

PRACTICAL WIRELESS

APRIL
1974

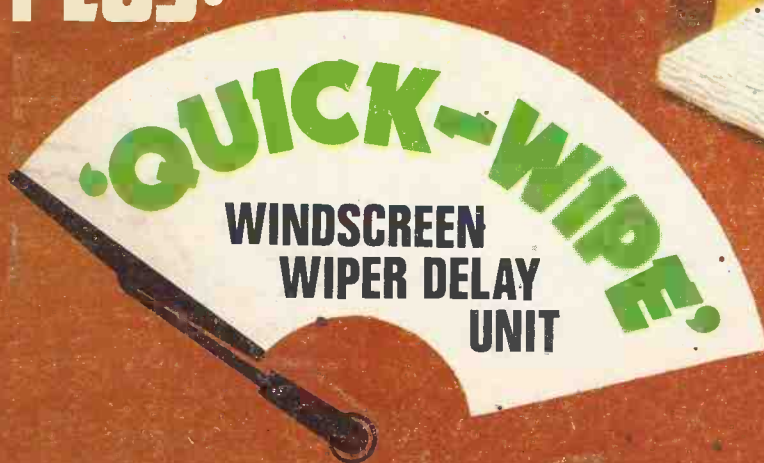
25p



the
'SLIMLINE'
5-Band
Receiver



PLUS:



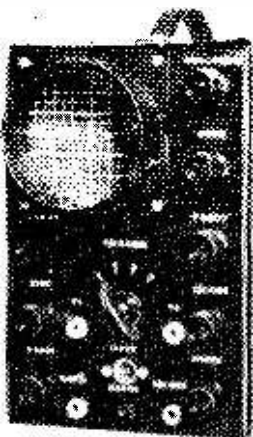
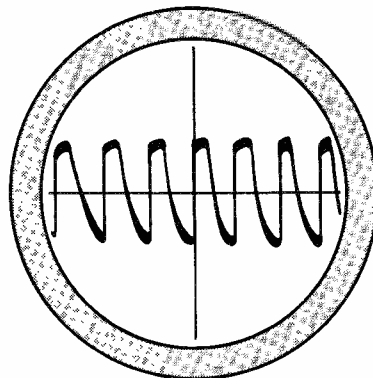
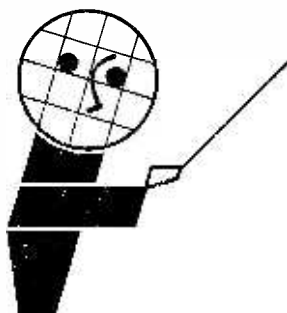
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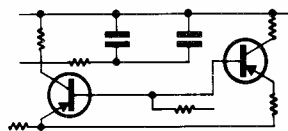
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PRACTICAL WIRELESS

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APRIL 1974

BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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BACK NUMBERS

We regret that we are unable to supply back numbers of Practical Wireless. Readers are recommended to enquire at a public library to see copies. Requests for specific back numbers of Practical Wireless and Television only can be published in our CQ Column.

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We regret that we cannot answer technical queries by telephone nor can we provide information or advice on manufacturers' products other than that given in the magazine. We will endeavour to assist readers who have queries relating to articles published but we cannot offer advice on modifications to our published designs. All correspondents expecting a reply should enclose a stamped addressed envelope.

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ON LEADING BRAND HI-FI

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★ FULL LABOUR AND MATERIAL GUARANTEES FOR 12 MONTHS

LOW DEPOSIT TERMS OVER 8 MONTHS

	List Price	RSC Price
WHARFEDALE DENTON	£39.93pr	£29.95
WHARFEDALE LINTON	£48.69pr	£35.95
LEAK 150	£46.82pr	£37.50

Prices shown correct at time of going to press 12.2.74

AKAI GXC 36D Tape Unit	£76.95 (Rec. Price £109.50)	Carr. £1
AKAI 4000DS Tape Unit	£76.95 (Rec. Price £109.50)	Carr. £1
AKAI 1721L Tape Unit	£79.95 (Rec. Price £114.50)	Carr. £1
AKAI GXC46D Tape Unit	£104.75 (Rec. Price £149.50)	Carr. £1
GOLDRING GL72 T/Table & P.U.	£29.95 (Rec. Price £37.29)	Carr. 75p
with Free Goldring G800 Cartridge worth over £10 fitted to above unit.		
GOLDRING GL75 T/Table & P.U.	£34.95 (Rec. Price £47.19)	Carr. 85p
with Free Goldring G800 Cartridge worth over £10 fitted to above unit.		
BSR MP60 T/Table & P.U.	£9.95 (Rec. Price £14.95)	Carr. 40p
T/TABLES with MAGNETIC CARTRIDGE/PLINTH & COVER		
GARRARD SP25 with G850	£16.95 SPECIAL PRICE	(Carr. £1)
MacDonald MP60 with G800	£17.95 SPECIAL PRICE	(Carr. £1)
GARRARD AP76 with G800	£28.95 SPECIAL PRICE	(Carr. £1)



MARQUESS 30 MacDONALD MP60
MARQUESS 30 MODEL 60 AMPLIFIER

A HIGH FIDELITY 30 + 30W STEREO SYSTEM

AUDIO FIDELITY MODEL 60 AMPLIFIER.
PAIR AUDIO FIDELITY MARQUESS 30 SPKR'S.
MacDONALD MP60 with G800 Cartridge. Total Value over £165
Ready wired on Plinth with Cover.
Cabinet finished in Teak Veneer.
Send S.A.E. for leaflet. Carr. £3

£99.95

HI-FI 10 + 10W STEREO SYSTEM

AUDIOTRINE STEREO 20 AMPLIFIER
GARRARD TUNABLE with Sonotone Cart-ridge wired on Plinth with cover
PAIR DIPLOMAT 10W SPEAKERS
Teak Veneer finish

SPECIAL PURCHASE Worth Double **£55**

RSC G66 MkII 6.6 WATT high quality STEREO AMPLIFIER

Controls: Bass, Treble, Vol. and Bal. 10 J transistors plus Diodes. Output rating I.H.F.M. Frequency range 20-20,000 c.p.s. Bass Control ± 12db. Treble Control ± 13db. Selector switch for P.U. or Tape/Radio. For loudspeaker output impedances of 3 to 15 ohms. For standard 200-250v. A.C. mains operation. Attractive Black and Silver finished metal fascia plate and matching control knobs. COMPLETE KIT OF PARTS INCLUDING FULLY WIRED PRINTED CIRCUIT and COMPREHENSIVE WIRING DIAGRAMS & INSTRUCTIONS **£12.75** Carr. 40p
Or FACTORY BUILT IN TEAK VENEERED CABINET as illustrated **£16.50** or dep. £2-12 and 8 monthly payments £2-12 (Total £19.00).

AUDIOTRINE HIGH FIDELITY SPEAKERS

Heavy construction. Latest high efficiency ceramic magnets. Plasticised Cone surround. "D" indicates Tweeter Cone providing extended frequency range up to 15,000 c.p.s. Impedance 3 or 8-16 ohms. PLEASE STATE CHOICE.
Exceptional performance at low cost.

HF909T 8" 10W	£2.98	HF120D 12" 15W	£5.50
HF102D 10" 10W	£3.30	HF126 12" 15W	£6.85
HF120 12" 15W	£4.95	HF126D 12" 15W	£6.85

FANE 807T HIGH FIDELITY SPEAKER

A full range 8in. 10 watt unit for excellent sound quality, in suitable enclosure. Cast chassis Roll P.V.C. cone surround and long throw voice coil to achieve very low fundamental resonance of 30 c.p.s. Tweeter cone is fitted to extend high note response. Frequency range 25 Hz to 15 KHz. Gauss 10,000. Impedance 3 or 8-15Ω. **£3.99**
PLEASE STATE IMPEDANCE REQUIRED List £4.99
MODEL 808T 8" 15w. with parasitic Tweeter. **£5.50** List £6.49
Response 25 Hz to 15 KHz. Gauss 13,000 Imp. 3 or 8-15Ω.

R.S.C. MkIII SUPER 30 HIGH FIDELITY STEREO AMPLIFIER

BUILD AN AMPLIFIER WORTH APPROXIMATELY DOUBLE THE KIT PRICE INCLUDING CABINET
Only high grade components by leading manufacturers

- ★ Push Button Selector Switching
- ★ Jack Socket for Headphones
- ★ Neon Indicator
- ★ Satin Silver Finish Metal Fascia
- ★ Solid State Circuitry
- ★ Twenty Silicon Transistors
- ★ Four Diodes, Four Rectifiers

Send S.A.E. for full descriptive leaflet.

R.S.C. STEREO FM III TUNER. in cabinet **£37.50**
Visually matches Super 30 Mk. III

For Magnetic or Ceramic Pick-Ups regardless of Price. Output (per channel) 15 watts RMS into 8Ω. Frequency Response 7 Hz to 70 KHz ± 1 1/2 dB.

FACTORY BUILT UNIT INC. CABINET with 12 months' guarantee. Or Dep. £7 and 8 monthly payments £5-17 (Total £48.36). **£42.50**



COMPLETE KIT (less cabinet). Carr. 70p. Cabinet if req. **£22.50** £5 extra.

HI-FI SPEAKER ENCLOSURES

JE8 Size 16" x 11" x 9". Pressurised. Gives pleasing results with any 8in. Hi-Fi speaker. **£5.50**
SE10 For outstanding results with 10in. Hi-Fi spkr. Size 25 1/2 x 16 x 9in. Ported **£6.75**
SE8 For optimum performance with any 8in. Hi-Fi speaker. Size 19 x 10 1/2 x 9in. SE12 For excellent performance with 12in. Hi-Fi speaker and tweeter 25 1/2 x 16 x 9in. **£7.95**

AUDIOTRINE HI-FI SPEAKER SYSTEMS

Consisting of matched 12in. 11,000 line 15 Watt 15 ohm high quality speaker, cross-over unit and tweeter. Smooth response and extended frequency range ensure surprisingly realistic reproduction. Or SENIOR 15 WATT INCLUDING HF126 15,000 LINE SPEAKER **£7.65** Carr. 39p

R.S.C. TA6 6 Watt HI-FI AMPLIFIER

200-250v. AC mains operated. Response 30-20,000 c.p.s. -24dB. Separate Bass and Treble 'lift and cut' controls, 3 input sockets for Mike, Gram, Radio or Tape. Input selector switch. Output for 8 x 15 ohm spkrs. Max. sensitivity 5mV. O/P rating I.H.F.M. Enclosed enamelled case 9 1/2 x 2 1/2 x 5 1/2in. Silver finish fascia 10 1/2 x 3 1/2in. Complete kit, wiring diagrams and instructions. Or FACTORY BUILT **£10.95** Carr. 40p.

R.S.C. TA12 MKIII 6.5-6.5 WATT STEREO AMPLIFIER

Fully Transistorised. Solid State. Hi-Fi o/p of 6.5 watts per channel. Designed for optimum performance with any crystal or ceramic Gram. P.U. Cartridge, Radio Tuner, Tape Recorder, etc.
COMPLETE KIT OF PARTS WITH FULL WIRING DIAGRAMS & INSTRUCTIONS **£12.99** Carr. 40p
Factory built with 12 mths guarantee **£16.95**
Or in Teak Veneer housing **£19.95**
Dep. £2-50 & 8 mthly pymts £2-50 (Total £22.50). Send S.A.E. for leaflet.

AUDIO FIDELITY FRI SPEAKER KIT

Response 30Hz-15KHz. Imp. 8-15 ohm 8" Bass Unit. Pressure-Tweeter. Cross-over etc. **£11each** Carr Free
SPECIAL OFFER **£14.95** Pair Carr. 45p.

'YORK' HIGH-FIDELITY 3 SPEAKER SYSTEM

Moderate size only 25 x 14 x 10in. approx. COMPLETE KIT
★ Response 30-20,000 c.p.s. Impedance 15 ohms
★ Performance comparable with units costing considerably more **£25** Carr. 75p
Consists of (1) 12in. 15 watt Bass unit with cast chassis. Roll rubber cone surround for ultra low resonance. (2) 3-way quarter section series cross-over system. (3) 8 x 5in. high flux middle range speaker. (4) Dome Pressure Tweeter. (5) Quantity acoustic damping material. (6) Handsome Teak veneered cabinet. (7) Circuit and full instructions. Terms: Deposit £3-71 and 8 monthly payments £3-12 (Total £28-67).

R.S.C. TRANSFORMERS, L.F. CHOKES & RECTIFIERS FULLY GUARANTEED.

RIDGET CLAMPED TYPE 2 1/2 x 2 1/2 x 2 1/2in.

250v., 60mA, 6.3v. 2a	£1.10
250-0-250v., 60mA 6.3v. 2a	£1.16

FULLY SHROUDED UPRIGHT MOUNTING

250-0-250v. 60mA, 6.3v. 2a., 0-5-6.3v. 2a.	£1.55
250-0-250v. 100mA, 6.3v. 4a., 0-5-6.3v. 3a.	£2.45
300-0-300v. 100mA, 6.3v. 4a., 0-5-6.3v. 3a.	£2.45
300-0-300v. 130mA, 6.3v. 4a. c.t., 6.3v. 1a.	£2.45
For Mullard 610 Amplifier	£2.95
300-0-350v. 100mA, 6.3v. 4a., 0-5-6.3v. 3a.	£2.45
300-0-350v. 150mA, 6.3v. 4a., c.t., 5v. 3a.	£2.95
425-0-425v. 200mA, 6.3v. 4a., Twice 5v. 3a.	£2.95
425-0-425v. 200mA, 6.3v. 4a., Twice 5v. 3a.	£2.95
460-0-460v. 250mA, 6.3v. 4a., c.t., 5v. 3a.	£2.00

TOP SHROUDED DROP-THERO TYPE

250-0-250v. 70mA, 6.3v. 2a., 0-5-6.3v. 2a.	£1.49
250-0-250v. 100mA, 6.3v. 3.5a.	£1.71
250-0-250v. 100mA, 6.3v. 2a., 0-5-6.3v. 1a.	£1.75
250-0-250v. 80mA, 6.3v. 2a., 0-5-6.3v. 2a.	£1.81
250-0-250v. 100mA, 6.3v. 4a., 0-5-6.3v. 3a.	£2.45
300-0-300v. 100mA, 6.3v. 4a., 0-5-6.3v. 3a.	£2.45
300-0-300v. 130mA, 6.3v. 4a., c.t. 6.3v. 1a.	£2.85
Suitable for Mullard 610 Amplifier.	£2.85
250-0-250v. 100mA, 6.3v. 4a., 0-5-6.3v. 3a.	£2.45
300-0-300v. 150mA, 6.3v. 4a., 0-5-6.3v. 3a.	£2.85

FILAMENT or TRANSISTOR POWER PAOK

Type 6.3v. 1.6a. 55p.	6.3v. 2a. 60p.	6.3v. 3a. 85p.
6.3v. 6a. £1.45.	12v. 1a. 61p.	12v. 3a. or 24v. 1.5a. £1.50.
0-9-18v. 11a. £1.25.	0-12-25-42v. 2a. £1.95.	

SELENIUM RECTIFIERS F. W. (Bridged) All 612v. D.C. output. Max. A.C. input 18v. 1a, 25p. 2a. 89p. 3a, 55p. 4a, 72p. 6a, 88p.

SMOOTHING CHOKES

160mA, 7-10H, 250 Ω	77p.
100mA, 10H, 200 Ω	88p.
80mA, 10H, 350 Ω	55p.
60mA, 10H, 400 Ω	28p.

CHARGER TRANSFORMERS 0-9-15v. 1a. £1-10. 2 1/2a. £1-25; 3a. £1-40; 5a. £1-60; 6a. £1-85; 8a. £2-20
AUTO (Step UP/step DOWN) TRANSFORMERS 0-110/120v. 200-230-250v. 50-80 watts £1-25. 150 watts, £2-10 250 watts £3-00; 500 watts £6-40

OUTPUT TRANSFORMERS

Push-Pull 8 watts EL84 to 3 Ω or 15 Ω	85p
Push-Pull 10 watts 6V6, ECL86 to 3-5-8-15 Ω	£1.55
Push-Pull EL84 to 3 or 15 Ω 10-12 watts.	£1-50
Push-Pull Ultra Linear for Mullard 610, etc.	£2-45
Push-Pull 15-18 watts, sectionally wound 6L6, KT66, etc., for 3 or 15 Ω	£2-20
Push-Pull 20 watt high quality sectionally wound EL84, 6L6, KT66 etc. to 3 or 15 Ω	£3-85

RSC

DISCO SYSTEM

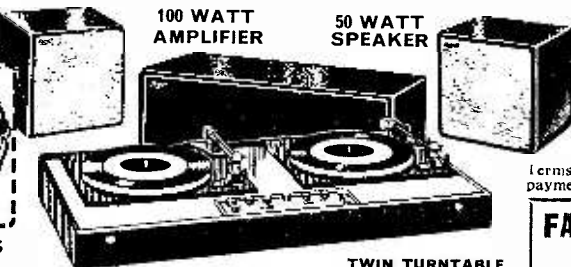
50 WATT SPEAKER

100 WATT AMPLIFIER

50 WATT SPEAKER



HEADPHONES MICROPHONE



TWIN TURNTABLE WITH PRE-AMP

R.S.C. COLUMN SPEAKERS

All types 15 Ohms covered in Rexine and Vynair TYPE C4100 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN

TYPE C132 30-40 WATTS Fitted two exceptionally efficient, low feedback howl characteristic high flux 13" x 8" 20 watt speakers. Terms: Dep. £23.95 and 8 mthly payments £2.67 (Total £25.81) Carr. 65p **£21.95**

TYPE C4100 100 WATTS Inc. four 12" 50 watt speakers for conservative rating. Extra heavy construction. Size approx. 68x16x10" Acoustically filled and pressurised. Terms: Dep. £22.00 & 12 mthly. pyts. £4.20 (Total £27.48). Carr. £1.50 **£66.00**

TYPE C818 50 WATTS Low feedback characteristic. Fitted three 13" x 8" deep cone high flux speakers with high power voice coils. Size approx. 64" x 14" x 11". Dep. £4.72 & 8 mthly pynts **£32.72**

IDEAL FOR VOCALISTS AND PUBLIC ADDRESS

- Units listed below
 (a) 100w POWER AMPLIFIER
 (b) PAIR OF HI-FI HEAD PHONES
 (c) MATCHING DYNAMIC 'MIKE' (attached to h'phone)
 (d) PAIR 50 WATT SPEAKERS
 Black Rexine covered Cabinets. Size approx. 18" x 18" x 8"
 (e) RSC TDI DISCO CONSOLE

(a) (b) (c) (d) & (e) **£149.95**
Carr. £3.00

Terms Deposit £50 and 18 monthly payments of £7.06 (Total £177.08).

RSC TDI DISCO CONSOLE

Incorporating twin Garrard SP25 or BSR MP60 type turntables and Sonotone or Aco Cartridges with Diamond styl. Separate Vol. controls for each turntable. Also MONITORING FACILITIES, plus Treble and Bass Controls. Separate input for 'mike' with vol. control switch. Black Vynide covered Cabinet with lid, see illustration on left. Or Dep. £28.50 and 12 mthly pynts **£69.95**
(Total £77.98) Carr. £1.50

FANE ULTRA HIGH POWER LOUDSPEAKERS

All power ratings are R.M.S. continuous. 2 YEARS' GUARANTEED High flux ceramic magnets. ALL CARRIAGE FREE.

'POP' 100	'POP' 60	'POP' 50
18" 100 Watt 14,000 gauss 8/150	15" 60 Watt 14,000 gauss 8/150	12" 50 Watt 12,000 gauss 150
£27.50	£15.75	£12.75
Dep: £3.50 and 8 mthly payments of £2.50 (Total £31.50)	Dep. £2 and 8 mthly payments of £2 (Total £18)	Dep £1.71 and 8 mthly payments of £1.71 (Total £15.28)
FOR BASS GUITAR, ELECT. ORGAN, ETC.		

'POP' 55 12" 60W
Gauss 15,000 Imp 8/15 Or Dep £2.45 and 8 monthly payments £2 (Total £18.45) Carr. Free **£15.95**

FANE SPEAKERS 'POP' 25/2 12 in. 25 WATT

Dual Cone 15 Ω (for uses other than Bass Guitar or Electronic Organ). Carr. free **£8.75** or Dep. £1.15 and 8 mthly payments £1.15 (Total £10.35).

GROUP EQUIPMENT PACKAGE OFFERS

F.A.L. PHASE 50 MK.III AMPLIFIER	FR. FANE POP 50 L/SPEAKERS	PACKAGE PRICE
£39.98	£25.50	£51.95
Terms: Deposit £17.32 and 12 monthly payments of £3.38 (Total £25.98)	Terms: Deposit £20 and 12 monthly payments of £3.90 (Total £66.80)	Carr. £1.10
F.A.L. PHASE 50 MK.III AMPLIFIER	FR. FANE POP 50 L/SPEAKERS	PACKAGE PRICE
£39.98	£25.50	£59.99
Terms: Deposit £20 and 12 monthly payments of £3.90 (Total £66.80)	Terms: Deposit £20.00 and 12 monthly payments £3.80 (Total £66.80)	Carr. £2.00
F.A.L. PHASE 50 AMPLIFIER	PAIR L12/20 SPEKRS (in Cabinets)	PACKAGE PRICE
£39.98	£26.80	£59.99
Terms: Deposit £20.00 and 12 monthly payments £3.80 (Total £66.80)	Terms: Deposit £20.00 and 12 monthly payments £3.80 (Total £66.80)	Carr. £2.00

HIGH QUALITY LOUDSPEAKER UNITS

ALL TWO TONE REXINE AND VYNAIR FINISH L125 50 WATT Fitted pair of 12" 50 watt high flux speakers for conservative rating. Impedance 8-15 ohms. Carr. £1.50 Or deposit £5.95 and 8 monthly pyts. of £4.72. Total £43.71
L12/20 12" 25 WATT 13,000 Ohm. Size approx. 14" x 14" x 9". Carr. 60p. Dep. £2.25 & 8 mthly pynts £1.04 (Total £10.57) **£37.95**

ALL RSC PRICES INCLUDE VAT

INTEREST CHARGES REFUNDED on Credit Purchases settled in 3 months

MINSTREL 8W GUITAR AMP.
Incorporating Tremolo and 13" x 8" or 10" Speaker. Output 8 watts R.M.S. Continuous. 3 Jack Inputs for Microphone and Instrument. Mains Neon Controls: Volume, Tone, Tremolo Speed Tremolo Intensity. Terms: Deposit £3.95 and 8 monthly payments £2.89 (Total £25.07). Carr. free **£19.95**

FANE CRESCENDO SPEAKERS
Full range available at ALL BRANCHES

FAL PHASE 50 Mk.III AMPLIFIER 50 WATT.

Solid state. 4 Separately controlled inputs Plus master vol. control. Ind. Bass and Treble Controls. Protective circuit to guard against damage from accidental shorts. Output for Speaker/s 3 to 30 ohms. Size 17" x 7" x 7 1/2". 200-250V. A.C. mains. Output 50 watts music rating. Or deposit £9.95 & 8 monthly payments £4.31. Total £44.41. **£39.95**



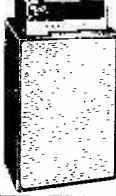
RSC PHANTOM '50' Combined 50W Amplifier and 12in. Loudspeaker.

For Lead Guitar, Mic., Gram, Radio, Tape (Not for use with Bass instruments). Inc. 3 inputs and 2 vol. controls plus Treble, Bass and Presence. Output Jack for additional 15 ohm Speaker. Attractively finished in black with silver-finished fascia and trimmings. Compact size. Fitted carrying handle. Terms: Deposit £20.00 and 12 monthly payments £3.90 (Total £66.80). Carr. £1.50 S.A.E. for leaflet. **ONLY £59.95**



REGENT 50 AMPLIFIER

A powerful high quality all-purpose unit for lead, rhythm, bass guitar, vocalists, gram, radio, tape. Peak Output rating. Loudspeaker unit either horizontal or vertical mounting.
★ Two extra heavy duty 12in. 50w Loudspeakers.
★ Four Jack Inputs and two Volume Controls for instant use of up to four pick-ups or "mikes". Bass and Treble controls. Send S.A.E. for leaflet.
Credit Terms: Deposit £24.50 & 12 monthly payments of £4.68. (Total £60.66) Carr. £2.50 **£72.50**



GP30 AMPLIFIER For Guitar, Vocal or Instrumental Group

A 4 input, 2 vol. control Hi-Fi 30 watt unit with Separate Bass and Treble controls. Current valves. Peak output rating. Strong Rexine covered cabinet with handles. Attractive black/silver P.V.C. fascia. Neon indicator. For 200-250V. A.C. mains. For 3 or 16 ohm speakers. Send S.A.E. for leaflet. Terms: Deposit £4.40 and 8 monthly payments of £3.09 (Total £29.12). Carr. 75p **£25.85**



R.S.C. BATTERY/MAINS CONVERSION UNITS

TYPE BM1. An all-dry battery eliminator. Size 5 1/2 x 4 1/2 x 2 1/2 in. approx. Completely replaces batteries supplying 1.5v and 90v, to battery radio where A.C. mains 200/250v. 50c/s is available. Carr. 30p. **£4.15**



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HI-FI CENTRES LTD.

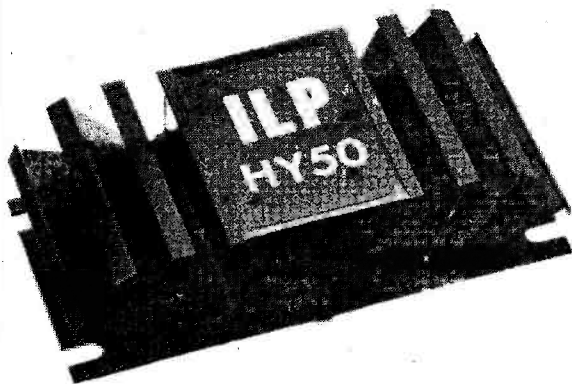
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- MAIL ORDERS & EXPORT ENQUIRIES TO:— AUDIO HOUSE, HENCONNER LANE, LEEDS, 13. Tel: Pudsey (09735) 77681.
- TERMS C.W.O. or C.O.D. No C.O.D. under £1. POSTAGE 25p EXTRA UNDER £2. 30p EXTRA OVER £2 OR AS QUOTED. TRADE SUPPLIED. S.A.E. PLEASE WITH ENQUIRIES.
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I.L.P. (Electronics) Ltd

SECOND GENERATION 25 WATT HYBRID



A brand new hybrid fabrication technique, recently perfected in our laboratories, has enabled us to achieve our latest range of completely integrated devices. We have now finally reduced the modular amplifier to a simple input/output device requiring only the addition of a basic unstabilized (split line) power supply. The HY50 takes medium power modules to their logical conclusion by incorporating with it a heatsink, which is designed in special high conductivity alloy, sufficient for normal audio use without additional chassis sinking. All this without significantly increasing the size of the module comparable in size to a packet of 'King-size' cigarettes.

Consistent with modern thinking a triple rated output circuit with a load fuse allows for peak transient response without distortion but ensures the necessary protection.

OUTPUT POWER: 25 watts RMS, 50 watts peak music power
LOAD IMPEDANCE: 4-16Ω into 8Ω
INPUT SENSITIVITY: Odb (0-775 volts RMS)
INPUT IMPEDANCE: 47KΩ
TOTAL HARMONIC DISTORTION: Less than 0-1% at 25 watts typically 0-05 better than 75db
SIGNAL/NOISE RATIO: 10Hz-50KHz ± 1db
FREQUENCY RESPONSE: ± 25 volts
SUPPLY VOLTAGE: 105 x 50 x 25 mm
SIZE:

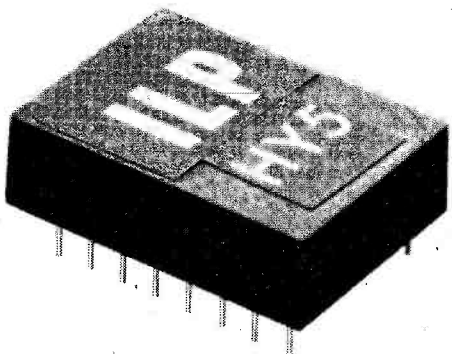
SPEC.

25 watts RMS, 50 watts peak music power
 4-16Ω into 8Ω
 Odb (0-775 volts RMS)
 47KΩ
 Less than 0-1% at 25 watts typically 0-05 better than 75db
 10Hz-50KHz ± 1db
 ± 25 volts
 105 x 50 x 25 mm

Price £5-80 mono, £11-60 stereo

Price inclusive of VAT & P & P

NEW HY5 PRE-AMPLIFIER



Unchallenged for two years, the HY5, our unique multifunction preamplifier/tone hybrid, has been brought into line with the advancements in our power hybrids.

Like the HY50, the new HY5 has no external components & has been redesigned to run off a split power-line with improvements in signal/noise, overload, capability & reduced distortion. The output has been increased to match the power module (Odb), and to share the same power supply. Overall size is reduced by the use of a new thin film circuitry while the device still retains all the functions of the earlier device.

When combined with the HY50 & power supply only potentiometers are required to complete a simple mono amplifier with input & output facilities expected to be found on Hi-Fi amplifiers.

The combination of two HY5's two HY50's sharing a common power supply (PSU50) are linked by a balance control to form a complete stereo system.

INPUTS

Magnetic Pick-up 3mV (within 1db RIAA curve)
 Ceramic Pick-up up to 3mV
 Microphone 10mV
 Tuner 250mV
 Auxiliary 3-100mV
 Input impedance 47kΩ 1kHz

OUTPUTS

Tape 100mV
 Main output, Odb (0-775volts)

ACTIVE TONE CONTROLS

Treble ± 12db at 10kHz

Bass ± 12db at 100Hz

OVERLOAD CAPABILITY (equalization stage) 40db on most sensitive input

OUTPUT NOISE LEVEL (below 10mV magnetic input) 68db

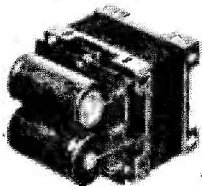
DISTORTION 0-05% at 1kHz

SUPPLY VOLTAGE ± 16-25 volts

SUPPLY CURRENT 15mA

Price £4-85 mono, £9-70 stereo

Price inclusive of VAT & P & P



POWER SUPPLY PSU50

The new PSU50 has a low profile look being only 2½ inches high and can be used for either mono or stereo systems.

SPEC.

OUTPUT VOLTAGE ± 25 volts

INPUT VOLTAGE 210-240 volts

SIZE L. 70, D. 90, H. 60 mm

Price £5-23

Price inclusive of VAT & P & P

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UK's LARGEST RANGE OF KITS & GADGETS

TEST EQUIPMENT

- MULTIMETERS**
 (carr. etc. 30p)
- M210 (Case £1-25) 20K/Volt Slimline 6-75
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- SE250B Pocket Signal Injector 2-10 carr. 15p
 - SE500 Pocket Signal Tracer 1-70 carr. 15p
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 - TE40 AC Millivoltmeter 1-2mHz 19-75 carr. 35p
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- New Revolutionary Super tester 680R**
 680R Multi-tester Accessories £18 50
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 - Phase Sequence 5-95
 - EHT Probe 5-95
 - Shunts 25/50/100A 4-50

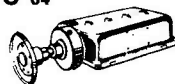
- A SELECTION OF INTERESTING ITEMS**
- C3025 Compact transistor tester 6-50 p & p 15p
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 - E1310 Stereo mag. cart. preamp. 4-80 p & p 25p
 - E4100 Telephone amplifier 7-50 p & p 25p
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- MW/LW CAR RADIO AKAI GXC40**
 + or - Earth with speaker Stereo cassette recorder, and fixings. £6-50 carr./packg, 30p.
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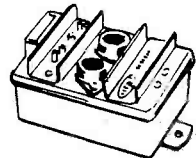
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UHF TV TUNERS CHANNELS 21 to 64
 Brand new transistorised geared tuners for 625 Line Receiver IF output. £2-50. Carr. 20p.



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 - 130 Mono control unit 4-55
 - 605 Power supply for 115 3-90
 - 610 Power supply for 120 4-55
 - 615 Power supply for 2 x 120 5-75
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 - 240 Auto packing light 5-90
 - 275 Mic. preamplifier 6-08
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 - 575 Sq. wave generator 20Hz-20KHz 14-80
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ALL KITS OFFERED SUBJECT TO STOCK AVAILABILITY

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BUILD THIS TUNER

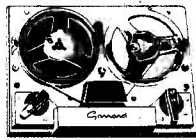
MW/LW Radio Turner to use with any amplifier. Features Mullard RF/IF module Ferrite aerial, built in battery. Excellent results. Size 7" x 2 1/2" x 3 1/2". All parts £4-85, carr. 15p.

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- All transistor circuits with hand books

BUILD THIS RADIO

Portable MW/LW radio kit using Mullard RF/IF module. Features MW - bandspread for extra selectivity. Slow motion tuning. Fibre glass PVC cabinet. 600MW output. All parts £7-98 (battery 22p), carr. etc. 32p.



GARRARD BATTERY TAPE DECK

GARRARD 2 speed 9 volt tape decks. Fitted record/play and oscillator/Erase heads. Wind and rewind controls. Takes up to 4" spools. Brand new complete with head circuits. £9-50 carr. 30p

TOP QUALITY SLIDER CONTROLS

60mm stroke high quality controls complete with knobs (post, etc. 15p any quantity).

Singles Log and Lin
 5K, 10K, 22K, 50K, 100K, 250K, 500K, 1 Meg. 45p each.

Ganged Log and Lin
 10K, 22K, 50K, 100K, 250K, 65p each. (Quantity discounts available)

Complete with knobs.

MARRIOT TAPE HEADS

4 TRACK MONO or 2 TRACK STEREO '17' High Impedance £2-00

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R730/E73 2 track mono Record/Erase low imp. 75p pair. Erase Heads for '17' and '18' 75p

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(Post, etc. 15p any quantity).

