MARCH 1974

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PRACTICA

VOL. 49 NO. 11 ISSUE 805 MARCH 1974

BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO, AND ELECTRONICS CONSTRUCTOR

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Price increase

IKE many other magazines and paper products "Practi-cal Wireless" has become victim of a world paper shortage resulting in massive increases in the cost of raw materials. In order to maintain the high standard of providing technical information and projects to our readers, we regret that we have been compelled to increase the cover price to 25p.

NEWS & COMMENT

1048 SAVE MONEY—Leader article and April preview

1049 NEWS...NEWS...NEWS...

1061 TELEVISION—Coming in the March issue

1062 PRODUCTION LINES—Products reviewed by Colin Riches

1071 NEXT MONTH IN PRACTICAL WIRELESS

1081 HOTLINES on recent developments by Ginsberg

1097 ON THE AIR

1097 Broadcast Short Wave-Malcolm Connah

1098

VHF/FM—Simon David

1098

Medium Wave-Charles Molloy

1101 Amateur Bands, Short Wave/VHF—David Gibson G3JDG

CONSTRUCTIONAL

1050 VERSATILE WAVEFORM GENERATOR-J. B. Dance, M.Sc.

1058 DRY BATTERY CHARGER-R. A. Butterworth

1065 I.C. CRYSTAL HARMONIC CALIBRATOR—J. Andrews

1070 FLUORESCENT LAMP UNIT-from your 12V battery-Paul Cooper

1072 "P.W. CRATA" Cassette Recorder and Tuner Amplifier-Richard Collin

1085 PRESELECTOR FOR 10-30MHz-F. G. Rayer, G3OGR

1094 TAKE 20 No. 58 GRIP TESTER—David Andrews

OTHER FEATURES

1080 TECHNICROSS No. 3

1082 IC of the MONTH-LM377N 2 + 2W Audio Amplifier-M. J. Darby

1087 RADIO BY CABLE & SATELLITE

1088 OSCILLOSCOPE TECHNIQUES PART 1-Alan C. Ainslie

EXTRA WITH THIS ISSUE

INSET P. W. DATACARDS in COLOUR

No. 7 F.M. Aerial Systems

No. 8 BBC VHF Radio Stations.

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Prices are those current as we go to press. We regret that we cannot answer technical queries by telephone nor can we provide information or advice on manufacturers' products other than that given in the magazine. We will endeavour to assist readers who have queries relating to articles published but we cannot offer advice on modifications to our published designs. All correspondents expecting a reply should enclose a stamped addressed envelope.

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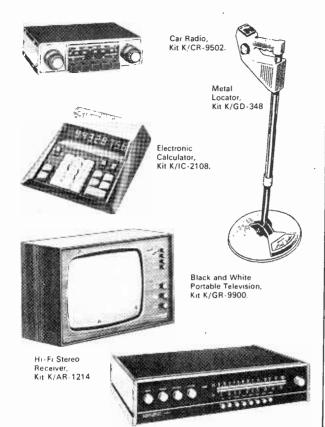
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	AUTO TRANSFORMERS												
Ref.	VA	Wei	ight			Size					Taps	P	& P
No.	(Wotts)	16	oz				-				·upi	5	
113	20	-	0	5.8		5-1	v	4.5	0-115	210-	240	1 . 22	22 22
64	75	2	4	7.4		6.7	Ŷ	6.1	0-115	210-	240	2.40	30
4	150	3	4	8.9	ċ	7.7	×	7.7	0-115	200-	220-240		36
66	300	6	4	9.9	Ċ	9.6	×	8.6			110-1-10	5.63	52
67	500	12	8	12:15								8.36	67
84	1000	19	8	14.0							***	15-19	82
93	1500	30	4	14-0 3							**	21.99	02
95	2000	32	0	17-2 3							14	28.70	-
73	3000	40	Ó	21.6								39.17	
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					30	VOLI	KANGE		
Ref.	Amps.	Weigh	t	Size on	٦.	Secondo	ry Taps	P	8 P
No.		lb oz						£	Þ
112	0.5	1 4	6-1 x	5.8 x	4.B 0	-12-15-2	0-24-30V	1.42	22
79	1.0	2 4	7·0 x	6.7 x	6-1	11	**	1.92	36
3	2.0	3 4	8.9 x	7.7 x	7.7			2.90	36
20	3.0	4 8	9.9 x	8-3 ×	8.6			3-58	42
21	4.0	6 4	9.9 x	9.6 x		**		4.25	52
51	5.0	6 12	12·1 x	8.6 x			**		
						1.51	11	5.30	52
117	6.0	8 0	12·1 x	9·3 x				6.31	52
88	8.0	12 0	12:1 x	11.8 x	10.2		**	8-18	67
89	19.0	13 12	14.0 x	10.2 x	11.8	- 11	- 10	10.33	67
					-				•
						0 7 (3)	FRANG	E	

				JU VOLI KANGI	-
Ref.	Amps.	Weight	Size cm.	Secondary Tabs	P & P
No.		lb oz		1 1	€ 0
102	0.5	1 12	7.0 x 6.4 x	6 I 0-19-25-33-40-50V	1.90 30
103	1.0	2 12	8-3 x 7-4 x	7.0 ,, ,,	2.80 36
104	2.0	5 8	9.9 x 8.9 x	8.6	3.87 42
105	3.0	6 12	9-9 x 10-2 x	8.6	5.26 52
106	4-0	10 0	12·1 x 10·5 x	10.3	6.99 52
107	6.0		14·0 x 10·2 x	11.9	10.35 67
118	8.0		140 x 127 x	11.9	13.51 97
119	10.0	25 0	17·2 x 12·7 x	14.0	16.93 *
				60 VOLT RANGE	
				OF THE RAINGE	

wet.	Amps.		16 .	SIZE CII	1.	seconaa	iry laps		& P
No.		lb oz						€	P
124	0.5	2 4	7.0		x 6.1	0-24-30-4	40-428-6	59C 1-93	36
126	1.0	3 4	8.9	x 7.7	x 7.7	111		2.70	36
127	2.0	6 4	9.9					4.25	42
125	3.0	8 12	12-1	x 9.9	x 10·2		44	6.46	52
123	4-0	13 12	12-1	8-11 x	x 10.2			8.36	67
40	5.0	12 00	14.0:	x 10 · 2 :	× 11 · 8			9 85	87
120	6.0	15 8	14.0	x 12·1	x 11.8			12:14	82
121	8.0	25 00	14.0:	(14.7)	k 11 · 8	17		13.65	
122	10.0	25 0	17-2:	x 12.7	x 14·0			20.09	
189	12.0	29 00	17-2	(14·0)	c 14 · 0		**	22.49	

	MINIATU) RE	TP	RANSFORME	RS WITH SCRE	ENSP	& P
Ref.	MA.	We	eight		VOLTS		Р.
238	200		2	2 8x2 6x2 0	3-0-3	1-31	10
212	IA IA	- 1	4	6 · 1x5 · 8x4 · 8	0-6 0-6	1.52	22
13	100		4	3 9x2 6x2 9	9-0-9	1-12	ĪŌ
235	330,330		4	4-8x2-9x3-5	0-9. 0-9	1.52	10
207	500, 500	- 1	00	6 · 1x5 · 4x4 · 8	0-8-9, 0-8-9	2.03	22
208	IA, IA	- 1	12	7 · 0×6 · 4×6 · I	0-8-9.0-8-9	2.73	30
236	200, 200		4	4 · 8×2 · 9×3 · 5	0-15, 0-15	Ī-52	10
214	300, 300	- 1	4	6-1x5-8x4-8	0-20, 0-20	1.60	22
221	700 (D.C.)	- 1	8	7 · 0×6 · 1×6 · 1	20-12-0-12-20	i 4i	30
206	IA, IA	2	12	8 · 3×7 · 7×7 · 0	0-15-20, 0-15-20	3.08	36
203	500, 500	2	4	8 · 3×7 · 0×7 · 0	0-15-27, 0-15-27	2.82	38
204	IA, IA	3	4	8 · 9×7 · 7×7 · 7	0-15-27, 0-15-27	2.86	38
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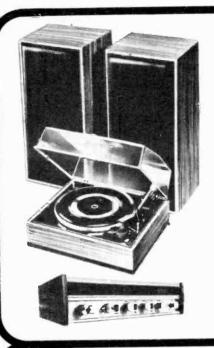
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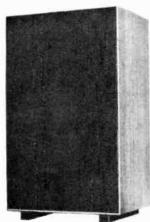
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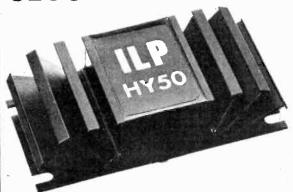
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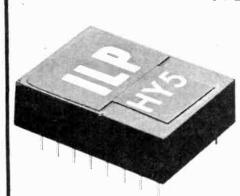
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8N7420N 0 20 0 18 0 16	8N7493N 0.75 0.70 0.63	8N74173N 1 66 1 66 1 45
8N7422N 0 28 0 28 0 25	8N7494N 0.85 0.80 0.75	8N74174N 1 80 1 80 1 57
SN7422AN 0-38 0-38 0-33	8N7495N 0.85 0.80 0.75	8N74175N 1 29 1 29 1 13
8N7423N 0 37 0 34 0 32	8N7496N 1 00 0 90 0 83	8N74176N 1 44 1 44 1 26
8N7425N 0.37 0.37 0.32	SN74100N 2-16 1-89 1-89	8N74177N 1 44 1 44 1 26
8N7427N 0.37 0.37 0.32	8N74104N 0-60 0-53 0-45	8N74180N 1-44 1-44 1-26
SN7428N 0-43 0-43 0-37	SN74105N 0-60 0-53 0-45	BN74181N 5 18 5 18 4 53
8N7430N 0 20 0 18 0 16	8N74107N 0.51 0.51 0.45	BN74182N 1 44 1 44 1 26
8N7432N 0-37 0-37 0-32	SN74110N 0-57 0-57 0-50	8N74184N 2-16 2-16 1-89
8N7433N 0-43 0-43 0 38	BN74111N 0-86 0-86 0-75	8N74185AN
BN7433AN 0-57 0-57 0-50	SN74116N 2-16 2-16 1-89	2 16 2 16 1 89
SN7437N 0 43 0 43 0 37	8N74118N 1 00 0 90 0 83	BN74188N 6 48 6 48 5 67
SN7438N 0 43 0 43 0 37	SN74119N 1 92 1 92 1 68	8N74190N 2 30 2 30 2 01
SN7438AN 0 - 57 0 - 57 0 - 50	8N74120N 1-05 1-05 0-92	8N74191N 2 30 2 30 2 01
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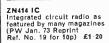
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	ACY17	35p	BCY70	16p	GET115 75p	OC72	25p		40p	2N3819	25p
	ACY39	65p	BCY71	20p	GET880 55p	OC77	55p	2N697	15p	2N3866	75p
	AD149	50p	BCY72	13p	LM309K	OC81	28p	2N706	10p	2N3903	
ĺ	AD161	89p	BD124	80p	1.87	OC83	25p	2N930	20p	2N 4002	14p
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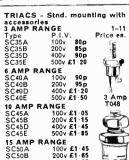
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B05/60	600v	27p	
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	.I.V.		21
B1/05 B1/10	50 v 100 v	25p 25p	
B1/20	200v	28 p	_
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₹H x ₹F x ⅓			
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W01	100v	30 p	100
W02	200v	32p	1111
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2 AMPS F			1 1
B2/05	50v	35 p	
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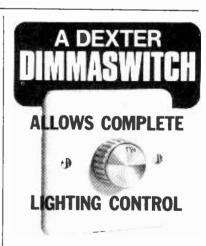
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C	1/3	4 · 7 – 470K	1 · 3	1:1	0 · 9 nett		
ř	1/2	4 · 7-10M	1 - 3	1:1	0 · 9 nett		
č	3/4	4 · 7~10M	1 - 5	1 2	0 9 nett		
č	1	4 · 7-10M	3 . 2	2 - 5	1 · 9 nett		
мo	1/2	10-1M	4	3 - 3	2·3 nett		
ww	1	0 - 22 - 3 - 9	9	9	8		
ww	3	1-10K	7	7	6		
ww	7	1-10K	9	9	8 nett		

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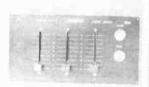
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Nine Transistors, 9 Tuneable wavebands as Roamer Ten Built in ferrite rod aerial for MW/LW. Retractable chrone-plated telescopic aerial for TWF and SW. Push Pull output using 600 mW transistors, 9 Transistors and 3 diodes, tuning condenser with V.H.P. section, separate coil for aircraft, moving coil loudspeaker, volume ON/OFF and wavechange controls Attractive all white case with red grille and carrying strap, Size 91" × 7" × 21" approx. Parts Price List and Plans 30p (Free with parts).

Total Building Costs

£6.95

P P & Ins. 44p (Overseas P & P £1-85)

POCKET FIVE

3 Tunable wavebands, M.W. L.W. and Trawler Band, 7 stages, 5 transistors and 2 dinder supercondition 7 stages, b transmors and 2 diodes, supersensitive ferrite rod aerial, moving coil Total Building Costs loudspeaker, attractive black and gold case. Size 54" x 14" x 22 28 P. P. and 23" approx. Plans and Parts Price List 15p (Free with parts). (+10° vAT 22p)



£2-28 Ins. 26p (+10% VAT 22p) (Overseas P & P £1.25)



Total Building Costs £2·50 PP&Ins. **TRANSONA** FIVE

Wavebands, transistors and speaker as Pocket Five. Larger Case with Red Speaker Grille and Tuning Dial. Plans and Parts . Plans and Parts e List 15p (Free with

+10% VAT 25p) (Overseas P & P £1.25)

TRANS EIGHT 8 TRANSISTORS and 3 DIODES

6 Tunable Wavebands: MW, LW, 8W1, 8W2, SW3 and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves. Sin. Speaker. 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black kinds with polished metal inserts. Size 9 × 51 × 2½in. approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and plans 25p (FREE with parts).

EDU-KIT

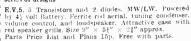
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- * 3 Transistor Regenerative
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- * Sensitive Pre-Amplifler

Components Include: 24 Resistors ● 21 Capacitors ● 10 Transistors ● 3¼" Loudspeaker ● Earpiece ● Mica Baseboard ● 3 12-way connectors ● 2 Volume controls ● 2 Slider Switches ● 1 Tuning Condenser ● 3 Knobs ● Ready Wound MW/LW/SW Coils ● Ferrite Rod ● 6½ yards of wire ● 1 Yard of sleeving etc. ● Parts Price List and Plans 50p. (Free with parts).

NEW Everyday Series

Build this exciting New series of designs



Total Building **£2.73** P. P. & Ins. 30p (+ 10% VAT 27p) (Overseas P. & P. £1-25)

E.V.6. Case and looks as above. 6 Transistors and 3 diodes. Powered by 9 volt battery. Ferrite rod aerial, 3" loudspeaker, etc., MW/LW coverage. Push Pull output. Parts Price List and Plans 15p. Free with parts.

Total Building **£3.60** P. P. & Ins. 30p (+ 10% VAT 36p) (Overseas P. & P. £1.25)

E.V.7. Case and looks as above. 7 Transistors and 3 diodes. Six wavehands. MW/LW, Trawler Band. SW1. SW2. SW2. SW2. powered by 9 volt battery. Push Pull output. Telescopic aerial for short waves. 3" Loudspeaker. Parts Price List and Easy Build Plans 20p. Free with parts. Overseas P & P £1.05.

