# Wireless <br> World 

## Radio - Electronies • Television



F(1) IBTY=FIFTH

## TELEVISION



In the impressive link-up of national television services, large numbers of BICC Multi-Unit Cables and Polypole Couplers were used throughout Europe. They were employed with both V.H.F. link equipment and $T / V$ cameras. These cables and couplers are designed to provide a robust trailing cable system to withstand the hazards of outside television service. For further information please ask for Publication T.D.T.15.

## BICC multi-unit cables and polypole couplers

## Wirdless Worlal

RADIO, ELECTRONICS, TELEVISION

Monaging Editor :<br>HUGH S. POCOCK, M.I.E.E.<br>Editor:<br>H. F. SMITH

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# VAIVES,THUBES \&゙ CTRCUT"S 

## 30. GERMANIUM DIODES FOR TELEVISION RECEIVERS

## Advantages and Disadvantages

The point-contact germanium diode can often be used with advantage in place of its thermionic counterpart. Its compactness and long life make it suitable for inclusion in a coil unit. It is robust and non-microphonic. The interelectrode capacitance is low. There is no heater, therefore supplies are simplified and a possible source of hum is eliminated. And the forward resistance is low, giving improved detection efficiency.

The main limitations of the germanium diode, namely, its reverse current at negative voltages and its relatively large temperature dependence, can be easily allowed for in circuit design and chassis layout. Earlier diode troubles, such as sensitivity to atmospheric moisture, have been eliminated by present-day manufacturing techniques.


## The Diode Characteristic

The general form of the germanium diode current/voltage characteristic is shown in Fig. 1. There are certain significant differences from the characteristic of a thermionic diode. The comparatively steep rise of the positive portion obeys an exponential rather than a three-halves power law, with forward currents which are normally of the order of 5 or 10 mA at 1 or 2 V . At high positive voltages, beyond the normal working range, the characteristic becomes nearly linear (that is resistive), without the saturation effect which is seen in a thermionic diode.

The negative characteristic shows not only a negative current for negative voltages, but also a rapid growth of this current if the voltage is made sufficiently great. In this region (which is well beyond the working range) turnover takes place, and the characteristic reverses. This condition produces overheating and a destructive runaway. The normal reverse currents are quite small (a few microamps) and, if the published temperature and peak reverse voltage ratings are observed, reverse currents have no: harmful effect.

The characteristic, as it changes from the positive to the negative region, passes through the origin, therefore at zero voltage there is no current flow. In the immediate vicinity of this point (say within $\pm 10 \mathrm{mV}$ ) the ratio of forward to reverse resistance becomes small, and detection efficiency is much reduced.

## High and Low Current Types

The steeply rising forward characteristic of a highcurrent type of germanium diode implies a comparatively large reverse current and a comparatively low turnover voltage. Conversely, the less steep forward characteristic of a low-current type gives an extended reverse characteristic. These contrasted pairs of features are the basis of the possible range of diode types. They are the key to the choice of type for a particular application, and they are important influences on circuit design.

## Temperature Effects

Germanium diodes are affected by temperature, and all ratings apply at specified temperatures. It is necessary for the circuit designer to take into account not only the air temperature which is likely to occur in the receiver but also any heat which may be transmitted through the chassis. The appropriate forward current and reverse voltage ratings must be observed if the diode itself is not to generate destructive heat. It is not to be assumed, however, that a germanium diode is excessively sensitive in this respect. The dangers have been mentioned only in order to draw attention to the temperature rating-a rating which is not normally of much consequence where thermionic valves are used.


FIG. 2
Fig. 2 shows the standard symbol for a germanium diode in parallel with the familiar diode valve symbol. The figure is intended to assist in the reading of circuit diagrams. The differences between the two kinds of diodes should, of course, be borne in mind.

Further advertisements in this series will discuss the employment of the diode characteristic in a number of typical applications in television and f.m, receivers.

Reprints of this advertisement, supplemented by data for Mullard diode types, are available without charge.

Mullard Ltd., Technical Service Department, Century House, Shaftesbury Avenue, London, W.C. 2

## Telerision and V.H.F. Sound

THOUGH prophets are usually not lacking in courage, not many of them have been bold enough to speculate on the future of sound broadcasting vis-ä-vis television. But, without entering into competition with those few who have chanced an opinion, we may suggest that the B.B.C.'s newly launched scheme for v.h.f. broadcasting may well point the way towards a closely integrated sound/vision system of the future.

The new B.B.C. scheme, conceived several years ago, represents an idea in large-scale broadcasting that is without parallel in the world. Essentially it is based on combining Band I television stations with Band II three-channel v.h.f. sound transmitters. Propagation characteristics of these two sets of signals are not wildly different, and the scheme represents good engineering, being economical in both equipment and manpower.

Just as the addition of sound broadcasting transmitters to the television stations is a relatively inexpensive matter, the provision of v.h.f. sound facilities in television receivers is even more economical. A number of these combined sets have already made an appearance, and more are to be expected. Such combined broadcast receivers may, in the future, well satisfy the needs of the majority, and their widespread use may well lead to a closer integration between sound and vision broadcasting.
Apart from these possibilities, there is the question of quality of the new service. Interference is now almost intolerable on the medium frequencies; it goes without saying that listeners within the v.h.f. service areas will get a much quieter background. But what of improved frequency range and dynamic range? Here there are obvious limitations, including the landlines, but the B.B.C. has given assurances that the new transmissions will permit a substantial improvement in receiver performance.

## Electrostatic Londspealiens

[ ${ }^{\text {EVELOPMENTS }}$ in electrostatic speakers, now being described in articles appearing in our pages, may conceivably have an important effect on the
combined vision/sound receiver discussed in the preceding paragraphs. High-quality sound is not usually considered necessary in a television set, but improvement in this direction may be demanded when the set includes provision for v.h.f. sound reception. An obvious advantage of using the electrostatic speaker for such a set is that the necessary high polarizing voltage is already there without extra cost. It is too early to make guesses about the shape an ideal speaker would take; perhaps some change in the now-almost-traditional proportions of the television receiver cabinet would be needed.

Whether these speculations be justified or not, the resurgence of the electrostatic speaker is certainly a matter of the greatest interest. Every conceivable method of artificially reproducing sound has been explored, but for over a quarter of a century the moving-coil principle has met no serious challenger; now, good as it can be, further development seems unlikely. The moving-coil speaker has always had to carry two onerous limitations: the mass of its moving parts and the necessity for providing a diaphragm that is at one and the same time rigid and flexible. True, the mass has been utilized in designing for level output at low and medium frequencies, but the price of linearity in this range is a steady deterioration in output at high frequencies. This disability can be lessened only by allowing the diaphragm to "break up."
The electrostatic speaker, on the other hand, would appear to be the answer to the designer's dream. As was pointed out last month, its performance is always predictable, no matter what the size and shape of the diaphragm.

Since it has been shown that the electrostatic principle is not inherently non-linear, the field is open to almost limitless development. We have already heard working a prototype speaker which covers a frequency range from $40 \mathrm{c} / \mathrm{s}$ to the upper limits of audibility. There can be no denying that the quality of reproduction has a freshness not usually associated with the heavier diaphragms of moving-coil speakers. No doubt practical problems remain to be solved, but it seems likely that the electrostatic speaker, after a long period of hibernation, is coming back to vigorous life.

## V.I. F. $_{\text {. }}$ Broadcasting Starts

0N May 2nd, the v.h.f. station at Wrotham ceased to operate experimentally and started to work a regular service as the first station of the B.B.C.'s new f.m. broadcasting system. By the end of 1956, it is expected that eleven stations will be in operation and will cover $83 \%$ of the country with the Light, Home and Third programmes in a way which will be but little affected by interference. After Wrotham, a further ten stations are scheduled:-at Pontop Pike, Divis, Meldrum, Norwich, South Devon, Sutton Coldfield, Wenvoe, Holme Moss, Blaen Plwy, and Penmon.

At each station the three programmes will be radiated on frequencies $2.2 \mathrm{Mc} / \mathrm{s}$ apart in Band II. For Wrotham, the frequencies are $89.1 \mathrm{Mc} / \mathrm{s}$ (Light), $91.3 \mathrm{Mc} / \mathrm{s}$ (Third) and $93.5 \mathrm{Mc} / \mathrm{s}$ (Home). They will all be radiated from a common aerial array of the slot type. This has already been provided on many television stations (e.g., Sutton Coldfield and Holme Moss) and is evidence of the long-term planning of which this Band II service is the result.

The general plan is to have six $10-\mathrm{kW}$ transmitters at each station. In effect, they will operate in parallel pairs to provide three transmitters of 20 kW each and, with the acrial gain, an effective radiated power of 120 kW each. The interconnection of the transmitters is not straightforward paralleling, however.
If we call one pair $A_{1}$ and $A_{2}$, another $B_{1}$ and $B_{2}$ and the third $C_{1}$ and $C_{2}$, then the outputs of $A_{1}$ and $\mathrm{B}_{1}$ are combined and then mixed with the output of $\mathrm{C}_{1}$ and fed to one-half of the aerial array. The outputs of $A_{2}$ and $B_{2}$ are similarly combined and mixed with the output of $\mathrm{C}_{2}$ and fed to the other half of the aerial array.

The object of this somewhat curious arrangement is to minimize the effects of any fault. If any one transmitter develops a fault, the other one of the pair continues in operation and the result is merely a 3-db drop in signal strength. If a fault occurs in one-half of the aerial, the same thing happens. Indeed, there can be simultaneous faults in one-half of the aerial and in three of the transmitters on the same side of the chain with only a $6-\mathrm{db}$ reduction in the signal. Arrangements are made to reverse the connections of the transmitters to the aerials so that, in the event of such a double fault, the good half of the aerial can be connected to the good transmitters.

It might be thought that the parallel operation of transmitters around $100 \mathrm{Mc} / \mathrm{s}$ would be a difficult matter. Actually, however, they have a common drive. Each basic transmitter has its own drive unit but only one is used at a time to drive both transmitters of a pair, the other acting as a spare.

The system of modulation used is F.M.Q. ${ }^{1}$, developed by Marconi's, who built the Wrotham station and from whom 46 other transmitters for the scheme

[^1]have been ordered. The mean frequency is determined by a high-stability crystal oscillator and modulation is effected by a reactance-valve circuit which "pulls" the crystal frequency.

The general arrangement has been dictated by the requirement of extreme reliability, so that operating personnel are virtually unnecessary. Automatic monitoring devices are installed to call attention to any defect and, except for the repair of a fault, the stations should need no attention beyond routine maintenance.

The station at Wrotham differs quite a bit from this general description, for the apparatus is, in the main, that used for the experimental transmissions over the last few years. There are two $25-\mathrm{kW}$ transmitters with two $4 \frac{1}{2}-\mathrm{kW}$ stand-by types and two $10-\mathrm{kW}$ transmitters. The outputs of the two $25-\mathrm{kW}$ ones are combined and then the signal is split into two. With each half is mixed the output of one of the $10-\mathrm{kW}$ transmitters and each is fed, as before, to one-half of the aerial array. The final result is much the same, but the way in which it is achieved is different. It would clearly have been uneconomical to scrap two $25-\mathrm{kW}$ transmitters, which is what would have been necessary if Wrotham were to keep to the general plan for the other stations.


FATHER OF THE TRANSISTOR. This yeor's I.E.E. Kelvin Lecture was delivered by Dr. W. Shockley, leader of a team at Bell Telephone Laboratories which extended the foundations of semi-conductor physics and ultimately evalved the transistor. Dr. Shockley gave on occount af the basis of transistor physics and described some of the many applicotions of this device, such as in hearing aids and portable radio receivers. He also dealt with the prospects of using semiconductor junctions for converting light into electricol energy and disclosed that trials are to be carried out on rural telephone lines powered by sunlight.

# Tropospheric Scatter Propagation 

200-mile Transmission on Frequencies in the U.H.F. Band

IN Wireless World for July, 1952', a type of relatively long-distance transmission for frequencies in the lower part of the v.h.f. range was described, in which propagation is by a forward scattering process from irregularities in the lower part of the ionosphere, so that a portion of the radiated energy is returned to the ground and is receivable at distances up to about 1,250 miles.

According to the theory of Booker and Gordon ${ }^{2}$ a similar, but distinct, type of scattering should take place in the troposphere, even though the air there is not ionized. In this region the air is in a state of irregular motion, this turbulence being duc to local irregularities in the speed and direction of the air flow, thermal instabilities, etc. Such a turbulent medium may be visualized as one containing a large number of spherical blobs, and the dielectric constant of the individual blobs may differ widely from the mean dielectric constant of the medium as a whole. Therefore their refractive indices differ from that of the medium, in a degree depending on the scale of the turbulence, and they thus constitute a system of scattering centres for radio energy, the amount of energy scattered depending on the relation between the size of the blobs and the wavelength. The energy is scattered mainly in a forward direction, so as to be receivable at points far beyond the radio horizon of the transmitting aerial. Of course the amount of energy scattered by unit volume of the atmosphere is extremely small, but by the use of highly directive beam aerials for both transmitting and receiving, both being directed on to a given area in the troposphere, a large number of scattering centres can be brought into use, and a usable amount of energy made available at the receiver. There is increased forward beaming of the scattering with increased frequency, so that on frequencies in the u.h.f. band the scattered energy per unit volume of atmosphere is much greater than on lower frequencies.

## Practical Applications

Some experiments designed to put the above facts to a practical use have recently been carried out in America. They have been conducted jointly by Bell Telephone Laboratories and Massachusetts Institute of Technology on the lower frequencies in the u.h.f. band, and also by Syracuse University on a frequency of $915 \mathrm{Mc} / \mathrm{s}$, the latter experiment being still in progress.
The result of the first of these experiments has been to develop a system of "over the horizon" transmission, capable of being used for television picture transmission, as well as for multi-channel telephone service. The propagation medium will thus support the wide-band transmission necessary for the above services, and signals would appear to be usable over a range of about 200 miles. It is visualized, therefore, that the present requirement for u.h.f. radio links to be with-


The $60-\mathrm{ft}$. experimental aerial reflector used to receive u.h.f. television pictures at a distance of 200 miles by means of tropospheric scatter propagation.

Courtrsy Bell Telephone Laboratories
in "line of sight," i.e., about 30 miles apart, will no longer apply, and that the new system may, in time, supersede the present microwave radio relay network across the United States, in which the stations are spaced by about that distance. If that is so, and the system is economical in use, one can see immediate useful applications for it in Europe; for example, in the international exchange of television programmes.

The experiment was based on the fact that signals were consistently obtained beyond the radio horizon with the present radio link sysiem: signals which were most probably propagated according to the Booker and Gordon theory. The next step was to use higher power and erect larger aerials than are used in the conventional system. Ten-kilowatt transmitters were employed using aerial reflectors of 60 feet in diameter, that is 20,000 times the power and 30 times the aerial reflector area as compared with that used in the ordinary links. One of these aerial systems is shown in the accompanying illustration. By this means it was found possible to "beam" enough power on to the appropriate area of the lower atmesphere that sufficient energy was scattered in a forward direction so as to reach the receiving aerial far over the horizon, and there provide a workable signal. Towards the
end of 1953 it was found possible to transmit 12 speech-frequency channels over the system, and in 1954 television was first successfully transmitted between Holmdel, N.J., and New Bedford, Mass., a distance of 188 miles.

The system may be likened to that of a powerful searchlight, which casts a beam in a straight line. Such a searchlight aimed at the sky can be seen from the ground miles away, even when the searchlight is behind a hill. This is possible only because some of the light is scattered by the atmosphere and reaches the observer on the ground.
It is emphasized that, in the United States, the new system will, at first, probably act as a supplement to, rather than as a replacement of, the present radio relay link system.

The system should not be confused with the ionospheric scatter system mentioned at the beginning of this article. The maximum distances possible are much less in the present case, but, on the other hand, the ionospheric system will not support the wide-band transmission necessary for television.

The experiment being: conducted by Syracuse University appears to be on much the same lines as that just mentioned, the transmitter being at Lexington, Mass., and the receiver at Syracuse, N.Y., a distance of 254 miles, the intervening mountains ranging up to $3,000 \mathrm{ft}$. The transmitter power is 12 kW and the aerial reflectors 28 ft in diameter, these being identical at transmitter and receiver. A.M., f.m. and pulse signals are being used. The transmitting and receiving aerials are manually adjustable in azimuth and elevation in order to determine the most suitable angles for optimum results. These tests are designed - to determine which type of modulation is best suited to this type of radio link, and to determine the variations in reception with time of day, weather and seasons of the year.

## REFERENCES

1 "New Kind of V.H.F. Propagation," Wireless World, p. 273, July, 1952.
${ }_{2}$ Booker, H. G., and Gordon, W. E., "A Theory of Radio Scattering in the Troposphere," P.I.R.E., Vol. 38, No. 4, p. 401, April, 1950.

## "Adjacent-Cliannel" Colour Television

INVESTIGATIONS by the radio industry into the merits of various colour television systems for this country were discussed at a recent lecture by L. C. Jesty to the Television Society. One system under consideration, which has often been mentioned in Wireless World, is the modified version of the American N.T.S.C. system in which the colour signal is transmitted outside of the normal monochrome band, but overlapping the monochrome band of the station in the adjacent channcl. For example, the colour signal of Kirk O'Shotts (Channel 3) would be transmitted within the monochrome band of Sutton Coldfield (Channel 4), and although this would undoubtedly cause some interference it would probably not be so bad for the Midland viewers as having their own colour signal continuously present and interfering in Channel 4.

Of course, the amount of interference in this system would depend on the geographical proximity of the stations in the adjacent channels, and it appears that the radio industry's investigation so far has been largely concerned with this matter. Mr. Jesty showed a map which indicated the areas most likely to suffer from the colour-
signal interference, the worst-affected ones appearing to be largely in the North and the West. This, however, was only based on calculation and it would be necessary to carry out actual field tests if the system proved worthy of further investigation. Expressed in actual figures, the calculated results suggested that only about $1.5-2 \%$ of the viewing public would suffer from the interference for $1{ }^{\circ}$, of the time, and this, said Mr. Jesty, did not look too impossible.

## F.M. Tuner Kit

CAPACITOR and resistor kits for the F.M. Tuner described in our May 1955 issue have been put up by Erie Resistor, Ltd., and should now be obtainable from retailers. To assist constructors the $270-\Omega, \pm 10 \%$ and the $180-\Omega, \pm 10 \%$ resistors for $R_{2}, R_{8}$ and $R_{10}$ are included so that either EF80 or EF91 valves may be employed. The alternative resistors are included free of charge. Resistors $\mathrm{R}_{20}$ and $\mathrm{R}_{2}$, are, however, not included as the former is not made by Erie and the value of the latter has to be found experimentally.

The capacitor kit costs $£ 25 \mathrm{~s} 6 \mathrm{~d}$ and the resistor kit $£ 17 \mathrm{~s} 2 \mathrm{~d}$. It should be noted that $\mathrm{t}_{\mathrm{y}}$ pe NPOL is included for $\mathrm{C}_{6}$ and type NPOM for $\mathrm{C}_{11}$ as these are more suitable than type NPOK which was originally specified.

## Election Result Computor

BELOW is the electronic digital computor which the B.B.C. are using on election night to calculate the totals of seats won, lost and retained by the parties and also to forecast the final result. Built by English Electric, it is an engineered version of the N.P.L. ACE (Automatic Computing Engine) and is therefore appropriately named DEUCE (Digital Electronic Universal Calculating Engine). A feature of the machine is a magnetic drum storage system in which the two sets of recording and pick-up heads ( 16 heads on each) can be shifted automatically to any one of 16 positions across the 256 tracks on the drum in 25 milliseconds. This facility permits a great saving in electronic equipment and in fact about 1,300 miniature valves are used.

Numbers are represented in binary form by trains of pulses at a p.r.f. of $1 \mathrm{Mc} / \mathrm{s}$, each train (or "word") containing 32 binary digits or the equivalent of 9 decimal places plus a sign. "The magnetic storage drum will hold 8,192 of these "words." High speed of operation, however, is achieved partly by the use of acoustic delay lines of limited capacity for the main store, giving quick access to the stored information. Another saving of time is achieved by the precise timing of the coded instructions which initiate the various arithmetical operations. Most operations are, in fact, accomplished in 64 microseconds.


# WORLD OF WIRELESS 

Organizational, Personal and Industrial Notes and News

## B.B.C. Band III Television

WHEN announcing the plan for the clearance of mobile radio from Band III (see our May issue) the retiring P.M.G.-Earl De La Warr—stated that four of the eight channels ultimately to be made available for television would be allocated to the I.T.A. and the remainder for an alternative service in that band. In anticipation, therefore, of the P.M.G.-whoever he may be in the next Government-granting these channels to the B.B.C. for a second television service, the Corporation has ordered sound and television transmitters for two stations.

The $10-\mathrm{kW}$ vision transmitters with the associated $2.5-\mathrm{kW}$ sound transmitters are scheduled to be delivered by Marconi's towards the end of next year.

## Competitive Television

LONDON'S first competitive television programme is to be broadcast on September 22nd from the I.T.A.'s transmitter being built at Beaulieu Heights, Croydon. The I.T.A. announces that for a few weeks prior to the opening, high-power test transmissions will be radiated.

The transmitter, which will have an e.r.p. of 60 kW , will radiate in Channel 9 with offset carriers (vision $194.75675 \mathrm{Mc} / \mathrm{s}$, sound $191.27 \mathrm{Mc} / \mathrm{s}$ ). The approximate service area was given on page ${ }^{12}$, of our ${ }^{\circ}$ issue.

## Import-Export Ratio

THE provisional figure of $£ 7,625,000$ for British radio equipment exported during the first quarter of this year is an increase of more than $£ 650,000$ on the figure for the same period in 1954-a record-breaking year. The Radio Industry Council in announcing this figure draws attention to the continued marked rise in the overseas sales of sound recording and reproducing equipment. The value for the first three months of the year was $£ 1.3 \mathrm{M}$, an increase of more than $£ 430,000$ over the same period last year when exports for the whole year were valued at the record figure of $£ 3.7 \mathrm{M}$.

Although exports of valves and c.r. tubes increased during the period under review by some $£ 175,000$, and, moreover, imports of these accessories fell by nearly $£ 130,000$, there was still an adverse balance of trade of over $£ 50,000$ in this section of the industry.

Taking radio equipment as a whole, imports (according to figures issued by the Board of Trade) increased by $£ 650,000$-the increase recorded for exports.

## PERSONALITIES

Sir Edward Appleton, F.R.S., the new president of the Radio Industry Council in succession to Lord Burghley (who has held the office since 1952), has been principal and vice-chancellor of Edinburgh University since 1949. For ten years prior to going to Edinburgh Sir Edward was secretary (administrative head) of the Department of Scientific and Industrial Research. It will be recalled that in 1947 he was awarded the Nobel Physics Prize for his work on atmospherical physics and his discovery of the Appleton layer.
R. H. Hammans, recently appointed chief television engineer of Granada Theatres-one of the four programme contractors to I.T.A.-was with the B.B.C. from 1935 until taking up his new appointment. Originally on sound outside broadcasts he transferred to television O.B.s in 1937. Before going to the B.B.C. he was with the International Marine Radio Company for four years. Mr. Hammans, who operates an amateur station with the call G2IG, is executive vice-president of the R.S.G.B.
Alfred H. Whiteley, O.B.E., Comp. Brit.I.R.E., the new president of the Assaciation of Public Address Engineers, founded in 1926 at the age of 33 the Whiteley Electrical Radio Company, manufacturers of components, accessories and electronic equipment. He was elected a Companion of the Brit.I.R.E. in 1949 and became the first Companion to serve on the Council of the Institution.
T. D. Humphreys, M.Brit.I.R.E., who joined Reproducers and Ampliers, Ltd., as general manager in 1953, has been elected to the board. Before going to R. \& A., he was general manager of Radar Components, Lid., and was previously with A. C. Cossor, Ltd.
L. Kearton Parker has joined Winston Electronics, Ltd., of Hampton Hill, Middlesex, as chief sales engineer. He was for ten years with the Telephone Manufacturing Company, Ltd., which he joined in 1945 at the age of 29 , and was for some time head of the audio and acoustics section of the Development Department. From 1952 to February this year he was telecommunications consultant to the company.
In addition to those mentioned in our last issue who had received the Insignia Award in Technology (C.G.I.A.) Charles H. Rumble received the award for his thesis on the manufacture of matrices for the production of long-playing records. Mr. Rumble is a director of the Transcription Manufacturing and Recording Company, Ltd., of Mitcham, Surrey.

Sir George Nelson, who is chairman and managing director of the English Electric group of companies, which includes Marconi's, has been appointed a governor of the Imperial College of Science and Technology.

## OUR AUTIIORS


W. C. Pafford, contributor of the article on some problems of lighting in television studios, is both a television engineer and lighting engineer. In 1932 he joined the B.B.C. Midland Regional transmitter which was then transmitting sound for the 30-line television experiments. He became a maintenance engineer on 405 -line television in 1936 and was later in charge of maintenance and wartime operations at Alexandra Palace. Mr. Pafford, who is now a lighting supervisor on television O.B.s, is also an artist and a number of his cartoons, signed "Paff," have appeared in Wireless World.
G. H. Leonard, who describes a wobbulator adaptor for Band III in this issue, has for six years been with Ultra Electric, Ltd., where he is senior engineer in charge of radio and television test equipment. He was educated at University College, London, graduating with honours in physics in 1947.

## OBITUAR

Charles J. Pannill, who was the first chairman of the Board of editors of our American contemporary, RCA Review, until publication was temporarily suspended in 1942, died in New York in February. He was asscfiated with Professor R. A. Fessenden in his early wireless experiments and in 1912 received the first American radio operator's licence. He became general manager of Radiomarine Corporation of America in 1928 and was president when he retired in 1947.
Arthur H. Morse, who was with the Marconi Company as an engineer specializing in direction finding before going to N . America in the early 1920s to become managing director of the Canadian Marconi Company, died in New York on April 6th, aged 74. He joined Marconi's on their acquisition of United Wireless Telegraph Co., of which he was superintendent. In his book "Radio: Beam and Broadcast," published in 1925, he reviewed the history of radio patents, on which he was an acknowledged authority.

## IN BRIEF

Television Licences in force in the United Kingdom increased during March by 96,373 , bringing the total to over 4.5 million. The number of domestic sound-only licences totalled $9,208,936$ (including 62,506 issued free to blind persons). Television licences totalled 4,503,766 and car radio 267,794 , giving an overall total of 13,980,496.
Competitive Television.-The licence granted by the P.M.G. to the I.T.A. on April 6th for the operation of its stations will continue in force until July, 1964. It names only the Croydon station but permits the establishment of stations " at such other places in the United Kingdom, the Isle of Man or the Channel Islands, as shall be approved." The annual fee payable is $£ 500$.
B.R.E.M.A. Council.-The following member firms of the British Radio Equipment Manufacturers' Association have been re-elected to the exccutive council for the ensuing year. The names of the companies' representatives are in parentheses: Balcombe (E. K. Balcombe); Bush (G. Darnley Smith); Cole (G. W. Godfrey); Cossor (J. S. Clark); English F'.ectric (D. C. Spink); Ferguson (L. Bentley-Jones); G.E.C. (M. M. Macqueen, chairman); Gramophone Co. (F. W. Perks); Kolster-Brandes (P. H. Spagnoletti); Philips (A. L. Sutherland); Pilot (H. L. Levy) and Ultra (E. E. Rosen).
At the annual general meeting of the British Sound Recording Association on May 13th Norman Leevers, director of Leevers Rich and Company, was re-elected president for a second year of office. R. W. Lowden continues as honorary secretary, H. J. Houlgate, membership secretary and D. W. Aldous, technical secretary.

It was announced at the annual dinner of the British Wireless Dinner Club that Harold Bishop (B.B.C. Director of Technical Services) and Earl Mountbatten had accepted the invitations to become president and vice-president respectively. The membership now totals 68 .

Independent Commercial TV? A special licence was granted by the Post Office to the J. Arthur Rank Organization for relaying television programmes, including specimen "commercials," by a $6,800-\mathrm{Mc} / \mathrm{s}$ transmitter from the State Theatre, Kilburn, to the British Industries Fair at Olympia, where demonstrations of Cintel large-screen television were given.
The present extended schedule of B.B.C. Television Trade Tests (weekdays $11.0-1.0$ ) which was introduced last September will continue until August 31 st.

Since we published particulars of the international contest for Radio-Controlled Models in our May issue the dates have been changed. The boat competition will be on July 30th and the aircraft contest on the following day. Further details are obtainable from D. W. Aldridge, 1, Fowberry Crescent, Fenham, Newcastle-upon-Tyne, 4.
1.T.A. Headquarters.-Towards the end of June the I.T.A. plans to move from the temporary premises at Woods Mews, Park Lane, occupied since last October, to its permanent administrative headquarters at 13-14, Princes Gate, London, S.W.7.

Transistor-Grade Germanium-single crystal or poly-crystalline-is available to specified characteristics from G. A. Stanley Palmer, Maxwell House, Arundel Street, Strand, London, W.C.2, who will supply small quantities if required.
Band III Tests.-There has been some confusion regarding the times of the transmissions (vision 194.75 $\mathrm{Mc} / \mathrm{s}$, sound $191.27 \mathrm{Mc} / \mathrm{s}$ ) from the Belling-Lee station, G9AED, at Croydon. A test pattern is now radiated from 10.30-12.30 and 2.0-4.0 (Monday to Friday) and 10.0-1.0 (Saturday).

What is V.H.F.? What is f.m? Shall I need a new set to receive v.h.f.? These questions and many more are answered for the non-technical listener in a booklet prepared by the Engineering Information Department of the B.B.C. Sketch maps giving the approximate coverage of the first ten v.h.f. stations planned are included in the 12-page booklet obtainable free from the B.B.C. Publicity Department, 12, Cavendish Place, London, W.1.

Maximum Allowances for second-hand sound and television receivers purchased by dealers are given in the booklet "Used Radio and Television Set Values (1955)" prepared by the Radio and Television Retailers' Association and published by the Trader Publishing Company. It costs 2 s 9 d , including postage. The oldest sound and television receivers listed are of 1949 vintage. A nominal allowance of $£ 2$ is quoted for older television sets.

## EXHIBITIONS

Twenty papers on the production and properties of plastics will be presented at the Convention which is being held during the British Plastics Exhibition at Olympia from June 1st to 11th. Admission to the exhibition, which is organized by British Plastics and will be open daily from $10.0-6.0$, is 2 s 6 d .
"Silicones for Industry" is the title of an exhibition covering the production and application of silicones, which is being held at the Midland Hotel, Manchester, from June 13th to 18th. Invitation tickets can be obtained from the organizers, Midland Silicones, Ltd., 19, Upper Brook Street, London, W.1.
Instruments on Show.-The third British Instrument Industries Exhibition opens at Earls Court on June 28th. It will be open from 10.0-6.30 daily (except Sunday) until July 9 th. Admission is 2 s 6 d .
Amateur Radio Show.-The R.S.G.B. has tentatively booked accommodation in the Royal Hotel, Woburn Place, London, W.C.1, for the week November 21st-26th for this year's amateur radio show.
A Scottish Exhibition of electronic equipment in which 26 firms are participating has been arranged at the School of Engineering, Burnbank, Lanarkshire. It will be open daily ( 10.0 to 9.0 ) from June 6th to 11 th.

## BUSINESS NOTES

An order for six more v.h.f. transmitters, making 46 in all, has been placed by the B.B.C. with Marconi's. They will provide a three-programme service from Holme Moss; two transmitters being operated in parallel for each programme. The Corporation also has on order 58 transmitters from Standard Telephones \& Cables.

Aveley Electric, Ltd., representatives for Rohde and Schwarz, Munich (communication and laboratory equipment), are closing their office in Tottenham Court Road, London, W.1, on June 12th and moving into a new factory at Ayron Road, Aveley Industrial Estate, South Ockendon, Essex (Tel.: South Ockendon 3292).

Closed-circuit television equipment has been installed in a ship of the Royal Canadian Navy by Pye Canada, Ltd., to permit visual communication from the operations room to various key points in the vessel. A camera in the operations room will be focused on the plotting chart upon which the movements of other vessels are recorded. Receivers will be installed at five or six key points in the ship so that officers will have an immediate picture of the tactical situation rather than mere information about it.

Radio communication equipment, radar and other electronic aids to navigation and fishing have been installed by the Marconi International Marine Communication Company in the new fishery research vessel Sir William Hardy. Other recent Marconi Marine installations include communication equipment and d.f. gear in the new 32,000-ton-capacity steam turbine tanker British Victory, telegraphy-telephony transmitter, receivers, echometers and direction finders in the motor trawler Princess Anne, and an R/T transmitter-receiver and echometers in the motor trawler Bermuda.

McMurdo Instrument Company, of Ashtead, Surrey, announce that sales of their Unitags, both unassembled and assembled, are now conducted by Harwin (Engineers), Ltd., 101, Nibthwaite Road, Harrow, Middx. (Tel.: Harrow 0381), to whom all enquiries and orders for this component should be sent direct.

Airtech, Ltd., of Aylesbury and Thame Airport, Haddenham, Bucks, have been awarded, by the Canadian Department of Defence Production, the contract for the maintenance and repair of all radio and electronic equipment used by the Canadian air force in the United Kingdom.

Gresham Transformers, Ltd., have transferred the production of small transformers for the Electronics Division to their Lion Works on Hanworth Trading Estate, Feltham, Middlesex. K. G. Lockyer, B.Sc., A.M.I.E.E., A.M.Brit.I.R.E., who has been appointed manager of Lion Works, was formerly production manager with Solartron Laboratory Instruments, having previously been with Philips (Mitcham Works), Plessey and London Electrical Company.

A transposition of figures in Goodmans' advertisement in this issue has been noticed since the page went to press. The fundamental resonance of Type 1205 is $75 \mathrm{c} / \mathrm{s}$ and that of Type 1210 is $35 \mathrm{c} / \mathrm{s}$.

Among the contracts recently placed with Pye Marine for v.h.f. radio-telephone equipment are installations for 10 tankers operating on the Manchester Ship Canal; for Aberdeen fishing vessels-providing short-range intercommunication whilst fishing in pairs; and for the new Trinity House pilot vessel Pathfinder. Pye Marine have also provided a fixed station at the boat yard of SaundersRoe (Anglesey), Ltd., and a mobile set is taken on board new craft undergoing sea trials so that results of the tests can continually be communicated to the yard at Beaumaris.

THE LATEST B.B.C. mobile control room for television O.B.S which is fitted with three Marconi comeras and associated control and monitoring equip. ment. In the foreground are the 10-channel sound-mixing panel and the vision-mixer which will accept eight inputs. Behind are the picture monitors.

A new factory at W'est End, Congleton, Cheshire, has been bought by Aerialite, Ltd., for the manufacture of television aerial equipment, convertors and components.

The radio components ( Clix ) and wiring accessories departments of the Edison Swan Electric Company, Ltd., have moved from 21, Bruton Street, London, W.1, to the company's head office at 155, Charing Cross Road, London, W.C. 2 (Tel.: Gerrard 8660).

## EXPORT NEWS

The equipment for another radio link for the Swiss television network has been supplied by the General Electric Company, who equipped the trans-Alpine link in time for the European programme exchange last year. The new link connects Uetliberg (Zurich) with La Dole (Geneva)-a distance of about 150 miles-and also ties in with the earlier installation linking Chasseral and Monte Generoso.

An order worth over $£ 20,000$ to supply the Eire Department of Posts and Telegraphs with three 12-channel open-wire telephone carrier systems has been secured by the Automatic Telephone and Electric Company in face of keen Continental and American competition. The equipment will link Limerick and Tralee, Limerick and Ennis, and Mulingar and Cavan.

A technical assistance mission from the International Civil Aviation Organization is advising the Afghanistan government on bringing the country's two main airfields up to international standards. As part of the development scheme the Department of Civil Aviation has ordered from Redifon, Ltd., twelve 5-W radio-telephones, three $50-\mathrm{W}$ radio-telephones, two 500 -W h.f. transmitters for ground-to-air telephony, two non-directional beacons and four communication receivers. Twelve of these communication receivers, which cover the range $13.5 \mathrm{kc} / \mathrm{s}$ to $32 \mathrm{Mc} / \mathrm{s}$, have also been ordered by the New Zealand Posts and Telegraphs Department.

Six studio tape recorders (Type BTR/2A) have been ordered from E.M.I. International, Lid., by All India Radio, which has previously ordered 17 transportable tape recorders (Type TR/50A). Thirty-two of these transportable instruments have also been supplied to the Indian Ministry of Information and Broadcasting.

Redifon radio equipment has been installed in the fleet of $75-\mathrm{ft}$ motor trawlers built in Hong Kong for the South Korean government under a United National Korean Reconstruction Agency procurement plan.


# Components Exhibition 

TRENDS EVIDENT AT THIS YEAR'S R.E.C.M.F. SHOW


#### Abstract

The "private" exhibition held in London by the Radio and Electronic Component Manufacturers' Federation from 19th to 21st April is reviewed in these pages. In addition to describing in detail some of the new components and accessories shown, we give in each category a list of exhibitors and their main products. Test and measuring equipment, and also valves, are dealt with on pp. 274 and 277. New sound-reproducing equipment will be discussed in a later issue.


## RESISTORS

ONE of the most interesting and useful resistance devices scen for some time was shown this year by Erie. It consists of a low-value resis:or with a tensioned coil spring soft-soldered to one end, the whole being enclosed in a ceramic capsule. It is intended to combine the functions of a surge limiting resistor and fuse in the anode circuit of mains rectifiers and is appropriately called a fuse resistor. In the event of a heavy current flowing for an appreciable time the heat generated in the resistor melts the solder and releases the spring and so opens the circuit. The fuse "blows" about 15 sec after the breakdown, or short circuit developing.
Metallized film resistors are being more widely adopted where high stability is required and although the technique is not new it laid dormant for many years before revival in admittedly a modernized form a few years ago. The latest addition to this type is the new " $Q$ " model developed by Erg. It measures 2 in long by $\frac{11}{32} \mathrm{in}$ in diameter and is rated at 2 W . The metal film is deposited on a glass rod and then spirally cut to give the required resistance values.
Two main lines of development can be seen in connection with the ubiquitous carbon volume control. One is the introduction of still smaller models with, of course, lower wattage ratings. For transistor equipments only low-wattage types, are required at present. Egen have a sub-miniature pre-set open lype rated at $\frac{1}{10} W$ and


Left: Double "Q" volume control made by Dubilier


Right: Miniature $\frac{1}{1} \mathrm{~W}$
pre-set volume control
(Egen)
measuring approximately $\frac{3}{4} \mathrm{in} \times \frac{1}{2} \mathrm{in}$; Plessey have one, described as the Type $G$, on a circular base of just over $\frac{1}{2}$ in in diameter while Morganite have some models designed originally for hearing aids and later developed for other uses.

Reduction in size of the domestic-type volume control proceeds apace and several firms, Dubilier being one, have extended the idea by ganging their miniature "Q" type in order to save panel space. Concentric spindles are employed. Ganged type are popular in mobile equipments and especially in car radio sets where the frontal aspect has to be kept down.

The final main development is complete sealing of the element, the object being to give better stability under widely varying conditions of temperature and humidity. Many ingenious ways are employed to seal the spindle without introducing too much friction.

Manufacturers: A.B. Metal Prodts.; British Elect. Res.; Bulgin; Colvern; Dubilier; Egen; Electronic Cornp.; Electrothermal; Erg; Erie; Lalgear; Morganite; N.S.F.; Painton; Plessey; Salford; Welwyn; W.B.; Zenith.

## CAPACITORS

TWO fairly recent developments in electronics are largely responsible for a new trend in capacitor design. One is the transistor, which has called for some quite high-value capacitors for low-voltage operation ( 1.5 volts upwards). The other is the more recent jump to popularity of the printed circuit. This, and the transistor assault, has required capacitor makers to think in terms of sub-miniature parts, so we now have quite a large number of what can only be described as lilliputian capacitors, fixed and variable.
T.C.C. have introduced a range of low-voltage electrolytics designed especially for transistor circuits. Known as the CE58 series, they have capacitances ranging from $0.25 \mu \mathrm{~F}$ to $6 \mu \mathrm{~F}$ and in working voltages of from 25 for the small capacitance to 1.5 for the larger. Those in this series measure $\frac{5}{8}$ in long and only $\frac{1}{8}$ in in diameter. Some slightly larger models with higher working voltages are also available.

Sub-miniaturization of ceramic and other types is being applied for use in printed circuits, also the position and kind of connecting wires may be almost, if not quite, as important as the size of the component itself. Eric has introduced a range of components, including capacitors, described as "stripped." The omission of moulded cases and other "protection" has resulted in quite a big reduction in size. While the lead-out wires are arranged to suit their own particular versions of the printed circuit there are many Erie capacitors that meet without modification the requirements of other styles of printed circuitry.

Hunt's have modified several of their existing capacitors for printed circuit use. The main changes consist of fitting thin easily solderable wires to electrolytics and other capacitors which previously had unsuitable connections and bringing out the leads along the side of a tubular rather than at the extreme ends. The "Thermetic" Type W97 is a new Hunt's product and is one of the smallest metal-clad metallized-paper capacitors seen so far. A $400-\mathrm{V}, 0.001-\mu \mathrm{F}$ capacitor in this range measures only 0.135 in in diameter and 0.61 in long. The range includes $200-$, $400-$ and $600-\mathrm{V}$ type from 50 pF to $0.04 \mu \mathrm{~F}$.
A smaller version of the Polystyrene series of capacitor made by Suflex is now available; it measures only $\frac{1}{2}$ in


Wingrove and Rogers a.m./f.m. two-gang capacitor.


Hunt's capacitors modified for printed circuits.
long and $\frac{3}{16}$ in in diameter and is made in capacitance ranging from 5 to 250 pF . Some Suflex models now have the connecting wires brought at onc end instead of at both ends; these are intended primarily for printed circuit use, but have other applications as well.
Although Dubilier did not show capacitors made especially for printed circuits it was pointed out that so many of their capacitors are in the lilliputian class that they fit the requirements without modification. They have introduced a new range of lead-through capacitors for use with screened rooms and screened equipment of various kinds. They are metal clad and some models are actually two capacitors back-to-back with a common "earthing" plate between them. Some of the larger (physically speaking) models will carry as much as 5A; a $0.1-\mu \mathrm{F}$ type in this catcgory measures only $\frac{3}{4}$ in in diameter and extends $1 \frac{1}{8}$ in either side of the earthing flange. This model is for 250 V a.c. or d.c. working.

An interesting devclopment is a vitreous capacitor using glaze for both the coating and the dielectric. Known as the Vitricon range they are made by Welwyn Laboratories, and are said to be quite satisfactory for use up to $150^{\circ} \mathrm{C}$. At this temperature the insulation resistance is better than $10^{10} \Omega$. They are quite small and available in a wide range of valucs.
The demand for a tuning capacitor suitable for an a.m./f.m. receiver has been met by Wingrove and Rogers with a model having a normal capacitor section associated with a special wide-spaced anti-microphonic v.h.f. scction. The v.h.f. sections are sct in the middlc of a 2 -gang assembly each side of the dividing screen with the a.m. sections before and behind them respectively. A capacitance swing of 17.4 pF is provided for $\mathrm{f} . \mathrm{m}$. tuning. These are available to manufacturers only.
Jackson Bros. have a range of gang capacitors embodying what is described as a band-spread section in each unit. Thesc sections can be of various values and the smallest, giving about a $12-\mathrm{pF}$ swing, would serve a.m./f.m. requircments. The main capacitor unit is of the usual size for medium- and long-wave use.
Special two-gang variable capacitors for f.m. units and convertors giving under 20 pF coverage were shown by Plessey, Jackson and Wingrove and Rogers, while a long range of lilliputian variables in single, butterfly and splitstator patterns were seen on the Stratton stand. These have small-diameter spindles and provision is made for


Selection of latest T.C.C. capacitors including transistor sub-miniature types.
ganging any number by means of appropriately small flexible couplers.
Manufacturers: B.I. Callenders Cyldon; Daly; Dubilier; Erie; Hunt; Jackson Bros.; London Elect. Manf.; Mullard; Plessey; Stabiiity Radio; Stration; Suflex; T.C.C.; T.M.C.; Walter Inst.; Wego; Wingrove and Rogers.

## COILS AND TRANSFORMERS

BY combining a $10.7-\mathrm{Mc} / \mathrm{s}$ i.f. transformer with one of $465 \mathrm{kc} / \mathrm{s}$ or so in a single screening can a considerable saving can be effected in the space taken up by i.f. transformers in an a.m./f.m. receiver. Dual i.f. transformers of this kind were shown by the Wireless Telephone Company (one of the Plessey group) and by Weymouth.

The W.T.C. model is houscd in an aluminium can measuring $1 \frac{1}{4}$ in $\times$ lin $\times 2 \frac{1}{2}$ in high and the two transformers are mounted side-by-side lengthwise in the can with the dust cores accessible from top and bottom. Each is independently trimmed. The " $Q$ " of the a.m. transformer is given as 110 and that of the f.m. one somewhat less. The f.m. bandwidth is said to be about $330 \mathrm{kc} / \mathrm{s}$. In addition to the dual i.f.s. there is a dual a.m./f.m. ratio detector unit and a separate $10.7-\mathrm{Mc} / \mathrm{s}$ i.f. transformer.

In the Weymouth models the two transformers are assembled crosswise in the can with the dust cores accessible from two opposite sides. The f.m. transformer is designed for $10.7-\mathrm{Mc} / \mathrm{s}$ working, has a bandwidth of $330 \mathrm{kc} / \mathrm{s}$ measured between $6-\mathrm{db}$ points and a nominal " Q " of 80 . The companion a.m. transformer is designed for an $11-\mathrm{kc} / \mathrm{s}$ bandwidth ( $6-\mathrm{db}$ points), has a " Q " of 55 and is centred on $470 \mathrm{kc} / \mathrm{s}$. The ratio detector model has a peak-to-peak bandwidth of $400 \mathrm{kc} / \mathrm{s}$ and the a.m.rejection is said to be -45 db .

Stratton also were showing some $10.7-\mathrm{Mc} / \mathrm{s}$ and some $5.2-\mathrm{Mc} / \mathrm{s}$ transformers, and these included both ratio detector and Foster-Seeley types.

Except for improvements to detail nothing outstanding was seen in the design of iron-cored components. Further developments and expansion in the application of the resin potting technique was evident, and in the principal makes there are now some four different styles available; resin cast, metal potted with some kind of filling, hermetically sealed and open windings, now almost always vacuum impregnated.

## Manufacturers:

Advance; Associated Electronic; Elac: English Electric; Ferranti; Goodmans; Gresham; Igranic; Parmeko; Partridge; Plessey; R. \& A. Rola; Stratton; T.M.C.; Weymouth; wircless Wearite; Zenith.

Wirele ss Telephone (Plessey) a.m.|f.m. dual i.f. transformer.


## TELEVISION COMPONENTS

THE double-triode cascode r.f. amplifier and the triode-pentode frequency-changer form the basis of nearly all television receiver "front-ends." Tuners embodying them fall into two groups of similar external appearance and controls. Most have switch station selectors with 12 positions giving a choice among five Band I and seven Band III stations. The other control is an oscillator trimmer.

In one group, the turret tuners, there are individual coils for each station, fixed to strips carrying the connecting contacts which are mounted on a rotating framework. The individual coils are thus brought round to the circuit for connection. The other group is of the incremental inductance type. Wafer switches are used and between each pair of contacts is connected the small inductance needed to change the tuning from one channe! to the next. With this type, alignment must be done first on the highest frequency channel, then on the next channel lower and so on. With the turret tuner, however, the coils for each channel can be aligned independently.

The Cyldon Teletuner Mark 1 is of the turret type and is claimed to have noise factors of 5 db and 9 db on channels 1 and 8 with gains of 43 db and 36 db . The oscillator drift is stated to be under $100 \mathrm{kc} / \mathrm{s}$ for a temperature rise to $60^{\circ} \mathrm{C}$.

The N.S.F. tuners are examples of the incrementalinductance type. One model covers not only the 13 Bands I and III stations but has an extra switch position to enable reception to be obtained in the u.h.f. band if it becomes necessary in the future.

The Weymouth television i.f. strips are virtually com-

N.S.F. television tuner of the incremental-inductance type.
plete receivers except for the scanning circuits and power supplies. They comprise sound and vision i.f. amplifiers with the detectors, noise limiters, video stage and sync separator. The r.f. side is made as a separate unit which can be dropped into a cut-out in the main chassis.

This firm also showed a two-valve convertor for Band III which is designed to provide an output in Band I at the frequency of the local station. Aerialite also showed Band III convertors intended for use with any Band I receiver.

Little change was evident this year in scanning components save in details of design. The use of Ferroxcube, dust-iron and similar materials has obviously come to stay, as has the castellated yoke. Mullard now have such a yoke with 16 slots, enabling a better field distribution to be secured. Deflection assemblies for $90^{\circ}$ tubes were shown by several firms, including Igranic and Plessey, and can be picked out at once from the $70^{\circ}$ types by the enormous turned-up front ends of the line coils. It is interesting to see that in these assemblies the frame coils are not the conventional saddle type but are the so-called toroidal type. That is, there are four frame coils wound around the core material.

Line-scan transformers are of the type that has now become conventional, but it is obvious that increasing attention is being paid to insulation. In some Igranic models, for instance, the e.h.t. rectifier is mounted inside what can only be termed a plastic "bath-tub"!