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- AMPLIFIERS (carr. etc. 20p)
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 Stereo Preamp. 11-95
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POWER SUPPLIES FOR EVERY PURPOSE

- (All cases unless stated chassis)
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- P15 26/28 volt 1 amp (chassis) 2-90 post 20p
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- 0-01 Diam. Mono Filament £3-00 per 50 metre reel 0-13 Diam. 64 Fibres Sheathed. £1-00 per metre
- SPRAYS 15mm Diam. (Mares Tail Spray £10-50 7mm. Diam. £5-00)



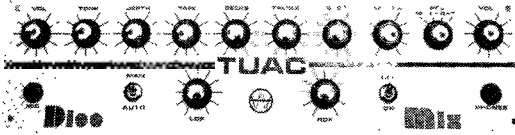
All types offered subject to availability. Prices correct at time of press E & OE. 10% VAT to be added to all orders. UK post etc. 15p per order unless stated.

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£25.50

Controls: Mic Vol, Tone, Over-ride depth, Auto Manual Sw. Tape Vol, L&R Deck Faders. Deck Volume. Treb. & Bass. H. Phon Vol, Selector. Master Vol, on/off sw. Max. output 1V RMS. **PANEL SIZE 18" x 4 1/2" DEPTH 3"**
POWER SUPPLY £3.50p

NEW!
3 CHANNEL LIGHT MODULATOR

- ★ 1,000 watts per channel
- ★ Operates from 1/8th watt to 100 watts
- ★ Full wave control
- ★ Fully fused and suppressed
- ★ 12 easy connections

£17.25

Single channel version **£6.50p**



ALL PRICES INCLUDE V.A.T. AND POSTAGE AND PACKING

ACCESS & BARCLAY CARDS ACCEPTED, JUST SEND US YOUR NUMBER. H.P. ARRANGED THROUGH PAYBONDS

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BARGAIN PARCELS 14lb at £1.60 plus 35p p.p.; 28lb at £3.00 plus 57 1/2p p.p.; 56lb at £4.95 plus £1.37 1/2 p.p. Contain pots, Res. Valves, Diodes Tagboards, Chassis, Valveholders, etc. Good value save ££s. Lucky Dip Service.

FANTASTIC BARGAIN. New 6 inch tubes. E450 4/B/16 4VH, medium Persistence, green. Ideal scope tube.

Also 7BP7. All unused as new. Price £1.55 post paid.

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AERIAL POLES 4ft high 2" in diameter push-in type as new 75p each p. & p. 25p each minimum four.

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ELECTRONIC IGNITION SYSTEM

This Capacitor-Discharge Electronic Ignition System was recently described in Practical Wireless and has proved extremely popular. We are able to offer the kit in two forms; the standard kit containing the electronic components only, enabling the customer to tailor these to his own layout, or the de-luxe version containing a ready-drilled roller-tinned printed-circuit board and fully machined die-cast case with A.M.P Electrical Spade Connector Block. Each kit is supplied with a custom wound transformer, first grade components and full constructional details.

The original circuit employed Germanium Power Transistors for the negative earth version. **WE NOW SUPPLY SILICON P.N.P. POWER DEVICES AT NO EXTRA COST!** All components available separately. Case size 4 1/2" x 3 1/2" x 2". Complete assembly and wiring manual 25p, supplied with de-luxe kit only, refundable on purchase of kit.

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Price: Standard Kit£7.97 U.K. Post Free
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Quantity Discounts:

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PLEASE STATE POS. OR NEG. EARTH WHEN ORDERING.

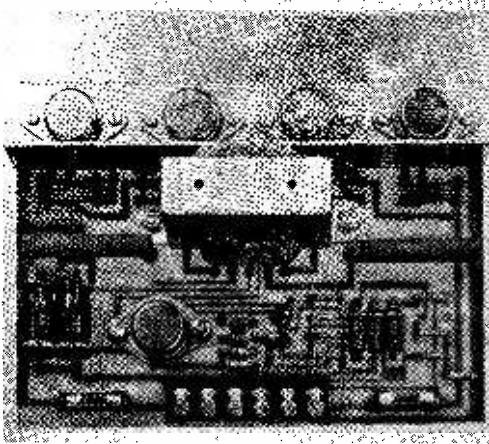
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NEW TUAC POWER MODULES

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| TP125
illustrated
£15-25 | ★ 125 Watts RMS continuous sine wave output
★ 4 RCA 150 Watt 15 Amp output transistors
★ Special layer wound driver transformer
★ Short, open, and thermal overload protection
★ Compact size: 7 x 6½ x 3 in. |
| TL100
£11-50 | ★ 100 Watts RMS sine wave
★ 2 RCA 15 Amp output transistors
★ Rugged transformer driver
★ Full thermal overload protection
★ Compact size: 5 x 5 x 3in. |
| TL60
£9-75 | ★ 60 Watts RMS sine wave
★ RCA 115 Watt output transistors
★ Only six connections to make
★ Same size as TL100 |
| TL30
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★ 2 RCA output transistors
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Power supplies vacuum impregnated Transformers with supply board incorporating stabilised pre-amp supply:
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Specification on all three power modules:
 All output power ratings + 1dB. Output impedance 8-15 Ohms. THD at full power 1% typically 0-5%. Input sensitivity 60mV into 10k. Frequency response 10Hz-25kHz +2dB. Hum and noise better than -75dB.

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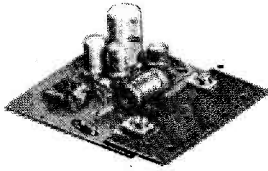
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AL10/AL20/AL30 AUDIO AMPLIFIER MODULES



The AL10, AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.S. The versatility of their design makes them ideal for use in record players, tape recorders, stereo amplifiers and cassette and cartridge tape players in the car and at home.

Parameter	Conditions	Performance
HARMONIC DISTORTION	Po = 3 WATTS f=1KHz	0.25%
LOAD IMPEDANCE	—	8 - 16 Ω
INPUT IMPEDANCE	f=1KHz	100 kΩ
FREQUENCY RESPONSE ±3dB	Po=2 WATTS	50 Hz - 25KHz
SENSITIVITY for RATED O/P	Vs=25V. Rl=8Ω f=1KHz	75mV. RMS
DIMENSIONS	—	3" x 2 1/4" x 1"

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter	AL10	AL20	AL30
Maximum Supply Voltage	25	30	30
Power output for 2% T.H.D. (RL = 8 Ω f = 1 KHz)	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min.

AUDIO AMPLIFIER MODULES

AL 10. 3 watts RMS	£2-19
AL 20. 5 watts RMS	£2-59
AL 30. 10 watts RMS	£3-01

POWER SUPPLIES

PS 12. (Use with AL10 & AL20)	89p
SPM 80. (Use with also AL30 & AL50)	£3-25

FRONT PANELS SP 12 with Knobs	£1-10
-------------------------------	-------

PRE-AMPLIFIERS

PA 12. (Use with AL10 & AL20)	£4-35
PA 100. (Use with AL30 & AL50)	£13-15

TRANSFORMERS

T491 (Use with AL10)	£1-98 P & P 15p
T338 (Use with AL20)	£1-93 P & P 15p
BMT80 (Use with AL30 & AL50)	£2-15 P & P 25p

PA 12. PRE-AMPLIFIER SPECIFICATION

The PA 12 pre-amplifier has been designed to match into most budget stereo systems. It is compatible with the AL 10, AL 20 and AL 30 audio power amplifiers and it can be supplied from their associated power supplies. There are two stereo inputs, one has been designed for use with *Ceramic cartridges while the auxiliary input will suit most †Magnetic cartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/off switch, balance, bass and treble. Size 162mm x 84mm x 35mm.

Frequency response—
20Hz - 20KHz (±3dB)
Bass control—
± 12dB at 60Hz
Treble control—
± 14dB at 14KHz
*Input 1. Impedance
1 Meg. ohm
Sensitivity 300mV
†Input 2. Impedance
30 K ohms
Sensitivity 4mV

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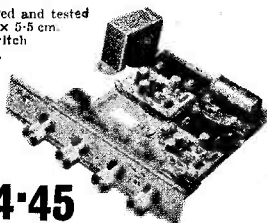
Practical Wireless
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ALL PRICES INCLUDE V.A.T.

The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and tested on a one-piece chassis measuring 20 cm x 14 cm x 5.5 cm. This compact unit comes complete with on/off switch volume control, balance, bass and treble controls.

Transformer, Power supply and Power amps. Attractively printed front panel and matching control knobs. The 'Stereo 20' has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively, into a separate cabinet. Output power 20w peak. Input 1 (Cer.) 300mV into 1M. Freq. res. 25Hz-25KHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Bass control ±12dB at 60Hz typically 0.25% at 1 watt. Treble con. ±14dB at 14KHz.



£14.45

50W pk 25w (RMS)

0.1% DISTORTION!
HI-FI AUDIO AMPLIFIER

THE AL50

★ Frequency Response 15Hz to 100,000—1dB.

★ Load—3, 4, 8 or 16 ohms.

★ Distortion—better than .1% at 1 KHz.

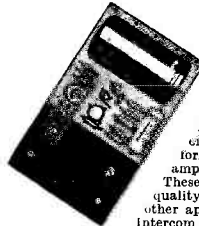
★ Signal to noise ratio 80dB.

ONLY
£3.58 each

★ Supply voltage 10-35 Volts.

★ Overall size 63mm 105mm x 13mm.

Tailor made to the most stringent specifications using top quality component and incorporating the latest solid state circuitry and AL50 was conceived to fill the need for all your A.F. amplification needs.
FULLY BUILT TESTED—GUARANTEED.



STABILISED POWER MODULE SPM80

AP80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 watt (r.m.s.) per channel simultaneously. This module embodies the latest component and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transformer MTS80, the unit will provide outputs of up to 1.5 amps at 35 volts. Size: 63mm x 105mm x 30mm. These units enable you to build Audio Systems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including:—Disco Systems, Public Address Intercom Units, etc. Handbook available 10p **PRICE £3.25**

TRANSFORMER BMT80 £2-15 p. & p. 28p

STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL50 power amplifier system, this quality made unit incorporates less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages. Three switched stereo inputs, and rumble and scratch filters are features of the PA100 which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.



SPECIFICATION

Frequency Response	20Hz - 20KHz ± 1dB
Harmonic Distortion	better than 0.1%
Inputs: 1. Tape Head	1.25 mV into 50K Ω
2. Radio, Tuner	35 mV into 50K Ω
3. Magnetic P.U.	1.5 mV into 50K Ω
All input voltages are for an output of 250mV. Tape and P.U. input—equalised to RIA A curve within ± 1dB, from 20Hz to 20KHz.	
Bass Control	± 15dB at 20Hz
Treble Control	± 15dB at 20 KHz
Filters: Rumble (High Pass)	100Hz
Scratch (Low Pass)	8KHz
Signal/Noise Ratio	better than -65dB
Input overload	+ 26dB
Supply	+ 35 volts at 20mA
Dimensions	292mm x 82mm x 35mm

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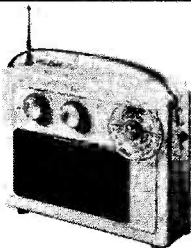
- ★ 4 Transistor Earpiece Radio.
- ★ 5 Transistor Push Pull Amplifier.
- ★ Batteryless Crystal Radio.
- ★ Signal Tracer.
- ★ 7 Transistor Loudspeaker Radio MW/LW
- ★ One Transistor Radio.
- ★ Signal Injector.
- ★ 5 Transistor Short Wave Radio.
- ★ 2 Transistor Regenerative Radio.
- ★ Transistor Tester NPN-PNP.
- ★ Electronic Metronome.
- ★ 3 Transistor Regenerative Radio.
- ★ 4 Transistor Push Pull Amplifier.
- ★ Electronic Noise Generator
- ★ Audible Continuity Tester.
- ★ Sensitive Pre-Amplifier.

Total Building Costs
£7-23 P P & Ins. 44p
(Overseas P & P £1-85)
(+ 10% VAT 72p)

Components include: 24 Resistors • 21 Capacitors • 10 Transistors • 3 1/4" Loudspeaker • Earpiece • Mica Baseboard • 3 12-way connectors • 2 Volume controls • 2 Slider Switches • 1 Tuning Condenser • 3 Knobs • Ready Wound MW/LW/SW Coils • Ferrite Rod • 6 1/2 yards of wire • 1 Yard of sleeving etc. • Parts Price List and Plans 50p. (Free with parts).

NEW ROAMER NINE

WITH V.H.F. INCLUDING AIRCRAFT

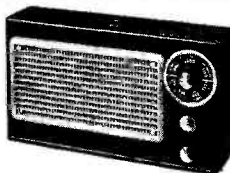


Nine Transistors, 9 Tuneable wavebands as Roamer Ten Built in ferrite rod aerial for MW/LW. Retractable chrome-plated telescopic aerial for VHF and SW. Push Pull output using 600 mW transistors. 9 Transistors and 3 diodes, tuning condenser with V.H.F. section, separate coil for aircraft, moving coil loudspeaker, volume ON/OFF and wavechange controls. Attractive all white case with red grille and carrying strap. Size 9 1/2" x 7" x 2 1/2" approx. Parts Price List and Plans 30p (Free with parts).

Total Building Costs
£6-95 P P & Ins. 44p
(Overseas P & P £1-85)
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NEW Everyday Series

Build this exciting New series of designs



E.V.5. 5 Transistors and 2 diodes. MW/LW. Powered by 4 1/2 volt Battery. Ferrite rod aerial, tuning condenser, volume control, and loudspeaker. Attractive case with red speaker grille. Size 9" x 6 1/2" x 2 1/2" approx. Parts Price List and Plans 15p. Free with parts.

Total Building Costs
£2-73 P P & Ins. 30p
(+ 10% VAT 27p)
(Overseas P & P £1-25)

E.V.6. Case and looks as above. 6 Transistors and 3 diodes. Powered by 9 volt battery. Ferrite rod aerial, 3" loudspeaker, etc., MW/LW coverage. Push Pull output. Parts Price List and Plans 15p. Free with parts.

Total Building Costs
£3-60 P P & Ins. 30p
(+ 10% VAT 36p)
(Overseas P & P £1-25)

E.V.7. Case and looks as above. 7 Transistors and 3 diodes. Six wavebands. MW/LW, Trawler Band, SW1, SW2, SW3, powered by 9 volt battery. Push Pull output. Telescopic aerial for short waves. 3" Loudspeaker. Parts Price List and Easy Build Plans 20p. Free with parts. Overseas P & P £1-05.

Total Building Costs
£4-08 P P & Ins. 31p
(Overseas P & P £1-85)
(+ 10% VAT 40p)

ROAMER EIGHT Mk I

NOW WITH VARIABLE TONE CONTROL

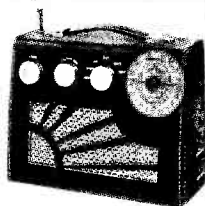


7 Tuneable Wavebands: MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Built in Ferrite Rod Aerial for MW and LW. Retractable chrome plated Telescopic aerial for Short Waves. Push pull output using 600mW transistors. Car aerial and Tape record sockets. Selectivity switch. 8 transistors plus 3 diodes. Latest 4" 2 watt ferrite magnet loudspeaker. Air spaced ganged tuning condenser. Volume/on/off, tuning, wave change and tone controls. Attractive case in rich chestnut shade with gold blocking. Size 9 x 7 x 4 1/2 in. approx. Easy to follow instructions and diagrams. Parts price list and plans 25p (FREE with parts).

Total building costs
£6-98 P P & Ins. 47p
(Overseas P & P £1-85) (+ 10% VAT 69p)

ROAMER TEN

WITH VHF INCLUDING AIRCRAFT



10 Transistors. Latest 4" 2 watt Ferrite Magnet Loudspeakers. 9 Tuneable Wavebands. MW1, MW2, LW, SW1, SW2, SW3, Trawler Band, VHF and Local Stations also Aircraft Band.

Built in Ferrite Rod Aerial for MW/LW. Retractable, chrome plated 7 section Telescopic Aerial, can be angled and rotated for peak short wave and VHF listening. Push Pull output using 600mW Transistors. Car Aerial and Tape Record Sockets. 10 Transistors plus 3 Diodes. Ganged Tuning Condenser with VHF section. Separate coil for Aircraft Band. Volume on/off. Wave Change and tone Controls. Attractive Case in black with silver blocking. Size 9" x 7" x 4". Easy to follow instructions and diagrams. Parts price list and plans 30p (FREE with parts).

Total building costs
£8-50 P P & Ins. 52p
(+ 10% VAT 85p)

POCKET FIVE

3 Tuneable wavebands. M.W. L.W. and Trawler Band, 7 stages, 5 transistors and 2 diodes, supersensitive ferrite rod aerial, moving coil loudspeaker, attractive black and gold case. Size 6 1/2" x 1 1/2" x 3 1/2" approx. Plans and Parts Price List 15p (Free with parts).



Total Building Costs
£2-28 P P & Ins. 26p
(+10% VAT 22p)
(Overseas P & P £1-25)

TRANSONA FIVE

Wavebands, transistors and speaker as Pocket Five. Larger Case with Red Speaker Grille and Tuning Dial. Plans and Parts Price List 15p (Free with parts).

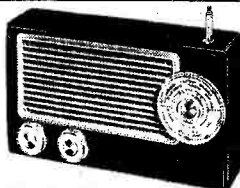


Total Building Costs
£2-50 P P & Ins. 26p
(+10% VAT 25p)
(Overseas P & P £1-25)

TRANS EIGHT 8 TRANSISTORS and 3 DIODES

6 Tuneable Wavebands: MW, LW, SW1, SW2, SW3 and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves. 3in. Speaker. 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with polished metal inserts. Size 9 x 5 1/2 x 2 1/2 in. approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and plans 25p (FREE with parts).

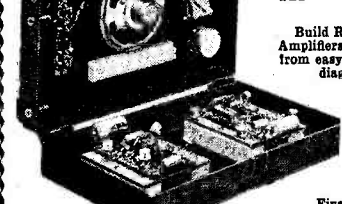
Total building costs
£4-48 P P & Ins. 33p
(+ 10% VAT 44p)
(Overseas P & P £1-25)



ROAMER SIX CASE AND LOOKS AS TRANS-EIGHT

6 Tuneable Wavebands: MW, LW, SW1, SW2, Trawler band plus an extra Medium waveband for easier tuning of Luxembourg, etc.. Sensitive ferrite rod aerial and telescopic aerial for Short Waves. 3in. Speaker. 8 stages—6 transistors and 2 diodes. Attractive black case with red grille, dial and black knobs with polished metal inserts. Total building costs **£3-98** P P & Ins. 31p (Overseas P & P £1-85) (+ 10% VAT 39p)

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10 1/2 x 6 1/2 in. with a massive Ceramic
Magnet, 44oz. Gauss 13,000 lines.
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Useful Response 25 to 18,000 cps
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8in. or 10in. ELAC HI-FI SPEAKER



Dual cone plasticised roll sur-
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50-16,000 cps. Bass resonance
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8in. 10 watts

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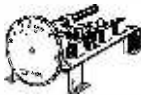


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WADDING 18in. wide. 15p ft.

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Medium Wave.
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Ferrite aerial. 9 volt.
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TRANSISTOR MONO
MIXER. Add musical
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Calibrated slide dial tuning.
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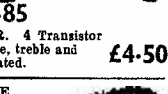


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As above less cabinet.

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Push-Pull Ready built with volume, treble and bass
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Post Free
30-14,500 c/s. 12in. double
cone, woofer and tweeter cone
together with a BAKER
ceramic magnet assembly
having a flux density of
14,000 gauss and a total flux
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resonance 40 c/s Rated 20
watts. NOTE: 3 or 8 or
15 ohms must be stated.

Module kit, 30-17,000 c/s
with tweeter, crossover, baffle
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Please state 3 or 8 or 15 ohms. Post Free

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VERSION
50 watt 8 or 15 ohms



MAJOR 100 WATT ALL PURPOSE TRANSISTOR AMPLIFIER

All purpose transistorised.
Ideal for Groups, Disco and P.A
4 inputs speech and music. 4 way
mixing. Output 8/15 ohm. a.c. Mains.
Separate treble and bass controls.
Guaranteed. Details SAE. £49
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7 valve version. 4 input 10 wide range controls. For mikes,
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A die, punch and Allen Screw

Size	Price
3/8"	74p
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7/8"	92p
1"	99p
1 1/8"	99p
1 1/4"	100p
1 3/8"	115p
1 1/2"	120p
1 3/4"	135p
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2 1/2 in diam. Ceramic Former. Screw Terminals 1 in. diam.
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3 inch Panel Meter 50 Microamp, unusual scale require
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1,400 r.p.m. Reversible 48 Watt. £1.95
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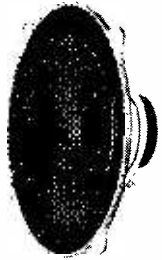
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An inexpensive unit for the
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Bass Resonance 45cps
Flux Density 12,000gauss
Useful response 45-13,000cps
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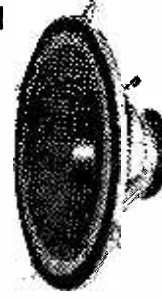
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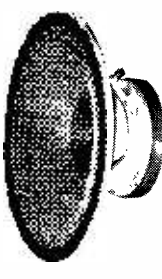
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Truly pocket-sized

With all its calculating capability, the Cambridge still measures just $4\frac{1}{2}'' \times 2'' \times \frac{11}{16}''$. That means you can carry the Cambridge wherever you go without inconvenience - it fits in your pocket with barely a bulge. It runs on ordinary U16-type batteries which give weeks of life before replacement.

Easy to assemble

All parts are supplied - all you need provide is a soldering iron and a pair of cutters. Complete step-by-step instructions are provided, and our service department will back you throughout if you've any queries or problems.

Total cost? Just £27.45!

The Sinclair Cambridge kit is supplied to you direct from the manufacturer. Ready assembled, it costs £32.95 - so you're saving £5.50! Of course we'll be happy to supply you with one ready-assembled if you prefer - it's still far and away the best calculator value on the market.



Features of the Sinclair Cambridge

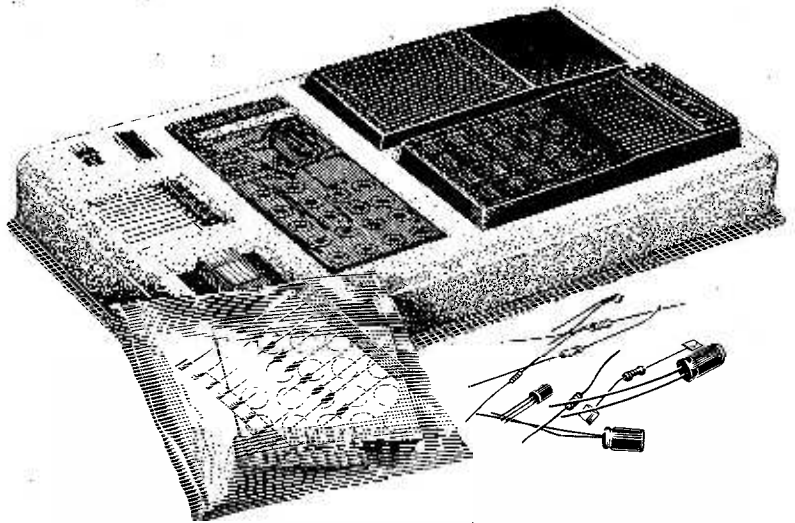
- * Uniquely handy package. $4\frac{1}{2}'' \times 2'' \times \frac{11}{16}''$, weight $3\frac{1}{2}$ oz.
- * Standard keyboard. All you need for complex calculations.
- * Clear-last-entry feature.
- * Fully-floating decimal point.
- * Algebraic logic.
- * Four operators (+, -, x, ÷), with constant on all four.
- * Constant acts as last entry in a calculation.
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- * Calculates to 8 significant digits, with exponent range from 10^{-20} to 10^{79} .
- * Clear, bright 8-digit display.
- * Operates for weeks on four U16-type batteries. (MN 2400 recommended.)

A complete kit!

The kit comes to you packaged in a heavy-duty polystyrene container. It contains all you need to assemble your Sinclair Cambridge. Assembly time is about 3 hours.

Contents:

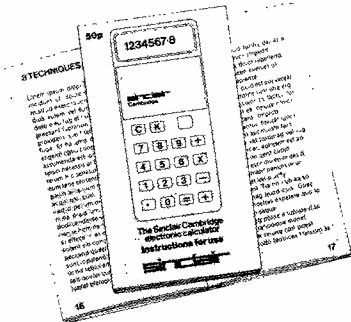
1. Coil,
2. Large-scale integrated circuit.
3. Interface chip.
4. Thick-film resistor pack.
5. Case mouldings, with buttons, window and light-up display in position.
6. Printed circuit board.
7. Keyboard panel.
8. Electronic components pack (diodes, resistors, capacitors, transistor).
9. Battery clips and on/off switch.
10. Soft wallet.



This valuable book – free!

If you just use your Sinclair Cambridge for routine arithmetic – for shopping, conversions, percentages, accounting, tallying, and so on – then you'll get more than your money's worth.

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How? It's all explained in this unique booklet, written by a leading calculator design consultant. In its fact-packed 32 pages it explains, step by step, how you can use the Sinclair Cambridge to carry out complex calculations.

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It seemed only logical to combine the knowledge of do-it-yourself kits with the knowledge of small calculator technology. And *you* benefit!

Take advantage of this money-back, no-risks offer today

The Sinclair Cambridge is fully guaranteed. Return your kit within 10 days, and we'll refund your money without question. All parts are tested and checked before despatch – and we guarantee a correctly-assembled calculator for one year.

Simply fill in the preferential order form below and slip it in the post today.

Price in kit form: £24.95 + £2.50 VAT. (Total: £27.45)

Price fully built: £29.95 + £3.00 VAT. (Total: £32.95)

PW 4/74	
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Please send me	Name _____
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<input type="checkbox"/> a Sinclair Cambridge calculator ready built at £29.95 + £3.00 VAT (Total: £32.95)	Address _____
*I enclose cheque for £ _____, made out to Sinclair Radionics Ltd, and crossed.	_____
*Please debit my *Barclaycard/Access account. Account number _____	_____
*Delete as required.	
PLEASE PRINT	

TO encourage safety in the mere presence of electrical, electronic, radio or television apparatus, let alone during their operation, is not only laudable but vital. Hence the British Electrotechnical Approvals Board for Household Equipment (now affectionately BEAB) is extending the BEAB Approval Scheme to include audio and radio products including record players, radios, radiograms, mains/battery portable receivers with (curiously) "continuously rated audio outputs up to 6 + 6 watts stereo or 10 watts mono". Manufactured equipment that is licensed to bear the BEAB approval marking has to be first subjected to some detailed and stringent tests at the BSI laboratory.

The specification for the tests, detailed in BS 415: 1972 (with amendments), highlights for the more casual of the manufacturers, and probably some of the amateur constructor fraternity, areas of potential risk in mains driven equipment that all too often are taken for granted. There are, of course, extreme cases like the ladies' dangling necklace test and the test which inserts artificial fingers into apertures almost in determination to find live contact.

Generally the scheme is an excellent one. In most British equipment, that is designed and manufactured by responsible people, it is unlikely that no thought will be given to hazards such as shock, fire risk, ionised radiation, implosion and the like.

What has been needed is some form of yardstick by which a known hazard can be measured. Let us not be carried away by any thought that this standard is for manufacturers only. There are frequent cases where more strict attention to detail is needed by everyone who has mains driven appliances or electronic equipment.

We have only one serious complaint: that is the use of graphical symbols to indicate the nature of the supply (a.c. or d.c.) and to indicate live terminals. To the uninitiated layman, technical symbols mean nothing and he will not be inclined to buy BS3939 to find out before operating his new purchase.

Elsewhere in this issue we have highlighted only a few of the points in BS415 that we feel the general public need to know about. It is stressed that the detailed specification is designed to cover most contingencies of normal operation; we recommend manufacturers, suppliers and users to refer to this for more information.

M. A. COLWELL—*Editor*.

The May issue of Practical Wireless will include a special pull-out feature to make a handy booklet "Guide to Long Distance Reception of Radio and TV", (useful for locals, too!). Also appearing will be constructional projects: the medium wave "Mini-Pop" (goes in a jacket pocket); an audio booster and power supply to enable you to hear cassette recordings in the car; a trace doubler to enable you to convert a single-beam oscilloscope for four displays. We shall also be giving first details of a super new project that we know will appeal to sports fans all over the world. Don't miss out—order your copy regularly NOW.

(All advanced details are subject to the current national industrial situation).

Further details on page 1167

Export sales of British made Dolby

IN a recent statement Phoenix Videosonic Ltd., of Braintree, Essex, Europe's only manufacturer of Dolby Noise Reduction Units announced significant export sales to Europe, North America and Japan.

A Videosonic spokesman stated: "Videosonic leads the world in the technical specification of its equipment: in the PD4 we have introduced a new high level Dolby 'B' circuit providing a unique range of over 95dB between noise and 0.1% distortion. At this time the PD4 represents the ultimate way to take the PSSST! out of tape.

To further extend our lead in the World Hi-Fi market, the PD2b has been introduced as the world's first battery operated Dolby Unit, allowing 'field' use in the most rigorous conditions. The integral microphone pre-amplifier makes this an ideal unit for reporter or similar usage.

World recognition of Videosonic technical manufacturing competence has been most encouraging, and we can only take pride in our immediate penetration of the Japanese market in the face of very strong local competition. We are advised that our range of Dolby products will be displayed and demonstrated in the top 850 Hi-Fi Retail Shops in Japan, and that local response to date has been very positive. Our first shipment to Japan leaves this week.

Portable Fluorescent Lamp (March P.W.)

WILL readers please note, that the transformer specified is now no longer available. An improved transformer is available from Messrs G. F. Milward at 77p plus 20p p & p. This includes full modification details and uses fewer components. A 21 in. 13W tube is available at 50p + 20p p & p, and it is claimed that this tube gives a greater light output than the 15W tube. S.A.E. to G. F. Milward for further details.

Bargains galore

IF you are in the "Ally Pally" area on March 24th, pay a visit to the Collector's Bazaar which is being held in the Palm Court.

This is a five-bazaar event which includes militaria, vintage post cards, vintage toys, transport relics and, of most interest to our readers, vintage records, horn gramophones, phonographs and probably some items of vintage radio equipment.

Practical Wireless visited one of these bazaars held at St. Johns Wood a few months ago, and it was there that Colin Riches purchased an Edison "Gem" phonograph to be featured in a future "Going Back."

If any readers want to find out the details of hiring a stall at the bazaar (£3.50 for the day) contact the organiser John Carter, Smewins, Shottesbrooke, nr. Maidenhead, Berks, SL6 3SR (Tel. Shurlock Row 539).

Otherwise, put on your cycle clips and pedal along to Alexandra Palace, Wood Green, London N.22, on March 24th. They'll let you in at 1 p.m. but be sure to have your entrance fee of 30p at the ready.

Hi-Fidelity 74

HI-FIDELITY 74 is a rival exhibition to the Sonex show. It will be run at the same time and held at the Heathrow Hotel, Bath Road. It's the idea of Malcolm Blockley who is the Hi-Fi Division Sales Manager of Pysers-Britex Ltd.—the sole UK distributor of Marantz, Teledyne and Kenosonic equipment.

The organiser states that this show has been arranged because many manufacturers are fed-up with trying to demonstrate their products in small, cramped hotel bedrooms.

Hi-Fidelity 74 will run from March 27th to 31st inclusive but the first two days will be for the trade and press only.

Blast them out!

IN order to reduce the effects of interference from an East German station at night, the BBC has increased the transmitting power of the Radio 4 Moor-side Edge transmitter to 300kW.

R and TV Components Ltd.

IN their March advertisement, the price of postage and packing for the "Stereo 21" should have read £1.60. Apologies to R and TV Ltd.

Public Address Exhibition

Readers who have an interest in outdoor activities, such as rallies, will be planning events for the coming season. To get up to date on public address installations, it would be worthwhile to visit Sound '74, the international exhibition of the Association of Public Address Engineers. A lecture programme will be held concurrently on p.a. design, building acoustics, microphones, and the financial side of public address work from the practical point of view.

The A.P.A.E. has received more stand space bookings than previously, but there are still a few left for those who wish to come in at a late stage, including suppliers of disco equipment.

Admission is free to all in-

terested persons: tradesmen, manufacturers, buyers, and users of public address and allied equipment in the entertainments business. Tickets can be obtained from exhibitors or from the A.P.A.E. Secretariat, 6 Conduit Street, London W1R 9TG.

The scope of activities covered is extended to include audio-visual effects.

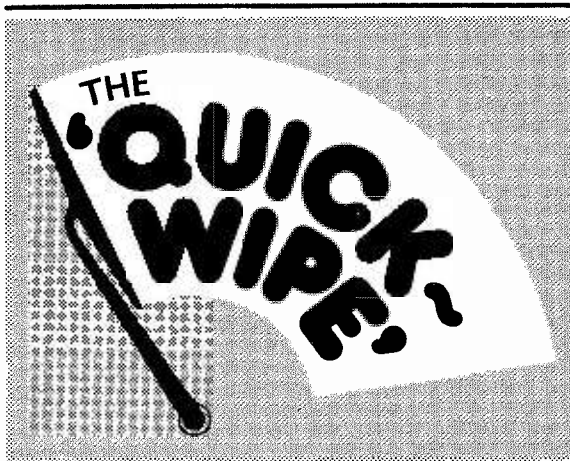
Overseas readers will be interested to learn that the A.P.A.E. are exhibiting in Hall 9A at the Hanover Fair from 25th April to 3rd May 1974 and at the I.C.E.T.I.A. exhibition at Melbourne, Australia from 7th to 11th October.

Practical Wireless will be on show at the Hanover Fair.

