# Wireless World 

## RLECTROVICS <br> Radio . Television



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ELECTRONICS, RADIO, TELEVISION

## MAY 1959

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## Transistor

## Transmitter for $500 \mathrm{kc} / \mathrm{s}$

The recently introduced Mullard OC24 power transistor is suitable for high-frequency applications and it can dissipate several watts at the collector. The combination of these qualities has made possible the design of a $500 \mathrm{kc} / \mathrm{s}$ push-pull amplifier capable of delivering an output of 4 watts into a resistive load. This amplifier can be used as the output stage of a transmitter such as that shown in the accompanying circuit.

The transmitter was designed for operation in the International Marine Frequency Band. It is particularly useful for lifeboats and life rafts, but it can be adapted, using an automatic-keying system, for life-jackets, air-sea rescue equipment, helicopters and radio beacons for coastal stations. The long life and reliability of the transistors make them particularly suitable for the type of apparatus suggested above, in which standby conditions of long duration are experienced. The low-consumption, light weight and compactness add to these advantages. A 4 ampere-hour accumulator will power the transmitter for some 60 hours. For emergency applications a self priming battery, which requires no attention (other than charging and sealing) until it is needed for use, is suitable.
The transmitter comprises an oscillator, a modulator, a driver and a power amplifier stage. The oscillator is crystal controlled and uses an OC45 transistor. The resonant circuit in the collector line is tuned to the series-resonant frequency of the crystal. The crystal is connected in series with the feedback winding to control the frequency of oscillation.
The modulator is a silicon transistor ( OC 201 ) also recently announced. The output from the modulator is applied to a driver amplifier and then to a push-pull power amplifier which feeds an aerial. The modulator, driver and power-amplifier stages are all operated under Class B conditions.
The design of the Class B push-pull amplifier follows the same basic technique as that for an audio amplifier except that, as the collector circuit is tuned, no bias is required to eliminate cross-over distortion. The use of a shared emitter resistor reduces the effect of variations in base-emitter voltage $\mathrm{V}_{\mathrm{b}_{\mathrm{e}}}$, and reduces the lengthening, caused by hole storage, of the collectorcurrent pulse. This reduction of the hole-storage curent gives a marked improvement in the efficiency of the amplifier. The winding details for the output transformer are shown on the circuit.

The design procedure for the driver and modulator stages is similar to that for the output stage. A 6 V supply is used for the modulator because of the voltage limitations of the oscillator transistor. This supply is also used because it is convenient for the modulator, and because of the keying system adopted.

A crystal-controlled oscillator with a tuned collector is used. Feedback is obtained by a transformer
coupling from the parallel-tuned circuit in the collector circuit, to the base. The crystal is connected in series with this feedback winding. The collector circuit is tuned to the series-resonant frequency of the crystal. The series resistance of the crystal is low enough for the feedback current to start oscillation. The oscillator operates under Class A conditions, the base bias is provided by a potentiometer (R1R2). The emitter resistor is bypassed to r.f. signals.

It is hoped to publish details of the modulation arrangements and the automatic keying system (transmitting SOS signals) at a later date.

The tuning procedure adopted is the usual one of rough tuning at reduced power, followed by adjustment at full power. A resistor of $27 \Omega$ is connected in the emitter lead of the modulator amplifier Tr 2 , the 12 V supply is then connected to the transmitter, and the oscillator tuned-circuit is adjusted to the series-resonant frequency of the crystal. The modulator amplifier is tuned next. The driver and poweramplifier stages should then be tuned for a maximum power output (about 2 watts) across the $68 \Omega$ load.
The emitter resistor of Tr 2 should then be short-circuited. The complete transmitter, from the oscillator to the power amplifier, should be progressively readjusted. Careful tuning of the power amplifier is necessary, because excessive collector current flows if the stage is off tune. The full output of 4 watts should now be obtained.
An experimental transmitter was built and the performance tested over a temperature range from 0 to $60^{\circ} \mathrm{C}$. The output falls gradually at temperatures above $25^{\circ} \mathrm{C}$, although quite reasonable output is still available at $60^{\circ} \mathrm{C}$. Field tests were carried out under licence using a $520 \mathrm{kc} / \mathrm{s}$ crystal, the transmitter being retuned to this frequency. A transmitting aerial 30 ft high and a receiving aerial of about 30 ft of wire were used. Strong signals were received within 12 miles across land. This is not the maximum range over land, and a range of at least 50 miles can be expected at sea.

Oscilfator Transformer TI

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$$

$$
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& n_{2} 52 \text { turns? conductors }
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n_{4} & 6 \text { turns } \\
\text { conductors }
\end{array}
$$

$$
n_{4} 6 \text { turns }
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$$
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\end{aligned}
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\text { pot-core assembly LA } 35
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Output Transformerta $n_{1} 2+2$ turns $\} 2 l$ swg enamelled $\mathrm{n}_{2} 4$ turns copper 19/0028 bunched conductors Ferroxcube pot-core
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## Making and Selling Valves

IT has been rightly said that valves and cathode ray tubes are at the heart of our affairs, and although in this journal we are concerned primarily with the technical aspects of their use, we cannot always stand aloof from the manner of their supply and marketing. Commercial considerations will always be an important factor in setting the pace of development in an industry where capital costs are high.

British valve manufacturers and their Association, the BVA, have never lacked critics of their marketing methods, and these critics have not concealed their satisfaction in the abandonment by the BVA of price-fixing agreements in 1956 just prior to the publication of the "Report on the Supply of Electronic Valves and Cathode Ray Tubes of the Monopolies and Restrictive Practices Commission,"* and again last month in the decision of the BVA not to offer evidence at the Restrictive Practices Court hearing in support of a continuation of agreements on "exclusivity" and maximum discounts or of the practice of limiting the number of wholesalers handling BVA valves.

The Restrictive Trade Practices Act, 1956, which requires registration of certain types of agreements and restrictions, is in many ways a new form of legislation-at least in this country. It has established a Court and a Registrar who may bring before the Court any association whose agreements are deemed to be contrary to public interest. The onus then rests on that association of proving to the satisfaction of the Court that the practices in question are, in fact, in the public interest.

What is "the public interest"? In wartime it was the restriction of the supply of valves to the public to a mere trickle. To the man in the street today it could mean the reduction of prices to the absolute minimum-if necessary by cut-throat competition, which would divert the whole of the manufacturer's resources to the cheaper production of existing types. To others it might mean an increase in prices so that more money could be applied to the discovery of entirely new valve techniques to keep this country in the lead and to improve the balance of trade. The Act enunciates no fewer than seven criteria by which the public interest is to be assessed. These are of a highly complex nature and must involve lengthy stage-by-stage legal argument before it can be decided whether an agreement may stand-or must be abandoned.

[^1]In the case of the BVA many of its trading agreements have their origin in the early days of broadcasting when the dumping of foreign valves was a serious menace to an industry which had not yet built up adequate capital resources. Today they are in a much stronger position. Set manufacturers and servicemen in general prefer to use BVA valves; in 1955, according to the Report mentioned earlier, imported valves not sold through BVA channels were estimated to amount to $5 \%$ of the total supply. Faced with the alternatives of fighting for the maintenance of the old-established collective agreements or standing on their own feet, the member firms of the BVA have, we think wisely, decided to take the latter course. The decision is unlikely to influence the prices of valves and tubes which have for a long time been determined by far more fundamental factors than trade agreements. The industry has already declared its profits and opened its books for analysis by the Monopolies and Restrictive Practices Commission and the results are set out in great detail in their 1956 Report. It should be compulsory reading for all would-be critics-in particular those who complain that set makers get valves for 2 s 6 d each which cost the best part of $£ 1$ to buy in the shops. This comparison overlooks the fact that the cheaper valves will be subject, as part of a set, to distributive costs which are of the same order as those which apply to a maintenance valve. It is true that valve manufacturers charge on an average $10 \%$ more to a wholesaler than they do to a set maker, but this is accounted for by the smaller bulk of supplies, the cost of special packaging and by the fact that short production runs of replacement valves for maintenance are often very expensive. Again on average, the valve manufacturer's profit on cost to the set maker in 1954 was about $18 \%$ and to the wholesaler $28 \%$. If this difference were levelled, television sets might cost anything up to $£ 10$ more to the customer. It is clearly in the consumer's interest that the sixteen odd valves he must buy in the set cost him less per valve than the two maintenance valves that, on a statistical, basis, he may have to buy during the life of the set. (The ratio of "first-equipment" to maintenance valves sold is about $8: 1$.)

In spite of the fact that the valve makers have had difficulty in finding proof of specific and substantial public benefit from some of their past trading restrictions, we think that valve users, both professional and domestic, are well served by what is undoubtedly an efficient and well-managed industry.

## Fifth International Instrument Show

HELD for the first time at the International Instrumentation Centre, London, this year's international instrument exhibition was a little smaller than last year's, and many of the exhibits had been seen before, in at least prototype form. Nevertheless, since most of the larger instrument shows are restricted to British exhibitors, this one offers a welcome opportunity for comparing foreign developments, and there are always some interesting novelties.

## Data Recorders

One of these is the PS. 200 tape data recorder by Precision Instrument Co. (U.S.A.). This uses 1 -in magnetic tape, carrying 14 tracks. Two pairs of 2:1 tape speeds, selected from the range of $1 \frac{7}{8}, 3 \frac{3}{4}, 7 \frac{1}{2}, 15$, 30 , and $60 \mathrm{in} / \mathrm{sec}$, are available by motor-pole switching and drive-belt change. Four varieties of recording are available: direct; f.m. (using a kc/s carrier-frequency equal to nine-tenths tape speed in in/sec); pulse-width


Type PS200 tape data recorder, showing tape magazine being changed and (left) one of the printed circuit panels. (Precision Instrument Co.)


Type TF823 variable multi-octave-band filter (Peekel)

## EXHIBITS BY FIFTY-SIX FIRMS

## OF TEN NATIONALITIES

modulation; digital. One of the most interesting features is that tapes are mounted in rectangular magazines which can be changed in a few seconds by a plug-in arrangement whereby the tape is self-threading. The whole of the gate is visible all the time through a window. Another feature is that the weight of the equipment has been reduced from nearly half a ton to 65 lbs by the use of transistors and printed circuits, making the equipment fully portable for field use. It will, incidentally, run off 24 -volt d.c. as well as the usual a.c. Control is by push tabs, which are back-lighted to show clearly the state of operation.

An altogether different type of data recorder is one that was shown by Elema-Schonander (Sweden), in which a jet of ink is squirted at a moving paper strip from the centre of a galvanometer movement which deflects the jet. Instead of the mess which this procedure might be expected to create, beautifully fine traces are produced, thanks to the extreme fineness of the jet; and when several channels are in use the traces can cross and recross without mutual interference. It is remarkable, too, for an ink-and-paper instrument, that frequencies can be recorded up to $1,000 \mathrm{c} / \mathrm{s}$, with sensitivity as high as $0.2 \mathrm{~mm} / \mathrm{mV}$.
Yet another interesting recording technique appears in the Hughes Aircraft (U.S.A.) "Memotron" c.r. tube -a 5-in tube in which traces applied in the conventional manner are not only displayed but retained on the screen until erased. This result is achieved by means of a

dielectric storage mesh and two electron guns: a writing gun and a flood gun. This type of tube is incorporated in a complete c.r.o.-the " Memoscope."
For audio workers, the Peekel (Holland) TF. 823 variable multi-octave band filter is a particularly interesting and useful instrument. It consists of a low-pass filter, a high pass filter, and six intervening octave filters, covering between them roughly $30 \mathrm{c} / \mathrm{s}$ to $16 \mathrm{kc} / \mathrm{s}$. Each filter can be individually adjusted by a vertical sliding linear attenuator with a dB scale, so that an infinite variety of frequency characteristics can be set up, for such purposes as equalization, intelligibility and distortion studies, and bridge measurements. The attenuator scales being arranged across the front panel, their settings trace a visual frequency curve. With all the attenuators at zero, the insertion loss is nil. Input and output impedances; $200 \Omega$.

The portable sound spectrum meter by the same firm, mentioned last year, now appears in improvec form.

Much of the very extensive Brüel \& Kjaer (Denmark) range of instruments is for a.f. work, and a notable newcomer is their Type 4131 capacitive microphone. It is a precision instrument for sound measurements as well as for high-quality studio use. The free-field response is practically flat from $20 \mathrm{c} / \mathrm{s}$ to $18 \mathrm{kc} / \mathrm{s}$, and the sensitivity is $5 \mathrm{mV} /$ microbar. Combined with it is a cathode follower, and a full range of accessory equipment is available.
The most interesting feature of the new $\mathbf{B} \& \mathrm{~K}$ valve voltmeter-which is of the high-sensitivity amplifier type, covering $2 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}$ and 1 mV to $1,000 \mathrm{~V}$-is the arrangement for enabling peak, average, and true r.m.s. values to be measured. The r.m.s. facility is provided by a network as shown in the circuit diagram, approximating closely to a parabolic character*.

The same firm showed a series of deviation bridges for production-line use in component manufacture. A special knee-operated test connector release speeds operation, and the scales are marked in percentage deviation from standard in impedance and phase-angle. Bridges are available for test frequencies of $100 \mathrm{c} / \mathrm{s}, 1 \mathrm{kc} / \mathrm{s}, 10$ $\mathrm{kc} / \mathrm{s}$, and $1,000 \mathrm{kc} / \mathrm{s}$.

## pH Meters

Except in so far as they excmplify extra-high-inputimpedance voltmeter techniques, pH meters hardly come within the scope of Wireless World, but the Seibold (Austria) Model GV-52 is a striking illustration of how what used to be a delicate and non-portable assemblage of laboratory apparatus requiring skilled handling can now be obtained as a single smooth functional unit which is operated simply by dipping one end in the liquid to be

[^2]tested, pressing a button and reading the meter at the other end.

A notable feature of the exhibition as a whole was the increasing use of transistors and other semiconductor devices. Its advantage in the "Precision" tape recorder has already been noted. H. Struers (Denmark), whose unusual types of regulated power supply units were


Square-law (parabolic) network for r.m.s. measurements used in the new B \& K valve voltmeter Type 2409.

Type SL7626 microwave search frequency meter (Sivers).

Deviation bridge with kneeoperated connector release for component testing. (Brüel \& Kjaer.)

mentioned two years ago, have taken advantage of the high current ratings of transistors to design a unit ("Transistavolt") supplying $0-\epsilon \mathrm{A}$ at a voltage adjustable from 5.6 to 6.3 V . The internal resistance is less than 5 ml , the ripply voltage 1 mV , and mains fluctuations from $-15 \%$ to $+10 \%$ affect the output voltage less than $0.02 \%$.

Several transistorized power units are supplied by Valor Instruments (U.S.A.), who have also a transistor checker which must be invaluable wherever many transistors are used. It locates burnt-out transistors, identifies type ( $\mathrm{p}-\mathrm{n}-\mathrm{p}$ or $\mathrm{n}-\mathrm{p}-\mathrm{n}$ ), measures leakage current, checks voltage breakdown, identifies terminals, and checks characteristics and electrodes shorts and open-circuits.

Microwave equipment figured largely, and Polarad Electronics (U.S.A.) have again upheld their reputation for spectrum analysis equipment. Model SA. 84 covers the remarkable frequency range 10 to $44,000 \mathrm{Mc} / \mathrm{s}$ in eight bands. There is only a single tuning control, with direct-reading linear dial. The frequency deviation is adjustable from 0.5 to $5 \mathrm{Mc} / \mathrm{s}$.

Sivers (Sweden) again showed a very wide range of microwave cavity wavemeters, waveguide joints and switches, etc., to which they have now added Type SL. 7626 search frequency meter-a compact and handy instrument for measuring oscillator frequencies over the wide band 1 to $10 \mathrm{kMc} / \mathrm{s}$. Two signals can be separately measured on linear vernier scales, and inaccuracy as low as 0.2 to $0.5 \%$ is claimed.

# WORLID OF WIRELESS 

## Budget Changes

THE exemption of cathode-ray tubes (both new and rebuilt) from purchase tax, previously standing at $60 \%$, is welcomed as it removes an anomaly and is a first step in bringing the radio industry into line with others where there is no P.T. on spares. In announcing this concession the Chancellor of the Exchequer stated "this tax has been represented to me as being unduly burdensome, and technical developments in the reconditioning of tubes have made it difficult to administer the tax with equity".

To ensure that this concession "does not give an opportunity for tax avoidance on sets themselves", the Treasury has made an order stating that "television receiving sets of the domestic, portable, or road vehicle types and apparatus of the domestic type designed for receiving television programmes re-transmitted by wire, except kits of parts . . . (whether or not in a cabinet) which are complete or substantially complete except that they lack a cathoderay tube... are to be treated for tax purposes as if a cathode-ray tube formed part of the receiver, and the value of a new tube of appropriate size and character is to be included in the full value of the receiver, upon which tax is charged."
With the general reduction of purchase tax by a sixth (except in the $5 \%$ rate), the tax on television sets, sound receivers, radio-gramophones, record players and reproducers, record changers, turntables, pickups, valves, r.f. tuners, gramophone records, etc., is reduced to $50 \%$.

## Radio in Space Research

AT the first meeting of the newly-formed National Committee on Space Research a report on the U.K. observations of artificial earth satellites by radio and optical methods was presented by the I.G.Y. Artificial Satellite Sub-committee. The report was an outline of work in progress, covering the types of observations and giving details of the twelve U.K. radio observing stations (and other organizations) and their facilities. Several prominent people well known in the radio world are members of the National Committee on Space Research, including Dr. R. C. Cockburn, Professor A. C. B. Lovell, Dr. J. S. McPetrie, J. A. Ratcliffe and Dr. R. L. Smith-Rose.

[^3]
## Mobile Radio

THE Third Report of the Mobile Radio Committee ${ }^{\star}$ to the Postmaster General proposes the introduction of $25-\mathrm{kc} / \mathrm{s}$ carrier separation, instead of $50-\mathrm{kc} / \mathrm{s}$, in the land-mobile "low" band ( 71.5 to $88 \mathrm{Mc} / \mathrm{s}$ ). It will be recalled that its Second Report covered the reduction of channel spacing in the "high" band $(165$ to $173 \mathrm{Mc} / \mathrm{s}$ ) from 100 to $50-\mathrm{kc} / \mathrm{s}$. This recommendation is in the process of being implemented.

The present report has been adopted by the P.M.G. and the new channel spacing comes into force on June lst. Five years is being allowed for the changeover to $25-\mathrm{kc} / \mathrm{s}$ equipment by present users. After June 1st all new land-mobile schemes in the low band will have to use equipment meeting the $25-\mathrm{kc} / \mathrm{s}$ specification. The report includes a revised allocation of channels amongst the various categories of users.
R.E.C.M.F.-At the annual general meeting of the Radio and Electronic Component Manufacturers' Federation in March, Major L. H. Peter (Westinghouse) handed over the presidency to E. M. Lee (Belling \& Lee). The new vice-presidents are K. G. Smith (N.S.F.) and A. F. Bulgin (Bulgin \& Co.). The new council consists of the representatives of the following member firms: Bakelite (G. J. Taylor); Belling \& Lee (N. Dundas Bryce); Garrard (H. V. Slade); A. H. Hunt (S. H. Brewell); Multicore (Richard Arbib); Painton (C. M. Benham); Plessey (P. D. Canning); Reliance Cords and Cables (C. H. Davis); Salter \& Co. (C. Ottewell); S.T.C. (L. T. Hinton); T.C.M. Co. (Dr. G. A. V. Sowter) and Texas Instruments (Dudley Hayward). This year's chairman and vice-chairman are Hector V . Slade and Dr. G. A. V. Sowter, respectively.
B.R.E.M.A. Audio Group.-At the first general meeting of the recently formed Audio Manufacturers' Group of the British Radio Equipment Manufacturers' Association, Major J. F. E. Clarke, chairman and managing director of Clarke \& Smith Manufacturing Co., was elected chairman of the Group. The companies elected to the management body were : B.T.H. Sound Equipment; Clarke \& Smith Manufacturing Co.; E. K. Cole; Dynatron Radio; Electric Audio Reproducers; E.M.I. Sales \& Service; Grampian Reproducers; Jason Motor \& Electronic Co.; Lowther Manufacturing Co.; and Trix Electrical Co.
VHF/UHF Convention.-The fifth international amateur v.h.f./u.h.f. convention organized by the R.S.G.B. and the London U.H.F. Group will be held at the Prince of Wales Hotel, De Vere Gardens, London, W. 8 , on May 30th. The morning session will be devoted to informal discussions and the afternoon to lectures. Tickets for the convention and dinner, costing 22 s 6 d , are obtainable from F. G. Lambeth, 21 Bridge Way, Whitton, Twickenham, Middx.

Ghana is to have a television station operating in time for the visit of H.M. The Queen in November. The station, which will be in Accra, the capital, and will operate on the $625-$-ine $7-\mathrm{Mc} / \mathrm{s}$ standard, is being provided jointly by Marconi's and Pye. A large number of television receivers is to be installed in community centres, hospitals and public places.

* H.M.S.O. 1s 3d.

Careers.-A number of organizations in the field of radio and electronics are participating in the careers section of the forthcoming National Education and Careers Exhibition. Organzed by the National Union of Teachers, it will be held at Olympia from May 26th to June 5th.

Hospital Equipment.-Radio and electronics manufacturers are among the 150 exhibitors at the International Hospital Equipment and Medical Services Exhibition, which is being held at Olympia from May 25th to 30 th. The exhibition, which is sponsored by the Institute of Hospital Administrators, is open to the public from 1.0 to 6.30 . Admission costs 2 s 6 d .
A.P.A.E. News.-Although the Association of Public Address Engineers has not held an exhibition for several years, the committee has met regularly to further the interests of its manufacturer and user members. This year's annual meeting and luncheon at the King's Head Hotel, Harrow, was well attended and a small private exhibition was arranged for members. The president for $1958 / 59$ is S. V. Williams, of Pamphonic Reproducers, who was invested with the badge of office, a recent gift to the Association by A. E. Buchan, of Aberdeen, who was president in $1953 / 54$. The honorary secretary is Alex. J. Walker, 394 Northolt Road, South Harrow, Middx.
Full House.-As far back as March 16th all tickets for G. A. Briggs' concert-demonstration at the Royal Festival Hall, London, on May 9th had been sold.

University of London.-Two lectures are being given in London at the end of April by Professor B. D. H. Tellegen, of Philips Research Laboratories, Eindhoven, and the University of Delft, under the scheme for the interchange of British and Dutch lecturers. The first lecture, entitled "The Gyrator as a Network Element," will be given at King's College on the 29th, and the second, entitled "The Search for a Complete Set of Ideal Non-linear Network Elements," at Imperial College on the 30th. Admission to both lectures, which start at 5.30 , is free; tickets are not required.

Sound Reproduction.-A series of six lectures on high-fidelity and stereophonic sound reproduction is being given by J. Moir at Norwood Technical College on successive Tuesday evenings, from May 19th. Full details of the course, for which the fee is 10 s , are obtainable from the College, Knight's Hill, London, S.E. 27 .

Broadcast Receiving Licences.-Combined TV/ Sound licences in the U.K. increased during February by 108,549 , bringing the total to $9,152,927$. Domestic sound-only licences decreased during the month by 109,440 , reducing the total to $5,189,399$. Car radio licences rose by 3,603 to 372,297 . The overall total of receiving licences was $14,714,623$.

Radio Control.-The Post Office issued the three thousandth licence for the radio control of models, such as aircraft, boats and cars, etc., in March. These licences, which cost $£ 1$ and remain in force for five years, were introduced on June 1st, 1954.

## Personalities

A. G. Touch, M.A., D.Phil., since 1954 Director of Electronics Research and Development (Ground) in the Ministry of Supply, has been appointed senior superintendent of the Radio Department at R.A.E., Farnborough, in succession to Dr. J. S. McPetrie (see W.W., November 1958, p. 526). After graduating at Oxford, Dr. Touch joined Watson-'Watt's radar team at Bawdsey research station in 1936. For his contributions to the development of meter-wave AI and ASV he received a substantial award on the recommendation of the Royal Commission on Awards to Inventors. From 1941 to 1947 he was liaison officer with the British Joint Services Mission in Washington. On his return to this country he became superintendent of the Blind Landing Experimental Unit at Martlesham Heath, Suffolk, and from 1952 to 1954 was Deputy Director of Electronics Research and Development (Air) in the M.o.S.
D. W. Fry, M.Sc., M.I.E.E., having been appointed director of the Atomic Energy Establishment, Winfrith, his place as deputy director of the Atomic Energy Research Establishment, Harwell, is to be taken by F. A. Vick, O.B.E., Ph.D., since 1950 Professor of Physics in the University College of North Staffordshire. Mr. Fry was at T.R.E. throughout the war working on problems of centimetre-wave techniques. Dr. Vick was assistant director of scientific research in the Ministry of Supply from 1939 to 1944.
E. M. Lee, B.Sc., M.I.E.E., M.Brit.I.R.E., successor to Major L. H. Peter as president of the Radio and Electronic Component Manufacturers' Federation, has been managing director of Belling \& Lee since its formation in 1922. He is also a director of Insulators Limited (Plastics). During the war he was chairman of the Joint Industries and Services Technical Components Committee. Mr. Lee is keenly interested in the educational side of the industry and is chairman of the Radio Trades Examinations Board.

E. M. LEE

E. W. HAYES
E. W. Hayes, M.I.E.E., becomes head of the B.B.C.'s Planning and Installation Department on the retirement of A. N. Thomas. Mr. Hayes joined the Corporation in 1933 and was appointed assistant to the Superintendent Engineer Transmitters in 1946. For three years from 1948 he was resident engineer in the British Far Eastern Broadcasting Service, Singapore, and since 1951 has been head of the Transmitter Equipment Section of the Planning and Installation Department. Mr. Thomas, who joined the B.B.C. in 1926, served at a number of transmitting stations before transferring in 1929 to the Research Department where he assisted in the establishment of synchronized transmitter networks.
D. B. Weigall, B.A., A.M.I.E.E., who succeeds Mr. Hayes as head of the Transraitter Equipment Section of the Planning and Installation Dept., has been with the Corporation since 1933. He was seconded for two years in 1940 as chief engineer to the Malayan Broadcasting Corporation and in 1943 was seconded to the Ministry of Information as technical adviser on broadcasting.
L. Essen, U.B.E., D.Sc., Ph.D., A.M.I.E.E., has received the Wolfe Award of $£ 500$, which is the first of ten annual awards to be made under the terms of a will to the research worker who is considered by the Department of Scientific and Industrial Research to have made an outstanding contribution to the research work of the Department during the previous 12 months. Dr. Essen, a senior principal scientific officer at the National Physical Laboratory, receives the award for his work on the establishment of the cæsium atomic frequency standard as a basis for the future standard of time. Dr. Essen joined the N.P.L. in 1929.
J. W. Godfrey is retiring from the position of Editor, Technical Instructions, in the B.B.C.'s Engineering Training Department. He joined the B.B.C. maintenance staff in the London control room in 1929 and in 1935 transferred to the Technical Recording Section. He became an instruction writer in 1942 and four years later was appointed to his present position in which he has been largely responsible for building up this section of the Corporation's Engineering Training Dept. Mr. Godfrey, who is editor of the B.S.R.A. journal Sound Recording and Reproduction, is joint author with G. Parr of "The Technical Writer." He is being retained by the B.B.C. in a part-time consultant capacity.
S. W. Amos, B.Sc.(Hons.), A.M.I.E.E., a frequent contributor to Wireless World, succeeds Mr. Godfrey as editor in the Technical Instruction Section of the B.B.C. on May 1st. He has been with the B.B.C. since 1941. He spent three years as an instructor in the B.B.C. Engineering Training School before joining the Section in 1946. He has been assistant editor in the section since 1957. He is joint author with D. C. Birkinshaw of the four-volume B.B.C. engineering text book "Television Engineering," issued by our publishers, and author of "Principles of Transistor Circuits'."

S. W. AMOS.


HECTOR V. SLADE.

Hector V. Slade, M.B.E., this year's chairman of the Radio and Electronic Component Manufacturers' Federation, became managing director of the Garrard Engineering and Manufacturing Co. in 1957 on the retirement of his father. He joined the company as an apprentice in 1935. On returning from military service in 1947 he became assistant managing director and in 1952 joint managing director.
J. W. Soulsby, chief radio officer in the British India Steam Navigation Company's Uganda, has been elected chairman of the Radio Officers' Union, for the fifth successive year. He has been on the staff of the Marconi Marine Company since 1918. The vice-chairman of the Union is W. S. Armstrong, elected for the third year in succession. He was for some years on Marconi's sea-going staff but since 1947 has been a member of the company's technical shore staff and is now an inspector.
A. R. Williams has retired from the managing directorship of Grampian Reproducers, which he founded in 1932. At the recent annual meeting of the Association of Public Address Engineers he was made an honorary life member in recognition of his services to the public address industry. For 21 years prior to forming Grampian he had been with Marconi's, where he was for some time commercial manager.
E. D. Hart, M.A., A.Inst.P., A.M.I.E.E., for the past five years general secretary of the Scientific Instrument Manufacturers' Association, has joined the board of Industrial Exhibitions Limited. He was with Marconi Instruments for twelve years before joining, in 1952, the Equipment Division of Mullards as head of the technical department.
T. C. Owen, advertisement manager of Wireless World, has retired after 47 years' association with the journal. In 1912 he joined Marcon's, who issued The Marconigraph, which in 1913 became Wireless World. In December, 1917, after being invalided out of the Army, Tom Owen transferred to Wireless Press Ltd., and he was appointed advertisement manager when Wireless World was acquired by Iliffe \& Sons Ltd. in 1925. He is succeeded as W.W. advertisement manager by G. Benton Rowell, who had been assisting him since 1950.
C. C. Whitehead, author of the article on variablegain magnetic amplifiers, was for 12 years in the Royal Corps of Signals and six years with the B.B.C. before starting his industrial career in 1938 when he joined the Telephone Manufacturing Co. He was with them for a two-year contract in charge of the radio section to fulfil a foreign order for v.h.f. communications equipment. He then joined Marconi's, where for ten years he was on development and research work. From 1950 to 1953 he was chief development engineer with Bailey Meters \& Controls, and since 1954 has been senior engineer (research and development) with the Sperry Gyroscope Co.

## OBITUARY

Professor J. T. MacGregor-Morris, D.Sc.(Eng.), M.I.E.E., Emeritus Professor of Electrical Engineering, University of London, died on March 18th, aged 87. He received his scientific education at University College (London), where he was a student under Professor (later Sir) Ambrose Fleming, and afterwards spent some years as his assistant. He was, therefore, well qualified to write in 1954 a biography of Sir Ambrose Fleming entitled "The Inventor of the Valve." In 1898, at the age of 26, MacGregor-Morris started organizing classes in electrical engineering at what subsequently became Queen Mary College, London. When the college was affiliated to London University he was appointed Professor of Electrical Engineering and occupied the chair until his retirement in 1938.

Alexander James Muir, M.B.E., who died as a result of a road accident at Malvern on February 28th, was well known in the field of radar. He joined D.S.I.R. in January, 1927, and worked as an assistant at Ditton Park. In 1935 he was one of Watson-Watt's original team of six to build the first radar station at Orfordness. He moved to the research establishment at Bawdsey with the inception of the programme for CH stations, and later to R.R.E., Malvern, where he was still actively engaged on radar development at the time of his death. Sir Robert Watson-Watt pays tribute to Muir's work in his book "Three Steps to Victory."
H. Howitt, secretary and later director of the British Radio Valve Manufacturers' Association from its formation in 1926 until his retirement in 1936, died on April 5 th at the age of 85 .

# Radio Components Show 

## NEW DEVELOPMENTS SEEN AT THE R.E.C.M.F. EXHIBITION

0NCE again the annual show of the Radio and Electronic Component Manufacturers' Federation was held in Grosvenor House and Park Lane House, London, W. 1 (6th-9th April). The number of firms exhibiting was the largest ever and the stands were crowded with visitors from abroad and with British engineers and technicians from industrial firms and Government establishments.

Our technical staff found a great many new techniques in component design as well as the less spectacular. but none the less important, steady improvements in established products. The following review is a selection of those exhibits which seemed to us to hold the greatest originality and technical interest.

Resistors:-The main trend indicated by development over the last year is not a new one-both fixed and variable resistors are getting smaller; but at this year's exhibition the effects of miniaturization were very marked indeed. Possibly the most far-reaching example of this was the introduction by S.T.C., Painton and Dubilier of ranges of miniature high-stability carbon resistors. The Dubilier Type S27 resistor, rated at $\frac{1}{6} \mathbb{W}$, is the smallest of a new range in sizes rated up to $2 \mathbb{W}$ and 800 V , using turnedbrass silver-dipped end-caps. The finish applied is three coats of a silicone varnish and the now carinc identified by the serial letter " S ," corresponds (with the exception " R " the to-W size) to the existing " R " series. The new S.T.C. resistor is also rated at tow but Painton's Type 70, though of roughly the same physical size (about 0.35 in long and 0.1 in in diameter) is rated at $\frac{1}{6}$ watt -this increase is due to the use of their Sintox base material, which has a heat conductivity similar to that of steel. An improved ceramic with low-alkali content is used by Welwyn as the base in ranges of oxide-film resistors both for high-power-dissipation and high-stability applications. This, and improved overall-coating and film-depositing processes. allow the use of these resistors at temperatures of at least $150^{\circ} \mathrm{C}$.
A new power resistor from Dubilier -the PW series-is of all-insulated construction. The wire element is wound on a glass-fibre core, silicone impregnated and placed in a ceramic "coffin" which is sealed with a ceramic cement. Ratings are 5, 7 and 10 watts in $\pm 10 \%$ and $\pm 5 \%$ tolerances.

The difficulty of removing heat from high-temperature components such as power resistors is nor a new one; but as units become more com-
pact the difficulty increases. One solution to this problem for mams droppers is the provision of a "chimney" in the form of an aluminium tube through the resistor itself. This technique was emp.oyed by Pye in theis $110^{\text {c }}$ relevision receiver* and the logical development is to dispense with a separate former and use the
packed in silicone rubber; but the main cooling effect was achieved by conduction into the chassis. A resistor, which, to outward appearances, was a 5 -W type, was stated to be capable of dissipating 20 to 50 W : this method would seem to be ideally suited to a cooled-chassis technique. $\dagger$

For more normal applications Morganite have introduced a new range of non-insulating torm carbon resistors in standard values between $10 \Omega$ and $10 \mathrm{M} \Omega$. These are available in 5, 10 and $20 \%$ tolerances and are known as "Type X."

Painton's new $\frac{1}{5}$-W high-stability resistor is no coubt partly responsible for the small size of a new professional vision or sound attenuator of the quadrant type. This, too new to have a type number yet, is only half the thickness of the normal type, yet

it is providec with plug-in connections and microswitches for operating internal scale and warning lamps. Electronic Components, too, have introduced a new small fader unit; but this consists of two "half-thickness" attenuators mounted together so that the double unit plugs into the same space as the existing single type. Again, internal switches for scale and warning lamps are incorporated, and there is also a companion unit of reduced height ( $4 \frac{1}{2}$ in) with a smaller number of studs. Another new Painton product is the Bournes Trimpot. This is superficially not unlike the "Flatpot" shown last year-it is a small rectangular pre-set; but it is available in a wide diversity of mounting styles and values and can be operated at up to $175^{\circ} \mathrm{C}$. It is +"4 Cooling Airborne Electronic Equipmenli, by $\begin{aligned} & \text { orld } \\ & \text { February, } 1959, ~ p . ~ \\ & 87\end{aligned}$
fully sealed and the element can be either of wirewound or carbon construction.

Among the many printed-wiring adaptations of ordinary potentiometers were noted several of the mount-through type in which the ordinary spindle-bush nut clamps the unit to the board, the tags being extended forward to locate on the printed wiring (Egen 315 series, Reliance 2 W wire-wound, etc.). One pre-set unit designed expressly for printed-wiring use was shown on the Colvern stand. Rated at $\frac{1}{2} \mathrm{~W}$ this is available in values up to $50 \mathrm{k} \Omega$.

Perhaps the most interesting trend in controls for domestic equipment is that manufacturers are tending, more and more, to buy complete control sub-assemblies rather than separate units. Some of these are mounted on the cabinet; but some pre-set groups are designed for printedwiring mounting with very little mechanical support other than tags. Several manufacturers expressed the hope that there would be an increase in the use of flexible links between the knobs exposed to the rigours of everyday domestic life and the delicate printed-wiring board.

Single controls are, of course, still being produced in vast numbers and several new devclopments feature increased safety or a better product at a lowest cost. As an example of the first trend, Morganite were showing volume controls with a hard p.v.c. spindle. This is splined on to a short steel stub which takes the place of the spindle on an otherwise normal unit. Originally produced for the Scandinavian market, this control obviously presents no danger of electric shock should the control knob be broken or pulled off.

A large number of potentiometer failures in domestic equipment are due to the sprayed track being damaged by the wiper. Several years ago Plessey produced their moulded-track units to overcome this; but as they are rather more expensive than the sprayed-track type their use has been confined to betterclass apparatus. However, they have now produced a moulded-track potentiometer to sell at a price only slightly higher than a sprayed-track type by using a far less costly assembly than is usual. The main feature of the Type Y is a triangular-section spindle formed from sheet brass: at the inside end this is splayed to make the switch operating cam, brush carrier and stop, whilst the slight springiness enables a simple, moulded push-on knob without a retaining spring to be used. Another new


Triangular-spindle potentiometer with moulded track (Plessey).

Plessey product is a range of moulded-track sub-miniature preset potentiometers rated at $\frac{1}{4} \mathrm{~W}$ and designed for panel grouping for television receivers.

A cam-corrected precision potentiometer usually requires a higher driving torque than the uncorrected type. In an effort to reduce the additional drag Colvern have developed a cam-corrected potentiometer with a very light action. In this the cam acts as the "slip-ring" contact and a very light cranked wire bears on it. This twists against light spring pressure, rotating a fork carrying the brush, so moving the brush and achieving correction. The Reliance SPP25 is a precision potentiometer with an accuracy of $0.1 \%$ which is achieved, not by a correcting mechanism, but by careful manufacture. The other new products from the Reliance Manufacturing Company are a sine/cosine resolver potentiometer (Model CO3) with $2 \%$ accuracy and a miniature (Type J12) helical potentiometer 1 -in long and of $\frac{1}{2}$-in diameter. Siemens Edison Swan offer a 10 -turn helical type only 0.3 in by 0.6 in and Ferranti have produced a 3 -gang precision potentiometer only $\frac{3}{4}$-in in diameter which weighs only $\frac{1}{2} \mathrm{Oz}$ and has a linearity tolerance of $0.1 \%$. Ferranti state that its production has been made possible only by the design of a new winding machine capable of handling wires of diameter down to $5 \times 10^{-4} \mathrm{in}$.
 Ardente (V); Armand-Taylor (W); British Electric Resistance (W) V); Bulqin (W); Colvern (V); Dubilier ( $\dot{C}, H S, W, V$ ), Egen (V); Electronic Combonents (W), Vgen Electrothermal (HS. W); Erie (C, HS, W); Fortiphone ( $V$; Jobling (HS); Labgear (W); McMurdo (W); Morganite (C, V); N.S.F. (V): Paintrn (HS. W. $V$ ): Plessey ( $W$.S.F. Reliance Mfg. (V); $\dot{\text { S.T.C. }}$. (HS): TM.C. (W), Welwyn (HS, W); Zenith (W). *Abbreviations: C, composition; HS, high stability; W, wirewound; V, $\begin{array}{r}\text { variable }\end{array}$ (wirewound or composition).

Variable Capacitors:-A major trend at once evident in tuning capacitors for radio receivers was that the double, spring-loaded antibacklash gear is becoming popular for at least one stage of the reduc-

Co'vern wirt-wound pre-set potentio. meter printed-wiring boards.
tion drive. Among the numerous samples seen a $50: 50$ distribution between cut gears and the stamped-from-sheet type was noted. Cost, of course, is the deciding factor; but the superiority of the cut gear is evident at once from handling the drive. A cut gear is used on the Wingrove and Rodgers two-gang $C 86 / 302$, which is a double type of maximum capacitance 500 pF and 10 pF . Designed for a.m./f.m. receiver manufacturers, this capacitor has an exceptionally rigid frame and the reduction-drive provided is $3: 1$. Another product shown by this company was a miniature 3 -gang capacitor (Type C78/23), only $2 \frac{1}{4} \times 1 \frac{1}{2} \times$ $1 \frac{1}{2}$ in approximately, with a maximum capacitance of 196 pF per section. The small size is realized by the use of a gap of only 12 "thou" between fixed and moving vanes. Jackson, too, were showing a two-gang a.m./f.m. capacitor-in this case pressed gears are used and the vane shape is modified slightly to give a good frequency distribution over the scale (Type LFM2). Very rigid f.m. sections are a feature of this model, and a new version of Jackson's "OO" two-gang capacitor for transistor applications is fitted with a concentric slow-motion drive and "spikes" for printed-wiringboard mounting.

> Plessey tuning capacitor with antibacklash reduction gear and integral wave-change switch.


Plessey have extended the scope of wavechange switches ganged to the tuning capacitor with several new models: the Type $S$ has a fork mechanism which actuates at each end of travel of the capacitor a double-pole changeover switch. This is not unlike one "wafer" of a push-button switch and is completely insulated from the frame of the capacitor. The Type V capacitor is a two-gang a.m./f.m. type fitted with a cut-gear reduction drive which is notable for a very smooth action.

Fixed Capacitors:-Electrolytic capacitor developments during the lasi yeat have been confined mainly to reductions in overall size. One point made by Daly was that the use of etched foil for the cathode, as well as for its more customary use as the anode, can allow a reduction in size to be effected. An improvement in technique is responsible for the increase in maximum operating temperatures announced by T.C.C. for their tantalum-anode capacitors. The range covers capacities and working voltages from $200 \mu \mathrm{~F}(6 \mathrm{~V})$ to $16 \mu \mathrm{~F}$ (150V) in polarized types (non-polarized versions exhibit half the capacity of the polarized types) and the operating temperature range is now $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.

Possibly the most interesting development in ceramic capacitors was a $0.1 \mu \mathrm{~F}$ type, shown by Hunt, which measured about $\frac{1}{2}$-in square by 1 mm thick. Some of the gilt is taken off the gingerbread by the maximum voltage rating (30), but this capacitor should be ideal for transistor applications where space is very limited. Made by a new process of rolling-out the dielectric material, a permittivity of 6,000 is realized.
B.S. 415 seems to have been responsible for a considerable divergence of opinion over the amount of external insulation needed on isolating capacitors for use in live-chassis apparatus; several manufacturers produce isolating units with only a light, external insulating coating, whilst others produce capacitors in a moulding of a material capable of withstanding the test potentials. Erie produce both types in tubular and disc shapes, and they were showing also two new high-voltage ceramic-capacitor series, designed specifically for line timebase applications. The type numbers are 2163B ( 15 to $25 \mathrm{pF}, 2 \mathrm{kV}$ ) and 2163 C ( 18 to $56 \mathrm{pF}, 3$ to 4 kV ). A modification of Erie's PAC component
assembly (the Mk. III) features individually replaceable components from their "Pluggable" ranges with tags at 0.25 -in centres.
Polycarbonates are thermoplastic compounds containing aromatic rings linked by the carbonate group electrically not unlike polystyrene; but with a higher softening point. Suflex capacitors utilizing polycarbonate dielectrics exhibit much the same characteristics as polystyrene types; but they can be used at temperatures up to $140^{\circ} \mathrm{C}$. Stantelac capacitors (S.T.C.) also use a synthetic film dielectric; but the films are so thin that they cannot be handled; they are coated onto aluminium foil which is itself only $8 \mu$ thick! Working voltages are 50 and 100 , and the capacity range is $0.01 \mu \mathrm{~F}$ to $2.2 u \mathrm{~F}$.

The Dubilier Type 560 is a highgrade paper dielectric capacitor encapsulated in mineral-loaded resin. It is claimed to be resistant to mechanical shock and moisture: it exhibits an insulation resistance better than $2 \times 10^{\prime} \mathrm{M} \Omega$ at $30^{\circ} \mathrm{C}$ and life expectancy for a 1 in 10 failure rate is better than 10,000 hours at $70^{\circ} \mathrm{C}$ and $50 \%$ d.v. overload. Hunt's popular "Moldseal" range is now produced with a new coating material which is more resistant to mechanical shock than the original substance and the end-mounting printed-wiring adaptations of this range feature a new moulded end cap. This holds the lead-out wires rigidly in position and provides a three-point support for the capacitor.

