are bolted together front-to-back, corresponding controls can be ganged together.

Better Television Sound reproduction is becoming more common. Forward facing speakers appear in many sets-the elliptical type being used to save space-and several models have two speakers, one on each side of the screen. This last trend gives a symmetrical arrangement which is often combined with a bow-fronted cabinet.

Television and Radio Distribution equipment is shown by Aerialite, Belling \& Lee and Wolsey Electronics. The Wolsey Electronics systems can distribute Band-III signals on their own frequencies, or the Band-III programmes can be "translated" to a Band-I channel for distribution over large areas. V.H.F./ f.m. can also be distributed on the original frequencies by the system. Another valuable feature is that other
programmes, such as Radio Luxembourg, can be translated tor a v.h.f./ f.m. signal, allowing the use of a combined v.h.f./TV receiver, or a v.h.f.-only receiver instead of an a.m./f.m. set.
"Sounds Fantastic"-a demonstration of sound recording given at frequent intervals by the B.B.C.- includes recorded comparisons of v.h.f. and medium-wave reception and recordings from the B.B.C. archives.

Local Oscillator Stability in f.m. receivers can be assured in two ways -by an a.f.c. system, or by crystal control of the oscillator. A.s a desirable means of tuning is push-buttons or a switch, crystal control is particularly suitable. S.T.C. are showing among their range of quartzcrystal units a three-crystal assembly on a single B7G valve base.

Video-tape recording is being demonstrated by Tyne-Tees Television, the north-eastern programme contractors, on the I.T.A. stand. The equipment used is a mobile version of the standard Ampex video-tape recorder.

Easier Servicing is a major consideration in the design of many television sets. One recent trend is the use of detachable circuit panels. Decca have a hinged chassis on three models which swings out at the back of the set to give easy access. McMichael have a chassis which unclips and can be withdrawn. Alba's



Tape level indicators using two neon lomps are not very often seen. The neons are arranged to light at different levels so that, by making the loudest sounds light one nean but not the other, the peak recording level can be restricted between two values. Two examples of this type of indicator may be seen in the Alba R59 (shown here) and R.G.D.MK103 recorders.


Slim television receivers, based on the short-necked $110^{\circ}$ tube, are displayed by almost all set manufacturers this year. 17 -inch and 21 -inch screens are the most popular sizes. Advantage is taken of the shape of the $110^{\circ}$ tube to produce bow-fronted cabinets which ovoid to some extent the "boxy" look of conventional designs. The 17 -inch G.E.C. BT304, shown here, has a curved protection glass following the line of the cabinet. Other designs are wedge-shaped, diminishing towards the back.
"packaged service" system, introduced last year, in which $90 \%$ of the components are mounted on two replaceable plug-in printed-circuit panels, has been extended to three new models.

Car Aerial Sockets for transistor receivers have already been featured by Perdio and are now provided by many manufacturers. The use of an cxternal aerial in a car avoids changes in the signal input level from the directional internal ferritecored aerial as the car moves about. Another new type of socket which is being increasingly provided on all types of receiver is one for feeding the input of a tape recorder.

Definition Control by pushbuttons in television receivers introduced at a previous Show, is not widely used, but has beent continued in two Stella sets, the 21 -inch ST. 1001 U and the 17 -inch ST. 1007 U . One button is for "soft" pictures and the other for "crisp" pictures.

Selectivity varying automatically to give the optimum signal-to-noise ratio at various signal input levels (a stronger signal produces a wider bandwidth) is one of the unusual features of the new Perdio "Continental" transistor receiver. Other unusual features of this receiver include an 87-197 metres short-wave
band, a loudspeaker as large as 8 in by 5 in , and fixed bass boost to partially compensate for acoustic losses due to the small cabinet.

In-the-room Aerials are continuing to gain in popularity, due in part to the increasing number of transmitters and improved recciver performances. At last year's show there was a large number of set-top small "V"s. 'This year Belling-Lee introduce a new $V$ aerial designed for use in areas where the small Vs do not "provide enough signal. Called the "Metropolitan," this aerial features elements which extend to about 40 in and a tunable matching network in the base pedestal. This network can be adiusted by a "front-panel" control.

Tape Tracking in Both Directions is possible with the new Truvox R7 recorder. Thus both tracks on the tape can be recorded or' replayed without having to turn the reels over. Other unusual features of this recorder are a "slide" volume control, and the provision of two alternative fast forward and rewind speeds to permit more accurate selection of a particular position on the tape while fast winding. Two other new tape recorders are also introduced by Truvox.

Simplified H.T. Supplies for television sets become possible by the
use of silicon junction diode rectifiers. S.'Г.C. are showing one inexpensive type rated at 400 volts p.i.v. and 500 mA up to $50^{\circ} \mathrm{C}$ ambient temperature. R.G.D. are using them in their latest 17 -inch and 21 -inch television sets with $110^{\circ}$ tubes-the models 610 , 611 L and 710.

F.M.-only receivers are not very often seen, although their numbers are somewhat increased this year by new models being shown by Ferranti (see photograph), H.M.V. and Ferguson.

Diplexers are usually thought of in connection with television as devices for combining Band-I and Band-III aerial leads, or separating signals in these bands which have been carried on a common lead. Where two Band-III programmes are available, it has hitherto been necessary to change aerial leads
wnen separate directional aerials nave been used. Labgear introduce now a diplexer for the combining of Channels 9 and 11 onto one cable. It is claimed to have a negligible insertion loss.

X-Aerial Range of Choice is extended this year. The Wolsey Type X75 is for Band-I stations only, while Labgear have a complete range of combined Band-I/III types. These new aerials feature improved feeder-to-aerial matching. The Labgear series provides not only for independent orientation of the Band-I and Band-III sections, but also for adjustment of the two sections for different linear polarizations of the Band-I and Band-III transmissions.

"Sputnik"-shaped, Labgear's new set-top aerial receives Band-I, -11, and -III stations in areas of good signal strength.

Bass Tone Controls are being increasingly provided in addition to the more usual treble controls even, for example, in relatively inexpensive radio-grams.

Full D.C. Component of the video signal is said to be retained in the Alba 17 -inch television receiver, T656. This is an unusual feature not found in the majority of sets nowadays.

Slim Television Trolleys have been introduced for the new slimcabinet receivers with $110^{\circ}$ tubes. As an example one model by Whiteley has a table top measuring 19in $x$ 13 in .

Components shown by Dubilier include ganged volume controls for stereo and subminiature electrolytic capacitors for printed circuit and transistor applications. Featured on T.C.C.'s stand is a working model of a rocket-telemetry apparatus illustrating the use of this company's printed-circuit switch panels,

Clock-switched Receiver showil by Ekco, the Radio-Time, incorporates an alarm clock. It can be arranged that, at a predetermined time, the receiver and also a 5 -amp mains supply are automatically switched on, and that after any predetermined period up to an hour the receiver is switched off.

Ipswich is in an area which will receive a reasonably good Band-III signal; but the Band-I transmitter is some distance away. Both BellingLee and Antiference introduce new aerials designed for this type of location. The Antiference aerialType HL303-has Band-I and Band-III sections of three elements each. The Belling-Lee Type 24A has two Band-I and four Band-III elements, and fits in with the firm's "Unit Plan" system for choosing from a variety of masts and lashingkits.

Polaroid Television Filters are a new feature to be seen in this year's range of television receivers by Pam. The filters are said to eliminate reflected light completely so that receivers can be viewed with all room lights on or in daylight without darkening the room. In addition the tonal quality of the pictures is said to be improved.

Sound Volume Expansion is an unusual feature of a tape recorder shown by Amplion. From 6 to 8 dB can be provided using lamps in a balanced bridge circuit.

Stereo Recording facilities are not very often provided even where stereo playback is possible. Exceptions to this rule are, in the field of tape recorders, the Reflectograph Model 570 and a new Veritone "Venus" model, and, in the field of microphones, the Lustraphone double ribbon model and a new twin crystal microphone shown by Cosmocord.

Rcvivals of old technical ideas include "variable selectivity" in the Ekco export a.m. receiver Model A733, and "bandspreading" for the short-wave bands in two new Philco receivers. New versions of old ideas in styling include a thermometer-like station indicator on the G.E.C. a.m.


Shorter $110^{\circ}$ tube, the 17 -inch CMEI705, developed by Siemens Edison Swan, is used in this Ekco TP347 receiver to give what is cloimed to be the slimmest-ever portable television set. The tube has a new type of electrostatic focusing system, based on a cylinder lens, in which focusing action takes place over a shorter distance than normal. As a result the tube length (/I inches) is about $1 \frac{1}{4}$ in shorter than the equivalent $110^{\circ}$ 17-inch tube of orthodox gun design.
receiver Model BC401 and, on Ekco and Ferranti receivers, a pair of tuning scales, each of which is printed tipside-dows relative to the other to allow easy reading of the station names with the receiver at any angle. Another increasingly common styling feature is the employment of edge-on control knobs outside their usual field of television receivers.

Band-III Aerials of high gain, good back-to-front ratio and negligible side-lobe response are often required for "de-ghosting," especially in fringe areas. New eleven-element aerials by Antiference an. 1 Labgear feature these characteristics, and aerials by C Aerials, Ltd., have a specially shaped folded dipole to achieve these ends. It is claimed that, with the shaped dipole, side lobes virtually disappear, and a reflector is not necessary. Band-I elements can be fitted to the Band-III arrays and a transparent junction-box cover enables inspection of the connections to be made without unsealing the box.

$9 \times 2 \mathrm{~mm}$, sub-miniature wire-ended fuses in a range of values between 60 mA and IA are shown by Bulgin.

# New Horizons in Computing 

PARIS INFORMATION PROCESSING CONFERENCE AND "AUTOMATH" EXHIBITION

"THE day is rapidly drawing near when digital computers will nu longer be made by assembling thousands of individually manufactured parts into plug-in assemblies and then completing their interconnection with back-panel wiring. Instead, an entire computer or a large part of a computer probably will be made in a single process. Vacuum deposition of electrodes on blocks of pure silicon or germanium and the subsequent diffusion of the electrode material into the block to form junctions is a most promising method. The successful development of this method would allow large numbers of transistors and all of their interconnecting wiring to be made in one operation. Vacuum deposition of magnetic materials and conductors to form coincident-current magnetic core memory planes is a second promising method that will allow an entire memory to be made in one operation. The vacuum deposition of superconductive switching and memory circuits is a third method that will make possible the printing of an entire computer."

## Advanced Engineering

The above quotation is from a paper by K. R. shoulders and the late D. A. Buck (inventor of the cryotron) which was read by A. Baker at the International Conference on Information Processing held recently in UNESCO House in Paris. While the Conference was not by any means restricted to the engineering design of computers, but included sessions and symposia on such things as mathematical methods, linear programming and machine translation of languages, it did contain a group of papers of rather special appeal to electronics people. Summed up by the paragraph above, they dealt with the advanced engincering methods of the future which may well become known as "third generation" computing techniques.

At the moment we have the "first generation" of clectronic computers, which are thermionic-valve machines. These are already on the market, and we are now rapidly passing into the "second generation" of transistor and magnetic-core machines, which have emerged from the laboratories and are on the point of becoming commercial. Although the conventional transistor seems an ideal component for computers it does not prevent the researchers from developing this "third generation" idea which sees the manufacture of computers more in terms of chemical processing than electronic assembly.
But what is the real need for this new approach? What advantages does it offer? There is, of course, the ever-present drive towards simpler and cheaper methods of fabrication. But the main purpose of the new line of development is the achievement of higher speeds of operation. At present the speed of information transfer in electronic digital computers is in the region of $10^{\circ}$ binary digits per second. Advanced transistor techniques are likely to increase this by a factor of 10 quite soon. But many appli-
cations are envisaged for which speeds in the region of 10 ' bits $/$ second are required. This is particularly true of the future class of computers which will have the property of "learning" by trial-and-error methods and will torm part of self-adaptive control systems^. An essential feature of their operation is the execution of a great many random trial calculations before the optimum control condition is obtained, and here extremely high speed is required if the computer has to work in the natural time scale of the control system.
With digit pulses of millimicrosecond length the problem arises of time delays in the transfer of information through the computer due to the finite speed of the conduction of electricity. . For electrical signals in free space the upper limit is the speed of light. In solid conductors, a signal travelling a mere matter of 6 to 8 inches takes 1 millimicrosecond. One can see, then, that machines with dimensions and wiring lengths of the order of several feet would create difficulties in the precise timing arrangements which are so important to the correct operation of digital computers (because time intervals represent numerical values).
This means, in general, that no computer for this $10^{\prime \prime}$ bits/second order of speed can be much more than 2 feet cubed in size. It also means that such a small size places a limit on the allowable power and heat dissipation of the circuitry. Many conventional electronic components are therefore ruled out, not only on the score of size but also because their power consumption is too high.

## Superconductive Components

The three main groups of components which are at present being investigated for possible use in these small-size high-speed computers are mentioned in the opening paragraph-semiconductor "solid circuits," magnetic film devices and superconductive components. All lend themselves to the fabrication of circuitry by "printing" methods, and, in fact, the term used by Buck and Shoulders in their paper is "microminiature printed systems."

Actually this paper is concerned more with superconductive (or "cryogenic" as they are sometimes called) components than the others. It describes experimental work which has the ultimate aim of printing cryotrons small enough to fit into 1 -micron squares. Conductors will have to be only 0.1 micron in width. The basis of the method is the selective etching away of a deposited metal film, but some very unusual processes are involved. The original metal film (e.g. lead or tantalum) is deposited on an insulating base by vapour plating. A "resist" or protective pattern is then formed on this by electron bombardment in the presence of hydrocarbon or siloxane vapours. The bombardment causes polymerization of the vapour and so produces a deposit

[^1]un the metal film where the electron beam is directed. Finally, the unprotected metal, not covered by the "resist," is etched away by a vapour process, using a suitable gas for the metal concerned (e.g., chlorine for molybdenum films).

The magnetic devices so far investigated for printed computers are based on very thin magnetic films of a few hundred to about a thousand angstrom units. Very little has been done on logical switching elements but considerable experimentation has been devoted to magnetic storage systems. These consist of regular arrays of sniall circular spots of magnetic material, a few millimetres in diameter, deposited by evaporation on to glass bases. Each spot acts in much the same way as a ferrite toroidal core in the familiar matrix type of magnetic store. The material has a rectangular hysteresis loop and it can be switched from one direction of magnetization to the other by currents passing through adjacent conductors, which can be printed on both sides of the glass base.

Actually the magnetic spots are given a preferred direction of magnetization, or uni-diametrical anisotropy, by evaporating the material (e.g., Permalloy) on to the glass base in the presence of a steady magnetic field. In operation the spots change from one direction of magnetization to the other by a simple rotation of the magnetization. Coincident-current methods can be used for the driving system, as in the present ferrite toroidal-core type of matrix stores.
A paper by J. I. Raffel and D. O. Smith described an experimental magnetic film store for 32 ten-bit words which used $1.6-\mathrm{mm}$ spots centred 2.5 mm apart, but it is thought that spot densities of the order of 1,000 per square centimetre should be obtainable. Apart from this possibility of large storage density, the main advantage of the magnetic film is its low switching coefficient-defined as the product of switching time (microseconds) and applied field (oersteds). This is at least ten times smaller than the value for ferrite toroids, so in general one can obtain much faster switching times and use much smaller driving currents. Experiments have indicated, in fact, that switching times in the range 1-10 millimicroseconds are possible.

## Parametric Oscillator Devices

The problem of time delays in high-speed computers can, however, be tackled in another way besides that of straightforward size reduction. The technique is to use lengths of conductors which are precisely related to the phases of the signals-in other words, transmission lines. This, in fact, is being done in experiments on a new class of para-metric-oscillator $\ddagger$ computing circuits working at microwave frequencies. A paper by J. Wesley Leas described a parametric oscillator system which can be used to gate, amplify and store binary information expressed in terms of two possible phases of the oscillation (see Fig. 1). The oscillation frequency was $2,000 \mathrm{Mc} / \mathrm{s}$ and the pump frequency $4,000 \mathrm{Mc} / \mathrm{s}$.

It is probably true to say that this work actually stems from the original discovery in 1954 by Eiichi Goto, a Japanese scientist of Tokyo University, that parametric oscillators can be used for binary computing circuits**. The computing elements so formed were named "parametrons" and were ex-

[^2]

Fig. I. Construction of microwave parametric-oscillator computing element.
tensively developed in Japan for building digital computers, and now about fifty per cent of the machines in that country make use of them for logical circuitry. It was noticeable in the "Automath" exhibition at the Grand Palais in Paris that, of the 27 exhibitors, four were Japanese firms and all showed parametron computers. (Incidentally, there was only one British stand-Standard Telephones and Cables-and that was present as part of its own international group and displayed a computer designed by a Dutchman.)

As already mentioned, the parametron is basically a parametric oscillator. It has a pump frequency which is twice the oscillating frequency, and the pump signal maintains the parametric oscillation in a resonant circuit by periodically varying the reactance of one tuning element of the circuit. In most of the Japanese machines the variable reactance is a ferrite-cored inductor (see Fig. 2). Because the pump signal is twice the oscillation frequency, it is possible for the oscillation to have either of two phases, $180^{\circ}$ apart. These represent the two states, " 0 " and " 1, " of the binary circuit. Which state (i.e., phase) the circuit is in at any moment is determined by the forcing or locking effect of the input signal to the parametron. This is a small signal at the oscillation frequency coming from previous parts of the computing system, and it has a phase, representing " 0 " or " 1 ," which has been determined by previous logical operations.
The linking of parametrons into complete arithmetic circuits is done on the principle of "ballot box" or " majority decision" logic. The outputs of an odd number of parametrons (asually three) converge as primary windings on a transformer whose secondary provides the state-determining signal for the succeeding parametron. If two of the outputs have the " 1 "phase of signal and the third output has the opposite " 0 " phase, then by simple cancellation the signal produced at the transformer secondary will have the " 1 " phase and will trigger the succeeding parametron into the " 1 " condition.
For "AND" and "OR" gating operations, one of the three inputs to a parametron is arranged to carry a permanent signal, " 0 " or " 1 ." If a " 1 " is used for this, a " 1 " signal applied to either or both of the other two inputs will produce a " 1 " output at the secondary-that is, an "OR" gate. If a " 0 " phase is used for the permanent signal input, then a " 1 " output will be obtained only if
a " 1 " signal is applied to both of the other two inputs simultaneously-in other words, an "AND" gate. From such arrangements complete arithmetic circuits can be built up on well-established principles.
Since it is necessary for the parametron to be continually changing its state the oscillation has to be periodically quenched, so that after each quenching it can be started again in a new phase. This is done by a square-wave pulsing system which, in fact, provides the clock pulse or synchronizing signal of the whole computer. Each pulse must, of course, allow several cycles of oscillation to occur in order to establish a binary digit, "0" or " 1 ," on the phase principle, so the clock frequency necessarily has to be somewhat lower than the parametric oscillation frequency. Most of the Japanese machines are restricted by their variable reactors to oscillation frequencies of about $1 \mathrm{Mc} / \mathrm{s}$ and consequently the clock p.r.f. is limited to the $100 \mathrm{kc} / \mathrm{s}$ region. This, in fact, is onc of the main disadvantages of the existing computers because of the limitation it sets on the speed of the arithmetic circuits.

The obvious way of overcoming this limitation is to use very much higher frequencies of parametric oscillation. This, in fact, is what has been done in the system described by J. Wesley Leas. His $2,000 \mathrm{Mc} / \mathrm{s}$ oscillator takes the form of a halfwave resonator, constructed on the strip line principle by photographic engraving of a copper-clad insulating board. The variable reactance element in the resonator is a semiconductor diode, and the capacitance of this is varied by the $4,000-\mathrm{Mc} / \mathrm{s}$ pump signal delivered through another resonant system. Regarding the device as an amplifier of the small input triggering signals, the gain is about 5 times. With the $4,000-\mathrm{Mc} / \mathrm{s}$ pump signal the digit pulse rate can be up to $4 \times 10^{\prime}$ pulses per second. Advanced experiments with oscillators using waveguide components and pump frequencies of $10,000 \mathrm{Mc} / \mathrm{s}$ suggest that digit rates as high as $2 \times 10^{\prime \prime}$ pulses per second ( $2,000 \mathrm{Mc} / \mathrm{s}$ ) might be possible.

A good many sessions at the Conference were devoted to the logical design of computing systems. This subject is nowadays considered more the province of the mathematician or programmer than the electronic engineer, but even so the engineer
has to be brought into it eventually. One recent trend in logical design is the speeding up of computation by what amounts to "time and motion study " in the organization of the machine's facilities. Another trend is towards more complete utilization of the computer by systems in which several programmes of calculation can be run at the same time. This idea was exemplified at the "Automath" exhibition by two Continental com-puters-the French Gamma 60 (Compagnie des Machines Bull) and the German ER56 (Standard Elektrik Lorenz)-both of which were transistor machines.

The basis of the idea is to divide up the computer into a number of autonomous units (for example a storage system can be divided into several sections) which can be used independently instead of acting as a complete interlocking assembly. These units already exist to some extent in conventional computers (e.g., arithmetic unit, store, input equipment, output equipment) but in normal operation are dependent on each other. The calculation proceeds from unit $X$ to unit $Y$, and while $Y$ is working $X$ is left idle. But in the newer machines, while $Y$ is working X is used for part of another calculation. This system, of course, calls for a central programme control unit for distributing the work (the sections of different calculation programmes) to the units when they become available. It also has to ensure that the several programmes do not become mixed up! In the Gamma 60 machine this programme control unit is called the "central controller"; in the ER56 it is called the "traffic pilot."

## "Intelligent Machines"

Other sessions at the Conference dealt with new character recognition schemes based on the morphological rather than the geometrical approach (in which the recognition depends on the positions of "picture elements" relative to the frame of reference). In so far as these morphological methods are able to cope with characters in unfamiliar positions (upside down, say) they might be regarded as more "intelligent" than previous schemes. But perhaps the most advanced sortie into the field of " machine intelligence," as it is called, was a paper delivered by R. Grimsdale of Manchester University which demonstrated the ability of a computer to do crea-


Fig. 2. A unit from a Japanese parametron computer ( 25 parametrons). The small black semi-circles at the top are the ferrite cores of the variable reactors. Along the bottom are the ferrite cores of the input transformers.
tive thinking. This thinking takes the torm of constructing programmes which satisfy certain criteria. The criteria are supplied by human beings, but the human beings have no idea of what form the invented programmes will take. In iact the experimenters admit to being agreeably surprised at the resourcefulness of the machine in producing hitherto unthought-of programmes!

Some degree of randomness is an essential part of creative activity, and in fact the machine operates by generating random sequences of instructions and modifying these by the trial-and-error "learning"
process* until the programme conforms to the criteria. For this purpose the programme is performed and tested on a "sub-computer" which is actually the same machine used in a different way. Eventually Dr. Grimsdale and his colleagues hope to devise a thinking machine which will invent its own criteria, based on certain logical concepts. After this, to end with another quotation, "Purposeful thinking to human advantage can only follow if the machine is given contact with the outside world. . . ."

* See "Learning Machines," Wireless World, January, 1959, issue.


## BOOKS RECEIVED

## B.B.C. Engineering Monographs

No. 21 "Two New B.B.C. Transparencies for Testing Television Camera Channels," by G. Hersee, A.M. Brit. I.R.E., and J. R. T. Royle. Pp. 19; Figs. 10.
No. 22 "The Engineering Facilities of the B.B.C. Monitoring Service," by C. J. W. Hill, A.M.I.E.E., A.C.G.I., and H. S. Bishop, Assoc.I.E.E. Pp. 16; Figs. 11. Describes equipment used at the Caversham receiving station.
No. 23 "The Crystal Palace Band I Television Transmitting Aerial," by W. Wharton, A.M.I.E.E., and G. C. Platts, B.Sc. Pp. 15; Figs. 9.

No. 24 " The Measurement of Random Noise in the Presence of a Television Signal," by L. E. Weaver, B.Sc., A.M.I.E.E. Methods based on the sampling of random noise in minimum energy regions of the video spectrum. Pp. 16; Figs. 5.
The price of the above, which are obtainable from B.B.C. Publications, 35 Marylebone High Street, London, W.1, is 5 s each.

Metal Industry Handbook and Directory 1959. General properties of non-ferrous metals and alloys, tables of data and lists of suppliers. Pp. $564+$ XVI. Price 2Is. Iliffe \& Sons Ltd., Dorset House, Stamford Street, London, S.E.1.

Radio Engineer's Pocket Book, by F. J. Camm. Twelfth edition of a compendium of useful formulæ and figures. Pp. 178. Price 6s. George Newnes, Ltd., Tower House, Southampton Street, Strand, London, W.C. 2 .

British Standard Specifications
3040: 1958. "Radio-freyuency Cable, for use with Domestic Television and V.H.F. Receiving Aerials." Pp. 15. Price 4 s 6d.
3041: 1958. "Television and V.H.F. Broadcast Receiving Aerial Feeder Connectors." Pp. 10; Figs. 3. Price 4s.
3045: 1958. "The Relation Between the Sone Scale of Loudness and the Phon Scale of Loudness Level. Pp. 7. Price 3s.
3081: 1959. "Basic Dimensions for Printed Wiring." Recommendations for rectangular grid dimensions, fixing holes, strip width and minimum spacing, etc. Pp. 6. Price 3s.
2134: Part I: 1959. "Fixed Electrolytic Capacitors." General requirements and tests. Pp. 15. Price 7s 6 d .
The above are obtainable from British Standards Institution, 2 Park Street, London, W.1.

Electronic Apparatus for Biological Research, edited by P. E. K. Donaldson. Contains a great deal of standdard electronics theory and practice, but with some
chapters on transducers, electrodes and complete circuits peculiar to biological work. Pp. 730; Figs. 949; Plates 47. Price £6. Butterworths Scientific Publications, 4 and 5 Bell Yard, London, W.C.2.

Noise in Industry. Edited by A. E. Stevens, B.A. (Oxon), B.Sc., F.Inst.P. A review of the effects of noise on hearing and possible methods of amelioration. Pp. 6. Issued for the information of managements by Amplivo:; Ltd., 2 Bentinck Street, London, W.1.


Film scanning unit developed by the B.B.C. for the rapid transmission of motion pictures over the transatlantic cable for subsequent TV broadcasting. A specimen frame of 16 mm film, as received, is shown (below). Some details of the system are given on page 362 of this issue


## International Regulations

AT irregular intervals an international conference is called by the International Telecommunication Union to revise the regulations on which the operation of all radio services is based, and to deal with technical and administrative matters coming within the terms of the International Telecommunication Convention.

The revision of the regulations now in use, which were drawn up at Atlantic City in 1947, is the main task of the conference which opened in Geneva on August 17th. It is at this conference that the block allocation of frequencies to the various radio services (broadcasting, marine, aeronautical, telecommunications, mobile radio, amateurs, etc.) is decided.

A delegation of 45 , led by Capt. C. F. Booth of the General Post Office, is representing the U.K. at this conference. The delegation includes representatives of various Government Departments, the Armed Forces, B.B.C. and I.T.A., as well as advisers from operating agencies and other organizations.

The conference is expected to last four months.
"Live" v "Mono" v "Stereo"

AS a result of the interest shown in his Royal Festival Hall demonstrations of mono and stereo sound reproduction, G. A. Briggs has decided to carry the expcriment a stage further at a lecturedemonstration to be held at the Colston Hall, Bristol on October 9th. For this purpose he is having special recordings made of solo and concerted items in which all available resources will be employed to obtain the best possible recordings by both mono and stereo techniques. We believe this will be the first occasion on which a comparison between live performances and both monodic and stereophonic reproductions of the same items has been attempted in public.

## College of Technologists

LAST November the National Council for Technological Awards announced its proposal to create an award higher than the Diploma in Technology, to be known as the M.C.T. (Membership of the College of Technologists). This college, which is an administrative and not a teaching body, will operate within the framework of the National Council for Technological Awards.

A Board of Scientific and Industrial Studies is to be responsible for the academic and industrial aspects of the administration of the new award and among its fifteen members are:-Dr. R. C. G. Williams (Philips' chief engineer), Dr. G. B. B. M. Sutherland (director, N.P.L.) and Dr. J. S. Tait (principal, Northampton College of Advanced Technology).

The Council's intention is that this award should be a "mark of outstanding distinction granted to a student who has proved his ability by completing a substantial programme of work demanding the application of his knowledge to the solution of a problem of value to industry".

## Medical Electronies

AT the second International Conference on Medical Electronics held in Paris at the end of June* a new international organization was formed under the presidency of Dr. V. K. Zworykin. It is to be known as the International Federation for Medical Electronics and its object will be to encourage the dissemination of information on medical electronics.
One of its functions will be to sponsor international congresses at regular intervals and the next will be held in this country in July, 1960. This conference is being organized by the Electronics and Communications Section of the Institution of Electrical Engineers. It is also planned to hold an international scientific exhibition on medical electronics in conjunction with this conference.
British members of the committee of the International Federation for Medical Electronics are Dr. C. N. Snyyth, of University College Hospital, who is a vice-president; B. Shackel (E.M.I. Electronics), treasurer; W. J. Perkins, of the National Institute for Medical Research; and Dr. R. C. G. Williams, of Philips Electrical.
*A report on the Conference will be published in our next issue.-ED

## B.B.C. Satellites

BY the end of this year the B.B.C. will have 23 television stations in operation and these will serve about 98.7 per cent of the population. There will also be a v.h.f. sound service for about 96.4 per cent of the population from 21 stations. The problem of bringing TV and the v.h.f. sound service to the remaining areas-many of them sparsely populated-is being solved by building a number of low-power satellites, Most of the stations will be unattended " translators" which will pick up signals from an existing B.B.C. station and re-transmit them on a different frequency. Initially there will be 14 TV stations, all in Band I, and eight of them will also be equipped with v.h.f. sound transmitters. V.H.F. sound is also being added to two existing television stations-Londonderry and the Channel Islands.

The new stations will be at Berwick-on-Tweed, Fort William, Galashiels area, Llandrindod Wells area, Loch Leven, Oban, Oxford/Berkshire, Wesi Cornwall, Barrow/Lancaster area, Enniskillen area, Ipswich area, Pembroke/Milford Haven area, Sheffield, and Skegness. The first eight of these stations will be equipped for both TV and v.h.f. sound.

The Radio Industries Club, which now has a membership of nearly 1,000, has elected Dennis Curry, a joint managing director of Currys Ltd., as president in succession to Sir Robert Fraser, Director General of the I.T.A. He is the first "retailer" president. The new chairman in succession to L. A. Sawtell (Mullard) is A. E. Bowyer-Lowe, and the new vice-chairman H. C. Roberts (Cossor). W. E. Miller (Trader Publishing Co.) has relinquished the honorary secretaryship of the club which he had held for 19 years. Harold Curtis, until recently with the Radio and Televsion Retailers' Association, has been appointed secretary.
I.E.E. Council.--The new president of the I.E.E. for 1959-60 is Sir Willis Jackson (Metrovick). The two newly elected vice-presidents are G. S. C. Lucas (B.T.H.), and O. W. Humphreys (G.E.C. Research Laboratories). Among the new ordinary members of the council are Professor H. E. M. Barlow, of University College, London; C. O. Boyse (A.T. \& E.); L. Drucquer (B.T.H.); H. G. Nelson (English Electric); and G. A. V. Sowter (Telcon).
I.E.E. Electronics and Communications Section.-The following have been elected to fill the vacancies which will occur on the Committee of the Electronics and Communications Section of the I.E.E. in September:M. J. L. Pulling (B.B.C.), chairman; J. A. Ratcliffe (Cavendish Laboratory), vice-chairman; P. A. T. Bevan (I.T.A.); Dr. J. Brown (University College, London); L. J. I. Nickels (Standard Telecommunications Laboratories); N. C. Rolfe (Newmarket Transistors and Cathodeon Crystals); and C. Williams (R.A.E.).

Audio Fairs Ltd., the non-profit making organization set up a few years ago by a group of audio equipment manufacturers to sponsor the London and provincial Audio Fairs has moved to 22 Orchard Street, London, W.1. (Tel.: Welbeck 9111.) V. G. P. Weake, director of Pamphonic Reproducers Ltd., and Bryan Savage Ltd., has been elected chairman of the council. M. L. Berry (Trix) is vice-chairman and L. H. Brooks continues as secretary. Other members of the council are:-D. A. Lyons (Trix), J. Maunder (Vitavox), Hector V. Slade (Garrard), G. E. Spark (Garrard) and T. R. B. Threlfall (Pye Records).

The Television Society announces that a new centre is being formed in the Cardiff area and that the Leicester centre is being revived. Readers in these areas can obtain information regarding these sections from the Society's headquarters, 166 Shaftesbury Avenue, London, W.C.2.

A full-time course (October to May) for students wishing to sit for Part III of the I.E.E. examinations is again being organized by the South East London Technical Colleg. Information regarding the course, for which the fee is $£ 17$, is obtainable from the Department of Electrical Engineering and Applied Physics, Lewisham Way, London, S.E.4.

Information Engineering.-An advanced 12-month course in information engineering is again being held at the University of Birmingham from October. On the satisfactory completion of the course graduates can qualify for the degree of M.Sc. Subjects available cover communications, radar, computers and control systems with some degree of choice to suit individual requirements. (Fee £81.)

Dip. Tech. Course.-Dr. G. N. Patchett, head of the Department of Electrical Engineering at the Bradford Institute of Technology, has sent us a brochure giving details of the four-year electrical engineering sandwich course for the Diploma in Technology provided at the College. Specialization in electronics with additional physics is provided for in the final years.
A.F.C.E.A.- The new president of the London Chapter of the Armed Forces Communications and Electronics Association is Col. J. A. Plihal of the U.S. Air Force. Being an American organization the officers of the Chapter are Americans but there are also British associate officers. The recently elected associate vicepresidents are:-Sir Harold Bishop (B.B.C.), Henry Chisholm (Cosser), Maj. Gen. E. S. Cole (War Office), Henry G. A. Kay (Benjamin), and Sir Reginald PayneGallwey. The associate treasurer is P. D. Canning (Plessey) and the associate secreary L. T. Hinton (S.T.C.).

Society of Relay Engineers.--The offices of the Society have been transferred from Kettering to Obelisk House, Flneden, Norinants (Tel.: Finedon 204). The secretary is ' $\Gamma$. H. is ${ }^{2}$ Il.

Computer Development.--The National Research Development Corporation is to give its support to Ferranti and E.M.I. Electronics in further development work on advanced high-speed computers. E.M.I. have been collaborating with the N.R.D.C. for the past four years in the development of large business computing systems which has resulted in the production of the EMIDEC 2400. The new programme will be devoted to the development of the EMIDEC 3400 suitable for large-scale high-speed scientific work. The experience gained from the operation of Ferranti computers has shown the need for the new very powerful high-speed computer now proposed-the ATLAS--for both scientific research and development and for data processing.

Reliability.-The sixth American National Symposium on Reliability and Quality Control in Electronics will be held in Washington, D.C., from January 11 th to 13 th, next year. Information regarding the submission of papers and attendance at the Symposium may be obtained from R. Brewer, of the Research Laboratories, The General Electric Co., Wembley, Middlesex.

Automatic Control.- The first International Congress for Automatic Control is to be held in Moscow from June 25 th to July 5 th next year. It is being held under the auspices of the International Federation of Automatic Control, of which the British Conference on Automation and Computation is the U.K. national member. The secretary of the I.F.A.C. is Dr.-Ing. G. Ruppel, Prinz-Georg-Str. 79, Dusseldorf, Germany.
"Photo-Emission" is the title of the latest film in the advanced science series for sixth forms and technical colleges which is issued by the Mullard Educational Service. It runs for 18 minutes on $16-\mathrm{mm}$ black and white sound film. It can be hired together with comprehensive teaching notes from the Educational Foundation for Visual Aids, Film Library, Brooklands House, Weybridge, Surrey.

Two new I.T.A. stations are scheduled to come into service in October; the East Anglian station on the 27th and the Northern Ireland transmitter on the 31 st . The Mendlesham, Suffolk, station will radiate in channel 11, with an e.r.p. of 200 pW , and the Black Mountain, Belfast, station in Channel 9 with an e.r.p. of 100 kW . Both stations employ directional aerials with horizontal polarization.

Isle of Man V.H.F.-The B.B.C.'s transmitting station at Douglas, Isle of Man, which has been radiating one v.h.f. sound programme since December, 1957, now broadcasts all three sound programmes. The frequencies are $88.4 \mathrm{Mc} / \mathrm{s}$ (Light); $90.6 \mathrm{Mc} / \mathrm{s}$ (Third) and $92.8 \mathrm{Mc} / \mathrm{s}$ (Home). The mean e.r.p. is 3.3 kW .

Brighton.-The B.B.C. has recently brought into service a permanent television transmitter at Whitehawk Hill, near Brighton, to replace the temporary transmitter at Truleigh Hill which has been in use since early 1953. It operates in the same channel (2).

Receiving licences in the U.K. at the end of June totalled 14,847,483. The number of combined television/sound licences increased by over 82,000 to 9,495,183. Sound-only licences were 5,352,295-a decrease of nearly 27,000 .

Reunion Dinner of R.A.F. radio ex-apprentices is being organized for September 19th at the Grand Atlantic Hotel, Weston-Super-Mare. Particulars from Flt. Lt. E. C. Hargest, No. 1 Radio School, R.A.F., Locking, Somerset.

Correction.-We have been asked to point out that in the advertisement on p. 104 of the June issue relating to the Mazda 6F23 r.f. pentode, the vertical (anode and screen current) scale of the bottom left-hand set of curves should be doubled, i.e., each division should represent 5 and not 2.5 mA .

## Personalities

Rear Admiral K. R. Buckley, M.I.E.E., M.Brit.I.R.E., Director of the Naval Electrical Department, Admiralty, since July 1958, assumes, the new title of Chief Naval Electrical Officer under the reorganization of the material and personnel departments of the Admiralty. He also becomes Director of Engineering and Electrical Training. Reat Adrairal Buckley commanded H.M.S. Collingwood, the naval electrical school at Fareham, Hants., for two vears prior to 1957 when he was appointed Command Electrical Officer at Portsmouth.

S:: Willis Jackson, the 1959/60 president of the Institution of Electrical Engineers, has been Director of Research and Education with Metropolitan-Vickers since 1953. For the previous seven years he had occupicd the chair of electrical engineering at the Imperial College of Science and Technology. From 1938 to 1946 he was professor of electrotechuics at Manchester University. Sir Willis, who was appointed a Knight Bachelor in last year's Birthday Honours, has served on many advisory councils and committees including the Scientific Advisory Council, Ministry of Supply (1947-1954), and the Research Council of the D.S.I.R. (since 1956).


Sir WILLIS JACKSON

M. J. L. PULLING
M. J. L. Pulling, C.B.E., M.A., who is elected chairman of the Electronics and Communications Section of the I.E.E. for the ensuing year, is Controller, Television Service Engineering, in the B.B.C. He joined the Corporation in 1934 and was superintendent engineer (recording) from 1941 until 1949 when he took charge of the television side of the er.gineering division. After graduating at King's College, Cambridge, in 1928 and spending a further year in the University radio laboratory he was for five years in the radio industry before he joined the B.B.C.
J. A. Ratcliffe, C.B.E., F.R.S., the new vice-chairman of the I.E.E. Electronics and Communications Section, is reader in physics in the Cavendish Laboratory, Cambridge. He is chairman of the Radar and Signals Advisory Board of the Ministry of Supply Scientific Advisory Council and was appointed to the recently formed National Committee on Space Research.
F. E. Godfrey, assistant secretary of the Radio Industry Council fo: ncarly eleven years, has retired. At the R.I.C., Mr. Godfrey has been concerned with education and training foi the industry and administered the R.I.C. trainixg scheme for technicians from its inception in 1952.
N. W. Hunt, chief engineer of Cathodeon Crystals, Ltd., of Linton, Cambridge, since its formation in 1953, has been appointed manager of the crystal division of Pye Proprietary Limited, of Melbourne, Australia.


Honorary Membership of the Brit.I.R.E. was awarded to E. K. Cole (left) and Dr. V. K. Zwarykin (right) at the Institution's convention, held at Cambridge University (see page 335). Here they are congratulating each other just after the ceremony in the presence of Professor E. E. Zepler, president of the Institution.
Dr. Henry Boot and Professor John Randall, F.R.S., are among this year's recipients of the American John Scott Award for "developing inventions for the benefit of mankind." They will each receive $\$ 1,000$ for their invention of the cavity magnetron. Dr. Boot, who was at Birmingham University, is now at the Services Electronics Research Laboratory, Baldock, Herts. Professor Randall is Wheatstone Professor of Physics at London University (King's College).
H. Carleton Greene, O.B.E., who is to succeed Sir Ian Jacob as Director-General of the B.B.C. at the end of the year, joined the Corporation in 1940 as German editor, in the European Service. For two years immediately after the war he was in charge of broadcasting in the British Zone of Germany. Four years ago Mr. Greene, who is 48, headed the commission set up to advise on the formation of a broadcasting organization in the Federation of Rhodesia and Nyasaland.

Martin Ryle, F.R.S., will be the first to occupy the Chair of Radio Astronomy established at the University of Cambridge. He will take up his appointment on October 1st. Mr. Ryle left Oxford University in 1939 with an M.A. degree and joined the Telecommunications Research Establishment where he worked on radar applications until the end of the war. He then went to Cambridge as lecturer in physics at the Cavendish Laboratory and more recently transferred to the Mullard Radio Astronomy Laboratory at the University.

Paul Adorian, M.I.E.E., M.Erit.I.R.E., managing director of Associated Rediffusiort, Ltd., has had the Fellowship of the City and Guilds of London Institute (F.C.G.I.) conferred upon him for his work in the fields of radio relaying, flight simulators and tactical teachers. He studied at the City and Guilds College from 1927 to 1932.

George S. C. Lucas, O.B.E., M.I.E.E., director and chicf engineer of B.T.H., has been made an F.C.G.I. "for radar and electronic research and services in technical education." He joined the B.T.H. research laboratories in 1925 and was head of the electrical and development section from 1932 until 1944 when he became head of the electionics engineering department.
Dr Manfred von Ardenne, who is well known for his television research work in the early 1930s, is now actively engaged in the field of medical electronics and read two papers at the recent Paris Medical Electronics Conference. He is now in a research institute in Dresden, East Germany.

Dr. Louis Essen, of the Standards Division of the National Physical Laboratory, which he joined in 1929, has been awarded the A. S. Popov Gold Medal by the Academy of Sciences of the U.S.S.R. This is the first time this medal, awarded for "the most distinguished scientific work in the field of radio-engineering performed during the period 1956-1958," has been given to a scientist outside the Soviet Union. The outstanding achievement which has won Dr. Essen this recognition has been his work leading to the establishment of an atomic frequency standard as a possible basis for the future standard of time.


Dr. L. ESSEN

E. E. ROSEN

Edward E. Rosen, managing director of Ultra Elecric, has been elected chairman of the Radio Industry Council in succession to G. Darnley-Smith (Bush Radio), who has held the office for the past seven years and one year previously. Mr. Rosen joined Marconi's in 1913 as a pupil and after serving in the 1914-18 war in the Royal Flying Corps, started his own company (Edward E. Rosen \& Co.) in 1920 for the manufacture of headphones and loudspeakers. The company became Ultra Electric, Ltd., in 1923. Hector V. Slade (Garrard Engineering) is the new vice-chairman of the Council. Mr. Slade is this year's chairman of the Radio and Electronic Component Manufacturers' Federation.
D. Q. Fuller, A.M.I.E.E., who in 1950 was made responsible for the early experimental work on transistors undertaken by the Pye Group, has been appointed director of engineering of Newmarket Transistors, a member of the group. Newmarket Transistors also announce the following appointments: George Roman, Dipl.Ing., who joined the company in 1956, becomes chief physicist; John B. Haggis, Grad.I.E.E., who has been with the Pye Group since 1945 and was working on television camera tube development with Cathodeon until 1954 when he transferred to Newmarket Transistors, is appointed chief production engineer; T. D. Towers, M.B.E., M.A., Grad.Brit.I.R.E., who joined the company as a circuit applications engineer early last year, becomes chief development engineer.
C. Ross, Grad.Brit.I.R.E., whose article on magnetic heads is on page 321, has been working on professional $16-\mathrm{mm}$ magnetic recording equipment in the research and development laboratory of Kelvin \& Hughes at Hillington, Glasgow, since 1957. After serving an apprenticeship with E.M.I. Engineering Development, Ltd., he worked as a technical assistant in the company's magnetic recording development laboratory specializing in magnetic heads until 1957, when, for a short while before joining Kelvin \& Hughes, he was attached to E.M.I. Studios.
A. N. Thomas, who, as reported in our May issue, recently retired from the B.B.C., has joined Pye Lid., as overseas consultant in the sales department of the Television Transmission Division.
F. Duerden, B.Sc.(Hons.), A.M.I.E.E., has been appointed manager of the electronics department of Bruce Peebles and Co. Lid., of Edinburgh, in succession to J. W. Haig Ferguson, M.A.(Cantab.), A.M.I.E.E., who has become divisional director. Mr. Duerden graduated at Manchester University and started his professional career in Marconi's research and development department. He then served as a radar officer in the R.A.F. and after the war joined Ferranti's, where he remained until joining Bruce Peebles as chief electronic engineer in 1956.

## BIRTHDAY HONOLRS

Among the recipients of honours in the Queen's Birthday List are several who took a leading part in the organization of the International Geophysical Year. They include Professor Sir David Brunt (K.B.E.) Professor W. J. G. Beynon (C.B.E.), and J. MacDowall (O.B.E.).

Leslie C. Gamage, chairman and managing director of the General Electric Company, receives a knighthood; A. V-M. Leslie Dalton-Morris, who became Air Officer Commanding on the formation of the R.A.F. Signals Command, is promoted to K.B.E.; and Group Captain G. R. Scott-Farnie, managing director of International Aeradio Ltd., becomes a C.B.E.

Among the new O.B.E.s are; Commander K. B. Best, R.N.(Retd.), director of communications at the Home Office; A. M. Beresford-Cooke, head of planning and construction, Engineering Department, I.T.A.; M. Davenport, principal, London Communications Electronic Security Agency; R. C. Harman, head of operations and maintenance, Engincering Department, I.T.A.; C. J. V. Lawson, engineer-in-chief, Cable \& Wireless; H. O'Neill, gencral secretary and treasurer, Radio Officers' Union; C. J. Strother, assistant to chief engineer, B.B.C.; and W. A. J. Thorn, deputy director (telecommunications), Ministry of Transport and Civil Aviation.

New M.B.E.s include: A. L. Budd, chief telecommunications superintendent, Air Ministry; I. Davies, lately communication officer, H.M. Embassy, Djakarta; S. F. Hodge, manager, International Aeradio Ltd., Sharjah; W. H. Mitchell, experimental officer, Royal Radar Establishment; G. W. R. Robinson, communications officer, H.M. Embassy, Washington; R. E. G. Trembath, International Aeradio's representative at Hargeisa, Somaliland; $\mathbf{N}$. Walker, senior executive engineer, Engineer-in-Chief's office, G.P.O.; and E. F. Woods, assistant to superintendent engineer, lines, B.B.C.

Recipients of the British Empire Mcdal include: A. L. Adams, chargehand, Marconi's W.T. Co.; and R. A. Grace, instrument maker, E.M.I. Electronics.

## OBITLARY

William Theodore Ditcham, A.M.I.E.E, who was associated with Capt. H. J. Round at Marconi's in the early development of direction finders during the first world war and with the experimental broadcasts from Chelmsford in 1920, has died in his 79th year. From 1925 to 1944 Mr . Ditcham was in charge of the development of Marconi's broadcasting transmitters, and was assistant engineer-in-chief when he retired in 1949 after 34 years with the company

Geoffrey Bennett, manager of the Liverpool factories of Automatic Telephone \& Electric Co. Ltd., died on April 27th aged 45. He started his career in telecommunications with the British Post Office and joined A.T.E. in 1945 after leaving the Royal Corps of Signals, in which he held the rank of Lieutenant Colonel.

Eric Frederick Kerridge, who was in charge of the technical publications department of Ferguson Radio Corporation, has died at the age of 45 . He joined the company in 1942

# News from the Industry 

Wharfedale Wireless Works, Ltd., the loudspeaker manufacturers of Idle, Bradford, Yorks, have been acquired by the Rank Organization. G. A. Briggs, the founder and managing director, who is well known also for his books and lecture-demonstrations, has agreed to remain in active management as have all the other executive directors.

Avo.-Changes are announced in the board of Avo, Ltd., which recently became a member of the Metal Industries Group. Sir Charles Westlake, chairman of Metal Industries, becomes chairman of the board of Avo with J. H. Rawlings, Avo's managing director, as deputy chairman. Other new directors are John Black, a director of M.I., and H. O. Houchen, managing director of Brookhirst Igranic, another M.I. subsidiary, recently formed to merge the interests of Brookhirst Switchgear, Ltd., and Igranic Electric Co. Mr. Rawlings is to be appointed to the board of Brookhirst Igranic.

The Plessey Company has concluded an agreement with Elettronica Metal Lux s.p.a., of Milan, Italy, providing for the manufacture of Metallux resistors in the U.K. Plessey, who for the past 18 months have been U.K. agents for these metal film resistors, will hold, in addition to sole manufacturing rights in this country, selling rights for both the U.K. and all Commonwealth countries.

Bendix Aviation Corporation, of America, has concluded an agreement with Cossor Radar \& Electronics, Ltd., whereby it obtains from Cossor know-how and patent licences for the manufacture of secondary radar airborne transponders.
P.A.M. Ltd., of Merrow, Guildford, manufacturers of Nera large-screen television equipment, have been absorbed by Tyer and Co., of Dalston, who are moving to the Guildford factory where they will continue the work previously undertaken by P.A.M. Both companies are subsidiaries of the Southern Areas Electric Corporation.

Anglo-French Collaboration.-In October, 1957, Marconi's W/T Co. and Compagnie Générale de T.S.F. agreed to collaborate in certain aspects of N.A.T.O. work. Their proposals for the provision and installation of equipment for all stations in the Early Warning radar chain have now been accepted and contracts totalling nearly $£ 7 \mathrm{M}$ are being placed by the governments concerned.

Ferranti, Ltd., have recenved an order from Bruce Peebles \& Co., of Edinburgh, for a $£ 60,000$ Pegasus digital computer. Initially, the computer, which will be installed next year, will be used for fundamental research and design calculations, and although priority will be given to Bruce Peebles' own work, the machine will be made available to other firms or organizations wishing to make use of it.
E.M.I. Electronics Ltd., are to supply a large EMIAC II computer to de Havilland Propellers Ltd., Hatfield, as an additional aid to research into guided missiles and other problems associated with high-speed flight. The installation will consist of twenty-two modules and cost £52,000.
Electrode Welding Co., Ltd., of Cobbold Road, London, N.W.10, has been appointed sole representative in the United Kingdom for electron gun mounts manufactured by Superior Electronics Corporation, of Clifton, New Jersey, U.S.A.

Decca Navigator, Mk. 10 , receiver has been reengineered to the ARINC (Aeronautical Radio Inc.) specification to fit American aircraft racking. The new receiver will be known as the Mk. 10A (Type 900).

Armstrong Whitworth Aircraft Ltd., of Coventry, have taken over the Technical Developments Division of Gloster Aircraft Company. Both are members of Hawker Siddeley Aviation Limited. The merger brings together two departments producing a complementary range of equipment with a wide application in the fields of instrumentation, automation and radio communication as well as aircraft and guided missile systems as a whole. E. W. Absolon, who has been chief engineer at T.D.D., has been appointed manager of the new division and A. E. Martin, who has been in charge of A.W.A. Commercial Electronics Department, moves to Gloucester as deputy divisional manager.

Standard Telephones and Cables have received an order from Cable $\&$ Wireless for the supply of 92 submerged two-way repeaters and eleven equalizers for the Scotland-Newfoundland section of the proposed Commonwealth round-the-world telephone cable. The repeaters, each containing duplicate three-valve amplifiers, will be inserted in the cable at intervals of about 23 nautical miles. The equalizers, for correcting inequalities of signal strength at different frequencies, will be inserted in the cable at intervals of some 200 miles. The order is valued at about $£ 1.8 \mathrm{M}$.

## COMPANY REPORTS

Ekco.-The Ekco group of companies, which includes E. K. Cole, Ltd., Ferranti Radio and Television, Dynatron, and Egen Electric, had a net profit after taxation of $£ 459,225$ in the year ended in March, an increase of $£ 142,474$ on the previous year.

Thorn Electrical Industries.-Group trading profits for the year ended last March amounted to $£ 2,953,536$. After deducting all charges, including taxation at $£ 927,257$, the net profit was $£ 979,371$ compared with $£ 681,832$ in the previous year.
Vickers, Ltd.-Reference is made in the annual review of Vickers to the Hollerith-Powers Samas merger in which the company now has a holding of 38 per cent of the equity in International Computers and Tabulators, Ltd., the new title of the merged companies.
Ferranti Ltd.-Consolidated profit for the year to March 31st was $£ 2,419,865$ compared with $£ 1,252,971$ for the previous year. After provision for tax the net profit was $£ 1,104,572$ against $£ 575,971$ last year.

Rediffusion, Ltd., which holds a $37 \frac{1}{2} \%$ interest in the television programme contractors, Associated-Rediffusion, reports a group trading profit of $£ 4.29 \mathrm{M}$ for 1958/59 which was $£ 280,000$ more than in the previous year. The group also includes Redifon, Ltd., and Rediweld, Ltd.
Elliott-Automation.-The accounts for the first full financial year of the Filliott-Automation Group show a net profit after taxation of $£ 458,628$. The Group was formed in August, 1957, with the merging of Elliott-Brothers (London), Ltd. and Associated Automation, Lid.

Garrard.-Profit for the year ended in January was £545,590 of which $£ 264,462$ will be absorbed by taxation.

International Aeradio, Ltd., in which 17 international airline operators are shareholders, had a gross group turnover during 1958 of just over $£ 2 \mathrm{M}$, an increase of $£ 200,000$ on the previous year.

Ever Ready Company (Great Britain), Ltd., announce Ever Ready Company (Grear Britain), Lid., $£ 1 M$ for taxation) of $£ 1,262,856$ for the year ended in February. This was an increase of $£ 342,757$ on the previous year.

## OVERSEAS TRADE

Radio link between Newfoundland and the Canadian mainland, used initially for television during the Queen's recent Canadian tour, includes the world's longest microwave over-water path. Standard Telephones and Cables' s.h.f. automatic space diversity equipment is used for the 70 -mile relay across the Cabot Straits in order to combat the difficult transmission conditions caused by the rise and fall of tidal waters. In all, twenty-three S.T.C. relay stations are used to cover the 524 miles between St. Johns, Newfoundland, and Sydney, Nova Scotia. The link provides for 600 twoway telephone circuits in addition to a television link in either direction.

Facsimile equipment, valued at over $£ 85,000$ and supplied by Muirhead, has been installed by a Japanese newspaper publisher. The equipment is used to transmit by radio from Tokyo complete pages of the newspaper which when received at Sapporo, on the island of Hokkaido, 500 miles away, are used for off-set printing, so that the paper is available almost simultaneously in both places-the actual delay is said to be 75 minutes.
Autosonic inspection equipment to the value of $£ 10,000$ has been ordered from Kelvin Hughes for the Chomutov steel works in Czechoslovakia. The equipment will facilitate the automatic scanning of rolled mild steel bars of up to 7.9 in diameter and will mark and reject any material containing internal defects in excess of a predetermined degree.
Sound and vision transmitters, combining filters and programme input and ancillary equipment for five new Band III television stations under construction in Sweden are to be supplied by Marconi's. One of the stations, at Borlänge, will have two sets of transmitters operating in parallel, and will have a vision e.r.p. of 60 kW . The remaining four stations will each have single transmitters feeding into a directional aerial. These will have different gain factors, so that the respective e.r.p.s will range from 10 kW to 60 kW .

Communication Receivers.-A contract for the supply of 350 radio-telephone receivers to the Canadian Department of Transport has been secured by Plessey International Ltd. The receivers, which will be used in aeronautical and other services, are designated PR51c and form part of the Plessey PR51 range of singlechannel h.f. receivers.
Weather Radar.-Two international Swiss airports, near Geneva and Zurich, are to be equipped with Decca weather radar. Both installations will be on high ground some distance from the airfields, with radio links to relay the radar information to the airfield meteorological offices.

Closed circuit television equipment is being supplied by E.M.I. Electronics for installation in a large gold mine in Ghana. Three cameras, mounted at vantage points to scan the working area and linked to receivers in the offices of the security officer, are being installed as an added security measure against pilfering.

Airborne ILS/VOR equipment, for installation in the Soviet Aeroflot TU104 jets used on the MoscowLondon route, has been ordered by the Russian Purchasing Authority from Standard Telephones and Cables.
I.L.S.-Two Pye instrument landing systems are to be installed at Moscow airport. The contract is worth about $£ 100,000$.

Radar for the double-ended ferries on the ManhattanStaten Island service, New York, is to be supplied by Decca. This order, valued at over $\$ 106,000$, is for twenty-three sets and brings the total to 37 supplied by Decca for the New York Ferry Services.