UK wavebands and frequencies

THE BBC Engineering Department have issued a useful data sheet which shows the frequencies and wavebands allocated to broadcasting in the United Kingdom. Below we give the details from that sheet:

Band	Frequencies	Service
Low frequency (l.f.) (long waves)	160-255kHz (1875-1176m)	} a.m. radio
Medium frequency (m.f.) (medium waves)	525-1605kHz (571-187m)	
High frequency (h.f.) (short waves)	3950-4000kHz (75-m band)	
	5950-6200kHz (49-m band)	
	7100-7300kHz (41-m band)	
	9500-9775kHz (31-m band)	
	11700-11975kHz (25-m band)	
	15100-15450kHz (19-m band)	
	17700-17900kHz (16-m band)	
	21450-21750kHz (13-m band)	
	25600-26100kHz (11-m band)	
Band I	(v.h.f.) 41-68MHz (channels 1 to 5)	405-line television
Band II	(v.h.f.) 88-97.6MHz	f.m. radio
Band III	(v.h.f.) 174-216MHz (channels 6 to 13)	405-line television
Band IV	(u.h.f.) 470-582MHz (channels 21 to 34)	625-line television
Band V	(u.h.f.) 614-854MHz (channels 39 to 68)	625-line television
Band VI	(s.h.f.) 11700-12500MHz (11.7-12.5GHz)	Not yet in use for broadcasting

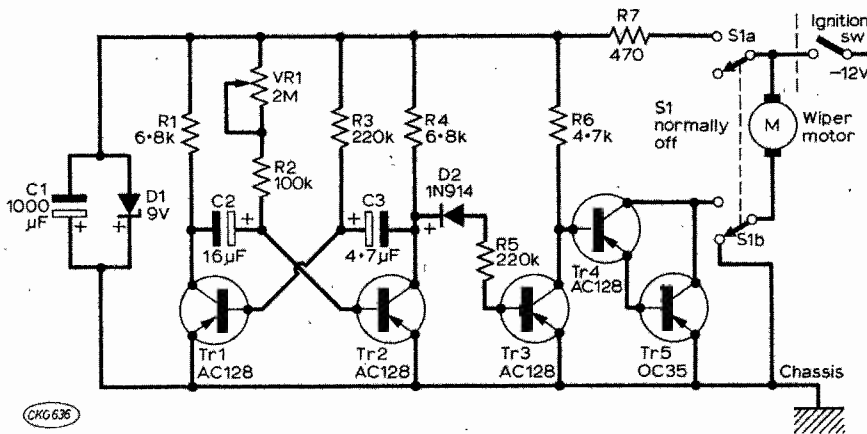
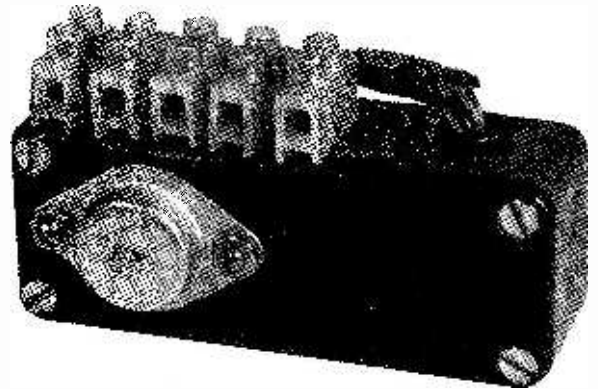


A VARIABLE TIME SWEEP WINDSCREEN WIPER

P. S. COLLINS

IMAGINE the situation: you are driving your car in drizzly rain, you put on the windscreen wiper. One sweep is sufficient, so you switch it off. Five, ten or fifteen seconds later the windscreen needs another wipe, so you switch on the wiper again for another single stroke. This could go on for some time and tends to be wearisome.

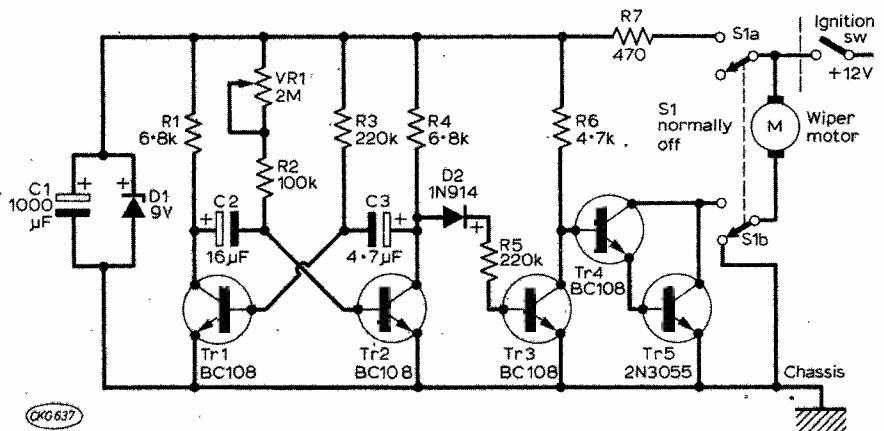
The circuit here described saves this tiresome routine and allows you to relax in the automation of a variable time-sweep wiper. Although the circuit is designed for wiper motors with automatic parking facility, there is some information at the end of the article which will be helpful to those who have wiper motors without this facility.



CKG 636

Fig. 1. Circuit of the Quickwipe for a vehicle with a **POSITIVE** earth system. It is essential to be quite sure which side of the battery is connected to chassis.

Fig. 2. In this circuit for a **NEGATIVE** earth system, different transistors are used and capacitors and diodes are reversed compared to those in Fig. 1.



CKG 637

Figures 1 and 2 are the circuits for positive and negative earthed vehicles; the difference lies only with the active components and reverse connection of the polarised ones. The circuit action remains the same. Tr1 and Tr2 form a multivibrator generating a pulse of fixed length with a variable repetition rate. VR1 allows this rate to be varied between approximately 3 and 30 seconds. Tr3, 4 and 5 form a pulse amplifier to drive the wiper motor.

The fixed pulse length is $\frac{3}{4}$ second which is sufficient time to drive the motor long enough for its internal switches to take over the drive and thus return it to the park position. Switch S1 is centre off. One switch, S1b, switches for continuous operation, earth being directly applied to the motor.

In the other position, S1a, applies 12 volts to the circuit and S1b connects the motor as the load for the pulse amplifier. The vehicle wiper switch may now be regarded as redundant, or left in the circuit, as desired.

CONSTRUCTION

The whole unit can be comfortably housed in a die-cast box measuring $3\frac{1}{2} \times 1\frac{3}{8} \times 1\frac{1}{8}$ in. Figure 3

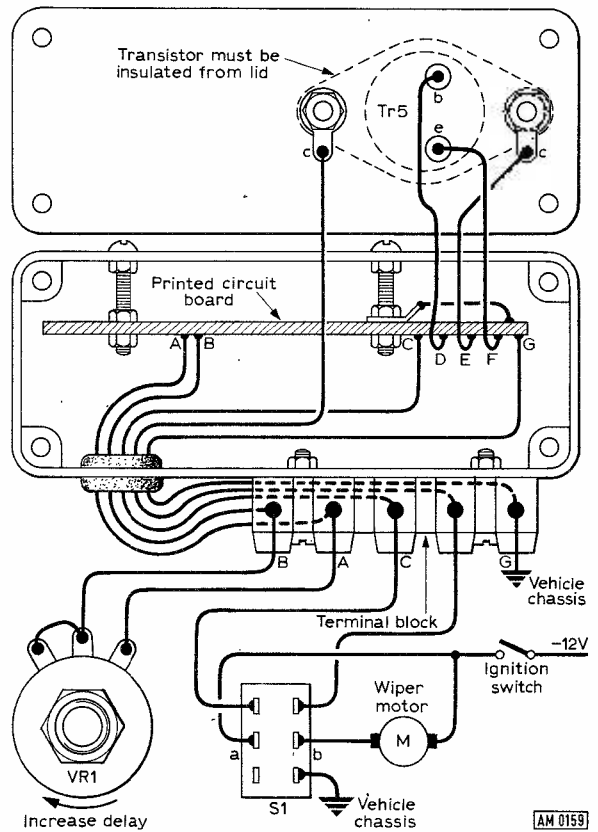
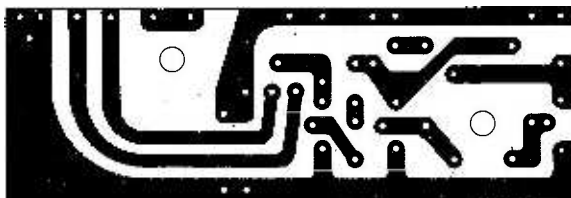
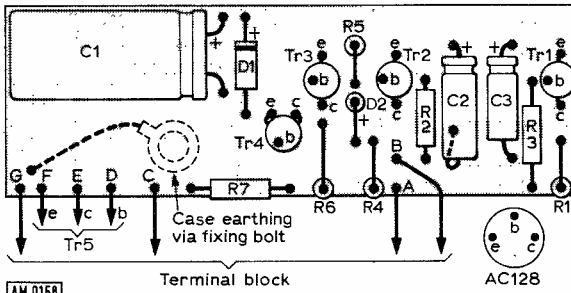
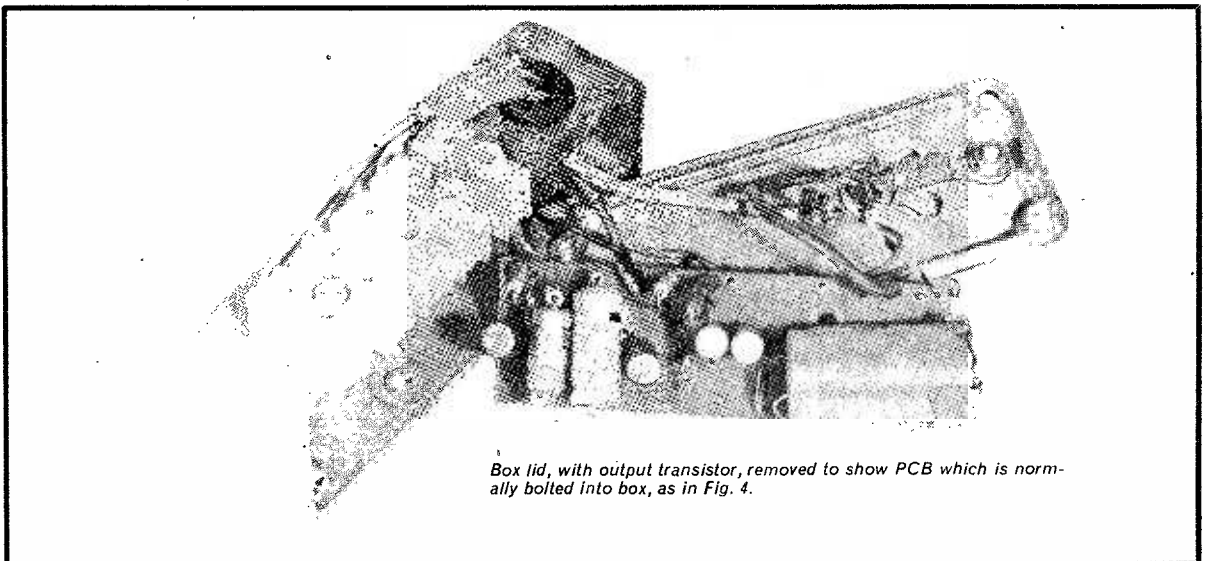


Fig. 3, left, shows PCB actual size and component layout for POSITIVE earth unit. Fig. 4, above, illustrates external wiring of Quickwipe.

shows the printed circuit board. Tr5 is mounted on the lid with insulating washer and bushes. All leads from the circuit board and Tr5 are connected to a five-way terminal strip fixed to the side of the box. This enables easy connection to the vehicle's wiring, as shown in Fig. 4.

Confirm the chassis polarity of the vehicle before constructing the unit, then use Fig. 1 OR Fig. 2 as appropriate.



Box lid, with output transistor, removed to show PCB which is normally bolted into box, as in Fig. 4.

★ components list

Resistors

R1 6.8kΩ R5 220kΩ
 R2 100kΩ R6 4.7kΩ
 R3 220kΩ R7 470Ω
 R4 6.8kΩ VR1 2MΩ linear
 Resistors 10% 1/4W except R7 1/2W

Capacitors

C1 1000μF 25V C2 16μF 16V C3 4.7μF 16V

Semiconductors

D1 9V zener 400mW D2 1N914

Positive Earth Tr1—4 AC128 Tr5 OC35

Negative Earth Tr1—4 BC108 Tr5 2N3055

Miscellaneous

S1, Double pole—double throw switch, centre off.
 Diecast box (RS Comps.—"Box 992"). Printed circuit board. Insulation kit for Tr5. Five way terminal block.

NOTE: It may be possible to arrange the fixed pulse length to correspond with the time taken for the wipers to travel one complete sweep, in the case of wipers without the self-park facility. This could be achieved by altering the values of R3 and C3.

These points are offered only as helpful guides. The author has conducted no tests in this regard and cannot therefore give any facts regarding accuracy or success. ■

PW TECHNICAL CROSSWORD PUZZLE No. 3 Solution

1	U	2	S	3	E	4	V	5	I	6	B	7	R	8	A	9	T	10	O	R
	E		I		M		E		U		E									
9	C	10	R	11	A	12	G		13	S	14	P	15	E	16	C	17	I	18	F
	V		N		I		P		O		T		I							
12	R	13	I	14	T	15	A		16	A	17	18	19	20	21	22	23	24	25	26
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15	B	16	E	17	S	18	S		19	E	20	M	21	T	22	O	23	L	24	L
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25	F	26	I	27	L	28	A	29	M	30	E	31	N	32	T	33	I	34	C	35
	E		I		I		I		D		S									
28	R	29	O	30	C	31	H	32	E	33	L	34	L	35	E	36	S	37	E	38

TELEVISION

IN THE APRIL ISSUE

CLOSED-CIRCUIT TV

Next month we start a new series aimed at giving an essentially practical account of closed-circuit TV equipment, its use and the servicing techniques required. To start with, the basic element in CCTV work, the vidicon camera tube, is explained along with its basic circuitry.

TRANSISTOR FIELD TIMEBASES

Fully transistorised field timebases have been around for some time now, particularly in colour receivers, and have proved to be generally very reliable. Nevertheless it is time we took a look at common faults and their causes, also at the operation of the class A output stage generally used.

THE DIODE DROPPER

The use of a diode dropper in the heater circuit reduces heat dissipation and is also cheaper than using a completely resistive dropper. The action of the diode dropper circuit is often misunderstood however, which can lead to the use of an incorrect accompanying resistor value and damage to the valves in the chain. The circuit action will be explained and the procedure for determining the value of the accompanying resistor given, either for designing a new circuit or for working out a diode dropper substitution for an existing set.

SERVICING TELEVISION RECEIVERS

The next chassis to be dealt with by Les Lawry-John is the Pye 149 single-standard monochrome chassis and its derivatives, the 569, 769 and 173.

PLUS ALL THE REGULAR FEATURES

Details of the April issue are subject to the current national situation at the time of going to press.

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GUIDE TO multi-range test meters

H. LEEMING G3LLL

IT does not seem many years since test meters were so expensive that, in the radio and TV trade, at least, one was shared between several engineers, the losers having to make do with wet fingers and neon screwdrivers! Test meters are now relatively cheap so that no enthusiast or handyman can really afford to be without one; whether it be for attending to the Hi-Fi system, fixing the car, or even sorting out a fault on the front door bell. Despite their simplicity in operation these meters can deceive the unwary and so it is hoped that a little basic theory will be of practical assistance.

The multi-range test meter commonly contains ranges such as AC and DC voltage, DC current and at least one resistance range. Other functions may be included on the more elaborate instruments but all use the basic meter movement plus the switching of various internal components in or out of circuit.

The DC Voltmeter

The meter movement fitted to most modern test instruments needs a current of something in the range of 1 to 1/100 of a milliamp to move a pointer across the full extent of the scale. The theoretical circuit of the basic meter movement is shown in Fig. 1. The "internal resistance" is not an actual resistor, but is the resistance of the coil of wire in the meter movement. From Ohm's Law, (voltage = current × resistance) this 1mA meter movement shown will require a voltage of 0.1 volt for full scale deflection, ($1/1,000 \times 100/1 = 0.1$ volt). This basic meter could therefore be used to measure voltages of up to 0.1 volt or currents of up to 1 milliamp—not very useful!

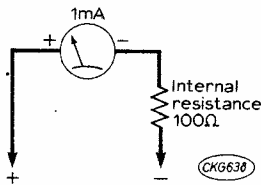


Fig. 1: Representation of meter movement must include resistance of moving coil.

The meter movement is basically a current operated device, but it can be made to read various quantities. A little thought will show that a 1mA meter movement will read full scale if 1 volt is

applied to it through a series resistance which, including internal resistance, totals 1,000 ohms. From Ohm's Law, 1 volt across 1,000 ohms causes a current of 1mA to pass. A voltmeter using a 1mA meter movement is said to have a sensitivity of 1000 ohms per volt.

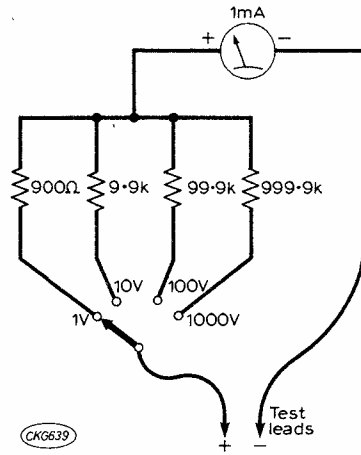


Fig. 2: Series resistors for voltmeter allow for coil resistance. Only of importance on lower ranges.

Fig. 2 shows the meter wired to read four ranges of voltage and it will be seen that the total resistance of the meter is 1,000 ohms for every volt of the range in question. For this reason it is referred to as 1,000 OPV and this would usually be marked on the meter scale.

Such a meter does have its disadvantages and its relatively low resistance can greatly affect circuit voltages as will be shown. In Fig. 3a two 1 ohm resistors are connected across the supply and the voltage between X and Y is measured. If the meter is switched to the 1 volt range it has a total resistance of 1,000 ohms (remember 1,000 OPV) this resistance being shunted across R2. As the meter resistance is very high, compared to R1 and R2, its effect is negligible and the reading is given accurately as 0.5 volts. If, however, the meter is transferred to the circuit in Fig. 3b and another reading is taken the resulting accuracy is quite different. Once again, the reading should be 0.5 volts, but note what happens when the meter is

connected across R2. R2 is shunted by the meter's resistance of 1,000 ohms and the resistance of the bottom half of the circuit drops to around 900 ohms. The voltage divides itself according to the ratio of the resistors and the meter reads just below 0.1 volts.

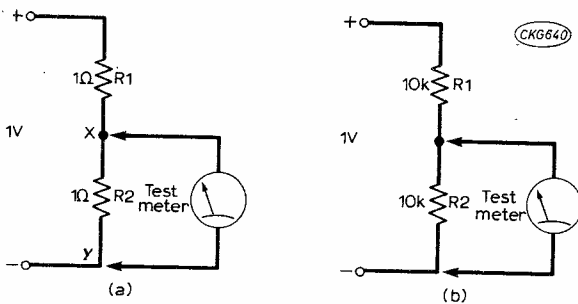


Fig. 3 (a) and (b) : to demonstrate effect of meter resistance on high and low resistance circuits.

The meter is not really wrong, it simply reads the voltage that is present when it is connected. Using the same meter a more accurate reading could be taken by switching to the 10 volt range when the test meter's resistance would rise to 10,000 ohms; the meter's resistance in parallel with R2 would then total 5,000 ohms and whilst the voltage reading would still be low at 0.33 instead of 0.5, it would be a little more realistic. Could we take the same argument further and switch to the 100 volt range with a meter resistance totalling 100,000 ohms, and obtain an accurate result? Unfortunately, no, since when the meter was switched to this range the pointer would move so little that we would not be able to take an accurate reading from it.

If we want a more accurate reading in a high resistance circuit the answer is a more sensitive meter movement that will allow us to insert larger values of voltage multiplier resistors. If for instance, we substitute a meter with a 50 micro-amp movement, (0.05mA), we will obtain a sensitivity of 20,000 OPV. Using circuit Fig. 3b we would then obtain, on the 1 volt range, a reading that was almost correct, (20,000 ohms being shunted across R2), or by switching to the 10 volt range using this higher sensitivity meter we would obtain a reading that was accurate to within all normal requirements.

As has been illustrated, the DC voltmeter can only read the voltage which is present when it is connected. It cannot guess at the voltage which appears when it is disconnected. When using a voltmeter one should get into the habit of comparing the resistance of the range being used with the resistance of the circuit being measured.

In many cases when operating in a high resistance circuit a more accurate reading will be obtained if a higher voltage range is used. If in doubt a reading should be taken on two adjacent ranges of the test meter. With any good quality instrument these readings should be about the same, but if they are not it implies that the meter is loading the circuit on the lower voltage range.

Valved or Transistorised Voltmeters

To obtain higher sensitivities using normal techniques requires very expensive and delicate meter movements. It is not common practice, therefore, to make multi-range test meters with a sensitivity

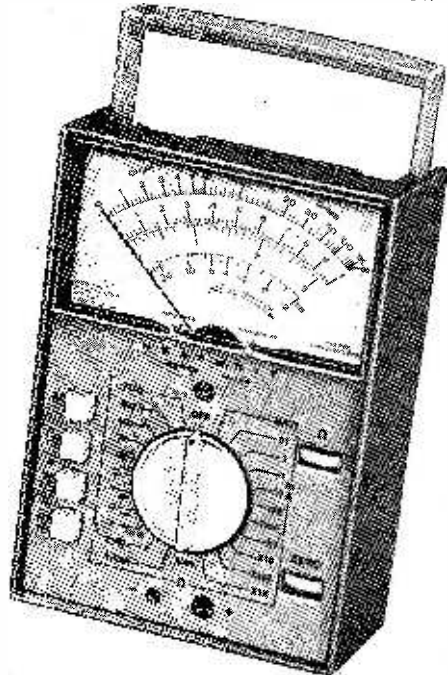
of much over 50,000 OPV. In some circumstances an even higher sensitivity is required, so that test meters of as high a sensitivity as this would be of little use at measuring, say, 0.1 volts in a circuit with resistance of several megohms. To enable higher sensitivities to be obtained, the valve and then the transistorised voltmeter were introduced. In these devices amplification is used so that an input resistance of 10 megohms or more is presented, even on the lowest voltage ranges. Such instruments are essential if tests are to be made in some high impedance transistorised circuits where very small voltages are present.

Frequency Response

Most test meters are basically intended for making tests at the mains frequency and their accuracy often falls off at frequencies in the audio range. One should check the frequency response of a test meter before relying upon it to check audio or bias frequency voltages. In the latter case it should be remembered that high frequency bias voltages can damage the rectifier in some test meters, and also that even if the meter's frequency response is adequate that its loading (possibly only a few hundred OPV) can, in many circuits, much reduce any voltage present. If it is desired to accurately measure voltages at high audio or radio frequencies the valve or transistorised voltmeter is again essential.

The AC Voltmeter

The AC ranges of multi-range test meter function in very much the same way as the DC ranges except that a rectifier is incorporated to enable the basic DC meter movement to function, see Fig. 4. As with the DC voltage section of the meter, the amount of loading on the circuit being tested is indicated by the sensitivity in ohms-per-volt. Rectifiers have a tendency to be non-linear at low current



The Heathkit IM-104 multimeter, a modern design providing 53 ranges on four scales. Frequency response up to 50kHz on AC voltage ranges. Input resistance of 10 MΩ on DC voltage ranges.

(Courtesy Heath (Glos.) Ltd.)

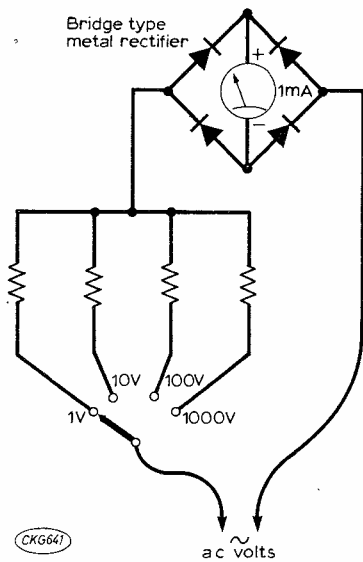


Fig. 4: Incorporation of meter bridge rectifier on AC voltage ranges.

levels and so, in the interest of accuracy, it is common to reduce the sensitivity of the test meter when switched to the AC ranges. The popular Avo Model 8, for instance, has a sensitivity of 20,000 OPV on the DC ranges but only 1,000 OPV on the AC ranges.

The Direct Current Ranges

The basic DC meter movement, as we have seen, will reach full scale when a small current is passed through it. The example shown in Fig. 1 needed 1mA for full scale deflection. If it is desired to measure a larger current, some of the current must be by-passed. The circuit with various resistors which are known as "shunts" is shown in Fig. 5. The value of shunt resistor R3, for instance, is calculated so that when the test meter is measuring 1A, 999 milliamps go via R3 and 1mA passes through the meter.

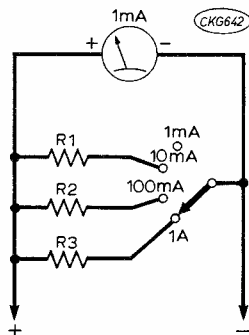


Fig. 5: Switchable shunts to increase current range of basic meter.

It is important to note that when measuring current, some voltage is required to operate the meter, as was shown earlier, when dealing with the DC voltmeter. In this case 0.1 volts will be dropped across the meter terminals. In most cases when making measurements, as in Fig. 6a, this small voltage drop will make negligible difference, being small in relation to the voltages in the circuit. If we try to make a test as shown in Fig. 6b however,

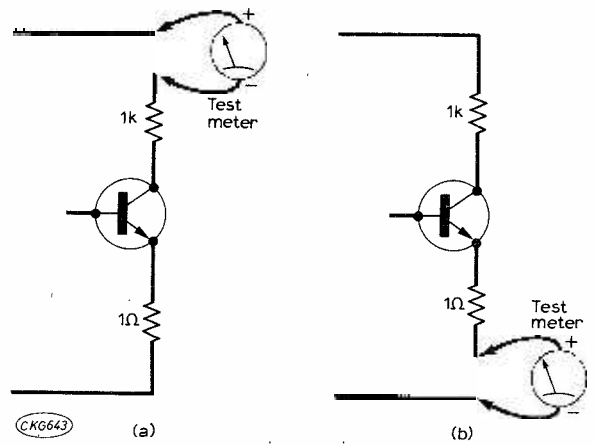


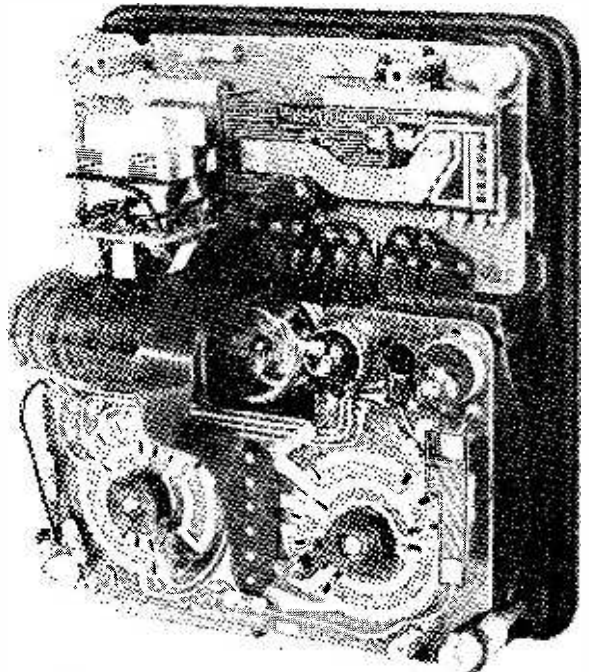
Fig. 6 (a) Correct and (b) Incorrect method of inserting meter in transistor circuit.

this is not the case. Here the effect of adding the meter in series with the circuit is to considerably increase the value of the emitter resistor. Increasing this effective value would mean that the current which flowed with the test meter connected would be much less than the current which normally flowed in the circuit.

When checking current flow in low impedance circuits, it is better to measure the voltage across a known resistor and then to calculate the current.

The Resistance Ranges

Figure 7 shows a basic method of resistance measurement. If the test prods are touched together R2 can be adjusted until the meter reads full scale, the current being provided by the battery. As we have seen a 1mA meter when used as a voltmeter



An excellent view of the latest AVO Model 8. It uses printed circuit techniques for shunts and switchboards. (Courtesy AVO Ltd, Dover)

has a sensitivity of 1,000 OPV and here, if the battery is exactly 1.5V, R1 plus R2, plus internal resistance must equal 1,500 ohms, when R2 is set to provide full scale deflection with the test prods touching. If now, instead of touching the test prods together, we connect them to a resistor being tested, of 1,500 ohms, the meter will then read half-scale as an external resistor of the same value as the built-in resistance has been added to the circuit. The centre of the scale would be marked 1,500 ohms and with suitable calibration resistors of between, say, 50 and 50,000 ohms, resistors could be checked using this set-up, with reasonable accuracy.

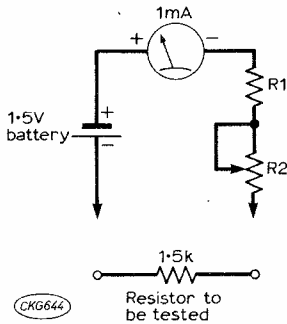


Fig. 7: Basic circuit for measuring resistance.

To divide the range by 10 we can shunt the meter as was done on the current ranges so that the sensitivity of the circuit becomes 100 OPV, enabling R1 and R2 to be reduced to 1/10 of their previous value. Alternatively, we can multiply the range by 10 by fitting a 15V battery and increasing R1 and R2 tenfold. In this way we obtain a meter with a centre scale range of 150, 1,500 and 15,000 ohms on three ranges enabling resistors from below 10 to above 500,000 ohms to be checked with good accuracy.



A large, clear scale with an anti-parallax mirror is the highlight of the latest AVO.

Use of Ohms Range

From the above discussion it will be seen that a current is passed through the component to be tested and that a voltage is also applied across it. In most cases this will do no harm, but it is wise to be aware that voltages of up to 25 or so are possible on the high resistance ranges and that currents in the order of 100mA or more may be found on the low ohms ranges of some test meters. When checking circuits where there is the slightest risk of damage being caused, it is wise to avoid using the highest or lowest ohms range on the test meter and to concentrate tests on the range which applies low voltage and low current. If magnetic devices, such as tape heads, are tested, note that they will be magnetised by the meter current. These tests should not be made, therefore, unless a de-fluxer is available to remove the residual magnetism. It should be noted that no checks of resistance can be made unless the circuit which is being tested,

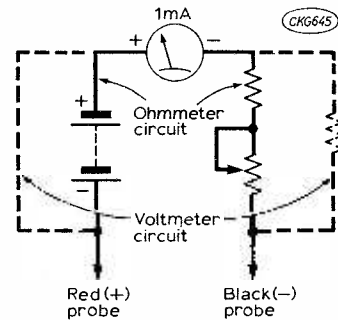


Fig. 8: Illustration of reverse polarity of probes in an ohmmeter circuit.

is completely dead. All voltage sources should therefore be disconnected before tests take place, as, quite apart from giving the wrong results, severe damage can be caused to the test meter and equipment if resistance tests are attempted on live circuits. Devices such as transistors, diodes and electrolytic capacitors are inherently polarity sensitive so the polarity of the voltage output of the test meter should be noted whilst making tests on these devices. As will be seen from Fig. 8 using normal circuit arrangements the polarity of the test prods is normally **opposite** on the ohms range to that marked on the meter for the voltage and current ranges.

Decibels

Many test meters have a scale marked in decibels marked in + and - values over a total of 15dB's or so. It must be clearly understood that the decibel is **not** an absolute value, such as the ohm or volt, but, as will be seen from the shape of the dB scale, is a logarithmically based system of comparison. Whilst many test meters are calibrated so that 0dB=0.775V this is just an arbitrary figure. In practical use, such as measuring the frequency response of an amplifier, the signal level is adjusted so that the output when measured with the test meter set to a suitable range, reads 0dB. If the input frequency is then varied the output variation, and hence the frequency response of the equipment being tested, can be read off directly in decibels.



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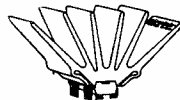
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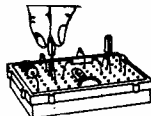
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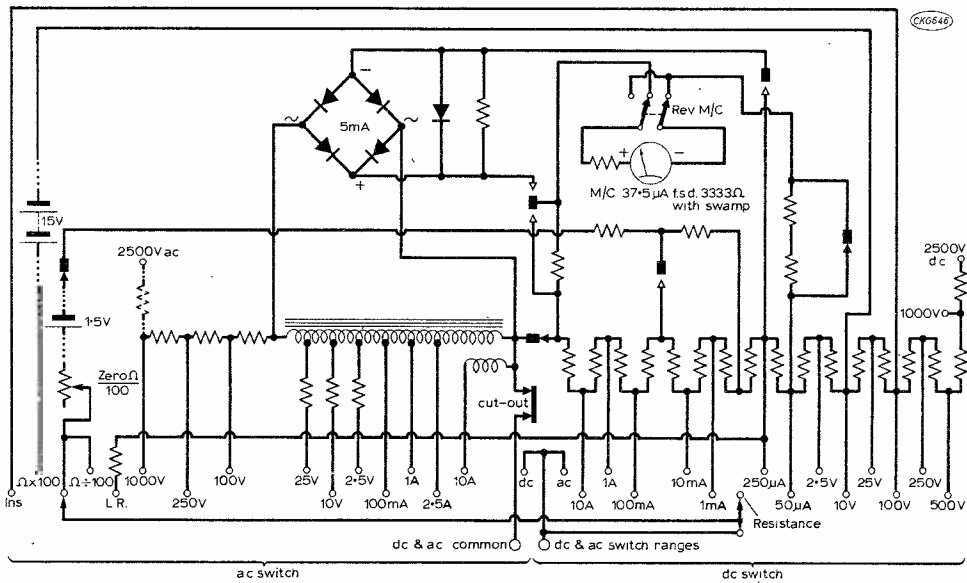


Fig. 9: Basic circuit of the Model 8 Avometer Mk II to show the complexity of a modern multi-meter. (Courtesy AVO Ltd Dover)

To be really useful in making this kind of test the response of the test meter and the output of the audio generator must be flat with frequency, otherwise one is liable to end up in the position of the wheel-tapper who condemned 100 wheels only to find he had a cracked hammer! Remember, it costs next to nothing to print a decibel scale on a meter but it costs pounds to incorporate the response and accuracy needed to make it really meaningful for even simple audio frequency response measurements.