Total **£4-08**

P P & Ins. 31p Overseas P & P £1:85 (+ 10% VAT 40p)

ROAMER EIGHT Mk I

NOW WITH VARIABLE TONE CONTROL

TONE CONTROL

7 Tunable Wavebands: MWI,
MW2, LW, SW1, SW2, SW3
and Travier Band. Built in
Perrite Rod Aerial for MW and
LW. Retractable chronic blated Telescopic aerial for
Short Waves. Push pull output using 600mW transistors.
Car aerial and Tape record sockets. Selectivity switch.
Stransistors plus 3 diodes. Latest 472 wat territe magnet
loudspeaker. Air spaced ganged tuning condenser. Volumej
on/foff, tuning, wave change and tone controls. Attractive
case in rich chesinut shade with gold blocking. Size 9 x 7 x
4 in. approx. Easy to follow instructions and diagrams.
Parts price list and plans 25p (FREE with parts).

Total building costs Overseas P & P £1-85) **26-98** P P & Ins. 47p (+ 10% VAT 69p)

ROAMER TEN

WITH VHF INCLUD-ING AIRCRAFT

10 Transistors, Latest 4 2 watt Ferrite Magnet Loudspeakers. Loudspeakers.

9 Tunable Wavebands,

MW1, MW2, LW, SW1.

SW2, SW3, Trawler

Band, VHF and Local

Stations also Aircraft Band.

Built in Ferrite Rod Aerial for MW/LW. Retractable, chrone plated 7 section Telescopic Aerial, can be angled and rotated for peak short wave and VHF listening. Push Pull output using 600mW Transistors, Car Aerial and Tape Record Bockets. 10 Transistors plus 3 Diodes. Ganged Tuning Condenser with VHF section. Separatic coil for Aircraft Band. Volume on/off. Wave Change and tone Controls. Attractive Case in black with silver blocking. Size 9" × 7" × 4". Easy to follow instructions and diagrams. Parts urise int and plane 300. (FEEE with ing. Size $9'' \times 7'' \times 4''$. Easy to follow instructions and diagrams. Parts price list and plans 30p (FREE with

Total building costs (Overseas P & P £1-85)

£8.20

(+ 10% VAT 85p)



Components include:

Components include:
Tuning Condenser: 2 Volume Controls; 2 Slider Switchest
Pine Tone 3" Moving Coil Speaker: Terminal Strip: Ferrite
Rod Aerial: 2 Plugs and Sockets: Battery Clips: 4 Tag
Roards: 10 Transistors: 4 Biodes: Resistors: Capacitors:
Three 3" Knobs. Units once constructed are detachable
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ROA	MER	SIX
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CASE AND LOOKS AS TRANS-EIGHT

Trawler band plus an extra Medium waveband for easier tuning of Luxembourg, etc. Sensitive ferrite rod aerial and telescopic aerial for 8bort Waves. 3in. Speaks 8 stages—6 translistors and 2 diodes. Attractive black case with red grille, dial and black knobs with polished metal inserts. Size 9 × 5 ½ × 2jin. approx. Plans and parts price list 25p (FREE with parts).

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and 20mm. 100mA, 200mA, 250mA 500mA, 1A, 1.5A, 2A QUICK-BLOW 4p ea, ANTI-SURGE 5p ea,

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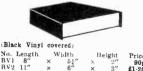
K 4007, 80 ohms Imp. Insertion loss 3:1B £1-21

CAR STEREO SPEAKERS Angied) £3.85 per pair.

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BAl	51"	×	23"	×	11"	42p
BA2	4"	×	4"	×	11"	41p
BA3	4"	×	29"	×	11"	41p
BA4	51"	×	4"	×	14"	47p
BA5	4"	×	21"	×	2"	41p
BA6	3"	×	2"	×	1"	34p
BA7	7"	×	5"	×	21"	66p
BA8	8"	×	6"	×	3"	84p
BA9	6"	×	4"	×	2"	54p

BIB HI-FI ACCESSORIES

De Luxe Groov-Kleen Model 42 £1-84

Ref. 32. Tape editing Kit £1-54



SOCKETS

PS 38 DIN

PS 40

PS 41

PS 42

P8 43

PS 44

PS 45

PS 47

P8 99

PS 23

PS 24

PS 25

PS 26

PS 27

PS 29

PS 30

PS 31

PS 32

PS 33

P9

PS

P8

P8

P8

PS

PS 9

PS 10

PS 11

PS 12

PS 13

PS 14

CP 1

3

CP

CP

CP

CP

CP

CP CP 8

CP

CP 10

PLUGS

PS 36 DIN 3 Pin

PS 37 DIN 5 Pin 180°

Ref. J. Tape Head Cleaning Kit 61p

PLUGS AND SOCKETS

5 Pin 9409

Jack 2-5mm Switched

Jack 3-5mm Switched

Jack Stereo Switched

Jack 1" Switched

Phono Single

Co-Axial Surface

Co-Axial Plush

Car Assist

INLINE SOCKETS

PS 21 D.I.N. 2 Pin (Speaker)

D.I.N. 3 Pin D.I.N. 5 Pin 180

D.I.N. 5 Pin 240°

Jack 2.5mm Plasti.

Jack 3.5mm Plastic

Jack 1" Plastic Jack 1" Screened

Phono Screened

Car Aerial

Co-Axial

Jack Stereo Plastic

1 D.I.N. 2 Pin (Speaker)

D.I.N. 5 Pin 2409

Jack 2.5mm Screened

Jack 3-5mm Plastic

Jack 1" Plastic Jack 1" Screened

Jack 3.5mm Screened

Jack Stereo Screened

Single Lapped Server

Stereo Screened

Twin Common Screen

Twin Oval Mains Cable

Four Core Common Screen

Four Core Individually Screened 0-30

Microphone Fully Braided Cable 0-10
Three Core Mains Cable 0-07

D.I.N. 3 Pin

D.I.N. 4 Pin

8.U.N. 7 Pin

Phono

PS 16 Co-Axial

CABLES

Car Aerial

Jack Stereo Screened

Ref. 56. Hi-Fi Stereo Hints & Tips 32p

Ref. 34. Cassette Case £1-27

PS 35 DIN 2 Pin (Speaker)

Model 9. Wire Stripper/Cutter 83p ANTEX SOLDERING IRONS

X25. 25 watt £1.93 CCN 240. 15 watt £2:15 Model G. 18 watt 22:15 SK2. Soldering Kit #9-86 STANDS: ST1 £1-21, ST2 77p SOLDER: 188WG Multicore 702 82p 228WG 70z 82p. 188WG 22ft 28p 228WG Tube 22n

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Į	102 For model CN240 3/322	38p
i	104 For model CN240 3/16"	38p
	1100 For model CCN240 3/32"	38p
	1101 For model CCN240 3/8"	38p
	1102 For model CCN240 1"	38p
	1020 For model G240 3/32"	38p
	1021 For model G240 1/8"	38p
I	1022 For model G240 3/16"	38p
ı	50 For model X25 3/32"	38p
ı	51 For model X25 1/8"	38p
I	52 For model X25 3/16"	38p
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	C4	75	th W Resistors mixed prefer	red 0.55
Ì	C5	5	Pieces assorted Ferrite Rods	0.55
Į	C6	2	Tuning Gangs, MW/LW VHF	
l	C 7	1	Pack Wire 50 metres ass	
Į	C 8	10	Reed Switches	0.55
1	C 9	3	Micro Switches	0.55
ı	C10	15	Assorted Pots & Pre-Sets	0.55
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i	C13	20	Electrolytics Trans. types	0.55
l	C14	ł	Pack assorted Hardware - Nuts/Bolts, Grommets etc.	0.55
l	C15	4	Mains Slide Switches	0.55
l	C16	20	Assorted Tag strips & Panels	0.55
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Resistor Colour Code Disc Calculator

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ACOS GP93-1. 280mV at lem/sec	£1.6
ACOS GP96-1. 100mV at lcm/sec	£2·6
TTC J-2005. Crystal/Hi Output	95
TTC J-20 10C Crystal/H1 Output Cor	npatibl
TTC J-200 CS Stereo/Hi Output	£1-6
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Speaker Cable

Low Loss Co-Axial

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5	Log and Lin 4-7K, 10K, 22K, 47K, 100K, 220K, 1M, 2M	470K
5 5 5	VC 1 Single less Switch VC 2 Single D.P. Switch VC 3 Tandem Less Switch VC 4 1K Lin Less Switch VC 5 100K Log anti-Log	0·14 0·26 0·44 0·14
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The E12 Range of Carbon Film Resistors, 1/8th watt available in PAKS of 50 pleces, assorted into the following groups:— R1 50 Mixed 100 ohms-820 ohms 40p R2 50 Mixed 1K ohms-8-2K ohms 40n R3 50 Mixed 10K ohms-82K ohms 40p R4 50 Mixed 100K ohms-1 Meg. ohms 40p THESE ARE UNBEATABLE PRICES-LESS THAN 1P EACH INCL. V.A.T.

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AL10/AL20/AL30 AUDIO AMPLIFIER MODULES



The AL10, AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 wats R.M.S.

The versatility of their design makes them had for near in record by very time recorders.

ideal for use in record players, tape recorders, stereo amplifiers and cassette and cartridge tape players in the car and at home.

Parameter	Conditions	Performance	
HARMONIC DISTORTION	Po 3 WATTS f 1KHz	0.25°	
LOAD IMPEDANCE		8 - 16 Ω	
INPUT IMPEDANCE	f=1KHz	100 k Ω	
FREQUENCY RESPONSE Œ 34B	Po 2 WATTS	50 Hz ~ 25KH:	
SENSITIVITY for BATED O/P	-Vs-25V. R1=8Ω t 1KHz	75mV. RMS	
DIMENSIONS		3" × 21" × 1"	

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter	AL10	AL20	AL80	
Maximum Supply Voltage	25	30	30	
Power output for 2% T.H.D. (RL = 8Ωf 1 KHz)	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min.	

AUDIO AMPLIFIER

MODULES		
AL 10. 3 watts	B 318	£2-19
AL 20. 5 watts	EMS	£2.59
4.1 20 10 motte	DAIS	63-01

POWER SUPPLIES

PS 12. (Use with AL10 & AL20) SPM 80. (Use with also AL30 & AL50) 88p £3 25 PRONT PANELS SP 12 with Knobs £1:10

PRE-AMPLIFIERS

PA 12. (Use with AL10 & AL20) £4.35 PA 100. (Use with AL30 & AL50) £13.15

TRANSFORMERS

T461 (Use with AL10) £1.38 P & P 15p T538 (Use with AL20) £1.93 P & P 15p BMT80 (Use with AL30 & AL50) £2:15

PA 12. PRE-AMPLIFIER SPECIFICATION

The PA 12 pre-amplifier has been designed to match into I most budget stereo systems. It is compatible with the AL 10, AL 20 and AL 30 audio power amplifiers and it can be supplied from their associated power supplies. There are two stereo inputs, one has been designed for use with *Ceramic cartridges while the auxiliary input will suit most †Magnetic cartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/off switch, balance, bass and treble. Size 152mm × 84mm × 35mm.

Frequency response 20Hz 50KHz (3dB) Bass control -± 12dB at 60Hz
Treble control --

Treble control = ± 14dB at 14KHz *Input 1. Inpedance 1 Meg. ohm Sensitivity 300mV 1Input 2. Impedance 30 K ohms Sensitivity 4mV

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ALL PRICES INCLUDE V.A.T.

The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and tests on a one-piece chassis measuring 20 cm \times 14 cm \times 5.5 cm. This compact unit comes complete with on/off switch This compact unit course complete with on/off aw volume control, halance, base and treble controls. Transformer, Power supply and Power amps. Attractively printed front panel and matching control knobs. The "Stereo 20" has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively, into a separate cabinet. Output power 20s. peak. Input 1 (Oer.) 300mV into 1M. Freq. res. 25 Hz-25kHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Bass control ± 124B at 50Hz typically 0.25% at 1 wat. Treble con. ± 14dB at 54kHz.



50W pk 25w (RMS)

0.1% DISTORTION! HI-FI AUDIO AMPLIFIER

THE AL50

- Frequency Response 15Hz to 100.000-1dB
- ★ Load—3, 4, 8 or 16 ohms.
- ★ Distortion—better than 1% at 1 KHz
- ★ Signal to noise ratio 80dB.

£3.58 each

- ★ Supply voltage 10-35 Volts
- ★ Overall size 63mm 105mm × 13mm.

Tailor made to the most stringent specifications using top quality component and incorporating the latest solid state circuitry and ALSO was conceived to fit the need for all your A.E. amplification needs.

PULLY BUILT TESTED GUARANTEED

STABILISED POWER **MODULE SPM80**

AP80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 watt (r.m.s.) per channel simul lancously. This module embodies the latest component and circuit techniques incorporating complete short circuit protection. With the addition of the Maint Transformer MT80, the unit will provide outputs of up to 1 amps at 35 works. Size: 63mm s. 105mm s. 30mm.
These units enable you to build Audio Systems of the highest many and the state of the size of t other applications including: Disco Systems, Public Address-Intercom Units, etc. Handbook available 10p PRICE £3:25

TRANSFORMER BMT80 £2:15 p. & p. 28p

STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the marked the PA100 sterro pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL50 power amplifier system, this quality mate unit incorporate, no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages.

Three switched stereo inputs, and rumble and scratch filters are features of the PA100 which also has a STEREO/MONO switch, volume, balance, and continuously variable has a STEREO/MONO switch, volume, balance, and continuously variable has a silicon for the second selection.

SPECIFICATION

Bass Control
Treble Control
Filters: Rumble (High Pass)
Scratch (Low Pass)
Signal/Noise Ratio Input overload

Supply Dimensions

T00H2
8K Hz
better than - 65dH
+ 25dB
+ 25dB
+ 35 volts at 20mA
292mm × 82mm × 35mm
ONLY £13 · 15
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SPECIAL COMPLETE KIT COMPRISING 2 AL50's, 1 SPM80, 1 BMT80 & 1 PA100 ONLY £25:30 FREE p. & p.

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Guaranteed Satisfaction or Money Back

 \mathbf{S}^{o} the winter's economic crunch has come as most realistic prophets have forecast. We have read, heard, seen and experienced at first hand some of the revivals of the immediate post-war social and economic problems, not forgetting that dreaded winter of 1947. We do not intend here to rub the salt further into the wound but rather to look at ways and means of making our lives just a little more bearable.

Practical Wireless showed foresight in the autumn of 1973 which paid off. The power crises ever looming in our midst, we grabbed at the expected misfortunes in the electricity supply industry by publishing at the right time an emergency lighting unit to operate from a car battery. This proved so popular that we are now short of copies for office use. For those of you who missed it we publish in this issue a slightly different version (suggested by a P.W. reader) that uses a ready-made oscillator coil.

If you have thoughts about visiting the SONEX or other hi-fi exhibitions in the vicinity of London Airport in March, but are seriously wondering where the money to buy is going to come from, because of the Chancellor's mini-budget restrictions, again take a crumb of comfort from P.W. For less than a pound you can have not only the widest variety of do-it-yourself designs over the next three months, but also the freedom to control your own spending over whatever period you choose. You can purchase components and build your own equipment at leisure

without worrying about interest charges.

This month's issue sees the start of a new hi-fi project with a difference. We do not recall ever seeing a similar project before in a magazine that incorporates a cassette recorder. We could then be justified in claiming yet another first for the do-it-yourselfer. The result is that you can save on the cost of a system for the home that gives you a.m. and f.m. radio, tape record/playback, the playing of pre-recorded cassettes, and with an added pick-up you can play back stereo discs. This quality system is in stereo and the cassette machine is left to your choice to suit your requirements and, most important, your pocket. If you are seriously interested in quadraphonic sound there is ample room in the unit to include a second pair of amplifiers and an uprated mains transformer.