The permanent magnet for focusing and for ion traps was well in evidence. Goodmans showed a new focusing unit in which the magnets are held by a die-casting, while Elac showed several types. Among these is the Duomagnette with two opposing ring magnets. The Marrison \& Catherall unit is designed to minimize astigmatism and both the focus and the shift controls can be adjusted from outside the receiver.
*Makers: Acrialite (C); Cyldon (T); Elac (F); Goodmans (F); Igranic (D, Tr.); Long \& Hambly (M); Marrison \& Catherall (F); james Neill ( F ); N.S.F. (T); Plessey (D, F, T, Tr); Weymouth (C); James Neill (F);
*Abbreviations: $C$ convertors; $D$, deflector coils; $F$, focus units and ion-trap magnets; $M$, masks; $T$, tuners; $T r$, transformers.

## SUB-ASSEMBLIES

AMONG the larger items in this category was a new a.m./f.m. tuner shown by Weymouth. It covers the medium- and long-wave bands and the full f.m. allocation from 84 to $96 \mathrm{Mc} / \mathrm{s}$, and the wavechange switch also has a position for "Gram." The r.f. amplifier is a 6AM6 and is operative only on the f.m. band, while the frequency changer is a 6BE6. Maximum power consumption is 0.6 A at 6.3 V for 1.t. and $12-22 \mathrm{~mA}$ at 200 V for h.t. Another new tuning unit, for the medium-wave band, was shown by Cyldon, but this contained no valves and was simply a
system of pre-set permeability-tuned coils operated by push-buttons, with facilities also for manual tuning.
Printed circuits were very much in evidence and a wide range of circuit configurations, including Band I/Band III television tuners and aerial cross-over networks, $35-\mathrm{Mc} / \mathrm{s}$ i.f. transformers, computor panels, transistor circuits and r.f. filters, were displayed by T.C.C. These were made by the conventional etching process, but examples of a new method of manufacture were to be seen on the Erie stand. In this the insulating base material is embossed with the required circuit and the copper foil is pressed into the declivities, the excess copper on the raised parts being milled off afterwards. The method is claimed to avoid any troubles which may be caused by acid remaining from the etching process and also to give thicker conductors capable of carrying more current.

The valve-circuit support shown by McMurdo last year, with the valveholder mounted on top of a plug-in pedestal, is now supplied by the makers with the customer's circuit components already assembled and potted in a solid cylinder of resin around the pedestal.
Makers*: Advance (D); B.I.C. (D); Cyldon (T); Erie (P); Ferranti (D); Hunt (P); McMurdo (VC); Plessey (P, LA); T.C.C. (P): Wego (D); Weymouth (I, LA); Wright and Weaire (LA).
*Abbreviations: $D$, delay networks; LA, coil assemblies; $P$. printed circuits: $T$, tuning units; $v C$, valve circuit assemblies.

## AERIAL EQUIPMENT

ALTHOUGH the new f.m. broadcast service is due to commence long before Band III television will materialize the whole emphasis in the acrial display at the show this year was Band III aerials and adaptors.

It is now apparent that anywhere outside the immediate vicinity, or swamp area, of a Band III station something more elaborate than a simple dipole, or dipole adaptor, will have to be used. This may not always be necessary in order to get a strong enough signal, but very often to differentiate between the direct signal and a signal arriving by an alternative path or paths and produced by reflections from buildings of one kind or another. These invariably give rise to ghost images.

Simple adaptors for existing types of Band I acrials will find many applications and some quite ingenious and inexpensive arrangements were seen this year. For example. Belling-Lee have a kit comprising a number of rods and two plastic insulators for holding them in position on a single dipole. The rods extend each side of the centre insulator and lie parallel with the dipole and partially enclose it. They behave on Band III as two transmission lines end-feeding the exposed end parts of the Band I

Belling-Lee combined Band1 dipole and director and folded dipole for Band III.
aerial. These end parts behave as three-quarter wavelength aerials fed in phase. The result is that on Band III there is a gain of about 3 db over a plain dipole.

Other firms have applied various schemes which enable the Band I aerial to be made to operate as an harmonictype aerial giving a gain over the existing aerial. Adaptors of one kind or another for " H " and " X " acrials were shown by Acrialite and Antiference.

The more elaborate kind of adaptor takes the form of two or
 more elements of Band III length fitted to an existing " H " or multi-clement aerial and utilizing in some cases one of the existing larger clements to reinforce the pick-up on Band III. Sometimes the mast is employed as an untuned reflector element. These adaptors arc arranged to be fixed either in line with the existing Band I elements or at any desired angle, the latter to cope with conditions arising from the Band I and Band III stations being differently sited. Aerialite, Antiference and Belling-Lee showed these additional aerial parts mounted on outriggers for attachment to the cross arm of an existing " $H$ " type and capable of swinging to any direction required irrespective of the alignment of the "H." In all cases the aim is to provide more gain from the Band III system than given by the accompanying Band I acrial, as this will generally be found necessary.

Whereas a four-element aerial is about the largest it is practical to use for Band I, it will be quite practical to go to a 10 - or 12 -element Yagi on Band III, given a suitable kind of mast. The smallest independent Band III aerial was a 3 -element one, the largest had 10 to 12

Antiference combined Band-1 " H " and Band-Ill 4-element Yagi television aerial.


elements, giving a gain over a plain dipole of 14 db or more. Like the Band I 4-element Yagi these multielement types can be mounted either as a stack, i.c., onc above the other with appropriate spacing, or as a broadside array; the two system being a half wavelength apart and side-by-side. Being generally smaller stacking or broadside mounting is more practical on Band III than on Band I. All the firms making aerials had several designs of this kind.
When separate Band I and III aerials feed into a single input on the receiver, or a combined aerial such as a Band I with adaptor elements feeds into scparate inputs on the set, a filter is required between the aerial system and the receiver to prevent inter-action between the aerials. These filters take various forms, but basically they separate out the signals on the two bands and direct them along their correct courses. Belling-Lee call their unit a " Diplexer Tuned Filter." Antiference call theirs a "Y Box" and it provides rejection of the unwanted band of something over 20 db ; its insertion loss is said to be no greater than 0.75 db on any channel and it is intended for $70-$ to $80-?$ cables.
A Band III acrial of very unusual design is made by J-Beam Aerials. It consists of a horizontal skcleton slot flanked on each side by a 4 -element vertical Yagi. The combination is matched to an $80-\Omega$ cable and it is said to give a gain over a plain dipole of 14 db . The ends of the slot form bent-over acrial elements for the Yagis and the long sides the matching section for end-feeding the two Yagis. Although J-Beam Aerials specialize in end-fed television aerials this must surely be a unique application of the principle.

Manufacturors: A.B. Metal Products; Aerialite; Antiference; Belling-Lee; B.I. Callenderis Cables; Henley's; J. Beam; Permanoid; Sutlex: Telcon: Transradio.

## SWITCHES

THE advent of a.m. /f.m. reception has obviously brought with it some complications in recciver switching. The new switches designed for this type of circuit by A.B. Metal Products bring to mind the days of press-button tuning, for they use a piano-key type of action. A maximum of eight keys can be provided in one unit and there are six sets of changeover contacts on each key. Mountings for coils are also incorporated. Slider switches intended for a.m./f.m. receivers were shown by Plessey, and these had a two-way action with as many as 10 poles available.

Amongst the rotary switches a new precision type on the Electronic Components stand was notable for the even pressure of the wiper contacts on the fixed contacts, obtained by a helical spring inside the wiper (see sketch). The switch has 32 positions and can be supplied with one, two or three poles and up to six banks. Another rotary switch using helical springs in a similar way was shown by N.S.F. and was capable of carrying up to 10 amps. A version of the well-known German Winkler rotary switch is now being made by Painton, and a notable improve-

A.B. Metal Products piano-action switch.

ment is the use of a moulded panel to carry the fixed contact studs. The contacts can be silver-, gold- or rhodium-plated.

A new range of micro-switches was shown this year by Pye, with operating pressures ranging from 3 oz to 18 oz . Some of these are worked directly by the plunger while others have a lever acting on it. The contact ratings are all $5 \mathrm{~A}, 250 \mathrm{~V}$ for a.c. and $5 \mathrm{~A}, 12-29 \mathrm{~V}$ for d.c. Bulgin have extended their range of micro-switches and were again showing the more recent sub-miniature types which are not in the usual Bakelite cases.
Makers*: A.B. Metal Products (L, P. R, S); B.E.R.C.O. (R); Mulginers*: A.B. Metal Piamond, H . (L, $\mathrm{L}, \mathrm{R}$ ); Electronic Components ( $\mathrm{P}, \mathrm{R}$ ); Erie (R); N.S.F. (L, P, R, S. S ); Painton ( $\mathrm{L}, \mathrm{P}, \mathrm{R}$ ); Plessey
 R, S); Wh hiteley (P, R, S); Wright and Weaire (R).
*Abbreviations: L , lever or toggle; M , micro-switch; P , push . button; R , rotary; S , slide.

## CHASSIS FITTINGS

THE rapid development of printed circuits is having a noticeable effect on the type of chassis fittings now coming on to the market. Flat, strip-type connectors were shown by Bulgin, McMurdo and Belling-Lee (see picture) and specially designed valveholders by Carr Fastener, McMurdo and British Mechanical Productions. Some of the valveholders have tags which project downwards through holes in the printed circuit plate, but the one shown by British Mechanical Productions has long spring fingers bent upwards which press on the edges of the circuit when the holder is let into a hole in the plate.

A wide range of spring clips for various applications was displayed by Simmonds Aerocessories, the two latest additions being clips for holding screening cans and a small coil-former support (see sketch). Another new fixing device was a self-locking plastic nut shown by Carr Fastener. It snaps into a hole in the metal and when a self-tapping screw is driven into it the plastic expands and grips tightly.

Tag-strip in a very simple and cheap form was a popular exhibit on the Creators stand. Known as "Plantag" it consists of a rigid P.V.C. moulding of Lshape cross-section with tags in one plane and fixing holes in the other, and it can be supplied in any length. By warming the P.V.C. the strip can be bent round in a circle if required.

Prefabricated cabinets were again the main feature of


Printed-circuit valveholder by British Mechanical Productions


McMurdo miniature connectors
the Widney Dorlec stand, and this year die-cast corner units were on view. Imhof have now entered this field in conjunction with Elliott Brothers, the instrument manufacturers, and they were showing an interlocking system for fixing the struts of the cabinet frame into the corner pieces (see sketch).

Makers: Aerialite; Antilerence; Associated Electronic Engineers Belling-Lee, British Mechanical Productions; Bulgin; Carr Fastener Creators; Colvern; Egen; Electrothermal Electronic Components Hassett \& Harper; Hellerman; Igranic; Imhof; Long \& Hambly McMurdo; Micanite; Painton; Plessey; Ross Courtney; Simmonds Spear; Standard Insulator; Stocko; Stratton; Telcon; Thermo plastics; T.M.C.; Transradio; Tucker-Eyelet; Tufnol; Weymouth Whiteley; Widney-Dorlec; Wimbledon; Wingrove \& Rogers.

## RELAYS

THE switching of r.f. circuits on coaxial cable presents a difficult problem in relay design because of the impedance mismatching which can occur. Besson \& Robinson have tackled it successfully, however, and were showing three coaxial changeover relays with very low standing-wave ratios. The latest one, type A07, is characterized by having permanently fixed cable tails instead of sockets. The v.s.w.r. is $1: 1.1$ while the impedance is $45 / 60$ ohms or $70 / 80 \mathrm{ohms}$ and the operating voltage $17 / 28$ volts d.c.

A new relay notable for its sensitivity was shown by Magnetic Devices. It operates on a current of 1 mA at under 0.5 V and will switch two circuits of either 5 A at

250 V a.c. or 5 A at 30 V d.c. The mechanism is hermetically sealed and mounted on an octal plug-in base. Like many other of the relays on show it has a balancedtype armature to prevent false operation by external shock or vibration. The Besson \& Robinson K01, for example, an alternative to the Post Office type 3,000 relay, will withstand accelerations of up to 25 g .
Makers: Besson \& Robinson; Magnetic Devices; N.S.F.; Oliver Pell Control; Plessey; Pullin; T.M.C.; Walter Instruments; Woden: Zenith.

## IIATERIALS

IN the production of high-permeability nickel-iron alloys by conventional melting processes, the properties of the material are often adversely affected by the inclusion of impurities originating in the crucible lining or deoxidizing fluxes. It is also difficult to control the composition due to the different rates of loss of the constituent elements. A powder-metallurgy process developed by Henry Wiggin and Company uses carbonyl nickel, iron and other metallic powders as raw materials, and retains the original measured proportions and produces an alloy which is less susceptible to the presence of water vapour in the hydrogen atmosphere used for inal heat treatment. There is also less susceptibility to surface effects which reduce permeability when the strip is rolled, and an initial permeability of 25,000 is maintained down to a thickness of 0.0005 in in Ni77, Fel4, Mo4, Cu5 alloy.

Most manufacturers of core laminations are concentrating on the production of oriented-grain silicon steels, primarily for " $C$ " and " $E$ " cores fabricated from bent strip. Strip thickness down to 0.002 in are available from


Multicore solder thermometer.


Clips for screening cans and coil former support by Simmonds Aerocessories.


Besson \& Robinson coaxial relay with fixed cable tails.


Belling-Lee connectors for printed circuits.
G.K.N. loudspeaker fixing screw

Telcon-Magnetic Cores. Geo. L. Scott also supply flat laminations of this material 0.012 in thick for cores assembled in the conventional manner. Joseph Sankey and Sons have introduced a new interlaminar coating which will withstand re-annealing temperatures of $800^{\circ} \mathrm{C}$ and is also waterproof.

Ferrite moulded cores for television line timebase transformers and deflection yokes, and extruded rod for r.f. inductors and aerials have been added to the range of moulded magnetic materials made by Salford Electrical Instruments,

Among "hard" magnetic materials the new Mullard "Ticonal L" anisotropic alloy, designed for loudspeaker magnets, is of special interest to manufacturers of loudspeakers using a centre-slug type of magnet assembly. It has a remanence of 14,000 gauss, and increases of up to 10 per cent on the previous upper limit of flux density of gauss $/ \mathrm{cm}^{2}$ are possible.

Most manufacturers of winding wires are now in production with polyurethane coatings which need not be previously removed before soldering. A new coating with exceptional resistance to the action of solvents has been developed by Connollys. It is known as "Conyclad" and consists of a basic layer of vinyl acetal enamel, coated with nylon. The outer layer protects the base enamel from "crazing" under the action of varnish solvents, and eliminates the annealing process which is normally adopted to reduce crazing.

The successful production of wave-wound coils depends upon the mechanical as well as the electrical properties of the wire, and Fine Wires, Ltd., have produced a range of single and multiple conductors with a variety of textile coverings specially for use on wave-winding machines.

Manufacturers of r.f. cables have anticipated the demand for Band III television aerial downleads with coaxial cables in which the dielectric is cellular polythene. Compared with a sold polythene dielectric cable the attenuation may be reduccd by as much as 40 per cent, and typical figures for a 0.290 in outside diameter cable are $3.3 \mathrm{db} / 100 \mathrm{ft}$ at $200 \mathrm{Mc} / \mathrm{s}$ with a capacitance of $17 \mathrm{pF} / \mathrm{ft}$. Another advantage of the cellular type of filling is that no elaborate precautions are necessary to seal the ends, as there are no connecting passages between the air cells, and moisture cannot penetrate the dielectric.
Polythene-insulated cables can give rise to microphonic noise which may be troublesome at very low signal levels. This has been overcome in Telcon " $G$ " coaxial cables by coating the outer surface of the polythene with graphitic conducting film to disperse charges which might otherwise fluctuate with intermittent movement of the outer braiding. This year a further improvement has been effected in a " $G G$ " cable in which similar treatment is applied to the inner surface of the insulant.
Silicone elastomer materials are finding increasing applications in the preparation of insulating cloths, tapes and sleeving. In the "Symel" grade of sleeving made by H. D. Symons the mechanical strength is improved by glass braiding applied on the inside and/or the outside of the silicone. A similar combination of special interest for high-temperature applications was shown by Suflex, Ltd.
Electrical insulating tapes coated with a thermosetting adhesive have been added to the already wide range of "Scotch Boy" tapes made by the Minnesota Mining and Manufacturing Company. Curing is effected during the normal drying-out process in coil manufacture, to give a permanent bond which will withstand subsequent varnishing or impregnation. The composition of the adhesive is controlled to obviate any possibility of initiating corrosion in the wires.
Impregnating resins of the ethoxyline type with low viscosities at room temperature are among the new plas-
tics introduced by Aero Research, Ltd. No solvent is necessary and polymerization on heating is effected without the evolution of any vapours which might cause voids. Another recent "Araldite" product is a cold-setting adhesive for fixing electrical strain gauges.
Formers for the resistance elements of wire-wound potentiometers are usually of phenolic plastic strip, and difficulty is often experienced in finding material of suitable thickness which will not crack when bent. A suitable grade has been developed by H. Clarke \& Co. (Manchester) which can be bent into circles of less than lin diameter without cracking.

Printed circuits and dip soldering techniques have made new demands on the services of solder manufacturers, who have responded with a full range of special alloys, fluxes, and chemicals for preparing and preserving metal surfaces. Other new products in this field include a neat and robust junction pyrometer by Multicore for measuring rapidly the temperature of soldering baths or soldering iron bits. The scale is calibrated in Centigrade and Fahrenheit with a maximum of $400^{\circ} \mathrm{C}\left(752^{\circ} \mathrm{F}\right)$. Enthoven have demonstrated a new cored aluminium solder which functions at ordinary soldering iron temperatures without any auxiliary aids such as ultrasonic vibration. Copper wires can be soldered to aluminium of light-gauge and commercial purity and also to a number of aluminium alloys.

Finally, since screws can be regarded as a raw material as far as radio engineers are concerned, we mention two interesting developments by Guest, Keen and Nettlefold. One is the introduction of B.A. and wood screws in solid nylon, which, apart from their obvious non-conducting and good dielectric properties, are free from corrosion. The tensile strength is 5 tons/in ${ }^{2}$ at room temperature and 7 ton $/ \mathrm{in}^{2}$ at $-40^{\circ} \mathrm{C}$. The other Nettlefold screw is a combination of a left-hand wood screw and a B.A. screw on the same shank for fixing loudspeakers to baffle boards. The left-hand wood thread ensures that any movement when finally tightening the fixing nuts will tend to draw the screw further into the woodwork.
Makers
Technical : Aerialite (C, IS, W); Aero Research (IM); Associated Bray (CF, CE); B I. Cal (B, C, IM, IS, W); Bakelite (IM); Geo ${ }_{\text {Prastics }}(\mathrm{IM})$; Bullers (CF CE); Cle CO, IS, W); British Moulded (C, IM (IM); Bullers (CF, CE ); Clarke (CF, IM, IS); Connollys Duratube , ; Cosmocord (CF); Creators (IS); De La Rue (IM, IS); Duratube and Wire (B, C, CO, IS, W); Ediswan (W); Englis! Electric (L); Enthoven (S); Fine Wires (W); Guest, Keen and Nettlefolds (BO); Hellerman (CF, IM, IS); Henley's (C, CO, IM, W); Insulating Components and Materials, Ltd. (IM); Langley London (IM); Long and Hambley (IM. IS, RP); Magnetic and Electrical Alloys ( $L, M$ ); Marrison and Catherall ( $M, L$ ); Micanite and Insulators (CF, IM. IS); Minnesota Mining (IM); Multard (DC, M); Multicore (S); Murex (RM, M); Mycalex (CF, IM), James Neill (M); Permanoid (C, IM, IS, W); Plessey (CE, DC, M); Reliance Wire (C, CO, IS, W); Rola Celestion (D, L, M); Salford (DC, M): Sankey (L); Geo. L. Scott (L); F. D. Sims (C, CO, W); S.T.C. (M); Steatite (CF. CE); Stratton (CF); Suflex (B, CO, IM, IS, W); Swift Levick (M); H. D. Symons (IM, IS); Taylor Tunnicliff (CE); Telcon (C, DC, IM, L, M, RN, W); Telcon Magnetic (L); Telephone Manufacturing Co. (DC); Thermo Plastics (CF, IM); Transradio (B, C. IS, W); Tufnol (IM); United Insulator (CF, CE, IM); Vactite Wire (RM, W); Whiteley Electrical (CF, M)
*Abbreviations: B, braiding; BO, bolts; C, cables; CE, ceramics. CF, coil formers, bobbins; CO, cords; DC, dust cores, ferrites; IM, insulating materials; IS. insulating sleeving; $L$. core lamina tions and strip; $M$, magnets and magnetic alloys; RM , refractory metals; RP, rubber products; S , solder; W , bare or covered wires.

## Directory of Metals

A COMPREHENSIVE guide to the physical properties of the non-ferrous metal elements and their alloys is contained in the "Metal Industry Handbook and Directory 1955." Not the least useful section of this work is the list of proprietary alloys, their makers, properties and uses.
A separate set of tables gives the specific resistances of alloys which are not normally found in electrical reference books, and there is a large section on the technique of electroplating, anodizing and other electrolytic processes which should be of value to workers in the radio industry.

Published by the Louis Cassier Company, Ltd., Dorset House, Stamford Street, London, S.E.1, this directory costs 15 s .

# Wide Range Electrostatic Loudspeakers 

By P. J. WALKER*

2-Problems of Air Loading : Different Requirements of Moving-coil and Electrostatic Drive Units

IN the first part of this article we showed that it was possible to design and construct electrostatic driving units which were capable of applying a force which virtually acted directly on to the air, and we showed that this force was linear. This state of affairs applied over a bandwidth of several octaves for any single unit, depending upon the efficiency required from that unit, and it was further shown that that bandwidth could be placed anywhere in the audio range.

The only mechanical impedance likely to affect performance is the suspension compliance of the diaphragm, necessary to offset the negative compliance due to electrical attraction. We can therefore begin to draw an electrical analogue circuit of the mechanical elements of the loudspeaker as in Fig. 1, showing the force fed in series with a capacitance. In practice the compliance will considerably exceed the electrical negative compliance, so that this capacitance $\mathrm{C}_{d}$ is almost solely due to the diaphragm compliance.

For simplicity we will restrict consideration to units driven from constant-voltage sources, so that no elements need be included to indicate amplifier source impedance.
Since the loudspeaker will be coupled to the air, we can now add the front air load radiation resistance $\mathrm{R}_{f}$ and the front air load mass, $\mathrm{M}_{f}$ and we can include the impedance $Z$ which represents the impedance presented to the back of the diaphragm.

The impedance Z may include dissipative terms in the form of absorption and/or acoustic radiation resistance. With most acoustic devices the analogy elements change with frequency and the problem, as with all loudspeaker design, is to arrange matters so that the power developed in the radiation resistance(s) is independent of frequency.

The electrostatic unit differs from the moving coil in that there is no large mass component (cone and


Fig. I. Elementary equivalent circuit of mechanical and acoustical parameters of an electrostatic loudspeaker.
speech coil) which normally appears as a large inductance in series with $\mathrm{C}_{d}$. The absence of this inductance profoundly alters the requirements for $Z$, and since $Z$ is the cabinet or back enclosure it is to be expected that the form of cabinet for electrostatic units will follow trends entirely different from those that have been evolved for moving-coil units. A further difference is that the shape of the diaphragm area is more versatile, so that $\mathrm{R}_{f}$ and $\mathrm{M}_{f}$ may be independently varied over reasonable limits.

Due to the absence of large mass we can, if we wish, arrange the constants so that $\mathrm{R}_{f}$ is large compared with the other elements, and therefore becomes the controlling factor for the equivalent current in the circuit, i.e., the velocity of motion of the diaphragm. This means that the impedance looking back into the loudspeaker can be very low. When this is so, any increase in the acoustic resistance on the front of the diaphragm will result in reduced power output. If, on the other hand, the impedance of the loudspeaker is made to appear high by arranging that the total impedance is


Fig. 2. Mass and radiation resistance loads on circular diaphragm in free air. The normalized frequency scale is in terms of the relationship of diaphragm size to wavelength.
large compared with $\mathrm{R}_{f}$ then an increase in acoustic resistance on the front of the diaphragm will result in increased power output. This ability to control the impedance looking back into the diaphragm is a useful feature in designs where $\mathrm{R}_{f}$ is subject to fluctuations due to surroundings, horn reflections, etc., and, in particular, where one loudspeaker unit is influenced by another unit at cross-over frequencies.

In order to show the action of an electrostatic unit which is small compared to the wavelength of the radiated sound it is convenient to commence with a circular shape, because impedance information is readily available for such a shape. Load impedance for other shapes is best obtained by considering the diaphragm as a number of unit areas of equal size and calculating the impedance of each unit area, taking into account the mutual radiation due to the presence of all other unit areas.

Fig. 2 shows the load on a piston operated in an unlimited atmosphere without a baffle. The diaphragm compliance reactance $\mathrm{X}_{c}(\mathrm{E})$ is also drawn. Between $f_{1}$ and $f_{2}$ the controlling factor is the air mass, and the velocity of motion will vary directly with frequency until resonance between $X_{c}(E)$ and $X_{m a}$ is approached. R , however, falls rapidly with frequency, and the power output will fall at approximately 6 db per octave with declining frequency. (Exactly the same would occur with a moving coil unit, control this time being the mass of cone and speech coil designated $\mathrm{X}_{m}(\mathrm{MC}) . \quad \mathrm{X}_{c}(\mathrm{MC})$ is the moving-coil suspension compliance.)

Multiple diaphragms without baffles, having the above characteristics, form the basis of design for loudspeakers to provide the directivity of a doublet. Such a system has useful attributes in relation to the listening rooms, a subject to be dealt with in a later article.

Above $f_{2}$ the velocity of the moving-coil unit would still be controlled by $\mathrm{X}_{m}$ (MC) (except for cone " break-up") and, since the resistance becomes constant, the response will fall with increasing frequency. In the electrostatic case above $f_{2}$ the velocity will be controlled by the air load resistance, and the response will be independent of frequency.

Extending this comparison to units in very large baffles we have the curves of Fig. 3. Here the radiation resistance varies with the square of the frequency below $f_{2}$. With a moving coil the response will be level below $f_{2}$ and will fall with frequency above $f_{2}$. With the electrostatic the response will be level below $f_{2}$ and also level above $f_{2}$, but there will be a step in response so that the output level above $f_{2}$ will be 3 db higher than that below $f_{2}$.

A simple arithmetical example will make clear the reason for this step. With constant force F applied to the diaphragm, the velocity of movement will be F F $\frac{\mathrm{F}}{\sqrt{\mathrm{R}^{2}+\mathrm{X}^{2}}}$
and the power expended usefully in the radiation resistance will be $\mathrm{P}=\left(\frac{\mathrm{F}}{\sqrt{\mathbf{R}^{q}+\mathbf{X}^{2}}}\right)^{2} \times \mathrm{R}$ At $f_{\mathrm{B}}$ in Fig. 3, neglecting Z due to the declining air mass reactance, we have for a constant force $\mathrm{F}=1$, $\mathrm{P}=\frac{\mathrm{R}}{\mathrm{R}^{2}}=\frac{2}{4}=\frac{1}{2}$. At $f_{\mathrm{A}}$, on the other hand, the air mass predominates and, if $R$ can be neglected in calculating the velocity of motion, $\mathrm{P}=\frac{\mathrm{R}}{\mathrm{X}^{2}}=\frac{0.01}{(0.2)^{2}}$


Fig. 3. Mass and radiation resistance curves for a circular diaphragm in a lorge baffle. The power radiated at any frequency $f_{A}$ well below $f_{2}$ is half thot radiated at frequencies $f_{\mathrm{B}}$ well above $\mathrm{f}_{2}$ (see text).
$=\frac{0.01}{0.04}=\frac{1}{4}$, or half the power at $f_{\mathbf{B}}$. A similar relation-
ship will be found for any other pair of values of $R$ and X at points below $f_{2}$.

This change in level can be overcome by deviating from the circular piston shape. For wavelengths large compared to the diaphragm size the resistance per unit area is dependent upon the new area and not upon the shape, whereas the mass is mainly dependent upon the smaller dimension. By elongating the diaphragm shape the output level below $f_{2}$ can be made equal to that above $f_{2}$.

We have so far been considering a comparatively small diaphragm in a flat baffie, the latter being very much larger than the piston, and the size of the complete system is obviously that of the baffle. The reason that the piston has been kept small is purely for the convenience of the moving-coil unit, because its diaphragm is driven at only one point. In the electrostatic case we no longer have this restriction, and it will always be preferable to increase the size of the piston (without increasing the total size of the complete system). This will usually be necessary because there is a limit to the available amplitude of movement, and thus, for a given power output per unit area, we have a minimum limit to the radiation resistance in order that the diaphragm excursions may be attainable. Increasing the size of the piston for a given power output has the double advantage of reducing power requirements per unit area, and, where the loading is below $2 \rho \mathrm{c}$, of increasing the radiation resistance per unit area, and therefore reducing the amplitude required to provide that power output. For reasons of efficiency we shall in any case limit the high-frequency response of the unit so that
optimum design is obtained by increasing the area of the diaphragm to the point where the piston just begins to become directional at the frequency which we have chosen for cross-over (set by the efficiency laid down in the design requirements).

Continuing the consideration of the air load on diaphragms, reference should be made to horn loading. Here we have large resistive and mass components due to the horn. Fig. 4 shows the load of an idealized horn to which has been added $\mathrm{X}_{m}(\mathrm{MC})$, the cone mass of a typical moving-coil loudspeaker which might be used with such a horn. It will be seen that at low frequencies the cone mass is largely swamped by the horn impedance, so that the design of horns for electrostatic units differs very little from the design for moving-coil units. Although we can now have the advantages of a virtually distortionless driving unit, we are still left with the disadvantages of practical horns, which are present independently of the drive units. Horns are normally used to match the high impedance of moving-coil diaphragms to the low impedance of the air. Since we have no such fundamental mismatch with the electrostatic loudspeaker, and since diaphragm shape and size are not fundamentally restricted, we shall not normally have to resort to the use of horns to the same degree. It should be remembered, however, that any back enclosed volume is a direct function of throat area, so that in some applications it is possible to use space for providing a length of horn in exchange for saving in size of capacitive enclosure. Again, we may wish to restrict the front-wave expansion in order to maintain a reasonable resistance per unit area at low frequencies (utilizing the corner of a room, for example).

One of the most desirable diaphragm shapes for electrostatic designs is that of a strip having a length (together with floor or wall image) large compared to $\lambda / 3$ at the lowest frequency of interest, and a width small compared to wavelength at the highest frequency of interest. The strip may be curved along its length if desired, provided the radius of curvature is not less than $\lambda / 3$ at the lowest frequency.

To consider the load on such a strip it is convenient to assume the strip as being infinite in length (legitimate provided it is at least $\lambda / 3$ in length). With such a diaphragm there will be no expansion of sound in the direction of the length since all pressures along the length of the strip will be equal. Expansion from any given element of the diaphragm takes place in one plane only and will therefore take the form $S=S_{0} x$. This is the expansion of a parabolic horn. At low


Fig. 4. Throat air resistance and reactance curves of idealized horn with moving-coil mass reactance superimposed.
frequencies the front air load resistance is falling directly with frequency (instead of $f_{2}$ as with the circular piston shape). The advantages of the strip shape may now be enumerated:-
(a) The air resistance even at low frequencies (since $\mathrm{R} \propto f$ ) is sufficient to develop adequate power with reasonable diaphragm amplitude
(b) The narrow diaphragm gives good dispersion for several octaves (up to the frequency at which width $\approx \lambda / 3$ ).
(c) The narrow diaphragm enables other units to be placed close to it, thus being less than $\ddagger$ wavelength apart at cross-over frequency.
(d) The frequency limitations, amplitude at the low end, and directional problems at the high end, fit in nicely with the 4-5 octave range which we established in Part I of this article for satisfactory efficiency. Thus a strip shape can form one basis of design for our ideal-the perfect loudspeaker.
It will be obvious that a curved front source similar to that illustrated in the photograph of Fig. 5 in Part I of this article will give similar distribution to a strip, and, due to the larger surface, smaller spacing may be used and higher efficiency may thus be achieved. In such a case however, the diaphragm must be large compared to wavelength in both dimensions, because it is the nature of curved surfaces to become directional when the radius of curvature is comparable with the wavelength. When the diaphragm is large compared to $\lambda$ it is impossible to design an intimate acoustic cross-over. This small inherent imperfection would appear to preclude its use in a "perfect" loudspeaker design, although its " efficiency" advantages will have obvious applications in some practical compromise designs.

Although designs free to the air on both sides have useful attributes, it is obviously desirable also to produce loudspeakers in cabinet form, enclosing the rear. This rear enclosure, if it is to be of reasonable size, will be the controlling factor for the diaphragm velocity, at least at low frequencies.

With any unit, the high-frequency limit will be set by efficiency requirements, and the low-frequency limit by amplitude limitation or by the compliance of the enclosure in series with the diaphragm compliance. This compliance will resonate with the air mass on the front and back of the diaphragm (unless the diaphragm is so large that the loading is $\rho c$-for example, as in the curved diaphragms previously mentioned). Since the total mass is small, this resonance will usually occur above the lowest frequency of interest. It may be dealt with in two ways, (1) by adding acoustic mass within the cabinet to reduce the resonant frequency to the lowest required frequency, or (2) critically damping the resonant frequency and maintaining response below this frequency either by re-matching or by a secondary acoustic resonant circuit, or both.

There are innumerable ways in which either of these alternatives may be achieved. Consider the first alternative. Suppose that the enclosure is made deep and narrow (or fitted with partitions so that it appears deep and narrow to the loudspeaker): then, at wavelengths just under four times the depth, the reaction on the diaphragm will be positive. This will effectively force the resonance to the $\frac{1}{4}$ wavelength reasonance of the depth of the enclosure. Absorbent wedges may now be fitted to control the resonance and to present


Fig. 5. Strip loudspeaker, long compared with wavelength, and of width d, mounted in a wall, with the back of the diaphragm loaded by a tube with cross-sectional area equal to that of the diaphragm and of a length 5d, blocked at the far end. Resistance (fibre--glass wedge) included in tube to control impedance.
a purely resistive load at all higher frequencies. Sound compression within the wedges becomes isothermal, decreasing the speed of sound, so that the depth of the enclosure can be reduced accordingly.

Fig. 5 shows the impedances of a strip unit loaded on this principle together with a curve showing the power output radiated as sound for constant applied voltage. The output is extended by more than an octave over that which would be obtained if the same volume of enclosure were allowed to act as a lumped capacitance.

Turning now to the second method of extending the low frequency range, Fig. 6 shows a diaphragm loaded by a capacitance leading through resistance and inductance into a larger capacitance. Both

Fig. 6. Diaphragm loaded by an equivalent capacitance $C_{1}$ leading through an acoustic mass and resistance $M_{2}$ and $R_{2}$ into a larger capacitance $C_{2}$.

volumes have dimensions many times less than the wavelength in the ranges where they are operative.

If the constants are adjusted to give a step in response as the frequency is lowered, then the total volume of the enclosure is reduced accordingly and the response restored to level by re-matching at the step frequency.
Fig. 7 shows a strip diaphragm loaded by a capacitance with series resistance, all elements continuing along the whole length of the structure. With this assumption there will be no waves in the enclosure along its length so that the constants can be calculated on a sectional element of thickness $t$. If the cross section of $\mathrm{C}_{2}$ has dimensions which are many times smaller than the wavelength, then $\mathrm{C}_{2}$ will behave as a capacitance (independent of length). If this proviso is not met then $R_{2}$ must be distributed to avoid $\mathrm{C}_{2}$ appearing as a multi-resonant circuit.

Where the unit crosses over to another unit for low frequencies then $\mathrm{R}_{2}$ may be adjusted to give a Q of 0.7 so that the cross-over components are already present in the acoustic circuit.

When the lower-frequency unit is arranged so that the two diaphragms arc close and intimately coupled, then $R_{1}$ will be increased in value by the mutual radiation of the low-frequency unit. $R_{2}$ is then reduced to restore $Q$ and we find that if $R_{1}$ is larger


Fig. 7. In a long cylindrical structure the air column will be driven equally at all points along its length and no appreciable longitudinal standing waves can be established, at frequencies other than that corresponding to $\lambda / 4$.
than $\mathrm{R}_{\mathbf{2}}$ a useful self-compensating effect takes place.
If the voltage applied to the low-frequency unit is reduced at cross-over due to tolerance in its crossover components then $R_{1}$ is automatically reduced and the output of the higher-frequency unit increases at cross-over. At cross-over $\mathrm{P}_{\text {out }} \propto \frac{\mathrm{R}_{1}}{\left(\mathrm{R}_{1}+\mathrm{R}_{2}\right)^{2}}$

Where the enclosure of Fig. 7 is used for the unit covering the lowest part of the audio range, bass response may be extended by rematching or by introducing a secondary resonant circuit and utilizing back radiation from the diaphragm. If an aperture is provided at one end of the enclosure, opening to the air, then, when the enclosure length is $\frac{1}{4}$ wavelength, resonance will occur along its length, and there will be radiation from the aperture. $3 / 4,5 / 4$ resonances, etc., will not arise, because the enclosure is excited by a force distributed along its length. At frequen-
cies above the $\ddagger$ wavelength, the enclosure will behave approximately as a capacitance, as if the aperture were not present.

The next part of this article will deal with electrostatic units as part of delay lines, and the application of various complete designs, " built in," " boxed in " and "doublet" in relation to the listening-room. Complete electrostatic loudspeakers can take several different forms, each of which in terms of frequency response, distortion and sound dispersion can meet a specification virtually to perfection. When the listen-ing-room and subjective factors are considered it becomes impossible to lay down a rigid specification. To adopt a quotation "Each design is perfect, but some designs are more perfect than others'"!
Acknowledgement. Fig. 2 is based on Fig. 5. 9, p. 127 of "Acoustics" by Leo. L. Beranck (McGraw Hill).
(To be continued)

## LETTEIS TO THE EDITDI

The Editor does not necessarily endorse the opinions expressed by his correspondents

## Situations Vacant

WITH the present state of full employment in the electronic profession, the competition amongst employers to find suitable men is fierce. This is shown by the numerous posts advertised in technical journals. The time has come, however, for employers to pay a little more attention to the "Sits. Vac." replies.

Three members of my laboratory have, over a period of the last six months, written to a dozen advertisers. The results have been very disheartening; only 40 per cent of the applications were acknowledged. The applicants were qualified men: A.M.I.E.E., A.M.Brit.I.R.E., Higher National, National and City and Guilds certificates. In good faith they have taken some trouble to apply for positions, expecting that they would be treated with good manners by the advertiser, and have been embittered by the callous manner in which their applications were treated.

I would ask "Sits. Vac." advertisers to read page 498 of Electronics for March, 1955. and then to make moves at least to treat engineers with the courtesy their professional status deserves.
J. GILBERT.

Biophysics Dept., Postgraduate Medical School of London.

## Transistor Symbols

IT would seem that an over-riding factor when assessing the desirability of a logical system of transistor symbols is whether the advantages of the system are more important than international standardization. It is impossible to ignore the fact that there is a well-established convention at present widely used in both Europe and the U.S.A., and it is, to say the least of it, unlikely that any alternative suggestions at this late stage will replace the accepted practice. I would suggest that it is better to follow the generally accepted convention and concentrate on clearing up minor differences about points such as the thickness of base line and the presence of a circle to isolate the transistor from the rest of the circuit.

Leaving on one side the question of standardization, there is still a doubt whether your suggested symbols (April and May, Editorial Comment) do in fact add to an understanding of the devices. The symbol you suggest is particularly undesirable since it is very misleading to regard a transistor as a back-to-back arrangement of two diodes.
Finally, the point raised about the abbreviation to use in circuit diagrams can be met without causing confusion
by using the same " $V$ " for the crystal valve as for the thermionic version. B. R. BETTRIDGE.

General Electric Company, London, W.C.2.

BOTH D. Nappin and W. E. Thompson (your May issue) regard the transistor as a new device needing a new symbol, but surely this problem arose as the normal valve developed.

It was no doubt thought that gas triodes and neon stabilizers were separate devices, that each needed a new letter symbol, but in fact they are both given the letter $V$, and no confusion is caused by this. The type of device is made clear by the circuit symbol.

I suggest, therefore, that the letter $V$ be kept to include the transistor.

London, N.1.
M. LEVY.

WHILST in fuil agreement with the general scheme of transistor symbols proposed in your April and May Editorials, I should like to plead for the symbol originally shown for the $n-p-n$ junction transistor in Wireless World, July, 1954, p. 325, Fig. 2(c), rather than the new version in Fig. (f) of the May Editorial. This later version is likely to cause error, particularly when pencil sketches are copied in the drawing office or print room. Furthermore, the original version appears more logical and distinct, being characterized by a black and white triangle like the symbol for the $p-n-p$ transistors.
London, N.W. 3 .
FRANCIS OAKES.

## Electronics on the Farm

R. S. DRAKE'S letter (your May issue) is very interesting and certainly very pertinent. Within limits one must admit that a manufacturer should know! However, I beg leave to suggest that there is justification for some comment, if not criticism.

Popularity obviously justifies manufacture and sale, but it does not follow that it confirms excellence of design and practical value. Established habits die hard.

It may be true that there is no serviceable electronic "switch" or "trigger," but I feel that there is no valid objection to a glass-enveloped tube in a fencer unit. These units must in practice be effectively boxed and weather-proofed, and in any case we have electric lights all over the place on farms these days.

I still hope to find an electronic dry battery unit on sale in the not-too-distant future; a unit which is neatly boxed
and requires no servicing beyond the occasional plugging in of a relatively inexpensive replacement. Furthermore, I consider that this unit should carry its own test equipment. I see no reason why this should be very expensive, even if it does have to involve more than a neon tube or a blade of grass, and I think loose test equipment is an anachronism. In theory it enables one to test the fence at any point, but in practice this is an advantage of negligible value. Nine times out of ten one naturally puts the unit at the gate or most convenient point of approach, and again nine times out of ten if the fence is "down" the only effective way of locating the fault is to walk the fence. Finally, more often than not it is easier and more convenient to switch off before one walks so that one can repair in comfort. Of course, one can wear gloves, one can withstand the shock, one can use a handkerchief, kick down a weed or pull off a branch. But how often does one in practice? In practice it is far more desirable to be able to check when there, without having to remember to take the tester, than to be able to test at all sorts of odd points.

No doubt my desired unit would not be cheap, but I fail to see why it should be any more expensive than the average unit now on the market.

Hempstead, Essex.
H. G. TAYLOR.

## "As She Is Spoke"

I HAVE just been reading M. G. Scroggie's letter in your May issue, and I notice that the linoleum in my immediate vicinity is very clean. This must be due to the fact that Mr . Scroggie has been wiping the floor with me.
. . apologise to him for having wrongly deduced from
his previous letter that he objected to the use of the word "recording" as a noun; I now realize that he only objected to its use in reference to a recording.
As Mr. Scroggie now concedes that we can have a recording on a record, I readily agree that there should be no logical objection to using the words "tape record" to refer to a recording on tape. In fact, I notice that this nomenclature has already been adopted by your journal, so that just about clinches the argument.
Wharfedale Wireless Works, Ltd., G. A. BRIGGS. Bradford.

## Earthing Metal Braiding

IN the illustration of the component layout for P. J. Baxandall's pre-amplifier in your February issue, the method shown of making a connection to a metal braid screening is by wrapping a connecting wire round it. This, I know, is a common method, but it involves soldering which may injure the sleeve or insulated wire directly beneath. It also does nothing to remove the jagged ends of the braiding, and I have known them penetrate the insulation beneath and cause a short when the conductor is sharply bent.
Another method, suggested to me long ago, is better on both counts, but does not appear to be widely known. About one inch from the end of the braiding the wires of the "warp" are separated and so are the wires of the "weft." This leaves a diamond shaped hole and the slecve or insulated conductor within the inch of braiding is pulled out through the hole. The braid thus left empty forms a convenient pigtail for connection to the remainder.
London, N.W. 7.
W. J. CLUFF.

## Commercial Literature

Audio Amplifier, the Cape 25, by Cape Electrophonics, mentioned in the March issue. An error of $0.08 \%$ was made in the distortion figure, which should be $0.12 \%$ at $64 \mathrm{c} / \mathrm{s}$ with 26 watts output. At $1,000 \mathrm{c} / \mathrm{s}, 25$ watts output, the distortion is claimed to be $0.03 \%$.

Band-III Aerials, including composite Band-I/Band-III types, add-on units for existing aerials; indoor types and also converters, pre-amplifiers and downleads. Described in a leaflet from Aerialite, Castle Works, Stalybridge, Cheshire. Also a non-technical leaflet explaining aerials and converters for Band III.

Marine Communications Receiver covering long, medium and trawler wavebands with Consol navigational aid. Power supply from $12-\mathrm{V}$ or $24-\mathrm{V}$ ships' battery. General specification in a leaflet (also containing a list of available Consol charts) from Pye Marine, Oulton Works, Lowestoft.

Small Electrolytic Capacitors with paper dielectric construction and very low leakage currents. Capacitances of $0.5-50 \mu \mathrm{~F}$, working voltages of $250-25 \mathrm{~V}$ d.c. and sizes up to 2 in $\times 0.6$ in (diam) approx. Technical bulletin from the Telegraph Condenser Co., North Acton, London, W.3.

Magnetic Permeability Tester for measuring metallurgical uniformity of production samples from foundries, rolling-mills, etc. Brief outline in a leaflet from Excel Sound Services, Celsonic Works, Garfield Avenue, Bradford, 8, Yorks.

Impregnation Plants for impregnation of coils, transformers, ctc., with varnish, resin or other materials under alternate vacuum and pressure. Also available for "potting" work Features described in a leafiet from Blickvac Engineering, $96-100$, Aldersgate Street, London, E.C.1.
Geared-down Motors, fractional horsepower, either serieswound, variable speed, for a.c./d.c. or capacitor-induction, constant speed, for a.c. only. Output speeds ranging from 0.2 r.p.m. to $840 \mathrm{r} . \mathrm{p} . \mathrm{m}$. with torques from 3 lb -in to $75 \mathrm{lb}-\mathrm{in}$. Technical specification from M.R. Supplies, 68, New Oxford Street, London, W.C.1.

High Quality Sound Reproduction equipment including combined amplifier and record-playing units; separate record
players and amplifiers; and loudspeaker units. Leaflets from Pye, P.O. Box 49, Cambridge.

Inexpensive Oscilloscope with circuit for measuring voltage of waveform, or a selected portion of it, on a voltmeter within the range $0.2-500 \mathrm{~V}$. Deflection sensitivity, $1 \mathrm{~cm} / \mathrm{V}$; bandwidth, $3 \mathrm{Mc} / \mathrm{s}$; and time base frequencies, $3 \mathrm{c} / \mathrm{s}$ to $120 \mathrm{kc} / \mathrm{s}$. Leaflet from E.M.I. Electronics, Hayes, Middlesex.

Power Oscillator, giving 120 watts into $10 \Omega$ with frequency range of $10 \mathrm{c} / \mathrm{s}-10 \mathrm{kc} / \mathrm{s}$, for driving vibration generator. Leaflets on this, and also on moving-coil electro-dynamic exciters with peak thrusts from 2 to 300 lb , from Goodmans Industries, Axiom Works, Wembley.

Timer, for hand-setting, driven by synchronous motor. Can be provided with dial for any time range between $0-30$ seconds and $0-7$ days. Normal switching capacity 5 A at 230 V Descriptive leaflet from the Electrical Remote Control Co., East Industrial Estate, Harlow New Town, Essex.

Aluminium Soldering Tool. A steel wire brush in the soldering bit vibrates and cleans the work surface while a pool of molten solder around the bit protects the cleaned area from the air. Illustrated leaflet from Belark Tool \& Stamping Co., 33, Sussex Place, London, W.2.

Nickel Alloys in Valves; applications of the metal in cathodes, grids, anodes, supports, springs, non-magnetic components and glass-to-metal seals described in an illustrated booklet from Henry Wiggin \& Co., Thames House, Millbank, London, S.W.1.
"The Cosmocord Story" is the title of an illustrated booklet describing the development of the firm's work in piezo-electric crystal devices and also some of the present manufacturing techniques. From Cosmocord, 700, Great Cambridge Road, Enfield, Middlesex.
V.H.F. Equipment from Germany. F.M. transmitters; receivers for radio relay systems; dual-receiver equipments; f.m. transmitter aerials; broadband receiving aerials; and test equipment; made by Rohde \& Schwarz. Leaflets from the British agents, Aveley Electric, 44, Tottenham Court Road, London, W.1.

# Physical Society's Exhibition 

NEW ELECTRONIC DEVICES AND TECHNIQUES

This report is followed by surveys of recently introduced valves and allied devices; also of test and measuring gear. These surveys cover exhibits at both the Physical Society's and R.E.C.M.F. shows. Some products appeared at both, so no distinction is made here between the two exhibitions.

## RESEARCII

MANY physical effects have been exploited in the search for the ideal electro-acoustic transducer (loudspeaker) and a new one, demonstrated by D. M. Tombs, of Imperial College, makes use of the fact that a corona discharge between points is accompanied by a wind, generated by the migration of ionized air particles. Under normal conditions the wind is unidirectional, because of the difference in mobility between the negative and positive ions, but by interposing a grid, suitably biased, between the point electrodes the opposing streams can be balanced. If, now, an alternating signal voltage is superimposed on the grid, acoustic radiation is possible and was in fact demonstrated. From the initial asymmetry of air movement one deduces that, in its present state of development, the transfer characteristic would be non-linear-a sort of "ionic Stentorphone"; but at least it opens a new line for investigation in improving what most people agree is the weakest link in the sound reproducing chain. A similar electrical principle is involved in the "corona triode" also shown by Mr. Tombs. Like the transistor it requires no heater current, and it gives a gain of 5 with an a.c. resistance of $500 \mathrm{M} \Omega$ and a mutual conductance of $25 \mu \mathrm{~A} / \mathrm{kV}$.
A photocell amplifier with a simple wide-range a.g.c. system was shown by the Armament Research Establishment. It makes use of the fact that the input resistance of a valve is inversely proportional to the grid current; thus an input potential divider is established with the photocell impedance which automatically reduces the grid voltage due to steady illumination. The a.c. gain is not affected and light modulation does not vary more than $\pm 3 \mathrm{db}$ over a frequency range of $10 \mathrm{c} / \mathrm{s}$ to $10 \mathrm{kc} / \mathrm{s}$ even when the steady background illumination is varied over a range of $1,000: 1$ from, say, 0.0002 lumen to 0.2 lumen.