Communications equipment valued at $£ 73,000$ has been supplied by Racal Engineering Ltd., for the Canadian Government. The consignment includes over 100 RA. 17 communication receivers and ancillary equipment.

Iran.-The representation in Iran of a British manufacturer of sound radio and television receivers is sought by Sherkat Nesbi Bafandegi Baradaran Jurabchi, near Saray Haj Hassan Bazar, Teheran. They ask for a descriptive catalogue and wholesale export prices.

Canada.-Ray Hamerton Lid., of 317 Fort Street, Winnipeg 1, Manitoba, wishes to take up the agency for British-made loudspeakers, amplifiers and turntables which are not already represented in the province.

## NEW ADDRESSES

Kelvin House, Wembley, Middx., is the new headquarters of the Aviation, Marine and Industrial Divisions of S. Smith and Sons, which includes KelvinHughes and Smith's Aircraft Instruments.

Technograph.-The new London office of Technograph Printed Circuits, Ltd., and Technograph Electronic Products, Ltd., is at Eros House, 29-31, Regent Street, S.W.1. (Tel.: Regent 5273.)

Siemens Edison Swan's London district office has been transferred to Crown House, Aldwych, W.C. 2 (Tel.: Temple Bar 8040). The stores will remain at Tyssen Street, Dalston, E.8.

Telerection Limited, aerial manufacturers, have opened a new factory in Weymouth and closed their Cheltenham plant. The address is Antenna Works, Lynch Lane, Weymouth (Tel.: Weymouth 2140).

Decca Radio and Television Ltd., have moved their offices and factory from Brixton Road, London, S.W.9, to Ingate Place, Queenstown Road, London, S.W.8. (Tel.: Macaulay'6677.) The spares and service department is still at Brixton Road (Tel.: Reliance 6011).

CQ Audio, Ltd., manufacturers of sound reproducing equipment, whose premises in Sarnesfield Road, Enfield, were severely damaged by fire some months ago, have taken possession of a new factory at Bush Fair, Tye Green, Harlow, Essex (Tel.: Harlow 24566).


Headquarters of A.E.I. Electronics Apparatus Division (incorborating BTH and M-V) at New Parks, Leicester, opened by Rt. Hon. Aubrey Jones, M.P., Minister of Supply, at the end of June. With a total floor space of $180,000 \mathrm{sq} \mathrm{ft}$, the new building comprising factory (right), offices and laboratories ( $T$-shaped block, left and rear-centre) and canteen (front centre).

# Magnetic Tape Heads 

Factors Influencing Their Design and Construction

By C. ROSS, Grad. Brit. I.R.E.

IAGNETIC recording has a wide variety of applications, and the magnetic head can be considered the "heart" of the machine, for its performance governs to a high degree the capabilities of the recording machine. The advent of ferrites has made high-frequency recording possible, and improved the performance of the audio range recorders also. In general, the highest frequency that it is desired to reproduce governs the speed of the magnetic tape across the magnetic heads. Tape speeds for instance, of the order of $0.25 \mathrm{in} / \mathrm{sec}$ may be used for very low frequency recording or conversely, speeds of 200 in $/ \mathrm{sec}$ and above are used for high-frequency work. For high quality sound recording, which this article is based upon, speeds of 7.5 to $30 \mathrm{in} / \mathrm{sec}$ are in common use. The replay head provides a limitation to the maximum number of cycles of magnetic signal per inch of recording media which can be resolved satisfactorily.

There are three main factors to be considered when dealing with tape heads and associated circuits. They are frequency response, distortion and signal to noise ratio. Good quality magnetic heads are now commercially available and with suitable circuits will perform satisfactorily up to a frequency limit of $1800-2000$ cycles per inch per second.

Almost without exception in the high-quality professional field, the recording machine has three heads mounted on an easily detachable rigid plate. The tape is first demagnetized by the crase head. Saturation of the tape takes place at its gap, which is large in relation to the record and replay gaps, and the tape is taken through many cycles of magnetization which gradually decrease due to the motion of the tape past the head. The record head has two magnetizing components, one the signal and the other consisting of a high-frequency "bias" to reduce distortion. The signal produced on the tape is then reproduced by the replay head and fed into suitable frequency-corrected amplifier stages. This process is relatively well known.

The various types of magnetic head will now be discussed in detail, and the importance of various mechanical relationships illustrated; the three types are assumed to take the general form shown in Fig. 1.
Erase Heads. - The impedance of the erase head is chosen so that the voltage developed across it is not excessive when operating normally. The high frequency current required is usually derived from a tuned power amplifier stage driven by an oscillator of low distortion. The frequency of the oscillator is often $7-10$ times the highest audio frequency which is to be recorded, the danger being heterodyne interference between a harmonic of the signal and the oscillator frequency. Harmonic distortion of the erase current (and bias current) waveforms should be kept as low as possible. Distortion causes noise to be kept on the tape; this is mainly due to the presence
of even-order harmonics producing an unsymmetrical waveshape, hence leaving the tape polarized to a small extent. This noise is very pronounced when the tape has been erased using a plain permanent magnet in place of h.f. erasure. A figure of less than $0.5 \%$ total harmonic distortion is usually required in practice to give a clean, low noise tape background. Core losses can be minimized by using a ferrite material in conjunction with a non-conducting gap spacer. In practice it has been found that although a better flux distribution about the working gap is possible with a conducting gap spacer (phosphor-bronze, etc.), the heat generated due to eddy currents is excessive in "full track" erase heads and the insulator type is superior. The metal spacer tends to "throw out" the flux, whilst the poorer flux distribution about the non-conducting gap spacer is approximately balanced by the lower losses, and the heat generated is negligible. The gap length of the erase head is not critical, and a


Fig. 1. Generalized sketch of a magnetic head with relevant dimensions
length of 0.012 in to 0.020 in is satisfactory for tape velocities of 7.5 and $15 \mathrm{in} / \mathrm{sec}$.
Record Heads.- The basic requirements of a record head are a low reluctance magnetic circuit with small hysteresis and eddy-current losses, and a well-defined straight-edged front gap, its length being relatively unimportant compared with the replay head front gap. Ferrite material is inherently granular and unsuitable for the gap portion of the record head, although successful heads have been made by using pole shoes of high-permeability metal to form a clean straight gap.

The C.C.I.R. recording standard is widely adopted now. This means that the tape has been recorded to a definite induction/frequency characteristic. Taking the characteristic adopted for the tape speed of $7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$ as equivalent to that of a circuit with a time constant of 100 microseconds and providing that the replay amplifier has the


Fig. 2. Circuit with response equivalent to the C.C.I.R. recording standard
inverse of this response of 100 microseconds, the output would be constant over the band of frequencies recorded on the tape. This is only true if the replay head has no losses whatsoever and is in fact "ideal".
The response is conveniently described in microseconds, for it is the response of a simple R-C combination shown in Fig. 2. $\mathrm{V}_{\text {out }}$ represents the voltage across an "ideal" replay head winding when a tape is reproduced having the C.C.I.R. induction/ frequency characteristic of 100 microseconds.

To produce a recording which has the required C.C.I.R. characteristic, a certain amount of high frequency pre-emphasis or "equalization" is incorporated in the recording amplifier to overcome losses in the tape magnetizing process and the record head. For a tape velocity of $7.5 \mathrm{in} / \mathrm{sec}$ approxmately +11 dB of equalization is required at $10 \mathrm{kc} / \mathrm{s}$


Fig. 3. Typical recording pre-emphasis circuit
(reference $1 \mathrm{kc} / \mathrm{s}=0$ ) to produce a recording which has the C.C.I.R. characteristic, given a good-quality record head. A typical current versus frequency curve is shown in Fig. 3, the record head working at peak optimum bias for a signal frequency of $1 \mathrm{kc} / \mathrm{s}$.

The efficiency of a record head largely depends on the front-to-back depth ( F in Fig. 1) of the working gap and the type of tape used, but it is difficult to calculate accurately because it depends upon the leakage and fringing across the gap to some extent. In general, the back-tofront depth is made as small as possible consistent with reasonable working life of the head. This also applies to erase and replay heads.
The optimum bias required is governed by three major factors: high-frequency losses in the head itself, the nature of the tape coating and the signal frequency. Fig. 4 shows how the recorded signal varies when the bias current is altered from a low value to a high value and the dotted line indicates the recorded signal harmonic distortion (for a given signal level). This peak in the tape signal recorded is shown occurring at a bias current of 8 mA , but this condition exists only at a certain signal frequency, i.e. $1 \mathrm{kc} / \mathrm{s}$. Inspection of the graph in Fig. 5 will show how this peak varies with signal frequency. Therefore
it can be seen that the bias current governs to a large degree the performance of the record head. Operation of the record head with insufficient bias current can cause distortion and an accentuated high-frequency response. However, it has been found that it is advantageous to over-bias the record head so that the tape signal at $1 \mathrm{kc} / \mathrm{s}$ drops by 2 dB (from the peak value obtained using 8 mA bias current as shown in Fig. 4). This ensures that the effects of any discontinuities in the tape coating, contact variation between head and tape, etc., are kept to a minimum. This necessarily affects the h.f. pre-emphasis required by the record head to produce a recording conforming to the C.C.I.R. specification, assuming the head was originally operated at peak optimum bias. The extra pre-emphasis required can be obtained by adjustment of the record amplifier characteristic, which is made variable in professional machines. Distortion of the signal on the tape can be caused also by an excessive magnetization level. The maximum signal level allowed in practice is one which produces $2 \%$ to $3 \%$ total harmonic content. The main component is usually the third harmonic due to the tape coating magnetization characteristic. Some types of tape can accept a higher level of magnetization than others for a given distortion, and if the signal-to-noise ratio of the system is to be as high as possible, the tape which can accept the maximum magnetization level for this given distortion level should be chosen.
Replay Heads.- The losses in a replay head can be split into two groups: frequency-dependent losses and wavelength-dependent losses.
Other factors to be considered are sensitivity, e.g. the voltage output should be as high as possible from a given signal level on the tape, and the voltage waveform an exact replica of the magnetic signal on the tape. There is a limitation to the number of turns of wire wound on the magnetic core, for highfrequency resonance with the self-capacitance of the winding is undesirable. High-frequency resonance is an extreme condition usually, although transformer coupling of a replay head to the input of the amplifier requires careful design of the transformer to avoid this condition.
The front-to-back depth F of the gap directly affects the sensitivity, because the shunting effect


Fig. 4. Effect of bias current on the level and distortion of the recorded signal


Fig. 5. Variation of optimum bias with signal frequency
is greater when the gap depth is large. This dimension is a compromise, the back-to-front depth being made as small as possible consistent with an allowance made for head wear during service. A figure of between 0.007 in and 0.010 in is commonly used in practice.
Effect of Front-to-back Depth on Sensitivity. A simplified equivalent circuit of a typical magnetic head is shown in Fig. 6.

Referring to Fig. 6.
$\mathrm{E}=$ magnetomotive force.
$\mathrm{R}_{1}=$ reluctance of tape and tape contact with head.
$\mathrm{R}_{2}=$ front gap reluctance.
$\mathrm{R}_{3}=$ core plus rear gap reluctance.
$i=$ flux entering poles from tape.
I =flux through core (and hence coil).
$\mu=$ mean permeability.
$l=$ mean length of magnetic path.

$$
\begin{aligned}
\text { Now } i & =\frac{\mathrm{V}}{\mathrm{R}_{1}+\overline{\mathrm{R}_{2}} \mathrm{R}_{3}^{-}} \\
\therefore \mathrm{I} & =\frac{\mathrm{V}}{\mathrm{R}_{1}+\overline{\mathrm{R}_{3}} \cdot \overline{\mathrm{R}_{3}}} \cdot \frac{\mathrm{R}_{2} \mathrm{R}_{3}}{\mathrm{R}_{2}+\mathrm{R}_{3}} \cdot \overline{\mathrm{R}_{3}} \\
& \left.=\frac{\mathrm{R}_{3}}{\mathrm{R}_{1}\left(\mathrm{R}_{2}+\mathrm{R}_{2}\right.}\right)+\overline{\mathrm{R}_{2} \mathrm{R}_{3}}
\end{aligned}
$$

From Fig. $1, \mathrm{R}_{2} \propto \frac{\mathrm{dF}}{\mathrm{D} \times \overline{\mathrm{F}}}$

$$
\begin{aligned}
& \quad \mathrm{R}_{3} \times \frac{\mathrm{dR}}{\mathrm{D} \times \mathrm{R}}+\mathrm{D} \times \frac{1}{\mathrm{R} \times \mu}=\frac{\mathrm{dR}}{\mathrm{D} \times \mathrm{R}} \\
& \left(\text { if } \frac{1}{\mathrm{D} \times \mathrm{R} \times \mu} \leqslant \frac{\mathrm{dR}}{\mathrm{~d} \times \mathrm{R}}\right)
\end{aligned}
$$

Solving for I using two values for $\mathrm{R}_{2}$, the change in output voltage of the winding can be found, due to the front-to-back depth being altered, say, from a small to a large dimension. The object is to make the magnetic flux mainly traverse the magnetic circuit around which the coils are placed, rather than taking the short-cut presented by the front gap reluctance $\mathrm{R}_{2}$.


Fig. 6. Simplified analogue circuit of a typical magnetic head


Fig. 7. Method of calculating gap loss
Effect of Gap Length $d F$ on Sensitivity. This can be catculated in a similar manner to the previous example, thus using two values for $\mathrm{R}_{2}$ again but incorporating different values for dF , the result is an increase of output when dF is changed from a small to a large dimension $\left(R_{2} \frac{d F}{\bar{D} \times \bar{F}}\right)$.

Summarizing: Output $\alpha \frac{1}{\mathrm{~F}} \times \mathrm{dF}$.
Frequency Response-The gap length dF is the most important dimension. The gap loss can be calculated by simple integration. From Fig. 7, dF represents the effective magnetic gap which is usually $20 \%$ greater than the actual mechanical gap, due to "end effect," etc. The gap loss at


Fig. 8. Output from a good quality reply head with theoretical response from a C.C.I.R. recording ot $7.5 \mathrm{in} / \mathrm{sec}$
any given wavelength $\lambda$ may be represented by the average value of the sinusoidal signal illustrated, between the limits set by the length of the effective magnetic gap dF. It can be seen that when this gap equals the wavelength $\lambda$ the output will be zero, for the poles will have a similar polarity at any point along the curve. By taking the average value of the curve $f(\omega t)$ between the points $-\mathrm{dF} / 2$ to $+\mathrm{dF} / 2$ in terms of $2 \pi$ a general expression is obtained. The reference axis " O " is placed where $f(\omega t)$ is a maximum, therefore $f(\omega t)$ becomes cos $\omega \mathrm{t}$. The average value is thus:

$$
\begin{aligned}
& \frac{\lambda}{2 \pi \mathrm{dF}} \quad \int_{-\pi \mathrm{dF} / \lambda}^{+\pi \mathrm{dF} / \lambda} \cos \omega \mathrm{t} \mathrm{~d}(\omega \mathrm{t}) \\
= & \frac{\lambda}{2 \pi \mathrm{dF}}[\sin \omega \mathrm{t}]_{-\pi \mathrm{dF} / \lambda}^{-\pi \mathrm{dF} / \lambda} \\
= & \frac{\sin (\pi \mathrm{dF} / \lambda)}{\pi \mathrm{dF} / \lambda} \\
\therefore & \text { Gap loss }=20 \log _{10} \frac{\sin \pi \mathrm{dF} / \lambda}{\pi \mathrm{dF} / \lambda} \mathrm{dB}
\end{aligned}
$$

The output of a good quality replay head from


Fig. 9. Screening and poles with short tape contact affect the low-frequency response of replay heads.


Fig. 10. Typical response irregularity at low frequencies.
a C.C.I.R. recording at $7.5 \mathrm{in} / \mathrm{sec}$ is indicated in Fig. 8, whilst the theoretical output is shown by the dotted line, the difference between the two curves represent the eddy and hysteresis losses, etc., of the particular head.
Effect of Screening Can and Pole Shape upon Low Frequency Response. The replay head is usually screened magnetically against hum pick-up from nearby motors, etc., in the machine, and also erase and bias pick-up from the erase and record heads, assuming in the latter case that the signal is being monitored by the replay head.

When the screening can is in close proximity to the tape and pole-pieces it can act as a secondary pole-piece and has the effect of increasing or decreasing the field from the tape according to the length of the tape embraced, and the signal wavelength.

Fig. 11. Screening-can aperture shaped to reduce low-frequency response irregularities.


Any sharp discontinuity in the profile of the pole-pieces adjacent to the tape surface can also produce similar effects. Generally, these undesirable conditions can be reduced to negligible proportions by making any such discontinuity at least $5 \lambda$ (max.) away from the gap, where $\lambda$ (max.) is the longest wavelength that it is desired to reproduce. Typical examples of replay head are shown in Fig. 9 whilst the effect upon low frequency equalized replay response is indicated in Fig. 10. To completely overcome this type of poor low frequency response it is advisable therefore to make the pole-pieces of the replay head a smooth curve up to, and away from, the tape surface. Where a screening can is used, the edges of the aperture through which the pole-pieces protrude should be far enough away from the tape to prevent its influence upon the magnetic field of the tape, alternatively an angled aperture may be used (Fig. 11).
Alignment of Replay Head Gap to Recorded Signal Azimuth. Correct azimuth alignment is very important where good overall high-frequency performance is required. This is obtained by rotating the replay head about an axis, preferably located at the mid point of the gap width, normal to the tape surface. This mid-point location ensures that the lateral movement of the head during adjustment is kept to a minimum. The replay head is rotated until its gap is exactly parallel with the azimuth of the recorded signal on the standard tape. Adjustment is made at the high-frequency end of the audio-frequency band covered by the recording machine, i.e. where the wavelength of the signal

Fig. 12. Calculation of loss due to vertical misalignment of gap.

is approximately twice the length of the effective magnetic gap of the replay head. For example, alignment procedure can be outlined as follows. The machine (assuming a single-channel type with three heads), is set to "replay," loaded with the standard C.C.I.R. tape for the relevant tape velocity. The replay head is adjusted to give the maximum peak in output from the high-frequency azimuth band on the standard tape. Then with the standard tape removed and replaced with "clean" tape, the machine is switched to record and a tone of similar frequency recorded. The azimuth of the record head is then adjusted to give the maximum peak output from the replay head which is monitoring this signal. On a machine with two heads, e.g. erase and record/replay the latter test does not apply, but correct alignment is important where pre-recorded tapes are to be used and interchange of tapes from machine to machine is required.

The effect of azimuth misalignment can be calculated in a similar manner to the gap loss, given the angle of tilt away from correct azimuth, the width of the replay track and the signal wavelength. Referring to Fig. 12, the loss is given by:-

$$
\frac{\lambda}{2 \pi W \tan \alpha} \int_{\frac{-\pi W \tan \alpha}{\lambda}}^{\frac{-\pi}{\lambda} \tan \alpha} \cos \omega \mathrm{t} . \mathrm{d}(\omega \mathrm{t})
$$

$$
=\frac{\lambda}{2 \pi \mathrm{~W} \tan \alpha}[\sin \omega \mathrm{t}] \begin{aligned}
& +\pi \mathrm{W} \tan \alpha \\
& \\
& \frac{-\pi \mathrm{W}}{\lambda} \tan \alpha \\
& \lambda
\end{aligned}
$$

$$
=\frac{\sin \pi W \tan \alpha}{\frac{\lambda}{\frac{\pi W}{\lambda} \tan \alpha}}
$$

therefore loss in $\mathrm{dB}=20 \log _{11} \frac{\sin }{\pi} \frac{\pi W \tan \alpha / \lambda}{\tan \dot{\alpha}}$ $\pi W \tan \dot{\alpha}$

Fig. 13. Variation of output with deviation of gap from the vertical. Solid cure "ideal", dotted curve typical measured response where the gap is not straight and varies in length across the track.

minutes of arc

It can be said that any misalignment of this nature has the effect of increasing the replay head gap to the amount $W \tan \alpha$ which of course is quite an additional effect to the actual gap itself, previously calculated.

For the machine running at $7.5 \mathrm{in} / \mathrm{sec}$, a misalignment of only two minutes of arc at a recorded frequency of $10 \mathrm{kc} / \mathrm{s}$ will cause a reduction of output of 0.6 db , assuming a full width recording on standard $\frac{1}{4}$ in tape.

Using the above formula to display graphically the relation between head rotation and replay output for a given wavelength and track width, it can be seen from Fig. 13 that a number of peaks in output can be obtained, of differing amplitudes, the main peak accurring at the true azimuth. The


Fig. 14. "Dig-out" wear of the gap spacer.
solid line represents the ideal case, where the gap is perfect in every respect. In practice, however, various curve shapes are obtained, depending upon gap straightness, and variations in the gap length along the track width, etc. The dotted curve indicates a typical case in practice. In some cases, one of the secondary peaks may be quite large in amplitude compared with those illustrated in the ideal case, and may be mistaken for the true azimuth peak. Providing the magnetic head is rotated over a fair range, from about -2 deg to +2 deg (taking true azimuth to be 0 deg ), selection of the major peak is not difficult.
Effects of Wear. - The performance of a magnetic head which is essentially in contact during its working life, for a.f. application, is subject to gradual change. The relationship of the various mechanical surfaces, gaps, etc., to performance have been discussed, and the back-to-front depth F is the main factor to be considered. This dimension gradually decreases with wear, until it may become zero, which is the end of the working life of the head. It was found that this dimension was inversely proportional to the sensitivity of the head, e.g., lower bias and signal currents required for a given tape level for a record head and higher output voltage from a replay head for a given tape induction (and frequency in both cases). Therefore, a magnetic head has its peak performance and efficiency just before the end of its useful life.
Spurious Effects.-Soft gap spacer material can cause a falling off in high-frequency response and, in some cases, azimuth change. The characteristic " dig-out " wear is illustrated in Fig. 14 representing a much enlarged view looking along the gap. Copper, aluminium and similar materials used as gap spacer shim exhibit this effect, for they are soft compared with the laminated pole-pieces. Beryllium copper, phosphor-bronze, etc., have been found suitable.

The pole-piece material governs the rate of wear to a large extent, and, in general, three types of alloy are in common use: " Radiometal," " Mumetal" and "Supermumetal." "Radiometal" has the greatest resistance to wear, for it is mechanically harder than the latter two alloys. It is also magnetically "harder," which reduces the sensitivity of the head to a small extent (compared with using Mumetal or "Supermumetal"), depending on the reluctances of the air gaps in the magnetic circuit. Pressure pads in many cases cause uneven head wear, and shorten the life of the head, and should be unnecessary for tape work providing the tensions are correct.
Poor finishing of the working gap face causing burring over of the pole-piece material which may bridge the non-magnetic gap spacer can cause rapid changes of response during the first few hours of operation.
Some types of magnetic head have a working face dimension which is greater than the tape width, and after some hundreds of hours use, a shallow channel of tape width is worn therein, which may cause amplitude flutter of high frequencies and in some cases frequency flutter or wow. Regrinding during the working life of the head is then desirable. At all events, it can be recommended that any new magnetic head should be "run-in" before tests are made, by passing. a few thousand feet of tape across them.
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# FERROELECTRICS 

## 2.-DOMAINS: AND SOME APPLICATIONS OF CERAMICS

By J. C. BURFOOT,* Ph.D.

THE first article described the spontaneous polarisation $P$ of a single domain of a ferroelectric, and its hysteresis loop, and showed that although ordinary ferromagnetism is due to permanent dipoles, in ferroelectricity induced dipoles can also be involved. The ferroelectricity disappears above a transition temperature $\mathrm{T}_{0}$, and near that temperature, the dielectric constant $\epsilon$ and some of the piezoelectric and elastic coefficients show anomalously large values which can be related to the polarisability $\alpha$. The dipoles and the large polarisabilities occur for different reasons in different materials; we cannot generalise.
Materials.- The earliest material known to be ferroelectric (1921) was the tartrate named Rochelle salt $\left(\mathrm{NaKC}_{4} \mathrm{H}_{4} \mathrm{O}_{6} .4 \mathrm{H}_{2} \mathrm{O}\right)$; potassium dihydrogen phosphate $\left(\mathrm{KH}_{2} \mathrm{PO}_{4}\right)$ followed in 1935, barium titanate $\left(\mathrm{BaTiO}_{3}\right)$ in 1944, and guanidine aluminium sulphate hexahydrate, familiarly known from its initial letters as gash, in 1955, and some alums. It will suffice to. study the first three and allied chemicals, but ferroelectricity has also been found in ammonium

[^3]sulphate and fluoberyllate, thiourea, colemanite, glycine sulphate, and others. The $\mathrm{T}_{0}$ values range from $-260^{\circ} \mathrm{C}$ to about $600^{\circ} \mathrm{C}$. Some values are given in Table I. Other members of some of these groups are anti-ferroelectric; that is, their individual dipoles are arranged in ways which produce zero overall polarisation, though dielectric anomalies remain.

In applications of ferroelectrics it is inconvenient to have to keep the temperature T such as to give particular values of the properties being used. So it is important to be able to select a material with which room temperature (or working temperature) is suitable. Similarly the values available for the given property should cover as wide a range as possible, and if the anomalies can be made either very peaky (against T) or flat, as required, there will be more applications. As one example of such versatility, here in single domain properties, consider replacing some of the barium in barium titanate crystals by lead. It happens that in this case all compositions of this solid solution are possible, and all are ferroelectric, and $\mathrm{T}_{0}$ increases continuously from $120^{\circ} \mathrm{C}$ to
$490^{\circ} \mathrm{C}$ as the percentage of lead increases. Iron impurity deliberately introduced into barium titanate lowers $\mathrm{T}_{0} ; 5 \%$ of iron lowers it $100^{\circ} \mathrm{C}$; the resistivity is also altered. There are other possibilities when we consider polycrystalline forms.

The crystal structure of barium titanate and lead titanate ( $\mathrm{PbTiO}_{3}$ ) is shown in Fig. 7(a). Above $\mathrm{T}_{0}$, the lattice cell is cubic, $4 \AA$ in size ( 254 million $\AA$ $=$ one inch), and the titanium ion is at the centre. Below $\mathrm{T}_{0}$ it is displaced by an amount $x$, equal to $7 \%$ of the cell-side, relative to the octahedron of oxygen ions (in $\mathrm{PbTiO}_{3}$ ); the A ions are displaced $11 \%$ in the same direction. In barium titanate, the corresponding figures are 30, and $1 \frac{1}{2} \%$, but in this case, the octahedron is also distorted, the ions marked I being displaced $1 \%$ in the opposite direction. It would not be correct to assume a dipole strength made up of terms like ( 4 e times $x$ ) for the titanium for two reasons: (i) the crystal bonding is not all " ionic," so the effective charge on the titanium is less than 4 e , (ii) each off-centred ion is in a local field which must distort the electron cloud surrounding it, because of electronic polarisability, so that each ion becomes itself a dipole at its displaced position, and of unknown strength. Notice that the extent of off-centring quoted is that which is observed; it gives no indication whether or not it is induced (by co-operative effects). Also below $\mathrm{T}_{0}$, because of the spontaneous polarisation $P$ now developed, the electrostriction discussed in the previous article in

TABLE I

| Material | $\left\lvert\,\left(\begin{array}{c} \left.\mathbf{T}_{\mathbf{0}}^{\mathbf{C}}\right) \end{array}\right.\right.$ | $\begin{gathered} \mathbf{M a x} \\ \mathbf{P} \\ (\mu \\ \mathbf{c o u l}^{\mathbf{c m}^{-2}} \end{gathered}$ | Material | $\begin{gathered} \mathbf{T}_{0} \\ \left({ }^{\circ} \mathrm{C}\right) \end{gathered}$ | Max. $P$ <br> ( $\mu$ coul. $\mathbf{c m}^{-2}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{BaTiO}_{3}$ <br> $\mathrm{KNbO}_{3}$ <br> $\mathrm{PbTiO}_{3}$ <br> $\mathrm{KTaO}_{3}$ <br> $\mathrm{NaTaO}_{3}$ <br> $\mathrm{L}_{\mathrm{LiNbO}}^{3}$ <br> $\mathrm{CdNb}_{2} \mathrm{O}_{7}$ <br> $\mathrm{PbNb}_{2} \mathrm{O}_{6}$ | $\begin{array}{r} 120 \\ 415 \\ 490 \\ -260 \\ 475 \\ >450 \\ >450 \\ -88 \\ 570 \end{array}$ | $\begin{array}{r} 26 \\ 30 \\ -100 ? \\ -10 \\ \\ -10 ? \end{array}$ | $\mathrm{KH}_{3} \mathrm{PO}_{4}$ <br> $\mathrm{KH}_{2} \mathrm{AsO}_{4}$ <br> $\mathrm{FbH}_{2} \mathrm{PO}_{4}$ <br> $\mathrm{RbH}_{2} \mathrm{AsO}_{4}$ <br> $\mathrm{CsH}_{2} \mathrm{PO}_{4}$ <br> $\mathrm{CsH}_{2} \mathrm{AsO}_{4}$ | $\begin{array}{r} -151 \\ -177 \\ 127 \\ 162 \\ -1114 \\ -1130 \\ -13 \end{array}$ | $\begin{aligned} & 4.8 \\ & 5 \\ & 5.7 \end{aligned}$ |
|  |  |  | Gash <br> Methyl <br> ammonium <br> aluminum <br> alum | $\begin{array}{r}  \\ -\quad 96 \\ \hline \end{array}$ | $\begin{gathered} 0.6 \mathrm{at} \\ -180^{\circ} \mathrm{C} \\ \\ 0.6 \mathrm{at} \\ -107^{\circ} \mathrm{C} \end{gathered}$ |
| Rochelle salt Lithium ammon- |  | 0.25 | Ammonium sulphate Ammonium fluoberyllate | -49 97 | $\begin{gathered} 0.25 \mathrm{at} \\ -58^{\circ} \mathrm{C} \\ 0.19 \mathrm{at} \\ -110^{\circ} \mathrm{C} \end{gathered}$ |
| tartrate <br> Lithium <br> thallium | -170 |  | Thiourea | -105 | $\begin{gathered} 3.1 \mathrm{at} \\ -110^{\circ} \mathrm{C} \end{gathered}$ |
| tartrate | -260 | 0.14 | Colemanite <br> Glycine sulphate Glycine selenate | -2 47 22 | 0.5 at $-38^{\circ} \mathrm{C}$ <br> 2.2 at |

Rochelle salt is unusual in that it also has a lower transition temperature, below which the ferroelectricity disappears. This will not be discussed in these articles. Gash decomposes betore reaching $T_{\text {. }}$.
relation to Fig. 6(b) causes a spontaneous strain $\mathrm{S} \propto \mathrm{P}^{2}$; actually the cell becomes about $1 \%$ elongated in the direction of P , with very little change of volume. This elongation is many orders larger than similar effects in ferromagnetics.


Fig. 7. (a) Perovskite cell $A B O_{3}$. $A=B a^{++}$or $\mathrm{Pb}^{++}$etc., $B=\dot{T}_{i}+{ }_{1}+$ etc., $O^{--}$. (b) Centres of $\mathrm{PO}_{4}$ groups in $\mathrm{KH}_{2} \mathrm{FO}_{4}$, projected on horizontal plane.

In Rochelle salt, the unit cell contains 4 each of the atoms given in the chemical formula, and is a very complicated structure. In $\mathrm{KH}_{2} \mathrm{PO}_{4}$, the cell containing 8 each of the formulae is about $10 \AA, 10 \AA$, $7 \AA$. The K atoms and $\mathrm{PO}_{4}$ groups are centred $31 /$ vertically apart, if we describe the $7 \AA$ cell dimension (the ferroelectric axis) as "vertical." But those PO, groups whose projections in Fig. 7(b) are neighbours are only separated vertically by half of $3 \frac{1}{2} \mathrm{~A}$, so that the top of one $\mathrm{PO}_{4}$ group is level with the bottom of a neighbour. Then in a $\mathrm{PO}_{4}$ group each top O is only $2 \frac{1}{2} \AA$ from an O belonging to the bottom of another $\mathrm{PO}_{4}$ group, the line of separation being almost horizontal. Midway between each of these close oxygen atom pairs is a hydrogen atom; its position has been discovered by neutron diffraction experiments. Below $\mathrm{T}_{0}$, the hydrogen atoms move along the $\mathrm{O}-\mathrm{O}$ line, $0.20 \AA$ from the midway position, in such a way that each $\mathrm{PO}_{1}$ group finds two of the four hydrogen atoms closer than before; the P atom, in that $\mathrm{PO}_{4}$ group which is approached, moves vertically away from that O atom by $0.05 \AA$; the K atoms move $0.06 \AA$ vertically the other way. Thus the hydrogen displacements cannot cause the polarisation, because they are across the ferroelectric axis. But apparently their charge causes the necessary polarisation vertically in the $\mathrm{PO}_{4}$ groups. Also below $T_{0}$, the spontaneous $P$ together with the piezoelectric effect causes a distortion of the $10 \AA \times$ $10 \AA$ base so that its angles are now $\frac{10}{}{ }^{0}$ different from right-angles.

These structures are relatively simple, and indicate the very different natures of the dipoles in different ferroelectrics. The ferroelectricity of gash and others with $\mathrm{H}_{2} \mathrm{O}$ groups could be associated with H situated between $\mathrm{O}-\mathrm{O}$ as in $\mathrm{KH}_{3} \mathrm{PO}_{4}$. But there may also be effects due to $\mathrm{N}-\mathrm{H}-\mathrm{O}$ combinations, and in ammonium sulphate, for example, only the latter is possible. Ammonium fluoberyllate $\left(\left(\mathrm{NH}_{4}\right)_{2} \mathrm{BeF}_{4}\right)$ shows the O is not essential. In non-ionic thiourea $\left(\mathrm{NH}_{2} \mathrm{CSNH}_{2}\right)$, the responsible structure is $\mathrm{N}-\mathrm{H}-\mathrm{N}$ or $\mathrm{N}-\mathrm{H}-\mathrm{S}$. Notice that in $\mathrm{KH}_{2} \mathrm{PO}_{4}$ there is one unique crystal direction for the ferroelectric axis, whereas in the barium titanate type, there are three equivalent directions (six senses) and the co-operative

(a)
(b)

Fig. 8. (a) A crystallite boundary, (b) A domain wall.
effects select one, either at random or under pressure of the piezoclectricity. These " easy" directions are determined by the forces controlling the crystal structure as we have now seen, and by the piezoelectric effects. We saw one example of this "anisotropy" in the previous article when discussing the values of the dielectric constant $\varepsilon$ in different directions.

Domains.-We have so far discussed the ferroelectric material as though it were a perfect crystal lattice, with aligned dipoles, extending in all directions. But in fact many of its most interesting properties occur because this is not true. Just as in magnetics, the material contains domains, i.e., regions defined by the dipole alignment; in each domain the alignment is different. You must distinguish carefully between a domain and a crystallite (in polycrystalline material). Crystallites are differentiated by a break in the lattice, domains by a "break" in the direction of alignment. The distinction is shown schematically in Fig. 8. Usually domains are the smaller entity. Ferromagnetic properties are largely determined by the domain structure. We shall see that there is special interest in materials in which the grains are so small that separate domains cannot form in them.

In Fig. 9(a) the field E shown will bodily reverse the polarisation in the domain Y. The simple theory which disregarded domains, will show how large E must be to do it, and this field value (which is often enormous) would be the coercive field. But if domain walls are present, they can move, and in Fig. 9(a), E will tend to cause the wall to move to the right, till the whole crystal is one domain instead

of two. This may be a much easier way to do it than the other, so that the measured coercive field is very much smaller than the value from the simple theory. If a wall is not present (Fig. 9(b)), one may nevertheless form, say at the left edge, if this " nucleation" of a wall happens to be easier than reversal. The wall shown is a " $180^{\circ}$ wall "; more complicated structures usually occur.

A wall between domains may not be a happy thing, in spite of there being (Fig. 8(b)) no lattice misfit there. (For the moment I ignore the differences of cell size in neighbouring domains due to polarisation.) It depends on the details of the way $P$ changes over its direction and magnitude from the one domain to the other. In addition, the changes of cell size due to polarisation may be different in neighbouring domains, so that some lattice misfit does after all occur. There must be some distortion of the ideal lattice near the boundary to conform with this, and since this may extend some distance from the boundary, the wall must be regarded as having a thickness. In magnetics this may be a hundred lattice cells; in some ferroelectrics, less than one.

The interplay of these factors affects the polarisation " in" the wall thickness, either in direction or magnitude, in a complicated way. Figs. 9(d),(e) show details of two of the possibilities in the simple case Fig. 9(a). Here I have supposed there are only two easy directions of polarisation: up and down; if this anisotrophy is strong the detail suggested in Fig. 9(d) is a strong violation, and the material may prefer 9(e). But the cell sizes change with polarisation, and 9(e) may involve more elastic "discomfort."

These microscopic details of the wall are usually summarised by a single number, calculated if possible from the detailed knowledge above, and called the wall energy per unit area of wall, e.g., in cobalt the wall energy is $\sigma=8$ ergs./sq. cm. The purpose of this is to be able to discuss domain changes on a relatively large (macroscopic) scale, temporarily forgetting the microscopic detail. $\sigma$ is defined as the work that would have to be done if we could form the wall* deliberately, and it is used, for prediction of domain behaviour, by the well-tried principle that the total work done must be as small as possible (principle of minimum energy). However, the figure used can be different for a wall in different situations, so that $\sigma$ must be used with caution. Often in practice, $\sigma$ is deduced from experiment, rather than calculated, and is then used to predict the results of of other experiments.

Wall Movements.-The work done (hypothetically) in forming an imagined domain structure (compare above ${ }^{\star}$ ) differs according to where any particular wall is supposed to be. This is partly because the wall area may differ, partly because impurities and local imperfections of the lattice may alter $\sigma$, and partly because the bulk of the material would be harder to force into state $y$ than into state $x$ (Fig. 9(a)) when E is present. Also because of the polarisation, there may be "free pole" at the crystal faces, and in some cases also at domain walls; this may be regarded as the source of disturbing fields which affect the work necessary. Ferroelectrics differ from ferromagnetics in this respect because, since they are not perfect insulators, charge carriers can migrate through the material to compensate any free pole if given sufficient time; this
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docs not occur in ferromagnetics, because carriers of single magnetic poles do not exist. The wall position adopted is the one (A) needing minimum work, but there may also be positions (B) corresponding to local minima, i.e., ncighbouring positions to (B) may be less favourable than (B), but position (A) would be better. A wall may become trapped at (B), unable to reach (A) because intervening positions correspond to higher energies. Nucleation of a new wall may be easier than intrinsic reversal, but more difficult than moving an existing wall. Here also we can regard nucleation as being difficult because there is a high-energy situation intermediate between the states "before" and "after."

When a field causes an existing wall to begin to move, it does so at a measurable rate, and the account may be made simpler by using an effective " mass" for the wall, to describe this sluggishness or inertia. Other macroscopic concepts are adopted also, such as an "elastic" binding to position (B); This can be broken and there may be "frictional " and "viscous" oppositions when the wall is moving.

Much of the modern mastery of magnetic materials in production is through techniques to control these factors influencing the wall motions, for example by controlling the nature and distribution of the impurities. Above the coercive field, the viscous impedance to wall motion controls the rate at which the walls move. For magnetic walls it is due to eddy current damping, magnetic relaxations, or other effects, and is rather imperfectly understood; in ferroelectrics it has as yet hardly even been measured.

The coercive field is that field which only just provides sufficient drive to move the walls across material containing traps. Until that occurs, the viscous impedance cannot operate. To account for the coercive field, however, it is not knowledge of the viscous impedance which is needed but an evaluation of that factor which makes the driving field $H$ inoperative below a certain value. This is explained for magnetics in terms of the local trapping already described; we saw that the external field affects the energy functions which control the wall; when H is as great as $H_{c}$, the neighbouring positions are no longer energetically unfavourable and the escape is made. Control of the impurities therefore controls $H_{c}$. At smaller fields, the wall may still move slightly, while remaining bound, and will return to (B) when the field is removed. This gives the bottom part of the hysteresis loop.

If the traps are not all equally deep, the escape may allow the wall to move only to a neighbouring trap, unless a slightly larger $H$ is applied; thus the steep side of the hystcresis loop is not usually vertical. But if a barrier against nucleation must be overcome first, and is a higher barrier than any trap barriers, the loop side becomes vertical. This is seen in some ferroelectrics. If in addition the only P directions involved are those parallel and antiparallel to E , then higher E cannot cause further slight increases of the overall $P$ by turning it from the easy direction towards E, as happens in magnetics. So no rounding of the loop corners occurs-the loop is "square."

There is another point to consider, however, viz. that thermal random motions may overcome barriers without such large applied fields. This becomes very rapidly impossible as we consider higher barriers, but in any case when the barrier (against escape from a trap, or against nucleation) is low enough for this possibility to be worth considering, we have to
recognise the fact that it leads to results whose characteristics are quite different. For when thermal activation is a possibility, the passage from (B) to (A) will always occur, given only sufficient time. This appears to be the case in some ferroelectrics, and we shall see later that it leads to important restrictions on the use to which we can put the material.

We have seen that the breadth $2 \mathrm{E}_{c}$ of the hysteresis loop is not a simple intrinsic property of the crystal lattice, but is strongly influenced by the domain structure. So are many of the other properties previously discussed in terms of single-domain theory. For example, in Fig. 9(c), the overall P may be very small, although $P$ for each layer is large. The dielectric constant $\epsilon$,-which measures changes of $P$ in response to changing $E$, would be unaltered in such a structure; it may even be a little increased if the walls are free to move sideways so that in a given field the favoured layers increase in size at the expense of the alternate ones. (This contribution of wall motions to the dielectric constant would disappear at higher frequencies because of the inertial property of the wall.) However, the piezoelectric effect of $E$ is opposite in alternate layers, so that they impede one another's changes of shape and the $P$ changes are reduced; this reduction in $\epsilon$ is a clamping effect additional to that which occurs even in a single domain if the frequency used is above the mechanical resonance frequency of the piece of material. Clearly the apparent piezoelectric coefficient of such a structure is also less than the intrinsic one and this decrease will be greater the thinner the layers are.

Domain Structures.-The domain structures in ferromagnetics may be very different from those in ferroelectrics. For we saw that the spontaneous distortions are very much less in magnetics. Also because carriers of free pole do not exist, ferromagnetics often have " closure domains," which are domains in the crystal surface oriented to avoid free pole at the surface. Similarly, powdered materials in which the particles are too small to break up into domains (because the wall energy would form too large a proportion of the total energy) are unable to become polarised spontaneously, and so always retain the cell sizes typical of temperatures above $\mathrm{T}_{0}$. This is because of the self-depolarising effect at the surfaces of the particles, an effect which is 1000 times bigger than in magnetics. This "unnatural" cell size is observed for $\mathrm{KH}_{2} \mathrm{PO}_{1}$ particles smaller than six-millionths of an inch. But in a conducting liquid, even particles as small as two-millionths have the normal cell size, because the surface polarisation can be neutralised by charges migrating through the liquid. $\mathrm{KH}_{2} \mathrm{PO}_{4}$ is a very good insulator, so that migration through itself is relatively slow.
Magnetic domains can be made visible because suitable tiny magnetic particles floated on to the surface will move into the fields at the domain interfaces and a similar technique has recently been reported for ferroelectrics. Most investigations have made use of the fact that plane-polarised light, sent through ferroelectric material in a direction across the ferroelectric axis, travels differently according to the orientation of its polarisation, so that a polarising microscope will show up domains differently. This method will not distinguish domains with antiparallel polarisation, and for these it. is usual to etch the crystal faces; a suitable etchant will attack the positive ends of domains more than negative ends and the resulting pits can be seen in an ordinary


Fig. 10. $180^{\circ}$ domain walls in a barium titanate crystal.
microscope (Fig. 10). None of these methods will display rapid alterations of domain structure.

Ceramics. - Ferroelectric devices have mostly used barium titanate, with or without additives, because of the high values of its various coefficients ( $\epsilon, d, \ldots$ ) though Rochelle salt has been used a good deal for transducers. A few words about crystal material will serve to show why ceramic forms are often used instead.

Crystals of barium titanate are grown by crystallisation from potassium fluoride flux, a highly unpleasant material, in platinum crucibles, with the addition of tungsten trioxide or perhaps iron to obtain large crystals, that is, up to 1 cm across. The process depends on the correct thermal gradients and concentration gradients, and often only a small proportion of the extract consists of good crystals. Sodium carbonate and barium chloride fluxes have also been used, in carbon crucibles, and in inert atmospheres, and crystals have been grown also by special techniques from the pure liquid, but a hexagonal or cubic lattice which is not ferroelectric readily results instead. When successful, the crystals are about a tenth of a millimetre thick and exceedingly fragile. A good crystal should have the ferroelectric axis everywhere directed through its thickness. There are unwanted "twinning" domains for which this is not so. These can usually be removed by "poling" with a temporary d.c. field, for a small voltage applied between the faces of these crystals gives a field of several kilovolts per centimetre. But even this process can easily fracture the crystal, because of the high stresses set up by the piezoelectric effect at the edges of these twinned areas. The geometry is such that these stresses do not occur at the $180^{\circ}$ walls discussed earlier.

The ceramics are made by grinding barium titanate (or its components) and any additives, and by extrusion or pressing with or without a binder, and sintering at high temperature, say $1200-1400^{\circ} \mathrm{C}$, to make a glassy product. The result may be regarded as a very complicated polycrystalline material, with the crystallites randomly directed, unless the manufacture included the application of special fields. Many of the crystallites will have grown into one another at their corners by a diffusion process. In general, each crystallite contains several domains, and the domain walls can move under
electrical or mechanical stimulus in ways similar to those for single crystals. The one-directional properties discussed earlier will be "averaged out" in the virgin material and though this may be altered by applying fields, it is clearly not so easy to explain simply the properties of such materials. But the ceramics are hard and resistant and can be made any reasonable size or shape. Solid electrodes can be fixed on to them in a number of ways, including evaporation, printing, or the firing-on of metallic pastes. Finally they may be given protective coatings, especially if they are at all porous.
Each crystallite is in a polarised state and may be highly stressed because of its surroundings. Without electrical treatment, the polarisation will average out to zero. A small field will lengthen some grains and shorten others during the time it is applied, so that the apparent piezoelectric coefficients ( $d$, etc.) will also be small or zero. But the effect of that field on the intrinsic polarisation of the various parts, is to increase it where it is positive (say) and decrease it where it is negative. Thus these effects do not average out, so that the dielectric constant $\epsilon$ can be measured and used as an index of the extent to which the ceramic properties approach those of the singlecrystal material. Usually more intense sintering makes for higher $\epsilon$, an improvement which can also be followed by watching the density of the ceramic. The crystal density is $6.0 \mathrm{gm} / \mathrm{cc}$. and ceramic densities about $5.7 \mathrm{~cm} / \mathrm{cc}$. are common.
"Poling" the virgin ceramic causes some degree of alignment, so that hysteresis loops and the other properties we have discussed can now be observed. The polarisation now lies, not all parallel as in a single crystal but along the nearest easy direction (to the poling) in each crystallite. It can be shown that the maximum P possible should then be $86.6 \%$ of the single-crystal value ( 26 microcoulomb $/ \mathrm{cm}^{2}$ in barium titanate). But the high $d$ together with stresses left in manufacture and stresses introduced by poling, and the gaps between crystallites, means that only about 7 microcoulombs $/ \mathrm{cm}^{2}$ is achieved as retentivity. The saturation value may be twice as "much, so it is clear that the loop no longer has the " good" square shape.
Similarly, the piezoelectric coefficients are, say, a quarter of the single-crystal values. It is interesting too that when the applied field causes thickness expansion of a disc of the material, the accompanying radial contraction, quoted as a fraction, is often less than half the fractional thickness change, because thickness expansion of the crystallites shows up as an expansion of the disc, whereas to some extent radial contraction of the crystallites can occur without full corresponding contraction of the disc. In a crystal, the contraction in each of two directions is half the expansion in the third, so there is no volume change; in the ceramic there is an apparent change of volume.
As in the crystalline forms, $\mathrm{T}_{0}$ and the other properties can be altered by suitable additives, and now the state of sub-division and the nature of the annealing provide further controls since they alter the internal stresses. In this way one can make the curves of the various anomalies (against $T$ ) less peaky for applications where this is desirable; usually the maximum value will then be less. If the internal stresses are not very uniform throughout the material, there will be a spread of $\mathrm{T}_{0}$ values, and the flattening may be thought of as due to the superposition of these. In barium titanate ceramics $\epsilon$
increases as grain-size decreases. Added calcium titanate lowers P and raises the coercive field $\mathrm{E}_{c} ; 10 \%$ raises it from $2 \frac{1}{2}$ to $5 \mathrm{kV} / \mathrm{cm}$. Admixtures of strontium titanate give values of $\mathrm{T}_{0}$ which differ under different heat treatment during preparation, as the barium and strontium ions rearrange themselves; the strontium ion is $11 \%$ smaller than the barium ion so that certäin special regularities of arrangement will occur if temperature conditions allow. Addition of antimonates is said to reduce $\epsilon$ at $\mathrm{T}_{0}$. It would be impossible to summarise all the possibilities. I shall merely quote arbitrarily some of the many materials which have been used.

Applications.-Some uses of ferroelectrics depend on the large values of some of their properties near $\mathrm{T}_{0}$; others depend rather on the non-linearities, e.g., $P$ plotted against $E$ is not a straight line as in ordinary dielectrics, and the small-signal $\epsilon$ is not constant against signal size and bias. In general, the first group has been well developed over a number of years so that devices are commercially available, while the second group is largely represented by development work, and "one-off" models to be found in various laboratories.

In the first group the non-linearities are usually a nuisance to be minimised if possible, and the valuable high coefficients, as we have seen, depend strongly on temperature. The hysteresis loop in particular, for applied voltages large enough to traverse it, causes losses due to the energy dissipated as heat, and this in turn is likely to cause drifts in the coefficient being exploited ( $\epsilon, d$, etc.), due to the temperature changes. Questions of temperature stability therefore become important. Many wellknown electro-mechanical transducers use ferroelectrics because of the large values of $d$ available, and miniature capacitors may use ferroelectric dielectrics because of the high $\epsilon$.

The second group depends on the non-linearities, and here there is one large subgroup which does not use the hysteresis and another which does. Each covers a range of possibilities, but for the first we may use the envelope name "dielectric amplifiers," and the hysteresis uses are largely of interest in digital computers, either as memory devices or for switching purposes.

Transducers.-Devices which convert small mechanical oscillations or impulsive motions into electrical signals include microphones, gramophone pickups, vibration detectors, accelerometers, detectors for ultrasonic waves, strain-gauges, and detectors for small displacements. Those which convert electrical signals into mechanical motions include vibrators, loudspeakers, sonic pulse generators in delay lines, and generators of ultrasonics for non-destructive probing of solids, for determinations of physical properties, for cleaning of surfaces during various processes, and for cutting difficult materials. We must consider also the use of piezoelectric crystals to determine and control oscillator frequencies, and their use in narrow-band wave filters, e.g., to remove an r.f. carrier from the sidebands; these uses depend on the fact that a piezoelectric crystal has a natural frequency of resonance determined by its geometry, and that with electrodes it behaves electrically for nearby frequencies as an impedance often represented as a series LCR combination and parallel capacitance. The effective $Q$ factor can be made very high by careful mounting, sometimes in a vacuum and the device is used as the heart of the filter.

We saw that ferroelectrics exhibit an effective piezoelectricity below $\mathrm{T}_{0}$ due to the spontaneous polarisation $P$ acting as a bias, so that they may be used in any of these piezoelectric devices. The ceramic forms must be poled to produce the $P$. The time and temperature instabilities of ferroelectrics mean that where high frequency-stability is sought, quartz is still used. But in many of the other devices, ferroelectrics have been used for many years, initially Rochelle salt, but increasingly barium titanate and its derivatives. This is so particularly in view of the versatility of the ceramic forms, which are made in blocks, discs, hollow cylinders, and many other shapes, and in sizes up to several inches; shapes can be arranged to focus radiated acoustic energy. Fig. 5 last month showed $d$ values around $10^{-6}$ statcoul./dyne, 100 times larger than quartz values. (Divide by 30,000 for values in coulomb/ newton.) In addition, the high $\epsilon$ values of ferroelectrics give the devices lower capacitive impedances than with traditional materials, so that the charge measurement at low frequencies is easier.

The cutting and plating of piezoelectric materials is a well-documented subject. The piezoelectric uses of ferroelectrics do not differ in principle, and this is not the place to repeat the details. We have already discussed the various piezoelectric coefficients. Briefly, when in use to produce mechanical stress or motion, the mechanical impedance of piezoelectrics is high enough to match well into liquids or solids. For use in air, the lower mechanical impedance and greater motion of a bimorph unit or "bender" is used (Fig. 11); the variations of response


Fig. 11. Bender unit. The components are cut so as to vibrate longitudinally in opposite directions. They are cemented together and the motion shown is $31 / b$ times greater than the longitudinal motions.
with temperature are then less. Twister units are also used. The natural frequency of any piezoelectric device is altered by altering its dimensions; the natural frequency of a bender is relatively low, so that they are in use for audio-frequency devices. For ultrasonics (say $100 \mathrm{kc} / \mathrm{s}$ ) a simple longitudinal vibrator may be used, and a more perfect single resonance is then generally obtainable. For work in the megacycle regions one may use the thickness vibrations of a suitably cut plate of the piezoelectric (transverse vibrations are also used). For this mode, the mean frequency used will correspond to a wave length $2 b$ if $b$ is the crystal thickness (e.g., $b$ about $1 / 20 \mathrm{~mm}$ in X-cut quartz for fundamental $60 \mathrm{Mc} / \mathrm{s})$. Here the requirement is usually that over the required frequency range as much of the electrical power as possible should be transferred. Suitable design may give $70 \%$ transfer over a frequency range of $10 \%$. The input signal to a ferroelectric must remain small enough to avoid disturbing the spontaneous P so a high $\mathrm{E}_{c}$ is an advantage. $4 \%$ lead titanate in barium titanate ceramic has allowed transfer of 1 watt per sq. mm. For microphones, on the other hand, power is not so important as uniform response over a large frequency range. $5 \%$ barium zirconate (itself not a ferroelectric) in
ceranic barium titanate is suitable for transducers, its natural frequency changing $4 \%$ over $50 \mathrm{C}^{\circ}$.

In pickups, a $30-\mathrm{mil} 2-\mathrm{cm}$ element will give signals of 1 volt. Ceramic barium titanate benders now replace Rochelle salt, which cannot survive high humidity. For pressure-sensitive microphones, double strip designs include cases in which the ferroelectric is the diaphragm disc, and others where a metal diaphragm actuates the free end of the strips. Vibrators and accelerometers may often be used in combination, to excite vibrations in engineering structures at selected frequencies and to detect the amplitude of the response; when the structure is part of a rotating machine, both devices must often be light; an $\frac{1}{8}$ in $\times 10-\mathrm{mil}$ barium titanate strip has


Fig. 12. Dielectric constonts. (i) Borium titanate crystal, along ferroelectric axis; (ii) A typical ferroelectric ceromic. Dotted curves, effects of bias (10 and 14 $K \mathrm{v}$ 'cm).
produced 10 millivolts for movements of 1 part in a million of its size. This is an order more than resistance strain-gauges, and a vibration straingauge giving 100 mV for 1 in a million has been reported more recently.

Capacitors.-The high dielectric constant of ferroelectrics near $\mathrm{T}_{\mathbf{0}}$ leads to their use in capacitors wherever high value or small size is required and temperature stability is not too important. Fig. 12 shows the dielectric constant of barium titanate crystals and the results achieved in ceramics by additives such as strontium titanate or calcium titanate. In these the high $\epsilon$ range has been brought down to a convenient temperature, and flattened to improve temperature stability. The $\epsilon$ peak values indeed are lowered, but the value at operating temperatures is not. The high $\epsilon$ values allow capacitors to have smaller dimensions and they can be in any of the standard shapes. Pressing is used for the familiar disc-shape, and extrusion for capacitors of cylindrical shape. Power factors are usually about 0.01. For capacitors, of course, the ${ }^{-}$nonlinearity is a disadvantage, and results in the $\epsilon$ value increasing if measured with a larger a.c. voltage, and also altering if there is any bias across the capacitor. Fig. 12 shows the effect of bias. The non-linearity is less marked away from low frequencies and $T_{0}$. Mixtures of zirconates and niobates are also used, particularly when higher temperatures are encountered; $\mathrm{T}_{0}$ is high for such materials as lead titanate, potassium and lithium niobate (see Table I), and some antiferroelectrics, but it is often falling resistivity of ceramics which limits their use at high temperature.

Very small components are made with ceramic
films only a few 'mils thick. These have working voltages around 300 volts d.c. and breakdown at about 1 kV , for values up to $0.01 \mu \mathrm{~F}$; higher values are made by packing several such films together, as in mica capacitors. The lead inductances can be kept low since the components are small. The leakage conductance varies strongly with temperature, but it has been kept up to 200 megohms well above $100^{\circ} \mathrm{C}$ for $0.1-\mu \mathrm{F}$ film capacitors.