If you have your own hi-fi set-up already, but you could do with a useful piece of test gear to help you set it up or locate some of those obscure faults, you will be interested in the Trouble Tracer that we published in the last two issues and the

Waveform Generator in this issue.

Finally, most of you will already be hooked on our P.W. Datacard system; numbers 7 and 8 in this issue are specially designed for those who require "finger-tip" information on local reception and guidance on aerial installations.

M. A. COLWELL—Editor.

The April issue will include a new unique portable 5-band radio receiver; a "short-wipe" unit for clearing April showers from your car windscreen; an article that explains impedance matching in audio equipment; a special tool kit arranged by Practical Wireless for its readers at a favourable price. Cut your costs again—order the April issue of P.W. now. See the footnote and further details on page 1075.

IMPORTANT MESSAGE TO ALL READERS

Readers of "Practical Wireless" and most other magazines will be aware of the restrictions imposed by the Government and as a result of Trades Union action in various industries. To ensure that you receive your copy of "Practical Wireless" at the earliest possible date, we have to rely on effective communications and delivery through the post and by railway. We also depend on the operation of electrical equipment and printing machinery. Petrol and diesel oil are vital to the needs of our job in quick and effective processing of editorial and advertising material,

We are sure that you will understand the many problems that confront all of us. We therefore request your patience and understanding during any temporary period when publication may be delayed.

We regret that due to the effects of the current industrial situation, the number of pages in this issue has had to be limited. We apologise to advertisers who were unable to insert their full allocation of product announcements and to those unable to appear at all in this issue. Such is the "pulling-power" of Practical Wireless and its advertisements that we recommend booking early for the next available issue.

Plessey IC book

LESSEY Semiconductors has produced a comprehensive 235-page Databook giving details of its extensive range of silicon integrated circuits.

Continuous emphasis on the development of processes and circuits by Plessey has been demonstrated by the successful introduction of Bipolar Process III circuits and MNOS electricallyalterable non-volatile memories. The first products from these new processes are detailed in the Databook along with the wide range of both special and standard products currently available.

Copies of the Integrated Circuit Databook are available on application to Plessey Semiconductors Limited, Cheney Manor, Swindon, Wiltshire,

Sonex rival

I-FIDELITY '74 is a rival exhibition which will run concurrently with Sonex at the Heathrow Hotel. More details next month.

ISB for broadcast radio?

ORK on the problems of a.m. broadcasting on medium and long waves has been carried out at Siemens laboratories in West Germany. The independent sideband (ISB) system, proposed by the Hamburg Institute of Radio Engineering is being seriously considered to overcome some of the problems of increasing mutual interference.

Siemens engineers are quick to point out that the review of broadcasting frequency allocation, due within the next eighteen months, should recommend ISB to enable expansion up to double the number of programme channels for the same number of transmitters. An added advantage is that ISB offers the equivalent to SSB in terms of interference, bandwidth and fading, and could be implemented locally without the need for international agreement.

The major drawback is that receiver design will have to be altered so that a phase shift network can be employed for the 150 to 4kHz band to separate the two side-bands by at least 40dB. ISB receivers would be capable of processing signals in the SSB and DSB modes, with improved reception on DSB by listener selection. Transmitters would probably handle signals with the dynamic range reduced by 30dB.

Modules and valves

T a recent visit to the huge Mullard manufacturing complex at Blackburn recently, we were privileged to see the making of those "liquorice allsorts" coloured capacitors that are now familiar on printed circuit assemblies. Readers will also be pleased to learn that valves, mostly for television, are still being made in millions although the range of types has been rationalised to fit the economic needs of setmakers and servicemen.

We also saw the assembly of Mullard modules: the LP1185 f.m. i.f. strip; LP1186 d.c. voltage controlled tuner for Band II; LP1159 a.m. i.f. strip; LP1162 4 watt amplifier; LP1164/1 r.f./i.f. amplifier for a.m./f.m. radio; LP1402 f.m. tuner with capacitor tuning. Mullard are working on a modular design stereo decoder for release soon.

Our picture here shows the polyester foil type capacitor going through the colour code dip painting process. These are only a few of the vast activities on this 46 acre site employing approximately 4,000 people.

Torbay A.R.S.

THE Torbay Amateur Radio Society, G3NJA, has produced its first magazine. One of the main features is that of v.h.f./u.h.f. conversions of commercial equipment for the Amateur. This has been written by E. Hayman, G3ABU.

The T.A.R.S. are willing to add any readers' names to their magazine mailing list. Alternatively readers may become Associate Members for the sum of 50p annual subscription. They would then receive a free copy.

The magazine will be produced on alternate months and further gen may be obtained by sending a s.a.e. to Frederick J. E. Bolton, G3VTQ, Top Flat, 23 Waverley Road, Newton Abbot, Devon.

Radar pioneer dies

IR Robert Watson-Watt, C.B., F.R.S. died on 5th December at the age of 81. Sir Robert will be one of those famous names in the U.K. associated with great electronic inventions and in his case radar.

Early in his career he worked on the use of radio to detect thunderstorms. Radio direction finding found fame for him in World War II. Civil applications include airlines and shipping; a fitting tribute being the recently opened computer assisted radar tower and communications system for shipping within a 20 mile range of Liverpool.

The communications system was installed by Decca Radar Limited.



A Versatile WAVEFORM GENERATOR

J. B.DANCE M. Sc

THE Signetics NE566 integrated circuit function generator can be used to construct a simple unit which will provide a variety of waveforms over a very wide frequency range.

The prototype unit will be described in detail. However, a number of variations will be discussed so that individual readers can make modifications which may make the unit more useful for their

own particular purposes.

The basic waveform generator produces triangular waves and square waves, and it is especially suitable for use in audio amplifier testing. An additional circuit can be used to produce sine waves in addition to the other two waveforms. The circuit can be modified to produce rising or falling waveforms of high linearity instead of the triangular waveforms. In this case short rectangular pulses are available at the output which previously provided square waves.

THE BASIC CIRCUIT

The circuit of the basic function generator is shown in Fig. 1. The voltage at the slider of VR1 is applied to pin 5 of the NE566V and also pin 6 via C1. The

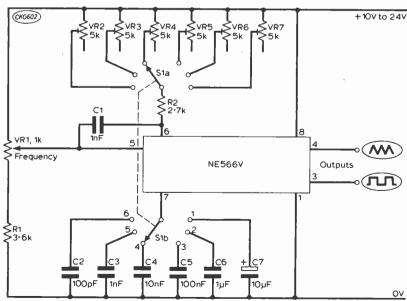
current passing to this latter pin is determined by the value of the voltage at this pin and by the resistance between it and the positive line. This current is used to charge and discharge the capacitor selected by S1b.

A Beckman 'Helipot' precision ten-turn helical potentiometer is employed for VR1 together with a Beckman turns counting dial; this enables the frequency of oscillation to be set reasonably accurately. The value of R1 has been chosen so that the potential at pin 5 never falls below three-quarters of the positive power supply line potential (as recommended by the manufacturers of the integrated circuit).

The frequency of oscillation is proportional to the voltage between the positive power supply line and pin 5; this voltage is in turn proportional to the resistance of VR1 between the positive line and the slider. In the circuit of Fig. 1, the frequency of oscillation is set to 10Hz, 100Hz, 1kHz, 10kHz, 100kHz



▲ The finished waveform generator with its direct reading dial. The necessary components to produce a ramp waveform can be added to the circuit board. For converting triangular waveforms to sinewaves a separate unit is required.



◀ Fig. 1: Circuit of generator producing square and triangular waves over a wide range of frequencies.

or 1MHz (depending on the range) when the slider of VR1 is set at $10\cdot0$. At other settings of the dial, the frequency is closely proportional to the dial setting. For example, a dial setting of $5\cdot67$ on the lkHz range produces an output of 567Hz.

Many types of capacitor (especially electrolytic types) have very wide tolerances in their capacitance value. It is therefore necessary to calibrate the frequency at one point on each range to obtain accurate frequency readings. In the circuit of Fig. 1 this is accomplished by the adjustment of a different trimmer potentiometer (VR2 to VR7) for each range used. The switch which selects the trimmer, S1a, is ganged with that which selects the range capacitor, S1b.

FREQUENCY COVERAGE

The frequencies available from the six adjustable ranges employed are shown in Table 1. The upper frequency limit of 1MHz is determined by the characteristics of the integrated circuit used. In the table it has been assumed that a frequency range of 20:1 may be covered using any one capacitor. However, more accurate frequency settings may be obtained by limiting the coverage of each range to 10:1, as was done in the prototype.

RANGE	CAPACITOR	FREQ. COVERAGE			
1 / 2 / 3 / 4 / 5 / 6	10µF 100nF 100nF 10nF	0 5Hz- 10Hz 5Hz-100Hz 50Hz- 1kHz 500Hz-10kHz 5kHz-100kHz 50kHz- 1 MHz			

TABLE 1. Total frequency coverage possible with six capacitors. In practice each range is reduced to a ratio of 10:1.

The writer has found that a frequency range of about 30:1 is about the limit with any one capacitor. At settings of the frequency dial of less than about 0.3 the output waveforms become distorted, whilst oscillation ceases at settings below about 0.25. It was noted that the square waveform at 1MHz was somewhat distorted. The lowest frequency range in the prototype was 0.5 to 10Hz and it is assumed that most readers will not require frequencies below this value. Extra ranges can easily be added if required. However, an additional trimming potentiometer must be included in the S1a circuit for each extra range. A 100 µF capacitor in the S1b circuit can be used to produce a range of 0.05 to 1Hz, a $1000\mu F$ capacitor a range of 0.005 to 0.1Hz and a $10000\mu F$ capacitor a range of 0.0005 to 0.01Hz(0.0005Hz is one cycle in about 33 minutes).

When using very large capacitors, check that their leakage current is not excessive. The lowest possible frequency is probably about one cycle every few hours, but the writer has not tried to obtain frequencies quite as low as this. Some industrial applications may be found for generators of extremely low frequencies.

CONSTRUCTIONAL NOTES

The basic oscillator circuit of Fig. 1 was constructed in an Eddystone die-cast box of approximate dimensions $4^{1}_{2} \times 3^{1}_{2} \times 2^{1}_{4}$ in. (Cat. 6908P). The Helipot VR1 and switch S1 are mounted in the base of the box and the circuit board along one of the

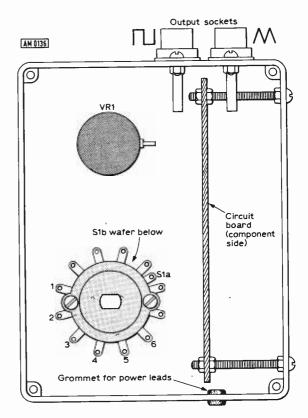


Fig. 2: General layout of components in the die-cast box.

longer sides Fig. 2. No components were mounted on the lid of the box since this procedure enables the lid to be removed without the inconvenience of having wires between it and the main part of the box.

The six miniature Beckman trimmer potentiometers are mounted on the circuit board Fig. 3, their connecting tags being inserted through holes in the board and bent over before the connecting wires are soldered. The integrated circuit socket is also mounted on the circuit board by passing the pins through holes in the board and soldering the connections to them.

C1 is mounted on the circuit board, but C2 to C7 are mounted around the switch S1. No power supply was included in the box, since it is generally more convenient to employ an external 12V battery. However, a mains power supply could be included if a rather larger box is employed.

If the circuits for the ramp and short pulse generator are required, they must be included in the basic oscillator unit itself. However, if the triangle-to-sine wave converter is made, it will probably be more convenient to construct it on a separate circuit board.

CALIBRATION

The best way of calibrating the frequency settings involves the use of a digital frequency meter which automatically counts the pulses from the oscillator over a timed period. Alternatively a pulse counter may be used with a manually operated stop watch.

Calibration may also be carried out using a good oscilloscope with a calibrated time base. Alternatively the calibration may be set by adjusting the

trimming potentiometers so that the output 'zero beats' with the signal from a calibrated generator. At higher operating frequencies harmonics of the square wave output may be allowed to beat with a radio signal, using a receiver.

If very low frequency ranges are incorporated in the unit, the operating frequencies are best determined by connecting a voltmeter across the square wave output and timing the movements of the meter needle.

It is normally best to calibrate the unit at a point near to the highest frequency on each range. The linearity of the resistance of VR1 with the dial setting is very good (better than 0.25%). However, the writer has found that the frequency of oscillation of the NE566V may depart from linearity by up to about $\pm 1\%$ at the lower frequencies in each range.

If a constructor does not like an instrument in which the oscillation ceases at the very low frequency end of each range, it is possible to set the dial so that it reads from 1.0 to 11.0. In this case a 100 ohm resistor, preferably of 0.5% tolerance, should be inserted between the upper end of VR1 and the positive supply line in Fig. 1 so that the readings are directly related to the frequency of oscillation. Operation in this way is likely to increase the errors in the frequency settings, since the percentage linearity tolerance of a precision helical potentiometer is typically about ten times better than the resistance value tolerance.

OUTPUTS

The circuit of Fig. 1 provides good square waves and also linear triangular waves, both at 50 ohm output impedance. These outputs are adequate for many applications, since the triangular waves can

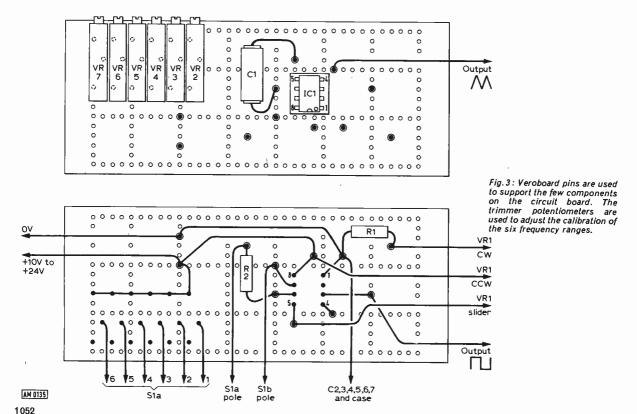
often be used instead of sine waves when their harmonic content is not disadvantageous.

Both of these output waveforms are superimposed on steady positive potentials. The latter can be removed by capacitive coupling except at low frequencies where it is difficult to obtain an adequate time constant to preserve the waveform. The average potential of either of the output waveforms can be made equal to earth potential by employing a power supply consisting of suitable positive and negative supply voltages both isolated from earth.

TRIANGLE-TO-SINE CONVERSION

If a sine wave with a relatively low harmonic content is required, a diode-resistor shaping network may be employed. A fairly complex circuit is required if the shaping must be carried out reasonably accurately. A simpler solution involves the use of the conversion circuit described below.

At a fixed gate voltage, the first part of the drain characteristic of a junction field effect transistor (FET) approximates to half a sine wave. However, further increase of the drain voltage produces little effect on the drain current. The first part of this characteristic can be employed to shape a triangular wave into a reasonably good sine wave. If a triangular wave is applied to this circuit the positive going part of this waveform will produce a drain current of half a sine wave. In order that both the positive and negative parts of the triangular wave shall produce the corresponding parts of a sine wave, the type of circuit shown in Fig. 4 may be employed. This utilises the fact that the drain and source electrodes of an FET are essentially interchangeable.