The basic causes of the residual interference from the gas discharge in fluorescent lamps, and similar phenomena in vacuum filament lamps, are being investigated by Siemens and a demonstration was given showing how the radiation is related to the electrode emission and the filament current. Normal gas-filled filament lamps do not radiate.
Research into the properties of new and existing materials was prominently represented at this exhibition. Wayne Kerr were showing examples of potting resins specially compounded to minimize mechanical and thermal shocks, and the reduction of valve microphony obtained by the use of semi-flexible resins was demonstrated. Butyl rubber as a moulded insulator for high-voltage transformers was shown by B.T.H.

Much interest is being shown in silicon as a semiconductor for diodes on account of its low reverse voltage, which is held to much higher temperatures than in germanium. B.T.H. demonstrated the method of growing crystals and also a method of radioactive analysis to show


Corona wind loudspeaker (D. M. Tombs).
the distribution of residual impurity in the growing crystal.
Development continues in the production and utilization of new ferrites. Plessey were demonstrating a ferrite switch depending on the large change of incremental permeability when the operating point is changed from remanence to saturation, and have also produced a range of nickel ferrites with magnetostrictive properties.
The Faraday magneto-optic effect in which the plane of polarization of electromagnetic waves in a medium is rotated under the influence of a magnetic field is exploited in special ferrites to attenuate or modulate microwaves (Radar Research Establishment), (Plessey). It is also used for current measurement in high-tension power distribution systems, where the use of a current transformer would present difficulties (British Electrical and Allied Industries Research Association).
Ferroelectric behaviour in ceramics formed the subject of a comprehensive exhibit by G. E. C. Research Laboratories, and it was shown that the large change in permittivity at the Curie point could be exploited to generate a fire alarm signal. Dielectric amplifiers based on the hysteresis characteristics of these materials were also demonstrated.

## NON-INDUSTRIAL ELECTRONICS

IMAGE converter tubes are well known for their use as "electronic shutters" in high-speed photography, but hitherto the shortness of exposure has been limited to about $30 \times 10^{-9}$ second by the inability of the electrical circuit to convey pulses of such short duration. Mullard were showing how this exposure can be reduced some ten times to $3 \times 10^{-9}$ second by using r.f. techniques--the pulse being conveyed by a coaxial line to a modified image converter tube with coaxial connections and a ring of resistors providing correct termination of the line. The switching pulse was actually generated by a spark, and it was the light from this spark that was being shuttered, a visual image appearing on the screen of the image converter. By using mirrors to vary the length of the light path from the spark point to the tube photo-cathode (and so altering the arrival time of the spark image relative to the shuttering pulse), it is possible to examine individual stages of
the spark formation-reducing the effective exposure time to as small as $3 \times 10^{-14}$ second.

The scanning and display principle used in the flyingspot microscope (represented at the show by the wellknown Cintel model) is now extending into other fields. One particularly interesting example was a scanning X-ray system shown by the Royal Cancer Hospital. Here, the place of the flying-spot c.r. tube is taken by a special X-ray tube in which an electron beam scans a platinumfoil target about the size of a post-card. The raster of X-rays so produced passes through the thin target and the tube face and after being modulated by the object under examination is picked up by a scintillation detector. The signal pulses from this are then integrated and amplified and used to intensity modulate a display c.r. tube which is being scanned in synchronism with the X-ray tube. Because of the great sensitivity of the scintillation detector the system is claimed to be about 20 times more sensitive than conventional $\mathbf{X}$-ray apparatus.

Another exhibit using the flying-spot principle was an equipment for counting and sizing small particles, demonstrated by Mullard. This works on the same general principle as the Mullard apparatus shown last year, but for sizing purposes the scanning spot is given a secondary deflection, downwards across the particle and back again, at the end of the first line scan. The length of the excursion is then used as a measure of the particle size.

For the actual process of counting and registering pulses the well-known Dekatron was very much in evidence in a large number of instruments. There is now, however, a new type of decade counting tube which is a good deal faster in operation than the glow-discharge transfer method. This is the Mullard E1T, a miniature c.r. tube using electrostatic deflection of the beam into ten different positions, and in a demonstration it was shown counting at a p.r.f. of $100 \mathrm{kc} / \mathrm{s}$. Counting is also the basic operation in digital computors, and in this field the same firm were demonstrating how transistors can be used in place of valves for various functions-with considerable advantage in reliability and heat dissipation.

There were actually no complete digital computors to be seen at the exhibition, but several of the analogue kind. A particularly interesting one, shown by Elliott and using d.c. amplifiers as functional units, is designed so that problems can be set up on a series of detachable panels, each of which plugs into a d.c. amplifier. It is thus possible to remove a problem en bloc and keep it set up whilst leaving the main instrument free for other work. A miniature analogue computor was demonstrated by Saunders-Roe, while Southern Instruments had a correlogram computor with photo-electric line followers to work from continuous line records on film or paper.

## INDUSTRIAL ELECTRONICS

THE measurement and recording of fundamental physical quantities such as displacement, velocity, acceleration, temperature and pressure forms the basis of the application of electronics to industrial processes. Initially, a transducer is required to convert the physical quantity into a voltage or current which can be amplified by valves or magnetic amplifiers. The output from this transducer is generally applied to a self-balancing potentioneter, operated by a servo motor, and the setting of the potentiometer is recorded on a moving chart or may be used to control industrial processes through relays or larger servo motors. Typical of this widely represented branch of the electronic art are the Foster continuous-balance electronic potentiometers, the Cambridge Instrument multi-point electronic recorder and the Boulton and Paul automatic manometer for use in wind tunnels or in any fluid pressure system.

Variation of capacitance forms a sensitive method of measuring distance or displacement and is applied in the prototype of a probe for the exploration of the internal diameter of small bores. It is used in conjunction with the three-terminal bridge shewn last year by Wayne Kerr and can be calibrated to give direct readings of distance at balance.


Pye miniature pH meter.


Fatigue testing of rod specimens by ultrasonic vibration (Mullard).

The thickness of electroplated films can be measured magnetically as in the B.S.A.-Tinsley gauge in which the adhesion of a small magnet is balanced against the tension of a light spring balance; or thermo-electrically as in a method developed by the British Non-ferrous Metals Research Association and shown by Elliott Brothers. A hot probe and a cold probe are applied to the surface of the plating and the thermal e.m.f. generated between the plating and the base material appears between the two probes. A magnetic amplifier is used between the probe output and any suitable indicator, recorder or relay.

Measurement of thickness by ultrasonic methods where only one side of the material is accessible, as in the case of pressure vessels, may be effected in several ways. In the Dawe Instruments "Visigauge" standing-wave resonance in the thickness of the plate increases the power absorbed from the driving oscillator and this change is displayed as a "pip" on the vertical scale of a cathode-ray tube. The horizontal scale is a function of frequency, which is swept cyclically through an appropriate range, and can be calibrated to read thickness directly. In the Kelvin-Hughes depth and thickness accessory for their standard ultrasonic flaw detector, a short pulse is applied simultaneously to the plating under test and to a liquid delay line of adjustable length. Both return pulses are displayed on a c.r. tube, and, when adjusted to coincidence, the depth can be read off directly. The instrument is calibrated for mild steel and has a range of $\frac{1}{4}$ in to 4 in . By a technique, in which an electrical step function is applied to a thick barium titanate disc with heavy mechanical damping to give a stress with a sharply defined leading edge, the Ultrasonoscope Company (London) have succeeded in resolving echoes in stecl and aluminium for thicknesses down to 0.02 in .


Elliott analogue computor.

Magnetically-controlled top for automatic titration (Pye).
Applications of ultrasonics for the non-destructive testing of materials were shown by the National Coal Board (elastic properties of coal) and by A. E. Cawkell (for checking the compressive strength of concrete in fabricated building units). A spectacular demonstration of the time that can be saved in fatigue testing of metals was given by Mullard. Short rod specimens, welded to a tapered mechanical transformer element were excited with ultrasonic power of the order of kilowatts at a frequency equivalent to the haIf-wave longitudinal resonance of the bar. Under these conditions velocities are a maximum at each end, and compressional and tensile stresses at the middle. Strain is measured by capacitance probe near the free end. To show the magnitude of the forces which could be applied, specimen bars were raised to incandescence in the centre in a matter of seconds. Normally, of course, the specimen would be water-cooled.

Continuous monitoring of thickness of sheet materials during manufacture by the absorption of beta rays (electrons) from a radioactive source has long passed the development stage, and ruggedly housed units suitable for use under factory and mill conditions are made by a number of firms. Typical of this trend is the Type 150 beta gauge made by Isotope Developments. In the Ekco thickness gauge, provision is made for automatic overall standardization every 30 minutes with servo correction for amplifier sensitivity and source decay or contamination. The thickness at predetermined points across the width can be sampled at intervals, the duration of which can be pre-set by the operator. To meet the needs of the paper industry Baldwin Instruments have produced an accessory to their "Automat" beta ray thickness gauge designed to measure the weight per unit area, and thus the "height" or "profile" of the paper surface, across its whole width.


Isotope Developments Type 150 beto ray thickness gauge.


Southern Instruments correlogram computor.


Mullard high-speed photography apparatus.


A continuous record is obtained on a pen recorder. As an alternative to electron penetration, the back-scatter due to gamma radiation is now coming into use for the measurement of thickness. In a prototype instrument shown by Ekco Electronics, cobalt 60 is used as the radiation source and a differential circuit is used to separate the reflected photons from the primary radiation. The detecting photomultiplier tube is associated with a circuit time constant long enough to remove random fluctuations from the indicator. Baldwin Instruments also showed a prototype back-scatter thickness gauge designed to measure metal sheet thickness where only one side is presented, and a transmission gamma-ray thickness gauge for revealing non-uniformity due to variations of ingot temperature in hot steel rolling mills.

In chemical analysis increasing use is being made of electronic methods. The measurement of hydrogen ion concentration ( pH ) is already well established and the
trend is towards miniaturization, as exemplified in the Pye Type 11084 instrument.

In the estimation of acids and alkalies by titration, the end point is usually indicated by a pH meter and in the Pye Type 11600 instrument the out-of-balance signal from the pH meter is used to control a magnetic stop valve with fast and slow rates of dispensation of the neutralizing reagent. The end point may be pre-set to any value within $\pm 0.1 \mathrm{pH}$ and the changeover from fast to slow dispensation can be set to come into operation up to 5 pH units before the end point.

A different method of titration with many interesting features is employed in the automatic titrimeter shown by Electronic Instruments. Instead of using calibrated acio or alkaline solutions of known concentration, the starting point is a neutral salt of indeterminate strength. A current is passed through the salt solution in a cell with semipermeable ends and acid or alkali is liberated at the electrodes, depending on the direction of the current. The current is integrated by a low inertia motor and counter unit of the type designed by Electro Methods and gives a direct measure of the amount of reagent generated and used for the titration ( 1 gram equivalent ion is equivalent to 96,494 coulombs). The process is stopped automatically when the predetermined end point is reached on the pH meter.

Rapid analysis of the constituent elements of solutions is possible by a method known as polarography, in which a progressively rising e.m.f is applied to a mercury dropping electrode. Current flows in well defined steps in which the starting e.m.f. is related to the identity of the conducting ion and the height of the step to its concentration. In the Tinsley recording polarograph the first derivative $d i / d v$ of the current-voltage relationship is displayed, which gives better resolution, and a square-wave method developed by Barker and Jenkins, of A.E.R.E., and utilized in the Mervyn Instruments polarograph gives greater latitude in dealing with constituents of widely different concentration.

## MISCELLANEOUS EXIIIBITS

A MAGNETIC reactor, having various applications involving frequency shift of an oscillator by means of an externally applied audio or d.c. voltage has been developed


Plessey magnetic ferrite reactor
by Plessey. A fruitful field of usefulness is for frequency modulating v.h.f. oscillators and transmitters and for automatic frequency control of a v.h.f. oscillator.

The reactor consists of a small ferrite former with a few turns of wire wound toroidally on it and forming part of the tuned circuit of the oscillator it is required to control, or frequency-modulate as the case may be. The toroidal coil is mounted in an electromagnet system in such a way that by applying either a d.c. or an a.c. voltage to the electromagnet winding the incremental permeability of the ferrite core, and hence the inductance of the toroidal winding, can be varied. An inductance change of the order of 10 per cent is attainable. The unit shown by Plessey is designed for use at frequencies of from 50 to $100 \mathrm{Mc} / \mathrm{s}$.
Some really lilliputian input and output audio transformers were exhibited by Fortiphone. The company has, of course, had a wide experience in the manufacture of very small parts for hearing aids. The transformers shown were mainly for transistor circuits and were in ratios of between 2 and 10 to 1 and either encapsulated in potting resin or open. The smallest measures $\frac{5}{4}$ in $\times \frac{3}{8}$ in $\times$ $\frac{3}{3}$ in, while the largest of the miniatures is only $\frac{3}{3}$ in $\times \frac{3}{4}$ in $\times$ sin. Primary inductances (with no d.c. flowing) of 30 H or so are achievable with some of these tiny transformers.

Recent improvements in the precision-type silveredmica capacitors made by Johnson, Matthey consist of using thinner mica and a larger silvered area than hitherto and thus providing more pFs per unit area.

# TEST AND MEASURENG GEAR 

Apparatus Shown at the R.E.C.M.F. and Physical Society's Exhibitions

MANY of the instruments to be mentioned were shown in prototype or pre-production form, and are therefore subject to modification before they become available, if they do. Likewise many of those which were available for the first time had been previously reported in Wireless World so are not mentioned again unless the modifications were substantial.

After a period during which the design of unamplified meters had seemed almost to have reached finality, signs of renewed activity were to be seen in a considerable number of new models. The demand by the Services for hermetical sealing has been met by several makers. The well-known Avometers 7 and 8 now have counterparts in Araldite "D" tropical dress as 7X and 8X The trend towards wide-angle deflection continues. British Physical Laboratories showed sub-panel-mounted meters to accord with contemporary styling, and Everett Edgcumbe a new system of scale lighting distributed by a Perspex surround. Pullin now have two multi-range d.c./a.c. test meters of the Amp-Volt-Ohm type, one with a 1 mA movement and the other $50 \mu \mathrm{~A}$, for which a special 20 -way multi-bank switch was developed; there is also a miniature d.c./a.c. 19 -range set. The same firm showed a moving-coil voltmeter mounted in a probe for
measuring television e.h.t. up to 25 kV ; full-scale current, $40 \mu \mathrm{~A}$. An ingenious device enables the whole of the scale to be used for either positive or negative voltages without reversing connections. To the Pye series of "Scalamp" high-sensitivity instruments has been added a voltmeter taking a full-scale current of $1 \mu \mathrm{~A}$ (i.e., $1 \mathrm{M} \Omega$ per volt, for those who prefer to put it in that roundabout way). The lowest range is 10 mV f.s.

Another conception of rugged sensitivity is the Doran portable combined pointer and reflecting galvanometer, obtainable with various full-scale readings; examples are $\pm 0.12 \mathrm{mV}$ ( $10-\Omega$ coil) and $\pm 1.5 \mu \mathrm{~A}$. Among new frequency meters are those by Pullin and Electrical Instrument $C o$.; the latter also showed differential a.c. meters in which two opposing rectifiers are connected to a centre-zero movement, obtainable with f.s.r. from $\pm 50 \mu \mathrm{~A}$ upwards.

The valves in valve voltmeters have hitherto been of the vacuum type, but this year a sign of the times is the British Physical Laboratories" "Transranger" multirange voltmeter and megohmmeter in which an instrument outwardly uniform with their test meters having a movement requiring $25 \mu \mathrm{~A}$ for f.s.d. nevertheless is fully deflected by $1 \mu \mathrm{~A}$, the gain being provided by an internal


Pullin e.h.t. probe voltmeter.


Combined pointer and reflecting galvo made by Doran Instruments.

transistor amplifier. Changes due to temperature coefficient are neutralized by initial setting-up procedure. Voltage is measurable from 0.001 to 500 , and resistance from 0.001 to $100 \mathrm{M} \Omega$. A new Avo multi-range d.c. voltmeter also takes $1 \mu \mathrm{~A}$ f.s., but uses conventional valves. So does the Marconi Instruments TF 1041 on its d.c. ranges, which extend up to $1,000 \mathrm{~V}$; but for a.c. measurements use is made of a probe containing a rectifier valve of the coaxial type, by means of which the frequency range is maintained level within 1 db up to $700 \mathrm{Mc} / \mathrm{s}$. Resistance is measurable from $0.2 \Omega$ to $500 \mathrm{M} \Omega$. This instrument is in production. So is the latest version of the Pye d.c. microvoltmeter, in which a galvanometer moving coil is made to set up an a.c. signal which is amplified and rectified. A somewhat similar means of stepping-up sensitivity is used in a new Pye instrument, called a "Nanoammeter" because on its most sensitive range the f.s. reading is $10 \times 10^{-9} \mathrm{~A}$.
A considerable number of new or improved oscilloscopes were shown, including several each by Cossor, Nagard and Solartron. Most if not all of these use post-deflection accelerator tubes to give adequate traces at the very high speeds which now are expected of even general-purpose instruments. Along with this goes wide bandwidth in the deflection amplificr; for example, $5 \mathrm{c} / \mathrm{s}$ to $10 \mathrm{Mc} / \mathrm{s}$ in the "Solascope" CD514, notwithstanding that this is a relatively inexpensive model. A new Cossor model (1056) covers from $5 \mathrm{kc} / \mathrm{s}$ up to no less than $80 \mathrm{Mc} / \mathrm{s}$. The E.M.I. Type WM5 includes the valuable feature of meter-read voltage and time along the X and Y axes of the trace, together with the ability to put a television picture on the screen and select any part of any line of it by means of a marker and then switch over to normal waveform examination of the selected part. A cathode-follower probe unit with interchangeable attenuator heads enables the wide frequency band to be maintained up to the point of application. E.M.I. distributed amplifiers, suitable for oscilloscopes, handle a bandwidth of over $100 \mathrm{Mc} / \mathrm{s}$; to the carlier high-level Type 2C has now been added a low-level type that can be cascaded with it to give an overall gain of $\times 300$.

It is interesting to compare methods of providing more than one trace. Cossor continue to use their single-gun split beam, with improved non-interaction, in their new Model 1059. Nagard and Southern Instruments use the 20th Century Electronics multi-gun tubes, of which advantage is taken in Southern's M972 of the ability to make one of the traces a horizontally expanded version of the other. In the Mullard L101 the two traces result from electronic to-and-fro switching of a single beam during each flyback. Lastly, Cintel provide any number of traces by means of separate c.r. tube units, which can be assembled like bricks. Incidentally, the Nagard "Unitel" system imparts similar flexibility to the oscilloscope as a whole.

A number of new attenuators were to be seen. The Advance A63 turret model for frequencies from zero to $1,000 \mathrm{Mc} / \mathrm{s}$ provides 10 db steps from $0-50 \mathrm{db}$ using resistance arms. It is of $75-\mathrm{ohm}$ coaxial construction, and the operations of withdrawing both end connections axially, bringing a new attenuator pad into line, and closing up the contacts, are all performed by a continuous rotational movement of the control knob. Separate 75 -ohm encapsulated attenuator pads for use up to
E.M.I. cathode follower probe with some of the interchangeable heads available.
$300 \mathrm{Mc} / \mathrm{s}$ were shown by British Physical Laboratories. Coming to microwaves, an assembly was shown by Wayne Kerr for calibrating S-band attenuators from a piston attenuator at $80 \mathrm{Mc} / \mathrm{s}$ to within $0.015-0.02 \mathrm{db}$. Elliott demonstrated absolute calibration of X-band attenuators by a process of adding together two signal outputs previously adjusted to equality, thereby giving a 6.02 db step, from which further steps can be determined. The B443 continuously-variable X-band attenuator shown by the same firm is a beautiful piece of instrument making. It is calibrated direct in db , standing-wave ratio and voltage reflection coefficient, and of the total range up to 100 db that up to 40 db is of high precision.

In the field of bridge work a most imposing exhibit


Elliott precision " $\times$ " -band attenuator.


Encalsulated attenuator unit, FA200, made by British Physical Laboratories.


Top view of turret attenuator made by Advance components.
was the Smith bridge on the Tinsley stand, for the measurement of thermometer resistors to within 4 in $10^{8}$. Notable features are the massive switchgear and the elaborate precautions to ensure constancy of the manganin resistance standards, such as the method of spirally winding a helix of the annealed wire between Perspex discs, and the devices for maintaining constant and uniform temperature. A modern version of the Kelvin double bridge for low resistances was shown by the Cambridge Instrument Co. For use with the r.f. capacitance bridge by Electronic Tubes for the measurement of interelectrode capacitances can now be obtained a series of jigs to Anglo-American Service standards, each for a particular type of valve holder. Doran showed a new universal a.c./d.c. bridge and a bridge amplifierindicator; Griffin and George a "Nivoc" unit system from which bridges can be assembled; and Salford Instruments an incremental-inductance bridge of the Owen type, with c.r.t. balance indicator. In the Muirhead D728 equipment the impedance and phase angle of twoterminal networks between 0.3 and $100 \mathrm{k} \Omega$ are measured at 50 and $10^{3} / 2 \pi \mathrm{c} / \mathrm{s}$ by comparison with resistance in a balanced amplifier circuit. The same firm showed an instrument for comparing the voltage and phase of two sinusoidal signals. Comparison is also the basis of an instrument by the Electrical Instrument Co. for measuring and grading components. Its standard is normally their push-button decade capacitor (also shown), and a useful feature of the comparator is a sensitivity switch by which the meter can be made direct-reading in percentage deviation of the component under test. The display mechanism in the Wayne Kerr CR and LR bridges, by which mistakes in reading are rendered almost impossible, appears in improved form in the production versions of those instruments.
The same admirable attention to operational convenience is found in the new decade oscillator of the same make, in which the frequency from $10 \mathrm{c} / \mathrm{s}$ to $110 \mathrm{kc} / \mathrm{s}$ is directly shown. The decade principle for oscillators has been used by Muirhead for some years, and the latest example is their D695, considerably smaller than previous models but with a high performance. Where spot frequencies ( $5 \mathrm{c} / \mathrm{s}$ to $50 \mathrm{kc} / \mathrm{s}$ ) and output voltages ( 5 mV to 20 V ) will do, the Cawkell OSP31 oscillator gives 0.1 per cent frequency calibration at a low price-and there is a 1-per cent model at a lower price. The beat-frequency principle is used in the Furzehill $50 \mathrm{c} / \mathrm{s}$ to $20 \mathrm{kc} / \mathrm{s}$ oscillator, a feature of which is a $\pm 50 \mathrm{c} / \mathrm{s}$ incremental control. For the exceptionally low frequency range $0.03-30 \mathrm{c} / \mathrm{s}$ Airmec use a rotating capacitor to modulate a h.f. signal which is rectified and amplified to yield the output.
Most of the new oscillators and signal generators for the higher frequencies have been inspired by developments in television and f.m. broadcasting. The Advance range has been supplemented by Type R1, covering the whole v.f. $30 \mathrm{c} / \mathrm{s}$ to $3 \mathrm{Mc} / \mathrm{s}$ in one range, and $3-10 \mathrm{Mc} / \mathrm{s}$ in
another, using a RC type of oscillator. Bands I, II and III and the relevant i.f.s are included in a low-priced sweep oscillator by Taylor, in which $5-250 \mathrm{Mc} / \mathrm{s}$ is covered in one beat-frequency range; wobbulation is by reactance valve. The Cossor "Telecheck" Model 1323 also covers all three bands and their i.f.s in a more elaborate specification that includes a crystal oscillator to provide accurate frequency marker pips on the trace. Owners of the earlier Model 1322, which is similar except for the absence of Band II, may be interested in Model 1324, which is an alignment generator specifically for testing f.m. receivers, and includes a display of the discriminator characteristic. The Avo Type TFM a.m. and f.m. signal generator, shown in prototype last year, has not yet reached finality, but is expected to cover $5-255 \mathrm{Mc} / \mathrm{s}$ with an a.m. signal and $80-100 \mathrm{Mc} / \mathrm{s}$ with f.m. The frequency scale is direct reading and fitted with a device for correcting it by known frequencies. At the laboratory level, Marconi Instruments have recently introduced the TF1077 f.m. signal generator covering $19.7-102.5 \mathrm{Mc} / \mathrm{s}$. A piston attenuator is used, and frequency modulation is by varying the permeability of a ferrite core on which the r.f. inductor is wound. A new M.I. a.m. signal generator is the TF801B, covering the unusually wide frequency range of $10-500 \mathrm{Mc} / \mathrm{s}$. Range changing is by contactless switch, and the r.f. valves are of the disc-seal type. For still higher frequencies ( L band, $960-1,250 \mathrm{Mc} / \mathrm{s}$ ) there is now the TF1078, with a piston attenuator having a range up to 110 dbm . Yet another new generator of the same make is the OA1000, for the increasingly important $Q$ band $(33,300-37,500 \mathrm{Mc} / \mathrm{s})$. The oscillator is, of course, a klystron, its frequency being stabilized by a variety of the Pound system. A feature of the latest version of the Airmec general-purpose $30 \mathrm{kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ signal generator is a horizontal direct-reading illuminated frequency scale 4 ft long on every range.

With applications in such fields as television, radar, communications and nucleonics, the need for pulse generators is growing, and new types were shown by Solartron, British Physical Laboratories and E.M.I., with pulse width adjustable down to a few millimicro-seconds. The Mullard L141 generator produces pulses in pairs separated by an interval variable from $1 \mu \mathrm{sec}$ to 0.1 sec , B.P.L. also exhibited a pulse-height voltmeter, independent of pulse width and repetition rate above 700 p p.s. For amplified testing Solartron have a square-wave generator (GO511) with rise and fall times as low as 40 and $25 \mu \mathrm{sec}$ respectively on the highest frequency range. An entirely different kind of special waveform is produced by the Dawe " white noise" generator Type 419, in which a thyratron in a magnetic field generates a noise output uniform from $20 \mathrm{c} / \mathrm{s}$ to $5 \mathrm{Mc} / \mathrm{s}$, reducible to $500 \mathrm{kc} / \mathrm{s}$ or $20 \mathrm{kc} / \mathrm{s}$ for testing apparatus over narrower frequency bands. For taking frequency characteristics, etc., such a generator simulates transient signals such as speech more closely than does c.w., and acoustic standing waves are avoided.



Capacitance Bridge Type B22l made by Wayne Kerr.

Left: Cossor Model 1324 F.M. alignment signal generator with probe and capacitance coupling.


Type OAI, 000 " Q "'-band signal generator made by Marconi instruments. Interior view.


Airmec rack-mounted frequency measuring equipment with electronic counter.
voltmeter, and crystal calibrator. The instrument covers $8-70$ and $168-230 \mathrm{Mc} / \mathrm{s}$, is safe when used with a.c./d.c. scts, and for such a comprehensive equipment is inexpensive. The same maker exhibited an electronic counter rack with very clear direct-reading illuminated display of the number of cycles, suitable for quick and accurate frequency measurement.

## VALVES INI <br> SEMI-CONDUCTOIRS

THE most unusual valve be seen this year was undoubtedly the backward-wave oscillator or "carcinotron" shown by Mullard. It is similar in form to the ordinary travelling-wave tube but the r.f. field energy travels in the opposite direction to the electron beam flow. A characteristic feature is the very wide tuning range, which is obtained simply by varying the electron beam accelerating potential (see graph). The collector potential is 200 V and the beam current 25 mA , while the power output is 50 mW at $11,000 \mathrm{Mc} / \mathrm{s}$ or 120 mW at 18,000 $\mathrm{Mc} / \mathrm{s}$.

In conventional travelling-wave tubes there were two new types shown by English Electric, the N1001 and N1002. Operating as amplifiers, they both have a gain of 25 db over the frequency range $1750-2300 \mathrm{Mc} / \mathrm{s}$, the N1001 giving an output of 20 W and the N1002 an output of 1 mW . Another microwave valve using velocity modulation of the electron beam is the klystron, and on view was a new Ferranti type with the high output power of 500 watts at $9,400-9,700 \mathrm{Mc} / \mathrm{s}$. The cathode of this valve is designed to give a very heavy beam current and the power dissipation of the collector, which has to be watercooled, is 4 kW .

Of particular interest amongst the receiving-type valves on show was the Osram KT55 beam tetrode. This is intended for use as an audio amplifier in a.c./d.c. circuits (the heater rating is $0.3 \mathrm{~A}, 52 \mathrm{~V}$ ) and two of the valves connected as pentodes in push-pull will give an output of 25 watts from a mains supply of 220 volts. In this pentode condition the KT55 has the high mutual conductance of $16 \mathrm{~mA} / \mathrm{V}$. Another new audio valve for large output powers was the Mullard EL.34. It is notable for its

$500-\mathrm{Mc} / \mathrm{s}$ sine wave recorded on 20th Century oscilloscope tube S6A20-3.
high maximum anode voltage of 800 V , which permits operation in push-pull circuits with output powers up to 100 watts (at 5 per cent distortion). Both the KT55 and the EL34 are on the octal base.

High power and high mutual conductance were also the outstanding features of the new Ediswan beam tetrode 13E1, a d.c. control valve intended for use in stabilized power supplies or servo control systems. The slope is actually $40 \mathrm{~mA} / \mathrm{V}$, while the maximum anode dissipation is 90 watts.

Cold cathode triodes, or trigger tubes, for use in clectronic switching circuits are still very popular because they are reliable, long-lived and need no heater supplies. Osram were showing one, the CCT6, which can be uscd in circuits having wide component tolerances, while the Mullard Z803U is notable for the stability of its trigger characteristics.

New entrants into the transistor field are Pye Industrial Electronics, who have come out with a complete range of germanium junction $p-n-p$ types, hermetically sealed, for audio and i.f. applications. Under the series type number of V10, they have collector voltages of 10 V and various input and output resistances. A similar range of junction $p-n-p$ types have been produced by G.E.C. It comprises the EW53 and EW59, which are intended for power applications and will operate at frequencies up to a few hundred kilocycles, and the EW58, designed for low-power, low-frequency amplifiers such as in hearing-aids. Yet another series of junction transistors which may be already well known are the TJ1, TJ2 and TJ3, shown by Brimar and S.T.C.

A junction transistor using silicon is the next thing to be expected, but in the meantime we have a range of silicon junction diodes, types ZS10A, B and C, produced by Ferranti. These are characterized by their extremely low reverse current of less than $10 \mu \mathrm{~A}$ for a reverse voltage of -50 V and by their ability to operate at temperatures as high as $100^{\circ} \mathrm{C}$. Forward currents are 0.1 A continuous and 1 A peak. A developmental silicon junction diode was also shown by S.T.C.


English Electric trovelling-wove tubes NIOOI and N1OO2


Ferronti 500-watt klystron.

Germanium junction diodes are still being deveioped, however, and one interesting example was the G.E.C. type EW54, intended for power rectification. Fitted with cooling fins it will give a rectified output of $50 \mathrm{~V}, 24 \mathrm{~A}$, and good regulation is obtained because of its low forward resistance of 0.05 ohm . For h.t. power supplies based on relaxation-oscillator generators, Mullard were demonstrating a power transistor used with germanium junction rectifiers to produce a d.c. output of 150 V at 5 watts from a 12 -volt supply. The photo-electric properties of the germanium junction were also represented, by the S.T.C. miniature germanium photocell type P40A, which is so small that six of them can be arranged in a row across standard teleprinter tape for "reading" the punched holes.

Amongst conventional plate rectifiers the most interesting development was a range of new Westinghouse types with aluminium cases which are bolted flat to the chassis to conduct the heat away. This enables the size of the rectifier to be reduced for a given power rating. A similar reduction in size is given by elements each capable of handling 27 volts in the tubular selenium rectifiers shown by Salford.
Oscilloscope c.r. tubes were well represented, and an outstanding one for high "writing" speeds was the 20 th Century S6A20-3, which has three post-deflection accelerator electrodes and is capable of recording a $500-\mathrm{Mc} / \mathrm{s}$ sine wave with a time-base speed of 650 cm per microsecond. Mullard were showing two new 3 -inch tubes, DG7-32 and -36, the first-mentioned being notable for its low final anode voltage of 500 V .

G.E.C. germanium junction diode EW54 (right) and EW5I point contact transistor (left).

Left: Ediswan beam tetrode $13 E 1$.

# 20-Watt Highh-0uality Amplifier 

## 2.-Constructional Details and Performance

By W. A. FERGUSON,*<br>B.Sc.(Eng.), A.C.G.I., Grad. I.E.E.

N the first part of this article some considerations were discussed which affect the choice of valves and circuit arrangements in the output stages of amplifiers designed for use in high-quality sound reproduction.

In amplifiers designed to handle power outputs greater than 12 to 15 watts and in which low-distortion operation towards peak power output is still required, the use of distributed load operation with valves of the 25 -watt anode dissipation class is of particular interest. By using this method of valve loading the effective power output of a low-distortion triode push-pull stage (approximately 12 watts) can be raised to 30 to 35 watts whilst the benefits of low inherent distortion and relatively low output impedance are well maintained. Performance typical of the Mullard EL34 output pentode with partial screen-grid loading was illustrated in Fig. 3 of the previous article.

The present article describes a design for a highquality amplifier of 20 watts rated output in which similar load conditions are used for the EL 34 valves in the output stage. The amplifier is intended to allow of the highest standard of sound reproduction when used in association with suitable pre-amplifier circuits, high-grade pickups and loudspeaker systems.

TABLE I
Summary of Performance of Prototype Amplifier
Power output:
20 watts minimum from $30 \mathrm{c} / \mathrm{s}-20 \mathrm{kc} / \mathrm{s}$.

## Power response:

within 0.5 db of $1 \mathrm{kc} / \mathrm{s}$ level at 20 watts over range $30 \mathrm{c} / \mathrm{s}-20 \mathrm{kc} / \mathrm{s}$.
Frequency response ( 1 watt level):
within 1 db of $1 \mathrm{kc} / \mathrm{s}$ level $2 \mathrm{c} / \mathrm{s}-100 \mathrm{kc} / \mathrm{s}$.
Harmonic distortion ( $400 \mathrm{c} / \mathrm{s}$ ):
$<0.05 \%$ at 20 watts.
Intermodulation distortion ( $40 \mathrm{c} / \mathrm{s}, 10 \mathrm{kc} / \mathrm{s}$; ratio 4:1):
$0.7 \%$, with peak corresponding to 20 W sinewave power.
$1.0 \%$, with peak corresponding to 29 W sinewave power.
Hum and noise:
-89 db relative to 20 W with $10-\mathrm{k} \Omega$ source resistance.

## Sensitivity:

220 mv for 20 W output.

## Phase shift:

$10^{\circ}$ maximum at $10 \mathrm{c} / \mathrm{s}$.
$20^{\circ}$ maximum at $20 \mathrm{kc} / \mathrm{s}$.
Output impedance:
approximately $0.3 \Omega$ at $40 \mathrm{c} / \mathrm{s}, 1 \mathrm{kc} / \mathrm{s}$ and 20 $\mathrm{kc} / \mathrm{s}$ at 20 watts output.


General view of top of prototype 20 -watt amplifier, which uses EL34 output valves.

A summary of the overall performance of the amplifier is given in Table 1.

A circuit diagram and list of component values is given in Fig. 1. The circuit arrangement is basically similar, except for the output stage, to that used in the Mullard 5 -valve 10 -watt high-quality amplifier design in that the output stage is driven from a cathode-coupled twin-triode phase-splitting amplifier which is in turn preceded by a high-gain voltage amplifier stage. The first stage in the amplifier is d.c. coupled to the phase splitter in order to minimize low-frequency phase shifts. The main feedback loop includes the whole circuit, the feedback voltage being derived from the secondary of the output transformer and injected in the cathode circuit of the first stage.

Output Stage.-The main feature of interest in the output stage is the use of the Mullard EL34 highslope output pentode with partial screen-grid loading, the screen grids being fed from taps on the primary of the output transformer. Measurements during the course of design showed that optimum conditions are obtained in this form of output stage when about $40 \%$ of the primary winding of the output transformer is common to anode and screen grid circuits. In the present design a C-core transformer is used which has tappings at $43 \%$ of primary turns. $\dagger$

The anode-to-anode loading of the output stage is 6.6 kQ and, with a feed voltage of 440 at the centretap of the output transformer primary the combined anode and screen-grid dissipation of the output valves is 28 watts per valve. With the particular screengrid to anode load ratio used, it has been found that improved linearity is obtained at power levels above 15 watts when resistors of the order of $1,000 \Omega$ are inserted in the screen-grid feeds. The slight reduction

[^2]in peak power-handling capacity which results is not significant in practice. Separate cathode-bias resistors are used to limit the out-of-balance d.c. current in the output transformer primary; the use of further d.c. balancing arrangements in the output stage has not been considered necessary. It is likely, however, that some improvement in performance, particularly at low frequencies, would result from the use of d.c. balancing. It is necessary in this type of output stage that the cathodes are by.. passed to earth even when a common cathode resistor is used. Thus a low-frequency time-constant in the cathode circuit cannot be eliminated when automatic bias is used.

Power Supply.--The power supply is conventional and uses a Mullard GZ32 indirectly heated full-wave rectifier in conjunction with a capacitor input filter. Paper smoothing capacitors have been used in the prototype amplifier, though the alternative use of electrolytic capacitors is possible. The value of the limiting resistors $\mathrm{R}_{23}$ and $\mathrm{R}_{24}$ will depend on the winding resistances of the mains transformers used. Their purpose, when required, is normally one of voltage control only. Where a transformer having very low winding resistance is used, a secondary
voltage rated at 400-0-400 may be found adequate.
The rating of the mains transformer is such that an additional 30 mA may be drawn from the h.t. supply to feed pre-amplifier circuits and radio feeder. Additional decoupling will be required for these supplies.

Driver Stage.-This stage uses a Mullard ECC 83 twin-triode and fulfils the combined function of phase splitter and driver amplifier. It is of the cathode-coupled form and enables a high degree of push-pull balance to be obtained. With the high line voltage available the required drive voltage for the output stage is obtained at a low distortion level, which is approximately $0.4 \%$ for 20 watts power output. The anode load resistors $R_{11}$ and $R_{12}$ must be matched within $5 \%, \mathrm{R}_{12}$ having the higher value for optimum operation. Optimum balance is obtained when the effective anode loads differ by $3 \%$. It is necessary also that the grid resistors $R_{13}$ and $R_{14}$ in the output stage are of small tolerance since they form part of the anode loads of the driver stage. High-frequency balance will be largely determined by wiring layout since equality of shunt capacitances is required. Low-frequency balance is controlled by the value of the time constant $\mathrm{R}_{8} \mathrm{C}_{5}$ in the grid circuits


## LIST OF COMPONENT VALUES

| $\mathrm{R}_{1}$ | $1 \mathrm{M} \Omega \ddagger$ watt | $\pm 20 \%$ |
| :---: | :---: | :---: |
| $\mathrm{R}_{1}$ | $4.7 \mathrm{k} \Omega+$ watt | $\pm 20 \%$ |
| $\mathrm{R}_{3}$ | $2.2 \mathrm{k} \Omega^{\star}$ | $\pm 10 \%$ |
| $\mathrm{R}_{4}$ | $100 \Omega^{\star}$ | $\pm 5 \%$ |
| $\mathrm{R}_{5}$ | $4.7 \mathrm{k} \Omega \frac{1}{4}$ watt | $\pm 10 \%$ |
| $\mathrm{R}_{6}$ | $100 \mathrm{k} \Omega^{\star}$ | $\pm 10 \%$ |
| $\mathrm{R}_{7}$ | $390 \mathrm{k} \Omega^{\text {* }}$ | $\pm 10 \%$ |
| $\mathrm{R}_{8}$ | 1.0 M \& watt | $\pm 20 \%$ |
| $\mathrm{R}_{9}$ | $82 \mathrm{k} \Omega \frac{1}{2}$ watt | $\pm 10 \%$ |
| $\mathrm{R}_{10}$ | $270 \mathrm{k} \Omega \frac{1}{2}$ watt | $\pm 10 \%$ |
|  | $180 \mathrm{k} \Omega \dagger \frac{1}{2}$ watt | $\pm 10 \%$ |
|  | $180 \mathrm{k} \Omega \dagger \frac{1}{2}$ watt | $\pm 10 \%$ |
|  |  | $\pm 10 \%$ |
| $\mathrm{R}_{14}$ | $470 \mathrm{k} \Omega \ddagger \ddagger$ watt | $\pm 10 \%$ |
| $\mathrm{R}_{15}$ | $8.2 \mathrm{k} \Omega^{*}$ ( $15-\Omega$ | oad) $\pm 5 \%$ |
| $\mathrm{R}_{16}$ | $2.2 \mathrm{k} \Omega \frac{1}{4}$ watt | $\pm 20 \%$ |
| $\mathrm{R}_{17}$ | $470 \Omega 3 \mathrm{~W}$ min | $\pm 5 \%$ |


$\mathrm{C}_{9} \quad 8 \mu \mathrm{~F} 450 \mathrm{~V}$ wkg.
$\mathrm{C}_{10} 50 \mu \mathrm{~F} \quad 50 \mathrm{~V}$ wkg.
$\mathrm{C}_{11} 50 \mu \mathrm{~F} \quad 50 \mathrm{~V}$ wkg.
$\mathrm{C}_{12} \quad 8 \mu \mathrm{~F} 500 \mathrm{~V}$ wkg.
$\mathrm{C}_{13} \quad 8 \mu \mathrm{~F} 500 \mathrm{~V}$ wkg.
$\mathrm{L}_{1} 10 \mathrm{H}, 180 \mathrm{~mA}, 200 \Omega$
$\mathrm{T}_{1}$ Power transformer
Secondary 410-0-410V, 180 mA ; $5 \mathrm{~V}, 3 \mathrm{~A} ; 6.3 \mathrm{~V}, 4 \mathrm{~A}$ centretapped; 6.3 V 2.5 A centretapped.
$\mathrm{T}_{2}$ Partridge Type P3878
$\mathrm{V}_{1}$ Mullard EF86
$\mathrm{V}_{\mathrm{g}}$ Mullard ECC83
$\mathrm{V}_{3}, \mathrm{~V}_{4}$ Mullard EL34
$V_{5}$ Mullard GZ32

* High-stability carbon.
$\dagger$ Matched within 5\%. $\quad \mathrm{R}_{12}>\mathrm{R}_{11}$.
$\ddagger$ Preferably matched within 5\%.
and this value has been chosen to ensure adequate balance down to very low frequencies. A disadvantage of the cathode-coupled form of phase splitter is that the effective voltage gain is about one-half of that obtained from one section used as a normal voltage amplifier. Due to the high $\mu$ of the ECC83 (100) the effective stage gain in the circuit is still about 25 times.

First Stage.-This stage is a high-gain pentode voltage amplifier using the Mullard EF86 low-hum pentode. The stage gain is approximately 120. High-stability cracked-carbon resistors are used in anode, screen-grid and cathode circuits and give appreciable improvement in measured background noise level as compared with ordinary carbon resistors. This stage is d.c. coupled to the input grid of the phase splitter in order to minimize low-frequency phase shift in the amplifier and improve low-frequency stability when feedback is applied.

Negative Feedback.-The sensitivity of the amplifier without feedback is 6.5 mV for 20 watts output. With feedback approximately 220 mV is required for the same output level, the designed overall loop gain being 30 db . The loop gain, overall frequency response and phase shift characteristics of the complete amplifier are shown in Fig. 2.

In spite of the high degree of negative feedback used in the present design an adequate margin of stability has been achieved. Complete stability is maintained under open-circuit conditions in the prototype amplifier. An increase in feedback of at least 10 db , obtained by reducing the value of $\mathrm{R}_{1,5}$ should be possible before signs of high-frequency instability occur. In the form of design used oscillation with capacitive loads is the form of instability most likely to occur, but even with very long loudspeaker leads, instability is unlikely to arise.

Distortion.-The harmonic distortion of the prototype amplifier at $400 \mathrm{c} / \mathrm{s}$, measured without feedback under resistive load conditions, is shown in Fig. 3. The distortion curve towards the overload point is also shown for feedback conditions. At the 20 watt level the distortion level without feedback is well below $1 \%$ and with feedback applied falls to below $0.05 \%$. Harmonic distortion at $400 \mathrm{c} / \mathrm{s}$ reaches $0.1 \%$ at approximately 27 watts output. The loop gain characteristics are such that at least 20 db feedback is maintained from $15 \mathrm{c} / \mathrm{s}$ to $25 \mathrm{kc} / \mathrm{s}$ and 26 db down to $30 \mathrm{c} / \mathrm{s}$.

Measurement of intermodulation products has been made, using a carrier frequency of $10 \mathrm{kc} / \mathrm{s}$, and a


Fig. 2. Loop gain and frequency response and phase shift characteristics with feedback.


Fig. 3. Harmonic distortion and input/output characteristics of prototype amplifier.
modulating frequency of $40 \mathrm{c} / \mathrm{s}$, with a ratio of $40-\mathrm{c} / \mathrm{s}$ to $10-\mathrm{kc} / \mathrm{s}$ amplitudes of $4: 1$. With the combined peak amplitude of the mixed output at a level corresponding to the peak sine wave amplitude at 20 watts r.m.s. power, intermodulation products expressed in r.m.s. terms totalled $0.7 \%$ of the $10 \mathrm{kc} / \mathrm{s}$ carrier amplitude, and at 29 watts approximately $1 \%$.

The output/input characteristic shown in Fig 3 shows that excellent linearity is obtained up to 20 volts across $15 \Omega$, corresponding to 27 watts output.

Sensitivity.-The sensitivity of the amplifier is approximately 220 mV for 20 watts output and 300 mV at the overload point at mid frequencies. The background level in the prototype amplifier was 89 db below 20 watts, measured with a source resistance of $10 \mathrm{k} \Omega$. This is equivalent to about $5.5 \mu \mathrm{~V}$ at the input terminals. It is possible to increase the overall sensitivity of the amplifier by 6 db whilst still maintaining a low background level, high loop gain and a high margin of stability. However, considerations involved in the design of suitable pre-amplifier circuits, in particular the necd for adequate signal-tonoise ratio, render a higher sensitivity of doubtful advantage.

Power Response.-It is important that adequate power-handling capacity is available at the lowfrequency end of the audible range. This is determined chiefly by the characteristics of the output


Fig. 4. Layout of principal components in prototype amplifier.
transformer employed, and it is desirable that associated pre-amplifier circuits should attenuate the very low frequencies which the amplifier is incapable of handling at rated power output without excessive distortion. With the output transformer at present employed at least 20 -watts capacity is available down to $30 \mathrm{c} / \mathrm{s}$, and the frequency response at the 20 -watt level is linear from $30 \mathrm{c} / \mathrm{s}$ to $20 \mathrm{kc} / \mathrm{s}$.

Output Impedance.-Due to the low inherent output impedance of the output stage, combined with a high degree of negative feedback, the output imped-
ance is very low, measuring approx. $0.3 \Omega 2$ on a $15-\Omega$ termination for 20 watts output at $40 \mathrm{c} / \mathrm{s}, 1 \mathrm{kc} / \mathrm{s}$ and $20 \mathrm{kc} / \mathrm{s}$. This corresponds to a damping factor of approximately 50 .

Phase Shift and Transient Response.-In practice a compromise must be effected between the phase shift of the amplifier, particularly at high frequencies, and the margin of stability required with a given loop gain. In the present design emphasis has been laid on ensuring as high a margin of stability as possible. The phase shift is held to a comparatively low level in the audible frequency range and, as seen from Fig. 2, reaches about $20^{\circ}$ at $20 \mathrm{kc} / \mathrm{s}$. Excellent response to signals of a transient nature is obtained, and the rise time of the amplifier is of the order of $5 \mu \mathrm{sec}$.

Mechanical Construction.-A diagram of the layout of the chief components as used in the prototype amplifier is shown in Fig. 4. Although this differs extensively from the layout used in the original experimental circuit no difficulty due to instability has been encountered in either arrangement. A busbar earth return has been used with chassis connection at the input socket. With minor exceptions all resistors and capacitors are mounted on group terminal boards, shown dotted on the diagram.


Underside of chassis showing one possible grouping of the smaller components.

# Wobbulator Adaptor for Band III 

Attachment to Existing Band-I Swept Frequency Oscillators

By G. H. LEONARD, B.Sc. (Hons.) Lond. *

THE introduction of new television channels in Band III has posed many problems for development and manufacturing organizations, not the least of which has been the problem of production test equipment. At the time that the production of Band I/Band III receivers was first contemplated by the author's firm, the few types of test gear for Band III which were then available were not considered suitable for mass production work. The most pressing need was for a swept frequency generator or wobbulator for the alignment of tuner units, and the equipment about to be described was built to fulfil this requirement.

The design of equipment for internal use by a manufacturing organization is inevitably governed to some extent by "domestic" considerations. In this case the fact that substantial numbers of commercial Band-I


Fig. 1. Frequency sweep of the Band-1 wobbulator is shown ot $A$, while its $2 n d$, 3 rd and 4 th harmonics are at $B, C$, and 0 respectively.
wobbulators (Samwell \& Hutton Type 41) were already in use for Band I alignment led to consideration being given to the provision of an adaptor to provide r.f. in Band III, the rate of frequency sweep being so arranged that the existing display facilities could be utilized. A further consideration was the company's policy of manufacturing tuners initially for Channels 8 and 9 only, provision being made for interchangeable coils to adapt the tuner for any channel when required. This gave some latitude in the initial specification of the equipment, in that, although the basic system needed to be suitable for any channel, equipment could initially be made with some limitation in performance other than on the two specified channels.