Manufacturers*: Ardente (V); B.I.C.C. (P); Bird (T); Bulgin (M); C.C.L. (E); Daly (E); Dubilier (C, E, F, M. P); Erie (C M, T, V); Hunt (C, E, F, M, P); Jackson (T, V); L.E.M. (C, F, M. T. T); Mullard (T, V); Mycalex and T.I.M. (M); Plessey (C, E, F, P, T, V); Salford ( $F$ ); Stability (C, F); Stration (V): S.T.C. (C, E, F, M, P); Suflex (F); T.C.C. (C, E, F, M, P, T); T.M.C. (F, M, P); Walter (T); Wego ( $\mathrm{F}, \mathrm{M}, \mathrm{P}$ ): Wingrove and Rodgers ( $\mathrm{T}, \mathrm{V}$ ). *Abbreviations: $C$, ceramic or glass; $E$, electrolytic; $F$, plastics film: $M$, mica; $P$, paper; $T$, trimmer; $V$, variable (tuning, etc.).

Transformers and Inductors: Wound-strip transformer cores are usually regarded as too expensive for use in domestic-equipment because of high costs, due mainly to the " banding" process of holding the C -shaped sections of the core together. However it has been shown, by "rethinking" the C-core process, that it is a realistic form of core for lowcost transformers. An example of a new low-cost assembly process was shown on the Telcon-Magnetic Cores stand. The wound core is cut, not across the middle of the long sides; but as near to one end as is prac-
ticable. The bobbin carrying the windings is then placed on the smaller sections; the larger sections are placed in position and a d.c. of sufficient magnitude to attract firmly together the core sections is then


C-core transformer assembled by new method (Telcon-Magnetic Cores).
passed through a winding. A resin potting compound is poured round the assembly to a sufficient depth to cover the join between the core sections. In this way the cores automatically align themselves and the whole transformer is held rigidly.

Also on show on the Telcon-Magnetic stand were some examples of their Y-cores. These are woundstrip cores for 3-phase transformers; but instead of being formed in the usual E-shape they resemble a "star" (as opposed to "delta"). This is claimed to give a superior phase balance and to ease winding problems.
Partridge Transformers have pro-


Partridge Type MC7 microphone transformer.
duced a new range of microphone transformers-the MC5, MC6 and MC7. All three use Mumetal cores and are fitted into $\frac{1}{\frac{1}{6}}$-in thick Mu metal round cans with a single-hole mounting so that they can be rotated for minimum hum pick-up. The MC6 is provided with two $150-\Omega$ primaries for use with a $600-\Omega$ balanced line and the MC7 matches
a $30-\Omega$ line into the grid circuit, both have a response within 1 dB from $30 \mathrm{c} / \mathrm{s}$ to $20 \mathrm{kc} / \mathrm{s}$. The MC5 is a smaller and cheaper unit with a more limited response providing a $50: 1$ ratio from $20-\Omega$ line.

To provide a "tropicalized " transformer of high reliability at low cost Hinchley Transformers have "potted" vacuum impregnated units into drawn aluminium cans, using pitch as the sealing material. This is claimed to be more satisfactory in reducing electrolysis of the insulants than the usual pitch-dipped type of construction. Also featured were mains-isolating transformers for ser-vice-bench and domesuc use.

Weymouth were showing samples of their popular Type " $H$ " coils wound on a new former moulded from high-impact polystyrene. This reduces losses and improves performance. Also shown by Weymouth was a high-precision delay line. It is possible to "repeat" inductors to fairly close limits on production (Weymouth quoted $1 \%$ ) but the lumped effect of small errors could cause a precision delay line to be useless. In view of this the inductors are wound with adjustable iron-dust cores and each line is set up for optimum performance.

Both Plessey and Weymouth are now producing double-tuned i.f. transformers for transistor receivers: whilst slightly more costly than the single-tuned versions they do offer improved performance, particularly on selectivity. One very neat solution to "Q-boosting" problems was noted on the Plessey stand in their range of miniature i.f. transformers for transistor circuits. This range is identical in performance with the established sub-miniature range employing pot-cores; but by the use of bigger ( $1 \frac{3}{6}-\mathrm{in}$ square) cans losses can be cut down to the point where the pot core is no longer necessary except for the final transformer. The use of a pot core here is avoided by fitting a U-shaped ferrite section round part of the coil only. The increase in permeability enables a small enough quantity of wire to be used to realize a $Q$ of 160 . In the double-tuned range of transformers the detector diode and filter have been fitted inside the screening can to reduce 2 nd harmonic radiation.

Another example of the accuracy possible with modern coil-winding techniques was shown by Plessey. This was a permeability-tuned coil for the 20 to $40 \mathrm{Mc} / \mathrm{s}$ range for use in their 1750 -channel communications equipment. A $0.4 \%$ tolerance on inductance between a set of six
inductors at any insertion of the cores is allowed, and to realize this an accuracy of turn spacing of $2 \times 10^{-3}$ in is required.
Manufacturers*: Ardente (LA, LR, TA); Belling and Lee (LR, TR), Bulgin (LR); Duoiner (LA); Electro Acoustic (TA, TR); English Eiectric (LA, TA TR); Erie (LR); Fortiphone (LA, LR, TA, TR); Goodmans (LA, TA); Gresham (LA, TA, TR); Haddon (LA, TA, TR); Hinchley (LA, TR); Henry and Thomas (LR); Lion (LA, LR, TR); Mullard (LA. LR); Painton (LR); Parmeko (LA, TA, TR); Partridge (LR); TA, TR); Plessey (LA, LR, TA, TR); Reproducers and Amplifiers (LA, TR); Reproducers and Amplifiers (LA, TA); Richard Allan (TA); Rola Celestion (TA);
S.T.C. (LA, LR, TA); Stratton (LR, TR); Teledictor (LA, TA); T.M.C. (LA, TA); Wayne Kerr (TA); Welwyn (LR); Weymouth (LA, LR, TA, TR), Whiteley (LA, LR, TA, TR); Wireless Telephone (LA, Weaire (TA); Zenith (LA, TA).
\#Abbreviations: LA, a.f inductors; LR, r.f. inductors; TA, d.f. transformers; TR, r.f. and pulse transformers.

Aerials and Accessories:-A new loft aerial provided an interesting example of economy in design. Produced by Kimber-Allen, it consists of a ground-plane Band-I aerial with a telescopic vertical element which gives a variation in gain of about 20 dB as well as enabling resonance to be achieved on any channel in Band I. The horizontal groundplane element is shortened and carries the Band-III directors and reflector; proximity coupling is used so that a common feeder can be used and a Band-II "twig" is available (only one is used). The feeder connection is simplicity itself-a saddle connector for the coaxial-cable outer conductor is effective and quick and the inner conductor is clamped under the head of the bolt retaining the Band-I vertical element. A universal clamp and a key-hole mounting com-


Wolsey A3/3/3 hgh-gain distribution amplifier for Bands I, II and III.
plete what should be a popular and effective design. Labgear were showing a new dual-band aerial-Band-I dipole and director with five directors for Band III The Band I dipole carries two "twigs" which are claimed to cause the whole dipole to behave as a co-linear array, so boosting signal pick-up.

Wolsey Electronics were showing a new range of equipment for com-munal-aerial installations including padded and terminated outlet boxes with attenuations between 38 and 20 dB , and splitter networks. Designed to fit conduit or for surface mounting the outlet boxes are fitted with isolating capacitors to BS415 (so protecting other users of the installation should one receiver become faulty) and they provide two outlets, î̂ desired, one for f.m., one for TV. The A3/3/3 amplifier consists of three of Wolsey's high-gain amplifier strips and a power supply and it can be provided with a conduit type outlet. Providing a 50 dB gain on one channel each in Band I and Band III and over the v.h.f./f.m. band, it is designed for feeding large blocks of flats, small estates, etc.

A new triplexer by Antiference (Type Y4) is designed for mast-head or gutter mounting. It uses a plastics moulding to carry conventional


Above: High-pass aerial-lead filter (Belling-Lee).

components and it is claimed that it can be used as a diplexer between f.m. and television aerials also. The out-of-band lusses are 20 dB and pass-band attenuation is 2 dB .

Two new products from Belling and Lee should prove popular-one mainly for export, the other for the home market. The L1418 is a $300 \Omega$ twin-feeder outlet box moulded in high-density polythene. Solderless connections are made by crimping, in both the box and its associated plug The L1425 is a high-pass multisection filter with a characteristic impedance of $80 \Omega$. It has an insertion loss in the region of 2 dB at frequencies down to $40 \mathrm{Mc} / \mathrm{s}, 55 \mathrm{~dB}$ at about $38.5 \mathrm{Mc} / \mathrm{s}$ and 90 dB at about $33 \mathrm{Mc} / \mathrm{s}$. The trim flat case carries a plastics clip to hold the unit on the receiver back and it is supplied complete with a standard coaxial plug Belling and Lee were also showing some examples oi multisection telescopic rods for on-thereceiver aerials.
Manufacturers*: Antiference (AS, DA); Belling and Lee (AS. DA, D): J-Beam iAS, CA. DA); Kimber-Allen (DA); K.L.G. (DA); Labgear (AS, DA. D): Wolsey (AS, DA, D).
*Abbreviations: AS, accessories; CA. communications aerials; DA. dumestic aerials; D , distribution amplafiers and equipment.

Switches:-Miniaturization is still the main trend in switch development. One of the smallest rotary switches on show was a wafer type by Ardente, measuring about $\frac{1}{2}$ inch in diameter. An interesting feature of the design is that each switch bank consists of a pair of wafers with fixed contacts, between which a shorting contact is moved round by the drive shaft. An example with three banks was shown, but more can be used. The switch has 6 ways and up to 3 poles and is continuously rotating.

Miniature OAK type rotary wafer
Electronic Components front-af-panel stud switch.



Ardente miniature rotary wafer switch.
switches (about 1 inch in diameter) were shown by N.S.F., who also had a miniature version of their Ledex rotary solenoid, which drives 4-6 wafers in 12 steps with an input power of about 7 watts. The OAK switches, in common with several other rotary swatches seen on other stands, had wafers made of a glass fibre material instead of the usual resın bonded paper This is a new trend, giving better insulation resistance and greater mechanical strength.
Probably the ultimate in minaturization has been accomplished by Electronic Components in a new rotary stud switch, which is made to disappear altogether-at least from its usual place behind the control panel. In fact, the mechanism is designed to fit on the front side of the panel, underneath its control knob. A particular advantage of this scheme, apart from space saving, is that


Siemens Edison Swan printed-circuit connectors. the studs are freely accessible for cleaning or lubricating when the control knob is removed.

Manufacturers*: A. B. Metal Products ( K , T, P, R, SL); Ardente (P, R, SL); B.E.R.C.O. ( $\mathrm{R}, \mathrm{S}, \mathrm{T}$ ). Bulgin ( $\mathrm{K}, \mathrm{T}, \mathrm{M}, \mathrm{P}$, R. SL. ST, TH); Diamond $H$ ' (T. R), Egen ( $\mathrm{P}, \mathrm{R}$ ); Fortiphune ( $\mathrm{T}, \mathrm{R}$ ). Henry and Thomas (K, T); Kimber-Allen (T), Magnetic Devices (P), N.S.F (K, T. P, R. SL); netuc Devices (P), N.S.F; Plessey (K, T. P, R, SL); S. T.C. (TH); T.M.C. (K. T. T); Walter (T, P, R SL, ST); Welwyn (T, P); Whiteley (K, P, R, SL. St).
*Abbreviations: K, key. T. lever or toggle; M , micro. P push-button, R. rotary; SL , slide, ST, stud; TH, thermal delay.

Chassis Fittings: - Right - angle valveholders have been introduced by Painton to permit horizontal mounting of valves on printed circunts, thereby making possible more compact circuit assemblies and simplifying heat sink arrangements. A new nylon printed-circuit valveholder shown by Cinch is available with a detachable half-circle clip

Neoprene designed to fold over and enclose the transistor (Electrothermal).

Different types of multi-way connectors for printed circuits are still being developed. The latest, from Siemens Edison Swan, is a simple and compact system of round pins and sockets inserted into flat pieces of nylon, each unit being 1 -inch long and containing ten pins or sockets. An inexpensive connector for multi-way cables shown by Plessey has the pins and sockets shrouded in single-piece polythene mouldings, which eliminate the need for gaskets and provide the necessary anchorage. The pins or sockets are crimped or soldered to the cable away from the mouldings then inserted into keyed holes in the polythene.

New terminal arrangements included a terminal block with spring-


Belling-Lee cooxial Unitors.
loaded wire grips instead of screw clamps (Hellermann). Spring loading is also used for quick release in some large insulated pillar terminals (Mycalex) for providing mains supplies on benches or counters. The insulated pillar is deflected by the fingers, allowing the ends of the flex wire to be inserted in a serrated brass grip.

A new design of coaxial cable connector by Electronic Components simplifies considerably the task of preparing the cable ends and assembling the connector parts. It is unnecessary to bare the braid sleeve. A knife-edged metal collar is inserted between the inner insulator and the braid, which is clamped on to the collar by means of a threaded bush which grips on to the outer covering of the cable. Belling-Lee have extended their " Domino" miniature Unitors to include coaxial connectors. The plugs and sockets are mounted in pairs with earth pins on small insulating blocks, and these blocks are assembled in groups in metal shrouds to form the Unitors. Ordinary single-pole connector blocks can be assembled with the coaxial ones if necessary. For jointing coaxial cables Hellermann were showing cable crimps consisting of copper cylinders with nylon bushes inside and small concentric metal bushes to take the cable inners. Crimping is done by a special tool.

Widney Dorlec have increased the versatility of their "prefabricated " cabinet system by providing for movable tapped holes in the main frame members to take the fixing screws of equipment panels. This avoids the need for having the
main members already drilled and tapped at regular intervals. A predrilled metal strip is bolted behind the main frame members and the holes in this are used as a location for drilling into the main frame. Small tapped blocks are then inserted behind the clearance holes in the main frame to take the panel fixing screws.

Manufacturers*: Antiference (CPS); Bakelite (P); Belling and Lee (CPS T, F, J, V); B.E.R.C.O. (DL, K): Brayhead (EFC); Bulgin (V, EFC, CPS, DL, ES, T, F, J, K); Carr Fastener (EFC, CPS, T, F; V); H. Clarke (T); Colvern (RPS); Cosmocord (K); Creators (EFC, G, TV); Egen (CPS); Electro Methods (CPS, T); Electronic Components (CPS. DL); Electrothermal (CPS. EFC); Fortiphone (CPS); Goodmans (CR); Hallam Sleigh and Cheston (CR): Harwin (EFC, CPS, T); Hasset and Harper ( $\mathrm{CR}, \mathrm{EFC}$, ${ }^{\text {ESS }}$; Hellermann (EFC, G. T, K); Imhof (CR); Insulating Components (DL, $P, T$, $V$ Jackson (DL, DR); K.L.G.'(T);' Long and Hambly (G); Lustraphone (EFC) Mong and (V, CPS); Mica and Micanite (EFC, T, V); Morganite (CPS); Mullard (CR): N'S.F. (CPS); Painton (CPS, DL, T, K); Permanoid (CPS); Plessey (CR, CPS, DR. T, $\mathrm{P}, \mathrm{F}, \mathrm{K}, \mathrm{V})$; Salter (EFC); Siemens Edison Swan (CPS, T, Valter Simmonds (EFC); Spear (EFC, CPS); Simmonds (EFC); (EFC, G); Stocko (EFC, T); Stratton (CR, CPS, DL, DR, K); Suflex (ES); T.C.C. (P); Telcon (CPS); Thermo-Plastics (CR, DL, ES, T); Thorn (P); T.M.C. (J); Tucker ( EFC , G); Tufnol (T); Walter (P); Weymouth (DL, T. K); Whiteley (CR, CPS, $T, K, V$ ); wimbledon (CR. EFC, WL, ES); Wingrove and Rogers (DR, T); Wolsey (CPS).
*Abbreviations: CPS, connectors, plugs and sockets; CR. cabinets, racks and chassis: DL, dials; DR. drives; EFC, eyelets, fasteners and clips; ES, escutcheons; F, fuseholders; G, grommets; J, lacks; K, knobs, P, printed circuits; $\mathbf{T}$, terminals and tagboards; $V$, valveholders.

Sub-Assemblies: - Manufacturers of television tuners are now producing them in alternative versions to cope with varying requirements. The Plessey-Brayhead tuner, for example, which has so far been in production with a 10 -position turret, is now
available with 14 -position and 18 position turrets. The 14 -position tuner provides for all 13 television channels and the 18 -position one for 13 television channels and four f.m. sound channels-both models looking far enough ahead to include the extra position for possible u.h.f. broadcasting in Band V. Provision is made also for dual-frequency i.f. strips- $34 / 38 \mathrm{Mc} / \mathrm{s}$ for television and $10.7 \mathrm{Mc} / \mathrm{s}$ for f.m. sound. Other versions of the tuner are available for 625-line television sets and f.m. sound-only receivers.

An interesting f.m. tuner introduced by Cyldon is based on a printed circuit which includes the coils, and these are tuned by an eddycurrent system. Rotation of the control shaft operates a cam which causes small metal plates to approach, or move away from, the printed coils -the cam being designed to give a linear tuning scale. A single ECC85 double triode is used, one half acting as an r.f. amplifier and the other as an oscillator/mixer. The gain is 60 dB at $87 \mathrm{Mc} / \mathrm{s}$ or 57 dB at $101 \mathrm{Mc} / \mathrm{s}$. The printed circuit is made from glass fibre and the oscillator drift is $35 \mathrm{kc} / \mathrm{s}$ for a $15^{\circ} \mathrm{C}$ temperature rise.
Band-pass crystal filters of small size and high selectivity for the i.f. sections of communications receivers were shown by Cathodeon Crystals. Three types, intended for channel spacings of $50 \mathrm{kc} / \mathrm{s}, 25 \mathrm{kc} / \mathrm{s}$ and possibly $12.5 \mathrm{kc} / \mathrm{s}$, have centre frequencies of $10.7 \mathrm{Mc} / \mathrm{s}$ and bandwidths (at -6 dB ) of $25,12.5$ and $6 \mathrm{kc} / \mathrm{s}$ respectively. The crystals and other components are mounted on printed circuits and hermetically sealed in compact metal cans ( $2 \mathrm{in} \times 2 \mathrm{in} \times 1 \frac{1}{4} \mathrm{in}$ ) with two terminals.

Encapsulated circuits for many different functions were noted. As an example, Wayne Kerr had a resin-

cast voltage stabilizer consisting of a chain of small neon tubes with a series/parallel striking network. Versions with stabilizing voltages from 370 V to 5 kV are available. The structure can be made slighrly radioactive to ensure an adequate level of residual ionization after periods of storage.
Manufacturers*: A.B. Metal Products (T); Belling-Lee (F, IS); B.I.C.C. (DN); Brayhead (T, AD); Bulgin (IS); Cathodeon (F); head ( C , (T) ; Dubilier (DN, IS); Erie (PC); Cyldon (I); Dubilier (IN); Labgear (P. IS); Goodmans (F); Hunt (IS); Labgear (F. (DN); Lion (DN); Morganite (IS); Mullard (DN, F.T.C. (IS, F); Stration (IS); T.C.C. (DN, IS); T.M.C. (F, IS); Wayne Kerr (F, IS); Wego (DN); W'eymouth (DN, F); Whiteley (AD, IS).
*Abbreviations: AD r.f. adaftors; DN delay nerworks: $F$, filters; IS, interference delay networks. ${ }^{\text {s., }}$, pre-assembled composumpts; T, runers.

Valves and Tubes:-For use in the cascode r.f. amplifier stages of television tuners, Mullard have introduced a new variable-mu doubletriode, the PCC89, of considerably improved performance. It has a frame grid, by means of which the grid-cathode spacing is reduced, and as a result the slope is as high as $12.5 \mathrm{~mA} / \mathrm{V}$-which is twice that of the conventional PCC84 now commonly used. The noise factor is 5.5 dB at $200 \mathrm{Mc} / \mathrm{s}$.

Another new double triode for this application is the Ediswan Mazda 30L15 (with conventional grid) which has a slope of $9 \mathrm{~mA} / \mathrm{V}$, while its companion triode-pentode frequency changer is the 30 C 15 . Brimar also have a new triode pentode, the 6BR8. The two sections have separate cathodes and the valve is mainly intended for a.f applications in which the two stages are connected in cascade. An r.f. beam tetrode from the same firm, the 6688, is intended for wide-band amplifiers and has the high slope of $16.5 \mathrm{~mA} / \mathrm{V}$.


The Nodistron numerical indicator tube of S.T.C. has been improved in a new model, G10/201E. This glow-discharge device has larger numerals, is now capable of working from both d.c. and a.c. and has no wire mesh anode in a visible position to obscure the view of the numerals.
Television cathode-ray tubes with $110^{\circ}$ deflection angles are now wellestablished on the market A new addition to the types already available (from Mullard and Siemens Edison Swan) is the 17 inch C17AA from Brimar. It has electrostatic focusing and operates with a final anode voltage of 16 kV .

As ion trap magnets are not used in these tubes other means have to be provided to adjust the alignment of the beam emerging from the electron gun. This is provided for by wire-ring magnets produced by Eclipse (James Neill), which are magnetized across a diameter and fitted round the tube neck. Known as "steering magnets," strengths of the order of 10 to 30 oersteds are used.
Manufacturers*: Ferranti (CC, IT, M, R, T); M-O (CC, IT, M, PC, R, T); Mullard (CC, IT, M, PC,' R, T); Siemens Edison Swan (CC, IT, PC, R, T); S.T.C. (CC, IT, $\mathrm{M}, \mathrm{R}, \mathrm{T}$ ).
*Abbreviations: CC, cold-cathode; IT, industrial and transmitting; $M$, microwave; PC, photocells; R, receiving; $T$, cathode-ray tubes.

Semiconductors:-The v.h.f. transistor is now very much a reality. As an example. some of the micro alloy diffused types available from Semiconductors will give useful gains at frequencies up to $200 \mathrm{Mc} / \mathrm{s}$. Mullard have introduced a new series of r.f. transistors made by the alloy diffusion technique, and the first of these, the OC170, has an average cut-off frequency of $70 \mathrm{Mc} / \mathrm{s}$ and a current gain of 80 . The maximum collector dissipation is 60 mW . Newmarket Transistors have developed an alloyjunction drift transistor, the V15/ 20R, with a maximum cut-off frequency of $75 \mathrm{Mc} / \mathrm{s}$.

The above are all germanium transistors. Silicon types, with their ability to work at temperatures up to about $150^{\circ} \mathrm{C}$, are now being produced in appreciable quantities, mainly for switching applications. Texas Instruments showed an extensive range of grown-junction n-p-n types, including an h.f. tetrode, 3S004, capable of giving a power gain of 20 dB at $70 \mathrm{Mc} / \mathrm{s}$. Silicon alloy-junction transistors for switching applications have been introduced by both Semiconductors and S.T.C. As an example of performance, the rise time obtainable with the SA496
made by Semiconductors is 80 millimicroseconds A range of p-n-p junction silicon transistors was shown by the Brush Crystal Company. These types, OC430 to OC470, have total power dissipations of 330 mW and are intended for use in d.c. amplifiers, class-B output stages and switching circuits.

An interesting experiment in tackling the problem of variations in characteristics between transistors of the same type number has been started by Mullard. They are introducing packages of specially selected and tested transistors which give guaranteed minimum overall gain figures when used in suitable circuits.


An a.f. package contains a matched pair of OC78 output transistors and an OC78D driver. This is to give an audio output of $500-600 \mathrm{~mW}$ with a maximum input requirement of $30 \mu \mathrm{~A}$. An r.f. package contains three OC44/OC45 transistors (for oscillator/mixer, 1st and 2nd i.fs), guaranteeing a minimum overall gain of 74 dB . In general, better gain figures are said to be achieved than the averages obtained with randomly chosen transistors.

Power handling capacities of transistors continue to be developed. A notable example on show was the Texas Instruments power transistor 2N458, which has maximum collector ratings of 80 volts and 5 amps . Newmarket have introduced a range of power types (in experimental production) with a junction geometry of a special kind which gives higher emitter efficiency and current gain than is normally obtainable at high currents (here up to 6 amps ). A new Mullard type, OC27, intended for the output stages of car radios, will give an output of $4 W$ in class-A output stages operating from 7 - or 14volt supplies.

In the rectifier field, S.T.C. were showing a new range of selenium h.t. rectifiers which correspond with their well-known RM series but have somewhat smaller radial dimensiöns. Texas Instruments have extended the range of their Zener voltage refer-
ence diodes to cover Zener voltages up to 91 volts. The maximum power dissipation of these types is 8 watts.

Manufacturers*: Brush (D, TR): Ferranti (D, TR); M-O (D, TR); Mullard (D. TR, TH); Newmarket (TR); Sallord (D, MR); Semiconductors (TR); Siemens Edison Swan (D, TR); S.T.C. (D,MR, TR, TH); Texas (D, TR); West.ighouse (D, MR). *Abbreviations: $D$, diodes; $M R$, metal rectifiers; TH, thermistors; TR, transistors.

Materials:-A modification of the transfer moulding process is used by Insulating Components and Materials and Anglo-American Vulcanized Fibre to produce transformer bobbins for high-temperature operation. The material used is an epoxy-resin and glass-fibre mixture and bobbin walls as thin as 0.015 in can be achieved.

Swift Levick had on show a highsaturation magnetically soft material for use as pole-pieces where very concentrated fields are required. Called Vaco-Iron, it is a mixture of cobalt, iron and a small quantity of vanadium; but, in spite of the vanadium content, it can be machined easily and with high accuracy. The saturation flux is about $25 \%$ higher than ordinary mild magnet steel.

Strictly speaking, Magloy (Plessey) is not a new magnetic material, but the result of a process. Normally when a magnet of, say, Alnico, is required it is cut into sections such that they conform to the shape of a leakage field about the poles of another magnet. The sections are then allowed to cool through the Curie point in the leakage field; then they are joincd to make a magnet of complex shape. In the Magloy process a shaped field, produced by an arrangement of conductors, is used instead of a leakage field, so far more complex shapes can be produced in one piece. Also, Magloy magnets can be covered with aluminium jackets which serve two purposes-they prevent the approach of other magnetic assemblies to the point where the Magloy magnets sustain damage, and they provide a convenient mounting arrangement.
Manufacturers:- Insulating Materals: Anglo-American Vulcanized Fibre. Bakelite, Geo. Bray, CIBA, H. Clarke, Creators, Enanlon, Formica, Hellerman. Henry and Thomas, I.C.I., Insulating Components and Materials, Jobling, K.L.G, Langley London, Long and Hambly, Mansol. Mica and Micanite, Micante and Insulators, Minnesota, Mycalex T.I.M.. Plessey, Siemens Edison Swan Standard Insulator, Siemens Edison Swan, Standard Insulator, Steatite, Symons, Telegraph Construction, T.C.C. ${ }^{\text {side, }}$ Thermoplastics, Tufnol, Wandle-
serr.

Magnetic Material: Darwins, Marrison, Mullard, Murex, James Neill, Plessey, Salford, Swift Levick, Whiteley.

Audio Equipment:-The automatic trip mechanism in a record player can often be damaged if the pickup arm is moved too far away from the record. The possibility of such
damage is, however, prevented by using a cam action for this trip in i new range of E.M.I. 4 -speed record players. A finger-tip speed-change control is provided by using a larger knob than usual and placing its edge


Above: Rolo Celestion twin re-entront loudspeaker.

Left : B.S.R. T.D. I tape deck.
vertical and partially protruding through the base plate, instead of, as is more usual, horizontally above the base plate.
New tape decks were shown by Collaro and B.S.R., this being the first tape deck, as distinct from other audio equipment, that B.S.R. have made. The B.S.R. Monardeck T.D 1. is a single-speed ( $3 \frac{3}{4} \mathrm{in} / \mathrm{sec}$ ) device powered by a single motor. The record/replay head gap length is $2 \times$ $10^{-4} \mathrm{in}$. The new Collaro deck uses a single pair of heads (unlike their other model). Three speeds are provided ( $1 \frac{1}{6}, 3 \frac{3}{4}$ and $7 \frac{1}{2} \mathrm{~m} / \mathrm{sec}$ ) and three motors are used.

In a new twin loudspeaker for relatively low-level public address purposes introduced by Rola Celestion two re-entrant horns placed back-toback each load a corresponding loudspeaker cone. The two voice coils are placed at opposite sides of the same magnetic gap so that only a single magnet is needed. A slot along the bottom of each horn gives some downward sound radiation in addition to that to two sides from the horn mouths. The frequency response is from 375 to $8000 \mathrm{c} / \mathrm{s}$ and the power-handling capacity 3 watts.

The problems of inhibiting cone break up and relieving stresses at the corners in rectangular "slot" speakers have been tackled by Rola Celestion in their $x$ by $2 \frac{3}{4}$ in C 28 model by means of two long strengthening protruberances in the cone covering most of the cone length on either side of the voice coil, and by making the rolls in the surround larger at the corners and across the breadth than along the length.

Several items shown also at the London Audio Fair are discussed in our review of that exhibition.

[^4]Pickups and Microphones:-Ardente; B.S.R.; Collaro; Cosmocord; Electronic Reproducers (Components); Fortiphone; Garrard; Goldring; Lustraphone, S.T.C.; Technical Ceramics; Vitavox; Walter; Whiteley Electrical
Tape Recorders:-B.S.R.; Collaro; E.M.I.; Multimusic; Truvox; Walter; Wright and Weaire.
Turniables:-B.S.R.; Collaro; E.M.I.; Garrard; Goldring; Staar.

## Test and Measuring Equipment:-

 In the Wayne-Kerr LT100 the resistance of a thermistor in a glass probe is measured using a Wheatstone bridge powered by a U2 battery. The thermistor resistance varies non-lınearly with temperature. This normally results in a nonlinear scale, but this is avoided in the Wavne-Kerr LT100 with the aid of compensating non-linear resistances i) the form of Zener diodes. Temperatures from 0 to $100^{\circ} \mathrm{C}$ can be measured and leads to the probe up to 1000 ft long are available.Two new multi-range meters were shown by Tavlor. In the pocket-size 127A the maximum sensitivity is $20,000 \Omega / V$ on the d.c. ranges, and resistances up to $20 M \Omega$ can be measured (up to $200 \mathrm{k} \Omega$ centre scale). A centre-pole meter with a f.s.d. of $40 \mu \mathrm{~A}$ is used. In the Taylor 100 A an $8 \mu \mathrm{~A}$ f.s.d. centre-pole movement gives a maximum sensitivity on the d.c. ranges of $100,000 \Omega / \mathrm{V}$. All the d.c. and a.c. range scales are coincident except for the most sensitive a.c. range ( 10 V f.s.d.). Another useful facility on this meter is a pushbutton for reversing the polarity.

A new a.m. signal generator covering frequencies from $2 \mathrm{Mc} / \mathrm{s}$ to 225 $\mathrm{Mc} / \mathrm{s}$ was shown by Avo (Type 378). The spurious f.m. is claimed to be particularly low on this instrument. This is achieved by means of a circuit in which non-linear crystal diodes are used to ensure that the a.m. occurs at a constant impedance.

Monufacturers:-Avo; British Phys:cal L.ahnrator'es Dawe: Lahgear; Lion Electron'c Developments: Measuring Instruments (Pull:n): Siemens Edison Swan; Taylor; Wayne Kerr.

# "Variahle-ヶ" Magnetic Amplifier 

System of Controlling Gain Giving a Versatile Circuit

By C. C. WHITEHEAD

MAGNETIC amplifiers at the present time are undergoing developments comparable with those of semiconductor amplifiers and the valve amplifiers of two or three decades ago. Each type of amplifier (valve, semiconductor or magnetic) has its advocates, who press for its application over as wide a field as possible. In truth these alternative forms of amplifier are, in various fields of application, both competitive and complementary.
Broadly speaking the magnetic amplifier scores over its rivals when the following conditions have to be met:-

1. Mechanical robustness. It is relatively free from maintenance troubles.
2. The ability to deal with large power in relatively small space.
3. The ability (given suitable design) to work under very unfavourable environmental conditions, e.g., wide variations of ambient temperature and pressure, dust, dirt, moisture, etc.
4. High overload capacity. In comparison with valve or semiconductor amplifiers of similar rating it has relatively enormous overload capacity.
5. It is capable of developing full gain with very low input impedance-especially useful in d.c. amplifier applications.

The magnetic amplifier is not, however, the most desirable choice when: (a) an extremely high input impedance is needed; (b) an extremely fast response (rise-time on a step-function input) is required.
The simplest form of magnetic amplifier is shown in Fig. 1, where $\mathrm{L}_{8}$ is an iron-cored choke in which air-gaps have been reduced to the absolute minimum and the core material has a closed circuit, of, as far as possible, uniform cross-section throughout normal to the magnetic flux. These features ensure that the core is relatively easily and fully saturated. The special oblique line symbol indicates this type of core. An additional winding is for convenience provided to carry the control current (d.c.) to saturate the core. Specially developed magnetic alloys (such as HCR, Deltamax, Orthonol, in which the optimum combination of permeability and satura-

tion flux density have been achieved) enhance the performance.
The degree of saturation of the choke is dependent upon both the a.c. supply voltage and the d.c. control current. If the supply voltage $\left(V_{8}\right)$ is constant, and the impedance of $L_{8}$ is decreased due to saturation by the control current ( $\mathrm{I}_{\mathrm{c}}$ ) ampereturns, the voltage across the choke $\left(\mathrm{V}_{\mathrm{LS}}\right)$ decreases owing to the voltage drop in the load impedance $\left(\mathrm{Z}_{\mathrm{L}}\right)$. So consequently does the degree of saturation of the core, necessitating a larger value of control current to obtain a given degree of saturation.


The current-gain of this amplifier (see Appendix) is defined as
$\frac{\text { Change of load current }}{\text { Change of control current }}=\frac{\mathrm{dI}_{\mathrm{L}}}{\mathrm{dI}_{\mathrm{o}}}$
The self-limiting action just described is quite analogous to that of the valve cathode follower. There is a high degree of inherent negative current feedback, with the result that control ampere-turns ( $\mathrm{N}_{\mathrm{c}} \mathrm{I}_{\mathrm{o}}$, see Appendix) and load ampere-turns ( $\mathrm{N}_{2} \mathrm{I}_{\mathrm{L}}$ see Appendix) are always equal, a univeral characteristic of basic non-feedback magnetic amplifiers. The power-gain of the amplifier (see Appendix) is easily seen to be $\frac{\mathrm{dI}_{\mathrm{L}}{ }^{2} \mathrm{R}_{\mathrm{L}}}{\mathrm{dI}_{0} \mathrm{R}_{0}}$ where $\mathrm{R}_{\mathrm{L}}$ and $\mathrm{R}_{\mathrm{o}}$ are the load and control circuit resistances respectively. Modest power gains of the order of 10 to 20 ( 20 to 26 dB ) are commonly attained. That is to say, the current gain is usually in the region of $\sqrt{ } 10$ to $\sqrt{ } 20$.

This simple amplifier has other disadvantages besides that of relatively low gain. A considerable voltage at the supply frequency is induced in the control winding. If we make $N_{\mathrm{o}}>\mathrm{N}_{\mathrm{L}}$ in order to enhance the current gain (which, as in the case of a transformer, is simply $N_{c} / N_{L}$ ) the induced voltage into the control winding may be very high indeed, and especially so since, owing to saturation, the loadcurrent waveform is non-sinusoidal. The power fed back into the control circuit is abstracted from that delivered to the load, and if the source of control

of the supply, has produced a pulsating d.c. current ( $\mathrm{I}_{f b}$, see Appendix) flowing in the closed loop around the load windings as shown, tending to saturate the cores, and so producing a high value of $I_{L}$ at $I_{c}=0$. This feedback current is seen to be strictly proportional to the load current, so that over the region of the right-hand branch of the characteristic, where the control and feedback currents are acting in the same sense in the individual cores in the appropriate half-cycles, the slope of the $\mathrm{I}_{\mathrm{L}} / \mathrm{I}_{\mathrm{c}}$ characteristic (and therefore the current gain) is greatly increased. Over the region of the left-hand branch. where $I_{c}$ and $I_{f o}$ are acting in opposition, the slope of the characteristic is correspondingly reduced.
In order to make use of this increased gain, another winding (the so-called bias winding) is for convenience provided, in order to set the working point, where $I_{c}=0$, at a convenient part of the characteristic.

In passing, the curious resemblance between the characteristic of Fig. 5(b) and that of the $I_{a} / V$ curve of a triode valve will be noted, and, in fact, with a high degree of feedback such as is usually attained in an amplifier of this type, it is possible to operate the amplifier in modes analogous with the Class A, Class B or Class C of the valve amplifier. In Fig. 5(a) the analogue of Class A operation is shown, where $\mathrm{I}_{\text {mean }}=\frac{1}{2} \mathrm{I}_{\text {, max }}$.

Consider now Fig. 6. If $\mathrm{N}_{\mathrm{L}}=\mathrm{N}_{\mathrm{C}}$ we have at all times that $\mathrm{I}_{\mathrm{L}}=\mathrm{I}_{\mathrm{c}}, \mathrm{dI}_{\mathrm{L}} / \mathrm{dI}_{\mathrm{c}}=1$ and the slope of the characteristic is $45^{\circ}=\theta_{0}$ when there is no feedback (i.e. when the rectifiers are omitted or are inoperative). With feedback (i.e. the rectifiers are operative) the right-hand branch of the characteristic subtends an angle $\theta_{1}$ and the left-hand branch subtends an


Fig. 4 The output-current/control-current characteristics of the amplifier in Figs. 2 and 3.
angle $\theta_{3}$ with the abscissa. If we assume a " feedback factor" due to the rectifiers, which factor we will call $\beta$, we find that

$$
\begin{aligned}
\theta_{1} & =\tan ^{-1} \frac{1}{1-\beta} \\
\text { and } \theta_{2} & =\tan ^{-1} \frac{1}{1+\beta}
\end{aligned}
$$

which define the increase and reduction of slope respectively. Bearing in mind that normally we use only the right-hand branch of the characteristic, the relationship between the current gain of the amplifier without feedback ( $\mathrm{A}_{0}$ ) and with feedback ( $A^{\prime}$ ) is simply

$$
\mathrm{A}^{\prime} \frac{\mathrm{A}_{0}}{1-\beta}
$$

and the change in current gain due to the action of the rectifiers is $1 /(1-\beta)$. In accordance with convention this change in gain may be expressed in "decibel" terms as $10 \log _{10}$ $A^{\prime} / A_{0}$ or $10 \log _{10} 1 /(1-\beta)$. It generally happens that in usual designs $\beta$ seldom lies outside the limits 0.94 and 0.99 . Therefore we can tabulate the change in gain due to the use of the rectifiers as follows:-

| $\beta$ | $\mathrm{A}^{\prime} / \mathrm{A}_{0}$ | dB |
| :---: | :---: | :--- |
| -0.94 | 16.7 | 12.25 |
| 0.95 | 20.0 | 13.0 |
| 0.96 | 25.0 | 14.0 |
| 0.97 | 33.3 | 15.25 |
| 0.98 | 50.0 | 17.0 |
| 0.99 | 100.0 | 20.0 |

As a simple numerical example, let us assume a transductor assembly with a normal power gain (without rectifiers) of 20 . This means a current gain of $\sqrt{ } 20$ or 4.45. If we now install rectifiers giving a feedback factor of say $95 \%$ ( 0.95 ), we cause two things to happen:-

1. We cause $I_{0}$ (which we have neglected in the immediate discussion above) at $\mathrm{I}_{\mathrm{c}}=0$ to increase to $20 \mathrm{I}_{0}$.
2. We cause the current gain to change from 4.45 $(6.5 \mathrm{~dB})$ to $89(19.5 \mathrm{~dB})$, a change of 13 dB .
If we can arrange to control, continuously, the effectiveness of the rectifiers, we have a means of controlling the inherent gain of the amplifier from $A_{o}$ to ' $A^{\prime}$, which range of control is dependent basically upon the value of $\beta$, as tabulated above. This can conveniently be done as indicated in Fig. 7, where $Z_{c}^{\prime}$ is a variable impedance (or resistance) shunting the rectifiers. Owing to the fact that it is not usually convenient to make $Z_{c}{ }^{\text {e }}$ large in comparison with the reverse resistance of the rectifiers, the full range of control of gain indicated in the table is not attained, but something pretty close to it (generally within 1 dB ) can be realized.

The writer has succumbed to the temptation to call this device a " variable- $\mu$ " amplifier for the
following reasons. The "variable $-\mu$ " valve is made by using a grid structure of variable pitch. As the static bias on this grid is increased in the negative sense, the fine-pitch (high- $\mu$ ) portion of the grid, by shutting off the anode current from the underlying portion of the cathode, becomes ineffective, whilst the coarse-pitch (low- $-\mu$ ) portuon of the grid remains effective. Notice that two things are happening here:-

1. There is a change in $\mu$, defined as $d V_{a} / d V_{g}$ ( $I_{a}$ constant), due to the change from a grid of high $\mu$ to one of low $\mu$.
2. There is a change in the mutual conductance $\left(g_{m}\right)$, defined as $d I_{u} / d V_{k}\left(V_{a}\right.$ constant $)$, due to the reduction in effective cathode area.

Which of these two effects is the more important


Fig. 6 Comparison of amplifie, characteristics with feedback (full line) and without feedback (broken line)."


Fig. 7 Method of controlling the effectiveness of the rectifiérs to get variable gain.


Fig. 8 A d.c. amplifier, with control of gain and mean level of output.
depends upon whether, corresponding with 1 and 2 above,

1. $\mathrm{Z}_{\mathrm{L}}$ (the load impedance) is much higher in value than the valve internal resistance ( $\mathrm{R}_{\mathrm{a}}$ ) and the valve is operating as a constant-voltage generator.
2. $\mathrm{Z}_{\mathrm{L}}$ is much lower in value than $\mathrm{R}_{4}$, and the valve is operating as a constant-current generator.

Since practically all variable $-\mu$ valves are tetrodes or pentodes, operating under condition 2 , the change in mutual conductance is the more important effect by far. The term " variable $\mu$ " is theretore (as other writers have pointed out) a misnomer, but sticks by reason of custom, and convenience. "Variable-mutual-conductance," "variable- $\mathrm{g}_{\mathrm{a}}$ " or "variable-perveance" (American) do not trip off the tongue so easily. "Variable $\mu$ " valves have the following characteristics-

$$
\mathrm{dI}_{\mathrm{a}} / \mathrm{dV}=k . \mathrm{V}_{6} \text { if } \mathrm{Z}_{\mathrm{L}} \ll \mathrm{R}_{\mathrm{s}} .
$$

In the magnetic amplifier under discussion,

$$
\mathrm{dI}_{\mathrm{L}} / \mathrm{d} \mathrm{Z}_{\mathrm{c}}=\mathrm{k} \cdot \mathrm{Z}_{\mathrm{c}} \text { if } \mathrm{Z}_{\mathrm{L}} \ll \mathrm{Z}^{2}
$$

where $Z_{i}$ is the internal impedance of the amplifier. This establishes an analogy. The validity of the term "variable $\mu$ " as generally understood falls


Fig. 9 Biasing point can be fixed for both high- and lowgain characteristics or varied to obtain greater signal handling capacity at low gain.
down in both cases if $Z_{L} \gg R_{a}$ or $Z_{i}$, and is only truly applicable in the classical sense in the case of the valve amplifier if $Z_{L} \gg R_{a}$, a condition which rarely obtains in practice.

The amplifier of Fig. 7 has another interesting attribute. It may be controlled by means of $Z^{\prime}{ }_{c}$ alone. As Fig. 6 shows, if bias and control windings are omitted, variacion of $Z_{C}$ causes $I_{L}$ to vary between the limits $I_{0}$ and $(1 / 1-\beta) I_{0}$. No source of control current is needed. The amplifier in effect provides its own control current. This is sometimes very convenient. In the conditions of either maximum or minimum output (or gain, when $\mathrm{Z}_{\mathrm{c}}^{\prime}$ is used as a gain control) the amount of power dissipated in $\mathrm{Z}_{0}$ is negligible, and is never greater than the amount of power dissipated in a control winding having the same resistance and number of turns as the control windings in series, for any given level of output power. The writer, for want of a better name, has dubbed this an "impedancecontrolled amplifier." He will be grateful if any reader can think of a better term.