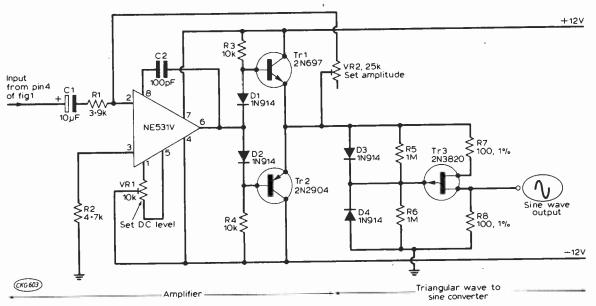


Fig. 4: Suitable circuit for converting a triangular wave to a sine wave.

PRACTICAL SINE CONVERTERS

It should be clear that the amplitude of the triangular wave applied to the circuit of Fig. 4 is quite critical if one requires a good sine wave output. If the input to this circuit is too large in amplitude, the output pulses will have fairly flat sections in place of the normal sine wave peaks. If the input amplitude is too small, the output will be approximately the same form of triangular wave as the input.

It must therefore be possible to alter the amplitude of the triangular wavefed to the circuit of Fig. 4. In addition, the output impedance of the source of the triangular waves must be small and there must be no steady voltage superimposed on the triangular waves. An amplifier of variable gain and of low output impedance is therefore employed between the output of the 566 circuit and the input of the triangle-to-sine converter.

CONVERTER CIRCUIT

The circuit of a practical triangle-to-sine wave converter is shown in Fig. 4. The triangular wave input from the circuit of Fig.1 is capacitively coupled to the input of a Signetics NE531V high slew rate operational amplifier; it therefore follows that this circuit is unsuitable for use at very low frequencies with the values shown, since the coupling time constant would be inadequate.

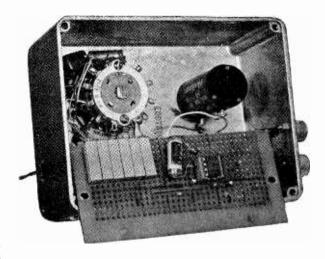
The complementary output transistors Tr1 and Tr2 provide a low impedance output to the converter circuit of Tr3. The preset potentiometer VR1 is set so that the potential at the emitters of Tr1 and Tr2 is zero volts when no input is applied to the circuit.

The voltage gain of the circuit of Fig. 4 from the input to the emitters of Tr1 and Tr2 is equal to the resistance of VR2 divided by R1. The amplified triangular wave is applied to the circuit of Tr3, the operation of which has already been discussed. The author found that the sine wave output voltage was of the order of 0.7V peak to peak and that it has no steady component superimposed on it.

The gain control, VR2, must be set carefully so that the output waveform shows minimum distortion, adjusting the gain whilst examining the output waveform by means of an oscilloscope. If, however, a waveform analyser is available, VR2 may be adjusted for minimum third harmonic distortion.

A satisfactory sine wave was obtained using fixed resistors for R7 and R8. However, one of these resistors may be replaced by a 50 ohm resistor in series with a 100 ohm preset trimmer so that the output may be adjusted for minimum second harmonic distortion (preferably using a waveform analyser). It should then be possible to obtain a sine wave output with very low distortion.

The writer tried replacing the NE531V integrated circuit with a μ A741V which has the same connections. It was found that the NE531V could operate at higher frequencies, but in neither case could satisfactory operation at 1MHz be obtained.



The secret of the direct frequency read-out lies in the use of the multiturn Helipot potentiometer, right centre.

A simple circuit using two cascaded emitter followers for driving an FET triangle-to-sine converter was published in the February 1973 issue of *Wireless World*. However, a circuit with voltage gain is required when the triangular wave output from a 566, operated from a 12V supply, is to be converted into a sine wave.

RAMP WAVEFORM GENERATORS

The circuit of Fig. 1 can be easily converted into a generator which produces either a rising or a falling linear ramp waveform. At the end of each ramp the output quickly returns to its initial level and another ramp commences.

In order to produce a rising ramp waveform, the capacitor connected to pin 7 is allowed to charge, but at the end of the charging period it is rapidly discharged. The ramp waveform appears at pin 3 of the 566 in place of the triangular wave. A falling ramp is produced in a similar way; at the end of the discharging period, the capacitor connected to pin 7 is rapidly re-charged.

RAMP CIRCUITS

Fig. 5 shows the components which must be added to the circuit of Fig. 1 to allow either rising or falling ramps to be produced. When the switch S2 is in position 1, the additional components shown dotted are not used and the circuit therefore provides the normal square and triangular output waveforms. When S2 is in position 2, a falling ramp waveform is generated, whilst in position 3 a rising ramp is formed. Short negative going pulses are available at pin 4 when S2 is in position 2 and short positive pulses when S2 is in position 3.

Let us now consider in detail the operation of the falling ramp generator when S2 is in position 2.

If the output from pin 4 is in its high voltage state, little current passes through D1 of Fig. 8. The base and emitter of Tr1 are therefore at about the same potential and this transistor passes little

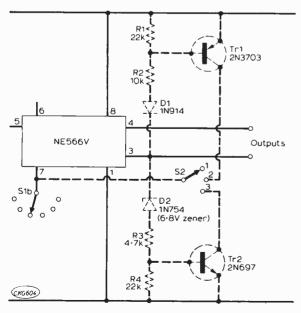


Fig. 5: Additional circuitry, shown dotted, to produce rising or falling ramp waveforms.

* components list

R1 3.6kΩ 5% ±W R2 2·7kΩ 10% ½W VR1 1kΩ 0.25% linearity (Beckman 'Helipot' Type 7246) VR2-7 5kΩ trimmer pots (Beckman Type 89P) C1 1nF C2 100pF C3 1nF All 25V polystyrene C4 10nF , C5 100nF C6 1μF All 25V polyester C7 10µF 24V electrolytic Miscellaneous IC1, NE566V (Low cost alternative is LM566-Ambit International). 8 pin DIL socket. S1, 2 pole, 6 way rotary switch. Turns counting dial for Helipot (Beckman Type RB). Die-cast box (Eddystone Type 6908P). Piece of plain veroboard. (Note: VR1 with dial and VR2-7 available from Athena SMC Ltd., 140 High Street, Egham, Surrey). Basic Components for Triangular-Sine Wave Converter R1 3.9kΩ R2 4·7kΩ R3 10kΩ R4 $10k\Omega$ R5 $1M\Omega$ R6 1ΜΩ All 10% 1W R7 100Ω .R8 100Ω Both 1% 1W VR2 25kΩ (Beckman Type 89P) VR1 10kΩ C1 10uF 15V C2 100μF 15V D1-4 1N914 Tr1 2N697 Tr2 2N2904 Tr3 2N3820 NE531V (Low cost alternative Is LM318H—check leadout connections)

Basic Components for Ramp Wave Converter

current. The output from pin 3 therefore falls linearly with time, unaffected by the additional components.

When the output from pin 4 falls to its low voltage state, however, D1 conducts and the base of Tr1 becomes negative. This PNP transistor therefore conducts and rapidly charges the capacitor selected by S1b. The voltage at pin 3 therefore rises rapidly to its maximum value before a further falling ramp is generated.

The output from pin 4 consists of short negative going pulses which occur each time the ramp waveform at pin 3 rises to its maximum value. These waveforms are shown in Fig. 6. When the capacitor selected by S1b is small, the negative going pulses at pin 4 were found to be about $0 \cdot 2\mu s$ in length.

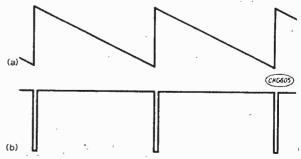


Fig. 6: Waveforms obtainable from the circuit of Fig. 5.





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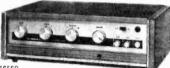




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When a large capacitor is in circuit, however, it takes longer to charge from the current passing through Trl. Nevertheless, the time for which the waveform at pin 4 is in its low voltage state is a very small fraction of the total operating time.

The operation of the rising ramp generator, when S2 is in position 3, is rather similar. When the output at pin 4 is in its low voltage state, the zener diode D2 passes little current and Tr2 remains cut off. During this time the ramp waveform at pin 3 is rising.

When the voltage at pin 4 switches to its upper level, however, the zener diode conducts and Tr2 receives a positive bias at its base. This NPN transistor therefore conducts and rapidly discharges the capacitor selected by S1b. The potential at pin 3 therefore returns quickly to its lowest level and the ramp commences to rise again.

The output from pin 4 consists of short positive pulses which occur each time the ramp at pin 3 returns to its lowest level.

The rising ramp generator was found to give a poor waveform on the 1MHz range. However, the rising and falling ramp generators both operated satisfactorily on the other ranges and also at very low frequencies. The writer tried them at frequencies down to about 0.01Hz and at such frequencies the waveform takes a fraction of a second to return at the end of each ramp.

When either of the ramp generators is employed, the one half of the triangular waveform is eliminated. The frequency of oscillation of the 566 is therefore approximately doubled when S2 is in position 2 or 3. Constructors who intend to use the unit mainly for ramp waveform generation may wish to calibrate the unit so that the ramp frequency can be read directly from the Helipot dial. The dial reading must then be halved to obtain the frequency of the triangular or square wave.

APPLICATIONS

The fundamental frequencies from the waveform generator can be used to test the functioning of audio amplifiers; they also cover the long wave band and the low frequency end of the medium wave band. In addition, the outputs contain harmonics (mainly odd harmonics) which can be used to test the functioning of radio receivers throughout the medium wave band and also at somewhat higher frequencies.

Both the triangular waves and the ramp waveforms are very suitable for the detection of crossover distortion in audio amplifiers, since these waveforms are essentially linear. If the triangular wave output is fed to the input of an audio amplifier which introduces cross-over distortion in its output stage, the type of waveform shown in Fig. 7a is obtained. The values of the resistors in the audio amplifier which control the quiescent current in the output stage may be altered so as to increase this current slightly; the cross-over distortion should disappear when the quiescent current is sufficient.

It is easier to detect cross-over distortion when using the triangular or ramp waveforms than when the more conventional sine wave is employed. A frequency in the mid-audio region is ideal for this test (perhaps 1kHz). The linearity of the waveform on the oscilloscope screen may be measured by placing a straight edge along the tips of the waveform.

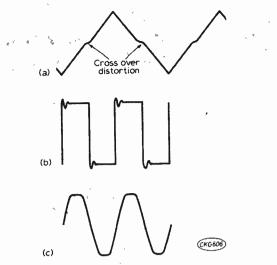


Fig. 7a-b-c . Waveforms at the output of an audio amplifier using input signals from the waveform generator.

The square wave output is also very useful for testing audio amplifiers. At fairly high frequencies one may examine the output from an amplifier for ringing of the type shown in Fig. 7b. Ideally there should be no overshoot or ringing. An audio amplifier which can faithfully reproduce a square wave at a frequency of about 10kHz must have a good frequency response in the high audio frequency region since square waves contain many harmonics and will be reproduced satisfactorily only if the amplifier has a fairly level response at frequencies of up to at least three times the fundamental frequency of the square wave.

If an audio amplifier has only a moderately good high frequency response, the corners of the output waveform will be rounded off at 10kHz, as shown in Fig. 7c. An approximate value for the frequency response of the amplifier may be obtained by estimating the time taken for the output waveform from the amplifier to rise from 10% to 90% of its final value. The maximum frequency at which the response is reasonably constant is of the order of 1/(3 x the rise time). If the rise time of a square wave is very short, one sees only the lines at the top and bottom of the oscilloscope display, the rising and falling parts of the waveform being so short that they are barely visible.

One can also use the square wave output from the 566 unit to examine the low frequency response of audio amplifiers. As one reduces the frequency of the square wave, the upper and lower parts of the output waveform do not remain horizontal, but develop a definite slope. At very low frequencies, a differentiated waveform will be obtained. The input of the oscilloscope marked 'DC' should be used for these low frequency tests, since the 'AC' input is connected to a series capacitor inside the oscilloscope which may distort the waveform.

In the audio amplifier tests discussed above, it has been assumed that the amplifier under test has a volume control at its input which can be adjusted to provide the required signal output level. At high levels it will be necessary to include a series canacitor in the input circuit to block the steady voltage at the 566 outputs. In this case care should be taken to ensure that the coupling time constant is adequate for the lowest frequency to be employed.

DRY BATTERY CHARGER

R.A.Butterworth

OST of us either make or buy a mains supply unit to operate our battery tape recorders, receivers etc., when used at home to save the cost of dry batteries. However batteries are still needed around the home and unfortunately they seem to cost more each time. One could of course use rechargeable cells but they are expensive and need a rather special charging unit which is also expensive.

If we could get a few more hours out of our dry battery we could cut our costs considerably, even one more 'run' would be equivalent to cutting the cost by a half. With the charging units described here two, three or more 'lives' can be given to a set of batteries, perhaps not quite as long a period of operation as the first but certainly for periods long enough to make the building of a charger show an economical return for the effort involved.

The idea of reforming dry cells is by no means new. Investigation of the possibilities were made as long ago as the early 1950's with encouraging results. With modern methods of manufacture and materials, the life of the primary cell can be considerably extended if a few basic rules are born in mind. These are:

1 The battery must be charged before its voltage (on load) drops from 1.5V to below 1V.

2 It must be put on charge as soon as possible after being removed from service and put into service as soon as possible after re-charge.

3 It is not economical to charge a single unit, a 1.5V 'pen light' HP7 for example. Therefore it is better to have one set of batteries in service and another on charge.

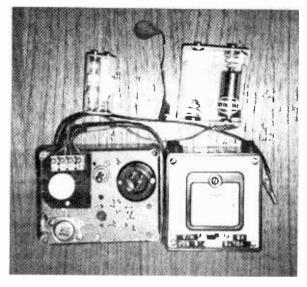
4 The charging rate should be adjusted to distribute the charge, in other words avoid heating up the cell by charging at too high a current.

5 If there is the slightest suspicion of battery leakage throw them away or you will have a horrible mess to clear up.

The cylindrical types like the U2, U11 and HP7, respond much better than the layer batteries, such as the PP3. The use/charge cycle is less than half that of the cylindrical types. The table gives details for popular zinc-carbon types which have responded successfully to several use/charge cycles with the equipment shown.

Battery holders

Standard battery holders can be used to hold the cells whilst charging in blocks of 2, 4, or 6. From experience it would appear that, after setting at the current shown, if after the first couple of hours there

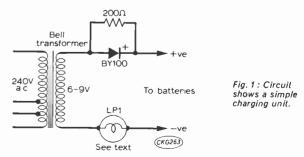


is no drop in the charging current, then discard the battery as the electrolyte has probably dried out. If the batteries get appreciably warm or show signs of leaking throw them out. Different sets of batteries have given a different number of cycles. This, the author believes, is due to 'freshness' of the unit cells when first purchased; in other words how long they had been on the shelf in store.

DRY BATTERY CHARGING

Battery	Use	No. of Cells	Cur	rging rent A Max.	Approx. hours of charging	No. of
U2	Torches, 'f Hand lamps Radios	´2 4 6	150	300	5	3
U7	Small Torches, Radios	1 or 2	100	150	4	4
U11	Cassette Tape Recorders	4 ! i	100	250	5	4

In the circuits shown in Figs. 1 and 2 it will be noted that very little smoothing of the d.c. output has been incorporated. This is deliberate; investigation has shown that it is advantageous to have a little a.c. present. This "dirty d.c." appears to shake up the electrolyte and therefore assists in the reforming.