With these requirements in mind, consideration was given to the possibility of a heterodyne adaptor being designed to provide a Band-III output, using the Band -I output of the existing wobbulators in conjunction with a local oscillator. Examination of this proposal showed that each $10-\mathrm{Mc} / \mathrm{s}$ sweep available on Band I had at least one, and in many cases, two, harmonic sweeps covering such a large proportion of Band III that the output from such a heterodyne device would be likely to contain unwanted frequencies over at least a portion of the sweep. In practice this could lead to
errors in alignment which would not necessarily be predictable, a drawback sufficiently serious to rule out further consideration of heterodyne methods. Examination of the harmonic problem, however, drew attention to a further method which was eventually adopted.

One of the sweep ranges on the Band-I wobbulators was $60-70 \mathrm{Mc} / \mathrm{s}$ and it was noticed that the third harmonic of this sweep, $180-210 \mathrm{Mc} / \mathrm{s}$, covered Channels 8 to 11 with a sufficiently large margin to allow for the skirt bandwidth of Band-III tuners. Tripling this output of the wobbulator would therefore cover four channels in one sweep, and the desired channel could be selected by adjustment of the sweep and shift controls of the wobbulator display. A simple prototype showed that the system was workable. Consideration was then given, in consultation with the makers of the wobbulators, to the final design of an instrument capable of covering the whole of Band III.
The frequency sweep obtained from the instrument must ideally cover the whole of Band III plus a considerable margin to allow for the examination of the skirts of a response curve. This calls for a very wide sweep and a compromise has been necessary so that the sweep covered is sufficient to allow some examination of the skirts of Channels 6 and 13 while at the same time excluding unwanted harmonics. The frequency relationships are shown in Fig. 1, the wobbulator coverage being suitably modified.

Using a sweep of 171 to $219 \mathrm{Mc} / \mathrm{s}$, there is a margin


Fig. 2. Block diagram of the adaptor.
of $5.25 \mathrm{Mc} / \mathrm{s}$ below Channel 6 sound and $3.25 \mathrm{Mc} / \mathrm{s}$ above Channel 13 vision; adjacent harmonics do not fall within the band but are, however, still too close for comfort and special measures are needed to eliminate them.

Within the desired band the output of the instrument is held flat within close limits. At first sight this does not appear necessary; from the alignment point of view a slope of up to 1 db over any one channel might well be tolerable but this would mean that a consider-

[^3]able difference in basic level could exist between, for example, the two end channels, which would then place any comparison of sensitivities in doubt. The flat response, which is achieved by means of an a.g.c. system, enables sensitivity measurements to be made anywhere in the band with some confidence.

Frequency markers are obtained by beating the Band-I input with crystal-controlled oscillators. The use of the input for this purpose enables a conventional form of oscillator to be used, and it is only necessary to select a crystal frequency sufficiently high to ensure that only one harmonic occurs in or near the Band-I sweep.

A block schematic of the adaptor is given in Fig. 2 and the complete theoretical circuit in Fig. 3. V1, V2 and V3 form a stagger-tuned amplifier for the band $57-73 \mathrm{Mc} / \mathrm{s}$, gain control being obtained by cathode biasing of V1 by the "SET R.F." control. The output from V3 is sufficient to severely overdrive the grid of the tripler valve V4. The strong third harmonic component present at the anode is selected by a tuned circuit consisting of the variable inductance $L$, and the stray circuit capacitance, the frequency setting being in the region of $195 \mathrm{Mc} / \mathrm{s}$. The Band-III r.f. so developed is amplified by V5, V6 and V7, all of which are EF95 pentodes, having characteristics which render them particularly suitable for use at this frequency. $L_{i}$, the anode coil of V7, is tapped down to give a low impedance feed at approximately 75 ohms to the attenuator and also to the 2 nd and 4 th harmonic rejection filters containing $L_{16}, L_{1 ;}$ and $L_{18}$. The

Band-III amplifier is only partially stagger-tuned, the response being arranged to peak somewhat below the centre of the passband in order to increase the discrimination against 4th harmonic. This unwanted component is most likely to be developed during the "low" end of the Band-I sweep (input frequencies about $57-58 \mathrm{Mc} / \mathrm{s}$ ) when the 4 th harmonic falls very close to the desired band. Tuning is so arranged that at this end of the band the Band-III amplifier has a response between $171-174 \mathrm{Mc} / \mathrm{s}$ which is considerably above the response between $228-232 \mathrm{Mc} / \mathrm{s}$. Since the highest second harmonic is $25 \mathrm{Mc} / \mathrm{s}$ below the desired band, this slight bias to the low frequencies has little or no effect upon the second harmonic content and the peak in the amplifier gain is well within the range of the a.g.c. system.

The Band-I wobbulator frequency sweep is generated by an oscillator whose output frequency is continually swept by a motor-operated variable capacitor revolving at $1,500 \mathrm{r} . \mathrm{p} . \mathrm{m}$. In consequence, any variation of gain with frequency in the system has the effect of modulating the r.f. output voltage with a waveform whose repetition rate is $25 \mathrm{c} / \mathrm{s}$. This modulation is detected by the upper crystal diode CG12E, so connected that an increase in output gives a positive signal. The resulting $25-\mathrm{c} / \mathrm{s}$ waveform is fed to the grid of the high-gain audio stage V8 where it is amplified by over 100 times and reversed in phase. The output from the anode of V8 is fed in the form of an a.c. bias to the "earthy" end of $L_{9}$, the grid coil of $V_{1}$; thus any increase in output appearing at the

Fig. 3. Complete circuit diagram of the adaptor. Lead-through i,000-pF capacitors are used for decoupling the valve heaters. All resistors not marked with wattages are small $\frac{1}{8}$-watt types. Coil-winding data is given in the separate table.


CG12E will cause a large increase in bias at the grid of V1, with a consequent reduction in gain to cancel the rise in output. The system is very effective and allows considerable latitude in the tuning of the BandIII amplifier; it is therefore possible to arrange the response so that unwanted harmonics are minimized.

The time constants of the a.g.c. system are chosen as a result of practical experi-


Fig. 4. Circuit of the attenuotor used in the output of the adaptor. ence. When the attenuator is switched from one position to another a momentary change in impedance occurs when the wiper is between contacts, giving rise to a large momentary change in output. If the time constants in the circuits of V 8 and Vl are too long this causes a damped, very low frequency oscillation of output level which may be observed as a variation in response curve amplitude or as a fluctuation of the carrier meter reading. It has been found possible to make the system "dead beat" by a suitable choice of time constants.

The marker system, which was developed in close co-operation with the wobbulator manufacturers, operates in the following manner. V9 and V1l are crystal-controlled oscillators, the screen grid circuit in both cases being tuned to the fundamental and the anode circuit to the 4th harmonic of the crystal frequency. The two frequencies so developed are $\frac{1}{3}$ of the sound and vision carrier frequencies of Channel

9. V12 is a crystal-controlled oscillator operating on $1.666 \mathrm{Mc} / \mathrm{s}$ (which is $\frac{1}{3}$ of the spacing between two sound or vision carriers) and produces a substantial harmonic content. The outputs of the three oscillators are mixed at the grid of V10, producing frequencies at $\frac{1}{3}$ of each of the following:-
(1) Channel 9 vision frequency.
(2) Channel 9 sound frequency.
(3) Other vision carrier frequencies (by mixing $\frac{1}{3}$ Channel 9 vision frequency with $1.666 \mathrm{Mc} / \mathrm{s}$ and its harmonics).
(4) Other sound carrier frequencies (by a similar process).
The $57-73 \mathrm{Mc} / \mathrm{s}$ sweep is injected at the suppressor of V10 and a heterodyne beat is produced as the wobbulator sweep passes through each of the above frequencies, the higher frequency components of these beats being by-passed and the lower frequency components being amplified by V13 and fed to one Y plate of the wobbulator display tube. The beats appear on the trace as quite narrow markers, the amplitude of which may be controlled by the potentiometer in the grid circuit of V13.

The four-position switch is arranged to break the h.t. supply to any one oscillator, permitting four marker arrangements to be made available. These are: -
(1) Channel 9 sound and vision only (V12 not oscillating).
(2) All sound markers (V1l not oscillating).
(3) All vision markers (V9 not oscillating).
(4) All sound and vision markers (all oscillators functioning).
This marker system does not lend itself to the im-

## COIL DATA

L1: 5 turns 28 s.w.g. enamel covered wire on L3: $\int \frac{3}{32}$-in former, permeability tuned.

L4: 2k turns
L5: $1 \frac{1}{2}$ turns
22 s.w.g. tinned copper wire on
L6: $2 \frac{1}{2}$ turns ${ }_{3}^{9} 2$-in former, brass-slug tuned.
L7: $6 \frac{1}{2}$ turns
L8: 2 turns
L9: 6 turns
28 s.w.g. enamel covered wire on


L12: 33 turns 28 s.w.g. enamel covered wire on L14: ${ }^{9} \frac{9}{32}$-in former, permeability tuned.
$3 \frac{1}{2}$ turns 22 s.w.g. tinned copper wire on
 diameter.
$\int 5 \frac{1}{2}$ turns 18 s.w.g. tinned copper wire on
L17: $\left\{\begin{array}{l}\text { ", air" former } \frac{3}{4} \text {-in long and } \frac{5}{8}-\text { in internal } \\ \text { diameter. }\end{array}\right.$

L18: $4 \frac{1}{2}$ turns 18 s.w.g. tinned copper wire on "air" former $\frac{{ }^{\frac{9}{2}}}{3}$-in long and $\frac{1}{2}$-in internal diameter.
mediate identification of channels other than Channel 9 , but this has been simplified by bringing the wobbulator X shift and sweep control circuits out to a number of preset potentiometers. These are selected by a channel selector switch so that any desired portion of the sweep is presented at the centre of the display, over-riding vernier controls being provided for fine adjustment. The circuit of this section is not shown since it is associated with the wobbulator rather than with the adaptor.

An alternative marker system has been investigated with which no such ambiguity arises. This employs two oscillators, one operating on the desired channel sound frequency and the other on $1.166 \mathrm{Mc} / \mathrm{s}$, i.e., $\frac{1}{3}$ of the sound-to-vision separation. This system gives the sound marker, vision marker, a spurious marker corresponding to sound frequency minus $3.5 \mathrm{Mc} / \mathrm{s}$ or, by switching off the $1.166-\mathrm{Mc} / \mathrm{s}$ oscillator, the sound marker only. This system possesses the disadvantages that separate crystals are required for each channel and that each must be switched on channel selection. As the preset shift and sweep settings are desirable for mass-production use, the advantages of the second system were not considered to be worth while in view of the extra complication involved.

During development certain facts relating to the attenuator system came to light. It became evident that a constant-input-impedance network was desirable in order to avoid changes in the tuning of $\mathrm{L}_{\text {; }}$; which might affect performance, while other design


Fig. 5. Keying system used in examining response of the adaptor.


Fig. 6. System for blacking out alternate half-cycles of wobbulator display time-base, showing relationships of waveforms to frequency sweep.
considerations demanded a minimum possible insertion loss and ease of mechanical construction. The final attenuator design chosen was built in three Advance Components A37 attenuator cases, the circuit shown in Fig. 4 being employed.

Considering the $20-\mathrm{db}$ section, it will be observed that, provided the output is terminated in 75 ohms, the input impedance is constant at 68 ohms for any switch position and the resistor values are such as to produce the desired attenuation. A resistor is in series with the input so that the impedance into which the $5-\mathrm{db}$ step attenuator works is also 75 ohms. This, and the $1-\mathrm{db}$ section, have circuits of a similar type. The output impedance of the attenuator is not 75 ohms but this is not important theoretically, since if the output cable is properly terminated no reflections should occur. In practice no undesirable effects have been noticed but a $3-\mathrm{db}$ pad has, however, been incorporated in order to reduce the effects of variations of termination on the attenuation. When measurements are made working into a 75 -ohm input circuit, and damping of the circuit by 75 ohms is desired, the use of an external $6-\mathrm{db}$ pad is recommended.

Because of the small values used in the $1-\mathrm{db}$ section and the physical limitations imposed by the Advance Components casting, high-stability resistors cannot be used and, in any case, theoretical considerations suggest that a simple resistive rod should possess better r.f. characteristics than the spiral of highstability types. The resistors employed were made from ordinary $\frac{1}{4}$-watt resistors by removing the ceramic cases, scraping the rods to the required value and enclosing them in protective plastic sleeves. The lower values of $\frac{1}{4}$-watt resistor frequently have a metal band sprayed on to the rod to obtain the desired value. The presence of this band increases the capacitance between the end caps of the resistor, so for the range where these bands were known to exist a lower value was chosen and the band scraped off. The use of this type of resistor is, of course, theoretically questionable in the matter of stability, but in practice no important errors have yet been observed.

The initial alignment of the Band-I and Band-III amplifiers is carried out using a signal generator. For final adjustments, and in order to establish that the a.g.c. circuit is operating satisfactorily, it is necessary to check the instrument under normal operating conditions with the swept frequency input from the wobbulator. This can, of course, be effected by connecting a detector to the output socket and displaying any variations in the detector voltage on the wobbulator cathode-ray tube. However, this method has the disadvantage that since the wobbulator Y amplifier is a.c. coupled no indication of amplitude is obtained. Although the latter parameter is indicated by the carrier meter, it has been found inconvenient to observe both meter and tube while adjustments are taking place; furthermore, it is desirable that variations in amplitude through the band should be easily observed in relation to the r.f. output level. Since a detector connected to the output produces a d.c. voltage proportional to the mean output level, with superimposed a.c. corresponding to any variations, the desired display is achieved by the use of a piece of ancillary equipment to "chop up" or "key" the detector output as shown in Fig. 5, so that an alternating voltage whose amplitude varies with the total output is produced. The


Fig. 7. Circuit diagram of keying unit used in Fig. 5.
wobbulator display employs a $50-\mathrm{c} / \mathrm{s}$ sinusoidal time base, with alternate half-cycles blacked out, which is related to the frequency sweep as shown in Fig. 6. The keying device is operated at $25 \mathrm{c} / \mathrm{s}$ so that the display shows a zero-volts base line in addition to the response of the adaptor.

The keying unit employs a beam-switch type of circuit (Fig. 7) using two pentode valves with a common anode load. The keying waveform shown in Fig. 6 (derived from a mains-synchronized $25-\mathrm{c} / \mathrm{s}$ multivibrator) is applied to the two suppressors in antiphase so that when one valve conducts the other is cut off. One valve has its grid returned to earth and the other is d.c. connected to the detector, a variable biasing arrangement allowing the currents through the valves to be made identical under
no-signal conditions. When r.f. is applied to the detector the resulting d.c. alters the bias of one valve so that the currents are no longer equal and a $25-\mathrm{c} / \mathrm{s}$ waveform appears at the anodes. This is fed to the wobbulator $Y$ amplifier and, since the time base operates at $50 \mathrm{c} / \mathrm{s}$, produces two traces on the screen, a zero-volts base line and the response of the adaptor. The separation of the two traces indicates the amplitude of the adaptor's output.

The keying unit is used not only to examine the response of the adaptor but also to check the output level against a standard signal generator. For this test the adaptor output is set to give a definite separation between the traces; it is then disconnected and replaced by the signal generator, whose output is adjusted to give the same separation. This method is used to calibrate the carrier meter on the adaptor.

The adaptor is built so that it may be conveniently linked with the wobbulator to provide a compact Band I/Band III unit, the adaptor forming a pedestal on which the wobbulator stands with its display tube at eye level. The unit has a light alloy angle frame, the circuits being built up on flat plates which are screwed in. This arrangement facilitates assembly and provides a rigid pedestal for the wobbulator. The Band-III amplifier is completely screened and this screening is bonded to the rear of the attenuator in order to avoid earth currents. Lead-through capacitors, used for decoupling h.t. and heater lines, form convenient anchoring points and all "hot" leads are kept as short as possible. The channel selector switch and preset controls are mounted along one side, the edge of the switch knob being engraved so that the switch position is easily seen.

Finally, the author would like to acknowledge the parts played by M. Phillips, who was responsible for the original conception and basic design of the instrument, and A. H. Jacob, who carried out the practical work.

## Hadar Meight Finder

SHOWN in the illustration is the latest Marconi Type S13 long-range radar height finder which, it is understood, will be installed at London Airport by the Ministry of Transport and Civil Aviation. It operates in the $10-\mathrm{cm}$ waveband and provides a peak pulse power output of about 500 kW and has a working range of about 150 nautical miles. An accuracy of $\pm 500 \mathrm{ft}$ at 50 nautical miles is claimed.
The aerial system, which is designed to transmit a very narrow beam of radar pulses only 1 degree in the vertical and 4.5 degrees in the horizontal planes respectively, consists of a slotted waveguide positioned along the focal line of a vertical paraboloid reflector. It is made to oscillate in the vertical plane at about 10 times a minute and scans an angle of between $-1^{\circ}$ and $+25^{\circ}$ to the horizontal. Horizontal rotation of the aerial is effected as required by remote control when an aircraft has been located on the plan position display of any available search radar. It can also be rotated continuously at about 10 r.p.m. if required.

In the form shown the transmitter and receiver are housed in the concrete building with the aerial mounted on its roof, but a separate gantry can be used for the aerial where existing buildings for the equipment are available.

The photograph shows the Marconi rador height finder, Type SI3, with the oerial system mounted on the building housing the transmitter and receiver.


# Some Problems in Television 

## Lighting

By W. C. PAFFORID, a.c.g.I., D..I.C.

VIEWERS sometimes complain that the lighting in television appears to vary from one camera to another. This apparently elementary matter is difficult to explain without first briefly outlining the principles involved in lighting for this new medium.
The subject itself is complex, involving not only physical optics and illumination, but also photographic principles and artistic appreciation. Not least among these is the study of the human eye and reaction to tonal quality and balance. Broadly, there are two distinct basic functions of lighting for television.
First, it must create the right artistic effect for any given production so that the mood of drama or comedy is effectively conveyed to the viewer; for example, "drama" is usually portrayed in "low-key" lighting with heavy shadows and contrast, whereas "comedy" is assisted by "high-key" lighting which creates a lighter mood with less contrast and brighter atmosphere. But this aspect of lighting obviously requires special study and may be regarded as beyond the scope of this particular article.
Secondly, television cameras need a certain basic light level and a suitable disposition of lamps in order to obtain pictures which are technically acceptable. In theory it is possible to estimate the total lighting required by any given scene by referring to the illumination-efficiency curves (Fig. 1) of the lamps to be used. In practice, however, the assessment of the kilowatts of lighting required to give a predetermined level of incident light is largely a matter of experience. The pre-war Standard Emitron camera for instance



PhOTOCATHODE ILlumination

Above: Fig. 1. Typical curves showing the spread of light for a $2-\mathrm{kW}$ lens spot.

Left : Fig. 2. Signal-light curve of image-orthicon camera tube.
was comparatively insensitive and required a scene brightness of $200-300$ foot-candles. The more recent C.P.S. Emitron tube now used in the studios needs less than half this amount of incident light. The latest image-orthicon cameras, used on outside broadcasts, are so sensitive that intelligible pictures can be obtained with as little as 1 foot-candle of incident light.
Although acceptable pictures are obtained with a basic light of about 10 foot-candles, in practice it is found that an incident light value of $25-30$ footcandles allows an image-orthicon camera to use a lens stop of $f / 8$, which gives maximum optical efficiency and also a good depth of focus. It also helps in the

| Type of <br> Camera | Incident <br> foot- <br> candles | Permis- <br> sible <br> Contrast | Average <br> Lens Stop <br> f/number |
| :--- | :---: | :---: | :---: |
|  | Standard Emitron | $200-300$ | $50 / 1$ |
| C.P.S. Emitron | $100-130$ | $30 / 1$ | 6.0 |
| Image-Orthicon | $25-30$ | $20 / 1$ | 8 |

operation of the tube, which for best results should be made to work on the linear part of the signal-light curve (see Fig. 2).

If the illumination on the photocathode is too low we not only run into low signal-noise ratios, but also the detail in the darker parts of the picture is crushed into the blacks. On the other hand, if the level is too high there is a tendency to flatten out the highlights and run into instability. Having established the correct basic illumination, it is now necessary to consider the disposition of the various sources of light.
"Hard light," derived from a lens spotlight or other focus source is suitable for use as a key light, and "soft light" which consists of floods is used for filler and general softening of hard shadows. Additional "sparkle" can be added to the picture by using the film-studio technique of introducing "back light." The diagram in Fig. 3 shows an elementary lighting plot using a single camera at A. In this case the lighting engineer has a fairly straightforward job to do, and by adjusting these three lamps a wellbalanced portrait can be obtained.

But if we now introduce a second camera at B, then clearly it will not be looking at a very well-balanced portrait, as the key light is now acting as a threequarter back light. To put this right it is necessary to re-balance the light sources while with three cameras a further compromise is necessary until the light balance has been restored as seen from each camera position.
It will be appreciated, therefore, that when in addition to this, the subject is, say, a crowded stage in a

Fig. 3. Three-point lighting intended for a camera ot $A$ is not right for a second camera at B.


Fig. 4. General arrangement of cameras for, say, a theatre.
colour or, say, a well-balanced composition made up of areas of blue-green and orange-red, which to the eye would be completely satisfying. But when translated into a monochrome picture by a panchromatic camera, the tonal composition will probably be something very different. Generally, the background needs a good a.c. light component or, in other words, a well broken-up design. Supposing, for the sake of argument, we use a chess-board type of background then, in long shot, we shall get good results. But, unfortunately, as soon as we move into a close-up, there is the danger of one camera seeing a portrait against a dark background, and the other camera getting the same portrait lit against a light background, which is usually disastrous.

A good practical example of this sometimes occurs in ice shows where the lens catches a large proportion of reflected light off the ice, leaving the figures sadly silhouetted against an unbroken white background.
A further contributory cause of unbalance, especially on faces, could be due to a mismatch in a colour response of the tubes in question, particularly if fluorescent lighting is present.
Another reason why pictures from different cameras do not always appear to match up can be demonstrated by the case of televising a boxing match with
theatre, and possibly the available lighting positions in the auditorium or circle are restricted, then it becomes difficult to get a good balance on all three cameras. A good deal of ingenuity is called for and the lighting engineer may have to decide which camera is likely to take most of the important close-ups on principal actors, for instance. The more general shots may have to take second place. Another problem, of course, is that the best camera positions, particularly in a theatre, are not always the easiest from a lighting angle.

Fig. 4 shows a typical camera set up for an outside broadcast from a West End theatre, where two cameras (non-tracking) use zoom lenses for close-up work and usually cut across the stage into the opposite corner of the stage set. A third camera is sometimes used in the auditorium or circle to give wide-angle shots. The main problem is to get sufficient light for the close-up work and at the same time to keep a balance so that rapid switching from one camera to another is not accompanied by an apparent change in light level. In this respect the colour and design of the background become very important.

For example, the background in a stage setting may well depend for its harmony on a delicate choice of



Fig. 5. In a boxing match the lighting is constant, but a wide-angle view gives a higher average brightness than a narrow angle, with the result that the waveforms differ as shown.
two cameras in the same position. In these circumstances there can be no question of different camera angles or of unbalanced lighting because boxing matches are always lit with a perfectly symmetrical overhead rig which remains static. The problem of lighting has now become one of "picture content." This is shown in Fig. 5 where camera 1 may be using a wide-angle lens giving a picture which is largely composed of white. If the adjacent camera is using a close-up lens then the picture content is predominantly black and contrasty. Clearly, a rapid series of cuts from camera 1 to camera 2 will subject the eye of the viewer to sudden changes of brightness as seen on the cathode-ray tube in the receiver. Hence the unfortunate illusion that the lighting is varying. It is, however, possible to introduce an artificial correction in the camera channel circuit by altering the electrical signal.

Probably the most difficult feature of the imageorthicon camera tube is that it has a very limited contrast range, consequently the lighting contrast has also to be kept down to the order of 20 to 1 . If this is exceeded we get the familiar "throwoff" (black halo around bright objects), and also "ghosting cffect" due to excessive secondary electrons emitted from the target where image highlights occur. It is usual, therefore, to employ much softer lighting for television than that used in film studio work.

Most of the above problems have been taken as typical examples occurring on outside broadcasts where physical limitations are the main obstacles. But lighting difficulties are just as prevalent inside the studios although, in this case, it is more a question of complexity of production, involving camera angles, microphone-boom positions and the use of multiple stage-sets. A fast-moving production, for instance, may use nine or ten different set designs, each requiring its own lighting plot, and each balanced so that there are no irritating changes in light level. In a studio play, for example, it is essential to maintain continuity of mood from camera to camera, whether in close-up or long-shot. This applies even more so with a ballet presentation which relies largely on its pictorial appeal. It is desirable, therefore, that not only should the studio-lighting installation be capable of a high degree of artistic control, but equally im-


## MINIATURE TRANSISTOR HEARING AID

ALTHOUGH weighing only $1 \frac{1}{2}$ oz and measuring less than $2 \frac{3}{8}$ in $\times 1 \frac{7}{8}$ in $\times \frac{1}{2}$ in, the "Minuet" hearing aid employs a 4 -stage resistance-coupled transistor circuit designed to give high-quality reproduction with sufficient gain and output for the majority of cases of deafness. At $30^{\circ} \mathrm{C}$ the gain is 20 db and the maximum acoustic output 125 db referred to 0.0002 dyne $/ \mathrm{cm}^{2}$.

A single 1.3-V Mallory cell (type RM625) gives approximately 175 hours' working on the total current demand of 2 mA . This cell, which is of the disc type, fits in a miniature drawer in the base of the instrument and can be replaced without opening the case. An intricate plastic moulding forms the chassis and provides a rigid housing for the various components. The microphone is resiliently mounted to eliminate case noises.

In addition to the usual volume control there is a combined on-off switch and two-position tone control with normal and top-cut responses. Alternative earpieces are available with normal rising response or a flat response curve and there is a choice of mounting clips.

The price is $£ 5613 \mathrm{~s}$ and the makers are the Multitone Electric Co., Ltd., 223/7, St. John Street, London, E.C.1.

Multitone " Minuet " transistor hearing aid.

# B.B.C. Television Frequencies 

## Medium- and Low-power Stations on Offset Carriers

0NE of the provisions of the Stockholm Plan for v.h.f. broadcasting in Europe is that sound and vision carriers of some television stations should be offset by a maximum of $20 \mathrm{kc} / \mathrm{s}$ to avoid mutual interference between transmitters sharing a channel. The B.B.C. is, therefore, operating some of its recently introduced medium- and low-power stations on offset carriers and the deviation adopted is plus or minus $6.75 \mathrm{kc} / \mathrm{s}$ for the vision frequency and $20 \mathrm{kc} / \mathrm{s}$ for sound. In the appropriate columns in the following table the nominal channel frequencies are accordingly marked + or - where they are offiset. With the exception of the frequencies given for Londonderry (which have yet to be approved by the P.M.G.) all the information has been confirmed with the Engineering Information Department of the B.B.C.

In conformity with the general practice on the Continent the B.B.C. has adopted the principle of indicating that the carrier frequencies are offset by suffixing the channel number with + or - (i.e.,

Channel 2- for North Hessary Tor).

In the fifth column is given the e.r.p. of the permanent vision transmitter, but where there is at present a temporary transmitter in use this figure is followed by the e.r.p. of the low-power installation in brackets. Stations not yet in operation are marked with an asterisk in this column.

Another provision of the Stockholm Plan to minimize interference, and adopted by the B.B.C., is the use of directional aerials. For stations with directional aerials we give in the appropriate column the minimum and maximum e.r.p. for both the permanent and temporary transmitters. No figure is available for the e.r.p. of the temporary North East Scotland transmitter at Redmoss which will be replaced by the permanent station at Meldrum (marked $\dagger$ ) at the end of the year. Incidentally, the temporary Belfast station at present operating at Glencairn will be replaced next month by the permanent station at Divis.

The e.r.p. of the new B.B.C. London transmitter which is being

| $\bar{\omega}$ <br> $\stackrel{E}{E}$ <br> U | Station | Carrier <br> Frequencies (Mc's) |  | $\begin{gathered} \text { Vision } \\ \text { E.R.P. }(k W) \end{gathered}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Vision | Sound |  |  |
| 1 | Alexandra Palace (London) | 45.0 | 41.5 | 34 | $V$ |
|  | Divis (Belfast) ... ... | 45.0 - | 41.5 - | 20 (0.4) | H |
| 2 | Holme Moss, Yorks. | 51.75 | 48.25 | 100 | $v$ |
|  | N. Hessary Tor, Devon | 51.75- | 48.25 - | 1-16 (0.5) | $V$ |
|  | Rosemarkie, Inverness | 51.75 | 48.25 - | 1* | H |
|  | Dover area, Kent ... | 51.75 | 48.25 | 0.1-1* | H |
|  | Londonderry, N. Ireland | 51.75 | $48.25+$ | $0.5^{*}$ | H |
|  | Truleigh Hill (Brighton) ... | 51.75 | 48.25 | (0.3) | V |
| 3 | Kirk o'Shotts, Lanarks. | 56.75 | 53.25 | 100 | $V$ |
|  | Tacolneston (Norwich) | 56.75 | 53.25 | 1-10 (0.14-1.3) | H |
|  | Rowridge, I.O.W. ... | 56.75 - | 53.25 - | 1.32 (0.3-9) | $V$ |
|  | Blaen Plwy, Cardigan. | $56.75+$ | $53.25+$ | 1* | H |
| 4 | Sutton Coldfield, Warwicks. Meldrum, Aberdeenshire Carlisle area, Northumb'd Jersey, <br> C.I. | 61.75 | 58.25 | 100 | $\checkmark$ |
|  |  | 61.75- | 58.25- | 20( $\dagger$ ) | H |
|  |  | $61.75+$ | $58.25+$ | 1* | H |
|  |  | $61.75+$ | $58.25+$ | I* | H |
| 5 | Wenvoe, Glam. | 66.75 | 63.25 | 100 | $V$ |
|  | Pontop Pike (Newcastle) | 66.75 - | 63.25 - | 10 (1) | H |
|  | Douglas, I.O.M. ... | $66.75+$ | $63.25+$ | 1 (0.25) | V |

built at Crystal Palace and is scheduled to be brought into service next year will be 200 kW .

We are unable to include details of the proposed I.T.A. stations as they have not yet been agreed. It was, of course, stated by the P.M.G. some months ago that the London and Lancashire transmitters would share Channel 9 $(194.75 \mathrm{Mc} / \mathrm{s}$ vision and 191.25 $\mathrm{Mc} / \mathrm{s}$ sound) and that the carriers of the London transmitter would be offset by $+6.75 \mathrm{kc} / \mathrm{s}$ and $20 \mathrm{kc} / \mathrm{s}$, respectively.

## TV PROGRESS REPORT

WORK began in April on the Channel Islands station at Les Platons, Jersey, which the B.B.C. hopes to bring into service in September. Transmissions from the South Devon station at North Hessary Tor will be received on the S.W. coast of Guernsey and relayed by radio to the Les Platons stationsome 20 miles away-for retransmission. Until the permanent transmitter is in use in South Devonprobably early next year-the Channel Islands television service may not be consistent.

The contract has been placed for the erection of the permanent $560-\mathrm{ft}$ stayed mast for the East Anglian station at Tacolneston, near Norwich. This mast will carry the aerials for both television and the v.h.f. sound transmissions. It is hoped that the permanent television transmitters will be installed and the aerials ready for the station to replace the temporary equipment about the middle of next year.

Some difficulty has been experienced in securing a suitable site on the Isle of Man for the permanent station. The ideal position is said to be at the summit of Snaefell, but objections have been raised by the Ministry of Civil Aviation as it is feared the television station might cause interference with the Ministry's transmitting and receiving station already operating on Snaefell. Further tests are, however, to be carried out next year. In the meantime the opening of the permanent station at Divis, Northern Ireland, in July should give a service to the population in the north of the island. The temporary transmitter at Carnane, near Douglas, serves about $60 \%$ of the population.

# Cathode Followers- 

With Particular Reference to Grid Bias Arrangements

By "CATHODE RAY"

LLOOKING at the basic circuit diagram (Fig. 1) we might think there wasn't much that could be said about the cathode follower. As for its grid bias, with beautiful simplicity the one and only resistor in the circuit sees to that as well as doing its main job. So it appears.

But when one thinks one knows all about cathode followers, some unsuspected complication comes to light. I hope, however, that you will not take that remark as the prelude to an astonishing new revelation. I doubt whether I am about to disclose anything new, but it may be new to some who have not made a special study of cathode followers or who have not yet had to adapt the theoretical circuits to practical work. There are one or two things about arranging their grid bias, for instance, that are not always made clear in the books.
First we had better have a quick review of cathode followers in general. Their chief use is to enable a waveform derived from a high-impedance source to be reproduced accurately across a comparatively low or variable impedance. They can do this because (1) their input impedance is exceptionally high; (2) their output impedance is exceptionally low; and (3) they cause exceptionally little distortion. These features are due largely to the $100 \%$ voltage negative feedback resulting from the position of $R$, on the cathode side of the valve. From the point of view of the output terminals, the impedance appears to be R in parallel with approximately $1 / \mu$ times the valve's actual anode resistance, $r_{a}$. This $r_{a} / \mu$ is the same thing as $1 / g_{m}$. For instance, if $g_{m}$ (the mutual conductance of the valve) is $5 \mathrm{~mA}, \mathrm{~V}$, that is 0.005 amps per volt, and $1^{\prime} 0.005$ is 200 , which is the apparent number of ohms resistance in parallel with $\mathrm{R}^{\star}$. This is far lower than a valve having its output taken from the anode side, and load impedances down to a few thousand ohms can be connected across it without making much difference to the output voltage.

I need hardly repeat the various ways (explained in all the books) by which negative feedback reduces distortion. In the cathode follower all the output is fed back, so (as regards a single valve at least) reduction of distortion is a maximum.
The high input impedance comes in two ways. The fact that the anode is held at a constant potential cuts out the "Miller effect," which in an anode-loaded valve greatly magnifies the effective grid-to-anode capacitance. On the other side, the effective grid-tocathode capacitance is only a small fraction of its book value, because the potential of the cathode follows that of the grid $\dagger$, the grid-to-cathode signal voltage being only the difference between the input and output voltages. Thus the cathode follower has

[^4]all the benefit of high-resistance inpur possessed by any valve operatcd with its grid negative, but without mosi of the spoiling effect of capacitance to anode and cathode.
Unless we are careful with our grid bias arrangements, however, we may throw away something of these advantages.

As I said at the beginning, R in Fig. 1 provides grid bias at the same time as coupling impedance. But doing two things at once often means that neither is done properly-or at best only one of them. I wouldn't say that the simple Fig. 1 circuit never givco satisfaction. Like some of the films reviewed in the cinema trade press ("Might get by with unsophisricated audiences ") it is all right if you are easily satisfied. If the resistance of $R$ is too small for grid bias purposes, then grid current flows at the positive peaks of input, and bang go the high input impedance and freedom from distortion. If too large, negative peaks reach the " bottom bend" and the valve ceases to cathode-follow. But if R is chosen midway between these two calamities it will be much smaller than optimum as a coupling resistance.

## Adapting the Diagram

To see this in all its naked clarity we shoild draw a characteristic-curve diagram. Fig. 2 is a sample $\ddagger$. It starts with an ordinary set of anode-current/ anode-voltage curves, as found in valve catalogues. Those in Fig. 2 refer to a rather mediocre triode, having $r_{a}=10 \mathrm{k} \Omega, \mu=17$, so $g_{m}=1.7 \mathrm{~mA} / \mathrm{V}$. Let me emphasize that these figures, like all such published for valves, refer to only one set of working conditions (represented by one point on the diagram) and vary a good deal over the area of the diagram. If it were not so, the curves would be evenly-spaced straight lines. Because they never are, there is always distortion. Each curve, of course, represents the way the anode current $\left(\mathrm{I}_{t}\right)$ varies with anode voltage $\left(\mathrm{V}_{a}\right)$ at the fixed value of grid voltage $\left(V_{g}\right)$ marked beside the curve. Take special note of the fact that $V_{a}$ is the voltage relative to the cathode (as, indeed, is also $\mathrm{V}_{\square}$ ). In the ordinary use of a valve that is the same thing as the voltage relative to earth or -h.t. or the lower input terminal, for all these things are tied to cathode either directly or through a by-pass capacitor.
It is because one gets so used to assuming this that the cathode follower is apt to muddle one. When the input voltage varies the grid potential, it varies the cathode potential too; so one can't use the cathode as a fixed-potential point from which to reckon all voltages. The obvious zero-potential reference point is E. And the valve electrode held at constant potential by it is not the cathode but the anode (separated only by the

[^5]fixed voltage $V_{H T}$, as shown in the inset to Fig. 2). So our reckoning of the valve electrode voltages has to be upside down as compared with ordinary usage. $\mathrm{V}_{a}$ on the curve sheet therefore really means minus the cathode voltage (relative to fixed anode). And $\mathrm{V}_{g}$ can't be used directly at all, because it is between two varying-potential points. What mathematicians call the independent variable is not $\mathrm{V}_{g}$ but $\mathrm{V}_{\text {IN }}$. But this amounts to the same thing as $\mathrm{V}_{a g}$, the voltage of the grid relative to anode. Can we somehow get $\mathrm{V}_{a g}$ or $\mathrm{V}_{\text {IN }}$ curves on to the diagram?

Well, if we look at the inset we see that $\mathrm{V}_{a g}$ is the difference between $\mathrm{V}_{G}$ and $\mathrm{V}_{g}$, which are both on the diagram. So all we have to do to plot a curve of " $\mathrm{V}_{g g}=x$ volts" is to join together all points at which $\mathrm{V}_{a}{ }^{n g}-\mathrm{V}_{g}=x$; that is, $\mathrm{V}_{a}=x+\mathrm{V}_{g}$. So where $\mathrm{V}_{g}=0, \mathrm{~V}_{a}$ must be 250 to locate a point on this curve. That is point $a$. Next, at $\mathrm{V}_{g}=-2, \mathrm{~V}_{a}$ must be $250-2=248$; so we find the point on the $\mathrm{V}_{g}=-$ 2 curve at which $\mathrm{V}_{a}=248$, namely $b$. And so we go down the $\mathrm{V}_{g}$ curves, moving a corresponding number of $\mathrm{V}_{a}$ volts to the left every time, to give the " $\mathrm{V}_{a g}=$ 250 "curve when all the points are joined up. In the same way curves for $\mathrm{V}_{a g}=$ anything else can be drawn; I have done the 237.5 and 262.5 volt curves. The reason I chose 250 for a start is that we are going to assume for example that $\mathrm{V}_{\text {Нт }}$ is 250 . That being so, $\mathrm{V}_{\mathrm{IN}}$, which is $\mathrm{V}_{\mathrm{HT}}-\mathrm{V}_{a g}=0$ anywhere on the $\mathrm{V}_{a g}=$ 250 curve, as marked in brackets (to show that it applies only on the assumption that $\mathrm{V}_{\mathrm{HT}}=250$ ). So our starting point, representing zero input voltage, must be somewhere on this curve. But where?

If it were down near the foot, where $I_{a}$ is small or even zero, there would be plenty of room for increase of current during the positive half-cycles of $\mathrm{V}_{\text {IN }}$, but the negative halves would be cut off. And if the starting point were placed at the top, the negative halves would be all right but the positive halves would be in the positive grid region and grid current would flow. So we follow the usual procedure for valve diagrams and put the starting point about half way between zero grid bias and cut-off bias. We see that cut-off bias at $V_{a}=250$ is about -16 volts. But half that, -8 volts, looks rather alarmingly low down, so I have put it at -7 . Then the "load line" is the one drawn through " $\mathrm{V}_{a}=250, \mathrm{I}_{a}=0$ " (point $c$ )
and the newly located starting point (o). It is shown dotted.

What this dotted load line does is to show the drop in $\mathrm{V}_{a}$ below 250 volts when current passes through the resistance ( R ) represented by it. At $\mathrm{I}_{a}=0$, no volts are dropped in R , so $\mathrm{V}_{a}$ is the full 250 V h.t. (point $c$ ). At the starting point $o, I_{a}=10 \mathrm{~mA}$, and we see that $\mathrm{V}_{a}=243$; a drop of 7 V . The resistance that requires 7 V to pass 0.01 A through it is $7 / 0.01=700$ ohms. So the dotted line represents a load resistance $R$ of $700 \Omega$.

## Results

Next, let us see what happens when an input signal swings the grid alternately positive and negative. This is where the other two $\mathrm{V}_{1 N}$ curves are needed. If the peak voltage of the input is $12 \frac{\downarrow}{2}$ volts, the working point moves along the dotted line as far as the curve " $\left(\mathrm{V}_{\mathrm{L}, \mathrm{M}}=+12.5\right)$ "-and where, incidentally, $\mathrm{V}_{g}=$ -2 , which is about as far as we can go in that direction and still be quite sure of grid current not starting —and in the other direction to " $\left(\mathrm{V}_{\mathrm{IV}}=-12.5\right)$ " which is about as near cut-off as it is wise to go.

If you like you can try alternative load resistances and working points to see if you can get less distortion at this input, or more output for equal distortion, but I shall be surprised if you do much better working from " $\mathrm{V}_{\text {is }}=0$." How do we know how much output is obtained? Well, the inset shows that any change in $\mathrm{V}_{\text {our }}$ must be at the expense of $\mathrm{V}_{a}$, so is equal and opposite to it. The movement of the working point along the dotted line takes us from 243 V at the start to 235 V at the positive peak and 249 V at the negative, which is -8 V and +6 V respectively; so the peak values of $\mathrm{V}_{\text {out }}$ are +8 V and -6 V . Another and more accurate way of obtaining these values is to read the rise and fall in $I_{a}$ and multiply by $R$; this gives them as +7.7 V and -6.2 V .

We note from this that (1) unlike the anode-loaded amplifier, Vour has the same polarity (or is in the same phase) as $\mathrm{V}_{\text {IN }}$; (2) the device is by no means distortionless, for equal + and $-\mathrm{V}_{\mathrm{IS}}$ give considerably unequal + and $-\mathrm{V}_{\text {out }}$ (as a matter of interest, the 2 nd harmonic distortion calculated in the usual way from the above data is $5.4 \%$ ); and (3) the voltage


Fig. 1. Basic circuit diagram of cathode follower.

Fig. 2. Showing how to use the ordinary $I_{a} V_{a}$ valve curves to construct cathode-follower characteristic curves.



Fig. 3. By using a much higher value for $R$ in Fig. I than the $700 \Omega$ in Fig. 2, maximum output is greatly increased and distortion reduced.
voltage ratio $\mathrm{V}_{\text {OUT }} / \mathrm{V}_{\text {IN }}$ is also better-103/114=0.9, or only $10 \%$ ioss instead of $44 \%$.

By using a higher resistance, the maximum voltage output could be pushed considerably higher and the distortion still lower; but if only a voltage output were needed there would be no point in using a cathode follower at all-the input signal would do. Presumably there is some additional load in parallel with R. If
" amplification," $V_{\text {out }} / V_{\text {IV }}$, is $13.9 / 25$ (peak to peak), which is 0.56 , or a loss of nearly half. We also note that the grid voltage $\mathrm{V}_{g}$ swings between -2 and about -14 , or 12 V peak to peak, so the voltage amplification of the valve itself is $13.9 / 12=1.16$. If the valve were used in the ordinary way, with R on the anode side, $\mathrm{V}_{g}$ would be the same as $\mathrm{V}_{1 \mathrm{~N}}$ (as regards signals at least), and its negative peak would be the same as the positive ( 5 V ), so the negative $\mathrm{V}_{\text {out }}$ would be only 5.1 V and the distortion would be greater ( $10.2 \%$ ). As compared with this, the cathode-follower arrangement gives about half the amplification, but about half the distortion and a shade more output.

But it is a pretty miserable output-less than 7 V peak using 250 V h.t. As anyone who is accustomed to valve load diagrams will see at once, the reason is that the slope of the dotted load line is too steep, signifying that the resistance is too low. The less the slope, the greater the range of voltage represented by it between the grid-current and cut-off boundaries. To get the utmost voltage output, the resistance should be so large as to be represented by a nearly horizontal line right down near the $\mathrm{V}_{a}$ scale. But then the current range would be almost nil, and the valve would be incapable of supplying appreciable signal power. For maximum power, a designer would choose a medium slope, such as that of the dotted line in Fig. 3, which represents a resistance of $15 \mathrm{k} \Omega$. $\mathrm{V}_{g}=-7$ again puts the starting point (o) about half way along the useful part of the line, and if we draw a $\mathrm{V}_{a g}$ line through it we find $\mathrm{V}_{a g}$ here is 190 V . So $\mathrm{V}_{1 \mathrm{~N}}$, being $\mathrm{V}_{\mathrm{Ht}}-\mathrm{V}_{a g}$, is +60 V . If again we are cautious about grid current and allow a full -2 V as the minimum grid bias, the positive limit is at point $d$, where $\mathrm{V}_{a g}$ turns out to be 133 V . This makes $\mathrm{V}_{\mathrm{iN}}$ 57 V more positive than at the start, so the negative limit is found by making $\mathrm{V}_{1 \mathrm{~N}} 57 \mathrm{~V}$ less than at the start, namely +3 V , and drawing the $\mathrm{V}_{a g}=250--3=$ 247 V curve.

The output is now probably easier to read direct as change in $\mathrm{V}_{a}$ than indirectly as $\mathrm{I}_{a}$; it is +52 V and -51 V . Not only is that more than seven times what it was with $R=700$, but the distortion is far lessbelow a half of one per cent. Actually we could probably go up to at least $\pm 60 \mathrm{~V}$ peak output withour much increase in distortion or risk of grid current. The
it is a d.c. path, then its effect is of course exactly the same as reducing $R$. If it is an a.c. path (such as a resistance load fed through a blocking capacitor) the real load line pivots on $o$ instead of on the 250 -volt point on the $\mathrm{V}_{a}$ scale, and if $o$ has been placed low by making R very high it is so near cut-off that distortion sets in sharply at quite a small output.

The fact to which everything so far has been leading up, however, is that when the resistance of $R$ has been chosen to give reasonable operating conditions it is far too much for grid bias. In Fig. 3 the preferred starting point is " $\mathrm{V}_{\text {IN }}=+60$," and if that positive bias were not supplied it would mean that the grid was 60 V too negative. So now we come at last to our main object-to discover how best to provide this +60 V or whatever it may be. There are a lot of different ways. Also there are some snags.

The simplest and best, if circumstances make it possible, is to connect the grid straight to a source of signal that also provides the necessary positive bias. If the source is the anode of another valve, that is probably the answer: Fig. 4(a). If 60 V is altogether too low for the anode of that stage, it may be practicable to design the cathode follower to work well with a more positive grid.

But perhaps there is some good reason against this -the cathode-follower load is low or widely variable, the previous anode voltage is unavoidably high, or maybe the signal source is not an anode at all, or the cathode-follower may be needed to work from different sources so must be self-contained as regards bias. In such cases it is usually necessary to admit the signal through a blocking capacitor to make sure that the bias it not short-circuited by the signal source. The grid must then be connected to a source of bias through a high resistance " grid leak," so as not to shortcircuit the signal source. An obvious method of getting the bias is from a potential divider across $\mathrm{V}_{\text {rt }}$ (Fig. 4(b)). Perhaps there already is such a potential divider, whether called by that name or the more unpleasant one of " bleeder," needed for some other purpose, and it is only a matter of tapping it at a suitable point. But if not, it is easy enough to find suitable values for $R_{2}$ and $R_{3}$, because the grid takes no current, so $V_{\text {bias }}$ is to $V_{\text {HT }}$ as $R_{3}$ is to $R_{2}+R_{3}$. For the same reason, $R_{2}$ and $R_{3}$ can be quite high
resistances, of the megohm order, provided they are reliable. If there is any question of an undesirable amount of hum getting at the grid from + h.t., a largish capacitance $C_{2}$ can be added.

But if $R_{2}$ and $R_{3}$ are high, as suggested, why have $R_{1}$ at all? True enough; if the resistance of $R_{2}$ and $R_{3}$ in parallel is made equal to whatever would be considered a suitable grid-leak resistance, then $R_{1}$ is unnecessary and the circuit simplifies to Fig. 4(c). A suitable grid-leak resistance is the same as in a conventional amplifier; that is to say, the resistance should not be higher than the valve maker recommends as a top limit, nor low enough to load the signal source seriously. Something of the order of one megohm is usual.

## One Resistor: Two Valves

Since one of the main objects of a cathode follower is to load the signal source as little as possible, it may happen that even the valve maker's top limit for grid resistance is lower than one wants to have across the signal source. My impression is that the valve makers cover themselves pretty well by fixing a low limit, and one can usually get away with a considerably higher value. But however that may be, one of the special features of a cathode follower is that the grid leak resistance seen by the signal source can be far higher than it is from the valve maker's point of view. This remarkable ability to have the best of things both ways is not achieved in the circuits seen so far, but it is in Fig. 4(d). This, I think, is the commonest bias arrangement for cathode followers, but I doubt whether everybody who uses it does so with the conscious intention of obtaining
the advantage just mentioned. Nor, perhaps, is everybody who uses it aware of a possible snag that we shall come to in a moment.

The principle of Fig. 4(d), of course, is that $R$ in Fig. 1 provides slightly more than the positive bias needed to neutralize the negative excess provided by it, so a point can be found on it which gives the right amount and to which $\mathrm{R}_{1}$ can be connected. In our Fig. 3 example the total drop in R was 67 V , of which 7 was needed for negative bias and therefore 60 had to be neutralized. A simpler way of looking at it, perhaps, is to regard the upper portion of $R$, $\mathrm{R}_{4}$ in Fig. 4(d), as the conventional bias resistor to provide the required voltage, 7 in this example. Either way, if $R_{4}+R_{5}$ were $15 k \Omega$ as before, $R_{4}$ would have to be $7 / 67$ of this, or $1,565 \Omega$, and $R_{5}$ $15 \mathrm{k} \Omega$ less this.