Fig. 7 also indicates an amplifier with a normal control winding and a bias winding, $Z^{\prime}{ }_{o}$ then being used to control the gain, in "variable- $\mu$ " fashion. This can be done over a number of stages by the use of ganged variable resistances for the $\mathrm{Z}^{\prime}$ 's.
Fig. 8 shows an amplifier-a "d.c." amplifier in which the mean output level is set by means of the current in a bias winding, whilst the gain is controlled in the way already described. "Complementary" rectifiers are used to obtain a d.c. output.
There is one interesting difference between the magneric amplifier and its valve counterpart, a difference in favour of the former. In the variable- $\mu$ valve amplifier the "undistorted" signal-handling capaity of the amplufier is reduced at low values of controlled gain. This is otten inconvenient, since low values of gan are often required with large signals, and vice versa. In the case of the " variable $\mu$ " magnetic amplifier the signal-handling
capacity is restricted with increase of gain and vice versa. In the case of the valve amplifier, nothing can be done about this restriction in signal-handling capacity, since both the signal and the bias are operating upon the same electrode. In the magnetic amplifier separate "electrodes" (windings) are used, and it is possible, as Fig. 9 shows, either to work with a constant bias current, giving the same signal-handling capacity at both high and low gain, or to vary the bias in accordance with the input signal, by means of a circuit such as that shown in Fig. 10, in orde- to obtain greater signalhandling capacity at low gain setting. In this figure, an auxiliary bias winding is supplied with current derived from the load voltage, and acting in opposition to the normal bias current, reducing the effective bias as the gain is increased. This could of course also be done by means of the manually-controlled scheme of Fig. 11, which will usually be preferred.
One very useful feature of the d.c.-controlled magnetic amplifier is that any number of control windings of similar or differing current-gain values may be used, up to the limit that it is physically possible to install, and that there is no interaction between them. They may of course be connected to signal sources at widely different mean potentials, floating or earthed. Consequently such an amplifier is a useful computer component for algebraic addition, since

$$
I_{L}=I_{0}+\left(k_{1} I_{1}+k_{2} I_{2}+k_{3} I_{3} \ldots \text { etc. }\right)
$$

where $k_{1}, k_{2}$ etc. are the current-gain factors of the control windings, and $I_{1} I_{2}$ etc. the corresponding control currents. If in addi-ion we have the "variable$\mu$ " feature we have

$$
I_{L}=K_{V}\left(I_{0}+k_{1} I_{1}+k_{2} I_{2}+k_{3} I_{3} \ldots \text {.etc. }\right)
$$

where K is the controlled "variable- $\mu$ " gain, multiplying a number of algebraically added quantities by a common factor. "Circuitwise," as the Americans say, $\mathrm{I}_{0}$ can be eliminated in the output, one obvious method being by using a push-pull stage. This use of the amplifier is indicated in Fig. 12.
Finally, in Fig. 13, the results of an experiment upon a stage in which no attempt had been made to


Fig. 10 Amplifier with ouxiliary bias winding to give automatic bias setting with varying gain.
optimise the performance in any way, are shown. The various quantities are in linear units. Several interesting things appear. The current gain and power gain are roughly linear over the full range of $\mathrm{R}^{\prime}$. The voltage-gain behaves in a peculiar manner, being linear over the first $5 \%$ of $\mathrm{R}^{\prime}$ c and constant over the upper $50 \%$. The load resistance was of the optimum value, which for optimum efficiency is, as in the case of a triode valve, equal to $\mathrm{V}_{\mathrm{B}} / \mathrm{I}_{\mathrm{Lmax}}$. There is, it will be noted in this case, a classical "variable- $\mu$ " action over a small portion of the characteristic, but this is not of much practical importance since it amounts only to some 6 dB in range, whilst the whole of the variable-gain region amounts to roughly 14 dB .
The range of variable current gain obtainable with this type of amplifier per stage (about 20 dB as a maximum) does not seem impressive when compared with the $25-30 \mathrm{~dB}$ change obtainable with the variable- $\mu$ valve amplifier, but it is fully adequate for the great majority of applications. Most amplifiers


Fig. II Ganged manual control of bias and gain.


Fig. 12 Magnetic amplifier used as a multiplier or an adder.


Fig. 13 Characteristics of the amplifier on the right with different settings of the gain control $R_{c}^{\prime} . I_{L}=$ load current, $V_{L}=$ load voltage, $P_{L}=$ load power, $|A|_{L}=$ current gain, $|A|_{\nu}=$ voltage gain, $|A|_{p}=$ power gain.
of this type, if properly designed, will be working with a $\beta$ of about $96 \%$, which after allowing for the limitation in range of $\mathbf{Z}_{c}^{\prime}$, will give a variablegain (current) range of about $13-14 \mathrm{~dB}$ per stage. The numerical example given earlier corresponds closely
with the results obtained with an experimental amplifier built by the writer.
To conclude, the writer would like to acknowledge his indebtedness to his colleagues for technical assistance and constructive criticism.

## APPENDIX

## Nomenclature, explanations and definitions

$\mathrm{N}_{\mathrm{L}}$ : number of turns in series in the load circuit winding(s).
$\mathrm{N}_{\mathrm{C}}$ : number of turns in series in the control circuit winding(s).
$I_{L}$ : current (average a.c., or if rectified, d.c.) flowing in the load circuit.
$I_{\mathrm{C}}$ : current (d.c.) flowing in the control circuit.
$\mathrm{I}_{\mathrm{b}}$ : current (d.c.) flowing in the bias winding. ( $\mathrm{N}_{\mathrm{b}}$, the number of turns in series in the bias winding, is not mentioned in the text, as it is not necessary for purposes of explanation.)
$R_{L}, Z_{L}$ : resistance, impedance in the load circuit, exclusive of the resistance or impedance of the load windings of the transductor.
$R_{0}$ : resistance in the control circuit, exclusive of the resistance of the control windings of the transductor.
$R_{c}^{\prime}$, $Z_{c}^{\prime}$ : value of the gain-control resistance or impedance.
$\mathrm{L}_{8}$ : effective series inductance of the transductor in the load circuit.
$\mathrm{L}_{\mathrm{c}}$ : choke inductance used in control circuit of singlecore magnetic amplifier stage.
$\beta$ : the " feedback factor" due to the use of rectifiers. (In practice, generally lies within the limits $94-99 \%$.) $\mathrm{I}_{f b}$ : mean value of (pulsating d.c.) current ${ }^{\text {tlowisig in }}$ series with the load windings and "feedback" rectiters.

Current-gain: by definition, $\mathrm{dI}_{\mathrm{L}} / \mathrm{dI}_{\mathrm{c}}$, and by anatogy with customary (though incorrect) practice in the case of the valve amplifier, where the voltage gain is defined
as (in dB terms) $10 \log _{{ }_{10}} \mathrm{~V}_{n \boldsymbol{m}} / \mathrm{V}_{\mathrm{n}}$, we define the currentgain as $10 \log _{10} \mathrm{I}_{\mathrm{L}} / \mathrm{I}_{\mathrm{C}}$. This also gives $\frac{1}{2}$ the power gain, if $\mathrm{R}_{\mathrm{L}}$ and $\mathrm{R}_{\mathrm{L}}$ are equal.

Power-gain: by definition change of power in load change of power in control current source resistance.

$$
=\mathrm{dI}_{\mathrm{L}}{ }^{2} \mathrm{R}_{\mathrm{L}} / \mathrm{dI}_{0}{ }^{2} \mathrm{R}_{\mathrm{C}} .
$$

Voltage-gain: by definition $d V_{L} / d V_{0}=d I_{L} R_{L} / d I_{C} R_{0}$ and is not used in the text, because the magnetic amplifier is normally used as a current amplifier.
$A_{0}$ : the basic current-gain of the amplifier, as above defined, when $\beta=0$.
$A^{\prime}:$ the enhanced current-gain of the amplifier, when rectifiers are used, $\mathrm{A}^{\prime}=\mathrm{A}_{\mathrm{o}} /(1-\beta)$
$\mathrm{V}_{\mathrm{s}}$ : the supply voltage (a.c.).
$V_{\text {Ls }}$ : the voltage drop in the load circuit across the choke or transductor due to the load current.
$\mathrm{V}_{\mathrm{L}}$ : voltage across the load, average a.c. or (rectified) d.c.
$\mathrm{I}_{\mathrm{o}}$ : the magnetizing current (a.c.) of the transductor or choke. Defines the minimum load current, unless special arrangements are made.

Transductor: term used to connote the core-and-windings assembly used in magnetic amplifiers. It of singlecore type (as Fig. 1 in the text) it would be referred to as a "saturable reactor."

All gains are given in terms of current gain. Rough indicetions of power gains are obtained by squaring the lincar values, or doubling the dB values. The purist will object (and rightly) that this is only correct if we assume that input and output impedances are equal, but for changes in gain the objection does not apply.

# London Audio Fair 

NEW EQUIPMENT FOR SOUND REPRODUCTION

UJNFORTUNATELY space does not permit a description of all the new products shown at this year's Fair but a selection of those thought to be of more than usual interest is given in this review. While the main emphasis was on stereo, considering audio equipment generally, the most obvious changes were in a field parlly outside stereo, that of tape recording.

Tape Recording and Reproduction. -The many new tape recorders shown included two by Trix, a company whose products have previously been in other fields of audio. The "Everest" is a two-speed ( $3 \frac{3}{4}$ and $7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$ ) model with a specified frequency range of $30-12,000 \mathrm{c} / \mathrm{s} \pm 3 \mathrm{~dB}$ at $7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$ and a signal/noise ratio of 50 dB . The "Companion" is a single speed ( $3 \frac{3}{3} \mathrm{in} / \mathrm{sec}$ ) portable, weighing only 21 lb which incorporates the recently introduced B.S.R. "Monardeck" tape mechanism.

In the Tandberg Model 5 shown by the Harting-Tandberg group the track width has been reduced sufficiently to accommodate four instead of the usual two tracks on normal width tape. This model can reproduce tapes in which the four tracks are divided into two staggered stereophonic pairs; alternatively, erasure, recording and replay of the tracks one at a time is possible.

A considerably lower crosstalk figure is required for satisfactory recording and reproduction of independent rather than stereo signals, since the difference between the
crosstalk figure in the region of -50 dB or better is claimed for the Tandberg stereo Model 5 for four tracks, and for two-track stereo models shown by Reflectograph (Model 570) and Grundig (TK55).

The reproducing head magnetic gap length is now very frequently made as short as about $10^{-4}$ in so as to reduce the speed required to give a high-frequency response up to the region of the highest audible frequencies from $7 \frac{1}{2}$ to $3 \frac{3}{2} \mathrm{in} / \mathrm{sec}$. Unless care is taken in the design of the tape transport mechanism, wow and flutter are now likely to be the factors limiting quality when halving the speed from $7 \frac{1}{2}$ to $3 \frac{3}{4}$ in $/ \mathrm{sec}$. However, several of the new recorders claim acceptable total wow and flutter figures of about $0.25 \%$ at $3 \frac{\mathrm{in}}{4} / \mathrm{sec}$. A speed as slow at $+\frac{5}{8} \mathrm{in} / \mathrm{sec}$ is provided on the new Stuzzi "Tricorder". At $1 \frac{7}{8} \mathrm{in} / \mathrm{sec}$, the next higher of the three speeds available, the response is stated to be 3 dB down only at $8 \mathrm{kc} / \mathrm{s}$ and the wow and flutter only $0.3 \%$ r.m.s. Up to $5 \frac{3}{4}-\mathrm{in}$ diameter reels can be handled and space for an extra head and amplifier is provided. For office use, stethoscope type headphones for taking dictation from the recorder and an adaptor for recording telephone conversations are available. Remote control facilities are also provided.
Independent level adjustment and mixing facilities for two or more
channels are now fairly often incorporated into tape recorders. The use of d.c. to heat the filaments of valves amplifying low-level signals, so as to reduce the hum level, was also noted in several cases. No pressure pads are used in a number of the newer models (notably throughour the 「elefunken range) and one possible source of head wear is thus avoided.

Tape tension is made more constant in the Telefunken M85 series by using a spring-loaded finger on which the tape bears. As the angle formed by the tape at the finger alters with the amount of tape on the reel, the component along the tape of the force due to the spring alters so as to reduce changes in the tape tension.

American Ampex professional tape recorders, including their tape duplicator series $\mathrm{S}-3200 \mathrm{C}$ for copying $3 \frac{3}{4} \mathrm{in} / \mathrm{sec}$ or $7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$ master tapes at a speed of 30 or $60 \mathrm{in} / \mathrm{sec}$, are now available in this country from Rank Cintel.

Special features of a small studio recorder shown by Telefunken (M23) include 4 -charnel mixing facilities, a recording level meter calibrated in dB , and alternative type of plug-in head assembly which can be located accurately enough to avoid the need for additonal azimuth adjustment. A smooth fade-in on pre-existing recordings is automatically obtained by bringing the tape gradually into contact with the erase and recording heads.
Reflectograph were brave enough to demonstrate stereo recording as well as subsequent reproduction. Two ribbon microphones, spaced about three feet apart and angled slightly outwards and downwards, were placed about a foot above an accordionist who moved about in


Right: Tandberg Model 5 four-track reproducer with add-on unit for stereo
recording on the left.
Above: Reflectograph stereo recorder with the two halves of the lid containing the monitor loudspeakers detached.
front of the microphones while playing. The sizë of the room was only about 10 ft by 12 ft , but the experiment was completely successful.

Two transistorized recorders were seen. One of these, the Stuzzi Magnette, has already been described in Wireless World (June 1958, p. 276). The other is the Fi-Cord whose size is only $9 \frac{5}{8}$ in $\times 510 \times 2 \frac{5}{8}$ in and which weighs only $4 \frac{1}{2} \mathrm{lb}$ This recorder is unusual in that the ratio of the two available speeds of $7 \frac{1}{2}$ and $1 \frac{7}{6} \mathrm{in} / \mathrm{sec}$ is four rather than the almost universal two to one. Four special miniature 2-V accumulators are used, and a charger is supplied. A high-frequency transistor oscillator supplies the erase and bias voltages and also the h.t. for the valve level indicator.

Tape of half the standard thickness giving double the playing time of standard tape for the same reel size or $33 \frac{1}{3} \%$ more playing time than longplaying tape of two thirds of the standard thickness, was introduced by E.M.I., B.A.S.F., M.S.S. and M.M.M. (Scotch Boy). A p.v.c. base chemically s:milar to that generally used for standard thickness tape was used by B.A.S.F., whereas M.S.S. and M.M.M. (Scotch Boy) used a polyester base.

Pickups.-An unusual mechanical arrangement seen in the Go dring 700 variable-reluctance stereo pickup uses a cantilever pivoted about its middle rather than one end. This enables the two sets of magnetic gaps to be placed one at each end of the cantilever rather than both at one end. By thus separating the gaps crosstalk problems are reduced. The lateral and vertical compliances are both $4 \times 10^{-8} \mathrm{~cm} /$ dyne and the effective mass at the stylus tip is 8 mgm .

In the Connoisseur crystal stereo pickup, by using two very small ( 0.2 in $\times 0.06$ in $\times 0.025$ in) ceramic crystals and partially de-coupling the crystal assembly from the stylus in the usual way by means of a rivid cantilever, the effective stylus tip mass has been reduced sufficlent.y to rase the resonance between this mass and the record groove wall compliance up to about $18 \mathrm{kc} / \mathrm{s}$.

An effective stylus tip mass of only 0.6 mgm has been achieved in a new Cosmosord mono crystal cartr:dge. An unusual feature of this cartridge is that the compliance of $12 \times 10^{-8}$ $\mathrm{cm} /$ dyne is provided in the cantilever itself which is not rigid This cartridge was mounted in a specially balanced arm whose static side thrust and vertical frictional forces are equivalent to only 0.02 and 0.05 gm respectively The arm is little affected hy external vibrations. The design of the pickup has already been described in Wireless World (April issue, p. 182) and the design of the arm will be described in a forthcoming issue.
A modification of Cecil Watts' "Dust Bug" which can be clipped on to most pickup arms and which is recommended for use with record changers was shown by Cosmocord. A downward-bearing spring counteracts the weight of the "Dust Bug", whose tracking angle can be adjusted. The decrease in stylus and record wear resulting from the removal of dirt in the grooves more than compensates for any harmful effects due to an increase in the side thrust caused by friction between the "Dust Bug " and the record.

Radio Tuners.-An impressive specification is quoted for the Avan-

Top (left) ond bottom (right) views of the Fi-Cord tronsistorized tape recorder in a speciol transparent cover.

tic combined v.h.f./f.m. and medium wave a.m. tuner type BM612. For f.m. reception two i.f. stages and two limiters precede the Foster-Seeley discriminator to give a sensitivity of $2 \mu \mathrm{~V}$ for an a.m./f.m. rejection ratio of 50 dB . A.f.c. is provided, and the extent of this can be varied to avoid the "capture" by strong stations of neighbouring weak stations whose reception may be desired. Interstation noise suppression to a variable extent is available with both a.m. and f.m. reception. The a.m. selectivity is $\pm 4.5 \mathrm{kc} / \mathrm{s}$ for a 6 dB loss in output.

Pre-amplifiers and Amplifiers.-A stereo balance control range of up to about $\pm 4 \mathrm{~dB}$ is now frequently provided. Such a control can be simply obtained by connecting the fixed ends of a single potentiometer at similar points in each of the two amplifiers. The connections must be made where the movable contact on the potentiometer will be earthed (so that crosstalk is eliminated) and also, of course, where the resistances in the potentiometer can influence the gain. As the balance control potentiometer is altered, the gain of one channel is increased while that of the other is reduced. If the average gain is arranged to remain the same, readjustment of the level control will probably be unnecessary.

Ganged pairs of switched precision resistors were used instead of ganged potentiometers for the level control in the Rogers HG88 and Jason J4-4 amplifiers so as to reduce variations in the balance as the level is altered.
Very comprehensive facilities for checking balance are provided in the Stereosound PP6 amplifier. The balance between the two amplifiers and pre-amplifiers can be checked by feeding $100 \mathrm{c} / \mathrm{s}$ ripple from the h.t. before smoothing to both inputs in parallel. The outputs from the two amplifiers are sampled at special tertiary windings on the output transformer, backed off against each other, and fed to a valve tuning indicator. Maximum separation of the illuminated portions of the indicator shows zero input, and thus correct balance of the amplifier. The balance of the whole system, including loudspeakers, can be aurally checked using an internally generated approximately sawtooth oscillation. This oscillation also is fed equally to both inputs in parallel, and the balance control adjusted until the metronome-like sound appears to come from mid-way between the two loudspeakers.
Two types of channel switching are frequently offered: the two signals can be interchanged between the two reproducing systems and the phase of one of the two signals can be reversed.
Although Lowther have shown low-level transistor amplifying stages for some time as separate units, such

Right: Goodmans Triaxiom 12/20 loudspeoker with crossover unit mounted on the magnet.


Wharfedale Coaxial 12 loudspeaker with tweeter level control.

Right: Stereosound PP6 amplifier incorporating visual and oudible methods of checking balcince.

stages are only now being incorporated into complete pre-amplifiers. Examples were shown by Lowther and Sound Sales (A-Z). Steep-cut low-pass filters in which the cut-off point can be continuously varıed were noticed in the Lowther control units and Rogers HG88 amplifier.

Mixing units using valves are already available from several manufacturers, and a simple high-impedance resistive unit can now be supplied by T.S.L.

Those who like to "roll their own" will be pleased by the appearance of several stereo amplifier kits such as those shown in the Audio Fair by Altobass and Jason, for example. For amplifying the signals from pickups on musical instruments such as the guitar, the 10 -watt Valencia made by Grampian combines amplifier and loudspeaker in a single baffle/cabinet with readily accessible tone controls.
Loudspeakers and Cabinets.-An interesting system of mounting was shown by Rogers in their 1284 3 -speaker system. The 8 -in and 12 in low-frequency speakers are connected in parallel and mounted at the top and bottom respectively of a column chaped cabinet $37 \mathrm{in} \times 15 \mathrm{in} \times$ 14 in . The 12 -in speaker faces a normal carcular opening (equal to the effective cone size) in the bottom of the cabinet. The 12 -in speaker is, however, spaced $1 \frac{1}{2}$ in from its opening so that this space forms a reflex port for the radiation from the rear of the speakers. The opening in the bottom of the cabinet is filled with a layer of foam plastic $\frac{8}{\text { in }}$ thick so as to add resistive loadings to bath the front of the 12 -in speaker and the port. The foam plastic also prevents all frequencies above about $200 \mathrm{c} / \mathrm{s}$ from being radiated from the bottom
of the cabinet, thus producing a crossover effect between the two bass speakers. The foam plastic layer furthermore tends to act as a secondary diaphragm. This arrangement is claimed to result in damping of both the normal resonances of a reflex cabinet, and also lowering of their frequency by a factor of about 1.4 down to about $75 \mathrm{c} / \mathrm{s}$ and $35 \mathrm{c} / \mathrm{s}$.

The analogue computer for investigating the effect of various parameters (including resistive loading in var.ous places) on both the steady and transient response from reflex loudspeaker cabinets which was described in our April issue (p. 162) was shown by Exco.
Two methods of avoiding cabinet wall resonances used by Wharfedale in their new speaker systems are the inclusion of $\frac{3}{4}$ in polystyrene panels mechanically strengthened on both sides by a thin skin of plywood in their PST/8, and the gluing and battening of ceramic tiles in critical positions in their W3 and W4 cabinets.

In small cabinets, for an inward cone excursion the temporary increase in the air pressure inside the cabinet may be considerable over an appreciable range of frequencies. If this causes the surround to balloon outwards, not only is the tension exerted by the surround on the cone increased and more non-linear distortion thereby produced, but furthermore, the sound from the surround will be out of phase with that from the rest of the cone and some cancellation will occur. For this reason a more rigid than normal surround must be used for speakers in small cabinets. A single halfwave corrugation of rubber-treated resin-impregnated fabric forms the surround for the Wharfedale WLS/12 which has been specially
developed for sole use in their relatively small W2, W3 and W4 reflex systems.

New coaxial speakers were shown by Goodmans and Wharfedale. Two concentric magnetic gaps with completely separate cones are used in the Wharfedale Coaxial 12. The angle of the 2 -in diameter inner tweeter is only about 80 degrees. This tweeter is fitted with an inner aluminium dome and the total weight of its moving parts is only 1 gm . The Goodmans Triaxiom 12/20 actually has three cones. The outer two are mechanically connected in the usual way so that at higher frequencies where the radiation from the large outer cone falls off because of its weight the lighter inner cone takes over and tends to move by itself to prevent any overall loss in output. The innermost tweeter magnet and cone are completely separate. The cone is loaded by a horn of elliptical cross-section so that dispersion is wider in a plane parallel to the breadth of this ellipse than in a plane parallel to the length.

A number of modifications have been made to the well-known Tannoy dual concentric coaxial loudspeaker. The useful flux in the gap for the low-frequency outer cone has been increased by about $20 \%$ by reducing the overall magnetic reluctance by partially shunting the gap for the high-frequency inner diaphragm at the rear of the magnet. This shunt is made so thin that it becomes magnetically saturated. The field in the high-frequency gap, which is limited by magnetic saturation at the pole pieces. thus remans unchanged. The rear of the highfrequency daphragm is now damped by a small cavity with a hole in it which is filled with acoustically resistive material.

## LETITERS TO THE EDITOR

The Editor does not necessarily endorse the opinions expressed by his correspondents

## Evaluating Aerial Performance

MR. C. F. WHITBREAD'S letter in the April issue raises two points which could usefully be further discussed. These are (a) the extent of the validity of my approximations, and (b) the practice of feeding a receiving aerial into a matched load although considerations of noise-factor dictate a mismatch. Matching is, I believe, standard commercial practice and mainly justified by the fact that the bandwidth of many commercial aerials would not be adequate without it.

Bandwidth as defined in my article is a property of the aerial only and takes no account of what is done between the aerial terminals and the grid of the first valve in the receiver. Use of a matched load should tend to double the bandwidths given by my formula.
Generally speaking I would say that if the bandwidth given by the formula is less than the required systembandwidth one or other of a number of undesirable consequences tend to follow, such as the necessity of a matched load, or the various effects listed in my discussion of standing wave ratio in the second part of the article. I have not yet had a chance to check up on the references, but referring to p. 864 of Terman ("Radio Engineers' Handbook ") Fig. 101 (which is after Schelkunoff) confirms my formula over a bandwidth of at least $25 \%$ to within the accuracy to which the curves can be read. The resistance variation, to which your correspondent refers, introduces some asymmetry in the impedance characteristic but is not significant in relation to the context.
The average characteristic impedance of an aerial (Terman, loc. cit.) is given by $276 \log _{10} \frac{\text { length }}{\text { radius }}-120$ and comes to about 550 ohms for a Channel 1 dipole made from 1 -in tubing, so that from my formula, $B=\frac{4}{\pi} \times \frac{73}{550} \times 44=7.4 \mathrm{Mc} / \mathrm{s}$. Doubling this on the assumption of a matched load gives $14.8 \mathrm{Mc} / \mathrm{s}$ which is not far short of your correspondent's figure of $17.25 \mathrm{Mc} / \mathrm{s}$. The impedance plot shows a change of only $\pm 15 \%$ in the resistive term over the bandwidth used in my example.
L. A. MOXON.

## Long Distance U.f.f. Reception

I WAS extremely interested in Mr. H. V. Griffith's article in your April issue, as I have myself been making fairly regular observations on sporadic-E propagated signals in Band I since 1955.
In general my observations have only served to corroborate previous evidence concerning the prevalence and behaviour of sporadic-E propagation, but in view of Mr. Griffith's article I would like to make the following comments, which may be of interest.

Over the path from Europe to Tangier, at distances of 1,000 to 1,500 miles, sporadic- E propagation is considerably more prevalent than over the paths observed at Tatsfield. Observations made during 1955/1958 gave the following results, in terms of days on which signals were observed:-

$$
\begin{aligned}
& \text { 1955-July 1st to August 31st ........... } 32 \\
& \text { 1956-Tune 10th to September 14th } \\
& \text { 1957-May 8th to August 14th } \\
& \text { September 8th to October 8th ..... } 64 \\
& \text { 1958-April 22nd to June 30th }
\end{aligned}
$$

Over the months May/August signals were observable on more than $50 \%$ of the days. By far the most prevalent, and the strongest, signals came from the various B.B.C. television transmitters. On some occasions these signals provided pictures of entertainment quality for a whole evening. Signals were also observed from Belgium, Czechoslovakia, France, Germany, Holland, Italy, and Switzerland. I believe that it has been stated, I think by Mr. Bennington, that paths of the order of 1,000 to 1,200 miles are the best from the point of view of sporadic-E propagation. This may account for the prevalence of such signals in Tangier, which lies at an ideal distance from the source of many television transmissions in Band I.
During 1956 and 1957 I was also in a position to observe some channels in Band III. These observations showed that during some periods of sporadic-E activity, signals of up to nearly $100 \mathrm{Mc} / \mathrm{s}$ were being propagated. Between June 30th and July 14th, 1956, a B.B.C. transmission on $89.1 \mathrm{Mc} / \mathrm{s}$ was heard on three occasions, and an Italian transmission on $89.9 \mathrm{Mc} / \mathrm{s}$ once. During 1957, between May 18th and August 11th, the B.B.C. on $89.1 \mathrm{Mc} / \mathrm{s}$ was heard on 19 occasions, a German station on the same frequency on four occasions, and an Italian station on $89.9 \mathrm{Mc} / \mathrm{s}$ also on four occasions. In addition, at a station some 100 miles south of Tangier, a German f.m. broadcast station caused severe interference on $93 \mathrm{Mc} / \mathrm{s}$, on July 31st and August 1st.
J. E. le B. TERRY,

Tangier, Morocco. RCA Communications, Inc.

## Alternatives to the Wien Bridge

WITH regard to Mr. J. F. Young's comments in your April issue, I should like to point out that the reference in General Radio Experimenter, Vol. 6, November, 1931, describes the use of a Wien Bridge for the measurement of audio frequency by balancing the bridge network and not for a resistance-capacitance tuned oscillator.
Resistanze-capacitance oscillators appear to date from 1921 when a U.S. Patent $1,442,781$ was filed by Nichols describing a single-stage amplifier giving $180^{\circ}$ phase shift together with a 4 -section resistance-capacitance ladder network. However, the earliest references to the $W$ ien Bridge and similar circuits as the tuning element of an oscillator which I was able to locate after an extensive search made some years ago are those given in my letter published in your April issue.

London, W. 5 .
W. V. RICHINGS,

Dawe Instruments, Ltd.

## Printed Circuits

IT is interesting to follow the correspondence with regard to the disadvantages of printed circuits to the servicing engineer.
As specialists in the development and manufacture of printed circuits, we appreciate the need, not only for the development of new types of processes and applications for printed circuits but to ensure their advantages and popularity with manufacturers, users, and that most important last link in the chain, the man who has to maintain the apparatus in efficient working order.
For this reason we have introduced as a new development (patent pending) the printing on the top (component) side of printed panels a mirror image of the circuit in colour. This means that when the components are mounted the panel, the main cause of criticism that, to quote Mr. Kisch in the March issue, "a disjointed array of resistors and capacitors fixed apparently at random and one is unable to see the interconnections," no
longer applies and the engineer sees a complete traceable circuit. Of course, as most components, valve holders, etc., normally have bare metal or wire ends on the top side of the panel, it is possible to fault-find with the normal test equipment on the component side of the panel.

## D. L. PHILLIPS,

Coventry. $\quad$ Mills \& Rockleys (Production), Limited.
I HAVE followed the letters re printed circuits with great interest. I would like to add my views on this important subject. I agree with Mr. Flack only on the point that printed circuits should not really be so difficult to service as claimed. We have surmounted many obstacles in the past, we remember amongst others the chassis without an inspection flap at the bottom of the cabinet which was separate to the tube, and could not be tested outside its cabinet without either extending the leads or having a special lead adaptor from the makers, and the multi-chassis monstrosity which defied any attempt to service it until it was completely dismantled from its cabinet and precariously assembled all in separate pieces on the bench.

Let us cut out the humbug and realize that printed circuits are here to stay on one count only, cheapness. We are all well aware that wiring failures have never been even a factor in television or radio breakdowns compared to other causes. The odd dry joint has arisen, but the printed circuit is equally prone to this. Without insulting anyone's intelligence, it is obvious that the conventional chassis with its greater flexibility of wiring can withstand vibrations better.
Regarding the points raised about tracing faults in printed circuits. I regard these as red herrings, correct interpretation of meter readings must invariably reveal the fault and in the old-type chassis makers often bound their wires in tight bundles in any case, making tracing just as hard. Mr. Flack appears to have taken a peculiar stand in a. technical journal, for if he wants greater reliability why not start much higher up the scale with say, valves, controls, line output transformer, etc.? What about designing sets well within the valve maker's ratings? Will he now tell us that the present-day sets using only 14 valves are more reliable because they have fewer valves to give trouble?

Let me hasten to say, however, that I believe we are forced to accept printed circuits, etc., because the trade must keep competitive to maintain a high level of employment. I only want to be completely honest (at least in this journal) and face up to the undeniable fact that the printed circuit, those banks of shoddy, preset controls, the 14 -valve chassis are retrograde steps in quality, but forced upon us by the iniquitous purchase tax.
I cannot but admire the ingenuity displayed by the manufacturers in producing cheaper, bigger screens, glossier cabinets, brighter pictures, in spite of rising costs, and how they manage to prune substantial amounts of solidity with every succeeding model and still get the performance they do. Happily, the customer rarely looks inside, and we, the servicing fraternity, have never counted anyway Even though the compromise between design and production has invariably worked out to the detriment of the service engineer the public are getting cheaper and cheaper sets, and even they can't have it both ways.

London, S.W. 18.
J. L. WILDGOOSE.

MAY I, on behalf of all service engineers, thank Mr . Flack for descending from the Olympus of the golfing weekend, to discuss the problems of the poor souls, towards whom the passing buck inexorably gravitates.

In the matter of printed circuits, his company is not among the most hated. There are, however, among the silent observers, those to whom the criticisms iustly apply, including one ingenious designer, save the mark, who, having backed his printed panel by a stout metal plate and anchored it firmly in position by short connecting leads, proceeds to fit valves through the plate!

There has also been introduced a new, diabolical method of securing control knobs which has I am sure, caused consternation in the courts of heaven.

In conclusion I firmly believe, in company with all other service engineers, that the incredible mistakes that are made, includin: the urgent circular commanding modifications to be carried out to protect customers from eloctrocution, are not the work of idiots but are part of an international plot, designed to ensure that most technicians will be in mental homes in the event of their services being needed in a national emergency!

Leigh-on-Sea.
L. W. TURNER.

## Rigidity of L.S. Diaphragms

FURTHER to Mr. H. A. Hartley's letter in your March issue, on the effect of damp on foam plastic, I have soaked a prece of expanded polystyrene in water for five weeks, and its modulus in bending, measured while still wet and before drying out is almost unchanged, i.e., the material has not become limp. In practice, when foil or other materials are used to form sandwiches, not only will the foil reduce water absorption, as Mr. Hartley suggests, but even if water absorption does occur, the bending stiffness will be unaltered. as it depends almost entirely on the skins (see article p. 564 , Dec. 1958 issue), the core being merely a lightweight device to keep the skins apart and to prevent them from buckling. If Mr. Hartley's material gives trouble, I can only conclude that it is not the same type as mine and that with correct choice of plastic water absorption is not a problem.

Banbury.
D. A. BARLOW.

## Plymouth Effect

I WAS very surprised to read in your December 1958 issue that the flutter effect which Mr. Grant has labelled "The Plymouth Effect" is still being puzzled over, so I would like to put forward my observations, the conclusions I came to and "the way around the problem" I found quite satisfactory before I left Plymouth in early 1957

The sharpish ridge known as Maker Heights over which the signals have to pass is around 450 ft in height and causes considerable upcurrents of air or turbulence, similar to convectional currents, and somehow the warm rising air meeting the colder upper air presents alternative paths to the signals, reflecting and refracting them. I reached this conclusion after 'scoping and noticing the amplitude variations in Cawsand and making use of a highly directional radar device from approximately the same route as the signals would meet the ridge, which gave not only the expected solid response signals from the ridge but gave, when moved up approximately 150 ft above the ridge, a group of continually varying signals at the same range above the ridge in space. Thus, the transmission having to pass varying paths, the signals received in Cawsand arrived in and out of phase with each other, varying in amplitude considerably. Lines were pulled when overall delays occurred, and there were overall brilliance variations also.

I found the best way round the problem was to screen " H " aerial from direct transmissions and to 6 wing it $70^{\circ}$ out to sea. and thus receive the re-radiated transmissions from Staddon Height aerials lattice masts (fin horizontally to the right on your December maps) and use the $40 \%$ of the "direct" signal-thus making use of the main ghost noticed on direct reception without any ghosting whatsoever.

Just before I left I did contact Mr. Cooms of the B.B.C. to suggest the possibility of improving the reflecting surface of the Staddon Height masts to give us a better "ping off".

Hoping the above may help to lay the TV ghost of our village before my return in May 1960

Singapore.
A. MAYHEW.


Self-Monitoring Colour Tube to give automatically the correct chrominance balance in a colour television receiver is suggested as a possibility by J. J. Belasco and J. J. Chantrill in B.B.C. Engineering Monograph No. 23 (February, 1959). The proposed tube is a single-beam type working on the beam-indexing principle-the red, green and blue colour signals being gated to modulate the beam according to its position as it scans red, green and blue vertical phosphor strips. In this respect the tube is similar to the wellknown Philco "Apple" c.r.t. (January, 1957, issue, p. 2) but instead of the beam-position information being obtained by a secondary emission process a photoelectric system is used. This involves vertical strips of photoconductive or photoemissive material laid on the viewing side of the fluorescent screen to correspond with the colour phosphor strips. All the red photo-sensitive strips are connected together and similarly with the green and blue strips, and the resultant three connections provide signals for gating purposes. The chrominance balancing system makes use of a small group of photosensitive strips at the edge of the picture, masked from view and not connected to the others. These are activated by a white bar produced by injecting a pulse into the video amplifier during the line suppression period. They consequently monitor the red, green and blue components which are combining to form the white bar. The voltage outputs from the monitoring strips are compared with reference voltages which have the correct relative proportions to form white when combined. The colour error signals so produced are then used to adjust the gain of each colour channel for the following line period.

Compatible Stereo "left" and "right" signals from widely-spaced (about 6 ft or more) microphones are possible according to Bell Telephone Laboratories. The Bell modification to the ordinary left and right signals to make them compatible depends on the psycho-acoustic phenomenon known as the "precedence" or Haas effect. This effect arises if two identical or simlar cound waveforms are reproduced at different places at nearly equal intensity levels with a delay of between 5 and 35 msec
between them, when the apparent loudness of the delayed or e $e$ ho sound is reduced by about 10 dB below its actual intensity. The Bell modification combines each stereo signal with the other signal delayed by about 10 msec and with its level reduced by about IdB When both the !eft and right modified channels are reproduced then, berause of the Haas effect, the delayed signals are each masked by the corresponding undelayed signals on the other channel, so that apparently only the left and right signals are repruduced, as required. When only one channel is rep:oduced the combination of one signal with the other one delayed and at a slightly reduced level is said to provide a compatible signal This modification has been developed primarily for use with stereo broadcasts in which a seorate transmission is used for each channel, but in which an unmodified receiver tuned to only one of the two transmissions is requrred to give a compatible signal.

Levitation, though normally associated with the occult, can be achieved on strictly physical principles with an apparatus recently demonstrated by G.E.C. Research Laboratories. In this a small bar permanent magnet is made to hang in mid-air a

few inches below an energized electromagnet. Normally, of course, the bar magnet would either drop to the ground or fly up to the electromagnet. The secret of the trick is therefore to adjust continuously the field of the electromagnet so that its pull just balances the pull of gravity on the bar magnet. This is done by a servo system. The energizing current in the electromagnet is made to depend on phase variations in a tuned circuit which are produced by a disc of metal on top of the bar magnet altering the inductance of a coil mounted on the electromagnet. A $2.6-\mathrm{Mc} / \mathrm{s}$ oscillator supplies two signals to a phase detector, one direct and one through the sensing tuned circuit containing the coil. Phase changes in the tuned circuit due to movements of the bar magnet are thereby detected, and they produce a signal which is used to control the electromagnet current in a corrective sense. Positive feedback has to be applied in the control system to achieve stability.

Solid Circuits is the name given to small blocks of semiconductor material in which transistor, diode, resistance and capacitance elements are formed into complete circuits bv snecial manufacturing techniques of diffusion, etching, masking, deposition, etc. (see Nov. 1957 issue, p. 516). They have now reached the stage of commercial development and are expected to be available for certain applications in the U.S.A. some time during the year. Texas Instruments recently exhibited two examples. each measuring less than $\frac{1}{4} \mathrm{in} \times \frac{1}{8} \mathrm{in} \times \frac{1}{5} \mathrm{in}$. One was a multivibrator circuit, containing as integral parts of the semiconductor material the equivalent of twelve normal electronic components-two diffused-base transistors, two capacitors and eight resistors. The other was an oscillator contarning the equivalent of nine components-one transistor, five resistors and three cavacitors. The whole object of solid circuits is, of course, to reduce drastically the size and weight of electronic apparatus in such things as satellites, airborne equipment and computers. The criterion here is "component density" (though "volumetric efficiency" is sometimes quoted), and with solid circuits it is 34 possible to achieve densities of up to 34 million components per cubic foot. This compares with several thousand per cubic foot for conventional circuitry.

High-Temperature Diode, made of the semiconductor material gallium arsenide. is another recent introduction by Texas. Instruments in America It is said to be capable of operating in the extremely wide tem$+325^{\circ} \mathrm{C}$ range of $-65^{\circ} \mathrm{C}$ to $+325^{\circ} \mathrm{C}$.

# Elements of Electronic Circuits 

## 2.-CLAMPING OR D.C. RESTORATION

By J. M. PETERS, B.Sc. (Eng.), A.M.I.E.E., A.M. Brlt. I.R.E.

I

T is sometimes necessary for the potential at a point in a circuit to be restricted to variations within fixed limits. The use of a clamping diode makes this possible. The name is chosen because the vave


Fig. 1.
appears to fix or "clamp" the point to the desired potential.

A common arrangement using a diode and CR circuit is shown in Fig. 1. For the purpose of explaining the action of this circuit we will assume that the peak voltage of the applied square wave $V_{A}$ in Fig. 2 is 20 volts.
(i) The application of 20 volts to R (AB in Fig. 2) causes the diode to conduct.
(ii) When the diode conducts R is short circuited, hence the time constant is very small. C quick y charges to 20 volts, causing $V_{R}$ to decay to zero (BC).


Fig. 2.
(iii) $V_{A}$ now falls from $C$ to $E$, i.e., from +20 volts to -20 volts. So -20 volts is applied to the circuit. $\mathrm{V}_{\mathrm{o}}$ is, owever, also ai -20 volts, hus making the voltage across the resistance $\mathrm{V}_{\mathrm{B}}=-40$ volts.
(iv) Since the anode of the diode is now negative with respect to the cathode the valve does not cond.ct. Consequently as the time constant CR is $\mathrm{n} \sim \mathrm{w}$ ong, C only discharges ery sligh ly (EF).
(v) When $V_{A}$ goes from $F$ to $G$ the applicd vortage again becomes +20 volts. $V_{c}$ is, however sti, only about -19 voits, making $V_{\mathrm{g}}=+1$ volt.
(vi) $C$ quickly charges, $V_{R}$ quickly falls to zero again and the cycle is repeated. Except, therefore, for a very small positive excursion at the commencement of the positive-going applied pulse, the maxi-
mum positive value of $\mathrm{V}_{\mathbf{\Delta}}$ is "clamped" to zero volts.

It can also be shown that if the diode connections are reversed as in Fig. 3, $\mathbf{V}_{\mathrm{B}}$ is made all positive and


Fig. 3.
the maximum negative value of $\mathrm{V}_{\Delta}$ is "clamped" to zero. In each case a direct voltage component is introdiced int the origınal applied waveform, -20 volts in the circuit of Fig. 1 and +20 volts in the circuit of Fig. 3. It is often said that d.c. (voltage) restorat on takes place under these conditions.

We will now consider what happens when .. buasing voltage is applied to "the diode. With the diode biased. the "clamping" voltage may be made as required. In the example in Fig. 4 au. input square wave of 30 volts peak (Fig. 5) is applied to .


Fig. 5.
diode whose cathode is biased at +10 V . The result is as shown in the lower part of Fig. 5, where the maximum positive excursion of $V_{A}$ is clamped to +10 volts. Similarly, if the bias is reversed the maximum negative excuston of $\mathrm{V}_{\mathrm{A}}$ is clamped to -10 volts.

Now let us consider the use of a triode valve for clamping. Here, as shown in Fig. 6, the grid and


Fig. 6.
cathode act as a diode to the applied square wave $\mathrm{V}_{\mathrm{A}}$, which, for the purposes of the description, is assumed to be 10 volts peak (Fig. 7). $\mathrm{V}_{\mathrm{g}}$, the grid voltage, is therefore clamped to zero. The negative excursion of the input wave will now exceed the cut-off bias of the triode, with the result that the anode voltage waveform $\mathrm{V}_{\mathrm{a}}$ is clamped to h.t.

It is important to note that, as illustrated in Fig. 7, a peak nput voltage of 10 V can cut off a valve which has a cut-off bias of 15 V . This is due to the intro-


Fig. 7.
duction of a -10 V d.c. component which makes the maximum negative excursion of the applied voltage $\left(\mathrm{V}_{\mathrm{g}}\right)=-20 \mathrm{~V}$.

Before leaving this section it may be of interest to note that applying a similar treatment to the diode detector in conventional radio circuitry may offer a more satisfactory explanation of its operation than that sometimes given in textbooks.

## CORRECTION

In the first paragraph of last month's article (p. 156) the sentence beginning "If the input voltage is maintained at steady value. ." should continue to read as follows: ". the voltage across "the resistor will drop as the capacitor $C$ charges chrough $R$. This rate of charge through the resistor depends on the values of $C$ and $R$; the greater the values of $C$ and $R$ the longer will this time be." Also, the next paragraph should begin: "On discharge, it can be shown from theory . . ."

## High-Voltage Generaior

EQUIPMENT for generating voltages up to about one megavolt is finding increasing application in industry for such purposes as testing high-voltage cables, insulators and switchgear, as well as for use in electron microscopes, X-ray apparatus and various kinds of particle accelerators.

Miles Hivolt, Ltd., who in this country market the


The three units of the Madel CD600/4 high-voltoge generotor with oil-filled output cable on supporting stand.
high-voltage generators made by the Société Anonyme de Machines Electrostatiques of Grenobles, recently demonstrated one of the S.A.M.Es. $600-\mathrm{kV}$ generators at their works at Shoreham Airport.