-continued on page 1061

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AD161/2	69p	OC71	20p	1N4001	6р
BC107	10p	TIS43	28p	1N4002	6 ł p
BC108	10p	2N1711	24p	1N4003	7p
BC109	10p	2N2219	25p	1N4004	74p
BC147	10p	2N2646	45p	1N4005	8p
BC148	10p	2N2905	83p	1N4006	8 p
BC149	12p	2N2907	25p	1N4007	9p
BC168	13p	2N2926O	10p	W O 0 5	30p
BC169C	12p	2N2926Y	10p	WO4	33 p
BC182L	10p	2N2926G	10p	741C 8-pin	
BC204	14p	2N3053	18p	D.I.L.	86p
BC209C	14p	2N3055	49p	741C 14-pin	
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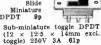
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BRITISH INSTITUTE OF ENGINEERING TECHNOLOGY

Charger units

Fig. 1 shows a simple unit which can be easily put together and used to try out the idea. A good quality bell transformer, BY100 diode, m.e.s. lamps, lamp holder and a 2200 IW resistor and you are in business. The writer found this unit successful but it lacked flexibility. If the bell transformer shown in Fig. 1 has various outputs then the number of cells to be charged can be varied and by changing the lamp the charging current can be varied within limits.

Fig. 2 is a more elaborate unit and in the author's case serves two purposes; A dry battery charger and mains unit for various equipment used in the shack. Should additional smoothing be required then it is a simple matter to add this. It is advisable to install the meter permanently so that the charging current can be monitored. A d.p.d.t. switch with a suitable shunt series resistor would enable both voltage and the current to be monitored. Diode D6 provides for reversal protection and prevents the battery discharging through the 470Ω resistor.

Zinc-carbon batteries are very amenable to recharging.

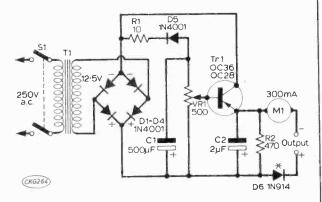


Fig. 2: A more elaborate design.

★ components list (Fig. 2)

R1	10Ω ½W
R2	470Ω 1W
VR1	500Ω 3 W linear wirewound
C1	500µF 20V
C2	2μF 20V
Tr1	OC36, OC28 or similar rating
T1	Mains transformer 12.5V 1A secondary
D1-D4	1N4001 diodes
D5	1N4001 diode
D6	1N914 diode (see text)
M1	Meter 300mA f.s.d.
S1	Double-pole on/off toggle switch
LP1	3.5V or 6.5V 0.1/0.2A (Fig. 1)

NEXT MONTH

An Automatic Battery Charger for 12 volt car batteries.

TELEVISION

IN THE

ASSEMBLING A MODULAR COLOUR SET

There are various ways of going about building a colour receiver. One approach is to make use where possible of manufacturers' surplus units. David Robinson describes the set he built on this basis and how the various problems of interfacing different units not originally intended for use together were overcome.

LOG-PERIODIC SET-TOP AERIAL

A simple log-periodic set-top aerial can be made using printed circuit board. Full constructional details will be provided.

TV SET SAFETY

With the introduction of the BEAB television receiver testing system and BS415:1972 there has been a tightening up in safety requirements. It is essential that anyone handling TV sets should be aware of what is involved. A detailed account starts next month.

FAULT FINDING

John Law looks at the power supply and line timebase circuits used in BRC 16in. dualstandard portable models. These make excellent second sets.

PHASEIN COLOUR TV

The phase of the chrominance signal indicates the colour being transmitted: phase is thus the key to colour television. A special article next month describes the basic technique and PAL signal processing, paying particular attention to practical points that are not always made clear.

PLUS ALL THE REGULAR FEATURES

Details of the March issue are subject to the current national situation at the time of going to press.

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PRODUCTION LINES colin riches

JOSTY KITS

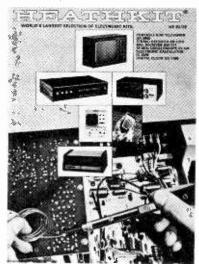
Our Advertisement Manager has asked me to point out that Swanley Electronics will not be supplying "Josty" kits as per their December advertisement.

HEATHKIT CATALOGUE

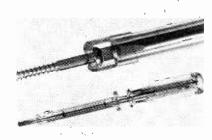
The latest catalogue from Heath (Gloucester) Limited contains details of the company's kits and some new models featured for the first time include the GR-990 12in. Black and White Television kit for either 12V or mains operation; the GD-39 Home Intrusion Alarm, disguised as an unobtrusive book — an ultrasonic burglar alarm/surveillance system; the CR-1008 a.m. Radio and the CM - 1045 Small Engine Tune - up Meter.

Also included are the 10-104 Solid State 15MHz Oscilloscope; IB-1103 180MHz Frequency Counter; the GC-1005 Electronic Digital Clock which incorporates a 'snooze' alarm; the CR9502 Push-Button a.m. Car Radio and the IC-2108 Desk Top Electronic Calculator.

Readers may obtain their free catalogue by writing to Heath (Gloucester) Limited, Bristol Road, Gloucester, GL2 6EE.



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Thunder Screw Anchors Ltd. announce an addition to their range of screwdrivers by the introduction of four screwholding screwdrivers. Two are suitable for slotted head screws and two for recessed head screws, their dimensions being 81in. and 91in. overall length, 3/16in. and \$in. blade diameter respectively. The screw is firmly held at the tip of the screwdriver by sliding the springloaded shank over the head of the screw, (see picture) leaving one hand free to hold the article to be fixed. It is possible to fix screws or bolts in the most difficult of places, where to hold a screw in the hand might normally be impossible.

Prices, excluding V.A.T. are 20372 and 20376 69p each, 20374 and 20378 79p each.

We understand that due to the shortage in the foreign plastics industry, supplies of these screwdrivers may be subjected to extended delay. However, this firm does have some further useful and novel tools that would be of interest to readers. Supplies are through retail outlets. Thunder Screw Anchors Ltd., Victoria Way, Burgess Hill, Sussex, RH15 9NF.

MICROELECTRONICS

We apologise to Microelectronics for being unable to include their advertisement in the Feb. issue. If readers refer to this month's issue, page 1028, they will see that the company markets the Minicomp 100 Random Number Selector. When the button on the front panel is pressed, numbers are displayed at high speed on a Nixietube read-out before a random number is displayed—in effect a miniature "ERNIE".

The circuit includes 6 TTL logic i.c.'s and three transistors and the manufacturers say that typical applications include number selection for dice, roulett, bingo etc. Price of the Minicomp 100 kit is £42·50. A fully assembled version is available at £45·00.—Microelectronics, 51 Mexfield Road, London, SW15 2RG. (Tel. 01-870 2368).

ONE-HAND DESOLDERER

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A soldering stand is supplied with every tool and the price of the complete unit is £6.49. Henry Picard & Frere Limited, 357/359 Kennington Lane, London, S.E.11.



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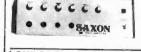
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The object was to design a unit which would provide 1MHz, 100kHz, 10kHz markers at good strength to at least 30MHz or higher. The calibrator to be described will, when used with the average receiver, provide strong frequency markers to above 30MHz and will give markers as high as 144MHz at reduced level.

OPERATION

The crystal oscillator runs at 1MHz and is based on the Colpitts circuit. In the design, good stability results in respect of both temperature variation and variation of supply rail voltage. In order to maintain this performance silver mica capacitors are specified for C2 and C3. The crystal in the prototype required about 40pF in series and this is made up by C1 plis TC1. If necessary, C1 can be altered to suit different

The output from the crystal oscillator is taken from the collector of Trl. The waveform is roughly a sine wave and in order to drive the dividers must be squared. Tr2 acts as a buffer amplifier and is biased into saturation on positive half cycles. This gives a square wave output of five volts peak to peak, which is used to drive the dividers.

The SN7490N (IC1-IC2) are TTL logic binary dividers and contain two gates and four bistables. They are used in this circuit to divide the 1MHz square wave by a factor of ten, giving in the first case 100kHz and in the second 10kHz. The output is a square wave of five volts (approx.).

The three outputs, one from each divider and the 1MHz waveform from Tr2 buffer are selected by S1 and are used to drive 1C3 and Tr3. These stages form the harmonic generator.

HARMONIC GENERATOR

From a pulse rising at an infinite rate an infinite frequency spectrum could be derived, and if the pulse were to be repetitive at some frequency, say 1MHz, then the spectrum would be related to the repetition rate of the pulse. However after the rise the pulse amplitude must decay again in time for next transition. If the decay is fast and at half the pulse repetition time then obviously a square wave would result. This could be shown to contain, in a pure case only, odd harmonics of the basic repetition rate. Now if the decay point were to be shifted from the half repetition rate time, then the even harmonic content would become apparent. Therefore in generating both odd and even harmonics of a fre-

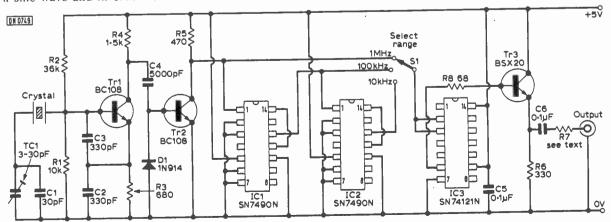
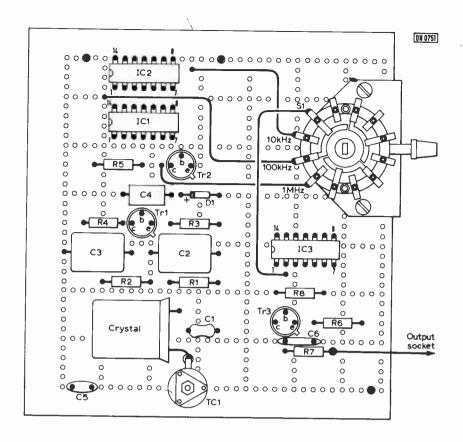


Fig. 1: Circuit of the calibrator



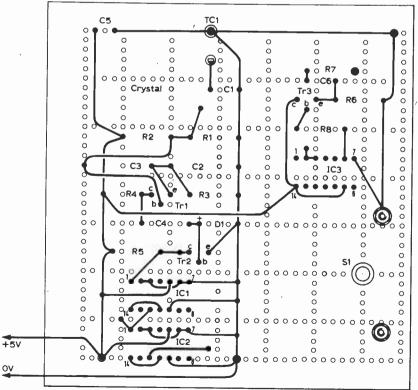


Fig. 2: Veroboard layout for the i.c. crystal harmonic calibrator

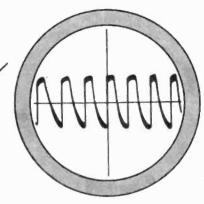
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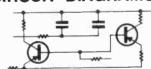
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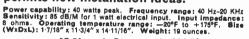
ARP12 DY86 EB91 EF80 EBF89 ECC81 ECC82 EY86	6p 20p 5p 10p 15p 12p 12p 20p	EF184 PCF80 PCC84 PCL82 PCL84 PCL85 PL36 PY81	20p 6p 6p 15p 15p 20p 17p	PY801 PY82 PY33 UI91 6BW7 6F23 30F5 30FL1	17p 10p 20p 20p 12p 15p 12p 20p
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quency or rate, the main functions governing them are the rise or transition time of the pulse and its duration with respect to repetition rate.

It can now be seen that the principal requirement for a harmonic generator is that it must generate a pulse with a rapid transition or rise time which is as narrow as possible with respect to the repitition rate.

A number of methods exist whereby a fast pulse may be generated, these include tunnel diodes, reverse recovery effect of diodes, fast switching transistors etc.

For ease and cheapness the method used here is a standard SN74121N monostable (IC3) which drives Tr3 the emitter follower into saturation. The SN74121N has provision for external timing components, but none are used here. This gives a pulse width of 30-40nS. The output rise time (transition time) is quoted as 10nS, but this is speeded up considerably by Tr3, which is a high speed switching device. Tr3 also provides a low output impedance.

The 75Ω resistor R7 is worth mentioning. The output impedance of the emitter follower (Tr3) is not governed directly by R6. It is in fact much lower than this and for matching purposes may be taken as zero. If it is desired to pass the signal along a coaxial line or to use an attenuator then R7 should be chosen to match the impedance of the cable in use, in the range of $50\text{-}300\Omega$. However, many people will simply want to connect receivers or to squirt the output into a few feet of wire in which case make R7 50Ω .

POWER SUPPLIES

The limiting factors here are the integrated circuits. The voltage required is five volts $\pm 10\%$. The design of the oscillator assures stability to within a few Hz for a $\pm 20\%$ change in supply potential. This should not however present too great a problem as many constructors now run some form of equipment from which a five volt supply could be borrowed to operate the calibrator.

Fig. 3 shows the circuit of a simple stabiliser for use with this calibrator.

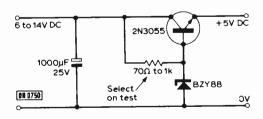


Fig. 3: Simple stabiliser

CONSTRUCTION

Building the calibrator should not present any problems, all components may be assembled on perforated board of suitable matrix. However in order to realise the best h.f. performance the leads around 1C3 Tr3 should be kept as short as possible and the output socket wired direct to Tr3 emitter. In particular, ensure that the output lead from pin 6 of 1C3 is short and direct to Tr3 base.

The crystal, if of a miniature type, may be fastened to the board and secured with a loop of wire. Solid

vibration free wiring in the crystal oscillator circuit will avoid microphony. If S1 cannot be wired direct to the board, all leads to it should be kept short. When completed and tested the board may be fitted in a small metal case or die-cast box.

★ components list

Resist			0	
	10kΩ	R5		
R2	$36k\Omega$	R6		
R3	Ω 086		50-300Ω	
R4	1 · 5kΩ	R8	68Ω	
Capac	itors:			
C1	30pF silver	r mica		
C2	330pF silve	er mica 2%		
	330pF silve			
C4	5000pF po	lystyrene		
	0·1μF cera			
	0·1μF cera			
TC1	3-30pF Ph	ilips trimme	r	
Semio	onductors:			
Tr1	BC108			
Tr2	BC108	Texas Instr	uments	
Tr3	BSX20			
Integr	ated Circuit	S		
IC1	SN7490N			
IC2	SN7490N	Texas Ins	struments	
1C3	SN74121N			
Misce	llaneous		•	
	1 pole 3 w			
Crys	tal 1Mhz HC	ill or simila	r	

TESTING

Connect a suitable five volt supply to the calibrator and couple the output to a receiver (b.f.o. on) tuned to 1MHz. If all is in order a marker will be heard. Tune the receiver throughout its range and check that markers are present. Switch S1 to 100kHz and check that there are 100kHz markers present. Switch to 10kHz and carefully check that 10kHz markers are present.

If no markers are present on any range first check the oscillator circuitry. If markers appear only at 1MHz intervals check the dividers for a fault.

The simplest way of controlling the injection of markers to a receiver is to vary the coupling. Obviously the markers are less strong around 30MHz and the coupling may have to be increased. Direct coupling without the use of an attenuator is likely to overload the receiver and may introduce spurious responses. A little experiment will reveal the best method of operation.

Once the unit has been checked the frequency may be accurately set against WWV or MSF on either 2.5, 5.0 of 10MHz. The calibrator should be rechecked from time to time against the standard frequency services to maintain its accuracy. TC1 may be adjusted as necessary to maintain this accuracy.

We regret that the December 1973 issue of *Practical Wireless* is now out of print

PORTABLE FLUCRESCENT LAMP UNIT A FURTHER DESIGN PAUL COOPER

12volt d.c. portable flourescent lamp unit is a very useful piece of equipment to own—especially in these days of power cuts! This article describes an alternative to the unit described in the December 1973 issue of Practical Wireless. There is the bonus that it is easier to build the circuit on a standard piece of veroboard than to produce a special printed circuit board and, by using a ready made transformer, reduces the cost.