The $\epsilon$ and the power factor of ceramics " age" over several months, $\epsilon$ (and also d) decreasing $20 \%$, while $Q$ increases. For most purposes, the values are stable enough several weeks after manufacture, or appropriate heat treatments will remove the aging. We saw that $\epsilon$ is partly due to the domain walls moving when a field is applied. In a ceramic the walls are subject to more stringent interference by irregularities than in a crystal. We may expect it to be more difficult to escape from a temporary trap B to the "deepest" trap A, and this will take place only after some time. Once there, the motions are more restricted, so that $\epsilon$ is then smaller. The power factor, for frequencies below $10 \mathrm{Mc} / \mathrm{s}$, also ages and has been ascribed to movement between traps.

Poor electrical strength means that ferroelectrics are not very suitable for power capacitors. The instability with time and temperature results in their being used for by-pass and blocking capacitors, and also as smoothing capacitors at higher voltages, rather than in tuned circuits.

## Acknowledgements

A section of the photograph Fig. 10 was used in a paper by the author in Proc. Phys. Soc., 1st April, 1957. Fig. 12 (i) is taken from a paper by W. J. Merz in Phys. Rev., 76, 1221, 1949, and (ii) and the dotted curves from Fig. 7 of a paper by P. Popper in fourn. Inst. Elec. Eng., 2, 450, 1956.
(To be continued)


[^4]
# PARIS AIR SHOW 

NAVIGATIONAL AND COMMUNICATIONS EQUIPMENT AT THE 23rd SALON

1PREDOMINANT impression gained Irom a brief visit to this year's Salon International de l'Aeronautique at Le Bourget airport was the extensive use of transistors in all kinds of sircraft radio equipment. As an example the French firm C.S.F. showed a light, fixed-loop radio compass which weighed only 12 lb , compared with the 40 lb of previous models, and measured only $14.6 \mathrm{~cm} \times$ $16.5 \mathrm{~cm} \times 11.4 \mathrm{~cm}$. It has push-button selection of four pre-set frequencies and the directional accuracy is $\pm 2^{\circ}$. Current consumption is less than 400 mA . This firm also had an f.m. radio sltimeter which was transistorized except for the transmitter oscillator. The weight was 20 lb . Accuracy of measurement was $10 \%$ above an altitude of 100 ft . On the Air-Equipement stand an automatic pilot equipment was noticed which used silicon transistors throughout, and this design has already been installed in a good many American military aircraft.

On the communications side an outstanding example of what can be done by transistorization was the neat Bendix RA-21A v.h.f. receiver. This provides for 560 channels at $50 \mathrm{kc} / \mathrm{s}$ spacing in the range $108-136 \mathrm{Mc} / \mathrm{s}$. It is a triple superhet circuit, transistorized except for four valves in the front end, and uses printed wiring and inductors. There is an automatic tuning system utilizing rotary stepping solenoids, and the selected frequencies are displayed by a digital indicator. The receiver unit, including power supplies, weighs only 8 it, and measures $7 \frac{3}{4}$ in $\times 2 \frac{3}{8}$ in (front panel) by $12 \frac{3}{4}$ in deep.

This receiver can be used for communcations alone or as an input to a navigation unit, which is a fully transistorized equipment of corresponding size giving VOR (v.h.f. omni-directional radio range) and "localizer" information. The companion v.h.f. transmitter for these receiving equipments gives an r.f. power output of $25-30$ watts. It is transistorized in the i.f. circuits and the switching relay circuits and weighs $14 \frac{1}{2} \mathrm{lb}$ including power supplies

It is well known, of course, that transistors are now being used in the electronic circuits of guided missiles, where their small size, reliability and low power consumption are particularly advantageous. As an example, G.E.C. were exhibiting a transistorized version of the guidance equipment for the Royal Navy's ship-to-air guided missile Seaslug. The equipment is made up of 40 units, each of which is readily replaceable. Printed circuits are used in these units and also in the "cable form" which consists of two double-sided printed boards extending along the whole length of the equipment. The system is said to be about half the weight and size of the equivalent valve equipment and to require only one third of the operating power.

A transistor pre-amplifier, designed as a replaceable plug-in unit, is used in a Murphy airborne tape reproducer which operates at $3 \frac{3}{4} \mathrm{in} / \mathrm{sec}$ and weighs 20 lb . This equipment has separate heads for the two tracks on the tape and when the tape is automatically reversed at the end of its travel (by a
microswitch control system) the appropriate head is switched to the pre-amplifier. The reproducer is intended for use in conjunction with a passenger announcement equipment, and there is an automatic fade-up and fade-down system to avoid abrupt changes between the recorded programme and the announcements.
Incidentally, this firm also displayed their "leader cable" equipment which is used in the blind landing system recently developed by the Royal Aircraft Establishment. The principle of this azimuthal guidance system, based on the magnetic fields picked up from two cables laid either side of the runway, was described in our December, 1958, issue (p. 579). The a.c. signal frequeacies in the two cables are $1,070 \mathrm{c} / \mathrm{s}$ and $1,750 \mathrm{c} / \mathrm{s}$ respectively. After separation by filters in the airborne receiver the two signals are applied to a cathodefollower comparator circuit. Any inequaiities in amplitude, due to the aircraft being displaced from the runway centre line, cause the comparator to produce an unbalance voltage which is fed as a correcting signal to the aircraft's automatic pilot.
A good many radar equipments were on show, of course, some of them being associated with com-puter-controlled systems for automatic navigation and fire-control in fighter aircraft. Such a system was shown by the French firm S.I.N.T.R.A. for use with the famous fighter aircraft Mirage III. In the sphere of ground-based radar an interesting development of special value to traffic controllers was demonstrated by C.S.F. This was an image transformation equipment by which radar displays can be presented with enhanced brilliance on television screens. The heart of this equipment is a special storage tube, TMA 403, with a p.p.i. "writing" section at one end and a television-scan "reading" section at the other end. Storage time can be varied by an operator from a few seconds to several minutes.
The idea of the system is to avoid the need for viewing radar screens in a darkened room-often a source of difficulty in airports because the control tower staff cannot always leave their posts to look at the radar. Furthermore, because of the storage facility provided by the image transformer, it becomes possible to see the routes of. aircraft by the tracks they leave on the screen.
The demonstration by C.S.F. at Le Bourget was actually a television display of a p.p.i. radar picture generated at Orly airport (to the south of Paris)showing that transmission or distribution of radar pictures over long distances is a practical proposition. The transformation was done at Orly and the 625 -line television picture was transmitted northwards to Le Bourget by microwave links.
Apart from the advantages mentioned above, this system, which has already been installed in a good many American airports, offers the possibility of mixing other sources of display information with the radar picture. For example, distance marker rings or "electronic maps" can be superimposed on it.

signal to be limited is applied as the pump input signal to a parametric oscillator. For input pump powers below a certain level, no oscillations are produced and the pump output increases with the pump input. For input pump powers above this level, oscillations are produced and the pump output is limited at a fixed level. An advantage of this method of limiting is that it can theoretically be made phase distortionless.

High Efficiency Class-C Power Amplifiers are by no means new: indeed, there is a German patent of 1917 (by G.D.T.) which deals with the use of harmonic resonators in the anodecircuit of a class-C stage as a means of broadening and flattening the anode current pulse-and so improving efficiency. Although superficially similar, the arrangement described by V. J. Tyler in a recent Marconi Review (Vol. XXI, No. 130), differs in that the grid-drive to the amplifier does not contain the harmonics for which resonators are provided. In its simplest form Tyler's amplifier is driven by a square wave (containing only the odd harmonics) and has two "loss-free" parallel-tuned circuits, which resonate at the second and fourth harmonics of the signal frequency, in series with the tank: these resonators aid the anode-voltage waveform to take up a shape not unlike the output from a single-phase rectifier without reservoir capacitor. Two experimental amplifiers, one of high power rating, one of low, are quoted as giving anode efficiencies of $93.8^{\circ} \%$ and $90.4^{\prime \prime}$. Output powers as much as three times that given by a normal class-C stage are obtained with ordinary transmitting valves and a further example quotes KT45 valves (television line-output pentodes) as producing 200 watts of r.f.-an increase of power output of over $400 \%$ of the normal class-C output. Another favourable point is that mistuning of the anode circuits does not produce a sharp rise in anode dissipation, also the arrangement is capable of high linearity with anode modulation because the output voltage and supply voltage are rigidly inter-related.

Hybrid Monostable Circuit, using a valve and a transistor, has been designed by E. Patterson, of English Electric Aviation, to produce pulses for binary circuits from the small signals given by photocells in an optical shaft encoder. Since ten of these circuits were required for each encoder-one per channel-it was desirable to have a circuit containing the minimum number of components, with no transformers, and operating from existing power supplies. The output impedance of the photocell circuit was of the order of 0.5 MO , requiring a high impedance input to the device. A regenerative
hybrid circuit, in which a pentode suppressor grid was controlled by a transistor switch driven from the pentode anode via a diode, was found to give the required high gain and monostable switching characteristic. The circuit produced rectangular pulses on the suppressor greater than 10 volts from 0.1-V sine waves or 20 mV pulses. Triggering

pulses could be obtained from the anode by suitable filtering. Pulse rise times of the order of $3 \mu \mathrm{sec}$ were obtained, and investigation has shown that faster rise times are possible. Since this circuit was developed, the designer has become aware of an article in Electronics for April, 1959, "Series Diode Increases Multivibrator Sensitivity," in which the author, M. M. Vojinovic, shows how the stability of the circuit is controlled by the diode in the feedback path. The high impedance offered by the diode before breakdown is sufficient to prevent the loop gain from exceeding the critical value. However, when the anode voltage is sufficiently high the diode breaks down and regenerative action commences. For the best performance of the circuit shown, component values must be chosen to suit the frequency and amplitude of the input signal in order to avoid frequency multiplying or dividing effects.

Parametric Limiters are discussed by A. E. Siegman in a letter to Proc.I.R.E. for March 1959. The

Ophitron, from the Greek for a serpent, has been chosen by the G.E.C. as the name for a backward wave oscillator using a new type of electrostatic focusing in which the electrons travel in a wavy path. The electron path shape and electrode configuration are similar to those used for slalom focusing (sce Technical Notebook for May .1958), the electrodes consisting of two charged flat plates one in front of and the other behind a ladder-like slow-wave structure. The relative petentials of the various electrodes in an Ophitron are, however, different from those used for slalom focusing; the two plates now being at unequal potentials with one much more positive than the other; although, as for slalom focusing, the ladder line is made more positive than either plate. With these changed potentials, the electrons in an Ophitron remain always on the same side of the ladder line so that the crests of the wavy electron path now lie between the ladder rungs rather than in front of or behind them as with slalom focusing. This results in better interaction between the electrons and slow-wave ladder line than with slalom focusing. The curves in the wave-likit beam path result in focusing forces which counteract the space-charge repulsion. It is expected that because of the removal of ions to the focusing plates, the noise will be less than with magnetic focusing, the usual method of focusing used. Ophitrons should also be

less susceptible to stray magnetic fields than magnetically focused valves. The first Ophitron made by the G.E.C. is for the $10,000 \mathrm{Mc} / \mathrm{s}$ band and delivers a few tens of mW power over a $40 \%$ bandwidth. Its weight and dimensions are only $70 z$ and 6 in by $\frac{3}{4}$ in diameter respectively.

# Scientific Uses of Television 

ONE ASPECT OF THE BRIT.I.R.E. CONVENTION AT CAMBRIDGE

I)OMESTIC television development, though not exactly at a standstill, certainly seems to be passing through a phase of marking time. At the present juncture nobody but an incurable optimist would think of running a technical conference on this subject alone. The Brit. I.R.E., though undoubtedly optimistic in outlook, was realistic enough to give its recent Convention, held at Cambridge University, the carefully worded title of "Television Engineering in Science, Industry and Broadcasting." The net was therefore cast wide and some interesting fish were caught, including a psychologist talking on subliminal perception, an American on space television, two Russian engineers on various aspects of Soviet television and the well-known television pioneer, Dr. V. K. Zworykin, who gave the Clerk Maxwell Memorial Lecture and surprised everyone by not talking about television at all.

As to the scientific applications of television, it was quite obvious that a great deal of specialized study has been devoted to what is generally known as "industrial television" or "clesed-circuit television" equipment. A few years ago, when the potentialities of television as a "remote eye" for viewing in difficult positions were first realized, there was an enthusiastic rush to couple television cameras on to everything possible connected with visual inspection. This enthusiasm has now been tempered with the knowledge of what can happen to such equipment when it is subjected to heat, n:oisture, radioactivity and so on, and out of this experience new designs have evolved. The photoconductive pick-up tube owes its present high state of development largely to industrial television, and now the normal range of visual observation is being extended into the infra-red, the ultra-violet and to regions of extremely low light levels.

One example of observation at low levels of illumination occurs in astronomy, and here one is thinking in terms of individual light quanta rather than in the more familiar light units. The great problem is in examining celestial bodies through the semi-transparent layer of the carth's atmosphere. For a good many years photographic plates and photoelectric devices have been used for integrating the light from very weak sources, and more recently special electronic image converter tubes have been developed in which clectron-sensitive photographic film is enclosed in the vacuum chamber. These methods, however, tend to be cumbersome and complicated in practice, and as a result television has been tried as a possible alternative. A paper by B. V. Somes-Charlton described what has been achieved since about 1951 when the author, in collaboration with P. B. Fellgett, first carried out tests with television caneras coupled to telescopes at the Cambridge Observatories.

The image orthicon pick-up tube was used because of its high sensitivity, and in 1956 some tests indicated that there was a gain in light sensitivity by a factor of 3 over the best photographic film
available. This is not a great deal, and it is possible that film emulsions have caught up in the meantime, but the television technique still has the great advantage of electronically variable contrast, which is of tremendous value in clarifying the detail of images.

To give an idea of the performances of light detectors Mr. Somes-Charlton said that ideally each photon of the incident light should effect the reduction of one grain of silver halide in a photographic emulsion or liberate one electron from a photocathode. This would represent a "quantum efficiency" of 1. In fact the best approach to this was given by the photomultiplier tube, with an efficiency of 0.05-0.1 (the human eye having a maximum of 0.05 ), while the image orthicon tube gave a figure of $0.02-0.03$ and photographic films $0.001-0.01$ (with a reported recent improvement to as high as 0.1). However, some recent experiments had been conducted by R.C.A. in America on modified image orthicon pick-up tubes containing special image intensifiers using phosphor-photocathode stages and electron accelcrating voltages. With these it was claimed that an image of 400 lines definition could be produced with a photocathode illumination of only $10^{-6}$ or $10^{-7}$ foot candles.

Incidentally, Mr. Somes-Charlton demonstrated a simple apparatus which he had used for testing the relative performances of pick-up tubes and photographic plates in sensitivity and resolution. It consisted of a metal plate perforated with holes of graded diameters having behind them grey filters of graded densities. The whole mask was illuminated from behind by a cold light source and viewed from the front by the television or photographic camera. The performance of the camera, television or photographic, could then be judged by which particular holes were just on the limits of visibility due to their reduced contrast (dense filters) and resolution (small diameters).

## Space Television

Another method of mitigating the effects of the earth's atmosphere on astronomical observations was mentioned in a paper by B. I. Sardiko of the U.S.S.R. (read by B. A. Berlin). This was the use of stereoscopic television on telescopes spaced widely apart. But probably the most advanced idea of all is to get outside the earth's atmosphere altogether by means of space vehicles. One proposal bas been for an astronomical telescope orbiting in space and fitted with a television scanning system controlled from a ground observatory. At the Convention A. J. Viterbi, who has been connected with recent satellite launchings in the U.S.A., discussed some of the important design criteria for such a television system, which, for close observation of some of the planets, would have to work over ranges of the order of 25 million miles.
Because of the low received signal power (estimated at $10^{-18}$ watt) and the high noise level, the
channel bandwidth has to be severely restrictedin fact, to as narrow as $1 \mathrm{c} / \mathrm{s}$. . Bandwidth compression to this extent is achieved by recording the video information on magnetic tape at normal speed then replaying and transmitting it over a long period of time (for example, one 200-line image would take about 1.85 hour to transmit). Another problem arises from the fact that the carrier frequency of the transmitter is varied by the Doppler effect as the vehicle travels rapidly through space. This means that simple frequency modulation cannot be used for overcoming the noise in the transmission channel. Instead the video information is used to frequency modulate a sub-carrier, and the subcarrier modulates the phase of the carrier signal.

At the receiver the Doppler-shifted carrier is recovered from the noisy signal by a "coherent tracking filter." This is a form of servo-mechanism called a "phase-locked-loop" containing a variablefrequency oscillator which is kept locked in phase and frequency to the incoming signal by control from an error signal. The output from this oscillator is then mixed with the received signal to recover the original frequency-modulated signal, and this is passed to a discriminator to give the final video information. The discriminator has to deal with a very noisy signal and it again takes the form of a "phase-locked-loop" servo-mechanism. The local oscillator is controlled by an error voltage and it is this voltage which provides the video output signal.

## Radiation Problems

Compared with space projects, nuclear energy has become almost a common-or-garden application for television techniques. Here the transmission problems may not be difficult but the environmental ones certainly are. For observation purposes in a nuclear reactor the television camera has to contend with heat and radioactivity. The heat problem can be tackled by gas cooling and, according to a paper by P. Barrart and I.. M. W/alters, nothing practicable can be done about radiation shielding. Lead shields for protection against gamma rays would be far too big and heavy, while neutron-absorbing materials would have undesirable effects on the operation of the reactor.

The paper includes an interesting table showing the effects of radiation on the electrical and other properties of electronic components. Resistors and capacitors are changed in value by only a few per cent (varying with the materials used in their construction), television pick-up tubes suffer a temporary increase in dark current and semiconductor devices show much higher leakage currents than normal. It emerges, however, that the most serious effect of all is not electrical but optical-the discoloration of the glass in the camera face-plate and lenses due to changes in its molecular structure. It is only necessary to replace the affected glassware and the camera is fit for use again.

Another paper, by E. C. Sykes, dealt with the use of television for microscopical examination of nuclear fuel samples which have been irradiated in a reactor. The camera is coupled to the microscope in such a way that the optical image is directly focused on to the sensitive area of the pick-up tube, so that no camera lenses are required. Apart from allowing safe observation of the specimens by several people simultaneously, the television system offers a useful facility for the accurate size measure-
ment of details such as hardness indentations. Two electronic cursors, consisting of vertical and horizontal black lines, are generated on the picture by a system of black-out pulses and time delays. These can be moved across the picture by calibrated controls, and since the overall magnification of the microscope-television system is known it is possible to make accurate size measurements-actually to within $\pm \frac{1}{4}$ micron at an overall magnification of 3,000 times.
Incidentally, this paper discussed some interesting practical experience on the use of stereoscopic television for observation of manual operations carried out remotely by master-slave manipulators. It was found that stereo television was not so helpful to the operator in achieving speed and dexterity as single-channel television with strong oblique lighting from two directions which gave visual positioning information by means of the shadows.

## Medical Observations

The development of medical colour television was reviewed in a paper by R. D. Ambrose and A. R. Stanley, who also discussed future possibilities in the particular field of endoscopy. The endoscope is an optical tube which permits observation of the interior of the body without recourse to surgery. Normally it is only possible for one person to make observations, unless photography is used, so the possibility of coupling a television camera to the external end of the endoscope tube offers some distinct advantages. The main problem is in getting enough illumination into the interior of the body, particularly for colour television. It is also desirable to have smaller and more manœuvrable cameras than are available at present, and there has been work on the development of miniature transistorized cameras for this purpose.

Another aspect of medical television mentioned in a paper by J. H. Taylor was the use of infra-red light, with a television equipment designed for this region, to examine the inside of the eye. The point here is that the eye pupil does not close in infra-red light. In other parts of the body it becomes possible to study details of the superficial venous system because the skin is transparent to infra-red radiation. Mr. Taylor described a high-grade television equipment using a special vidicon-type pick-up tube with a spectral response of 4,000 to 10,000 angstrom units (the visible region being 4,000 to 8,000 ). Another tube, for the ultra-violet region, has been developed with a response giving down as far as 2,350 angstrom units.

Television techniques are now being used for image amplification in X-ray fluoroscopy, and here one is dealing with very low light levels in the region of $10^{-3}$ to $10^{-1}$ foot-lambert. E. Garthwaite and D. G. Heley described a special image orthicon tube developed for this work.

Finally, if we have not made any mention of the papers on the domestic side of television it does not necessarily mean that we agree with a certain speaker at the Convention banquet who made fun of the Convention title "Television Engineering in Science, Industry and Broadcasting." He said it was problematical whether there was any science in Industry or even any industry in Science, but he was quite certain from personal experience that there was neither science nor industry in Broadcasting!

## TAETIERS TO IUHE EDITOR

## The Editor does not necessarily endorse the opinions expressed by his correspondents

## Monophonic or Monodic?

"FREE GRID" makes a reasoned plea in your June issue for "monodic," but he has misled you by saying that monophonic reproduction means "one-sound reproduction." This is not at all the intention of those who, despite "Free Grid's" diverting contribution and your weighty editorial, are srill in favour of "monophonic."

The primary meaning of $\phi_{0}, 2, \eta$ is not "sound" but "voice "; an educated friend tells me that the original Homeric meaning was "voice" and that only much later did the word acquire the derived meaning of "sounds from inanimate objects." What could be more appropriate than "monophonic" to refer to the use of a single-channel reproducer, which, like you and "Free Grid," speaks with one voice?

Having established the semantic propriety of "monophonic," let us bear in mind its two great advantages:
(1) it is already well established, particularly in America, and
(2) it makes a convenient pair with stereophonic.

Incidentally, "Free Grid" cannot claim the paternity of "monodic"; it was suggested in my letter published in the January issue of Electronic $\mathcal{E}$ Radio Engineer, as an alternative to "monophonic."
London, N.2.
E. L. E. PAWLEY

## "Free Grid" Comments :

Even if Mr. Pawley's remarks about the Greek word ofnv? $\eta$ were correct, I do not see how the case for the use of "monophonic" is thereby strengthened. As for his argument about this word being well established in the U.S.A., must we follow American usage in this matter as we have done in the terminology of household sanitation? But Mr. Pawley obviously bases his main argument on the original meaning of the word $\psi+\cdots \cdot y$, and so I had better confine myself to that.
Going right back to the obsolete verb phao ( $\phi x_{(1)}$ ), meaning, inter alia, to speak, we find several words associated with it, but the only two which concern us here are $4(00 y$ and $\phi(0) \eta$, , both of which are transliterated into our alphabet as "phone." The first of these words started life meaning " mouth," and was used figuratively in such expressions as "to put to the mouth (or edge) of the sword." A handy example is to be found in Exodus, XVII, 13, where, in the Septuagint, occur the words $\epsilon v$ poun $\mu \alpha x^{\alpha, \rho x_{s}}$ to describe the rough house which Joshua gave the Amalekites.
(how, eventually came to mean the effect of putting to the sword, namely, slaughter. While wor originally meant the mouth of the sword, its stable mate $\phi$ mely meant the voice of the seword (poetical fellows these Greeks), which was a picturesque way of saying the sound of slaughter, and in particular the noise of battle.

Now the noise of battle is a confused jumble of sound, and in those days the first thing that would be heard would be the clash of arms, a very inanimate sound. Thus the primary meaning of $\psi \cdots \cdots$ was obviously an inanimate sound, but I will, of course, admit that it would soon be followed by the thoroughly animate sound of the cries of wounded horses and men; but the inanimate meaning of $\phi, \ldots \eta y$ beat the animate one, even if only by a short head!
London, S.E.1.
"FREE GRID"
IF "monophonic" is to be excluded because it does not ". . . . call to mind . . . . the rich polyphonic sounds of music and well modulated voices . . . .", then can we permit the transmission of monodic works through a stereophonic system?

Furthermore, if it seems incongruous to transmit poly-
phony over a "monophonic" system, would it not be even more so to employ a "monodic" system, since the term "monody" means "a song for one person." It is derived from the Greek word for an ode sung by a single actor in the ancient Greek tragedy, and is also used in connection with early opera in distinction from polyphonic style.

Whilst paying due homage to the erudition of your cognoscenti, may I suggest that the term monodic be left alone since it already has a perfectly sound connotation. Keeping the prefix "mono," and I am sure that " mono" and "stereo," once accepted, will always be recognized terms, may I suggest that one might do worse than take from biology the term monophyllous (singleleafed), and change it to monophyllic. In spite of its "ph" and " 11 " the word is easy to say and there is less likely to be confusion with a term borrowed from a more remote science or art. Monothetic is another fairly neutral alternative. "Monophonic" is still the best sounding term, however irregular the derivation.

Eccles, Lancs.
Wm. THURLOW SMITH,
"Eroica" Sound Recording Services.
I THINK the B.B.C. have found a very pleasant sounding word in "monophonic," and whatever its origins and whatever it means we will enjoy using it. Your "monodic" sounds like a cold in the head.

Lausanne, Switzerland.
R. H. WILLIAMS.

## Mavars

I HAVE just read the excellent and entertaining article on MAVARS by "Cathode Ray" in the May issue of Wireless World.

In the discussion of names for the parametric device, reference to my article in the September 26, 1958, issue of Electronics gives the erroneous impression that I am the originator of the term MAVAR. Although I wish I could claim credit for this, such is not the case. Unfortunately, a search of my notes fails to disclose who was the first to use this term, so I cannot set the record completely straight.

Another name which has been proposed and which has some merit is the REACTATRON (Proc. I.R.E., January 1959, p. 42). This term is intended to describe specifically the diode parametric amplifier, although I see no reason why it cannot be extended to other forms. It avoids the use of the term " mixer" which "Cathode Ray" feels so strongly about.

New York.
SAMUEL WEBER, Associate Editor, Electronics.

## Facsimile Television

IN connection with the recent experiments in transatlantic television via the cable ${ }^{\star}$, it is interesting to recall some very early history. I understand that the present technique is to transmit the successive frames of a film at slow speed by means of a special telecine machine and record them on the other side of the Atlantic. The film is then televised in the normal way after processing.

In 1934, on the occasion of the London to Melbourne Air Race, the G.B. Newsreel Company used the normal Radio Facsimile Service to transmit from Australia the separate frames of a cinematograph film of the winners arriving in Melbourne. The received pictures were rephotographed on to cine film in London. I believe it took about 20 hours facsimile transmission for a few seconds of film projection, but the attraction of seeing the film in the cinemas the day after the event more than justified the means. As in the present case some "compression " of the signal was achieved by omitting alter* See pp. 314 and 362 of this issue.-Ed.
nate frames of the film at the transmitting end and replacing them by repeats of the previous frame in the final printing process.

Mr. Castleton Knight, who pioneered this experiment, expressed surprise to me some time ago that "Wireless pictures" as he called them, had not become a daily occurrence. His record has remained unchallenged for 25 years and it would be a pleasant gesture if the results of his efforts were taken from the vault where they now rest and televised for our enjoyment along with those of the present experiment.

Enfield, Middlesex.
L. C. JESTY,

Sylvania-Thorn Colour Television Laboratories, Ltd.

## Wide-Band Aerials

I HAVE read with interest the two articles by Mr . F. R. W. Strafford in the April and May issues entitled "A Second Band III Programme?-The Aerial Problem."

I think it should be pointed out to your readers that a very satisfactory solution to this wide-band aerial problem exists. The type of aerial to which I make reference is known commercially as the Labgear "Spacematch," which became available on the market in August 1958.

The "Spacematch" aerial, at Band III frequencies, is essentially a form of long wire array having "V" configuration. The length-to-diameter ratio has been made quite low by adoption of the skeleton cone principle. By a proper choice of element diameter and included angles the impedance at the extremities of the aerial may be made to approximate the characteristic impedance of free space. Under idcal conditions, using this technique, the gain normally associated with a " $V$ " beam type of aerial may be further enhanced to the extent of 3 dB . I agree with Mr. Strafford that a wide-band aerial providing a gain of about 9 dB would be extremely valuable and, indeed, it would suit most applications inbetween circumstances permitting the use of simple inside aerials and those requiring extremely elaborate high-gain fringe arrays. Naturally television broadcasting stations have been so situated as to minimize the number of fringe arrays required.

In practice, individual elements of the "Spacematch" aerial have been made approximately $1 \frac{1}{4}$ wavelengths long on Band III, which brings the unit into $\frac{1}{2}$-wave resonance just outside the low frequency end of Band I. However, because of its fan-like construction, it exhibits the broad width associated with this type of aerial and provides remarkably uniform response not only over Band III but also over the whole of Band I. Naturally, the excellent gain yielded on Band III (8 or 9 dB ) cannot be maintained on Band I and its performance is similar to that of a simple dipole. Models are available, however, which incorporate the addition of a channelized Band I reflector where reception conditions make this necessary.

Cambridge.
S. R. KHARBANDA,

Labgear Limited.

## Displaying Valve Characteristics

I WAS most interested to read of Mr. R. G. Christian's method of displaying valve characteristics and their axes in the June issue.

The author appears to be satisfied with presenting what are, in effect, dynamic characteristics, and a change in anode load therefore affects these characteristics. From the students' point of view this is undesirable, and it is much better to use the actual anode voltage to give the $\mathbf{X}$ deflection, rather than the supply voltage, since the static characteristics would then be given as shown by the accompanying Fig. 1.

If a step voltage waveform is applied to the grid, the valve load line can ba displayed as a shortening of the high-voltage ends of the traces. (Fig. 2). This property extends the usefulness of the demonstration because dis-


Fig. I. Beam tetrode charocteristics.

Fig. 2. Triode anode choracteristics. showing load line.


Fig. 3. Triode anode characteristics with current negative feedback.

Fig. 4. Low-power transistor emitter characteristics.

cussion can be made of the choice of a suitable anode load. The effect of negative feedback on the characteristics can be shown by the use of feedback circuits in common use. In particular, the effect of current negative feedback on output impedance can be demonstrated if a series resistance is used in the cathode lead. (Fig. 3).
In addition, if the step voltage is applied through a high resistance, a step current waveform can be obtained, which may be used to show the emitter input characteristics of transistors (Fig. 4). A high resistance should be put in series with the collector supply to ensure that the thermal runaway point is not exceeded.
The problem of the return trace, as mentioned by Mr. Christian, may be overcome by flyback blanking.

The accompanying photographs were obtained from a device showing several anode characteristics simultaneously, which has proved most useful in the work of the B.B.C. Engineering Training Department and it is described in the Bulletin of Electrical Engineering Education, Vol. 20, June 1958 (published at the College of Science and Technology, Manchester).
Wood Norton, Worcs. D. J. HENMAN,
B.B.C. Engineering Training Dept.

# Resistors in Parallel 

## CHART FOR USE WITH PREFERRED-

value resistors

By M. A. HAMMOND

THE accompanying chart provides a quick reference to the preferred-value resistors which, when connected in parallel, give a required non-preferred value of resistance.

Example: A resistance of 30 ! is required. At the 30-! ! point of the right-hand scale move horizontally to the left until a point of intersection of two diagonal lines is encountered. By following each of these diagonals from the intersection to the left-hand scale, it will be seen that $47 \Omega 2$ and $82 \Omega$ are the required preferred values to be paralleled for a resultant 3042 .
Alternative points of intersection can be found very close to the $30-\Omega$ line formed by intersections of the $39-12$ and $120-2$ lines and of the $56-!$ and $68-\Omega$ lines respectively (left-hand scale).

It is obvious that this will apply to the higher decades also if the necessary " noughts" are added to the significant figures and providing both resistors to be paralleled are in the same decade. For example, the resistance resulting from paralleling 18 k ! ? and 180 2 cannot be extracted from the chart.
Acknowledgement is made to J. W. D. Cunningham and L. F. Poole, for observations made while compiling the chart.


## Small Radar for Small Ships

As$S$ the "mains supply" most usually available on a small vessel is a nominal $24-V$ d.c. derived from accumulators, power consumption must be kept to a minimum and the radar must work from an input which may vary between 20 V and 32 V . The voltage-variation

problem is overcome in the new Marconi Marine "Consort " by the use of a transistor regulator which reduces the input to a constant $19-\mathrm{V}$ d.c., and e.h.t., h.t., negative bias and special supplies (such as the c.r.t. heater power) are derived from this $19-\mathrm{V}$ d.c. by a transistor oscillator. To reduce the power de7 mand the equipment is normally ,kept in the "stand-by" condition in which the valve heaters only are energized and the current consumption then is 4A. A "press-to-view" button, mounted on the display unit, switches on the remaining supplies and the scanner motor, when the current consumption rises to about 10 A . After roughly two minutes (governed by the heating and cooling of a bi-metal strip)

Radome-protected scanner on its tripod base, installed on Marconi-Marine's demonstration yacht, Elettra II.
the radar reverts automatically to the stand-by state.
Voltage regulator, power supplies, transmitter and receiver are all contained in one case and printed wiring is used as far as is possible for its advantages of low cost and exact correspondence between boards.

The scanner employs a 3 - ft -long slotted-waveguide array driven by a $1 / 24$-horse-power motor. The use of this small drive power is made possible by enclosing the array in a fibre-glass radome which also prevents the ingress of sea spray. Fibre-glass is used, too, as the support for a "lens" formed from thin close-spaced vertical wires. This is mounted at the mouth of a short horn section extending from the waveguide aerial and it is used to reduce the amplitude of residual side-lobes.

Scanner-mount height limits the maximum range realisable to about 14 miles: other scales are $8,4,1.5$ and 0.6 miles. Only a relatively small transmitter power is required to give effective cover to 14 miles so the peakpower output (p.w. $0.15 \mu \mathrm{sec}$, p.r.f. $2,000 / \mathrm{sec}$ ) of about 2.5 kW is sufficient. Because the magnetron does not heat up appreciably at this low rating, its frequency does not drift seriously. This initial stability, together with a greatly-improved version of the 723AB localoscillator klystron (English Electric) and a little " spare" bandwidth in the receiver, enables the complications of a.f.c. to be dispensed with. In fact, the fine-tuning control is preset, mounted on the display-unit rear panel.
The display unit, which is designed for mounting on the deckhead, bulkhead or table, uses a 5 in -diameter c.r.t. This is fitted with a magnifying lens to increase the effective diameter to about 8 in. Rotating-coil scan-
ning is used for which the drive is obtained by a direct mechanical link (Bowden cable) to the scanner and the only "user control" fitted on the display unit is the press-to-view switch.
A complete installation weighs just over one hundredweight and costs about $£ 800$.

## Sound Equipment at Stratford-on-Avon

NEW sound-amplifying equipment has been fitted at the Shakespeare Memorial Theatre, Stratford-on-Avon. Designed and installed by R.C.A. (Great Britain), Ltd., the equipment provides single-channel speech reinforcement from three microphones on the stage and a $40-\mathrm{W}$ amplifier feeding four line-source column loudspeakers placed in the auditorium, a two-channel sound-effects system (fed from two tape decks) with two amplifiers and five loudspeakers which may be placed anywhere on the stage, another single "effects" channel feeding a loudspeaker mounted over the stage, and a stage/ orchestra liaison system through which the orchestra can follow the action although they are unable to see the stage. The signal to each of the five loudspeakers can be raised and lowered in turn, so that an impression of movement may be created. All four amplifiers are identical and they can be inter-switched so that a failure in one is not obvious to the audience.

## SIIHTT-WAVE CONIITIONS

Prediction for fuly


## Prediction for August



THE full-line curves indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications nver four long-distance paths from this country during July and August.

Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period.


## Wire-stripping Screwdriver

THE "Stripmaster" is a screwdriver which carries in its shatterproof moulded-plastics handle a metal cutter with a keyhole-shaped aperture. The cutter forms a quick and effective wire stripper: in use the wire is passed through the large end of the "keyhole", forced down the slot and then pulled out, so stripping cleanly the insulation without "nicking" the wire. The overall length of the screwdriver is 6 in and the screwdriver

blade-width is $\frac{1}{8} \mathrm{in}$. Retailing at 3 s 6 d , the "Stripmaster" is distributed by L. J. Hydleman and Co., Ltd., Grove Park, London, S.E. 5 .

## Sub-miniature Wire-tound Resistors

THE Alma Components Type RM2 precision subminiature wire-wound resistor is rated at $\frac{1}{10} \mathrm{~W}$ and is designed to fit into both the 0.1 -in and 0.15 in printed circuit grids. Only 0.25 -in in diameter and slightly over 0.3 -in long, this resistor is available in values from 1000 to $200 \mathrm{k}!$, and with two standard tolerances ( $\pm 1 \%$ and $\pm 0.1^{\circ}, 1$ ) at $20^{\circ} \mathrm{C}$. The temperature coefficient is less than $\pm 0.002 \%^{\circ}$ per ${ }^{\circ} \mathrm{C}$ and a stability of $0.05 \%^{\prime}$ over 1,000 hours running time is achieved. Manufacturers: Alma Components Ltd., 55I, Holloway Road, London, N. 19.

## Electronic Coil Winder

PRECISION winding of multi-layer coils withour paper interleave and with wires down to 0.002 in in diameter (No. 47 s.w.g.) is one of the features of the new Douglas electronic coil winder described as the "Supermatic Layer Winding Machine."
Separate electrical drives are used for the headstock


Douglas (Avo) electronic-controlled coil winder.
and for the wire traversing mechanism and any deviation from exact layer winding with adjacent turns touching is immediately corrected by means of a "sensing" head on the traversing carriage and asoociated electronic apparatus. Another feature of the new coil winder is that it can be set up to wind singlelayer coils with precise spacing of the turns, the spacing being maintained as predetermined by the electronic equipment.

The makers are Avo Ltd., Avocet House, 92-96. Vauxhall Bridge Road, London, S.W.1.

## Q-meter

THE new Marconi Type TF1245 Q-meter incorporates separate low and high frequency circuits to enable $Q$ values from 5 to 1,000 to be measured at frequencies between $1 \mathrm{kc} / \mathrm{s}$ and $300 \mathrm{Mc} / \mathrm{s}$ with an accuracy which decreases with increasing frequency from $\pm 5 \%$ at $100 \mathrm{Mc} / \mathrm{s}$ to $\pm 20 \%$ at $300 \mathrm{Mc} / \mathrm{s}$. Both the l.f. and h.f. measurement circuits are of the usual series-resonant type in which the $Q$ is obtained from a measurement of the voltage across the tuned circuit capacity. The signal voltage is injected across a $0.02 \Omega$ resistor in the l.f. circuit and a $0.1 \mathrm{~m} \mu \mathrm{H}$ inductor in the h.f. A 8 Q range of $\pm 25$ is also provided. An external oscillator is necessary to make measurements, and two specially designed units are available, the TF 1246 covering $40 \mathrm{kc} / \mathrm{s}$ to $50 \mathrm{Mc} / \mathrm{s}$ and the TF1247 covering $20 \mathrm{Mc} / \mathrm{s}$ to $300 \mathrm{Mc} / \mathrm{s}$. Matching transformers may be obtained to allow these oscillators to be used also as general-purpose signal generators.


Marconi Q-Meter Type TFI 245 (right) with external oscillator Type TFI 247 (left).

The TF1245 Q-meter costs £176 and the address of its manufacturer is Marconi Instruments Ltd., St. Albans, Herts.

## Low-frequency Power Amplifier

A SINE-WAVE output power of 100 watts (r.m.s.) with a distortion less than $2 \%$ may be obtained at any frequency from $10 \mathrm{c} / \mathrm{s}$ to $5 \mathrm{kc} / \mathrm{s}$ from the Grampian v.l.f. amplifier. The input inpedance is $10 \mathrm{k} \Omega$ and 3 V is required for full output. Output impedances between $10 \Omega$ and $100 \Omega$ are available according to requirements, and the frequency response is flat within $\pm \frac{1}{2} \mathrm{~dB}$. This amplifier costs £360 or more according to the number of


Grampian v.l.f. amplifier with Ediswan Type R666 input oscillator.
than 100 M ? at $130^{\circ} \mathrm{C}$ to be achieved and the black epoxy-resin encapsulation material does not support combustion. Also a range of pulse transformers developing between 7 kV and 50 kV at up to 60 MW peak power is available. The manufacturers are Wayne-Kerr Laboratories of Roebuck Road, Chessington, Surrey.
output tappings or other special modifications required. The address of its manufacturer is Grampian Reproducers Ltd., Hanworth Trading Estate, Feltham, Middlesex.

## Paraffin Power for Porlables

A NEW version of the thermo-electric, receiver power supply (Type T.E.G.1) previously illustrated on p. 227 of our May, 1956, issue is now available in this country. The doped zinc-antimonide and constantan


Thermo-electric generator supplying power to an "all-dry" portable receiver.
couples normally give outputs of 80 to 90 V at 10 to $11 \mathrm{~mA}, 1.0$ to 1.2 V at 0.21 to 0.52 A and 8 to $10-\mathrm{V}$ gridbias: it is thus suitable for many "all-dry" receivers. The T.E.G. 1 is imported from the U.S.S.R. by International Technical Developments, Ltd., of Willow Road, Poyle Estate, Colnbrook, Buckinghamshire, and it costs £16, or $£ 20$ with lamp.

## Resin-cast Transformers

WAYNE-KERR LABORATORIES have introduced a range of resin-cast transformers in ratings between 5 and 350 W . Designed to replace oil-filled units where the possibility of oil leakage cannot be tolerated, the transformers use C-core construction and comply with the requirements of R.C.S.214. Vacuum impregnation with a polyester resin enables insulation resistances of better

## Fixed Capacitors

A RANGE of isolation and suppression capacitors covering values between 470 pF and $10,000 \mathrm{pF}$ is announced by T.C.C. The dielectric is high-permittivity ceramic and a non-cracking heat-resistant protective coating prevents the ingress of moisture and provides insulation sufficient for the capacitor to be mounted in contact with other components or the chassis, whilst still complying with the requirements of B.S.415-1957. The maximum rating is 500 d.v. ( 300 r.m.s. a.v.), capacity tolerance is $-20+80 \%$ and the capacitors also comply with B.S.2818-1957 (for fluorescent-lighting interference suppression).

A new T.C.C. range of low-working-voltage paperdielectric capacitors has each foil electrode wound with two thicknesses of paper; but with improved machinery and new materials the physical size is comparable with that of the metallized-paper type. With a maximum d.v. rating of 150, the Type 143 is made in capacities from $0.02 \mu \mathrm{~F}$ to $0.5 \mu \mathrm{~F}$, the sizes ranging between $\frac{5}{8}$-in long by $\frac{1}{4}$-in diameter and $1 \frac{3}{8}$-in long by $\frac{9}{96}$-in diameter respectively. The capacity tolerance is $\pm 20 \%$ and the temperature range is -30 to $+60^{\circ} \mathrm{C}$. Manufacturers: The Telegraph Condenser Co., Ltd., London, W.3.

## Two X-band Isolators

ONE of the new Sanders (Electronics) ferrite isolators is a small-size unit for use in commercial systems. It has an isolation of better than 35 dB over a $\pm 500 \mathrm{Mc} / \mathrm{s}$ bandwidth around any required frequency between 8.2 and $12.4 \mathrm{kMc} / \mathrm{s}$. Its insertion loss is 0.7 dB , and its input voltage standing wave ratio better than 0.9 to 1 . Up to 150 W mean power can be handled by this unit, and it costs £35. The other isolator is for laboratory use over the broad frequency band from 8.2 to $12.4 \mathrm{kMc} \mathrm{c} / \mathrm{s}$. Its isolation is at least 30 dB , its insertion loss less than 1 dB and its input v.s.w.r. better than 0.87 to 1 . Up to 15 W can be handled by this unit and it costs $£ 85$. Both these isolators are manufactured by W. H. Sanders (Electronics), Ltd., of Gunnels Wood Road, Stevenage, Herts.


Sanders broadbond microwave isolator.

# Equatorial Sunset Effect 

Observations Over a Whole Sunspot Cycle Point to an Unexplained Propagation Anomaly

By A. M. HUMBY,* M.I.E.E.

N August, 1947, a year of high solar activity (Fig. 1), the writer observed at Singapore that teleprinter operation of the Admiralty circuit to London became extremely difficult, if not impossible, from about 1900 to 2100 local time Singapore, i.e., 1200 to 1400 G.M.T., a condition which the operating personnel (often only too ready to blame the man at the other end) referred to, in those days, as the "Whitehall Lunch-time Effect"!
The circuit had been equipped with suitably directive aerials at each terminal for operation on a number of frequencies between $4 \mathrm{Mc} / \mathrm{s}$ and $22 \mathrm{Mc} / \mathrm{s}$, according to the time of day, season and epoch of the 11-year solar cycle.
For distances exceeding $4,000 \mathrm{~km}$ propagation takes place by a number of complex modes, and it has been found empirically that, for a given frequency, propagation via the $\mathrm{F}_{\mathrm{w}}$-layer is usually practicable so long as the ionosphere at "control
*Royal Naval Scientific Service.


Fig. 1. Mean Zurich sunspot numbers for the years 1946 to 1958 inclusive.


Fig. 2. The "control points" mentioned in the text; $S_{1} S_{2}$ on Singapare/London and $C_{1} C_{2}$ on Colombo/London greatcircle paths respectively.
points," distant $2,000 \mathrm{~km}$ from each terminal (Fig. 2), supports transmission at that frequency irrespective of the condition of the ionosphere elsewhere along the great-circle path. If this condition is not satisfied at each "control point" a change to a lower frequency is usually necessary.
In certain cases E-layer propagation may be possible. the investigation of which involves two additional "control points" distant $1,000 \mathrm{~km}$ from each terminal.

The extent to which the frequency may be lowered depends upon such factors as the effective radiated power of the transmitter, absorption of signal, and the level of atmospherics and the type of aerial at the receiving terminal. The condition of the ionosphere at any given location is assessed from regular ionosphere soundings carried out at a large number of measuring stations throughout the world, and from this data groups of charts are prepared on a month-to-month basis representing world-wide variations


Fig. 3. Upper and lower predicted frequency limits for radio-teleprinter operation between cingapore and London, August 1947.
of ionization with the time of day, season and solar activity.

Considerable success is now being achieved by ionospheric forecasters in determining the most probable upper- and lower-frequency limits in any given case, and fortunately for the radio engineer discrepancies between prediction and practice are gradually being eliminated.

Predictions of the type referred to above for the case of the Singapore/London circuit for August 1947 are shown in Fig. 3, from which it would appear that a wide band of frequencies should have been suitable for teleprinter operation between 1200 and 1400 G.M.T.; in point of fact although communication on several frequencies within the predicted limits was attempted, this period, as stated


Fig. 4. Communication conditions on Singapore/London and Colombo/London radio circuits near local sunset (equatorial region) for equinox months of 1949.
earlier, was one which proved in practice to be one of extreme difficulty.

The period 1900 to 2100 local time Singapore, i.e., shortly after sunset, was characterized by :-
(a) A reduction of signal intensity in each direction of the Singapore/London circuit.
(b) Excessive multipath distortion arising from the reception of a number of echo signals arriving over different radio paths with sufficiently large time delays to prohibit operation of the circuit at normal teleprinter speed ( 50 bauds).
However, on many days the signal-to-noise ratio was adequate to permit Morse operation at slow speeds (e.g., 15 to 20 bauds), where, on account of the much longer time intervals between transmitted signal elements, multipath effects were less troublesome. Reception in these cases was carried out either by ear, or by undulator recorder, methods which in themselves are less sensitive than the teleprinter one to multipath distortion.
(c) Direction of arrival of incoming signals being diffused, or "flat," suggesting considerable azimuthal scattering of the received energy.
With the introduction in the autumn of 1949 of hourly circuit-merit figures indicative of the diurnal performance of all Admiralty radio-teleprinter circuits, it became apparent that a similar, though somewhat less pronounced, difficult period was also being experienced daily on the Colombo/London circuit from about 1900 to 2100 local time Colombo, i.e., 1400 to 1600 G.M.T.


Fig. 5. Upper and lower predicted frequency limits for radio teleprinter operation between Colombo and London during August 1949.


Fig. 6. Number of teleprinter operating days on Singapore/ London radio circuit for equinox and solstice months of 1949/1950.

Figs. 4(a) and 4(b) show the deterioration in performance of these two citcuits near local sunset at Singapore and Colombo respectively for the months of August, September and October, 1949.
As in the case of the Singapore/London circuit, frequency predictions for the Colombo/London circuit based on the "two control-point" method ( $C_{1}$ and $C_{2}$ of Fig. 2) indicated that a reliable teleprinter circuit should have been practicable during the above period of the day (Fig. 5).
Further investigation disclosed that the above difficulty on each circuit was essentially a condition peculiar to the equinox as distinct from the solstice. Let us compare, for example, the performance of the Singapore/London circuit for the six equinox months [Fig. 6(a)], with that for the six solstice
months [Fig. $6(\mathrm{~b})$ ], of the twelve-month period August, 1949, to July, 1950, inclusive.
The continuation of such records throughout the period 1949 to 1958 inclusive has provided confirmation that the effect under discussion was substantially non-existent in solstice months.

The performance of the Singapore/London and Colombo/London circuits for equinox months are compared in Fig. 7 for each year commencing 1949 and ending 1958, and it will be seen, by reference to the annual solar indices shown in Fig. 1, that the equatorial-sunset effect under discussion was associated with years of high solar activity.

To summarize.-The effects described above relate to difficulties of communication with terminals situated in equatorial areas, the salient feature being a considerable azimuthal scattering of signals for about two hours near local sunset at the equatorial terminal, notably during the equinox months of years of high solar activity.

Directly related to this phenomenon would appear to be that reported by Osborne ${ }^{1}$, as part of the work of the Radio Research Board. He has drawn

(a) SIMGAPORE/LONDON

Fig. 7. Number of teleprinter working days on Singapore London and Colombo/London circuits during equinox months from 1949 to 1958 inclusive.
attention to the disintegration of the $F_{2}$ layer at Singapore near the time of local sunset during equinox months; and has referred to the possibility of the frequency of occurrence of this equatorial scatter being greatest at the maximum of the 11year solar cycle. The effect in practice, he states, is that reflected signals from the $F_{2}$ region are not always intelligible, even though the signal strength may be high, whereas at the solstices propagation conditions are better at these hours, when the layer often remains intact throughout the evening.
Some light on the extent to which circuits to other equatorial points are affected in this way has been thrown by Hitchcock ${ }^{2}$ who has drawn attention to the fact that during the autumn of 1956 many radio circuits operating in low latitudes suffered severe propagational difficulties shortly after local sunset. This took the form of severe fading, or weakening, of signals sufficiently serious to degrade, or interrupt, the services. In all cases, he states, the normal operating frequency, and the alternative frequencies used in an attempt to maintain communication, were well clear of the predicted upper and lower limits. And he adds, moreover, that the effect was not generally noticeable on circuits during sunspot minimum years.
In view of the apparent correlation between the circuit data from various sources and the results of ionospheric soundings, it is possible that there is a fundamental obstacle to the sky-wave operation of tropical, or partly tropical, circuits under the conditions which have been referred to.

Since the last war the number of high-frequency circuits has considerably increased, and the period 1947 (high solar activity) through 1954 (low solar activity) to 1958 (exceptionally high solar activity) has thus afforded an excellent opportunity of studying many of the effects of the solar cycle on communication by ionospherically reflected rays.

In this connection it is perhaps not without interest to recall the following statement made by Appleton in 1947 " " Sir Edward Appleton (in reply): I strongly support Dr. Smith-Rose's plea for continued, and indeed extended, post mortem examination of operational results. Only in this way is it possible to check the accuracy of our ionospheric predictions. Moreover, nature has many surprises for us in work of this kind, and, with a laboratory as large as the earth itself, it is only with the cooperation of an army of radio operators that we can ensure that many interesting abnormalities do not escape attention."

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# Elements of Electronic Circuits 

## 4.-USE OF SHORT TIME CONSTANT CIRCUITS WITH DIODES AND TRIODES

By J. M. PETERS, B.Sc. (Eng.), A.M.I.E.E., A.M. Brit. I.R.E.

WE have seen in Part 1 (April issue) that the application of a square waveform to a CR circuit of very short time constant compared with the recurrence period results in a distorted waveform across the resistor. In the extreme case, when the time constant is very much less than the period, the output becomes a spike and approximates to the mathematical differential coefficient of the input wave. In other words, the shape of the output wave corresponds to the rate of change, with respect to time, of the input voltage wave; hence the term " differentiation."

Now let us examine what happens when a diode is connected in parallel with such a $C R$ circuit (Fig. 1). The recurrence period of the square wave


Fig. I.
input is assumed to be 1 millisecond whilst the time constant is 1 microsecond.

Immediately the diode anode is driven positive by the square wave the diode conducts. As the rise time of the applied wave is finite, i.e., cannot occur instantaneously, the spike $X$ shown dotted in Fig. 2
$V_{\text {APP }}$

(a)

(b)

Fig. 2.
does not appear in practice and a small positive "blip" results. In effect, the diode clamps the positive excursion of the input wave to zero (Fig. 2 (a)). The negative excursion of the differentiated wave remains; the portion YZ is the result of C discharging through $R$. If the diode connections are reversed the spike appears all positive, as shown in Fig. 2 (b).

By means of this simple device it is therefore possible to derive waveforms consisting of very sharp positive- or negative-going spikes of the repetition frequency of the applied square wave.

If the same short time constant CR circuit is connected in the grid circuit of a triode (Fig. 3)


Fig. 3.
and a square waveform applied as before the result is as shown in Fig. 4. The triode's grid and cathode take the place of the diode's anode and cathode respectively and the spiked waveform now appears at the grid. As the negative excursions of the spike


Fig. 4.
drive the triode beyond cut-off the resultant waveform at the anode appears as short positive-going square-topped pulses. The valve therefore performs a "squaring" function.

If instead of coupling the grid leak to earth it is taken to h.t. (Fig. 5), then an even narrower


Fig. 5.


Fig. 6.
square-topped anode voltage pulse can be obtained (Fig. 6). In this arrangement C discharges exponentially towards the h.t. voltage. The voltage/time gradient is steeper than when R is connected to earth and the anode voltage pulse is consequently narrower.

In the examples shown the maximum excursion of the square pulse is $\pm 50$ volts, C is instantaneously charged to 100 volts, while the h.t. voltage is assumed to be 300 volts. It will be scen that the effective voltage in Fig. 6 is therefore 400 volts, compared with only 100 volts in Fig. 4.

Short Pulses from a Sine Wave.-It is possible for a distorting amplifier followed by a stage of bias differentiation (Fig. 7) to convert a sinc wave into a narrow square-topped trigger or sync pulse. This is illustrated in Fig. 8.

Grid limiting by the distorting amplifier V1 produces an approximately square waveform at the anode of V1. Differentiation by the short time constant CR circuit and squaring of the spike by V2 results in the V2 anode voltage waveform shown.


Fig. 7.



Fig. 8.
The repetition frequency of this pulse, which can be used for triggering or synchronizing purposes, is that of the applied sine wave.

The usefulness of a pulse of this kind will be appreciated later when its application as a trigger pulse for circuits such as the multivibrator will be described. As already described, a narrower pulse can be obtained by connecting R to h.t. instead of to earth.

Technical Digests are aygain to be issued monthly by the D.S.I.R. Each month's digest will consist of fifteen summaries of ideas and techniques recently published in this country's 300 ol so technical periodicals. Each summary will be presented on a separate sheet. A year's subscription costs three guineas and particulars are obtainable from the D.S.I.R. Charles House, 5-11, Regent Street, London, S.W.1.

# International Transistor Convention 

1.-NEW SEMICONDUCTOR TECHNIQUES AND APPLICATIONS DESCRIBED

A

LTHOUGH the seats in the Earls Court lecture halls gave more the sensation of a surface barrier than a comfortable diffused junction as one would have wished, it is a tribute to the quality of the papers presented at the I.E.E.'s Transistor Convention that all sessions throughout the six-day event had large and attentive audiences. There were about 2,000 delegates altogether, of whom 400 were from 26 overseas countries. Particularly crowded was the opening session, which had the special attraction of introductory lectures by the joint inventors of the transistor, Professor Bardeen, Dr. Brattain and Dr. Shockley-a triumvirate which the Supporting Chairman, G. Millington, mysteriously linked with Faith, Hope and Charity.
While Professor Bardeen and Dr. Brattain outlined the history and recent development of the transistor, Dr. Shockley seized the occasion to talk about the principal product of his company, the four layer p-n-p-n junction diode, or "transistor diode" as he called it. This device, with its negative resistance characteristic (see October 1957 issue, p. 502), is becoming an important competitor to the conventional transistor in switching circuits because of its much greater power handling capacity. Dr. Shockley predicted that in two or three years transistor diodes will attain power levels 10 to 100 times higher than equivalent transistors with comparable frequencies and efficiencies. One recent experimental device was capable of switching on 1kW in 20 millimicroseconds (or nanoseconds, as Continental speakers preferred it).
The great problem in this high power work, Dr. Shockley explained, was to produce a uniform avalanche current multiplying effect over large-area junctions, and he mentioned two new operating principles, called impulsive charging and majority carrier extraction, by which this effect could be achieved.