Suppose the valve maker's rating for maximum grid-to-cathode resistance is $1 \mathrm{M} \Omega$. Then we would probably make that the value of $R_{1}\left(R_{4}\right.$ being by comparison negligible). It looks at first sight as if the impedance across the input terminals is practically the same ( $\mathrm{C}_{1}$ having been made large enough for its impedance to be negligible at the signal frequency). But imagine for the moment that the lower end of $R_{1}$ were taken away from $R_{4}$ and $R_{5}$ and connected to the grid, so that both ends of $R_{1}$ were at the same potential. Then obviously no current would flow through $R_{1}$. The same would be true if it were connected to a second signal source the same as the first, for both ends would still be at the same signal potential at every instant. If it were connected to the cathode, that end would receive (in our calculated example) nine tenths of the input signal, in phase. So only one tenth of the input signal voltage would

(a)

(d)

(b)

(e)

(c)

( $f$ )
F.g. 4. Various methods for enabling the higher resistance indicated in Fig. 3 to be used in practice, by providing appropriate grid bias.
actually come across $\mathrm{R}_{1}$, and therefore it would take no more current than $10 \mathrm{M} \Omega$ connected across the whole input voltage. Connected as in Fig. 4(d) it receives about eight tenths of the input voltage, and so acts as a load of $5 \mathrm{M} \Omega$.

There is more juice still left in the orange, for $\mathrm{C}_{1}$ does not have to be large enough to be negligible in comparison with $1 \mathrm{M} \Omega$ but with $5 \mathrm{M} \Omega$. Now the voltage loss in $\mathrm{C}_{1}$ is only $1 \%$ if the reactance of $\mathrm{C}_{1}$ is one seventh of the effective load resistance. If that resistance were literally $R_{1}$, the reactance would have to be one seventh of a megohm; and if the lowest frequency to be handled were $20 \mathrm{c} / \mathrm{s}$ that would mean $\mathrm{C}_{1}=$ a little over $0.05 \mu \mathrm{~F}$. But with $\mathrm{R}_{1}$ as in Fig. 4(d) it need be only $0.01 \mu \mathrm{~F}$ for the same results.

Now for the snag. The negative feedback in a cathode follower consists of the whole output voltage (signal voltage across $\mathrm{R}_{\mathbf{4}}+\mathrm{R}_{5}$ ) fed back to the grid, and in this version of the circuit it can only reach the grid via the signal source. To simplify things let us for the moment imagine that the lower end of $R_{1}$ is moved up to the cathode. Then the impedance of the signal source and $R_{1}$ act as a potential divider across $R_{4}+R_{5}$, and only that part of the fed-back voltage which is developed across $R_{1}$ actually reaches the grid. If the signal source impedance at any signal frequency were $1 \mathrm{M} \Omega$, then, with our $1 \mathrm{M} \Omega$ $\mathrm{R}_{1}$, only half the voltage would be fed back, and we would have only half a real cathode follower Things are not quite so bad with $\mathrm{R}_{1}$ where it actually is, but in our example it would be nine tenths as bad. Remembering again that the main point of using a cathode follower is usually to work from a highimpedance source, this rather subtle propensity must not be overlooked. The impedance of the signal source at any signal frequency should not be more than, say, one tenth of the actual value of $R_{1}$. Even this precaution may not be strict enough if the source impedance is largely reactance and we want to keep phase shift in the cathode follower very small.

The signal source impedance normally consists of the anode resistance of the valve (after allowing for the effect of negative feedback, if any) in parallel with the load impedance.

A variation of Fig. 4(d) that one sometimes sees is Fig. 4(e). The only difference is the by-pass capacitor $\mathrm{C}_{3}$, sufficiently large to have negligible impedance (compared with $\mathrm{R}_{4}$ ) at any signal frequency. So far as signals are concerned, $\mathrm{R}_{1}$ is connected straight to the cathode (which is, if anything, a slight disadvantage, , and the cathode-to-earth resistance is $R_{5}$. But so far as d.c. is concerned it is $R_{5}+R_{4}$. So if we were doing a Fig. 3 diagram for this circuit we would have to draw the dotted line at a slope to represent $\mathrm{R}_{5}+\mathrm{R}_{4}$, and then draw through o a steeper line representing $R_{5}$ alone, this being the line along which signal voltages would operate. Personally I consider $\mathrm{C}_{3}$ a waste of money.

Lastly, to overcome the loss of feedback in circuits (d) and (e), type (f) has been suggested, in which $\mathrm{R}_{1}$ is " decoupled to earth" for signal voltages, but receives its bias voltage from the junction of $\mathrm{R}_{4}$ and $\mathrm{R}_{5}$ as before. The impedance of $\mathrm{C}_{4}$ at the lowest signal frequency should be very much less than $\mathrm{R}_{6}$. For this to be so, $R_{1}+R_{6}$ is almost sure to be appreciably higher than $R_{1}$, which means that the input signal load, which is $R_{1}$, is appreciably lower than the valve maker's limit which (if we follow his advice) is $\mathbf{R}_{1}+\mathrm{R}_{6}$. This arrangement seems to me to have no great advantage over (c), and is less simple. On the other hand, (c) - and (b) - have the advantage that the cathode potential is stabilized (given constant $\mathrm{V}_{\mathrm{HT}}$ ) at a few volts above a level fixed by the ratio of $R_{2}$ to $R_{3}$.

Summing up: (a) is much the best if it can be arranged; if not, (c) is most likely to perform as expected, whereas (d) enables one to achieve a much higher signal input resistance but has to be carefully considered for possible loss of feedback. The others also ran.

SHORT-WAVE CONDITIONS Predictions for June


THE full-line curves given here indicate the highest frequencies iikely to be usable at any time of the day or night for reliable communications over four long-distance paths from this country during June.

Broken-line curves give the highest frequencies that will sustain a partial service throughout the same period.

*.............. FREQUENCY 8ELOW WHICH COMMUNICATION SHOULD BE POSSIBLE FOR $25 \%$ OF THE TOTAL TIME

-     -         - predicted average maximum usable frequency
— FREQUENCY BELOW WHICH COMMUNICATION SHOULD
BE POSSIBLE ON ALL UNDISTURBED DAYS


# F.M. TUNING INDICATOR 

# Obtaining Zero Voltage Readings with Conventional " Magic Eye" Indicators 

By J. R. DAVIES

THE writer, when engaged in the design and development of an f.m. tuner, was confronted with the necessity of providing a tuning indicator which could be made to give readings that were true and reliable. Also, the indicator had to be reasonably inexpensive and capable of use by non-technical persons.

At present, it seems to be fairly general practice to employ conventional tuning indicators in the f.m. receivers which are manufactured in this country, these indicators being operated from the rectified voltage appearing across the stabilizing capacitor (assuming a ratio discriminator), or from the grid resistor of an i.f. limiter valve. This system is not without its disadvantages; partly because it is necessary to ensure that the i.f. stages are accurately " peaked" (and remain so " peaked" for considerable periods of time) at the centre frequency, and partly because the initial deflection of the indicator on tuning in a strong signal is liable to be much greater than the small additional increment given at what is assumed to be the point of correct tuning.

An alternative method of obtaining tuning indications is available when a balanced ratio discriminator is employed. With such a circuit the audio take-off point provides a d.c. potential with respect to chassis which varies as the receiver is tuned through the signal being received. The d.c. potential decreases as the signal frequency deviation decreases, and it reverses polarity as the signal passes through the centre frequency. Assuming that the diode load resistors are accurately balanced about chassis, this d.c. potential may be employed to operate a tuning indicator; the position of correct tuning being represented by zero voltage.
either side of zero for the point of maximum indication. This error is quite small when it is considered that the d.c.-potential swing of the audio take-off point in most conventional f.m. receivers is usually well above 2 volts positive and negative.

The Circuit.-The circuit employed is shown in Fig. 1. In this diagram the audio take-off point from the balanced ratio discriminator is connected, via $\mathrm{R}_{\text {, }}$ and $\mathrm{R}_{2}$, to the grids of a double triode, V1. The cathode of $\mathrm{Vl}(\mathrm{a})$ is taken direct to chassis, whilst the cathode of $\mathrm{Vl}(\mathrm{b})$ is taken to a potential which is positive with respect to chassis.

Let us assume that the potential at the audio take-off point is sufficiently negative to allow $\mathrm{Vl}(\mathrm{a})$ to pass only a small anode current. Vl(b), due to the positive potential on its cathode, is cut off. In consequence of this, the potential at the grid of V2 is that given by the potentiometer $R_{4}, R_{5}$ and $R_{6}$. Due to the low anode current passed by V1(a), the cathode of V2 has a potential which is considerably higher than that at its grid. In consequence, the triode section of V2 is cut off, and the display indicator presents zero shadow angle.

If the negative potential with respect to the chassis at the audio take-off point is advanced towards zero (ultimately to reach a positive value), V1(a) passes a continually increasing current. This causes the cathode potential of V2 to drop until a stage is reached when the indicator shadow commences to "open." As the audio take-off potential continues to approach zero, the shadow opens further. At a potential close to zero, positive grid current commences to flow through $\mathrm{R}_{\text {}}$ and the increase of anode current in V1(a) ceases.

The circuit described in this article takes advantage of this fact, and employs a conventional 6U5 "Magic Eye" tuning indicator in conjunction with a 12AU7 double triode. Interpretation of the pattern display given by the indicator is obvious since zero voltage is represented as maximum shadow angle, and excursions into either positive or negative voltage cause the shadow to "close." The sensitivity is high, zero shadow angle being given by a voltage around 2 volts on either side of zero. Due to the inherent nature of the circuit, maximum indication may not necessarily be given at zero volts, but at a potential which is very close to zero volts. Empiric tests with sample valves gave errors of less than 0.1 volt on


Fig. 1. The circuit of the indicator device described in this article.

The potential at the cathode of V 2 , in consequence, becomes comparatively steady.

Very shortly before the commencement of grid current in V1(a), Vl(b) commences to conduct. However, its rate of change of anode voltage is lower than that of $\mathrm{Vl}(\mathrm{a})$, and so the latter valve gives the greater control over shadow angle. After the condition of positive grid current has been reached the potential at the anode of Vl(a) remains comparatively steady. As the audio take-off potential continues to rise, that at the anode of V1(b) now commences to drop further. In consequence, the grid of V2 goes further negative with respect to its cathode, and the indicator shadow commences to close again. Zero shadow angle is achieved when the audio take-off potential has gone sufficiently positive.
(It may be worth mentioning that, during the positive excursion of the audio take-off voltage, the grid potential of V2 does not affect its cathode current to any large extent, since the latter flows mainly between cathode and target.)
Operation.-It will be remarked that the circuit of Fig. 1 cannot give an accurate indication of zero voltage as the only "reference point" is that at which positive grid current commences to flow in V1(a); and this will vary from valve to valve. Also, the positive potential at the cathode of $\mathrm{Vl}(\mathrm{b})$ may affect the operation near zero voltage.
However, empiric tests with a working circuit show that the device provides a maximum indication at points which are very close to zero voltage. Four different 12AU7s of varying ages give maximum indications which are all within 0.1 volt on either side of zero. Also, four-hour tests for drift do not show any measurable shift of the potential required for maximum shadow angle. Again, changes in h.t. line voltage between 200 and 250 , and in heater voltage between 6 and 6.6, produce no noticeable shift. This is not sufficient evidence, of course, to assume that the circuit will function as well for all 12AU7s; and it is possible that the worst instances of drift, or of inaccurate voltage indication, will occur in the early life of a brand new valve.
The values of $\mathrm{R}_{7}$ and $\mathrm{R}_{8}$ are fairly critical. The writer was tempted to make $\mathrm{R}_{8}$ a variable component, but the values shown in Fig. 1 coped satisfactorily for the valves tested in his particular case. Decreasing the value of $\mathrm{R}_{8}$ decreases the sensitivity of the circuit, and the indicator ceases to function altogether before the potential which gives maximum indication is shifted at all seriously. Increasing the value of $\mathrm{R}_{8}$ results in an indication of maximum shadow over a period between the potential which initiates positive grid current and a further positive potential. The consequent lack of sensitivity is immediately apparent.

Due to the fact that the potential at the cathode of V2 rises as the audio take-off potential goes negative, a dimming of the indicator pattern takes place for high negative control voltages. This dimming becomes just noticeable at approximately 4 volts negative, and the indicator is almost completely extinguished around 10 volts negative.

The potentiometer $\mathrm{R}_{5}$ is employed to set the grid of the 6U5 to the potential which gives optimum sensitivity. Before adjustment, the slider should be set to the high-potential end of the track and the audio take-off point short-circuited to chassis. The slider is then brought down until the 90 -degree shadow angle given by the short-circuit is reduced to approximately 85 degrees. The setting of $R_{s}$ is not


Fig. 2. Relationship between shadow angle and control voltage for typical $6 U 5$ and I2AU7 valves.
very critical, and it might be possible to use fixed components in this part of the circuit.
The capacitors $C_{1}$ and $C_{2}$ are included to prevent modulation voltages from blurring the indicator pattern. A graph showing shadow angle against audio take-off potential for a typical 12AU7 and a 6U5 is given in Fig. 2.
Performance.-After the circuit had been put into working order (with the aid of a potentiometer and centre-tapped dry battery to stimulate the voltages appearing at the audio take-off point) it was tested with a working f.m. receiver. To ensure that the different source impedance did not affect accuracy of indication, a valve-voltmeter was also connected between the receiver's audio take-off point and chassis. However, the different source impedance did not introduce any measurable shift in the potential needed to give maximum indication.
In use, it was found that the readings given by the indicator were very satisfactory indeed. Normally, the shadow remained open until a station was tuned in; whereupon the shadow closed abruptly. At the centre frequency of the station, however, the shadow opened once more, and it was consequently possible to obtain a beautifully precise indication of correct tuning. Subjective tests carried out by having nontechnical persons tune in the receiver resulted in an accurate position of optimum tuning being achieved in every case.
Acknowledgments.-Acknowledgments are due to Allen Components, Ltd., for facilities made available to the writer for the development of this circuit.

## RECEIVER SALES

A SURVEY of the retail sales of domestic receivers during the first quarter of this year, prepared by B.R.E.M.A., shows that by comparison with the same period last year the demand for television receivers increased by $70 \%$ and sound receivers and radiogramophones by $51 \%$. The table gives the 1955 monthly retail sales. The totals for the first quarter of 1954 are in parentheses.

|  |  | Sound | Radiograms | Television |
| :---: | :---: | :---: | :---: | :---: |
| January <br> February <br> March | $\cdots$ $\cdots$ $\cdots$ | 98,000 <br> 99,000 <br> 95,000 | 35,000 <br> 33,000 <br> 24,000 | $\begin{array}{r} 103,000 \\ 98,000 \\ 85,000 \end{array}$ |
| Quarter's total | ... | $\underbrace{292,000}_{12}$ | $\frac{92,000}{500)}$ | $\begin{aligned} & 286,000 \\ & (168,500) \end{aligned}$ |

## NEW DECCA RADIR

JUST over five years ago Decca produced their first radar set (Type 159) which was marketed at about half the price of existing equipment. Two other models (Types 12 and 45) were subsequently produced and together these three models have been fitted in over 3,700 shipsabout two-fifths of the world's radarequipped vessels.

The majority of the world's medium- and large-tonnage vessels are now equipped with radar and it was to meet the demand for a set for small ships-coasters, trawlers, etc.--that Decca recently produced the Type 212. Although considerably smaller, lighter and cheaper than its predecessors it is claimed to meet the stringent M.o.T. specification for marine radar and has been submitted for type approval.

A feature of the earlier Decca sets was the fitting of the r.f. head as part of the scanner unit, thereby eliminating a long waveguide run. As it is essential in smaller vessels to reduce top weight, and, also, it is possible to have a short waveguide run, the r.f. unit in the new model is separate.

The set, which has a 9 -in p.p.i., has six ranges $-0.5,1,3,8,15$ and 30 miles-with calibration rings varying from 0.2 to 5 miles according to the range scale in use. It has a minimum range of 30 yards and a discrimination of 25 yards on the shorter ranges.
The r.f. unit, giving a peak output power of 10 kW , has a pulse duration of either $0.1 \mu \mathrm{sec}$ or $0.2 \mu \mathrm{sec}$ accord-


The 212 display unit may be mounted on the bulkhead, deckhead or, as shown, on a pedestal.
ing to the range in use. The unit can be mounted either below deck or (in a special waterproof case) at the base of the mast. The familiar Decca separate half-cheeses for transmission and reception, have given place to a single parabolic cylinder scanner of approximately 4 ft across.

Decca have equipped two vehicles with this radar unit which are now touring the ports in the U.K. and on the Continent.

## CLEB

Barnsley.-The subject for the mecting of the Barnsley and District Amateur Radio Club on June 24th is "Fifty Years of Ham Radio" and the speaker is P. Denison (G8OK). Meetings are held at 7.0 at the King George Hotel, Peel Street, Barnsley. Sec.: P. Carbutt (G2AFV), 33, Woodstock Road, Barnsley, Yorks.

Birmingham.-"The Application of Valves for Communication Purposes " is the subject of the talk to be given by G. Nicholson (G3HKC) to members of the Slade Radio Society on June 10th. On 24th L. Glew, of Marconi Instruments, will speak about instruments at v.h.f. The ciub room at Church House, High Street, Erdington, is open every evening and lecture meetings are held on alternate Fridays at 7.45. Sec.: C. N. Smart, 110, Woolmore Road, Erdington, Birmingham, 23.

Chelmsford.-At the next meeting of the Chelmsford Group of the British Amateur Television Clubon June 9 th-members are to hear
a description of a portable monoscope unit. The group meets at the home of the secretary, M. Barlow (G3CVO), 10, Baddow Place Avenue, Gt. Baddow, Essex. Test transmissions are radiated each Saturday evening on $436 \mathrm{Mc} / \mathrm{s}$ by R. L. Royle ( $\mathrm{G} 2 \mathrm{WJ} / \mathrm{T}$ ), one of the members.

Cleckheaton.-T. C. Isaac (G4RQ), of Ambassador Radio, will speak on "High Quality Sound" at the meeting of the Spen Valley and District Radio and Television Society on June 1st. The club meets on alternate Wednesdays at 7.30 at the Temperance Hall, Cleckheaton. The final meeting of the session will be on July 13th. Sec.: N. Pride, 100, Raikes Lane, Birstall, Nr. Leeds, Yorks.

Coventry.-At the meeting of the Coventry Amateur Radio Society on June 20th, at 7.30 at 9, Queens Road, Coventry, D. Clift (G3BAK) will speak about v.h.f. transmission and reception. Sec.: J. H. Whitby (G3HDB), 24, Thornby Avenue, Kenilworth, Warwicks.


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# RAND0M 

By "DIALLIST"

## F.M. and Hi-Fi

THE B.B.C.'s decision not to strive after really high fidelity in its Band II service is due mainly to the fact that the cables provided for its use by the G.P.O. have a bandwidth limit of somewhere about $8 \mathrm{kc} / \mathrm{s}$. Nor will the G.P.O. allow radio links. A pity, of course; still, I don't think that those in the Home Counties who buy or build first-rate v.h.f. sets will be very disappointed by the quality of those Wrotham transmissions which emanate from studios or concert halls in London-Broadcasting House and Wrotham are linked by good lines. I have listened to Wrotham for a couple of years and found the programmes a revelation in the quality that can be obtained from a good receiver. There was a high-grade m.w. set in the same room as the v.h.f. receiver. As both were fitted with a muting arrangement it was possible to change instantly from the one to the other. Even to one who can lay no better claim than I to being musical, the difference was amazing. On the v.h.f. transmission, for example, you could pick out particular instruments in a big orchestra and follow them easily. I can't do that on any m.w. orchestral programme.

## Blessed Relief

MY new abode is well over 100 yards from the nearest main road. Thanks to the distance and to the fact that the aerial is some $50-60 \mathrm{ft}$ above the level of the road surface, I get no interference with television reception worth talking about; in fact, the limiter isn't in use at all and I can allow my whites to be really white. Much as I rejoice in this happy state of affairs my heart bleeds for those unfortunate enough to live on or near the road in question. It is one of the links between London and the south coast and, at this time of year anyhow, there is a constant stream of motor traffic along it all day and most of the night as well. Perhaps people grow so used to ignition interference that they cease to notice it particularly. I can't think how they can, for I'm sure I couldn't watch pictures that were continually marred by those awful lines of white spots.

Nevertheless, one finds that a good many of the houses standing right alongside the road are surmounted by "Hs," "Xs" or "Ks" and that many of these "look" right over it towards Alexandra Palace.

## Sets of Yesteryear

AMONG the long-forgotten papers that came to light when I was sorting things out on the eve of moving house was a 24 -page receiver supplement of the then weekly W.W. of December 9th, 1932. One of the first things that caught my eye was the advertisement of the DeceeAcee receiver: "Will work off a.c. or d.c. mains without alteration. The only set of its kind." With built-in loudspeaker (which many sets of those days had not) this s.g.-detpentode 3 -valve receiver cost 18 guineas. There was also a 4 -valve model with two h.f. stages, at 23 guineas. The fashionable set then was clearly the 3 -valve "straight" costing £10-£12 for battery models and $£ 16$ upwards for mains models. More engaging is a page containing front and back view drawings of a typical 3 -valve chassis "which will
enable the features of modern sets to be readily identified." The said features include: vari-mu h.f. valve, power-grid detector and pentode output (coupled by l.f. transformer, parallel-fed), screened bandpass coils, single-dial tuning, metal chassis (with decoupling circuits mounted below), full-wave valve rectifier and electrolytic smoothing condenser. There were some bargains in wireless sets in those days. For $£ 3$ you could buy a 2 -valve " Brownie," complete with moving-iron loudspeaker, but without batteries. Batteries and all, the K-B " Pup" cost £4 10s and there were a.c. and d.c. models of the same set for $£ 710 \mathrm{~s}$. There were quite a few superhets. The all-wave "Faraday," containing 4 s.g. valves and a power pentode and offered in a.c. or d.c. models went for 27 guineas and the G.E.C. had an a.c. mains model (with heterodyne whistle filter and automatic station index) for 26 gns . The same firm offered a 6 -valve allwave, battery-operated superhet, constructed to tropical specification, for 24 guineas.

## Wireless: Unlawful Use of

IN these queer days when we are so hedged about by a multiplicity of little-known laws, orders and regulations, many of us must do what we "didn't orter" at one time or another without being aware of the fact. The charge of making unlawful use of wireless telegraphic apparatus, in that he received a

police message when not authorized by the Postmaster General to do so, brought recently against an army officer is a case in point. The Andover magistrates very sensibly granted the accused an unconditional discharge, the chairman remarking that not one member of the bench had previously realized that it was an offence. If you own a receiver covering Band II, you can hardly fail to pick up such messages at times. I've often done so when tuning in Wrotham; in fact, I recall puzzling our local police superintendent one day by saying: "I hope you got that report off all right." "What report do you mean?" "Why, the one that headquarters was gingering you up about by wireless this morning." I wasn't run in.

## Offenders in Spite of

## Ourselves

If the authorities are going to make a practice of bringing such charges, one foresees that they'll have their hands pretty full when the B.B.C.'s Band II system gets into its stride and v.h.f. sets are in use in homes everywhere. And what of those who have telephony from nearby police stations forced upon their unwilling ears by way of the loudspeakers of their television sets? Having filled up the appropriate forms, they beg the P.M.G.'s engineers to rid them of the nuisance, only to learn that occasional (or it may be frequent) breakthrough is inevitable at such short range. Will some legal reader of $W^{\prime} . W$. tell us whether such folk could charge the police with aiding and abetting them to break the law?


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#### Abstract

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| :---: | :---: | :---: |
| K. 400 | Knob |  |
| K. 410 | Dial* | $1 \frac{1}{2}{ }^{\prime \prime}(38.1 \mathrm{~mm}$.) $\varnothing \times 21$ S.W.G., engraved $0-10$ over $270^{\circ}$ |
| K.410/P | Dial* | ditto, not engraved |
| * Rivets to Knob; we will fit and river, if requested |  |  |



| List No. | Item | Dimensions, etc. |
| :---: | :---: | :---: |
| K. 402 | Knob | $\begin{aligned} & 18^{\prime \prime \prime}(41.3 \mathrm{~mm} .) \triangleq \times \frac{25^{\prime \prime}}{\mathrm{l}^{\prime \prime}} \\ & \text { high } \end{aligned}$ |
| K. 406 | Skirt | $\begin{aligned} & 2 \frac{1}{\hbar_{" \prime \prime}^{\prime \prime}} \\ & \text { thick } \end{aligned}$ |
| K. 412 | Dial | $\begin{aligned} & 2 \frac{3^{\prime \prime \prime}}{}(69.9 \mathrm{~mm} .) \varnothing \text { Ø } \times 21 \mathrm{~S} . \text { W.G., } \\ & \text { engraved } 0-100 \text { over } 180^{\circ} \end{aligned}$ |
| K.412/P | Dial | ditto, not engraved |



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## Talking Machines

I RATHER pride myself on historical accuracy and feel compelled to draw attention to a chronological inexactitude in an otherwise excellent article by S. Kelly on "Needles for Talking Machines" in the May issue.

Speaking of the needle or stylus the author says "Sapphire or diamond in 1900, steel needles from about 1910 to 1935 . . "" which surely implies that steel-needle machines were rare, or at any rate in the minority, before 1910. I have no statistics before me but relying on my memory of those years (which has often made the B.B.C. scrapbooks bite the dust) I venture to say that the author's statement is at least misleading.

Now let us get this matter straight. At the time of Queen Victoria's death (Jan. 22nd, 1901) there was certainly a large number of sapphire-using cylinder machines in use and I have one on the table before me as I write. But even then the needle-using disc machines were -if I may coin a word-"populescent" and by the time of King Edward's Coronation (Aug. 9th, 1902) had virtually stolen the market. Side by side with my Victorian cylinder machine I have the H.M.V. disc-and-needle-using "dog" model.

Sapphires were available with some disc machines, but, in the early years of the present century, which is the period in question, by far the greater number used needles only; in fact, it is not too much to say that discs necessarily meant needles. If I can be proved wrong I am willing to spend a night of penance on a bed of upturned steel gramophone needles like an Indian fakir.
The author is also rather misleading when, a little later in his article, he says "about 1910 the disc finally ousted the cylinder for domestic reproducers. ..." Surely this implies that the cylinder died with King Edward (May, 1910). Actually the cylinder, like Charles II was "an unconscionably long time a
dying" and although the process started long before 1910, it lingered on until after the beginning of the Kaiser's war.

Several cylinder machines are listed in Gamage's catalogue of 1913 and I recollect buying one for 3 s 6 d -yes three shillings and sixpenceand it certainly wasn't a toy one. It's only disadvantage over the more costly ones was that it would not take the famous Edison "Amberol" cylinders which were the L.P. "microgroove" records of the period. For these cylinders the screwed rod which moved the stylus across the record had a much finer pitch than the one normally used.

## Electronics in the Garden

IN THE SUMMER of 1940 I attended a lecture given by Dr. P. Dalton before the Brit. I.R.E. on the interesting subject of radio therapy. I remember how this new therapy affected the processes of the body and how it had been discovered. Apparently it had been found that wireless operators sitting near the works of powerful s.w. transmitters had suffered ill effects.

I have often wondered whether this therapy with its strong effect on normal biological processes could not be applied to our gardens to speed up the growth of plants and an item I spotted recently in an American newspaper has convinced me that it can. It has been observed that in the vicinity of certain high-powered television transmitters weedse grow wilder and tulips taller and I am getting to work immediately on the probiem.

If the editor keeps his promise to let us have $W$. $W$. on the fourth Tuesday of each month, this issue will appear on May 24th which is not only Queen Victoria's birthday but the day on which the present Queen will open the famous Chelsea Flower Show of the Royal Horticultural Society. I intend to be right there in the electrical section where they always demonstrate how our seedlings can
be warmed from the mains via a step-down transformer and a buried cable.
I am going to suggest that a compact oscillator unit working on TV frequencies is marketed enabling us to feed oscillations into a special transmission line and radiator buried among our plant roots or maybe suspended just above them. Frankly I don't know what will be the results as I'm no biologist but I remind myself that the scientists who detonated the first atom bomb in New Mexico in July, 1945, weren't any too sure about results.

## "Pidgin" Radio

IT IS an old saying that the lazy man works the hardest and I have been rather forcibly reminded of it by a few remarks that appeared in the correspondence columns of $W$.W. a month or two ago about wireless and mathematics. To my way of thinking the man who tries to take the "easy" way of trying to understand the intricacies of radio without a preliminary grounding in mathematics will find the going very heavy.

He generally proceeds by way of mechanical analogies which, seemingly apt and excellent at first, break down and leave the non-mathematical student stuck firmly in a mertal morass. The mathematical man, on the other hand, sails along without the necessity of conjuring up mental pictures of the phenomena which his equations represent.
An analogous state of affairs was often to be observed over a quarter of a century ago, when the homeconstruction phase of wireless was at its height. I frequently came across men who were very ardent and, indeed, very skilful home constructors who were unable to understand a "theoretical" circuit diagram, a form of shorthand which enabled the essentials of the receiver of that period to be seen literally at a glance. These earnest constructors, however, could and did follow the intricacies of the practical wiring plan with a skill and celerity which left me breathless and which must have needed a lot of hard work to acquire.

If I may be permitted to use an analogy after condemning them earlier in these remarks, the nonmathematical radio aspirant may be likened unto the speakers of "pidgin" English in New Guinea and elsewhere. To learn standard, or at any rate basic, English would take only half the time, pain, power and sheer hard work which they put into acquiring a knowledge of this truly astonishing lingo.


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he AVO Valve Characteristlc Meter Mark III offers the Radio Engineer far more than is generally implied by the words "a valve tester".
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## HIGH GRADE INSTRUMENTS for radio and electronic engineers

2 tin. scale moving coil A.C rectifier meter. Square flush mounting. Type $\mathbf{S} 25$.


$3 \frac{\mathrm{in}}{} \mathbf{2}$ moving iron $\mathrm{AC} / \mathrm{DC}$ meter. Round flush. Type $\$ 35$.
"Fulscale" meter 4in, dia scale moving coil having $270^{\circ}$ arc with a 9 in. scale length.



High torque moving coil portable meter. Precision grade to BS.89.


METERS


Ohmmeter for the rapid and direct measurement of very low values of resistance. Model RM. 155.

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These represent just a ferw of our wide range of high quality instruments which


Breakdown Tester for measuring the breakdown voltage of electrical components and insulating materials. . Model RM. 215. are used by the electrical and electronic industries. Maywe supply you withour comprehensive catalogue?



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The screen of the DG16-21 cathode ray tube is a rectangle measuring $5 \frac{1}{2} \times 1 \frac{1}{2}$ inches - the logical shape for radar ' $A$ ' scan and many instrument applications. A number of these tubes can be stacked vertically to provide multiple displays within a confined space... they are the answer to those problems in design where circular tubes make equipments excessively bulky.

$\Omega \Omega$ comparison

## for multiple trace

Deflection : Electrostatic,
symmetric or asymmetric.
$V_{h}: 6.3$ volts.
$I_{h}: 0.3 \mathrm{amp}$.
Base: B14A.

TYPICAL OPERATING CONDITIONS

| $\mathrm{V}_{\mathrm{a} 3}$ | $\mathrm{V}_{\mathrm{a} 2}$ | $\mathrm{Val}_{\text {I }}$ | $\mathrm{V}_{\mathrm{g}}$ | Deflection Sensitivity |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 5,000V | $\begin{aligned} & 600 \text { to } \\ & 700 \mathrm{~V} \end{aligned}$ | 1,800V | $\begin{aligned} & -25 \text { to } \\ & -70 \mathrm{~V} \end{aligned}$ | $S_{x}$ | $S_{y}$ |
|  |  |  |  | $0.19 \mathrm{~mm} / \mathrm{V}$ | $0.21 \mathrm{~mm} / \mathrm{V}$ |

The DG|6-2| has a green luminescent medium persistence screen. Versions with other screens are contemplated and your comments are inyited.

> See Mullard Cathode Ray Tubes and Valves on STAND No. 23-BLOCK F BRITISH INSTRUMENT INDUSTRIES EXHIBITION Earis Court, 28th June to 9 th July

## 

## NEW!! For TV Band III

## Taylor Signal Generator

For Television frequencies up to $240 \mathrm{Mc} / \mathrm{s}$.

## Model 67A

Frequency rangé: $100 \mathrm{kc} / \mathrm{s} .-240 \mathrm{Mc} / \mathrm{s}$. in six ranges.
Accuracy: $\pm 1 \%$.
Attenuation: 100 dB . Continuously variable.
Modulation: 400 cycles, $30 \%$ depth.
Output impedance: 75 ohms.
Direct A.F. output provided.
Cash Price $£ 22 /$-j- Prompt Delivery
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## Taylor TV Sweep Oscillator

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Covering Band III
Frequency-modulated oscillator designed for the rapid and accurate alignment of TV receivers. Also suitable for checking any band pass amplifier.
Frequency range: $5-250 \mathrm{Mc} / \mathrm{s}$.
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STAND NO. 27. Block 'A.' British Instrument Industries Exhibition (June 28 to July 9)


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## Response is not all the story

$\mathrm{T}_{\text {нe }}$ Frraogaph was the first portable Tape Recorder to be designed and wholly manufactured in Britain. To-day the bewildered buyer may well hesitate when confronted with a choice of so many makes offered. But if he is serious - and not lightly choosing something for his casual enjoyment - he would do well to ponder the following fact.

Frequency response is often popularly quoted in advertisements as 50-12,000 c.p.s. This, of itself, means nothing in evaluating the excellence or otherwise of a recorder. Two other interdependent factors must be regarded, viz.-signal/noise ratio and distortion, if the true worth of the instrument is to be gauged.

Furthermore, the limits in which the response is held must be given or the statement is again valueless. The Ferrograph frequency response is guaranteed to be within $\pm 3 \mathrm{db}$ up to 10,000 c.p.s. at


BRIEF SPECIFICATION
Twin Track (to International standards)
Playing British and American pre-recorded tapes
Playing Time with 1,750 ft. Reel 45 minutes per track at $7 \frac{1}{2}$ i.p.s. (other speeds prorata)

Quick Rewind
in less than 60 seconds
Signal Level Meter
giving positive reading
Frequency Response
$\pm 3 \mathrm{db} 50 / 10,000$ c.p.s. at $7 \frac{1}{2}$ i.p.s.
"Wow" and Flutter Less than $0.2 \%$ at $7 \frac{1}{2}$ i.p.s.
Signal to Noise Ratio Better than $50 \mathrm{db}, 200 / 12,000$ c.p.s. Unweighted, including hum, 45 db .
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Less than $5 \%$ variation
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$2 \frac{1}{2}$ watts into 15 ohms

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They like the unique integrated feedback to provide complete stability independent of phase changes in the load current . . the method used for eliminating the loop gain outside the audio range without prejudice to the input signal . . . the way that feedback is again used to provide optimum design stage by stage and to control the effective time constants. They like its use yet again to provide a unique self-balancing phase changer without the usual asymmetry to the H.T. line. They like, too, the fact that the specification is fully met with commercially tested valves without matching or alignment of any kind. They extol the conservative ratings and restoration from overload (several nation-wide broadcasting corporations officially uprate the output to 20 watts, since with this degree of overload, distortion


Linearity and overload of the QUAD II amplifier
The QUAD II power amplifier is primarily designed as part of the complete QUAD II amplifier. The power amplifier is also supplied separately as a quality standard when with a suitable input transformer it can be fed direct from a 600 ohm line.
*The unique output stage design principles are discussed in Wireless World, September, 1952.
acoustical manufacturing co. LTD., huntingdon, England

## announcing the

## 2400 rear



A Relay of noteworthy dimensions, designed in size and performance to suit present day electronic equipment. The new 2400 Relay is available with twin light duty or single heavy duty contacts.
When fitted with a 10,000 ohm coil, the pull-in is approximately 4 milli-amperes; contact pressure and clearance have not been sacrificed to achieve this sensitivity
DIMENSIONS: Above chassis $2 \frac{1}{2}^{\prime \prime}$ high $\mathbb{X} I^{\prime \prime}$ wide $\mathbb{X} \frac{5}{8}{ }^{\prime \prime}$ deep. WEIGHT: 4눌 ounces.


## TRANSFORMER PROBLEMS WE HAVE SOLVED...

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# SIGNAL GENERATORS for the frequency range $30 \mathrm{c} / \mathrm{s}-30 \mathrm{Mc} / \mathrm{s}$ 

## L. F. SIGNAL GENERATOR TYPE 702

- Frequency Range: $30 \mathrm{c} / \mathrm{s}-30 \mathrm{kc} / \mathrm{s}$.

Stability: $\pm 0.05 \% \pm 0.5 \mathrm{c} / \mathrm{s}$.
Output: A screened and balanced transformer enables balanced, unbalanced and fully floating outputs to be obtained.

- Attenuator: A 600 ohm constant impedance attenuator provides steps of 20,40 and 60 db of attenuation under all output conditions.
- Output Level: 100 mW into 600 ohms or 15 volts open circuit.



## H. F. SIGNAL GENERATOR TYPE 701

- Frequency Range: $30 \mathrm{kc} / \mathrm{s}-30 \mathrm{Mc} / \mathrm{s}$.
- Output Level: Constant to within 1 db over entire frequency range.
- Output Impedance: 75 ohms $\pm 10$ ohms on the 0 db step of the attenuator and 75 ohms $\pm 3$ ohms on all other settings.
- Attenuators: A slide wire and step attenuator calibrated both in db and volts open circuit enable the output to be reduced to 1 microvolt.
- High Output: A signal voltage of from 5-20 volts is available from a high impedance output socket.

The L.F. Signal Generator Type 702 may be connected to the H.F. Signal Generator Type 701, to enable signals over the complete frequency range $30 \mathrm{c} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ to be obtained from the output plug of the latter instrument.

Full details of these or any other Airmec instruments will be forwarded gladly upon request.


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a lightweight mobile transmitter/receiver 68U

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Prompt Delivery, all types, $2,000-20,000 \mathrm{kc} / \mathrm{s}$ When ordering $10 X$ replacements, why not use our hermetically sealed Type $2 X L$ ?

## CATHODEON CRYSTALS LIMITED

LINTON•CAMBRIDGESHIRE. TEIEPhoneLINTON 223



ALUMINIZED CATHODE RAY TUBES
THE EDISON SWAN ELECTRIC COMPANY LIMITED, 155 Charing Cross Road, London, W.C. 2 and Branches. Member of the A.E.I. Group of Companies.

'Grams: Attenuate, Wolt, London.


$\square$ Stamford Works, Broad Lane, Tottenham, N. 15 Telephone: Stamford.HIII 5606 (3 Ines)



Features that the enthusiast will appreciace are the suppression of switch clicks, the extra heavy balanced turntable, and the very fine degrees of speed control available. Each of the nominal speeds, 78,45 and $33 \frac{f}{f} \mathrm{r} . \mathrm{p} . \mathrm{m}$. can be adjusted by approximately $2 \frac{1}{2} \%$. Wow and Flutter have been reduced to less than $0.2 \%$ and less than $0.05 \%$ respectively. The model is equipped for dual voltage ranges of 100 to 130 and 200 to 250 volts, 50 or 60 cycles
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is fully tropicalised and is supplied complete with plastic stroboscope, special grease,
all fixing screws, washers, remplate and instruction manual
Supplies are limited, see your dealer now.
EARRARD ENGINEERING AND MANUFACTURING CO. LTD.


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There may be an art in making good coffee, but even with the most fragrant brew the filtration problem is quite a simple one: to separate the infusion from the grounds which have a size ratio of $1: 10,000$. By comparison, many electrical filters are called upon to discriminate between wavelengths whose ratio is only $1: 2$. What is more, they must maintain their performance, with scientific accuracy, in spite of varying temperature; they must be economical ; they must be small. If this kind of conflicting requirement is giving you a headache you will find strong,

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## Suflex Polystyrene Capacitors

- High Q
- Excellent stability
- Compensating negative temperature coefficient

A quality component which may be economically used in commercial equipment

The 12 -inch Audiom 60 is a versatile single-cone medium heavy duty reproducer with an outstanding smoothness in response and performance. It is available with $\mathbf{3 5}, 55$ or 75 c.p.s. bass resonances, the first two types being ideally suited for use as bass units in crossover systems.


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| Nett Weight | 121b. $13 \mathrm{oz}$. ( 5.8 kg.$)$ |
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Three element array with cranked mast and universal surface mounting bracket.
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Eight element array with $1 \frac{1}{2}$ in. mast cap 10ft. mast and heavy duty single chimney lashing equipment type 6.

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ASR-1150 has a pure output waveform, is unaffected by changes in mains frequency, and works equally well from no-load to full load, which is 1150 VA . It has a stabilised output at 230 V unless otherwise ordered.
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# The NEW "ASR-I|50" costs only £24 net 

# Output Level Stabilised to $\pm \frac{1}{2} \mathrm{db}$ 

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To the established features of the Wayne Kerr Video Oscillator has been added, at the suggestion of the B.B.C., a 50 cycle Square Wave for the examination of the low frequency characteristics of Video networks. This output is achieved by interrupting a stable D.C. Source with a polarised relay energised from the mains. The rise time of the square wave is better than $0.02 \mu \mathrm{sec}$.

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FREQUENCY RANGE:
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OUTPUT RANGE: $\quad+10 \mathrm{db}$ to -50 db on 1V p-p.
Level: Constant to $\pm 0.5$ dbatany Frequency
Impedance: $75 \Omega$. [setting. TOTAL HARMONIC CONTENT: Less than $1 \%$.

In transportable case $£ 155$, or for standard $19^{*}$ Rack mounting £148.

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## POWER

## RECTIFIERS

These Mercury Vapour and Xenon filled power rectifiers are robust and can be relied upon for long and satisfactory service. The output table shown herewith is calculated for a three-phase, full wave arrangement. Full technical data and operating instructions
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Ready-to-assemble Bass Reflex Console Cabinet for $10^{\prime \prime}$ or $12^{\prime \prime}$ unit $£$ Io. 1o.o. Corner Console Cabinet for $8^{\prime \prime}$ unit £5.10.0.

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De luxe version of the "Editor" incorporating mixing and monitoring facilities and single knob control super tape deck. IDEAL FOR USE WITH PRE-RECORDED TAPES. In padded simulated crocodile case. For $200-250$ v. A.C. mains.
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BRIEF SPECIFICATION
$\star$ High Fidelity twin track recording heads $\star$ Infinite impedance output ensuring perfect matching $\star$ Powered by specially designed motor $\star$ Minimum wow and flutter $\star$ Built-in 3 -stage specially matched pre-amplifier with miniature Mullard valves $\star$ Weight 161 b . $\star$ Overall size $12 \frac{1}{2} \mathrm{in} . \times 10 \mathrm{in} \times 4 \frac{1}{2} \mathrm{in}$. $\star$ For use on A.C. mains $220 / 250 \mathrm{v}$.

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S.L. 86


## For Low Voltage or Mains

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 PERMANENT MAGNETS are used in this new FERRANTI RIBBON PICK-UP(designed by D. T. N. Williamson)

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STAND 5 (Block B) BRITISH INSTRUMENT INDUSTRIES EXHIBITION, Earls Court, JUNE 28-JULY 9


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1.6-14 \mathrm{Mc} / \mathrm{s}
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Newly designed to use the most modern valves and components available, this station incorporates local or remote pushbutton selection of up to four channels, remote control being possible to a distance of 15 miles.

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Technically identical with the world-famous Deck supplied, in bulk, to Recorder Manufacturers. With B.S.S. sense of tracking, it is fully approved for playback of pre-recorded tapes. List Price remains ot 22 gns.

Detalls of complete recorders incorporating the TRUVOX Tape Deck are avallable on request.

The full range of Truvox Tape Recorder Components and Accessories is listed below-send for fully descriptive leaflets.

> TAPE DECKS • AMPLIFIER • RADIO JACKS •FOOT CONTROL. TELEPHONE ADAPTOR • MONOSET \& STETHOSET HEADPHONES - CORNER DIFFUSION SPEAKER

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First introduced in 1938, this 10 in . speaker has been improved in stages and now embodies the following details of good design:

Flux density 14,000 lines. Total flux 74,000 lines. Rigid, open, die-cast chassis.
Cone with bakelised apex and special radial corrugations.
Centring device in bakelised fabric.
Aluminium dome.
Cloth suspension, which involves hand-assembly by experts who have attained a world-wide reputation.

Bass resonance now $45 \mathrm{c} / \mathrm{s}$.
Any speaker maker could produce a loudspeaker including some or all of these specifications. Only WHARFEDALE can produce one which sounds like the W10/CSB.
After the Super $12 / \mathrm{CS} / \mathrm{AL}$-which costs $£ 17$ 10s. Od.the W10/CSB is the best single speaker in the Wharfedale range. At $£ 95 \mathrm{~s}$. 0 d . plus $£ 3 \mathrm{ls}$. 6 d . P.T. the performance is outstandingly good; some idea of the frequency range is given by the response curve.


## Wharfedale Wireless Works Ltd.,



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"MAXI-Q" IS THE REGISTERED TRADE MARK OF DENCO (CLACTON) LTD. IT IS ALSO A MARK OF TECHNICAL SUPERIORITY AND GUARANTEED QUALITY

Coverage from 3.8 to 2,000 metres in 7 ranges-Each coil is packed in an aluminium container which may be used as a screening can for the coil itself-Brass threaded adjustable iron cores-Colour coded moulded polystyrene formers-Chassis/Plug-in Technical Bulletin DTB. 1 1/6-Dual Purpose Technical Bulletin, DTB. 4 1/6 - Colour Code Identified Coils: BLUE Signal Grid Coil with Aerial Coupling winding-YELLOW Signal Grid Coil with intervalve coupling windingGREEN Grid Coil with reaction
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Obtainable from all reputable stockists or in cases of difficulty direct from works.
General Catalogue covering technical information on full range of components $1 /$ - post paid.

[^6]
'Frequentite' is the most suitable insulating material for all high frequency applications. Seventeen years ago we introduced the first British-made low-loss ceramic, and consultation with us before finalising the design of new components is a wise precaution.

## WHY ENGINEERS SPECIFY EGEN

 potentiometers-Egen Potentiometers are based on long experience of requirements of television and electronic equipment manufacturers. In design, dependability, accuracy and freedom from wear they are outstanding, but, above all, they are completely NOISELESS.

DUAL POTENTIOMETERS with concentric operating
 spindles. The new Egen Dual Potentiometers incorporate all these outstanding design features -multiple contact rotors, smooth easy movement, thorough screening between sections, plus a convenient soldering tag for earthing screened connections on each metal case. Switch and Potentiometer soldering tags are of high-grade brass heavily silver plated for easy soldering; they are positively located and withstand soldering heat and bending without loss of rigidity. Control spindles can be supplied to suit customers' requirements.

PRE-SET POTENTIOMETERS. Completely enclosed in high-grade phenolic mouldings. Solder tags heavily silver plazed for quick soldering. Fully insulated spindles with integral control knobs. Tapped for 2 -hole 6 B.A. fixing on $\sum^{2 /}$ centres. Type 126, wire-wound. Type 127, carbon.


STANDARD CARBON POTENTIOMETERS. Made by an entirely new method ensuring a highly stableresistance element, which is also very durable. Silent and smooth in operation, these controls offer both mechanical and electrical reliability. Soldering tags are heavily silver plated to resistoxidisation, and the mains switch has an efficient quick make-and-break action.

PRE-SET RESISTOR. This has a wire-wound resistance element, traversed by a nickel-silver slider. Adjustment is effected by a worm drive spindle fitted with a knurled and slotted knob. This component is smooth and noiseless in action and is designed to meet the many and varied requirements of the Electronic Industry. Egen pre-set resistors can be supplied in multi-bank assemblies to suit individual requirements. There are also twin-track models, and types with an electrically divided slider, giving adjustment on two resistors with
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| T | $t$ watt | $\frac{1}{2}$ watt | 250 | 10 ohms | $5^{*} \times \frac{1}{3}$ |
| R | $t$ watt | watt rance ava | $500$ | $\begin{aligned} & \text { megohms } \\ & 10 \%, 5 \% \end{aligned}$ | ギ× が |
| HIGH STABILITY RESISTORS |  |  |  |  |  |
| H53 | 1 watt | t watt | $750$ | 10 hm to 500 | $1.1{ }^{\circ} \times 0.1 \%$ |
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|  |  | WIREWO ms to 100 | VD RES ohms | ORS <br> 10 watts |  |
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TYPE 545 -This new high-speed laboratory oscilloscope, in combination with new Type $53 \mathrm{~K} / 54 \mathrm{~K}$ Fast-Rise Plug-In Unit...opens the way to quicker, easier analyses of fast-rising waveforms... providing faithful displays and accurate measurement facilities well beyond the range of previous oscilloscopes of its size and cost. The Type 545 -Type $53 \mathrm{~K} / 54 \mathrm{~K}$ combination offers a vertical-amplifier passband of dc to 30 mc ( 12 -millimicrosecond risetime) at calibrated sensitivities to $0.05 \mathrm{v} / \mathrm{cm}$, with a full $4-\mathrm{cm}$ linear vertical deflection. A wide range of calibrated sweeps, with calibrated sweep delay from $1 \mu \mathrm{sec}$ to 0.1 sec , and high accelerating potential, 10 kv , fully complement this greatly extended vertical-amplifier range.

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Input impedance $20 \mu \mu \mathrm{f}$, 1 megohm.