The Model CD600/4, as this $600-\mathrm{kV}$ generator is known, will give 4 mA output, which, while not impressive by this figure alone, actually represents 2.4 kW at 600 kV . This equipment is relatively small in size, being easily assembled in a single vehicle if necessary and, complete, weighs a little over $2,000 \mathrm{lb}$.

These are electrostatic generators (once called "influence machines") and closely resemble the Van de Graaff generator in principle, though not in form.

Basically the S.A.M.Es. generator consists of a stationary glass cylinder (the stator in the diagram) with another cylinder of insulating material (the rotor) revolving around it at relatively high speed. A positive charge is "sprayed" on to the revolving cylinder from electrodes $P$ and $P^{\prime}$, the priming charge being provided by an auxiliary generator $G$. The charge is carried round to the collector electrodes C and $\mathrm{C}^{\prime}$ where the voltage builds up to the working value. Prototype generators of this kind were shown at the Physical Society's exhibition in 1951 and 1954.
The CD600/4 generator consists of three main units, a pressurized electrostatic convertor unit, auxiliary electronic generator and remote-control console; these three are shown in the photograph. The pressurized unit contains the glass stator, rotor and its driving motor and the high-voltage resistance network and stands 8 ft l0in high. It is filled with hydrogen at a pressure of about 25 aumospheres, and is water cooled. The rotor


Schematic arrangement of the S.A.M.E. electrostatic highvoltage generator.
driving motor is a three-phase machine running at about 2,800 r.p.m. Cooling water circulates in the pressurized unit at between 1 and 2 gallons a minute.

The auxiliary, or priming generator, consists of a r.f. oscillator, high-voltage unit and a small electrostatic generator and provides priming voltages of from 10 to 50 kV according to the output required. It is built into a floor-standing cabinet 4 ft 4 in high and includes voltage-regulating and stabilizing circuits and the various safety devices essential in high-voltage generators. Voltage stabiluzation is $\pm 1 \%$ of the selected output in the Model CD600/4 and it can be as close as 1 part in $10^{5}$ in some of the high-stability versions of these generators, such as, for example, the $50-\mathrm{kV}$ model "Samtron 50."

The remote control console is a cabinet 3 ft 3 in high and houses equipment for selecting and measuring the priming and output voltages and current.

Comprehensive safety and protecting devices are in-
corporated in the equipment and it would seem impossitle to damage any apparatus used with the generators by accidental flash-over, internally or externally. If sparking occurs the electromagnetic waves radiated are picked up by a relescopic aerial on the auxiliary generator unit and this "signal" is used to suppress the proming voltage and the output falls to zero. After a brief interval of time it slowly builds up again to the exact pre-selected value. Voltage or current overloads also "trip" the generator. The total consumption of the CD600/4 is about 3.5 kW .


RADIO CONTROL FOR THE CANBERRA U Mk. 10:-Short Brothers and Harland Limited have produced a remote control system for this aircraft which is used as on unpiloted "target" for guided missile tests. The Canberra is controlled from the ground vio o v.h.f.-radia link, the commands being in the form of pairs of tones. Twenty-four of these pairs are available and a transponder is installed in the aircraft to improve its radar "visibility" The photograph shows part of the interiar of the control station.


THE full-line curves indicate the highest frequencies likely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during May.
Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period.

# Long-Distance Propagation 

DETAILS OF FORTHCOMING TESTS BETWEEN ASCENSION ISLAND AND SLOUGH

THE Department of Scientific and ${ }^{\text {ndustrial Research }}$ with the co-operation of Cable and Wireless, Ltd., will in June set up an experimental radio station at Ascension Island, from which two of their staff will conduct test transmissions to their Radio Research Station at Slough, Bucks, for a year. The object of the tests will be to investigate propagation over long distances.
The D.S.I.R. officer in charge of the project at Slough is A. F. Wilkins, who was closely associated with Sir Robert Watson Watt in the early development of radar. The two officers going to Ascension are L. A. Brackstone and R. Aria. On the Cable and Wireless side, arrangements have been made by R. J. Hitchcock, head of the section dealing with radio propagation, who is also a member of the Ionospheric Communications Committee of the Radio Research Board.
Explaining the objects of the tests, Mr. Hitchcock writes:
"Over certain parts of the earth's surface we now know a great deal about the characteristics of the ionized layers of the upper atmosphere by means of which highfrequency radio communication is established. But we do not know much about the exact path followed by radio waves in the course of their journey from transmitter to receiver, and this, in spite of the fact that commercial high-frequency circuits have been in operation for the past 30 years or more. The actual paths taken by radio waves are called the 'modes of propagation,' and it is to unvestigate the nature of these modes that the tests at Ascension Island have been planned.
"It may well be asked why such investigations are necessary, for if we point a directional transmitting aerial in Nairobi towards, say, London, and use the right order of frequency for the route, the signal will in all probability be receivable in London. The answer lies in the fact that, in common with all forms of engineering, it is becoming increasing!y important to do the job efficiently. In Cable and Wireless, Led.'s particular case, the necessity providing the spur is an ever-increasing congestion of the radio spectrum, an increasing demand for reliability and, possibly the most important factor of all, an ever-increasing demand for additional channels on existing and planned circuits.
"Considered academically, high-frequency systems are exceedingly wasteful, for although signals are required only at the few acres where the receiving aerials are located, they fall over great areas of the earth's surface to no useful purpose. Furthermore, we have no assurance at present that we are in fact putting down the maximum possible energy at the point where it is required. These are the sort of problems we must tackle if we are to improve the efficiency of our radio systems and remain competitive in the rapidly progressing communications world.
"Preliminary investigations into modes of propagation have been going on for some years, and many will recall the transmissions already made from the Ascension Island relay station for the D.S.I.R. Useful though these transmissions have proved, they were only a start, and we now go deeper into the matter with more complex and specialized apparatus.
"A receiver and transmitter have been developed at

Slough which, even if separated by great distances, may yet remain accurately in tune with one another while the radio frequency is automatically changed.
"This particular equipment is capable of sending and receiving signals on nearly 2,000 different frequencies between $5.5 \mathrm{Mc} / \mathrm{s}$ and $50 \mathrm{Mc} / \mathrm{s}$ in the space of about 15 minutes.* Only the transmitter will go to Ascension. The receiver will remain at Slough, where the signals will be observed and analysed.
"Possibly, from the Cable and Wireless point of view, the most important group of experiments will be those associated with aerial effects. Aerial design is largely dictated by propagation considerations, and an interesting series of tests is planned to see the effects of shooting into the ionosphere at different angles. We have always wanted to know the best angle to the horizon at which we should transmit radio energy on long radio routes, and all the indications at present are that this angle should be very low. In this experiment three dipoles at different heights above ground are to be erected on a 150 ft mast. By placing this mast as near as possible to the water's edge and transmitting from each dipole in turn, it is possible to alter the shape of the vertical polar diagram of transmitted energy and to see what effect this has on the received signal at Slough. It is believed that this is the first time a controlled experiment of this nature has been made. In addition, our own rhombic aerials at Ascension Island will be used to test the effects of good and poor sites as represented by having sea in front of one aerial and rock in front of the other.
"Although we shall not be making any direct observations in connection with the new 'forward scatter' techniques now being used foi communications, we shall be using a very important new technique based on the radar principle, and developed by A. F. Wilkins and his colleagues, to measure 'back scatter.' This is the small fraction of energy scattered back to the transmitter from the ground reflection areas along the radio path. The technique shows not only the location of these areas, but also indicates the relative strengths of the signals in these areas. A change of frequency and/or aerial can substantially change the 'back scatter' pattern, and its value to the transmitting engineer, in ensuring that he is covering the reception point with the strongest possible signal, can be appreciated.
"We should not overlook the effect this project is having in expanding our good relations with the D.S.I.R. In recent months A. R. Harrison, Manager at Ascension Island, S. G. Crow, the previous engineer at Ascension, and J. Berry, his relief, have all visited Slough to inspect the equipment and discuss details of the project.
"We know the D.S.I.R. would very much like to carry out the next series of large-scale experiments from Singapore, to which place one piece of research equipment is already on its way. With our extensive traffic commitments between there and the U.K., we must look forward with particular interest to the results of investigations into the complexities of this route."

[^5]
# A Second Band-III Programme? -The Aerial Problem 

Requirements for Wide-Band Coverage With Useful Gain

By F. R. W. STRAÏFORD,^ M.I.E.E.

(Concluded from page 174 of the April issue)

THE previous article dealt with the conventional Yagi array and showed that such aerials were less efficient than simple dipoles when operated three channels from the optimum design frequency. Since Yagi aerials represent by far the largest proportion of Band-III installations. and are particularly concentrated in the fringe areas, it will be seen that quite a serious problem must be overcome before the fateful day.

The lazy way of approach is the add-on technıque which, in this instance, would mean duplication of the existing aerial optimized for the additional channel and somehow erected over the already overcrowded chimney and connected through yet another dinlexing filter to the input feeder. Remembering that the greatest problem will exist in the genuine fringe area where double-stacked sixelement Yagis mounted on 12 ft poles are commonplace, the prospects are quite alarming.

Obviously, the


Fig. 1. Basic half-wave dipole (a). the equivalent series circuin for Jeriving intrinsic bandwidth (b) and equivalent series circuit for deriving loaded bandwidth (c). sensible long-term approach is to replace the existing Band -III aerial with one which will receive both stations with equal efficiency. In order to rationalize production the aerial should cover the whole frequency band, namely, 174$216 \mathrm{Mc} / \mathrm{s}$. The two extremities of this band are already occupied by other services but the P.M.G. has pledged to release them for the television service in due course.

It is the object of this article to study the requirements for the design of a wide-band aerial capable of providing a directive gain of the order of 9 dB , and to suggest the lines upon which development might proceed.
Bandwidth of a Half-wave Dipole. - Whether a single dipole with reflector, or a combination of suitably connected dipoles are used, the bandwidth must be $42 \mathrm{Mc} / \mathrm{s}$ when operated into a $75-$ ohm feeder and load resistance. In this instance the loss should not exceed 1.0 dB at the extremities.

[^6]The 3-dB handwidth has been studied, empirically, by various workers including the author ${ }^{1}$ and it would appear that a bandwidth of about $84 \mathrm{Mc} / \mathrm{s}$, that is, twice the desired coverage, based upon $3-\mathrm{dB}$ points will result in a $42-\mathrm{Mc} / \mathrm{s}$ bandwidth for the $1-\mathrm{dB}$ loss which is the target in this instance.
The intrinsic $3-\mathrm{dB}$ bandwidth of a half-wave dipole, fed at the centre, may be derived empirically by replacing the dipole by a loss-less quarterwave transmission line in series with a resistance equal to the radiation resistance of the dipole referred to the centre, Figs. 1(a) and (b). For a cylindrical dipole Schelkunoff ${ }^{2}$ calculates an average character stic mpedance $Z_{c}$ given by the formula:-

$$
Z_{r}=120\left(\log _{2} 2 l / r-1\right) \quad \ldots \quad . . \quad 1.0
$$

The input impedance of the equivalent dipole circuit of Fig. 1(b) is:-

$$
\begin{aligned}
Z_{1} & =\mathbf{R}_{a}+Z_{c} \operatorname{coth} \frac{j \pi l}{\lambda} \\
& =\mathbf{R}_{a}+Z_{c} \operatorname{coth} \frac{j \pi}{2}\left(1 \pm \frac{\delta \lambda}{\lambda_{o}}\right) \\
& =\mathbf{R}_{a}+\mathrm{i} Z_{\cdot} \tan \frac{\pi \delta f}{2 f_{a}}
\end{aligned}
$$

where $t_{n}$ is the resonant frequency. The $3-\mathrm{dB}$ halfpower points occur when the resistive and reactive components are of equal magnitude, i.e. when

$$
\mathrm{R}_{a}=\mathrm{Z}_{\mathrm{c}} \tan \frac{\pi \delta f}{2 f_{n}}
$$

Equating and solving for $\delta f$ we obtain:-

$$
\delta f=\frac{2 f_{o}}{\pi} \tan ^{-1} \frac{\mathrm{R}_{a}}{\mathrm{Z}_{c}}
$$

The total bandwidth is given by:-

$$
\Delta t=2 \delta f
$$

So that:-

$$
\Delta t=\frac{4 f_{r}}{\pi} \tan ^{-1} \frac{\mathbf{R}_{a}}{\mathrm{Z}_{r}}
$$

Since the ratio $R_{a} / Z_{c}$ is always much less than unity, equation 1.1 may be further simplified as $\tan x$ equals $x$ for small values. Hence we may now write the general empirical formula for the total 3-dB bandwidth of a centre-fed halfwave dipole as:-

$$
\Delta t \doteqdot \frac{4 f_{n} \mathbf{R}_{a}}{\pi \mathrm{Z}_{r}}
$$

This result was also derived by Smith ${ }^{3}$ by an alternative approach.

Equation 1.2 is very useful for preliminary design
work and has been experimentally confirmed ${ }^{1}$. These results for the calculated and measured bandwidth for a very thin dipole checked remarkably well, but there was some discrepancy for the thicker dipole. This was due to overlooking the fact that the radiation resistance for the thick dipole was lower than that for the thin one so that equal values for $\mathrm{R}_{a}$ were used in both calculations. Had a lower value of $\mathrm{R}_{a}$ been inserted in the thick dipole calculation much closer overall agreement would have been reached.
The interesting point about equation 1.2 is that it gives the intrinsic bandwidth for the $3-\mathrm{dB}$ points. In the presence of a load resistance equal to the radiation resistance, and this is the practical arrangement, Fig. 1(c), the bandwidth now becomes:-

$$
\begin{align*}
\Delta f & =\frac{4 f_{o}\left(\mathrm{R}_{a}+\mathrm{R}_{T}\right)}{\pi \mathrm{Z}_{c}} \\
& =\frac{8 f_{o} \mathrm{R}_{a}}{\pi \mathrm{Z}_{c}} \quad \cdots \quad\left(\mathrm{R}_{a}=\mathrm{R}_{T}\right)
\end{align*}
$$

Hence, the working bandwidth is twice the intrinsic bandwidth, so that by working on the basis of 3-dB intrinsic bandwidth one automatically obtains the $1-\mathrm{db}$,working bandwidth as previously explained.
As a starting point for preliminary calculations, let the dipole radius be 0.25 in . The mid-band frequency is $195 \mathrm{Mc} / \mathrm{s}$ and $l$, which is about $90 \%$ of a physical quarter-wavelength, works out to 13.75 in . The radiation resistance of such a dipole, erected at least one wavelength from the ground and clear of surrounding conductors, is of the order of 50 ohms. Combining this data in equations 1.0 and 1.2 the required $1-\mathrm{dB}$ loaded bandwidth works out to $34.5 \mathrm{Mc} / \mathrm{s}$, so that the 0.5 -in diameter dipole does not make the grade since the bandwidth is less than the required $42 \mathrm{Mc} / \mathrm{s}$. In order to meet the requirement it will be found that the elements must be increased to 2 in in diameter, but this is accompanied by a drop in radiation resistance to about 40 ohms. The mis-match loss to a 75 -ohm load through a 75 -ohm feeder will be slightly less than 0.4 dB , but this must be added to the IdB loss at the margins of the band, and one must not forget the inherent feeder losses-they all add up!
The dipole need not have cylindrical elements. It is an advantage to employ a shape which provides a low value of average characteristic impedance but maintains the radiation resistance nearer to the 70 ohms of the thin dipole. The bi-conical dipole of Schelkunoff ${ }^{2}$ achieves this objective. The basic


Fig. 2. Basic bi-conical dipole (Schelkunoff) shown at (a) with a skeletonized equivalent using thin flored rods.

3. Three methods of arranging eight half-wave dipoles to produce a gain of 9 dB . (a) has an area of 65 sqft , (b) an area of 67.5 sq ft and (c) an area of 47 sq ft . Dotted lines represent booms and masts.
arrangement is shown in Fig. 2(a) but the cones may be skeletonized by the use of a bundle of flared rods, Fig. 2 (b), with little effect on its properties.
The bi-conical dipole possesses the rather amazing properties of having constant values of distributed inductance and capacitance per unit length so that the exact characteristic impedance may be calculated.
This is given as:-

$$
\mathrm{Z}_{0}=120 \log _{e}(\cot \theta / 2)
$$

Note that when $\theta$ is very small:-

$$
Z_{0} \doteqdot 120 \log _{\mathrm{t}} 2 l / r
$$

This latter expression is used to derive the average characteristic impedance of a thin cylinder by integrating equation 1.5 between the limits $l=0$ and $l=l$ from which equation 1.0 is obtained.

A bi-conical dipole constructed of six $14-\mathrm{in}$. rods 0.25 in in diameter and flared so that $\theta=20^{\circ}$ has a characteristic impedance of 260 ohms and a radiation resistance of 70 ohms. Substituting these values in equation 1.2 the loaded $1-\mathrm{dB}$ bandwidth is $66 \mathrm{Mc} / \mathrm{s}$ and is more than adequate for full Band-III coverage. By reducing $\theta$ to $5^{\circ}$ the $1-\mathrm{dB}$ bandwidth is just $42 \mathrm{Mc} / \mathrm{s}$. In these circumstances, however, it is a more practical proposition to use simple cylindrical rods or tubes of about 1.0 in diameter to obtain the same result at the expense of somewhat lower radiation resistance. Gain and Directivity.-Having shown that a fat dipole, suitably shortened to maintain mid-band resonance, will provide adequate wide-band response it remains to consider how one or more of these
may be arranged to provide a power gain of, say 9 dB as a fairly modest target.

The power gain of N dipoles, spaced at east 0.75 wavelength to reduce mutual interaction, and connected so that all values of instantaneous induced currents are in phase at the feeder input, is given by:-

$$
G=10 \log _{10} N(d B) \ldots
$$

To obtain 9 dB gain N must equal 8 and this number of dipoles must be stacked in some convenien. manner of which Figs. 3(a), (b) and (c) are examples. All these arrangements present quite formidable mechanical problems in terms of mounting them on chimney stacks and providing adequate strength for $80 \mathrm{~m} . \mathrm{p} . \mathrm{h}$. wind gusts. A further problem is that of connecting all dipoles in the appropriate phase. Series connection of dipoles does not work when unbalanced coaxia' feeder is used-in fact, it does not seem to work at all well when balanced open-wire feeders are used. Parallel connections must therefore be made to the main feeder and the net impedance must be suitably transformed to match its characteristic impedance, which is usually of the order of 75 ohms. If N elements are connected in parallel, each having a radiation resistance of 50 ohms, the resultant resistance presented to the main feeder will be $50 / \mathrm{N}$ ohms so that eight elements will amount to 6.25 ohms. If no transformation is introduced the mis-match less into a 75 -ohm feeder will exceed 5.0 dB , which would be intolerable. The mis-match may be removed by the use of the transforming properties of feeders whose electrical length is made any odd integral multiple of one quarter-wavelength. Such a feeder terminated by a resistance $R_{o}$ has an input resistance given by $\mathbf{R}_{i}=Z_{o}{ }^{2} / \mathbf{R}_{a}$ so that $Z_{n}=\sqrt{\mathbf{R}}, \overline{\mathbf{R}_{a}}$. It is desired to connect eight 50 -ohm dipoles to a main feeder of 75 ohms characteristic impedance so that each interconnecting feeder must present an impedance of 600 ohms. Hence, the characteristic impedance of each inter-connecting feeder will be given by $\mathrm{Z}_{n}=$ $\sqrt{50 \times 600}=175$ ohms. Lines having this characteristic impedance are readily constructed from 0.25 -in diameter rods spaced abour 2.25 in between centres. According to the mode of connection the array may be given omnidirectional, bi-directional, or uni-directional characteristics. To maintain a high signal-to-noise ratio and minimise the effects of multi-path reflections a uni-directional array must be chosen, in which case the arrangement of Fig. 3(b) would have to be used and fed in such a manner that the currents in the left (or right) set of dipoles were lagging in phase by $90^{\circ}$ with respect to the other set. Unfortunately the quarter-wave transformer is frequency selec-tive-it must obviously be so-and the use of inductive and/or capacitative parallel stubs must be included and laborious
adjustments made to give the desired overall bandwidth. These adjustments are invariably made by using apparatus for the measurement of the standingwave ratio of the reflections set up in the main feeder and an overa I figure of less than two-to-one must be achieved before the performance can be regarded as satisfactory for the stringenc requirements that have been set.

From the viewpont of stacked dipo es the arrangement of Fig. 3(c) is desirable since the major support comprises the mas which need not be more than, say, 15 ft in length. By introducing the $90^{\circ}$ phase shift in one set of elements the uni-directional characteristics will be obtained and the gain will rise by a further 2.5 dB , the theoretical limit being 3 dB
Corner-reflector Aerial.-An aiternative, and very simple, cerlaı giving al forward gain of the order of 9 dB with good directivity, and which uses only one dipole, is the corne. reflector which has been very thoroughly nvestigated by Moullin ${ }^{4}$. The reflector need not be constructed from sheet material, an open-mesh netting, or a row of rods, may be substituted provided that their spacing does not exceed 0.1 wavelength A manageable, although not altogether attractive sample, was made by the author for operation on Channel 9 prior to making a further mode on a reduced scale for uperation it the B.B.C. experimental trequency of $654.25 \mathrm{Mc} / \mathrm{s}$. This atter aerial was described by the author in a previous article ${ }^{5}$ The origina model was designed for Channel 9 because measurements were more readily available in terms or existing measur.ng apparatus.

Fig, 4 shows a plan of the corner-reflector aerial in which the fal dipole is placed at a distance $d$ from the apex. When the included angle is $90^{\circ}$ Moullin obtains the .wo curves relating power gain and radiation resistance to $d$ in terms of wavelength These curves are based upon the assumption that the reflector is of infinite length and breadth. Moullin goes on to show that the reflectors may not only be made finite in size, but may be reduced to practica proportions without serions change in


Fig. 4. Variation with spacing (d) of radiation resistunce and gain for a corner-reflector aerial.


Fig. 5. Polar diagram of the corner-reflector aerial.
characteristics. It will be observed that, up to $d=\lambda / 2$ the radiation resistance rises from zero, through 72 ohms up to 120 ohms while the power gain remains flat at 10 dB . Fron $d=1 / 4$ to $\lambda / 2$ the mis-match loss to a 75 -ohm feeder will not exceed $1.6 / 1.0$ so that less than 0.3 dB will be lost. If, therefore, the dipole is located at a distance $d=31 / 8$ from the apex a deviation of $\pm 33 \%$ about the design frequency can be allowed. Since only $\pm 10 \%$ is required for complete coverage of Band III the attractiveness of this simple aerial will be obvious. The author constructed an experimental corner reflector for Channel $9(194.75 \mathrm{Mc} / \mathrm{s})$. The overall dimensions of each leg were 5 ft long and 3 ft wide and consisted of $0.25-\mathrm{in}$ diameter rods spaced 6.0in apart. The dipole consisted of two $1.75-\mathrm{in}$ diameter tubes 12 in long and tapered to 0.25 in diameter over the last two inches from the centre to which the coaxial feeder connections were made. A forward gain of a little over 9 dB was obtained with a front-to-back ratio of 14 dB and a beam width between half-power ( $3-\mathrm{dB}$ ) points of 65 degrees.

Four sharp minima, very useful for de-ghosting, in excess of 40 dB were observed towards the rear. The directional response is shown in Fig. 5. This is plotted in dB which does not make it appear in such a flartering light as the conventional voltage-ratio scale, which the author does not support since it does not link up with all the other parameters of a complete TV system from transmitter to receiver, where everything else is expressed in dB.

The projected area of this aerial on the axis of the beam is about 21 sq ft which is considerably less than anything obtained by stacking sufficient dipoles to give the same gain. There is no reason why the rods comprising the reflector should not be replaced by wire netting of $6-\mathrm{in}$ mesh suitably reinforced at the corners to give self-support. Such an aerial should give comparable results and a fairly low windage might be achieved by the use of the latter form of construction.
Summarising, there does not appear to be any simple way of providing the unique properties of the Yagi array over a wide frequency range without recourse to a much larger structure with its attendant mechanical problems. This contention would appear to be supported by a study of the theoretical and experimental work carried out to date, and particularly, by examination of specifications for wide-band aerials designed for television transmitters and general v.h.f. and u.h.f. telecommunications equipment.

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## Principles of Transistor Circuits

ANYONE who is about to embark on the design of transistorized equipment, and has had no previous experience of transistors, is faced with a wealth (or shall we say a welter?) of literature on the subiect, ranging from advanced physical treatises through complex network analyses to the most superficial of popular treatments. There is a great need for a concise introduction to the design of transistor amplifiers, receivers and other circuits, which will give the student, engineer or amateur constructor only the sort of information that is really essential to his purpose.
Such a book has just been issued by our publishers"Principles of Transistor Circuits" by S. W. Amos, B.Sc. (Hons), A.M.I.E.E. Assuming no previous knowledge of the subject, it starts off with two chapters on the physical principles and electrical characteristics of
transistors. But the main emphasis is on the application of these principles to the practical problems of design, and the bulk of the book is concerned with the determination of such quantities as input resistance, stage gain, optimum load, power outdut, values of coupling capacitors and transformer winding inductances.

The mathematics is confined to simple algebraic manipulation and is illustrated by a large number of numerical examples, which show the order of practical magnitude of the various quantities. Some details are included of photo-sensitive devices, transistor relaxation oscillators, and the newer types of high frequency transistors.
The book, which contains 167 pages and 105 diagrams, is available from booksellers, price 21 s , or direct from our publishers at 21 s 11d including postage.

# Convention on Stereophony 

INTERESTING PAPERS AND LIVELY DISCUSSION AT THE I.E.E.

1LMOST every conceivable aspect of stereophony was discussed at the excellent two-day convention held recently at the Institution of Electrical Engineers in London, but only the more recent developments or lesser-known aspects of the subject which were discussed are reported here. The full papers and discussion will be published in the Proceedings of the Institution.

Theory of Hearing.-F. H. Brittain described some of the results on stereophonic listening which have been obtained by Dr. B. Sayers and Dr. D. M. Leakey working under Professor C. Cherry at the Imperial College of Science and Technology. These results indicate that in hearing the position of a sound source is obtained from the difference between the times of arrival at the two ears of the sound, as distinct from the intensity difference at the two ears of the sound as has sometimes been thought. The variations of this time difference produced by head movements as small as one tenth of an inch are used to remove the ambiguity as to whether the sound source is in front or behind (both positions would produce the same sounds at the ears).

When listening to two loudspeakers in a stereophonic system each ear hears both loudspeakers, but the sounds at each ear from the two loudspeakers apparently combine to form a single sound provided that the time difference between the sounds from the two loudspeakers is less than about 0.5 msec . For longer time differences up to about 3 msec , such as might be produced by off-centre listening or a spaced-microphone recording technique, partial apparent combination at each ear of the sounds from the two loudspeakers can still occur.

The apparent arrival time of each combined sound relative to the arrival times of each of its two constituent sounds from the two loudspeakers depends on the relative intensities of these two constituent sounds, and also, for delays between the two constituent sounds of more than about 0.5 msec , increasingly on the arrival time of the earlier of the two sounds. This latter phenomenon is known as the Haas or precedence effect.
The difference between the apparent arrival times of the combined sounds formed at each ear gives the apparent single source position. Thus intensity differences between the two loudspeakers are converted in hearing into apparent time differences between the two ears. This somewhat surprising asymmetry between sounds from the loudspeakers and the corresponding sounds at the ears can (in case any readers are sceptical about it) be derived trigonometrically (see for example the paper by H. A. M. Clark, Dr. G. F. Dutton and P. B. Vanderlyn in Proc.I.E.E. Part B, Vol. 104, Sept. 1957, p. 422). This asymmetry arises because each ear hears both loudspeakers-an elementary fact of loudspeaker as distinct from headphone stereophonic reproduction that is sometimes forgotten.

Reproducing Conditions-Rooms.-In stereophonic reproduction interfering reflections from the walls of the listening room should be avoided by absorbing material in suitable positions according to T. Somer-
ville of the B.B.C. In the excellent B.B.C. demonstrations, given at the I.E.E. during the convention, reflections were avoided by hanging curtains so as to form a sort of room within a room.

The deliberate use of reflections from the room walls using directional loudspeakers has been suggested as a means of producing apparent loudspeaker sources farther apart than the actual loudspeakers and thus as a means of increasing the apparent size of the overall sound field beyond the region between the two loudspeakers. However, this increase will not occur for the reverberant sound which consists mainly of low frequencies at which loudspeakers are not directional.

Reproducing Conditions-Loudspeakers.-A discrepancy between the apparent size of the reverberant and direct sound fields also arises in the sometimes used system in which signals at frequencies below about $300 \mathrm{c} / \mathrm{s}$ in the two channels are added together and reproduced by a single loudspeaker. This economical system is generally advocated on the grounds that stereo information is mainly confined to the upper frequencies and that sound source positions can be located less and less accurately as the frequency decreases. This latter point was challenged by H. A. M. Clark and by F. H. Brittain who stated that he had been able to locate mortars fired on Salisbury Plain at great distances to an accuracy of one degree although their sound on arrival did not contain any energy above $50 \mathrm{c} / \mathrm{s}$ and had a maximum energy at $20 \mathrm{c} / \mathrm{s}$.
Compatibility.-A combination of the two stereophonic signals to form a single signal which can be reproduced by ordinary unmodified single-channel equipment so as to sound as good as or only slightly inferior to the corresponding non-stereophonic signal is said to be compatible.

The sum of the left and right stereophonic signals is often stated to be compatible, but a number of criticisms of this view were put forward in two papers by T. Somerville and D. E. L. Shorter of the B.B.C. This sum signal is least compatible when a multi-microphone recording technique has been used. Such a technique may be necessary to correct for poor acoustics and is often used in "pop" music or drama to correct the relative intensities of the various parts of the sound source. When the alternative of a single pair of coincident (or nearly so) microphones is used its optimum position may not be the same as that for a single microphone for a single-channel recording. Also when a coincident microphone recording technique is used, this sum signal may be equivalent to that from a microphone of unsuitable polar response, though according to Dr. W. S. Percival this response can be improved by altering the phase of one of the stereophonic signals by ninety degrees before addition. Incidentally, use is often made of the fact that signals obtained with microphones with one kind of characteristic can be combined to produce signals which would have been produced by microphones with different polar responses. When a pair of spaced microphones is used the difference between the times of arrival of the same sound at the two microphones may produce some cancellation at
various frequencies th the sum signal. A revealing earopener was provided in the B.B.C. demonstration when, with a soprano, choir and orchestra, the emphasis on the soloist was very much greater when the sum of the left and right signals rather than the stereophonic recording was played.

Broadcasting.-Two new systems were mentioned by T. Somerville and D. E. L. Shorter. These use primarily amplitude modulation, and this can be at frequencies in the ordinary medium waveband as distinct from the more usual frequency-modulation multiplex systems at v.h.f. In the R.C.A. system the left- and right-hand signals are carried one on the upper and the other on the lower sideband, so that this might be described as a double single-sideband system. An ordinary detector will give an output proportional to the sum of the left- and right-hand channels. In the Philco system the sum of the left- and right-hand signals is used to amplitude-modulate the carrier in the usual way and provide a compatible output from an ordinary unmodified receiver, while the difference berween the left- and right-hand signals is used to phase-modulate the carrier. The difference modulation is confined to frequencies above $300 \mathrm{c} / \mathrm{s}$ to avoid certain complications in the receiver circuit. In both these systems distortion is possible in the detector when one modulation is much deeper than the other.

In an interesting paper by J. J. Geluk of the Netherlands Broadcasting Union (some of the results from which have also been given by the same author jointly with H. J. van der Heide in E.B.U. Review, Part A (Technical) for Feb. 1959, p. 15) a comparison was made between a number of versions of the v.h.f./f.m. multiplex system in which the sum of the left- and right-hand signals is used to frequency-modulate the main carrier and provide a compatible signal for an unmodified receiver, while the difference between the left- and right-hand channels is used to frequency-modulate a sub-carrier of the main frequency. In all the cases considered the total maximum deviation was kept at $75 \mathrm{kc} / \mathrm{s}$ while being sub-divided in various ratios between the two modulations. Three factors of importance in comparing various systems are the loss in the power transmitted from the main compatible carrier caused by the power which must be diverted to maintaining and modulating the sub-carrier; the differing amounts of filtering between the carrier and sub-carrier necessary to secure a sufficiently low cross-talk and finally, the various amounts of spurious radiation which could cause adjacent-channel interference. A possible detector for the difference signal was described using four double-triodes in which the difference signal is used to synchronize a multivibrator. By limiting the output from the multivibrator rather than limiting the difference signal itself very efficient limiting is obtained. With efficient receiver limiting, the sub-carrier deviation can be decreased so that the power loss on the main channel is only 2.7 dB and also cross-talk between the two signals and spurious radiation are reduced.

Systems in which the sub-carrier is amplitude rather than frequency modulated were also considered by Geluk. The detector can be simpler than with an f.m. sub-carrier, but the r.f. stages are more difficult to design, since a flat amplitude response over the channel bandwidth is required to avoid distortion rather than the more easily obtained flat phase response required for an f.m. sub-carrier. The cross-talk tends to be higher using an a.m. sub-carrier so that, unlike the case with an f.m. sub-carrier, it is unlikely that two

Independent signals could be satisfactorily transmitted. As was pointed out by D. E. L. Shorter, a time-division multiplex system would be equivalent to using a subcarrier spaced by the switching frequency and a.m. by the difference signal.

In considering the optimum division of available power between the sum and difference signals, it is often assumed that the peak level in the sum is considerably greater than that in the difference. In fact, the usual difference between these levels is only about 4 dB , according to Shorter, and can be less even than this value.

Considerable interest was aroused by the discussion of the Percival system, of which some details have already been given in Wireless World (Vol. 64, Nov. 1958, p. 521) and in which the directional information is separated from the signals themselves and processed so as to occupy a bandwidth of only about $100 \mathrm{c} / \mathrm{s}$. The processing is primarily based on the Haas or precedence effect which can be stated in the form that in hearing the apparent direction of a sound is determined primarily from the first few milliseconds of it. Thus the directions of a number of nearly simultaneous sounds can be apparently given by stereophonically reproducing only their beginnings provided that these beginnings are not simultaneous to within a few milliseconds. Even when the whole orchestra is supposed to start together the attacks of the individual instruments seldom coincide exactly and the system usually remains unbeaten. The processing of the directional information thus mainly consists in heavily weighting the initial transients of signals.

One advantage of separating the directional from the main signal is that the latter signal can be obtained from one or more microphones independently of the directional signal, and so can be made more compatible.

Some attention was given to the possibilities of stereophonic sound in television. This is surprising since in this case the widest possible sound source corresponds to the widest possible picture so that little benefit would seem to be obtainable from stereo in home viewing even considering large projection models. The difficulty of changing the apparent sound field to correspond with every change in the field of view is also obvious.

Pickup Design.-Two lesser-known but still very important sources of distortion which apply equally well to monophonic or stereophonic pickups were discussed in a paper by D. G. Jaquess relating to the Decca stereo pickup. These sources of distortion are, first, impacts between the stylus and groove when vertical groove motions are not satisfactorily traced (which cause most of the wear on the record), and secondly, longitudinal stylus movement in the direction of the unmodulated groove.

The reasons for using two balanced pairs of magnetic gaps in the design of variable-reluctance stereophonic pickups were discussed in a paper by S. Kelly. If each magnetic gap between the moving armature and a fixed pole piece is not balanced by a corresponding gap on the other side of the armature, then, as the side thrust varies across the record due to changing tracking error and frictional force in the modulated groove, the lengths of the unpaired gaps will alter so as to alter the relative sensitivities of the two channels. The sensitivity of at least one of the channels will for a similar reason vary with the playing weight, though for gap lengths parallel to the two modulation directions this will not affect the relative sensitivities of the two channels. Another
(Continued on page 241)
disadvantage of an unbalanced gap system is that induced hum cannot be cancelled by suitably winding two separate coils for each channel.

An interesting sidelight on the hazards of pickup manufacture mentioned by P. Wilson in the discussion is that the rejection rate is about $75 \%$ for the coils of two American pickups using 54 and 56 gauge wire.

Four-track Tapes and Cartridges.-Two important disadvantages of tape relative to disc-its higher price per reproducing time (particularly for stereophonic tapes) and the inconvenience of threading it on to the tape deck-have both been tackled recently in America. Some of the results were described in papers by A. D. Burt and D. R. Andrews and also by Dr. G. F. Dutton. The price per time of tape has been reduced both by using four instead of two tracks acress the $\frac{1}{4}$ in width and also by halving the speed to $3 \frac{3}{7} \mathrm{in} / \mathrm{sec}$. To secure the same response at high frequencies at $3 \frac{3}{4} \mathrm{in} / \mathrm{sec}$ as at $7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$ the effective gap length of the reproducing head must be halved down to about $10^{-1} \mathrm{in}$, but this can be achieved.

To keep losses caused by spacing of the tape from the replay head due to the tape roughness to an acceptable value the tape must be made smoother. Smoother tape (and also greater freedom from dropouts) are also necessary to allow the halved wavelengths at the slower speed to be recorded satisfactorily. The allowable angular azimuth error of the gap length direction is proportional to the recorded wavelength divided by the linear error along the tape between the two sides of the gap, i.e., this error is proportional to the tape speed divided by the track width, and thus remains unchanged. In stereophonic reproduction crosstalk problems are reduced by staggering the four tracks so that no two stereo tracks are adjacent to each other. The signal-to-noise ratio tends to deteriorate when four rather than two tracks are used since the signal is proportional to the number of magnetic particles, i.e., the tape width, and the noise is more nearly proportional to the square root of the number of magnetic particles. An increased recording emphasis at frequencies near the region of maximum hearing sensitivity has been suggested as a method of reducing the apparent signal-to-noise ratio. According to Dr. G. F. Dutton however, results on orchestral output spectra show that peak signal levels in this region can only be increased by about 4 dB or less before overloading occurs.
The slower speed also increases the difficulty of making the transport mechanism sufficiently free of wow and also (particularly) of flutter. For example, a slipping clutch providing take-up tension tends to be jerky and produce longitudinal oscillations of the tape. The flutter produced by such oscillations will be more serious at the shorter wavelengths recorded at the slower speed. The inertia of a given capstan which tends to smooth out irregularities in the tape motion will be quartered at the slower speed. The wow and flutter for the R.C.A. $3 \frac{3}{4} \mathrm{in} / \mathrm{sec}$ tape cartridge on its deck was quoted as about $0.3 \%$.

Easier handling of the tape has been achieved in a number of ways. For example, half loops at the ends of the tape are automatically caught and pulled through the transport mechanism in a development of the Armour Research Foundation of America. The paper by A. D. Burt and D. R. Andrews described the R.C.A. cartridge. In this the tape is enclosed in a plastic container which can be readily slotted into its correct playing position on the tape deck. Thus the cartridge can be removed even when the tape is only partially
played through, and a particular tape cannot be "lost" by being transferred on to another reel by mistake. The two hubs carrying the tape before and after playing do not have any flanges on them at the side of the tape so that the whole space between the hubs can be filled with tape throughout the playing time. Windows in the cartridge allow the amount of tape which has been played to be seen. The tape is secured by a loop at each end which slips over a peg on each hub. At the end of each reel the change in the position of the end of the tape as the peg completes its last revolution can be used to actuate a trip mechanism to stop the tape or reverse it and replay on another track. Interlocks (which can be removed) between the transport mechanism and cartridges carrying pre-recorded tapes prevent such tapes from being accidentally erased.
Is Stereo Worth While-Dr. W. S. Percival was brave enough to give an opinion on this question. With both stereo and mono reproducers their value increases proportionately to their price at low price levels but tends to flatten out to a constant value at high price levels. At first the value for money increases more rapidly with single-channel than with stereo reproducers. The maximum attainable value is, however, greater with stereo so that at some point the value-for-money curves cross for the two types of reproducer. Dr. Percival would not, however, commit himself as to what price this occurred at!

## New Range of Kits

ITEMS from the American Heathkit range are becoming available in this country from Daystrom, Ltd., of Gloucester. Kits already obtainable from the audio range include two stereo combined amplifiers and preamplifiers, a loudspeaker system and two transistor receivers, and from the test and measuring gear range an oscilloscope and valve voltmeter. A kit for an amateur 40-W transmitter covering the $80,40,20,15$ and 10 metre bands is also available. Forthcoming kits will include an R-C bridge, audio oscillator, watmeter, sensitive a.c. valve voltmeter and low-level stereo pickup and tape head amplifier.

The S-88 stereo combined amplifier and pre-amplifier incorporates two 8 -watt ultra-linear push-pull output stages using ECL82 triode pentodes. A low-pass filter cutting off at a rate of about 18 dB per octave above 4,8 or $12 \mathrm{kc} / \mathrm{s}$ can be switched in. A balance control with a range of $\pm 4 \mathrm{~dB}$ is incorporated, and the two stereo signals can be interchanged. Similar facilities are provided in the S-33 amplifier kit, except that there is no low-pass filter, and the output uses two EL84s in single-ended ultra-linear stages to give 3 watts per channel.

The UXR-1 transistor receiver kit covers the medium and long-wave bands and uses six transistors. A pushpull output stage feeds a 7 -in $\times 4$-in loudspeaker. The UJR-1 kit is intended for beginners and also covers the medium and long-wave bands. It uses a single transistor (with reaction) to feed headphones with an impedance between 2000 and 4,000 ohms.

The 0-12U 5-in oscilloscope kit has a maximum Yamplifier sensitivity of $14 \mathrm{mV} / \mathrm{cm}$ and a frequency response flat within 1 dB from $8 \mathrm{c} / \mathrm{s}$ to $2.5 \mathrm{Mc} / \mathrm{s}$. An X-amplifier with a maximum sensitivity of $170 \mathrm{mV} / \mathrm{cm}$ and a response flat within 1 dB from $1 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}$ is provided, or, alternatively, a time base with a repetition frequency variable from $10 \mathrm{c} / \mathrm{s}$ to $500 \mathrm{kc} / \mathrm{s}$ is available.
The V-7A valve voltmeter can measure alternating or direct voltages $(1.5 \mathrm{~V}$ to $1,500 \mathrm{~V}$ f.s.d.), resistances ( $0.1 \Omega$ to $1,000 \mathrm{M} \Omega$ ) and power ratios. The input impedance is $11 \mathrm{M} \Omega$ on the d.c. ranges, and the frequency response on the a.c. ranges within 1 dB from $40 \mathrm{c} / \mathrm{s}$ to $7 \mathrm{Mc} / \mathrm{s}$.

## ANOTHER KIND OF QUIET MICROWAVE AMPLIFIER

YES, I know they are usually called parametric amplifiers, but that is an octosyllabic mouthful, liable moreover to be confused by the quick reader with paramagnetic amplifiers, which could be parametric or on the other hand could be the crystal maser described last month or in fact something altogether else. So I prefer the title given in America* MAVAR, meaning " Mixer Amplification by Variable Reactance." Except that as I abhor the term " mixer" "/ a modulator or "frequency changer I make the " m " stand for " microwave," as in "maser," even though in theory the mavar could be used for other waves.

If you are thinking that " maser" and " mavar" sound like twins, that is all to the good, because it quite rightly suggests some likeness between the devices so named. They both amplify, and both yield a much better signal/noise ratio than conventional amplifiers, enabling weaker signals to be effectively received. This is most valuable at the very high frequencies called microwaves-wavelengths of a few centimetres or millimetres. Both kinds of amplifier tend to be sharply tuned, unlike travelling-wave tubes, which cover a wide frequency band.

## Amplification in Masers

In the maser, the amplification comes from the release of energy when atoms or molecules drop back from an "excited" or energized state to their normal state, in response to stimulation by the weak signal. The frequency at which it amplifies is determined by the energy difference utilized; in the ammonia maser this is fixed by Nature, making it a very precise and reliable frequency standard; but in the more practical cold-crystal or solid-state maser it can be varied by a magnetic field. The basic principle of the mavar is completely different. and while its chief application is in the microwave band and one variety makes use (like one variety of maser) of electronic spin in paramagnetic atoms, these resemblances are coincidental rather than essential.
The solid-state maser, as we saw, is almost unbelievably simple for the highly sophisticated apparatus it is-just a special kind of crystal stuck in a metal box at the end of a waveguide, tuned by a magnet and cooled by liquid helium or oxygen. The difficulty lies in understanding exactly what goes on in the crystal, because it involves rather advanced knowledge of atomic structure and behaviour. The general idea of energy lifts and drops in an atom is
not too hard to grasp, however not too hard to grasp, however.