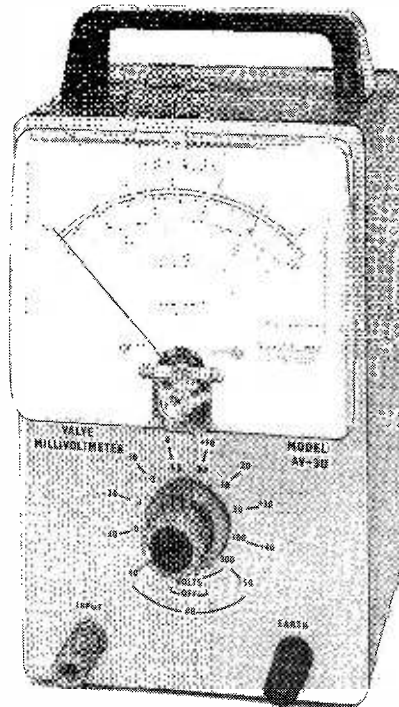
Precautions in use

Multirange test meters are precision instruments which can easily be damaged by over-loading. Whilst many meters have built-in automatic protection, these circuits only give a **limited** protection; they do not cater for gross overloads. A moment's carelessness can leave an instrument which is beyond economical repair. To avoid disasters follow the makers' instructions, together with the following suggestions:—

1. Always leave the instrument switched to a high voltage range when not in use. **Never** on a current or ohms range.
2. Never connect meter to any live circuit when switched to ohms.
3. Be extra careful to avoid short circuits when using the current ranges.
4. When measuring unknown voltages or currents switch to the highest range **first**, and only change over to a lower range if less than, say, one third of full scale deflection is registered.

Buying a meter

There is a host of small test meters available, many of which should be more than adequate for the average hobbyist. Aim to get a meter which has a sensitivity of 10,000 OPV or more on the DC ranges and which has a scale which is clear to read. A resistance range coverage of from, say, 1 ohm to 2 megohms, will fill most needs. AC current ranges are not really of any great importance, as



This valve millivoltmeter, type AV-3U, is mains operated and has a sensitivity of 10mV f.s.d. on the lowest range and 300V RMS on top range. (Courtesy Heath (Glos.) Ltd.)

current can always be calculated from resistance and voltage measurements, but a few DC current ranges will be found useful.

When comparing meters it can be advantageous to take along a battery and a few known values of resistors. There is nothing like a practical test to prove whether readings are plain and straightforward or confused and ambiguous. The cost?—£15 will buy a meter which is likely to be more than good enough but look around and testers costing well under £10, which are by no means cheap and nasty, can be found. ■

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PART 6—GROUNDED EMITTER AMPLIFIERS

LAST month's emitter followers were all types of current amplifiers. In every case the output voltage was the same, or slightly less than the input voltage. Many applications require voltage amplification—e.g. raising the output level of a microphone to an extent that when current amplification is applied the resultant signal could drive a loudspeaker. The grounded emitter amplifier will provide a reasonable degree of voltage and current amplification and is, perhaps, the most used type of amplifier stage in the whole of electronics. Because both voltage and current is amplified we call the grounded emitter stage a *power amplifier* but not necessarily in the sense that you can expect several watts of useful output; specialised power stages are better equipped for the latter purpose and these will be covered later in the series.

mid-way between the two supply rails. At the same time we could connect a source of voltage through a capacitor to the base of the same transistor and (assuming the source voltage was zero at the time) this would not affect our *bias* condition. However, as soon as we begin to generate a voltage from the source this would cause current to be added or subtracted from the bias current (depending on the polarity of the a.c. signal) and would cause the voltage at A to rise and fall in exact relation—except for the 180° change of phase. Having point A biased “mid rail” allows maximum peak swings of voltage without the transistor clipping (going totally out of conduction) or bottoming (going into saturated conduction) unsymmetrically. In the ideal amplifier the voltage seen at A should faithfully represent that from the source.

In practice the method of obtaining this mid-rail bias shown in Fig. 42 is not very satisfactory because the h_{FE} for the transistor must be accurately known and this can vary widely from one device to another (even though they may be of the same type number).

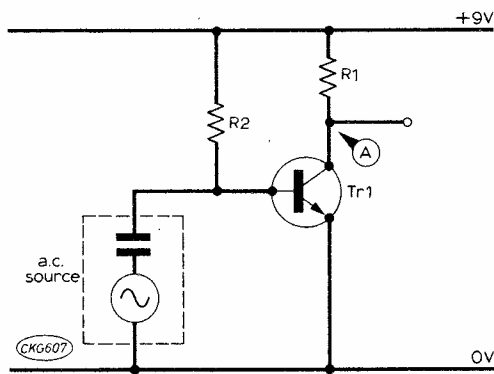


Fig. 42: It is difficult to predict a value for R2 to set the potential at A to mid-rail unless the h_{FE} for Tr1 is accurately known.

Base current

A simple way of compensating for this device variation is to use the potential at A as the voltage source for providing the base current—shown in Fig. 43. If the potential at A is too high the base current will be increased, hence the collector potential falls; conversely if A tends to be too low the base current decreases and the potential at A is forced to rise. By careful selection of component values this feedback bias circuit caters well for quite wide variations in the gains of transistors. It is not perfect by any means but is an improved way of getting a mid rail voltage reliably. You can make up the circuit of Fig. 43 on T Dec and try different BC108 devices. The voltage you measure should not fall outside the range of +3.5 to +5.5V. For those interested it is quite easy to arrive at the component values. First of all assume that the collector load is to be 1k Ω . For the potential at A to be +4.5V (assuming a 9V supply) the drop of 4.5V across R1 will be caused by a collector current of

Referring to Fig. 42, we know that we can make the voltage at point A go to +9V by ensuring that the transistor is cut off (i.e. by passing zero base current) and conversely we can make it fall to zero volts by passing a certain amount of base current through R2. By knowing an accurate value of h_{FE} for the transistor we could calculate a value for R2 that will cause just sufficient collector current to flow that the voltage drop across R1 will be 4.5V. Theoretically we could hold the voltage at A exactly

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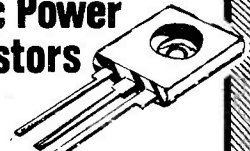
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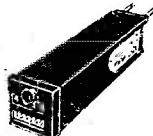
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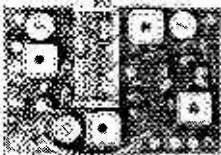
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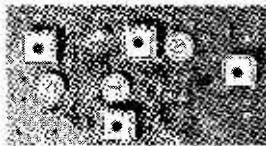
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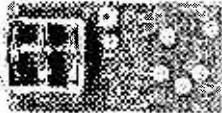
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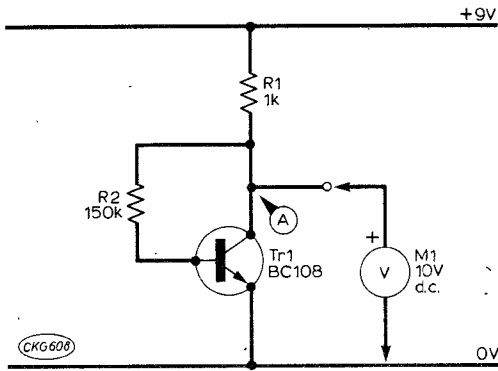


Fig. 43: Using the potential at A as the driving source for base current helps compensate for variations in h_{FE} .

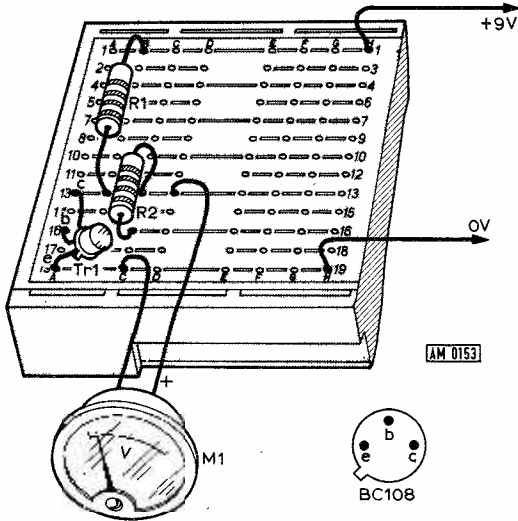


Fig. 44: Component layout for Fig. 43.

4.5mA. If we expect an h_{FE} of around 200 for the BC108 this means that the base current needed to cause 4.5mA collector current is $4.5/200 = 0.0225\text{mA}$. The value of R2, to give this current is calculated from the potential difference across it (potential at A minus the 0.6V base emitter drop) divided by the base current $3.9/0.0225\text{k}\Omega = 170\text{k}\Omega$. The small base current drawn will theoretically modify our original assumption of the potential at A but is so small that it can be ignored. Strictly speaking we should have shown R2 as having a value of 170k Ω but because of other experiments to follow we have made it 150k Ω . The effect of this is to cause the quiescent voltage to be slightly less than mid-rail—but near enough for the experiment.

A crystal microphone is a very easily obtainable source of a.c. voltage that is of a capacitive nature and this can be connected straight across the base of Tr1 and ground of our circuit without affecting the bias conditions (see Fig. 45). Note that we have split the value of our original R2 between two resistors (R2 and R3) in series. Initially leave out the capacitor C1 and connect a meter set to a low a.c. range through a capacitor to point A. Most modern

test meters have this capacitor built into them if you use the input socket marked "Output". The capacitor is there so that the meter only responds to a.c. components on top of the d.c. quiescent voltage at A. Whistle loudly into the microphone and you should see a slight movement of the meter (probably 1V maximum).

Remember, though, that the output from the microphone is unlikely to be greater than a few tens of millivolts. Clearly there is some form of voltage amplification. If you think about it, though, the a.c. fluctuations at A are being fed back, out of phase, to the base through resistors R2 and R3. This will negate the input signal and the overall gain of the amplifier is going to be considerably impaired. We can, however prevent the a.c. component of the feedback signal reaching the base by connecting a capacitor from the junction of R2 and R3 to ground. Do this while whistling into the microphone and you should see at least a two to one improvement in amplification. We call C1 a decoupling capacitor and it should be of a high enough capacitance to shunt even the lowest frequencies to ground.

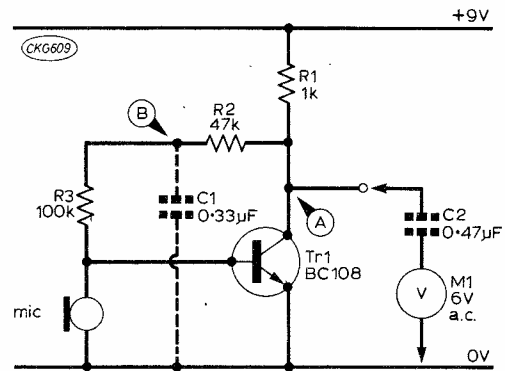


Fig. 45: A signal from a crystal microphone can be superimposed on the bias current but the components have to be slightly modified. Use a meter with an "Output" connection switched to a.c. or alternatively insert C2 when using an a.c. voltmeter.

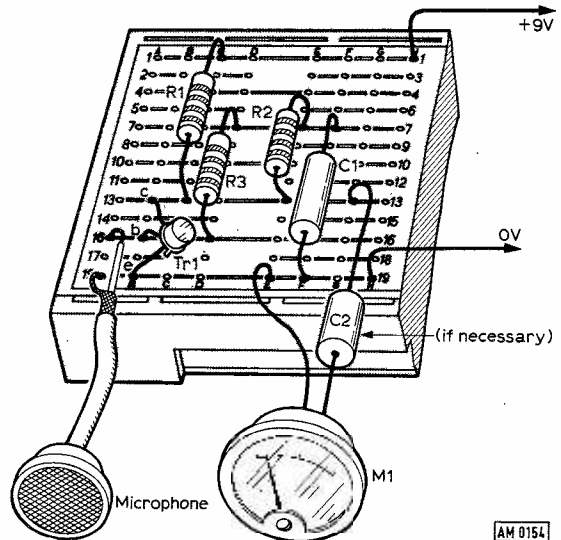
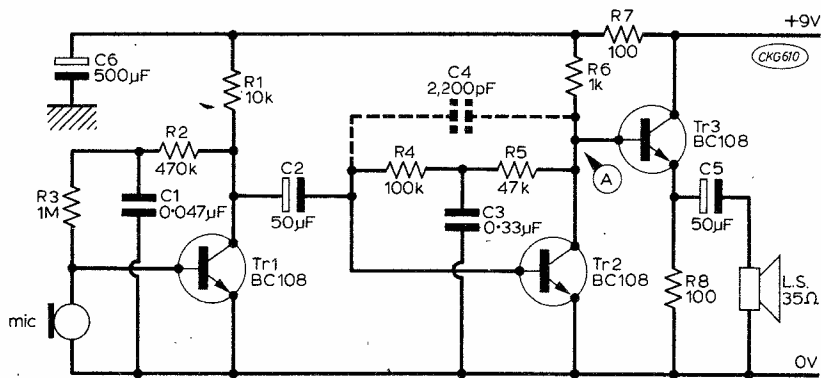
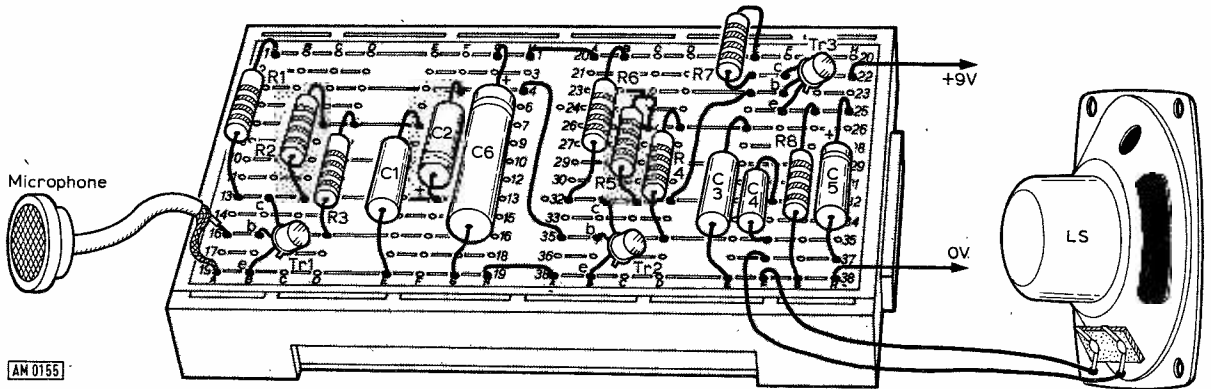


Fig. 46: Component layout for Fig. 45.



◀ Fig. 47: A basic amplifier capable of driving a small loudspeaker from a crystal microphone and suitable for an intercom or baby alarm.



▼ Fig. 48: Component layout for Fig. 47.

The output current from a crystal microphone is very small—because of its high impedance—particularly at low frequencies but there must be quite a reasonable current generated between collector and emitter of the transistor to give rise to the voltage swings we can see at point A. Thus the transistor can be seen to give both current and voltage amplification. The component values in Fig. 45 are not really ideal for coupling from a crystal microphone because we require a fair amount of a.c. base current from the source, and as mentioned earlier, there is not much of this available at low frequencies. The low frequency response of this amplifier would therefore be pretty poor. We can, however, use exactly the same approach to make a stage that needs only one tenth of the input current by increasing all our resistance values by factors of ten (the first stage of Fig. 47). The output from the collector of Tr1 is now coupled as an a.c. signal source to the base of Tr2 which, excluding C4, is identical to the stage we have just described. Before connecting C4 or Tr3 measure the a.c. signal at point A exactly as before; you should see a really high voltage swing (getting on for three or four volts) and more than that, you can get a useful reading for ordinary speech a few inches away from the microphone.

The circuit is clearly providing more voltage gain and has a more useful response at the lower frequency of the human voice. Obviously by increasing the gain at low frequencies we must be overdoing it at high frequencies therefore we insert capacitor C4 which is used, deliberately, to feedback signal from the collector of Tr2 to its base. Because it has a low value it will provide more negative feedback

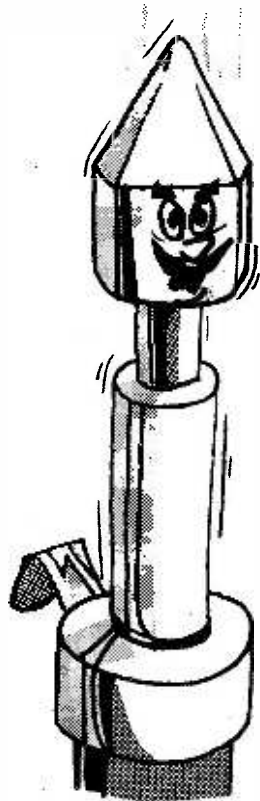
at high frequencies than at low frequencies and hence helps to linearise the frequency response of the two stage amplifier. Use the “whistle and speech” test to see that the amplitude for the whistle is reduced but the level for normal speech has not been appreciably affected. Because we now have a useful voltage swing at A for speech we can use a current amplifier (an emitter follower) to give sufficient current at that voltage to drive a loudspeaker. This is provided by Tr3.

Note that it is necessary to decouple the power rail between the output stage and the amplifiers by means of R7 and C6. Without these components the current drawn by the output transistor could cause voltage variations on the line which are then seen as a form of signal by the preceding stages and amplified. This leads to instability and the whole circuit would oscillate wildly.

The amplifier of Fig. 47 does not have a particularly good frequency response but is quite adequate for intercom or baby alarm applications. No volume control is provided and in some circumstances you might encounter acoustic feedback (howl-round). This can be prevented by keeping the microphone and the loudspeaker well apart.

A problem with the circuits we have covered, so far, is that the voltage gain is very much dependent on the h_{FE} of the transistor in question. There are other circuits which—at the expense of a little gain—enable us to get what there is under reasonably accurate control.

To be continued



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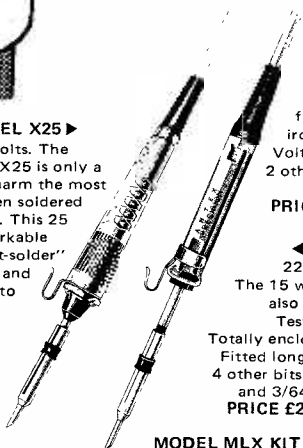
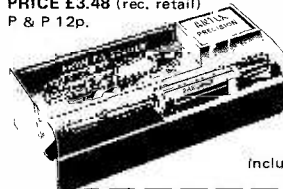
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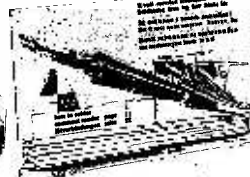
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IMPEDANCE MATCHING



THE WHYS AND WHEREFORES

C. BUDD

THE concepts of input impedance and output impedance are not really difficult to understand although there is no single rule to cover every situation. What is correct practice depends almost entirely on the individual design requirements.

The most important rule of impedance matching is derived from the maximum power transfer theorem.

The maximum power transfer theorem

If a signal source with a purely resistive output source is required to drive a purely resistive load, maximum power will be transferred from source to load when the load resistance is equal to the output impedance of the source. It should be noted that the theorem assumes that the input and output impedances to be purely resistive, which will rarely be the case in practice, and that to deliver maximum power to the load is the sole requirement.

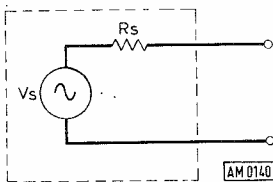


Fig. 1: Equivalent circuit of signal source with resistive output impedance.

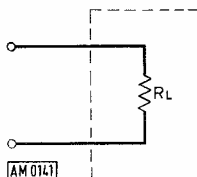


Fig. 2: Equivalent circuit of resistive load.

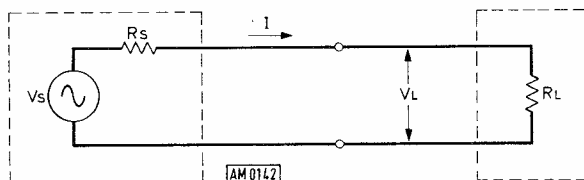


Fig. 3: Equivalent circuit of the source of Fig. 1 driving the load of Fig. 2.

Assuming that our signal source may be represented by an a.c. voltage source in series with a resistance (Fig. 1) and that our load may be represented by a pure resistance (Fig. 2), we can combine the two (Fig. 3) and write some pertinent equations as follows.

Calling the power delivered to the load P

$$V_L = \frac{V_S R_L}{R_L + R_S} \text{ by potential divider action}$$

and $I = \frac{V_S}{R_L + R_S}$ where I is the a.c. current flowing

$$P = IV_L$$

$$\therefore P = \frac{V_S^2 R_L}{(R_L + R_S)^2}$$

where V_L = load voltage, V_S = source voltage, R_L = load resistance, and R_S = source resistance.

Given the source voltage and the source and load resistances we can, with this formula, calculate the power delivered to the load. But we can do more than that. If we assume arbitrary values for V_S and R_S we can plot a graph of R_L against P. The curve obtained will be similar to that in Fig. 4. From the graph it may be seen that the power transferred is at maximum at approximately the point where R_L equals R_S . It may be shown that P reaches a maximum when R_L is exactly equal to R_S .

Maximum power transfer between source and load occurs when the source resistance is equal to the load resistance.

Other considerations

In practice, however, it is not as straightforward as this because maximum power transfer may not be our only concern. Consider the simple audio output stage shown in Fig. 5. The purpose is to match the speaker impedance to the output impedance presented by the transistor.

From the maximum power transfer theorem, one could reasonably assume the the "correct" load resistance would be the output resistance of the transistor, but this is not so. In this case maximum

efficiency (i.e. power transfer from amplifier to load) is not our main concern.

Of greater importance is the maximum power that the stage will deliver without distortion due to bottoming (the transistor being turned off by the input signal) or saturation. In fact the load resistance into which the stage will deliver the maximum power without distortion, known as the optimum load, is equal to the supply voltage divided by the quiescent collector current and has nothing to do with the actual output resistance of the stage.

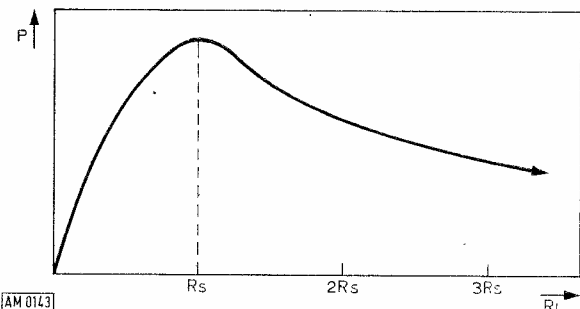


Fig. 4: Sketch graph showing that the power delivered to the load is at a maximum when $R_L = R_s$.

In a practical case the optimum load will generally be higher than the output resistance for an audio power amplifier, and this is the reason that commercial audio power amplifiers, intended to drive load impedances of 3, 8 or 16 ohms, often have output impedances of a fraction of an ohm.

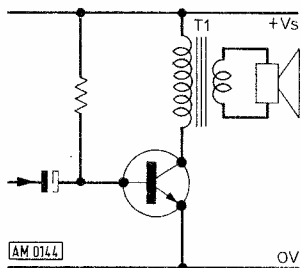


Fig. 5: Simple audio output stage.

Reactive components

An input or output impedance will have reactive components as well as a resistive one. If possible, the reactive element of the source impedance should be cancelled by those of the load impedance. In other words, a source with an equivalent series capacitance should "see" a load with an equivalent series inductance, the reactance being equal, but opposite, to that of the source capacitance.

In this way, the source capacitance and the load inductance form a series-tuned circuit which, ideally, has zero dynamic impedance (zero resistance). Any net reactance in the source-load circuit is undesirable since it reduces the maximum power that can be delivered to the load by the source. Such "reactance balancing" is only possible at a single frequency and in a system of large relative bandwidth (e.g. an audio preamplifier) it is of no use.

At r.f. however, the relative bandwidth will generally be much less and it is usually easy to make the reactive elements of source and load cancel out in the frequency band in use. As an example, one of the functions of the aerial tuning unit in a transmitting system is to cancel out the reactive elements of the aerial impedance.

Equal load and source resistance

Now let us consider another situation in which it would be better to deviate from the rule of making the load resistance equal to the source resistance because maximum power transfer is not our only concern. Fig. 6 shows the equivalent circuit diagram of a typical crystal microphone or ceramic pick-up. The output impedance of such a device consists of a fairly large resistance (typically a few megohms) in series with a small capacitance of perhaps two or three hundred picofarads. If the capacitive element was absent, the transducer drives a pre-amp with an input resistance equal to R_s and all would be well.

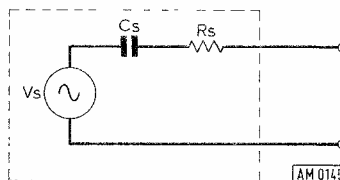


Fig. 6: Equivalent circuit of typical crystal microphone or ceramic pick-up.

However, at the lower audio frequencies, the reactance of C_s in a practical transducer becomes large enough to be significant in comparison to R_s and attenuation of the bass frequencies would result if the input impedance of the pre-amp were equal to R_s .

Since an inductance in series with the transducer would only cancel the capacitance at a single frequency and would, in any case be ridiculously large, the simplest solution to the problem is to make the input impedance of the pre-amp very large compared to R_s . The reactance of C_s at bass frequencies would then be insignificant compared to the total resistance in circuit and no significant attenuation of the bass frequencies would occur.

High impedance input

The circuit diagram of a crystal microphone driving a pre-amp with an ample input resistance of $10M\Omega$ is shown in Fig. 7. One could reasonably think, from the maximum power transfer theorem, that the large ratio between the resistive component of the source impedance and the load resistance would result in a large loss of available power.

This is the case, but it may be shown that the power gain of a common source f.c.t. stage (and that of a common cathode valve stage) is proportional to the value of the resistor (R_1 in Fig. 7) shunting the input, which is roughly equal to the

—continued on page 1166

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AUTOMATIC 12V CAR BATTERY CHARGER

Richard Collin

THIS simple automatic battery charger was originally designed for use with the very popular battery operated fluorescent lamp described in the December issue of *Practical Wireless*. Its purpose was to keep the battery in a fully charged state, restoring energy used when mains power is available.

The circuit is of course suitable for charging any 12 volt car battery at a maximum rate of 2.25A. When the battery reaches full charge (13.5 volts) a "crowbar" circuit operates and shuts off the charge current. Interruption of the mains supply restores the crowbar to its off state.

Circuit description

The circuit diagram is shown in Fig. 1. A mains isolation transformer with a 30V centre-tapped secondary winding feeds a full-wave thyristor circuit to provide the charging current. The thyristors are triggered by the d.c. potential applied to the gate electrodes via diodes D1 and D2 and the associated smoothing capacitor C1.

Resistors R1, R2 and R3 limit the gate current together with the indicator lamp LP2. Resistor R1 and lamp LP2 also limit the current through the crowbar thyristor CSR3 when it is 'on'. Resistors

R4 and R5 are connected in parallel. They limit the charge current to 2.25A to protect the transformer, CSR1 and CSR2. Diode D3 is included to stop current flowing back from the fully charged battery into the crowbar circuit once it has triggered.

The crowbar trigger potential is set by the 6.8V zener diode D4 in the gate circuit of CSR3. By using the potentiometer across the circuit output it is possible to adjust the voltage of the output to a predetermined level at which the crowbar circuit 'fires'. The crowbar thyristor 'shorts' the main gates to earth and stops them from receiving gate pulses, so stopping conduction.

★ components list

R1	68Ω 5W wirewound resistor
R2, R3	270Ω ½W
R4, R5	1Ω 10W wirewound
R6	1.2kΩ ½W
R7	330Ω ½W
VR1	2.2k potentiometer (miniature preset)
C1	640μF 25V
LP1	Mains neon indicator
LP2	6.3V 0.2A lamp
S1	Single pole, single throw toggle
FS1	3A fuse
T1	Mains transformer, secondary 30V centre tapped, 3A
CSR1	2N3228 TO-66 or any 50V 5A thyristor, and mounting hardware
CSR2	2N3228 TO-66 or any 50V 5A thyristor, and mounting hardware
CSR3	TIC44
D1	1N4001
D2	1N4001
D3	1N1612R or any 50V 5A stud type (stud is anode) and mounting hardware
D4	6.8V 1 watt zener diode

Lamp holder (m.e.s.), connecting wire, mains lead, fuseholder, nuts, bolts, etc. Heatsinks (see Fig. 3.)

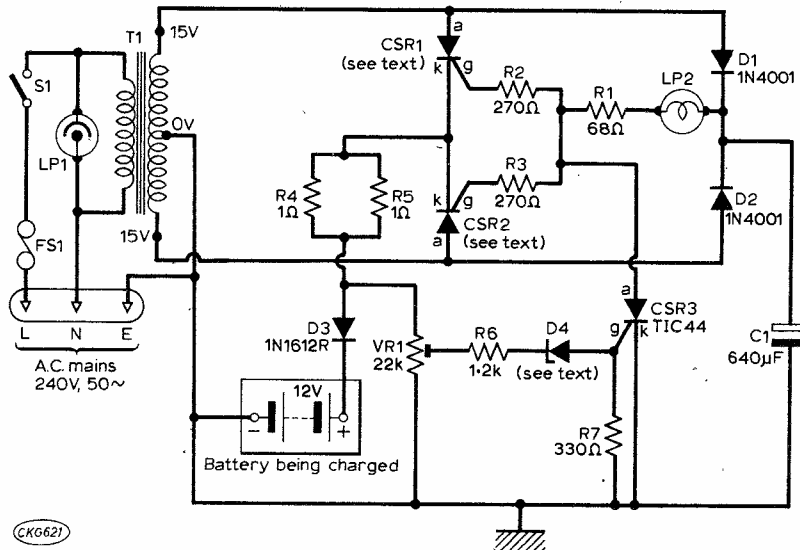


Fig. 1: Schematic circuit of the automatic battery charger.

When the board is complete and all wires to the transformer are connected make a final wiring check. Then set VR1 fully anticlockwise, and switch on the mains. Measure the voltage across C1; it should be approximately 20V.

Then connect a fully charged 12V battery (about 13.4V off load) across the output terminals. Advance VR1 slowly until the crowbar circuit just operates (lamp LP2 comes 'on'). The voltage measured between earth and R4, R5 and D3 junction should then be about 14V. Do not move the setting of VR1 again—sealing with a dab of glue is a good safeguard. Switch off the unit and disconnect the battery.

Connect a discharged battery to the unit and switch on. If an ammeter is available check the charge rate—about 2.25A. Alternatively measure the voltage across R4, R5; this should be about 1.1V. The crowbar circuit should not operate until the battery is fully charged and reaches 13.4V. Once operated the crowbar cannot be reset unless the mains supply is interrupted.

During power cuts this will be "automatically" accomplished. ■

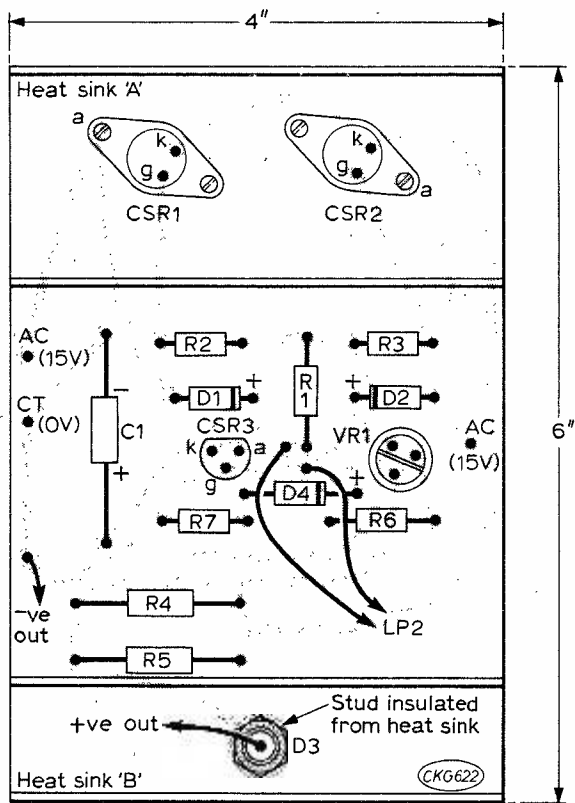


Fig. 2: Printed circuit board and component layout.

The circuit board layout is shown in Fig. 2. All components should be mounted onto the board and soldered up. Ensure that electrolytic C1 is connected correctly and check also the polarity of the thyristor and diode connections. The main thyristors, CSR1 and CSR2 and diode D3 must be mounted with insulators on their respective heatsinks. A smear of silicon grease should be applied to each side of the mica washers to ensure good thermal contact. Resistors R4 and R5 should be spaced clear of the board as they will run quite warm.

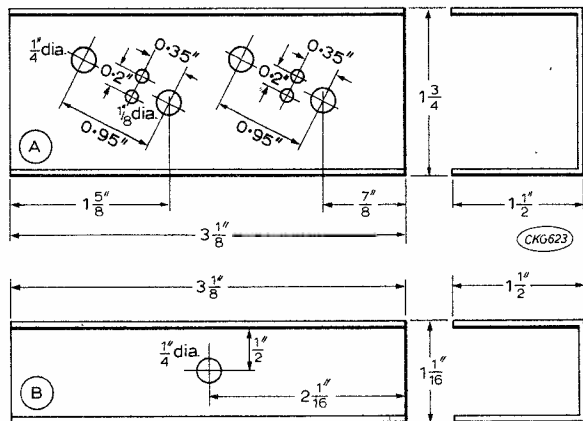


Fig. 3: Heat sink details, in 16 s.w.g. aluminium.

IMPEDANCE MATCHING—continued from page 1162

input impedance of the stage. Thus, a high input impedance makes for higher power gain and, hence, greater output power from the stage as well as improving the bass response, as it does in this particular application.