TRANSFORMER

A transformer specifically for '12 volt inverters to run flourescent tubes from car batteries is available from G. F. Milward* for only 50p + post packing & VAT. It saves the time taken to wind the transformer, which is something which might put off the inexperienced amateur from building the project.

The revised circuit diagram is shown opposite.

The circuit is basically the same as in the original article except for the extra tertiary winding on the transformer which is connected in parallel with capacitor C3. The unit will work without this winding connected but in the circuit shown it tunes the transformer thus producing a better output.

It is most important that terminals 1, 2, 3 & 4 of the transformer are connected to the right points on the circuit diagram (as shown by the dots) since if, say, 3 and 4 are reversed the circuit will not oscillate. To cure this, should it occur, connections 3 and 4 should be interchanged and the circuit should then oscillate. (For the complete setting-up procedure see the original article.)

LAYOUT

The Veroboard layout is shown opposite for 0·1 inch matrix veroboard. The board size is the same as for the original printed circuit board so no problems should occur in mounting this board in the completed unit. Note that the fixing hole in this circuit board is in a different place to that of the original board, so a different hole will have to be drilled in the unit case.

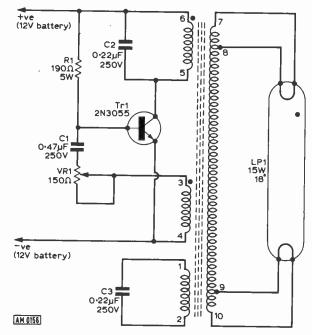
The transformer is fixed to the circuit board by two links of insulated copper wire as shown in the circuit board layout diagram.

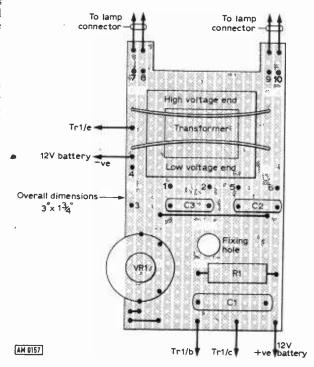
Resistor R1 should be mounted about ¹4in clear of the circuit board and clear from C1 as it gets hot! Since drilling of the holes for the legs of potentiometer VR1 cuts the circuit board tracks completely, care must be taken to ensure contact when soldering the legs in.

Exact values of R1 and VR1 are not very critical. Values were chosen because of availability.

As my unit was built primarily as an emergency light for use in power cuts, the case has been designed to stand on a table with the tube vertical, and it is made of wood.

* G. F. Milward, 369 Alum Rock Rd, Birmingham, B8 3DR.





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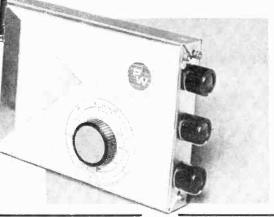
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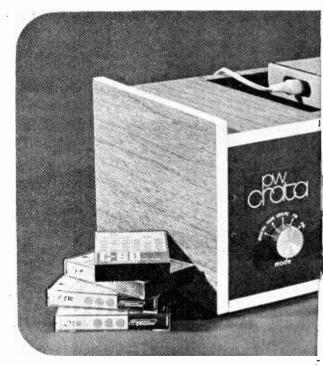
APRIL ISSUE ON SALE IN MARCH

'SIMINE' 5-BAND RECEIVER

This unusual receiver is designed to give five ranges from 160kHz to 27MHz, using simple plug-in coils to cover broadcast and amateur transmissions. Only eight transistors are used, and, with a telescopic aerial the "Slimline" becomes a versatile a.m. receiver to take almost anywhere.



The above details are subject to the current national industrial situation at the time of going to press.



THIS constructional feature describes a stereomultiplex AM/FM tuner-amplifier providing 10 watts RMS output per channel into 80 loads with facilities for incorporating a cassette tape recorder. The integrated unit provides very good results which, although not to true high fidelity standards, will give satisfying listening for a moderate outlay.

Facilities on the prototype included full Band II FM coverage together with one preset AM station and an input for a ceramic cartridge. Additional circuitry and printed boards are shown in this article so that inputs for magnetic cartridge and tape heads can be accommodated, together with record/play-back connections for a cassette or reel-to-reel tape recorder. Additional tuning capacitors may also be fitted along with a selector switch to provide more extensive AM coverage. The AM section uses an internal ferrite aerial, but an external aerial may be added if required. The stereo decoder incorporates automatic mono/stereo switching and stereo beacon lamp drive.

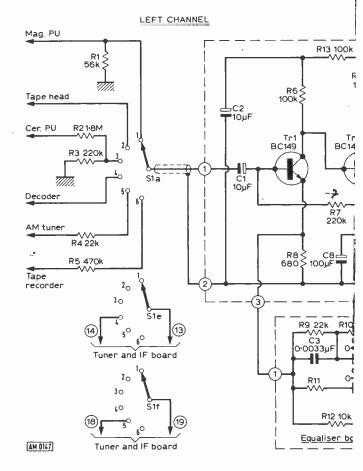
The complete unit is built up on five main circuit boards. The power supply is built directly onto the chassis which is constructed from aluminium angle and strip. The following unit numbers will be used as a prefix to identify components which are mounted off the circuit boards:—

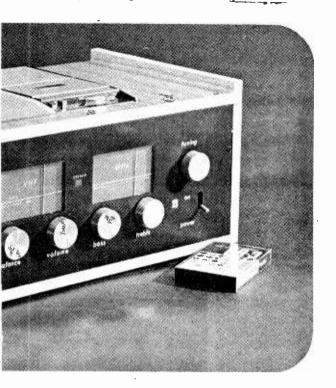
- 1 Pre-amplifiers
- 2 Power amplifiers
- 3 Tuner and IF
- 4 Stereo decoder
- 5 Power unit and input/output sockets.

The front panel is fashioned from 3mm Perspex, using Letraset marking and gives a very professional finish to the unit.

The complete circuit uses 3 integrated circuits, 19 transistors and 7 semiconductor diodes. The FM tuner head is a Mullard module, simplifying construction and greatly reducing alignment problems.

PART 1





RICHARD COLLIN

★ Performance Specification

AMPLIFIER

Power output: 10 watts RMS per channel into 8Ω Frequency response: 20Hz to 30kHz \pm 3dB at full

power 50Hz to 20kHz ± 1dB (power

amplifier)

Channel separation: 54dB at 1kHz and 10 watts
Noise: -60dB at 10 watts (ceramic cartridge input)

Total harmonic distortion: 0.2% at 1kHz and 1

10 Walls

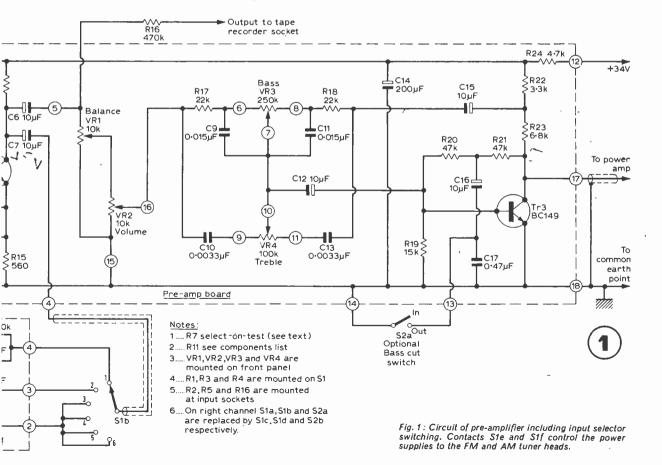
Tone controls: Bass ± 16dB at 50Hz
Treble ± 14dB at 15kHz

F.M. TUNER

Frequency range: 88 to 104MHz Channel separation: 40dB

PRE-AMPLIFIER (UNIT 1)

The inputs from the various programme sources, attenuated and matched as necessary by R1-R5, are selected by S1a (S1c for the Right channel). Transistors Tr1 and Tr2 are connected as a highgain pair and amplify the input signals to a level sufficient to drive the tone control circuit. The bias resistor R7 for the first stage may need to be selected for optimum operation. This will be dealt with in a later part of the article. Its final value should lie between 120 and $270 \mathrm{k} \Omega$.



* components list frate and

		1000	PRI	E-AMPLIFIE	RS	
_ 1	Resis	tors /	and de			1
7	1R1	56kΩ♥	1R10	560kΩ	[R17	22kΩ ✔/
	R2	1.8MΩ	R11	22kΩ for 17ip	s R18	22kΩ❤
	R3	220kΩ		12kΩ for 33ip	s R19	15kΩ + *
	R4	22kΩ		6.8kΩ for 7½i	ps R20	47kΩ
	/R5	470kΩ	R12	10kΩ	R21	47kΩ 💉
4	€ R6	100k Ω	[R13	100kΩ-	R22	3·3kΩ
	R7	220kΩ*	R14	12kΩ	R23	6·8kΩ * •
# #	R8	680Ω	R15	5600	R24	4.7kΩ • •
7	R9	22kΩ	R16	470kΩ	* Se	ee text
	All	resistor	s &W	5% carbon fi	lm	
	VR1	10kΩ	dual li	n V	R3 250ks	Q dual lin
	VR	10kΩ	dual le	oa VI	R4 100ks	2 dual lin

Capacitors

C1	10µF 16V	C7	10µF 16V	C13	3300pF
C2	10µF 16V	C8	100μF 10V	C14	200µF 30V
C3	3300pF	C9	0.015µF	C15	10µF 16V
C4	0.01/4F	C10	3300pF	C16	10µF 16V
C5	0.01µF	C11	0.015µF	C17	0.47µF
C6	104F 16V	C12	10uF 16V		

Non-electrolytic capacitors should be polyester or polystyrene

Semiconductors

Tr1	BC149	Tr2	BC148	Tr3	BC149

NOTE—With the exception of the four dual-ganged potentiometers, two sets of the above components are required for the two channels.

Miscellaneous

S1 6 pole, 6 way, 3 wafer rotary switch S2 DPST miniature toggle switch Pre-amplifier printed circuit board

Equaliser printed circuit board

POWER AMPLIFIERS

Resistors

	R11 0·47Ω 2·5W w/w
R2 100kΩ R7 47Ω	R12 0-47Ω 2-5W w/w
R3 22Ω R8 100Ω 2·5W w/w	
R4 470Ω R9 100Ω 2·5W w/w	
	film unless stated otherwise
VR1 50kΩ	

VR2 100Ω miniature presets (horizontal mounting)

Capacitors

C1 25µF 25V	C4 0.01µF 100V	C7 200µF 30V
C2 47/1F 40V	C5 0.22 F 100V	C8 1,500µF 25V
C3 1.000 uF 25V	C6 0.001 µF 750V	C9 0.047µF 100V

Samicanductors

Tr1	BC158	Tr4	2N6288	(RCA)
Tr2	BC148	Tr5	2N6111	(RCA)

Tr3 2N6288 (RCA)

Tr3, 4 and 5 are supplied with the necessary mounting hardware

NOTE—Two sets of the above components are required for the two channels.

Miscellaneous

Printed circuit board. Heat sinks and brackets (see Figs. 8 and 9)

NOTE—RCA Semiconductors for this project are available from E.C.S. (Windsor) Ltd., Thames Avenue, Windsor, Berks.

Total requirements are: 2 2N6111 at 50p

5 2N6288 at 54p

1 CA 3089 E at £1.96

CA 3090 Q at £4 · 23

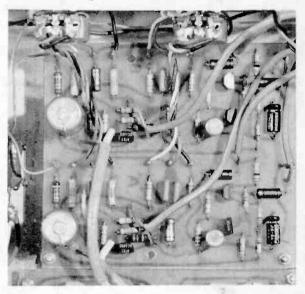
Add 40p post and packing per order and 10% VAT

Feedback around Tr1/Tr2 provides high stability and is also used to set the gain and, for the magnetic pick-up and tape-head inputs, the frequency response. The appropriate feedback path is selected by S1b (S1d for the Right channel). The value of R11, which with C5 provides equalisation for the tape-head input, must be chosen according to the tape speed to be used.

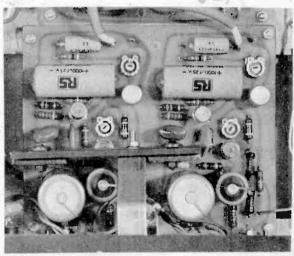
A constructor not requiring the full complement of input facilities may of course omit the unwanted circuitry and connectors.

An output is taken via R16 for connection to a tape recorder, allowing recording of a programme being played through the amplifier (subject to the provisions of the Copyright Act, 1956). The signal at this point is equalised but is unaffected by the Volume and Tone controls. Because of the high value of R16, the two channels can be paralleled at the input of a mono recorder with only slight worsening of stereo crosstalk within the amplifier.

The tone controls are in the familiar Baxandall configuration, providing both lift and cut at bass and treble frequencies. Transistor Tr3 is the active

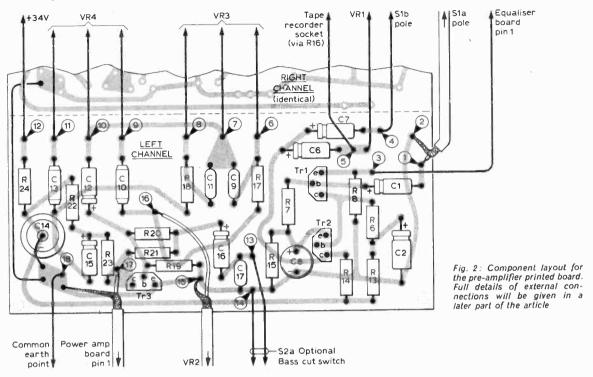


Prototype boards for the pre-amplifier (above) and power amplifier (below)



element of this stage and also makes up for the losses incurred by the frequency selective circuits. A bass cut or rumble filter may be provided by removing the short circuit from across C17.

Ensure correct polarity of the electrolytic capacitors when assembling the circuit boards. In the R7 position fit $220k\Omega$ resistors, leaving the wires long as the value may need to be changed later. Once



AM 0148

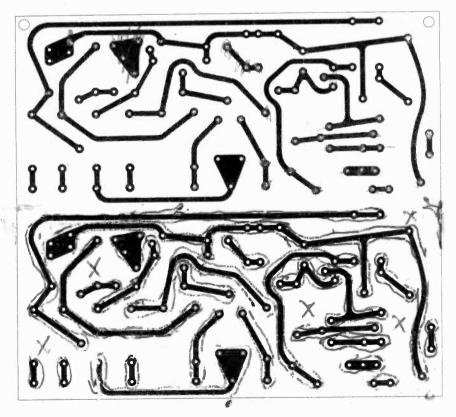
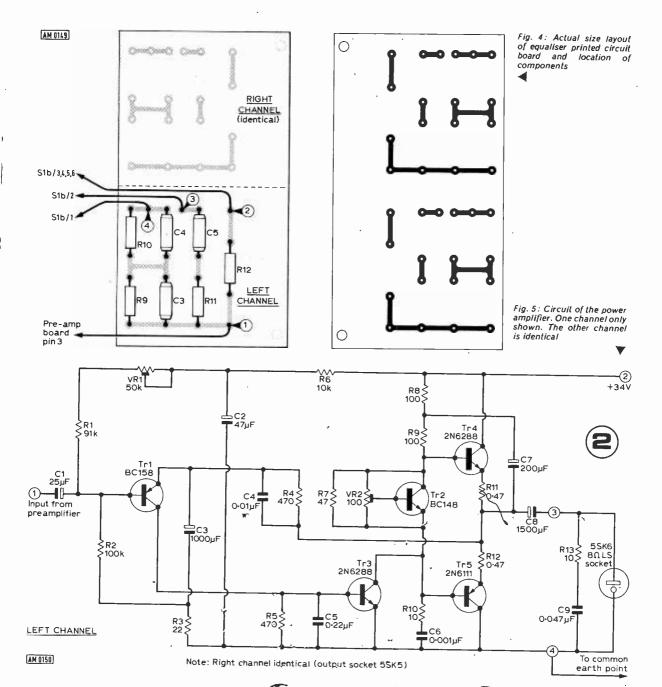


Fig. 3: Actual size layout for the pre-amplifier printed circuit board



complete, these boards may be placed in a safe place until the chassis and power unit are completed. A number of components included in the pre-amplifier circuit diagram are not mounted on the boards. These are dealt with in a subsequent part of the article.