The general idea of the mavar is also simple, but its working is not at all easy to visualize clearly. I have been finding it a severe test of my doctrine that anything which can be dealt with mathematically can be explained to the non-mathematical by analogy,

[^7]diagram or model. And yet it involves no recondite concept such as $\psi$ waves; only straightforward basic circuit theory.
Briefly, a mavar is like the frequency changer in a superhet, except that (a) the local oscillator varies a reactance instead of a resistance, and (b) amplification takes place without change of frequency.
Fig. 1 is a circuit diagram of a simple frequencychanger stage as used in many receivers, especially for radar. Currents of two different frequencies, due to incoming signal and local oscillation, are mixed by coupling them into the same circuit. If everything in that circuit were linear, no signal at any other frequency would appear. Merely mixing is not enough. Hence my dislike of the name "mixer" for an arrangement in which the key component is the crystal, Cr , which is essentially a non-linear resistor-i.e., one whose current/voltage graph is not a straight line, so that its resistance varies with the current through it or voltage across it, contrary to Ohm's law.
Ohm's law or not, the current through a resistor is equal to the applied voltage divided by the resistance (at that voltage). Alternatively-and in what follows we shall find it simpler-the current is equal to the voltage multiplied by the conductance. Either way, if the resistor is linear the resistance and conductance are constants, so the current has exactly the same waveform and mathematical form as the voltage. If the voltage has two frequencies, the current has two and only two.
Let us call the voltage at any instant $v$, and suppose it consists of two frequencies (oscillator and signal) $f_{0}$ and $f_{s}$, with peak amplitudes $\mathrm{V}_{o}$ and $\mathrm{V}_{8}$. For brevity we use the usual symbol $\omega$ for $2 \pi f$, and have $v=V_{0} \sin \omega_{o} t+V_{\mathrm{g}} \sin \omega_{\mathrm{a}} t$ If we multiply this by a constant conductance $G$,


Fig. I. Simple frequency changer circuit, in which the crystal diode, $\mathrm{C}_{r}$, is essentiolly a non-linear resistor. If a non-linear reactor is used insteod, the system is nearly a movar.
then the result (the current, $i$ ) obviously has the same form.
But now let us suppose that the conductance depends on the voltage. In a diode, for example, the conductance is less than the average during the negative half-cycles and more during the positive halfcycles. A simple case would be one in which the conductance was equivalent to a fixed amount, $G_{o}$, plus
an amount varying in proportion to the voltage, $v G$. The whole conductance is usually denoted by a small letter to show it is variable:

$$
\begin{align*}
\text { And, since } i & =\underset{v g}{g}=\mathrm{G}_{o}+v \mathrm{G} \\
i & =v\left(\mathrm{G}_{\mathrm{o}}+v \mathrm{G}\right) \tag{2}
\end{align*}
$$

We have already written out $v$ in full (1), so we can fill it into (2) to obtain
$i=\left(\mathrm{V}_{\mathrm{o}} \sin \omega_{0} t+\mathrm{V}_{\mathrm{s}} \sin \omega_{0} t\right)\left[\mathrm{G}_{0}+\left(\mathrm{V}_{0} \sin \omega_{0} t\right.\right.$
$\left.\left.+\mathrm{V} \sin \omega_{\mathrm{g}} t\right) \mathrm{G}\right]$
If you are one of those who can only tolerate trigonometry in very small doses there is no cause for alarm, for all you are being asked to do is take note of the fact that this expression inevitably involves $\sin \omega_{0} t \times \sin \omega_{0} t$. And if you look up any list of trigonometrical formulæ you will find that this (usually in the form $\sin A \sin B$ ) is equal to a half of $\left[\cos \left(\omega_{0}-\omega_{\mathrm{a}}\right) t-\cos \left(\omega_{0}+\omega_{a}\right) t\right]$. (The appearance of cos instead of $\sin$, and a minus sign between them instead of a plus, signifies no more than the phase relationship; they are still, with reference to a suitable starting point, sine waves.) So we have two new frequencies, equal to the difference and sum of those put in, and can take our pick of them for the i.f. signal, by tuning to it by means of C in Fig. 1.

Incidentally, anyone who might feel like working out (3) in detail but who doesn't want unnecessary work can take advantage of the fact that $V_{0}$ is usually so small compared with $\vee_{0}$ that its effect on $g$ is negligible, and so the second occurrence of $\mathrm{V}_{\mathrm{t}} \sin \omega_{0} t$ in (3) can be omitted without much error. The sum and difference frequencies still come.

Those who are completely allergic to any sin-andcos at all can convince themselves of at least the production of the difference frequency by a diagram such as Fig. 2, which is a typical current/voltage characteristic of a diode. The input voltage waveform is drawn on end, below, with the signal frequency exaggerated in amplitude to show it up clearly. Being different in frequency from the oscillation, it alternately strengthens and weakens it, giving the phenomenon known as beating. The beat frequency is equal to the difference between the two input frequencies, but there is no voltage at the beat frequency. All the positive half-cycles in one whole beat are nullified by negative half-cycles. Nor, if this voltage were applied to an ordinary resistor, represented by a straight-line graph, would there be any beat-frequency current to use as an i.f. signal. But when applied to a diode the negative half-cycles are suppressed as shown, and the current averages to give a beat-frequency component, shown dotted. There is also a sum-frequency current, but it is masked from sight by the currents at the original frequencies.
Let me emphasize again that the reason for the production of sum and difference frequencies is that the conductance of the diode depends on the applied voltage, as shown one way in Fig. 2 and another way by $g=\mathrm{G}_{o}+v \mathrm{G}$. Actually the conductance in Fig. 2 would not follow such a simple formula, but the principle is the same.

I have recapitulated the elementary principles of frequency changers at length, well known though they must be to all radio students, because the likenesses and differences of the mavar will be clearer if this basis for comparison is fresh in the mind. The mathematical treatment is bulkier but no more
difficult in principle than what we have just gone through.
The difficulties begin when we try to visualize what is happening. Directly we substitute a reactance for the diode we rule out the Fig. 2 kind of diagram, which only works when current and voltage are in phase. If it were an ordinary constant reactance, then vector diagrams would come to our aid. But if you

can make a vector diagram work satisfactorily for a circuit in which the reactance is a function of the voltage you are a better man than I.
The reason for wanting some sort of visual aid perhaps more than usual is that the story told by the mathematics is something we should probably never have expected. And if you are one of the types who regard all mathematical results with suspicion until supported by clearer evidence you may even have some difficulty in believing it.

## Negative Resistance

The mathematical result in this case is that if the usual non-linear resistance of the simple additive frequency changer is replaced by a reactance, it looks to the signal like a negative resistance. In other words, power finds its way from the local oscillator into the signal, at the frequency of the signal, and in proportion to the signal voltage. In still other words, the signal is amplified, without change of frequency, and the power for doing this comes from the local oscillator, working at a different frequency. As we shall see, this result is not absolutely inevitablecertain conditions have to be fulfilled-but that it should happen at all is surely interesting enough to stimulate investigation.
Either inductive or capacitive reactance can be used, but I think capacitive is better for a first study, because the simplifying assumption that it is free from resistance is very nearly true of familiar capacitors. It also offers better possibilities for mechanical models, real or imaginary. What may take a little more getting used to is capacitance that varies according to the voltage across it. (Inductance that varies with the current through it is only too familiar.)

The basic fact about capacitance is that it is a measure of the amount of electric charge a given voltage can store. Just like, in fact, the size of a tyme

(a)

(b)
or balloon, where the charge is air and the voltage is pressure. In symbols:

$$
\begin{equation*}
\mathrm{Q}=\mathrm{CV} \tag{4}
\end{equation*}
$$

This says that the charge is directly proportional to both voltage and capacitance. We are quite used to applying varying voltages to capacitors, but usually their capacitances are constant. So the effects of variable capacitance are less familiar, except perhaps to specialists such as engineers of the Compton Organ Co., who do exactly the reverse of most of us-vary C sinusoidally while keeping V constant. The result is the same, however.

It is unfamiliarity with this, presumably, that gives rise to the question with which successive generations of students try to baffle their teachers: If a capacitor is charged and then dismantled, what happens to the charge (and its energy)? It is assumed that the insulation of the plates is maintained. The charge, $Q$, therefore remains; and, in so far as $C$ is reduced by the dismantling, V rises. For proof, see (4). This is the basis for the "Cathode Ray" voltage raiser, proposed in the May 1950 issue. (No doubt lots of other people proposed it centuries ago, so don't write in to tell me.)

## Current Flow

Now of course a charge in motion is a current, so if one varies either V or C (but not both at once in opposite directions so that $\mathrm{V} \times \mathrm{C}$ is constant) a current must flow in and out. Expressed more precisely, and using small letters to indicate variables:

$$
i=\frac{\mathrm{d} q^{\star}}{\mathrm{d} t}
$$

If C is constant, then $q(=\mathrm{C} v)$ varies at C times the rate that $v$ is varied. So we have

$$
i=\mathrm{C} \frac{\mathrm{~d} v}{\mathrm{~d} t}
$$

Supposing $v$ is our usual sine wave, $\mathrm{V} \sin \omega t$ :

$$
i=\mathrm{C} \frac{\mathrm{~d}(\mathrm{~V} \sin \omega t)}{\mathrm{d} t}
$$

Fig. 3(a) shows a single cycle of $v$, and underneath at (b) is drawn a curve showing the rate at which $v$ is varying. It is easily derived from (a); for example, $v$ increases fastest at the start, making $\mathrm{d} v / \mathrm{d} t$ a positive maximum; it isn't varying at all at the peaks, so then $\mathrm{d} v / \mathrm{d} t$ is zero; and so on. It is, in fact, a cosine wave. The well-known calculus

[^8]result is $\mathrm{d}(\mathrm{V} \sin \omega t) / \mathrm{d} t=\omega \mathrm{V} \cos \omega t$. And the capacitive current is proportional to this, as we have just seen, so
\[

$$
\begin{equation*}
i=\omega C V \cos \omega t \quad \ldots \quad \ldots \tag{5}
\end{equation*}
$$

\]

which is the same waveform as $v$ but advanced quarter of a cycle in phase. That is the familiar fact of a.c. theory, commonly expressed by showing a current vector leading a voltage vector by $90^{\circ}$. We are familiar, too, with the fact that when you multiply $i$ by $v$ to find the power you get a positive product during the first and third quarters of the cycle, when $v$ is charging $C$, and an exactly equal negative product during the second and fourth quarters, when $C$ is discharging back into the source. The net power either way is therefore nil.

Again, we have gone through all this old stuff
Fig. 4. These waveforms represent: (a) the applied signal voltage $v$; (b) the slope of (a), which could represent the current driven $v$ through a constant capacitance; (c) the variation of the capacitance due to the pump oscillator, working at twice the frequency of $v$; (d) the slope of (c); (e) current due to v applied to the variable capacitance
(c), found by multiplying (b) by (c). (c). found by multiplying (b) by (c); (f) current due to variation of (c) with v applied, found by multiplying (a) by (d); (g) total current, equal to (e) plus ( $f$ ); (h) triple frequency part of (g); (i) the part of (g) at same frequency as (a), and in opposite phase, signifying negative
resistance. resistance.

(i)

for the sake of comparison with the less familiat case of capacitance varying and voltage constant. If we make $c$ vary in the same way as $v$ did ( $c=$ $\mathrm{C} \sin \omega t$ ) then obviously the result is the same except for interchange of V and C , which as (5) shows makes no difference at all.
It is quite interesting to realize that precisely the same current-making result can be obtained by varying capacitance exposed to a constant voltage as by varying voltage across a constant capacitance. Note in particular that there is no net transfer of power.

But in a mavar both vary at once, just as both voltage and conductance vary at once in a frequency changer. What makes the mavar a little more complicated is that what we are interested in is not just the product of two varying quantities (as in $i=v g$ for the frequency changer, or $q=c v$ ) but their slope or rate of change. We have found that, when $v$ alone is varying the current is $c \mathrm{~d} v / \mathrm{d} t$, and when $c$ alone is varying it is $v \mathrm{~d} c / \mathrm{d} t$, so when both are varying:

$$
\begin{equation*}
i=c \frac{\mathrm{~d} v}{\mathrm{~d} t}+v \frac{\mathrm{~d} c}{\mathrm{~d} t} \quad \cdots \quad . \tag{6}
\end{equation*}
$$

As before, let us make our signal voltage

$$
v=\mathrm{V} \sin \omega_{\mathrm{s}} t
$$

We know that

$$
\frac{\mathrm{d} v}{\mathrm{~d} t}=\omega_{\mathrm{l}} \mathrm{~V} \sin \omega_{a} t
$$

And, as we did with $g$, we can make $c$ consist of a constant part, $\mathrm{C}_{0}$, and a part varying at the frequency of the local oscillation:

$$
c=C_{0}+C \sin \left(\omega_{0} t+\theta\right)
$$

The $\theta$ denotes the phase difference, if any, between the two voltage waves. The rate at which $\mathrm{C}_{\text {o }}$ varies being obviously nil,

$$
\frac{\mathrm{d} c}{\mathrm{~d} t}=\omega_{0} \mathrm{C} \cos \left(\omega_{0} t+\theta\right)
$$

Filling these into (6) and working out how much current there is at each frequency we have

$$
\begin{aligned}
& i=\omega_{s} \mathrm{C}_{0} \mathrm{~V} \cos \omega_{\mathrm{a}} t+\omega_{\mathrm{CV}} \sin \left(\omega_{0} t+\theta\right) \cos \omega_{s} t \\
& +\omega_{0} \mathrm{CV} \sin \omega_{a} t \cos \left(\omega_{0} t+\theta\right) \\
& =\omega_{\mathrm{B}} \mathrm{C}_{\mathrm{o}} \mathrm{~V} \cos \omega_{\mathrm{s}} t+\frac{\omega_{\mathrm{B}} \mathrm{CV}}{2}\left[\sin \left(\omega_{0} t+\theta+\omega_{\mathrm{B}} t\right)\right. \\
& \left.+\sin \left(\omega_{0} t+\theta-\omega_{s} t\right)\right] \\
& +\frac{\omega_{0} \mathrm{CV}}{2}\left[\sin \left(\omega_{0} t+\omega_{0} t+\theta\right)\right. \\
& \left.+\sin \left(\omega_{0} t-\omega_{0} t-\theta\right)\right] \\
& \begin{aligned}
&=\omega_{\mathrm{a}} \mathrm{C}_{0} V \cos \omega_{\mathrm{g}} t+\frac{\mathrm{CV}}{2} {\left[( \omega _ { \mathrm { g } } + \omega _ { 0 } ) \operatorname { s i n } \left(\omega_{0} t+\theta\right.\right.} \\
&\left.+\omega_{\mathrm{a}} t\right)+\left(\omega_{\mathrm{a}}-\omega_{\mathrm{o}}\right) \sin \\
&\left.\left(\omega_{0} t+\theta-\omega_{\mathrm{g}} t\right)\right] \ldots(7)
\end{aligned}
\end{aligned}
$$

The first term of the final result is of course the current that $v$ would cause if the capacitance consisted only of $\mathrm{C}_{0}$. The "cos" indicates that it is $90^{\circ}$ out of phase, dissipating no power.
The first of the two terms in the square bracket represents the "sum" frequency current, and the second the "difference" frequency. If we assume $\theta=0$, then (remembering that $\sin -x=-\sin x$ ) whatever frequencies are chosen the first term must be positive and the second negative. This means

that the sum-frequency current is a positive sine wave and would draw power from a sine voltage at that frequency, but the difference frequency is a negative sine wave so would deliver power to a sine voltage at that frequency. If we choose our frequencies so that $\omega_{0}-\omega_{\mathrm{g}}=\omega_{0}$ (i.e., $\omega_{0}=2 \omega_{\mathrm{g}}$ ) then the second term simplifies to $-\omega \sin \omega_{0} t$, indicating power flowing into the signal. Which, as Euclid said, erat faciendum, meaning it's just the job.

That is why in mavars the local oscillator, colloquially termed the pump, usually works at twice the signal frequency. The closer scrutiny we shall later give (7) will show that this is not the only possible useful frequency, but it will do to be going on with.

## Graphical Illustration

Meanwhile we must do our best for those who find purely mathematical treatment obscure or unconvincing. We can, with a bit of an effort, accomplish the same thing less precisely but more graphically by drawing waveforms. In Fig. 4 (a) is one cycle of the applied voltage $v$-a sine wave. Next, at (b), is a graph of the slope of (a), $\mathrm{d} v / \mathrm{d} t$-a cosine wave. (c) represents the variable part of $c-$-a double sine wave, because the pump frequency is twice the signal frequency. Next, at (d), comes $\mathrm{d} c / \mathrm{d} t$ a double cosine wave. The part of the current due to variation of $v-c \mathrm{~d} v / \mathrm{d} t$-is got by multiplying (b) by (c), and is shown at (e). And the part due to variation of $c$, which is (a) multiplied by (d), appears at (f). Finally, the complete current is obtained by adding (e) to (f), as at (g).
This appears pretty clearly as a mixture of a sine wave of three times the frequency of (a), starting in phase with it, and a sine wave of the same frequency as (a), but opposite in phase. They are shown separately at (h) and (i). Because (h) is different in frequency from the voltage (a), it conveys no net power-its single half-cycle of current in opposition
to the voltage half-cycle exactly balances its two half-cycles in the other direction because it comes near the voltage peak. But (i) is always into the voltage source, feeding it with power.

Any to whom even this procedure smacks too much of maths and who are more mechanically minded may like to try the following. Take a weight, say 1 lb , and suspend it by about 4 ft of string from the centre of the lintel of an open doorway, preferably one not in frequent use (Fig. 5). Attach the middle of a piece of thin elastic (or the ends of two pieces) to the weight. Standing on the side away from the door, hold one of the free ends in each hand. Now set the weight swinging towards and away from you and then rest your hands on the door posts. The swinging will gradually die out like the pendulum of an unwound clock. But if you alternately increase and decrease the stretch of the elastic by moving your hands away from and towards the weight, at twice the frequency of the weight's swing and in phase with it, you should with a little practice be able to keep the weight swinging indefinitely (which means until you get tired). You must not cheat by moving your hands other than strictly at right angles to the direction of swing. If the elastic is kept in contact with the


Fig. 6. If the r.f. resistance of a circuit, $R$ by itself, is periodically varied by o mavar from 0 to $2 R$ os shown ot (a), the $Q$ of the circuit is affected as shown ot (b), which resuls in ne: amplification.
(b)
door posts, even the most sceptical should be convinced that power is being fed in by periodical variation of mechanical capacitance (which is the compliance of the elastic). The constant and greater part of this capacitance is due to gravitational pull on the weight. The velocity of the weight represents $i$, and the pull on the weight due to gravity and elastic represents $v$.
This helps to explain how in both electrical and mechanical systems having reactance which depends on voltage or stress there sometimes occur subharmonic oscillations (frequencies lower than one would expect). Loudspeakers, for example. This is quite a big subject in itself, so the brief hint must suffice, while the attention of the trigonometrists is directed back to equation (7).

$$
\text { If } \theta=\frac{\pi}{2} \text { (which is } 90_{o} \text { ) then, since } \sin \left(x+\frac{\pi}{2}\right)=
$$ $\cos x$, the whole current becomes " wattless." When $\theta$ is increased to $\pi$, the difference-frequency term represents power taken instead of given. If the pump is not synchronized with the signal, so that $\theta$ continuously drifts on, the signal circuit gets on the average as much positive resistance as negative, which (it might seem) would do the signal no good. Fortunately this is not so, for the signal amplitude

is proportional to Q or $1 / R$; consequently a given amount of negative resistance builds up the signal more than the same amount of positive resistance damps it down. Suppose the resistance of the signal circuit without benefit of mavar was R ohms, and that owing to lack of synchronism the resistance contributed by the mavar alternated slowly between +R and -R . The +R could do no worse than halve the signal amplitude, but the -R would eliminate all circuit resistance and start the signal building up towards infinity, as shown in Fig. 6. The signal would of course be amplitude-modulated at the frequency by which the pump oscillator was straying from exact synchronism with twice the signal frequency.

## Other Pump Frequencies

For microwaves, this need for the local oscillatot to be twice the signal frequency is likely to be a nuisance. Although the simplified way in which we have looked into the mavar principle doesn't directly show it, the fact remains that other fre-quencies-including lower ones than the signalare possible. Equation (7) does show that there is an opposite-phase current at the difference frequency, no matter what $\omega_{0}$ may be in relation to $\omega_{0}$. So far, we have considered only the special case in which $\omega_{0}=2 \omega_{s}$, so that $\omega_{0}-\omega_{s}=\omega_{s}$. When $\omega_{0}-\omega_{\mathrm{s}}$ is something different, say $\omega_{\mathrm{i}}$, a resistive so-called idling circuit must be provided for this current to flow in. Its flow there sets up a voltage at the same frequency across the reactance, and that, in combination with the pump voltage, results in a current into the signal circuit.
In some experiments by Chang and Bloom, their choice of frequencies (in Mc/s) was $f_{\mathrm{s}}=380$, $f_{0}=300$, and $f_{1}=220$. Twice $f_{\mathrm{o}}$ (produced as a harmonic by the non-linearity of the reactance) minus 220 yields $f_{\mathrm{s}}$. In their work they used a germanium diode as the varying capacitance. (Its use for a.f.c. has already been described in Wireless World-by G. G. Johnstone, August 1956, p. 354.)
The original mavar made use of electronic spin in paramagnetic crystals to vary inductance, in a rather similar way to the 3 -level maser described last month. But it needs such an enormous amount of pump power ( 20 kW has been mentioned!) that the whole thing is in danger of going up in smoke. The diode scheme, which needs only milliwatts, looks much more practical, though there may well be doubts about the higher frequencies. Still another, and again remarkably different, method of putting the mavar principle into action is by means of varying space charges in a tube. This arrangement, the precise functioning of which does not exactly leap to the mind's eye, has been developed by the Zenith Radio Corporation of America and was described on the Technical Notebook page in the November 1958 issue.

Although a noise figure of 1 dB is claimed for this tube, the tendency is for mavars to be nearer the $3-4 \mathrm{~dB}$ mark-not so quiet as masers with their liquid helium, but markedly better than conventional amplifiers. Besides avoiding extreme refrigeration, mavars also handle much more power than masers. So we are likely to hear quite a lot more about them. Why (you are asking) are they so quiet, in spite of working at room temperature? Because the business part of the device is a reactance, which being non-resistive doesn't generate thermal noise.

# Manufacture s' Products 

## NEW ELECTRONIC EQUIPMENT AND ACCESSORIES

## Versatile Signal Lamp Fitting

A NEW signal lamp fitting possessing a number of novel features is the new Bulgin model D788. It fits panels up to 0.5 in thick, can be supplied to take a wide variety


Versatile Signal and Indicator Lamp (Bulgin).
of British or American indicator and signal lamps, filament or neon in bayonet or screw types; the lamp socket is adjustable for depth within the body and the lamp can be renewed from either the front or the rear. The front bezel can be either plastic or metal. It fits into a $l^{\frac{1}{32}-\text {-in }}$ diameter panel hole.
The front lens, which is nearly 1 in in diameter, can be either plastic or glass, in the former material it can be either transparent or translucent but in glass only transparent lenses are available. In either material there is the choice of five colours.
The makers are A. F. Bulgin and Co., Ltd., Bye Pass Road, Barking, Essex.

## Measuring Relays

FRENCH Leland Leroux "Sensitact" relays are now available in England. Each relay consists of a screened moving-coil galvanometer with pointer and contact attached, and two scparate contacts adjustable over the full range of the scale provided. Sixteen models are available with full-scale deflections ranging from 10 mA down to 0.02 mA . For the most sensitive model the minimum change of control power necessary to make or


Leland Leroux "Sensizact" measuring relays.
break contact is abcut $0.05 \mu \mathrm{~W}$; the maximum power which can be handled by the contacts in all models is 200 mW . The response time is from 0.1 to 0.2 seconds, depending on the positions of the adjustable contacts. The cost of these relays ranges from $£ 1310$ s to $£ 15$, and they are available in this country from Leland Instruments, Ltd.. 22-23, Millbank, London, S.W.1.

## Miniature Silvered Mica Capacitors

THE new range of protected miniature silvered mica capacitors recently introduced by the Telegraph Condenser Co. Ltd., North Acton, London, W.3, measure


New miniature T.C.C. silvered mica capacitors Types CSMI5 (end connections) and CSMI5s (side connections).
only $\frac{7}{16} \times \frac{1}{4} \times \frac{3}{32} \mathrm{in}$, yet the rated working voltage is 350 d.c. and the test voltage 1,000 d.c. The range covers capacitances of 10 pF to 220 pF with tolerances of from $1 \%$ to $20 \%$ as required. These capacitors have a power factor of less than $20 \times 10^{-4}$ at $1 \mathrm{Mc} / \mathrm{s}$ and a temperature coefficient of +5 to +50 parts per $10^{6}$ per degree C over the temperature range $-70^{\circ} \mathrm{C}$ to $+100^{\circ} \mathrm{C}$ and the insulation resistance is berter than $10^{5} \mathrm{M} \Omega$.

The new capacitor is available in two styles, one, the CSM15, with flat end-connecting strips and the other, CSM15s, with side-entry connections.

## Miniature Long-scale Meters

A RANGE of small, flush-mounting, moving-coil measuring instruments, based on the design of the welltried Crompton Parkinson industrial switchboard meters, has been introduced for use in electronics, telecommunications equipment and test gear. These have pointer rotations of $240^{\circ}$ and are available with 2 -in or $2 \frac{1}{2}$-in diameter dials and assembled in either moulded-plastic or die-cast metal cases, the latter being a sealed type conforming with the requirements of British Draft Defence Specification 62.

The $2 \frac{1}{2}$-in models provide a scale $4 \frac{1}{4}$ in long, while that of the smaller meter is $3 \frac{1}{5} \mathrm{in}$. The range includes d.c. microammeters, milliammeters, ammeters and voltmeters, also a.c. milliammeters and voltmeters, the resistance of voltmeters being $1000 \Omega / \mathrm{V}$.

In a flush-mounting moulded case a $0-200$ d.c. micro-


Crompton Parkinson $240^{\circ}$-scale moving-coil milliammeter in moulded case.


Left: Neosid miniature pot-type coil, shown with screening can removed.


Hermetically sealed "7 ransipack" d.c. convertor using semiconductors.
toroidal transformer and is claimed to have an efficiency of $85 \%$. It measures $4 \frac{7}{16} \mathrm{in} \times 2 \frac{7}{16} \mathrm{in} \times 1 \mathrm{in}$, weighs 11 lb 150 z and costs $£ 123 \mathrm{~s}$.

The makers are Transipack, 29 Burnt Ash Hill, London, S.E. 12.

## Bass Loudspeaker

ALTHOUGH developed primarily as a replacement for the bass loudspeaker originally used in their "Quartet" 4-speaker system (see Dec. 1958 issue, p. 607), the Fane Acoustics 12 -in H.D. unit is also available separately.

It has a smooth response from 30 to $4,500 \mathrm{c} / \mathrm{s}$ with a gradual roll-off beyond, and a maximum input power rating of 20 W (continuous). The total flux is 160,000 lines; the flux density being 12,000 gauss and the voice-coil diameter 2 in . The cone is curved-sided and is reinforced by a double roll at its junction with the foam plastic surround to inhibit bell-like vibrations. The cost of this speaker is $£ 9$ (not liable to purchase tax), and it is manufactured by Fane Acoustics, Ltd., Batley, Yorkshire.

## Tape Bulk Eraser

AN a.c. mains energized coil is wound on the centre limb of an E-shaped core to provide the magnetic field for the "Instant" eraser. The push-button switch is depressed and the dimpled side of the eraser passed over the entire area of both sides of the tape reel. The eraser is then removed some way from the reel (to allow the erasing field to decrease gradua! 1 ) and the push - button allowed to spring back. Erasure of the tape is then complete. Reels should not be
"Instant" tape bulk eraser.
 erased in situ on recorders with magnetic chassis as so much flux may be diverted through the chassis as to give incomplete erasure. This eraser costs 27 s 6 d and is available from Osmabet, Ltd., 14, Hillside Road, London, N.15.

## Magnetic Tape Splicer

IN the "Editape" splicing block, the tape holds itself in position in the shallow slot because of the special cross-sectional shape of this slot (see inset on photograph). The narrow slit crossing at $45^{\circ}$ is for guiding the tape cutting blade-which should preferably be nonmagnetic The splicing block costs 7 s 6 d (including 90stage) and is available from Sound Developments, 9, Osborne Road, Kingston-upon-Thames.

"Editope" splıcing block with insel showing special crosssectional shape of shallow slot for retaining the tope

# News from the Industry 

Philips-Cossor Link.-Philips Electrical Ltd. have acquired control of Cossor Radio and Television Ltd., a subsidiary of A. C. Cossor Ltd., together with the right to use the Cossor trade mark in the fields of domestic sound radio, television and sound reproduction in all countries except Canada and Pakistan. The new directors of Cossor Radio and Television Ltd. are A. L. Sutherland, director of Philips since 1956, E. W. Brades, director and sales manager of Philips' associare company Stella Radio and Television, and J. S. Clark, joint managing director of A. C. Cossor Ltd. and a director of a number of companies within the Cossor group. D. I. Turner, former sales promotion manager of Cossor, is appointed sales manager. For the time being correspondence should continue to be addressed to Highbury Grove, London, N.5.

Pilot Radio has become a wholly owned subsidiary of Ultra Electric Ltd., who have also acquired from the Pilot Radio Corporation, of America, "Pilot" trade marks in 17 European countries. Pilot Radio, whose works are at Park Royal, Middlesex, was formed in 1935.
E.M.I.-S.T.D. Link.-An agreement has been entered into between E.M.I. Sales \& Service Ltd. and Scientific \& Technical Developments Ltd. (S.T.D.), of Wallington, Surrey, whereby E.M.I. will undertake world distribution outside the U.K. of the "Orthotone" range of high-fidelity units. Equipment will carry both "Emisonic" and "Orthotone" trade marks. Distribution to the Trade in the U.K. will continue to be the direct concern of S.T.D. The identity and management of S.T.D. remains unchanged and the manufacture of all "Orthotone"products will continue at the Wallington factories.

Miniature Relays.-One of the subsidiaries of the Elliott-Automation Group, C. P. Clare, Ltd., which was formed towards the end of last year to manufacture and sell under licence the products of C. P. Clare \& Co., of Chicago, received $£ 12,000$ worth of orders for its miniature relays in its first full month of operation.

The "Gramdeck" turntabledriven tape tr_nsport and transistor record/replay mechanism mentioned in "Technical Notebook" in our July 1958 issue (p. 330) is now marketed by Andrew Merryfield Ltd., 29-31, Wright's Lane, London, W.8. It costs $£ 13 \mathrm{l} 2 \mathrm{~s}$.

Marconi's and A. T. \& E. have been jointly awarded a contract by the United States government for the supply of a mobile microwave telephone and telegraph communication system linking many of the U.S. Air Force bases in this country. The radio equipment, which is capable of carrying 240 telephone channels and operates in the 4000$\mathrm{Mc} / \mathrm{s}$ band, will be supplied by Marconi's and the telephone carrier equipment, which operates in the $60-552 \mathrm{kc} / \mathrm{s}$ band, by A. T. \& E., who, in association with Telephone Manufacturing Co., will also supoly the telegraph channelling equipment. The overall value of the order is about $\$ 3.5 \mathrm{M}$.

Educational Technical Developments Ltd., of Market Place, Reading, Berks., has been formed by R. Clyne, well known in the industry as a supplier of kits and parts, etc. (who is chairman), and P. T. V. Page, until recently manager and director of instruction at E.M.I. Institutes (who is principal): The company is proviling "Radiostructor" postal tuition courses with which the student is given components for constructional work.

Datum Metal Products Ltd. is the new title adopted by Davis \& Thompson Ltd., of Watford, Herts., manufacturers of Datum instrument racks, cases, chassis and consoles. The company is a member of the Camp Bird Group.

E.M.I. ELECTRONICS are supplying this microwave link eqcipment to convey the B.B.C. television service from the mainland to the Orkneys' transmitter.

Telemechanics Ltd., of Hythe, Southampton, which was formed by F. M. Hills in 1946 and became part of the Pena Group, has been reacquired from the liquidator of Pena by Mr. Hills, who is managing director. The company, which is engaged in the manufacture of "Telemax" test equipment, marine broadcast receivers and power units, can offer production facilities to the industry.

Cossor airborne radar transponders for traffic identification have been ordered by B.O.A.C. for its fleet of Boeing 707 jet aircraft. The transponder, which replies to ground interrogation with a coded train of pulses, is compulsorily fitted in highflying civil airliners in the U.S.A., and arrangements are being made for its use in Europe.
Truvox.-Because of the report which appeared in some journals regarding the liquidation of Truvox Holdings Ltd., we have been asked to state that the liquidation of this non-operative company in the Truvox Group in no way affects the activities of Truvox Ltd., manufacturers of tape recorders. The company was liquidated "for purely administrative reasons."

Pye.-The Norwich studios of Anglia Television Ltd., the programme contractors for the I.T.A.'s Mendlesham, Suffolk, station is being equipped with cameras and control gear by Pye, who are also supplying an O.B. unit. The transmitting equipment at Mendlesham is also being provided by Pye, whose transmitters are in use at the I.T.A.'s Lichfield and St. Hilary stations.

Decca harbour surveillance radar, Type 32, has been installed in the re-furbished radar station at Gladstone Dosk, Liverpool. The $3-\mathrm{cm}$ radar equipment, which has seven displays all fed from a common scanner, provides a composite picture of the harbour and its approaches. In bad visibility when pilots ask to be kept under observation minute-byminute information of the exact position of the shio is passed by radio to assist the pilot in navigating the river and approach channels.

## EXPORT NEWS

Microwave transmitters and assocjated equipment for a radio network providing a te'ev's'on and telephone l'nk between Sundsvall and Boden (a distance of 300 miles) have been ordered by the Royal Board of Swedish Telecommun cat ons from Standard Telephones and Cables. Tha nstallation. which w'll work in the $4000-\mathrm{Mc} / \mathrm{s}$ band, will provide six parallel two- vay channels each capable of carrying 950 te'ephone circuits or one television transmission complete with sound.

Television cameras, specially designed by Pye for use in reactors, are being demonstrated during a tour of American and Canadian atomic energy pants by Victor Hessen, manager of Pye's Atomics Division, and Donald Jackson. chief mechanical engineer of the company's Transmission Division. The equ:pment was shown at the Atom:c Fair which was held recently in Ohio.

Ultrasonic inspection equipment to the value of $£ 10,005$ has been ordered from Kelvin Hughes for installation in a Czechoslovakian steel works. The equipment will facilitate the rap.d scanning of rolled mild steel bars for internal defects and consists of a remote control console containing the c.r.t. presentation and recording equipment and the remote operating controls for a scanning unit situated above the main feed conveyor.

Teiecommunication Equipment.-As part of the programme for the expansion of the telecommunications service between East and West Pakistan and overseas, the Posts and Telegraphs Department has ordered from Marcon's three high-power h.f. transmitters for telegraph and teleprinter circuits.

Television transimitters, cameras and ancillary equipment are being supplied by Pye for two new commerc al stations being built in Australia. One is in Adelaide and the other in Perth.

Lisbon Trade Fair.-Among the 350 or so manufacturers participating in he British Trade Fair, which is being held in Lisbon from May $29 t h$ to June 14 th, are a number in the radio and electronics industry. Some are participating in group exh:bits, but many have taken individual stands including a number of domestic sound and television equipment manufacturers. Among the 300 or more exhibite in the display staged by the Council of Industrial Design are a number of sound and television receivers.

Italy - Industrial Products Agencies S.r.l., of Via Carlo Fea 11, Rome, are seek.ng agencies of United K.ngdom manufacturers of electronic and nuclear instruments; microwave equ-pment; impulse generators; magnetic sound and vision recording equipment and servo mechanisms.

## TRANSISTOR EXHIBITION

THE manufacturers and organizations listed below have taken stands at the International Transistor Exhibition being organized in conjunction with the Transistor Convention sponsored by the I.E.E. The exhibition, being held at Olympia, London, concurrently with the convention (May 21-27), opens each day at 9.0 and closes on the 21 st and 25 th at 6.0 , the $22 \mathrm{nd}, 23 \mathrm{r}$ d and 26 th at 8.0 , and 27 th at 4.0 . It will not be open on Sunday. Tickets for the exhibition are obtainable free from the organizers, Industrial and Trade Fairs, Ltd., Drury House, Russell St., London, W.C.2.

Those wishing to attend the convention, which is being organized by the Electronics and Communications Section of the I.E.E., must apply to the Institution (Savoy Place, London, W.C.2) for registration forms.

Alma Components
Ashburton Resistances
Associated Electrical Industries
B.B.C.
B.T.H.

Belling \& Lee
Birlec
Brush Crystal Company
Compagnie Francaise Thomson-Houston
Compagnie Generale de T.S.F.
Dawe Instruments
Dependable Relay Co.
Edwards High Vacuum
Electrovac Hacht \& Huber
Elga Products
Elliott Brothers (London)
English Electric Valve Co.
Ever Ready Co.
Ferguson Radio Corp.
Ferranti
G.E.C.
G.E. Industrial Supplies
G.P.O.

Hatfield Instruments
Heraeus Quarzschmelze
I.C.I.
I.E.E.

Johnson, Matthey \& Co.
Kynmore Engineering Co.
Livingston Laboratories
Mallory Batteries
Mansol (G.B.)
Mining \& Chemical Products
Ministry of Supply
Mullard

## Newmarket Transistors

## Plessey Company

Pye
RCA Great Britain
Racal Engineering
Radio Heaters
Rank Cintel
Raytheon Manufacturing Co.
Rivlin Instruments
Roband Electronics
Roe, A. V., \& Co.
Sanyo Electric Company
Semiconductor Information Service
Semiconductors
Shockley Transistor Corp.
Siemens \& Halske A.G.
Siemens Edison Swan
Sintering \& Brazing Furnaces
Societa Generale Semiconduttori
Solartron Electronic Group
South London Electrical Equipment Co.
Standard Telephones and Cabies
Sylvania Electric Products
Tekade
Telefunken
Texas Instruments
Tokyo Shibaura Electric Co.
U.K. Atomic Energy Authority

Ultra Electric
Union Miniere Du Haut-Katanga
University of Birmingham
Venner Electronics
Vidor and Burndept
Wayne Kerr Laboratories
Welwyn Electrical Laboratories
Westinghouse Brake \& Signal Co.
Whiteley Electrical Radio Co.
Wire Products \& Machine Design
Wirepots

## MAY MEETINGS

## LONDON

5th. Brit.I.R.E.-"An experimental diode parametric amplifier and its properties" by I. M. Ross, C. P. Lea-Wison, A. J. Monk and A. F. H. Thomson at 6.30 at the London School of Hygiene and Tropical Medicine, Keppel Street, W.C.1.

8th. I.E.E. Medical Electronics Discussion Group.-_" Microwave radiation hazards" by Dr. D. H. Shinn (Marconi's) and Dr. N. L. Lloyd (Ministry of Supply) at 6.0 at Savoy Place, w.C.2.

13th. I.E.E.-"The application of statistical techniques to the electronic valve industry" by E. G. Rowe at 5.30 at Savoy Place. W.C. 2.

13th. Brit.I.R.E.-" Improving communication techniques-what have engineers to learn from information theory? " by Professor D. Gabor at 6.30 at the London School of Hygiene and

Tropical Medicine, Keppel Street, W.C. 1.

14th. I.E.E.-"On the conceivable future of telecommunications" by Professor E. C. Cherry at 6.30 at Savoy Place, W.C. 2.

14th. Physical Society Acoustics Group.-" High energy ultrasonics" by E. Neppiras at 5.30 at Imperial College, Prince Consort Road, S.W. 7.
15 th. Institute of Navigation."Electronic surveys in the Caribbean" by Capt. E. G. Irving, R.N., at 5.15 at the Royal Geographical Society, I Kensington Gore, S.W.7.

21st. Physical Society.-Presidential address by J. A. Ratcliffe at 5.45 at the Royal Institution, 21 Albemarle Street, W.1.

## BIRMINGHAM

8th. Institution of Electronics.-
"The design of transistor h.f. ampli-
fiers" by L. E. Jansson (Mullard) at 7.0 in the Byng Kenrick Suite Lecture Hall. New College of Technology, Gosta Green.

## BRISTOL

Sth. Television Society.-Mullard Film Meeting at 7.30 at the Grand Hotel (Joint meeting with R.S.G.B. and R.T.R.A.).

## CHELTENHAM

lst. Brit.I.R.E.-_" Transistor amplifiers" by $F$. Butler at 7.0 at North Gloucestershire Technical College.

## PRESTON

6th. I.E.E.-Annual general meeting at 7.15 followed by "Domestic highfidelity reproduction ", by J. Moir at the North-Western Electricity Board Demonstration Theatre, Friargate.

## CONFERENCES AND EXHIBITIONS

Latest information on forthcoming events both in the U.K. and abroad is given below. Further details are obtainable from the addresses in parenthesis.

## UNITED KINGDOM

Symposium un Instrumentation and Computation in Process Development and Plant Des:on, Central Hall, Westminster, London, S.W. 1 .... May 11-13 (Institution of Chemical Engineers, 16 Belgrave Square, London, S.W.1.)
International Convention and Exhibition on Transistors, Earls Court, London, S.W. 5
(l.E.E., Savoy Place, London, w.i.......)

International Plastics Exhibition and Convention, Olympia, London, W. 14 (" British Plastics," Dorsei House, Stamford Street, London, S.E.1.)
British Computer Society's Conference, Cambridge $\qquad$ .1.)
British Computer Society's Conference, Cambridge ............. June 22-25 (British Computer Society, Finsbury Court, Finsbury Pavement, London, E.C.2.)
International Convention on Television Engineering, Cavendish Laboratory, Cambridge (Brit. I.R.E., 9 Bedford Square, London, W.C.i.)
National Radio and Television Show, Earls Court, London, W.5. .Aug. 26-Sept. 5 (British Radio Exhibitions Ltd., 49 Russell Square, London, W.C.1.)
Scottish Industries Exhibition, Kelvin Hall, Glasgow
Sept. 3-9 (Matthew H. Donaldson, 2 Woodside Terrace, Glasgow, C.3.)
Farnborough Air Show .......................................................... 8-14 (Society of British Aircraft Constructors, 29 King Street, London, S.W.1.)
Conference on Dielectric Devices, University of Birmingham .... Sept. 14-17 (Electrical Engineering Department, The University, Birmingham, 15.)
Conference on Modern Network Theory, University of Birmingham, Sept. 21-24 (Electrical Engineering Department, The University, Birmingham, 15.)
Conference on Some Aspects of Magnetism, Sheffield University .. Sept. 22-24 (Institute of Physics, 47 Belgrave Square, London, S.W.1.)
International Scientific Research Exhibition, Olympia, London.. Oct. 3-10 (I.S.R.E. Ltd., Oswaldestre House, Norfolk Street, London, W.C.2.)

Radio Hobbies Exhibition, Royal Horticultural Hall, London, S.W.1, Nov. 25-28 (P. A. Thorogood, Museum House, Museum Street, London, W.C.1.)

## OVERSEAS

Interdisciplinary Conference on Self-Organizing Systems, Chicago, May 5-6 (Scott H. Cameron, Armour Research Foundation, Chicago 16, U.S.A.)
Electronic Components Conference, Philadelphia May 6-8 (Brig. Gen. Edwin R. Petzing, A.G.E.P. Secretariat, University of Pennsylvania, Philadelphia, Pa., U.S.A.)
Radio Engineering Convention, Melbourne
May 25-30 (Australian I.R.E., 157 Gloucester Street, Sydney, New South Wales.)
 (British Overseas Fairs Ltd., 21 Tothill Street, London, S.W.1.)
International Air Show, Le Bourget, France
June 12-21 (Union Syndicale des Industries Aeronautiques, 4 rue Galilé, Paris XVle.) International Conference on Information Processing, Paris June 15-20 (B.C.A.C. Group B, c/o I.E.E., Savoy Place, London, W.C.2.)
I.R.E. International Symposium on Circuit and Information Theory, Los Angeles

June $16-18$
(Richard A. Epstein, Jet Propulsion Laboratory, Pasadena, California, U.S.A.)
International Chemistry Conference and Exhibition, Paris .... June 16-30 (Conférence Internationale des Arts Chimiques, 28 rue Saint-Dominique, Paris 7.)
International Electronic, Nuclear and Cinematographic Exhibition, Rome (Rassegna Internazionale Electronica Nucleare Via dell a Scrofa 14 Rome)
Second International Conference on Medical Electronics, Paris .. June 24-27 (Secretariat, 131, Boulevard Malesherbes, Paris XVIIe.)
National Convention on Military Electronics, Washington .... June 29-July 1 (L. R. Evringham, Radiation Inc., Orlando, Fla., U.S.A.)