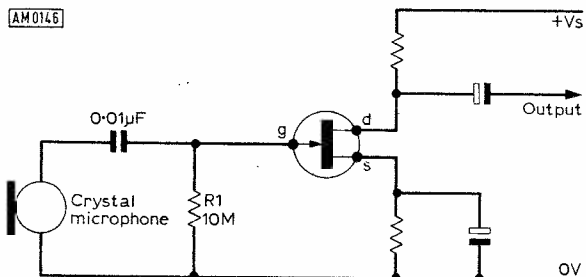


Fig. 7: A crystal microphone driving an audio preamp with a high input impedance.

Power fall-off

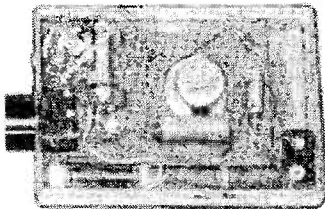
There are many such situations in which maximum transfer of power from source to load is not our only concern and load resistance should not be made equal to source output resistance. But the basic principles should be borne in mind. The maximum possible power will be delivered to the load when the input resistance of the load is equal to the output resistance of the source and any reactive components in the source impedance should be cancelled out by equal but opposite reactive elements in the load impedance.

In many practical cases exact equality of source and load resistances is not easy to achieve. It may be seen from Fig. 1 that the power transfer falls off more rapidly with decreasing load resistance than it does with increasing load resistance. Therefore, if it is necessary for a mismatch to occur, it is clearly much better to make the load resistance greater than the source resistance. ■

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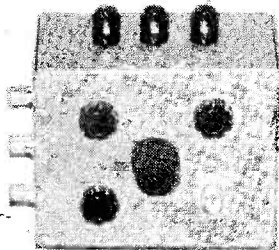
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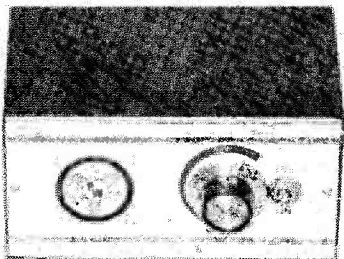
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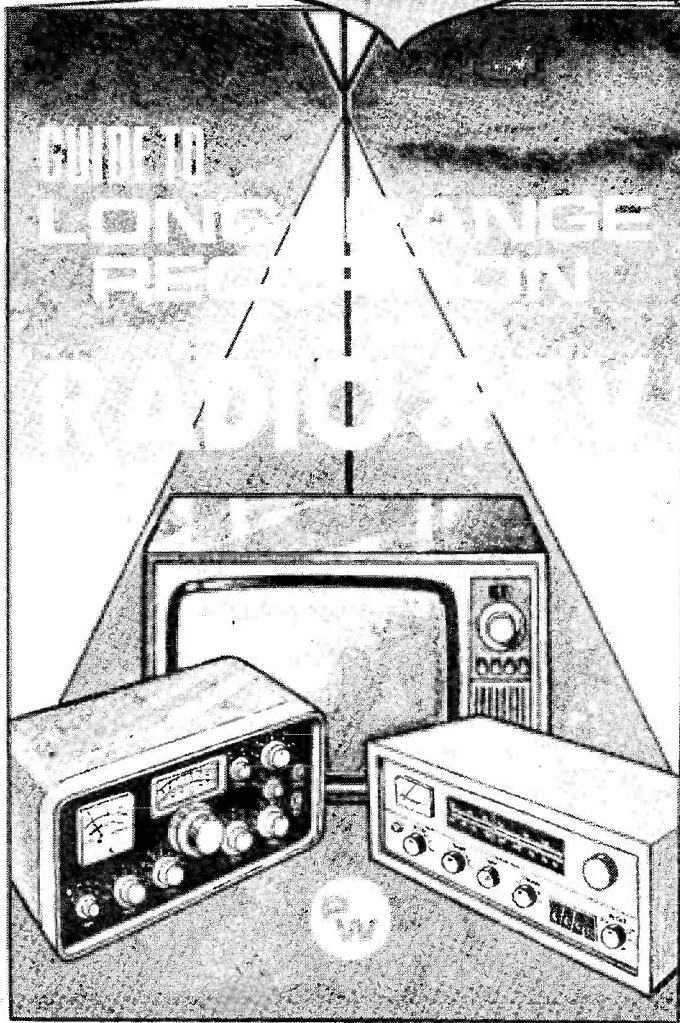


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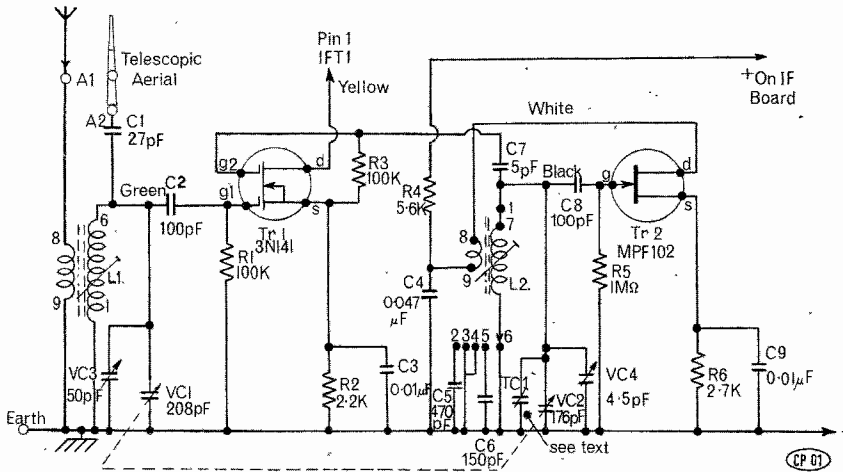


Fig. 1. First part of the circuit of the Slimline receiver. This contains the mixer stage Tr1 and the oscillator Tr2. Padders C5 and C6 are automatically connected into circuit when the appropriate coil L2 is inserted.

Fig. 2. The output from the mixer stage feeds into the first IF transformer IFT1 and amplified by Tr3 and Tr4. The capacitors across the windings of the IFT assemblies.

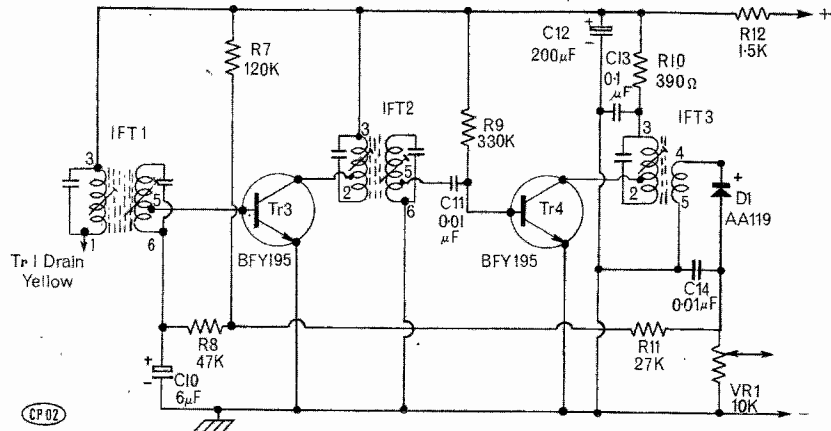
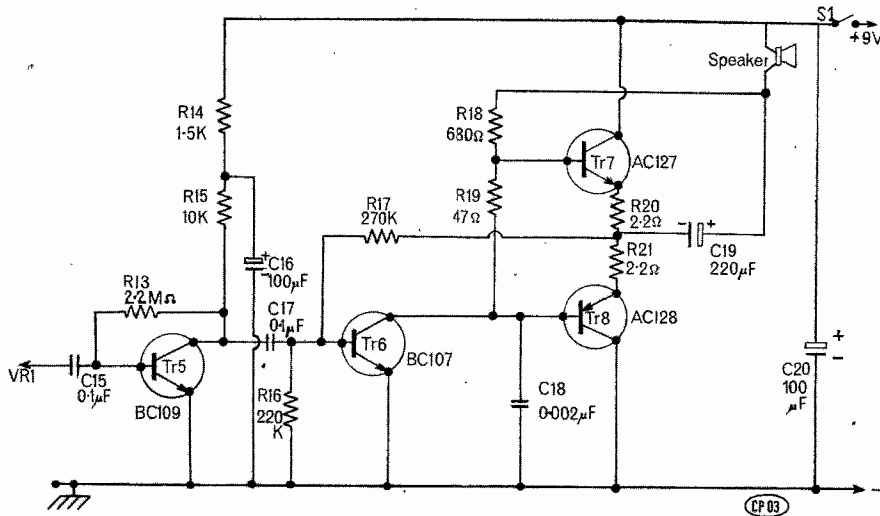


Fig. 3. The audio signal from the detector diode D1 in Fig. 2 is fed via the volume control to Tr5 and further amplified by Tr6, 7 and 8 and thence to the speaker.



Portable Receiver

THIS portable receiver is in a 7×5in. case only 1in. deep, though to these dimensions must be added those of the Trimmer, Fine Tuning and Volume/On-Off controls at one end, and the Band-setting dial on the front. These do not however increase the size very much. The receiver may be operated with its own telescopic rod aerial, with an improved aerial such as a few yards of thin insulated flexible wire or with a conventional aerial.

The coverage of the five bands is approximately as follows:—

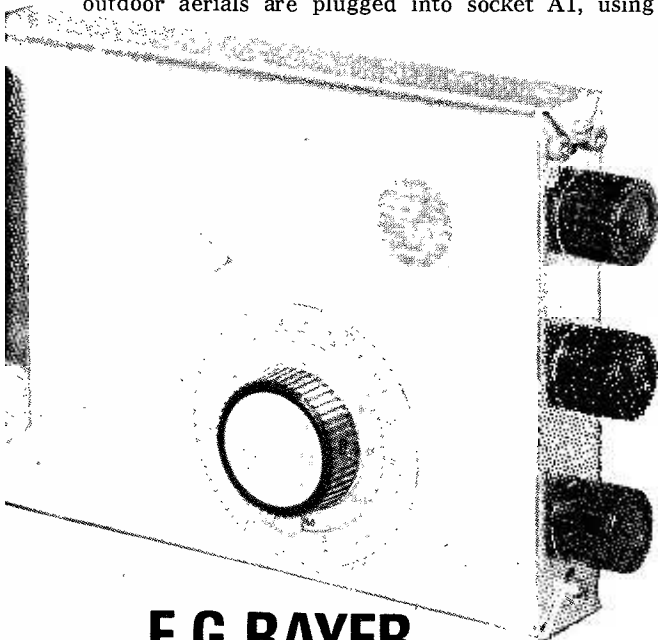
Band 1	160—350kHz
„ 2	580—1500kHz
„ 3	1.75—4.0MHz
„ 4	5.9—11.5MHz
„ 5	13—27MHz

The receiver thus has a wide general utility, tuning medium and long waves, if required, in addition to the most popular short wave bands.

Eight transistors and one diode are employed and the receiver is wired and assembled in separate units. A dual-gate 3N141 mixer is used with an MPF102 FET oscillator, followed by two BFY195's and AA119 diode for IF amplification, demodulation and AGC. The audio section has a BC109 pre-amplifier and BC107 driving an AC127 and AC128 complementary output stage, which provides adequate power for the internal speaker.

CIRCUIT DETAILS

The telescopic aerial, or a **short** wire aerial, is connected to socket A2 Fig. 1, but longer indoor or outdoor aerials are plugged into socket A1, using



F. G. RAYER

the primary coupling winding of the aerial coil L1. This circuit is tuned by VC1 and the panel trimmer VC3 is provided so that this can be peaked for maximum efficiency with any aerial. Signals are taken to gate 1 of Tr1 and gate 2 is coupled by C7 to the oscillator Tr2. The oscillator coil L2 is tuned by the second section of the ganged capacitor VC1/VC2. VC4 is a bandsread tuning control to allow easy tuning on the short wave bands.

L1 and L2 are plug-in coils so there is no need to obtain coils for those bands which are not required. Band 1 is for long wave coverage and may not be wanted in some areas. The extreme high frequency end of this band is not used (above about 350kHz) as instability arises when this stage is tuned near the intermediate frequency, as would be expected.

Band 2 is for medium wave coverage while Band 3 includes shipping and other transmissions, as well as the 160m and 80m amateur bands. Most general short wave broadcasts come in Band 4 and also Band 5.

Capacitors C5 and C6 in Fig. 1 are padders and the correct value is brought into circuit for each coil when it is inserted, by wiring to the appropriate socket pins. TC1 is an integral trimmer on VC2. If VC1/2 is a type without trimmers a separate 30pF or similar small pre-set must be connected here.

Fig. 2 is the circuit of the IF amplifier. IFT1 and IFT2 are double tuned and IFT3 single tuned and these, with the two BFY195's, result in good selectivity and gain. The demodulator diode D1 provides audio signals for the volume control VR1, and automatic gain control bias for the first IF stage. Current for the IF stages is taken from the 9V supply, through R12, the mixer drain circuit being supplied through the primary of IFT1. The on-off switch S1 is incorporated with the volume control VR1.

The circuit of the audio stages is shown in Fig. 3. Tr5 is a low level high gain amplifier with output to the driver Tr6 which drives the NPN/PNP pair Tr7 and Tr8, R17 providing stabilisation of the DC operating conditions. The circuit is intended for an 18 ohm speaker but it will be found that good results are obtained with a 25 ohm or 35 ohm unit.

CONSTRUCTION

Both sides of the mixer/oscillator board are shown in Fig. 4. Plain perforated Veroboard is most suitable, with 0.15in matrix. The resistors and capacitors are inserted as shown and the board turned over and leads soldered underneath. In most places the wire ends of the components are long enough to reach other points. Soldered joints should be small and leads kept near the board, with sleeving on leads which may touch each other. The tag MC is later secured with a 6BA or 8BA bolt, to hold the board clear of the panel and to form a negative or earth return.

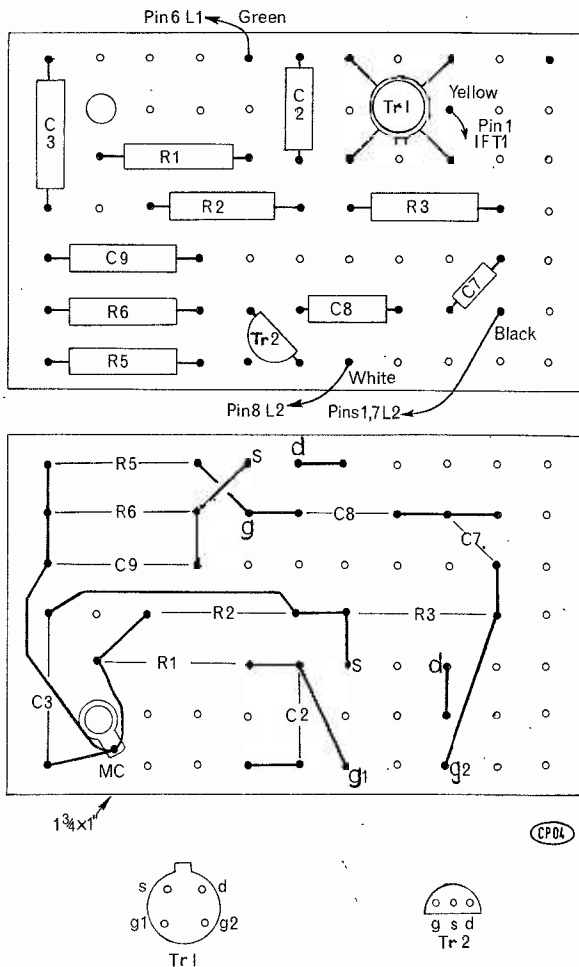


Fig. 4. Layout of the mixer/oscillator board. Veroboard pins can be used where necessary, if component leads are too short.

Important. An insulated gate transistor of the 3N141 type has an extremely high gate internal resistance and it can be destroyed by the static charge of metal or plastic tools, or by touching its leads with the fingers. Despite this, there is virtually no danger to the transistor if it is installed correctly and once R1, R2 and R3 are connected to it, these protect the gate circuits from static charges.

Leave Tr1 until other wiring on this board is finished. Tr1, as supplied, should have a thin spring or loop which short circuits its four leads, to protect it. This is not removed until the transistor is soldered in place. If it has to be unsoldered for any reason, a length of thin, clean wire should be wound round the four leads, under the transistor, before this is done. Spread the leads with a matchstick so that they come through the holes shown in Fig. 4, bend over the wires from R1, R2 and R3, and solder them to the transistor leads.

It is convenient to use colour coded leads for the external connections. These may be green from C2 for VC1 and pin 6 of L1, yellow for the drain circuit, white from Tr2 drain to pin 8 of L2 and black for VC2 and pins 1 and 7 of the holder for L2.

The IF board is shown in Fig. 5. Holes for the IFT pins and screening can tags should be drilled first. The pins are identified by their spacing, and should be arranged as in Fig. 5. A very small round file may

be useful in adjusting the positions of holes, if drilling is not quite correct, so that the IFTs fit without strain on their pins. Holes should also be drilled so that the cores can be reached. Two small tags are secured with the bolts MC, which also fix two angle brackets in place. These brackets allow the board to be fixed to the receiver panel.

Note the polarity of C10, C12 and D1. Proceed with the wiring as for the mixer-oscillator board, with insulated sleeving where required. The wire ends of R12 and C14 can be left projecting, so that other connections can be soldered on later.

The AF amplifier board is built in a similar manner, components being positioned as in Fig. 6. As it is rather difficult to see the transistor lead positions when these are in place, short pieces of coloured sleeving may be put on these wires first, to identify them—green for emitter, blue for base and orange for collector.

Capacitors C16 and C20 are arranged vertically. Bolts secure the tags MC and small brackets, as with the IF board. If necessary, these brackets can be cut from a small spare section of flanged universal

★ components list

Resistors

R1 100kΩ	R8 47kΩ	R15 10kΩ
R2 2.2kΩ	R9 330kΩ	R16 220kΩ
R3 100kΩ	R10 390Ω	R17 270kΩ
R4 5.6kΩ	R11 27kΩ	R18 680Ω
R5 1MΩ	R12 1.5kΩ	R19 47Ω
R6 2.7kΩ	R13 2.2MΩ	R20 2.2Ω
R7 120kΩ	R14 1.5kΩ	R21 2.2Ω

All resistors 5% $\frac{1}{4}$ watt

VR1 10kΩ log. pot. with switch S1

Capacitors

C1 27pF	C8 100pF	C15 0.1μF
C2 100pF	C9 0.01μF	C16 100μF 10V
C3 0.01μF	C10 6μF 4V	C17 0.1μF
C4 0.047μF	C11 0.01μF	C18 0.002μF
C5 470pF	C12 200μF 10V	C19 220μF 6.4V
C6 150pF	C13 0.1μF	C20 100μF 10V
C7 5pF	C14 0.01μF	

VC1/2 208—176pF gang (Jackson 00)

VC3 50pF (Jackson C804)

VC4 4.5pF (Jackson C804)

TC1 30pF trimmer, see text

Semiconductors

Tr1 3N141	Tr4 BFY195	Tr7 AC127
Tr2 MPF102	Tr5 BC109	Tr8 AC128
Tr3 BFY195	Tr6 BC107	D1 AA119

Inductors

IFT1/2 IF Transformer (Denco IFT18/465)
IFT3 IF Transformer (Denco IFT14)
L1/2 Plug-in coils, 9 pin miniature valve type for ranges required (Denco—'Blue' for aerial coils and 'Red' for oscillator coils)

Miscellaneous

Speaker, about 2½in dia., 18 to 35 ohms. Telescopic aerial. Small sockets (2). B9A valveholders, plain (2). Perforated veroboard 0.15in matrix, 1½ x 1in, 3½ x ½in and 2½ x ¾in. Knobs (4). Perspex for dial.

Casework Plates 7 x 5in (2) (CU168)

Flanged members 7 x 1in (2) (CU54A)

Flanged members 5 x 1in (2) (CU52A)

All from Home Radio.

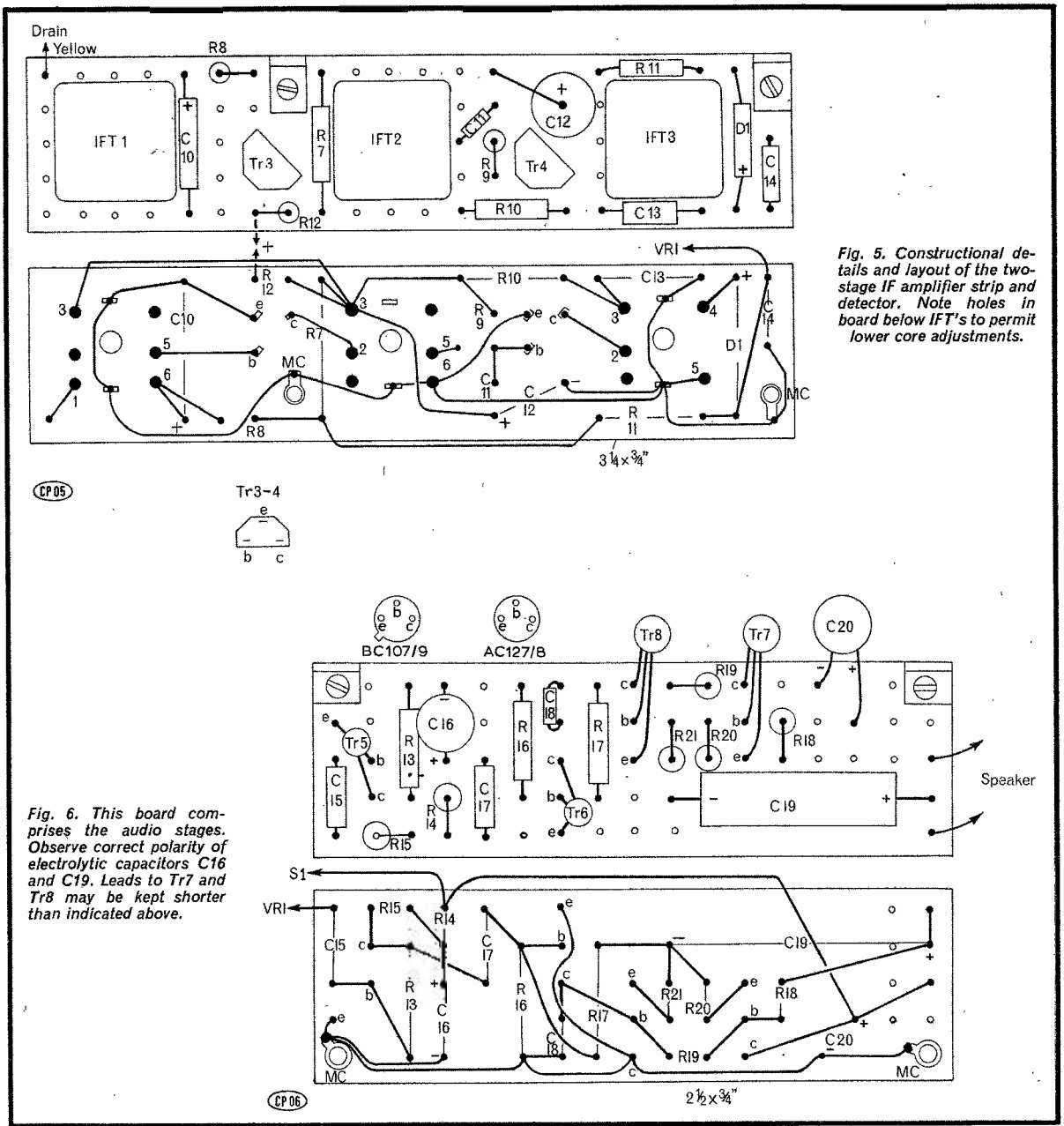


Fig. 5. Constructional details and layout of the two-stage IF amplifier strip and detector. Note holes in board below IFT's to permit lower core adjustments.

Fig. 6. This board comprises the audio stages. Observe correct polarity of electrolytic capacitors C16 and C19. Leads to Tr7 and Tr8 may be kept shorter than indicated above.

chassis, as used later for the coil holders. Both brackets and insulated board are drilled for 8BA bolts.

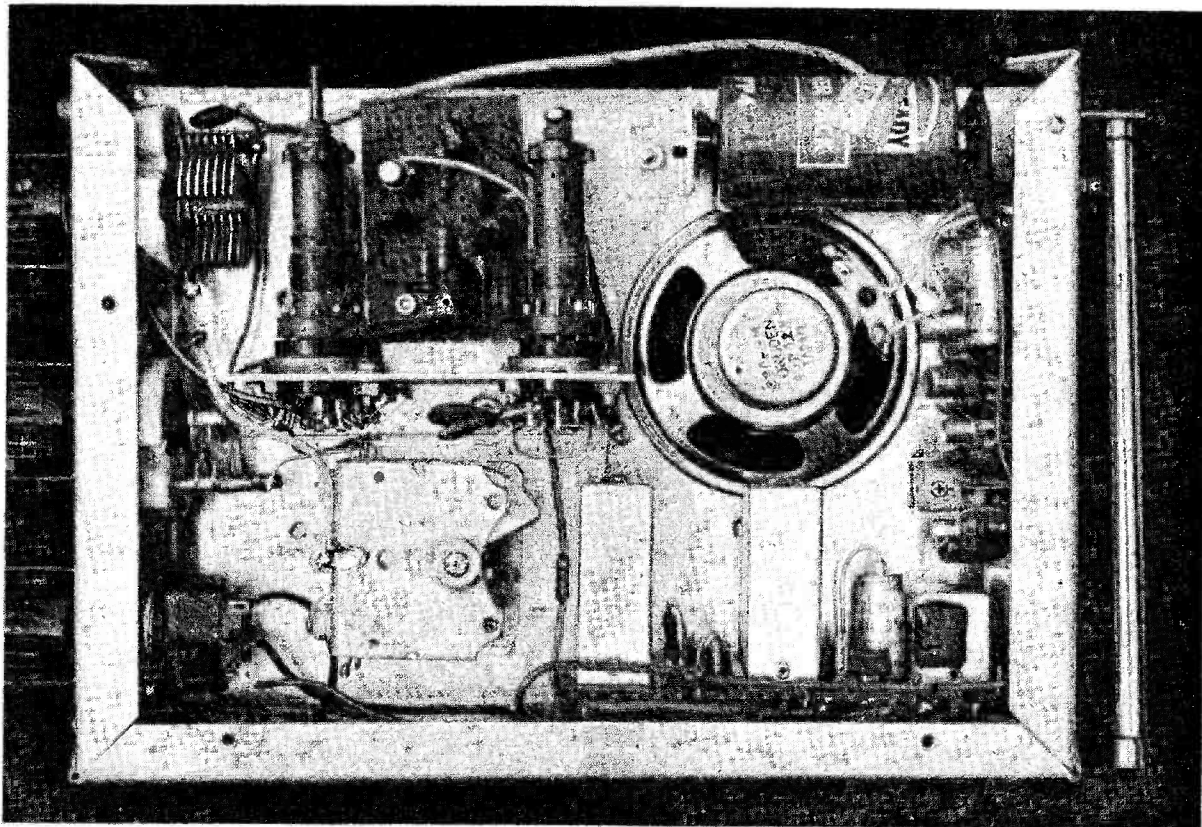
A piece of metal with a flange, for mounting the coil holders, is cut $2\frac{3}{4} \times 1$ in so that the holders can be fitted as in Fig. 7. A small section is cut away near L2 as shown, to allow the speaker to fit.

The flange is bolted lin. from the edge of the panel, as in Fig. 8. There is little free space so items should be positioned carefully. The flange is held with 6BA countersunk bolts and nuts. The ganged capacitor is held with three 4BA bolts, which must be cut or filed short so that they do not project beyond the thickness of the capacitor's front plate.

Wiring can then be completed as in the diagrams. The IF, AF and mixer-oscillator boards are held

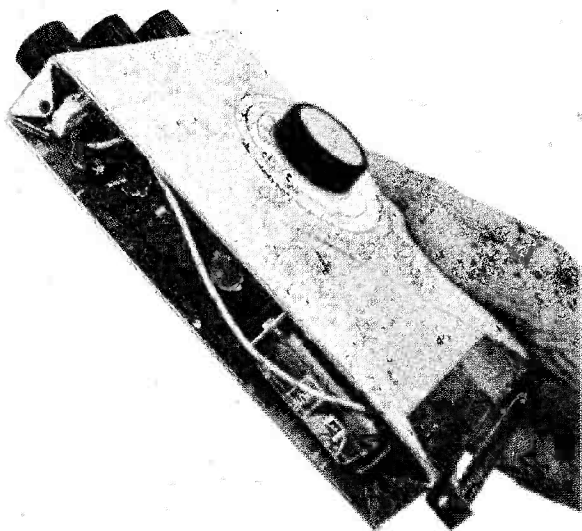
with 8BA countersunk bolts. The one 5×1 in flanged runner is fixed with bolts or self-tapping screws so that VC3, VC4 and VR1 can be mounted, but the other flanged members are left off until later. Leads between units are run against the metal. The speaker is cemented over a $1\frac{3}{4}$ in diameter hole and the leads soldered to it. Other connections will be seen in Figs. 7 and 8.

The battery is mounted by a bracket, to which a negative snap connector is bolted. This both holds the battery and provides the negative connection. Two small sockets provide A1 and Earth connections. When all wiring is finished, except for the telescopic aerial, the receiver can be aligned. Do not forget to remove the shorting collar or wire from the mixer transistor.



IF ALIGNMENT

As the IFT's are supplied pre-aligned, the cores should not be touched until reasonable results are being obtained. A properly fitting tool must be used, such as that available from the IFT maker, as a wedge-shaped blade may easily break the cores so that they cannot be rotated. Where a signal



Removal of edge panel permits easy coil changing or replacement of battery.

Inside the Slimline receiver. Main components may be identified from Fig. 8.

generator is available, place the output lead of this near the yellow lead (mixer drain) and adjust the cores for best output.

If no generator is available turn the audio gain control to near maximum and tune in a weak but stable signal, such as that obtained from a local BBC transmitter, with no aerial at all in use. With this tuned in correctly, adjust the five cores slightly, as may prove to be necessary, for best volume. An alternative is to connect a high resistance test meter across VR1 (positive to chassis) and use a somewhat stronger signal, so that cores can be peaked for the best reading. When these cores have been adjusted, they should be left alone since their settings are not changed when dealing with the mixer and oscillator circuits.

MIXER/OSCILLATOR ALIGNMENT

If VC1/2 has trimmers, open fully the trimmer on VC1 and screw down the trimmer on VC2 and set VC3 and VC4 about half open. Each range is dealt with separately. Suppose that Range 3 is aligned first. Adjust the core of L2 (Red coil) so that band coverage is approximately correct. Then tune in a signal around 3.5 to 4.0MHz and adjust VC3 for best volume. Leave VC3 at this setting and tune to a signal around 1.9MHz. The core of L1 is then adjusted for best results, after which there is little need for much adjustment of VC3, throughout the band. When VC3 is peaked for best results, it should be neither fully closed nor fully open.

The other ranges are dealt with in the same manner. The cores of L2 are adjusted in that

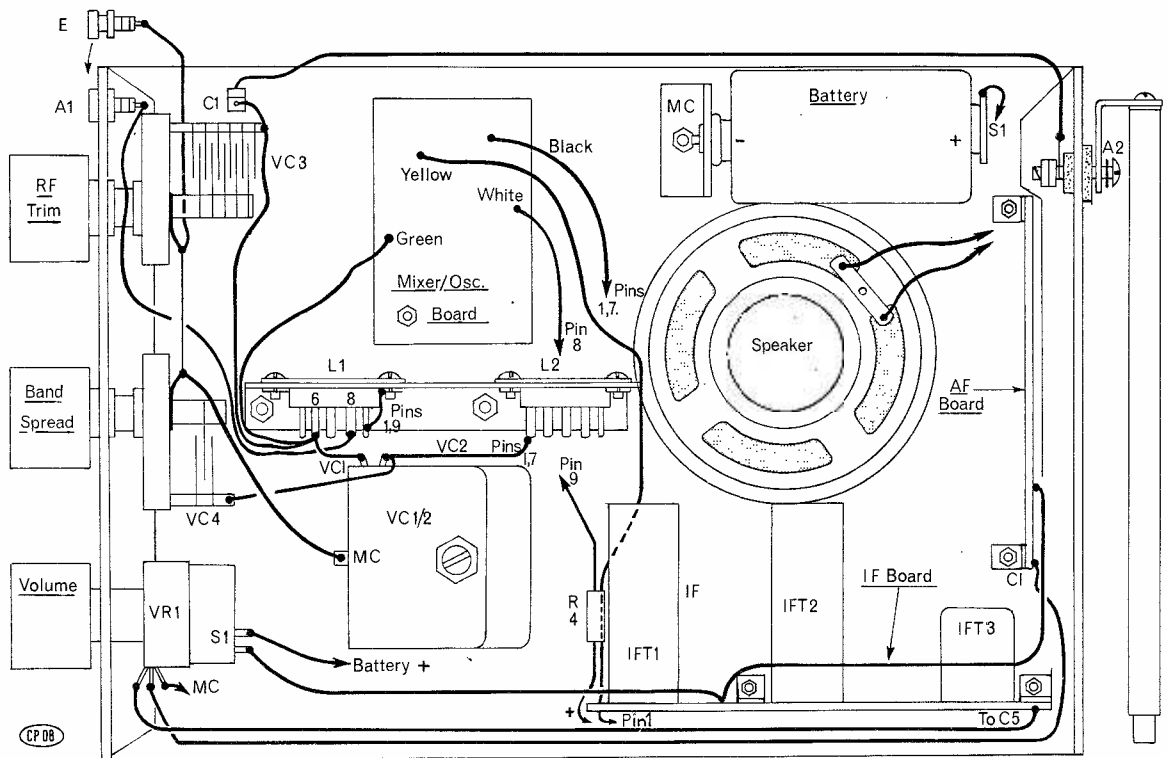


Fig. 8 Location of the three boards and major components. The battery is held in position by the bracket holding the negative clip.

direction which takes them away from the smaller winding for Ranges 1 and 3, otherwise continuous oscillation may prove troublesome at the high frequency end of these bands. This arises from the degree of coupling between L2 and its feedback winding. Should excess oscillation or "squegging" of the oscillator be troublesome, R4 could be increased in value. On the other hand, if Tr2 has somewhat reduced gain the value of R4 could be reduced. However, with the value shown, several MPF102 transistors proved satisfactory, so this should not be necessary.