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| P450 | $2.5 \mu \mu \mathrm{f}, 10$ megohms | $2.5 \mathrm{v} / \mathrm{cm}$ |
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## Type 545 Oscilloscope Characteristics

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NO. 1 -SYMPHONY "TUNER. A T.R.F. model designed for the quality reception of local stations. Quality is adequate for ampliffers of the highest fidelity class. Inflaite Impedance detection. Controls: gain, wave-change and radio/gram miniature valves. Overall dlmensions: 9 in. wide $\times 6$ in. deep $\times$ bin. high. Power required: 6.3 v . at 1 amp. and $250 / 300$ v. at $15 \mathrm{~m} / \mathrm{a}$. Price $£ 7-7-0$ Carr. of nkg. $5 /$.


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No. 2/VS "SYMPHONY" SUPERHET TUNER. As No. 2 but incorporating on the wave-change switch an extra position for radio, thus making two radio positions. One is the standard one with 9 kc, separation and the extra one providing virtually T.R.F. band-width and quality on local stations. Price fl3-13-0. Carr. \& pkg. 5/All above tuners are made to plug in to any of our "Symphony" Amplifiers In a matter of seconds by means of the octal plug fitted at the end of a flexible multi-cable. They are ideal for providing in conjunction with our "Symphony " Amplifiers, the same high quality on radio as is obtained from these amplifiers on gramophone, but they are equally suitable for use with other high fidelity amplifiers, and where the output circuit requires modification to match a given amplifier this can be caited with a magic eye tuning indicator for $£ 2-2-0$ extra. Furthermore, they can be fitted with a pre-amplifying stage to match the Decia Magnetic Piekups or the Collaro Studio type "p" pickup head for use with Pickups or the Collaro Studio type $p$ pickup head for use with
amplifiers which would not otherwise have enough gain for these amplifiers which would not otherwise have enough gain for these comparatively low output pickup heads. In these cases, two separate by the pickup manufacturers-are incorporated in the radio/gram switch Please send for our catalogue giving further details.

## TAPE DECKS AND AMPLIFIERS

TRUVOX TAPE DECK MARK III. TR2/U. Latest version to take pre-recorded tapes. Price 22 gns . Illustrated leaflet $2 \frac{1}{2} d$. TAPE AMPLIFIER TYPE C, expressly designed by Truvox to work perfectly with their Deck, 3 valves plus rectifier and Magic Eye level indicator. Price 16 gns .

NEW MODEL PORTABLE RECORD PLAYERS


We are pleased co announce the entry on to the market of two "Symphony" Record Players designed to represent the greatest value in this line ever offered. Model No. I contains the Collaro 3-speed single record playing unit AC3/554 and modal No. 2 contains the Collaro Autochanger RC54. They are available with either Type "O" insert, "p" insert or transcription insert. Prices (in attractive rexine case), No. 1 £10-19-6, No. 2 E14-19-6. Carr. '7/6. Transsription insers $6 / 9$ extra.

GOODMANS CORNER CABINETS (right) for the AXIOM 150 Mark 2 manufactured by us to Messrs. Goodmans' specificatior. and approved by Messrs. Goodmans. Helght, 44 in . Price: complete kit in plain board with lin, chick felt, 8 gns. Price: ready built, 10 gns. Finished in figured walnut, 16 gns. Other veneers to order Carriage extra according to area. Quotation by return.


a perfect performance at low price SAIFORD ELECTRCAI INSTRUIIINIS LTD. PEEL WORKS • SILK STREET • SALFORD. 3 • LANCS LONDON OFFICE : MAGNET HOUSE • KINGSWAY WC2 Tre: Temole Bor of 669

A Subsidiary of THE GENERAL ELECTRIC COMPANY LTD OF ENGLAND

# RETOLLITIOHIRI in designsund performance! 

# HLNTS "THERYETIC" MIDGET METALLISEID PAPER rapacitors with a true hervetic seal fllly approved to Joint services stavdarid r.c.s.i36/a CATEGORY 40/100, CLASS II.I. 

THMMPERATUREE FAMTE : $-100^{\circ} \mathbb{C} 0+1690^{\circ} C$

The W97 capacitor, although of diminutive size, is an extraordinarily robust unic. Most miniature units are prone to weakness in end connections and general mechanical flimsiness. Such undesirable features are eliminated in the W97 by the special processes used and extreme care in manufacture. CAPACITQR UNIT
A single metallised paper is used to wind this unit which is made possible by the use of Hunt's Patent covering the "castellated" pattern. Recent development by Hunt on a special impregnating material gives the unit remarkable brackets of operating temperature.

## CASING

Hunt's patented double metal tube, sealed with the special "Thermetic" compound, provides positive closure on the casing and lead entry, ensuring positive hermetic sealing.
INSULATION OF CASING
The capacitors are supplied $v$ ithout an insulating medium on the casc. If specially requested they $\mathrm{ra}_{3}$; be supplied with, an approved plastic sleeve which increases the dimensions by $0.07^{\prime \prime}$ in length and $0.03^{\prime \prime}$ in diameter. TERMINATIONS
The terminations are of 24 gauge tinned phosphor bronze wire having an nominal length of 1 ". Special attention is paid to the retinning of the wires after the capacitor is fully processed. Connection is made to the unit by applying copper spray to the metallising. The pigtail is soldered to this bond giving a perfect connection of exceptional strength.

## INDUCTANCE

W97 "Thermetic" Midgets have a very high self resonant frequency-the following figures are quoted as a guide. 50 pf at 600 volts, which is the lowest capacitance in the range, has a self resonant frequency of 280 megacycles. At the other end of the range, $0.04 \mu \mathrm{~F} 200$ volts, which is the maximum capacitance, it is 8.5 megacycles.
INSULATION RESISTANCE
This is measured at working voltage at a temperature of $20 . \mathrm{C}$. The minimum capacitance in the range, 50 pF at 600 volts, has an insulation resistance greater than $2,000,000$ megohms. The maximum capacitance in the range 0.04 山F at 200 volts, has an insulation resistance greater than 25,000 megohms. The intermediate capacitances are approximately pro rata.
POWER FACTOR
Less than $2 \%$ at 1,000 cycles per second at 20 C .
CAPACITANCE TOLERANCE
Stanjard $\pm 20 \%$. Closer tolerances are available, for capacitances exceeding 500 pF .

## W97 IS A 'MUST' <br> for the <br> MAKERS OF ELECTRONIC EQUIPMENT

A. H. Hunt (Capacitors) Ltd, Wandsworth S.W.18- BAT 1083 And in Conado: HUNT CAPACITORS (Canada) Ltd., AJAX, ONTARIO.

LIST CAP $\mu F$. DIMENSIONS (inches)

| NO. |  | L. <br> Wkg. | D. |
| :--- | :---: | :---: | :---: |
|  | 200 voles D.C. | Wk. |  |
| BM7 | 0.002 | 0.610 | 0.135 |
| BM8 | 0.004 | 0.610 | 0.135 |
| BM11 | 0.004 | 0.500 | 0.180 |
| BM9 | 0.005 | 0.610 | 0.135 |
| BM12 | 0.005 | 0.500 | 0.180 |
| BM13 | 0.01 | 0.500 | 0.180 |
| BM14 | 0.02 | 0.610 | 0.180 |
| BM15 | 0.03 | 0.610 | 0.260 |
| BM16 | 0.04 | 0.610 | 0.260 |


|  | 400 volts D.C. | Nkg. |  |
| :--- | :---: | :---: | :---: |
| BM4 | 0.0004 | 0.610 | 0.135 |
| BMS | 0.0005 | 0.610 | 0.135 |
| BM6 | 0.001 | 0.610 | 0.135 |
| BM18 | 0.002 | 0.500 | 0.180 |
| BM19 | 0.003 | 0.500 | 0.180 |
| BM20 | 0.005 | 0.610 | 0.180 |
| BM21 | 0.01 | 0.610 | 0.260 |


|  | 600 volus D.C. | Wkg. |  |
| :--- | :---: | :---: | :---: |
| BM25 | 50 | pF. | 0.500 |
| BM1 | 0.0001 | 0.610 | 0.180 |
| BM26 | 0.0001 | 0.500 | 0.135 |
| BM2 | 0.0002 | 0.610 | 0.135 |
| BM27 | 0.0002 | 0.500 | 0.180 |
| BM28 | 0.00022 | 0.500 | 0.180 |
| BM29 | 0.00025 | 0.500 | 0.180 |
| BM3 | 0.0003 | 0.610 | 0.135 |
| BM30 | 0.0003 | 0.500 | 0.180 |
| BM36 | 0.0004 | 0.500 | 0.180 |
| BM31 | 0.0005 | 0.500 | 0.180 |
| BM32 | 0.001 | 0.500 | 0.180 |
| BM33 | 0.002 | 0.610 | 0.260 |
| BM34 | 0.003 | 0.610 | 0.260 |
| BM35 | 0.004 | 0.610 | 0.260 |

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- Heavy Duralumin Baseplate $15^{\prime \prime} \times 11 \frac{1}{2}$ "
- Three independent motors
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- Interlocked switching
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- Fast forward or reverse in 45 seconds
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- Azimuth adjustment to Record/Playback Head

BRENELL RECORDING AMPLIFIER ALSO AVAILABLE I6 $\frac{1}{2}$ GNS BRENELL ENGINEERING CO. LTD., 2 NORTHINGTON, ST., LONDON, W.C.I.

## Protection against damage from IMPACT and VIBRATION <br>  <br> TYPE GBC 1000 <br>  <br> TYPE GBC 2000

" BARRYMOUNT" cup-type isolators are designed primarily to absorb high-impact shocks with concurrent isolation of frequencies above 40 c.p.s. and general sound isolation. Utilisation of rubber in compression with substantially equal stiffness in all directions provides a smooth load-deflection curve.
Load ratings indicated for Mobile Applications (including shipboard installations) are such as to ensure a vertical natural frequency between 25 and 35 c.p.s. The design and assembly of the metal parts are such that they are self-captivating for maximum security.

Samples are available immediately ex stock

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"Barrymount" isolators are made in England under licence from Barry Controls Incorporated o' U.S.A.

## BARRY ( B MOUNT



# mith the brilliant WEW Superspeert SOLDERING IRON 

## STAR FEATURES

* Heats up from cold in 6 seconds-by a light thumb pressure on the switch ring.
* When not in use, current is automatically switched off-thus greatly reducing wear of copper bit. Electricity consumption is correspondingly reduced.
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* Can be used from a car battery.
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Designed on an entirely new principle, this light-weight, versatile iron is eminently suitable for soldering operations in the RADIO, TELEVISION, ELECTRONIC and TELECOMMUNICATION industries, particularly for all SERVICE work. For general purpose work the Superspeed Iron is the ideal stand-by soldering tool.

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SIZE: LOUDSPEAKER:...................... $6 \frac{1}{3}$ in. built-in Monitor POWER SUPPLY: ............ 200/250 o. 50 cucles A.C INPUT CHANNELS:...... High impedance for microphone; tow ar high impedance for radio POWER CONSUMPTION: ......... 100 watts approx RESPONSE: $\qquad$ 50-12,000 c.p.s. $\pm 3 \mathrm{db}$


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48-50 GEORGE ST., LONDON, W.I. Phone WEl beck $237 /$ ( 5 lines)

* Monomaster Finger-tip contro!
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* Simple loading
$\star$ Fasl rewind and wind-on
Servo self-energising brakes provide very rapid slop from full speed


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THE E-F TECHNBCAR ADYISORY SERYICE
Regardless of whether your magnetic amplifier problem is simple or complex, the fact remains that the only reliable solution is that whtch entirely eliminates risk.

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The Venner Lightweight Silver-Zinc Accumulator is ideal in every application where minimum size and weight are essential. It is particularly suitable for radio and "walkie-talkie" equipment.
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 THE B. 30 SERIESThese packs have been developed to provide an answer to the problem of reliable operation on overcrowded broadcast bands. The use of an R.F. stage results in much improved sensitivity and selectivity.

UP TO 4 WAVE BANDS - GRAM. SWITCHING
Fully tropicalised, iron-cored coils wound on moulded bakelite formers. Ceramic based, compression-type trimmers. Close tolerance silvered mica padders.

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Coverage $12.5-550 \mathrm{~m}$. in 4 bands.

| B32/G - TUNING CAPACITY | $483-532 \mathrm{pF}$. |
| :--- | :--- | :--- |
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Coverage 12.5-37, 33-100, 190-550 \& 800-2,00C m.
B34/G - TUNING CAPACITY $483-532 \mathrm{pF}$.
B35/G - " $\quad$ 354-399 pF.
Coverage $16.50,190-550 \& 800-2,000 \mathrm{~m}$.
PRICES: B30-33 93/9 + $30 / 6$ P.T.
B34-35 84/5 + 27/5 P.T.
FOR USE WITH THESE I.F. TRANSFORMERS
WEYRAD TYPES
P.3, P.4,
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Operating at
465-479 Kc/S.
A very wide choice of I.F. stage arrangements is possible. The types listed cover transformers of the highest possible electrica and mechanical quality, low cost versions for manufacturers and special types providing variable selectivity characteristics.
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$9 / 10$ each
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P.5.A ............................................ 10/- each

WEYMOUTH RADIO MFG. CO., LTD.
CRESCENT STREET, WEYMOUTH, DORSET


# ANNOUNCEMENT FM RECEIVER ALIGMMENT GENERATOR MODEL 1324 

This Alignment Generator will be available later this year to provide the Service Engineer with a compact test set with which all essential alignment procedures on FM Broadcast Receivers may be undertaken.
Accurate trimming for correct overall and IF response curves is easily carried out and facilities will be provided for discriminator alignment and checks on its sensitivity and distortion. Watch for the release date and price.

## Telecheck and Marker Generator for Bands I and III

Model 1322 - used in conjunction with a cathode ray oscillograph - provides equipment for the display, measurement and correct adjustment of RF and IF response curves of television receivers. This entirely new instrument comprises a swept oscillator covering the Television BANDS I and III ( $5-75 \mathrm{Mc} / \mathrm{s}$. and 155-255 Mc/s.) and a frequency marker oscillator so that precise calibration of the oscillograph display may be made ; accuracy of the frequency of the marker pips being verified by reference to an internal crystal. The
alignment oscillator is set to the video carrier to which the receiver is tuned and the sweep (either I $\mathrm{Mc} / \mathrm{s}$. or $10 \mathrm{Mc} / \mathrm{s}$.) is automatically derived from the time base voltage of the display oscillograph. The response of the "strip" under test to the frequency band applied is then presented on the screen of the cathode ray tube. The RF output of Model 1322 is available at 75 ohms and is adjustable from a maximum of 40 millivolts to a minimum of 10 microvolts through a coarse and fine attenuator.

## TELECHECK CONVERTER FOR BAND III

This adaptor provides owners of Model 1320" Telecheck " with an extension of the frequency range of the original instrument into the BAND III television channel. Thus, alignment procedures adopted for BAND I RF/IF "strips" are available also for BAND III receivers. A selection of the desired BAND is made by means of a switch. Pattern generator facilities for picture time base linearity checks have been retained. Model 1321 Adaptor is designed for permanent attachment to the standard "Telecheck " providing a neat, light and compact unit. Mounting is effected by four screws and the inter-connecting wiring is carried in a single insulating sleeve.

| BRITISA NSTRUMENT |  |
| :---: | :---: |
|  |  |
| INDUSTRIES |  |
| EXNIBITION |  |
|  | Tin ${ }^{\text {a }}$ |
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# Cossol 



Write for illustrated leaflets about both these instruments:


## The latest GOLDRING

variable reluctance CARTRIDGE No. 500
is the complete answer . . .
SEE TECHNICAL REPORT: "THE GRAMOPHONE," JAN. 1955

The No. 500 High-fidelity pickup cartridge, is earning a great reputation as a faultless link between records and amplifiers of the present day. DIAMOND STYLI NOW AVAILABLE

## $\star$ GOLDRING HICH QUALITY TRANSCRIPTION ARMS

The new Goldring High-quality transcription arm which features a cantilever counterbalance adjustable to give a range of stylus pressures, and is designed primarily as a worthy housing for the high-quality No. 500 cartridge. It is precision engineered, and, with the No. 500 cartridge, is virtually resonance-free. Two versions are available, one for home installations, and the other for professional use. Transcriptions up to $17^{\prime \prime}$ dlameter may be reproduced by the latter version.

TYPE TR/I For Connoisseur HOME APPLICATION. TYPE TR/2 For PROFESSIONAL APPLICATION Write for descriptive leaflets and technical information to:

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Type O-120


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Portáble, Lightweight, High-sensitlvity Audio 'scope. $4 \mathrm{mV} / \mathrm{cm}$. r.m.s. (max.). Push-pull Plate deflection. External terminal connections to " $X$ " Amplifier and C.R.T. available. $3 \mathrm{c} / \mathrm{s}$ to $25 \mathrm{Kc} / \mathrm{s}$.

Servo and General Purpose 'scope. $7 \mathrm{mV} / \mathrm{cm}$. r.m.s.
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## You are there...

The scream of a jet plane and the roar of a blast furnace run from one end of the audio frequency range to the other, but for really good reproduction a loud-speaker must have much more than just a wide frequency range.

Suitably mounted and driven, R. \& A. reproducers
have all the attributes to take you there.



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15 ohm. T.V. DOWNLPAD CABL? Nominal Attenuation at 50 M cs -2.5 dB '100 ft .
P.V.C Sheath.

Plain Copper Wire Braid

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1/.029" Ennealed Copper Conductor
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Specialists in


High quality electrical filter units built around Ferroxcube cores can now be supplied to communications equipment designers' individual specifications. These fllter units have significant advantages over comparable types designed without the use of Ferroxcube, particularly in the frequency range $300 \mathrm{c} / \mathrm{s}$ to $500 \mathrm{kc} / \mathrm{s}$. For audio frequencies the use of Ferroxcube cores permits the winding of compact coils with very high inductances. This results in a considerable reduction in the size and cost of the associated condensers and hence of the filter unit as a whole. The high $Q$ values obtained for a given volume, especially above $10 \mathrm{kc} / \mathrm{s}$, enable sharp cut off characteristics and low pass-band losses to be achieved, while negligible stray flux facilitates the production of compact and mechanically robust filters. Electrical filter units are among a number of high quality components now being made available by Mullard. Full details of the complete series of components will be gladly supplied upon request.

## Mullard

'Ticonal' permanent magnets Magnadur cepamic magnets Ferroxcube magnetic cores.


Robust construction, no seramics or mica to break or flake.
Greatest efficiency, elements situated under bits.

Heat-capacity ample for use on production lines.

Sole Distributors


Phane: ROYal 4439. Grams: (Overseas) "Antexlim London" SUPPLIERS TO H.M. \& FOREIGN GOVERNMENTS, LEADING ELECTRONIC, BEARING AID, INSTRUMENT, RADAR, badio, t/v, \& ELECTROI mEdiCAL imanuFacturers, HOSPITALS \& URIVERSITIES TEROUGHOUT THE WORLD

| Model | Consumption | Voltage | Bit Diameter | Weight | Length | Price | Spare Bits |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12 | 12 watts | 6, 12, 24 or 50 | 3/16" ( 4.8 mm ) | 0.5 oz | $65^{\circ}$ | 25/- | 2/0 |
| $11^{*}$ | 10 watts | 6 only | $5 / 32^{\prime \prime}(4 \mathrm{~mm})$ | 0.5 oz . | 6 " | 35/- | $7 / 6$ |
| 9 | 8.3 watts | 6, 12 \& 24 | $5 / 32^{\prime \prime}(4 \mathrm{~mm})$ | 0.25 oz. | 6 | 25/- | 1/8 |
| 6A | 6 wates | 6 anly | $3 / 32^{\prime \prime}(2.4 \mathrm{~mm})$ | 0.25 oz . | $6^{\prime \prime}$ | 25/- | 1/8 |
| 6 | 6 watts | 6 only | $1 / 16^{\prime \prime}(1.6 \mathrm{~mm})$ | 0.25 oz. | $6 "$ | 25/- | fixed bit |

## OSCLLLOSCOPE мовед 2300

This Model meets the need for a compact and robust instrument in which nothing has been sacrificed in order to achieve true portability. It has many of the facilities required in the laboratory as well as ruggedness demanded in the field. Note these features:

- Cathode Ray Tube diameter $2 \frac{3}{4} \mathrm{in}$. Square Wave Response adequate for Television synchronising waveforms.
- Direct-coupled $X$ and $Y$ Amplifiers.
- Hard-valve Time Base-range 7 c.p.s. to $50 \mathrm{Kc} / \mathrm{s}$.
- Deflection Sensitivity 50 mV . R.M.S./cm.
- Trace Expansion control from zero to 15 in .
- Frequency Response D.C. to 3 Weight: $6 \frac{1}{4} \mathrm{lbs}$. Size: $7 \frac{1}{4} \times 4 \frac{3}{4} \times$ Mc/s. $7 \frac{1}{4} \mathrm{in}$.

Full details of this and other instruments on application to:



# Osmor News 

OSMOR RADIO PRODUCTS Limited (Dept. W66) 418 BRIGHTON ROAD, SOUTH CROYDON, SURREY. CROYdon 5148/9

# NEW MINIATURE HIGH ' $Q$ ' COILS capable of terrific performance 

F.M. Frequency Modulation comes to the design of coils and a really first-class circuit of complete receiver and tuner. Free circuit, point to point wiring diagram, and full constructional information. (Send 5 d . in stamps.)

OSMOR ' $Q$ ' COIL PACKS Size only $1 \frac{7}{4} \times 3 \frac{1}{4} \times 2 \frac{1}{}$ with variable iron-dust cores and Polystyrene formers. Built-in trimmers. Tropicalised. Prealigned Re-ceiver-tested and guaranteed. Only 5 ceives-tested annections to make. All types for Mains and Battery Superhets Ideal for the reliable Ideal fortione of new construction or new sets, also for con-
version of the 21 version of the 21
Receiver.
TR1196, $\begin{array}{ll}\text { Receiver. } & \text { TR1196, } \\ \text { Type } & \text { Wartime }\end{array}$ Utility and others.
The NEW Osmor
'SWITCH PACK' is now ready! Complete and Prealigned full circuit included. State which station required. 2 M.W., 1 L.W. or 3 M.W. 48/= Inc. P. Tax.

## SUPER ' $Q$ ' For Maximum Selectivity

A full range is available for all popular wavebands and purposes. The magnetic screening of the cup prevents other components from absorbing the coil's power, thus
maintaining the high " $Q$ " value. Simple one-hole fixing. $\pm$ Only lin. high. $*$ Packed in dampproof containers. * Adjustable iron-dust cores. $\star$ Fitted tags for easy
connection.
L. or M.W. 5/- inc. CIRCUIT.


Send 5d. (stamps) for fully descriptive literature including Circuit and practical Drawings, "The really efficient 5 -valve Superhet,", 6 -valve s'het., 3-valve (plus rectifier) T.R.F. circuit. Battery portable Superhet circuit, Coil and Coilpack leaflets, and full radio and component lists, and interesting miniature circuits, etc.

OSMOR STATION 7/6 SEPARATOR COMPLETE The Separator may easily be tuned to eliminate any one station within one ranges stated and ranges stated and inso few seconds. Sharp tuning is effected by adjusting the brass screw provided. TXPE METRES TYPEMETRES TYPE MBTRES $\begin{array}{rrr}1-141.250 & \text { 4-319.405 } & \text { 7-1450.1550 } \\ 2-215.283 & 6-395-492 & 8-410-5501 / c .\end{array}$ 3-267-341 6-455.567
Our Technical Dept. will be pleased to answer any enquiry by manufocturers and athers relating to circuits which OSMOR coils or coil packs are used or are intended to be used.

## READERS' QUERIES!

Dears Sirs,
I want to add a little negative feed-back to my 5 -valve superhet. Please give me a simple scheme.

The simplest way to apply a measure of N.F. is to omit the bias decoupling capecitor of the ourput valve.
Dears Sirs,
I wish to insert a meter as an indicator when peaking your coilpack, and to determine the optimum signal. Please state a position which will not entail too much destruction of the wiring.

The meter may be placed across the bias resistor of the frequency changer. The meter must be a high-impedance $R F$ meter

PRE-STRETCHED PVC
BROWN OXIDE
HIGH OUTPUT
LOW BACKGROUND NOISE
EASE OF ERASURE
HIGH TENSILE STRENGTH
NON-CURLING

The QUALITY tape at
a competitive price...
$32 / 6$ per 1200 ft reel
On the well-known universal Ferrovoice Spool
600 ft 19/6
300 ft $12 / 6$

The popular FERROVOICE PAPER TAPE is still available



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[^8]
# VAIVES,THUBES \&゙ CTRCUT"S 

## 30. GERMANIUM DIODES FOR TELEVISION RECEIVERS

## Advantages and Disadvantages

The point-contact germanium diode can often be used with advantage in place of its thermionic counterpart. Its compactness and long life make it suitable for inclusion in a coil unit. It is robust and non-microphonic. The interelectrode capacitance is low. There is no heater, therefore supplies are simplified and a possible source of hum is eliminated. And the forward resistance is low, giving improved detection efficiency.

The main limitations of the germanium diode, namely, its reverse current at negative voltages and its relatively large temperature dependence, can be easily allowed for in circuit design and chassis layout. Earlier diode troubles, such as sensitivity to atmospheric moisture, have been eliminated by present-day manufacturing techniques.


## The Diode Characteristic

The general form of the germanium diode current/voltage characteristic is shown in Fig. 1. There are certain significant differences from the characteristic of a thermionic diode. The comparatively steep rise of the positive portion obeys an exponential rather than a three-halves power law, with forward currents which are normally of the order of 5 or 10 mA at 1 or 2 V . At high positive voltages, beyond the normal working range, the characteristic becomes nearly linear (that is resistive), without the saturation effect which is seen in a thermionic diode.

The negative characteristic shows not only a negative current for negative voltages, but also a rapid growth of this current if the voltage is made sufficiently great. In this region (which is well beyond the working range) turnover takes place, and the characteristic reverses. This condition produces overheating and a destructive runaway. The normal reverse currents are quite small (a few microamps) and, if the published temperature and peak reverse voltage ratings are observed, reverse currents have no: harmful effect.

The characteristic, as it changes from the positive to the negative region, passes through the origin, therefore at zero voltage there is no current flow. In the immediate vicinity of this point (say within $\pm 10 \mathrm{mV}$ ) the ratio of forward to reverse resistance becomes small, and detection efficiency is much reduced.

## High and Low Current Types

The steeply rising forward characteristic of a highcurrent type of germanium diode implies a comparatively large reverse current and a comparatively low turnover voltage. Conversely, the less steep forward characteristic of a low-current type gives an extended reverse characteristic. These contrasted pairs of features are the basis of the possible range of diode types. They are the key to the choice of type for a particular application, and they are important influences on circuit design.

## Temperature Effects

Germanium diodes are affected by temperature, and all ratings apply at specified temperatures. It is necessary for the circuit designer to take into account not only the air temperature which is likely to occur in the receiver but also any heat which may be transmitted through the chassis. The appropriate forward current and reverse voltage ratings must be observed if the diode itself is not to generate destructive heat. It is not to be assumed, however, that a germanium diode is excessively sensitive in this respect. The dangers have been mentioned only in order to draw attention to the temperature rating-a rating which is not normally of much consequence where thermionic valves are used.


FIG. 2
Fig. 2 shows the standard symbol for a germanium diode in parallel with the familiar diode valve symbol. The figure is intended to assist in the reading of circuit diagrams. The differences between the two kinds of diodes should, of course, be borne in mind.

Further advertisements in this series will discuss the employment of the diode characteristic in a number of typical applications in television and f.m, receivers.

Reprints of this advertisement, supplemented by data for Mullard diode types, are available without charge.

Mullard Ltd., Technical Service Department, Century House, Shaftesbury Avenue, London, W.C. 2


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## "BELLING-LEE" NOTES



There may be many readers who do not know the "Q Code." Q.S.L.? means "can you give me acknowledgment of reception," whilst Q.S.L. means "I am receiving you." It is customary amongst amateur transmitters and operators generally to acknowledge the reception of a signal by sending a "Q.S.L." card. We are following the practice, and are sending a card, reproduced above, as acknowledgment of every report of reception of G9 A.E.D., i.c., the "Belling Lee" experimental band III T.V. transmitter on the I.T.A. site at Beulah Hill, Croydon.

We would like the report to give the following information, name and address, type of aerial, nearest higher ground, height of aerial, type of receiver, interference (a) ghost (b) ignition. Sensitivity setting, picture quality, better/equal/worse combined with band 1. Date and time of observation.

The hundreds of reports already show a very healthy pattern over the whole of the service area shown by the I.T.A. map. When the I.T.A. go on the air with 60 Kw . against the "Belling Lee " 1 Kw., it will mean that everybody who received our transmitters will receive a picture about 10 times better. This will be due to the increased power and increased mast height. "Wireless World " readers will not need to be reminded that this does not mean reception at ten times the distance.

The report received at the date of going to press indicates that our suspicions and fears regarding ghosts have been justified, but the cure is easier than we thought possible, even if in our favour. Tests have been made with a band III dipole as a reference, and ghosts are received from church itowers, lightning arrests, electrical pylons and countless new objects, but in most cases they can be "laid" by the use of a multi-element array.
Generalising, the coverage from G9 A.E.D. is more satisfactory than we expected, but as we are still uncertain as to the effect that roofing materials will havé on higher frequencies, we are uncertain as to the ranges that are possible with indoor and loft mounting aerials. We have a reported case of reception on a "doorod" at twelve miles; but we do not attach a lot of importance to it. We believe it to be freak teception.

Advertisement of BELLING \& LEE LTD.
©t. Cambridge Rd., Enfield, Middx.数年, Written 18th April, 1955


## L. 576 HERMETICALLY SEALED TERMINALS

750 V . d.c. Working at 40,000 feet<br>I,500V. d.c. Working at sea level

These terminals, employing glass-to-metal seals, are made for bringing connections out of sealed transformers or other sealed components. Very useful as insulated pillars where high insulation is required. When mounted, they withstand instantaneous and repeated thermal shocks of at least $250^{\circ} \mathrm{C}$., and will support at least 40 lbs . per sq. in. air pressure without leakage. They are self-capacitant 1.45 mfds . Supplied tin-plated to permit soldering with modern resin cored solders, solder pastes, or solder rings.


## Special Features of Type W.M. 5

NUMBER 1-TIME AND VOLTS MEASURING SYSTEM

The unique E.M.I. visual null bridge measuring system with meter presentation of time and voltage, gives rapid and precise measurements which are independent of variations in amplifier or CRT linearity sensitivity or supplies

The illustrations show how easily various voltage or time-of-rise measurements can be made.

PROCEDURE:-

1. Measure Waveform volts peak to peak (using metered $Y$ shift volts control).
2. Align $10 \%$ point with cursor line junction (using metered $X$ and $Y$ shift controls).
3. Align $90 \%$ point with cursor line junction (using metered $X$ and $Y$ shift controls):
4. Read indicated time-of-rise from time meter.

Time Measurements: $100 \mathrm{~ms}-10 \mathrm{mys}$ ( 11 ranges) accuracy $\pm 21 \%$ FSD. Voltage Measurements: $100 \mathrm{mV}-500 \mathrm{~V}$ AC/DC (7 ranges) accuracy $\pm 21 \%$

## BRIEF SPECIFICATION :

Y Amplifier: $\mathrm{DC}-25 \mathrm{Mc} / \mathrm{s}$ Bandwidth. Differential dual input.
X Amplifier: DC- $8 \mathrm{Mc} / \mathrm{s}$ Bandwidth. Differential dual input
Y Sensitivity. $20 \mathrm{~mm} / \mathrm{V}$ (Can be extended to $400 \mathrm{~mm} / \mathrm{V}$ ).
Y Input: up to 500 V peak DC/AC.
Sweep; repetitive triggered or delayed* speed
$150 \mathrm{~cm} / \mu \mathrm{s}-33 \mathrm{~cm} / \mathrm{s}$.

- An additional linear sweep of controlled duration may be used to display signals which occur during the delay period.


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stringent valveholder applications. Ediswan Clix P.T.F.E. Valveholders are fully type approved for Services Grade 1, Class 1 conditions. Full details of these valveholders and other components in the Ediswan range are given in catalogue CR. 1681. Manufacturers and Development Groups may have a copy on request.

## EDISWAN

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THE EDISON SWAN ELECTRIC COMPANY LIMITED, Member of the A.E.I. Group of Companies 155 Charing Cross Road, London, W.C. 2 and Branches. Telephone: Gerrard 8660. Telegrams: Ediswan, Westcemt, London CR3

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## Marconi Surveying

Before planning any communication system, and particularly a microwave or V.H.F. multichannel system, a survey of the propagation conditions over the proposed path or area is essential. Similar, but less exhaustive surveys, are also necessary before planning V.H.F. mobile systems. Such surveys are undertaken by Marconi's, one of the very few radio manufacturers who do so. The teams engaged in the work may be called upon to operate in desert, swamp and jungle, over which line and cable routes would be impractical, on windswept moorlands or in densely populated city and suburban areas. Surveys are being, or have already been carried out all over the world, including: Uganda, Kenya, Tanganyika, Nigeria, Gold Coast, Tangier, Azores Norway, Turkey, Greece, Malaya, Ceylon, West Indies, Sweden, and also, of course, in Britain.

Over 80 countries now have Marconi-equipped telegraph and communications services. Many of these are still giving trouble-free service after more than twenty years in operation.

LEFT. Balloon operations on the Ipoh-Telok Aison route in Malaya.
RIGHT. The mast is up and the motor generator is running during the survey of the Niperian multichannel system.
BELOW. The V.H.F. mobile survey team erect their mast.

## VORTEXION <br> HIGH QUALITY TAPE RECORDER


$\star$ The total hum and noise at $7 \frac{1}{2}$ inches per second $50-12,000 \mathrm{c}$. p.s. unweighted is better than 50 dbs .
$\star$ The meter fitted for reading signal level will also read bias voltage to enable a level response to be obtained under all circumstances. A control is provided for bias adjustment to compensate low mains or ageing valves.
$\star$ A lower bias lifts the treble response and increases distortion. A high bias attenuates the treble and reduces distortion. The normal setting is inscribed for each instrument.

* The distortion of the recording amplifier under recording conditions is too low to be accurately measured and is negligible.
* A heavy mu-metal shielded microphone transformer is built in for $15-30$ ohms balanced and screened line, and requires only 7 micro-volts approximately to fully load. This is equivalent to 20 ft . from a ribbon microphone and the cable may be extended 440 yds . without appreciable loss. $\star$ The .5 megohm input is fully loaded by 18 millivolts and is suitable for crystal P.U.'s, microphone or radio inputs.

The amplifier, speaker and case, with detachable lid, measures $8 \frac{1}{4} \mathrm{in} . \times 22 \frac{1}{2} \mathrm{in} . \times 15 \frac{3}{4} \mathrm{in}$. and weighs 30 lb . PRICE, complete with WEARITE TAPE DECK ........................................... 88400

* A power plug is provided for a radio feeder unit, etc. Variable bass and treble controls are fitted for control of the play back signal.
* The power output is 3.5 watts heavily damped by negative feedback and an oval internal speaker is built in for monitoring purposes.
* The play back amplifier may be used as a microphone or gramophone amplifier separately or whilst recording is being made. $\star$ The unit may be left running on record or play back, even with $1,750 \mathrm{ft}$. reels, with the lid closed.

POWER SUPPLY UNIT to work from 12 volt Battery with an output of 230 v ., 120 watts, 50 cycles within $1 \%$. Suppressed for use with Tape Recorder. PRICE 18000.

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For A.C. Mains and 12 volt working giving 15 watts output, has switch change-over from A.C. to D.C. and "Stand-by" positions. Consumes only $5 \frac{1}{2}$ amperes from 12 volt battery. Fitted with mu-metal shielded microphone transformer for 15 ohm microphone, provision for crystal or moving iron pick-up with tone control for bass and top. Outputs for 7.5 and 15 ohms. Complete in steel case with valves. PRICE $\mathbf{6 3 0} 160$.


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SUBJECT(S) OF INTEREST
JUNE

# A HIGH Mu PENTODE with low hum, noise and microphony 



The AC/SP3 RHi is available in two grades. The valves in both grades are characteristlcally identical, the grading ' $A$ ' or ' $B$ ' relating only to relative levels of hum, noise and microphony. B Grade valves are suitable for the majority of applications, but for particular applications where the noise level is very important Grade A may be preferred.

Under typical operating conditions with $\mathbf{V}_{\mathbf{a}}=\mathbf{2 5 0} \mathbf{v}$, $R_{a}=150 \mathrm{~K} \Omega, R g=150 \mathrm{~K} \Omega, \mathbf{R g}_{2}=500 \mathrm{~K} \Omega, R_{\mathrm{k}}=1 \mathrm{~K} \Omega$, with the heater fed from a centre-tapped $A$.C. supply the equivalent hum voltage at the grid of an average grade $A$ valve is approximately $5 \mu \mathrm{~V}$, whilst the combined noise (excluding hum generated by the valve and grid resistances, using a high quality A.F. amplifier) is not greater than $8 \mu \mathbf{V}$.

The following table compares the noise, hum and microphony from the two grades of valve.

$$
\begin{aligned}
& \text { ' } A \text { ' } \times 5.6 \text { down on ' } B \text { ' } \quad \text { ' } A \text { ' } \times 2 \text { down on ' } B \text { ' } \\
& \text { MICROPHONY } \\
& \text { ' } A \text { ' } \times 8 \text { down on ' } B \text { ' }
\end{aligned}
$$

## THE EDISWAN MAZDA AC/SP3 RH

 is an indirectly heated Pentode with a special heater construction designed to reduce hum due to A.C. fields within the valve.Provided precautions are taken to minimise hum due to external wiring, the AC/SP3 RH may be used in the early stages of amplifiers where the reduction of hum, noise and microphony is of primary importance.

Full technical information on request.

\author{
EDISWAN <br> MAZDA <br> Valves \& Cathode ray tubes <br> The Edison Swan Electric Co. Ltd. 155 Charing Cross Road, London, W.C. 2 and Branches <br> [^9]}

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Leonard Carduner (President, British Industries Corp., New York): Mr. Leak, please tell our readers what the "Point One" amplifier combination does in a high fidelity music system.
H. J. Leak: As you know, Mr. Carduner, the amplifier is actually the "heart" of the system. Your record player, radio tuner, or tape recorder feeds electrical impulses into the pre-amplifier and amplifier. These, in turn, strengthen the signals and feed them into a speaker

It is difficult to strengthen a signal without distortion. "Point One" means that the Leak reproduces voice and instruments with insignificant harmonic distortion 0 : $0.1 \%$ at 8 watts! This gives the illusion of the actual "presence" of the performer.

L.C.: In demonstrating the "Point One" amplifier at Audio Fairs, the most impressive thing we do is to turn the amplifier on its side, show people the terminal board "custom" construction used in American scientific instruments, almost never in radios.
H.JI.: We had a practical reason for this . . . because every terminal connection is easily accessible. It keeps servicing costs down
L.C.: Yes, and many have praised the control panel of the "Point One" pre-amplifier, because it offers every sensible adjustment to match the new hi-fil records . . . and full 25 db bass and treble range.
H.J.L.: In fact, the "Point One" has more adjustments than the Leak amplifiers supplied to the B.B.C., but no superfluous settings to add unnecessary cost.
L.C.: Well, you have one very important exclusive feature. Plug-in jacks on the Leak front panel make it easy to give any tape recorder the full benefit of the Leak circult, in recording and playback. People with portable tape recorders, who put them away when not in use, can connect them instantly. Practical features like this make the " Point One" most enjoyable to use.


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head,
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Note.-This is the one that fits our $37 / 6$ tate.- cabinet.

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 A snlp for the connoisseur-turnover head 29/6. plus 2/- post and packl ng.G.E.C. METAL CONE SPEAKER This fine speaker is coming to the front rapidly-price $£ 8 / 15 /-$ Octagonal cablnet made to maker's specification £11/10/-, walnut of nak.

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Each is fitted with rubber shroud. For B7G button base and
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THE "ELPREQ" Band III SIGNAL GENERATOR is the very efficient and inexpensive answer. It:-

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3. Can be made to give a pattern on T.V. Receiver screen.
4. Can be accurately calibrated with included equipment.

All the parts including valves, tuning condenser and metal chassis are available as a Kit at 25/- post free, Constructional data free with Kit or available separately price $2 / 6$

## The "CONVERTIBLE"

BATTERY PORTABLE WHICH CONVERTS TO


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The Elpreq "Convertible" is an all-dry battery operated superhet using frame aerial and 1.5 volt valves Type 1R5, 1T4, 1S5, and 3S4. It is particularly selective and gives powerful results on long and medium waves. Battery consumption, however, is quite low. The cabinet is ultra-modern and finished crocodile and/or lizard skin in two shades. The control-board is similarly finished, and with the three-coloured dial, gives the whole a factory-built aspect.
Full constructional details of this superhet and of the Picnic Player unit which, by the undoing of four screws, slips into the cabinet in place of the radio, will be found in our booklet "The Convertible" price 2/6 (returnable if parts purchased).
Cost of portable cabinet and all parts for Convertible, including valves, speaker, but not batteries, is $£ 7 / 7 / 6$ (H.P. deposit 22/5) carriage 5/-. speaker, but not batteries, is ${ }^{\text {Cabinet available separately, price } 37 / 6 \text {, plus } 3 / 6 \text { postage. }}$


It is a scientific fact that aperture size controls glare and increases depth of focus and our newly patented Novaspex adapts this principle to T.V., they defintrely :-

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 depth.Banish bye-strain and headaches, Novaspex are as comiortable as sun-glasses. Send your order today
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STOP PRESS! BAND III CONVERTER KIT
Suitable for any type of T.V. £3/10/- complete. Instructional data available separately for $2 / 6$ post free.


## THE BATTERY-MINI

Thls effelent little receiver will add to the pleasure of your picnics and eveninge in the garden, etc., it is an
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- Ferrite Rod Aerial.
- Very Low Consumption from Internal Batteries. - Neat Bakelite Cabinet with Carrying Handle.
- Uses three B7G Low Drain Valves.

The total buliding cost is only $\mathbf{2 4} / \mathbf{1 8 / 6}$, plus $3 / 6$ postage which includes a cabinet and everything except batteries. Constructional Data free with components, or separately price 2/6.

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## BARGAINS TO CLEAR

2-VOLT ACCUMULATORS
Made for the Forces by one of he most famous firms in the approx. $0 \times$ Amp-hour, size ebonite case, pre-charged, only need fllling with acld, $2 / 8$ esch, plus 9d. post and inburance.

## PORTABLE CABINET


purposes to which they are somewhat solled, due to storage but mechanically $0 . K$. Price $1 / 9$, post 6 d .
5-AMP. SURFACE SWITCHESHICRAFT


## WAVE-CHANGE SWITCHES

One dozen asorted wave-change switches, deal for experimeners. Note: theseare unused and not removed asoortment. Price 5/-, post and packing $1 /$ -


## 110-VOLT 2亩-AMP. RECTIFIER

 UNITThis is an excelient unit sultable for Ariving 110 v. D.C. equlpment from 230 v. A.C. mains or for charging batteriea for stand-by Highting, etc. Made or the Government-new and unused, ith switchgear. Price $£ 17 / 10 /=$ each.

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Sultable for electric fences, indoor aerials, etc., $3 /-$ per

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## SPADE TERMINALS Heavy duty type made for M. o.s. Price 7 d . for M.O.S. Price 7d. each, 6/- per dozen.

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 BEETHOVEN CHASSIS
 only firtt-class componenta, fully aligned and tested, 110-240volt A.C. mains operation. Three wave bands covering medium and two shorts. Complete with five valven, I requency changer, double diode triode, pentode output and full wave rectiker. and Insurance $7 / 6$.

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The astonishing "Occasional 65 "-two and ready to switch on-complete with all ratves and 51 n , speaker-Covers both medtum and long wave bands and uses dust cored colls in a unique modern elrcuit which glves slmost superhet performance. Price 28/5/-, plus $3 / 6$ post-Bakelite or wrooden ablnet avalable price 16/6, post $2 / 6$.


BENDIX RA-IB COMMUNICATIONS RECEIVER
Origimally intended for the American Forces this fine recelver, (A small quantity of Which has been released by the ministry of supplybla avallable to you if you sct promptly apreading arrangement possible, it covers the following bands:-
Band I $\quad .15$ to $\quad .315 \mathrm{mc}$.
\(\left.\begin{array}{lcccc}Band 2 \& .315 \& to \& . .680 \mathrm{mc} . <br>
Biand 3 \& .680 \& to \& 1.5 \& \mathrm{mc} . <br>
Rand 4 \& .18 \& to \& 3.7 \& \mathrm{mc} . <br>

Band 5 \& 3.7 \& to \& 7.5 \& \mathrm{mc} .\end{array}\right\}\)| cetres. 20 to 200 |
| :---: |
| metren | Band $5 \cdot 3.7$ to $\left.\begin{array}{lllll}7.5 & \text { me. }\end{array}\right\}$ metres.

Hand $6 \quad 7.5$ to 15.0 mc.
The sensitivity is 4 micro volih for full output. It 11 ses 8 valves and operates from batteries ( 12 or 24 volt or from the mains through a power pack. It has Controls. all of which are brought to the front panel, Include: aerial switch, aerial compensating eondenser, inain tuning condenser, band selector, C.W. switch, power on/ofi ewitch, and volume control.
Very compactig buit in orackle finiahed case, these seta are brand new having never been used and in, perfect working order-apecial price this Furance $10 /=$. Order now to avoid disappolntment. Circuit diagram and component dista given free with sets, or ayallable meparately price 2/6, post íree. Mains Power Pack for Bendix RA-1B, $£ 3 / 10 /$.


TABLE RADIO CABINET
Due to a apecial purchase, we are able to offer this very fine cablnet, size approx. $151 \times 14 \times 6815$. Whanut venee red and satin iniahed. $37 / 6$, carrlage rect one for the Windsor chasgil above with 61 la speaker.

THE "WINDSOR 5"
This is a 5 -valve A.C. superhet covering the usual long, medium and ahort wavedial with an extra long polnter travel. The latest type loctal valvea are used and the cbassis is corrplete and ready to operate. Chasals size 15 im . $\times 6 \mathrm{ln}-\times$ 6in. Price $88 / 19 / 6$ complete with 8 in . speaker. Carriage and insurance 101 .
E.P. terms If required erms If required


THE
CLEVELAND "ORGANTONE"
The Oleveland "ORGANTONE" is a S-valve 3 -wave bsid superhet covering long, medium and short wave.
to very stringerit apecification. Oaram miniature valves are employed and low loss iron cored colls account for an excellent gignsl to noise satio. Full A.V.C. is applied to both frequency changer and I.F. stages, and particular
 care has been taken
The output stage utilises variable negative feed back for tone control, and, but for stand ard pentode correction, no eut in the ordinary sense is apolied. A gram. position is provided and reproduction of records is particulariy good. An amply proportioned power transformer with s primary tapped for $110-280$ volt gives complete isolstiou from the mains.
Chasis size is $12 \mathrm{in} . \times 7 \mathrm{in} . \times 7 \mathrm{in}$ - Acsle aize is $10 \mathrm{fin} . \times$ ifin
Thls receiver has been tested in partleularly diffeult areas and ite ctablity and nots prolection have produced exceptional resulta.
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The firat Cleveland chassle wan good, but thls one is really superb. It has a 7 -valve circuit with 8 watts output, fitted with independent basi and treble controls. It is really an efficlent R.F. circuit coupled to high-fidelity ampllider. The chassia size is the same as the Organtone, namely $12 \times 7 \times 7$ with the 10 a $\times 4$ mulit Price $£ 14 / 10 / \%$, carriage and packing $7 / 6$. H.P. terma 1 ! required.

## RECORD PLAYER BARGAIN

3-speed record player with plek-up using the famous Acos "Hi G" turnover cryatal-motor also by very famous maker-apeed selec. tion is by Bakelito knob. All on
unit board ready for installation. A wonderful bargalo at $86 / 10 /=$ plue 5/- carriage- Hire Purchase 15/-deporit.