German Radio, Television and Audio Show, Frankfurt
Aug. 14-23 (Messe- und Ausstellungs-GmbH., Frankfurt a.M.)
Western Electronic Show and Convention, San Francisco
Aug. 18-21 (Wescon, 1435 South La Cienega Boulevard, Los Angeles 35, Calif., U.S.A.)
International Congress on Acoustics, Stuttgart (Dr. Ing. E. Zwicker, Breitscheidstr. 3, Stuttgart.)
Salon Belge de l'Electronique, Brussels (Comité des Fxposition de a Radio-Flectricité de la Te cievision è de pt. 19-24 Connexes, 7 rue de Florence, Brussels, Belgium.)
National Symposium on Telemetring, San Francisco ( .......... Sept. 28-30 (Robert A. Grimm, Dymec Inc., 395 Page Mill Road, Palo Alto, Calif., U.S.A.) Irish Radio and Television Show, Mansion House, Dublin Sept.28-Oct. 3 (Castle Publications, 38 Merrion Square, Dublin, Eire.)
I.R.E. Canadian Convention, Toronto

Oct. 7-9 (Convention Office, 1819 Yonge Street, Toronto, 7.)
National Electronics Conference, Chicago (N.E.C., 84 E. Randolph St., Chicago, Ill., U.S.S.A.)

Conference on Electrical Techniques in Medecine and Biology, Philadelphia


## (HatIess at Hattield

People take off their hats at Hatfield. You can't help respecting the Comet-and everything that goes with it. Such as TRIXADIO. World record and sun beating Comet 4 has built-in TRIXADIO Passenger Announcement System for the convenience of its transmondial travellers.
The purpose of the Trix Electrical Company is to meet the exacting needs of engineers who seek high quality, long service and realistic costs. Trix equipment is built with integrity-and the pioneering spirit which is constantly in search of perfection.


* The first completely transistorised Aircraft Passenger Announcement and music system.
$\star$ The first Aircraft system using high efficiency Sound Column Radiators.
$\star$ Low weight-low power requirements-reduced wiring cost.
the trix electrical co. ltd.

I-S MAPLE PLACE, LONDON, W.I. Tel : MUSeum 5817 ( 6 lines). Cables \& Grams: Trixadio. Wesdo. London.
I

# RANDOM RADIATIONS 

## By "DIALLIST"

## Man-made Blackouts

ONE gathers that there has been considerable uneasiness in the U.S.A. owing to the discovery that wireless and radar signals can be blocked by bursting a nuclear bomb at a great height above the earth's surface. Before any announcement on the subject was made officially in America, Russian scientists had attributed the unexpected density of the inner radiation zone (which at the magnetic equator is $1,500-4,000$ miles above the earth) to the effects of nuclear explosions. Later, an official statement was made in the U.S.A. that, as part of the I.G.Y. programme, three such bursts had taken place last year at heights of about 300 miles. In each case the flash of the explosion was followed at once by a faint luminosity extending along the magnetic line of force through the burst point. This line of force returns to our atmosphere in the northern hemisphere near the Azores. Aircraft stationed in the region for observation purposes noted a short auroral glow. The work was then taken up by the satellite Explorer IV which, travelling day after day "through the manmade 'shell' of trapped radiation," sent back to earth measurements which enabled its intensity and shape to be worked out. It has been suggested that anyone mad enough or wicked enough to start a nuclear war could put the other side's distant early warning radar system almost, if not entirely, out of action by leading off with a number of bursts in the right places.

## Towards Better TV

THOUGH at the time of writing the Television Advisory Committee's report has not been completed, it seems almost a certainty that the definition recommended for Bands IV and $V$ will be 625 lines. If $8-\mathrm{Mc} / \mathrm{s}$ channels are adopted by international agreement ( $6-\mathrm{Mc} / \mathrm{s}$ for vision and $2-\mathrm{Mc} / \mathrm{s}$ for sound), this should certainly mean an overall improvement in picture quality. The change would, presumably, also mean adopting negative vision modulation and f.m. sound modulation. Improvements are always to the good and one must welcome them; but I've
always felt that when we do make use of Bands IV and V we should change things in a big way to, say, 1,000 lines or more and not be content with a mere fifty-per-cent rise in the number of lines. If, as the years go by, scanning remains the only practicable method of transmitting and reproducing television images, systems with a far greater number of lines than 625 are bound to come.

## Stereo Sound

AT the I.E.E.'s Stereophonic Sound Recording, Reproduction and Broadcasting Convention* it was clear that nobody yet really knows all the hows and whys of the process. 1 think that, like other animals, we were provided with two ears to enable us to turn our eyes towards the place from which the sound comes in case it is a warning of lurking danger. If the sound lasts an appreciable time, we seem to do this by turning our heads so as to phase up the waves reaching our eardrums. But what of short sharp counds such as the snapping of a twig? They don't last long enough for this to be done, yet we do instinctively look towards their source. Dr. Percival maintained that the directional signals are mainly in the transients and this may possibly explain our quick reactions to * See also p. 239 of this issue-Ed.
snappings, pops, bangs and so on. Then, as T. Somerville, of the B.B.C., pointed out, the use of two loudspeakers reproducing the right-hand and left-hand sounds would give directions in the horizontal plane only. For there to be an impression of vertical directivity three or more would be needed. Curious that; for our two ears certainly make us look up or down as the case may be for the source of any sound. No doubt it'll all be worked out in time and one of the most valuable things about a convention of that kind is that it helps people to realize just how much they don't know and stimulates them to try to find all the answers. Meantime, stereo-sound as it comes from our loudspeakers seems pretty good to me and recording it or listening to it has become one of the most popular of hobbies.

## TV on the Railways

CLOSED-CIRCUIT television is, I see, to be installed at some of the level crossings in France which can't be seen from the nearest signal box. At many of those on busy roads it has been necessary to have an employee permanently on duty; in future the man in the signal box will be able to see for himself just what's going on and to open or close the gates as required. Something of

this kind would be a vast improvement in the flatter parts of this country such as Cambridgeshire, where there are many level crossings. Quite a few of these are unattended and one can't always get a view of the rails for any great distance in either direction. Fixed high up, so as to be out of harm's way, the camera could be moved by the signalman by remote control so as to let him see vehicles approaching the crossing from either direction and enable him to open or close the gates at the right moment. Actually, television is already in use on our railways for other purposes. There's a camera, for instance, at the approaches to King's Cross Station in London which enables train arrival times to be checked and in marshalling yards.

## Mendlesham's TV Station

IF all goes well, the I.T.A. should be able to open its East Anglian TV station earlier than many people expected. Test signals are to start in July or August with an e.r.p. of 10 kW from a temporary aerial mounted at a height of about 500 ft on the unfinished mast. Full-power trade tests should start in October, provided that the $1,000-\mathrm{ft}$ mast is finished by then. That must depend a good deal on the weather and I take it that what is most wanted is that there should be no high winds. I haven't been Mendlesham way lately, so I don't know yet how that gigantic mast is getting on. When finished it should indeed be worth seeing, for I believe it will be the tallest TV mast in the country. It should be visible over a largish part of the Suffolk landscape.

## Guarantee Periods

SOME of the firms which rebuild cathode-ray tubes guarantee their products for seven months, others again for nine and a few for a full year. Rather a queer state of affairs, that! I expect that as time goes on they'll all adopt an agreed guarantee period. I've long felt that our valve and tube manufacturers should fall into line with those of other countries by giving a year's guarantee on all their wares. 1 don't think I'm wrong in believing that the bulk of British-made valves and c.r. tubes exported do carry such a guarantee. They certainly have to in territories where they have to compete with those manufactured in countries where this is the normal period of guarantee.

## Navigation Demands

 Perfection!In the functioning of the wealth of electrical gear which helps the modern sailor through log and dangerous waters - Radio, Radar. echo sounding and all the internal signalling equipment must be one hundred per cent efficient - the strength of every circuit lies in the quality of its electric and electronic components.


BULGIN have specialised in this field for over 35 years and their research division is daily overcoming problems, the solution of which will help to make the seas and the skies even safer. Let us help you with your problems.

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LIST No. S.259/PD


LIST No. S. 565 with K. 107 knob


LIST No. S.600/PD

## What is Truth?

AS I grow older, I come more and more to share the opinion of the late Henry Ford that "history is bunk," as I am constantly reading and hearing contradictory versions of historical events. I have always supposed that the first public demonstration of television was given by Baird at 22 Frith Street, Soho, in January 1926, but now I see that the famous Oxford Street store, which used to house the 2LO transmitter, is claiming that TV was demonstrated on its premises in 1925.* What am I to believe?

Then again, the Editorial Comment in the April issue tells me by its title that the Editor is in a similar difficulty about the late King Canute,

"Contradictory versions of events"
or Knud as his Danish compatriots call him. The Editor obviously favours the outmoded story that Canute sat on the beach near Southampton in the year A.D. 1028, and commanded the incoming tide to recede, fondly imagining that it would do so.

Nowadays most historians are agreed that Canute was no fool, and only staged this act to prove to his sycophantic followers that he had no magic powers. I am not, of course, suggesting that the Editor is wrong; after all, he had to choose between two versions just as I shall have to do in the case of the date and venue of the first public TV demonstration.

The classic instance of this difficulty of deciding between two versions of the same thing is not concerned with history but with natural history. We often read that the foolish ostrich sticks his head in the sand, thinking that because he can-

[^9]not see his approaching enemies, they cannot see him. The other version is that the ostrich is a highly intelligent bird which camouflages himself by crouching down amid the local desert scrub, and at the same time puts his head on the ground so that he can hear more clearly his enemy's footsteps and so decide whether he is coming or going.

You pays your money and you takes your choice.

## Lawless Listening

I WAS surprised when recently reading my wireless licence, to learn that I am not allowed to use a portable set with an external l.t. battery unless I am using it on my own premises or in some vehicle, marine or territorial, occupied by me. Thus, if my I.t. battery runs out when I am having a picnic on the beach, I must not plug the set into my car's electrical circuit, nor may I stagger down with the car battery so that I can connect it up to my portable set with a suitable series resistance.

Reading the regulations has made me very nervous, and as a result I nearly caused a nasty accident to a child the other day. I was taking advantage of one of those few lovely days we had recently, and was sitting on the beach with my portable. The I.t. ran out and I stepped across the road to a local electrical shop for a replacement. All they had in stock was a large $1 \frac{1}{2}$-volt dry cell which would not go into the battery compartment, but I bought this and soon had it connected up.

Unfortunately, a passing policeman saw me and as he walked in my direction I hastily disconnected the "evidence" and hurled it in the sea, narrowly missing the head of a child who was paddling. Baulked of his lawful prey, the policeman proved himself a man of resource and booked me under the Anti-litter Act. Can any of you legal pundits tell me if it would be a good defence to plead that the cell, when hurled away, fell on the seaward side of low tide mark.

## Correcting the O.E.D.

I SUPPOSE every reader has heard of the Oxford English Dictionary. It is to be found even in Cambridge, and by no means always in the inner recesses of booksellers' shops, hiding its head shamefacedly among those
volumes which the police periodically seize, and the magistrates order to be destroyed.
I refer to the O.E.D. here because it is proposed to issue a new supplement to it, and I have been looking at a list of suggested new words and expressions running from AL-AZ. Even in this small part of the alphabet there are more than 800 new words or phrases. In the list each word has printed alongside it the year in which it is thought it was first used.

There seems to be a large number of words and expressions wrongly dated; not only ordinary nontechnical ones but also the specialized ones which concern various technologies. I give herewith over a dozen words from the list, together with the years of first usage assigned to them, which will be of particular interest to readers of Wireless World.

| Alive (Electricity) | No Date |
| :---: | :---: |
| All-electric | No 1934 |
| All-mains | 1948 |
| Ampere-hour | 1940 |
| Ampere-turn | 1902 |
| Appleton layer | 1948 |
| Appleton region | 1932 |
| Asdic | 1939 |
| A.S.V. (Radar) | 1945 |
| Attenuation (Electricity) | 1943 |
| Audio | 1940 |
| Audio-frequency | 1923 |
| Automatic gain control | 1940 |
| A.V.C. .. .. | 1940 |

The Editor of the O.E.D. Supplement, 40, Walton Crescent, Oxford, seeks to know if any earlier use of these words is known. Before any of you get killed in the rush to enlighten him, I would point out that he does not want just vague memories. He wants to know exactly where the earlier usage occurs, and he wants each word dealt with on a separate sheet of paper of $6-\mathrm{in} \times$ 4 -in dimensions, which he will supply if necessary.

## Psychotrons

IN THE March issue, I was discussing the extra-spatial electrons of which I supposed ghosts and their world to be constructed. It has occurred to me that the expression "extra-spatial electrons" would be far too clumsy to come into general use as it will tend to do in years to come when some experimental research worker eventually plays Hertz to my theoretical Clerk-Maxwell. I would, therefore, suggest the word psychotrons to describe these extraspatial electrons.

I think that in 20 years time we shall be as familiar with the science of psychotronics as we are now of electronics. At least, some of us will be; by then others will be on the far side of the psychotronic curtain.

## ruberson <br> choose the

# Model 8 AvoMeter 

 for their Television \& Electronic LaboratoryPhotograph by courtesy of Thorn Electrical Industries Lid.

## $F$

N are typical of the many leading manufacturers of electronic, radio and television equipment who rely on AVO instruments.
The Model 8 AvoMeter shown in use is a 30 -range self-contained A.C./D.C. moving coil instrument, produced primarily for the electronic, radio and television engineer. The upper photograph shows a mounted pivot under examination. This is only one of many operations carried out in a special air-conditioned dust-free zone in the AVO factory to ensure the highest possible standards of accuracy and reliability.

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|  | AS 757 | AS 758 | AS 759 | AS 852 | AS 854 | AS 855 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Output voltage : | Bench$\pm 0-50$ | Bench or rack$\pm 0-30$ | Sub-Unit$\pm 1 \cdot 5-13 \cdot 5$ | Bench or rack$\pm 30-50$ | Sub-Unit <br> $\pm 11.5-32.5$ | Sub-Unit |
|  |  |  |  |  |  | $\pm 32.5-50$ |
| Output curreat : | $0-14$ | 0-10A | $0-14$ | 0-10A | $0-14$ | $0-14$ |
| Output reaietance : | $0.01 \Omega$ | $0.01 \Omega$ | $0.01 \Omega$ | $0.01 \Omega$ | $0.01 \Omega$ | $0: 01 \Omega$ |
| Output Z to $100 \mathrm{Kc} / \mathrm{s}$ : | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ | $0.2 \Omega$ |
| Stability factor | 200:1 | $150: 1$ | 200:1 | $150: 1$ | 200:1 | 200: 1 |
| Elpple and aoise (peair to peak) : | 1 mv | 1 mv | 1 mv | 1 m 7 | 1 mv | 1 mV |
| Mains input : | 90/130 Volta, 200/240 Volts. Permiesible devimition $\pm 7 \%$ |  |  |  |  |  |
| Dimensioas : | $124^{\circ} \times 8^{\circ} \times 13^{\circ}$ $\left.(33 \times 21 \times 33 \mathrm{~cm})^{4}\right)$ | $22^{\circ} \times 104^{\prime \prime} \times 16^{*}$ $(56 \times 27 \times 41 \mathrm{~cm}$. | $7 t^{\circ} \times 51^{\circ} \times 51^{\prime \prime}$ $(18 \times 15 \times 14 \mathrm{~cm}$. | $22^{\circ} \times 100^{\circ} \times 16^{*}$ $(56 \times 27 \times+1 \mathrm{~cm}$. | Appz. $8^{*} \times 6^{*} \times 6^{\circ}$ $(20 \times 15 \times 15 \mathrm{~cm}$. | $\begin{gathered} \text { Appx. } \\ 8^{\circ} \times 0^{\circ} \times 8^{\circ} \\ (20 \times 15 \times 15 \mathrm{em} .) \end{gathered}$ |
| Appr. weight : | $\begin{gathered} 25 \mathrm{lbs} . \\ (11.5 \mathrm{~kg} .) \end{gathered}$ | 55 lbe. ( 25 kg .) | $\begin{gathered} 71 \mathrm{ls.} \\ (3.5 \mathrm{~kg} .) \end{gathered}$ | $\begin{gathered} 60 \mathrm{lbs} . \\ (27 \mathrm{~kg} .) \end{gathered}$ | 81 bs. ( 3.8 kg .) | $\begin{gathered} 8 \mathrm{lbe} \\ (3.8 \mathrm{~kg} .) \end{gathered}$ |

[^10]
## Stabilised transistor power supplies



THE SOLARTRONELECTRONIC GROUPLTD
THE S OLAR THAMES DITTON SURREY Telephone: Emberbrook 5522 Telegrams and Cables: Solartron, Thames Ditton - International Telex: 23842 Solartron T.Dit.


## ... a higher $\alpha^{\prime}$ version of the recently announced OC200

The new Mullard silicon alloy transistor OC201 is similar to the recently introduced OC200, but with the average current gain increased from 20 to 30 and the minimum fox increased from 0.5 to $2 \mathrm{Mc} / \mathrm{s}$.

Like other transistors in the silicon alloy range now being introduced by Mullard, the OC201 has a low bottoming voltage and all the advantages of the well-known OC71 germanium series. In addition these silicon transistors feature a low collector leakage, reduced noise figure and high permissible operating temperature.

The maximum collector voltage of the OC 201 is 25 V , but its low bottoming voltage allows it to be operated from supplies as low as 1.2 V . The linearity of current gain with collector current is well-maintained up to 50 mA .

The $2 \mathrm{Mc} / \mathrm{s}$ cut-off frequency and high permissible junction temperature rating of $150^{\circ} \mathrm{C}$ of this silicon transistor enable it to be operated at relatively high frequencies with a power dissipation of 100 mW at $100^{\circ} \mathrm{C}$.

The OC201 is now being put into large scale production and designers can depend on it to remain available for many years as a standard transistor. Write on your company notepaper to the address below for complete data.

## ABRIDGED DATA

Silicon p-npp alloy junction translstor OC201
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## DELAYED PULSE AND <br> SWEEP GENERATOR

A versatile pulse generator designed to meet the need for a comprehensive
instrument covering a wide range of pulse work. Four main facilities are provided: a pre-pulse, a main pulse delayed on the pre-pulse, a negative going sawtooth and a fast rising pulse formed from a pure line.


## BRIEF SPECIFICATION

## Period

Continuously variable from 0.9 usec to 1.05 sec i.e. $0.95 \mathrm{c} / \mathrm{s}$ to $1 \cdot 1 \mathrm{Mc} / \mathrm{s}$. Accuracy $\pm 5 \%$.

## Pre-pulse

$40 \mathrm{~m} \mu \mathrm{sec}$. 8 V peak in $75 \Omega$, positive going.

## Main pulse

Width: Variable from $0.09 \mu \mathrm{sec}$ to 105 msec $\pm 5 \%$.
Amplitude: Control gives 4:1 attenuation of each of four maximum outputs as follows: 5 V max in $75 \Omega$ rise time $10 \mathrm{~m} \mu \mathrm{sec}$ 10 V max in $150 \Omega$ rise time $<20 \mathrm{~m} \mu \mathrm{sec}$ 25 V max in $600 \Omega$ rise time $<40 \mathrm{~m} \mu \mathrm{sec}$ 50 V max in $1000 \Omega$ rise time $50 \mathrm{~m} \mu \mathrm{sec}$
Polarlty: Positive or negative going.
Accuracy: $\pm 2 \%$.

## Delay

Conclusion of pre-pulse to advent of main pulse, delay variable from $0.09 \mu \mathrm{sec}$ to 105 msec . Accuracy $\pm 5 \%$.

## Sweep

D.C. coupled negative going sawtooth same width and delay as main pulse. 15 V peak max.

## Cable pulse

Obtained from short circuited pure line. One positive and one negative going pulse coincident with main pulse.
$25 \mathrm{~m} \mu \mathrm{sec}$ wide $3 \mathrm{~V} \max$ in $75 \Omega$, rise time $<8 \mathrm{~m} \mu \mathrm{sec}$.

Sync, trigger or single shot facilities provided. Full data available on request.

[^11]
## For large sets ...

A line-up of large radar valves specially designed to provide high performance and reliability at a very competitive price.


## Magnetron JP9-75

Unlike other magnetrons of similar ratings, the JP9-75 is specifically designed for marine installations with subsequent suitability and economy. It provides highly
stable pulse operation with pulse durations of 0.1 and 1.0 microsecond and will deliver peak output powers of up to 80 kilowatts. Frequency is within the range 9345 to $9405 \mathrm{Mc} / \mathrm{s}$.

Pulse Modulator XH8-100 (CV1787)
Hydrogen-filled pulse modulator with a peak cathode current of 90 amps . Directly equivalent to the American 4C35.

Klystron KS9-20A (CV2792)
Mechanically tuned reflex klystron directly equivalent to the American 2K25.
Frequency range 8500 to $9660 \mathrm{Mc} / \mathrm{s}$.


The valves in this advertisement
are not shown to scale. 1

Pulse Modulator QV20-P18 (CV2752)
Vacuum pulse modulator with a peak anode current of 18 amps . Directly equivalent to the American 4 PR60A.

## Valves for

 Marine

## For small sets ...

This Mullard line-up of radar valves is designed to achieve the maximum economies in power consumption and in the cost of associated components - both essential requirements in small ship installations.


## Pulse Modulator EL360

Another Mullard development. This vacuum pulse modulator is recommended for operation with the
JP9-2.5 magnetron.
Maximum peak cathode current 4.0 amps .

## Klystron KS9-20 (CV1795)

Mechanically tuned reflex klystron directly equivalent to the American 723A/B. Frequency range 8702 to $9548 \mathrm{Mc} / \mathrm{s}$.
approximately 3 kW . Tested for operation with pulse lengths down to 20 millimicrosecs.

## Magnetron JP9-2.5

A new valve designed by Mullard specifically to meet the demand for a low power pulsed magnetron for use in " economical " radar navigation equipment. Operating frequency within the range 9345 to $9475 \mathrm{Mc} / \mathrm{s}$ and peak output power


Vacuum Pulse Modulators

Klystrons

Abridged guide to Mullard Valves for Radar Please write to the address below for further information.

| Magnetrons | Mullard No. <br> JP8-02 <br> JP9-01 <br> JP9-2.5 <br> JP9-7 <br> JP9-7A <br> JP9-7B <br> JP9-7D <br> JP9. 15 <br> JP9-75 <br> JP9-80 <br> JP9-80A <br> JP9-250 <br> JP9-250A <br> JPI 6-40 <br> JPT6-01 <br> JPT8-01 <br> JPT9-01 <br> JPT9-02 <br> JPT9-60 | $\begin{gathered} \text { Services } \\ \text { No. } \\ = \\ \text { cV3676 } \\ \text { CV370 } \\ \text { CVIB66 } \\ \text { CV3997 } \\ \text { CV3569 } \\ \text { CV5018 } \\ \text { CV2284 } \\ \text { CV3953 } \\ - \\ \text { CV } \\ \text { CV2420 } \\ \text { CV3560 } \end{gathered}$ | American No. $=$ 7028 2142 $=$ 2142 A 6972 4152 4152 A 4150 $4 J 78$ $=$ $=$ $2 \overline{2} 1 \mathrm{~A}$ |
| :---: | :---: | :---: | :---: |
| Hydrogen-filled Pulse Modulators | $\begin{gathered} \text { XH3-045 } \\ \text { XH8-100 } \\ \times H 16-200 \\ \times H 25-500 \end{gathered}$ | $\begin{aligned} & \text { CV372 } \\ & \text { CV1787 } \\ & \text { CV2520 } \\ & \text { CV3521 } \end{aligned}$ |  |
| Vacuum Pulse Modulators | EL360 | $\left\{\begin{array}{l}\text { CV2295 } \\ \text { CV3599 }\end{array}\right.$ | 3E29 |
|  | $\begin{aligned} & \text { QVIO-P8 } \\ & \text { QV20-P18 } \\ & \text { QYS50-P40 } \end{aligned}$ | $\begin{gathered} \mathrm{Cv}_{27} 52 \\ \mathrm{C} 313 \end{gathered}$ | 4PR60A |
| Klystrons | $\begin{array}{r} \text { KS7-85 } \\ \text { KS7-85A } \\ \text { KS9-20 } \\ \text { KS9-20A } \\ \text { KT9-150W } \end{array}$ | $\begin{aligned} & \overline{-} \\ & \text { CV1795 } \\ & \text { CV2792 } \end{aligned}$ | $\begin{gathered} 2 K 26 \\ 5976 \\ 723 \mathrm{~A} / \mathrm{B} \\ 2 \mathrm{~K} 25 \end{gathered}$ |

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## Pentode Video Stage with Cathode Compensation

In the April issue of Electronic © Radio Engineer there is an article which discusses the general theory and design requirements of a cathode-compensated pentode video amplifier. Step and steady-state response curves are included and it is shown that by allowing some overshoot in the step response an improvement in both rise-time and bandwidth can be obtained.

## ARTICLES IN THE MAY ISSUE INCLUDE

Subjective Impairment of Television Pictures.
This article describes subjective tests carried out to determine the effect of noise in degrading television pictures, both 105 -line and 625 -line. Based on these tests a method of relating signal-noise ratio to the degree o: user satisfaction is derived.
Digital Voltmeter.
This article describes a digital decade voltmeter employing Dekatron selector tubes. It is shown that the instrument has great accuracy, high operating speed and very high input impedance

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MODEL 1439 WIDE-BAND AMPLIFIER
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The Amplifier is designed to provide simultaneous distribution of signals anywhere in Bands I, 11 and 111 , enabling a common aerial to be used for a number of television or VHF radio receivers or other applications requiring a wide band voltage amplifier.
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Input and output impedance: $72 \Omega$ (matched coaxial).


## MODEL 1440 PRE-AMPLIFIER

This instrument is a directly coupled pre-amplifier of high stability which has been designed for use in cascade with a further amplifier or with a recording device.
Frequency response : d.c. : $0-50 \mathrm{kc} / \mathrm{s}$, a.c. $: 5 \mathrm{c} / \mathrm{s}-50 \mathrm{kc} / \mathrm{s}$. Gair: continuously variable 10-55 (d.c.), 165 (a.c.) Input: balanced or unbalanced, impedance $11.2 \mathrm{M} \Omega$ (grid-grid.)
Output: balanced or unbalanced, impedance $2000 \Omega$ (output 1-output 2).
Output voltage: 5 V pk-pk max. (output I-output 2). Calibration signal: 1 mV or 10 mV .


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The Instrument Company of the Cossor Group

## New oscillograph 1059

## ADVANCED *TRUE DOUBLE-BEAM OSCILLOGRAPH

* 

True double-beam-i.e. both beams use a common $x$-axis and there is no beam switching.

## CATHODE-RAY TUBE

Cossor 4 in . ( 10 cm .) double-beam, p.d.a،, type 93D with green fluorescence, operating with overall accelerating potential of 3 kV or 6 kV .

## YI AMPLIFIER

$1 \mathrm{c} / \mathrm{s}$ to $10 \mathrm{Mc} / \mathrm{s}(30 \%$ down).
Rise-time : 0.04 usec.
Output deflection : $6 \mathrm{~cm}(4 \mathrm{~cm}$ at $10 \mathrm{Mc} / \mathrm{s})$.
Sensitivity: calibrated $100 \mathrm{mV} / \mathrm{cm}$ to $10 \mathrm{~V} / \mathrm{cm}$. Sensitivity control: in steps 3:1 and 10:1 with continuously variable intermediate control. Input Attenuator impedance : $1.2 \mathrm{M} \Omega$ and 65 pF .

## Y2 AMPLIFIER

Identical with Y1 amplifier.

## SIGNAL DELAY

200 musec approximately. Not more than 10 musec differential between channels.

## PRE-AMPLIFIER (2)

Gain 10. $5 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}(30 \%$ down). Input Resistance: $3 \mathrm{M} \Omega$.
One for A1 amplifier, the other for A2 or $X$ amplifier.

## PROBES (OPTIONAL EXTRA)

Frequency-compensated "L" attenuator.
Input impedance: $6 \mathrm{M} \Omega$ and 15 pF .
Insertion loss: 10:1.

## TIME-BASE

Triggered.
Range: $0.03 \mu \mathrm{sec} / \mathrm{cm}$ to $15 \mathrm{msec} / \mathrm{cm}$ in eleven steps. Triggered from positive or negative signals derived externally or from Y1 amplifier.
Sensitivity: pulse -1 cm . deflection or 2 V external. Sine wave -2 cm deflection or 2 V r.m.s. external at frequencies up to $5 \mathrm{Mc} / \mathrm{s}$. Expansion amplifier, continuously variable gain up to $S$ times. Time-base output available at front panel on slow speed ranges. Delayed time-base: continuously variable delay $2 \mu \mathrm{sec}$ to $150 \mu \mathrm{sec}$. Delay jitter not greater than 1 part in 1,000 . Sensitivity pulse -1 cm deflection or 2 V external.

## X AMPLIFIER

$10 \mathrm{c} / \mathrm{s}$ to $750 \mathrm{kc} / \mathrm{s}(30 \%$ down).
As time-base amplifier : continuously variable expansion up to 5 times.
As independent $X$ amplifier: senstivity variable from $1 \mathrm{~V} / \mathrm{cm}$ to $100 \mathrm{~V} / \mathrm{cm}$ in 5 ranges.

## CALIBRATION

Voltage measurement: internal calibrating voltage (square wave) referred through sensitivity control of the amplifiers. Accuracy $\pm 3 \%$. Time measurement : by directly calibrated X shift control ( $\pm 5 \%$ ) and/or by $20 \mathrm{musec}( \pm 3 \%)$ black-out pips (for accurate measurement of rise-time).

## POWER SUPPLY

Mains: 100 V to 130 V and 200 V to 250 V . Frequency: $50 \mathrm{c} / \mathrm{s}$ to $100 \mathrm{c} / \mathrm{s}$.
Consumption: 550 W .
Internal supplies are stabilized where necessary.

## SIZE AND WEIGHT

| Height: | $17 \frac{1}{2} \mathrm{in}$. | $(43.2 \mathrm{~cm})$. |
| :--- | :--- | :--- |
| Width: | 12 in. | $(30.5 \mathrm{~cm})$ |
| Depth: | $24 \frac{\mathrm{in}}{\mathrm{in} .}$ | $(62.9 \mathrm{~cm})$ |
| Weight: | 80 lb. | $(36.3 \mathrm{~kg})$. |

## ACCESSORY

Camera Model 1428.

## COSSORINStRUMENTS LTD <br> The Instrument Company of the Cossor Group



## ELECTRONICS

New. concepts in electronics have been developed at AWA, as a result of experience with missile systems. Now they have a wider application. Here are some of the new AWA devices now available to industry.

## TRANSISTOR

## GALVANOMETER

AMPLIFIER


This Amplifier has been designed to drive viscous damped recording galvanometers which normally have a resistance of 50 ohms and a working range of D.C. to $2 \mathrm{Kc} / \mathrm{s}$ in frequency. The amplifier has a switched attenuator at its input and will accept single ended or push pull signals from $\pm 1$ Millivolt to $\pm 500$ volts and will feed a maximum of $\pm 50$ Milliamps to the galvanometer. There is also a range of ancillary units available for use with this Amplifier as part of a comprehensive instrumentation system. Standard specification: Dimensions: $4 \frac{1}{4}$ in. $\boldsymbol{x}$ $3 \frac{3}{4} \mathrm{in} . x 10 \mathrm{in}$; Frequency response: Flat from $D C$ to $2 \mathrm{Kc} / \mathrm{s}$, $5 \%$ down at $3 \mathrm{Kc} / \mathrm{s}, 3 \mathrm{db}$ down at $6 \mathrm{Kc} / \mathrm{s}$; Noise level: less than 10 Microvolts; Input impedance: 40,000 ohms on range 5, 110,000 ohms all other ranges; Gain: Maximum 7.5 Milliamps/ Millivolt, minimum 0.04 Milliamps/Volt; Power requirements: $\pm 6$ Volts D.C. 220 Milliamps each line.

COMEL 8 \& 12 SWEEP OSCILLATOR
AND VIBRATION CONTROLLER


This unit is designed to drive vibrator ampliters and has a wide frequency range. The sweep speed is variable over a range $12: 1$ and automatic frequency sweep facilities are provided. Frequency range: 10 c.p.s. to $32 \mathrm{Kc} / \mathrm{s}$ in ranges of 5 octaves each. There are 7 switch speeds ranging from 5 secs./octave- 60 secs./ octave. Variety of Outputs available. Vibration Controller: Input: 4 V r.m.s. at appropriate frequency. Output: Up to 100 mV r.m.s. into 600 ohms. Pick Off: Sensitivity 10 mV r.m.s. per " $g$ " peak. Overall Dimensions: $35^{\prime \prime} \times 22^{\prime \prime} \times 14^{\prime \prime}$. The Vibration Controller will control $\pm 40$ " $g$ " or as determined at low frequencies by the excursion of the vibrator table.

All devices are adaptable to suit customers' own requirements. For further information consult :

## COMMERCIAL ELECTRONICS DEPT.

SIR W. G. ARMSTRONG WHITWORTH AIRCRAFT LTD., Baginton, Coventry MEMBER OF THE HAWKER SIDDELEY GROUP


# Magnetic Attraction Applications - 2 

Advertisements in this series deal with general design considerations. If you require more specific information on the use of permanent magnets, please send your enquiry to the address below, mentioning the Design Advisory Service.

The performance of modern magnets enables engineers to design equipment with smaller dimensions or improved performance, and has made practical the development of efficient magnetic couplings which transmit torque through hermetically sealed diaphragms.
The magnets in magnetic couplings cannot exert the same useful force as similar magnets would when in contact. This is due to two reasons:-
(a) There is of necessity, a gap in the magnetic circuit to accommodate a partition between the two sections of the coupling.
(b) The direct pull between the magnetic poles cannot be used since it is only the shearing force that transmits the torque.

Fig. 1



Fig. 2


When the poles are coincident there is no resultant tangential force as in fig. 1.
When the poles are displaced, the force between the poles is at an angle so that the force can now be considered to consist of two vector quantities F. (radial) and F. (tangential) as in flg. 2.

Maximum torque is generally obtained when the poles are displaced by about half a pole width.
It will be obvious from the above diagrams that torque is produced over a limited range by the angular displacement between the two sections and that the torque transmitted by a given coupling depends on the number of poles, their strength and their distance from the axis of rotation.

In the example fig. 3 , the material forming the partition separating the two sections of the


Fig. 3

coupling has received considerable attention. If non-conducting materials are considered, difficulties are introduced in design and manufacture due to lack of strength and difficulty with hermetic sealing. Metals are particularly suited to manufacturing methods as they can be welded or brazed to produce really sound hermetic seals. It should be noted however, thateddy currents are produced by the moving magnetic flelds and the resultant heating and loss of torque may become serious if the coupling is driven fast.
For certain applications, it is advantageous to make the partition from stainless steel, which has the advantage of great physical strength so that the thickness of material may be kept to a minimum, and the reluctance of the magnetic circuit reduced. Moreover, the relatively high resistivity of stainless steel tends to keep the eddy currents and heating effects to a low and tolerable value. Stainless steel has a further advantage in that it is slightly magnetic and consequently reduces the effect of the air gap; but if the pole spacing is small, loss of -flux and performance may result from direct conduction of flux between the poles by the stainless steel.
Hermetically sealed magnetic couplings are in everyday use giving effective torques up to 100 lb ./ft. with pressure differences of up to $1,000 \mathrm{lb}$./sq. in. between the two sections, and larger sizes present no difficulties in design and construction.

If you wish to receive reprints of this advertisement and others.in this series write to the address below.

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## ... secured by Plessey



Approximately twice life size

## SUB-MINIATURE COAXIAL CONNECTORS

As a contribution towards increasingly compact equipment, Plessey have introduced this new, highest quality and fully comprehensive range to allow a new approach on applications hitherto restricted by the limitations of existing connectors. Designed for the matched impedance coupling of high frequency coaxial cables operating in the super high frequency bands, these connectors-

* have a working voltage of 650 volts Peak at sea level, and matched impedance coupling of 50 ohm lines is accommodated.
* have hard gold plated contacts on silver plate to give maximum performance with minimum voltage drop.


For further information, please write for Publication numbers 128 and 114.


3 WATTS The Hand Portable Electronic Megaphone weighs only 5 lb . The transistor amplifier gives more than 3 watts output. It uses standard torch batteries which last about six months.
The Portable Electronic Megaphone with adjustable stand and separate microphone

Pye Portable Public Address equipment is transistorised for maximum portability and minimum current consumption. It is the perfect answer to all situations where mobility, temporary use or lack of power supplies make it impractical to use more conventional systems.
Ideal for police, fire services, political meetings and electioneering vehicles, garden fetes and sports meetings, touring coaches and all types of ships, passenger and freight control on railways, building operations and many others too numerous to mention. Intrinsically safe versions of this equipment are available which have been certified as suitable for use in methane and pentane atmospheres by the Ministry of Power and the Ministry of Labour Factory Inspectorate.


10 WATTS The Portable Transistor Amplifier weighs only $5 \frac{1}{2} \mathrm{lb}$. and measures $8^{\prime \prime} \times 3 \frac{1}{2}^{\prime \prime} \times 6^{\prime \prime}$. It will deliver 10 watts output for a consumption of 1.8 amps from a 12 volt battery. It is ideal for use in moving vehicles or on sites where a mains supply is not available. A comprehensive selection of microphones and loudspeakers is available.


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- by appointment

TO HRH. DUKE OF EDINBURGH SUPPLIERS OF
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Fan Marker Beacon

The Pye PTC IIzo Marker Beacon is designed to meet the requirements of the I.C.A.O. Specification relating to a $75 \mathrm{Mc} / \mathrm{s}$ en Route Marker Beacon for air navigation. The Beacon radiates a horizontally polarised fan-shaped vertical beam modulated at $3000 \mathrm{c} / \mathrm{s}$.
The equipment is self-monitoring and includes automatic changeover to a standby transmitter. Suitable for use on $100-200 \mathrm{~V}$. a.c. with a maximum power consumption of 0.75 kVA .

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## Frequency shift

## Keyer

A very high stability oscillator/driver produces a linear frequency shift signal suitable for keying any transmitter having a suitable input connection. The equipment may be used for the transmission of teleprinter signals, high speed telegraphy, facsimile or narrow band F.M. telephony. Three crystal controlled spot frequencies and the facility of connecting an external oscillator are provided.

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## GK. 188 <br> 

## OUTPUT FREQUENCY

1.0 to $7.0 \mathrm{Mc} / \mathrm{s}$.

TRANSMITTER MULTIPLICATIONS
Pre-selection of correct frequencyshift for transmitter frequency multiplication of $2,3,4,6,8,9$. or 12 separately adjustable for each channel.

## FREQUENCY SHIFT

Adjustable 0 to $1000 \mathrm{c} / \mathrm{s}$.
Linear up to $\pm 700 \mathrm{c} / \mathrm{s}$.

## POWER OUTPUT

3 watts into 50 to 75 ohms.

## KEYING SPEED

Up to 375 w.p.m. ( 300 bauds).

## OVERALL STABILITY

$20 \mathrm{c} / \mathrm{s}$ for $0^{\circ}$ to $50^{\circ} \mathrm{C}$ and $\pm 10 \%$
mains voltage variations.

POWER SUPPLY
$100 / 125$ or $200 / 250$ volts $50 / 60 \mathrm{c} / \mathrm{s} \mathrm{a.c}$.

## Redifon AFS. 13 TWINPLEX COMBINER

This compact unit when used in conjunction with the GK 188 provides two channels on which entirely independent teleprinter or telegraphy signals may be transmitted simultaneously thus doubling the traffic capacity on one carrier.

- Channel 1 of twinplex transmission may be received on standard F.S. receivers.
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## II This incomparable

 Ferrograph of mine＂It was a letter from a customer．He was telling us how－
temporarily at a loose end after selling his business－he decided to take up tape recording as a hobby．＂Because for years good music had been my secret passion＂he wrote，＂I wanted to make sure that I bought the right machine．How glad I am today that I did take so much trouble， for few purchases have ever given me so much pleasure as this incomparable Ferrograph of mine．Quite literally，it has opened wide the doors to the great masters and enabled me to enjoy their music as never before．＂
Of course not everyone is a keen student of music and the extremely high standard of performance attainable with a Ferrograph would not be required by those content to use a Tape Recorder merely as a pleasant source of home entertainment．We make no secret of the fact that－due to a policy of restricted output（inevitable when quality instead of quantity is the controlling factor）－the Ferrograph costs more than most others．But this is the price one pays for quality without compromise－for the ultimate in performance－for the satisfaction of knowing that there is nothing better even if you are as rich as Croesus．

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With standard monaural Recording／ Playback facilities
Model $4 \mathrm{~A} / \mathrm{N} 3 \frac{1}{2} / 7 \frac{1}{2}$ i．p．s．$\quad 81 \mathrm{gns}$ ．
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＊Model 4AH／CON 71／2／15 i．p．s． 86 gas．
－Suffix CON－denotes chassis．form for building into own cabinet．

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With optional stereo sound playback facilities in addition（when used with Stere－Ad Unit．）
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Stere－Ad Unit（when required） 30 gns ．

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With full stereophonic recording and playback facilities Model $887 \frac{1}{2} / 15$ i．p．s． 105 gins．
full technical details．

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Ferrograph BRITISH FERROGRAPH RECORDER CO．LTD．
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All round the World this Airmec receiver is known and used for its remarkable performance at an extremely low cost.

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Main tuning control showing a portion of the seven frequency scales, the coarse and fine logging scales and the movable cursor.

- Frequency coverage from $15-45 \mathrm{kc} / \mathrm{s}$ and $100 \mathrm{kc} / \mathrm{s}$ - $30 \mathrm{Mc} / \mathrm{s}$.
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## ADDITIONAL FEATURES

- Separate incremental tuning control for use with crystal calibrator.
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(1) Image rejection over 100 db .
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£ 16
Input $230 / 240 \mathrm{~V}$. Output 50 V . to 250 V . in 16 steps of $\mathbf{1 2 . 5}$ V. at 25 Amps. These are Auto Transformers with Quick Make-and-Break Tapping Switches.


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1450 V. $300 \mathrm{~mA} . \varepsilon 8100$ $3 \mathrm{kV} .2 \mathrm{~mA} . \ldots . . \in 40$ $10 \mathrm{kV} . .23 \mathrm{~mA} . . .696$ $4 \mathrm{kV} .2 .5 \mathrm{~mA} . \ldots$ E5 0


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63 V DC 13 Amps and 220
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INPUT 420 V . OUTPUT 0/420 V. Change per Step, 6.5 V. $(1.6 \%)$

## 40 Amps.

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It is extremely compact ( $8 \frac{1}{2} \mathrm{in} . \times 6 \frac{1}{2} \mathrm{in} . \times 13 \mathrm{in}$.) and has a performance and specification unequalled by many much larger instruments.

A D.C.-coupled amplifier ( -3 db at $6 \mathrm{Mc} / \mathrm{s}$ ), voltage calibration, wide-range calibrated time base ( .5 sec to $1 \mu \mathrm{sec}$ per cm .) and a precision flat-faced C.R. Tube are only a few of the features that put the S31 far ahead of any other portable scope.

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Above: $2^{\prime \prime}$ square moving coil voltmeter

## * designed to harmonise with all modern electronic equipment <br> * fixings conform to accepted practice * PRIGES ARE highly competitive

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RESISTANCE TO IMPACT SHOCK OF 200 g in any plane.
VIBRATION FATIGUE TEST-two million cycles at peak resonant frequency.
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Rectifier moving coil for A.F. applications.

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Design registrations pending.


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Over 50 standard ranges in any of the seven case types.

Delivery ex stock for standard ranges.
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Literature available on request to The ENGLISH ELECTRIC Co. Ltd., Instrument Department, Stafford.

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our comprehensive range of attenuators we announce the addition of 4 new models. These attentuators employ resistive ladder network and provide accurate attenuation over a wide frequency band. They are small compact units ideal for building into customers' own equipment or for bench use in the laboratory. Full details are given in leaflet No. W57, gladly sent on request.
by Whartedale

QEGISTERED TRADE MARK Model W3
The W3 is a three-speaker system in which compactness has been achieved without sacrificing quality of reproduction and without introducing " small box " tonal character. It is ideal for use on a stereo or single channel input where room space is limited, as the cabinet may be stood vertically on the floor or placed horizontally on a table or shelf. The sensitivity is high enough to give full domestic volume with any good commercial FM receiver with about 3 watts output.

BASS
L.F. output is produced by a special 12 in . unit type WLS/ 12 fitted with a heavy cone and a new type of suspension which permits large linear excursions and gives a low fundamental resonance of $25-30 \mathrm{c} / \mathrm{s}$.