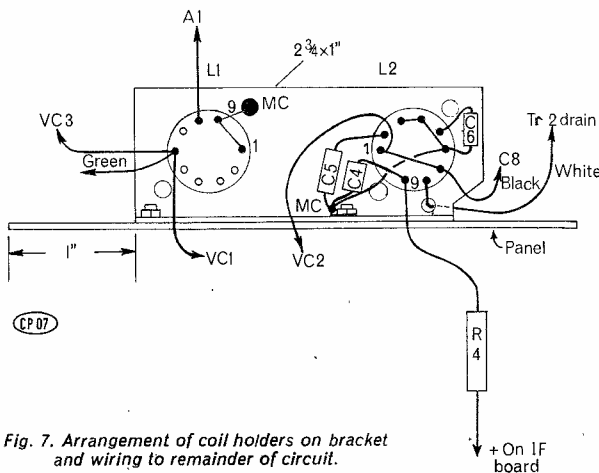


Fig. 7. Arrangement of coil holders on bracket and wiring to remainder of circuit.

FINISHING OFF

The aerial is fixed to a small right angle bracket which is pivoted on a 6BA bolt passing through the side of the case. The hole is drilled to take an insulated bush and an insulated washer rests between the bracket and case. A spring washer is placed under the screw head and the nuts locked together so that the aerial can be extended vertically with the case flat or standing upright. A flexible lead runs from the aerial to C1.

The dial is marked on card and is about $2\frac{3}{4}$ in. in diameter. The control knob is a shallow type to which is attached a $2\frac{3}{4}$ in. diameter disc of $\frac{1}{16}$ in. thick Perspex. This can be fixed with adhesive or self-tapping screws. A line is marked across the Perspex. A disc can be easily cut with an adjustable tank or washer cutter, but if this is not available a pointer knob could be substituted for the disc.

The case is completed by screwing on one 7×1 in member and the remaining 5×1 in member. The 5×1 in members fit inside the 7×1 in members so that the top 7×1 in flanged member can be taken off to change the battery or coils. The back, a 7×5 in flat plate, is permanently attached with self-tapping screws, but only one screw is run into the top member flanges.

There is some opportunity for individual choice in the way in which the case is finished. If left bare or painted, gauze or perforated metal should be fitted over the speaker aperture inside. The case shown was covered at the front with fabric and self-adhesive material as used for shelves, boxes, etc.

CASSETTE RECORDER AND TUNER AMPLIFIER

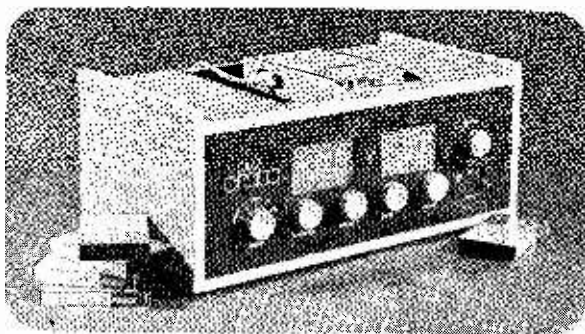
PART 2

RICHARD COLLIN

POWER AMPLIFIER ASSEMBLY

The first stage in assembly is to mount all components except the plastic power transistors onto the board, ensuring correct polarity of electrolytic capacitors. Solder each joint carefully—do not overheat the components, but make sure joints are properly made. Check that all parts are in the correct position and then cut off all excess lead wires. Note that R13 and C9 are mounted on the speaker sockets, not on the printed board.

Next fit the output and driver transistors onto their respective heat sinks ensuring that the mica washers and nylon bushes are correctly located. Check that each device is isolated from the heatsink after assembly. Then form the leads for insertion into the printed board. **Do not** bend the leads less than $\frac{1}{8}$ in from the transistor body. **Do** support the leads near the body with long-nose pliers whilst forming. **Do not** radius the bends tighter than $\frac{1}{8}$ in.



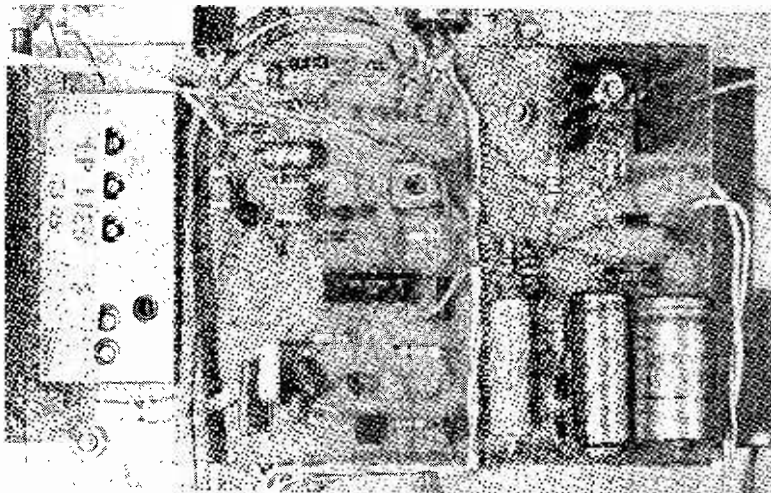
Mount the strip of four output devices onto the circuit board and solder up the connections. Then mount the two driver transistors in a similar fashion. Once soldered ensure that the power transistors are not bent back and forth on their leads—plastic packaged devices can be easily damaged by stressing the lead outs. Once complete the power board should be put away safely until needed later on.

TUNER AND IF CIRCUIT (UNIT 3)

The AM section utilises the Ferranti ZN414 integrated circuit IC1 and a single transistor amplifier Tr1. A small ferrite rod aerial forms part of a double-tuned aerial circuit which is used to eliminate swampy effects of strong local transmissions by improving the selectivity. The circuit and printed board illustrated are for the single-station version. Further channels may be added by inserting a suitable two-pole rotary switch at the points marked "X" and "Y" in Fig. 10 to select additional pairs of trimmer capacitors for each station required.

The ferrite aerial may be insufficient in some areas of poor signal strength. The AM aerial socket, which is loosely coupled to the ferrite rod by two turns of insulated wire, allows adequate reception under such conditions by connection of an external aerial.

In the FM section, a Mullard varicap tuned module type LP1186 feeds an RCA IF amplifier integrated circuit IC2 through a ceramic filter tuned to 10.7 MHz. This integrated circuit requires only one IF coil to provide the audio output for the decoder and also an AFC control voltage.



The prototype Tuner and IF board shown here has some variations in layout from the final version given in Fig. 12

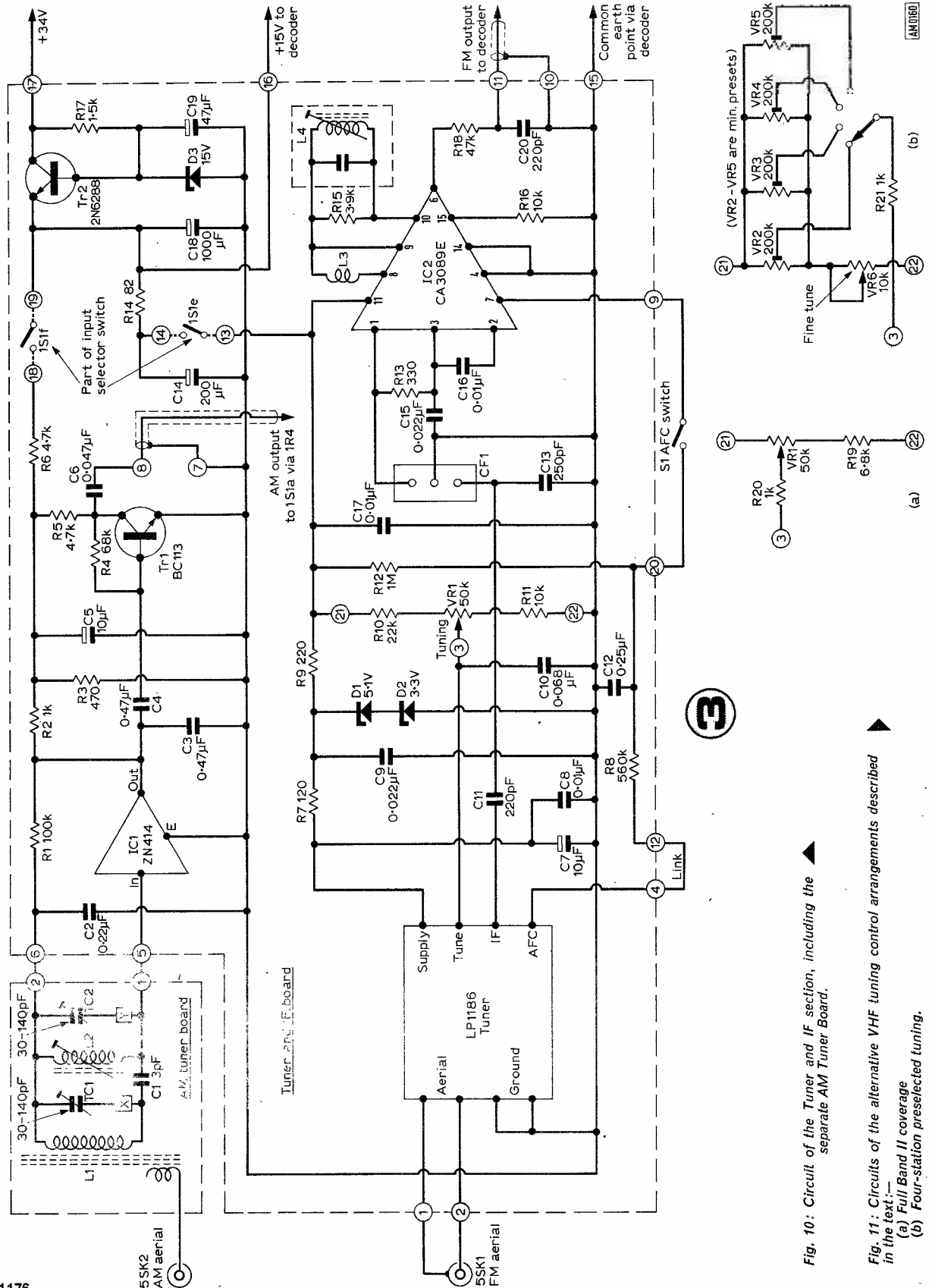


Fig. 10: Circuit of the Tuner and IF section, including the separate AM Tuner Board.

Fig. 11: Circuits of the alternative VHF tuning control arrangements described in the text:
 (a) Full Band II coverage
 (b) Four-station prescanned tuning.

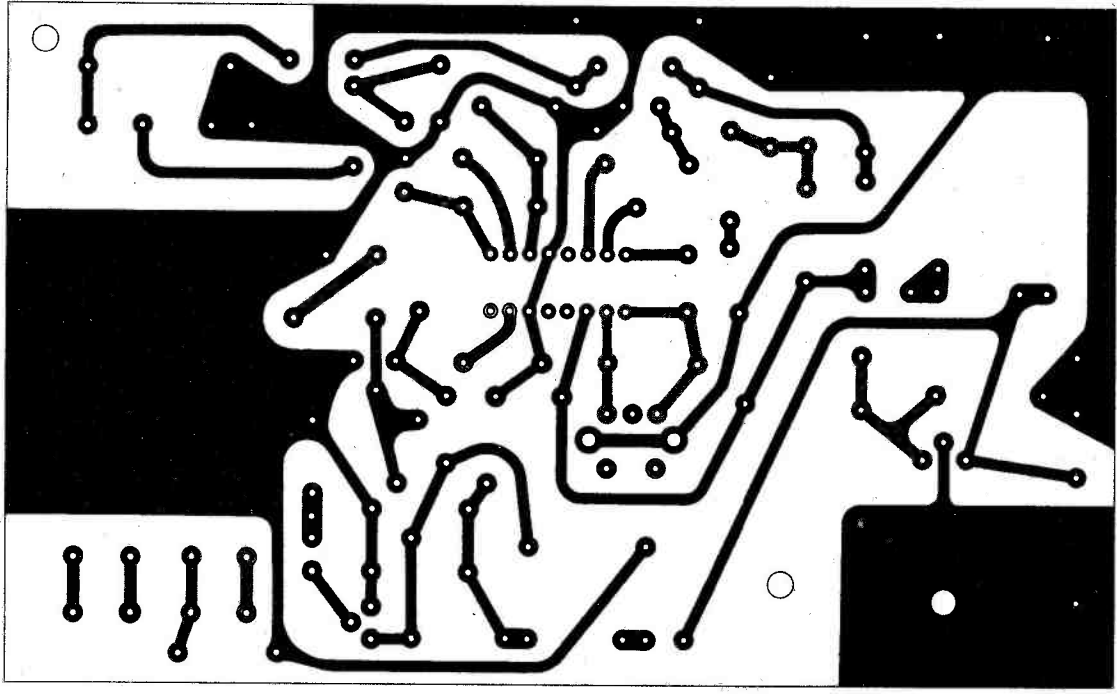
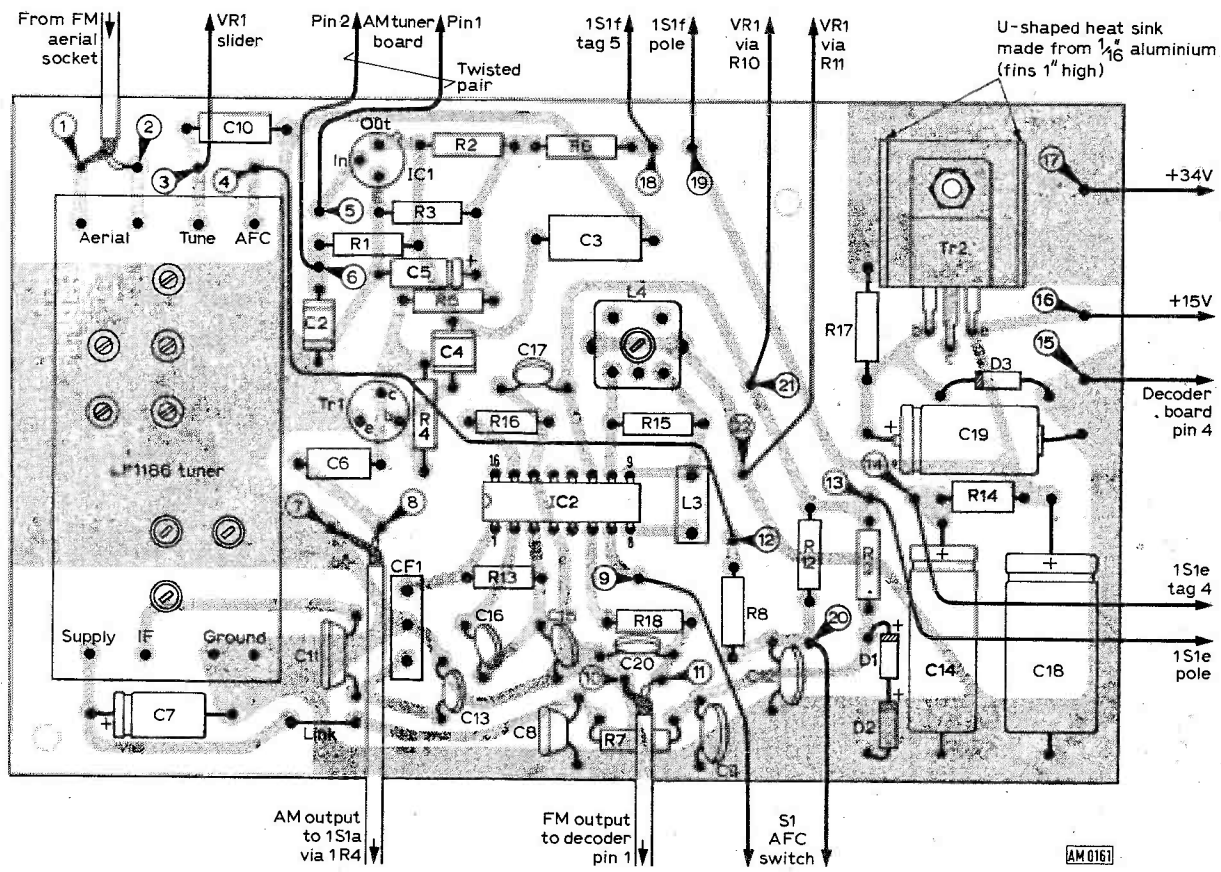


Fig. 12: Component location and printed circuit layout for the main Tuner and IF board. Both drawings are actual size.

★ components list

TUNER & IF BOARDS

Resistors

R1 100kΩ	R11 10kΩ
R2 1kΩ	R12 1MΩ
R3 470Ω	R13 330Ω
R4 68kΩ	R14 82Ω
R5 4.7kΩ	R15 3.9kΩ
R6 4.7kΩ	R16 10kΩ
R7 120Ω	R17 1.5kΩ
R8 560kΩ	R18 47kΩ
R9 220Ω	
R10 22kΩ	VR1 50kΩ lin

Note—The alternative VHF tuning arrangements require the following changes in components.

- (1) Full range continuous tuning (Fig. 11a)
Delete R10 and R11 above and add
R19 6.8kΩ R20 1kΩ
- (2) Preselected tuning (Fig. 11b)
Delete R10, R11 and VR1 above and add
R21 1kΩ VR2-VR5 each 200kΩ min. preset
VR6 10kΩ lin
All fixed resistors ¼W 5% carbon film

Capacitors

C1 3pF ceramic	C11 220pF ceramic
C2 0.22μF ceramic	C12 0.25μF ceramic
C3 0.47μF polyester	C13 250pF ceramic
C4 0.47μF polyester	C14 200μF 25V
C5 10μF 16V	C15 0.022μF polyester
C6 0.047μF polyester	C16 0.01μF polyester
C7 10μF 16V	C17 0.01μF polyester
C8 0.01μF polyester	C18 1000μF 16V
C9 0.022μF polyester	C19 47μF 16V
C10 0.068μF polyester	C20 220pF ceramic
TC1 30-140pF compression trimmer	
TC2 30-140pF compression trimmer	

Semiconductors

Tr1 BC113	IC1 ZN414 (Ferranti)
Tr2 2N6288 (RCA)	IC2 CA3089 E (RCA)
D1 BZY88 C5V1	D2 BZY88 C3V3
D3 BZY88 C15	

Miscellaneous

- L1 55 turns of 30swg enamelled copper wire on 2½" x ⅝" dia. ferrite rod
- L2 Single-tuned Medium Wave coil
- L3 RF Choke 15μH Toko 7BA 150J
- L4 Toko KACS-K586-HM
- CF1 Crystal filter Vernitron FM4 or Toko CFS10-7
- S1 SPST min. toggle switch
- FM tuning head Mullard LP1186
- Tuning drive drum 1½" dia.
- Slow-motion cord drive spindle
- Cord tension spring ½"
- 3 small nylon pulleys
- Printed circuit boards

Notes

1. RCA semiconductors are available from E.C.S. (Windsor) Ltd. (see Part 1 of this project).
2. Toko components are available from Ambit International.

The values given for the tuning control circuit allow coverage of 88-100 MHz. A restricted coverage has the advantage of making the tuning finer and spaces the stations farther apart. The alternative circuit of Fig. 11a provides coverage of the full band 88-104 MHz whilst a four-station preselected tuning arrangement is given in Fig. 11b.

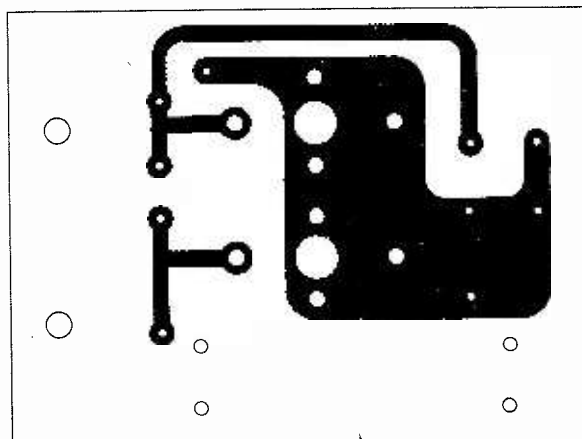
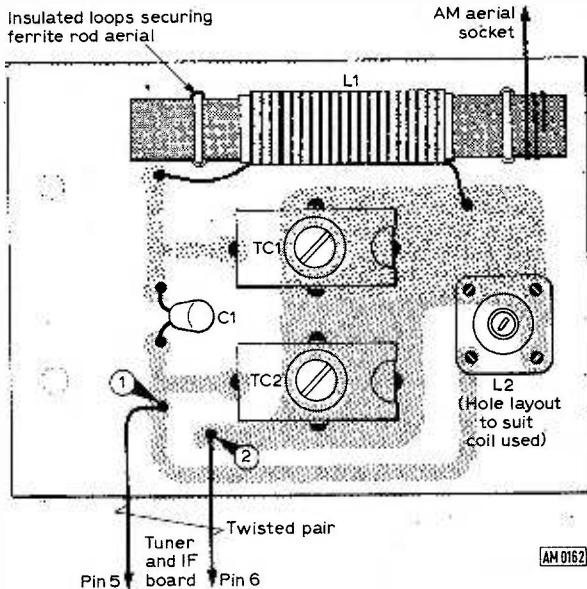


Fig. 13: Location of components and actual size layout for the AM Tuner Board.

Four power supplies are derived from the main 34V rail through a series stabiliser transistor Tr2 and various filter networks.

1. The decoder 15V supply is taken direct from the stabiliser and decoupled via C18.
2. The AM tuner 1.5V supply is provided by a resistive potential divider across the 15V supply R3/R6. Decoupling is provided by capacitor C5.
3. The FM IF and tuner varicap supply is taken from the 15V supply via R14 and decoupled by C14/C17. This supply is 12V.
4. The FM tuner 8V supply is provided from the 12V supply by R9, D1/D2 and R7. Decoupling is provided by C7, C8 and C9.

When assembling the printed board care must be taken not to overheat the integrated circuit pins and also not to short-circuit the adjacent connections as they are fairly close together. Ensure that all electrolytics and diodes are polarised correctly and that the ZN414 leads are correctly positioned. The ceramic filter CF1 may be mounted any way round—the centre pin is earthed and either of the other two pins may be input or output. The series stabiliser transistor Tr2 does not require isolation from either its heatsink or the copper print on the board.

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CRATA—continued

The AFC switch is mounted on the tuner back panel near the aerial sockets—it may be sited on the front panel if required, but do not locate it near to the mains neon and switch.

The AM aerial board, Fig. 13, on which the ferrite rod is mounted should ideally be mounted such that it can be rotated through 90° for maximum signal pickup. Alternatively it may be rigidly mounted in the correct position if the tuner will always be sited in one particular place. The leads between the printed board and the rotary switch in the multi-station version should be kept very short. A suitable position for the switch is immediately above the Input Selector.

Due to pressure on editorial space, details of the Stereo Decoder have been held over until our May issue which will also describe the Power Unit and Chassis.

oscilloscope

PART 2

techniques

ALAN AINSLIE

OSCILLOSCOPE DISPLAYS

The very heart of any oscilloscope is the cathode ray display tube. After all the electronic functions have been executed the ultimate result is displayed, visibly, on the face of the tube. We shall take a look at a few types of CRT and their associated circuitry as applied to oscilloscopes.

The electron beam, produced by an electron gun, passes through a deflecting mechanism and arrives at the screen where it causes the screen material to fluoresce. The whole mechanism is housed in an evacuated glass container and, in an oscilloscope, only the front face is visible. Fig. 1 shows the general arrangement. For oscillographic use we require a bright spot of light, intense but very small.

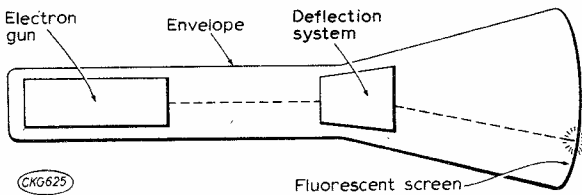


Fig. 1: Main elements in a CRT intended for use in an oscilloscope.

It is the purpose of the electron gun to produce the narrow stream of electrons of high energy to cause local luminescence of the screen. When the beam hits the phosphor screen it causes fluorescence. However, if the beam is cut off suddenly the screen continues to glow with phosphorescent light. It is this phosphorescent light that determines the after-glow of the tube.

ELECTRON GUN

A hot cathode on the axis of the tube produces electrons by thermionic emission, as in a conventional electronic valve. By a suitable arrangement of anodes an electric field distribution inside the tube is created focusing the electrons into a high velocity pencil, arranged to converge on to the screen. A simple gun arrangement is shown in Fig. 2. This type of arrangement is often used and is known as a pentode or five electrode gun.

The cathode is heated to emissive temperature and is surrounded by the grid, in this case shaped like a top-hat with a hole in it, known as a Wehnelt cylinder. The grid is maintained slightly negative with respect to the cathode and focuses the space charge around the cathode along the axis of the gun.

The first anode (A1) is positive with respect to the cathode by perhaps a couple of hundred volts. Fig. 3 shows how the electrons are accelerated out of the grid area towards the first anode, and in so doing are focused at Z by the equipotential lines, shown dotted. The diameter at Z is used as an "image" and consequently should be as small as possible for a small spot on the screen. The electron beam enters the first anode diverging and a number of stops are added to keep the beam width small and keep out fringe electrons which impair definition. The diverging electron beam emerging from the first anode now needs to be focused on to the screen, or put another way, an image of Z is projected on to the screen.

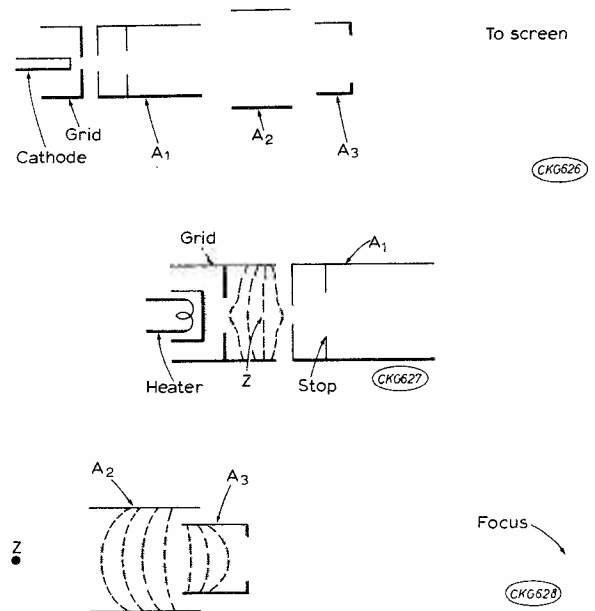


Fig. 2: top, arrangement of electrodes used in a pentode gun. Fig. 3, centre, shows the beam focusing action of the grid and A1. Fig. 4, bottom, the effect of the remaining anodes A2 and A3 in focusing the beam on to the screen.

Fig. 4 shows how the second (A2) and third (A3) anodes accomplish this focusing. The second anode is at a higher potential than A1, and A3, the final anode, is at a still higher potential. Thus the equipotential lines are as shown dotted. The beam of electrons now converges as it crosses the A2-A3 fields and by adjustment of the voltage between A2 and A3 the beam can be focused on the screen of the CRT.

In simpler types of CRT A2 is omitted giving a tetrode electron gun. The final focusing takes place between A1 and the final anode and geometrically is suitable for a fine spot. However, if focusing is achieved by varying A1 (the final anode potential is fixed as we shall see later) this affects the velocity of the beam because A1 is the primary accelerating anode. The change in velocity changes the position of the point Z and the range of focus is restricted for a good spot size. This situation in practice means that when the grid potential (brightness) or the A1 potential (focus) is altered the other potential must be changed as well, giving restricted focus and brightness range. It is for this reason that the pentode type of tube is almost universally used.

BEAM DEFLECTION

An electron has a negative charge of 1.6×10^{-19} coulombs. This is a very small charge, and conversely any electric field acting on the electron will produce only a very small force. However the mass of the electron is very small and so large accelerations can be produced with only moderate potentials.

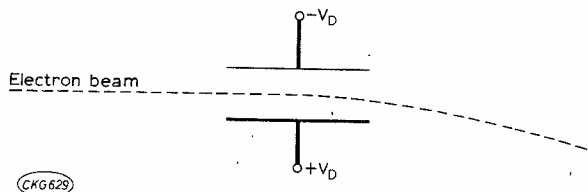


Fig. 5: Effect of the deflecting plates on the electron beam.

If a beam of electrons, focused into a fine pencil, is allowed to pass between two parallel plates as in Fig. 5, the electrons will experience a force towards the positive plate and it can be shown that the deflection is proportional to the deflecting voltage (V_d) and inversely proportional to the accelerating voltage (V_a). A purely mathematical outlook shows that electrostatic deflection produces a (theoretically) linear deflection mechanism.

DEFLECTION PLATES

In order to keep the sensitivity as high as possible the tube is physically large and the deflector plates are placed as close together as possible, usually of the form shown in Fig. 6 to permit high deflection sensitivity to be achieved without the beam catching the actual deflector plates. If this occurs (for example if the timebase is overdriven to give X expansion) secondary emission occurs at the surface of the plates, and the low energy secondary electrons can be accelerated towards the screen causing flare and high background illumination. This undesirable

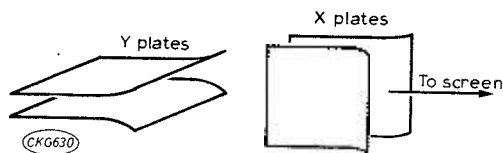
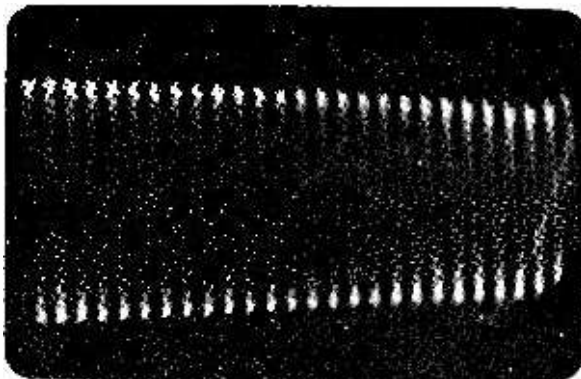


Fig. 6: Arrangement of the X and Y plates, the Y plates being nearer to the gun system.

effect can be avoided by coating the plates with a material of low secondary emission, or providing "beam catchers," small cups that accept the beam when driven off the screen. The X plates are usually mounted nearer to the tube face so that the Y plates have the maximum sensitivity.

To ensure that the electron beam does not become distorted in any way by extra acceleration due to the deflector plates they are arranged to be at the same potential as the final anode. Of course this is only true when the beam is travelling along the axis, but to prevent any gross errors on deflection it is common to provide symmetrical or push-pull deflection. This ensures that the mean electric field is not altered by deflection.



Trapezium distortion on a simple CRT operating with asymmetrical deflection on both axes. The focus and definition make this scope useful only for the simplest applications.

If the plates and final anode were at differing potentials then there would be a deformation of the circular cross-section of the beam (remember it is NOT in focus at this point, only at the screen where the cross-section area should be almost zero) by the plates attracting, or repelling, the outer electrons at opposite sides of the beam. This gives a sausage-shaped spot and the remedy is to make the final anode potential variable so that it may be matched to the Y plates. The X plates are then adjusted to be equal to the Y plate potential (as we shall see in a later section, it would be difficult to alter the Y plate potential). The control for setting the final anode volts is known as the "Astigmatism" potentiometer and is usually a front panel control.



The same CRT displaying a 1kHz square wave. Astigmatism is most noticeable as is the lack of HF response due to the simple deflection amplifier.

Another cause of incorrect spot size and shape is due to the pencil of electrons tending to spread, all being negatively charged. However, in high voltage tubes the velocity of the beam is high enough to keep the electrons in line by the magnetic field that they produce. The mechanism of electrostatic deflection relies on the electron beam being in the field of the deflector plates for a finite time. This means that when a very high frequency, say above 100MHz, signal is applied to the plates the signal may have changed before the electrons have emerged.

If, for example, a beam of electrons takes 10ns to travel through the plates a 100MHz signal will have completed one cycle and the deflection will be zero. In modern high velocity tubes the effect only occurs over 150 or 200MHz and the remedy is to arrange a series of deflectors, linked so that the velocity of the signal down the plates is the same as the velocity of the electron beam. However there are few uses for deflection amplifiers that can produce 200MHz output so this is of academic interest only.

THE FINAL ANODE

In order to produce the high velocity beams that are required to display fast transients, a high accelerating voltage is required. As we have seen, if this is applied to the final anode deflection sensitivity will be reduced so we apply the accelerating potential after deflection, called post deflection acceleration or PDA. Several methods of applying the PDA potential are used but they all aim at not reducing the deflection sensitivity, most important when the deflection amplifiers use transistors having only a limited output voltage swing.

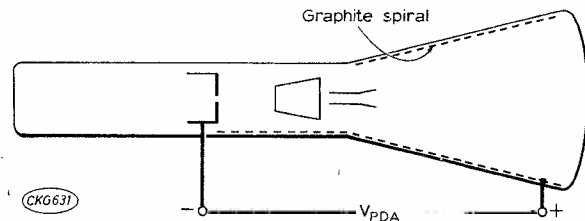


Fig. 7: Location of post deflection acceleration electrode in CRT.

The most popular form of PDA until a few years ago was the form shown in Fig. 7 and used in a lot of Cossor CRT's. The electron gun and tube are as they have been described so far and the beam is accelerated and deflected and focused normally. Around the inner wall of the tube is wound a resistive graphite spiral, connected to the final anode, and at the other end to a few kV positive. The beam is thus accelerated through this field to arrive at the screen with high velocity.

The screen tends to charge negatively at these high energies because more electrons are being gained than lost by secondary emission from the screen. The back of the phosphor is therefore given a very thin coating of aluminium and this conducts the charge to positive PDA, eliminating "screen sticking". This occurs where a local area of screen acquires a negative charge and tends to repel the beam, giving low light output. The aluminium also produces a more axial accelerating field giving better geometry and increased light output by reflecting the light forwards.