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This instrument comblnes the Mk. IIU Truvor Tape Deck and the Cleveland Wide Band Amplifier with a spectal high flur speaker and forms one.of the finest tape recorder comblnations available to-day. It will, of course, play prerecorded tapes as well an make its own recordings of medio, music, meetlage, telephone conversations, letters, ctc. etc. The price, complete with reel of tape and ready to operate, is

## 39 Gns.

Cartiage and insumace 12/6. Hire Pur chase terms if required.
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## THE CLEVELAND OCTAVIAN

In thin inntrument is combined the exceptional qualities of the G.E.C. metal cone loudspeaker in Its Ideal cabinet (the Octagonal illustrated below) and a most modern 3-valve amplifer. This combination will give a realism of musical reproduction not easily
obtained even at twice or three times its price and is defnitely the reproducer for bring. obtained even at twice or three times its price and is defnitely the reproducer for bring-
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Conforming exactly to the designer"s speclification - for G.E.C. metal cone spesker-price $812 / 10 /-$ or $37 / 6$ deposit, carriage and insurance $5 /$ - extra

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| $4 \frac{1}{2} \mathrm{v}$. Heavy Duty Bell Battery. Size $6 \frac{1}{2} \times 4 \frac{1}{2} \times 2 \frac{1}{2} \mathrm{in}$. ................ $4 / 6$ <br> 72 v. H.T. I. 5 v. L.T. Size $6 \times 5 \times 1$ in. 16 <br> 150 v . H.T. Size $2 \frac{z}{2} \times 5 \frac{1}{2} \times 1$ itin. <br> $67 \frac{1}{2} \mathrm{v}$. Size $2 \frac{1}{8} \times 1 \frac{1}{8} \times 3 \frac{3}{4} \mathrm{in}$. <br> All batteries sealed and unused. All plus $1 / 6$ post and pkg. Special redućtion for quantities. |
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$16 \times 16 \mathrm{mfd} .350 \times .3,6$ each
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$0.1 \mathrm{mfd} .12,000$ volts test Mansbridge Condensers. Heighe $6 \frac{1}{5} \mathrm{in}$.
$\begin{array}{ll}0.1 \\ \text { Width } 3 \frac{1}{2} \text { in. Depth } 2 \frac{1}{2} \text { in. Fixing Centres } 4 \text { in. Plus } 1 /- \text { post } \ldots . . . & 5 / 6\end{array}$
PAXOLIN SHEET
$18 \times 4 \frac{1}{2} \times 1 / 16 \mathrm{in}$., $1 /$ each; $10 \times 10 \times 1 / 16 \mathrm{in}$. $1 / 6$ each; $20 \times 10 \times 1 / 32 \mathrm{in} ., 1 / 6$ each; $20 \times 10 \times 1 / 16 \mathrm{in}$, , $3 /$-each.
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Carbon $\frac{1}{4}$ watt $2 / 6 ; \frac{1}{3}$ watt $3 /-; 1$ watt $4-; 2$ watt $6 /-$ per doz.
WIre WOUND AND VITREOUS. 5 watt $1 / 6 ; 10$ watt $2 / 6$; 15 watt $3 /-$ 20 wate $3 / 6$ each.
HIGH STABILITY. 古 watt 5\% 6d.; $\frac{1}{2}$ watt $5 \%$ 9d.; 1 watt $5 \% 1 / 3$ each. A few values in $1 \%$ and $2 \%$ still a vaitable.
ALL ORDERS FOR RESISTORS C.O.D. PLEASE AS WE CANNNOT GUARANTEE TO STOCK ALL VALUES.
W.W. V/CONTROLS. ALL WELL KNOWN MAKES. Pre-set $2 / 6$ each. Spindle rypes $3 /$ each. Values from 5 ohms to 50 k .
V/CONTROLS WITH SWITCH 5k, 50k, $\frac{1}{2}$ meg., I meg.... 3/6 each V/Controls Less Switch. Most values spindleand presee ......... 2/- each
$0-300 \mathrm{~mA} 2 \frac{1}{\mathrm{in}}$. Flush Mounting. Brand new. Guaranteed $8 / 6$ each $0-500 \mathrm{~mA}$. $2 \frac{1}{2} \mathrm{in}$. Fiush Mounting. Brand new. Guaranteed $10 / 6$ each
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27/- doz
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TAG STRIPS. 3 -way $2 /-4$-way $26 ; 5$-way $3 /-7$-way $4 /-: 28$-way 12 - doz SLEEVING. $2 \mathrm{~mm} .2 / 6 ; 3 \mathrm{~mm}, 3 / 6 ; 4 \mathrm{~mm} .4 / 6 ; 5 \mathrm{~mm}$. ... $5 / 6$ per doz.yds.
POINTER KNOBS. Small black with white line, standard tin.
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WANDER PL UGS Red and Biack ...................................7/6 doz.
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STANDARD SCREENING CANS 3-piece I/-each; Spring Loaded
BELLING LEE PLUGSAND SOCKETS, 5 -pin $1 / 9 ; 7-$ pin $2 / 6$;
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AIR SPACED TRIMMERS $5,10,15,20,25,50$ and 75 pf preset and spinde types $1 / 6$ each
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3/- doz.

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6 V . at $10 \mathrm{~mA}, 2 / 6$ each
27/6 doz.
OUTPUT TRANSFORMERS. Multi-ratio, $5 /$-each; Pentode

## DRUM DRIVES, 3 传in <br> WEST DRIVES, , int

4/- each
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ARCOLECTRIC (Whitney Lamp), Red, Green, Clear, $1 / 6$ each 15/- doz.
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adjusting lamphalder, $1 / 9$ each
8-pin, 3/6; 10-pin, 4/-; 12-pin …................................... 6/- pair
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BRAND NEW \& GUARANTEED £9.15.0 Carr. and ins. $4 / 6$. 3 -ohm speakers suitable for this chassis available $8^{\prime \prime} 17 / 610^{\prime \prime} 25 /{ }^{-}$ This chassis is a genuine bargain and delivery is reasonably good.

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By Plessey -3 speed Model 331, 45 and 78 R.P.M. This brand new antochanger Mirer Unit will play 7, 10 and 18 inch records. Xtal Cartridge Type Pick Up with Sapphire Helght 5lim. Depth 2in. Special Bargain Price whilst atock lasts

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QUALITY PUSH-PULL OUTPUT TRANS. 20w.

Super 8ilent Lams. Seationalised windings Prim. Ind, 75H. Leakage Ind. . 075 H Prim. Imp. to individual requirements Sec. 3.25 and 15 ohms. Fully shrouded and terminated. 3 gns.
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Complete with two detachable diamond heads and transformer. Cash Price E20/19/9 or sent for 63 Deposit and 10 monthly payments of 40 J -. Post and packing paid.

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## REMINGTON <br> ‘60'

ELECTRIC SHAVER

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Balance after 14 DAYS FREE TRIAL $15 /-$, and 8 monthly payments of 24/a Cash Price 69.17 .11 . $A C / D C$ 2n0-250r. Brand new. Sent post paid in slik lined presenfation case.

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## We offer at a fraction the real value these very useful motors with Reduction Drive

## DATA

200/240 v. A.C. shaded pole motor (speed approx. 2,000 R.P.M.), driving a reduction gear giving a.final rotary speed of 6 R.P.M. and a reciprocating arm speed of 6 swings per minute. Arm movement or gearing can be easily removed.

Price 12/8d. each


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Tape Recorders, Gram. Drives, Models, Display purposes, Beam Aerial Drives, Timers, Machine Feeds, etc., etc.
The above are only à few suggested uses.

Two For 22/6d. Carriage $1 / 6 \mathrm{~d}$.


Manufactured by J. STEAD \& CO. LTD., SHEFFIELD, 2.


Constructed to VHF standards throughout. Covers the band 2 with RF, Mixer, 2-IF, and ratio detector stages. Provision is made for single or push pull output, or added Shore Waveband. Although " hand buile" in small quantitles, an ateractive price is maintained.
Model "A." FM tuner. A popular and small unit, with good sensitivity. These are in use from Bognor to Ely, and little changed since first described by Amos and Johnstone in the "Wireless World." New "hammer " finish front plate and tuning scale carries a magic eye; this and power unit are optional.

The "Mullard" 5-10 amplifier. Our version is condensed to only $12 \times 5 \mathrm{in}$. plan, with symmetrical front layout. With FM. a truly high fidelity outfit is possible under $£ 35$.

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& \text { CB4/2. with push pull output................ £26 } 0 \\
& \text { A"., basic tuner.. } \\
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& \text { - Mullard" amplifier our version.................. } 630
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## TS-13/AP <br> PORTABLE SIGNAL GENERATOR

for 3CM operation with self contained Wavemeter and Power Monitor.

## 1. FREQUENCY RANGE

For general use $9375 \pm 70 \mathrm{mc} / \mathrm{sec}$. Freq. sensitivity of power monitor $\pm 1 \mathrm{db}$ in range $9375 \pm 70 \mathrm{mc} / \mathrm{sec}$. Freq. sensitivity of calibrated attenuator $\pm 2 \mathrm{db}$ from -13 dbm to -65 dbm in above frequency range.

## 2. FREQUENCY STABILITY

Sawtooth Operation. Frequency modulation of approximately $0.1 \mathrm{mc} / \mathrm{v}$. Thermal Drift. Set stabilizes after approximately 3 minutes warm-up. Frequency Stability. Wavemeter calibration changes within limits listed below:

| Temp. ( ${ }^{\circ} \mathrm{F}$.) | Limits (dial div.) |
| :---: | ---: |
| 60 | -3 and +1 |
| 75 | -2 and +2 |
| 90 | -1 and +3 |

## 3. VARIATION OF ATTENUATOR

The attenuator is individually calibrated to be accurate to $\pm 2 \mathrm{db}$ at approximately $75^{\circ} \mathrm{F}$.

## 4. PULSE CHARACTERISTICS

Triggered Operation. Positive trigger required:-Not less than 15 V., 1-20 microseconds.
Negative trigger required:-Not less than 50 v., 5-20 microseconds (repetition rate $350-4000$ c.p.s.). Pulse width:-Continuously variable

4 (contd.).-from less than 1 to greater than 2 microseconds, measured at half power points. Pulse phasing:-From 6 microsecs. minimum to 200 microsecs. maximum.
Self Synchronous Operation. Recurrence rate:-1000 c.p.s. $\pm 20 \%$. Duty cycle:-Between 20 and $60 \%$.

## 5. TYPES OF OUTPUT

Triggered operation with variable width, phaseable pulse output, self synchronous operation with short and long pulse output (square wave), CW, and FM (with sawtooth input).
6. PEAK POWER OUTPUT (CW) (Pulsed Modulated) At least 50 microwatts for $1 / 2$ of full scale of meter deflection. Peak power within $10 \%$ of CW power.

## 7. POWER LEAKAGE

Insufficient to interfere with normal operation.
8. SWITCHES AND FUNCTIONS

POWER-ON/OFF. Line switch.
CALIBRATE/USE, CW output in CALIBRATE position, permitting monitoring of output power. Triggered or self synchronous pulsed output in USE position.
PULSE/SQUARE WAVE. Selection of triggered or self synchronous operation
SYNC/SELF SYNC. Pulsed output in synchronism with input trigger of 350 to $4000 / \mathrm{sec}$. recurrence rate or Self synchronous square wave operation at approx. 1000 c c.p.s. $\pm 20 \%$ recurrence rate.

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$300-700 \mathrm{Mc} / \mathrm{s}$ frequency meter. TS174 ${ }_{\text {frequency meter. }}^{\text {flich }}$ GENERAL RADIO type 804 B . $8-300 \mathrm{Mc} / \mathrm{s}$. signal generator.

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## A DUAL-CHANNEL PRE-AMPLIFIER and TONE CONTROL UNIT

Attractively finished in "Old Gold " and TREBLEE in conjunction with main volume control.
It can be used with any amplificr and with any pick-up, the range of frequency control provided by the for all types of plck-ups and sill natures of recordings, f.e., Engllah, American and long-playlng without recourse to -plek-up correction. The extreme flexibility of the bass and treble control is auch that the level of bass
and treble can be set to sult any conditions lrrespective of the volume output of th amplifer. Response characterlstics are given in 12 -watt amplifier advt. The unlt measures only $9 \mathrm{in}, \times 4 \mathrm{in} \times 21 \mathrm{in}$. Including self.contained power supply and can be accommodated elther on or away from the maln amplifier, f.e., on the front panel of a cabinet or any omer position. Price
6 J 5 ), $£ 3 / 16 / 9$. Complete assembly data la avaliable separately for $1 /$-. Completely assembled and ready for use, $25 / 5 /$.
!! THE IDEAL SET FOR USE IN CARAVANS, ETC. !! A 5 -VALVE 2 -WAVEBAND SUPERHET battery for only $\mathbf{E f}^{\prime} 17^{\prime} 6$
(plus 5/- Carriage and Insurance.) These Recel vers. which we have recently acquired by bulk purchnse, bro ox-British Minfstry of supply, rud s.re new and unused. They are a two-wave band Sopertet
with R.F. Stage, coveriag Short Wave 18 to 50 metres and Medium Wave 200 to 550 metres, fully calibrated on a clock face dial. A 5in. loudspeaker is built in and the whole Chnasis is contained in a metal cablnet with lid and carrying bandle which measures $121 \mathrm{in} . \times 7 \mathrm{ln}$. $x$ 7 in . overall. Valve line up is 7A7, 7Q7, 7A7, 7B6 and


They are male for 6 VOLT D.a supply
and the current consumption 15 $4 / 8$ amps.
They possess excellent sensitivity and will give very good results on a very short aerial.


## SELENIUM RECTIFIERS

L.T. Types
$2 / 6 \mathrm{v}$. $\frac{1}{2}$ a.h.w.... $1 / 9$
6/12 v. $\frac{1}{2}$ a.h.w. 2/9
F.W. Bridge Types

6/12 v. 1 a. ...... 4/11
6/12 v. 2. a ...... 8/9
CO-AXIAL CABLE, 75 ohms tin, 7 d yard Twin screened feeder, 10d. yd.

SILVER MICA CONDENSERS. $5,10,15,20,25$, $30,35,50,100,120,150,180,200,230,300,330$, $400,470,500,1,000$ pfd. $(.001 \mu \mathrm{~F}), .002 \mathrm{mfd}$. ( 2,000 pid.). All at 5 d . each, $3 / 9$ dozen one type.

DIAL BULBS, M.E.S., 8 จ. 0.15 a., $6 / 9$ doz.; 6.5 v. 0.3 a., $6 / 9$ doz.; 4.5 v. 0.3 a., $6 / 9 \mathrm{doz}$.

## ELECTROLYTICS (Current production)

| Tubular Types |  | Can Types |  |
| :---: | :---: | :---: | :---: |
| $8 \mu \mathrm{~F} 450 \mathrm{v}$. ${ }^{\text {c.. }}$ | 1/9 |  |  |
| 8 mfd .500 v | 2/6 | 16 mfd . 850 v ... | 1/11 |
| $16 \mu \mathrm{~F} 350$ v. | 2/3 | $16 \mu \mathrm{~F} 450$ v. | 2/9 |
| $16 \mu \mathrm{~F} 450 \mathrm{v}$. | 2/9 | $24 \mu \mathrm{~F} 350 \mathrm{v}$. | 2/11 |
| $16 \mu \mathrm{~F} 500$ v. | 3/9 | $32 \mu \mathrm{~F} 350 \mathrm{v}$. | 2/11 |
| $32 \mu \mathrm{~F} 350 \mathrm{~V}$. | 3/9 | 32 mfd .450 v . | 4/9 |
| $32 \mathrm{mfd}$.500 v ... | 5/9 | 64 mid . 450 | 4/9 |
| $8-16 \mu \mathrm{~F} 500 \mathrm{v}_{0} \ldots$. $25 \mu \mathrm{~F} 25$ | 4/11 | 100 mfd .450 v . | 4/9 |
| $50 \mu \mathrm{~F} 12 \mathrm{v}$. | 1/3 | $8-8 \mu \mathrm{~F} \quad 450$ v.... | 3/6 |
| $50 \mu \mathrm{~F} 50 \mathrm{v}$ | 2/3 | $8-8 \mathrm{mfd}$. 500 v . | 4/9 |
| 100 mfd . 12 v... | 1/9 | $8-16 \mu \mathrm{~F} 450 \mathrm{v} . .$. | 2/11 |
| $100 \mathrm{mfd} .25 \mathrm{~V} \ldots .$ | 2/3 | $16-16 \mu \mathrm{~F} 450$ v. | 4/11 |
| 8 mfd . 350 v ... | 1/3 | $16-32 \mu \mathrm{~F} 350$ | 4/9 |
| 8 mfd .450 v .... | 2/3 | $32-32 \mu \mathrm{~F} 350$ | 4/9 |
| 16 mfd .500 v . | 3/9 | $32-32 \mu \mathrm{~F} 450$ | 5/11 |

YOLUME CONTROLS with long spindles, all values, less switch, $2 / 9$; with S.P. switch, $3 / 9$.
WIRE WOUND POTS: 20 ohms, 500 ohms, $5 \mathrm{~K}, 20 \mathrm{~K}, 100 \mathrm{~K}$ (medium length spindles), $2 / 9$. 220 ohms, $2 \mathrm{~K}, 10 \mathrm{~K}$, 20K, Preset type, $1 / 9$ each
EX GOVT. AMMETERS. Moving coil. G.E.C. 0-5 amps., 2in. scale, $11 / 9$.

EX-GOVT. E.H.T. SMOOTHING CONDENSERS .25 mfd , $, 4,000 \mathrm{v}$. Blocks
$.5 \mathrm{mfd}, 2,500 \mathrm{v}$. Blocks
.5 mfd ., $3,500 \mathrm{v}$. Cans
1 mfd. plus $1 \mathrm{mfd} .8,000 \mathrm{v}$., large blocks (common negative isolated)
1.5 mfd ., $4,000 \mathrm{v}$. Blocks

EX-GOVT. BLOCK PAPER CONDENSERS
$2 \mathrm{mfd} .800 \mathrm{v} . \quad \ldots \quad 1 / 9 \quad 6-6 \mathrm{mfd} .450 \mathrm{v} \ldots .55 / 9$
$4 \mathrm{mfd} .500 \mathrm{v} . . .22 / 9 \quad 8 \mathrm{mfd} .500 \mathrm{v} . . .5 / 9$
4 mid. 1,500 v.... $4 / 9 \quad 8-8 \mathrm{mfd} .500$ v.... $6 / 11$
4 mfd . $2,000 \mathrm{v} . . . . \quad 6 / 9 \quad 15 \mathrm{mfd} .500 \mathrm{v} . . . . \quad 7 / 9$ 4 mfd .400 v . plus 2 mfd .250 v ., $1 / 11$.
M.E. SPEAKERS. All 2-3 ohms, 8 in . R.A. field, 600 ohms, $11 / 9.10 \mathrm{in}$. R.A. field, $1,500 \mathrm{ohms}, 23 / 9$. 10 in . R.A. field, 1,000 ohms, $23 / 9$.

SPECIAL OFFERS. Mains Trans. $200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$. Primary Secs, $250-0.250 \mathrm{v} .200 \mathrm{~mA}$. 6.3 v .8 a .5 v . 3 a., 21/9. Small output Transformer, 5,000 ohms to 3 ohms., $1 / 11$.

GOODMANS $3 \frac{1}{2} \mathrm{in}$. P.M. SPEAKER (ex equip.), with battery pentode trans., 12/9.

## HEAVY DUTY BATTERY CHARGER

For normal 200/250 v. A.C. mains input. To charge 12 v . battery, Variable charge rate of up to 10 amps . Fitted Meter and Fuses. Guaranteed 12 months. Carr. 7/6. £6/19/6. DRYDEX HANDLAMPS. Suitable for garage
lights, etc. (Normal price 29/6). Limited number. lights, etc. (Normal price 29/6) Limited
Brand new boxed, fitted with bulb, $19 / 6$.
H.T. ELIMINATOR AND TRICKLE CHARGER KIT with louvred crackle finished case. Mains input $200-250 \mathrm{v}$. Outpur 120 v .40 mA ., and 2 v . $\frac{1}{2}$ a. Price with circuit, 29/6.
Or in working order, 37/6.

## R.S.C. TRANSFORMERS

 FULLY GUARANTEED, INTERLEAVED AND IMPREGNATED
## MAINS TRANSFORMERS

Primaries 200-230-250 v. $50 \mathrm{c} / \mathrm{s}$.
FULLY SHROUDED UPRIGHT MOUNTING
$250-0-250$ ซ. 60 mA .6 .3 v. 2 a., 5 v. 2 a
Midget type, $21-3-3 \mathrm{in}$.
17/6
$350-0.350$ v. $70 \mathrm{~mA}, 6.3 \mathrm{v} .2$ a. 5 v. 2 a. ... $19 / 9$
$250-0-250$ v. $100 \mathrm{~mA} ., 6.3$ v. $-4 \mathrm{v}_{\text {., }} 4 \mathrm{a}_{\text {. }}$ c.t.,
0.4-5 v. 3 a.
$250-0-250$ v. $100 \mathrm{~mA} ., 6.3$ v. 4 a.,. 5 v. 3 a. ... $23 / 9$ $250-0.250$ v. $100 \mathrm{~mA} ., 6.3$ v. 6 a., 5 v. 3 a.,
for R1355 conversion
$300-0-300$ v. $100 \mathrm{~mA}, 6.3$ v. 4 a., है v. 3 a... $23 / 9$
$300-0-300$ v. $100 \mathrm{~mA} ., 6.3$ v. 4 v. 4 a., c.t
0-4-5 v. 3 a
550-0.350 100 .................................... $26 / 9$
$350-0-350 \mathrm{v}, 100 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{v}_{\text {, }}, 4 \mathrm{a}$. c a
0-4-5 v. 3 a. $26 / 9$
50-4-5 v. 150 m...................................
$350-0-350$ v. $150 \mathrm{~mA}, 6.3 \mathrm{v}, 2$ a 6.3 v. 2
5. v. 3 a. ...............................................
$425-0-425$ v. $200 \mathrm{~mA}, 6.3$ v. 4 a., c.t., 6.3 v.
4 a., c.t., 5 v. 3 a., suitable Williamson Amplifier, etc.
$450-0-450$ v, $250 \mathrm{~mA}, 6.3$ v. 6 a., 6.3 v. 6 a., 5 V 3 a.
$250-0-250$ v $70 \mathrm{~mA}, 6.3 \mathrm{v} .2 .5 \mathrm{a} . . . . . . . .$.
$260-0-260$ v. 70 mA ., 6.3 v. 2 a., 5 v. 2 a.... $16 / 9$
$350-0-350$ v. $80 \mathrm{mA}$. . 6.3 v. 2 a., 5 v. 2 a.... $18 / 9$
$250-0-250$ v. $100 \mathrm{~mA} ., 6.3$ v. 4 a., 5 v. 3 a. 22/9
$300-0.300$ v. $100 \mathrm{~mA} ., 6.3$ v. -4 v. 4 a., c.t.,
0-4-5 v. 3 a.
$350-0-350$ v. $100 \mathrm{~mA}, 6.3$ v. 4 a., c.t., 5
3 a
$350-0.350$ v. $100 \mathrm{~mA} ., 6.3 \mathrm{v},-4 \mathrm{v}, 4 \mathrm{a}$. c.t.
23/9

$350-0.350$ v 150 mA . 6.3 v. 2 a., 6.3 v 2 a $23 / 9$
$350-0.350$ v. 150 mA., 6.3 v. 2 a., 6.3 v. 2 a.p
5 v. 3 a. ............................................... 29/11
$350-0-350$ v 150 mA 63 v 4 a, 5 v. 3 a $29 / 9$
E.H.T. TRANSFORMERS. 2,500 v. 5 mA .,

2-0.2 v. 1.1 a., 2-0.2 v. 1.1 a., for VCR97,
VCR517 ............................................. 37/6

## FILAMENT TRANSFORMERS

Primaries $200-250$ v. $50 \mathrm{c} / \mathrm{s}$.
 6.3 v. 3 a. $\ldots . . .8$ 8/11 $\quad 6.3$ v. 6 a. ...... $17 / 6$ $\begin{array}{llll}12 \mathrm{v} .1 \mathrm{a} . & \ldots . . . & 7 / 9 & 6.3 \mathrm{v} .6 \mathrm{a} . \\ 0-2-4-5 . . . \\ 0.6 .3 \mathrm{v} .4 \mathrm{a} & 16 / 9 & 12 \mathrm{v} .3 \mathrm{a} . \text { or } 24 \mathrm{v} .\end{array}$

| 6.3 v. 2a. ...... | $7 / 6$ | $12 \mathrm{v.3}$ a. or 24 v. | $17 / 6$ |
| ---: | ---: | ---: | ---: | ---: |

CHARGER TRANSFORMERS
All with 200-230-250 v. $50 \mathrm{c} / \mathrm{s}$. Primaries: $0-9-15 \mathrm{v}$ If $a_{\text {, }}, 11 / 9 ; 0-9-15$ v. $3 a_{n}, 16 / 9 ; 0-9-15$ v. 5 a. $19 / 9 ; 0-9-15$ v. 6 a., $23 / 9$.

## ELIMINATOR TRANSFORMERS

Primaries $200-250$ v. $50 \mathrm{c} / \mathrm{s}, 120$ v. $40 \mathrm{~mA} . \quad 7 / 11$
120 v. $40 \mathrm{~mA}, 5-0-5$ v. 1 a, ................... 14/9

## OUTPUT TRANSFORMERS

Midget Battery Pentode 66:1 for 3S4, etc. 3/6
Small Pentode, $5,000 \Omega$ to $3 \Omega \ldots . . . . . . . . .$.
Standard Pentode, $5,000 \Omega$ to $3 \Omega$
Standard Pentode, 8,000 to $3 \Omega$
Battery Pentode, 10,000 ohms to 3 ohms.
Multi-ratio $40 \mathrm{~mA} . \quad 30: 1,45: 1,60: 1,90: 1$,
Class B Push-Pull
$\begin{array}{lll}\text { Push-Pull } 8 \text { Watts } 6 V 6 \text { to } 3 \text { ohms ................................... } & 8 / 9\end{array}$
Push-Pull $10-12$ Watts 6 V 6 to $3 \Omega$ to $15 \Omega 15 / 9$
Push-Pull $10-12$ Watts to match 6 V 6 to
3-5-8 or $15 \Omega$
$16 / 9$
Push-Pull 20 Watts high-quality sectionally $47 / \%$

Smoothing chokes
250 mA ., $3 \mathrm{H} ., 50$ ohms
11/9
$150 \mathrm{~mA}, 7-10 \mathrm{H} .250$ ohms ..................... $11 / 9$
100 mA , $10 \mathrm{H} ., 150$ ohms potted ............. $9 / 9$
$100 \mathrm{~mA} ., 10$ H. 200 ohms........................... 8/9
80 mA., 10 H. 350 ohms
$60 \mathrm{~mA} ., 10 \mathrm{H} .400$ ohms

## THE SKY FOUR T.R.F. REGEIVER



## EX.GOVT. MAINS TRANSFORMERS

All $230 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$. input.
8.8 v. 4 a. .............................. $9 / 9$

48 v. 1 a. ................................. 9/9 9/9
$0-11-22$ v. 30 a. ..............................................72/6
$16-18-20$ v. 35 a.
7.7 v. C.T. 7 amps., 4 times ......... 25/9

460 v. $200 \mathrm{~mA} ., 6.3$ v. 5 a. ......... 27/9
$300-0-300$ v. 80 mA .5 v. 3 а. ...... $8 / 11$ $278-0-278$ v. 100 mA .

A design of a 3 -valve $200-250$ v. A.C. Mains receiver with selenium rectifier. For inclusion in either of cabinets illustrated above. It employs valves 6 K 7 , SP61, 6F6G, and is specially designed for simplicity in wiring. Sensitivity and quality is well up to standard. Point-to-point wiring diagrams, instructions, and parts list, 2/6. This receiver can be built for a maximum of $£ 4 / 19 / 6$ including cabinet. Available in brown or cream bakelite, or veneered walnut.
P.M. SPEAKERS. All $2-3$ ohms. $0 \frac{1}{2} i n$. Plessey 16/9. 8in. Plessey, 16/9. 10in, R.A., 26/9. 10in. Plessey, 19/9. 10 in , Rola with Trans., 29/6.
R.S.C. BATTERY CHARGER KITS. For mains input $200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$. To charge 6 v . accurmulator at 2 amps., 25/9. To charge 6 v . or 12 v . battery at 2 a., 31/6. To charge 6 v . or 12 v . battery at 4 a., 49/9. ABOVE KITS CONSIST OF GREEN CRACKLE LOUVRED STE STEEL CASE, MAINS TRANSFORMER, FULL WAVE METAL RECTIFIER, Any type assembled and tested for $6 / 9$ extra.
R.S.C. 6 v. or 12 v. BATTERY CHARGER For normal A.C. mains input 200-230-250 v., 50 $\mathrm{c} / \mathrm{s}$. Selector panel for 6 v. or 12 v. charging. Variable charge rate of
up to 4 AMPS. Fused up to 4 AMPS. Fused, and with 5 amp meter. Well ventilated metal case with attractive crackle finish. Guaranteed for 12 months, 69/6. Carr. 2/6.

$300-0-300 \mathrm{v} .150 \mathrm{~mA}, 810-0-610 \mathrm{v} .150 \mathrm{~mA}$., $1,220 \mathrm{v} .350 \mathrm{~mA}$.
400 v. C.T. 150 mA .4 v. 5 a., 6.3 v. 6 a.,
6.3 v. 0.6 a., 4 v. 6 a., 4 v. 6 a., 4 v. 3 a.,

22/9

## EX-GOVT, AUTO TRANSFORMERS

15-10-5-0-105-215-235 v. 500 watts
Double wound $10-0-200-240$ v. to $10-0$ -
275-295-315 v. 1,000 watts
Double wound $0-110-240$ v. to $0-130-140$ -
150-160-170 v. 1,500 watts
Carriage on any of above $5 /-$ extra.
EX-GOVT. SMOOTHING CHOKES
$250 \mathrm{~mA} ., 10 \mathrm{H} .50 \mathrm{ohms}$
250 mA ., 10 H .100 ohms
$250 \mathrm{~mA} ., 3$ H. 50 ohms.
$150 \mathrm{mA},. 10 \mathrm{H} .50$ ohms
$100 \mathrm{~mA}, 10 \mathrm{H} .100$ ohms. Tropicalised
$100 \mathrm{~mA} ., 5 \mathrm{H} .100$ ohms. Tropicalised
$50 \mathrm{~mA} ., 50 \mathrm{H} .1,$.000 ohms. Potted
$90 / 100 \mathrm{~mA} ., 10 \mathrm{H} .100 \mathrm{ohms}$. Potted
$50 \mathrm{taA}, 5-10 \mathrm{H}$.
L. T. type 1 amp.

## 14/9

## CHASSIS

18 s.w.g. undrilled aluminium amplifier type (4-sided).
14 in . $\times 10 \mathrm{in} . \times 3 \mathrm{in}$. $7 / 11$ $16 \mathrm{in}, \times 10 \mathrm{in}, \times 3 \mathrm{in} .8 / 3$ $18 \mathrm{~s}, \mathrm{w} . \mathrm{g}$ aluminium receiver type.
 7 1in. $\times 44 \mathrm{in} . \times 2 \mathrm{in}$. $2 / 9$ $10 \mathrm{in} . \times 5$ in. $\times 2$ in. $3 / 3$ $10 \mathrm{in} . \times \sin . \times 2 i \mathrm{in} .3 / 11$
$11 \mathrm{in} . \times 6 \mathrm{in}, \times 2 \mathrm{in} .3 / 11$

16 s.w.g. aluminium receiver type.
$12 \mathrm{in} . \times 8 \mathrm{in} . \times 24 \mathrm{in} .5 / 3$ $16 \mathrm{in} \times 8 \sin \times 2 \frac{1}{12}$ in. $7 / 6$ $20 \mathrm{in} . \times 8$ in. $\times 2 \frac{1}{2}$ in. $8 / 11$ 16 s.w.g. aluminium amplifier type, 4 -sided.
$12 \mathrm{in} . \times 8 \mathrm{in} . \times 2$ in. $7 / 11$ $16 \mathrm{in} \times 8 \mathrm{in} . \times 2 \mathrm{hin} .10 / 11$ $20 \mathrm{in} . \times 8$ in. $\times 2$ in. $13 / 6$ $20 \mathrm{in} . \times 8 \mathrm{in} . \times 2 \operatorname{in} .13 / 6$
$14 \mathrm{in} . \times 10 \mathrm{in} . \times 3 \mathrm{in} .13 / 6$

## R.S.C. HIGH FIDELITY 25 watt AMPLIFIER A4

## A NEW DESIGN FOR 1955

 HIGH GAIN " PUSH PULL OUTPUT." BUILT-IN PRE-AMP. TONE CONTROL STAGES. INCLUDES 7 valves, sectionally wound output transformer, block paper reservoir condenser, and reliable small components. AN INPUT OF ONLY 20 millivolts IS REQUIRED FOR FULL OUTPUT. THIS MEANS THAT ANY TYPE OF MICROPHONE OR PICK-UP IS SUITABLE. Two separate inputs controlled by separate volume controls allow simultaneous use of "Mike " and Gram., or Tape and Radio, etc., etc. Individual controls for Bass and Treble "lift" and "cut" Six negative feedback loops giving total of 24 D.B. Frequency response $\pm 3$ D.B. $30-20,000 \mathrm{c} / \mathrm{s}$.

Hum level 66 D.B. down. Certified total harmonic distortion of only $0.35 \%$ measured at 10 watts. Comparable with the very best designs. SUITABLE FOR SMALL HOMES OR LARGE HALLS, CLUBS, GARDEN PARTIES, DANCE HALLS, etc., etc. For ELECTRONIC ORGAN OR GUITAR. FOT STANDARD OR LONG PLAYING RECORDS. Size $12 \times 10 \times$ gin. For mains A.C. $200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$. Power consumption 175 watts. Outputs for 3 and $\mathrm{I}_{5}$ ohm speakers. The kit is complete in every detail. Chassis is fully punched. Easy to follow point-to-point wiring diagrams are supplied. EXTRA HIGH SENSITIVITY, HIGHEST QUALITY for
Or assembled ready for use $50 /-$ extra Or assembled ready for use $50 /-$ extra

Terms to include cover, mike, speakers, etc., on request. Cover as illustrated if required, price $1 \% / 6$ extra.
W.R. "STENTORIAN" High Adelity P.M. Speaker EFP1012. 10 watts, 15 ohm (or 3 ohm) apeech coll, Where a really good quality speaker at a low price is requlred we highly recommend this unit with an amazing periormance £3/17/6.

MICROPHONES. Crystal, hand or Desk type, high fidelity Acos, 50/-. Stand type with base and adjustable stem. £6/19/6. Both auftable for use with our amplifiers.

PLESSEY 3-SPEED MIXER AUTOCHANGERS with oryatal pack-up having alloy stylus with beparate sapphire polnts for long playing or standard records. (Whil play new, cartoned, Euaranteed. For 200-250 V. AC. malns. Limited stocks at oniy 10 gins. plus 5/-carr.
H.M.V. LONG PLAYING RECORD TURNTABLE COMPLETE WITH CRYSTAL PICK-UP (SAPPHIRE STYLUS). Speed 33\} f.p.m. BRAND NEW, OARTONED. Only $23 / 19 / 6$ ( 4 pprox. hall price). Cart 6/-(for 200-250 \%. A.C. Maing).
R.S.C. 4-5 WATT HIGH GAIN AMPLIFIER TYPE A5


A highly aensitive 4 -valve quality amplifier for tho home omall club, etc. Only 50 millivolte input is required for full output so that it is suitable for use with the latest high-
fidelity pick-up heads, in addition to sil other types of fidelity pick-up heads, in addition to sll other types of
pick-ups and practically aill mikes. Beparate Buss and plek-ups and practically ull mikes. separate buss and record equaliastlon. Hum level is negligible being 71 D.B. down. $15 \mathrm{D} . \mathrm{B}$. of negative feedback is used. H.T. of aupply of a Radlo Feeder Unit, or Tape Deck pre-ampliffer. For A.C. mains imput of 200-230-250 v. $50 \mathrm{c} / \mathrm{s}$. Chassls is not alive. Kit is complete in every detail and inclades fully punched chassis (with baseplate), with green crackle finish, and point-to-point wiring diagrams and instructions. use $30 /=$ oxtra plus $3 / 0$ y $54 / 15 / \%$ or assembled ready for use 30/- extra, plus $3 / 0$ carr.

COLLARO HIGH FIDELITY MAGNETIC PICK-UPS High Impedance type. Limilted number, brand new, boxed and perfect at fraction of normad price. Only $35 /$ DEFIANT RECORD PLAYING TURNTABLE COMPLETE WITH PICK-UP.
(High Impedance Magnetio Type). Unit is housed In a beautiful walnat veneered cabinet of attractive design.
For sil standard records ( $78 \mathrm{r} . \mathrm{pm}$.). Limited number.


## A PUSH PULL 3-4 WATT HIGH GAIN

 AMPLIFIER FOR $£ 3 / 7 / 6$.For mains Input $200-250$ v. $50 \mathrm{c} / \mathrm{s}$. Complete kit of parts Including point-toopoint wring diagrams and instructions. Amplifer can be used with any type or feeder unit or plek-up. with 400-0-400 \%. Trans, Output is for $2-3$ ohm spesker (We can supply a very suitable 10in. unit by Rols at 27/9). The ampllfer can be supplied ready for use for 25/- extra Full descriptive leaflet, 8 d .

R.S.C. MASTER INTERCOMM. UNIT. with prorision for up to 4" Listen-Talk Back Unlts " individually switched. A high gain amplifier enables speech and other sounds emanating from the rooms containing remote control units to be heard at the master control. The unit is in kit form and point-to-point wiring diagrams are supplied. A walnut veneered wood of Brown Bakelite cabinet is included. IS NOT "ALIVE." Ideal for use as "Baby Alarm." Is NOT "ALIVE." 4 wateal lor use as "Baby Alarm. Tilk Back Unit" in bakelite or walmut veneered cahininet, ean be supplied at 35/- each. The Master Unit can be aupplied assermbled and tested for $30 /=$ extra.


ALL DRY RECEIVER BATTERY SUPERSEDER KIT
All parta for an "All Dry" Battery Eliminator. Complete with case. Completely replaces $1.4 \nabla$. and 90 V mains supply of 200-250 v. $50 \mathrm{c} / \mathrm{s}$ is available. Price with elircuit, 3818. Or ready for use. $45 / 6$.
Size of unit $51 \times 4 \pm 2 \mathrm{sin}$.

BATTERY SET CONVERTER KIT. All parts ior con verting any type of battery receiver to all malna. A.C. 200

 tions oniy $48 / 9$. Supplied ready for use for $8 / 9$ extra.

## Redia surply ca carensop

32 THE CALLS.
Terms C.W.O. or C.O.D. No C.O.D. under-fl. Postage $1 /$ extra under $10 /-1 / 6$ extra under $£ 2,2 / 6$ extra under $£ 3$, Full Price List 6 d . Trade List 5 d .
Open to Callers: $9 \mathrm{a} . \mathrm{m}$. to $5.30 \mathrm{p} . \mathrm{m}$. Saturdays until I p.m.
R.S.C. A3 10 WATT "PUSH PULL" KIGH FIDELITY AMPLIFIER.
With Self contained Pre-amplifier and Tone control.


This smplifier, whilst having suffictent outpot to fill a small hall, is the ideal ampllfier for the quality enthusiast who knows that though the average listening level is less than one watt output of at least ten times this figure in order to obtain completely distortionless reproduction of sudden loud sounds.
The layout of the componenta has been planned to glve the very maximum of performance with the minimuma of constructional effort. Large safety factors In every conscreened input plugs, valves, and with easy-to-follow point to-polint wiring diagrams. Everything is supplled down to the last nut and bolt.
Two independent imputs are provided with two associsted inderendent volume controls so that prograwmes can be mixed together if desired, such as mlerophone announceIndependently controlled microphones, or even just gramophone/radio, fading over from one to the other. Varlable base lift and cut with variable treble lift and cut tone controls are fitted, giving full long playing record equallsation for nncorrected pick-ups. They are also provided so that the user can alter the tonal value to suit his personal taste and surroundings. Because of the large nerative designed that it provides ant the specifled power even with large variations of loudspeaker tmpedance. Terminals are provided for 3 ohm and 15 ohm loudsperkers
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|  |
| ． |

Drop thro＇ $350-0-350$ ₹． 70 mA ．， 6 v ． 2.5 amp．， 5 v． 2 amp．，14／6．

Drop thro $250-0.2507 .80 \mathrm{ma}$ ．， $6 \mathrm{\nabla}$ ． ，actp．， 5 v． 2 amp．，14／6．
$280-0-280$, drop through， 80 mA.
$6 \mathrm{\nabla} .3$ amp．， $5 \nabla .2$ amp．， $14 / 6$ ． 6 ₹． 3 amp．， $5 \nabla .2$ amp．，14／6．
250－0－250 80 mA．， 6 ₹． 4 amp．，14／－
Drop thro＇ $270-0-270,80 \mathrm{~mA}$ ．， 6 v ．

$$
3 \text { amp., } 4 \text { ャ. } 1.5 \mathrm{amp.} \text {. } 13 / 6 .
$$

 3 amp．，11／6．

Anto－trans．Onpat 200／250 H．T． 500 7．


Anto Trans，Input 200／250，H．T．
 P． 4 P． $3 /-$
Primary， 230 v．，fully shrouded，acreened primary， 13 v． 1 amp．，7／6
Pri 200 ₹．Sec．500－0－500 and 500－0－500 250 mA ．both windings．${ }^{4} \mathbf{V} .3$ amp．．
4 V .3 amp．， $38 / 6$ ．P．\＆ $5 /-$ ．
Mains Transformer，fully impregnated， ${ }_{600-0.600}$ input $210,220,230$ and 240.8 sec． 30 mA ．，complete with separate heater transformer．Input $210,220,230,240$ ．
 6．3
P．\＆P．
Mains Transformer，fully impregnated． Input 210，220，230， 240 ．Sec．350－0．350 100 mA ．，تith separate heater trans－ tormer．Pri． $210,220,230,240$ sec．
$6.3 \mathrm{~V}, 2 \mathrm{amp}, 6.3 \mathrm{v} .3 \mathrm{amp} ., 4 \mathrm{v} .6 \mathrm{kmp}$ ．

MANS TRANSFORMERS，Chaseis mounting，feet and voltage panel．
Primaries 200／250．
$350-0-35075 \mathrm{~mA} .6 .3$ จ． 3 a． $\operatorname{tap} 4$ v．
6.3 v． 1 a．，13／8．
$500-0-500125 \mathrm{~mA} .4$ 甲．O．T． $4 \mathrm{~mm}, 4$ ．
C．T． 4 A．， 4 v．O．T． 2.5 a．， $27 / 8$.

Oin．T． 7. Cabinat，front in contrasting Filnut veneers，size $16 \neq 1 \mathrm{ln}$ ．long， 111 ing high，by $12 z^{\text {ln }}$ ．Wide．Completa with two pleces expanded sluminium in gold
$12 \times 9$ gin．and 5 in．speaker baffie and chassis， $20 /-$ ，poot paid．
64in．M．E．Speaker， 1,000 ohm．Aeld．
R．\＆A．T．7．enargised 6 gin mpeaker Fith O．P．trans．．．beld coll， 175 olims 9／6．P．\＆P． $2 / 6$ ．
C．\＆A． 84 in ．M．E．speaker，with O．P． Volume Controls．Loog spindles leag P．$\&$ P．3d，each．
Volume Controls．Long spindle and
 long spindle double pole switch，minio． long spindle double pole swik
Trimmars， $5-40$ pl．， $5 \mathrm{~d} . \quad 10-110,10.250$.
$10-450 \mathrm{pt}, 10 \mathrm{~d}$.
Twin－Gang， 0005 Tuning Condeuser， $5 /=-$
With urmmers，7／6．
$T$ min ${ }^{2}$ hang， 0005 ，with foet，size $38 \times 8 \times 111 \mathrm{n} .$, ， $8 / 6$ ．
3 －rang ． 0005 ，with feet，sizo $4 \times 3 \times$

## 1j12．，7／ia．

T．V．Coils，moulded former，tron－cored Wiound for re－winding purposes only． Ali－cian
Ali－can
21
$\times 1 / i n ., 1 / 6$ each．
Used Metal Rectifler， 250 v． 150 mA ． 6／6．
Metal Rectiliar， 230 ₹． 45 mA. ． $6 /$－ Metal Reotifler，RM2， $125 \%$ ． 100 toA．． 3／6．


PERMEABLITYY Input 300 ohm bal anced line，coverace $54 \mathrm{Mo} / \mathrm{s}-89 \mathrm{Mc} / \mathrm{s}$ snd
 Vision IF，：$-45 \mathrm{Mo} / \mathrm{s}$. ． somnd $40.5 \mathrm{Mc} / \mathrm{s}$ ．Uses 6AK5 RF valve，GAK5
 for auto－gain control． Dimensious gin．wide．
61in．deep，4in．high，9in．blank－seale．Wldth tacluding scale－overlap 14in．Four stages permeability tuned．Complete with 3 valves，．Post and Pkg． $3 /$－．$£ 2 / 18 / 6$ ．
T．V．CONVERTER for the new commeroiel stations complete with 2 valves．Frequency：－can
be sef to any channel within the $186-186$ Mels．band．I．F．：－will work fnto any existing T．V． receivar designed to work between $42-68 \mathrm{Mc} / \mathrm{s}$ ．Sensitivity：－ $10 \mathrm{Ma} / \mathrm{g}$ ，with any normal T．V． set．Input：－arranged for 300 ohm feeder． 80 obm feeder oan be used with slight reduction in the first stage，R．F．AMPLIFIER 10 db ．Required power supply of 200 y DC At $25 \mathrm{~mA} .8,3$ y A．O．st 0.8 smp．huput fiter ensuring complete treedom from unwanted signals． 2 simple adjustments only． $22 / 10 /-, \quad$ P，\＆P．\＆／6．
USED 12in．TUBE，aluminlzed，heater cathode－short， 10 KV max． 2 ．heater complete with
lise and E．H．T．transformer 9 KV with ferrocart core，line and wldth control，EY51 rec．winding line and E．H．T．transformer 9 EV with ferrocart core，line and whdth control，EY51 rec．winding


GENERAL PURPOSE $3-1 N-1$ MATNS TRANSFORMER．Input $200 / 250$ ．Bec． $250 \vee .350 \mathrm{~mA}$ ．
 HIGH－IMPEDANCE PLASTIC RECORDING TAPE
 PLASTIC CABINET，as illustrated． 11

 in polished Walnut complete with T．．．F．F，
chaselis， 2 waveband scale，atation mames， chassis， 2 waveband scale．otation mames，
new wave－band，back－plate，drum，pointer， spring．drive spindle， 3 knobs and back．＇
 AS ABOVE，with superbet chassis， $23 / 6$ ．
P．\＆P．3／6． P．\＆P． $3 / 6$ ．
Used metal rectifier， 230 v， $50 \mathrm{~mA}, 3 / 8$ ．
gang with trimmers， $8 / 6 ;$ M，
 $3 v / \mathrm{hand}$ circuit， $4 / 6:$ heater trans．， $6 /-5$
 chandenser， $1 /=$ resistor kit， $2 /=$ ；condenser kit， $4 /$－．
Cyldon 5 channel T．V．Tuner，uses EF80 and 12AT7 iess valves， $12 / 6$ ，post pald．
Radiogram Chassis， 5 valve A．C．／D．C． 3 wave－band superhet $195 \cdot 255$ v．，19－49，200－580 and line－ap 10C1，10F9，10LDII U404 and 10P14．Twin mains ilter input， 2 dial lisbts and 8 in． P．M．，E8／1\％／6．P．\＆P．B／． CR100 Coil packs in first－class condition less oscillator section，complete with 4 －gang tuning condenser，19／6．P．\＆P．3／6．
CR100 465 Kc．I．F．s，types 3， 4 and 5 and F．B．O．，new condition，7／6 each． 465 Kc ．Xtal for CR100， $12 / 6$.
4－gang tuning condenser for CRIO0，9／6．
CONSTRUCTOR＇S PARCEL，modlum and long wave A．C．mandos $230 / 2502$－valve plus metal
 change switch，volume control，heater trans．，metal rectifler， 2 valves and ₹／boiders，amoothing wound， $22 / 6$ ．P．\＆${ }^{2}$ ． $2 / 6$ extra．Circuit and point－to－polnt， $1 / 3$ ．
CONSTRUCTOR
comprising
cliasels
 F／h．，I．F．and trans．eut－outs， back－plate， 2 supporting brack－
eta， 3 wave－band scalc，new耳avelength statlons names． Size of scale 114
drive，sp．．
drum． ${ }^{\times 41 \text { palleys，}}$ politer， 2 bulb bolders ${ }_{5}$

 2 amp．，of v． 2 mmp gind eltio



Battery charger，input $230 / 250$ v．output 6 and 12 volt 1 amp．Black crackle finished case size $10 \times 6 \times 4$ in Incorporating metal rectifier， main on－off switch，and output switeh， $21 /=$ ．P．\＆P．3／－．
OOTPUT TRANSFORMERS．Standard type 5,000 ohms lmp．，4／9；42－1 with extra feed－back windings，4／3．Miniature $42-1,3 / 3$ ．Mulli－ratio $3.500,7.000$ and $14,000,5 / 8$ ．10－watt pualh－ pull， 6 V 6 matching， $7 /$－ $90-13$ ghm mpeech coil， $6 / 6$ ．
PUSA－BAGE CONNECTING WIRE，Doz．yds．，1／6．Post pald．
STANDARD WAVE－CEANGE SWITCBES 4 －pole 3 －way， $1 / 1$ ；5－pole， 3 －way， $1 / 9 ; 3$－pole， 3 －way
 potato and vegetable peeler
 water pump．All aluminium construation，white stove－enamelled fnish．Orikinally intended
tor for adaption
 ohms，tapped at 100 ohms，vilreous， $1 / 16$ ； 0.3 amps． 950 ohms，lapped 700 and 825 ． 2／6；0．2 amp．， 1.000 ohms，vitreous，tapped $2 / 6 ;$
$640,600,3 / 6$ ．
．P．\＆
T．V．Width Controls， $3 / 6$.