## TREBLE

The upper registers are handled by 5 in . and 3 in . units connected in parallel via a quarter section $1 \mathrm{kc} / \mathrm{s}$. dividing network, with an extra series capacitor to protect the small speaker.
Two volume controls permit adjustment of midrange and treble to give tone control and facilitate balancing different speakers on stereo.
Cabinet size $28 \times 14 \times 12 \mathrm{in}$.
Weight 48 lb . complete. Impedance 15 ohms.
Max, input 15 watts.
Effective frequency range $30-17,000 \mathrm{c} / \mathrm{s}$.
Price $\mathbf{E 3 9 / 1 0 / \text { - complete, tax free. }}$
The elegant cabinet is fully finished on all four sides In a choice of wainut, oak and mahogany. Also available in whitewood price $£ 36 / 10 /$. Tropical model made with resin bonded plywood can be supplied at $£ 2$ extra.

## Model W2

This two-speaker model also employs the WLS/12 unit for the bass with crossover at I $\mathrm{kc} / \mathrm{s}$. to a Super 5 loudspeaker fitted with volume control for adjustment of H.F. response.

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The tables below give data relating to some of the Transmitting Valves manufactured by the English Electric Valve Company. The full list of these valves, complete specifications and characteristics can be obtained on application to the Company.
All valves listed below have thoriated tungsten filaments.

| E.E.V. <br> Type | EquivalentTypes | Service Type | Filament |  | Frequency MC/S § | Anode voltage max. (kV) | Anode dissipation max. (kW) | Type of cooling |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Voltage (V) | Current (A) |  |  |  |  |
| 5867 | 5867, TY3-250 | CVI350 | 5.0 | 14.0 | 150 | 3.0 | 0.25 | Natural to $30 \mathrm{Mc} / \mathrm{s}$ |
| 833A | TY4-350, 833A | CV635 | 10.0 | 10.0 | 30 | $\{3.0$ | 0.3 ) | $\left\{\begin{array}{l}\text { Natural }\end{array}\right.$ |
| $\ddagger 5762$ | TY6-5000A, ACT30 | CV2383 | 12.6 | 29.0 | 30/220 | 4.0 6.2 | 0.4 3.0 | Forced air Forced air |
| BR 161 | - | CV2322 | 9.0 | 175.0 | 30/50 | 12.0 | 15.0 | Forced air |
| BR 189 | - | - | 9.0 | $240 \cdot 0$ | 5/50 | 15.0 | 27.0 | Forced air |
| BR 1122 | - | - | $6 \cdot 0$ | 115.0 | 5/110 | 12.0 | 10.0 | Forced air |
| BW 161 | - | - | 9.0 | 175.0 | 30/50 | 12.0 | 30.0 | Water |
| BW 189 | - | - | 9.0 | $240 \cdot 0$ | 5/50 | 15.0 | 35.0 | Water |
| BY 189 | - | - | 9.0 | $240 \cdot 0$ | 5/50 | . 15.0 | 35.0 | Vapour |
| CR 192 | 6166 | - | 5.0 | 175.0 | 30/220 | $6 \cdot 0$ | 10.0 | Forced air |
| CRII00 | QY5-3000A | - | $6 \cdot 3$ | 32.5 | 110/220 | $5 \cdot 0$ | 3.0 | Forced air |
| 6181 | 6181, CRIIO1 | - | 120 | 1.6 | 900 | $2 \cdot 0$ | 2.0 | Forced air |

$\ddagger$ Previously BR 191 B
§ The lower value indicates the operating frequency at full rating. Operation at the higher value is possible. with suitable derating.

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Harmonic Distortion:
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MAXIMUM POWER OUTPUT
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OUTPUT SOCKETS.
Provide matchings for 3 ohm and 15 ohm loudspeakers.
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300 v. $30 \mathrm{~m} / \mathrm{a} .6 .3 \mathrm{v} .1 .5 \mathrm{a}$. for radio tuner. VALVES. B.V.A. EF86, EF86, ECC83, EL34, EL34. GZ34.
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## Aspects of design

This is the eleventh of a series of special features dealing with advanced problems in television and radio circuit design to be published by Siemens Edison Swan. The Ediswan Mazda Applications Laboratory will be pleased to deal with any questions arising from this or other articles, the twelfth of which will appear in the June 1959 issue.

# 11 <br> TRANSISTOR FREQUENCY CHANGER 

Most portable transistorised broadcast receivers in current production use a frequency converter stage consisting of a single transistor working as a self-oscillating additive frequency mixer. Although the use of two transistors in an oscillator-mixer combination is often desirable, it is apt to be too costly at present. For normal Medium Wave tuning coverage, the local oscillator must perform satisfactorily at $2.1 \mathrm{Mc} / \mathrm{s}$. For this reason it is usual to specify a rather better high-frequency performance for a mixer transistor than would be required in the I.F. stages. The XA102 has been designed to meet this need.
To keep the cost within reasonable limits, most designs take the form shown in the diagram. Oscillations are maintained by mutual inductance coupling between collector and emitter circuits, while the signal frequency is applied to the base. Thus the transistor is operating as a common-base oscillator, but to signal frequencies it is a common-emitter stage.
Because of the particular requirements of the circuit and the relatively high levels of voltage swing on the transistor, the smallsignal parameters of the transistor are not of much assistance when designing the oscillator transformer or choosing the running conditions of the stage. The final design is best arrived at experimentally, taking the following factors into consideration:(a) Battery supply voltage variations

Each cell may measure 1.6 volts when new, yet it will often not be replaced until it has dropped below 1.0 volts.

## (b) Bias Resistor Tolerances

A tolerance of $\pm 10 \%$ on resistors is desirable, $\pm 5 \%$ resistors being disproportionately expensive.

## (c) Tuning Frequency

Because a common oscillator coil is used (for reasons of economy) for the M.W. and L.W. bands, there is a considerable variation of power losses in the coil as the tuning is varied. The efficiency is lowest at the low-frequency end of the L.W. band where the dynamic resistance of the oscillator tank circuit is a minimum. The level of the heterodyne voltage is therefore lower on the long wave band than on the medium wave band.
(d) Transistor Parameters

The important parameters in this circuit are $\beta$ (common-emitter current amplification), $\mathrm{f}_{\alpha}$ (frequency of current amplification cut-off) and rbe' (extrinsic base resistance). Although the spread on these parameters is controlled in production there is no rigid relationship between them and it is possible for the effects of the resultant deviations to add up in any transistor used in the mixeroscillator stage.


The circuit should accommodate all of these variables yet maintain oscillations over the tuning range without squegging.
The conversion power gain obtained with the circuit shown is nominally 31 dB at $1 \mathrm{Mc} / \mathrm{s}$, excluding the losses in the 1st I.F. transformer. Base-emitter heterodyne voltage is approximately 250 mV peak on the M.W. band and 120 mV peak on the L.W. band.
For frequency stability the oscillator tank coil should have a high working $Q$, but this complicates the choice of turns ratios for the oscillator transformer. If the transistor is effectively tapped well down towards the "earthy " end of the tank coil, working Q will be high but power loss in the coil will also be high and it will be difficult to keep the circuit oscillating under the above limit conditions. If the transistor is tapped higher up the coil, oscillation amplitude may appear satisfactory but performance may vary widely with different transistor samples or with change of battery volts. Tracking between aerial and oscillator circuits may also be difficult to achieve. In the circuit shown, the turns ratios quoted are satisfactory provided there is very tight coupling between the emitter and collector windings, and the unloaded $\mathbf{Q}$ of the tank circuit is about 100 at $1 \mathrm{Mc} / \mathrm{s}$.
The resistors $R_{1}, R_{2}, R_{3}$ and $R_{4}$ form a conventional bias circuit which tends to stabilise the working point. But because of the relatively large amplitude of heterodyne voltage, the stage normally operates under Class $B$ conditions; consequently, the collector current will show a slight variation over the band because of the variation of heterodyne amplitude. The best value of working collector current for the XA102 is between 0.3 mA and 0.6 mA ; a higher value than this may increase the circuit noise while a lower value will make it difficult to accommodate limit conditions.
The value of the emitter by-pass capacitor $C_{1}$ requires careful consideration. If it is made too small, the resulting phase shift in the emitter circuit may significantly raise the signal-frequency input resistance of the stage, particularly on the L.W. band, where there is a danger of the input resistance becoming negative. On the other hand, if the capacitor is too large, it increases the risk of squegging. The correct procedure is therefore to use a capacitor which is just not large enough to cause squegging under extreme high-heterodyne conditions, allowing for the production tolerance on the component. Even if this is done, the emitter circuit may still influence the L.W. input resistance, and exaggerate the spread of input resistance between transistor samples. It is then advisable to employ a L.W. aerial coil with a low unloaded $Q$ of about 70 and to arrange a mis-matched coupling into the transistor such that the working $Q$ of the aerial coil is not greatly influenced by variations in transistor input resistance. This arrangement may result in some loss of sensitivity but it will give a more consistent L.W. performance.
The design of the $M$.W. aerial coil is more straightforward, it being common practice to arrange that the transistor loading halves the unloaded Q of the coil at about $1 \mathrm{Mc} / \mathrm{s}$. At this frequency, the input resistance of the XA102, when used in the circuit shown, is nominally $1,400 \Omega$.
If separate coupling windings, rather than tappings, are used on the aerial coils, these must be tightly coupled to the tuned windings. This avoids spurious responses caused by "ringing" of leakage inductances.
The output resistance of the stage at I.F. is to some extent influenced by internal feedback within the transistor and also by capacity coupling between the "hot" ends of the aerial and oscillator circuits, so the tuning condenser should have a screen between the two sections. For the circuit shown the 1st I.F. transformer should be designed for a mixer output resistance of the order of $35 \mathrm{k} \Omega$.

## EDISWAN MAZDA XA102 R.F. TRANSISTOR

The XA102 is a germanium PNP junction-type transistor particularly suitable for use as a frequency changer and/or oscillator on the medium and long wave bands. The transistor element is hermetically sealed in a small can.

RATINGS (ABSOLUTE VALUES FOR $\mathrm{T}_{\mathrm{amb}}=45^{\circ} \mathrm{C}$ )
Maximum Peak or Mean Collector/Base Voltage (Common Base Circuit)
(volts) -20
Maximum Peak or Mean Collector/Emitter Voltage (Common Emitter Circuit)
(volts) -16
Maximum Peak or Mean Emitter/Base Voltage (volts) - 12
Maximum Collector Dissipation (mW) 60
Maximum Junction Temperature
( $\left.{ }^{\circ} \mathrm{C}\right) \quad 65$
Maximum Storage Temperature .. .. ( ${ }^{\circ} \mathrm{C}$ ) 65
GENERAL CHARACTERISTICS ( $\mathrm{T}_{\mathrm{amb}} \doteq \mathbf{2 5}^{\circ} \mathrm{C}$ )
Maximum Collector Base Leakage Current (Emitter Open Circuit, $\mathrm{V}_{\mathrm{cb}}=-12 \mathrm{v}$ ) ( $\mu \mathrm{A}$ ) -5 Maximum Collector to Emitter Leakage Current (Base Open Circuit, $\mathrm{V}_{\mathrm{ce}}=-10 \mathrm{v}$ ) $\ldots \quad(\mu \mathrm{A})-70$
Maximum Emitter to Base Leakage Current
(Collector Open Circuit, $\mathbf{V}_{\mathrm{eb}}=-12 \mathrm{v}$ ) ( $\mu \mathrm{A}$ ) -10
Thermal Resistance in Free Air $\quad \ldots \quad\left({ }^{\circ} \mathrm{C} / \mathrm{mW}\right) \quad 0$.

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Current Amplification, Common Base $\quad$... (pF) 0.984
Current Amplification, Common Emitter $\beta$
(25 Minimum)
$\begin{array}{rccc}\text { Common Base Cut-off Frequency (Average) } & \left.\text { (Mc/s) } \begin{array}{c}8.0 \\ (6 \mathrm{Minimum})\end{array}\right) .\end{array}$

DIMENSIONS AND BASING


TYPICAL OPERATION AS SELF-OSCILLATING FREQUENCY CHANGER IN THE CIRCUIT SHOWN
Signal Frequency Tuning Coverage,

| Medium Waves | (kc/s) | 530-1620 |
| :---: | :---: | :---: |
| Long Waves | (kc/s) | 160-280 |
| Intermediate Frequency | (kc/s) | 470 |
| H:T. Line Voltage (at 1.4 volts per cell) | (volts) | -8.0 |
| Collector Current (at $\mathrm{f}_{81 \mathrm{G}}=1 \mathrm{Mc} / \mathrm{s}$ ) | (mA) | -0.43 |
| Collector to Emitter Voltage | (volts) | -6.3 |
| Base to Emitter Peak Heterodyne Voltage $\left(\mathrm{f}_{\mathrm{sI} \text { I }}=1 \mathrm{Mc} / \mathrm{s}\right)$ | (mV) | 250 |
| Conversion Gain at $\mathrm{f}_{\mathrm{BIO}}=1 \mathrm{Mc}$ 's (not in cluding losses in 1st I.F. transforme | (dB) | 31 |
| Input Resistance at Signal Freque |  |  | Input Resistance tignal ( $\mathrm{f}_{\mathrm{gla}}=1 \mathrm{Mc} / \mathrm{s}$ ) at Signal Frequency

Output Resistance at $\ddot{\text { I.F.F. }}$.-
(oh ms) 1,400
Output Resistance at I.F. .. .. .. tuhms) 35,000
VARIATION OF HETERODYNE VOLTAGE WITH TUNING FREQUENCY IN THE CIRCUIT SHOWN

VARIATION OF HETERODYNE VOLTAGE WITH BATTERY


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$\begin{aligned} & 7 \text { Watt AC/DC Chassis complete with paxolin and bracket } \\
& \text { Note: Transformer holes are not punched in chassis excepting }\end{aligned}$
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" ${ }^{11 \frac{1}{2} \mathrm{in},} \times \times 4 \frac{1}{2} \mathrm{in}$.
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Type "A" Pre-Amplifier, 4 tin. $\times 2 \mathrm{i}$ in.
$7 / 6$
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delta Q: 25-0-25.
TEST CIRCUITs: Separate 1.f. and h.f. test circuits have ranges of $1 \mathrm{kc} / \mathrm{s}$ to $50 \mathrm{Mc} / \mathrm{s}$ and 20 to $300 \mathrm{Mc} / \mathrm{s}$. CAPACItANCE RaNGE: $7 \cdot 5$ to $110 \mu \mu \mathrm{~F}$ with $1-0-1 \mu \mu \mathrm{~F}$ incremental, for either test circuit. 20 to $500 \mu \mu \mathrm{~F}$ with $5-0-5 \mu \mu \mathrm{~F}$ incremental for l.f. test circuit. shunt loss: $12 \mathrm{M} \Omega$ at $1 \mathrm{Mc} / \mathrm{s}, 0.3 \mathrm{M} \Omega$ at $100 \mathrm{Mc} / \mathrm{s}$. external oscillators: TF 1247,20 to $300 \mathrm{Mc} / \mathrm{s}$. TF $1246,40 \mathrm{kc} / \mathrm{s}$ to $50 \mathrm{Mc} / \mathrm{s}$. TF $1101,20 \mathrm{c} / \mathrm{s}$ to $200 \mathrm{kc} / \mathrm{s}$.

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| SPECIFICATIONS | 183 | IB2 |
| :---: | :---: | :---: |
| Frequency Range: | $30 \cdot 16,000 \mathrm{c} / \mathrm{s}$ | $40.15,000 \mathrm{c} / \mathrm{s}$. |
| Power Handling Capacity: | 25 watts. | 12 watts. |
| Bass Unit: | $12^{\circ}$ | $12^{\circ}$ |
| Bass Resonance: | $20 \mathrm{c} / \mathrm{s}$ | $20 \mathrm{c} / \mathrm{s}$. |
| Voice Coil Diam: | 3* |  |
| Total Flux: | 308,000 maxwells | 240,000 maxwells |
| Mid Range Unit: | Pressure driven horn | $8{ }^{\text {* }}$ |
| High Frequency Unit: | Pressure driven horn | 8 |
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| Enclosure Acoustic Treatm | Glass Fibre filling | Absorbent lining |
| Enclosure size: | $24^{\prime \prime}$ wide 12f" dee | $\times 14 \mathrm{l}^{\circ} \mathrm{high}$. |
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The transmitter was designed for operation in the International Marine Frequency Band. It is particularly useful for lifeboats and life rafts, but it can be adapted, using an automatic-keying system, for life-jackets, air-sea rescue equipment, helicopters and radio beacons for coastal stations. The long life and reliability of the transistors make them particularly suitable for the type of apparatus suggested above, in which standby conditions of long duration are experienced. The low-consumption, light weight and compactness add to these advantages. A 4 ampere-hour accumulator will power the transmitter for some 60 hours. For emergency applications a self priming battery, which requires no attention (other than charging and sealing) until it is needed for use, is suitable.
The transmitter comprises an oscillator, a modulator, a driver and a power amplifier stage. The oscillator is crystal controlled and uses an OC45 transistor. The resonant circuit in the collector line is tuned to the series-resonant frequency of the crystal. The crystal is connected in series with the feedback winding to control the frequency of oscillation.
The modulator is a silicon transistor ( OC 201 ) also recently announced. The output from the modulator is applied to a driver amplifier and then to a push-pull power amplifier which feeds an aerial. The modulator, driver and power-amplifier stages are all operated under Class B conditions.
The design of the Class B push-pull amplifier follows the same basic technique as that for an audio amplifier except that, as the collector circuit is tuned, no bias is required to eliminate cross-over distortion. The use of a shared emitter resistor reduces the effect of variations in base-emitter voltage $\mathrm{V}_{\mathrm{b}_{\mathrm{e}}}$, and reduces the lengthening, caused by hole storage, of the collectorcurrent pulse. This reduction of the hole-storage curent gives a marked improvement in the efficiency of the amplifier. The winding details for the output transformer are shown on the circuit.

The design procedure for the driver and modulator stages is similar to that for the output stage. A 6 V supply is used for the modulator because of the voltage limitations of the oscillator transistor. This supply is also used because it is convenient for the modulator, and because of the keying system adopted.

A crystal-controlled oscillator with a tuned collector is used. Feedback is obtained by a transformer
coupling from the parallel-tuned circuit in the collector circuit, to the base. The crystal is connected in series with this feedback winding. The collector circuit is tuned to the series-resonant frequency of the crystal. The series resistance of the crystal is low enough for the feedback current to start oscillation. The oscillator operates under Class A conditions, the base bias is provided by a potentiometer (R1R2). The emitter resistor is bypassed to r.f. signals.

It is hoped to publish details of the modulation arrangements and the automatic keying system (transmitting SOS signals) at a later date.

The tuning procedure adopted is the usual one of rough tuning at reduced power, followed by adjustment at full power. A resistor of $27 \Omega$ is connected in the emitter lead of the modulator amplifier Tr 2 , the 12 V supply is then connected to the transmitter, and the oscillator tuned-circuit is adjusted to the series-resonant frequency of the crystal. The modulator amplifier is tuned next. The driver and poweramplifier stages should then be tuned for a maximum power output (about 2 watts) across the $68 \Omega$ load.
The emitter resistor of Tr 2 should then be short-circuited. The complete transmitter, from the oscillator to the power amplifier, should be progressively readjusted. Careful tuning of the power amplifier is necessary, because excessive collector current flows if the stage is off tune. The full output of 4 watts should now be obtained.
An experimental transmitter was built and the performance tested over a temperature range from 0 to $60^{\circ} \mathrm{C}$. The output falls gradually at temperatures above $25^{\circ} \mathrm{C}$, although quite reasonable output is still available at $60^{\circ} \mathrm{C}$. Field tests were carried out under licence using a $520 \mathrm{kc} / \mathrm{s}$ crystal, the transmitter being retuned to this frequency. A transmitting aerial 30 ft high and a receiving aerial of about 30 ft of wire were used. Strong signals were received within 12 miles across land. This is not the maximum range over land, and a range of at least 50 miles can be expected at sea.

Oscilfator Transformer TI

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n_{1} \text { 18turns }
$$

$$
\begin{aligned}
& n_{1} \text { 18turns } \\
& n_{2} 7 \text { turns urns } \\
& n_{2} 52 \text { turns? conductors }
\end{aligned}
$$

$$
\begin{array}{ll}
n_{2} & \text { turns } \\
n_{3} & 2 \text { turns? } \\
n_{4} & 6 \text { turns } \\
\text { conductors }
\end{array}
$$

$$
n_{4} 6 \text { turns }
$$

$$
\begin{aligned}
& \text { Ferroxcube adjustable } \\
& \text { pot-core ossembly LA } 35
\end{aligned}
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$$
\text { pot-core assembly LA } 35
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Output Transformerta $n_{1} 2+2$ turns $\} 2 l$ swg enamelled $\mathrm{n}_{2} 4$ turns copper 19/0028 bunched conductors Ferroxcube pot-core
as sembly LA6



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## "BELLING - LEE" NOTES <br> Parameters of design

The insulants that hold the contacts

## No. 5 of a series

Capacity is a property possessed by two conductors separated by an insulant, and is dependent upon the physical arrangement of the conductors and the dielectric contact of the insulant. Capacity is an essential feature of any R.F. circuit, but can be disastrous in the wrong place, e.g. between certain contacts in a valve socket or between certain contacts and earth. This is just another fact that a young designer must be aware of, and take into account. It is generally advisable to keep capacity as low as possible in valve sockets. With plugs and sockets for use in R.F. circuits, the impedance and not capacity becomes the important factor.

Phenolic moulding powders are available in considerable variety, each to a close specification. It is therefore possible to choose a powder best suited for most applications. The range is very wide both mechanically and electrically. For electrical work consideration must be given as to whether or not a material will "track" following a voltage breakdown between contacts or contact and earth, if so, subsequent breakdowns will occur at lower voltagefollowing the carbonised track of the first flash.
Some of the mineral filled powders have excellent electrical properties, they are very hard, non absorbent and track resistant, but as they are abrasive, their use causes excessive tool wear, and as tools can be very expensive, they are not very popular, and if practicable, other suitable insulants are preferred.
Nylon filled powders are exceptionally good and not brittle, though they are slightly absorbent.
Power factor is important when losses in R.F. circuits have to be considered and for high insulation resistance, e.g. in high impedance circuits such as valve voltmeters and electrometers.
Few pheno'ic mouldings can be described as ante-wetting, but certain glazed electrical ceramics and the waxy insulants like polythene are particularly resistant to the coalescence of droplets.

Polythene has a low melting point, and an important contour could easily be deformed when soldering to an adjacent contact. Polytetrafluorethylene (Fluron, P.T.F.E.) has a much higher melting point, is harder, and can be machined or moulded. The raw material is much more expensive to buy than polythene, and it is expensive to process.
Nylon-we have seen, is used as a filler in phenolic mouldings-or it may be injection moulded by itself. Although it is to some degree absorbent, its surface does not "wet."

This "wet ability" is important when a component is subject to condensation, e.g. in unsealed equipment in an aircraft.
Polystyrene has very good R.F. insulation properties. It can be machined-with care, or it wilt craze-but it is now generally moulded. It is a brittle substance, but a tougher high-impact material is available with somewhat degraded electrical properties as a co-polymer of styrene with other resins.
Polyvynal Chloride (P.V.C.) is uscful as an insulant for mains, has a very long life and good mechanical properties, but should not be used where R.F. is present.
We have said nothing about rubber, but the chemistry of rubber and rubber-like substance, has made great strides. Most natural rubber contains free sulphur and if used in close proximity to silver-plated contacts, they will tarnish. Remember, this tarnish is silver sulphide and not an oxide. Although this tarnish is not high resistance, it is undesirable. and can increase the difficulty of soldering. It is possible to obtain a grade of natural rubter containing no free sulphur. Natural rubber will breakdown and crack after long exposure to ultra viole: light, so one of the synthetic rubbers is usually specified where an article will be exposed to sunlight, for instance when used as the centre insulator of a V.H.F. dipole. When rubber is used in a situation where oil is present, neoprene (synthetic) should be specified. Neoprene is also used for certain seals.

Silicone rubber is, of course, a synthetic, it is a silicone polymer which withstands exceptionally high temperatures without deterioration. Very useful for seals.

## What is meant by Sealing

We have mentioned sealing on several occasions. Perhaps it would be useful to explain this for the benefit of the younger students and junior engineers. Why is it necessary? Let us look at a simple case. Wherever there is a temperature differential, " breathing" tends to take place. Where seals are imperfect. damp, grit or fungus spores can be sucked in to contribute to degradation of an equipment. Seals and the, sealing of electrical equipment, is a very difficult problem. Particularly if for use under tropical conditions, as if imperfectly sealed, moulds wilh develop if there is any substance present to support their growth. which there should not be. Where moisture gains access condensation takes place. It is easy to seal a corned beef can. but try to take two or more leads through it and the trouble begins. Sealing and the testing of seals will be dealt with next month.

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The L. 1397 is a similar socket, but with right-angle stem. When the stem is soldered through the board the socket is in the same direction as the board emerging on an engraved control panel at the end of the board. This makes it possible to stack printed circuits one above the other, with close-spaced rows of test points on engraved panels similarly stacked. The body and nut of these sockets are nylon and available in a standard range of colours; black, red, green, yellow, blue, white, although other colours can be supplied to order. The contact surface is either gold- or silver-plated ( $-/ \mathrm{Au}$ or $-/ \mathrm{Ag}$, respectively), the contact resistance being less than 2 milliohms.
The breakdown voltage is 8 kV . under dry conditions and the weight of the component is 0.7 gm .

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We offer this popular and PICATION, but ineorDorating some impmwements in the general lavout. BIGH QUALITY EEPRODUCTION up to a maximum of 10 watts output. The CONTROL UNIT is separat and completely enclosed; it is normally fitted to the Main Ampllifer Chassis as shown in the illustration but, if it is desired to use the unit remote from the Main Chassio, it can be quice easily detached and used ap to 2 yards distance. We incorporate BPECI FTRED COMPONENT and NEW MULLARD FALVES. We also give the purchaser the cholce of two of the best LTD., and also the lateet by PARTRIDGE ( $\varepsilon 1 / 8 /$ /- extra), which is generally recognised a the best U/L Output Transtormer made today and ensures maximume vindistorted output and the widest frequency range. We also suppis the PARMEKO MAINE TBANSFOBMER and this has extra puwer avallable to supply a Radio Tuning Unlt amounting to 250 volte OF PABTS (PARMCKO TRANSFORMEG) MODEL $510 / \mathrm{RO}$.............. £11.10.0 (Plus $8 / 6$ Carriage and Insurance). Aternativelv we muply Assembled and TEsTED (plun 8/0) ............ \&13.10.0 H.P. TERMB: Dep. fal $14 /$ and 12 monthly payments of $19 / 10$, corpliete assembly Bend B.A.E.
MANUAL. A VERY EIGE QUALITY 3WWTT AMPLIFIRR PROVIDING EXCELLENT REPBODJO TION AND EAVVING AM ATTRACTVE ENGRAVED PERSPEX FRONT PANEL. Price for COMPLETE KIT OF P
$\$ 7.10 .0$
(plus $8 / 6$ carriage and ingurance).
£8.19.6
G.P. Terms deposit £2 and 8 monthly payments of $£ 1$.

Doveloped from the very popolar 3 -valve 3 -watt Amplifer dexigned in the Mullard Laboratones. Our kit is complete to the Mullard apectication including supply of spectifed componenti valves and Paris and L.P. records plua a Redio position. getra power to THE COMPLETE ABSEMBLY MANUAL AVAILABLE FOR $1 / 8$.

## the best value on the market

## Stem' $\int_{\text {TAPE REP RECORDER }}$ DIRECT-MANUFACTURER to USER

nO "mIdDLEMAh's" DISCOUNT IS INCLUDED IN OUR PRICES
IT INCORPORATES:

- The latest COLLARO TRANSCRIPTOR TAPE DECK.
- The model HF/TR3 "Fidelity" AMPLIFIER. (Dascribed below)
- HIGH QUALITY 7in. x 4in. P.M. Speaker.

1,200ft. reel High Quality Emitape.
ACOS Crystal Mierophone.
BEFORE CHOOSING YOUR TAPE RECORDER YOU SHOULD HEAR THIS MODEL-TRULY " Hi-Fi" RECORDINGS ARE OB. TAINABLE and it is comparable to much higher-priced Recorders. ALTERNATIVELY send S.A.E. for ILLUSTRATED LEAFLET,

## PRICE

## $£ 49.10 .0$

> Terme Dep. £9/18 and 12 monthly pay. ments of $£ 3 / 18 / 7$ or Dep. $£ 16 / 10 /=$ and 12 monthly paymente of $£ 3 / / 6$

(Plus $£ 1 / 10 /$ carriage and insurance of which $£ 1$ is refunded on return of packing case.)

## THE MODEL HF/TR3 TAPE AMPLIFIER

ncorporating
3-SPEED TREBLE EQUALISATION by means of the latest FERROXPRICE for COMPLETE $£ 12 / 15 /$ KIT OF PARTS. FULLY ASSEMBLED $£ 16 / 10 /=$ HIRE PURCHASE. Deposis $\varepsilon 3 / 6 / 6$ and 12 months at $\varepsilon 1 / 4 / 2$.
A very high quality amplifier based on the vary successful Type "A" design completed in the MULLARD LABORATORIES. ONLY NEW HIGH-GRADE COMPONENTS are incorporated ineluding MULLARD VALVES and a GILSON OUTPUT TRANSFORMER . . other features are: Magic Eye Recording Hand Indicator-Effective Tone Control-Monitoring and Extension Speaker Sockets-has own Power Supply and can be used as independent Amplifier for direct raproduction of Gram Records or from Radio Tuner. Overall size $11 \times 6 \times 6 \mathrm{in}$.-Truvox-Collaro-or Brenellplease specify which. Send S.A.E. for leaflet or $2 / 6$ for Assembly Manual.

> HOME CONSTRUCTORS YOU CAN BUILD THIS PORTABLE TAPE RECORDER from $£ 39.15 .0$

## THE NEW MULLARD TYPE "C"

TAPE PRE-AMPLIFIER-ERASE UNIT INCORPORATING THE NEW FERROXCUBE POT CORE PUSH-PULL OSCILLATOR and 3 SPEED TREBLE EQUALISAT FERROXCUBE POT CORE INDUCTOR PRICES. INCLUDING SEPARATE SMALL POWER SUPPLY UNIT COMPLETE KIT $£ 14.0 .0 \quad$ ASSEMBLED AND $£ 17.0 .0$ OF PARTS \&14.0.0 TESTED

Deposit $£ 3 / 8 /$ and 12 months of $£ 1 / 4 / 11$. Assembled unit only.
ALSO AVAILABLE EXCLUDING POWER SUPPLY UNIT FOR
£11.15.0 and £14.10,0 respectively. (Carr. and Ins. 5/- extra, Send S.A.E. for leaflet or $2 / 6$ for Complete Assembly Manual. WHEN ORDERING PLEASE STATE MAKE OF TAPE DECK TO BE USED
We present this "Hi-Fi " Pre-amplifier strictly to Mullards specification, ete. incorporating ONLY NEW HIGH GRADE COMPONENTS and ehe SPECIFIED NEW MULLARD VALVES. It comprises a COMPLETELY SELFCONTAINED UNIT, all components and valves being contained in a well ventilated Box-Chassis nearly finished in Hammered gold with a very ventilated Box-Crively engraved PERSPEX FRONT PANEL.


WE HAVE IN STOCK THE NEW 2-SPEED TWIN TRACK TRUVOX Mk.VI £26.5.0 TAPE DECK
It incorporates PRECISION REV. COUNTER and PAUSE CONTROL and operates at $3 \frac{1}{4}$ or $7 \frac{1}{2} \mathrm{in} / \mathrm{sec}$.
WE OFFER THIS SELECTION
(a) The COLLARO Mk. IV TAPE DECK with the assembled $£ 34.10 .0$ and rested HFITR3 Amplifier
H.P. Deposit $£ 6 / 18 /$ and 12 months $£ 2 / 10 / 8$.
$£ 30.15 .0$
(b) As above but the HF/TR3 supplied as KIT OF PAR ..ck do not wire up the Deck Switch backs. We will do this for Cl or supply a wiring up the Deck Switch backs. We wil
(c) The TRUVOX Mk. VI TAPE DECK with the assembled and tested HF/TR3 amplifie
and HP Deposit $67 / 8 /$ and 12 ........................
(d) As above but the HF/TR3 supplied as KIT OF PARTS
(e) The BRENELL MK. V DECK with the assembled and tested HF/TR3 amplifier H.P. Deposit $\varepsilon 9$ and 12 months $\varepsilon 3 / 6 /$
() As above but the HFITR3 supplied as KIT OF PARTS.
£37.0.0
£33.10.0
(g) The PORTABLE CASE illusprated here (55) 200 EMITAPE ( $35 /-$ ), ACOS CRYSTAL MIKE (35/-), ROLA $10 \times 6 \mathrm{in}$. LOUDSPEAKER ( $30 /-$ ) ALL FOR. Carriage and Insurance on each above iol- extra.

NEED IS THE TYPE "C"PREAMPUIIER valve Preamplifier) ALL YOU
(a) The COLLARO MK. IV TAPE DECK and the MULLARD

TYPE "C"' PREAMPLIFIER \& Power Unit assembled, tested H.P. Deposit $£ 7$ and 12 months $£ / 11 / 4$.
(b) As in (a) above but the Type " $C$ " supplied as COMPLETE
(c) The TRUVOX Mk. VI TAPE DECK and the assembled

Type "C" Preamplifier and Power Unit.

## TO ADD FULL <br> TAPE RECORDING FACILITIES

To any modern " Hi-Fi" To aUDIO AMPdern (siER (such as our Mullard " 510 " "and 2
(d) A.P. Deposit E7/10/- and 12 months $£ 2 / 15 / \%_{0}^{\circ}$
(d) As above but the Type " C " supplied as complete KIT

OF PARTS $-\ldots . . . . . .7$ DECK and the assembled Type
" $C$ ". PREAMPLIFIER and POWER UNIT ......i7.... H.P. Deposit $£ 9 / 4 /$; and 12 months $£ 3 / 7 / 6$. KT

As above but the Type "C" supplied as complete KIT E 43.0 .0
(Carriage and Insurance on above quotes 10/- extra.)
PLEASE ENCLOSE S.A.E. WITH ALL CORRESPONDENCE.

[^16]
# MODERNISE YOUR OLD RADIOCRAM 

## It is CHEAPER and BETTER VALUE TO REPLACE YOUR OLD CHASSIS and GRAM UNIT

## !! RADIOGRAM CHASSIS !! ARMSTRONG "STEREO TWELVE" - £38.17.0 <br> The most complete unit vet produced for stereo giving 6 watts high fidelity push-pull output on each channel, 12 watts for monaural. Full Vifir band, medlum and long wavebancis. Stereo and monaural lapnts or records, tape and radio and a tape output for stereo and monaural tape recording. Comprchens re matchlag for sll types of crystal pick-ups. The perfect bRefs for a complete coonaural reproducting system or for a complete stereophonic syntem now or later.



ARMSTRONG "JUBILEE" An AM/FM chas- $£ 30.9 .0$ do with mine valves and two diodes and with pushFull VHF medtum and long wavebands with sutomatic frequency control on FM and fortite aertal on AM. Tape record and playback facilities. Can be adapted for stereo at any time by the
sddition of our compant, easy-to-fit converter amplifier

## ARMSTRONG "STEREO 44"

£29.8.0
Provision is made for Stereo and monaural playback from pick-np or tape. Ontpute provlded for Btareo or Monaural tape recordlings. Alternative Inputs enable the use of most crystal pick-uLs, together with tape recorders or tape preamplificrs (such as our FM transmiasions 87 -108 M/ces.

## DULC! " H4PP

£29.3.10
An 8 valve AM/FM 4 waveband chassis giving fi watts nilita linear output. Covere thort, and long wavebands. Tape outlet incorporated and sultable for 3 to 15 loudspeakers.
DULCI "H3"
£20.17.0
A 6 ralve AM/FM chasais giving 4 watts output. Covers medium and long wavebands, bands and ftape outlet incorporatod.
NEW KIRE PURCHAEE TERMS are svailable on all above. Hustrated leaflets avail able-send B.A.E.

AM/FM RADIO TUNING UNITS ARMSTRONG "S.T. 3 ",
£28.7.0
A self-powered high Adelity tuper covering full VHFF, medlum and loag wavebands with
automatle \&requency control on VBF. Excellent in comblnation with our MULLARD AMPLIFIERS but the cathode follower stage and variable feedback output control asie this tuner to be used with virtually any amplifer available.
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£24.19.0
A wavehand self-powered high idelity tuner covering the VHF/FM transmisions with our MUTLARDD AMPLIFIERS And also all Excellent periormance In comblnation ILLUETRATED LFAFLET showing recommended HIGH QUAIITYY LOUDSPEAKERS

## STERN'S FOR STEREO

OUR POPULAR MULLARD MAIN AMPLIFIERS ARE RECOMMENDED FOR USE WITH THE DULCI DUAL CHANNELSTEREO PREAMPLIFIERS The "8TEREOEIGHT" 923.200
PREAMPLIFIER (Carr. \& Ins.51-extra)
The "STEREO TWO" $\quad \mathbb{9 . 9 . 0}$
PREAMPLJIER PREAMPLJFIER (Carr. \& Ins. 5/-extra)
Both Preamplifiers can be supplied to eorrectly opernte AMPLIFIERA (described on page 131). For Stereo reproduction TWO Main Ampllfiera re necessary but for normal " Hf-M" reproduction the " Btereo Eight" and the "Stereo Two " are perfectly sultable to operate with ONE Main Ampllfer and the second Maln Amplias can then be aided at any time thus transiorming a standard "HI-KM " instal-
lation over to the Etereo.
WE OFFER PREAMPLIFIERS and AMPLIFIERE AT BPECIALLY REDUCED PRICES
STERN'S $\overline{12} \overline{\mathrm{O}} \overline{\mathrm{OLT}}$
"CAR RADIO * PRINTED CIRCUITS
\& POWER TRANSISTOR
+MEDIUM \& LONG WAVEBANDS
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UNIT ASSEMBLY . . CONSISTLING OF
TEREE SEPARATE UNITS EULLY WIRED, ALIGNED AN TEATED, requiring only 12 solder points to complete the Receiver.
A varsatile destgn with low current consumption. Doen not require a separate vibrator PRWICE fort the THREE COMPLETELY A\&\&EMBLED UNITB £15.0.0

## SPECIAL CASH ONLY BARGAIN

 $A$ bulk purchase enablos $u s$ to fofer this very y usefur INTERCOM SET or BABY ALARM For oniy $£ 5.5 .0$ Conslats of MASTER UNTT (illustrated) and one EXTEN.SION
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\author{

WESTON MODEL 772 TESTMETER <br>  <br> | A.C. VOLTS | D.C. | A.C. CUR- |
| :--- | :--- | :--- |
| 2.5 v. | CURRENT | RENT |
| 10 v. | $100 \mathrm{micr} / \mathrm{a}$. | 500 ma. |
| 50 v. | 1 ma | 1 amp. |
| 250 v. | 10 ma. | 5 amp. |
| $1,000 \mathrm{v}$. | 50 ma. | RESIST- |
| D.C. VOLTS | 100 ma. | ANCE |
| 2.5 v. | 500 ma. | 100 ohms |
| 10 v. | OUTPUT | 1,000 ohms |
| 50 v. | METER | 100 k. ohms |
| 250 v. |  | 10 megohm |
| $1,000 \mathrm{v}$. |  |  | <br> $1,000 \mathrm{v}$ <br> Supplied in perfect working order complete with rexine carrying case, internal batteries and instructions, $88 / 19 / 6$ each. P/P 4/\%.

}

COSSOR DOUBLE BEAM OSCILLOSCOPE


Operation $110 / 200 / 250$ volts A.C 120 wates. Time Base 10 posicions. 6 cps. to $250,000 \mathrm{cps}$. Amplifier 10 eps. to $2,000,000$ eps. Sensitivity. YI.Y2.3.1 v. D.C. 1.1 v. rms. X. 2.25 v. D.C. .8 v . rms.
Supplied in good working order complete with handbook and circuit. E27/10/- each. P/P Cl

## C.R. 100 SPARES KITS

Complete set of new valves $2 \times 66,2$ U50, complete set of new valves $2 \times 66$, 2 Ust
2 DH63, $2 \mathrm{KT} 63,6 \mathrm{KTW} 61$. Also set of resistors, condensors, pots, coggle switch and output transformer. Supplied new and boxed. 59/6 each. P/P $4 / 6$

## FERRANTI TESTMETERS TYPE $Q$

D.C. A.C. D.c. ohms
VOLTS VOLTS Current $3 \mathrm{v} . \quad 15 \mathrm{v} . \quad 7.5 \mathrm{ma}$. 25,000

 500 ohms per volt on all ranges. B.S.S. first-grade accuracy on all self contained ranges. Supplied in perfect working order complete with leads, battery, instructions and rexine covered carrying case. Price 72/6 each P/P $2 / 6$.

## ROTARY

## CONVERTORS



12 v. D.C. input 230 voit A.C. 150 watts, 50 cycles output. Housed in wooden case and ficted with recistance switch plug esistance, switch, plugs and A.C. mains voltcage outpus chee perfect condition, individually tested, $\mathbf{\epsilon 9 / 1 9 / 6}$ each. P/P $10 /$

PARMEKO MAINS TRANSFORMERS. In put 230 volts. Output $350 / 0 / 350$ volts 150 mA . 6.3 v. 4 amp., 5 v. 4 amp. Brand new, $32 / 6$ each P/P $2 / 6$.
R. 1155 " $N$ " TYPE SUPER SLOW MOTION DRIVES. Brand new, $12 / 6$ each. P/P I/-


CV9671 in, C.R.T. 4 y. HEATER. Suitable for oscilloscopes, etc., 25/- each. P/P 1/-
CRYSTAL MICROPHONE INSERTS. Only 4/6 each. P/P 6d.

ALKALINE NIFE ACCUMULATORS
Banks of 10 cells giving 12 v. 45 A.H. Unused in wooden crates, 65/10\% each. P/P 7/6. Size $26 \frac{1}{2} \times 8 \frac{1}{2} \times 5 \frac{1}{2}$ in
MIDGET NIFE ACCUMULATORS. Single units, ideal for models, etc., $2 / 3$ each. P/P 98 , 12-VOLT MOBILE AMPLIFIERS. Ex-Admiralty. Mic. or gram. inputs, 10 wates output to 3 or 15 ohm speakers. Not new but in good working order, $\mathbb{E 8 / 1 9 / 6 \text { each. P/P 5/-, }}$
RCA ET 4336 PLATE TRANSFORMERS. Special release, brand new in original transit cases. Primary tapped $200 / 250 \mathrm{v} .50$ cycles.
Secondary, $2,000 / 0 / 2,000$ v. 400 ma . tapped Secondary, $2,000 / 0 / 2,000 \mathrm{v}$. 400 ma ., tapped
$1,500 / 0 / 1,500 \mathrm{v}$. Price $£ 12 / 10 /$ each. P/P fi.




COSSOR 343 GANGING OSCILLATORS. A.M./F.M. signal generators covering $70 \mathrm{ke} / \mathrm{s}$ to $21 \mathrm{Me} / \mathrm{s} 400$ eycles int. mod. F.M. sweep 0 to $50 \mathrm{kc} / \mathrm{s}$. Operation $110 / 200 / 250 \mathrm{v}$. A.C. Supplied in perfect condition externally and internally, complete but not tested, $E 5 / 19 / 6$ each. P/P $7 / 6$. HOOVER MIDGET ROTARY TRANS. FORMERS. $2 t \times 4 \frac{1}{2} \mathrm{in}$. Input 12 y . D.C. Output 310 v. 30 ma . Brand new and boxed, $12 / 6$ each
G-VOLT VIBRATOR POWER PACKS. Output 120 v .30 ma . Fully smoothed, uses standard Mallory 4-pin vibrator. New and boxed. $12 / 6$ each. P/P 2/.

| METER BARGAINS |
| :---: |
| BARGAIN GRAM MOTORS. Garrard eentre drive motors complete with turntable, $220 / 250$ Y. A.C Adiustable mechanically from $0-45$ r.p.m. Only $22 / 6$ each. P/P $3 /$ - |

IOO-WATT ROTARY CONVERTORS. Input 24 v. D.C. Output 230 v. A.C. 50 cycles, 100 watts. Housed in grey metal case with input/output plugs. Supplied brand new, 92/6 each. P/P 7/6.