POWER AMPLIFIER (UNIT 2)

The familiar complementary—symmetry configuration is used and designed around silicon transistors. Good low frequency response and stability is ensured by the use of DC coupling throughout the amplifier. The output pair, RCA plastic packaged 'Versawatt' devices, deliver 10 watts RMS into an 8Ω load. A similar device Tr3 operates as a class 'A' driver.

The small forward bias required to minimise crossover distortion is provided by a small signal transistor Tr2 connected between the bases of the output
pair. The first stage Tr1 provides amplification of
the input signal and in addition acts as a DC comparator, enabling the output stage to be set up for
symmetrical clipping under overload conditions. The
DC potential at the output mid-point is connected
to the emitter of Tr1 via R4. The base potential
of Tr1 is determined by the potential divider R1,
R2, VR1 and R6. The high loop gain of the circuit
keeps the small difference between Vh and Ve constant, so that the output mid-point volti ge is defined
by the base potential of Tr1 regardless of component
tolerances. Negative feedback is provided by R4, C3
and R3.

Fig. 6: Component location for the power amplifier printed board

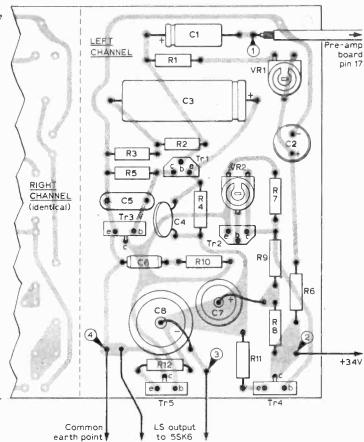
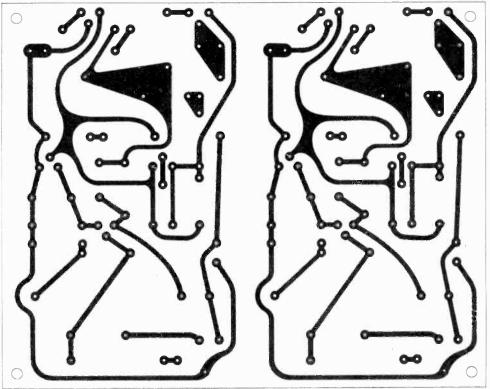


Fig. 7: Actual size layout for the power amplifier printed circuit board





-continued on page 1080

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*Uniquely handy package. $4\frac{1}{2}$ " x 2" x $\frac{11}{16}$ ", weight $3\frac{1}{2}$ oz. *Standard keyboard. All you needforcomplex calculations. *Clear-last-entry feature. *Fully-floating decimal point. *Algebraic logic. \times Four operators $(+, -, \times, \div)$, with constant on all four. *Constant acts as last entry in a calculation. *Constant and algebraic logic combine to act as a limited memory, allowing complex calculations on a Cambridge calculator costing less than £30. *Calculates to 8 significant digits, with exponent range from 10^{-20} to 10^{79} *Clear, bright 8-digit display. *Operates for weeks on four U16-type batteries. (MN 2400 recommended.)

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The kit comes to you packaged in a heavy-duty polystyrene container. It contains all you need to assemble your Sinclair Cambridge.
Assembly time is about 3 hours.

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- 6. Printed circuit board.
- 7. Keyboard panel.
- Electronic components pack (diodes, resistors, capacitors, transistor).
- Battery clips and on/off switch.
- 10. Soft wallet.



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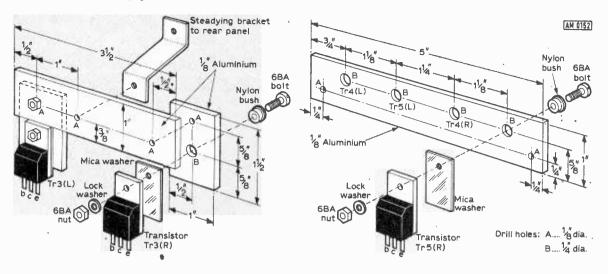
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Fia. 8: Design and assembly of driver transistor heatsink

A Zobel network C9/R13 is connected across the output terminals. The purpose of this network is to ensure that the loudspeaker load always appears essentially resistive to the output transistors. This means that the output stage is protected against inductive transients which could exceed the breakdown voltage of the transistors.

Fig. 9: Design and assembly of output transistor heatsink

PART 2 next month will describe the Tuner/IF and FM Decoder units





ACROSS

- Employs a coupling of ferrous esters (4)
- A shakerin the transformation scene (8)
- A stick-up in the rockery (4)
- 10 Radio engineers meet with such resistance? (8)
- Come back to fix a little drink (3)
- 19 The Spanish miss her in the end (4)
- 13 Already fixed on the wavelength? (3-3)
- 14 A key piece of mechanism (4)
- As familiar as Liz (4) 15
- 17 Bell's slowest ringing tone (4)
- 20 Basso loudspeakers amplify this single? (4)
- How to dispense with an earth! (6) You talk nonsense about defeat (4)
- 94 Dipole once connected with him! (3)
- If about to bewail a valve component! (8)
- 27 Not so hot in acoustic editing (4)
- 28 Salty type's crystallization at the mike! (8)
- Collections of old wirelesses (4)

DOWN

- Land in court with such maintenance? (7)
- Glass in pieces from these transmissions? (7)
- Jim pleased about the little rascal (3).
- The longest-ever tape? (6)
- They're well up about antennae (5)
 A composed musical performance (7)
 Such a charge about a cathode? (5)
 The more hearty kind of con-man (7)
 Birds do such load-shedding? (5)
 Do rlots break such colls? (7)
- 15
- 16
- 18 Told Sue about being so noisyl (7)
- More I'd swap for a position in golf (6) Classification of a crystal-set? (5)
- Nickel-coating is zero-rated? (3)

FOR AMUSEMENT ONLY ANSWERS NEXT MONTH

ON RECENT DEVELOPMENTS

WATCH IT!

AM looking at a Swiss electronics journal. There's a circuit which uses two ICs, a readout chip, and a one-transistor oscillator. Connected together they form an electronic clock complete with digital readout. The only circuitry which needs "building" is the single transistor oscillator and this comprises five resistors, five capacitors, a crystal and one of the ICs mentioned. For the record, the two chips are the SCL5437F (oscillator) and SCL5424F which drives the liquid crystal readout direct.

UNIVERSITIES HELP

One of the major criticisms levelled at universities is that their experiments are all too often of academic value only. While this may be true in some instances, it certainly is not true in the case of the University of Utah in the U.S. This establishment has a section devoted to making blind people see again. Although in the experimental stages, blind people have been able to see light patterns which have been simulated by an external "eye" and fed into their brains by small electrodes.

The light images or patterns are called phosphenes and are stimulated (in these experiments) by the generation (and careful control) of pulses, in other words, the vision has been created by purely electronic means. The width of the pulse and its duration determined the intensity or "shades" of the image which the totally (otherwise) blind person can "see". Researchers see no reason why some form of imaging device (like a solid state t.v. camera) should be used and the impulses fed into the brain-after suitable processing, of course. This latter idea is well within the realms of readily available electronics which one can obtain today.

Embedded image sensors could even be controlled by the eye muscles themselves. Already.

computer-generated images have been drawn quite accurately by a totally blind person. The image was viewed on a c.r.t. so that a fair comparison could be made.

If you know of a blind person, it would be unkindly premature to mention these experiments with too great an enthusiasm because it may well take many years to perfect it into a practical device.

A TOOTHGRAPH?

Still in the realms of medicine—well, almost, is the latest use of lasers. Now, the dental profession have taken an interest. By using a small laser it is possible to take holographic photographs of a person's teeth. One interesting thing to emerge from this useage is not that it will offer an invaluable aid in dental practice (although this is very true) but its use for security purposes. Apparently no two peoples teeth are the same so instead of fingerprints one could have toothgraphs or teggypix.

Criminals of the future will do well to heed the old addage—when in doubt, keep your mouth shut. In any case the idea should give Scotland Yard something to get its teeth into.

LARGE-SCREEN COLOUR

Perhaps one of the most interesting battles currently being fought is the one for television screens/tubes/systems. All sorts of ideas are currently under examination including a flat screen solid state beasty. News has arrived about another contender. This one is called a Video-Beam projector and houses optics inside the colour tubes. It shows promise for large screen colour television and claims the advantages of doing away with colour dots, lattices and shadow masks.

Each electron beam (one for each of the three colours) is fired at a "target" which has the relevant colour phosphor. This beam is reflected back inside the tube of a concave mirror which in turn reflects the image out of the tube onto the screen. Extremely good results are reported, however,

there is a snag—the projection distance is fixed at eight feet and is unalterable. The company working on the device do not see this as a problem and claim that once the colour tube "projector" has been adjusted at the manufacturing facility, it requires no adjustment or fiddling by the user.

No mention is made of the power requirements but one presumes that they are considerably lower than the 25–30kV needed for the earlier black-and-white projection systems where many people expressed concern about radiation from such a set up.

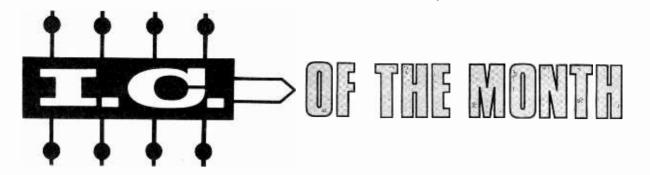
MULTI- CHIPS

A new IC chip, the 2240, is claimed by its makers to do just about anything. It is currently hailed as a programmable timer, binary counter, music synthesiser, A/D converter, ultra-long delay generator, digital sample and hold circuit, frequency synthesiser, pulse counter, binary pattern. generator, precision oscillator... etc., all in one innocent looking sixteen-pin dual in-line package. I have contacted the company with a view to obtaining further information which I will pass on as and when it arrives. It may be possible to include some circuitry of the more practical applications for the home constructor.

BIG CHIPS!

Remember the days when semiconductor devices were fragile and sensitive to fluctuations in power. Contrast that with the latest beast from International Rectifier. This is a silicon controlled rectifier which handles 2,500 Amps r.m.s. at up to 1,200 volts. A 2,000V version is already planned. The wafer for this device is almost $2\frac{1}{2}$ inches in diameter. This is probably the largest chip which has ever been employed in any semiconductor device.





Number 44

National LM377N 2 + 2W AUDIO AMPLIFIER

HE LM377N is an IC, manufactured by the National Semiconductor Company, which contains two separate two-watt amplifiers in a single device. The connections are shown in Fig.1. A 14 pin dual-in-line encapsulation is employed which can be fitted into a socket or soldered into a printed circuit board. A similar device, the LM377N-10, has metal tab connections which may be soldered to a printed circuit board. Pins 3, 4 and 5 and also 10, 11 and 12 of Fig. 1 are replaced by metal tabs on each side of the device. These are very convenient for soldering to a heat sink.

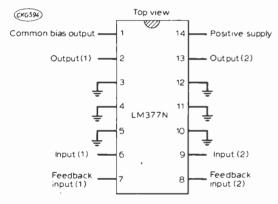


Fig. 1. Pin connections to the 14 pin DIL LM377N.

The LM377 devices are intended mainly for use in stereo equipment where the output power required does not exceed 2W. However, they can also be used in a bridge circuit where the two amplifiers in the device are used in push-pull to provide a monaural output of up to 4W.

Advantages

The following features make the LM377N especially attractive to the amateur constructor as well as to the professional circuit designer:—.

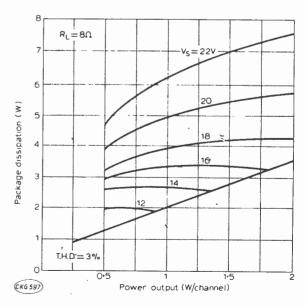
(i) The output stages are automatically centred at the correct bias so that the output voltage can swing an equal amount in either direction resulting in maximum power output at a given distortion level. (Some power amplifiers circuits require a preset potentiometer so that the bias can be adjusted manually.)

- (ii) The LM377N contains internal circuits which protect it from overheating. If the silicon chip becomes too hot, the device switches itself off until it becomes cooler.
- (iii) Protective circuits prevent the device from being damaged by excessive current. Such currents are likely to flow if either of the outputs is accidentally shorted to earth.
- (iv) The input impedance is relatively high, 3MΩ, and this increases the versatility of the device.
- (v) Any hum on the power supply line is reduced by 80dB. The separation between the two channels is typically 70dB.

Circuits

In all circuits the inputs of both amplifiers should be biased by the voltage from pin 1. The bias current is typically 0.5μ A to each amplifier.

In addition, feedback from each output should be applied to the feedback input of the same amplifier. The amount of feedback controls the gain.



Graphs relating supply voltage to output power for the LM377N.

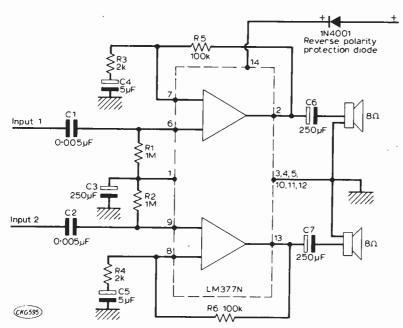


Fig. 2. Circuit of a practical stereo amplifier suitable for a record player. A volume control will be required on the input circuit.

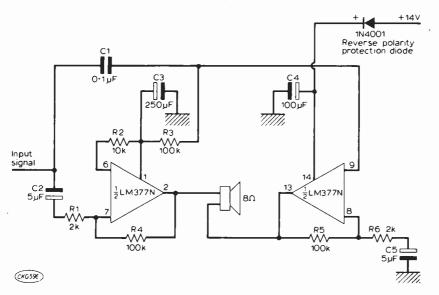


Fig. 3. This mono circuit utilises both amplifiers to provide 4W output.

A typical circuit for the use of the LM377N as the two power amplifiers of a stereo system is shown in Fig. 2.

Bias from pin 1 is decoupled by C3 and applied to the inputs at pin 6 and 9 via R1 and R2. The input signals are capacitively coupled through C1 and C2 respectively in order to prevent the bias from being affected by the impedance of any previous stage. The input impedance of the LM377N is relatively high and therefore the coupling capacitors can be fairly small in value.

In the upper amplifier of Fig. 2, the feedback is taken from the output at pin 2 through R5 to pin 7. The voltage gain is equal to R5/R3 which is 50 times or 34dB. The gain may be increased by reducing R3 but the distortion will increase.

Similarly, the gain of the lower amplifier is R6/R4=50. The typical gain of an amplifier without any feedback is 30,000 (90dB).