Crysta！Set，reedium and long wave，in plastie cabinet，18／－
Headphones，per pair，8／－．
Speaker Matehing Uait on aluminium chassis．3－15 ohms reverslble，12／6
Line and E．H．T．Transformor， 14 Kv ．， using ferrocart core，complets with line U37 rectifer winding， $35 /$－
Lino and E．E．T．Transformer， 9 K usisig fermeart core，complete with buili－in line and width control．Mounted
 Scan coils，low line low Impedance to match above， $27 / 6$ ． P \＆ P ．
Line and E．H．T．Transformer， 9 Ky ferrocart core．， comple trensormer and line and widtly controlo £ £ $/ 5 /-$ ．P．\＆P． $3 /$－．
As above，but complete with llae and 250 mA ．choke， 100 mpld ．and 150 m fd 250 wkg 380 mas ．A．C．ripple．$£ 2 / 19 / 6$

Valve Holders，mouided octal Mazda and laoctal，7d．each．Parolin．octal Mazda and loctal，＂4d．each．Moulded
B7G，B8A and B9A，7d．eacho B7G B7G，B8A and B9A，7d，eacho B7G
moulded and B9A with acrecuing can moulded
32 mid．， 350 wkg．
$16 \times 24,350 \mathrm{wkg}$ ．
$4 \mathrm{mfd} ., 200 \mathrm{wkg}$.
$16 \times 8 \mathrm{mfd}$ ． 500 wis．
$16 \times 16 \mathrm{mid}$, ， 500 wkg ．
$16 \times 16 \mathrm{mid} ., 450 \mathrm{wkg}$
$32 \times 32 \mathrm{mld}, 350 \mathrm{wkg}$ ．
$32 \times 32$ mitd．， 350 wikg．．．．．． $4 / 9$
25 mfd .25 mkg ．

86 mfd．， 500 wkg．，wire ends
8 midd．，, 300 v v．wkg．，wire ends
50 mad．， $25 \nabla$ ．wkg．，wire ends
100 mid．．， 850 wkg ．

150 mich．， 350 v．wiole．， 280 ma
A．C．ripple
$100+200 \mathrm{mfld}, 350 \mathrm{wkg}$
$16+16$ mind．， 350 wkg．
50 mifd．， 180 whg．．
65 mld．， 220 wkg
$8 \mathrm{mfd}, 150 \mathrm{wkg}$ ．
$60+100$ mfd．， 280 wkg．
50 mfd． 12 wkg

Miniature wire ends moulded， 100 pl．， 500 pf．，and ． 001 ，each， 7 d.
 size $134 \times 11 \times 3 / 161$ i．，4／6．
Combined 12 in ，mask snd escatcheon， in ilghtly tinted Perspex．New aspect edged in brown．Fits on front of
cabineth $12 /$ ．As above for 15 in．tube， calis．
Frame Oscillator Blocking Trans．，4／6． Line Osc．Blockink Trans．，4／6
Tube Moanting Bracket，slze $91 \times 4 \% \mathrm{in}$ ． 12in．tube clam
CHOKES：

 2 benry $180 \mathrm{mA},. 3 / 6 ; 250 \mathrm{~mA}$ ． 10 henry， 10／6；＇s heary 250 mA．， 60 ohms． 8／6．
 except Mazda 12 in ．with Veraler
adjustment， $15 /-$ ． adjustment， 15 P．M．Foons Unis for Mazdas，12in．，leans Verniter adjustment， $15 /$－
Wide Angle P．M．Focus Oniss，Vernier
adj．state tube， $25 /$ ． adj．state tube， 251 －．
Enerkised Focus Coii，${ }^{\text {Iow }}$ resistance mounting bracket． $17 / 6$ ．
Ion Traps for Mullard or Engliah Electrio tubes， $5 /$ ，post paid．
Btandard 485 Kc ．iron－cored I．F．s． $4 \times 11 \times 1$ ilin．，per pr．， $7 / 6$ ．Wearite
standard，
Iron－cored， $465 \mathrm{Ke}$. I．F．s， standard，iron－cored，
$3!\times 1 \mid \times 10 \mathrm{in}$ ．，per pr．， $9 / 6$ ． Lron－Cored $465 \mathrm{~K}_{\mathrm{c}}$ ．Whistle Filter，2／6． 485 EC．MIDGET LP．s．Q． 120 size 1 $\$ \mathrm{in}$ ．long， 1 ln ．wide，ile．deep by very tamous manuiwecturer．Pre－silignec adjusta

# RADIO \＆T．U．COMPONENTS（Acton）LTD． <br> （Late D．COHEN） <br> 23 HIGH STRIETT（Uxbridge Road）ACTON，W．3．Telephone：ACOrn 5901 



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Now in dust-proof heavy gauge anodised aluminium can and with miniature 5 or $9-$ pin base for plugging in.
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BOTH TYPES FITTED WITH PLATINUM POINTS IF SPECIFIED

Datal-A Sensitivity of 25 milli-wates and capable of handling mains voltage on the contacts with alternating currents up to 0.25 amps . Being polarised it has the advantage that the Armature contact can be biased to lock in either direction by suitable adjustment of the contact scrows which provides a useful facility where pulse operation is required. Speed of operation is high and the Relay will follow frequencies appreciably higher than 50 c.p.s. Resistance up $207,000 \mathrm{ohms}$ which is acceptable for Anode circuits. Alternatives to specification if required Sole Concessionnaires.

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POWER SUPPLY UNITS No. 5, complete except for the 6-v. accumulator, conalsts of the $6-\mathrm{v}$. 5 -amp. hand generator, with cut-out, $6-\mathrm{v}$. linput vibrator pack, providea all I.T. and H.T. oytpats for the 18 and 38 sela, spare maliory vibrator, hakelite accumu-
 webbing. new in sealed cartons, 40/-, carriage $81 /$-: ${ }^{\text {scot. } 7 / 6 \text {; N.I. } 10 / \text { - }}$
ELECTROLYTTC CONDENSERS, 32 -mfd. $450-v$, D.C.. by Zenith. Micamold. ete., new and guaranteed, cartons of 12 condensers, $10 \%$, post paid.
PROJECTION UNITS, consists of an optical mount, nitted with a bloomed $1 / 2.2$ Achromatic lens, 34 in . Focal length, at one end aho y conves/concave ground glass at the reflector, fraction of original cost, $10 /=$, post $1 / \mathrm{o}$.
SELSYN TRANSMITTERS (Magslipe), 3in, type, pure syncbro X-y-1-2-3, suitable as master or slave, $50-\nabla .50-$ escle single phace A.C. operated. When two or more of 100 per oent. follow in the other(s), both clockwige or antl-clockwise, supplied brand new with teat report, in tropicallsed sealed cartons, Value, \&8 each, our price 25/\% post $2 /-, 2$ for $50 /-$, post paid with wiring diagram.
TELEPHONE SETS, consits of 2 combined receivers and microphones, connected by 20rt. twin flexible, provides perfect 2 -way communication (up to mile with ats bex), self-energised, no battery required, complete ready for use, new, boxed, $12 / 6$, post $1 /$ "NELCO" ROTARY TRANSFORMERS (matched), brand new lateat manufacture

 20/-, poat $1 / 10$.
G.E.C. POWER UNTTS, Intended for 100 -watt B.F. ampllifers, input A.C. $200 / 220 /$ $240-$. plus $10-\mathrm{v}$. $45 / 120 \cdot \mathrm{e}$. p.s., output $550-7$. at $300-\mathrm{m} / \mathrm{A}$. D.C., and $6.3-\mathrm{\nabla}$. r.m.8., consists of eight U52 rectifiers, separate heater and H.T. transformers, 2 Dubilier
nitrogol 8 -mid. $1,200-\mathrm{r}$, capacltors, 2 heavy etc., etc., for 10 in . rack mounting, welght 104 lb ., new and unused, $\varepsilon$, $710 /$., carriage and crate, $15 / \%$; Scot. $20 /-$ extra.
WIRE STRIPPERS, strips the insulation from flexes and cahles up to fin. dia., micrometer adjuatment, brand new boxed, usual woolshop price 15/-, our price 3/8. post
$6 \mathrm{~d} . \mathrm{3}$ for $10 /=$ post paid.
ARROW SWITCHES, $250-\mathrm{F} .25$-amp. rotary 4 -positlon, 3 -hent and off, series parallel, panel mounting, complete with pointer knob, brand new, 2/8, post $1 / 3$, ditto smadier Diamond H., 20-v. 10-amp., 2/6, post 9d.
VENNER 24-VOLT TIME DELAY SWITCHES, consibta ot bigh-grade clockwork motor with external press wind, 2 electro-magnets, 5-pole can-operated contacts, in amart metal cases titted 4-way terminal block, new boxed, 7/6, post $1 /$-.
G.E.C. MINIATURE RELAYS, 40 -ohm., 4 -pole chnngeover platinum contacts, brand new boxed, $8 /$, post $6 d ., 90 /$ - doz., post paid.
ELECTRO-MAGNETIC COUNTERS, G.P.O. subscribers pattern, 3 -ohm. coll. 0.9999 repeating, size $4 \stackrel{x}{ } \times 1 \downarrow \times 1+$ in., $5 /=$, post $1 /$.
ELECTRIC BELLS, $12-\mathrm{o}$. D.C., single dome 3in. dia., 1 isin bigh, very superior, worto 30/-, our price, brand now bored, 3/6, past 9d.
Miny other bargains: send 3d. with S.A.E. for carrent lists.
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## C.R.T. ISOLATION TRANSFORMERS <br> Dasigned to cover practically every demand for Transformers for Cathode Ray Tubes having Heaster/Cathode short oircuit or for C.R. Tubes with falling emission. Type A. Low lealtage windings. Ratio 1-1.25 giving i $25 \%$ boost on Secondiry.  13.3 volt $10 / 6$ each $10 / 6$ each <br> Type B. Mains Input $220 / 240 / 6$ volts. Mrult Output 0-2-4-6.3-7.3-10 and 13 volta. Input has two taps which Increase output voits by $25 \%$ and $50 \%$ respoctively. This traneformer is saitable for most Cathode Ray This traneformer is seritable for most Cathode Ray Tubes, The MOST versatile Low Capacity C. Ab. Transformer with Universal Output and Solder Tags. 21:- each. <br> Type C. A most useíul low capacity wound trans. former for use with 2 volt Tubes with falling emisgion. Input $230 / 240$ volta. Output $2-2 \frac{1}{2}-2 \frac{2}{5}-2 \mathbf{N}^{-3}$ volts at 2 amps. With Tas Panel and Bolder Tags $17 / 6$ each. All Isolation Transformers are Individually boxed,

Volume Controls 80 colbie COAXIAL Midget typer. Long
spindles. Guaranteed 1 STANDARD fin. diam. year. All valnes 10,000 ohms to $2 \mathrm{Mep}-0 \mathrm{hms}$.

No $\mathrm{Br}_{\mathrm{w}}$ g.R.Sw. D.S. $\begin{array}{ccc}\text { No Bw. } & \text { g.P.Bw. } & \text { D.P.Sw. } \\ 3 /- & 4 /= & 4 / 9\end{array}$ | $3 /-$ | $4 /-$ | $4 / 9$ |
| :--- | :--- | :--- |
| COAXIAL PLUGS | $1 / 2$ |  | $\begin{array}{ll}\text { LINE CONNECTOR } & 1 / 8 \\ \text { OUTLET BOXES } & 1 / 6\end{array}$ Coaxial GEADE 8d. yd. SPECLAL

Seml-air spaced Polythene insulated. fin diameter. Stramded core. 9d. yd.
Loeses cut $50 \%$.

BALANCED TWIN FEEDER per yd. 6d. $\quad$ TWIN SCREENED BALANCED FEEDER $1 /=\left\{\begin{array}{c}80 \\ 0 h m\end{array}\right.$ 50 OHM COAXIAL CABLE, 8d. per yd. fin dia.
TRIMMERS, Ceramic, 30, 50. 70 pi ${ }^{4}$ 8d. 100 pfo, 150 pio, 1/3; 250 pf., $1 / 6$ : $600 \mathrm{pt}, 750 \mathrm{pf}$., 1/8
RESISTORS.-All valueg: 10 obms to 10 meg., \& w., 4 d. ;
 ohms to 10 Meg .
WIRE-WOUND RESISTORS-Best Makes Miniature ceramic Typo-5 w., 16 ohm to 4 K ., $1 / 9 ; 10$ w., 20 ohm 12 K . to $25 \mathrm{~K}_{\rightarrow}, 3 /$
WIRE-WOUND POTS. 3 WATT LAB. COLVERN," ETC. Pre-Set Min. TV Type Etandard Bize Pots, 2tin. Knuried Slotted Knob.
Ali valnes 25 ohms to 30
 Ditio Carbon
to 2 meg., $3 /$ pindle High Grade Al Valuea. 100 ohms to 50 K ., 6/6; $100 \mathrm{~K} .{ }^{\text {W/WT. }}$ 6/6. WIW EXT. BPEAKER CONTROL 10@, 3/ O/R TRANSFORMERS.-Heary Duty 70 mA., 4/6. Ditto tapped primasry, $4 / 9$. Multiratio, QPP, push pull 6/6.
Tapped Bmall pentode, $3 / 9$.
L.F. CHOKES. $15 / 10$ E. $60 / 65 \mathrm{~mA}, 5 /-; 25 / 20 \mathrm{H}, 100 / 120$ mA., $11 / 6 ; 20 / 15 \mathrm{H}_{\text {. }} 120 / 150 \mathrm{~mA}$., 12/6. MAINS TRANS.
 $2 \mathrm{a}, \mathrm{I}$ 17/6. MALNS HEATER TRANS. 6.3 v. 1 i a., $7 / 6$; 6.3 จ. 3 a., $10 / 6$.

## ELECTRODYNAMTC MIKE INSERT.-U.S.A. make Bargain Price 3/8. Matching Trans. 3/8.

SPEAKER FRET.-LEpanded anodised matal, 12in. $\times 12 \mathrm{ln}_{\text {. }} 41-$ EXT. L.S.- $\$$ witched Bocket on $\cdot 0$ ft and parallel switching, complete with plug, $2 /=$. 12 in . pash fitting, $2 / 6 \mathrm{dOz}$., D. \& D. 9 d .
fitting, $2 / 6$ doz., p. \& p. 9d. 2 yd. Non-kink Appliance Leads, Bargain 1/3.
TYANA. -Midget Soldering Iron. $200 / 220 \mathrm{~V}_{\mathrm{V}}$. or $230 / 250 \mathrm{\nabla}$. 14/11. TYANA TRIPLE TAREE, - Complete with detachable bench stand, 19/6, $200 / 220 \mathrm{~F}$, or 230/250 V.
NEW SOLON MIDGET IRON. -25 W ., 19/6. IDEAL FOR RADIO CONSTRUCTIORS. 200/220 \%. or 230 /2nd bozed V'HOLDERS. Pax: Int. Oot., 4d.: EF50, EA50, 6d. B12A CNT, 1/3. Moulded; Int. Oct. 8d. B7G, 9d.; with screening can, $1 / 6 ; 188 \mathrm{~A}$, B8G, B9A, $1 /$; VCR97, $2 / 6$.
Ceramic: EF50, B7G, 1/. Paxolin ENG. and AMER. $5 \cdot 7$, and 9 -pin, etc.,
Nuts, Bolts and Washers, 12 of eas. 1/- packets, 24 or 6 B.A 4d. 9 - or 10-way, 8 d. etc.
TOGGLE SWITCHES EX-GOVT.-" On-Off," 9d. Ersla M'core solder 60/40, 16 g . or $18 \mathrm{g.}$. 5/6; \& lb., 4 d . Yd. T.C. wire, 18 to 22 s.w.g., 2/-; $\frac{2}{2}$ lb. P.V.C. Connecting wire, 8
colourg. Single or Stranded, 2 d . उd. 2 K. 5 w . H.D. w/w Pota, colourg. Single or Stranded, 2d. उd, 2 K. $\$$ W. E.D. w/w Pots, 4/6. 10 K. 25 K., Colvern $w / w$ Pot. In spindle, $3 / 6$. BULGIN BIGH VOLTAGE VALVE CAPS, I. Oct.,
BULGIN BAGE
ALADDIN FORMERS and cores. tin, $8 \mathrm{~d} .: \operatorname{tn} 10 \mathrm{~d}$. SLOW MOTION DRIVES,-Epicyclic ratio 6:1 2/3.
INT, OCTAL CABLE PLUG (8-pin), with cover, $1 / 3$. $200-250$ Volt SELECTOR SOCKET (21n $\times 1 \mathrm{ln}$.) with Plug $1 /$ /. PILOT LAMPS. -6.3 V. 3 a., 8 d , 750 ohms. 4/3, . 2 amp., 1,000 ohms, $4 / 3$ LINE CORD.- 3 amp., 60 ohms per foot. 2 amp. 100
ohma per foot, 2 way, $1 / 6$ a yard; 3 -way, $1 / 8$ a yard.


ALL WAVE RADIOGRAM CHASSIS THREE WAVEBANDS M.W. $16 \mathrm{~m} .-50 \mathrm{~m}$ LATEAT MULLARD
L. W. $800 \mathrm{~m} .-2,000 \mathrm{~m}$. EBC 42, EL 41. EZ40 Brand New and Guaranteed, with 10 in . P.M. Speaker, A.C. $200 / 250$ v. Four position Wavechange switch.
Short-Medium-Long-Gram. Slow Motion Tuning. Short-Medium-Long-Gram. Blow Motion Tuning.
Speaker and Plek-up connections. Eigh $Q$ iron-dust Speaker and Plek-up connectlons. Eigh Q iron-due
cored colls, 465 Le/s I.F. Lateat circult technique
delayed. 4.2 watts. A.V.O. ath Negative fecedback. Outpat Chassis size $18 \mathrm{ff} \times 51 \times 2$ in., Glass Dial-10in. $\times$ 4 tin., borizontal or vertical type available, Ift by
2 Plot Iamps. Colour Black station names, L. W. Green, M.W. Red, 8.W. White. Four Knobs supplied. Walnut or Ivory to choice, allgned and callbrated. Chasais Isolated from taains. PRICE E10/15/--
Carriage and Insurance, $4 / 6$. (Without 10 in Speaker, fol15/-. Carr. \& Ins., 4/6.) A.C.-D.0. 10/= extra.
recommended for above chassis
Plessey Multi Speed Changer


PRICE Carriage Paid $£ 9.19 .6$ GREAT REDUCTION
Brand New Plessey 3-speed Autochanger Mixer Unit lor 7,10 and $12 i n$. Records. Twia Hi-Fi Xtal Head with Deopoint sapphire stglus. Plays 4,000 records
sprang mounting. Superb Quality. Bargain offer. sprang mounting. Superb Quality.
This Changer wili play:-
8 mixed 78 r.p.m. $10^{\circ}$ and $12^{\prime \prime}$ records.
$10331 \mathrm{r} . \mathrm{m} .7^{7}$ records
1033 j r.p.m. mixed $10^{\circ}$ \& $12^{\circ}$ records
Baseboard required $151 \times 12 t \mathrm{im}$.
Height required 51 in
Depth required $2 i n$.

* MIXER TYPE MECHANISM * DUAL POINT TURNOVER HEAD
similar model 3 speed single record unit with Acos 37 turnover head, each sapphire stylus will play 2,000 records. Starting switch automatically places
pick-up on records. 7 ln ., loin. or 12 in . suto-stop. Baseplate size $12 \times 81 \mathrm{ln}$. Helght required 2 in in. $\underset{\substack{\text { depth } \\ \text { Price carriage pald } \\ £ 7,15,6}}{ }$


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## RECORDING TAPE

$1,200 \mathrm{ft}$. on standard fitting $7^{\prime \prime}$ reels. Brand new boxed

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onır 17'6<br>REEL

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Ye Aerial Ping and socket, $1 / 8 \mathrm{pr}$
Sia. RADIO SCREWDRIVERS. $\frac{\text { Pr }}{}$ Sheffleld made blade 2 in. $\times$ inin. Ins. handle 5,000 v. 4 id. each. CONDENSERS.-New Btock .001 mfd. 6 kV. T.C.C. 5/6. Ditto, 12.5 kV ., $9 / 6 ; 2 \mathrm{pL}$ to 500 pl . M1ca, $6 \mathrm{~d} . \mathrm{i} .001$

 $1 / 3$; Tubulur 5 mfd . 500 v., 1/9.
SILVER MICA CONDENSERS.- $10 \%$
5 p 1 . to $500 \mathrm{pt}, 1 / \mathrm{m} .600 \mathrm{pL}$ to $3,000 \mathrm{pl}, \mathrm{i} / 3$.
1.5 pt . to $500 \mathrm{pf}, 1 / 9$. 515 pf . to $1,000 \mathrm{pt} ., 2 /-$

BLECTROLYTICS ALL TYPES NEW 8 TOCK.

| Trubulat Wire Ends |  |
| :--- | :--- |
| $16+16 / 500$ v. | 6an Types, Clipr, 3 d. |
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$1 / 275 \mathrm{v}$.
$2 / 450 \mathrm{~F}$.
$4 / 350 \mathrm{~F}$.
$4 / 350 \mathrm{~F}$.
$4 / 500 \mathrm{\nabla}$.
$4 / 500 \mathrm{v}$.
$8 / 450 \mathrm{v}$.
$8 / 450 \mathrm{v}$.
$8 / 500500 \mathrm{v}$.
$16 / 500 \mathrm{v}$.

| $8+8 / 500 \mathrm{v}$. |
| :--- |
| $39 / 500$ |

$32 / 500 \nabla$.
$32+32 / 350 \mathrm{~F}$
$32+32 / 500 \nabla$
$25 / 25$
$50 / 28$
v.
$6 / 1$
$2 / 1$
$2 / 3$
$1 / 6$
$2 /=$
$2 / 3$
$2 / 9$
$2 / 6$
$4 / 1$
$4 / 1$
$6 /=$
$5 / 6$
$7 / 6$
$1 / 9$
$1 / 4$
64.
4.6
$4 / 6$
$3 / 6$
$4 / 6$
$8 / 6$
$8 / 6$
$5 / 2$
$5 / 6$
$5 / 6$
$6 / 6$
$6 / 6$
$11 / 6$
$12 / 6$

SPECIALS. Can Types. 500 mid . $12 \mathrm{~V} ., 3 / \mathrm{s}: 1,000 \mathrm{mdd}$. KV. T.C.C., 3/6. Type 512 acrew base, 8 mfd. 500 \%., $3 /-$ 10 midd 500 V. $4 /$ / SIFIERS. E.H.T. TYPE FLY-BACK VOLTAGES, K $3 / 252 \mathrm{kV}, 4 / 3 ; \mathrm{K} 3 / 403.2 \mathrm{kV}$., $6 /-; \mathrm{K} 3 / 45$
 4/-; RM2, $100 \mathrm{~mA} .4 / 9$ : RM3, 120 mA ., 5/9: RM' 250 m $4 /=$ RM2, $100 \mathrm{~mA}, 4 / 9$ RM3, $120 \mathrm{~mA}, 5 / 9$ : RM6 250 .
$275 \mathrm{~mA}, 16 /-$.
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| :---: | :---: |
|  |  |
| nt, "Brillisnce-On-Uni" ." On-Off," "Volume,." |  |
| " Bass," "Wavechange," *Radio-Gram," " Be, |  |
|  |  |
| M., L., Gram.," .' Record-Play, ${ }^{\text {+" }}$ " Brightneas. ${ }^{\prime \prime}$ Ditto |  |
| not engraved, $1 /$ - each Size " B " lin engraved, |  |
|  |  |

POINTER KNOBS.-Brown with white marking line, smal 9d., large 1/-
COILS - "P" type. $2 / 6$ each. Midget * $Q$ " Type dj. dust con
ALUMINIUM CEASSIS.- 18 s.F.g. Plain, undrilled,
lolded 4 sides and riveted corners lattice fixing boles.
Sing $\times 4$ and soundly constructed with 2$\}$ in. sides,
1sin. $\times 1$ in., 10/6; and $18 \times 18$ in. $\times$ 3in.. $16 / 6$

UULL WAVE BRIDGE SELENIUM RECTIFIERS.2,66 or 12 \%. $1 \frac{1}{2}$ minap. $8 / 9 ; 2$ a., $11 / 3 ; 4$ a., $17 / 6$ HARGER TRANSFORMERS TRPC
tor charging at 2, 6 or 12 v., is amp., $13 / 6$, $4200 / 250$ V ACID HYDROMETER.-New ex-Govt. Unbreakable

BRIMISTORS.-CZI for 3 a, heater chalus, 3/6. CZ2 for 15 a., or 2 a-. 2/6. OZZ3, $1 / 6$.
COPPER ENAMEL WIRE.- $\frac{1}{2}$ tb. 16 to $20 \mathrm{~m} . \mathrm{w} . \mathrm{g} v, 8 / \mathrm{s}$ 22 to 28 s.w.g., 2/6; 30 to 40 g.w.g., 3/6.
SWITCE CLEANER Fluid. squirt spout. $3 / 9 \mathrm{tin}$.
TWIN GANG TUNING CONDENSERS, -. 0005 mPd . midget
with trimmers, $8 / 6 ; 376$ pf. midget less trimmers, $6 / 6$ : .000 Standard size with trimmers and feet, $9 /-$; lesu trimmers, 8/-; ditto, woiled, 2/6.
SLEEVING.-Tarious colours,
SLEEVING.-Various colours, 1, $2 \mathrm{~mm} ., 2 \mathrm{~d} . ; 3,4 \mathrm{~mm}$. LOUDSPEAKERS P.M. 3 OHM. 5in. 16/6, 6 Hin., $17 / 6$ in., 19/6. 101n., 25/. 21 -. Fam GRYSTAL DIODE - Very Sensitive. G.E.C., 3/6. R.R. PHONES,-(Hi-grade Amer.), $15 / 6 \mathrm{pr}$.

## VCR97 £2 <br> TESTED FULL PICTURE

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HALF PRICE. I0/6 PAIR

## TWO WONDERFUL BARGAINS



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## ELECTRO-VOICE MOVING COIL MICROPHONES

No. 600.C. With built-in matching transformer for direct connection to grid of amplifier valve. These mikes are ex the famous BC. 610 Transmitter and give perfect speech quality, they are all brand new with 9 ft . screen lead and 3 pin plug, packed in original carton. Prise $\mathbf{6 2}$, plus $1 / 6$ postage and packing.

We are offering AS NEW, COMPLETE TR.I196 TRANSCEIVERS, as illustrated. Outfit comprises, 6 valve Superher, 3 Vaive Transmitter, Power Unit and Relay Unit. All complete on Chassis. Present range $4-6.5 \mathrm{mc} / \mathrm{s}$. and output 2 watts. Can be easily converted to cover $1.5 \mathrm{mc} / \mathrm{s}-7 \mathrm{mc} / \mathrm{s}$ and power output up to 8 wates. It has a most versatile Receiver which can $1.5 \mathrm{mc} / \mathrm{s}-7 \mathrm{mc} / \mathrm{s}$ and power output up to 8 watts. It has a most versative Receiver which can
be easily adapted to cover any band of frequencies from medium broadcast to $30 \mathrm{mc} / \mathrm{s}$. The be easily adapted to cover any band of frequencies from medium broadcast to $30 \mathrm{mc} / \mathrm{s}$. The Transmitter range can also be easily extended and by simply adding 200 pl . condens
circuit will cover $1.5 \mathrm{mc} / \mathrm{s}$. Circuit and conversion details included with each unit.
circuit will cover $1.5 \mathrm{mc} / \mathrm{s}$. Circuit and conversion details included with each unit.
Each outfit is despatched in transit case at the amazingly low price of $£ 3 /-1$ plus carriage $10 / \mathrm{F}$ Each outfit is despatched in transit case at the amazingly low
If despatched without Transit Case, E2/10/- plus carriage $8 / 6$.

LARGE QUANTITIES OF OUR UNUSED COMPONENT BARGAINS STILL AVAILABLE AT PRICES BELOW MANUFACTURING COSTS.

Ceramic Variable Condensers split stator 15/15 Pf., 2/6 each. Ceramic Trimmers 22 Pf., 5/- per doz. Variable Condensers 100 Pf , ceramic insulation, 2/- each. Variable Condensers in screening case 50 Pf., $1 /-$ each. Permanoid Sleeving coils of approx. I gross yds. 1 mm . and 1.5 mm ., $8 / 6$ per coil. Wave Change Switches 2 wafer 6 pole 3 -way standard $\$$ spindles, $1 / 3$ each. Porcelain Stand-offs, insulators only, miniature lin., 2/-doz. Pots 100 K and I meg. $\frac{1}{2}$ spindle and 3 -gang each 70 K all at I/- each. Humdinger Pots 100 ohm. miniature wire wound, 2/- each. Colvern do, 200 ohm. w/wound $5 \mathrm{w}, 2 / \mathrm{e}$ each. 100 K Miniature Pots fin. long spindle, I/- each. Erie Resistors 47 K 2 watt boxed in 50's. and 5's. Erie Resistors $1,200 \mathrm{ohm}, \frac{1}{2} \mathrm{~W}$. boxed in 50's 2 watt 150 K I watt, 22 K I Watt, 70 K I watt; price, 2 watt 3d., I watt 2d.; $\frac{1}{2}$ watt Id. Paxolin Resistor Panels (size $4 \mathrm{in} . \times 3 \mathrm{in}$.) with fixing brackets contains $1-10 \mathrm{w} .5 \mathrm{~K}, 2-5 \mathrm{w} .120 \mathrm{~K}$. 1-47 K, 1-56 K, 5 w. Brand new each, 1/9. Wire Wound Vitreous 10 watt wire ends $500 \Omega$ each, 9 d .
Ferranti mlamp Meters Flush Square 2 in. $0-150,7 / 6$ each, do. $0-5 \mathrm{~m} / \mathrm{a} .9 / \mathrm{e}$ each.

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## - BRRDMATC.

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 TAPE RECORDING EQUIPMENTTHE MODEL 50 TAPE DESK (to take $10 \frac{1}{2} \mathrm{in}$. NAB Reels)
Programme Time: 62 minutes at $7 \frac{1}{2}$ i. p.s.
124 minutes at $3 \frac{3}{4}$ i.p.s.
Panel size: $20 \mathrm{in} . \times 14 \frac{1}{2} \mathrm{in}$.
Two speeds, $3 \frac{3}{4}$ and $7 \frac{1}{2}$ i.p.s. Double track heads. Push button control. Fast wind and rewind. Three heavy duty motors, Three seperately shielded heads. Complete with NAB reel adaptors. PRICE: (fitred with 6RP heads) $650 / \%$ -

ALSO AVAILABLE
MODEL 5C TAPE DESK (to take Sin. Reels)
Programme Time: 55 minures at $7 \frac{1}{2}$ i.p.s.
PRICE: (fitted with 6RP heads)
Large Panel ( $20 \mathrm{in} . \times 14 \mathrm{tin}$.) E47/10/\%.
Small Panel ( $13 \downarrow \mathrm{in}$. $\times 15 \frac{1}{2} \mathrm{in}$.) $\mathbf{E 4 5 / 1 0 / -}$
MODEL 5B TAPE DESK (to take 9in. Reels)
Programme Time: 31 minutes at $7 \frac{1}{2}$ i.p.s.
PRICE: (fitted with 6 RP heads)
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In rexine covered case, fitted with model 5B tape desk, type D.2. C.J.R. amplifier with monitoring. Provision for external loudspeaker.

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Sead your enquiries lof all Rado and Electries goods, especially thone in short supply. We have probably the largest variety of valves in the country. Let us know your requirements. AVO METERS IN STOCK

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RADIO-GRAM CHASSIS
3 Wave-band Superhet. Med., long and shore.
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4 Position Switching Gram., med., long, and short.
Provision for Extension Speaker. A.C. Mains. $110 / 250$ voles.
Chassis llin. $\times 7 \mathrm{in} . \times 2 \frac{1}{2} \mathrm{in}$. Scale 8 in . Square. Or Chassis $13 \frac{1}{2} \mathrm{in}$. $\times 6 \frac{1}{2} \mathrm{in} . \times 2 \frac{1}{2} \mathrm{in}$, Dial lOin. $x$
$5 \frac{1}{2}$ in. PRICE $\in 10 / 5 /=$
BRAND NEW AND GUARANTEED. CARR. PACKING AND INS. $10 /$.

## 600ft. Reels. RECORDING TAPE

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## EF50 (VR9IA)

The selected EF50, Red Byivania, original bozes
$10 /$ each, $90 /$ for ten.

## PYE 45 Mc/s STRIP <br> TYPE 3583 UNITS

Size $15 \mathrm{im} . \times 8 \mathrm{in} \times 2 \mathrm{in}$, Complete with $45 \mathrm{Mc} / \mathrm{s}$. Pye Strip, 12 valves 10 EF50, EB34 and EA50, volume sound wad vision can be incorporated on this chawis. With minimum space. New condition. Modification data supplied. Prlce E5. Carriage paid.

## 3 SPEED RECORD CHANGER <br> Plays mixed records. Well-known manufacturer


(CASE REMOVED FOR ILLUSTRATION)


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Brand new in sealed cartons, these contain 6 EPF50's, 5 LA50's, 1 8P61, a host of condensers, renistors, transformers, chokes, relays, switches, ${ }^{7}$ pots and $59 / 8$, carriage free

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Replacernents tor Mazda 27 M 1 sud 27 M 2 .

14 WATT HIGH FIDELITY F.M. AND RECORD AMPLIFIER
$200 / 250$ volt A.C. First Quality Components only. Stewart Transformers and Chokes. Partridge Output Transformer. Bass and Treble Controls (Boost and Cut). Supply Socket for Tuner Unit. Ideal for Denco F.M.
Feeder. 5 valves- $6 S N 7,6 S L 7,6 L 6,6 L 6$,
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BARGAIN PRICE EIT/I0/m.
T.C.C. 1 mid. $5 / 7,000$ ₹. whg., type CP58QO, Bakellte case, $7 / 6$ each. BI. $12,500 \mathrm{v}$. wkg., $4 /$ -

## COMMUNICATION RECEIVER <br> TYPE P.C.R.3.

Brand new, in original cartons: 6 valves. EF39, R.F. ptage. X61, Freq. Chanker. EF39, lat I.F. stage. EF39, 2nd I.F. stage. EBC33, Det. and L.F. amp. 6 V 6 G, Output. Kanges: $12 * 41$ metres; $41-120$ metres; 200-560 metres. Aerial Trimmer control. Volume control and toue control

- Power Supply Unit for 12 volt operation $82.15 /-$ Power Supply Parta to convert to A.C. maina el/17/6


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Recelver 27/73. This is a slx-valve superhet receiver With $465 \mathrm{kc} / \mathrm{s}$ I.F. Complete with nll valves: 2
EF39, 1 EK32, 2 EF36, 1 EBC33. In brand new EF39, I EK32, 2 EF36, E EBC33. In brand new OFFER, 27/6, plue 2/6 carriage.

## TRANSMITTER/RECEIVER

## * 38 " WALKIE TALKIE SETS

We have purchased large quantity of the above " 38 " Sets, and can now offer same complete in case with 5 valves 4-VP23 and ATP4, Throat Microphone, Headphones, Junction Box and Collapsible Aerial in absolutely new condition and guaranteed Air Tested. Freq. range 7.4 to $9 \mathrm{Mc} / \mathrm{s}$. Range approx. 5 miles. Voltage 150 v . an 13 v. L.T. Set of batceries, leads and cenvas carrying bag 25/.

## 59/6 carr. s/-.

## T/V. PRE-AMPLIFIER FOR LONDON AND BIRMINGHAM <br> 45 meg. pre-amp unit complete with 2-VR91 (sligh modification necessary) $17 / 6$, p.p. $2 / 6$.

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 8 '6

POST FREE dealfor tape recording and amplifiers. No matching transformer required. macking transormer required.

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 Finest Audio available. Complete kit of parts, includiag drilled chassis. 5 vaives: types 6АM6, 12AF8, EB91 and 26 AB . Also complete circuit and wiring diagram. £8/7/6. Or assembled and aligned, $£ 8 / 10 /-$. Altga-ment only $10 /$.

## TUNING CONDENSERS

0005 Midget $24 \times 14 \times 124 n$.
0003 Standsrd Slize, with trimmers.

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## INDICATOR UNIT TYPE $182 A$

 Unit containe VCRJ17 Cathode Ray 6 in. tube complete with Mu-metal mereen, 3 EF50, 48 P61 and 1 EUSG valves, 9 wire-wound volume controls and quantity of resistors and condensers. Suitable elther tor bacis of televiston (full picture guaranteed) or Oscilloacope. Oflered BRAND NEW (less relay) In original packing cases at 67/6. Plus 7 .'scope cireuit included.

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SCR-720 RADAR EGUIPMENT EX-U.S.A. CONSISTING OF THE FOLLOWING ITEMS:
RADIO MODULATOR B.C. II42A. RADIO FREQUENCY UNIT B.C. I09IAM. CONTROL BOX B.C.II50V. RECTIFIER RA-88-A. RECTIFIER RA-90-A AND POWER EQUIPMENT RA-88-A.
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ALL THE ABOVE ITEMS ARE SOUND AND CLEAN AND FORM THE MAJOR PART OF THE COMPLETE SCR-720 SET AND OFFERED AT A FRACTION OF THE ORIGINAL COST. LIMITED QUANTITY AVAILABL ONLY. PLEASE WRITE FOR FURTHER DETAILS, ETC.

50 WATT AMPLIFIER EX-GOVT. With 4-KT66s in paralleled push-pull Standard $200-250 \mathrm{~V}$, mains input, A.C. Output impedance 600 ohms line. High imp., gram. and microphone input. Bass boost control fitted. This excellent quality amplifier is housed In a strong metal case and is ready for use. Our price $\mathbf{2 5}$, carriage paid
ELECTRIC LIGHT SLOT METERS. 200-250 v. at 5 -10 amps. I/- in slot at 6d, per unit, by Measurement Led. All bakelite case, in very good condition. $50 /$;ip.p. $2 / 6$.
TELEPHONE L/SPEAKER No. 2 (By Vitavox). Semi-re-entrant all-metal. H/Dury 6 in. P.M. 15 ohms S/Coil, with 600 ohm built-in line transformer, housed in a strong wooden case. $£ 1 / 5 /=$, carriage $5 /$ VITAVOX PRESSURE UNITS. Heavy duty, P.M. 20 watts. Brand new. \{4/9/6, carriage 5/-
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#### Abstract

COMMUNICATIONS RECEIVER ADMIRALTY TYPE B. 28 (MARCONI CR.100). Valve line up 2 RF, F.C. separate local Osc., ${ }^{3}$ l.F.s, 2 nd Det., Output, B.F.O. and rectifier. Self contained power supply $200 / 250$ volts A.C. $50 \mathrm{c} / \mathrm{s}$. Variable selectivity (crystal filter). 6,000, 3,000, 1,200, 300 and 100 cycles. Frequency coverage $60 \mathrm{kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ in six ranges, continuous except for gap between 420 to $500 \mathrm{kc} / \mathrm{s}$. Size $16 \mathrm{in} . x$ $13 \frac{1}{2} \mathrm{in} . \times 12 \mathrm{in}$. Weight 82 ib . The set for the serious operator. Thoroughly overhauled in superb condition, complete with new valves and gir tested prior to despatch. A real bargain at only $£ 30$ plus $\mathrm{E} \mid$ carriage.


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motels, as new, E9/19/6 Used models E7/19/6
$\begin{gathered}\text { models, as new, } 6919 / 6 \text { Used models } 67 / 19 / 6 \\ \text { " } " \text { and "NODELS. Cover trawler }\end{gathered}$
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$\begin{aligned} & 7 / 6 \\ & 7 / 6\end{aligned}$
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16 mid.
450
v.
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Primary: 200-220-240 V .
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tunities are. available for dealing with tunities are available for physical principles of component design and the miniaturisation of
equipment. vacancles for young engineers who
THIERE are
wish to wish to take up sales and project engineering work involving commercial as weil as technica
requirements; this work necessitates a period of laboratory tralning before undertaking overseas travel.
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Staif Officer, B.I.C.C. Itd. Prescot Lancs
MURPEY RADIO 14593 Marphy radio, Itd. have vacancles in qualifed engineers to destgn and develop the following: 1. V.H.F. and U.H.F. Comamunications equipment. 2 . Alrborne and Ground radar equipment. 3 . Computing devices and servo systems. 4. Nucleonic equipment and measuring instruments, 5. Transistors. The salary range is $\underset{\text { is }}{\text { \& } 600-E 1,000 ~ p e r ~ a n n u m ~}$
depending upon experience. are available to englneers of H. Further postand of equivalent having less eqperience, the salary "range being $£ 450-£ 650$ per annum. These vacancles ate at Welwy Garden City but one or two vacancles of a similar nature are available at the Ruislip Works.-Applications, glving age, full details of qualifications, warded to Personnel Department. Murphy Radio, Ltd., Welwyb Garden City. [4432

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[4665
Shaftesbury Ave., W.C.2.
DECCA RADAR LIMITED require the services Dor a frst-class mechanical engineer for post is a special appointment and a substantial starting salary is envisaged on a rising scale; British nationality essential; pension scheme in operation - Please write, particulars and quoting RLAB9, to the ReResea Director, Decca Radar, Ltd., Radar Research Laboratory, 2, Tolworth Rise, Sur10130 I grew up in the radio components trade and of the right kind of helpi I need someone-now - With specielized knowledge and experience like my own, who knows the business inside out, who can compile and maintain a catalogue, ledge alone insumficient must; technical knowwrite me fully if you think you are the man but remember I want someone to help me
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RLA95. Surbiton, Surrey, quoting reference
$[0192$ DRAరGHTSMEN.-An expanding production cles for mechanical deslgners, senlor daughtsmen and detail draughtsmen, situated in the Midands: the worr involves the complete engicontracts and of domestic radio and television equipment.-Applicants interested in this type of work. with or without experience. are in-
vited to apply. giving details of career and salary expected to the Pesonnel Manaker (Ret.
GLB.) Box 2438 .

4398
THE GENERAL ELECTRIC Co., Ltd., Brown's anical Lane, Allesley, Coventry, requires mechdraughtsmen and draughtsmen, preferably with experience of radar-type equipments for work on guided weapons and like projects; also required, senior and junior electronlc development engineers, particuiariy in the feld of cording to age, qualifications and experience. Apply by letter. stating age and expertence, tc
the Personnel Manager, Ref. R.G.
0259
M Technicians Of SUPPLY requires Electronics possibly at Bickly ${ }^{2}$ arnborough, Hants (and or assist in. scheduling of R.A.F. telecommunication equipment showing breakdown into sub-assemblies and components; preparing lists of spares, connectors for aircraft installations: ensuring completeness of contractors drawings.
Qualifications-British of Brtish Recognized engineering apprenticeshit or equivalent in electronics. Must have long workshop experience radio/allied equipments, able interpret drawings. specffications, circuit diagrams. Knowledge component standardization and R.A.F. servicing requirements advantageous. Rin.c. or city and Guilds or equivasalaries within $£ 535$ (age 26) - 577 grades at tion forms from A.B. 1181 . London Appoint ments Office, Ministry of Labour and National Service, 1-6, Tavistock Square. W.C.1. [4674

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several years' experience on audio frequency several years experience on audio requency
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[4526
THE General Post Office has vacancies for and radio operators at its coast radio stations 21 and 35 years of age who hold the Post-master-General's First Class Certificate of Proficlency in Radiotelegraphy; selected candi-
dates will be considered later for permanent pensionable posts.-Application should be made to The Inspector of Wireless Telegraphy, Radio and Accommodation Department. Wireless Telegraph Section, Union House, St. Martins
ie Grand, London, e.C.1.
R ADIO (Meteorological) Technicians required R by Meteorological Office. Qualiffcations: Basic knowledge of radio and radar and exequipment, including oscilloscopes. Successful applicants serve in United Kingdom and overseas. Commencing London salary $£ 467 / 10$ at age 25 or over, rising annually to $£ 565$, subject
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$B^{\text {OSH RADIO }}$ Ltd., require sentor and Junior Kew engineers in their laboratories at Chiswick. Kew and Plymouth; applicants should preferEncineering or Physics, or equivalent qualifications: experience in the following fields of deradio or television. electronic equipment for aircraft. communication receivers, pulse clrcults and micro-wave techniques.-W Wite, piving full detalls and salary required, to the [4395
A standard is required to take charge of the engineering department in a factory whlch is part of a large organisation engaged in the manufacture of all branches of communications equipment. The successful applicant will be responsible for engineering development. design
and specification of all new items, as well as and specification of all new items, as well as
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| Ave., London, W.C.2. Advg., 212a, Shaftesbury |
| :--- |
| [4490 |

MANAGER required for a unit of a wellIn established engineering company engaged in large-scale production of radio and television; the successful candidate will have a specia ised knowledge of this class of work and
will be capable of advising and supervising the design laboratorles, tool design supervising the machine and assembly departments; this vacancy offers ample scope and opportunity to a man with high administrative ability; salary
up to $£ 2,500$ per annum; London area.-Please up to $£ 2,500$ per annum; London area.-Please reply ${ }^{\text {in }}$ in confidence, giving full details, to
[ 4535
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Ltd. Research Laboratories, 2, Tolworth Rise, Ltd., Research Laboratories, 2, Tolworth Rise,
Surbiton, Surrey.
$[0191$ TECHNICAL sales/service manager required - for British West African branches of large British company distributing domestic radio receivers, V.H.F. radiotelephone equipment, intercommunication telephones, domestic and commercial refrigerators, air conditioners and ground essential; ${ }^{\text {good }}$ refrigeration experience desirable: frmiliarisation course arranged with O.K. manufacturers prior to departure for Arrica; first-class passage sea/air, free furnished quarters, pull pay on leave after approximately 18 -month tours, pension scheme; apply in own handwriting stating age
(preferably between 21 and 30 ). whether (preferably between 21 and 30 ). whether married or single, full details education, qualience; original references should not be sent.-
Apply T. S. D., Box 1134 .

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TEST Engineers are sionacant - Midlands manufacturer required by a Leading and Fault-Finding on Radar Units and other Electronic Devices. (2) Construction and maintenance of Test Equipment. (3) Testing and Fault-Finding on domestic Radio and Television Recelvers. These progressive positions cover a wide range of activities and selection will be made not only on experience but also on abillty to respond to further training. ExApplicants should write, piving detalls of career Appicants should write. giving detalls of career Manager (Ref. GLB.). Box 2540 . $\quad$. 4426 A pplications are invited from senior proof the manufacture of electrical and mechanical products; applicants should have a good practical engineering background and a sound technical experience of tool design and planning and be capable of putting new projects on a excellent opportunities to men seeking permaexcellent opportunities to men seeking permaApplications, which will be treated in conndence, should glve full detalls of experience | and salary required, and be addressed to Box |
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| 3085 . |
| 4557 |

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Lower Sydenham, $\mathrm{F} . \mathrm{E} .26 \mathrm{~F}$.
A IRCRAFT radio aerials.-Gloster Aircraft an electronic engineer (H.N.C. or equivalent) an electronic engineer (H.N.C. or equivalent) aerials for aircraft; the work involves theoretical and practical knowledge of measurements from "H.F." to "X" bands and of the properties of different types of suppressed aerials. A SMALL laboratory is being established for the work; an elementary knowledge of aircraft
design and construction would be an advantage. -Applications, stating age, previous employers and experience, etc.. should be addressed to the Employment Officer. UNIVERSITY OF SOUTHAMPTON development of electronic instruments required in the department of aeronautical engineering; the selected candidate (Who should be of degree or H.N.C. standard) will be expected to apply his knowledge to the problems which occur in aerodynamic research and to co-operate on such problems.-Applications in writing. giving full details of education, qualincations and experience, together with names of two
persons to whom reference may be made to persons to whom reference may be made, to
The Secretary and Registrar, before May 32 st.
[4610
THE Mullard Radio Valve Co., Ltd., has a number of vacancles for Electrical EnResearch Work in the applications of transistors and kindred devices; the fleld offers opportunities for original work and at times requires considerable ingenuity; further advanced studies and publication of results is encouraged. IT is intended that the posts will eventually carry considerable technical responsibility in an cants should possess a good honours degree and some previous experience or, alternatively. a real interest in electronies would be an advantage.
COMMENCING salary will be according to individual qualifications and experience and will provide progressive remuneration for increased responsibilities; applications in writing, which dressed to-Personnel officer, The Mullard Radio Valve Co., Ltd., New Rd.; Mitcham Junction, surrey, quoting ref. JFG/H.1.
JUNIOR development engineers are urgently prequired to assist in lratory instruments; successful applicants will be engaged on interesting long-term projects concerned with the development of a wide range of equipment; the appointments are permanent and carry should have had previous development experience preferably in the instrument feld: academic qualifications ranging from H.N.C. to degree standard are preferable; salaries are dependent upon age, qualifications and experi-ence.-Apply stating tril dilails to the Eersonnel Manager, Furzehill Laboratories. SENIOR methods engineer required by a large situated in the London area; applicatoms are situated in the London area; applications are invited from men ivith good engineering qualiradio, television and services equipment; the accepted candidate will have extensive experience of this class of work and will be acquainted with the most up-to-date production methods, including work study and standard costs; for a man with the required knowledge, excellent prospects; salary range from provides £1,500 per annum.-Please reply, in confidence, glving full detalls of previous experience. to
[ 4536

First-class Design Draughtsmen required for high production press tools, jigs, fixtures, etc., for valve and cathode ray tube components. Background of practical experience and O.N.C. least qualification, but H.N.C. preferred. Experience in the use of tungsten carbide an advantage. Rates substantially above normal minimum for men of suitable experience. Five-day week, staff pension scheme, modern welfare amenities. Apply Personnel Superintendent,

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 eers and Maintenance Engineers required with practical experience of this class of work, based on sound knowledge of electronic principles. These vacancies are permanent and progressive. A company pension scheme in operation. London Area. Please write, in confidence, giving full details of qualifications to Box No. 3447.Special purpose machinery and equipment design draughtsmen required. O.N.C. least qualification, but H.N.C. preferred. Men with imagination and initiative to develop original ideas with minimum direction. Basic applied electrical knowiledge an advantage. Rates substantially above normal minimum for men with suitable experience. Five day week, staff pensions scheme, modern welfare amenities. Apply Personnel Superintendent,

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[^1]:    "F.M.Q." by W. S. Mortley, A.M.I.E.E., Wireless World, October 195i, p. 399.

[^2]:    * Mullard Valve Measurement and Application Laboratory. + Partridge Transformers, Ltd.-Type P3878.

[^3]:    * Ultra Electric.

[^4]:    - To be precise, one should multiply $1 / g_{m}$ by $\mu /(\mu+1)$, but that makes Tittle difterence unless $\mu$ is except:onally small.
    $\dagger$ That is why the rerm "anode follower" for the see-saw circuit is so silly; in it the anode docs just the opposite of following the grid.

[^5]:    If the principles of this kind of diagram are not understood, see next month's article.

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[^12]:    THE RADIO AND ELECTRICAL MART 253 B PORTOBELLO ROAD, LONDON, W.II. Phone: PARK 6026.