150-WATT ROTARY CONVERTORS. Two models available, either 12 or 24 v . D.C. input. Output 230 v. A.C 50 cyeles, 150 watts. Brand new E7/10/- each. P/P $7 / 6$ ea.


PARMEKOTABLE TOPTRANS FORMERS. Input 230 v. 50 eyclos. Output 620/550/375) 0/375/550/620 volts 250 mA . Also $2-5$ volt 3 amp . windings. Size: $6 \frac{1}{\frac{1}{2}} \times 6 \frac{1}{4} \times 5 \frac{1}{2} \mathrm{in}$. Brand new only 45)each. P/P 5/-

FERRANTI POTTED FILAMENT TRANSFORMERS. Hermetically sealed, ceramic terminations. All new and boxed, Type 1: $200 / 250 \mathrm{v}$ inPut. Output 6.3 C.T 5.6 a. tapped 5 v.
6.3 v. C.T 4 8a. tapped 5 v. 6.3 v. CT. 1 tapped 4 v., 1916 each., Type 2: Input ${ }^{9} 00 / 250$ v. Output 6.3 v. CT, 3.3 a., tapped 5 v .6 .3 v . CT, I a., rapped 4 v . CT, ${ }^{\text {C. }}$ a, $15 / 6$ each. P/P' 2/., each type.

GRESHAM POTTED LT. TRANSFORMER.

Input 230 volts. Outpur rapped 80 v., 75 v . and 70 v , at 4 amps. Supplied brand new, boxed, $42 / 6$ each P/P $3 / 6$.

HALLICRAFTER S. 27 COMMUNICA. TION RECEIVERS. F.M. or A.M. coverage 27 to $143 \mathrm{Mc} / \mathrm{s}$ on 3 bands. Incorporates S meter, var. sel. B.F.O., etc., output for phone or speaker. Operation 110 or 230 volt A.C. Supplied reconditioned in perfect working order, $£ 32 / 10 /$ each. P/P 10/-
R.II55 COMMUNICATION RECEIV. ERS. Trawler Band Models L \& N. Supplied in perfect working condition, $\mathbf{\epsilon / 2 / 1 9 / 6}$ each Standard model B receiver, fitted with improved $N$-type drive, in perfect working order, $£ 7 / 19 / 6$ each. $7 / 6$ carr. extra on both receivers. Combined A.C. Mains Power Pack and Audio Output Stage, 85/- extra. Illustrated instruction book with each receiver
EDDYSTONE MAINS POWER PACKS. 2001 250 volts input. Output 175 volts 60 ma . and 12 volts 2.5 amps. Double choke and condenser smoothed, $5 Z 4$ rectifier. Housed on grey metal case. Supplied new and unused $32 / 6$ each. P/P 3/6.
VORTEXION PORTABLE AMPLIFIERS Operation from $200 / 250$ volts A.C. or 12 volts D.C. Separate inputs for microphone or gram. Output matched to 7.5, 15, 250 or 500 ohms. Incorporates volume control and full switched tone control. Valve line-up: $6 \mathrm{Q} 7,6 \mathrm{~J} 5,6 \mathrm{~V} 6,6 \mathrm{~V} 6,5 \mathrm{Z} 4$. Size $8 \frac{1}{2} \times 6 \frac{1}{2} \times 17 \frac{1}{2} \mathrm{in}$., not brand new but supplied in perfect work-
ing order, fully tested $£ 10 / 10 /$ each. P/P $6 /$.
45 AMPERE NIFE ACCUMULATORS. Single cells, 1.2 v., $12 / 6$ each. P/P 2/-
POTTED MAINS TRANSFORMERS. Pri* mary 230 volts. Secondary $350 / 310 / 0 / 310$ voles 220 ma., 6.3 voles 13 mps . 5 volts 3 amps., $49 / 6$ each. P/P 3/-
R. 1294 Y.H.F. RECEIVERS. Coverage 500 to $3,000 \mathrm{Mc} / \mathrm{s}$. Perfect condition, with handbook £ 35 each. P/P $10 /$ -
PORTABLE PRECISION VOLTMETERS BRAND NEW instruments by famous manufacturer. Housed in polished teak case. Moving iron movement reading A.C. or D.C. volts on 2 ranges, $0-160 \mathrm{v}$, or $0-230 \mathrm{v}$., 8 in . mirror scale. Accuracy within $2 \%$. Supplied at a fraction of original cost, $65 / 19 / 6$ each. P/P $3 / 6$.
A.C. MAINS VOLTAGE REGULATOR TRANSFORMERS. Input 230 v . Output variable from 185 to 250 v . at 24 amps., or 185 250 v . input. 230 v . output, $£ 12 / 10 \%$ each. P/P $10 /$.

## UNIVERSAL AVOMINOR TESTMETERS

Small, compact, accurate instrument. Resistance measurements from 0 to 20 k . ohms, D.C. volts from 0 to 500 v. A.C. volts rom 0 to 500 V., D.C. current from 0 to 500 mA . Supplied in perfece working order, complece with leather sase and leads. 65/10/each. P/P $2 / 6$.


Carriage 10/6

SAYE MONEY AT DUKE G CO.


## R.P.6. $49 / 6$

Elegant cabinet, cloth covered in grey or red with sunken control panel, and speaker fret. Size $13 \times 17 \times 8$ in. deep. Takes a B.S.R. Monarch 4-speed autochanger: " $7 \times 4 \mathrm{in}$. elliptical speaker and most of the modern portable amplifiers.

## 79/6

Stylish cabinet by famous manufacturer. Cloth covered in contrasting colours (red and grey). Grilled front controls panel. Size $15 \times 19 \times 8 \frac{\mathrm{in}}{}$, deep. Beautifully made-
 you can be really proud. Takes 4 -speed B.S.R. Autochanger. $6 \frac{1}{2}$ in. round or elliptical speaker. Room for any amplifer of your own choice. Carr. and Ins. 4/6.


A beautifully styled cabinet. Made by a famous manufaccurer. In polka dot cloth with clipped lid and carrying handle. Size $16 \times 14 \frac{1}{2}$ $\underset{\text { Will }}{ }{ }^{8 \frac{1}{2} i n}$ take deep. B.S.R. Monarch 4-speed autochanger and $4 x$ 7in. elliptical most of the modern portable amplifiers. Carr. and Ins. 4/6.


## R.P. 7 SINGLE 35'6 PLAYER CABINET

Smart cabinet Size $14 \frac{1}{2} \times 12 \frac{1}{2} \times$ 6 tin. deep. Various 2-tone colour schemos with white handle and piping. Takes T.U.
B.S.R. single player unit, $4 \times 7$ in. elliptical speaker and amplifiers D.I or D.2. Carr. and Ins. $4 / 6$. nenemesers Dil or D.

+ STEREOPHONIC AMPLIFIERS £7/19/6 Beautifully made for portable stereophonic record players. Latest design with printed circuit, Dimensions $3 \times 5 \frac{1}{4} \times 9 \frac{3}{3}$ in. A.C. only. Mains isolated. Twin amplifiers each side giving 3-4 watts output. Incorporating ECL82 trlode pentode valve. Full tone, volume and balance controls. Complete and ready to fit. Knobs 3/6 per set extra. P.P. and Ins. 4/6.
£6'19'6 P.P. \& Ins. $5 / 6$.

COLLARO 4-SPEED AUTOCHANGERS stylus, P.P. \& lns, 5/6.
T.U. 9 B.S.R. 4-SPEED SINGLE PLAYER MIXER COLLARO CONQUEST

MOTOR BOARDS

12 months' guarantee
 $\times 7 \times 5 \frac{1}{2}$ in. Ideal for small P. \& P. 319 .
with turnover erystal p.u. and sapphire stylus.
B.S.R. MONARCH 4-SPEED

£7/19'6 Incorporating auto and manual control complete with studio erystal p.u. and sapphire
£4/9'6 U.A. 12 LATEST B.S.R. MONARCH 4 - SPEED P. \& P. 5/6. 88'9'6

STEREO AUTOCHANGERS TT GNS. With turnover cartridge for stereo L.P. and standard. Carr. \& ins. 5/6.

For 4 -speed autochangers. P. \& P. 1/3.

## * AMPLIFIERS $\star$



PORTABLE AMPLIFIER MARK D.I. 59/6 Brand new, Latest design with printed circuit. Dimensions $7 \times 2 \frac{1}{4} \times$ 5in. A.C. only. Mains isolated. 2-3 watts output. Incorporating EL84 as high gain output valve. Volume and tone controls. Knobs $2 / 6$ extra. P. \& P. 3/6

PORTABLE AMPLIFIER MARK D.2. 79/6 Printed circuit. Latest design Dimensions $7 \times 2 \frac{1}{2} \times 5 \mathrm{in}$. A.C. only. Mains isolated 3-4 watts output. Incorporating the latest ECL82 triode pentode output valve giving higher undistorted output. Volume and tone controls. Knobs $2 / 6$ extra. P. \& P. $3 / 6$.
PORTABLE AMPLIFIER MARK D.3. $89 / 6$ De luxe model. Printed eircuit. Latest design. Dimensions $7 \times 2+\times 5$ in. A.C. only. Mains isolated 3-4 watts output. Incorporating the latest ECL82 triode pentode output valve giving high undistorted output. Volume, treble and bass control. Knobs $3 / 6$ extra. P. \& P. 3/6. PORTABLE AMPLIFIER MARK D.4. 69/9 Brand now. By famous manufacturer. Especially players. portable record players. Dimensions
$3 \frac{1}{2} \times 4 \mathrm{in}$. A.C. only. $\frac{x}{2}$ valves; EL84 as high gain output valve; EZ80 as restiffer. Volume and tone controls. Knobs $2 / 6$ extra. P. \& P. 3/6
B.S.R. FUL-FI CRYSTAL

19/6 Brand new. Including sapphire needles for L.P. Brand new. Including sapphire needles for L.P.
and Standard, giving fullest range and finest and Standard, giving fullest range and finest to all standard piek-up arms. P. \& P. 9d. to all standard pick-up arms. P. \& P. 9d.

## BAKELITE <br> CABINETS <br> 5/9 <br> Attractive deslgn. Size 12

$\star$ IDEAL FOR STEREOPHONIG SOUND *
EXTENSION SPEAKERS Polished oak
cabinet of attrac-

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The unit is housed in an attractive walnutveneered cabinet as illustrated. Size approx. $18 \times 17 \times 14 \mathrm{in}$. high.

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A destgn of ain
valve 200.280 A.C. malns. L . and M. Wave T.R.F. lum rectifier. For inclusion is cabinet
illustrated or wal. nut veneered type. It employs valves 6K7, BP6I, 6F6G,
and
is and is specially
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Instructlons and parts llst. 1/9. This receiver can be built instructlons and parts list. 1/9. This receiver can be built in brown or cream bakellte or veneered walnut.

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All parts including cream or coloured plastic case, printed superhet circuit, ferrite aerial. Transistors, $2 \frac{1}{2} \mathrm{in}$. P.M. speaker. Long and medium wavebands. Size of unit $5 \frac{3}{3} \times 3 \frac{1}{4}$ $\times 1$ inin Detailed construction booklet supplied.


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HP1012, 10 watts 15 ohms (or 3 ohm ) speech coil. Where a really good quality speaker at a low price is required, we highly recommend this unit with an amazing performance. £4/10/9. Please state whether 3 ohm or 15 ohm required.


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FULLE SHROUDED UPRIGET MOUNTLNG


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Primaries 200-250 v. $50 \mathrm{c} / \mathrm{s}$.

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Primariea 200-250 $\mathbf{0 .} 60 \mathrm{c} / \mathrm{m}$

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| 6.38 .25 |  | 6.3 v. 62. |
| 0-4-6.3 7.2 2 | 7/9 | 12 v \% a or 24 v . |

OUTPUT TRANSFORMERS
Mdget Battery Pentode 661 for 3Sq, etc. ....... 3/8
Bramill Pentode 5,000 to 30 Standard Pat 000 to 30
8tandard Pentode $5,000 \mathrm{n}$ to $3 \Omega$
8tandard Pentode 8,000 to $3 \Omega$
Puab-pull 8 watts 6 V 6 to 8 ohms

Push-pull 10-12 watts to match 6V6 to $3-508$ or
Push-pull EL 8410 or is ohms ...................
Push-pull $15-18$ watts, sectionaliy wound, 6 L 6 ,

Pash-pull KT66, etc., to 3 or $18 \Omega$................... szio
smoothina chokes
$250 \mathrm{~mA}, 5 \mathrm{H} ., 100$ ohms
$100 \mathrm{~mA}, 1010 \mathrm{H}, 250 \mathrm{obm}$
80 mA ., $10 \mathrm{H} ., 850$ ohms
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1 amp. 0.5 ohm L.T. type

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Inductor Chokes, 10 henries, $17 / 6$.

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#### Abstract

Condensers 300 pf. or 500 pf., $4 / 6$ each to Co-axial Cable, semi airspaced 75 ohms 6d, yard $*$ Headphone CLR low resistance $7 / 6$ pair t Paper based recording tape, $1,200 \mathrm{ft}$. on plastic spool, detail $65 / 10 /$-, circuit and shopping List $I /-7$ Frame Output Trans former for Regentone 777 12/6 each * STC Rectifiers RMI $5 / 6$, RM2 6/9, RM3 7/6, RM4 16/6, RM5 19/6 + Ex Government Carbon Controls by Morganite brand new 250 K . Itin. spindle $\mathrm{I} / \mathrm{F}$ each Electrolytics for TV 100 mfd $450 \mathrm{v}, 3 / 6,100-200 \mathrm{mfd} 275 \mathrm{mfd}$. $60250 \mathrm{mid} .275 \mathrm{v} .7 / 6$ each t Morse


aerial and HF coil with circuit 7/pair $\rightarrow$ Collaro Conquest 4 speed automatic record changer $57 / 19 / 6$ + Mains Dropping Resistors SMD6 and SMD7 as used in Ultra Twin $505 / 3$ ea. A Pointer Knobs available cream, white, black and maroon 9d. each $\rightarrow$ Elliptical speakers 7 in . $x$ 4in. by Plessey p/6 each t Multiratio Output Transformars Optimum utput Transformers Opeimum Load ,000 12,000 ohm each $t$ in. Loudspeaker Unit 3 ohms mpedance with a matching output brand new bur soiled for ov6 rand new but soiled, offered at a pan price of 116 each * Ameri
phone complete with strap and plug 3/- t 100 resistors mixed. t. $\frac{1}{2}$ and watt popular values 100 for $12 / 6 \nmid$ Copper plated tubular rods 12 in . long designed to plug into one another $4 / \mathrm{doz}$. Monarch UAl2, the de Luxe 4 -speed automatic record changer. 4-speed automatic record changer. Instrument Model 230/250 v, 40 watts, $16 / 9+$ Acos Cartridge Type HGP37/37 and HGP59/5C. $18 / 6$ ea. Single Player, fitted with the GC2 cartridge, f6/19/6 with the Rectifiers. Bridge tharger Rectifiers, Bridge type, 12 v . amp. $4 / 3,2$ amp. 7/-, 3 amp . 10/e, 4 amp. $12 / 6,6$ amp. $15 / 9$ t Primary Secondary 2,6 and 12 , Primary Secondary 2, 6 and 12 v . $18 / 6$ amp. version $13 / 0,4 \mathrm{amp}$. version Relay Recffetted Richard Allan Relay Bafflette, Bin. unit with volume control and outpur transYersal Booster lsolation former, tapped Primary for 26 former, tapped Primary for 2, 6 $25 \%$ boost $13 / 6$ ary with Bin. $x$ 5in. Elliptical Loudspeaker Hi-flux Model 2516 peaker Hi-flux Model, $25 / 6$ Ex= with headphones, phone iunction b throat microand carriage $7 / 6$ boodmans 10 in carriage $7 / 6$ * $2 / 3$ dinans $10 i n$. ance $25 / 6$ + Plessey 0 impedance, $25 / 6$ Piessey Vin. $x 6 \mathrm{in}$. Loudspeaker Unit, 25/6 to Line V14, 33/9 Transformer for Pye Rectifiers by Westinghouse Cooled Rectifiers by Westinghouse 14RA $1-2-8-3,18 R A-1-1-16-1$. $9 / \%$ it
Osmor Chassis Cutter, type 2, Osmor Chassis Cutter, type 2,
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ALADDIN FORMERS and cores，tin．8d；tin．10d．
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 Precision engineered，size only $\times \frac{8}{8} \mathrm{~m}$ ．Bargain．ACOS CRYSTAL DESK MIKE， $33-2,8 w i t c h e d, ~ 35 /=$.
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12 in ，Baker 15 wh 3 ohm and 15 ohm models $105 /$
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CRYBTAL DIODE G．E．C．2／－，GEX34，4／－， 40 Cirenite， 3 R．R．HEADPHONES， 4,000 ohms，brand new， $16 / 6$ pair SWITCE CLEANER Fluid，squirt spout， $4 / 3$ tim．
 $\times 1$ inn．$\times 1$ inin．， $10 /-0.005$ standerd with trimmers
 VALVE HOLDERS．Pa．int．Oct．，4d．EF50，EA50，6d
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BRAND NEW £9．10．0 carr， 46
TERMS：Deposit $£ 5 / 5 /-$ and 5 monthly payments of $£ 1$ ．
MATCHED SPEAKERS 8 in．， $17 / 6 ; 10 \mathrm{in} ., 25 /-$ ；12in． $30 /=$

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Seminair spaced Polythene insulated $\frac{1}{2}$ in．dia，stranded core．Ideal Band III 9 d．
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BLACK CRACKLE PAIIT．Air drying， $3 /=\mathrm{f}$ in
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| 6H6GT | $3 / 612 \mathrm{~K} 7$ | $8 / 6$ Sylv． |  | S1＇61 | 516 |
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For testing and servicing of special installations in aircraft. A fair knowledge of electronics and familiarity with such installations are essential. Ex-Service N.C.O. Radar Mechanics would be most suitable.

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For the manufacture and maintenance of Test Equipment and Special Missile Service Equipment. Qualifications are desirable, but previous electronic experience is essential. Occasional visits to M. of S. establishments will be necessary. Ex-Service Radar and Radio Fitters would be most suitable.

## Mechanical Technician

For general mechanical duties including simple fitting and machining. Should preferably have a knowledge of pneumatic equipment and be able to produce simple sketch drawings for use by machine shops. Practical experience is more important than qualifications.

The above are Staff Appointments with excellent opportunities for advancement for the right men.


Please write, including full details of past experience to :- The Personnel Manager (Ref. 267),
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## 

dIGITAL COMPUTORS FOR NAVIGATION SYSTEMS
Vacancies exist for ELECTRONICS ENGINEERS
in a team engaged upon the development of digital computer circuits. Those appointed to these vacancies will be expected to show initiative and ingenuity in their approach and be capable of pursuing a line of research with the minimum of supervision. Qualifications required are O.N.C. or equivalent for Junior Engineers and H.N.C. or equivalent for Engineers. Some experience of transistor or computer switching circuits is desirable. Applications should be made to:
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## COTTAGE LABORATORIES LIMITED <br> require

ELECTRONIC and ELECTRO-MECHANICAL ENGINEERS with
good qualifications, and experience, capable of playing a senior part in the design and development of electronic equipments and associated control gear.
If you would like an interesting, permanent and progressive job in a small and lively company, backed by the resources of a large international group, then write or telephone:

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W. H. SANDERS (ELECTRONICS)

LIMITED
GUNNELS WOOD ROAD, STEVENAGE, HERTS. REQUIRES A
SENIOR DEVELOPMENT
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aged between 25 and 35 years, with at least five years' experience in the Design of Electrical Control Systems, knowledge of Magnetic Amplifiers would be an advantage.
Applicants should have degree
A.M.I.E.E. or H.N.C. (Elec)

The salary offered will be assessed according to age and qualifications. Housing accommodation available. Please write giving full details of age, qualifications and experience to:Personnel Officer at the above address.

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with Radio and Radar experience, required for servicing and demonstration of portable electronic distance measuring instruments. Applications from Ex-Service Senior N.C.O. Radio Fitters welcomed. State experience and salary expected. Replies to Cooke, Troughton \& Simms Ltd., Tellurometer Dept., Broadway Court, London, S.W.1.

THE BROADCASTING DIVISION of MARCONI'S WIRELESS TELEGRAPH COMPANY LIMITED, CHELMSFORD
is expanding its television studio sales section.
Remunerative and interesting vacancies exist for sales engineers who have experience in the planning, installation or operation of television studios and who are willing to travel to all parts of the world at short notice. Preference will be given to candidates with a working knowledge of at least one foreign language. Posts are permanent and pensionable.

Please apply, giving full details and quoting reference 2022C, to Mr. J. L. Scott,
Dept. C.P.S., Marconi House, 336-7 Strand, W.C.2.

MIDDLESEX COUNTY COUNCIL Education Committee
TWICKENHAM TECHNICAL COLLEGE
Egerton Road, Twickenham, Middlesex
Required for 1st September, 1959:-
LECTURER in ELECTRICAL ENGIN. EERING subjects for Ordinary and Higher National Certificate Courses. Ability to teach Electronics essential. Applicants should have had good industrial and preferably some teaching experience. A degree or equivalent qualification desirable
Salary in accordance with the Burnham (Technical) Report, i.e. $£ 1,260 \times £ 31 / 10-$ £1,417/10 per annum plus London allowance. Application forms and further particulars foolscap S.A.E.) from the Principal. Closing date 7th May, 1959.
C. E. GURR, M.Sc., Ph.D.

Secretary to the Education Committec.

## RADIO\&ELECTRONIC ENGINEERS . . .

The MORSE CODE is still, and always will be, the basic Code for individual Signalling, whether on visual or telecommunication circuits. So add this simple and interesting subject to your qualifications. Apart from the pleasure derived from this extra knowledge, it counts for much when a step up the ladderis under consideration Write for the CANDLER BOOK OF FACTS and see for yourself how fascinating the Candler method of teaching
the Morse Code will prove.
CANDLER SYSTEM CO
(56W) 52b ABINGDON ROAD, LONDON, W. 8 Candler System Co., Denver, Colorado, U.S.A.

## BRADFORD INSTITUTE OF TECHNOLOGY <br> A full time course of 6 months for the <br> INSTITUTION OF ELECTRICAL ENGINEERS <br> PART III <br> Examination will commence in November, 1959

Further details and forms of application may be obtained from the Registrar, Bradford Institute of Technology, Bradford, 7.
LATEST DATE OF APPLICATION, 1st JUNE

## MICROWAVE ENGINEERS

PYE TELECOMMUNICATIONS LTD. have a number of vacancies for development engineers with experience in the design of microwave radio relay systems for the transmission of television and multi channel applications.
Letters quoting age, experience, salary required, etc., should be addressed to:-

The Personnel Manager,
Pye Telecommunications Ltd., Ditton Works, Newmarket Road, Cambridge.

## ELECTRONIC ENGINEER

[^18]
## MARCONI INSTRUMENTS LTD.

## Technical Personnel Required

## SENIOR \& JUNIOR ELECTRICAL DESIGN ENGINEERS

## SENIOR \& JUNIOR MECHANICAL DESIGN ENGINEERS

DUTIES: To undertake the design of Test Equipment covering practically the whole electronic field, including Telecommunication, Guided Weapons and Nucleonics. Considerable personal responsibility and freedom is given, and there are no set rules regarding the number of people engaged on a project. the allocation of project leaders, etc.
QUALIFICATIONS: The ability to design equipment and aggressively progress a project through to the stage where a mode! is made and the information is available for a production drawing office. Senior engineers are usually of B.Sc. standard with practical experience in measuring techniques, while Junior engineers are often Graduate Members of one of the Professional Institutions, or have similar qualifications, but this is in no way mandatory. The abilty to progress the project through to a satisfactory conclusion is the prime reinitiative can be sure of progressive advancement

Comprehensive pension and assurance schemes are in operation, and Canteen and Social Club facilities are provided.
Call any day including Saturday mornings at,
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LONGACRES, HATFIELD ROAD, ST. ALBANS, HERTS.
or write giving full details to Dept. C.P.S., Marconi House, 336/7, Strand, London, W.C.2. quoting reference WW 2970B.

## $\star$ Plessey

the most rapidly expanding nuclear instrument company

## in Great Britain requires more

ELECTRONICS DEVELOPMENT STAFF
to design equipment for reactor control
health hazard measurement and nuclear physics research.

## Commencing salaries :

Electronics Engineers $£ 850$ to $£ 1,200$ p.a. Junior Engineers
Senior Draughtsmen up to £15 p.w. £ 800 to $£ 1,000$ p.a. Junior Draughtsmen up to $£ 15$ p.w.
Previous experience in nucleonics an advantage, but a growing industry needs new recruits This may be YOUR opportunity Please apply for further information:-

## Personnel Dept.

PLESSEY NUCEIONICS ITD. NORTHRMPLON

## INTERNATIONAL BLECTRONIC COMPANY, THE HAGUE, HOLLAND

has a vacancy in her research laboratory 'n The Hague for a

## TECHNICAL WRITER

age 22-35
Required for preparation of audio, radio and television manuals. Capacity for lucid exposition of technical information essential.

A special knowledge of laboratory or service experience would be an advantage, whilst a good style of writing is necessary.

Please apply by letter giving full information about education, etc., to "Die Haghe" Advertising Agency Ltd., No. 53511, Postbox 354, The Hague, Holland.

## FERRANTI LIMITED EDINBURGH



Applications are invited for the following staff posts:-

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qualified to final City and Guilds or equivalent standard and with some experience in the design of some experience in the design of ed to work as part of a team developing new test equipment including fully automatic pro iscluding fully automatic proplex radar circuits digital counplex rand cating circuits and new type of precision on and a matic instruments with digita matic instruments with digital readouts. Ref. D.E./59

## TEST ENGINEERS

who will be mainly concerned with the testing of recently developed radar systems. Some relevant experience is essential. These posts may be of interest to Senior N.C.O.s with the appropriate technical background. Ref. priate tech
FIELD TRIALS ENGINEER8 to join teams engaged in the field trials of experimental airborne radar and fire control systems and ground radar installations These posts offer the opportunity of working on advance system
in the electronic and radar field Ref. T.I.D./59.

## TEST ENGINEER

to design and maintain test equip. ment for pulsed magnetrons and osupervise testing of magnetrons on a production basis. Experience in electronic test equipment o his hature is essential. Ref T.E.(V)/59.

PRODUCTION ENGINEER
o control a small group engaged on the manufacture of high power microwave tubes. Applicants must have had experience in the processes used in manufacturing transmitting valves including furnace brazing, glass to metal seals and vacuum techniques Ref. Prod.E.(V)/59.
All the above posts are of staff status and the salary and conditions offered will be appropriate to the responsibilities in each case. Initial interviews will be arranged in either London or Edinburgh. Applicants should send details to the

PERSONNEL OFFICER
FERRANTI LIMITED
FERRY ROAD, EDINBURGH, 5 , quoting the appropriate reference number.

## TRANSMITTER DESIGN ENGINEERS

are required by Pye Limited of Cambridge for an extensive programme in the following fields:

1. High and low power MF and SW broadcast transmitters

High, medium and low power T/V broadcast transmitter
for Bands I, III, IV and V
3. High, medium and low power FM broadcast transmitters for Band II.
4. Very low power T/V translator transmitters.
5. UHF Tropospheric Scatter transmitters.

Previous development experience on similar equipment is desirable, but candidates with suitable transmitter operations/ maintenance experience and a sound engineering training may be considered. Qualifications to HNC standard would be an advantage.
Applications should be addressed to the
Chief Engineer, Pye Limited,
Cambridge.
quoting "TDE."

##  <br> TECHNICAL AUTHORS <br> are required by MARCONI'S at the following works:ST. ALBANS. To work in the Technical Literature (Telecommunications) Section. Applicants should have electrical engineering qualifications and some specialised knowledge, which might be in the deslgn or development of electronic equipment. <br> CHELMSFORD. To work on the preparation of handbooks on vision and sound transmitters and studio equipment and also on Radar subjects, including aerial tuning gear, displays systems, etc. <br> The dutles are varied and interesting and the posts provide permanent and pensionable positions in a well established Company. <br> Apply giving full details and quoting reference <br> WW2970C to Dept. C.P.S., Marconi House, <br> 336-7 Strand, London, w.c.2.

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## TELEVISION ENGINEERS

Required with experience of studio equipment for planning studio installations.
Commencing salarles (pensionable) in the
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Apply: Head of Television Broadcasting Department, Central Rediffusion Services Ltd., Television House, London, W.C. 2.

COSSOR INSTRUMENTS LIMITED

## require SENIOR ENGINEERS

## for

EXPANDING DEVELOPMENT DIVISION
Preference given to men with degree or equivalent academic qualifications plus several years design experience, although proven design ability and wide experience will be considered in lieu.
These are PROGRESSIVE POSTS in a young and expanding Company within an established group. Salary in accordance with qualifications and experience but based on a generous siale. Apply in confidence (Marked Personal) to:-

The Technical Director, COSSOR INSTRUMENTS LTD. Highbury Grove,
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# THE INDEPENDENT TELEVISION AUTHORITY 

invites applications for the appointment of

## ASSISTANT ENGINEER

in Charge at its transmitting station at Emley Moor, Yorkshire. The successful applicant would be required to control a shift and to act as deputy to the Engineer in Charge. He must have a firstclass knowledge of high frequency and television engineering, with practical experience in the operation and maintenance of television transmitters and ancillary equipment. The salary scale for this appointment is $£ 1,155 \times £ 105$ -£1,575 $\times £ 100-£ 1,675$. There is a contributory pension scheme. Applications quoting E7 stating age, exparience sud qualifications should be addrmsed to the

Personnel Officer, 62 Brompton Road, London, S.W. 3

## TECHNICAL INSTRUCTOR TECHNICAL WRITERS

(i) Technical Instructor required with good knowledge of radio and radar principles.
(ii) Technical Writers required for writing radar technical manuals. Applicants should have had previous experience in writing and have good knowledge of radio and radar techniques.
Please apply:
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## FOR SALE

Large quantity of Radio Components for disposal, in small or large quantities. Cable and flexibles, condensers, rectifiers, resistors, screws, torches and bulbs, transformers, valves, volume controls, etc.
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A. V. ROE \& CO. LTD.,
have vacancies for

## ELECTRONIC ENGINEERS

in the Computer Group of their
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(1.) SENIOR ENGINEERS
(a) for circuitry design on simulators,
(b) for circuitry design on digital computers with special knowledge of transistor circuitry.
(2.) JUNIOR ENGINEERS
to assist in the above projects.
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to assist in design development and to take maintenance responsibilities on existing machines.

## QUALIFICATIONS

Applicants for positions 1 and 2 should possess a Degree or Higher should possess a Degree or Higher
National Certificate and have had experience in the design of electronic apparatus and preferably in the design of simulators and digital computers. Applications for position 3 must have Applications for position 3 must have or have had experience with electronic or have had experience
apparatus in general.

Applications, quoting ref. WIRD/
Post 1
The Chief Engineer,
A. V. ROE \& CO., LTD. W.R.D.,

The Personnel Manager,
A. V. ROE \& CO., LTD.

Greengate, Middleton,
Manchester.

## ELECTRICAL ENGINEER

OR
PHYSICIST
required for Cathode Ray Tube Development Laboratory. This is an attractive opportunity for a suitably qualified engineer to concentrate on the development of C.R. Tubes, with new applications, in an expanding field. There are, at present, also openings for more junior technical staff, with a minimum qualification of O.N.C. or Inter. B.Sc. Please write, giving details of your previous posts, and qualifications, and quoting CR/W to

Personnel Officer,
M.O. Valve Co. Ltd.,

Brook Green,
Hammersmith, W.6.

## THE INDEPENDENT TELEUISION AUTHORITY

has vacancies for

ENGINEERS

for the operation and maintenance of television transmitters and ancillary equipment. The Authority is in a position to offer appointments with opportanities to suitably qualified young men who have either some experience in this field or who have had a good basio training in radio, radar or telerision. There would be opportunities for further training and all appointments are pensionable after the initial period of probation has been satisfautorily completed.
Service with the Authority may involve transfers to various locations in the British Isles, but preference for a particular area will always be considered.
Appointments will be made in the grade of Shift Engineer with a salary scale starting at $£ 725$ with regular annual increments. The starting salary would be determined, to a certain extent, by qualifications and experience. Applications giving details of age, academic qualifications and experience, quoting Ref. No. E4 should be addressed to the

Personnel Officer,
62 Brompton Road, London, S.W.3.

## ULTRA ELECTRIC LIMITED Radio \& Television Division. Require <br> SENIOR TELEVISION ENGINEERS

for their Research and Development Laboratories
Applications are invited from engineers with research and development experience qualifying for work on projects, such as:

Wide Angle Scanning
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## ASSISTANT INSTRUMENT ENGINEER <br> for <br> CHAPELCROSS <br> NUCLEAR POWER <br> STATION

to work in the Instrument Department which is respoustble for installation, bervicing and testing of ali Worita instrumentation, including nuclear, physics and industrial television equapment.
This is an opportunity for an engineer to gai experience of reactor and associated power plant instrumentation and control, He wili be responsible to the Lnstrument Engineer for liaison with ment during reactor start-up tests and for subsequent instrumentation tests and experiments, organisation and co-ordination of a planned and servicing problems on instrumentation and other duties, which may include responsibility for the acceptance of instrument installations from the Consultant Engineers and installation and calibration teste
A recoguised enginecring apprenticeshlp or comparable training and corporate membership of a senior engineering institution, or equivalent, are essential. Industrial instrumentation experiand co-ordinate the activities of technicians and mechanics. Physics, radar or light electrical background may be an advantage. Where mecessary, training in nuclear aspects of the work will be given.

## Salary between

6845 (at age 25) and $£ 1,315$
Contributory Buperannuation. Staff housing
send postcard for application form quoting
Reference 2977 J 48 to
Works Secretary
UNITED KINGDOM ATOMIC ENERGY AUTHORITY INDUSTRIAL GROUP Chapelcross Works, Annan, Dumiritesshire, Bcotland
Closing date 4th May, 1959

## THE INOEPENOENT TELEVIION AUTHORITY

invites applications for the appointment of Assistant Engineer at its Headquarters in Lendon. The successful applicant will be required to assist the Senior Engineer responsible for siting transmitting stations. Applicants should possess good qualifications in electrical engineering and should have had previous experience in radio, radar or television. Experience of V.H.F. propogation problems would be a distinct advantage. The appointment will be based in London, but will involve much travelling and frequent contact with local authorities, land owners, etc. Salary scale for this appointment is $£ 1,330 \times £ 100-£ 1,630 \times £ 105-$ £1,840. There is a contributory pension scheme. Applications giving age and full particulars should be submitted to the Personnel Officer, 62, Brompton Road, London, S.W.3, quoting Ref. No. E/3.

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14. South Wharf Road, London, W. 2 Telephone: AMBassador 0151/2<br>A.R.B. Approved Stockists

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 AMMETER
(made by Evershed \& - Vignoles) Sensitivity: 5 mA. D.C. Chart width: 6 in . Chart drive: Electric motor 230 v. A.C. Chart Speed: $\frac{1}{2}$ in. per minute. Interior light. PRICE, unused, complete with two gravity type pens, two syphon pens with trough, two bottles of ink, two bottles of dashpot oil and two charts, fully Packing \& Packing \& carr, fl. This model can also be supplied for 1 mA Range at an extra charge of

EVERSHED I2-PEN TIME RECORDER


Portable 12-channel instruPortable for simultaneous rement for simultaneous re-
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PRICE, unused and complete with accessories
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Packing and carriage
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SULLIVAN WHEATSTONE BRIDGES Four switched decades $1-1.0-10-100$ ohms. Switched ratios: $.001-.01-1.1-1.0-10-100-1000$. Built-in galvanometer and key. -Provision for use with an external galvanometer.
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Frequency range: 2.5 to $100 \mathrm{Mc} / \mathrm{s}$.; Deviation range: 5, 25 and $75 \mathrm{kc} / \mathrm{s}$. Minimum input: 55 mV . Input impedance 75 ohms. Power supplies $100 / 150$ and $200 / 250 \mathrm{~V}$. ...... 69500 Carriage and packing .................... \&1 00

INSULATION TEST SET TYPE CT-9I Maximum voltage 40 kV . Trip circuit adjustable to trip at any leakage current between I and
$250 \mu \mathrm{~V}$. Power Supplies $100 \cdot 150 \mathrm{~V}$. and 200 $250 \stackrel{\mu}{\mathrm{~V}} \mathrm{~V}$. Mains. Powe
PRICE, complere and in perfect cond. $\mathbf{E 9 0} 00$ Packing and carriage

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Variable auto-transformers, made by General Electric rype loor, or equivalent " Powerstat " made by Superior Electric Co. Rating 2 kVA . Input
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 $85 \mathrm{kc} / \mathrm{s}$. to 25 Mc STANDARD" TF-144G, plete with mains lead and put $1 \mu V$ to $1.8 . ;$ comPacking and carriage .............fl 0 GENERAL RADIO $605 \mathrm{~B}: 9.5 \mathrm{kc} / \mathrm{s}$ to 30 $\mathrm{Mc} / \mathrm{s}$. ; output $0.5 \mu \mathrm{~V}$. to 0.1 V . and fixed output of I V. Complete with mains lead and output lead Packing and carriage .................................... 0 0 RCA TYPE 710A. 360 to $560 \mathrm{Mc} / \mathrm{s}$. $1 \mu \mathrm{~V}$. to 90 mV ; complete with ourput cable, frequency correction chart and attenuator calibration chart ........................ $£ 450$ Packing and carriage .................... 150 TYPE 101 SIGNAL GENERATOR. 400 to $650 \mathrm{Mc} / \mathrm{s}$. Output power from 7.5 to 11 dB . above I microwatt. Output impedance 72 ohms. Internal square wave modulation; ohms. Internal squarepower supplies 230 V . A.C. Complete with output calibration charts, frequency charts and ouspur callbration charts, irequency charts and accessory cables
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HIGH SPEED OSCILLOSCOPE. Time
base from $2 \mathrm{c} / \mathrm{s}$, to $750 \mathrm{kc} / \mathrm{s}, 1$ and 10 micro second time markers. Mains operation
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E55 0
DUMONT MODEL 241 SiNĞLE BEAM
OSCILLOSCOPES. 51 in. Tube; Time Base OSCILLOSCOPES. 5 tin. Tube; Time Base A.C. Mains operation. PRICE, fully overhauled and guaranteed $£ 35$ Packing and carriage..................... fl 00

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| . |
| 85 | R-H I $/$ APRS, $1000-6000 \mathrm{mc} / \mathrm{s}$. $\begin{array}{lll}£ 85 & 0 & 0 \\ £ 70 & 0 & 0\end{array}$ - 12500 RDO, complete with three tuning units

Ditto, complete with model RD Panoramic Adaptor Further details on request.

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VCR-97-picture tested
3 BPP , new in cartons
5CPI, new, loose
5FP7, new, in cartons
Packing and carriage $3 / 6$ per tube.

MICROWAVE 3 CM EQUIPMENT TS-I3 SIGNAL GENERATOR WITH SELF-CONTAINED WAVEMETER AND POWER MONITOR. Range 9305 to 9445 $\mathrm{Mc} / \mathrm{s}$. Internal pulsing. Peak Power output 50 microwatts.
TS-45/APM3 SIGNAL GENERATOR. Frequency range $9,300-9,450 \mathrm{Mc} / \mathrm{s}$. Power output 10 mW . average; Power meter range 5 watts. Details and prices on application
M-V TYPE 57 3-CM STANDING WAVE INDICATOR. Range $9,100-9,700 \mathrm{mc} / \mathrm{s}$. Contains 723A/B Oscillator, Calibrated Wave meter, Attenuator, and Standing Wave Indicator. V.S.W.R. indicated on a Cathode Ray Tube PRICE, fully overhauled and guaranteed $£ 130$ Packing and carriage..................... $£ 200$
KLYSTRONS 723A/B, fully tested and guaranteed-price on application.

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 TS-I4/AP SIGNAL GENERATOR, 3,200 to $3,370 \mathrm{mc} / \mathrm{s}$.; Power output -20 to -100 dbm . Power measurement range $20-200 \mathrm{~mW}$. Pulse modulation with variable pulse width and phasing; power supplies 115 V. A.C. $£ 85$ o Packing and carriage .................. \&I 10 oWAVEGUIDE WATTMETER TYPE

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For Power measurement in the range of 40 to 500 kW . peak, V.S.W.R. measurement and Wavelength in the range of 8.9 to 10.2 cm . Waveguide inter-service type $10 \mathrm{~A} \quad 65$ ob Packing and carriage

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"s" Band ( $2,900-3,150 \mathrm{mc} / \mathrm{s}$.). Spectrum width to $10 \mathrm{mc} / \mathrm{s}$; Details and prices on KLYSTRONS 417-A, F-9. 10 cm .; Vernier tuning $100 \mathrm{mc} / \mathrm{s} . ;$ Ers 1.000 V . max.; Heater 6.3 V.; Prs-50 watts

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POWER UNITS, TYPE 234

A.C. mains operation 230 V .; output may be rapped at 180 to 270 V. D.C. at 80 mA . L.T.\begin{tabular}{l}
6.3 V. at $4 \mathrm{amps}$. Brand now ......... $£ 219 \quad 6$ <br>
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 Ditto complete with built-in 6 V 6 output stage, suitable for R-1155 and R-1 132 Receivers 

stage <br>
\hline 4.
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MAINS TRANSFORMERS Input 100 to 250 V .; output 6.3 V .0 .6 A. $6.3 \mathrm{~V} .2 .5 \mathrm{~A} . ; 275-0-275 \mathrm{~V}$. $80 \mathrm{~mA} \ldots . . .$. Packing and postage

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 PAGE No. 181
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The left hand bit was used with Savbit alloy and has made 10,000 joints. The centre bit was used for 1,000 joints and the bit on the right for 7,500 joints, each with a standard tinllead alloy.


| SAVBIT FOR FACTORIES <br> Ersin Multicore Savbit Type I alloy containing 5 Cores of non-corrosive flux is supplied to factories 16 and 18 s.w.g. are the diameters most suitable for the majority of soldering processes. Supplies reels. | SAVBIT FOR THE SMALL USER <br> The Size 1 Carton contains approximately 53 ft of 18 supplied in 14 s.w.g. and 16 s.w.g. Obtainable from radio Multicore 5 -Core Solder is also supplied in 4 specifications of <br> Price 5/- each (subject). | SAVBIT FOR THE SERVICE ENGINEER <br> Approx. 170 ft . of 18 s.w.g. SAVBIT is supplied on a I lb. reel packed in a carton. Price 15/- each (subject). |
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| SPECIAL HIGH AND LOW MELTING POINT SOLDERS <br> Comsol (Melting point $296^{\circ} \mathrm{C}$ ) P.T. (Melting point $232^{\circ} \mathrm{C}$ ) <br> L.M.P. (Melting point $179^{\circ} \mathrm{C}$ ) <br> T.L.C. (Melting point $145^{\circ} \mathrm{C}$ ) | STANDARD TIN/LEAD ALLOYS <br> Ersin Multicore 5-core Solder is available in the following standard alloys: <br> $60 / 40,50 / 50,45 / 55,40 / 60,30 / 70$, and $20 / 80$ and in 9 gauges on 7 lb . and 1 lb . reels. | HOME CONSTRUGTOR'S $2 / 6$ PACK <br> Now available containing alternative specifications: 19 ft . of 18 s.w.g. $60 / 40$ alloy or, for soldering printed circuits, 40 ft . of 22 s.w.g. 60/40 alloy. Both wound on Reels. $2 / 6$ each (subject). |
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[^1]:    * Her Majesty's Stationery Office, price 7s.

[^2]:    * "A True r.m.s. Instrument," by C. G. Wahrman. B. Gr K. Technical Review, No. 3, 1958, pp. 9-21.

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[^5]:    - Dr. Smith-Rose in his presidential address to the R S.G B. disclosed that in similar tests to Malta the frequency was changed every 0.4 sec by steps of $20 \mathrm{kc} / \mathrm{s}$. the two sets of eauipment being
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[^6]:    * Radio and Electronics Consultant.

[^7]:    " "The Mavar: A Low-Noise Microwave Amplifier," by Samuel Weber, Electronics, 26th Sept. 1958, pp. 65-71.

[^8]:    *If, most regrettably, you are unfamiliar with the differential calculus, there is no need to be dismayed by the appearance of $\frac{\mathrm{d} q}{\mathrm{~d} \ell}$, which is simply a short way of saying " the rate of change of charge with respect to time " or " the slope of a charge/time graph."

[^9]:    * Both "Free Grid" and (den't let's be coy) Selfridge's are right according to whether silhouettes (such as the test bars and crosses sometimes transmitted by the B.B.C. and I.T.A.) are or are not regarded

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