The field of the PDA is such as to produce a slightly convergent lens giving a smaller image and also, if it penetrates into the deflector plate region, causes acceleration before and during deflection, decreasing the scan even further. But in spite of this the PDA system offers a distinct advantage of increased trace brightness.

A fine wire mesh can be placed in the path of the beam just after deflection and if connected to the final anode acts as a screen to keep any PDA fields out of the deflection system. This arrangement gives rise to a PDA field that acts as a diverging lens, magnifying the deflection considerably, but also the spot size. Alternatively this mesh can be placed near the screen and PDA applied between the mesh and the screen. This gives very good results without affecting geometry but such tubes are prone to internal flashover.

SCREEN PHOSPHORS

The screen material or phosphor is arranged to give the highest possible light output of the correct colour and persistence. The table shows the range of phosphors used in cathode ray tubes, the most usual being P1 or P5, whilst P7 is sometimes used for medical applications.

Phosphor	Persistence	Fluorescence	Phosphorescence (Afterglow)	Uses
P1	Medium	Green	Green	Scopes (Visual)
P2	Long or Short	Blue/Green	Yellow/Green	Scopes (Visual)
P3	Medium	Yellow	Yellow	Television
P4	Medium	White	White	Scopes (Photography)
P5	Short	Blue	Blue	Television
P6	Medium	White	White	Television
P7	Long	Blue/White	Yellow	Radar
P8	Short	Blue/White	Yellow	
P9	Long	White	White	
P10	Permanent	Magenta	Magenta	Storage Tube
P11	Short	Blue	Blue/Green	Scopes (Photography)
P12	Long	Orange	Orange	Radar
P14	Long	White	Orange	Radar
P15	Short	Blue/Green	Blue/Green	Flying Spot Scanners
P19	Long	Orange	Orange	Radar

Table of phosphor types and principal applications.

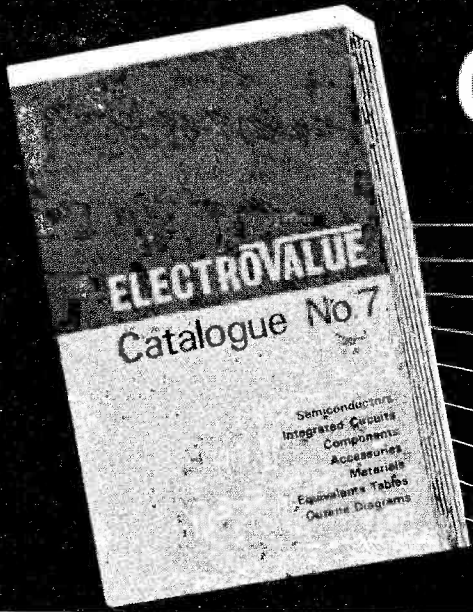
Although the trace produced on a tube can be intensely bright, even with only a couple of kV, the contrast between the trace and the background (grey/white) is usually quite small. A filter of about 65% transmission, of the colour of the trace, placed in front of the tube can increase the contrast by a large amount despite a decrease in light output.

GRATICULES

The graticule or measuring scale can be engraved on the filter or a better idea is to cut the graticule into a piece of perspex. If the markings are on the front, the observer can move so that the reflection of the line from the back surface of the graticule are in line with the actual lines. This ensures zero parallax when making measurements. The perspex can be lit from the side by a red bulb causing the cuts in the perspex to light up red, although white light is better for photography due to the uneven spectral response of films. Constructors making their own graticules out of perspex must bear in mind that the clearest line, especially with side illumination, is produced by cutting the perspex with a sharp knife and not by scratching.

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C	1	4-7-10M	3-2	2-5	1-9 nett
MO	1/2	10-1M	4	3-3	2-3 nett
WW	1	0-22-3-9	9	9	8
WW	3	1-10K	7	7	6
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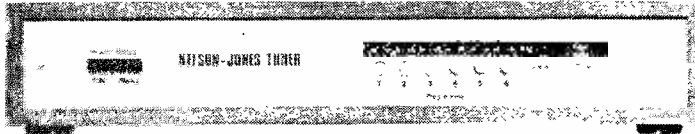
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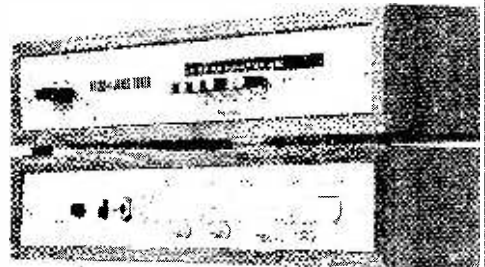
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PHOTOGRAPHY

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When using single lens reflex cameras, best suited to this type of work, it is important to remember that the image on the film is scanned from right to left (lens inversion) and the direction of motion of the blind could well be from left to right, giving a small vertical exposure if the scope sweep speed is slow. The average shutter takes 1/30 or 1/60 of a second to scan the film and so one must be aware of these difficulties when dealing with fairly slow sweep speeds at fast shutter speeds. For single shot photography it is best to have the shutter completely open before the appearance of the trace.

ABERRATIONS

The ideal characteristics of a cathode ray tube are not always realised in practice due to assumptions in the theory, or plain constructional error (anodes off axis, etc.). One of the most important flaws or "aberrations" is that known as "Astigmatism" and this has already been dealt with, together with its cure.

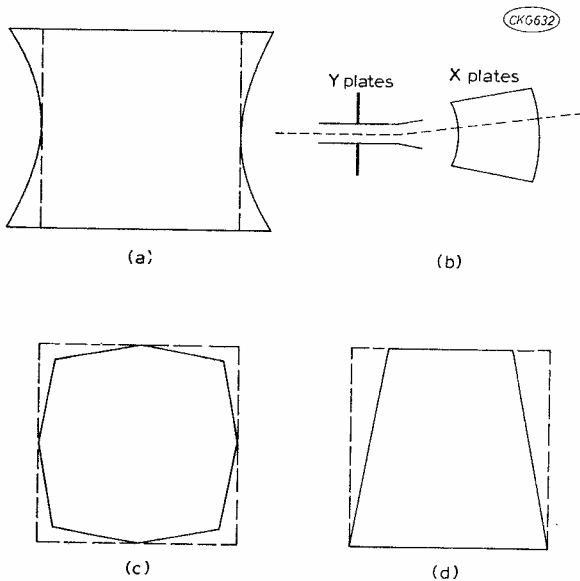


Fig. 8: Pin cushion distortion (a) can be corrected by shaping the plates as in (b). (c) illustrates barrel distortion and (d) trapezium distortion.

Most of the other aberrations are most apparent when the tube is displaying a raster. Ideally such a raster should be capable of being focused into a perfect square of scan lines, all in focus. Some defocusing occurs in deflections due to lens action between the final anode and plates, and between the plates. The effect between the plates is reduced by placing an "interplate shield" between the two sets of plates with a hole for the beam to pass through. This shield is at final anode potential and reduces the defocusing effects.

If the raster takes on the shape of Fig. 8a the distortion is known as pin-cushion distortion and is

caused by the deflected beam travelling through a greater distance between the second set of plates thus arriving at an oblique angle. This can be reduced by making the second pair of plates as in Fig. 8b. Fig. 8c shows barrel distortion caused by loss of extreme scanning sensitivity due to the PDA fields. This can only be reduced by careful design of the PDA spiral. Fig. 8d shows trapezium distortion. This is caused by asymmetrical Y deflection accelerating the beam as the driven Y plate goes positive and decreasing the X sensitivity accordingly. Specially designed plates are available for asymmetrical deflection only.

CRT DEFECTS

Other defects occur in specific tubes and it must be realised that any CRT is a compromise between conflicting factors. Consequently the best instrument tubes as fitted in laboratory scopes can cost several hundreds of pounds, but the home constructor can purchase surplus tubes for just a few pounds and many quite good home-made scopes have been built using these tubes.

With age or abuse cathode ray tubes tend to develop faults the most serious of which is likely to occur at virtually any time, is when the mechanical structure of the electron gun fails. The gun is constructed with tiny spot welds and severe shock or vibration can cause an element to be dislodged. If this happens the tube is almost surely destined for scrap.

Also linked to the mechanical structure of the tube is a fault producing what is known as a "soft" tube. This occurs when a small amount of air leaks into the bulb through an imperfect glass-to-metal seal. This may become evident only after many hours of operation and the symptoms are a diffuse display and a blue glow in the gun assembly. As the pressure inside the tube rises further, tracking occurs in the gun and external circuits can be damaged. In order to avoid this fault occurring it is necessary to take great care when handling the tube and making connections to it. Connections should never be soldered directly on to the tube pins as this is almost certain to break a seal or even crack the envelope, with glass flying everywhere at high velocity.

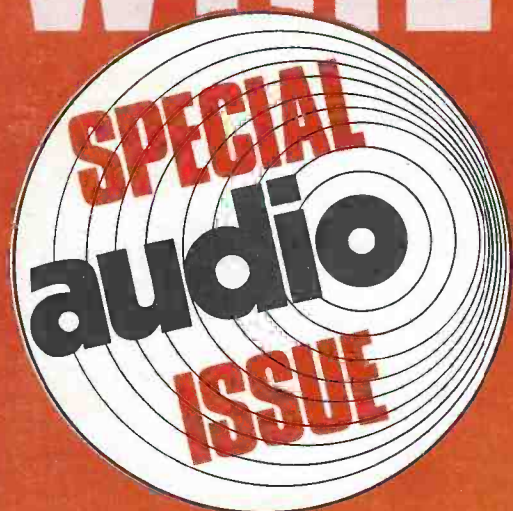
Perhaps the most common fault, linked directly to old age, is low cathode emission. The cathode surface loses emissivity either by the emissive layer evaporating or becoming poisoned by the remaining gas in the tube. The effect is that in order to see a trace at all the brightness control has to be advanced so far that the beam spot goes out of focus and silvery. The silvery effect is due to the cathode emitting in patches and on some scopes, if the focus control has sufficient range (making focus anode nearly the same potential as final anode), it is possible to produce an image of the cathode on the screen. The image looks a little like the full moon, the dark patches representing areas of low emission.

Sometimes a low emission tube can be improved by deflecting the spot off screen and turning brightness full up for a couple of hours. If this does not work a small transformer supplying 6.3V + 10% can be used to supply the heater (common practice in TV's). However the insulation of such transformers is doubtful over 1kV and a breakdown would make the tube heater/cathode short or damage it in an even worse manner. A small auto transformer is

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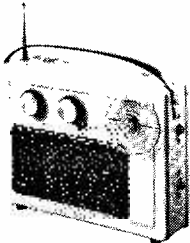
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WITH V.H.F. INCLUDING AIRCRAFT

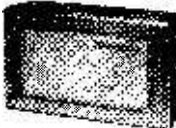


Nine Transistors, 9 Tunable wavebands as Roamer Ten. Built in ferrite rod aerial for MW/LW. Retractable chrome-plated telescopic aerial for VHF and SW. Push Pull output using 600mW transistors. 3 Transistors and 3 diodes, tuning condenser with V.H.F. section, separate coil for aircraft, moving coil loudspeaker, volume ON/OFF and wavechange controls. Attractive all white case with red grille and carrying strap. Size 9 1/2" x 7" x 2 1/4". Parts Price List and Plans 30p. (Free with parts).

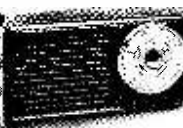
Total Building Costs £6-95 P P & Ins. 44p
(Overseas P & P £1-85)
(+ 8% VAT 55p)

POCKET FIVE

NOW WITH 3" LOUD-SPEAKER. 3 Tunable wavebands, M.W. L.W. and Trawler Band, 7 stages, 5 transistors and 2 diodes, supersensitive ferrite rod aerial, attractive black and gold case. Size 5 1/2" x 1 1/2" x 3 1/4" approx. Plans and Parts Price List 15p (Free with parts).



Total Building Costs £2-50 P P & Ins. 26p
(+ 8% VAT 20p)
(Overseas P & P £1-25)



TRANSONA FIVE

NOW WITH 3" LOUDSPEAKER. Wavebands, transistors and speaker as Pocket Five. Larger Case with Red Speaker Grille and Tuning Dial. Plans and Parts Price List 15p (Free with parts).

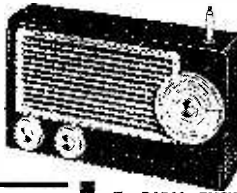
Total Building Costs £2-75 P P & Ins. 26p
(+ 8% VAT 21p)
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TRANS EIGHT

8 TRANSISTORS and 3 DIODES

6 Tunable Wavebands: MW, LW, SW1, SW2, SW3 and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves. 3in. Speaker. 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with polished metal inserts. Size 9 x 5 1/2 x 2 1/4in. approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and plans 25p (FREE with parts).

Total building costs £4-48 P P & Ins. 33p
(+ 8% VAT 36p)
(Overseas P & P £1-25)



ROAMER SIX

CASE AND LOOKS AS TRANS-EIGHT

6 Tunable Wavebands: MW, LW, SW1, SW2. Trawler band plus an extra Medium waveband for easier tuning of Luxembourg, etc. Sensitive ferrite rod aerial and telescopic aerial for Short Waves. 3in. Speaker 8 stages—6 transistors and 2 diodes. Attractive black case with red grille, dial and black knobs with polished metal inserts. Size 9 x 5 1/2 x 2 1/4in. approx. Plans and parts price list 25p (FREE with parts).

Total building costs £3-98 P P & Ins. 31p
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Total Building costs £2-95 P P & Ins. 30p
(+ 8% VAT 23p)
(Overseas P & P £1-25)

E.V.6. Case and looks as above. 6 Transistors and 3 diodes. Powered by 9 volt battery. Ferrite rod aerial, 3" loudspeaker, etc., MW/LW coverage. Push Pull output. Parts Price List and Plans 15p. Free with parts.

Total Building Costs £3-60 P P & Ins. 30p
(+ 8% VAT 29p)
(Overseas P & P £1-25)

E.V.7. Case and looks as above. 7 Transistors and 3 diodes. Six wavebands. MW/LW, Trawler Band, SW1, SW2, SW3, powered by 9 volt battery. Push Pull output. Telescopic aerial for short waves. 3" Loudspeaker. Parts Price List and Easy Build Plans 20p. Free with parts. Overseas P & P £1-05.

Total Building Costs £4-08 P P & Ins. 31p
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(+ 8% VAT 32p)

ROAMER EIGHT Mk I

NOW WITH VARIABLE TONE CONTROL

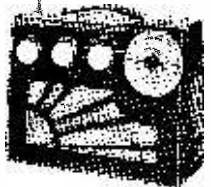
7 Tunable Wavebands: MW1, MW2, LW, SW1, SW2, SW3 and Trawler Band. Built in Ferrite Rod Aerial for MW and LW. Chrome plated Telescopic aerial can be angled and rotated for peak short wave listening. Push pull output using 600mW transistors. Car aerial and Tape record sockets. Selectivity switch. 3 transistors plus 3 diodes. Latest 4" 2 watt ferrite magnet loudspeaker. Air spaced ganged tuning condenser. Volume/on/off, tuning, wave change and tone control. Attractive case in rich chestnut shade with gold blocking. Size 9 x 7 x 4in. approx. Easy to follow instructions and diagrams. Parts price list and plans 25p (FREE with parts).

Total building costs £6-98 P P & Ins. 47p
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WITH VHF INCLUDING AIRCRAFT

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VOL. 50 NO. 7

ISSUE 813

NOVEMBER 1974

BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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We regret that we cannot answer technical queries by telephone nor can we provide information or advice on manufacturers' products other than that given in the magazine. We will endeavour to assist readers who have queries relating to articles published but we cannot offer advice on modifications to our published designs. All correspondents expecting a reply should enclose a stamped addressed envelope.

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STAFF CHANGES

Lionel Howes has been appointed Editor of Practical Wireless and of our associate magazine Television. Eric Dowdeswell has been appointed Assistant Editor of Practical Wireless.

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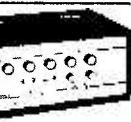
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As featured in the May 1973 issue of 'Practical Electronics', Superb Hi-Fi tuner Kit now available from Electro Spares. Including cabinet and all components - pre-set Mullard modules for R.F. and I.F. circuits. Motorola I.C. Phase Lock Loop Decoder for perfect stereo reception. No alignment needed. Guaranteed first time results - or send it back, and we'll return it in perfect order (for a nominal handling charge). Electro Spares price only £28.50 inc. VAT and p & p.

'GEMINI' STEREO AMPLIFIER

A superb unit with a guaranteed output of 30 watts RMS per channel into 8 ohms. Full power THD is a mere 0.02%, and frequency response is -3 dB from 20 Hz to 100 kHz into 8 or 15 ohms. Electro Spares have already sold 100s and 100s of these Kits. Get yours now! Depending on your choice of certain components, the price can vary from £50 to £60 inc. VAT and p & p.

- ★ All components as specified by original authors, and sold separately if you wish.
- ★ Full constructional data book with specification graphs, fault finding guides, etc. 55p plus 4p postage.
- ★ Price List only. Please send S.A.E. (preferably 9 x 4 minimum) for full details.

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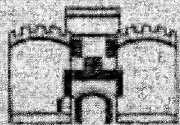
The Castle 8.RS.DD.



A highly sensitive, full range eight inch unit designed for use in the recommended cabinet, or one of similar dimension.

Suitable for use with good quality stereo installations, tape recorders, car radios, public address and background music systems, it has a frequency range of 50 to 20,000 kHz - the lower limit variable with increases in cabinet volume. Recommended retail price is £9.00 excluding VAT.

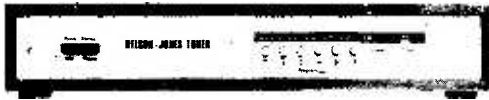
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THE NEW NELSON-JONES FM TUNER



PUSH-BUTTON VARICAP DIODE TUNING (6 Position)

('WW' JUNE '73)

Exclusive Designer Approved Kits

What are the important features to look for in an FM tuner kit? Naturally it must have an attractive appearance when built, but it must also embody the latest and best in circuit design such as:-

- MOSFET** front end for excellent cross modulation performance and low noise.
- 3 GANG** tuning for high selectivity.
- VARICAP** tuning diodes in back to back configuration for low distortion.
- CERAMIC** filters for defined IF response.
- INTEGRATED** circuit IF amplifiers for reliability and excellent limiting/AM rejection.

- PHASE LOCKED** Stereo decoder with Stereo mute, see below
- LED** fine tuning indicators.
- PUSH BUTTON** tuning (with AFC disable) over the FM band (88-104)
- IC STABILISED** and S/C protected power supply.
- CABINET** double veneered against warp.

The Nelson-Jones Tuner has all of these features and many more, and more importantly the design is fully proven not just with a few prototypes but with many thousands of working tuners spread across the world.

Typ. Specn: 20 dB quieting 0-75uV, Image rejection -70dB.I.F. Rejection -85 dB.

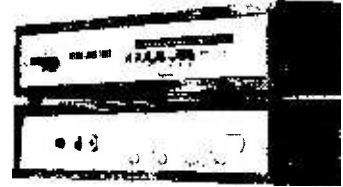
Basic tuner module prices start as low as **£12.31**, with complete kits starting at **£26.95** (mono) + P.P. 65p, and of course all components are available separately.

Our low cost alignment service is available to customers without access to a signal generator. Please send large SAE for our latest price lists which details all of the many options and special low prices for complete kits. All our other products remain available.

PORTANT AND HAYWOOD PHASE LOCKED DECODER (W.W. Sept. '70). Still the lowest distortion P.L. decoder available. THD typically 0.05% (at Nelson-Jones Tuner O/P level)! Supplied complete with Red LED.

Price **£7.02** when bought with a complete N-J tuner kit or **£8.29** if bought separately (P.P. 21p). **PLEASE NOTE.** Existing tuners are readily convertible and kits/parts are available for this purpose.

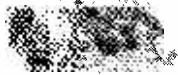
TEXAN AMPLIFIER. We have designed the tuner case and metalwork to match the Texan amplifier (see photograph). Complete designer approved Texan kits are available at **£30.78** plus P.P. 65p including Teak Sleeve.



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Available as basic or complete kits

Basic stereo tuner **£15** post free.
Basic mono tuner **£12** post free.
6 position push button units with integral pots **£2.92**.



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TYP. SPECIFICATION
2uV for 30dB S/N
Image rejection 40dB
IF rejection 65dB

PRICE Complete stereo kit £28.42
Complete mono kit £24.19
P. & P. 65p

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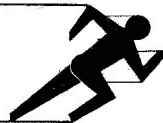
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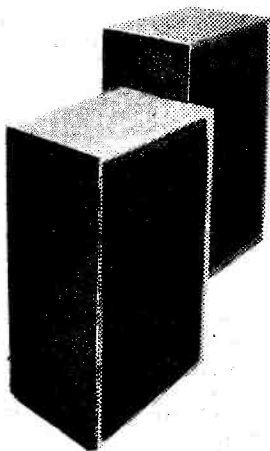
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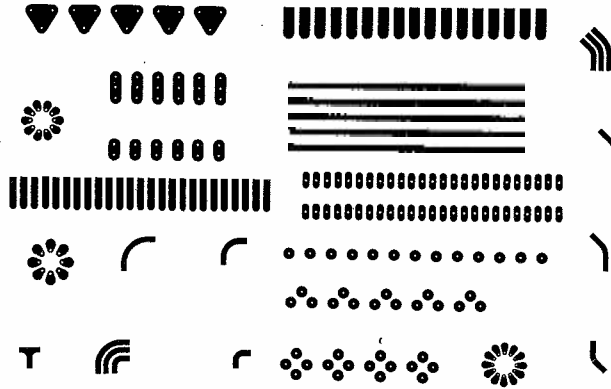
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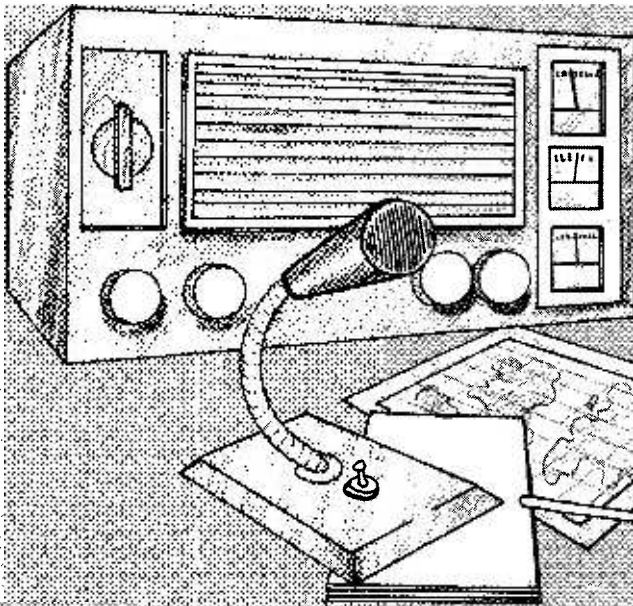
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Printed circuit board PCB transfer systems patent applied for.

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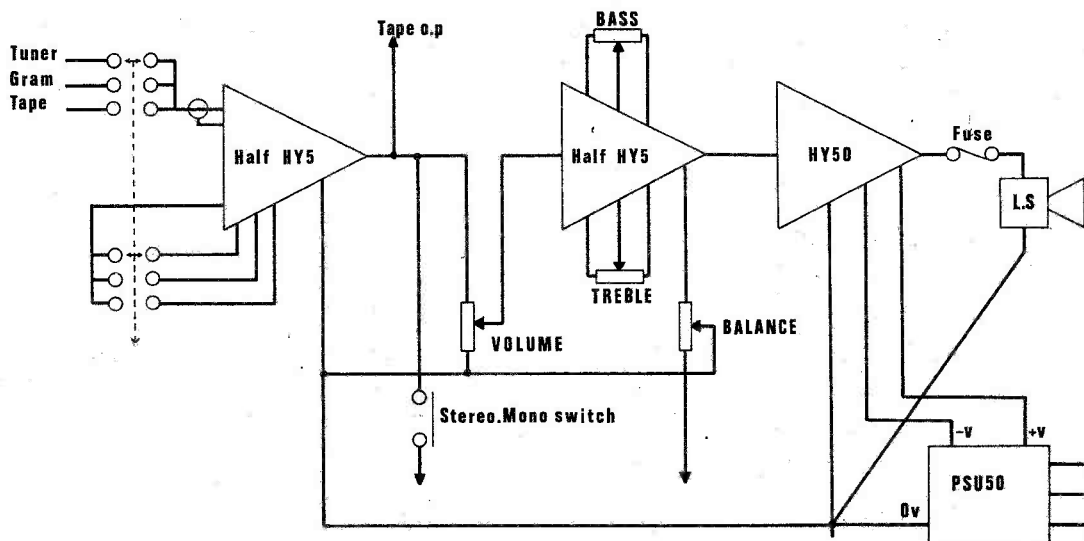
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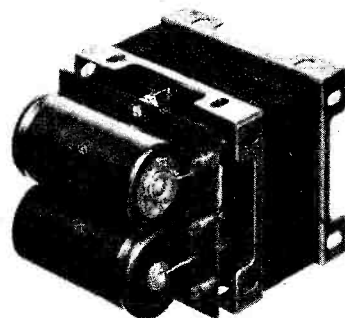
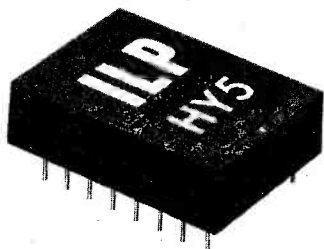


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The HY5 is a complete mono hybrid preamplifier, ideally suited for both mono and stereo applications. Internally the device consists of two high quality amplifiers—the first contains frequency equalisation and gain correction, while the second caters for tone control and balance.

TECHNICAL SPECIFICATION

Inputs: Magnetic Pick-up 3mV RIAA; Ceramic Pick-up 30mV; Microphone 10mV; Tuner 100mV; Auxiliary 3-100mV; Input Impedance 47k Ω at 1kHz. Outputs: Tape 100mV; Main output 0db (0.775V RMS). Active Tone Controls: Treble \pm 12db at 10kHz; Bass \pm 12db at 100Hz. Distortion: 0.5% at 1kHz. Signal/Noise Ratio: 68db. Overload Capability: 40db on most sensitive input. Supply Voltage: \pm 16-25V.

PRICE £4.50

- 36p VAT
P. & P. free

The HY50 is a complete solid state hybrid Hi-Fi amplifier incorporating its own high conductivity heatsink hermetically sealed in black epoxy resin. Only five connections are provided, input, output, power lines and earth.

TECHNICAL SPECIFICATION

Output Power: 25W RMS into 8k Ω . Load Impedance: 4-16k Ω . Input Sensitivity 0db (0.775V RMS). Input Impedance: 47k Ω . Distortion: Less than 0.1% at 25W typically 0.05%. Signal/Noise Ratio: Better than 75db. Frequency Response: 10Hz-50kHz \pm 3db. Supply Voltage: \pm 25V. Size: 105 x 50 x 25mm.

PRICE £5.98

- 48p VAT
P. & P. free

The PSU50 can be used for either mono or stereo systems.

TECHNICAL SPECIFICATIONS

Output voltage: 25V. Input voltage: 210-240V. Size: L. 70, D. 90, H. 60mm.

PRICE £5

- 40p VAT
P. & P. free

TWO YEARS' GUARANTEE ON ALL OUR PRODUCTS

CROSSLAND HOUSE · NACKINGTON · CANTERBURY · KENT

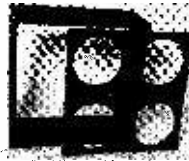
CANTERBURY (0227) 63218

CUSTOM CABINETS, 331 High Street, Rochester, Kent. Tel: Medway (0634) 404199

Speaker Cabinets in kit form represent HUGE SAVINGS



2' x 12" Cabinet



4' x 12" Cabinet



Disco Console (includes lid not shown)
Takes two slaves

For a long time now a large number of customers have asked us to produce cabinets in kit form, and above we show examples of cabinet styles and these are now available either fully built or in kit form ready for you to produce a professional finish in a very short time!

Kits are available in all specifications and all the kits contain everything you need as follows:-

- 1) 4 sides with handle cutouts, front edges rounded, 1 back with jack socket hole, and 1 baffleboard with speaker cutout
- 2) P.V.C. cut to size for frame and back, plus false front and back timbers, white front piping and speaker cloth
- 3) Recessed handles with fixing screws, jack socket, all fixing screws, corner plates, glue, and full instructions!

PRICE & TYPE LIST

Type	Size	Price manufactured	Kit price
2 x 12" (illustrated above)	36" x 18" x 13" x 3/4"	£19.50	£12.50
4 x 12" (illustrated above)	31" x 31" x 13" x 3/4"	£24.50	£17.50
4 x 12" P.A. Column	48" x 27" x 13" x 3/4"	£30.00	£21.50
1 x 18"	31" x 31" x 13" x 3/4"	£24.50	£17.50
1 x 15" with two top horn cutouts	36" x 20" x 13" x 3/4"	£21.00	£13.50
Mini Disco (state deck cutout BSR, GARRARD etc.)	33" x 20" x 10" x 1/2"	£20.00	£13.00
Maxi Disco (illustrated) (state deck cutout BSR, GARRARD etc.)	42" x 20" x 10" x 1/2"	£25.00	£18.50

Please ask for quotation on any other type or size of cabinet you may require.

ALL OUR PRICES INCLUDE VAT AND UK DELIVERY

PC ETCHING KIT

Contains 1lb Ferric Chloride, 100 sq. ins. copper-clad board, DALO etch-resistant pen, abrasive cleaner, etching dish & instructions, all for only £3.30

RESISTORS & CAPACITORS

500 assorted resistors £1.35. 2500 £4.70. 150 poly. ceramic, mica etc capacitors 80p.

VEROBOARD

100 sq. ins. assorted sizes and pitches (no tiny pieces) £1.10.

3W TAPE AMPLIFIERS

Polished wooden cabinet 14 x 13 x 9" containing a sensitive (20uV) 4 valve amplifier with tone & volume controls. Gives 3 watts output to the 7 x 4" 3Ω speaker. Also a non-standard tape deck. Supplied in good working condition with circuit. Standard mains operation. £4.50. Suitable cassette £1.10. Spare head 33p. Tape (ex-computer) 75p. Amplifier chassis only, complete and tested (2x ECC83, EL84, EZ80) and speaker £3.

VERSATILE POWER UNIT

Contains mains transformer, 2A thermal cut-out and bridge rectifier. Will give 1.7-10.5V output with 2 extra capacitors (supplied) £1.20. Also available as model garage with switch, lamp, jack plug etc. (Used for 'Hot Wheels') £1.70.

LEO III COMPUTER

Arriving late-October. All parts available, including 3000 reels tape, 1/2" decks, power units, etc.

All prices shown include 8% VAT and postage (mainland only) SAE list, enquiries.

GREENWELD ELECTRONICS (PW8)

Mail order dept., wholesale/retail shop 51 SHIRLEY PARK ROAD, SOUTHAMPTON. Tel 0703 772591. Other retail shops at 21 Deptford Broadway SE8, Tel 01-892 2009 and 38 Lower Addiscombe Road, Croydon. Callers Welcome.

FERRIC CHLORIDE

Anhydrous technical quality to Mill Spec in 1lb double sealed packs. 1lb 80p, 3lbs £1.65, 10lbs £4.45, 100lbs £35.

PO AMPLIFIER UNIT

Contained in steel case 5 1/2 x 5 x 3 1/2" are 2xGET118 transistors on heat sinks, 3 pot cores, 2 30V zeners, 4 audio transformers, 1% resistors & caps. With circuit diagram £1.

7lb BARGAIN PARCELS

Hundreds of new components—Pots, resistors, capacitors, switches, + PC boards with transistors and diodes, and loads of odds and ends. Amazing value at only £2.30.

COMPUTER PANELS

3lbs asstd £1.40, 7lbs £2.65, 56lbs £15. Pack containing 500 components with at least 50 transistors 95p, 12 High quality panels with power transistors, trim pots, IC's etc £2.50. Thousands of boards at shops for callers from 5p.

SLOT METER

Ex-Pay TV, takes 10p pieces, has 3 digit mechanical counter, coin counter, Sangamo-Weston impulse movement, nylon gearing, switch, etc. Only £1.20.

MISCELLANEOUS

Transformer, Mains pri 16-0-16V with 9V tap sec 1 1/2A £2. Post office 4 digit counters 60p. Balanced armature earpieces, use as mic or spkr 20Ω impedance 30p. 2N3055 35p. 80 + 80 + 20uF 350V 15p. 10 for £1.15. Multimeters: good range in stock from £3.50.

NEW

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ELECTRONIC IGNITION SYSTEM

This Capacitor-Discharge Electronic Ignition System was described in *Practical Wireless*, and has proved extremely popular.

The kit is supplied with a ready-drilled roller-tinned printed-circuit board and fully machined die-cast case with AMP Electrical Spade Connector Block together with a custom wound transformer, first grade components and full constructional details.

The original circuit employed Germanium Power Transistors for the negative earth version. WE OFFER SILICON P.N.P. POWER DEVICES AT NO EXTRA COST! All components are available separately. Case size 4 1/2" x 3 3/4" x 2". Complete assembly and construction manual free with kit, available separately 25p.

SUITABLE FOR 12V SYSTEMS WITH NEG. OR POS. EARTH.

PRICE: **£9-50** U.K. ORDERS PLEASE ADD VAT

Quantity Discounts:

Trade and Overseas	1-5 Nett	6-9 less 10%
Enquiries Invited	10-49 less 15%	50-99 less 20%
Mail Order Only.	100-999 less 25%	1000 up less 30%

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98 LICHFIELD STREET

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MAPLIN ELECTRONIC SUPPLIES

ORGAN BUILDERS

MES announce the very latest development in organ circuitry.