Many organizations are developing the basic $\mathrm{p}-\mathrm{n}-\mathrm{p}-\mathrm{n}$ structure and in some cases a third connection is made, analogous to the grid of a thyratron valve, to give a controlling or gating action. One example is the controlled silicon rectifier, of which some applications in industrial power control were described by H. S. Lowry. As distinct from the thyratron, the silicon controlled rectifier (as it is called) needs current pulses of about 1A for triggering purposes, and circuits were described using Unijunction transistors (January 1957 issue, p. 40) to provide them. One method of manufacturing $\mathrm{p}-\mathrm{n}-\mathrm{p}-\mathrm{n}$ devices was presented in a paper by R . Freestone. This consisted of forming an $\mathrm{n}-\mathrm{p}-\mathrm{n}$ structure by the "melt-back" system, in which impurities are segregated by controlled cooling in a furnace, and then adding the extra p-type layer by alloying a pellet of indium on one end.
While some delegates were probably surprised to hear talk about switching hundreds of amperes by semiconductor devices, others must have been
equally astonished at the discussions on transistors working at hundreds of megacycles (one was described for $3,000 \mathrm{Mc} / \mathrm{s}$ ). This very high frequency operation is made possible largely by diffusion manufacturing techniques, in which extremely thin base layers are produced by diffusing impurities into the surface of the semiconductor. The supreme example of this at the moment is the " mesa" transistor (see p. 350). Diffusion technique also makes possible the grading of impurities to give accelerating electric fields in the base layers of drift and alloy-diffused transistors. Unfortunately the high concentration of impurity on the emitter side leads to low emitter-base breakdown voltages, which can be a problem for circuit designers. One paper, by W. Fulop, suggested how this could be overcome by inserting an extra layer of high resistivity material between the emitter and the graded base. Analysis showed that the breakdown voltage would be improved without unduly affecting the frequency response.

Diffusion techniques are also important for another reason. They are very convenient for manufacturing " solid circuits," in which integrated circuit assemblies of transistor, diode, resistance, capacitance and conducting elements are produced electro-chemically on extremely small wafers of semiconductor material. A paper by T. M. Liimatainen described the use of photo-lithographic and photo-engraving methods for etching away selected areas of a semiconductor wafer into which a base layer had been previously diffused. When metal contacts and electrodes have been deposited and alloyed with the semiconductor the result is a "printed transistor". It can take the form of an individual package or be part of an integrated circuit assembly. Multiple units can be produced on a single semiconductor wafer. Typical examples have common-emitter current gains of 15 and alpha cut-off frequencies of $48 \mathrm{Mc} / \mathrm{s}$.

## Dielectric Devices

An entirely new class of semiconductor devices, known as dielectric diodes and triodes, is likely to arise out of recent research by various workers on space-charge-limited currents through insulating crystals (see p. 350). These currents are analogous to those flowing through the insulating vacuum of the thermionic valve. A paper by G. T. Winch described experiments on crystals of cadmium sulphide, through which steady current densities of several amperes per square centimetre had beer obtained with only a few volts applied.
The idea of space charge also came into a group of papers on the theory and measurement of transistor parameters. Ever since transistors began to be used extensively for switching and pulse work it was realized that the established small-signal a.c. theory, based on such things as alpha cut-off fre-

# and Exhibition 

## AT THE CONVENTION

quency, effective base resistance and collector capacitance, was not very helpful for non-linear operating conditions. In 1957, Beaufov and Sparkes, who presented papers at the Convention, introduced a new approach to transistor operation based on the concept of charge control. The central idea of this was that a number of current carricrs (say holes in a p-n-p transistor) was necessary between emitter and collector to sustain the current, and this number represented a stored "charge" which varied with the working point.

The so-called charge-control parameters worked out on this basis proved a very convenient way of dealing with large-signal transients in switching circuit design, and at the Convention several speakers paid tribute to its usefulness. J. J. Sparkes presented a paper on the measurement of these parameters (e.g. collector time constant is defined as $\mathrm{QB}_{\mathrm{B}} / \mathrm{I}_{\mathrm{C}}$, base charge over collector current), while R. Beaufoy showed how they are used in switching circuit design. Another paper, by A. Kruithof, demonstrated that the charge-control concept lends itself very weli to a graphical representation of transient response.

## Charge-Control Theory

Taking the idea even further, R. D. Middlebrook expounded a whole new theory which integrated the valve and the transistor on the basis that both are fundamentally charge-controlled devices, not voltage-controlled and current-controlled, respectively, as we are accustomed to regard them at present. One example of the approach is that in a charge-controlled device the transit time of charge carriers across the active region is inversely proportional to the $n$th power of the total charge in transit; $n$ being 0 when the current is diffusion limited in semiconductors, $\frac{1}{2}$ when it is space-charge limited in vacuo and 1 when it is space-charge limited in semiconductors.

Professor Middlebrook also conducted an experiment in subliminal perception by presenting about a dozen lantern slides loaded with mathematics in quick succession, but in spite of this his interesting paper was very favourably received. It should be well worth studying in more detail when the Proceedings are published by the I.E.E. Particular praise came from speakers who were concerned with the present unsatisfactory state of technical education in semiconductor, as compared with valve, theory and practice.

On the manufacturing side, one or two papers discussed the relative advantages of the three basic junction-forming techniques-alloying, growing and diffusion-in such factors as cost, complexity and reproducibility. It emerged that the diffused base transistor was likely to be the great thing of the future. There was no doubt that this device had a wider field of application than the others. It was
more complex and costly to produce at the moment, but the possibility of processing the junctions in large batches, combined with the wide market, would undoubtedly bring down the price in the future. The alloy junction transistor was notable for its design flexibility but showed potential disadvantages in cost and was poor in reproducibility. By contrast the grown-junction transistor had cost advantages due to reduced complexity and better reproducibility, but was lacking in design flexibility.

Reliability of transistors also came in for some discussion, and certain speakers were obviously worried by conflicting evidence in the papers concerned with it. For example, R. Brewer and W. W. D. W'yatt, in a reliability appraisal based on life tests, stated that there was no evidence of any major changes taking place which would constitute a "wearing-out" process in semiconductor devices. On the other hand, F. F. Roberts, J. C. Henderson and R. A. Hastie, describing an accelerated ageing experiment on germanium alloy transistors, mentioned that a rapid increase of collector-base leakage current (and noise) had occurred in some units at little more than 2,000 hours. This had been almost the sole cause of failure; current gains had shown deterioration only after the onset of the excessive leakage.

Two other deleterious effects, with the sinister names of "creep" and "wiggle," were mentioned. The first is a variation of reverse current produced when a sustained reverse bias is applied to a p-n junction. The second is a variation of transistor input capacitance (and conductance) with frequency, probably due to electron storage in the emitter-the "wiggle" being the distorting effect on pulse and switching waveforms.

Incidentally, one speaker made a strong plea to manufacturers to give more comprehensive technical data on semiconductor devices, particularly on their performance at different temperatures. He remarked that the tabular data usually presented was quite inadequate for design purposes. (Loud applause from the audience.)

On the applications side, there were very few papers concerned with domestic radio, television and audio circuits, and none on hearing aids, but d.c. amplifiers received some attention. A large number of contributors, however, dealt with the applications of transistors in line communications and data processing. In both of these fields, where amplifying or switching devices are needed in large quantities, the small size and low power consumption of the transistor make it an ideal component. The communications papers covered digital speech transmission systems as well as straightforward amplification in carrier telephony, while the data processing papers covered telephone switching as well as digital computing.

In the field of computing, circuits are now being developed to operate at puise rates of $50 \mathrm{Mc} / \mathrm{s}$ and above, with pulse rise times of only 1 or 2 millimicroseconds. As examples, G. B. B. Chaplin described a $50-\mathrm{Mc} / \mathrm{s}$ binary scaler using micro-alloy diffused transistors and showed a transistor-generated pulse of a few millimicroseconds on a $30-\mathrm{m}$ "/sec transistorgenerated c.r.o. timebase.

At these frequencies transistors have the advantage over valves, not only because of their lower impedances but because they can be packed very much closer together to minimize transmission time delays of pulses. There is, in fact, a limit on the
dimensions of a computer for such work since the transmission time delays of the wiring become significant and the required timing arrangements and speed of operation could be adversely affected. Mr. Chaplin demonstrated this fact most effectively by causing his millimicroseconds pulse to travel down a line a few feet long and be reflected from a short circuit to appear on the $30 \mathrm{~m} \mu \mathrm{sec}$ timebase at some distance from the generated pulse.

Many different types of switching and computing circuits were described in other papers. The discussion on them was wound up by a general plea from one speaker that there should be some kind of agreed standardization and simplification in such circuit techniques. This would enable manufacturers to concentrate on producing first-class transistors with the best possible characteristics for switching work.

## 2.-INTERESTING THINGS SEEN AT THE EXHIBITION

Dielectric Valves being investigated by the Electrical Engineering Department of Birmingham University are similar to ordinary valves except that the electrons flow through a dielectric rather than a vacuum insulator. Normally currents cannot be made to flow through a dielectric insulator as through a vacuum for two reasons: potential barriers are set up at any external contacts, and in addition, imperfections in the dielectric crystal lattice structure trap any electrons which may flow initially so that an electric field is produced which inhibits any further flow. However, these two difficulties have now been overcome. Thin plate crystals of cadmium sulphide have been grown with a sufficiently perfect lattice structure to pass currents of tens of amperes per square centimetre at a few volts, and in addition, external contact potential barriers have been avoided by diffusing indium contacts into the surface of such crystals. Dielectric valves offer a number of general advantages over ordinary valves or transistors. They should be much easier to construct than either transistors or ordinary valves, although, for a given high frequency response, the dielectric valve, like the transistor, will háve to be much smaller than the corresponding ordinary valve. Also, the current/voltage characteristics of dielectric valves can be modified by altering the characteristics and number of the remaining imperfections in the crystal. No heater is needed in a dielectric valve since the free electrons in the metal contacts flow directly into the dielectric.

[^5]the source and drain on opposite sides of the constriction. Along the constriction is formed a p-n junction called the gate across which the input signal is applied. This signal modulates the current between the source and drain so as to produce an output in the external circuit connecting them. In the Alcatron there is, however, an additional much longer $p$-n junction from the gate to the drain parallel to the gate junction but on the opposite side of the constriction. This extra junction acts rather like the screen grid of an ordinary valve and also reduces the effects of surface variations at the gate. The geometrical arrangement of the electrodes in the Alcatron is also different from that in the Tecnetron. The Tecnetron consists of a long cylinder with the source and drain at its ends and the gate in the middle. The Alcatron resembles a Tecnetron rotated about its drain, and consists of a flat disc with the drain at the centre, source at the circumference and ring-shaped gate between. Since the volume at the constriction for a given narrow width is thus much greater in the Alcatron than the Tecnetron, the Alcatron offers a higher allowable power dissipation and transconductance than the Tecnetron in its original form.

Mesa Transistor base layers thin enough (a few microns) to give a short transit time between the emitter and collector, and thus a high cut-off frequency, are made by gas diffusion of the appropriate base impurity into the surface of the collector. Such diffusion also produces a gradual change of the resistivity through the base from the pure basetype semiconductor to the collector type, from n-type to p-type material or vice versa as the case may be. This gradual change results in an electrostatic "drift" field in the base region which still further reduces the transit time between emitter and collector, and increases the cut-off fre-
quency by a factor of five or more over that of a transistor with a similar base thickness but in which the base material is uniform. In the mesa transistor the emitter and base connections are applied to the base surface close together so as to minimize the resistance between them, but edge on to each other to keep the capacity between them low. Finally the material outside the emitter and base connection area is etched away around the base to reduce the collector capacity, the material near the collector being left unchanged so as not to reduce the allowable collector dissipation. The name mesa is derived from the characteristic shape of a flat base plateau on a larger collector produced by this process. The highest quoted $x$-cutoff frequency for a mesa was $600 \mathrm{Mc} / \mathrm{s}$ for the Texas Instruments 2N1142: prototype and experimental mesa transistors were shown by Sylvania-Thorn and the French C.S.F. respectively.

Power Transistors.-Fairly high powers at a fairly high frequencya few tens of watts at a few $\mathrm{Mc} / \mathrm{s}$ are offered for example by the Texas Instruments 2 S012 or 2 S013 and experimental silicon transistors- shown by the French C.S.F. and Ferranti.
The highest power audio transistors seen were the Westinghouse silicon TS10 to TS26 series in which the allowable collector dissipation falls to zero at $150^{\circ} \mathrm{C}$ and in which the derating factor or thermal resistance is quoted as $0.7^{\circ} \mathrm{C} /$ watt. The extent to which the current gain decreases at high-current levels depends on the emitter injection efficiency and hence the impurity level in the emitter region. By adding to the normal indium emitter material some substance such as aluminium which is more soluble in germanium than indium this injection efficiency can be improved. This process is used in the Mullard OC28 and OC29 for example.
(Continued on p. 351)

Tetrode Transistor giving a power gain of 20 dB at $70 \mathrm{Mc} / \mathrm{s}$ was shown by Texas Instruments (3S004). In this transistor the thin base is sandwiched between the relatively much thicker collector and emitter. The extra bias electrode is placed on the edge of the thin base opposite the base connection. The bias current which thus flows through the base at right angles to its narrow dimension reduces its effective area. Although this reduces the current gain it has two overriding advantages. It reduces the base resistance and thus decreases the necessity for neutralization at high frequencies and, in addition, it increases the cut-off frequency by a factor of about five. A convenient method of varying the current gain available in such tetrodes is to vary the bias current.

Switching Devices.-A number of manufacturers were showing p-n-p-n multilayer sandwich constructions. If a sufficiently high potential (about 100 V ) is applied across such a device the normally reverse-biased central junction breaks down and switches the total freward resistance from a high to a low value. The width of the central $p$ and $n$ regions determines the voltage required for switching, a higher voltage being required for a wider region. The Westinghouse Dynistor has similar characteristics to such devices except that its reverse resistance is low.

A recent development of these p-n-p-n devices shown by Westinghouse (as the Trinistor) and also by the B.T.-H. Research Laboratories and International Rectifier is the addition of a third control electrode at one ot the central regions, generally the p-region. This electrode can be used to switch the device independently of the external circuit and at a lower switching power level, a control signal of a few tens of milliamperes at a few volts switching currents of up to a few tens of amperes Such devices thus have properties similar to those of thyrations or grid-controlled rectifiers, but in addition have a number of advantages. These advantages include the absence of a beater and its attendant warm-up time and standby power requirements, a much lower voltage drop (about 1V) in the conducting state leading to a higher efficiency, and a faster triggering time (about $1 \mu \mathrm{sec}$ ). Like thyratrons these devices can only be switched off by reducing the operating current below a certain value.

In the R.C.A. Thyristor currents of a few tens of milliamperes can be
switched off as well as on from the control electrode with a control signal of a few milliamperes at a few tenths of a volt, and a triggering time of about $0.1 \mu \mathrm{sec}$. The Thyristor is a modification of a mesa transistor with the base used as the control electrode. Its action depends on the fact that the collector can become an electron injector at high current levels.

Diodes for Special Purposes.Zener diodes shown by International Rectifier included a 5-W range for use up to 160 V and a very stable $8.4 \mathrm{~V}, 10 \mathrm{~mA}$ unit in which the voltage changes by only $0.001 \%$ per ${ }^{\circ} \mathrm{C}$. A veïy wide operating temperature range of from $-65^{\circ} \mathrm{C}$ to $+325^{\circ} \mathrm{C}$ is possible in an 800 mW gallium arsenide regulator introduced by Texas Instruments. Forthcoming additions te the range of Lucas semiconductor diodes recently made generally available will include both Zener and clipper diodes-the latter are Zener diodes with equal sudden current overload characteristics at a certain voltage for both forward and backward voltages.

Small photodiodes with diameters of less than 0.1 in were shown by Sylvania-Thorn and Texas Instruments. A photocell shown by the German Te-Ka-De consisted of two
n-type germanium regions separated by a very narrow p-type dislocation, so that a movement of the illuminated region of only $10^{-1} \mathrm{~cm}$ across the dislocation reverses the direction of current flow. This device is grown from two n-type crystals butted together at a small angle. This * method of producing an impurity layer offers possibilities of avoiding temperature variation effects.
A variable-capacity diode usable for a.f.c. up to $250 \mathrm{Mc} / \mathrm{s}$ was shown by Siemens Ediswan (Y100).

Silicon Carbide for making semiconductor devices which can operate up to $600^{\circ} \mathrm{C}$ is being investigated by Raytheon. Although it is difficult to make crystals larger than about 0.01 in across, diodes have already been constructed.

Hall Effect Devices for multiplication, modulation and magnetic field measurement were shown by the German Siemens and Halske. These included a unit with an effective air gap of $5.5 \times 10^{-4}$ in for reading magnetic tape. With this method of reading, the output is, of course, proportional to the flux rather than the rate of change of flux, and is thus independent of the tape speed.

Miniaturization Techniques were shown by the R.C.A and Texas In-


Texas instruments miniaturized multivibrator. This incorporates two transistors, two capacitors and eight resistors made in a single piece of silicon less than $\frac{1}{4}$ in by $\frac{1}{8}$ in by $: \frac{1}{2}$ in. The finger points to two such units, the one on the right being hermetically sealed They can be compared in size with a conventional transistorized printed circuit multivibrator held in the other hand. A greatly enlarged drawing of the Texas unit is shown above.
struments. Texas have succeeded in forming together in a single piece of semiconductor all the components of a circuit, including transistors, diodes, resistors and capacitors. Component densities of about 20,000 per
cuin can be obtaincd by this method as compared with, for example, 30/ cu in using sub-miniature printed circuit techniques. R.C.A. form their components separately in the shape of thin wafers 0.3 in square which are then stacked on top of each other to give the required circuit. Comporent densities of about $300 / \mathrm{cu}$ in can be obtained by this method.

Small transistors of about 0.10 in diameter by 0.15 in long for use in hearing aids were shown by Raytheon and Brush.

Transistor Test Set shown by Siemens Ediswan (Type R2285) uses variable feedback from the collector to the base of the transistor to be tested to produce oscillations which are made audible by a loudspeaker. When the oscillations just cease the overall gain round the feedback loop is unity so that the transistor gain can be determined from the setting of the variable feedback control. Collector leakage currents can also be measured.

As many as seven dynamic and five static $\mathrm{n}-\mathrm{p}-\mathrm{n}$ and $\mathrm{p}-\mathrm{n}-\mathrm{p}$ transistor parameters can be measured at any collector potential up to 30 V and any emitter current up to 5 mA by means of the compact ( $8 \frac{1}{2} \mathrm{in}$ by $6 \frac{1}{2} \mathrm{in}$ by $4 \frac{1}{2} \mathrm{in}$ ) Telefunken Teletrans 1. The seven dynamic parameters are measured at $1 \mathrm{kc} / \mathrm{s}$ and are the standard " $h$ " and "y" parameters. These include the current gain, inverse voltage transfer ratio, two transconductances and three resistances. The five static parameters include four cut-off currents and the base voltage. A bridge measurement circuit eliminates any effects due to mains voltage variations, and the measurement accuracy is $\pm 5 \ldots$

A series of adaptors is now available from Wayne-Kerr for enabling various transistor admittances to be measured from $100 \mathrm{c} / \mathrm{s}$ to $5 \mathrm{Mc} / \mathrm{s}$ to within $\pm 3 \%$ using their TA100 and B601 transformer ratio-arm bridges. These adaptors automatically set up the appropriate transistor and power

supply configurations while avoiding stray capacitances and couplings and unwanted loading due to the supplies. The three-terminal facility of transformer ratio-arm bridges by which the impedance between two points can be measured independently of the impedances between these two points and a third is particularly useful for transistor measurements.

In an automatic tester shown by S.T.C. the various parameters are measured in turn by integration for two successive five-second periods. Integration simplifies the measurement of small currents and reduces the effects of switching from one parameter to the next, while shortterm drifts are detected by comparing the two successive five-second integrals.

## Semiconductor Measurements

 shown by Siemens Ediswan included that of the three hybrid- $\pi$ transistor equivalent circuit parameters using the equivalent circuit and transistor in two arms of a bridge. If a broad frequency band input signal such as a square wave is used, the balance point will determine three parameters rather than the usual two.Current gain measurement using a transformer ratio-arm bridge was illustrated by the B.B.C. A variable fraction of the collector current is fed to one ratio arm, and the emitter current with a variable phase shift is fed to another ratio arm. The outputs from the two ratio arms are arranged to act in opposition in the secondary detector winding. The settings of the variable phase and amplitude controls for no secondary detector output then determine the phase and amplitude of the current gain.
G.E.C., Newmarket and Texas Instruments used the variation with temperature of certain semiconductor parameters such as reverse leakage currents to give, after calibration in an oven, a measure of junction temperature in the measurement of permissible ratings for a given temperature. The semiconductor device was continually switched between the temperature measurement and permissible rating test conditions.


Dawe prototype transistor oscilloscope Type 720 using only eight transistors.

When a diode is switched from the forward to the backward direction a reverse current flows temporarily until the remaining current carriers are removed from the mate-rial-a phenomena known as hole storage. The decay time constant of the reverse current pulse varies considerably with the particular operating conditions so that it is more useful to specify the total charge in the pulse. As shown by the G.E.C. this charge can be measured by charging up a condenser from a repetitive pulse and measuring the mean current produced, since this current is equal to the repetition frequency multiplied by the required charge.

Analogue Circuits for investigating system performance data which are too difficult to calculate are, of course, a very old idea, but two of the circuits shown had unusual general features. Mullard showed a large-signal analogue of a highfrequency transistor which used transistors to provide some of the nonlinear capacities required. S.T.C showed an analogue circuit of an alloy-junction transistor which was made three dimensional to take account of the fact that the minority carrier flow between emitter and collector is not exactly in parallel lines across the base but spreads out somewhat from the emitter.

Oscilloscopes using transistors were shown in experimental form by

B.B.C. experimental v.h.f./f.m. receiver incorporating balanced crystal mixer.

Telefunken versatile compact transistor test set "Teletrans /".

Cossor (on the Livingstone Laboratories stand) and B.T.-H, and in prototype form by Dawe. The Dawe Type 720 uses only 8 transistors. Its Y -amplifier has a maximum sensitivity of $30 \mathrm{mV} / \mathrm{cm}$ falling by 3 dB at $5 \mathrm{c} / \mathrm{s}$ and $50 \mathrm{kc} / \mathrm{s}$, and a high (for transistors) input impedance of $1 \mathrm{M} \Omega$. Although the resporse in the two experimental models extended to at least $500 \mathrm{kc} / \mathrm{s}$, they each used about 20 or more transistors.

Receivers for the v.h.f./f.m. band were shown in experimental form by the B.B.C. and Texas Instruments. The transistor cut-off frequency must be higher for r.f. amplification than for oscillation so that because of the difficulty of obtaining sufficiently high frequency transistors only the Texas receiver incorporated an r.f. stage. This used a 2 N1142 transistor, and a 2 N 623 is used in the combined mixer-oscillator stage. The B.B.C.' receiver used a 2 N 247 as an oscillator feeding two GEX66 diodes forming a balanced mixer to reduce local oscillator radiation.

Miniature a.m. receivers which included short-wave bands extending up to $12 \mathrm{Mc} / \mathrm{s}$ were shown by the two Japanese exhibitors Sanyo and Tokyo Shibaura. Thermistors for stabilizing the push-pull output stage against temperature variations are incorporated in the Sanyo receivers.

Stabilized Power Supplies.-In this field it would seem that the transistor has created a direct demand for itself. For experimental work with transistors a stable supply variable between about 1 and 30 V at a current of the order of 1 A is often necessary, and it is to the stabilization of such supplies that the small power transistor is peculiarly suited. Many manufacturers were showing mains-derived power supply units of this nature which were broadly similar: most used a form of emitter-follower circuit with the reference potential derived either from gas-filled stabilizer valves or Zener diodes. Output impedances of the order $0.05 \Omega$ are generally achieved.

When delivering a current near the maximum rating at a low voltage the major part of the supply's power is dissipated in the output transistors. To enable the use of an economic-ally-sized output stage most of the power units were fitted with a coarse voltage switch selecting two or three taps on the mains transformer, but G.E.C. were showing a unit capable of continuous variation between 6
and 20 V at 10 A . Two firms (Elliott and Hatfield) had adopted special means of utilizing a smaller output stage than was usual. The Hatifield L.E. 400 is rated at 30 V lA but the single output-voltage control varies not only the proportion of the reference voltage used (this time derived from Zener diodes) but also the input voltage by means of a continuously - variable transformer. Elliott use a rather different approach in their Type B. 673 supply. This has a maximum output of 50 V at 1.5 A and surprisingly small transistors are used for stabilization, which is achieved by switching the supply into largevalue electrolytic capacitors. A drop in voltage below a preset limit switches the supply on, and a rise switches it off: this is achieved by a bistable circuit whose reference voltage is derived from Zener diodes and the switching rate varies between about $3 \mathrm{c} / \mathrm{s}$ and $300 \mathrm{c} / \mathrm{s}$ for the minimum and full load conditions.

Mobile Power Supplies.-The difficulties of obtaining high, direct or alternating voltage from the lowvoltage d.c. supplies available in cars or aeroplanes are only too well known. The transistor, however, can be used as a repetitive switch which has very good performance compared with mechanical interruptors and, in such a mode, it dissipates but little power within itself. Most convertors follow the same general outline-oscillating transistors feed "chopped" d.c. into a transformer where it is stepped up to the required potential and, then, for a d.c. output, rectified and smoothed.

An example of one typical approach was the Ultra UA1701 convertor which is designed as a direct replacement for a rotary machine in some of this company's airborne equipment. Four transistors in a bridge oscillator circuit interrupt the $28-\mathrm{V}$ d.c. supply, feeding it to a square-(hysteresis)-loop transformer, whose output is rectified by junction devices to provide 250 V at 250 mA d.c. Efficiencies, on the whole, are good: for a d.c. output the use of a square-loop transformer helps considerably as this enables the transistors to be operated with the minimum of internal power loss. However, for an a.c. output the preferred practice seems to be to use
either a scparate sine-wave oscillator driving a fairly-efficient output stage, or to use the power transistors as sine-wave escillators, so avoiding the use of filters.
D.C.-to-a.c. convertors have been made in sizes handling hundreds of watts, but one which caught our eye was on the Elliott stand. This was rated at 20W (Type B.725) and gives a $400 \mathrm{c} / \mathrm{s}$ output which was displayed together with $400 \mathrm{c} / \mathrm{s}$ from an a.f

generator on a double-beam oscilloscope. There was a barely discernable difference between the waveforms. The use of these convertors seems worthwhile even for purposes such as fluorescent lighting in aircraft, cars and railway carriages. Many oscillators designed expressly for this purpose were shown in a variety of sizes from 6 up to about 150 W . A side issue of this is that G.E.C. have been able to reduce appreciably the magneto-strictive noise from the transformers by coating them with a $\frac{1}{4}$-in-layer of solid polyurethane.

Transistor H.T. Smoothing.Where there are severe limitations on space or weight a transistor may be used in place of the normal L-C h.t.-smooching arrangement. This was illustrated by a unit from the "Sea Slug" guided missile in which a small power transistor is used to smooth an h.t. supply. Again the circuit used is an emitter follower, the base being connected to a supply smoothed by a simple, small R-C filter.

Data Processing.-The Ferranti "Sirius" is a new, general-purpose digital computer designed mainly for the user who needs a computer but who does not have sufficient work to. keep a large machine economically occupied. The computing elements are transistortransformer units employing " ballotbox logic" and the 1,000-word store


Ferranti" Sirius " general-purpose digital computer.


Armstrong-Whitworth analogue-to-digital and digital-to-analogue convertors (upper and middle decks of large cabinet) wired together for demonstration.

$6.6 \mathrm{Mc} / \mathrm{s}$ i.f. strip (using toroidal coils) from S.T.C. i.I.s. receiver.

Rear view of Fergusonn "Digitizer" 5-bit analogue-to-digital convertor using "book-leaf" construction.
is made up from 20 torsional nickelwire delay lines using magnetostrictive input and output. The logic circuits are made up on colourcoded plug-in bóards. No cooling system is necessary. Notable features of this computer are its small size, $7 \mathrm{ft} \times 3 \mathrm{ft} 6 \mathrm{in} \times 4 \mathrm{ft}$; low weight, 5 cwt ; power consumption, 600 W ; and price, $£ 15,000$ complete with input and output apparatus (5-hole paper-tape equipment).

The Ferguson "digitizer" is a comparatively simple medium-speed analogue-to-binary code convertor giving a straight 5 -bit output. Housed in a cubic box of side 6 -in, it is mains powered and is built on the book-leaf pattern. The ArmstrongWhitworth analogue-to-digital convertor is rather more sophisticatedthis gives an 8 -bit output in both serial and parallel form and a 500 $\mathrm{kc} / \mathrm{s}$ digit-pulse rate is achieved by the use of surface-barrier transistors. It has a companion digital-to-
analogue convertor which accepts an 8 -bit number, stores it and then uses it to control transistor switches feeding a resistor network, from which the output voltage is produced.

Experimental use of the automatic letter-sorting machine has shown the G.P.O. that a serious barrier to the extension of its use is the difficulty of teaching quickly the special code fed in by the operator. To overcome this difficulty a translator has been developed at the Post Office Research Station which feeds to the sorting machine the required twoletter code. This code is derived from the three initial and two final letters of the name of the "post town" (this large number is necessary to avoid ambiguities) which are fed in by the operator from an ordinary typewriter keyboard. The translator unit uses a $5 \times 26$ matrix of squareloop cores, whose output is amplified by transistors and used to strike cold-cathode tubes feeding the sorter.
A device which could replace square-loop cores in computing applications is the p-n-p-n junction. On the stand of the A.E.I. Research

Laboratories these devices, which exhibit similar characteristics to those of a gas-discharge tube, were shown operating in a $5 \times 5$ matrix, a saw-tooth generator, a bi-stable circuit and two forms of ring-counter (see circuit diagram). Their chief advantage in a matrix is that they are individually replaceable, whereas in a core matrix a failure of one core usually means that the whole matrix has to be replaced.

Communications: - R.C.A. were showing a single-channel transistor v.h.f. receiver (the AR108) for the 108 - to $156-\mathrm{Mc} / \mathrm{s}$ band with a performance of a surprisingly high order- 50 mW output is obtained for a $2-\mu \mathrm{V}$ input, with a signal/noise ratio of 10 dB at $30 \%$ modulation. The large amount of power wasted in valve receivers is brought home with a vengeance by the power consumption of this set -8 to 10 W maximum at $12 \mathrm{Vd.c}$. for a 2-W a.f. output. The underside of the chassis of the AR108 is a little disappointing-all that can be seen is wiring between octal valve sockets! Into these sockets plug resin-encapsulated units each con-


Code translator for G.P.O. lettersorting machine.
taining all the components for a particular stage. The units are coded by colour and shape and the overall size of the receiver is such that two can be mounted side-by-side in a 19 -in rack (height 3 in ). It is also available in a $117 / 234-\mathrm{V}, 50$ to $60 \mathrm{c} / \mathrm{s}$ version.

Another striking example of miniaturization by the use of transistors was shown on the Ministry of Supply stand. This was a "Forward-area Time-division Multiplex Equipment" which is contained in one box, weighs only 30lb. and consumes 5 W of power at $12 \mathrm{Vd} . \mathrm{c}$. This provides four, good two-way telephone channels over a radio link or land line of very poor quality. Con-" trasted with its 8 -year-old "valved" equivalent which consisted of sixteen

R.C.A. 's all-transistce single-channel v.h.f. receiver using potted plug-in component assemblies and (below) potted plug-in unit from R.C.A. AR108 receiver.

boxes each weighing 50 to 80 lb . and consuming 1.5 kW the new equipment can be considered truly portable and suitable for "forwardarea" use.

The growing use of transistors in airborne equipment was noted at last year's S.B.A.C. show ${ }^{\star}$. The general trend seems to be to allow, a reasonable amount of "spare" space in the layout so that servicing is rather easier than with valved equipment. One example of this was an i.f. strip from the S.T.C. i.l.s. glide-slope receiver. Operating at $6.6 \mathrm{Mc} / \mathrm{s}$ this uses six stages of grounded-emitter amplification to provide $100 \mathrm{~dB} \pm 6 \mathrm{~dB}$ gain over a bandwidth of $200 \mathrm{kc} / \mathrm{s}$. Transmitters are at present limited by the lack of suitable transistors: however this gap is being filled, albeit slowly, and Wireless World, p. 491, October, 1958.

Mullard were showing aus "S.O.S." transmitter with a 4-W output at $500 \mathrm{kc} / \mathrm{s}$. This used a pair of OC24s in Class-B pushpull, driven from a crystal oscillator using an OC45. The efficiency realised was about $50 \%$.

Circuitry.-D.C. amplifier design, is at the best of times, a difficult business and it is not eased by the additional drifts present in transistors, but these disadvantages are being overcome. One item on the Mullard stand featured a display of 8 types of d.c. amplifiers, together with some performance data. The first type was a direct-coupled amplifier having a current gain of 500 and which used germanium devices. The drift exhibited by this was about $5 \mu \mathrm{~A} /{ }^{\circ} \mathrm{C}$, referred to the $2-\mathrm{mA}$ input. The use of silicon transistors and base stabilization by Zener diodes in the second example raised the input impedance from about $100 \Omega$ to $300 \mathrm{k} \Omega$ and cut the drift to $0.1 \mu \mathrm{~A} /{ }^{\circ} \mathrm{C} \cdot$ referred to the input. The third example, was a set of germanium long-tailed pairs with a drift of 1.5 mV , relative to the maximum input of 10 mV , from 20 to $35^{\circ} \mathrm{C}$. and again replacing the.: germanium devices by silicon reduces drift and increases input impedance. No. 5 illustrated the use of temperature stabilization of the input stage by means of a subsidiary amplifier controlling a small heating coil round the transistor. This reduced drift by a factor of 20 and temperature was sensed by a second transistor inside the coil. The sixth example used chopper techniques and the chopping was done by a silicon-diode bridge -a drift of about $2.5 \mathrm{~m} \mu \mathrm{~A} /{ }^{\circ} \mathrm{C}$ was achieved relative to $1-\mu \mathrm{A}$ input, with a gain of 1000 . Another chopped design used a transistor as a parallel switch across the input. This had a drift of only $0.5 \mathrm{~m} \mu \mathrm{~A}$ but the best system still seems to be the mechani-

Resear of ring-of-ten counter in demonstration form using p-n-p-n junctions (A.E.I. Research Laboratories).
cally-chopped amplifier. The last example, using a Carpenter relay, exhibited a gain of 50,000 with a very small drift, which is time-dependant. The temperature control method mentioned above was used in an amplifier panel offered by the G.E.C. as a basic "brick" for instrumentation purposes. This amplifier has a guaranteed minimum gain of 200,000 , a drift of $\pm 2.5 \mu \mathrm{~V}$ and a noise level of $5 \mu \mathrm{~V}$ peak to peak referred to the input. The output is $\pm 10 \mathrm{~V}$ and synchronous-chopper techniques are also used. All the transistors are germanium types arranged in feedback pairs and the low-noise GET106 is used for the first stage.
Work at the Royal Radar Establishment on the use of transistors in radar has resulted in the development of a very-linear timebase for a magnetically-deflected c.r.t. This uses an r.f. transistor as a switch (not specifically for its high cut-off frequency; but for its low leakage current) across the scan-determining capacitor, one plate of which is connected the input of an amplifier whose output is developed across a low value resistor in the emitter circuit. The output voltage is fed back to the other plate of the capacitor. Thus something very similar to the single-pentode Miller circuit is achieved. To neutralize the leakage current of the switching transistor
a similar transistor is connected, in the reverse sense, to the capacitor. The Miller voltage waveform developed across the emitter resistor in the output stage causes a linear current sawtooth to flow through the deffector coils, which are placed in the collector circuit. The waveform has a peak current of 1 A , is $120-$ $\mu_{\text {sec }}$ long, its linearity is better $1{ }^{\circ}$ and the leakage-current compensating circuit ensures that the velocity changes by less than $1 \%$ for a change in temperature from $15^{\circ} \mathrm{C}$ to $50^{\circ} \mathrm{C}$.

Medical Electronics:-A miniature, transistor heartbeat detector developed at R.A.E. Farnborough for use in physiological tests was shown on the Ministry of Supply stand. Skin potentials are developed which depend on heartbeat action; but normally, in an active subject, these are masked by the noise made by the working of the muscles. To overcome this, skin potentials are monitored at two places approximately equidistant from the heart, preferably on antagonistic groups of muscles so that the noise of one muscle contracting does not coincide with that of the other, which is then relaxing. A common electrode is placed near the heart and the two pick-up voltages, after amplification, are applied to a coincidence detector, which produces a $2-V$ pulse at each heartbeat only.


FORTY-NINE POLE TIME SWITCH AS MANY as forty-nine processes can be switched on over a total period of up to $2 \frac{1}{2}$ hours by the Venner programme record/playbock console Type TSA 50 shown in the photograph. The command pulses are stored on standard mognetic recording tape. This instrument is made by Venner Electronics Ltd., Kingston By-Pass, New Malden, Surrey.

# Automatic Component Testing 



Automatic: est machine and equipment in a laboratory at Sylvania-Thorn.

AN AUTOMATIC machine for the testing of components and the individual recording of their characteristics has been developed by Sylvania-Thorn Colour-Television Laboratories, Ltd. The machine applies up to 10 tests sequentially at the rate of 10,000 per hour, recording the results simultaneously on punched paper tape and on a paper roll, printing out through a teleprinter receiver.
If a component fails one test, other tests can be inhibited and another valuatle feature of the machine is that it can retest components after an environmental stress has been applied, giving a read-out interlaced with the original figures on the teleprinter. This second readout appears only when a change has occurred during the stress period. Test results, in the form of analogues, are converted by a transistor digitizer to a 5-bit code, which is then converted to telegraph code to operate the teleprinter. The machine can also test other components such as transistors.

An Apparently Insignificant Phenomenon Comes to Life

TWO months ago I objected to the term "parametric amplifier" because (among other reasons) some but not all of such amplifiers make use of paramagnetic materials, and the two words occurring in the same context are bound to be confused., To make matters worse, some but not all "masers" are paramagnetic, though they are not parametric in the currently accepted sense.

We are likely to hear more about paramagnetic materials and paramagnetism. Most of us know something about magnetism, which we usually associate with permanent magnets and with currents flowing through coils. These are considered officially under the respective headings ferromagnetism and electromagnetism. We may even remember vaguely that there were two other things, called diamagnetism and paramagnetism, but it was difficult to remember which was which, and anyway they seemed insignificant. Now that paramagnetism is in the news perhaps we have been hastily looking it up in our textbooks, and (unless you were luckier than I was) finding it highly confusing.

## Early Theories

About 130 years ago the great electrical pioneer Ampère, meditating on the discovery that a current flowing round a coil makes it a magnet, surmized that magnetism in iron, etc., was caused by small circulating currents in each atom. The idea was expressed more definitely by Weber, not so very long after. This, remember, was when very little was known about atoms, and, of course, nothing at all about electrons. Modern science, though it has upset so many old ideas, has confirmed this one, which was a remarkable flash of prophetic genius.
We now know that atoms are constructed largely of electrically charged particles - protons and electrons - which revolve in orbits and also spin on their own axes. Both these movements are essentially tiny electric currents flowing round tiny one-turn coils, and have the same result as we find on a vastly larger scale in magnet coils.

The fact that with very few exceptions materials as a whole are not magners can easily be explained on the very natural assumption that the magnetic fields of the individual atoms cancel one another out by their random arrangenent. The problem then is to explain the exceptions.

These exceptions, notably iron and its alloys, have an enormous multiplying effect (called permeability) on any magnetic field in which they are placed; and some of their magnetism remains after the field is switched off. Such effects, called ferromagnetism, were plausibly explained by Ewing as being due to the atomic (or rather molecular) magnets being forced gradually into alignment until forced back by a field in the opposite direction. This was the theory I was brought up on (in an establishment presided over by the said Ewing), and when later it was thrown out in favour of what was called the domain
theory, it seemed to me that this new theory was essentially the same as the old, except for the name and the larger size of the elementary magnets. However, when one goes into the thing in detail the differences are considerable, and if you want to know more about them you had better refer again to the series by Dr. D. H. Martin in the January to April issues of last year. Since our present subject is paramagnetism I will just mention in passing that ferromagnetic materials are those in which large groups ("domains") of atoms all face the same way magnetically, held so by internal forces many thousands or even millions of times stronger than magnetic fields sufficient to saturate iron. The reason why so few materials are ferromagnetic is that the particular atomic structure needed for it is quite exceptional.
(d)

(b)


Fig. I. All substonces, suspended between the poles of a magnet, tend to toke up one of these positions. Ferromagnetic and paromagnetic adopt position (a); diamag. netic, (b)

It's easy enough, of course, to tell which materials are ferromagnetic, by seeing if they are attracted by a permanent magnet. If we made the test more scientifically we would suspend a short rod of the stuff between the poles of a magnet, as in Fig. 1, so that it is free to turn round but not move in any other way. We all know that a piece of iron takes up the position shown at (a) with considerable alacrity, rather than lying across the field as at (b). Why?

We might say that the magnet attracts the piece of iron, and position (a) is the one that brings it nearest. To be more specific; iron being what it is, the field magnetizes it, making the end nearest N an opposite pole ( S ), and the same in reverse at the other end. Unlike poles attract, so energy would have to be supplied from outside to turn the iron from position (a) to (b). It is a general rule that the energy of a system tends to change from available to unavailable forms (heat), as when a metal object in water sinks. So the iron tends to move from position (b) to (a).
If we tried the same experiment with a bar of aluminium or frozen oxygen we would probably fail, unless we were as careful experimenters as Faraday. He found that some "non-magnetic" substances tended to take up position (a), though with considerably less alacrity than iron (of the order of a hundred million times less) while others such as copper and


Fig. 2. The effect of a magnetic field $(H)$ on a revolving electron (or proton) is to make its orbit slowly rotate around an axis parallel to H .
bismuth preferred position (b), though with possibly even less enthusiasm. If the former were like heavier-than-water bodies sinking, these could be likened to lighter-than-water bodies floating. He came to the conclusion that all substances other than the few ferromagnetic kinds fell into one or other class. Those that follow the example of iron, but so very much more feebly, are called paramagnetic, and the opposite kind are diamagnetic.

This exceedingly lukewarm reaction either for or against a magnetic field suggests no very obvious use. Certainly the materials wouldn't justify even a moderate cost as magnetic cores, or even antimagnetic ones! The whole thing seems to have only academic interest. Hence, no doubt, our haste to forget all we ever learnt. about it. The reason for a recent change in attitude is that paramagnetic effects involve energy changes in atoms, and these (in accordance with the quantum principle) are directly related to frequency.

## Magnetics in Molecules

But before tackling paramagnetism we must know that basically everything is diamagnetic, and that the paramagnetic substances (and, of course, still more the ferromagnetic) are those in which the diamagnetism is more than cancelled out by the opposite effect.
The first thing to get hold of is that nearly all molecules are constructed in such a way that the magnetic effects of their individual electrons exactly cancel out. So the molecules are not permanent magnets. Still less can any objects made of the molecules be permanent magnets. It would be possible and, in fact, natural for the molecules, even if they were magnetic, to be so jumbled up that their magnetic effects would cancel out in any piece of material. But that is not to say that the molecules (and material made of them) cannot be magnetized, by putting them in a magnetic field.
This is one of the places where the books became hard to follow. They plunge into a highly mathematical treatment of such matters as Larmor precession and Coriolis forces, finally emerging with the conclusion that when the magnetic field is applied the response is in the contrary direction; in other words, the permeability of the material is (very) slightly less than 1. This is rather surprising to simple minds, because if, say, the single electron in a hydrogen atom was flying round an orbit which caused it to generate a tiny magnetic field, one would expect that putting it in a magneric field would make it turn, like a compass needle, into such a position that its own field would add its modest quota to the whole. And that molecules, in which there are usually equal
numbers of electrons with opposite rotation, would experience equal and opposite forces, so as wholes would be unaffected. But that is too simple to be true.

Fig. 2 shows a pair of coils with current flowing through them, and as the direction of current viewed from the left-hand end is clockwise, by the corkscrew rule the magnetic field must be in the direction marked H . In this horizontal field an electron is spinning around in a horizontal circle, clockwise when viewed from below, so the current is clockwise viewed from above, and its own magnetic field $\left(\mathrm{H}_{0}\right)$ is downward. When the electron is at positions A and B it (and the current) is moving parallel to the main field H , so is not affected thereby. But in positions C and D it is moving across the field, and the left-hand rule tells us that it is forced in the directions of the arrows.
This still looks as if it would tilt the whole orbit so that its field would come into line with the main field, just as our simple minds predicted. But we have forgotten that an electron has mass as well as electric charge.
Fig. 3 shows a top spinning at an angle to the vertical, so that gravity acting on its mass creates a downward force through its centre of gravity C , and of course the table on which it is spinning exerts an equal upward force at the point. This pair of forces might be expected to make the top fall over towards the right, and if it were not spinning it would certainly do so. But the spin momentum of the top carries it around, and the combination of this with the force of gravity makes the leaning angle move comparatively slowly round in the direction of spin. The faster the top is spinning and the less it leans, the slower this motion, which is called precession. If the top could lean over horizontally, still spinning on its point, the top as a whole would rotate in a horizontal plane about its point.

If you have ever handled a gyroscope, you will know the rather uncanny feeling of trying to tilt it as in Fig. 2 and finding that ihe result is to make its plane of rotation turn over in an unexpected manner. Suppose the electron is at C. Then its orbital motion would be bringing it round to the front (opposite to the direction of the arrow, which refers to the conventional positive current); but the addition of the downward force actually brings it rather lower than A. In other words, the orbit as a whole begins to rotate around the lines of force H in a clockwise direction viewed from the left. This means a clockwise movement of the electron, or anticlockwise movement of the current, which causes a component of magnetic field opposing H . The total field is slightly reduced.
Now suppose that the same molecule has another electron rotating in the opposite direction. If you work it out you will find that it too reduces the total

Fig. 3. The effect shown in Fig. 2 is something like the fomiliar slow motion

field. So the permeability of material made of the molecules is less than 1. In other words, the stuff is diamagnetic, whether magretically its electrons are all oppositely balanced or not.

Those that aren't exhibit paramagnetism as well, and if (as is normally so) the paramagnetism is greater than the diamagnetism, they will as a whole be paramagnetic. Since the molecules are not magnetically balanced, each one is a tiny magnet. Nevertheless the material as a whole is not a magnet, because heat energy is pushing all the molecules around in a completely random fashion; and with the stupendous number of molecules in even a small piece, the chances of there being any appreciable excess pointing in any one direction for an appreciable length of time is negligible.

But it is different when an external magnetic field is applied. If one could switch off all fields, including the earth's, a collection of thousands of vigorously shaken compass needles would point in random directions. Restoring the earth's field would swing them all round in one direction, making a sizeable magnet. Similarly with the paramagnetic material. The total magnetic flux is increased, so the permeability is greater than 1.

Actually the response at any temperature much above the absolute zero is very small indeed, for practical magnetic fields can do very little to counteract the disordering influence of heat. It is as if the compass needles were situated in a beehive, with the insects pushing them about in all directions so that only a slight trend towards magnetic north could be discerned. Obviously, then, paramagnetism (unlike diamagnetism) depends largely on temperature, being considerable near absolute zero and falling off as the temperature rises.

But there is more to paramagnetism than this. Very much more! After having struggled with a number of books on the subject I have arrived at the considered opinion that this must be an exception to the rule that there is nothing that can't be explained simply and concisely. It involves all the atomic matters we have discussed during the past year or two, in far greater detail and with very much added. And since the task of creating Honours Physicists in One Short Easy Lesson is not one that I propose to attempt, we shall have to make do with something less. To real physicists it will appear hopelessly over-simplified.

## Energy Content

When an atomic magnet formed as just described, is placed in a magnetic field, it is thereby given an amount of energy which depends on the angle between its own magnetic axis and the field. If the two already coincide, like a compass needle that was already pointing north before it was put in the earth's field, it won't feel any inclination to move. But one lying across the field has potential energy, which is lost when it swings into alignment. One would expect the amount of energy to vary smoothly between one position and the other.

But you may remember ${ }^{\star}$ that one of the elementary facts about electron orbits around atomic nuclei is that the energy of an electron cannot change gradually by gradually enlarging or closing up its orbit; it can change only in certain fixed jumps,

[^6]according to quantum rules. The same applies to magnetic energy levels.

Obviously, too, the energy varies in proportion to the strength of applied field. And so we get the kind of energy diagram we saw two months ago-Fig. 4. The direct proportion between energy jump and frequency ( $\mathrm{E}=h f$ ) holds, of course; so if a paramagnetic material is stimulated by power at a frequency corresponding to one of the energy gaps, atoms (or rather molecules) tend to be lifted up or "excited" across that gap. We saw how this was applied in paramagnetic masers, which can be made to amplify or oscillate. For electron-orbit magnets, the frequencies are usually in the microwave region. A useful feature, not possessed by the much larger energy gaps between orbits, is that the frequencies can be varied by controlling the applied field strength.

Another thing that happens in paramagnetic substances, as in diamagnetic, is precession. Now there is a difference in the energy of the spinning electron (or whatever particle it is that is precessing) depending on whether its magnetic axis is with or opposing that of the applied field. It is as if a top could spin either right way up or upside down; the latter having the


Fig. 4. The energy levels of a paramagnetic molecule vary in proportion to an applied magnetic field, but at any one field strength they occur at $\dagger$ xed intervals.
greater energy, so that some outside boost is needed to effect the change-over.

One way of imparting such a boost is to apply a magnetic field at right angles to the first applied field, rotating at the precession frequency. Suppose the top in Fig. 3 is the electron, precessing under the influence of a steady vertical field (represented by gravity). If now one were to move the table with a horizontal circular motion, so as to give the top a rotating sideways pull in time with the rate of precession, it would tend to turn upside down.

The required frequency for upsetting spinning electrons is of the order of $10,000 \mathrm{Mc} / \mathrm{s}$. A rotating magnetic field exists in a waveguide or cavity into which power at the appropriate frequency is fed. The only thing is to make sure that the paramagnetic sample is placed in the right position, and that the steady field is applied at righi angles to the plane of rotation. When the frequency of the microwave power comes into tune with the frequency of the spin energy difference (or when the latter is brought into tune with the former by varying the steady field) the accepting of energy from the microwave power can be detected as a sudden increase in loss of the system. It is just as if a loosely coupled circuit had been brought into resonance.

The protons in the nucleus of an atom also spin,


Fig. 5. Outline of apparatus for detecting atomic resonances and measuring their frequency and hence the energy jumps represented.
and if they are unpaired they cause paramagnetism; but because protons are so much heavier for the same charge as an electron they spin much more slowly and the energy differences are small, corresponding to frequencies of only a few $\mathrm{Mc} / \mathrm{s}$.

All these effects are very much influenced by interactions between all the particles concerned. In solids these interactions are greater than in liquids and have the effect of broadening the resonance peaks.

Fig. 5 is a diagram of the sort of set-up used for tracing the resonance patterns of paramagnetic materials. By such means a vast amount of information has been accumulated on the complicated goings-on inside atoms. It is a research tool of firsttate importance.

Another application of paramagnetism we did just touch on in the July 1957 issue, is superconductivity. Has it ever puzzled you how things can be cooled down to within a small fraction of one degree of absolute zero $\left(0.000015^{\circ} \mathrm{K}\right.$ was claimed some time ago)? One can get down to somewhere around $1^{\circ} \mathrm{K}$ by successive use of liquid gases, finishing up with helium. Then a paramagnetic material, such as iron ammonium alum, which is inside the apparatus and has been reduced to this low temperature, is magnetized by a strong externally-applied magnetic field. The effect is to cause the material to give out heat, which is carried away by the helium. Switching off the field has the reverse effect-heat has to be taken in by the material, and if it is thermally insulated the only way it can do so is to reduce its own temperature, like a starved man living on his own fat.

You might think that at those low temperatures the tendency for heat to leak in from the surroundings would make such a drop in temperature a very temporary-almost momentary-affair. So it is a convenient as well as astonishing fact that 1 cubic centimetre of the paramagnetic alum mentioned has, at $0.05^{\circ} \mathrm{K}$, a thermal capacity equal to that of 16 tons of lead at the same temperature!

One way and another then, paramagnetism is acquiring practical as well as theoretical interest. And if some of the applications still seem a little highbrow to us radio engineers, perhaps at one time so did the physical researches that have now brought transistors on to the market in their millions.

## Addendum-" Hall and Holes"

ON p. 605 of the December 1958 issue I complained that nobody, repeat nobody, known to me had explained clearly how the Hall effect managed to distinguish between electron and hole currents seeing that both were in fact movments of electrons, and 1 appealed to any authors unknown to lodge claims.

It has been necessary to go as far as Australia for one. Dr. J. L. Salpeter has called attention to his 16-page paper, "The Concept of the Hole in Semiconductors", in Proc.I.R.E.Aus. for December 1955, which I have found extremely interesting. One has to travel rather a long way with Dr. Salpeter to get to the point in question, but at least one would realize by then that the hole is not quite so simple as it is sometimes made out to be.

In a letter, Dr. Salpeter points out that my Fig. 6, showing two atoms before and after an electron movement has brought about a shift of positive charge, leads to difficulty if one considers what is happening during the movement. There certainly seems to be, as he claims, no escape from going into the wave mechanics of electrons in a crystal lattice if one is to understand holes correctly. Some writers use the concept of negative mass, but I felt some reluctance about putting that forward!

## Low-noise U. H. F. Receiver

THIS seceiver, primarily designed for ground-station missile-telemetry applications, features continuous tuning over the 420 to $500 \mathrm{Mc} / \mathrm{s}$ band. Two tuning controls are provided, one for the r.f. circuits and one for the local oscillator; this, and the use of a low-noise grounded-grid r.f. stage (A2421), enables an overall noise factor of better than 10 dB to be realized. 'The groundedgrid mixer (CV408) feeds a cascode first, i.f. stage (E88CC), which is followed by three high-gain pentodes (E180Fs). The i.f. is $45 \mathrm{Mc} / \mathrm{s}$ and the overall bandwidth of the standard reaceivers is $\pm 2.25 \mathrm{Mc} / \mathrm{s}$ for a response at -3 dB (compared with the central frequency): this bandwidth is achieved by stagger tuning the i.f. stages and the manufacturers state that it can be increased to $\pm 3 \mathrm{Mc} / \mathrm{s}$ without


Armstrong - Whitworth low - noise u.h.f. receiver, "boxed" version. extra cost. Amplified a.g.c. is provided for the first i.f. stage and for operating the "magic-eye" tuning indicator; this bias is produced by a rectifier fed from an additional i.f. amplifier (E180F). The signal tetector (semiconductor diode) feeds ? cathode follower to provide a low-imped"ance output. The local oscillator (CV408) is run in the "oscillator high" condition and drift is given as $0.2 \mathrm{Mc} / \mathrm{s}$ after 12 hours continuous operation (provisional figure only). The aerial input (unbalanced) impedance is $70 \Omega$ at $450 \mathrm{Mc} / \mathrm{s}$.

The receiver is available in two forms: one for 19-in rack mounting, the other as a $8 \mathrm{in} \times 8 \mathrm{in} \times 15 \frac{1}{2}$ in boxed unit to fit aircraft racking. The 19 -in type (weight 42 lb ) includes a $200-250 \mathrm{~V} 50 \mathrm{z} / \mathrm{s}$ power supply; but the airborne version (weight 12 lb ) requires an external supply of 190 V at 110 mA d.c. (stabilized) and 6.3 V at 3.5 A for the valve heaters. Manufacturers: Sir W. G. Armstrong Whitworth Aircraft, Ltd., Baginton, Coventry.

Latest information on events from September to next March both in the U.K. and abroad is given below. Further details are obtainable from the addresses in parenthesis.

## UNITED KINGDOM

National Radio and Television Show, Earls Court, London, S.W. 5
Aug. 26-Sept. 5 (British Radio Exhibitions Ltd., 49 Russell Square, London, W.C.1.)
British Association Annual Meeting, York
Sept. 2-9
(British Association for the Advancement of Science, 18 Adam Street, London, W.C.2.)

Scottish Industries Exhibition, Kelvin Hall, Glasgow
Sept. 3-19 (Matthew H. Donaldson, 2 Woodside Terrace, Glasgow, C. . . 3.)
Farnborough Air Show
Sept. 8-14 (Society of British Aircraft Constructors, 29 King Strcet, London, S.W.1.)
Dielectric Devices (Conference), University of Birmingham ...... Sept. 14-17 (Electrical Engineering Department, The University, Birmingham, 15.)
Modern Network Theory (Conference), University of Birmingham, Sept. 21-24 (Electrical Engineering Deparment, The University, Birmingham, 15.)
Some Aspects of Magnetism (Conference), Sheffield University . . Sept. 22-24 (Institute of Physics, 47 Belgrave Square, London, S.W.1.)
Cabinet Styling Exhibition, Victoria Halls, Bloomsbury Square, London, W.C.1. (B.R.E.M.A., 49 Russell Square, London', W.C.1.)

Scientific Instrument Manufacturers' Association Convention, Hotel Metropole, Brighton

Oct. 22-24 (S.I.M.A., 20 Queen Anne Street, London, W.i.)

Radio Hobbies Exhibition, Royal Horticultural Hall, London, S.W.1 . .Nov. 25-28 (P. A. Thorogood, 35 Gibbs Green, Edgware, Middx.)

Physical Society's Exhibition, Royal Horticultural Halls, London, S.W.I
Jan. 18-22
(Physical Society, 1 Lowther Gardens, London, S.W.7.)
Engineering Materials and Design Exhibition, Earls Court, London, S.W. 5
Feb. 22-26
(Industrial and Trade Fairs Ltd., Drury House, Russell Street, London, W.C.2.)