THE DMO2

13 Master Frequencies on ONE tiny circuit board. LOOK AT THESE AMAZING ADVANTAGES

- ★ 13 frequencies from C8 to C9. ★ Each frequency digitally derived from a SINGLE h.f. master oscillator.
- ★ Initial tuning for the WHOLE ORGAN: ONE SIMPLE ADJUSTMENT. ★ Relative tuning NEVER DRIFTS! ★ External control allows instant tune-up to other musicians. ★ Outputs will directly drive most types of dividers including the SAJ110. ★ And each output can also be used as a direct tone source. ★ Variable DEPTH AND RATE tremulant optional extra.
- ★ Gold-plated plug-in edge connexion. ★ Complete fibre glass board (including tremulant if required) ONLY 37in. x 4.5in. ★ Very low power consumption.
- ★ EXTREMELY ECONOMICAL PRICE. ★ Ready built, tested and fully guaranteed.
- DMO2T (with tremulant) ONLY £14.25.
- DMO2 (without tremulant) £12.25.

★ S.a.e. please for full technical details.

Trade enquiries welcome.

SAJ110 7-stage frequency divider in one 14 pin DIL package. Sine or square wave input allows operation from almost any type of master oscillator including the DMO2 (when 97 notes are available). Square wave outputs may be modified to saw-tooth by the addition of a few components. SAJ110: £2.03 each OR special price for pack of 12: £25.00. S.a.e. please for data sheet.

Keyboards: High quality adjustable type.

- Sloping front 49-note C to C **£14.35**
- Flat front 48-note F to E **£14.35**
- Contact Blocks GB2 (2 make contacts) **19p**
- Palladium earth bar per octave length **15p**
- Stop Tabs rocker type not engraved (white, red, grey or black) with DFDT switch **49p**

REVERBERATION UNIT

Enhances the sound of any electronic musical instrument. Ready built spring line driver module suitable for use with almost any spring line **£5.84**

Two types of spring line available:

- Short line **£3.05**
- Long line **£7.59**

S.a.e. please for details, leaflet MES 24

BASIC ORGAN CIRCUIT

Leaflet MES 51 shows complete circuit for a basic fully polyphonic organ. Send only 15p for leaflet and start building now! REMEMBER—when you have built this organ you will later be able to use the same top quality component parts as the basis of a large sophisticated instrument with all the facilities you want. Watch our ads for details.

★ SAME DAY SERVICE



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Model 120 all aluminium two part construction. Top and sides, blue hammer finish, front, rear and base: white. Others: mild steel three part construction.

Top, base, sides and detachable rear panel, blue hammer. Detachable aluminium front panel finished in white.

Model	W	H	D	Price
120	8	2 1/2	6	£2.87
220	8	6	3 1/2	£3.78
221	8	6	6	£4.07
320	12	8	12	£8.42

Chassis for model 320 £2.84 extra.

Please send s.a.e. for free illustrated leaflet.

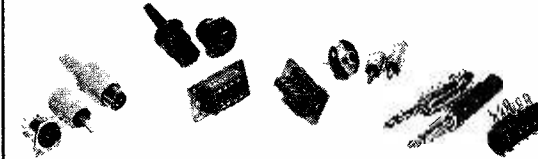
CAPACITORS

Sub-miniature Axial lead electrolytic

Mfd V Price	Mfd V Price
1 63 6p 68 6-3 6p	Mfd V Price
1 5 63 6p 68 16 6p	470 6-3 6p
2-2 63 6p 68 63 14p	470 10 14p
3-3 63 6p 100 10 6p	470 25 16p
4-7 63 6p 100 10 6p	470 40 25p
6-8 40 6p 100 25 6p	470 40 25p
6-8 63 6p 100 40 6p	680 6-3 14p
10 25 6p 100 63 16p	680 16 16p
10 63 6p 150 6-3 6p	680 25 25p
15 16 6p 150 16 6p	1000 4 14p
15 40 6p 150 25 6p	1000 10 16p
15 63 6p 150 40 14p	1000 16 25p
22 10 6p 150 63 16p	1000 25 25p
22 25 6p 220 4 6p	1500 6-3 16p
22 63 6p 220 10 6p	1500 10 25p
33 6-3 6p 220 16 6p	1500 16 25p
33 16 6p 220 25 14p	2200 6-3 25p
33 40 6p 220 40 16p	2200 10 28p
47 4 6p 220 63 25p	3300 6-3 28p
47 10 6p 330 4 6p	4700 4 28p
47 25 6p 330 10 6p	
47 40 6p 330 16 14p	
47 63 6p 330 63 28p	



PLUGS AND SOCKETS



- DIN PLUGS**
- 2 pin (1 flat) 8p
 - 3 pin 9p
 - 4 pin, 5 pin A 10p
 - 5 pin B (180°), 5 pin B (240°), 6 pin 10p
- MAINS**
- P360 3 pin 1-5A chassis plug with line socket. Per pair 28p
 - SA 2190 3 pin 5A chassis plug 26p
 - SA 1862 Line socket for above 28p
- DIN Sockets**
- 2 pin 6p
 - 3 pin, 4 pin, 5 pin A (180°), 5 pin B (240°), 7p, 6 pin 9p
- MCMURDO**
- RP8 8 way chassis plug 82p
- R88 8 way chassis socket 68p**
- 6td. 1" stereo plug Plastic 18p Screened 30p**
- PHONO**
- Open mono socket 1" 10p
 - Moulded mono socket 1" with 2 break contacts 14p
 - Moulded stereo socket 1" with 3 break contacts 18p
 - 3-5mm. plug plastic open socket 8p.
- JACK**
- Std. 1" mono plug Plastic 18p Screened 21p

WE KNOW YOU NEED IT!

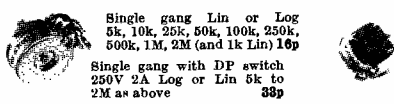


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POTENTIOMETERS

Rotary miniature carbon track 1" spindle.



- Single gang Lin or Log 5k, 10k, 25k, 50k, 100k, 250k, 500k, 1M, 2M (and 1k Lin) 16p
- Single gang with DP switch 250V 2A Log or Lin 5k to 2M as above 33p
- Dual gang (Stereo) without switch Log or Lin 5k to 2M as above 48p.

PRESETS
Sub-miniature 0-1W Vert or Horiz. 100, 250, 500, 1k, 2.5k, 5k, 10k, 25k, 50k, 100k, 250k, 500k, 1M 6p

NE555V 8-pin DIL 69p

RESISTORS

- Carbon Film 1W 5% 1Ω to 1M; 10% 1-2M to 10M E12 1p
 - Carbon Film 1W 5% 1Ω to 10k; 10% 1-2M to 10M E12 1p
 - Carbon Film 1W 5% 1Ω to 910k E12 & E24 1p
 - Carbon Film 1W 5% 10Ω to 10M E12 E24 4p
 - Metal Oxide 1W 2% 10Ω to 1M E12 & E24 4p
 - Wirewound 21W 10% 0-22ohms to 0-47ohms E12 14p
 - Wirewound 21W 5% 1ohm to 270ohms E12 12p
- E24 values 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and decades
E12 values 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 75, 91 and decades

LINEARS

- CA3046 LH0042C, TO99 (TO5), FET i/p Op Amp **24.25p**
 - LM301A. 8-pin DIL Op Amp **39p**
 - MC1303L. 14-pin DIL Stereo Preamplifier **£1.30p**
 - MC1310P. 14-pin DIL FM Stereo Decoder (no coils needed) **£3.15p**
 - MF060. electronic attenuator **£1.87p**
 - MF08010. 8-pin base, 1W Audio Power Amp **£1.30p**
 - MF04000B 1/2 watt Audio Amp **38p**
 - NE565V. 8-pin DIL Precision Timer **69p**
 - NE561B. 16-pin DIL Phase Locked Loop **£4.48p**
 - SG3402N Amplifier/Multiplier **£1.69p**
 - SG1455D. 14-pin DIL Four Quadrant Analogue Multiplier **£2.70p**
 - UA723C. TO99 (TO5), 2 to 37V Voltage Regulator **75p**
 - UA728C. 14-pin DIL, 2 to 37V Voltage Regulator **75p**
 - UA741C. 8-pin DIL Op Amp **39p**
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 - ZN414. TO5. TRF Radio **£1.20p**
- Full data, pin connexions, etc., on nearly all types listed in our catalogue. Price 25p

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- Rotary with adjustable 1 pole 2 to 12 way; 2 pole 2 to 6 way; 3 pole 2 to 4 way; 4 pole 2 or 3 way, each 38p.
Mains rotary DPST 250V 2A 20p
- Push to make non-locking 14p
 - Toggle 250V 1-5A with ON/OFF plate 25p.
 - High quality "sub-miniature" toggle switches
 - SPDT 1-5A 204V AC 56p
 - DPDT 1-5A 240V AC 75p
 - DPDT 3A 240V AC 77p
 - Four Pole DT 3A 240V AC **£1.87**
- Slide Sub-miniature DPDT 8p

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Our 80 page catalogue has over 20 pages showing connexion details and data for our complete range of transistors, diodes, IC's etc. + Over 100 Photographs + Over 100 line drawings. Seeing exactly what you're buying makes ordering so easy!

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750 VA Isolation Unit (Interwinding Screen) Housed in a tough Fibreglass case, with carrying handle. Complete with Heavy Duty 3 core power cable, splash proof outlet plug and socket, internal fuses 110 Volt and 240 Volt versions available. Price £26.50. Carriage £1.30

2" and 4" PANEL METERS

SIZE: 60mm Wide x 45mm High x 40mm Deep. Movement I.R.

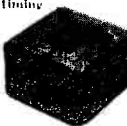
Table of meter specifications including micro A, mA, and Volt ranges for both 2" and 4" panels.

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1/2 watt CARBON FILM RESISTORS 1/2 watt at 70°C E 12 range 10Ω-1MΩ 5% tol above 470 KΩ 10% tol at 55p per 100.

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A reliable unit ideal for (Timing) Bathroom/Toilet Ventilators Stairway Cloakroom Lighting etc. Gives up to 30 mins delay before switching off. Delay 1-30 mins. adjustable. Max Load 400VA or 1000 watts resistive. White Case 3 1/2" x 3 1/2" x 2". Fitting instructions included. Trade Price £5.80. Post 30p.



MAINS KEYNECTOR

The safe, quick, connector for electrical appliances. 13 Amp rating, fused, will connect a number of appliances quickly and safely to the mains, ideal for timing, demonstrating, window displays, etc. Warning Light, interlocked to prevent connecting when live. Trade Price: £3.25. Post 25p.



TRANSFORMERS

SAFETY ISOLATING

Prim. 120/240V. Sec. 120/240V. Centre Tap with Screen.

Table of transformer specifications for safety isolating, listing VA, Ref. No., Price, Price Plugs, Price Open, and Post.

50 Volts

Prim. 200-240V. Sec. 19, 25, 33, 40, 50V.

Table of transformer specifications for 50 Volts, listing Amps, Ref. No., Price, and Post.

60 Volts

Prim. 230-240V. Sec. 24, 30, 40, 48, 60V.

Table of transformer specifications for 60 Volts, listing Amps, Ref. No., Price, and Post.

12 & 24 Volts Prim. 200-240V.

Table of transformer specifications for 12 & 24 Volts, listing Amps, Ref. No., Price, and Post.

30 Volts

Prim. 200-240V. Sec. 12, 15, 20, 24, 30V.

Table of transformer specifications for 30 Volts, listing Amps, Ref. No., Price, and Post.

MINIATURE AND EQUIPMENT

Prim. 240V with screen.

Table of miniature transformer specifications, listing Sec. 1, Sec. 2, Milliamps, Ref. No., Price, and Post.

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Table of rectifier specifications for One Amp, Two Amp, Four Amp, and Six Amp, listing P.I.V. and Price.

ADD 10p P & P PER ORDER

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Cased versions are 240 Volt Mains to 115 Volts, smart steel cased units coated in tough resin with power lead, fuse and 115 Volt American type socket up to 500VA, above 500VA cable entry.

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POWER UNIT Type CC 12-05

Output switched 3, 4, 5, 6, 7, 5 and 12 volts at 500 mA D.C. Operates from 240 V mains suitable for Radios, Tape Recorders, Record Players etc. Size 7.5 x 5.0 x 14.0cm. Price £3.85. Post 25p.



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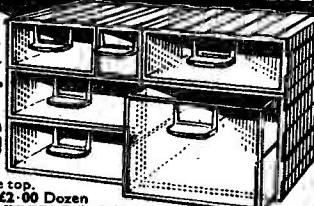
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BAKER 12 MAJOR £8.50

30-14,500 cps. Double cone woofer. Baker ceramic magnet 145,000 gauss. BASS RESONANCE 40 cps 20 watt RMS.

MAJOR MODULE KIT £10.95

30-17,000 cps. woofer, tweeter, crossover and baffle as illustrated. Size 19in x 12 1/2in.

NOTE—When ordering state 3, or 8 or 15 ohms.

BAKER LOUSPEAKERS 100% BRITISH MADE

Table of speaker specifications, listing Regent 12in, Deluxe 12in, Supert 12in, Group 25, Group 35, Group 50, and Group 60 prices.

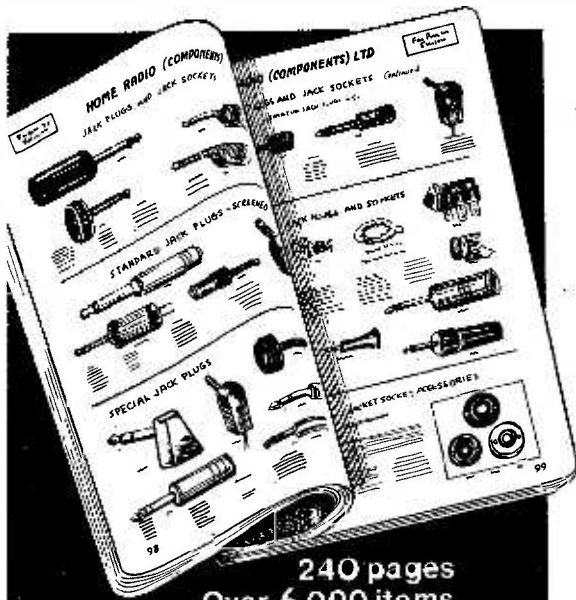
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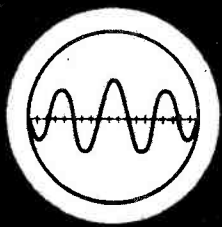
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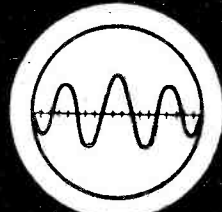
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TUAC



TRANSISTOR UNIVERSAL AMPLIFICATION CO. LTD.
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TUAC DISCOTHEQUE MIXER WITH AUTO FADE



Designed for the discerning D.J. of professional standard Offering a vast variety of functions. Controls; Mic Vol; Tone, over-ride depth; auto/Manual Sw; Tape Vol; L & R Deck Faders; Deck Volume; Treble and Bass; H. Phon Vol Selector; Master Vol On/Off Sw. Max output 1V RMS.

Specification. Deck Inputs—50mV into 1mΩ; Deck Tone Controls—Treble +28 - 15dB at 12kHz. Bass +22 - 15dB at 40Hz; Mic input—200 ohms upwards. 2mV into 10kΩ; Mic Tone Control—Total Variation Treble 15dB. Total Variation Bass 10dB; Tape input—30mV into 47kΩ; Power Requirements—30-45 volts at 100mA.

£26.50

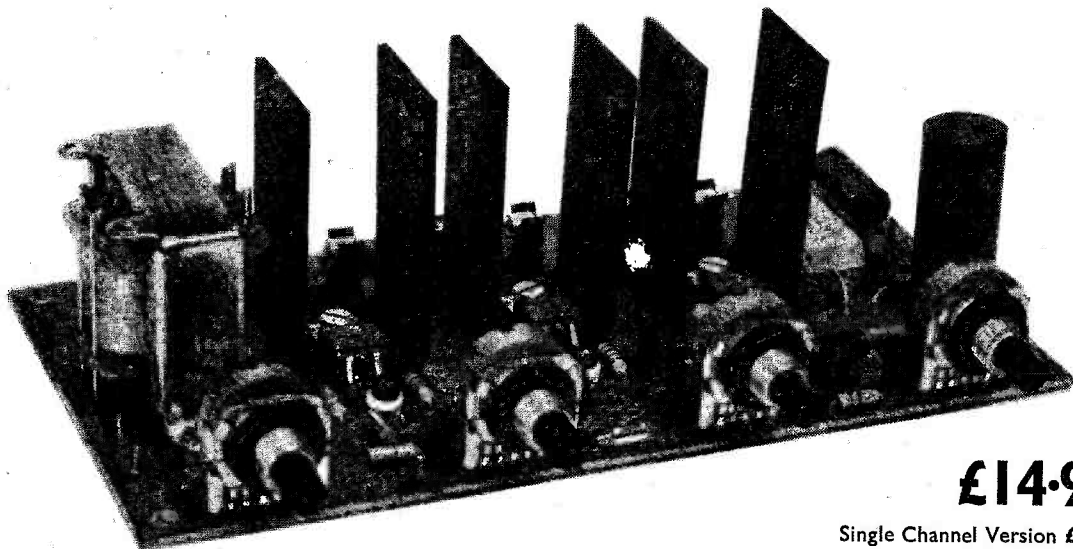
PANEL SIZE
18 × 4½ in.
DEPTH 3in.

TUAC MAIN DEALERS

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CALBARRIE AUDIO, 38 Cromwell Road, Luton Beds. Tel. Luton 411733.
SOCODI, 9 The Friars, Canterbury, Kent. Tel. Canterbury 60948.
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NEW! 3 CHANNEL LIGHT MODULATOR

- R.C.A. 8 Amp Triacs ● 1000W per channel ● Each channel fully suppressed and fused
- Master control to operate from 1W to 100W ● Full wave control—12 easy connections



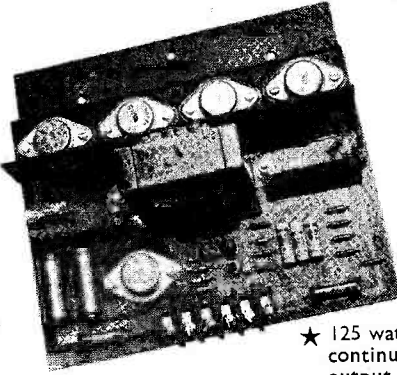
£14.90

Single Channel Version £6.60

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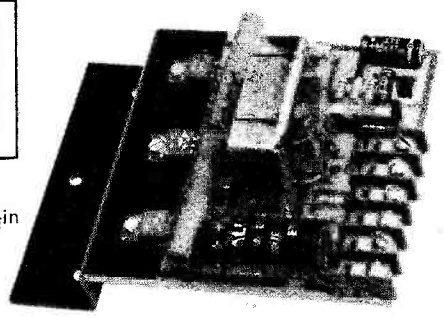


Specification on all power modules:
All output power ratings ± 0.5 dB;
Output impedance 8-15 ohms; THD at full power 2% typically 1%;
Input sensitivity 60mV into 10k Ω ;
Frequency response 20Hz-20kHz ± 2 dB; Hum and noise better than -70dB.

TP125
7 x 6½ x 3in
£17.00

- ★ 125 watts RMS continuous sine wave output

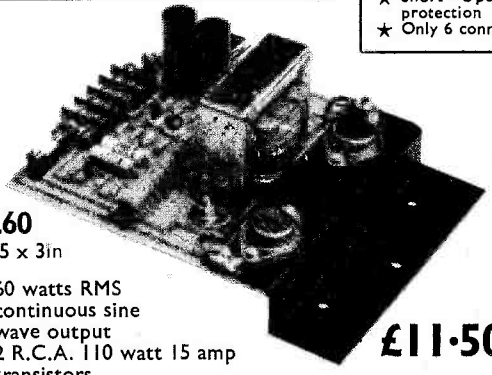
- ★ 4 R.C.A. 150 watt 15 amp output transistors



TL30
4 x 5¼ x 2½in
£9.30

- ★ 30 watts RMS continuous sine wave output
- ★ 2 R.C.A. 40 watt output transistor

- ★ Rugged layer wound driver transformer.
- ★ Short—Open—and Thermal overload protection
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TL60
5 x 5 x 3in

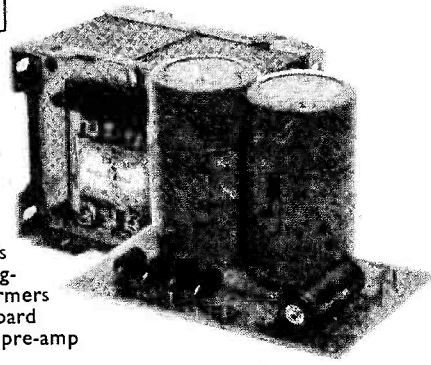
- ★ 60 watts RMS continuous sine wave output
- ★ 2 R.C.A. 110 watt 15 amp transistors

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TL100
5 x 5 x 3in

- ★ 100 watts R.M.S. continuous sine wave output
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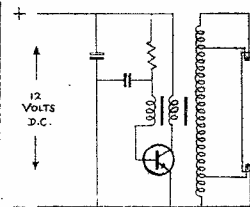
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H8/11	25µF	12V	4p
H8/12A	30µF	10V	4p
H8/13A	32µF	50V	4p
H8/14	40µF	25V	5p
H8/14A	40µF	16V	4p
H8/15A	40µF	35V	4p
H7/1A	50µF	10V	4p
H7/2A	64µF	2.5V	2p
H7/4	64µF	15V	4p
H7/9A	125µF	4V	4p
H7/10A	160µF	2.5V	3p
H7/11	160µF	25V	6p
H7/11A	150µF	16V	5p
H7/14	220µF	50V	10p
H7/14A	220µF	16V	6p
H7/15	220µF	25V	5p
H7/15A	220µF	35V	10p
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H6/4	320µF	10V	4p
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NAS0161X 100V	-26	NAS0651X 100V	-44	NAS1001X 100V	-60
NAS0162W 200V	-30	NAS0652W 200V	-58	NAS1002W 200V	-76
NAS0162X 200V	-28	NAS0652X 200V	-56	NAS1002X 200V	-74
NAS0164W 400V	-40	NAS0654W 400V	-84	NAS1004W 400V	-1-09
NAS0164X 400V	-38	NAS0654X 400V	-80	NAS1004X 400V	-1-04
NAS0166W 600V	-55	NAS0656W 600V	-1-05	NAS1006W 600V	-1-34
NAS0166X 600V	-52	NAS0656X 600V	-1-00	NAS1006X 600V	-1-28

Devices with Internal Trigger have "W" suffix. "X" denotes Standard Triac.

THYRISTORS

1-6 AMP MIN. TOS		4 AMP ISOLATED TAB		6 AMP ISOLATED TAB	
NAS006P	50PIV -25	NAS106P	50PIV -26	NAS206P	50PIV -37
NAS006Q	100PIV -28	NAS106Q	100PIV -30	NAS206Q	100PIV -42
NAS006R	200PIV -31	NAS106R	200PIV -36	NAS206R	100PIV -50
NAS006S	400PIV -40	NAS106S	400PIV -57	NAS206S	100PIV -77
NAS006T	600PIV -52				

8 AMP ISOLATED TAB		16 AMP ISOLATED TAB	
NAS306P	50PIV -41	NAS806P	50PIV -58
NAS306Q	100PIV -47	NAS806Q	100PIV -73
NAS306R	200PIV -58	NAS806R	200PIV -73
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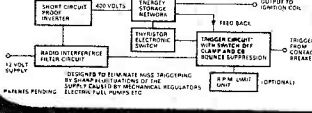
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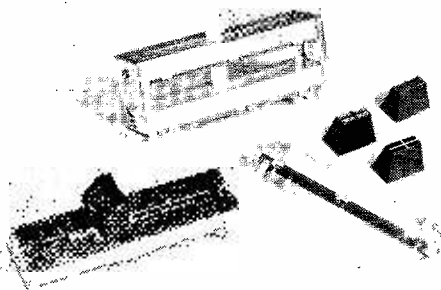
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EXHIBITIONS ?!

WHAT is happening to the R.S.G.B. National Mobile Rally? This annual event, as many readers will be aware, took place in the grounds of Woburn Abbey during the month of August.

It was not the day of continuous rain that made the exhibition part of the rally a wash-out—attendance was good despite the climatic conditions. Apathy on the part of the organisers and many exhibitors resulted in dismal displays on nameless stalls.

Who were these nameless exhibitors? These people were, in effect, representatives of one of our greatest national activities—Amateur radio and the amateur electronics constructor. The question being asked was, “surely this is not the R.S.G.B. National Mobile Rally? I must have taken the wrong turning!”

Exhibitors displaying new equipment and those displaying ‘surplus’ gear were intermixed. Yours truly spent a considerable amount of time trying to find the whereabouts of various exhibitors, without avail. Little information was forthcoming—even from the R.S.G.B. stand itself! Well-established and respected manufacturers and distributors were conspicuous—by their absence. Who can blame them?

Someone had better pull up their socks or we may see the rapid demise of what should be, as the title implies, our *National Mobile Rally*.

Do you remember the Radio Communications or Hobbies Exhibitions sponsored by the Radio Society of Great Britain? They were held annually in the London area and were extremely popular. What happened to them.

Practical Wireless and other major organisations, gave their support on numerous occasions and we are justly proud of the part that we contributed by showing our flag, on behalf of the radio and electronic constructor.

This hobby of ours encompasses an exceedingly wide sphere in the field of electronics and it is the responsibility of the Editor and his staff—as a team—to balance the editorial contents of each issue—to cater for many tastes. The satisfaction that the constructor derives from ‘switching it on’ is extremely gratifying and indeed therapeutic. We are indeed fortunate in that we live in an era of component plethora. Of course, there are shortages in many areas, but we suggest that the pessimists cast a careful eye over the pages of our *1974/5 PW Buyers' Guide to Radio and Electronic Components*.

Many new items are included, each month by advertisers in their respective columns. Take a good look at the small print, you could be pleasantly surprised!

We shall be exhibiting at the 1974 International Audio Festival and Fair, Olympia, London. Many *PW* constructional projects will be on show, including unique constructional designs not yet published in this country. A further exciting development in the *PW Tele-Tennis* constructional project will also be unveiled.

Members of the editorial and advertising departments will be in attendance to deal with enquiries. We shall also have a limited number of free ‘give-aways’ to visitors.

Don't forget the *PW* slogan—*Stay tuned to PW* for full coverage of the finest and up-to-the minute constructional projects.

A date for your diary—*Practical Wireless*, Stand B12, International Audio Festival & Fair, Olympia, 28th October—3rd November inclusive.

LIONEL E. HOWES—Editor.

NEWS...

Crofton move

CROFTON ELECTRONICS have moved. Their new address is: 124 Colne Road, Twickenham, Middlesex. (Tel: 898 1569).

A foolproof Electric Lock

SOME quite clever ideas have appeared in journals for electronic locks. But our vote goes to a professional approach recently announced which, as far as we can see, is almost fool-proof. The code for this lock is carefully stored in a CMOS shift register memory. When the “electronic” key is inserted, the code in the key is interrogated by the lock which compares it with the code in its memory. If the two codes are identical the lock will open. The key itself contains another shift register with the identical code in its memory banks. Even a small 32-bit memory would provide a possible four million combinations.

When the key is inserted into the lock it activates a micro-switch. This causes the lock to transmit a series of pulses which in turn make the “key” enter its code into the lock for comparison.

Because the key does not emit signals (i.e. magnetic or sonic or anything else) it is impossible to “read” the code from the key. Again, any exploratory signals sent into the lock would immediately alter or destroy its memory (fail safe).

One last cunning asset. The speed of operation of the memory circuits in the lock is fast when opening the door with the correct key. But slow by “logic” standards. If you were to permutate all combinations possible by plugging some sort of pulsing device into the lock instead of the key—it would take well over a year to run through all the possible combinations. Sorry—not available on the market yet and that's all the information we can get at present.

Not to be missed —

THE LATEST Heathkit Catalogue is now available free from: Heath (Gloucester) Limited, Bristol Road, Gloucester, GL2 6EE. Write, or phone Gloucester 29451, for a copy. Or if you happen to be in London or Gloucester, call in and collect one. The London Heathkit Centre is at 233 Tottenham Court Road, and the Gloucester showroom is next to the factory in Bristol Road.

The catalogue contains details of the very large range of electronic kits, many available for the first time in this country.

It talks in detail about kit building "The Heathkit Way" and shows how easy it is to build a Heathkit. Even a complete novice need have no worries as the instruction manual, with the aid of large pictorials and step-by-step instructions, leads you every step of the way.

Its 64 pages give details of many exciting models for home construction, ranging from a large selection of audio and Hi-Fi equipment through electronic calculators, digital electronic clocks, electronic thermometers, an ultrasonic burglar alarm, to test instruments for the electronic hobbyist and home car servicer. Even a 12 inch black and white portable television kit is available.

Heathkit's Catalogue

New kit models include an f.m. tuner with digital readout and computer tuner, a 4 channel SQ amplifier, a battery powered electronic thermometer and a de-luxe digital electronic clock with alarm. All models are available for cash or on extended credit terms through the very popular Heath Money Budget Plan. A free technical consultation service is in operation both before and after purchase.

You have been warned! Don't forget to order your copy of the December issue of *Practical Wireless* . . . look for your Free PW Miniature Screwdriver.

Start building the PW Kempton with our December issue. This is a quality stereo cassette player for your car; build yourself an inexpensive capacitance bridge that really works, and the third section of our 1974/5 PW Buyers Guide to Radio and Electronic Components will also be included in our December issue.

In the January 1975 issue of PW, we start the New Year with constructional series on radio control. Don't forget to place a permanent order with your newsagent, or write to our subscription department.

Further details of the December issue on page 609.

Hi-Fi Accessories by Bib

BIB HI-FI Accessories Limited announce the publication of a comprehensive 16-page full colour catalogue, which illustrates and describes their very large range of hi-fi accessories which now comprises more than 70 products.

The catalogue has been designed so that it can be easily reprinted in foreign languages and arrangements are already in hand to print it in French, German and Italian.

For the UK market a single sheet retail price list is inserted in the catalogue.

Bib Hi-Fi Accessories Ltd., PO Box 78, Hemel Hempstead, Herts, HP2 7EP.

Wolsey's Colour King at sea

WOLSEY ELECTRONICS equipment is now being increasingly used on marine installations and the most recent of these, through Aerialwork Limited of Southampton, their agents for Southern England, has been the installation of a communal TV and radio system to the officers and crews quarters on the car ferry "Eagle". In order to receive various transmitters whilst at sea, a Wolsey Broad Band "Colour King" u.h.f. aerial and FM411 array were erected with a rotator motor and remote control unit. The aeriels and mast were specially treated to withstand exposed sea conditions. The well-proved Wolsey "Mercury" amplifier was fitted and provision was made for a monochrome video cassette recorder and additional outlet points to public rooms should this be required at some future date.

The 11,500 ton "Eagle" which is controlled by one of the P & O Group of Companies—Southern Ferries—is the largest on/off car ferry to use the port of Southampton and operates a regular service to Lisbon, Algeciras and Tangier.

FM AERIAL pre-amplifier

KEITH CUMMINS

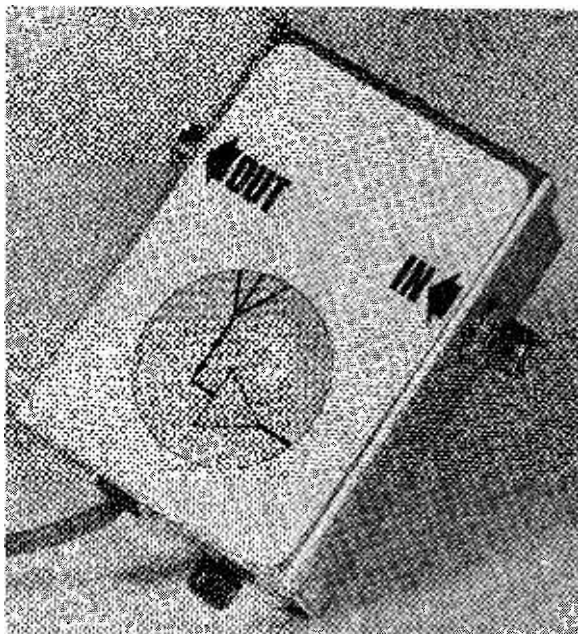
LONG-DISTANCE reception of weak FM signals is possible provided that a high gain aerial is used and that the receiver has high sensitivity. Some older types of receiver lack the sensitivity of their modern counterparts and the use of an aerial amplifier can improve reception considerably.

We have to be careful in the use of such an amplifier however, since high gain is not the only pre-requisite. If the amplifier adds as much noise as it increases the signal, then we are no better off. The amplifier must have a good noise factor, that is, it increases the signal by a much greater amount than it increases the noise.

Another aspect we have to consider is the type of reception we expect, having provided the amplifier. If the incoming signal is very weak indeed then we may be able to improve it, but if it fades away to nothing, no amount of amplification will bring it back again. This situation can exist during fading conditions, when total cancellation of the signal at the aerial occurs because of multipath reception. An amplifier can be useful, however, since it shortens the time during which the signal is unusable. Imagine a threshold level below which the signal must not fall if a satisfactory signal-to-noise ratio is to be maintained; if the amplifier lifts the entire incoming signal, this can fall to a lower level before becoming unsatisfactory.

CROSS MODULATION

The VHF FM band is becoming quite crowded and the weak signals we wish to amplify may be situated very close to a strong local transmission. Unless our amplifier is correctly designed, a strong possibility exists that cross-modulation will occur between the various signals present, due to the high amplitude of the local signals. The signals we wish to receive may then become completely lost in the mess which results. Once this has happened, it is impossible to



separate the signals again, so we must prevent such a thing happening in the first place.

Cross-modulation can not only occur in the amplifier but also in the input stages of the receiver. A valve receiver is far more tolerant of high input levels than its transistor counterpart. Too much amplification before the receiver's RF stage can therefore cause intermodulation and it will be seen that excessive gain can be a real disadvantage. Any aerial amplifier used for FM work should therefore not have so much gain that the local signals will cause cross modulation, have enough gain to substantially improve weak signals, and, itself, have

Fig. 1: The two FETs are connected in a cascode circuit, the first being an amplifier while the second is a buffer or isolating stage.