## OVERSEAS

Acoustics Congress, Stuttgart
Sept. 1-8
(Dr. Ing. E. Zwicker, Breitscheidstr. 3, Stuttgart.)
Firato 1959; International Electronics Exhibition, Amsterdam .... Sept. 1-8 (Firato Secretariat, Emmalaan 20, Amsterdam, Z.)
International Trade Fair, Salonika $\qquad$
$\qquad$
French National Radio \& Television Show, Paris $\qquad$ (Fédération Nationale des Industries Electroniques, 23 rue de Lubeck, Paris.)
Salon Belge de $1^{\prime}$ Electronique, Brussels Sept. 19-24
(Comité des Expositions de la Radio-Electricité, de la Télévision et des Industries Connexes, 7 rue de Florence, Brussels, Belgium.)
Telemetring Symposium, San Francisco
Sept. 28-30
(Robert A. Grimm, Dymec Inc., 395 Page Mill Road, Palo Alto, Calif., U.S.A.)
Irish Radio and Television Show, Mansion House, Dublin .... Sept. 28-Oct. 3 (Castle Publications, 38 Merrion Square, Dublin, Eire.)
Communications Symposium Utica
Oct. 5-7 (E. William Morris, 224 Fairway Drive, New Hartford, N. N., Ü., U.A.)

High Fidelity Music Show, New York . . . . . . . . . . . . . . . . . . . . . . . . . . . Oct. 5-10 (Institute of High Fidelity Manufacturers Inc., 125 East 23rd Street, New York 10, U.S.A.)
Radio-Interference Reduction, Chicago Oct. 6-8
(H. M. Sachs, Armour Research Foundation of Illinois Institute of Technology, Chicago.)
1.R.E. Canadian Convention, Toronto

Oct. 7-9
(Convention Office, 1819 Yonge Street, Toronto, 7.)
National Electronics Conference, Chicago
(N.E.C., 228 N. La Salle Street, Chicago, Iil., UU.S.A.A.)

Electrical Techniques in Medicine and Biology, Philadelphia
Oct. 12-14
(Dr. L. E. Flory, RCA Laboratories, Princeton, N.J., U.S.A.)
Magnetism and Magnetic Materials, Detroit (D. Metism and Magnetic Materials, Detroit....$)$

Computer Conference, Boston Nov. 10-12
. Nov. 16-19 (J. H. Felker, Bell Telephone Laboratories, Murray Hill, N.J., U.S.S.A.)

Dec. 1-3
Reliability and Quality Control Symposium, Washington ...... Jan. 11-13 (R. Brewer, G.E.C. Research Laboratories, Wembley, Middx.)

Solid-State Circuits Conference, Philadelphia
Feb. 10-12 (Tudor R. Finch, Bell Telephone Laboratories, Murray Hill, N.J., U.S.A.)
I.R.E. National Convention, New York . Mar. 21-24 (E. K. Gannett, I.R.E., 1 East 79 Street, N.Y. 21.)


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# IRANDOM RADIATIONS 

## By "DIALLIST"

## America via the Moon

AT the moment of writing no fewer than four different attacks are being made on the problems which beset long-distance wireless communications conducted on the direct transmitting - aerial - to - receiving - aerial systems in use today. The plain, blunt fact is that they're not sufficiently reliable: you can't guarantee a twenty-four-hours-a-day service on three hundred and sixty-five days a year. Amongst the chief snags are blackouts, fading and interferenceand these are not the only ones. Many readers will remember the demonstration given by Professor A. C. B. Lovell in the B.B.C. Reith lectures last year of the fact that it had proved possible in experimental transmissions to use the moon as a reflector of wireless waves. Recently a joint effort by him and the Pye people succeeded in establishing a link for both morse and the spoken word between Jodrell Bank and the U.S. Air Force centre in Massachusetts. The power used was 1 kW at $201 \mathrm{Mc} / \mathrm{s}$, but the e.r.p. with 40 dB of aerial gain would be $10,000 \mathrm{~kW}$. The large Jodrell Bank radio telescope, $250-\mathrm{ft}$ in diameter and costing a vast sum of money, is hardly a practical proposition as a transmitting aerial. But Pye Telecommunications are getting down to the job of developing a $25-\mathrm{ft}$ radio telescope, fed with radio waves of much higher frequency and with far greater power behind them. They will undoubtedly succeed before very long and it is likely that a very important advance in long-distance wireless communication will result.

## Other Approaches, Too

But that's by no means the only way in which the problem is being tackled. The use of artificial satellites as relays was proposed many years ago, and the Press Secretary of the White House said recently that he confidently expects global television to come into being in this way before the end of next year. The most surprising idea of the lot is the child of Westinghouse, of Pittsburgh. They are already producing various types of balloon aerials, some made of fabric incorporating large numbers of fine metallic threads. These aerials are light and easily
transportable. One suggestion is that they should be carried aloft in a deflated condition either by aircraft or by rockets and then be filled with suitable gas and launched.

## Films Across the Pond

IN the system which it has developed for transmitting news films across the Atlantic, by telephone cable, the B.B.C. seem to have accomplished something akin to pouring a quart into a pint pot. In other words, they've evolved a method of squashing the normal $3 \mathrm{Mc} / \mathrm{s}$ TV bandwidth down to well within $6.4 \mathrm{kc} / \mathrm{s}$ which was the channel width allocated for this purpose on the transatlantic cable. It has been done ingeniously by restricting the horizontal definition so that it corresponds to a $1.75 \mathrm{Mc} / \mathrm{s}$ bandwidth in a 405-line system, by reducing the number of lines to 200 with sequential scanning and by transmitting only alternate film frames; at the receiving end each frame is recorded simultaneously on two adjacent frames. The effective repetition frequency is thus $12 \frac{1}{2}$ frames a second. But that's not the whole answer, for if nothing more were done the bandwidth would still be $450 \mathrm{kc} / \mathrm{s}$ and therefore unusable over the cable. It had to be reduced to one hundredth of this figure and that was done by increasing the scanning time. This means
that a one-minute news film takes 100 minutes to transmit and record. Slow though the process may seem, it enables news films to be received on either side of the Atlantic a great deal earlier than if they were flown by fast 'plane. The $16-\mathrm{mm}$ film (almost universally used for TV news purposes) is scanned at the transmitting end by a slow-speed flying-spot scanner, the slow-speed video signal being used to modulate a $5 \mathrm{kc} / \mathrm{s}$ carrier. At the receiving end the demodulated signal is fed to a flying-spot telerecorder with twin optical systems. For scenes involving rapid movements every frame can be scanned instead of every other one. This means that the transmitting time is doubled, but even so this system is much quicker than any other method of getting pictures across the Herring Pond.

## New Giant Labs

WHAT a vast concern the research and development organization of the Bell Telephone System already is! It now employs nearly 11,000 people at 18 stations and soon it will be still bigger, for $\$ 20,000,000$ is to be spent on the erection of new laboratories at the Holmdel site, famous for the work done there by Jansky on aerials and Southworth on waveguides. Jansky was responsible for the invention of the rhombic aerial and, later, for Musa (multiple unit

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steerable aerial), an electrically steerable array of rhombic aerials, which was just about the last word in shortwave reception. The Musa principle was developed in the last war into the electrically steerable multi-rod array. At Holmdel, too, the need for shorter and shorter wavelengths led to an immense amount of invaluable work by Southworth and $h$ 's co-workers on waveguides and to the development of components and specialized valves which are now essential parts of microwave technique. A great deal of priceless work was done in the investigation of the background (sometimes foreground!) noise which can be such a nuisance in short-wave wireless. Jansky was specially interested in the continuous hissing heard when his rotatable aerial was directed towards a particular part of the heavens. He concluded that its origin was an area in the gi ${ }^{\circ} \mathrm{xy}$ some 27,000 light-years away. Thus he laid the foundations of radio astronomy, though it was Lovell who gave it practical form after the end of the war. The tropospheric for-ward-scatter systems had their origin at Holmdel and the work done on waveguides may point the way to a system in which something like 200,000 telephone circuits may eventually be carried by a circular waveguide.

## A Worth-while Guarantee

IT'S good to learn that several manufacturers have extended the guarantee period from six months to twelve months on all new cathoderay tubes. Mazda state that since purchase tax on replacement tubes was knocked off in the Budget there has been a five-fold increase in the demand. Their expectation is that the doubling of the guarantee period will lead to a still greater increase in the sales of new tubes, since people will prefer them to those which have been rebuilt or repaired. They may be right in this, though my own feeling is that so long as there is a biggish difference between the cost of buying a new c.r.t. and a rebuilt one, those firms which have a reputation for doing reliable rebuilding work and are prepared to give as long a guarantee period (as C.R.T. Lid. have announced) won't find themselves idle. The c.r. tube guarantee now lines up with the setmakers' overall guarantee, but there is still a mingy three-months' on valves. And as TV set owners and servicemen know, valve replacements are amongst the most frequently needed repairs.


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## Caveat Amator

I HAVE previously discussed the question of the growing menace of the tape recorder which seems more and more to threaten the sanctity of our private conversations. To my mind the most irritating thing about it is that from a scientific and commonsense point of view, there is some justification for such recording.

But I cannot see any justification at all for a new use of it which, I read, is coming into fashion among modern girls. We all know that in Queen Victoria's time, girls used to tie up their love letters with pink tape and pack them away with lavender-filled sachets. Modern girls have them microfilmed and filed.

Unfortunately certain girls are equipping themselves with portable tape recorders so that they can have a permanent record of any proposals they receive. With some, the idea is undoubtedly to confront their husbands in later days with what they said long years previously. But I expect that with many of them the idea is to collect a round dozen or so of proposals and then to play them back and pick the man who makes the best oratorical effort.

This will improve the standard of eloquence in proposals as men will naturally buy one of these machines to practise on. Thus instead of the few faltering words which most men manage to stammer out, girls of the future may hear something worthy of Shakespeare.

If I had my time over again, I would make the perfect tape recording and then post it to the girl I wished to marry. I doubt if my blonde of long ago could have resisted me if I had used the magic words with which Cupid wooed Psyche, especially if I had finished off by bursting into the famous song "Lovely Art thou" from the opera "Xerxes." This song is, of course, usually known to the vulgar more


A permanent record of a proposal
by its tune-Handel's Largo-than by its passionate words.

However, there is a real and serious danger that tape recordings may one day be accepted as evidence in a breach-of-promise action, and it would not be impossible for an unscrupulous blonde to forge a proposal. She could first obtain several tape recordings of her intended victim's voice in a perfectly normal manner. She could subsequently play these back, and feed the sequels into a sound-on-film recorder so that she could make a visual study of the idiosyncracies of the victim's voice.
Then, following the techniques of Rudolf Pfenniger, she could paint on a strip of virgin film totally fictitious utterances in her victim's voice. These could be played back, and fed to a tape recorder and this recording would then be taken to court, and played over to a sympathetic jury. Believe me, it is a very real danger, and no laughing matter.
[Popping the question on tape is not uncommon. The June issue of the Grundig Gazette, which circulates among dealers, records that Arthur Rowe. of Coventry, US a mailspool." $=$ ED. $]$ more romantic than a mailspool." 1 ED. $]$

## Audio and Photo

THE Photo Fair at Olympia in May had a lot in common with the Audio Fair held elsewhere a month earlier. Both exhibitions were intended to appeal to the same two classes of people, namely those whose chief interest lies in the design of the highclass instruments available at each show, and those who delight chiefly in the end-product, namely a work of art, visual in one case and aural in the other. In both shows were to be found many visitors who were interested in the means as well as the end, and not instead of it.

The Photo Fair was the bigger as it filled the National Hall at Olympia but I could not help thinking what a splendid opportunity there would be of lessening expenses and increasing interest if the Audio and Photo Fairs combined. Together they could easily fill the main hall at Olympia while the smaller National Hall could be fitted with a large number of soundproof demonstration theatrettes such as are needed by both shows, the photographic people, of course, needing them for amateur talkie demonstrations.

In both the Audio and the Photo Fairs this year stereo was a leading feature, and here the

Photo Fair scored heavily for stereoscopy has a hundred years of history behind it and has long since left its childhood days. At the Audio Fair it was only too painfully obvious that stereophony is still in the teethcutting stage of infancy, and those of you who are fathers will know what a howling hullaballoo that can mean.

## Si-Fi

I. OFTEN think that a small but somewhat important point of receiver design which manufacturers neglect is the provision of properly connected sockets for an external loudspeaker. Usually these are just inserted in parallel with the internal loudspeaker.

What's wrong with that, you may ask. Nothing at all if you are just going to use an extension loudspeaker a few feet away. Of course, if the set is of the "Hi-Fi" type even this will upset things a bit from the point of view of a musical purist. But I am not discussing things from the point of view of the longhaired fraternity, but from that of ordinary people like you and me who are addicted to the sugary sort of music usually known as "Si-Fi" because of the sighs it produces from its sentimental audience.

Now. I may be 2 bit of an extremist, but I have an extension loudspeaker in every room. They used all to be of the conventional 3 -ohm or less type, but I soon had to alter that. When you have only 3 ohms or less to play with, the resistance of long extension leads becomes a serious matter. Also, of course, the use of several 3 -ohm loudspeakers in parallel means that the output valve is virtually working into a short circuit. If you want to know what that sounds like, try connecting a couple of 6 -volt 36 -watt car bulbs ( $=\frac{1}{2} \mathrm{ohm}$ ) $\dagger$ in parallel with your loudspeaker.

Now I don't expect all manufacturers to provide me with a separate output valve for each of my extension loudspeakers but they could, I think, provide me with at least one extra secondary winding on the output transformer, such winding being of 15 ohms or so rather than 3 ohms. Naturally my extension loudspeakers would have to be of higher resistance too. If manufacturers can provide me with the extra 15 -ohm secondary, I can easily rewind my speech coils. After all, 30 years ago all readers of Wireless World wound their own speech coils. If you don't believe me turn up your issues of 1927 and see for yourselves by reading the words of F. H. Haynes who designed and fathered the Wireless World moving-coil loudspeaker. It is now, I believe, in the Science Museum; if not, it certainly ought to be, side by side with the "Everyman Four " receiver which certainly is there.
$\dagger$ [Or less if they are not dissipating 72 watts.-ED.]

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| Area of photo element | $1.25 \mathrm{sq} . \mathrm{cm}$. | $2.9 \mathrm{sq} cm.$. |
| Average cell current at 10V d.c.. <br> foot candles and lamp colour <br> temperature $2.700^{\circ} \mathrm{K}$. | 6 mA | 6 mA |
| Maximum ultimate dark current <br> at 100 V d.c. | $5 \mu \mathrm{~A}$ | $<2.5 \mathrm{\mu A}$ |
| Maximum cell dissipation at $25^{\circ} \mathrm{C}$. | 200 mW | 600 mW |
| Spectral response | Same for both cells- <br> sce curve. |  |



Mullard Limited
Mullard House, Torrington Place, London, W.C.I
Telephone: Langham 6633


## now in quantity production



This latest ELAC deflection unit incorporates the new MULLARD Ferroxcube core Type FX 1981, enabling a "pull tack " of 4 mm to be achieved without loss of sensitivity. Line inductances of 5 to 30 mH with $\frac{L}{\mathrm{R}}$ RATIO OF .8 and frame impedances of 2 to 70 ohms are readily available. The standard model is supplied complete with TUNGSTEN steel picture centring plates, positive tube neck clamping device and a terminal panel well removed from adjustment points.

## ELAC

 $110^{\circ}$ Scanning Coil

## Transisforized <br> UNIVERSAL

COUNTER

TMMER

Frequency Measurement

Random Counting

## Frequency Division

Time Measuremēnt

## Frequency Standard



This fully transistorized portable equipment provides for a wide range of time and frequency measurement as well as facilities for counting, frequency division and the provision of standard frequencies. The facilities available are briefly listed below:

TIME/UNIT EVENT (1 LINE): For the measurement of the time interval between two occurrences in a continuously varying electrical function in the range $3 \mu \mathrm{sec}$ to 1 sec . The time for 1,10 or 100 such events can be measured.

TIME/UNIT EVENT (2 LINE): For time measurement in range $1 \mu \mathrm{sec}$ to 2777 hrs . of any interval defined by a positive or negative going pulse in any combination.

EVENTS/UNIT TIME: For frequency measurement in range $30 \mathrm{c} / \mathrm{s}$ to $1 \mathrm{Mc} / \mathrm{s}$ over period of $0.001,0.01$, $0.1,1$ or 10 secs. Crystal accuracy $\pm 2$ parts in $10 \%$ week. For mains or 12 V d.c. operation.

Full technical specification available on request.

[^8]

It is gratifying to know that in a world of rising prices our policy of maintaining and, in many instances, reducing prices has resulted over the years, and especially at this period, in ever increasing sales.

We carry a stock of 2,000 types of receiving, transmitting and special purpose tubes, and invite your enquiries not only for commercial grade tubes but also for those tested to C.V., JAN and MIL specifications.


Our Organisation is A.R.B. Approved.

If you are not already on our Mailing List, please send for latest Price and Stock List.

## HALL ELECTRIC LTD

Haltron House, 49/55 Lisson Grove, London, N.W. 1

Tolephoat:
AMBassidor 1041 (5 lines)
Cables:
Hallectris, Lendse
TELE1 2.2578


## voltage stabilisation down to exceptionally low currents <br> 

Voltage stabilisation down to exceptionally low currents is provided by Mullard Zener Diodes. This feature is particularly marked in the higher voltage types where stabilisation is provided at currents as low as one milliamp. In all types the dynamic impedance is low and the zener characteristic is very sharp. Two ranges of these diodes are available. One with approximately $\pm 5 \%$ tolerance voltages, and the other with approximately $\pm 15 \%$ tolerance voltages. In both ranges the change of zener voltage with temperature is only very small, and the operating temperature is from -55 to $+150^{\circ} \mathrm{C}$. Write on your company notepaper for complete data.


IN SCREENED AND INDIFFERENT AREAS


PERFECT RECEPTION IS ASSURED WITH


THE INSTALLATION OF A

## TELEVISION-F/M RELAY SYSTEM

Where geographical obstacles or industrial locations exist to cause blind spots and interference. Teleng provides the answer with perfect reception. The Teleng Relay System is applicable to new or existing constructions and is the only single wire system to serve standard domestic receivers without modification. The cable is small- $\frac{3}{8} \mathrm{in}$. diameter-and is therefore unobtrusive throughout the entire layout. Complete Teleng systems can be purchased or leased and are backed by a planning and advice service of long experience.

## TELEFUSION ENGINEERING LTD

ONE OF THE TELEFUSION GROUP OF COMPANIES

Teleng Works, Church Road, Harold Wood, Romford, Essex Ingrebourne 42901

## THAT ELUSIVE WORKS MANAGER ...

## 



NO LOUDSPEAKERS, BELLS or FLASHING LIGHTS only the man who's wanted knows and replies.

Selective Induction is saving time, money and worry in Offices, Factories, Hospitals, Hotels, Departmental Stores etc., all over the Country. All key personnel carry small transistorised receivers bearing a number. When they are wanted their numbered key is pressed on a small transmitter. Immediately they must respond to the URGENT 'PEEP PEEP' in their pockets which summons them and them alone to ACTION! A verbal message can be transmitted if desired.

- Covers areas indoors or out, up to $10,000,000$ sq. ft.
- Designed for the man who cannot afford to be tied to his office.
- Equally suitable for large or small concerns.
- Low purchase price-vjrtually no indoor wiring-low rental terms.

Write or 'phone for further particulars - WE CAN BE FOUND IN TEN SECONDS

# personal <br>  <br> (the 'Peep Peep' in the Pocket) 

THE ONLY STAFF LOCATION SYSTEM WORTH INSTALLING


## NEW-A GENERAL-PURPOSE OSCILLOSCOPE

Type TF 1330

* D.C. to $15 \mathrm{Mc} / \mathrm{s}$ pass band * $50 \mathrm{mV} / \mathrm{cm}$ sensitivity * $02 \mathrm{~m} \mathrm{sec} / \mathrm{cm}$ writing speed
* 10 kV e.h.t. for bright clear trace
* Direct-reading time and voltage calibration independent of X-expansion or Y-gain


## BRIEF SPECIFICATION.

Y Amplifier bandwidth : D.C. to $15 \mathrm{Mc} / \mathrm{s}$. RISE TIME: $0.025 \mu \mathrm{sec}$. SENSITIVITY: Seven ranges, 50 $\mathrm{mV} / \mathrm{cm}$ to $50 \mathrm{~V} / \mathrm{cm}$. AMPLITUDE MEASUREMENT : : $2 \%$ accuracy. INPUT: Two switched coaxial inlets. Impedance: : $\mathrm{M} \Omega, 30 \mu \mu \mathrm{~F}$. Optional probe: 10 $M \Omega, 7 \mu \mu F$. DISTORTIONLESS SIGNAL DELAY: $0.25 \mu \mathrm{sec}$.
X Amplifier bandwidth: D.C. to $2 \mathrm{Mc} / \mathrm{s}$. Expansion: Up to at least $\times 5$. External input: DANSION: Up to at least $\times$.
Sweep Generator sweep velocity : 15 ranges, 0.1 $\mu \mathrm{sec} / \mathrm{cm}$ to $1 \mathrm{sec} / \mathrm{cm}$ ät minimum expanision. TIM MEASUREMENT: $2 \%$ accuracy. TRIGGER SELECTION:
A.C. coupled, D.C. coupled, TV field sync. A.C. coupled,
or Automatic.
or Automatic.
General TUBE: 5 inch, spiral accelerator. POWER SUPPLY: $200-250$ and $100-150 \mathrm{~V}$. WEIGHT : 48 lb . PRICE (complete) : $£ 300$; F.O.B. U.K. port.

Please send for leaflet G 154.


AM \& FM SIGNAL GENERATORS - AUDIO \& VIDEO OSCILLATORS FREQUENCY METERS - VOLTMETERS - POWER METERS DISTORTION METERS - FIELD STRENGTH METERS TRANSMISSION MONITORS . DEVIATION METERS OSCILLOSCOPES, SPECTRUM \& RESPONSE ANALYSERS Q METERS \& BRIDGES

Please address enquiries to MARCONIINSTRUMENTS LTD. at your nearest office:


SUPERGRADE

| SIZES | SUPERGRADE |  | STANDARD |  |  | SIZES | LONG PLAY |  |  | DOÜBLE PLAY |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | feet | $\pm$ s. d | feet | C. 5 . |  |  | feet | ¢ s: |  | feet |  | s. |  |
| $3^{\prime \prime}$ | - | - | 150 | 5 | 6 | 3 " | 225 | 8 | 6 | 300 |  |  | 0 |
| $4^{\prime \prime}$ | - | - | 300 | 10 | 6 | 4" | 450 |  |  | 1,200 |  |  |  |
| $5^{\prime \prime}$ | - | - | 600 | 10 | 0 | $5{ }^{\circ \prime}$ | 850 | 18 |  | 1,200 | 2 | 5 | 0 |
| 5!" | 1.200 | 210 | 850 | 17 | 6 | $9^{\prime \prime}$ | 1,200 | 115 | 0 | - | 2 | - |  |
| $7{ }^{\circ}$ | 1,200 | 2100 | 1,200 | 115 | 0 | $7{ }^{\prime \prime}$ | 1.800 | 210 |  | 2.400 | 4 | 0 | 0 |
| $8{ }^{\circ}$ |  | - | 1.750 | 210 | 0 | $84^{\circ}$ | 2,400 | 310 |  | 2. |  |  |  |

## MASTERPIECE..

Fulf lists of tape, prices. accessories, etc., ©: application.

# Mastertape 

MAGNETIC RECORDING TAPE BY
MSS RECORDING CO. LTD. Colnbrook, Bucks.
Telephone: Colnbrook 2431. Showroom and Studic
21, Bloomsbury Street, London, W.C.I. Telephone: MUSeum 1600.

# Four first-class performers 

These four Cossor Oscillographs, each designed for an important range of applications, offer first-class performance backed by rigid adherence to published specifications.



MODEL 1065 PULSE OSCILLOGRAPH

Tube: single-beam, P:D.A. Bundwidhl: d.c. $1015 \mathrm{Mc} / \mathrm{s}$ ( $-50 \%$ ).
Sensitivity: $250 \mathrm{mV} / \mathrm{cm}$. Qvershoor: less than $3 \%$. Time-base: triggered or repetitive over range $40 \mathrm{~cm} / \mathrm{sec}$ to $5 \mathrm{~cm} / \mu \mathrm{scc}$. $X$ Amplifier: gain 5 . continuously variable. Time-base delay: 2 ranges, continuously variable.
Calibration: voltage and time, by calibrated shifts Probe : $1.5 \mathrm{M} \Omega, 12 \mathrm{pF}$


MODEL 1049 INDUSTRIAL DOUBLE-BEAM OSCILLOGRAPH
$Y$ Amplifier: Al: dce to 200 kc 's $(-30 \%)$ at gain 900 : $\mathbf{A} 2$ : d.c. 10 $400 \mathrm{kc} / \mathrm{s}(-30 \%)$ at gain 30.
Time-Base: repctitive or triggered in 18 ranges, down to $7.5 \mathrm{scc} / \mathrm{sweep}$. Intensity modulation: three modes including beam bright-up. Calibration: time and voltage, by calibrated shift ( X and Y 1 ) and multiplier (Y2).

Let us send full details of Cossor Instruments or arrange for a representative to discuss your special needs.

MODEL 1058 FOR THE TV \& RADIO ENGINEER

Tube: single-bcam Bandwidth: d.c. to $6 \mathrm{Mc} / \mathrm{s}(-50 \%)$. Sensitivity: $250 \mathrm{mV} / \mathrm{cm}$. Time-Base: triggered or repetitive, over range $30 \mathrm{~cm} / \mathrm{sec}$ to $1.5 \mathrm{~cm} /$ 山sec. Special facilities for triggering from TV linc or Frame pulses on IV.D.A.P. composite video waveform. $X$ Amplifier: gain 5 . continuously variable. Calibration: time and voltage calibration facilities.


MODEL 1035 GENERAL PURPOSE DOUBLE-BEAM OSCILLOGRAPH
$Y$ Amplifiers: A1: $5 \mathrm{c} / \mathrm{s}$ to $5 \mathrm{Mc} / \mathrm{s}(-30 \%)$, Maximurn gain 3,000 . $\mathbf{A 2}: 5 \mathrm{c} / \mathrm{s}$ to $250 \mathrm{kc} / \mathrm{s}(-30 \%)$ at gain 30 , with trace inversion facility. Time-base: repetitive or triggered in 9 sweep ranges from 100 msec to $10 \mu \mathrm{sec}$. Time-base delay and pulse bright-up facilities. $X$ Amplifier: gain 5 , continuously variable. Calibratlon: voltage and time, by calibrated shifts

# COSSOR ${ }^{\text {nstruuments }}$ tio 

## New oscillograph 1059

## ADVANCED *TRUE DOUBLE-BEAM OSCILLOGRAPH

 *
True double-beam-i.e. both beams use a common $x$-axis and there is no beam swilching.


## CATHODE-RAY TUBE

Cossor 4 in . ( 10 cm .) double-beam, p.d.a., type 93D with green fluorescence, operating with overall accelerating potential of 3 kV or 6 kV .

## Yi AMPLIFIER

$1 \mathrm{c} / \mathrm{s}$ to $10 \mathrm{Mc} / \mathrm{s}(30 \%$ down).
Rise-time : 0.04 usec.
Output deflection: $6 \mathrm{~cm}(4 \mathrm{~cm}$ at $10 \mathrm{Mc} / \mathrm{s}$ ). Sensitivity: calibrated $100 \mathrm{mV} / \mathrm{cm}$ to $10 \mathrm{~V} / \mathrm{cm}$. Sensitivity control : in steps $3: 1$ and $10: 1$ with continuously variable intermediate control. Input Attenuator impedance: $1.2 \mathrm{M} \Omega$ and 65 pF .

## Y2 AMPLIFIER

Identical with Y1 amplifier.

## SIGNAL DELAY

200 musec approximately. Not more than 10 musec differential between charinels.

## PRE-AMPLIFIER (2)

Gain 10. $5 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}$ ( $30 \%$ down).
Input Resistance: $3 \mathrm{M} \Omega$.
One for A1 amplifier, the other for A2 or $\mathbf{X}$ amplifier.

## PROBES (OPTIONAL EXTRA)

Frequency-compensated "L" attenuator.
Input impedance: $6 \mathrm{M} \Omega$ and 15 pF . Insertion loss: 10:1.

## TIME-BASE

Triggered.
Range: $0.03 \mu \mathrm{sec} / \mathrm{cm}$ to $15 \mathrm{msec} / \mathrm{cm}$ in eleven steps. Triggered from positive or negative signals derived externally or from Y1 amplifier.
Sensitivity: pulse- 1 cm . deflection or 2 V external. Sine wave -2 cm deflection or 2 V r.m.s. external at frequencies up to $5 \mathrm{Mc} / \mathrm{s}$. Expansion amplifier, continuously variable gain up to 5 times. Time-base output available at front panel on slow speed ranges. Delayed time-base: continuously variable delay $2 \mu \mathrm{sec}$ to $150 \mu \mathrm{sec}$. Delay jitter not greater than 1 part in 1,000 . Sensitivity pulse -1 cm deflection or 2 V external.

## $\times$ AMPLIFIER

$10 \mathrm{c} / \mathrm{s}$ to $750 \mathrm{kc} / \mathrm{s}(30 \%$ down).
As time-base amplifier : continuously variable expansion up to 5 times.
As independent $X$ amplifier: sensitivity variable from $1 \mathrm{~V} / \mathrm{cm}$ to $100 \mathrm{~V} / \mathrm{cm}$ in 5 ranges.

## CALIBRATION

Voltage measurement: internal calibrating voltage (square wave) referred through sensitivity control of the amplifiers. Accuracy $\pm 3 \%$. Time measurement: by directly calibrated $\mathbf{X}$ shift control ( $\pm 5 \%$ ) and/or by $20 \mathrm{~m} \mathrm{\mu sec}( \pm 3 \%)$ black-out pips (for accurate measurement of rise-time).

## POWER SUEPLY

Mains: 100 V to 130 V and 200 V to 250 V . Frequency: $50 \mathrm{c} / \mathrm{s}$ to $100 \mathrm{c} / \mathrm{s}$.
Consumption: 550 W .
Internal supplies are stabilized where necessary.

## SIZE AND WEIGMT

| Height: | $17 \frac{1}{2} \mathrm{in}$. | $(43.2 \mathrm{~cm})$. |
| :--- | :--- | :--- |
| Width: | $12 \mathrm{in}$. | $(30.5 \mathrm{~cm})$ |
| Depth: | $24 \frac{\mathrm{in}}{}{ }^{2}$. | $(62.9 \mathrm{~cm})$. |
| Weight: | 80 lb. | $(36.3 \mathrm{~kg})$. |

## ACCESSORY

Camera Model 1428.

## UNANANSTRUMENTS LTD

The Instrument Company of the Cossor Group

## एHOCO <br> PLUGS \& SOCKETS

* all anele phono pugs and sockets are mad for the intienational standaro. * sockets are avalable from I.s war with front insuluting plate if reeureg.
'NOTE: ADD SUFFIX "A" TO SOCKET TYPE NUMBER IF FRONT INSULATING PLATE IS TO BE SUPPLIED WITH SOCKET, e.g., RAI703 "A "


RA1647


RA1648


RA1702


RA1703


IMPROVED PHONO PLUG


The design features of this plug are as follows:
I. Easy withdrawal.
2. Outer braiding easily connected to outer shell of pluge
3. Soldered joints, if required, are covered.
4. These plugs may be inserted side by side in standard sockets.
5. Plugs may be colour coded.



This component has been designed with many applications in view:
Switching inputs, Terminating inputs, Terminating outputs, etc., etc.


## ARIEL PRESSINGS LTD.

NORTH STREET, ILKESTON, DERBYSHIRE.

Phone: ILKESTON 3651. Grams: ARIEL ILKESTON, NOTTINGHAM.


# Isolation at <br> <br> Microwaves 

 <br> <br> Microwaves}

## L324 X-band isolator

This isolator is a ferrite loaded waveguide component with unidirectional characteristics designed to isolate an X-band microwave source from reflections caused by mismatch. It is a versatile component suitable for incorporation in equipment or for use as a laboratory aid. It is tunable for peak performance over X-band.

For information on other microwave components including circulators, co-axial mixers, switches, folded tecs, etc., write to the address below.

TYPICAL GRAPH OF VARIABLE ISOLATOR


## 

## Thio Cuttoutative Pook

## FOR THE FIRST TIME IN BRITAIN

NOW POWER - Simplan
WIRE-WOUND
 RESISTORS!


## HIGH GRADE RESISTORSAT LOW COST

A new Dubilier process makes available to the design engineer a power wire-wound resistor possessing highgrade characteristics which costs no more than an equivalent standard type. The resistance wire is uniformly wound on a silicone-processed fibre-glass core which is then sealed into a ceramic housing. The result is a remarkably stable resistor which is completely insulated except for the connecting wires.

## PERFORMANCE UNDER OPERATING

 CONDITIONS* Resistance change less than $5 \%$ after 100 hours at $40^{\circ} \mathrm{C}$. ambient temperature and $95 \%$ relative humidity.
* Resistance change less than $2 \%$ after three times normal load for 5 seconds.
* Resistance change less than $5 \%$ after 500 hours at full load in $25^{\circ} \mathrm{C}$. ambient temperature.
* Resistance change less than $1 \%$ and no physical effects due to soldering.


## MAXIMUM TEMPERATURE COEFFICIENT

 BETWEEN - 55 and $+275^{\circ} \mathrm{C}$.| TYPE | $0.05 \% /{ }^{\circ} \mathrm{C}$ | $0.03 \%{ }^{\circ} \mathrm{C}$ |
| :--- | :--- | :--- |
| PW5 | $0.5 \Omega$ to $2.5 \Omega$ | $2.5 \Omega$ to $2.0 \mathrm{k} \Omega$ |
| PW7 | $0.5 \Omega$ to $8.0 \Omega$ | $8.0 \Omega$ to $6.5 \mathrm{k} \Omega$ |
| PWIO | $1.0 \Omega$ to $10 \Omega$ | $10 \Omega$ to $10 \mathrm{k} \Omega$ |

DOBILTEBS
DUBILIER CONDENSER CO. (1925) LTD TELEPHONE: AOORN 2241

FIG. I. DERATING CURVE


FIG. 2. TEMPERATURE RISE/LOAD


| TYPE | PW5 | PW7 | PW10 |
| :--- | :--- | :--- | :--- |
| Wattage | 5.0 | 7.0 | 10.0 |
| Min. Value | $0.5 \Omega$ | $0.5 \Omega$ | $1.0 \Omega$ |
| Max. Value | $2.0 \mathrm{k} \Omega$ | $6.5 \mathrm{k} \Omega$ | $10 \mathrm{k} \Omega$ |
| Length | $\frac{7}{8}^{\prime \prime}$ | $125 / 64^{\prime \prime}$ | $17_{8}^{\prime \prime}$ |
| Wing |  |  |  |

Width and height of all three types are $3^{\prime \prime}$ "and "1/32" respectively.
 any two activities capable of being translated into electrical phenomena (within its frequency and phase shift limitations) can be recorded simultaneously for future study and application. Experience has shown that the scope of such an instrument when used for Research purposes is almost unlimited.

Model $3 \mathrm{C} / \mathrm{Fi} \mathrm{N}$ Full specification of Model 3C/FN 一 which is not for domestic use-availablo on application. Illustrated leaflet GA767, describing all other Ferrograph Tape Recorders, will be sent on request.

$$
\text { The Incomparable } F^{\prime N}
$$



## adjustable pot cores gives you

## outstanding

advantages

- Wide range of sizes
- Easily assembled
- Close tolerance permeability
- Precise and easy inductance adjustment
- Stability
- Single hole chassis mounting

Mullard Vinkors are the most efficient adjustable pot core assemblies commercially available. In addition to high performance. they have the distinct advantage of close tolerance permeabllity, thus enabling designers to precalculate to within $\pm 3 \%$ the inductance of the core when wound. Final adjustment, taking into account normal capacitor tolerance, can be easily effected to an accuracy of better than $0.02 \%$ by means of a simple self-locking device bullt into the core.
Write today for full details of the wide range of Vinkors currently available.

## Mullard

## VINEOR POT CORES



Today you can enjoy the ultimate reality of Hi-Fi with this superb STEREO AMPLIFIER

Designed specifically for the serious stereophonic enthusiast and available at a really competitive price.

## 10 WATTS <br> OUTPUT ON EACH CHANHEL

No additional pre-amps required.

RETAIL PRICE £33.10.0

## FEATURES FOR THE DISCRIMINATING

- Two identical matched power amplifiers, two identical pre-amplifiers, on a single chassis.
- High sensitivity suitable for all types of high fidelity pickups.
- C core transformers for high efficiency and small magnetic field.
- Switched tone controls, for accurate matching between channels, with true " flat "position.
- Separate tone controls for each channel to enable the response of the separate channels to be controlled on monaural sound.
- Separate inputs for pickups, tape decks and radio.
- Recording characteristic correction for 78 and L.P. records.
- Long switch spindles and separate escutcheons to enable amplifier to be built into customers' cabinets.
- Power available to drive tape deck or radio feeder unit.


## WRITE FOR LEAFLET <br> STEREO AMPLIFIER

AIRMEC LIMITED: HIGH WYCOMBE: BUCKS
Telephone: High Wycombe 2060


The 4300 range of carbon film resistors is available where a reliable high stability close tolerance resistor is required for use in critical circuits.

The range comprises five main groups$1 / 10$ W., $1 / 4$ W., $1 / 2$ W., $3 / 4$ W., and 1 W . Within the limits listed below resistors are available in all preferred values, Other values can be supplied to Order.


Standard Telephones and Cables Limited
Registered Office: Connaught House, Aldwych, London, W.C. 2


Tola ©eLesfion tud. THAMES DITTON, SURREY, ENGLAND. Telephone: Emberbrook $3402 / 6$


In addition to the wellknown Hivac ranges of subminiature valves, cold cathode tubcts and neon indicator lamps, there is an extensive and growing range of small filamentary indicator lamps.

The range includes wire ended types and lamps on MBC, MES, LES or BAT/S caps as well as telephone switchboard lamps conforming to British, Continental and American practice.

Both metal and carbon filaments are available and all voltages up to 60 V can be supplied.

May we provide details of current types or discuss your special requirements? .

STONEFIELD WAY SOUTH RUISLIP.
A member of the Automatic Telephone \& Electric Group.
Ruislip 3366


Thousands of "Super Comit" Aerials are providing perfect T.V. reception in the Greater London area alone. It resonates on both bands without adjustment. It can be fitted out of sight in any room at no installation cost. The "Super Comit" Aerial is much more sensitive than set-top models - and balanced signals are assured over a much greater area. Supplied in untarnishable "LUSTRE GOLD" and Cream finish. (Waterproof and therefore also suitable ior exterior fixing.) Retails at $22 / 6 d$., or with fitted Co-axial plug 25/.


## RCA



SSB-L1 Fixed Station. 60 watt ( 500 watt double sideband equivalent) eight channels $3-15 \mathrm{mc} / \mathrm{s}$.

## SINGLE SIDEBAND

## Communications system

Over 4000 RCA single sideband equipments are in use the world over as fixed and mobile stations.

- Eight Channels.
- Instant Selection of Upper or Lower sideband.
- Compatibility with double sideband systems.
- Remote aerial tuning facility for SSB-L1.
- Mechanical Filter giving outstandingly High Selectivity.
- Exceptionally Stable and Reliable Operation.
- Rugged construction for naval and military use.



SSB-L30M Mobile Station. 30 watt ( 250 watt double sideband equivalent) eight channels $3-15 \mathrm{mc} / \mathrm{s}$.


RCA GREAT BRITAIN LTD. LINCOLN WAY, SUNBURY-ON-THAMES, MIDDX. Tel: Sunbury-on-Thames 3101 An Associate Company of Radio Corporation of Ancrica.

## BIG-SELLERS

## FROM THE WHITELEY CABINET WORKS

W.B. cabinets and tables have acquired a high reputation for quality and those shown here reflect the traditionally high standards of materials and craftsmanship that distinguishes all W.B. products. Yet-they are offered at prices that will make for ready sales at all seasons. Your usual factor cañ supply from stock, and we shall be pleased to send supplies of illustrated leaflets on the W.B. products on request.


This contemporary styled table is finished in highly polished walnut veneer and fitted with self-adjusting "gliders." It is supplied packed flat ready for instant assembly, simply by inserting concealed bolts.
DIMENSIONS: $20 \times 20 \times 20 \mathrm{in}$.

- Price $\mathrm{E} 3 / 15 /$ -

'Junior' Table Price E4/10/Measures $20 \times 20 \times 21 \mathrm{in}$. high.


## $\star$ See our two new tables for

 "Slimline" T.V. receivers at the Radio Show on Stand number 63

This is one of our new serles of contemporary style cabinets in satin-striped sapele veneers. It is supplied in ready-toassemble form and put together in a few minutes with a screwdriver. It will provide absolute realism in reproduction when used in conjunction with Stentorian 8 in or 10 in . units, and has provision for Tweeter unit.
Size: $33 \times 19 \times 19 \frac{1}{2} \mathrm{in}$.
Price fili/li/-

# everybody's enthusiastic! 



Angus McKenzie in TAPE RECORDING \& HI-FI MAGAZINE

6Sometimes, all too rarely, a product received for review has ̀ ar quite outstanding performance and is reliable and robust. Such a product is the Simon SP4 . . . It has a superb performance in every way, with not one snag In the way of it-.. Staggering Performance . . Any owner of an SP4 can be very proud of it. I feel sure that this machine will go far to establishing a new standard of quality by which other machines will be judged.'
Percy Wilson m.A. in THE GRAMOPHONE
6 First-class marks for its comprehensive design, for its cleanness and thoroughness of construction, and for its excellent performance... This is a tape recorder that is outstanding by any standards the world over.'

## J. Moor in THE TAPE RECORDER

The novel features incorporated in the SP4 are generally of great value to the user, and are not gimmicks . . The Simon machine is not cheap but it has exceptional facilities, a good performance, is undoubtedly good value for money.'
J.C. G. Gilbert F.R.S.A., Assoc.I.E.E., M. Brit. I.R.E., F.T. .s. in MUSIC TRADES REVIEW

At last with the Simon SP4, I have found a machine that is not only simple to use, but is capable of producing professional results . . . Has facilities only found in truly professional machines costing £350 and upwards . . . This machine, both in performance and appearance, is unlikely to be superseded for many years.

## you must hear it!

The Simon SP4 is the machine you've been looking for! Its combination of high performance and range of exclusive features has set off a chain reaction of enthusiasm throughout the hi-fi world.

Look at this list of star features-never have so many been brought together in a portable recorder.

Read what the press says, then come and see it for yourself at your nearest dealer-try it, test it and you too will join the crowds of Simon enthusiasts.
*Automatic, in the Simon sense, is meant to be taken literally: it means continuous replay -the machine stops, reverses and changes to the other track with only a two-second pause, and with no necessity to touch any control. Similarly, up to three hours, continuous recording can be made without attention, the machine automatically stopping at the end of the second track.


ACCURATE TAPE POSITION INDICATOR
based on linear tape scale
-PIN-POINT' MODULATION with cathode ray magic eye
SIMON AUTOMATIC DECK fully 'push-button-controlled' AUTOMATIC TAPE REVERSAL without touching controls 3-WAY MIXING FACILITIES on both record and playback BASS AND TREBLE LIFT AND CUT with.independent controls REMOTE CONTROL FACILITIES on both record and playback HIGH QUALITY MONITORING

Paired bass and treble loudspeaker units
10 WATTS OUTPUT from ultra-linear push-pull amplifier PUSH-PULL OSCILLATOR for noise and hum suppression ACCIDENTAL ERASURE PREVENTION
by special record 'safety button'
ald be pleased to arrange HP terms


## well connected with...



Superspeed Cored Solder, incorporating Enthoven's unique 6-channel stellate core, is unchallenged as the most efficient cored solder wire for general assembly work on radio, television, electronic and telecommunication equipment. It speeds production, reduces costs and makes a vital contribution to the dependability of your products.

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for normal electrical assembly work

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Frequency range 2 Mc.- 18 Mc . Three pretuned channels selected by switch. Frequency control regulated either by manually tuned MASTER OSCILLATOR or crystal oscillator.
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## WHAT is the REMSCOPE?



## BRIEF SPECIFICATION

Dimensions: $23 \frac{1}{2}^{\prime \prime} \times 14 \frac{1}{2}^{\prime \prime} \times 24^{\prime \prime}$
Screen diameter: 10 cm
Resolution: $\quad 20-30$ lines/cm
Storage time: 1 week
Display time: $\quad 15$ mins- 2 hrs
Erase time: Less than 1 second
Writing speed: $2-4 \mathrm{~cm} /$ microsec

THE REMSCOPE is the latest storage oscilloscope designed and manufactured by Cawkell's. It can store a single transient signal for a week and display it for up to two hours during that week. A new image storage tube has been used and faster writing speeds than ever before can be achieved. An exceptionally wide range of sweep speeds and input attenuator ratios makes the " Remscope " suitable for a very large number of applications and every effort has been made to ensure optimum performance and, in particular, reliable triggering. Accurate time and voltage calibration signals are provided.

Max. Sensitivity: $5 \mathrm{mV} / \mathrm{cm}$
Max. Bandwidth: $0-3 \mathrm{Mc} / \mathrm{s}$
Sweep velocity: $3 \mathrm{~cm} /$ microsec$0.1 \mathrm{~cm} / \mathrm{S}$

Voltage accuracy: $\pm 1 \%$

Power supplies: $100-110,200-250 \mathrm{~V}$ $50-60 \mathrm{c} / \mathrm{s}$

# ... via the moon' 

MAY 14th, 1959.
A new chapter in communications history was opened when scientists from Manchester University at Jodrell Bank transmitted the first messages in morse code and speech to America via the moon.

The transmitting and receiving equipment which successfully sent the messages a distance of half a million miles was designed and manufactured by Pye telecommunications engineers.

Foremost in design and manufacture Pye Telecommunications equipment is today solving communications problems in more than 90 countries throughout the world . . . tomorrow in space.



FEATURING PYE TELECOMMUNICATIONS EQUIPMENT


Brief specification:
Service: AI, A2, A3 Telephony, M.C.W. Telegraphy.
Frequency Range: $A, 1.6-2.3 \mathrm{Mc} / \mathrm{s}$. B. $2.0-3.9 \mathrm{Mc} / \mathrm{s}$. C. $3.9-7.4 \mathrm{Mc} / \mathrm{s}$. D. 7.4-14.0 Mc/s.

Modulation Capability: $100 \%$ -
Receiver Sensitivity: $I \mu \mathrm{~V}$. for I watt output (modulation: $30 \%$ at $\mid \mathrm{ke} / \mathrm{s}$.). Signal-to-Noise Ratio: Better than 12dB (conditions as above).


BY aprointment

- h.r. OURE OF EDINBURGH sUPPLIERS OF
MADIO TELEPHONE EQUIPMENT
ye telecommunications hto

60 watt H.F. Fixed Station

The Pye 60 watt H.F. Fixed Station PTC93I/941 is designed for continuous unattended operation under all climatic conditions. It is ideally suited for ground-toair or point-to-point operation in those areas where local conditions restrict the use of v.h.f. An unusual feature-in a station of this size is push-button selection of any one of four channels either locally or, remotely, up to 15 miles. Extension and remote control units for channel selection or for the control of the entire station are available.

## PYE TELECOMMUNICATIONS LIMITED



FEATURING PYE TELECOMMUNICATIONS" EQUIPMENT


1 kW V.H.F.
Transimitter

The Pye PTC3600 I kW V.H.F. Transmitter is a medium power communications equipment. It is very suitable for long range en-route ground-to-air operation and also for airport ground-to-air control, teleprinter and V.F. point-to-point links. Comprehensive metering facilities are included.

## PYE TELECOMMUNICATIONS LIMITED NEWMARKET ROAD CAMBRIDGE

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will not change the characteristics of the GD 85 WR
C.V. (4516)

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Specially constructed for military and commercial service where tubes are to be subjected to severe shock and thermal extremes, this new tube will continue to operate satisfactorily beyond the point which is customarily associated with conventional tube structures.

BRIEF DATA
Nom. stabilized voltage 85 V
Striking voltage (total darkness or light) 125 V max.

Current range
Max. Incremental resistance
$500 \mu \mathrm{~A}$ to 5.0 mA
$<1000 \Omega$ Temperature Range: $-60^{\circ} \mathrm{C}$ to $+90^{\circ} \mathrm{C}$

For full information write to: Technical Services Dept.

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Data Sheets, Application Reports etc., advice and assistance in techniques of application are frecly available.


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## * FIXINGS CONFORM TO ACCEPTED PRACTICE

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## $\star$ PRICES ARE HIGHLY COMPETITIVE

For utmost reliability all 'English Electric' miniature instruments have been designed with a higher-than-normal torque/weight ratio in combination with lower power consumption. All types have been successfully subjected to the following tests:
RESISTANCE TO IMPACT SHOCK OF 200 g in any plane.
VIBRATION FATIGUE TEST-two million cycles at peak resonant frequency.
OSCILLATORY TEST-up to one million operations.

SPECIFICATIONS B.S. 89-1954 and other International Specifications.

TYPES
Moving coil for D.C. applications.
Rectifier moving coil for A.F. applications.

Thermo-couple operated moving coil for R.F. applications.

SIZES
Square: $2^{\prime \prime}, 2 \frac{1^{\prime \prime}}{2}$ and $3 \frac{1}{2}^{\prime \prime}$ nominal scale length.
Round: $2 \frac{1}{2}^{\prime \prime}$ and $3 \frac{1}{2}^{\prime \prime}$ nominal scale length.
Rectangular: $5^{\prime \prime} \times 6^{\prime \prime}$ or $3^{\prime \prime} \times 4^{\prime \prime}$ nominal case size.

Desigh registrations pending.
 wattmeter
Left: 2t" round moving coil microammeter
Over 50 standard ranges in any of the seven case types.

Delivery ex stock for standard ranges.
Non-standaŕd ranges to customer's specification within 21 days.

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New concepts in electronics have been developed at AWA, as a result of experience with missile systems. Now they have a wider application. Here are some of the new AWA devices now available to industry.

## U.H.F. RECEIVER

Designed as a Wide Band Low Noise Receiver for the $420 / 470 \mathrm{Mc} / \mathrm{s}$ Frequency Band. Available as either a $19^{\prime \prime}$ rack mounted unit c/w Stabilised Power Unit, or in an $8^{\prime \prime}$ Case with separate Power Unit. Basic arrangement consists of R.F. Amplifier, Mixer, Local Oscillator, I. F. Amplifier (A.G.C. Controlled) Cathode Follower Output Stage. Wide variations of this Receiver can be supplied to customers' own requirements.
Siandard Specification: Frequency Range: $420 / 470 \mathrm{Mc} / \mathrm{s}$; Bandwidth: 4.5 Mc/s; Noise Factor: 10db (approx.): Intermediate Frequency: $45 \mathrm{Mc} / \mathrm{s}$;


Sensitivity: 25 MicroV. for a 12 db signal to noise ratio; R.F. Gain: 12 db . I.F. Gain: 80 db ; Image Rejection: 40 db ; Input Impedance: 75 ohms (approx.) Unbalanced; Ourpur Iinpedance: 80 ohms (appiox.) ; Ourputs: (a) $0.5 v$ from Crystal Detector, (b) 300 mV at $45 \mathrm{Mc} / \mathrm{s}$.

## DIRECTIONAL COUPLER

Of the "Loop" type, suitable for measurements of R.F. power and Standing Wave Ratio in coaxial cables. Directional properties are largely unaffected by frequency changes, so coupler may be used to help obtain optimum termination for a 52 ohm coaxial system up to $600 \mathrm{Mc} / \mathrm{s}$.
72 ohm version of this instrument is also available.
Standard Specification: Case Size: 7" x4" x $2 \frac{1}{2}{ }^{\prime \prime}$; Weight: 4 lbs .3 ozs. ; Power Measurement: low range I w ew max.,

highrange 5w cw max. ; Accuracy (at frequency of calibration): low range $0 . I \mathrm{dbs}$, high range 0.2 dbs ; Directivity: 26 dbs (approx.); Coupling Coefficient: 30 dbs (approx.).


## PRECISION OSCILLATOR

The Oscillator has been designed round a disc sealed triode and particular attention has been paid to ensure good frequency stability. This has been achieved by the use of selected materials and concentric sleeve tuning. The latter in conjunction with Micrometer head tuning giving very good resolution In order to reduce R.F losses all cavities and lines are silver plated, polished, and rhodiun flashed.
The Oscillator can be supplied in the form illustrated for installation in the customers'own equipment, or as a unit complete with its own stabilised power supply mounted on a $19^{\prime \prime}$ panel. Standara Specification: Frequency: Adjustable to operate in the 450/550 Mc/s band. Actual Tuning Range in this band is approx. $30 \mathrm{Mc} / \mathrm{s}$; Frequency Stability: Better than 1 par, in $10^{2}$ (long term); Input: 300 v at 30 $m A, 6.3 v$ at $0.4 A$; Power Output: Max. output 1.25 w at $470 \mathrm{Mc} / \mathrm{s}$

All devices are adaptable to suit customer s own requirements. For further information consult:
COMMERCIAL ELECTRONICS DEPT.
SIR W. G. ARMSTRONG, WHITWORTH AIRCRAFT LTD.. Baginton, Coventry, England.

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says "That's a gay new box. Ah; 'scotcr' Brand Magnetic Tape. Eye can tell there's quality inside, just as everybody says.'

## YOUR EAR

says '"This 'sсотсн' Brand Tape certainly lives up to its reputation. It sounds perfect to me, and I'm an ear for music."

## YOUR COMMON-SENSE

says "The quality suits the sound engineer-the exclusive silicone 'dry lubrication' minimises wear on magnetic heads -the price suits the pocket--well, it's 'scotch' Brand for me every time!"

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Tensilized Polyester is the wonderful new 'scotch' Brand Magnetic Tape. It's extra strong, and gives you double the playing time! Resists stretching. Keeps its high quality of reproduction year after year!



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 MARKER STRIPS(a) Conductor hooked under

(c) Cable secured by crimping
(d) Upturned ends hold terminal under screws before tightening
(b) Cable clamps avallable if required R.H. (or L.H.) as desired

'Standard ' series are available with various types of terminals, up to 21 way'Miniature ' series up to 12 way. Insulating materials phenolic or 'Mikacin' as specified.

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Sorensen high current Regulators have been installed by the G.P.O. (London-Oxford-Birmingham Link), Thorn Electrical Industries Ltd. (Atlas Lamp Works), and Marconi Wireless Telegraph Co. Lid. (Baddow Research Laboratories).

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VOLTAGE SELECTORS

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## COMPONENTS



## VOLTAGE

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4 WAY BVS/4
RIAC.K P.F. MOULDING

Ashtead, Surrey. Tel: Ashtead 3401

## CHOOSING YOUR

Selecting a loudspeaker by audition is the most difficult problem confronting the purchaser of high quality equipment as it is necessary to differentiate the sound heard into two components-that due to the programme and that due to the speaker. The following procedure, whilst being by no means exhaustive, will help to ensure that the choice is the correct one to give the maximum musical pleasure in the years to come.


Not more than four loudspeakers should be tested at one time in order to avoid confusion and the listener should be symmetrically seated in relation to the loudspeakers.
Ask your dealer to feed a clean Ask your dealer to feed a clean
programme to one of the loudprogramme to one of the loudspeakers with all amplifier controls level. A good local studio VHF transmission is best for this test as very few records can be played on
wide range speakers without some wide range speaker
degree of filtering.
Adjust the volume level to give the correct perspective for the programme. (i.e., so that the volume is commensurate with the impression of distance in the programme.)
Listen to each loudspeaker in turn. In professional listening tests the greatest care is taken to pre-set the relative power fed to each loudspeaker as it is very important that they all operate at the same apparent loudness. If your dealer is not fitted up with this facility, then he or you will have to adjust the volume by hand-as accurately as possible.

Try to decide which loudspeaker is the most natural. Beware of sensationalism or "gimmick" balances. If the sound is sensational make sure it is the music that is sensational and not the loudspeaker.

Next take a modern recording or recordings of your choice (as sensational as you like this time). Using the loudspeaker previously selected as the most natural, play the recording and adjust the filters to reproduce the maximum quality Inherent in the recording. With these same settings refer back to the other loudspeakers to see that the one selected in the first test remains the best in the second test.

Should there still be doubt, try changing the relative positions of changing the relative position

There are of course additional tests which should be made adequate power output-adequate dispersion, etc. Best of all-but unfortunately seldom possible-is to borrow the speaker of your choice from a friend and try it at home.


The fact that the QUAD electrostatic shows up as first choice under these conditions does not invalidate the test procedure. It may be recommended for loudspeakers of all types, shapes and sizes.

## (1) (1) $\triangle$ for the closest approach to the original sound

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We hold stocks of many British instruments from leading makers. Our association with British manufacturers from (alphabetically speaking!) Advance to Wayne Kerr goes back many years and we maintain a comprehensive index and technical information service covering the electronic instruments of the world.
OUR FIRST CONSIDERATION一the right instrument for your application.
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Our importation service is second to none. Import licenses, treasury licenses for duty free importation, customs and clearance arrangements, checking on arrival, and most important of all implementation of the overseas manufacturers guarantee are taken care of without trouble to you.

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RESEARCH by Parmeko into the whole field of audio frequency amplification has led to the developmentand production of this new range of transformers for use with many of the well-known high fidelity amplifier designs.

PRODUCTION with specialized plant (many of the operations are performed on automatio machinery) by specialist personnel gives a degree of precision for which Parmeko transformers are now world famous.

## testing

is an essential part of the Parmeko production cycle. Every completed transformer is given a full functional test to ensure its complete reliability in service.

For further information write for illustrated technical leaflet No. 359

| $\begin{aligned} & \text { Cot. } \\ & \text { No. } \end{aligned}$ | Ousput | $\begin{gathered} \text { Uitra } \\ \text { Linear } \\ \text { Toppings } \end{gathered}$ | $\left\|\begin{array}{c} \text { Rating } \\ \text { (Watts) } \end{array}\right\|$ | $\begin{gathered} \text { Primary } \\ \text { Impedance } \end{gathered}$ | Primary Inductance lovso~ | $\begin{array}{\|c\|} \hline \text { P/5 } \\ \text { Leokege } \\ \text { induck- } \\ \text { ance } \end{array}$ | Secondary Impedonce | Construction | Amblifier Design |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| P2629 | ${ }^{\text {EL84 }}$ | No | 12.5 | 6000 or $8000 \Omega$ C.T. | $\begin{aligned} & \text { S5H } \\ & \text { MIN. } \end{aligned}$ | $\begin{aligned} & \text { 30MH } \\ & \text { MAX. } \end{aligned}$ | $\begin{aligned} & 3.75 \text { or } 150 \\ & \text { SER/PAR. } \end{aligned}$ | 5084/12C | Mullard 5-10 |
| P2642 | $\begin{aligned} & \text { EL84 } \\ & \times 2 \end{aligned}$ | 43\% | 12.5 | $8000 \Omega$ C.T. | $\begin{aligned} & 55 \mathrm{H} \\ & \text { MIN. } \end{aligned}$ | $\begin{aligned} & \text { 3OMH } \\ & \text { MAX. } \end{aligned}$ | $\begin{aligned} & 3.75 \text { or } 15 \Omega \\ & \text { SERIPAR. } \end{aligned}$ | 5084/12C | Mullard 5-10 or Brimar 2/8P2 8 Wate |
| P2643 | $\begin{aligned} & \mathrm{EL} 84 \\ & \times 2 \\ & \hline \end{aligned}$ | 20\% | 12.5 | $\begin{aligned} & 6000 \Omega \\ & C . T . \end{aligned}$ | $\begin{aligned} & \text { 5SH } \\ & \text { MIN. } \end{aligned}$ | $\begin{aligned} & \text { 30MH } \\ & \text { MAX. } \end{aligned}$ | $\begin{aligned} & 3.75 \text { or } 15 \Omega \\ & \text { SERPR } \\ & \hline \end{aligned}$ | 5084/12C | Mullard 5-10 |
| P2611 | EL84 | No | 3 | $5000 \Omega$ | 8 H MIN. AT 5OMADC | $\begin{aligned} & \text { MAMH } \\ & \text { MAX. } \end{aligned}$ | $\begin{aligned} & 3.75 \text { or } 15 \Omega \\ & \text { SER/PAR. } \end{aligned}$ | 5084/7C | Mullard 3 Watt <br> Type 'A: Tape Amplifier |
| P2934 | $\begin{aligned} & \mathrm{EL34}_{\mathrm{X} 24} \\ & \hline \end{aligned}$ | 43\% | 20 | $6600 \Omega$ C.T. | $\begin{aligned} & 90 \mathrm{H} \\ & \mathrm{MIN} . \end{aligned}$ | $\begin{aligned} & 30 \mathrm{MH} \\ & \text { MAX } \end{aligned}$ | $\begin{aligned} & 3.75 \text { or } 150 \\ & \text { SER/PAR. } \end{aligned}$ | $5084 / 3 \mathrm{C}$ | Mullard 20 Watt |
| P2647 | $\begin{aligned} & \mathrm{EL34} \\ & \times 2 \end{aligned}$ | 43\% | 20 | $660013$ C.T. | $\begin{aligned} & 90 \mathrm{H} \\ & \mathrm{MIN} . \end{aligned}$ | $\begin{aligned} & 8 \mathrm{MAX} \\ & \hline \end{aligned}$ | $\begin{aligned} & 3.75 \text { or } 15 \mathrm{D} \\ & \text { SER/PAR. } \end{aligned}$ | 6005/57 | $\begin{aligned} & \text { Mullard } 20 \text { Watt } \\ & \text { (' }{ }^{\prime} \text { Core) } \end{aligned}$ |
| P2820 | $\begin{aligned} & \mathbf{U C L B L}^{2} \\ & x^{2} 2 \end{aligned}$ | No | 8 | $6000 \Omega$ C.T. | $\begin{aligned} & \text { 60H } \\ & \text { MIN. } \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { 2IMH } \\ & \text { MAX } \end{aligned}$ | $\begin{aligned} & 3.75 \text { or } 15 \Omega \\ & \text { SER/PAR. } \end{aligned}$ | 5084,8C | Mullard ACJDG 7 Wate Amplifier |
| P2928 | ECL82 | No | 2 | 5600 ת | 12 H MIN AT JOMADC | $\begin{aligned} & \text { 46MH } \\ & \text { MAX. } \end{aligned}$ | 158 | 5089;5E | Mullard 2 Watt Sterco |
| P2932 |  | 20\% | 7 | $\begin{aligned} & 9000 \Omega \\ & \text { C.T. } \end{aligned}$ | 100 H MIN | 5OMH MAX. | 3.75/8/15 | 5084;9C | Mullard 7 Watt Stereo |
| P2632 | $\begin{aligned} & \text { N709 } \\ & \times 2 \end{aligned}$ | 20\% | 12 | $\begin{aligned} & 7000 \Omega \\ & \text { C.T. } \end{aligned}$ | $\begin{aligned} & \text { 60H } \\ & \mathrm{MIN} . \end{aligned}$ | 100 MH MAX. | $\begin{aligned} & 3.75 \text { or } 15 \Omega \\ & \text { SER/PAR. } \end{aligned}$ | 5080,6 | G.E.C. Osram 912 |
| P2649 | $\begin{aligned} & \mathbf{x} 2 \\ & N_{720} \\ & \times 2 \end{aligned}$ | 20\% | 12 | $\begin{aligned} & 7000 \Omega \\ & \text { C.T. } \end{aligned}$ | $\begin{aligned} & \text { 50H } \\ & \text { MIN. } \end{aligned}$ | $\begin{aligned} & \text { MOMH } \\ & \text { MAX } \end{aligned}$ | $\begin{aligned} & 3.75 \text { or } 150 \\ & \text { SER/PAR. } \\ & \hline \end{aligned}$ | 5084/120 | $\begin{aligned} & \text { C.E.C. Osram } 912 \\ & \text { (Printed Circuit Version) } \end{aligned}$ |
| P2580 | $\begin{aligned} & 6 \mathrm{6L6} \\ & \times 2 \end{aligned}$ | No | 40 | $\begin{aligned} & 1000 \Omega \Omega \\ & \text { C.T. } \end{aligned}$ | 100 H MIN | $\begin{aligned} & \text { 22MH } \\ & \text { MAX. } \end{aligned}$ | $\begin{aligned} & \begin{array}{l} \text { 1.7n } \\ \text { (8 sections) } \end{array} \\ & \hline \end{aligned}$ | 5080/23A | Williamson Amplifier |
| P2924 | EL84 | No | 4/5 | $5000 \Omega$ | 8H MIN. SOMADC | $\begin{aligned} & \text { BOMH } \\ & \text { MAX. } \end{aligned}$ | 4/8/16, | 5089:5E | 4/5 Watt Stereo |
| P2925 | $\begin{aligned} & E L 84 \\ & \times 2 \end{aligned}$ | 43\% | 10 | $8000 \Omega 2$ | $\begin{aligned} & 120 \mathrm{H} \\ & \mathrm{MIN} . \end{aligned}$ | $\begin{aligned} & \text { 4OMH } \\ & \text { MAX. } \end{aligned}$ | 4;8/16, | 9000/57 | High Quality 10 Watt Amplifier |
| P2926 | $\begin{aligned} & \mathrm{ELL3}^{24} \\ & \hline 2 \end{aligned}$ | 43\% | 20 | $\begin{aligned} & \begin{array}{l} 6600 \\ \text { C.T. } \end{array} \\ & \hline \end{aligned}$ | $\begin{aligned} & \text { THOH } \\ & \text { MIN } \end{aligned}$ | $\begin{aligned} & 35 \mathrm{MH} \\ & \text { MAX. } \end{aligned}$ | 4/8/168 | 9000/65 | High Quality 20-Wate Amplifier |
| P2927 | $\begin{array}{\|l\|} \hline \mathrm{kr} 88 \\ \times 2 \\ \hline \end{array}$ | 20\% | 50 | $\begin{aligned} & 6000 \Omega 8 \\ & \text { C.T. } \end{aligned}$ | $\begin{aligned} & 150 \mathrm{H} \\ & \text { MIN. } \end{aligned}$ | $\begin{aligned} & 10 \mathrm{MH} \\ & \text { MAX } \end{aligned}$ | 4/8/168 | 9000/73 | High Quality 50 Watt Amplifier $\qquad$ |



## a new peak in waveguide technique premoulded twisted guides

Waveflex Premoulded Twisted Flexible Waveguides are a new advance in waveguide technique. Formed with a predetermined and permanent longitudinal twist, they remain flexible in both E and H planes. The angle of twist can be much greater than with ordinary twistable waveguides, and premoulding relieves the end connections of all twisting stresses. Waveflex Premoulded Twisted guides have a multitude of applications in complex layouts and situations where space is at a premium.

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\end{aligned}
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## "BELLING - LEE" NOTES <br> Parameters of Design

Further notes on Sealing
No. 7 of a series
In the June issue we showed how an apparently solid wire or tube wall could in fact be a bundle of tiny tubes or capillaries and so provide an "open circuit" to an otherwise perfect seal. Now do not let there be any misunderstanding, the extent of such a leak can be very small indeed, and in some cases unmeasurable by ordinary means. To measure the perfection of a seal you must be able to measure the degree of leak. This has become very important with the increased precision of modern science. Theoretically, the perfect seal has never been made, as there could be leakage past the molecules of the material of the container. Many materials thought to be solid are in fact porous; castings in certain metals being notorious in this respect. The unit of leakage is the LUSEC, which is the rate of leak which produces a pressure change of 1 micron of mercury per second in a volume of 1 litre.
This peculiar word LUSEC is a method of writing L (litre) $\mu$ (micron) per sec., $10^{-4}$ Iusec $=$ a leak of 4.17 cc per year.

The most practicable method of measuring leaks of that order is with a mass spectrometer, which is an exceedingly expensive tool. There is an infra-red process which is capable of detecting a leak of $10^{-7}$ which is equal to approximately 1 cc in 250 years.

Perhaps we have started our discussion on sealing at the wrong end. The glass to metal seal is probably the ideal, and the methods of testing are necessarily more scientific as the leaks are so slow and difficult to detect.

We manufacture impedance matching transformers for use in connection with anti-interference aerials. The aerial transformer is always in an exposed position, subjected to sun during the day, and cold at night. There is temperature cycling. As it is an R.F. device, it has to be kept dry and is sealed. Originally, drawn sheet metal cans were used with synthetic rubber glands, and there was no trouble. They were used on ships all over the world. In the interests of economy, we changed to a cast metal container, but it was porous, filled up with water, and apart from impairing the efficiency of the equipment, the water, using the coaxial feeder as a pipe, with a good head of pressure, leaked down into the receiving apparatus. We had to seal the casting with a special varnish. If an electronic equipment
has to be sealed, it means that every connection to it must also be sealed, and you must be able to change fuses, plug-in and withdraw plugs, and carry out numerous adjustments all without breaking the seal.

Bear in mind that a length of feeder, coaxial or otherwise, with a connector at each end, must be truly sealed if so specified. The presence of any moisture would unbalance the feeder. To those without the experience of the problem, it may not be easy to appreciate just what it means to design a miniature connector to seal a length of cable with say twenty-four conductors.

We have had some experience of what happens to coaxial feeder from a television transmitter to the aerial. In the exposed situations generally chosen, it is exceedingly difficult to keep out water, and these feeder's are like big pipes. When monitors showed us a drop in radiated power, we suspected water first, and on more than one occasion, when we went "off the air," the engineers drilled a hole in the feeder at the lowest elbow, and the water gushed out. In many permanent installations such cables are pressurised with nitrogen to prevent the ingress of moisture. Aircraft equipments are also sometimes pressurised, not only to keep moisture out, but to retard voltage breakdown at high altitudeslow pressures. So sealing is used to keep gases or air in as well as moisture out.
The optical industry is also interested in sealing. There must be no moisture between the lenses of binoculars or telescopes as it would condense on the "inside" of the lenses which is not generally accessible. If air or water vapour can get in, so can micro-organisms, and there is at least one that can ruin lenses. Many industries must give careful consideration to sealing for a variety of reasons.
It does not seem so long ago that the standard method of testing for leaks was similar to looking for a tyre puncture, immerse the article in a bucket of water and look for the bubbles. Hot water with a little tepol was best, as the heat expanded the air inside the container and the tepol broke down the surface tension. It was soon appreciated that atmospheric breathing or temperature/pressure cycling was a far more stringent test, and far more realistic. There was a definite sucking action when outside pressure increased or the temperature inside dropped.

A special type of humidity chamber has been designed for these tests, which is often used in conjunction with a pressure chamber, but more about this another time.

Advertisement of
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Great Cambridge Rd., Eufield, Middx. Written 26th March, 1959
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## L. 14i7/FP/Au or Ag. MINIATURE FREE PLUG

## L.1417/FS/Au or Ag. MINIATURE FREE SOCKET

These are miniature versions of the coaxial connectors L.734/P and L. 734/J, for use with cables having an outside diameter of 0.16 in . This connector has a robust cable clamp intended for use in miniaturized equipment where reliability is a prime consideration. Available with contact surfaces either gold-plated (/Au) or silver-plated (/Ag). They can be mated with the coaxial inserts in the miniature "Domino" range L. 1391.

## D.C. breakdown voltage

(at atmospheric pressure):
L. 1417/CS 3000 V - L. 1417/FP/CS 3000V L. $1417 /$ FP/FS 1800 V

Max. working voltage: 400 V d.c.
Voltage proof: 1800 V d.c.
Cable size: Outside dia. 0.16 in. Max. dia. over outer conductor $\frac{1}{8}$ in. Max. dia. over inner conductor 0.03 in.

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Inner conductor, goid-plated brass. Outer conductor, aluminium alloy. Dielectric, P.T.F.E.
Circlip (L.1417/FS), Nylon.
Weight: 1.2 gm . ( 0.05 oz .).

## L.1417/CS.

## MINIATURE CHASSIS SOCKET

This socket accepts the plug L. $1417 / \mathrm{FP}$ described above. It has a nylon circlip, insulated body, and the socket is available gold-plated ( $/ \mathrm{Au}$ ) or silver-plated $(/ \mathrm{Ag})$. Weight 0.7 gm . ( 0.02 oz .).

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# Aspects of design 

This is the Thirteenth of a series of special features dealing with advanced problems in television and radio circuit design to be published by Siemens Edison Swan. The Ediswan Mazda Applications Laboratory will be pleased to deal with any questions arising from this or other articles, the fourteenth of which will appear in the September 1959 issue.

## The Mixer Stage of Television Tuners

The circuits employed in the mixer stage of a television front end tuner are nearly always designed around the triode pentode frequency changer in which, the pentode performs the operation of mixing and the triode acts as the local oscillator.

## Unwanted Features

This type of mixer has two unwanted features which become very evident on Band III namely, a high noise faitor of about 40 and a low input resistance which falls to something between .600 to 700 ohms at $200 \mathrm{Mc} / \mathrm{s}$. Fortunately the high noise contribution of the mixer can be rendered almost negligible by the use of an RF amplifier with high gain such as can be provided by the 30 L 15 . But the low input resistance of the mixer on Band III still remains and means have to be found of reducing the effect of this damping on the preceeding band pass transformer.

## Improving the Mixer Stage

There are four methods by which the effect of the low input resistance of the mixer can be reduced, the first two deal with circuit arrangements, the third with improvements that can be made in the design of the valve and the fourth with the most suitable pin connections.

## 1. Reducing Valve Input Damping

First, the influence of the valve input damping and input capacitance can be reduced by inserting a series trimmer capacitance ( 10 pF min.) in the secondary circuit of the RF transformer. This steps down the valve damping in the ratio of the valve inpuit capacitance to the series trimmer capacitance. On Band III there is a marked reduction in the effective damping. There is a further advantage: as a larger secondary inductance will be required, a better RF transformer can be made for the higher channels on this band.

## 2. Raising Mixer Input Resistance

Secondly, the input resistance of the mixer stage can be raised by designing the circuit to provide a small am:ount of regeneration from $g_{2}$ into $g_{1}$ via the $g_{2} / g_{1}$ inter-electrode capacitance. This can be done by including a small inductance between the $\mathrm{g}_{2}$ pin and its decoupling capacitor. By this means a negative component is ziven to the input resistance which tends to prevent its value from falling as the frequency is progressively raised. A small increase in the input capacitance of the mixer also occurs with $g_{2}$ regeneration but this is not important as it can be accepted when a series tuned circuit is used. The amount of regeneration must be kept within reasonable limits as its effect can vary to some extent with the spread of valve parameters and with wiring changes. Usually an added screen inductance of $0.02 \mu \mathrm{H}$ is suitable with the 30 C 15 .

## 3. Reducing Cathode Lead Inductance

One of the principal causes of low input resistance and one which can be modificd by valve design is that due to the cathode lead inductance, part of which is in the valve and part in the external circuit. Because this inductance carries the whole output current and is, at the same time, common to the input circuit, degeneration occurs, giving a positive component of input resistance which causes damping.

One way of reducing the cathode lead inductance is to bring out the cathode on two pins instcad of one. This can be done on the mixer valve without going to a ten pin valve base by making use of the triode cathode pin. If the pentode cathode is strapped internally to the triode cathode with a low inductance connection it will virtually halve the cathode lead inductance of the pentode in the valve base. By following this construction, the contribution of the cathode lead inductance to the total input resistance can be increased from 950 to 1800 ohms at $200 \mathrm{Mc} / \mathrm{s}$.
This feature of using twin cathode leads for the pentode mixer has been incorporated in the 30 C 15 which is the latest design of frequency changer valve in the Ediswan Mazda
range, In developing this valve, it was necessary to experiment with various alternative methods of strapping the two cathodes - internally to obtain the lowest value of cathode lead inductance.
The internal lead inductance is the sum of the inductances of the lead-in wires and various short straps of irregular shape; it can be determined by measuring the change of cold input capacitance that occurs as the measuring frequency is increased.
The capacitance that is measured is the $g_{1}$ to $k$ capacitance in series with the cathode and grid lead inductances. At frequencies up to about $50 \mathrm{Mc} / \mathrm{s}$ the input capacitance remains practically constant but following the normal characteristics of a series circuit the effective input capacitance starts to increase rapidly as series resonance is approached. The valve with the lowest lead inductance shows the smallest change of input capacitance with increase of measuring, frequency. The lower inductance obtainable with two cathode leads instead of one can be seen in Fig. 1. The same method of measurement enabled a selection to be made of the best arrangement of valve basing, using two cathode leads, which would provide the lowest cathode lead inductance.
Change of effective g , to k capacitance (valve cold)


## 4. Choosing the best pin connections

The disposition of the pins around the B9A base of the mixet must be chosen to bencfit the general design in relation to the external circuit, particularly with pinted sircuits when there is a greater opportunity of making the best use of the low cathode lead inductance within the valve.

For example for use with a printed circuit board it is an advantage to bring out the pentode grid and cathode on adjacent pins. This enables the grid trimmer to be very close both to the g , to k capacitance and the grid coil.

It is also an advantage if the grid and anode of the triode oscillator are located on pins adjoining the pentode grid and cathode in order to provide short connections to the oscillator coil.

The Ediswan Mazda 30 C 15 is designed to meet the requirements of low cathode lead inductance and suitable basing. In addition it will provide a conversion gain approximately 3 dB higher than that of the 30 C 1 .

SIEMENS EDISON SWAN LIMITED An A.E.I. Company Technical Service Department, 155 Charing Cross Rd., London, W.C. 2 .
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## NEW V.H.F. FREQUENCY CHANGER EDISWAN MAZDA 30C15

The 30 C 15 is a triode pentode frequency changer with a conversion conductance of $3.3 \mathrm{~mA} / \mathrm{V}$, for use in television receivers.

In design, the internal layout is arranged to minimise cathode lead inductance and the basing has been selected to make the valve particularly suitable for use in printed circuits, but it can also be used with advantage in wired circuits. The triode is identical to that used in the 30 Cl .

In addition to the advantage of improved basing and layout the 30 C 15 will provide a gain approximately 3 dB higher than the 30 C 1 .
$\begin{array}{lll}\text { Heater Current (amps.) } & I_{h} & 0.3 \\ \text { Heater Voltage (volts) } & V_{h} & 9\end{array}$

## TENTATIVE RATINGS AND CHARACTERISTICS

 Maximum Design Centre Ratings| Maximum Design Centre | Ratigg | Triode | Pentode |
| :---: | :---: | :---: | :---: |
| s) | patmax) | 1.5 | 1.7 |
| Screen Dissipation (watts) | pg. max $^{\text {s }}$ |  | 0.5 |
| Anode Voltage (volts) | Vamaw | 250 | 250 |
| Screen Voltage (volts) | $\mathrm{V}_{\mathrm{ge} \text { etmas }}$ |  | 175 |
| Heater to Cathode Voltage (volts r.m.s.) | $\mathrm{V}_{1-\mathrm{k}}^{\text {(r.m.s.s.mas }}$ |  |  |
| Cathode Current (mA) | $I_{\text {(mals) }}$ | 14 | 14 |

## Inter-electrode Capacitances ( $\mathbf{P F}$ ) $\dagger$

Pentode

| Anode to all | $\mathrm{Ca}_{\mathrm{a}}$-all |
| :---: | :---: |
| Grid 1 to all | $\mathrm{CgI}_{1}$-all |
| Grid 1 to Anode | $\mathrm{Cg} 1-1^{\text {- }}$ |
| Anode to Earth | $\mathrm{C}_{5}$ - F |
| Grid to Earth | C5-E |
| Grid to Anode | $\mathrm{C}_{2}$ | 5


|  | Grid 1 to all | $\mathrm{C}_{\mathrm{g} 1}$-al | 6.7 |
| :---: | :---: | :---: | :---: |
| Triode | Grid 1 to Anode | Cg 1 | . 01 |
|  | Anode to Earth | $\mathrm{C}_{5}-\mathrm{F}$ | 3.2 |
|  | Grid to Earth | C5-E | 3.2 |
|  | Grid to Anode | $\mathrm{Cg}_{5}$ | 1.6 |

$\dagger$ Inter-electrode capacity with holder capacity balanced out but with cylindrical screen can.
Maximum Dimensions
Overall Length (mm) ..... 56
Diameter (mm) ..... 22.2

## TYPICAL OPERATION

As frequency changer with oscillator voltage applied to pentode grid 1.

## Pentode

| Pentode |  |  |
| :---: | :---: | :---: |
| Supply Voltage (volts) | Va (in) | 200 |
| Anode Voltage (Decoupling Resistance $4.7 \mathrm{k} \Omega$ ) (volts) | V* | 164. |
| Screen Voltage (Dropping Resistance $27 \mathrm{k} \Omega$ ) (volts) | $\mathrm{V}^{\text {a }}$ | 138 |
| Resistance for Grid 1 Current Bias ( $\mathrm{k} \Omega$ ) | $\mathrm{R}_{ \pm 1}$ | 100 |
| Anode Current (approximate) (mA) | $\mathrm{I}_{1}$ | 7.6 |
| Screen Current (approximate) (mA) | $\mathrm{I}_{\text {g }}$ | 2.3 |
| Grid I Current ( $\mu \mathrm{A}$ ) | Ig | 33 |
| Conversion Conductance (mA/V) | $\mathrm{g}_{\mathrm{c}}$ | 3.3 |
| Heterodyne Peak Voltage (volts) | Vhel(phi) | 3.7 |
| Triode |  |  |
| Anode Voltage (volts) | $\mathrm{V}_{\text {i }}$ | 120 |
| Anode Current (Average) (mA) | $\mathrm{I}_{3}(\mathrm{aN})$ | 6 |

## APPLICATIONS NOTES

The base connections of the 30 C 15 provide the following advantages for printed circuit use:
(a) The pentode $g_{1}$ and cathode are brought out on adjacent pins. This enables the grid trimmer to be placed very close to the $\mathrm{g}_{1}$ to k capacitance thus minimising errors in alignment that can occur at differing frequencies if the trimmer has series inductance.
(b) The $g_{2}$ connection is conveniently placed close to the cathode.
(c) The heater pins are easily accessible for series connection in a printed circuit board while still allowing easy decoupling to the strapped cathodes.
(d) The position of the grid and anode pins of the triode oscillator makes it possible to use short connections to the oscillator coil.
(e) The reduction in cathode lead inductance increases the gain on Band III.

These points are illustrated in the following figure which shows part of a printed circuit layout using the 30 C 15 where the RF stage is assumed to be a cascode amplifier using the 30 L 15.

Although the triode sections of the 30 C 15 and 30 Cl are identical the internal coupling between triode and pentode in the 30 C 15 has been reduced. To obtain satisfactory injection of oscillator voltage into the pentode section the 30 C 15 requires additional external coupling.
SIEMENS EDISON SWAN LIMITED AnA.E.I. Company Technical Service Department, 155 Charing Cross Rd., London, W.C.2. Telephone: GERrard 8660 . Telegrams: Sieswan, Westeent, London.

Grid coil Osc.coil
TEST CIRCUIT AND CONDITIONS


| $V_{b}$ | $R_{a}$ | $R_{g_{2}}$ | $R_{g_{1}}$ |
| :---: | :---: | :---: | :---: |
| 200 | 4.7 k | 27 k | 100 k |
| $R_{\mathrm{D}}$ | $\mathrm{I}_{\mathrm{h}}$ | f | $\mathrm{C}_{g_{1}}$ |
| 10.5 k | 0.3 A | $1 \mathrm{Mc} / \mathrm{s}$ | 0.02 F |

HETERODYNE INJECTED IN $_{g_{1}}$

h h
Base B9A (Noval)


VIEW OF FREE END.

Tentative characteristic curves of Ediswan Mazda Valve Type 30 C 15.


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[^16]ADDRESS


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The Mk. 5 deck is the outcome of almost 10 years' exhaustive research and manufacturing experience. Its remarkable features include four operating speeds, four heads can be fitted and 81 in. professional spools accommodated. For ease of operation only two switches (interlocked for safety) are employed. These control record, playback, wind and rewind and have extended shafts for fitting extra wafers if necessary. This feature makes the deck quickly adaptable for use with a variety of Hi-Fii equipment. Speed stability is ensured by a large statically and dynamically balanced flywheel. Brakes are mechanically operated. Safety device to prevent accidental erasure is incorporated. Instant stop without spillage, fast rewind in either direction ( 45 sec . for $1,200 \mathrm{ft}$.) and azimuth adjustment are among its well-proved features. FOR STEREO conversion can be carried out at little extra cost.
Tape Deck, with provision for extra heads
28 gns . Complete record/playback amplifier with power unit $£ 24$ Stereo/rec. playback (including mounting rack).... £93 $16 \quad 0$ SEE THESE MODELS AT THE RADIO SHOW—STAND 333

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## COLSTON HALL BRISTOL <br> FRIDAY; 9th OCTOBER, 1959 at $7-30 \mathrm{p} . \mathrm{m}$. <br> We have pleasure in announcing a <br> CONCERT

## OF LIVE AND RECORDED

MUSIC
Introduced by G. A. Briggs with the collaboration of R. E. Cooke and R. L. West

## Artists taking part <br> LEON GOOSSENS <br> Oboe

HAROLD BLACKBURN
Bass
EDWARD FRY
Organ
PIANO TRIO:-
GERALD GOVER - piano
KENNETH: POPPLEWELL - violin
TERENCE WEIL - cello
Harold Blackburn appears by kind permission of Sodiers Wells Trust Ltd., and Kenneth Popplewell by kind permission of the B.B.C.
The demonstration will include comparisons of mono and stereo reproduction with live performances.
Special recordings have been undertaken for this purpose by E.M.I. A number of commercially available records will also be played.

## ADMISSION 3/6

All seats numbered and reserved Book early for best seats
Tickets will-be available on and after Monday, 10th August, direct from Wharfedale Wireless Works Ltd., Idle, Bradford, Yorkshire. Tel. Idee 1235/6. (Cash and stamped, addressed envelope with each order.) And also at the COLSTON HALL Box Office.
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TRANSISTORS: A.F. $7 / 6$ each. R.F. 15/- each
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All brand new in famous maker's cartons
(1) 17 in . rectangular aluminised 6.3 HTRS. 3 A current; max. anode voltage (2) F. Usual price E17.5.0. OUR PRICE E9.19.6. Crating and earr. 15/(2) Ferranti T12/44 and T12/54G 12 in . magnetic white fluorescence; 4 v . heater: max. anode 10 kV . As used in many TV receivers. Original price E17.5.0. Our price £4.19.6. Crating and carr. 12/6.
(3) Ferranti 9 in. Tube round white fluorescence, 5 v . heater, max. anode voltage 7 kV . Our price E2.19.6. Crating and carr. $11 / 6$.
JONES PLUGS AND SOCKETS. 4 pin $2 / 6$ pair; 6 pin $3 / 6$ pair; 8 pin $4 / 6$ per pair; 12 pin $6 / 6$ per pair. If cover required send $1 / 6$ extra per

WANDER PLUGS. Red and black
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PHILIPS TRIMMER TOOLS $1 /$ each
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POINTER KNOBS. Small black with white line, $7 / 6$ per doz. 5 mall white with black line $8 /$ - per doz. Both types $\frac{1}{4}$ in. spindle. Large price reductions for 1,000 lots and over.
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Large stocks of all types of resistors, condensers, valveholders always available ex stock Manufacturers' enquirics welcome.

# OUTSTANDING at the RADIO SHOW The "STUDIO" <br> STAND No. 49 <br> DEMONSTRATION ROOM 330 

## TAPE TRANSCRIPTOR

## WHICH WILL BE INCORPORATED IN MANY NEW TAPE RECORDERS BY LEADING MANUFACTURERS

- Fast rewind, 1,200 ft. in 65 seconds - Space for third head - Light piano-type keys - Three speeds $1 \frac{1}{8}, 3 \frac{3}{4}$ and 7솔 I.P.S. - Twin track single direction "Three digit counter ". Three motors - Very low "wow" and "flutter" - Pause control


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Developed through the years to its present high standard of perfection, this transcriptor is used by more tape recorder manufacturers than any other.

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Automatic Record Changer
FOR STEREOPHONIC AND MONOPHONIC PLAY

- Pick-up pivot bearing provides almost frictionless action.
- Complete automatic playing of any size of record from 7 in . to 12 in .
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## AND A NEW UNIT OF SUPERB QUALITY-THE RP 594

## GILIARO <br> LTD.

Specially made to meet a need for a simple, cheap unit mounted on a large unit plate. This four-speed unit is mounted on a beaded edge steel plate $12 \frac{1}{2} \mathrm{in} . \times 13 \frac{1}{2} \mathrm{in}$, with the turntable running in a well.

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## FIST MICROPHONE

Moulded in Nylon, this attragtively designed unit is weatherproof and almost indestructible under the most adverse conditions. It has a positive action Double Pole Changeover Switch, and is available with either Carbon or Electromagnetic Transmitter. When fitted with the $\mathrm{E} / \mathrm{M}$ Inset it also operates as a Receiver. For use on Mobile Radio, Walkie-Talkie, Police Motor-Cycle Wireless, etc.


We proudly draw attention to our newly designed FIST MICROPHONE and UNIVERSAL HANDSET, which find applications everywhere where quality, toughness and serviceability are major factors.

## UNIVERSAL HANDSET

Moulded in Propionate-one of the toughest plastic materials ever produced this beautifully styled, robust and lightweight instrument is designed to accommodate any known Transmitter or Receiver Inset. Built-in Double Pole Changeover Switch Double Pole is available. Stondard Insets: Moving Coil, Electro-magnetic, Single Moving Coil, Electro-magnetic Carbon. Carbon and Double Button Carbon. For use on Radio Stations, Mobile Radio, etc.


Handsets; Microphones; Headsets; Headsets with Boom Microphone; Headsets with Throat Microphone; Transmitter Insets; Receiver Insets;

Details of all S. G. Brown products sent on request. Hospital Headphones and Pillowphones; High Fidelity Headphones.

## STEREO $£ 7.7 .0$ <br> Independent twin channel amplifier with excess of 3 watts per

 channel.Concentric volume control (optimum balance arranged imme diately without additional knobs).
Choice of volume and tone controls separately fixed or integral with chassis and having continental styled knobs (brown and gold).
Stoved grey or blue hammer chassis $9 \frac{1}{2} \mathrm{in} . \times 5 \frac{1}{2} \mathrm{in} . \times 6 \mathrm{in}$.
input suiting most modern crystals; output matching 3 ohm speaker each channel.
for operation on AC mains $200 / 250 \mathrm{v}$.


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If your local dealer has not one in stock we will gladly loan him one for you to hear.


ELECTROVAC MANUFACTURING CO. (Dept. W.IO), Chapel Works, Sunnyside Road, Chesham, Bucks.

With the general introduction of $110^{\circ}$ television tubes, increased scanning power is required for both line and frame. This can be obtained either by more power from larger valves or by improving the efficiency of the circuit and reducing losses. For obvious reasons, the latter method is preferable, since it prevents a rise in power consumption and a consequent increase in heat dissipated by the components.

One of the most obvious reasons for losses, is the presence of metallic picture centring magnets on the tube neck behind the deflection coils. These magnets, due to their electrical conductivity, absorb about $10 \%$ of the scanning power, and convert it into heat.

Due to mechanical considerations, picture shift magnets are required to be made from a comparatively thin and tough material which can be accurately and inexpensively fabricated. Consequently, it is usual to employ one of the ductile sheet magnet materials such as the low percentage cobalt, chrome or tungsten steels. These, however, have a low electrical resistance and a low coercive force, which give rise to shunting of the magnetic field and demagnetisation of the magnet due to the leakage field.

The Mullard Laboratories have given this problem some consideration, and have produced a new type of magnet material specially for this application. This gives an improvement in scanning power of approxinately $10 \%$ for frame and $5 \%$ for line width compared with the usual metallic magnets.

The photograph illustrates the position of the shift magnets on a set of $100^{\circ}$ deflection coils. Two

"Magnadur" rod magnets for pin cushion piçture correction are also shown.

Some of the outstanding characteristics of this new material are:-
1 High electrical resistivity of approximately $10^{6}$ ohm. cm.
2 High coercive force of approximately 1,500 oersteds giving a high resistance to demagnetisation.
3 Can be formed to required shape within small limits by normal and inexpensive methods.
4 Requires no subsequent heat treatment.
5 Tough, flexible and resiliant.
For further details of these magnets and other Mullard magnetic components, write to the address below.

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'TICONAL' PERMANENT MAGNETS 'MAGNADUR' CERAMIC MAGNETS FERROXCUBE MAGNETIC CORES

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 heats up from cold in 6 secondsDesigned on an entirely new principle, this lightweight, versatile iron is eminently suitable for soldering operations in the radio, television, electronic and telecommunication industries. For test bench and maintenance work it is by far the most efficient and economical soldering iron ever designed.

Length, $10^{\prime \prime}$ : weight; 3it ozs.

For best results with this iron use ENTHOVEN SUPERSPEED CORED SOLDER and ALUMINIUM CORED SOLDER

Activated by light thumb pressure on the switch ring. When pressure is released, current is automatically switched off-thus greatly reducing electricity consumption, wear on copper bit and carhon element.

Can be used on 2.5 to 6.3 volt supply ( 4 volt transformer normally supplied) or from a car battery.

More powerful than conventional 150-watt irons; equally suitable for light wiring work or heavy soldering on chassis.

- Simple to operate; ideal for precision work.
Requires minimum main-tenance-at negligible cost: shows lowest operating costs over a period.

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We offer excellent remuneration, profitsharing retirement plan, hospital and medical insurance, and opportunities for advancement. We are located in Kitchener, Ontario, with a population of 70,000 .
Please reply in detail giving age, education, résumé of previous experience, marital status, etc., and enclose a recent photograph to:

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All applications will be answered and qualified candidates will be interviewed in the United Kingdom.

## MAKE THE MOST OF YOUR

 RECORDERThe Grampian DP4 Microphone is ideally suited to the recordist requiring a high quality instrument for use with a tape recorder. Designed with a uniform wide frequency response from $50 \mathrm{c} / \mathrm{s}$ to $15,000 \mathrm{c} / \mathrm{s}$, it fulfils the needs of Wire, Tape and Disc Recording, Public Address, Call Systems, etc.
Low, Medium or high impedance models are avaiable together with a complete range of stand adaptors, stands, swivel holders, and switch assemblies.

## OUTPUT LEVELS:-

## 25 ohms-

86 db below 1 volt/dyne/cm.
600 ohms
70 db below 1 volt/dyne/cm. ${ }^{2}$
50,000 ohms-


## 52 db below 1 volt/dyne/cm. ${ }^{\text {. }}$

Retail priç DP4/L/pack 1:-low impedance Microphone, complete with connecter, 18 ft screened lead, swivel holder and circular base. $£ 8 / 19 /-$ (exira for H 2 or M impedance models- $£ 1$ ).

## MATCHING UNIT G. 7

For use in cases where it is desired to use ow impedance microphone with a recorder or amplifier having a high impedance input. It can also be used in cases where very long microphone leads are necessary. Retail price $£ 3 / 5 /$ -

Literature on this and other equipment readily. available.


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Top Plates, 3d. each
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each.
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SIEMENS HIGH SPEED C/O RELAYS
$250+250$ Ohm Twin Coils $6 / 6$ 1,000 $+1,000$ Ohm Twin Coils $10 / 6$ $850+850 \mathrm{Ohm}$ Twin Coils $8 / 6 \quad 1,700+1,700 \mathrm{Ohm}$ Twin Coils $17 / 6$ postage and packing on all extra.


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Delivery ex stock. Quotations on application.

> H.T. 31 Input 11.5 v . Output 250 v. at 125 mA .
H.T. 32

Input, 1.58
v . at 65 mA .

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BATTERY TRANSISTOR AMPLIFIERS, output 4 to 5 watts. 12 v . or 6 v. in. Complete with Mike, Speaker, Mike and Gram sockets etc ideal for Car and Public Address, all functions including Race Meetings, Election Campaigns etc. Write for leaflet and particulars of this won derful buy.
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INDUCTION MOTORS suitable for Tape Recorders, Sewing Machines etc., etc.

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to put in hand any overhaul, alteration or modernisation of your sound-reproducing equipment-to stereo-twin-speaker presentationVHF/FM radio-or just some overdue replacement of the weakest link in the chain-a better motor, pick-up or speaker system.
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FULLY R.C.S.C. TYPE APPROVED, $10 \Omega$ to $22 \mathrm{~K} \Omega$, our RWV4-L style resistors conform to Inter-Services Spec. RCS II.
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| RWV4-J | VPF4 | 3 | 4 | $5 \Omega$ to $8 \mathrm{~K} \Omega$ |
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Pot Meters, carbon $5 \mathbf{K}$., $10 \mathrm{~K}_{\text {, }}, 23 \mathrm{~K} ., 50 \mathrm{~K}$.,
 initeh 4/-.
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Clock Movement, 7 -day mechanism, beautifully made and fully jewelled, iew only. Medreseo Hearing Aid, as supplied by National Health, completely orerhauled in phones anding owder. complete with earnormal price 23/15/-. 8ale price $22 / 18 / 6$. Somweave, loudspeaker fabric also snitable Vormally offered at bargaio price of 12,6 per yarl, 48 in . wide. sale price $10 / 6$ per vard. L2V 4 amp. Car Battery Charger, variable aharge rate, in whove enamelled case, with
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Ditto, hut with additiomal a v. rinding ior soparate rectiflers, made to sell at $21 /$ Sule price $13 / 6$, pluts $2 / 6$.
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Later Model with Noise Suppressor $£ 25$ Carriage England and Wales $30 /$-. . Send S.A.E. for furcher details.

## CR100 SPARES KITS

Contents: 15 valves, 2 or U50, DH63, KT63, X66, and seven KTW61. Output transformer, Resistors, Condensers; Potentiometers, PK screws, pilot lamps, drive cord, etc., etc. ALL BRAND NEW. $59 / 6$. screws,
Post $4 / 6$.
COMMUNICATIONS RECEIVERS R-1155B
A first class 10 valve Communication and D/F receiver, covering $75 \mathrm{Kc} / \mathrm{s}$. to $18 \mathrm{Mc} / \mathrm{s}$. ( $16.2-4,000 \mathrm{~m}$.) in 5 bands. The large scale and superior dual 'atio slow-motion drive make tuning easy, and che R.F. stage and 2 I.F. scages ensure world-wide reception. ALL the receivers we sell have been thoroughly overhauled and completely re-aligned, and are in first class order. ONLY £7/19/6.
ALSO available, R-1155-N as above, but has 1.5 to $3 \mathrm{Mc} / \mathrm{s}$. ( $10 \mathrm{~J}-20 \mathrm{Jm}$.) in place of the $75-200 \mathrm{Kc} / \mathrm{s}$. band. ONLY $\mathrm{E} 12 / 19 / 6$.

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 In handsome black-crackled steel cabinec to match the R-II55. Fitted with 8in. speaker. Just PLUG IN and switch on! Only the finest quality components are used, and we guarantee OUR power packs for 6 months. ONLY E6/lo/-. Deduct 10/- when purchasing receiver and power unit together. Send S.A.E. for further detals, or (FREE 14 page illustrated booklet giving technical data and circuits etc. (FREE with each receiver) Add $10 / 6$ carriage tor receiver, 5 - for power unit.
## HALLICRAFTER SX-24 RECEIVERS

Covers from $540 \mathrm{Ke} / \mathrm{s}$. to $44 \mathrm{Mc} / \mathrm{s}$. in 5 bands. With separate bandspread tuning. variable selectivity crystal filter, B.F.O., S meter, noise limiter etc. For $117-230$. A.C. mains ${ }_{3}$ in perfect working order and firse clas condition. 225. Carr. 10/.

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This Command Receiver covers 190-550 Ke/s. - (I.F. $85 \mathrm{Kc} / \mathrm{s}$.) and is ideal for double superhet conversion etc. Supplied BRAND NEW in original cartons, with all 6 valves and CIRCUIT. 89/6. Post $3 / 6$.


## MARCONI VaLVE VOLTMETERS

Ranges: 0 to $1.5,5,15$, 50 , and 150 volts. Fitted with probe unit for RF measurements. A.C. mains operation. In good condition and working order. A laboratory instrument for ONLY E8/19/6. Carr. 7/6.

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## CRYSTAL CALIBRATOR

No. 10. Consists of $500 \mathrm{Kc} / \mathrm{s}$. crystal oscillator and a variable 250-500 Kc/s heterodyne oscitlator. This enables all intermediate frequencies between $500 \mathrm{Kc} / \mathrm{s}$. and $10 \mathrm{Mc} / \mathrm{s}$. to be produced. These frequencies are indicated on the calibrated scale. The calibrator may actually be used up to $30 \mathrm{Mc} / \mathrm{s}$. The unit uses a CV-286 neon modulacor. IT4 crystal osc., 1T4 het. osc. and IR5 mixer. Operates from 300 v. $15 \mathrm{~m} / \mathrm{a}$., and 12 v. 0.3 A . but can be easily modified for 120 ban be easily modified Size $7 \times 7 \frac{1}{2} \times 4$ in. In first class condition, complete with valves, condition, complete with valves, circuit. One of our "best
 buys" at "ONLY 59/6. Post $3 / 6$.
FERRANTI TESTMETER TYPE $Q$. An exiremely compact self-contained multimeter. Volts 0 to $30,150,600$ A.C./D.C., with additional $0-3$ v D.C. and $0-15 \mathrm{v}$. A.C. ranges: Milliamps 0 to $7.5,30,150$ and 750 D.C. ohms $0-25$.K. Accuracy BSS first grade. 500 ohms per volt. Knife-edge pointer and clearly calibrated 2 tin. scale. Complete with leads, prods pointer and clearly calions in fitted velvet-lined $4 \times 7 \times 3$ in. case. Brand new condition, perfect working order. Bargain price. ONLY 59/6. Post 2/6.
 ADMIRALTY G-73 SIGNAL GENERATOR/WAVEMETERS

Combines the facilities of a well made signal generator with those of 2 erystal checked heterodyne wave meter. Generates $100 \mathrm{Kc} / \mathrm{s}$. to $25 \mathrm{Mc} / \mathrm{s}$. in 6 ranges ( CW or $400 \mathrm{c} / \mathrm{s} . \mathrm{mod}$.), or operates as wavemeter over same ranges. Carrier or modula tion level may be monitored on 500 microamp plug-in meter (not supplied). Has built-in $\mid \mathrm{Mc} / \mathrm{s}$, crystal oscillator for self checking calibration, coarse and fine atcenuators. $400 \mathrm{c} / \mathrm{s}$. output available separately Operates from $100-230 \mathrm{v}$. A.C. mains. Size $15 \times 10 \times 8 \mathrm{in}$. Supplied complete with valves, crystal, and list of crystal check points and instructions for drawing of individual graphs. Condition used bur O.K. 79/6. Carr. 10/6

RCP 20 RANGE TESTMETERS
1,000 ohms per volt, 400 microamp basic movemen D.C. VOLTS
2.5 v.
10 v.

10 v.
50 v .
50 v .
250 v .
$1,000 \mathrm{v}$
D.C. CURRENT
D.C.
1 ma .

1 ma .
10 ma .
100 ma .
100k. ohms

- -10 上 +69

In light oak case $6 \frac{1}{2} \times 6 \times 4 \frac{1}{2}$ in. including lid. Complete with test leads and prods, internal battery, and instructions manual. ALL BRAND NEW and tested.
Post 3/-
LIMITED NUMBER 7916.
VOLTAGE REGULATOR TRANSFORMERS. Input 230 v. A.C.. output variable from $187-250 \mathrm{v}$., OR input $187-250 \mathrm{v}$., output 230 v . at 24 amps. Rating 5.5 KVA . Wt. 42 Ib . Brand new condition. E9/19/6. Carr. 10/6.

MINIATURE RELAYS (ALL BRAND NEW AND BOXED).
G.E.C. sealed, wire ends, 670 ohms. 2 H/D makes, M1099 $10 . . .$. G.E.C. sealed, wire ends. 670 ohms. . 4 Clovers, platinum, M1092 $19 / 6$ G.E.C. sealed, wire ends. 5000 ohms 2 Clovers, platinum, M1052... $17 / 6$ S.T.C. size $1 \frac{1}{4} \times \frac{5}{4} \times \frac{1}{4}$ in. 250 ohms. 2 Clovers, double contacts Siemens High Speed, $1 \mathrm{~K}+1 \mathrm{~K}$ ohms. I C/over.

FURZEHILL BEAT FREQUENCY OSCILLATOR No. 5. Push-pull output $0-10,000 \mathrm{c} / \mathrm{s}$. of $0-5 \mathrm{v}$. at 10 ohms, or 0.50 v . at 600 ohms, monitored by $2 \frac{1}{2} \mathrm{in}$. M/C meter. Incorporates check. Operates from 100 250 y $50 \mathrm{c} / \mathrm{s}$ mains. In handome instrument case, $17 t x$ $9 \times 1$ in Despatched in $\frac{1}{2} x$ xase in perfect condition cast, complete with 7 valves, tested. complete with valves, laboratory instrument. for OIJLY E12/10/- Carr. 10/-
SEE ADVERTISEMENT OPPOSITE $\Rightarrow$


 | Funnel cooled. A.C. input 45 V. RMS. |
| :--- |
| D.C. output $30 \mathrm{v} . ~$ | $0_{\text {amps. BRAND }}$ NEW. Boxed. $45 /$ /- Post $3 / 6$. HEAVY DUTY L.T. TRANSFOR-

MERS. (Gresham.) Latest type potted, MERS. (Gresham.) Latest type potted,
oil filled, Pri. $230 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$. Sec. $0-70-75-$ $80 \mathrm{v}, 4 \mathrm{amps}$. Size $54 \times 4 \frac{1}{2} \times 6 \frac{1}{2} \mathrm{in}$, high.
Wt. 19 lb . BRAND NEW. $42 / 6$, carr, $5 /-$ Wt. 19 lb . BRAND NEW. 42/6, carr. S/-, DUAL PURPOSE TRANSFORMERS (Gresham). Pri, $230 / 250$ v. Secs. $240-$ $0-240$ v. 1.5 amps., 5 v .12 .5 amps. 5 v . 1.75 amps . Ideal for ISOLATING TRANSFORMER, to obrain T'WO 240 v. 360
wart lines. Potted, oil-filled, $7 \times 7 \frac{1}{3} \times 8$ wart lines. Potted, oil-filled, $7 \times 7 \frac{1}{2} \times$
$10 \frac{1}{2}$ in. high. Wt. SO Ib. BRAND NEW. 10 tin. high. Wt.
E3/10/. Carr. $10 /-$
MAINS ISOLATING TRANSFORMERS (Vortexion). Fully-shrouded. For testing A.C./D.C. sets in safety. 230 v . input. Output 230 v . 100 watts, $22 / 6$. Post $2 / 6$.
ADMIRALTY HT TRANSFORMERS Pri. $230 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$. Secs. $620: 550-375-0-$
 m/amps., 375 v. $250 \mathrm{~m} / \mathrm{amps}$.), plus
two 5 v.
3 two ${ }^{5}$ v. ${ }^{3}$ Amp. rectifier windings.
Total rating 278 VA. Upright mtg. Tota rating 278 VA. Mpright mig
Wt. 25 Ib . Made 1953. BRAND NEW Original boxes. 45/-. Carr. 5/-
INSTRUMENT TRANSFORMERS. 230 v. A.C. input. Outputs 0-65-130-195 v. $85 \mathrm{~m} / \mathrm{amps}$., $6.3 \mathrm{v} .5 \mathrm{amps} ., 6.3 \mathrm{v} .0 .3 \mathrm{amps}$. Shrouded. Size $3 \frac{1}{2} \times 3 \frac{3}{4} \times 3 \frac{3}{4} \mathrm{in}$. high. $\quad 15 /=$ post FREE.
AREBD MAINS TRANSFORMERS. Input $110-240 \mathrm{v}$. Output $345-0-345 \mathrm{v}$. $125 \mathrm{~m} / \mathrm{amps}$., $6.4 \mathrm{v} ., 4.5 \mathrm{amps} ., 5 \mathrm{v} .2 \mathrm{amps}$. $4 \frac{3}{3} \times 4 \frac{1}{4} \times 5 \frac{1}{3} \mathrm{in}$. high. We. 12 lb . Potted. Tag ends. RCA BRAND NEW. Boxed. 29/6, post $3 / 6$.
TRANSFORMER BARGAIN. InPUE $0-200 / 250$ tapped. Outputs $250-0-250 \quad \mathrm{v}$ $80 \mathrm{~m} / \mathrm{amps}$., 5 v. 2 amps; ; 6.3 v. 4.5 amps. Ex-Admiralty made 1952 . A fine $50 \mathrm{c} / \mathrm{s}$. mains tranny for ONLY 16/6, post FREE. MODULATION TRANSFORMERS. Collins type 20 watts 807 to $807,8 / 6$ each Post 1/6
FERRANTITYPE, for T $\times 36$ etc., pushpull 807's to plate and screen modulate push-pull 807 's, ratio $2: 1$. Fully shrouded. We. $6 \frac{1}{2} \mathrm{lb} 17 / 6$. Post $2 / 6$.
ADVANCE CONSTANT VOLTAGE TRANSFORMERS. Input 190-260 $50 \mathrm{c} / \mathrm{s}$. A.C. mains. Output 230 250 warts. 10 Gins. Carr. $7 / 6$.

## STANDARD TRANSFORMERS. Vacuum impregnared, interleaved, E.S

 screen, universal mounting. Size $4 \times 3 \frac{1}{2} \times$2 i in. ALL BRAND NEW. $18 / 6$ each $2 \frac{1}{2}$ in. A
Post $1 / 6$.
Type 1. $250-0-250$ v. $80 \mathrm{~m} / \mathrm{a}, .6 .3$ v. 3 A tapped at $4 \mathrm{v} .4 \mathrm{~A} ., 6.3 \mathrm{v} 1 \mathrm{~A}$ tapped at 4 v . and 5 v .2 A .
Type 2. As above, but 350-0-350 $80 \mathrm{~m} / \mathrm{a}$.
Type 3. 30 v. 2 A., tapped at 12,15 , 20 and $24 \quad v$., to give 3-4-5-6-8-9-10 $v$., etc. Type 5. $0-5-1 \mid-17$ v. 4 A Ideal for chargers.

## MORE METER BARGAINS

 METAL RECTLFIERS. Full wave brifge. BRAND NEW. Salforl
$1 \mathrm{~mA} .8 / 6,5 \mathrm{~mA} .8^{\prime} 6$. STC $2 \mathrm{~mA} .5 / \mathrm{s}$. MINIATURE 373 IF STRIPS. For FM tuner described iu "Prartical vireless. Complete with 3 of EF91, 2 of EF92; and 1 oi EBS1. A resul eurint of conversion Instructions and circait supplled iree. Complete ss rulves, 12/6. Post. either $2 / 6$.
RCA HF SWEEP GENERATORS


Laboratory type equipment desigued for alignment of wide band RFi and IF amplifiers. Coraprises generator and regulated power supply unit. each housed in grey crackled steel case $17 \times 10 \times 12 \mathrm{in}$.
Centre Frequency 0 of- $65 \mathrm{Mc} / \mathrm{s}$. Sweep width $0.2-20 \mathrm{Mc} / \mathrm{s}$.
Centre Frequency $5-65 \mathrm{Mc} / \mathrm{s}$. Sweep width $0.2-20 \mathrm{Mc} / \mathrm{s}$.
Marler oscllator irequency $5-70 \mathrm{Mc} / \mathrm{s}$. Operates from $105-125 / 210-230 \mathrm{v}$. Marker osclilator irequency $5-70 \mathrm{Mc} / \mathrm{s}$. Operates from $105-125 / 210-230$ r.
A.C. Mains. Complete with 13 valves and Technical handbook. BRAND A.C. Mains. Complete with 13 valves and
NEW condition, $\$ 39 / 10:-$. Carr. $10 /-$

## MEGGERS

E. \& V. Series 2 Megzers. 500 volts, $0-100$ Negohms. In leather case Pirgs-elass condition. ONLY £12/10/-
E. \& V. BONDING TESTERS, $0-5$ ohms at $12 \mathrm{~m} / a m \sin$ max. Hund generator type. In leather case. 79/6.
INSULATION TESTERS.
INSULATION TESTERS. "Record " hand generator type. 0 - 50 Meq-


HRO SENIOR RECEIVERS


Complete with ALL NINE general coverage plug-in coitecte for 30 Hets to $30 \mathrm{Mc} / \mathrm{s}$. Instruction booklet, and circult, but less exter.ual power supply unit. Table inodels, as new coudition. 21 GNS. Rack toonatiog, 18 GNS. Packing and carriage $22 /-$ extra. Acnd g.A.E. for furthr $r$ details.
HRO POWER PACKS. $11 / 230$. A.C. mains laput. Teqted, and in gond AR-88. D AND LF. SUPERB CONDITION, NOW IN STOCK.

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RF2t, $20-30 \mathrm{Me} / \mathrm{s}$. 5 sultched masitions
RF2h- 50 -65 Mc/s Super slow -motion drive
RFF27. $65-80 \mathrm{Mc}$ 's. Super slow-motinn divive.....
Unbored. but aw new contition. Pootage $3 / 6$ each.
CHARLES BRITTAN (Radio) LTD. 1i UPPER SAINT MARTIN'S LANE LONDON, W.C. 2

TEMple Bar 0545
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## SANGAMO

 3in. scale. Recent manufacture. Ideal for schools. Com plete in super qual ty canvas earryin case, with test prods and leads. BRAND NEW. Boxed $27 / 6$. Post $2 / 6$.SANGAMO-WESTON ANALYSER E772. A useful multi-range meter in rexine covered carrying case. Thoroughly overhauled and in perfect working order. $£ 7 / 19 / 6$. Carr $4 / 6$ see previous adverts.

AVO LC \& R BRIDES 5 pFd to 50 mFd . Resistance 5 ohms to 50 megohms. Inductance can be measured gainst external standard. Balance is indicated on a meter, which can be used as valve voltmeter from 0.1 to 15 v . Leakage test and Power Factor scale. For use on A.C. mains. Tested and guaranteed. 88/10/=. Posi $3 / 6$
HICKOCK I-I77 VALVE TESTERS. Checks dynamic murual conductance shorts, emission, gas, and noise. For UX4 UX5, UX6, UX7, Octal, Loctal, B7G and Acorn types. Portable, in wooden carrying case $15 \frac{1}{2} \times 8 \times 5 \frac{1}{2}$ in. We. $13 \frac{1}{2} \mathrm{lb}$.
BRAND NEW. BRAND NEW. Complete with instruc tion book and valve resting charts. For auto. transformer for 230 v. A.C. I2/6.

MARCONI TF987/I NOISE GENERATORS. Range $100 \mathrm{Kc} / \mathrm{s}$ to $200 \mathrm{Mc} / \mathrm{s}$. Determines noise factor of AM and FM receivers. Fully stabilised H.T. supply A.C. mains operation. Brand new and in original boxes. $£ 25$.

MARCONI SIGNAL GENERATORS $85 \mathrm{Kc} / \mathrm{s}$. to $25 \mathrm{Mc} / \mathrm{s}$. A.C. mains operation In fair condition and working order TFI44F. $£ 40$. TFI44G. $£ 50$.

MARCONITF. 340 OUTPUT METERS Perfect working order. $£ 19 / 10 /$ -
SCR522 TRANSMITTER/RECEIVERS $100-150 \mathrm{Mc} / \mathrm{s}$. Comprises BC624A rec. and 8 C 625 trans. All complete with valves and in first-class condition. BC624A less relay 19/6. With relay, BC625. These two, $29 / 6$

MOVING COIL PHONES. Finest quality Canadian, with chamois ear-muffs and leather-covered headband. With lead and jack plug. Noise excluding and supremely comfortable. 19/6. Post $2 / 6$. INVICTA LOUDSPEAKERS. Good quality In wooden unit (impedance 3 ohms.) In wooden cabinet $17 \times 17 \times 6$ in. Complete with 50 ft , lead and jack plug. BRAND NEW. 39/6. Carr. 5/6.

## VITAYOXPRESSURE UNITS TYPE

 N. 20 watts. P.M. Heavy duty.BRAND NEW, boxed. 8916. Carr. $5 / 6$.

RESISTORS
Morgan " $T$ " ( $\frac{1}{2}$ watt) and ". R " (I wate). Latest types, all BRAND NEW 100 assorted. $10 / \mathrm{L}$. Post $1 /$.
HEAVY DUTY
HEAVY DUTY SLIDER RESISTORS 1.25 ohm 20 amp ., $12 / 6$, post $3 / 6$ I ohm 12 amp ., $8 / 6$, post $2 /$-.
PRECISION RESISTORS. I legohm $1 \%$ I watt wire wound. Ex-U.S.A BRAND NEW. $10 / 6$ per dozen.
DCIA.C. CONVERTERS. Input 12 v . D.C. Output 230 v. $50 \mathrm{c} / \mathrm{s}$. A.C. at
135 watts. Fitted with $0-300$ v. A.C. 135 watts. Fitted with $0-300$ V. A.C.
$2 \frac{1}{2}$ in. meter and slider resistor for voltage adjusement. In stout wooden earrying case with lid. Perfect working order 69/19/6. Carr. $10 / 6$.
24 v . Input 230 v . A.C. $50 \mathrm{c} / \mathrm{s} 100$ wates ourput. In grey metal case. BRAND NEW. 92/6. Carr. $7 / 6$.
RADIATION METERS. Portable doserate meter, containing modern rype
rectangular 50 microAmp meter, CVX494 electrometer valve, etc BRAND NEW In canvas carrying case. $63 / 19 / 6$. Post $2 / 6$ for details of other equipment, see our previous adverts.


## CRYSTAL CALIBRATOR; No. 10



PORTABLE PRECISION VOLTMETERS
Brand new instruments by famous polished teak ' case polished teak case.
Moving iron instruMoving iran inst ment reading volts on 2 ranges A. 160 on 2 ranges 320 v., 8in. mir320 v., 8in. mirror scale. Ac${ }_{2}{ }^{\prime \prime}{ }^{\prime \prime}$. $65 / 19 / 6 \mathrm{ca}$. P/P $3 / 6$.


TINSLEY PHOTO VOLTAGE AMPLIFIERS
These special instruments incorporate a microamp mirror galvonometer and a double selenium photo-electric cell. Housed in aluminium case complete with 12 v . lamp and housing. Brand new $£ 15$ each. P/P, $7 / 6$.

AMERICAN 1,000 O.P.V. MULTI.
RANGE TESTMETERS


400 microamp basic mov. Seven A.C.ID.C. volt ranges 0 to $5,000 \mathrm{v}$. D.C. current 1 mA , $10 \mathrm{~mA}, 100 \mathrm{~mA}, 1$ amp. Res. 100 ohms, 100 K ohms and 1 meg. Decibels. Supplied brand new with test prods, batteries and instructions. $£ 3 / 19 / 6$ each. P/P $2 / 6$

MINE DETECTORS No. AA Complete equipment comprises search head, amplifier, headset, control box, telescopic rods for search head, test unit, test measure and haversack. Operation from Std. $67 \frac{1}{2} / 1.5 \mathrm{~V}$.
battery. Will detect ferrous or non-ferrous battery. Will detect ferrous or non-ferrous
metals. Very portable and sensitive. Supplied metals. Very portable and sensitive. Supplied
brand new in originai transit cases with brand new in original transit cases wh.
circuitand instructions. $99 / 6$ each. Carr. $10 / 6$.

DON Mk. 5 FIELD TELEPHONES Ideal for all inter-communication. Buzzer calling. Supplied fully tested, complete with batteries and instructions. $39 / 6$ each. P/P 3/6 ea., 5/-pr.


MAINS ISOLATION TRANSFORMERS. 230 v . input, 230 v . output, 5 mmp capacity. Housed in ventilated metal case, 65 each P/P $10 /$ -

750 watt AUTO TRANSFORMERS. Tapped from 110 to 230 v . Fine heavy duty type, 69/6 ea. P/P $5 /$
A.C MAINS VOLTAGE REGULATOR TRANSFORMERS. Input 230 v . Output var. 185 to $250 \mathrm{v}, 24 \mathrm{amps}$ or 185 to 250 V . input, 230 v . output $24 \mathrm{amps}, ~ E 12 / 10 \%$. P/P $10 /-$



## ROTARY CONVERTERS



12 v. D.C. input. 230 volt A.C. 150 watts so cycles output. Housed in wooden astage conerol slider resistance switch plugs and A C. swains plogs ge * output check meter. Supplied in perfect condition, individually tested $\varepsilon 9 / 19 / 6$ each. P/P 10/-

VORTEXION PORTABLE AMPLIFIERS Operation from 200 250 voles A.C. or 12 volts D.C. Separate
inputs for microinputs for microphone or gram. Out-
put matched to 7.5 , 15,250 or 500 ohms. incorporates volume control and full switched tone control. Valve line-up $6 Q 7,6 J 5,6 \mathrm{~V} 6,6 \mathrm{~V} 6,5 \mathrm{Z} 4$. Size $8 \frac{1}{2} \times 6 \frac{1}{2} \times 17 \frac{1}{2}$ in. not brand new but supplied in perfect working order, fully tested. $\mathbf{f 1 0 / 1 0 / - \text { each. P/P 6/:- }}$



## 24 VOLT ROTARY CONVERTORS.

Input 24 volts D.C. Output 230 volt: A.C. 50 cycles, 100 watts. Housed in metal carrying case with inlet; cutlet plugs. Crand new, 92/6 each.


FERRANTI TESTMETERS TYPE Q
D.C. A.C. D.C. Ohms. $30 . \quad 15 \mathrm{v} . \quad 7.5 \mathrm{ma} .25,000$

 | 150 |  |
| :--- | :--- |
| 600 | v. | $\mathbf{0 6 0} \mathrm{v}$ v. 1500 ma.

500 ohms per volt on all ranges B.S.S. first-grade accuracy on all self contained ranges. Supplied tained ranges. Supplied
in perfect workin- order
 complete with leads, rexine covered carrying case. Price 52/6 each. case.
P/P $2 / 6$.


ADMIRALTY POWER UNITS 234A. $200 / 250$ volt A.C. Input. Output 250 volts 15 mA . and 6.3 volts 6 amps. Fully smoothed double choke and paper condensers, fused and fitted with input and output plugs. Sockets are provided on the front panel for meter check. Housed in grey metal case for standard 19in. rack mounting. Supplied brand new. 59/6 each. P/P $7 / 6$.

CR. 100 SPARES KITS. 15 valves, resistors, pots, o/P trans. condensers, all new boxed, $59 / 6$ per set. P/P $2 / 6$.

ADVANCE CONSTANT VOLTAGE TRANSFORMERS. 190 to 260 volt input. Constant 230 volts output. 150 watts. Brand new, $88 / 10 /$ each. P/P 5/-.

BRAND NEW U.S.A. DRY 90 VOLT H.T. BATTERIES. Tapped $67 \frac{1}{2}, 45$ and $22 \frac{1}{2} v .5 /$ - each. P/P 2/-.


NIFE ALKALINE ACCUMULATORS. 12 volt 45 ampere. $£ 4 / 19 / 6$ each. $P / P 7 / 6$.

MARCONISIGNAL GENERATORS TF-517. $10-18 \mathrm{mc} / \mathrm{s} .33-58 \mathrm{mc} / \mathrm{s} .150-300 \mathrm{mc} / \mathrm{s}$. Operation $200 / 250$ volts A.C. Supplied in good working order, $\mathrm{E} 12 / 10 /$ each. P/P $10 /$.

MUIRHEADPRECISIONST UDSWITCHES. 2 pole, 2 bank, 24 position, $10 / 6$ each. P/P 1/4 pole, 4 bank, 24 position, $17 / 6$ each. P/P $1 / 3$.


MARCONI TF. 428 日/I VALVE VOLT. METERS. 5 ranges A.C. and D.C. 1.5, 5, 15, METERS. 5 ranges A.C. and D.C. $1.5,5,15$,
50 and 150 volts. Operacion $200 / 250$ volts 50 and 150 volts. Operation $200 / 250$ volts
A.C. Supplied in perfect working order A.C. Supplied in perfect working order
complete with internal H.F probe, $t \mid 7 / 10 \%$. complete with
each. P/P 10/-.


FURZEHILL BEAT FREQUENCY AUDIO OSCILLATORS. Frequency range 0 to 10,000 cycles. Outpue 10 or 600 range 0 to 10,000 cycles. Output 10 or 600
ohms. Separate 50 cycles check. Set zero ohms. Sepal. $200 / 250$ volt A.C. Operation. Supplied
control in perfect working order, fully tested, $£ 9 / 19 / 6$ in perlect workin
each. P/P 10/-.


HALLICRAFTER S. 27 U.H.F. COM. MUNICATION RECEIVERS. F.M. or A.M.coverage 27 to $143 \mathrm{mc} / \mathrm{s}$. on 3 bands. Incorporates $S$ meter, variable sel. b.f.o. a a n.l. etc. Output for phone or speaker. Operation 110 or 230 volts A.C. Supplied in good working order, $\mathbf{2 2 7 / 1 0 / - \text { each. P/P } 1 0 / - \text { . }}$

FIELD TELEPHONES TYPE F. Generator bell ringing. Supplied complete with batteries fully tested and complete wisl. wooden carrying case $59 / 6$ cach. P/P 3/6. 5/- pr.


HOURS OF BUSINESS: 9 A.M. TO 6 P.M. THURSDAY I P.M. OPEN ALL DAY SATURDAY. SEND S.AE, FOR LISTS.

* Tunable over medium and long wavebands
$\star 250 \mathrm{~mW}$ output push-pull
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$\star 7$ in. $\times 4$ in. high flux speaker
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Complete set of parts
including cabinet and all components. Now
£10.19.6
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FREE BOOKLET

Car radio components $8 /-$; A.Y.C. $4 / 3$; now 325 mW version $\mathrm{f} 11 / 11 / 6$. P. \& P. $2 / 6$. Size $9 \mathrm{in} . \times 7 \mathrm{in} . \times 3 \frac{1}{2} \mathrm{in}$. Weight 4 lb .

## NEW BARGAIN PARCEL

* Perdio style moulded cabinet with gold trimmings (red, blue or cream)
* J.B. $208+176$ pF screened gang .............................................. 10/6
 * 20.1 output transformer to match ....................... $10 /-$

* 5-transistor circuit diagram ..................................... $/$ * Cabinet size $5 \frac{1}{2} \mathrm{in}$. $\times 3 \frac{1}{2} \mathrm{in} . \times 1 \frac{1}{4} \mathrm{in}$.

SPECIAL INCLUSIVE PRICE 55/- P.P. $2^{1 /-}$
All the above components are made to fit the cabinet and printed circuit. Other components for the radio available.

## AUDIO GENERATOR

Check audio circuits easily and quickly
$\star$ EDISWAN Transistor $\quad \star$ Slize $2 \frac{1}{2} \mathrm{in} . \times 1 \frac{5}{8} \mathrm{in} . \times \operatorname{lin}$. * Clear Note KIdeal Modulator Morse Practice Unit.

$$
25 /=\text { PP. } 1 / \text {. }
$$

## THE TELETRON "TRANSIDYNE"

* 6 EDISWAN Transistors
$\star$ TCC printed circuit. $\star 120 \mathrm{~mW}$ output push-pull.
$\star$ Med. and long waves.
$\star$ Components identified.
$\star$ Long-life batteries.
$\star$ EASY TO BUILD.
$\star 2 \frac{1}{2}$ in. high flux Speaker.
Size $6 \frac{1}{4} \times 3 \frac{3}{4} \times 1 \frac{3}{4}$ in. Weight 20 ozs.
All components for construction including cabinet, printed circuit, etc., can be supplied for

$$
£ 11.19 .6 \text { Р.Р. 2/6 }
$$

## All parts sold separately.

SEND I/- FOR CIRCUIT; PLANS AND PRICES
TRANSISTORS
JUNCTION PNP FULLGUARANTEE
NOW FROM


EACH.
SEND FOR NEW FREE LIST OF LATEST TYPES WITH FREE DATA AND SUGGEST USES.

## MAJOR-2 <br> (two-transistor pocket radiō)



* 4 -stage reflex circuit $\star$ Tunable over.medium waves $\star$ No aerial or earth $\star$ Over 6 months on one battery + Size $4 \frac{1}{2} \mathrm{in} . \times 3 \mathrm{in} . \times 1 \frac{1}{4} \mathrm{in}$.
$\star$ Weight under 4 oz .
$\star$ Layout diagriams
Complete set of components including 2 EDISWAN transistors, $72 / 6$ post free. All components sold separately. FREE NEW BOOKLET.


## MA 0 R 3 (three-transistor radio)

As the Major-2 but with a third EDISWAN transistor and fitted with a volume control. Fantastic output! 90/post free. FREE LIST ON REQUEST.

## CAR RADIO 2-watt Amplifier

A permanent power transistor stage complete with $7 \mathrm{in} . \mathrm{x} 4 \mathrm{in}$, speaker. May be used with any battery portable using a 3 ohm speaker. Use it with the " 8 "".
Complete set of parts
65/- P.P. $2 / 6$
Unit build up and tested 77/6 P.P. 2/6
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AUDIO, RF and IF:
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$\star$ Headphone Output.
$37 / 6$ P.P. 1/6
$\star$ New Chassis; New Diagrams.
Ideal Pocket Unit; Easy to Use; Find the Fault in Minutes; May be used as a Signal Peaker.

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Todel A-10: 500 micro-amp. movement A.C./D.C. voltage at 2.000 ohms. per volt 10, 50, 250, 500 and I kv.

Resistance range: 10 k . and 1 megohm.
D.C. curren: 500 micro-amp., 25 mA ., 250 mA . Desibel range. Accuracy: D.C. $\pm 2 \%$ : A.C. $\pm 3 \mathrm{~m}$
Size: $\left.5 \frac{1}{8} \times{ }_{58}^{5} \times 1\right\}$. Weight 17 ozs
Price $£ 4 / 17 / 6$, inclusive of full handbook batteries and test prods. Fully guaranteed.
IDEAL POCKET INSTRUMENT FOR' THE AMATEUR AND PROFESSIONAL.

CRYSTAL CALIBRATOR No. 10 Crystal controlled. Full coverage from 500 $\mathrm{kc} / \mathrm{s}$. to $10 \mathrm{Mc} / \mathrm{s}$. $\mathrm{i} / \mathrm{s}$. Modulation. Calibraced dial. includes 2-IT4: IR5 valves. Full handbook, $59 / 6$. P.P. $3 / 6$
V.H.F. TRANS./RECEIVER TYPE 1986
124.5/156 Mc/s. coverage. $9.72 \mathrm{Mc} / \mathrm{s}$. I.F.: $23 \mathrm{Kc} / \mathrm{s}$. bandwidth. Io-channel V.H.F. airborne equipment. 24 volt D.C. input.

|  | With |  |  |  |
| :--- | :---: | :---: | :---: | :---: |
|  | Type | Less |  |  |
| Valves | Valves | P.P. |  |  |
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| Full circuit diagram $1 / 9$, post free. |  |  |  |  |

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The ideal F.M. conversion unit as "P.W.W." April/ May, 1957. Complete with 6 valves, three EFPl's, two EF92's and one EB91 I.F.T's, etc., in absolutely new condition. With circuit and conversion data.
12/6 (less valves)
37/6. (with valves)
Postage and Packing

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2 / 6 \text { (either type) }
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## BC 906D WAVEMETER

Complete with vernier dial in black crackle case 500 UA $2 \frac{1}{2}$ in. meter: 150 to $235 \mathrm{Mc} / \mathrm{s}$. Battery operated. Includes circuit. 155 valve. $45 /$-. P.P 5/6.

SYNCHRONIZER UNIT
Valves: $3-6 \mathrm{C} 6 \mathrm{M}$; $12-6 \mathrm{AC} 7 ; 6 \mathrm{Q7} ; 5-717 \mathrm{~A} ; 6-6 \mathrm{SN7}$ GT: 6H6. Transformers, chokes, dials, slow motion drive, etc. Brand new $£ 4 / 19 / 6$. P.P. 5/

ROTARY CONVERTER
4 v. D.C. to 230 v. A.C. 50 cycles. 100 wates. unused.
65/10/-
${ }_{7 / 6}$ Carr

## RF 25 AND 26 UNITS

Type 25: 30 to $40 \mathrm{Mc} / \mathrm{s}$. switched tuning. Includes 3-SP61: etc. $10 / \mathrm{m} . \mathrm{P} / \mathrm{P} .2 / 6$. Circuit diàgram 9 d 3-SP61: etc. $10 / \mathrm{m}$ P.P. 2/6. Circuit diàgram 9d.
TYPE 25 : 50 to $60 \mathrm{Mc} / \mathrm{s}$. slow motion vernier tuning. 2-EF54; EC52. 25/-. P.P. 2/6. Circuit 9d.

AN/ARN-5D GLIDE PATH RECEIVER 3 chännel UHF crysral controlled receiver operating on $332.6 \mathrm{Mc} / \mathrm{s}$. $333.8 \mathrm{Mc} / \mathrm{s}$. and $335 \mathrm{Mc} / \mathrm{s}$. Includes 28D7, 2-12SN7, 7-6AJS. 12SR7. relays I.F.s etc. Input $24 / 28$ volts D.C. $59 / 6$ P.P. $5 /$

## PACKARD BELL PRE-AMP.

Complete with screened case with 6SL7GT; 28D7; relay, leads, iack plugs, handbook, etc. sealed in carton. Low impedance mic. pre amp.

$$
\begin{aligned}
& \text { ONLY } 12 / 6 \frac{\text { P.P. }}{2 /-.} \\
& 426 \text { CONTROL UNIT }
\end{aligned}
$$

includes: 4-EF50; 2-SP61; EB34; multiban'، witches; pots; eranstormers, etc.

$$
30 /=\quad \text { P.P. } 2 / 6
$$

## TYPE 247 INDICATOR UNIT

R.F. POWER WATTMETER. I mA. 4 inch meter magic eye indicator: $100 / 240$ mains transformer chokes: EF50's; DIODES; RECTIFIERS, etc.

ONLY S3/19/6 P.P. $2 / 6$
APQ9 UHF UNIT
RADAR JAMMING UNIT; INCLUDES 2-807; 3-6AC7; 2-8012 HF; Gear drives; Blower motor: switches; dials; controls, etc.
£7/10/0
P.P. $7 / 6$.


PIRANI CONTROL UNIT Includes:
$\star$ bin. I mA. movement meter with mirrored scale.
$\star$ Fully set Wheatston= Bridge.
t Complete in best quality case.

* Built-in galvo-shunt.

ONLY \&5/19/6 P.P. 5/-.
Including Circuit diagram.
MARCONI NO. 19 SET CRYSTAL CALIBRATOR
CRYSTAL CONTROLLED OSCILLATORS; $10 \mathrm{Kc} / \mathrm{s}$. $100 \mathrm{Kc} / \mathrm{s}$., and $1 \mathrm{Mc} / \mathrm{s}$. includes 5-12SC7: handbook; on/off modulator: quartz crystal.

ONLY 79/6 P.P. 2/6.

## SURPLUS UNITS

NEW FREE LIST. TRANSMITTERS, WATTMETERS, RECEIVERS, WAVEMETERS. CONVERTERS, TESTUNITS, INDICATORS, I.F.S, R.F. UNITS, RADAR UNITS, CRYSTAL CAL'BRATORS. METERS, ETC., ETC.

## RADAR UNIT TYPE 1683

Complete withthe following valves 2—6C40; 832A; 0829B; 2-5R4G; 3-SAC7. 6V6GTO; 931 A photo multiplier with associated network. Also 2-blower motors. Input 30 - 115 volt 400 to $2,600 \mathrm{c} / \mathrm{s}$ cd 26 v. d.c. BRAND NEW and boxed.

$$
26 / 10 /=\begin{aligned}
& \text { Post } \\
& \text { free }
\end{aligned}
$$

WALKIE/TALKIE TYPE 38 TRANSMITTER RECEIVER
Complete with 5 valves. In new condition These Sets äre sold without Guarantee, but are $22 / 6$
H/phone $7 / 6$ pair. Junction Box $2 / 6$. Throa Mike 4/5. Canvas Bag 4/-. Aerial Rod 2/6.

## AIRCRAFT RADAR TYPE AN/APA-I

 Complete scope indicator unit with amplifier aerial switching unit; füll scope controls. linclu des 3BPI Tube; 6SN7GT; 6K6GT; 6G6GT $2 \times 2$; $6 \times 5 \mathrm{GT}$.$$
\begin{array}{ll}
\text { BRAND NEW } \\
\text { FULL HANDBOOK. }
\end{array} \quad 97 / 6 \quad 3 . P .
$$

## VHF TRANS./RECEIVER TYPE 1920

t $100 \mathrm{Mc} / \mathrm{s}$. to $120 \mathrm{Mc} / \mathrm{s}$. coverage.
\& $9.72 \mathrm{Mc} / \mathrm{s}$. I.F. $\& 40 \mathrm{Kc} / \mathrm{s}$. bindvridth. t 4-channel crystal controlled.
VHF airborne equipment.
Complete with 21 valves, crystal and 24 volt rotary unit all contained in metal case.

$$
26 / 19 / 6 \quad \begin{array}{ll}
\text { P.P. } \\
10 / 6
\end{array}
$$

Separate Circuit Diagram 1/9 post free

## TRANSMITTER/ RECEIVER

 Army Type 17 Mk. II Complete with Valves, High Resistance Headphones, Handmike and instruction Book and circuit. Frequency Range 44.0 to $61 \mathrm{Mc} / \mathrm{s}$. Range approximately 3 to 8 miles. Power requirements: Standard 120 V. H.T, and 2 v. L.T.Ideal for Civil Defence and com munications. $44.61 \mathrm{Mc} / \mathrm{s}$.


Calibrated Wav
45/- P.p. 10/- extra.


PIRANI DIFFERENTIAL LEAK DETECTOR
Includes:

* 2-arm Wheatstone Bridge.
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ㅊ Best quality $\because o o d$ case.
t Galvo-shunt.



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Brand new unused 90 volt U.S.A. betteries Tapped at $67 \frac{1}{2} \mathrm{v} . ; 45 \mathrm{v}$.; and $22 \frac{1}{\frac{1}{2}}$ volts. Ideat for portables.

$$
\begin{array}{ll}
W /=\text { each } & \text { P.P. } \\
& 2 /-
\end{array}
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STROBE UNIT
Complete with: 6-EF50; 5-EA50; \$P61. Relays, etc. $\quad 35 /=$ P.P.

## RAIDAIR SEA irblit RECEIVER $^{\text {R }}$



This Receiver is designed to determine the presence and measure the requency of any radar or radio signals within the range of 38 to 2,000 $\mathrm{Mc} / \mathrm{s}$. To determine what modulation may be present on these signals giving an identification of relative strength of these signals. The equipment consists of:-

5-stage IF ( $30 \mathrm{Mc} / \mathrm{s}$ Amplifier provision is made to feed the IF amplifier to a panoramic adaptor)
1 Detector
2 Stage Video Amplifier ( $100 \mathrm{c} / \mathrm{s}-1 \mathrm{Mc} / \mathrm{s}$, $\pm 2.5 \mathrm{db}$ )
I Beat frequency oscillator
The signal is fed through RF "plug in" heads consisting of types:-

TN16 $38-95 \mathrm{Mc} / \mathrm{s}$ I RF Triode first detector, 1 Oscillator
TNI7 74-320 Mc/s Butterfly resonant circuit I diode first detector, I triode oscillator
TNI8 $\quad 300-1,000 \mathrm{Mc} / \mathrm{s}$
Butterfly resonant circuit
I Crystal first detector
Triode oscillator
The above three units are available now.
TN19 obtainable (TN19-950-2,000 Mc/s available as extra)


## mainconi

S-BAND $(10 \mathrm{~cm})$ SPECTRUM ANALYSERType TF984


FREQUENCY RANGE 2,900 to $3,150 \mathrm{Mc} / \mathrm{s}$.
SENSITIVITY 200 MicroWatt for 5 cm . deflection. 20 Mean Watt for 5 cm . deflection.

SPECTRUM WIDTH I to $10 \mathrm{Mc} / \mathrm{s}$.
-SWEEP FREQUENCY 4 to $10 \mathrm{Mc} / \mathrm{s}$.
1.F.
$22.5 \mathrm{Mc} / \mathrm{s}$.
1.F. BANDWIDTH $\quad 100 \mathrm{kc} / \mathrm{s}$ for 3 db drop in lével.

Prices given on request.

Now available from stock -

## BC221 HETERODYNE FREQUENCY METERS

Function
An acourate meterodyne, frequency meter having crystal check points for calibrating
equipment using $C W$ or modulated $C W$. This tesk set mny be used for the following: - Measurement or calibration of the freguency of transmitters, oscillators, or signal generatora.
Mcasirement or calibration of the fiequency of receivers having a beatfrequency useillator with zero-beat
adjustment.

Electrical Characteristics
Fundamental Frequency range: 125 kcis
 to $50 \mathrm{Me} / \mathrm{s}$.
Overall Accuracs: $0.01 \%$ or 25 cyeles. whichever is the greater, within the specfliel temperature range.
Operating Temperature Range: $-30^{\circ} \mathrm{C}$ to
$+50^{\circ} \mathrm{C}\left(-22^{2} \mathrm{~F}\right.$ t $\left.+122^{\circ} \mathrm{F}\right)$.
RF Output (Functioning as a teat osclliator);
2 millivolts. 2 millivolts.

## ALSO AVAILABLE V.H.F. VERSIONS OF ABOVE

## TS174

TS175
Electrical Characteristics

| Callbrated Frequency Range: 20 to $280 \mathrm{Mc} / \mathrm{s}$. |  |
| :---: | :---: |
| Frndamental Frequency Hange: 20 to $40 \mathrm{Me} / \mathrm{s}$. |  |
| Accuracy: $0.05 \%$ (ibroughout the temperature range). |  |
| Slgnal Input: (Setisitivity) 20 millivolts to 2 volts. |  |
| glgnal Output: 50 to at 1,000 cycles. | 0 millivolts modulate |
| Temperature Range $\left(-40^{\circ} \mathrm{F} \text { to }+1.31^{\circ} \mathrm{F}\right) .$ | $-40^{\circ} \mathrm{C} \quad 10$ |

Callbrated Frequency Range:
80 to $1,000 \mathrm{Mc} / \mathrm{s}$.
Fundamental Frequency Range:
80 to
Accuracy: $0.05 \%$ (throughont the temperature range).
8lgnal Input (sensitivity)
Signal 'Output: 100 microrolts to 20 inilit-
volts modulated at 1, mio cyeles.
Temperature Range: $-40^{\circ} \mathrm{C}$ to $+55^{\circ} \mathrm{C}$ $\left(-40^{\circ} \mathrm{F}\right.$ to $181^{\circ} \mathrm{F}$ ).

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OUTPUT (2KVA) Completely Variable 0 to 270 voles. 9 amps.
INPUT 230 Volts, 50/60~
A SHROUDED FULLY VARIABLE TRANSFORMER FOR BENCH OR PANEL MOUNTING. SIZE:- APPROXIMATELY 81 CUBE. WEIGHT:-APPROXIMATELY 30 LB. PRICE:-RIDICULOUS ONLY- 15.0 .0 plus $12 / 6$ Carr. supplied new and boxed.


ROTARY CONVERTORS 12 v. D.C input, 230 volt A.C. 150 watts, SJ cycles output. Housef in wooden case and fitted with voltage control slider resistance, switch, plugs and A.C. miains voltage output check meter. Supplied in perfect condition, individually tested, $£ 9 / 19 / 6$ each. P/P $10 / \mathrm{F}$.

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L.T. SUPPLY UNIT by s.t.c.


Normal cost over $\mathbf{1} 100$
Essential equipment for Electronic, Engineering, research laboratories, schools, etc. Guaranced for 20 amp
Output: D.C. Variable up to 20 amps. and 24 V or trickle charge 125/350/ Input: A.C. $100 / 260$ volts $45 / 65$ ercles.
Size:
$16 \times 24 \times 3$ in. High. Size: $16 \times 24 \times 32 \mathrm{in}$. High.
Available in Grey Cabinet
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High Speed Single change-over
 $15 / 6$
$17 / 6$ H96C, $145 \Omega+1450$
$196 \mathrm{D}, 500 \Omega+500 \Omega$ 19/6 H96E, $1,700 \Omega+1,700 \Omega$


Vibrators 12 v. Multhy (ne
Headphones DLRI (pairs)
oz. mi
Headphones DLRI (pairs)
Earpieces. Balanced armed
sund
samanced armature ITB
Earpioces. Low rexistance solisicio Ear pilices. Low resestance solisibio G.P.0. Telephones. lamp signalting.

GUARANTEED METERS (New \& Boxed) Each
50 Micro amp. M/6. 2in. flush circ.
Scale Rotagens
. Scale Rothagens
500 Mioro M/C. ${ }^{2}$ 500 Mioro mmp . M/C. ${ }^{2}$ in.
square. Scale
20 amp. $\mathrm{M} / \mathrm{C}$. $2 \mathrm{n} / \mathrm{m}$. fluoh virc

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\end{aligned}
$$ shuat.

5 Milliamp. M/C,
scale
Mip.
ut shunt


CONSTANT VOLTAGE TRANSFORMERS
ferrantt 7l-Eya moving coil
Stabilized entput moltage in the range 200-250 \%. constant with $\pm 1 \%$, at inl limda 0 to $30 / 377^{\prime \prime}$ mmps. When the sapply voliage: is varylng over the range

- Frequency compensated $45-55$ and 54 -6i6 c/s.
- Exellenit output wave-form.

Unused. Complete with transionmer book at a fraction of the nommal cost, only $£ 65$ T. S.A. R-9B/APN-4 Radio Recelvers. First class
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$3 \times 9 \times 11$ in. Wejght 26 jb . Brand new.
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SPECIAL QUOTATIONS ON QUANTITY \& EXPORT ENQUIRIES

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UNUSED, complete with transformer and condenser.
Impedance $7 \frac{1}{2} \Omega$ Handling cap. 8 watts Ideal for outdoor use off cars, boats, etc.
Price 18/6. P.\&P. 3/6 35/- per pair, P. \& P.

Ex-Ministry of Supply P.A. Systerm. Complete with amplifier unit, 4 speakers, microphones, headphones and all spares packed in wooden cases. 6 or 12 volt D.C. $£ 7 / 10 /$-, carr. $30 /$ -


E8.10.0 only $\underset{(15 / 6)}{(\sin )}$
U.S.A.-Type 45ft. TELECOM AERIAL MAST. (7 sections, 6ft. 8 in . $\times 2$ tin., guys, etc.) This entirely complete set in carrying case $12 \frac{1}{2}$ Gns. Carr. 17/6, Or 2 sets for $\mathbf{C 2 5 .}$ Carr. extra. British Manufocture only.
ARMY TYPE 32ft. MASTS similar to above but 10 lin. screw-sections, suitable for permanent lightweight installation. Kit in canvas bag, E5/10/-. Carriage $12 / 6$.
TELEPRINTER EQUIPMENT, CREED Teleprinters 7B. Reperf. Type 7 TR/3.


## MICRO SWITCHES

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 BRAND NEW ministry releace NIVERSAL CONTACT
A.M. Ref. $5 C / 4098$

[^18]
## THE IRONGATE (M.O.) CO.,

$2 / 4$ IRONGATE WHARF ROAD, PRAED STREET, LONDON, W. 2.


FOR A.C. MAINS 200/250 v . Limited number only. new in maker's cartons. 2-speed 3i, and 7\%, twin track. 60 min. playing time at 3,30 min. at 71 . Inputs for mike and tuner. Sin. Speaker. Smart diotone blue/grey case.
$121 \times 91 \times 7 \frac{1}{2}$. $W$ Weight approx. $6 \frac{10}{} \mathrm{ib}$.

TODAY'S VALUE 635
LASKY'S PRICE, including Sin. Spool of Tape nud empty Spool, Crystal Hand 21 gns. Mike and Radio Jack

## SAVE POUNDS ON THIS

 TRUVOX TAPE DECK

Mk. III. Newr and unused, in maker's cartons, 2 -spd.. $3 \frac{1}{1}$ and $7 \frac{1}{2}, 3$ shatled pole B.T.H. motors. Twin track, hich impedance heads. Push-button controls,
tinkes standard 7 in. shools. Size: $141 \times x$
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LISTED AT 22 GNS.
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 collaro tape transcriptor mk. IV, itted digltal counter. Few only. LIST t23. Lasky's PRICE £1\%/19/6. Carr. and insur. $21 /$.TAPE RECORDER AMPLIFIER for use with Conlara Tape Deck. Maker's surphus. tmmplete with 4 ralves and power supplies. £ $7 / 19 / 6$. Pote 34i.

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COLLARO A-gpl., type 4 T200/PX with Studio tramertption P.U. LIST E19/10/LASKY'S PRICE £16/19/6, carr. paid. In Carrying Case, 25i- extru. GARRARD 301. f22/7/3. Strobe, £23/18/4.
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LENCO GL56 (stereo, binofluld diamond), 823/17/-,
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Also all other types.

TRANSISTOR TURNTABLES
0 voli. 45 r.p.m., complete with pick-up GARRARD BA/1, 99/6.
STAAR KINDER, 796.
Post 3/6.

PLASTIC TAPE SPOOLS 3in. 3ifn. 7in. 8\&in. $3 / 6 \quad 4 / 3 \quad 4 / 6 \quad 5 / 6$ 7in. Stetal Spools, $2 / 6$ each Post 1/*

## AMPLIFIERS TO SUIT ALL PURPOSES

 3-3 AMPLTFIER, bultt to Mullard's exact panel. 8 Gus. Post iree.

MULLARD 510 AMPLTFIER KIT. AlI specified componenta and your choice of trausforméra and choke by Partrilge,
Haddon. W B, Filison or Cilown with Haddon. W R, Filison or Gisun, with
printed circult. as low re 9 Ggs Detalls on request. Printed Circuit separately, 22/6.
Also a arailatle built ready for use. Price acenrling to transformers used.

3-WATT GRAM AMPLIFIER. 2 valve ECL8: and EZz8 rectifier, double wound misin transiormer 100 -250 A.C., tone
control. record equalisation switeh, size $73 \times$ Blin.. max. height 4 lin. Controis momited scparately. LASEX'S PRICE, complete with knobs, $55 /-$. Post $3 / 6$. Matched palr for stereo 5 Gns. Post $\mathrm{B} /$.

Special offer. single valve 2-watk. Gram Amplifer, 45/-. Post 3/8.

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3 channels, for use with all tape recordere and audio ampttere. Size: $4!\times$ äd $\times 4!\mathrm{in}$. LASKY'S PRICE 35/-. Poat $9 / 6$.


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ERASER And HULE TAPE ERASER and Heafl De-
magretizer, Erages complete reel of magnetic tape in \&f few seconds. 27/6, port free.

## HIGH FIDELITY TAPE RECORDER HEADS



Leading make. new and unused. Upper or lower track RECORD/PLA YBACK. high impedance. Double wound and wif
reproduce up to 12 ,0u0 e.p.c. ht $7^{1}$. 1 .u.s
 volte at 1 Kc at 7 ! i.p.s. ERASE, low Impedance. List et Paik. LASIKY: PRICE, per pair, 39/6. Post $1 / 3$. Please "plectify uiper or lewer trick.

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Acos Mic 29-1; Crystal stick Mike for high quality recording. broadcasting athl public addreas woris. list at Cis.


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## LASKY'S RADIO FOR COURTEOUS SERVICE \& TECHNICAL ADVICE

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- AF resspmbe - 2 in to nicive and its performance compares mott favourrabiy This recefvrr is rery semsitive and its performance compares mowt favourabiy
with anything obtatnable. It embontes the latest design developments together with anything obtainalle. It embortles the latert design developments tongether
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## 25 MFD . 23 MINIATURE BIAS CONDENSFRS


 .005 MFD. 6 d . each. . 01 MFD .9 d .
VARIABLE GANG CONDENSERS
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## SUB Mint

## SLEEVED-AU at $2 / 3$ each.

1 mid. $12 \mathrm{\nabla} ., 25 \mathrm{at} 2 / 2 \mathrm{~m}$ each. 15 v .
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$1 \mathrm{~K} .2 \mathrm{~K}, 5 \mathrm{~K}, 50 \mathrm{~K}, 220 \mathrm{~K}, 330 \mathrm{~K}, 1 \mathrm{M}, 2 /-$ each. 5 N , with mitch, 4.6 . $5 \mathrm{~K} .1,6,500 \mathrm{~K}$ preset 1 i . 1 IM Transistor Pots, 2L. 5 K Transistor Pots, $1 / 6$.


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Pubh-Pull outpon Push-Pull outpon componente, excluding cabinet and hatteries, supplled at epecial inclusire Arice of $\mathcal{E} 7196$. Plas $3 / 6$ P.P All parts

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500 v working, 680 pf .. $1.010 \mathrm{pti}, 1,000 \mathrm{pf}$, $2,200 \mathrm{pf}$,


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No. 10

(Battery powered I.4 v. valves). Brand new and unused. Complete with full working instructions, circuit diagram, carrying haversack, connecting lead and spare valves. Frequency range: 1.5 to $10 \mathrm{Mc} / \mathrm{s}$. (Nominal), but can actually be used up to $30 \mathrm{Mc} / \mathrm{s}$. Wgt. 5 lbs. Size 7 in. $x 7 \frac{1}{2}$ in. $x 4$ in. A miniature B.C. 221 in every respect. $A$
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PRECISION SERIES 834-S. (U.S.A.). Multi range tester for A.C./D.C. volts, ohms and milliamps. Basic movement 400 microamps. Housed in wooden box with carrying strap. Overall size $7 \frac{1}{2} \times 7 \mathrm{in}$. $\times 5 \mathrm{in}$. Complete with test prods batteries, etc. Ready to use $£ 5$. Post $2 / 6$.


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Heavy duty 20 watts all-metal. 15 ohms. Dia$\begin{array}{ll}\text { meter } & \text { I5in. } \\ \text { length } & 15 \mathrm{in} .\end{array}$ length 15 in.
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BAKER'S SELHURST SPEAKERS 12 in . P.M. 15 ohms 15 watts, $30-14,000$ c.p.s Our price $£ 4 / 10 /$
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Adjustable every 6in. to approx. Sft. Gin. when fully extended. (Folds up to only 4 ft. Gin. for storage). Suitabla for outdoor speakers, public addiess systems. floodlighting, etc., ets



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INCORPORATING THE LATEST MK. IV COLLARO TAPE TRANSCRIPTOR. THE LINEAR LT45 HIGH QUALITY TAPE AMPLIFIER. A HIGH FLUX $7 \times 4 \mathrm{in}$. LOUDSPEAKER, 850 ft . Reel of Best Quality L.P. TAPE. Spare Tape Spool and a Po-table Cabinet, size approx. $18 \times 13 \times 9 \mathrm{in}$., finished in Veneered walnut or Sapeie.

FEATURES INCLUDE
$\star 3$ SPEEDS. $\star$ FREQUENCY RESPONSE $\pm$ 3d.b. 50-11.000 c.p.s. $\star$ SWITCHED NEGATIVE FEEDBACK. EQUALIZATION FOR EACH SPEED. $\star$ OUTPUT 4 WATTS $\star$ MAGIC EYE RECORDING LEVEL INDICATOR. $\star$ TWIN TRACK OPERATION. Both bottom and top tracks can be recorded or played back withou: removing tape. $\star$ INSTANTANEOUS CHANGES can be made from one track to another. Fast rewind in either direction. $\star$ TAPE MEASURING AND CALIBRATING DEVICE. $*$ TAKES FULL 7in. DIAMETER RĖELS OF TAPE: $*$ NEGLIGIBLE HUM.
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For 200-250\% A.C. mains
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Push-pull output Latest high efficiency B.V.A valves. Dual separately controlled inputs for mike and gram. Separate bass and treble controls. High sensitivity. Output for 15 ohm loudspeaker. Guaranteed brand new, tested. and in perfect working order.

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Type RC/IzoH. Iimitad numher, at £3 196 . (appmox.

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THE SKYFOURT.R.F.RECEIVER


A design of a
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M. wave T.B.F. riopiver with selenfum reatifier. For inclusion In cabine illut rated or $\quad$ oill nut veneered type it emplors ratre
GK7, RPE1.
Splat 6K7, MP61, SFEGI designed for simplicity in wiving Senditivity and quality are well up un whamlaril. Pcint otn-point wiring diagram.
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SIX TRANSISTOR POCKET EADIO RECEIVER

All parts including cream or coloured plastic case, printed superhet circuit. ferrite aeria. Transsistors, 2 in. P.M speaker. Long and medium wavebands. Size of unit 5? ? $3 \frac{1}{4} \times 1 \frac{1}{1} \mathrm{in}$. Detailed construction

£9-19-6
Total cost of parts A working unit can be demonstrated a our County Arcade premises. All item are available sep arately.

Type BM1. An all dry battery eliminator. Size 5 . 4 90 v where A.C. mains $200-250$ v. $50 \mathrm{c} / \mathrm{s}$ is avallable. Suitable for all battery portable receivers requiring 1.4 v . and 90 v . This includes latest low consumption types. Complete kit with diagram 39'9 or ready for use 46/9.
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 Devign of a high qunlity Radio Tuner Unit (epecially guitable for use with any of our Ampiliterss). A Triode Heptode Frchanger is uned. Pentede 1.F. and doable biode SecondDetector, deluyed A.Y.C. is arranged so that A.V.C. dis. tortion is avoided. The $W$. Ch. Sw. incorporates Gram. position. Controls are Tuning. W. Ch. and Vol. Output
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£6/18/6. Carr. $4 / 6$. liste De luxe vereion wired for otereophony ほ

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 3 watt (total 6 Carr. \& packing $7 / 6$. watt) stereo amplifier providing really life-like reproduction. Suitable for use with all stereo, pick-up heads at present available. Ganged volume and tone controls. Preset balance control. Outputs for matched 2-3 ohm speakers. For $200-250 \mathrm{v}$. A.C. mains. Astonishing yálue.
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Primaries $200 \cdot 230-250$ r. 50 cf

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$12 \mathrm{\Sigma} .1$ v. .........7/8
OUTPOT TRANSFORMERS
Midget Battery Pentode 6 : 1 for $3 S 4$, nt
Midget Rattery Pentode © 61 :
Smanll Pentode $\mathrm{F}, 00 \mathrm{O} \cap$ to
standard Pentode $5,000 \Omega$ to $3 \Omega$
Standard Pevtonde $8,000 \Omega$ to $3 \Omega$
Push-putl 8 watt givb to $^{5}$ ohm
Push-pull 10-12 wutts 6 V f to $3 \Omega$ or $15 \Omega$
Posh-pull 10-12 watts to match 6 V 6 to $3-5-8$ or
Push pull Eisistio 3 or 15 ohais
Push-pull $15-18$ watts. Rectionaliy wound. 6 L ji.
Push-pull 20 watt high-quality kentionaliy wound GLE. KTGF, etc. to 3 or $15 \Omega$
............... 4
SMOOTHLNG CHOKES

$150 \mathrm{~mA}, 7.10 \mathrm{H..250} 2 \mathrm{~mm}$
$100 \mathrm{mA},. 10 \mathrm{H} . .200 \mathrm{ohms}$
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PHILCO F.M. RADIO TUNERS
With self-contained power pack. A 6 -valve de luxe unit housed in beautiful walnut veneered cabinet. For 110-200-250 v. A.C. mains Magic eye tuning indicator $12 \frac{1}{2}$ GNS.
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PUSH PULL ULTRA LINEAR OUTPUT "BUILT IN" TONE CONTROL/ PREAMP STAGES.



Two Input sockets with ioswaciated controis allow mixing of " nalke " and gram. as in A10. Figh sensitivity. Includes 5 valves, ECCB3, ECC8s, ELAt, EL\&H, 5 Y 3 . High Quality sectonslly wrounl output transformer specially designed for Ultra Linear operation. and rellable small cordensers of current manafacture. INDIVIDUAL CONTROL\& FOR BASS AND TREBLE " Jaft " and "Cut." Frequency response $\pm \mathbf{3}$ D.B. $30-30,000$ c/cs. Six negathe feedback loops. Hum level 60 D.B. duwn ONLY 23 millivolts INPUT
required for FULL OUTPUT, Suttable for uec with all abd mulerophones. Comparable with the very hest dealgus For STANDARD or LoNa PLAYING RECORDS. For MUSICAL INSTRUMENT etc. OUTPUT SOCKET with plug provides $300 \mathrm{v}, 30 \mathrm{~mA}$. and 83.3 r. 3.5 . For gutars, RADIO FEEDER UNIT. Size approx $12<-3-7 \mathrm{in}$. For A.C. mains $900-250$ ve or supply of in put for 3 and 16 ohms speakers. Kit is complete to last nut. Chassis is fully punched. Full instructions and point-to-polnt wiring diagrams supplied,
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If required louvred metal cover with 2 carrying handles can be supplied for 18/9. TERMS ON ASSEMBLED UNITS. DEPOSIT 18/9, and 12 monthiy payruents of $18 / 9$. Bend 8. A.E. for thustrated leatlet detailing Rewdy-to-assemble Cabinets, Speskers, Microphones etc. with cush and credit terms.

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JUNIOR 5 WATT. High Quality Ontput. Feparnte Rass aml Treble "cut" andi 'Hoost" eontrols. Sensitipity $15 \mathrm{~m} . \mathrm{v}$. High Fhus Rin. Ispeaker, Handeome st mongly made cabinet
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13 Ens. glus 10 - carr

STAAR GALAXY 4 SPEED MIXER AUTO-CHANGERS. Brand New, curtoned. Turnover sapphire styli. Many exclusive features. Unique design motor virtually free from rumble. for $200-250$ v. A.C. mains. Limited number tested and guaranteed $\mathbf{x} 5 / 19 / 6$.

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Size $18 \times 18 \times 8 i n .57,196$ or Deposit $13 / 10$ Slze $18 \times 18 \times 8$. 87,196 or
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 high quality 12 in . speaker of orthodox design support-lng a small elliptical speak. ug a amall elliptical speakand condensers to act as tweeter. Thls high fidelity unit is highly recommended for use with our All or any similar amplifler. Rating is
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CO-AXIAZ CABLE, 75 ohms, Mb., 8d. yard. Twin screenert feeder 11d. yard.

VOLUME CONTROLS with long epindles, all values, less switch, 2/9; with S.P. Ewitch, $3 / 9$.
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R3683 UNITS. Comprising chassis and strong cover $16 \times$ $10 \times 8 \mathrm{in}$. Over 70 resistors (many high stability) and condenserg, valve holderg, IFTs, co-ax. sockets, controts,
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All $200-250$ v. $50 \mathrm{c} / \mathrm{s}$. input.
Pr. 0-110-200-230-250 v., 275-0-275 v. $100 \mathrm{~mA} ., 6.3$ 50 a., 5 v. 3 a.
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$120 \cdot 0-450 \mathrm{\nabla} .250 \mathrm{~mA}$.
12.5 v. 3 a., 5 v. 3 a. ...... 6.3 v. 1 a., 5 r. 6 at 499
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$100 \mathrm{~mA}, 10 \mathrm{H}, 100$ ohms
100 mA ., 5 H .100 ohms, tropicalised 80 mA ., $20 . \mathrm{H} ., 900$ ohrmis
$60 \mathrm{~mA}, 5 \cdot 10$ H., 950 ohms

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assembled chargers 6 v. 1 a
$6 . v . ~$
6 6. v. 2 a. $6 / 12$ v. 1 a $6 / 12 v a^{a}$ $6 / 12$
$6 / 12$
v..$~$
4 a. 6/12 v. 4 a. ........38/9 Above ready for use $56 / 9$ mains and outpuse with Cases well output leads. Cinished in stoved and finished in stoved blue
hammer. Carr. \& pkg. $3 / 6$ CHARGER
TRANSFORMERS 200-230-250 v. $50 \mathrm{c} / \mathrm{s}$. 0-9-15 v. $1 \frac{1}{4} \quad$ a., $11 / 9$; $\begin{array}{lllll}0-9-15 & \text { v. } & 3 & \text { a., } & 16 / 9 ; \\ 0-9-15 & \text { v. } & 5 & \text { a., } & 19 / 9 ;\end{array}$ $\begin{array}{llll}0-9-15 & \text { v. } \quad 5 & \text { a., } & 19 / 9 ;\end{array}$

1919 0-9-15
 Consisting of Mains Trans former F. W. Bridge. Metal Rectified, well ventilated steel case. Fuses, fuse-holders, grommets, panels and circuit grommets, pan
6 v . or 12 v . 6 v . or 12 v . 1 amp... As above, with ammeter $\begin{array}{llll}\text { As above, with ammeter } & 32,9 & \text { and selector plug } \\ 6 & \mathrm{v} .2 \text { amps................ } 25 / 9 & \text { for } 6 \text { v. or } 12 \mathrm{v} \text {. } \\ 6 \mathrm{v} \text {. or } 12 & \mathrm{v} .2 \text { amps. } & 31 / 6 & \text { Louvred }\end{array}$ 6 v . or $12 \mathrm{v}, 2$ amps. $31 / 6$ Lor 6 v . or 12 v . 6 v . or 12 v .2 amps. (inclusive of ammeter) $41 / 6$ tractive hammer 6 v . or 12 v. 4 amps $41 / 6$ tractive hammer BATTERY CHARGER KIT use with 43 amps. 53 blue. Ready for $6 / 12$ v., 6 amp, consisting of and with mains F.W. Bridge Rectifier Mains Double Fused F.W. Bridge Rectifier Mains Double Fused.
Trans. and ammeter.
49/9. Only
Post $4 / 6$.

ASSEMBLED CHARGER

## 6 v . or 12 v .

 2 amps. Fitted Ammeter Louvred metal use with mains OnlyCarr.
3/9.
49/9

All for A.C. Mains $200-250$ v. $50 \mathrm{c} / \mathrm{s}$ Guaranteed 12 months

ASSEMBLED 6 v . or 12 y . $\begin{array}{lll}2 / 12 \text { v. a.h.w. } & 2 / 9\end{array}$
F.W. Bridge $6 / 12$ v. 1 a. $6 / 12$ v. 2 a. $\begin{array}{ll}6 / 12 \text { v. } 3 \text { a. } & 9 / 9\end{array}$ $\begin{array}{lll}6 / 12 & v .4 a & 12 / 3 \\ 6 / 12 & \text { v. } & a\end{array}$ $6 / 12$ v. 5 a. $6 / 12$ v. 6 a. $6 / 12$ v. 10 a. $6 / 12$ v. 15 a. $\quad 25 / 9$ H.T. Type H.W. 120 v . 40 mA . $3 / 9$ $250 \mathrm{v} .50 \mathrm{~mA} . \quad 5 / 9$ $\begin{array}{ll}250 \text { v. } 250 \mathrm{~mA} . & 10 / 9\end{array}$


PORTABLE AMPLIFIER
Size 64 ln . long. 5in high, $2 ; 1 \mathrm{n}$. deep. Will avit any type of crystal pick-up. Output triode. Coszor $1+2 \mathrm{Br}$ output pentode and contact-cooled rectifer. Trully isolited mains raneformer for $230-250$ A.C. mains. Basa reble and volume controls

49/6 Plus P. \&
5" SPEAKER WITH.
O.P. TRANSFORMER
purchased with the above $18 / 6$. Plus P. \& P. $1 / \beta$.

## F.M. TUNER UNIT

 25'- That P. A. 1/a.


8 WATT PUSH: AMPLIFIER COMPLIETE WITH GRYSTAL MIKE AND 8 in . LOUDSPEAKER
A.C. mains $110 / 230$ v. Slze 10 in. $\times 6$ in. $\times$ trin. Incorporating 6 valves, R.F. pen. 2 with all makes and trpes of pick-up and mike Negative feed back. Two ipputs, mike and mike and controls for same. Separate controls for Bass and Treble Hift. For uee with Std. or L.P. records, musical instruments auch as Guitars, eic.
§4.19.6 Piat P. \& P. 7ta
Or 20/- dejosil, pilis P. \& P. $7 / 6$ and 4 monthly nayments of $23 /-$


## PLAYER CABINET

Finished in 2-tove lentheretie, will take B.S.l. UAB. with room for ampllier and Tin $x$ hin. speaker. Overall size logith $\times$ tatin. $\times$ gin.
\&2.19.6


13 CHANNEL TUNER

34 to $38 \mathrm{Mc} / \mathrm{s}$, complete with PCFP8 and PCC84. Thesp have been removed fron $23 /=$ complete with knobs.
16.19. Me/s complete with knobs leas valves 13/- Pins P \& P. $8 / 6$


## AC/DC PCCKET MULTI-METER KIT



Comprising zin moving coul meter, seave callComprising Zin. moving cou meter, seare eall Voltage ringe A.C.fD.C. $0 \cdot 0.50,0-100,0-250,0-500$. Miliamps. 0-10, 0-600. Ohms range, $0-10,000$. Front panel, range switch, wire-wound pot for ohms zero setting). toggle switch, resistor and rectifier. Basle movement, 2 mA . In grey 19/6 Plus Built and tested Point to point wirlag diagram $1 /-\frac{7 / 6 \text { extra }}{7}$ (ree with kit

6 watt PUSH-PULL AMPLIFIER
A.C. mains $220 / 250 \mathrm{r}$. incorporating 4 valves and metal rectifer. 2 inputs, high and low, and controls for rame. Separate contmols for Bass and Treble lift. Slze of chassif
11 in . X 4 i in . x 2!ina
$59 / 6$ ‥ Pime


## 4 WAVE BAND COIL UNIT

Complete with tuning condenser. separate sec ions for short wave. Coverage $10-21 \mathrm{~m}$., $21-45 \mathrm{~m}$., NEW, by famous manufacturer. Completely $\begin{aligned} & \text { NEw, } \\ & \text { asembled on eub-chassis. } \\ & \text { With circuit dlagram. }\end{aligned} 19 / 6 \begin{gathered}\text { P. \& Plus } \\ \text { p. }\end{gathered}$

## CONSTRUCTORS' PORTABLE PARCEL

Comprising case, chassis, top plate, scale, Jin. P.M speaiter with O.P. trans.. twingang. $2470 \mathrm{Kc} / \mathrm{s}$ witeh trimmers, four salve holders, warechange 39/6 Plus $3 / 6$ Postage and paekin.


## LINE E.H.T. TRANSFORMER

By fanous mannfacturer. 14 Kv . Complete with bult-in line und widt', controus.
Windiug for Ey . Windiug for EYsi Rectifer $19 / 6 \begin{array}{ll}\text { Plus } \\ \text { P. P. } 2 / 6 .\end{array}$

## MAINS TRANSFORMERS

 3 v., 2 amp., 10/6. Postuge and packing on the above $3 / \mathrm{z}$

RADIO AND T.V. COMPONENTS (ACTON) LTD. 23, ACTON HIGH STREET, LONDON, W. 3 GOODS NOT DESPATCHED OUTSIDE UK.. ALL, ENQUIRIES S.A.E. TERMS OF BUSINESS C.W.O


SOUND POWER TELEPHONE UNIT. No batteries required. Fitted with neon indicator lamp and high pitched buzzer, operated by buik-Adraty Rebuilt and self-concained, ex Admeffecive up to half guaranteed working. Effective up to half a mile, waterproof
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PACKARD BELL RELAYS. $12 / 24$ volt, 650 ohms coil, 2 pole changeover, 1.5 amp. contacts.- Brand new. Price 5,6 each. P. \& P. 6d

NEW 10 watt DUAL VOLUME CON. TROL. 25 ohms, plus 25 ohms. 7/5 each. P. \& P. 1/6.
 leads. 27/6 each. P. \& P. 2/-.


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AUTO TRANSFORMERS, step up, step down, 110-200-220-240 v. Fully shrouded. New.
300 watt type $62 / 2 /$ - each. P. \& P. 2/6. SOC watt type $£ 3 / 3 /$ - each. P. \& P. 3/9. 1,000 watt rype $£ 4 / 4 /$ - each P. \& P. 6/6. Also 60 watts, $19 / 6$ each. Plus P. \& P. 2/-


12 v. D.C. AMPLIFIER? as new, for operation on 12 v car battery, 10 watts undistorted output, with 6 L 6 valves in push-pull. Mike/Gram input, tapped output $7 \frac{1}{2}, 15$, 62. 100,250 or 500 ohms. $£ 12 / 10 /$ each. Carr. $15 \%$.


TRUVOX LOUD HAILERS, brand new comolete with transformer and condenser. Impedance $7 \frac{1}{2}$ ohms. Handling capacity 8 watts. Ideal for speech. Price: 18,6 . P. \& P. $3 / 6$ Pair 42/- postage paid.

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Voltmeters
12 v. D.C. M.C. $2 \frac{1}{2} \mathrm{in}$. proj. rnd. 20 V. D.C. M.C. 2 in . fi. sq...... 25 Volt D.C. M.C. 2in. fl. rnd 30 Volt M.I. 3 in . proj. rnd.... 40 Volt M.C. 2in. fI. sq.
250 Vole A.C. rectified moving coil linear scale $3 \frac{1}{2} \mathrm{in}$. f1. rnd. 300 Volt A.C. M.I. $2 \frac{1}{2}$ in. fl. rnd. $22 /$ 400 Volt A.C. M.I. $4 \frac{1}{2}$ in. fl. rnd. $35 /-$ Milliammeters
5 mA . M.C. 2 in. fl. sq............ 12/6 30 mA . M.C. $2 \frac{1}{2}$ in. fl. rnd. ..... $9 / 6$ 30 mA . M.C. $2 \frac{1}{2}$ in. fi. rnd 50 mA . M.C. $2 \mathrm{in} . \mathrm{fl}$. $\$ 9 \ldots$ 500 mA . M.C. $2 \frac{1}{2}$ in. f1. rnd. $0-1 \mathrm{~mA}$ FLUSH MOUNTING PULIEN M C METER $4^{\circ} \times 5^{\circ}$ CORRECTLY CALIBRATED $57 / 6$

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350 mA . 2 in . rnd. plug-in...... $3 / 6$ 500 mA . 2 in . rnd. plug-in POSTAGE ON ALL METERS $1 /$ -


MIDGET ROTARY TRANSFORM ERS. $2 \frac{1}{d}$ in. dia. $\times 4 \frac{1}{2}$ in. Input 11.5 volt. Output $310 / 365$ volts at 30 mA . Brand new. 12/6 each. P. \& P. 1/6.

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ROTARY TRANSFORMERS made by Delco. Input: dual voltage 12 or 24 v . Output: $265^{\text {v. }} 120 \mathrm{~mA} ., 500$ v. 26 mA . Price 27/6 each. P. \& P. $3 / 6$.

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L.F. CHOKE FOR AR88. Fully shrouded, new. 10/6. P. \& P, 2/-


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Beautiful latest finish cabinet in contemporary style. Covered and washable.
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$\star 12$ channels. "Turret Tuned ${ }^{4}$-I.T.A./B.B.C. Extra coils at only $7 / 6$ a pair (with order).
* Chassis. 14 B.V.A. Valves. Salvaged but reconditioned and guaranteed 3 months.


12 MONTHS'
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REPLACEMENT
RE-BUILT
T/V TUBES
All sizes except 10 in . Completely rebuilt gun assembly new cathode, heaters, etc., giving the high standard required for long piecure life, quality and value. Carr. \& Ins. $15 / 6$. OR Yours for $8 / 6$ initial payment (plus carr. \& ins.) and 19 weekly payments of $8 / 6$.

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SUPER CHASSIS 79'6

5 valve superhet chassis including 8 in . P.M. speaker and valves. Four contro! knobs (tone, volume, tuning w/change switch). Four wavebands with position for gram p.u. and extension speaker, A.C. tns. \& carr. $5 / 6$.

## 14" T.V. CHAS§IS <br> TUBE \& SPEAKER

ITGNS
With 14 in . Rectangular Tube. 12 months' guarantee on Tube, 3 months' guarantec on chassis and valves, Chassis with rube and speaker (less valves). II guineas. Complete and working with valves and Turret Tuner. 17 gns . Ins. carr. (incl. Tube) $25 /$-.

## T.V. CHASEIS AT CLEARANCE PRICES

## THE POPULAR 12 in <br> $9 / 6$

A bargain for anyone wanting to make up their own T.V. at a very low cost. A chassis in one unit. Less valves and tube. Chassis size 12 < $14 \frac{1}{2} \times 11 \mathrm{in}$. I.F.s $10.5-14 \mathrm{Mc} /$ 's. Can be adapted for a 12 channel Turret Tuner and modified to take a larger tube. Carr. \& 7ns. 10/6.

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Salvage guaranteed. Standard size two gang. .0003 and .0005 . All Tested and guaranteed. P. \& P. 1/3.

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 $110 \mathrm{v}, 6 \mathrm{v}$. or 12 tor for 200/240 v.Carr. \& Ins. 30/-.

10/- extra) Automatic solder feed including
a 20ft. reel of Ersin $60 / 40$ solder and spare parts. It is a tool for electronic soldering or car wiring. Revolutionary in-design. Instantly raady for use and cannot burn. In light metal case with full instructions for use. Post $3 / 6$.

FAMILY RADIO 99/6
Five valve (octal) superher. A.C. 3 waveband and gram position. 4 controls. Modern attractive cabinet size $15 \frac{1}{4} \times 18 \times 10 \frac{1}{2} \mathrm{in}$. in cream and brown. Carr. \& Ins. 8/6.

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## HOME RADIO

 79/6A.C./D.C. Universal mains 5 valve octal superhet. 3 waveband receiver can be adapted to gram p.u. In attractive wooden cabinet. $9 \frac{1}{4} \times$ $18 \frac{1}{2} \times 11 \frac{3}{4}$ in. Ins. carr. $4 / 6$.

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Six or eight valve latest type midget valve design for A.M or F.M. Brand new. Cadmium plated. Size $12 \frac{1}{4} \times 7 \frac{1}{4} \times 2 \frac{7}{8} \mathrm{in}: ~ P$ \& P. I/ 9 RECTIFIERS $2 / 9$
250 v. $100 \mathrm{m.a}$. Full or half wave. Salvage guaranteed. Why hunt for those obsolete rectifier valves when you can cheaply replace with a modern selenium rectifier. P. \& P. I/3

SOUNDIVISION and I.F. STRIP $7 / 9$ Plessey. I.F.'s $10.5 \mathrm{Mc} / \mathrm{s}$ sound. $14 \mathrm{Mc} / \mathrm{s}$. vision. 8 valve-holders. Less valves. Size $8 \frac{1}{2} \times 5$ : $4 \frac{1}{2} \mathrm{in}$. Circuit incl. The tuner unit plugs directly into this chassis. P. \& P. 2/6.

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75 ft . of in. tape in sealed metal container. Post 9d.
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$7-10 \mathrm{kV}$. R.F. frequency approx. $22 \mathrm{Kc} / \mathrm{s}$. Uses $6 v 6$ or P61 as osc., suitable for Ultra Model V600, W700 and many other sets, or replacing E.H.T. mains transiormers. Idea? when using a larger tube. Size 偻 $^{2} \mathrm{in}$. dia. Base: 4 : $4 \frac{1}{2}$ in. Circu

COLVERN PRESET POTENTIOMETERS Brand new 200 ohms 10 K and 20 K P. \& P. 6d.

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Brand new. 38 mm . Incorporating picture shift control. P. \& P. $1 / 3$.

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Low impedance. 38 mm . Brand new.
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Wide angle $90^{\circ}, 38 \mathrm{~mm}$. Low impedance. P. \& P. $1 / 3$.

13 CHANNEL TURRET TUNER 65/-
Brand new. Well-known manufacturer. $38 \mathrm{Mc} / \mathrm{s}$. Complete with valves. .3 series line up and channel coils, covering channels 1, 2, 3, 4, 5, 8 and 9. Carr. and Ins, 3/6.

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Cut to any length. Good quality, $1 / 6$ postage on 20 yds .
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For all I.T.A. channels. Outdoor or loft. 3 elements. P. \& P. 2/6.

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B.B.C. indoor type. Folded dipole with 12 ft . Co-ax cable fited. Post $1 / 9$.
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Whip antennae. Plated. SOin. long collapsing to llin. One hole fixing. Post $1 /$ -
$\star$ TRANSFORMERS * HEATER
TRANSFORMER . $12 / 9$
12 volt at $\frac{1}{2}$ amp. 0-200-250 olt primary. P. \& P. $1 / 9$.


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2-I Ratio auto transformer 2 volt at 1.4 amp . primary, 4 volt secondary. P. \& P. 1/9.

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Salvage guaranteed. Standard size. 2-5 ohms. Matching pentode or tetrode. O.B. valve Matching ${ }^{\text {P. }}$ P P. $1 / 9$.

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To match our low impedance scanning coils. P. \& P. 1/3.

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Containing scanning coils, line cransformer, etc Less valves. Drawings íree with order
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POWER PACK AND AMPLIFIER $19 / 6$ R.F. E.H.T. Not rested. Amplifier stage. 6 V 6 with O.P. trans. 3 ohms matching. Smoothed H.T. 350 volt at 250 mA ., 6.3 v . at 5 amp.. 22 v . at 3 amp., 6.3 v . at 4 amp . and 4 v . centre tapped. Less valves. Drawings free. Size $14 \frac{1}{2} \times 8 \times 7$ in. Ins., carr. $5 / 6$.

POWER PACK AND AMPLIFIER $12 / 6$ Outpur staze 6 V 6 with O.P. trans. 3 ohms choke. Smoothed H.T. 350 v. at 250 mA . 6.3 v . at $5 \mathrm{amp} ., 22 \mathrm{v}$. at 3 amp ., 6.3 v . at 4 amp ., and 4 v . centre tapped. Less valves. Ins. carr. 5/6.


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UNREPEATABLE VALUE! RECORD PLAYER CABINET R.P.6. 2916
wzant eabinet, cloth covered in grey or red with sunkan control panel and speaker fret. Size $13 \quad 17$, 8 in. deep. Takes a B.S.R. Monarch 4 -speed autochanger. 7. 4 in . elliptical speaker and most of the modern portable amplifiers. Carr. and Ins. $4 / 6$


Smart cabinet. Size $14 \frac{1}{2} \quad 12 \frac{1}{2}$. 6 tin. deep. Various schemes with schemes
white handle and piping. Takes T.U. 9 B.S.R. single player unit, $4 \times 7$ in. elliptical speaker and ampliffer D.I. or D.2. Carr. and ins. 4/6.


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U.A.8. B.S.R. MONARCH 4-SPEED AUTOCHANGER £6.19.6
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COLLARO CONQUEST 4-SPEED AUTO.
CHANGER $66 / 19 / 6$. AUTOCHANGER II GNS.
P. \& P. on the above $5 / 6$.

STEREOPHONIC CABINETS $99 / 6$
Continental style cabinet including extra clip on speaker. $15 \frac{3}{3} \times 10 \frac{3}{3} \times 24 \frac{3}{2} \mathrm{in}$. deep. Takes B.S.R. 4 -speed stereo autochanger. Printed
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12 months' guarantee.
Beautifully made for portable stereophonic record players. Latest design with printed record players. Latest design with printed
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## bakElite cabinets

 Brand new. Colour brown Attractive design. Size $12,7,5 \frac{1}{i n}$. Ideal for small receivers, converters, small receivers, coetc. P. \& P. 3/9.

RP2
6915
A beautifully styled cabinet. Made by a famous manufactu with elipped lid and handle. Carrying $16 \quad 14 \frac{1}{2} \cdots \frac{1}{2}$ in. deep. Will take 4-speed Autochanger 4-speed Autochanger
and 4 in. elliptical and speaker and most of the

modern portable amplifiers. Carr. and Ins. 4/6.

## RP3

6916
A delightful looking cabinet 14i $\because$ : 17\% 8 8in. in 2 -tone $\begin{array}{ll}\text { leatheretre. Will } \\ \text { take a } & \text { B.S.R. }\end{array}$ Monarch A-speed autochanger and $6 \frac{1}{2} \mathrm{in}$. round speaker.
Carr. and lns. 4/6.

## RP4

## 79/6

Stylish cabinet by famous manulacturer. Cloth covered in contrasting colours Grey) (red and grey). Grilled front controls panel. Size

deep. Peautifully
deep. Beautifully made-a cabinet you can be really proud of. Takes 4-speed B.S.R. Autochanger. $6 \frac{1}{2} \mathrm{in}$. round or elliptical speaker. Room for any amplifier of your own choice. Carr. and Ins. 4/6.

## STURDY CASE 12 '6


$8 \frac{1}{2} \times 7 \frac{1}{2} \times 3 \frac{1}{2}$ in. deep. vered in burgundy and grey washable Rexine. Strong clasp. hinges and handle. Ideal for Portable Radio chassis or Transistor
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## PHOTOGRAPHIC SLIDE CASE $17 / 6$

 (List price £2 100 ) Rexine covered. Size $8 \times 127 \times 2$ in in. deep Will hold 150 of those expensive coloured ransparencies in num. ehe answers. This is the answer to thataggravating search for
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B.S.R. FUL-FI CRYSTAL TURNOVER CARTRIDGES 19/6
Brand new. Including sapphire needles for L.P. and Standard, giving fullest range and finest one obtainable for any player. Can be fitted to all standard pick-up arms. P. \& P. 9d.

MOTOR BOARDS $2 / 6$
For 4 -speed Autochangers. P. \& P. $1 / 3$.

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12 MONTHS' GUARANTEE


PORTABLE AMPLIFIER MK D1 59/6

Erand new. Latest design with printed circuit Dimensions $7 \times 2 \frac{2}{4} \times$ Sin. A.C. only. Mains isolated 2-3 watts output. Incorporating EL84 as high gain output valve. Volume and tone conerols.
Knobs $2 / 6$ extra. P. \& P. $3 / 6$.

## PORTABLE AMPLIFIER Mk. D. 27916

 7 Printed circuit batest design. Dimensions output. Incorporating ahe triode pentode undistorted output. Volume and tone controls. Knobs $2 / 6$ extra. P. \& P. $3 / 6$.PORTABLE AMPLIFIER Mk. D. 3 89/6 De Luxe model. Printed circuito. Latest desizn. Dimensions 7. 21 $\times \frac{1}{4} \times \sin$. A.C. only. Mains isolated. $3-4$ warts output. A.C. only. Mains latest ECL82 watts output. Incorporating the giving higher undistorted output. Volume, treble and bass control. Knobs $3 / 6$ extra. P. \& P. $3 / 6$.

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Brand new. By famous manufacturer. Especially built for portable record players. Dimensions $4 \frac{1}{2}$
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valves EL84 as high gain outp valves EL84 as high gain output valve, EZ80 as rectifier. Volume and tone controls. Knobs 2/6 extra. P. \& P. 3/6.
PORTABLE AMPLIFIER Mk. D. 5 39/6 Simple circuit employing ECL80 triode pentode output valve giving $2-3$ watts output. A.C. andy. Mains isolated. Single control for volume and onjoff switch and knob. P. \& P. 3/6.
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 RECORDER CABINETS$19 / 6$

Suitable for the Truvox ing deck. Less

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Type A. Low Leakare windines. Optional Boost $25 \%$
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$2,4,6.3,7.3,10$ and 13 volts. Optional boost $25 \%$ and $2,4,6.3,7.3,10$ and 13 volts. Optional boost
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$\left.\begin{array}{l}0.10 \text { merr. Ditto } 5 \% \text {, } 9 \text { d. } 103 \text { meg., } 10,0,6 d . \\ 10 \text { watt }\end{array}\right\}$ WIRE-WOUND RESISTORS
15 watt $\}$ 25 ohms 10,000 ohms
15,900 ohms $-50,000$ ohms 5 w., 1/9: 10 w. ....... $2 / 3$ WIRE-WOUND POTS, 3 w. Pre-set Min. T.V. Type Al values 25 ohms to 25 K . $31-$ ea., $30 \mathrm{~K} ., 50 \mathrm{~K} ., 41$ Ditto Carbon Track 30 K . WIREWOUND POTS, ${ }^{\text {d }}$ W Standard size pots,
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ALADDTN FORMERS and cores, $3 \mathrm{in}, 8 \mathrm{~d} . \mathrm{zin}, 10 \mathrm{~d}$. and in. sn $\times 1$ in : 2 - complete with cores SLOW MOTION DRIVES. Epicyclic ratio $6: 1,2 / 3$. TYANA. Midget Soldering Iron. $40 \mathrm{w} .16,9$.
REMPLOY INSTRUMENT IRON, $25 \mathrm{w} ., 17 /$
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MAINS DROPPERS. $3 \times 11$. Three Adj. Sliders, 3 cmp MAINS DROPPERS. $3 \times 11 \mathrm{in}$. Three Adj. Sliders, 3 cmp . por foot, 2 way, 6d. perfoot, 3 way, 7d. per foot

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Precision engineered. Size ouly $x$. $\quad$ in
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90 . B7G with cas, $1 / 6 ; B 12 A, 13$. B9A with can, 216 . 90. B7G with can, 116; B12A, 1/3. B9A with can, $2 / 6$.
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WAVECHANGE SWITCHES.
2 p. 2-way, 3 p. 2-way, short sp ndi
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 Wafer $16 /-4$ waler $19 / 6 ; 5$ wate: $8 / 6 ; 2$ walet, 126 wat 6 water 26/6. TOGGLE SWITCHES. S.P., 2/- D.P. 3/G: D.P.D.T., $4 / i^{-}$ MORSE KEXS, good quality, $2 / 6$.
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Cascode circuit using Valve ECC84 17 db gain. Kit $29 / 6$ less power: or 49/5 with power pack kit. Plans only $6 d$.
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Midget size:
Long spindle. GuarayLong spindis. Auspaj-
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5 K F. obms up to 2 M $\%$.
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Linear or Log ${ }^{4,9}$ Tranks. Lineay or log

80 casLe ÚOXXid)
Semainair opaned Polvthen insuated in. dia. Strande ore. Ideal Band In 9 d . FRINGE QUALITY AIRSPACED $1 / \mathrm{hrt}$ EAD SOCKETS LEAD SOCKETS PANEL SOCKETA 1 - OUTLET 6480 or 3008
 TRIMMERS, Ceramie, $30,50,70 \mathrm{pl} .9$ 9d. 100 pl . 150 pt . 1/3. 250, pf., $1 / 6.600$ pl., 750 pf., 19. Phillips, 1 i-. ea ALUMTNIUM CHASSIS. 18 s.w. F. Plain, undrilled
 With;18 $\times 9$ in, $8.6: 14 \times 11$ in., $10 / 6$; $15 \times 14 \mathrm{in}, 12.6$; and $18 \times 16 \times 3$ in., $16{ }^{\prime} 6$.
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NEON MAINS TESTER SCREWDRIVERS, $5 /$ CORED SOI TEP PADIOGRADE
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PAXOLIN SEEET, 8in. $\times 10 \mathrm{in} ., 1 / 6$. ION TRAPS $5 /-$

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"INSTANT" Bulk Tape Eraser and Head Demag-
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SENTERCEL RECTITERS. E.H.T. TYPE FLY BACR
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Dotector, transiormer and heater, ehoke. Circut nad
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 Mullard $3 \cdot 3$ quality Amplifier. Ready built, ev/27/6.
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$1 / 3 \pi 0 \mathrm{v}$.
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FULL WAVE BRIDGE SELENIUM RECT $+200 / 275$ r. $12 / 6$ 19. $\nabla$. 11 anp $8 / 9: 2 \mathrm{a} .11 / 8: 4 \mathrm{a}$. 17/6; f a 2 28 CHARGER TRANSFORMERS. Tampor input 200. 250


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AMERICAN RECEIVER RAS/ARRT Has 6 switched Bands covering 550 $\mathrm{K} / \mathrm{s}-42 \mathrm{Mc} / \mathrm{s}$. Valve line up 4 of 6SK7 2 of 6SA7, I ea. 6H6, 6SQ7, $615,6 B A 7,6 \mathrm{~V} 6 \mathrm{GT}, \mathrm{OD} 3 / \mathrm{VRISO}, 2$ stages of RF \& 2 of IF. Controls include 'S'" Merer, RF Gain, BFO, Audio Gain, Pitch, Automatic Noise Limiter, AVC, Phasing, and Selectivity Control for Xtal or If Adiustment to "Broad-Medium-Sharp." Outpur to Phones, but more than ample for Speaker. Exceedingly fine Vernier Tuning, with directly calibrated dial of tremendous seale length. Also incorporates 24 v Motor for driving unique pre-set Tuning Device. Power Supply required 6 v. \& 250 v. D.C. Size 101 in 73 in. 20 in . BRAND NEW AND UNUSED ONLY $42 / 10 \%$ AND AN AIRBORNE TRANSMITTER RE: CEIVER TYPE 1986. A Mobile 10 Channel Crystal Controlled VHF TX/RX covering $124.4 / 156 \mathrm{Mc} / \mathrm{s}$ IF Bandwidth $23 \mathrm{Kc} / \mathrm{s}$. Complete (less external atrachments) in metal case with all valves and 24 volts Rocary Power Unit Used but in first class Power Unit. Used, but in first class 66/19/6 (carriage 1016) . 0.1 MA DESK METER. Flush Circular 01 mA Meter A 2 ins. in bench in bench stand with sloping panel for Brand New. Fitted with terminals. Brand New and Unused. ONLY 30/(post etc. $2 / 6$ ).

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 TRANSMITTER POWER PACKS. 230 r , A.C. 2 neparate
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 SPEAKER TRANS, small. 6,noo/3, $3 / 8.6$
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## TRADE ENQUIRIES INVITED

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1,500 WHITE SPOT TRANSISTORS. "Manufacturer resh. Per 100, £25
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 TBS. $60-80 \mathrm{me} / \mathrm{s}$. Transceiver $808^{\prime}$ unorlulating $808^{r}$



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To the pnrehaser of each manofacturer matched inal wa glve iree of charge the correct Push-Pull INPUT AND OUTPUT TRANSFORMERS of High Grade con siruction and a complete \& Tratsistor Araplifier circult,
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Easy on the eye, certainly-but these rectangulat faces with their serene black-and-grey styling are more than merely attractive. The scale is the longest practicable, consistent with case size; the calibration divisions are the fewest compatible with the values to be read. As with every other item and component of Elliott instrumentation systems these instruments are designed and built with one aim: absolute functional efficiency.

| Model No. | Movement | Barrel Dia. | Case <br> Size | Scale Length | Amps. | Volts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2705 | Moving Coil | $2{ }^{\prime \prime}$ | $4)^{\prime \prime} \times 3{ }^{\prime \prime}$ | $3.40{ }^{*}$ | $\begin{array}{r} 50 \mu \mathrm{~A} \\ -1000 \mathrm{~A} \end{array}$ | $\begin{aligned} & 50 \mathrm{mV} \text { - } \\ & 1000 \mathrm{~V} \end{aligned}$ |
| 2706 | Moving Iron | $21^{*}$ | 4ズ× ${ }^{\frac{1}{2}}$ | 3.10" | $\begin{aligned} & 15 \mathrm{~mA} \\ & -50 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 10 \mathrm{~V}- \\ & 300 \mathrm{~V} \end{aligned}$ |
| 3705 | Moving Coil | 32* | $5 \frac{10}{} \times 4{ }^{\text {a }}$ | 4.20 * | $\left.\begin{array}{\|c\|} 50 \mu \mathrm{~A} \\ -1000 \mathrm{~A} \end{array} \right\rvert\,$ | $\begin{aligned} & 50 \mathrm{mV}- \\ & 1000 \mathrm{~V} \end{aligned}$ |
| 3706 | Moving Iron | 312 | 52** $\times 41^{*}$ | 3.80" | $\begin{gathered} 15 \mathrm{~mA} \\ -50 \mathrm{~A} \end{gathered}$ | $10 \mathrm{~V}-$ |

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12v, DC MAGNETIC SWITCH Cuts out on 2 amp. overload or dead short. 13/6. P.P. U.S. ARMY SIGNAL GENERATOR TYPE $222-\mathrm{A}$. $8-15$ and $150-230 \mathrm{mc} / \mathrm{s}$. 821 . And Tvpe $72-\mathrm{J} .100 \mathrm{Kc} .32 \mathrm{mc} / \mathrm{s}$. $£ 15 / 10 /-$ P. P These are precision instruments. 12v. DYNAMOTOR POWER PACK. TYPE DM21B: for BC $34250 /$. P.P.
FAMOUS MAKE LIGHTWEIGHT PENGIL BIT SOLDERING IRON, $220 / 240$ Y. 25 w Indicator light in handle (list price 24/6) Price 16/6. P. P
SCOOTER BATTERIES. 6 v i $\sigma$ A.H Hard-rubber case. Size $5 \times 5 \times 1 \mathrm{in}$. Weight NEW AND BOXED COLLARO CONQUES 4-SPEED RECORD AUTO CHANGERS $200 / 250$ v. A.C. $£ 6 / 19 / 6$. Carriage $5 /-$ OUR FAMOUS TRANSFORMERS OUR FAMOUS TRANSFORMERS. Input tapped $5,11,17 \mathrm{v} .5$ a. each. $24 / 6$. ${ }^{2}$ a. P. or . tapped 5, $11,17 \mathrm{~V} . \mathrm{S}^{2}$ a. each. $24 / 6$. P.P.
F.W. METAL RECTIFIERS. $12 / 6$ volt, 1 a., $7 / 6 ; 3$ a., $13 /-; 4$ a., $17 / 6 ; 6$ a., $27 / 6$.
PTUDIO "O"' P/U CARTRIDGES 21/- P.P
FLAT TYPE H.W. RECTIFIERS. $250 \mathrm{v}, 25 \mathrm{~m} /$ 7/6. $60 \mathrm{~m} / \mathrm{a}$. $7 / 6.300 \mathrm{~m} / \mathrm{a}$. 24/- All P.P. Most other types stocked.

All items new and guaranteed RELAYS. We hold large stocks. Any contact combination and operating. coil voltage supplied from 3/-.
KEY SWITCHES from 3/-.
TOGGLE SWITCHES DPDT $3 / 6$.
MIGRO SWITCHES Make and Break 5/6.
6SH7 VALVES ex equipment. All tested of for 10/-. P.P.

LISTS SENT ON REQUEST
Post orders only to
THE
RADIO \& ELECTRICAL MART
27 PRINGES COURT, WEMBLEY, mIDDX

## Regentone

The Regentone Group of Companies offer opportunities to senior and junior engineers and draughtsmen in the laboratories of the manufacturing division.
Applicants should have experience in the fields listed below and be fully acquainted with modern techniques, ${ }^{1}$ ncluding printed circuits.

TELEVISION

RADIO
R.F.|I.F. development, general circuit development, T.V.tuners, wide angle scanning, synchronisịng circuits, etc.
General radio design, production engineering of radio receivers.
DRAWING OFFICE Mechanical development of radio and television apparatus; detail drawing circuit diagrams, printed circuit masters and layouts.

TEST EQUIPMENT Test equipment design and test gear maintenance.
These are permanent and progressive posts and offer excellent opportunities for interesting work and good remuneration in a modern and expanding concern. APPLY IN WRITING, stating age, experience and salary required to TECHNICAL DIRECTOR, Regentone, Eastern Avenue West; Romford, Essex.

## PYE <br> LTD.

## TELEVISION RECEIVER LABORATORY

The following engineers are required to join our T.V. Receiver Design Department in Cambridge:

SENIOR T.V. ENGINEER for work on a variety of absorbing problems associated with the design and production engineering of television receivers for home and export markets and also T.V. relay systems. Applicants should have several years' experience of T.V. receiver design and production techniques.
SENIOR MECHANICAL DESIGNER who is capable of the solution of problems connected with T.V. receiver chassis and cabinet design. The successful applicant will have had several years' experience in this field and be fully conversant with present day mass production techniques.
Please write, quoting "TRX" to the:
CHIEF ENGINEER, PYE LIMITED CAMBRIDGE

## A PRODUCTION ENGINEER

is required by a Company in the West of England to take charge of all aspects of production of a range of electronic and precision mechanical special purpose equipments. This post is of considerable importance and only men with extensive practical experience in this field and possessing real ability and drive will be considered. The successful applicant will be given assistance with housing if required. There are excellent opportunities for further promotion within the Organisation backed by progressive salary scales and a Pension Scheme.
Write, giving concise details of age, education, experience, present position and salary to:

Box No. 3515, cło Wireless World.

## MULLARD SOUTHAMPTON WORKS <br> have a vacancy for an

ELECTRONIC DRAUGHTSMAN
to work on equipment designed for testing of transistors in mass production.
Candidates should be educated to O.N.C. standard and preferably have had experience in the electronic field.

The Company's conditions of employment' will be found to be attractive and the commencing salary paid will be commensurate with experience: Please apply in writing to the
Personnel Officer, Mullard Southampton Works, Millbrook Industrial Estate, Southampton.

## TRANS:STCR CIRCUIT ENGINEER is required by

PYE LIMITED OF CAMBRIDGE
for an interesting position in their radio development laboratory.
Applicants should have several years' experience in receiver design, together with some knowledge of printed circuit techniques; and a recognised qualification (degree, HNC or equivalent) is desirable. Previous experience of semi-conductor devices would be very useful but is not essential. Starting salary would be related to qualifications and experience, and housing assistance may be given in certain cases. Please address applications, quoting "TCE" to the Chief Engineer, Pye Limited, Cambridge.

## COUNTY BOROUGH OF BOLTON EDUCATION DEPARTMENT <br> BOLTON TECHNICAL COLLEGE

## FULL-TIME ELECTRONIC ENGINEERING COURSE

A three-year course in Electronic Engineering is now available. Candidates should be in the age range of 16 to 18, and have taken General Certificate of Education courses which include Mathematics and Physics at the Ordinary and/or Advanced level, or equivalent courses in technical institutions. Suitable candidates may obtain exemption from Parts I and II of the Grad.I.E.E. at the end of the course.

This rapidly developing industry offers new and attractive openings to qualified men, and students who have passed through the course are readily absorbed by industry.

Further particulars may be obtained from the Principal.


If you are between the ages of 25 and 35 years and believe that you have the qualifications and experience to take your place in teams engaged in preparing and firing the first large British -rocket with space potentialities, then write to the Personnel. Manager, de Havilland Propellers Ltd., Wevenage, Herts., quoting reference STM. 27
We are looking for both Senior and Junior Engineers of determination and spirit to fill posts in the following teams at Stevenage, Spadeadarn and Australia.
AUTOPILOT Engineers with a good knowledge of electronics and experienced in auto-pilot and electro hydraulic systems. Experience with semi-conductors would be valuable.
TELEMETRY Electronics Engineers experienced in radio systems. A knowledge of telemetry is desirable.
LINE INSTRUMENTATION Electro mechanical engineers with experience in galvonometers and pen recorders, tape recorders, transducers, etc.
GUIDANCE Electronics Engineers with knowledge of complex electronic systems and computors. Optical experience would be valuable. PROPULSION. Mechanical Engineers with knowledge of liquid propulsion systems and, if possible, rocket engines. Experience in the electrics controlling these systems would be advantageous.

Our Senior Engineers should have either:-
(a) An Engineering Degree
(b) H.N.C. or equivalent
(c) Membership of a recognised engineering institute.

Junior Engineers should have O.N.C. or equivalent qualifications. We are also keen to have ex-servicemen who have the necessary experience but who may perhaps lack the above qualifications. Their applications will be most carefully considered.
We also require:-
SENIOR ENGINEERS for firing procedures and trials planning groups. General electrical and mechanical knowledge is essential and preference will be given to applicants experienced in the G. W. Trials Field. These vacancies are at Stevenage.
SENIOR AND JUNIOR ENGINEERS who have experience in handling and interpreting data from imissile trials. Applicants should possess a general knowledge of electrical and mechanical engineering, or alternatively, should have a meteorological or mathematical background. Vacancies are mainly at Stevenage although a few senior appointments are available in. Australia.
All letters of application are treated in the strictes. confidence and any resultant interviews will be conducted on an informal basis.

## 脑 <br> Telecommunications <br> cambrideg <br>  <br> require <br> TESTERS

a †

## HAVERHILL in SUFFOLK

The Company is engaged in manufacturing a wide range of electronic equipments.
Applicants should have had a minimum of three years' practical experience in industry or have served in H.M. Forces as Wireless/ Radar mechanics:
The Factory is a modern one in a rapidly expanding market town.
HOUSES are available for suitable applicants.
Applications, giving full particulars of past experience, should be made in writing to:-

The Personnel Manager
PYE TELECOMMUNICATIONS LTD. Newmarket Road, Cambridge

## MARCONI INSTRUMENTS LTD.

## Technical Personnel Required

## SENIOR \& JUNIOR ELECTRICAL DESIGN ENGINEERS

## SENIOR \& JUNIOR MECHANICAL DESIGN ENGINEERS

DUTIES: To undertake the design of Test Equipment covering practically the whole electronic field, including Telecommunication, Guided Weapons and Nucleonics. Considerable personal responsibility and freedom is given, and there are no set rules regarding the number of people engaged on a project,
the allocation of project luaders, etc.
QUALIFICATIONS: The ability to design equipment and aggressively progress a project through to the stage where a model is made and the information is available for a production drawing office: Senior engineers are usually of B.Sc. standard with practical experience in measuring techniques, white Junior engineers are often Graduate Members of one of the Professional Institutions, or have similar qualifications, but this is in no way mandatory. The ability to progress the project through to a satisfactory conclusion is the prime requirement. Due to expanding activities, men with drive and initiative can be sure of progressive advancemen!.

Comprehensive pension and assurance schemes are in operation, aand Canteen and Social Club facilitics are provided.
Call any day including Saturday mornings at,
MARCONI INSTRUMENTS LTD: I.ONGACRES, HATFIELD ROAD ST. ALBANS, HERTS.
or write giving full details to Dept, C.P.S., Marconi House, 336/7, Strand, London, W.C.2. quoting refefence WW 2970B.

## ULTRA ELECTRIC LIMITED

Invite applications for the following positions in their modern, well equipped laboratories of the RADIO \& TELEVISION DIVISION.
(1). SENIOR TELEVISION DEVELOPMENT ENGINEERS
for work on:
(a) Wide Angle Scanning
(b) Colour Television
(c) Experimental Receivers-
(d) Combined TV/FM Radio Receivers
(2) TEST EQUIPMENT DEVELOPMENT ENGINEERS
for work on:
(a) VHF/UHF Amplifiers
(b) Video Amplifiers
(c) Pulse Eqưipment and Time Bases
Applicants should have qualifications up to degree standard, and have good basic experience.
These appointments offer scope for original research and development work and for personal advancement
Good salaries, adjudged and commensurate with qualifications, will be offered o suitable applicants A contributory Pensions and FREE Life Assurance Schem: is operated by the Company.
All applications will be regarded as strictly confidential, and should. give full details of present and past positions held, age, and qualifications. In the first instance please write to:
The Personnel Manager, Ultra Electric Ltd., Western Avenue, Acton, London, W.3.

## RADAR, WIRELESS and INSTRUMENT FITTER GIVILIAN INSTRUCTORS

(Male) required by Air Ministry in the provinces. Appointments unestablished, but good prospects of becoming pensionable. Trade training, practical experience and ability to teach are essential. Pay $£ 727$ at age 26 rising to $£ 900$. Apply to Air Ministry, C.E.4k
(CIV 78), London, S.E.1.

## ELECTRONICS RESEARCH LABORATORY STAFF

Senior qualified Electronics Engineers of Degree or Higher National Certificate standard are required for interesting work in connection with a number of projects in the field of Electronics, including the application of transistors to television and similar equipment. Applicants must have suitable academic qualifications and experience in laboratory procedure. They will normally be expected to be able to handle a project from its inception to its final conclusion. Box No. 1952, c/o "Wireless Worid."

# Plessey <br> urgently require Electronic enaineers 

## for

Slage and System Testing of
COMPLEX ELECTRONIG and
ELECTRO-MECHANICAL EQUIPMENTS
Candidates must be fully experienced in handlingnormal test gear (other than for VHF) and have a sound theoretical knowledge of electronics. The situations are permanent and the work is both interesting and varied.
SUCCESSFUL APPLICANTS WILL BE GIVEN EARLIEST PRIORITY FOR HOUSING: NEED NOT START UNTIL HOUSED AND WILL RECEIVE HELP WITH REMOVALS.
Applications from British subjects only, should be made either in writing or in person to:
PERSONNEL OFFICER,
THE PLESSEY CO. LTD., CHENEY MANOR,
SWINDON, WILTS.

ULTRA FLECTRIC LIMITED
Radio and Television Division
The following vacancies now occur in the Development Department:-
(i) SENIOR TELEVISION DE-
(ii) TEST EQUIPMENT DEVELOPMENT ENGINEER
(iii) DRAUGHTSMAN-RADIO AND TELEVISION
(iv) PROCESS ENGINEER

Substantial salaries will be offered to qualified men who must have had experience with leading manufacturers.
Pension Scheme.
Please write fully and in strict confidence to:

The Personnel Manager,
Ultra Electric Limited,
Western Avenuè, Acton, London, W. 3

## TELEVISION <br> RECEIVER ENGINEER for <br> AUSTRALIA

A qualified Senior Engineer with experience in production test and the design of good quality domestic receivers is required for-work in the factory of an Australian associate company near Adelaide.
Preference will be given to an Australian national who wishes to return home. Applications, giving age, education, experience and salary required, should be addressed in the first instance to
THE PERSONNEI. MANAGER,
BUSH RADIO LIMITED,
POWER ROAD, LONDON, W. 4


## mur hy radio limited COMMUNICATIONS EQUIPMENT

A Senior Engineer is required to work on the development of VHF and UHF radio links and other equipment, being responsible for one or two projects Qualifications required are an absolute minimum of HNC and at least 5 years industrial experience, especially in the development of HF, VHF, and UHF Receivers and Transmitters. Transisto experience would be an added advantage. Experience of M.O.S. Work and signers is also necessary. Applications signers is also necessary. Applications Manager (E.93), Murphy Padio Limired Welwyn. Garden City, Herts.

## ELECTRONIC ENGINEERS

Required for development work on test equipment connected with an advanced guided missile project. Applicants should have at least two years experience in similar work and preferably possess H.N.C. in electrical engineering, or equivalent City and Guilds qualification. Applications are invited and should be addressed to:-
The Personnel Manager (Ref. 374), DE HAVILLAND PROPELLERS LIMITED, Hatfield, Herts.

## B : K ELECTRONIC SERVICES

invite applications from ELECTRONIC ENGINEERS for calibration work on MICROWAVE test instrumentation.

Candidates should possess Higher National Certificate in Electronic Engineering, or equivalent. Age limits 23-35. Services experience desirable.

Unusual opening for responsible people in young B. \& K. division with first-class growth probability. Recognition of efforts assured by owner-managed private group. Starting salaries will be determined by level already attained.

Replies in confidence to The Technical Director; B. \& K. Electronic Services, c/o B. \& K. LABORATORIES LTD., Tilney Street, Park Lane, London, W.1.

## RADAR MATERIALS

Ah expanding research establishment situated in pleasant surrounding 3 in South Northants requires:

## PHYSICISTS

CHEMISTS

## RESEARCH ENGINEERS

## TECHNICIANS

to join a group working on the develop. ment and assessment of special materials for both transmission and absorption of microwave radiation.

Investigations are being carried out involving the development of silicone, involving the development of silicone,
polyester, epoxy and other resins, polyester, epoxy and other resins,
natural and synthetic elastomers, and natural and synthetic elastomers, and ferrites and ceramics with unique mag-
netic and dielectric properties over the frequency range $500-50,000 \mathrm{Mc} / \mathrm{s}$.
Candidates are required for, theoretical studies on the propagation of electro-magnetic waves through solid media, and on the physical performanice of suitable materials; for the development of electronic measuring techniques; and for investigations on the processing technology of materials to achieve the required properties.

Recent and prospective graduates, graduates with industrial or universitypostgraduate experience, and versatile technicians are needed. Experience in this particular field is not, however, essential. Starting salaries are based on qualifications and experience, and prospects for advancement lie either in research and development, or in supervising the introduction of projects into pilot and full-scale production. Apply to Box No. 3564, c/o "Wireless World" quoting as reference RADAR/10.

## IBM BRITISH LABORATORIES

IBM World Trade Laboratories (Great. Britain) Limited are engaged in the development of advanced data processing equipment and systems. Plans for the construction of a modern laboratory at North Baddesley, some four miles from the present location, are well under way.

Applications are invited for the following posts:

## GRADUATE MECHANICAL ENGINEERS

A team of Mechanical Engineers, preferably with experience of computing, is being formed to work on (a) advanced methods of packaging of printed wiring circuits and conventional component assemblies; : automatic component assembly techniques and reliable methods of interconnection between units are included in this work, and (b) mechanical and electro-mechanical devices.

## JUNIOR ELECTRONICS ENGINFERS

Required to join a tearm engaged in the development of solid state digital computing circuits. Experience of transistors and/or magnetic cores is desirable and a good degree in electrical or electronic engineering is preferred but those with H.N.C. will be considered.

## DESIGNER DRAUGHTSMEN

Required with two or more years' experience in electronic engineering with emphasis on printed wiring circuits and component packaging. H:N.C. and experience of computer applications preferred.

Attractive salaries will be offered to successful applicants. Pension, Life Insurance and Travel Accident benefits. Applications in strict confidence to the Personnel Manager, IBM World Trade Laboratories (Great Britain) Limited, Hursley Housé, Hursley, rear Winchester, Hampshire.

## UNITED KINGDOM ATOMIC ENERGY RUTHORITY PRODUCTION GROUP <br> INSTRUMENT MECHANICS

Windscale and Calder Works, and Chapelcross Works require experienced men with knowledge of electronic equipment and/or industrial instrumentation for fault diagnosis, repair and calibration of a wide range of instruments used in nuclear reactors, radiation laboratories and chemical plant. This interesting work involves the maintenance of instruments using pulse techniques, wide band low noise amplifiers, pulse amplitude analysers, counting circuits, television, and industrial instruments used for the measurement of pressure, temperature and flow.
Men with Services, Industrial or Commercial background of radar, radio, television, industrial or aircraft instruments are invited to write for further information. Training in our Instrument School will be given to successful applicants.
Married men living beyond daily travelling distance will be eligible for housing. A lodging allowance is payable whilst waiting for housing. Working conditions. and promotion prospects are good.

Appl:cations to:
Works Labour Manager, Windscale and Calder Works, Sellafield, Seascale, Cumberland.
or
Labour Manager, Chapelcross Works, Annan, Dumfriesshire, Scotland.

## UNITED KINGDOM ATOMIC ENERGY AUTHORITY

## INSTRUMENT MECHANICS

The Dounreay Experimental Reactor Establishment requires experienced men with knowledge of electronic equipment and/or industrial instrumentation for fault diagnosis and repair and calibration of a wide range of instruments used in nuclear reactors, radiation laboratories and chemical plant. This interesting work involves the maintenance of instruments using pulse techniques, wide band low noise amplifiers, pulse amplitude analysers, counting circuits, television, and industrial instruments used for measurement of pressure, temperature and flow.

Men with Services, Industrial or Commercial background of radar, radio, television, industrial or aircraft instruments are invited to write for further information Training in our Instrument School will be given to successful applicants.

Married men living beyond daily travelling distances will be eligible for housing. A lodging allowance is payable whilst waiting for housing. Working conditions and promotion prospects are good.

Applications to:
Deputy Works Labour Manager,
Dounreay Experimental Reactors Establishment, Thưrso, Caithness, Scotland.

spffly

## BRENTFORD

 DIVISION
## OPPORTUNITIES FOR ENGINEERS

If you are seeking

1. New, interesting and challenging work
2. Further experience of servo control engineering
3. The stimulation of 'top talent' colleagues
4. A higher salary and better prospects
you may care to consider what we can offer.
Because of our new projects concerned with advanced integrated control and instrument systems for future civil airliners and military aircraft, and new equipment for marine use as well, we are able to offer a few experienced engineers the chance to join the Company at a senior level. Our standards are high, but so are the rewards, and we can offer the assurance that real merit is always recognised.

If you have a degree or equivalent and five years experience in precision electro-mechanical engineering and would like to get to know us better, send concise details of your background and experience to:

The Personnel Manager,
SPERRY GYROSCOPE COMPANY LIMITED, GREAT WEST ROAD, BRENTFORD, MIDDX.

## THE INDEPENDENT TELEVISION AUTHORITY has vaçancies for <br> ENGINEERS

for the operation and maintenance of television transmitters and ancillary equipment. The Authority is in a position to offer appointments with opportunities to suitably qualified young men who have either some experience in this field or who have had a good basic training in radio, radar or television. There would be opportunities for further training and all appointments are pensionable after the initial period of probation has been satisfactorily completed.
Service with the Authority may involve transfers to various locations on the British Isles, but preference for a particular. area will always be considered.
Appointments will be made in the grade of Shift Engineer with a salary scale starting at $£ 725$ with regular annual increments. The starting salary would be determined, to a certain extent, by"qualifications and experience.
Applications giving details of age, academic qualifications and experience, quoting Ref. No. E4 should be addressed to the

Personnel Officer,
62, Brompton Road, London, S.W.3.

## NEWMARKET TRANSISTORS

## Electronic Ėngineer

Required for development of Transistor Production Test Equipment. Previous experience of Electronic Equipment related to High-speed Production Techniques would be of considerable advantage.
Transistor Circuit
Applications Engineer
Required for responsible work in Applications Section, Electronic Engineer (preferably between 25 and 35 years of age) with considerable and wide circuit experience, not necessarily in the transistor field.
Qualifications: at least Higher National Certificate:

## Junior Engineer

Required for Transistor Life Test Section, Junior Electronics Engineer with at least two years' experience.
Qualifications: Ordinary National Certificale.
Drive, with the ability to generate and develop new ideas is essential. Salaries commensurate with qualifications and/or experience.
Write, in confidence, to :
Personnel Officer,
Newmarket Tranisistors Ltd., Exning Rd., Newmarket, Suffolk.

Tel.: Newmarket 3381-4.

## THE GRNERAL RLLCTRIC C0. LTD. <br> APPLIED ELECTRONICS' LABORATORIES THE AIRPORT PORTSMOUTH

The General Electric Company Limited are setting up new laboratories at Portsmouth and design teams will be required to carry out development work on a number of interesting electronic projects. Vacancies exist at all levels for engineers and scientists experienced in the following fields:-
(1) DESIGN OF V.H.F. RECEPTION EQUIPMENT AND I.F. AMPLIFIER DESIGN.
(2) MICROWAVE DESIGN AND DEVELOPMENT.
(3) GENERAL PULSE CIRCUITRY USING BOTH VALVE AND TRANSISTOR TECHNIQUES.
(4) ELECTRO-MECHANICAL AND SERVO SYSTEMS.
(5) MECHANICAL DESIGNERS.

Engineering staff will be required to have a degree in physics, electrical or mechanical engineering, or corporate membership of an engineering institution, or exemption from the examination for such membership, and about three years expericnce in a relevant field.
VACANCIES ALSO EXIST FOR EXPERIMENTAL STAFF AND DRAUGHTSMEN.
Apply in the first instance to the Personnel Officer, The General Electric Co. Ltd., Brown's Lane, Allesley, Coventry.

## EKCO ELECTRONICS LIMITED

RADAR DEVELOPMENT AND ENGINEERING DEPARTMENT vacancies for

## DEVELOPMENT ENGINEERS

Ekco Electronics Ltd. is a leading company in both military and commercial applications of airborne radar equipment: Interesting new projects necessitate expansion of the design resources, and vacancies exist for qualified and experienced engineers with interests in the following fields:
Microwave components, aerial systems, etc.
Pulse and servo circuit techniques. Heat transfer problems.
Installation and trials.
Certain of these posts are of Senior Engineer status, and will carry considerable responsibility.

[^20]
## Applications ta:

PERSONNEL MANIAGER, E. K. COLEE LTD., MALMESBURY, WILTS.

## EIECTRONIC COMPUTERS FERRANTI LTD. MANCHESTER has vacancies for TEST ENGINEERS

for the desigh and operation of specialised equipment used in the production of Electronic Computers. A good theoretical; as well as practical knowledge of pulse and steady state circuitry is required and some experience with transistors would be advantageous.

These appointments will afford young men, with the appropriate knowledge and experience, an excellent opportunity for advancement in the field of electronic computing equipment.

Forms of application can be obtained from T. J. Lunt, Staff Manager, Ferranti Ltd., Hollinwood, Lancs.
Please quote reference KL. 3.

## DIGITAL DATA PROCESSING

The SHAPE Air Defence Technical Center has a few vacancies in the field of high-speed digital data-processing.

Applications are invited from suitably qualified persons with interest in one or more of the following fields:

Digital computation.
High-speed analog-digital conversion.
Computer input and output devices.
Transistor and magnetic-core techniques, applied to computers.
Cathode-ray tube displays.
The basic salaries will be based on the European average for corresponding background and experience. Successful applicants from foreign countries will benefit by a number of privileges including a foreign allowance of the order of $70 \%$ of the basic salary, and reimbursement of the cost of moving their families and household effects to The Hague and back to their country of origin on termination of contract. The total income is tax free in the Netherlands.

Applications, containing detailed information on training and past experience, should be sent as soon as possible to:

The Director, SADTC, P.O. Box 174
The Hague, Netherlands

## FERRANTI LTD. MANCHESTER

has vacancies in the

## SUPERVISING ENGINEERS

for post installation service to Ferranti Computers in this country and abroad. Applicants should have technical knowledge up to. H.N.C. standard or equivalent. Favourable consideration will be given to applicants who have a good back ground of training and experience on Service electronic and radar equipment. Successful applicants will have the opportunity, if they so desire, to be considered for periods of service in this capacity on Ferranti Computers installed in many countries abroad.
The above appointments will carry salaries fully commensurate with qualifications and experience. The Company operates a Staff Pension Scheme and an Instalment Assurance Scheme.

Applicatión is by form obtainable from:
T. J. Lunt, Staff Manager, FERRANTI LTD., HOLLINWOOD, LANCs.

Please quote ref.: KLS.

## RESEARCH LABORATORY

## AEI

Sol id-S'ate Physics Section require an assistant
with experience in the growth and examination of semiconductor crystals. Initiative and the ability to develop apparatus and techniques are looked for, together with qualification at least to O.N.C. level.

The Laboratory serves a large group of Companies and is situated in pleasant rural ${ }^{7}$ șurroundings ${ }^{\text {a }}$ near- Reading with fast train' service to London.

5-day Week.
Pension Scheme
Apply in writing, quoting reference No. SS/A/12, to the Persanne! Officer,

Research Laboratory,
ASSOCIATED ELECTRICAL INDUSTRIES LIMITED
Aldermaston Court,
Aldermaston, Berkshire.

## WIRED TELEVISION

An opportunity exists in a rapidly expanding industry for an Engineer, who will test and advise on the performance of wired T.V. distribution systems throughout England and Wales. A sound knowledge of T.V. principles is required. Apply to:-

Head of Wire T.V. Dept.,
Central Rediffusion Services Lid.,
Stratton House, Stratton St., W.i.

## VACANCIES IN GOVERNMENT SERVICE

A number of male vacancies offering good career prospects, exist for:-

RADIO OPERATORS
Write, giving details of Education, Qualifications and Experience to :-

Personnel Officer, G.C.H.Q. (3/R)
53, Ciarence Street, Cheltenham

## QUARTZ CRYSTAL ENGINEERS

A limited number of permanent staff vacancies are now available to persons
having experience with Quartz Crystal or having experience with Quartz Crystal or
the associated Piezo-electric devices. Additionally, there is a vacancy for a capable Electronic and Mechanical Maincapable Electronic and Mechanicauronent for small component manufacture.

The posts are most suitable for those possessing drive and initiative and are in new air conditioned laboratories providing up-to-date equipment. For further information write:-

PERSONNEL MANAGER,
CATHODEON CRYSTALS 'LIMITED, LINTON, CAMBRIDGE.

## MIDDLESEX EDUCATION COMMITTEE

SOUTHALL TECHNIGAL COLLEGE
DEPARTMENT OF ELECTRICAL ENGINEERING
The next entry to the full-time course in Electrical Engineering. and ,Applied Electronics will take place in September. Evening courses, commencing on 28th September, will also be held on Advanced Mathematics, Analogue Computers, Digital Computers; Transistors, ServoMechanisms, Pulse Techniques, Industrial Eléctronics, Radio Telemetry, Practical Numerical Analysis and Automatic Process Control. Details from the Principal, Technical College, Beaconsfield Road, Southall, Middlesex.

## SENIOR ELECTRONIC TEST ENGINEERS

A leading firm of electrical manufacturers requires staff for its Test Department. For this interesting work, which is in the Midlands, electronic engineers, with thorough experience in the telecommunications field, prererably with Higher National Certificates or City and Guilds Certificates in Telecommunications, but in any case with an understanding of complicated valve and transistor circitry and an ability to use delicate electronic test gear should apply giving full details of age, education and experiance to Box No. $4058 \mathrm{c} / \mathrm{o}^{\text {"c }} \mathrm{W}$. W. ."
The positions available involve a $39!\mathrm{hr}$. 5 day week and starting salaries are for Senior Test Engincers from $£ 875$ to $£ 1,025$ and for Test Engineers $£ 775$ to $£ 850$.

## EleCTRONLC ENGINEERS

Experienced Engineers, who have reached H.N.C. standards, are invited to apply for H.N.C. standards, are invited to apply for
positions where energy, skill and initiative positions where energy
will be well rewarded.
The work relates to the development of television components for large scale production. Previous experience in the design of tuners and/or scanning components is essential.

The positions are permanent and offer scope for further advancement. The commencing salary will be in accordance with previous experience based on a with previous experience based on a
generous and progressive scale. London gene.
area.
Please reply, in confidence, giving, full particulars to Box No. 4059 c/o "W.W."

BOURNEMOUTH MUNICIPAL COLLEGE OF TECHNOLOGY AND COMMERCE
Full-time and Part-time Courses for the INSTITUTION OF ELECTRICAL ENGINEERS PART III EXAMINATIONS
are dus to commence in September 1959. Details and application forms may be cbtained from the Priwejpal, Conumerce, Latusdowpe, Bournerpouth. Early application is adriamble

## COUNTY BOROUGH .OF GRIMSBY

Education Committee

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[^0]:    "Stereo in one Box" is more common than last year. Usually, if desired, one or more extension speakers can be connected so as to extend the overall sound field beyond the cabinet. In the E.A.R. Model 500 single-cabinet reproducer the speaker compartments can be spaced up to 5 feet apart or, if greater separation is required, detached altogether from the main cabinet.

[^1]:    ڤ See " Learning Machines," Wireless World, January, 1959, issue. $\dagger$ "Superconductivity," Wircless World, July, 1957.

[^2]:    $\ddagger$ For explanation see "Mavars," Wireloss World, May, 1959.
    ** See, for example, British Parent 778,883 (1954).

[^3]:    $\star$ Queen Mary College, London University.

[^4]:    "Unit System" has been adopted by Kelvin-Hughes for their new range of marine radars. Standard scanner and transmitter receiver are combined with alternative displays, power supplies and motor-generators to form range of radors to suit most requirements. Photograph shows largest display unit (Type 14/16P) which uses 16 -in c.r.t. and provides reflection-plotter and true-motion focilities.

[^5]:    Alcatrons shown by the French C.S.F. are experimental field-effect majority-carrier devices similar to the Tecnetron in consisting of a piece of n-type semiconductor material with a very narrow (about 10 microns wide) constriction in it. The supply voltage is applied between two terminals referred to as

[^6]:    * E.g., March, 1958 issue, p. 115

[^7]:    * PTFE (Polytetrafluoroethylene)-the basic polymer is manufactured in this country by I.C.I. Led., under the trade name "FLUON".

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    23 digit counter.
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    4 Dual channel tuned amplifier.
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    83 digit batching counter.
    9 Special purpose time measuring set.
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    11 Reaction time indicator.

[^11]:    DENMARK Tage Schouboe, Copenhagen $N$ FINLAND Oy Scienta Ab, Helsinki new zealand Imarex Lid, Anckland C3 norway Birger Christensen. Oslo

[^12]:    SWEDEN Elektronlund AB, Malmo C Switzerland Walter Bliam, Zurich 2/39 U.S.A. Bud Radio Inc, Cleveland 3, Ohio grit. gulana British Caribbean Agencies Lid Georgetown Demerara

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