The mean output potential is equal to approximately half the supply voltage. An electrolytic capacitor (C6 and C7) must therefore be placed between the outputs of the device and each speaker so that direct current cannot flow. If the value of the capacitors is reduced, an inferior bass response will be obtained.

Power supply

The LM377N can be fed from a supply line having any value between 10V and 22V. The absolute maximum supply voltage is 26V, but one should always allow a safety margin to avoid the risk of damage to the device.

A current of about 15mA is taken from a 20V supply when no signal is applied to either input, but the current rises towards 1A when full output power is being delivered to the speakers.

The maximum output power which can be obtained from each channel depends on the supply voltage used and also by the speaker impedance. A typical LM377N provides 2·5W per channel when fed from a 20V supply into 8Ω speakers, whilst all devices should provide a minimum of 2W per channel under these conditions.

The LM377N can dissipate up to about 2.5W continuously without a heat sink, but if the centre pins

of the device are soldered to $2\cdot 5$ sq. in of copper on a printed circuit board, the maximum dissipation is increased to about $4\cdot 2W$. Some form of heat sink seems required when an 8Ω speaker is employed, unless the power supply voltage does not exceed about 14V. In practice, however, the device is seldom operated at maximum power level for more than a moment (unless one likes to listen to sine waves!). Normally one is not likely to require a heat sink when using supply voltages of up to 18V provided that the speaker impedance is not less than 8Ω .

Mono Amplifier

A single LM377N device can be used in a single channel system to provide an output power of 4W, Fig. 3.

continued on page 1086

PRESELECTOR for

10-30MHz

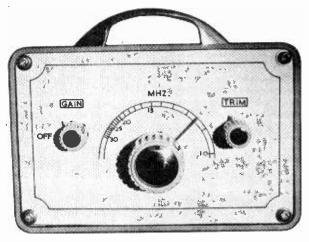
F. G. RAYER G30GR

ANY receivers are susceptible to second channel interference when working on the higher frequencies. This means that if the receiver employs an intermediate frequency of 470kHz, the oscillator is working at a frequency 470kHz higher than that of the wanted transmission and signals which are 470kHz higher than this, or 940kHz higher in frequency than the wanted transmission, can beat with the receiver oscillator frequency, to produce a signal which passes through the 470kHz amplifier, interfering with the wanted signal. On the lower frequencies, there is usually sufficient selectivity ahead of the mixer to avoid difficulty from this cause. But on higher frequencies, the receiver is unable to totally eliminate the offending signals which cause interference and whistles.

Even a well-designed receiver with one RF stage may not provide second channel rejection better than 15dB at 30MHz. If a signal strength scale of 6dB per S-point were used, as is quite usual, this would mean that if a wanted signal read S9, an unwanted signal of equal strength 940kHz higher in frequency would read S6+, which is a severe level of interference.

Such interference can be greatly reduced by raising the receiver intermediate frequency, or by increasing the second channel rejection ahead of the mixer. Changing the IF is probably impossible, but the unit here will enormously increase the second channel rejection.

The maximum benefit will be found with receivers which have no tuned RF stage, or only one RF stage, and employ a 455-470kHz intermediate



Completed preselector in its 6x4x4in cabinet.

frequency. With such receivers, 19m broadcasts may greatly mar reception of 20m amateur signals, for example. The unit can also be employed with other receivers including those with a 1.6MHz or other IF.

CIRCUIT

This is shown in Fig. 1. As second channel interference is not usually troublesome at signal frequencies lower than about 10MHz, the unit covers approximately 10MHz to 30MHz in a single band, thus avoiding any need for band switching. L2 and

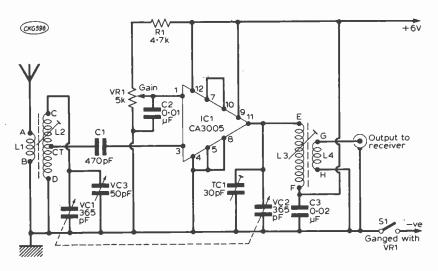


Fig. 1. Circuit of preselector using a single integrated circuit. Input, output and battery connections are at the rear. When placed between aerial and receiver useful gain will result as well as a reduction in second channel interference.

L3 are tuned with the ganged capacitor VC1/VC2 providing two extra tuned circuits before the receiver. In most cases this will almost completely eliminate second channel interference. VC3 is a panel trimmer to allow peaking the aerial circuit with almost any aerial.

The CA3005 IC operates with a 6V supply. It is listed as giving 20dB gain at 100MHz, but the full gain is not achieved here due to the circuit being arranged for operation from a single power supply, and because of the difficulty of matching the input and output impedances at all frequencies. The input is approximately matched by the centre tap on L2, while the transformer L3/L4 is arranged to give an output impedance suitable for most receivers.

Gain control is provided by VR1, to avoid overloading the receiver on strong signals.

IC BOARD

The board is wired as in Fig.2. Note that the projection on the IC corresponds to lead 12. Spread the leads slightly so that they may pass through the Veroboard holes as indicated.

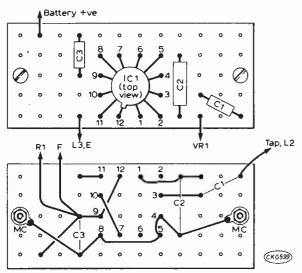


Fig. 2. Both sides of the small circuit board that carries the IC.

Two 6BA bolts with tags form the earthing points MC. Leave projecting leads from C1, for battery positive, VR1 and for VC2. Also solder on R1.

COILS

These use 24swg enamelled wire throughout, Fig. 3. For the aerial coil, begin at C as near the top of the former as possible, and wind on 4^{1}_{2} turns. Scrape the wire and twist the centre tap. Wind a further 4^{1}_{2} turns and finish at D. Leave a small space and beginning at A wind on 4 turns, finishing at B.

For the second coil, wind 9 turns from E to F, leave a space as before, and put on 5 turns from H to G.

The ends of the windings can be secured with a loop of cotton lightly smeared with quick-drying adhesive, and given a turn or two round the former. Fix one end by this means, wind on the turns mentioned, and secure the finish of the winding in the same way, pulling it tight by the cotton.

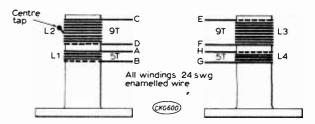


Fig. 3. Details for winding the two coils used in the preselector.

CHASSIS

The panel for the case listed is approximately 6 x 4in. Punch a clearance hole for the spindle of VC1/2. As this capacitor has an integral drive and the spindle cannot be cut shorter, it can be spaced back from the panel as in Fig. 4, to bring the knob nearer the front. This requires three 4BA bolts, each with two nuts, locked against panel and capacitor. VR1 and VC3 are also set back a little by extra nuts or washers.

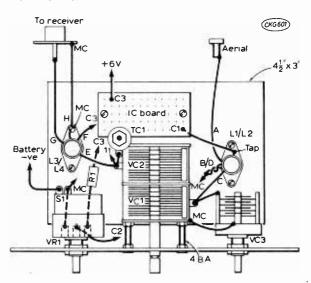
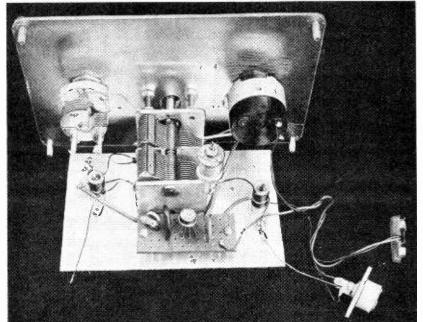


Fig. 4. Top view of the chassis showing position of the IC board and major components.

The chassis is a flat plate 4^1_2 x 3in. It is secured by two short 4BA bolts which pass through it and into the threaded holes in the capacitor frame. Place a few washers between plate and capacitor.

★ components list

Resistors R1 4·7kΩ ±W VR1 5kΩ linear with switch S1. Capacitors C1 470pF, C2 0·01μF disc C3 0·02μF disc. VC1/2 2 x 365pF with slow motion drive. VC3 50pF (Jackson C804) T C1 30pF trimmer. Miscellaneous Formers for coils, πin dia. with cores (2). Knobs. ICI, CA3005. Aerial socket and output socket. Instrument case about 6 x 4 x 4 lin.



Holes are drilled to take the circuit board bolts which are locked with extra nuts. Wiring must be clear of the metal. The coils are held with 8BA bolts and nuts.

WIRING

Wiring is then completed as in Fig. 4. TC1 has its lower tag soldered directly to the frame of VC1/2, the second tag being connected to VC2, together with the lead from pin 11, IC1.

The coil leads are cut to length, scraped, and soldered to the points shown. Note that H goes to the chassis at a bolt securing L3/L4.

The battery consists of four HP7 or similar cells, in a 4-cell holder. The holder is secured in the back of the insulated case, near the top, by a small bolt.

Finished preselector. Flexible connections are made to battery connector and output socket.

As the receiver employed a co-axial lead, a socket for this was provided as in Fig. 4. An earth circuit to the unit is then available through the co-axial outer conductor. If the receiver does not employ this type of aerial input lead, take a wire from G, L4, to the receiver aerial socket, and connect H and the chassis to the receiver earth terminal.

OPERATION

TC1 can be set at about half maximum capacitance. Tune in a transmission on about 10MHz, set VC1/2 nearly fully closed and rotate the cores of the coils for best reception.

Subsequently check that 30MHz signals peak with VC1/2 nearly fully open, and that VC3 also peaks up signals or background noise. If necessary, readjust TC1 to allow proper tuning with VC3, and check the core positions, so that little adjustment of VC3 is required, when tuning across the whole

Adjustments are best carried out by observing the receiver signal strength meter, or with the receiver AGC switched off, or by selecting weak signals which do not operate the receiver AGC. VR1 should be set for maximum gain when doing this. As an aid, a very short aerial may be temporarily taken to A. VC3 should then have quite a sharp peak, but this effect will be reduced with a long aerial when it may be preferable to place a small capacitor in the lead from aerial to A.

IC of the Month—continued from page 1083

The two amplifiers are used in a 'bridge' or pushpull circuit. The input signal is fed through C2 and R1 to the feedback input (pin 7) of the first amplifier and the same signal also passes through C1 to the non-inverting input (pin 9) of the second amplifier.

When the voltage at the pin 2 output increases, that at pin 13 therefore decreases by the same amount and vice-versa. The speaker is thus driven by this push-pull signal. This circuit has the advantage that no capacitor is required in series with the speaker, since the mean potentials of pins 2 and 13 are almost identical.

The bias from pin 1 is decoupled by C3 and fed through R2 to pin 6. It also passes through R3 to pin 9.

The gain of each amplifier is equal to the ratio of the feedback resistors, namely R4/R1=R5/R6=50. However, the push-pull action gives an effective overall gain of twice this value.

The LM377N is available from Athena Semiconductor Marketing Company Ltd., 140 High St., Egham, Surrey, at £2·70 plus VAT for small quantities, inclusive of p & p.

RADIO BY CABLE & SATELLITE

-continued from page 1087

Many countries have determined that this is unavoidable within the boundaries of the technical possibilities and it has been recognised by the UNO associated International Telecommunications Union in 1971 in Geneva. At the same time, however, it was established that the use of TV satellites is only possible by observing frequency, positioning and ground coverage plans which are to be drawn up at a special planning conference for this purpose which will take place in 1975/76.

EXPERIMENTAL WORKSHOP

We regret that due to pressure on editorial space this month, Part 6 of this series has been held over until the April issue.



LTHOUGH it is a task of exchange technology to handle the signals, in connecting individual communications (telephone, telex), in such a way that the connection is made quickly and reliably, broadcasting must ensure that the primary signal is transported long distances without distortion, be they telephone signals or for telegraphy, music, TV, picture transmission, data transfer or remote control. But what are the problems that arise?

A modern carrier frequency system with 2700 channels for speech has an amplifier spacing of $4.5~\mathrm{km}$; at a distance of 4500 km as is found in the trade area between the USA and Canada, 1000 ampli-

fiers are operated one after the other.

Assuming a medium amplification of 30dB (i.e. the signal output is increased each time by a factor of $10^3 = 1000$, the voltage by around a factor of $31 \cdot 6$) the overall amplification over the whole section amounts to the almost unbelievable figure of 10^{3000} . For comparison: the entire universe contains "only" around 10^{83} protons, since the creation of the earth approximately 15 billion years ago a total of "only" $5 \cdot 10^{17}$ seconds has passed.

Cables

To guarantee the necessary quality over so many stages, extremely high demands must be made, both on the technical equipment (amplifiers, converters, modulators etc.) as well as on the directions of transmission. With regard to the latter there are three "media" which have proved themselves and which are to be found predominantly or exclusively in long-distance traffic: cables, directional radio including satellites and—as a medium of the long-term future, suitably directed laser beams.

Cable, especially coaxial, is already considerably protected by its construction and laying against outside influences from space, the atmosphere and from technical installations, so that in cable transmission systems non-linearity and noise must be kept as low

as possible.

Disregarding the "symmetrical" carrier frequency cables, used predominantly with up to 120 speech channels for regional systems, there is a whole series of coaxial types at an impedance of around 75 ohm. There are many various internal sizes, e.g. from 1·2 mm for 300 speech channels or 2·6 mm for a choice of 960,1260 or 2700 channels. If one is prepared to reduce the amplifier spacing even more, one could increase the basic bandwidth considerably (e.g. to 40 to 60MHz or even higher).

"Hollow" cable recently developed can theoretically provide a transmittable overall bandwidth of around 100,000MHz. It is, in fact, a radio wave guide which should be most suitable for the transmission of digital signals (e.g. for pulse code modulation). Technically hollow cables are well advanced although there are certain reservations with regard to their economic application.

Satellites

The directional radio line, widely used for the transmission of TV modulation (video band) but also for multi-channel speech bands, is physically an ideal transmission medium. However, it requires the application of special "noise reducer" procedures due to the influences of extra-terrestrial, tropospheric and industrial radio signals. Partial bandwidths of up to 30MHz have shown themselves to be the best for the transmission of television or telephone channels in various frequency ranges between 2 and 12GHz. Transmitter output is in the area of several watts.

Satellite paths are basically extended directional radio lines with fields of 2 x 36 000 km length (to and from) with high transmitter outputs, extra large aerials and extremely sensitive receivers (maser) on the terrestrial stations. They are particularly suitable for trans-continental and trans-oceanic relays, operating at frequencies corresponding to those in directional radio technology.

A transmission medium of the future is the laser beam which is strictly monochromatic, polarised and coherent. In a free field of dissemination they are not practicable because of absorption as with normal light, but when suitably guided by lens conduction

and glass fibre, it reveals its full potential.

In particular the glass fibre bundle cable, offering an extreme bandwidth even with individual fibres, combined with the multifarious operating possibilities of universal cable, promises to be an important transmitting medium, both in long distance communications and in local traffic in densely populated areas. All of this is of course dependent on a corresponding advance in the components and subsystems in the field of optronics—an advancing technology being fully exploited now.

Satellites providing a country with programmes via only one transmitter can of course be received across borders. Even with rays with a one degree focusing, whose focal area is accommodated within the boundaries of the country cannot prevent this.

-continued on page 1086

Oscilloscope

PART 1

techniques alan ainslie

N this series we shall be taking a close look at oscilloscopes of the kind likely to be used by the average electronics enthusiast. This leaves a large range of classes of instruments, but we shall not be too concerned with the developments incorporated in the brand new, four figure price oscilloscopes as these can generally be classed as purely professional in appeal and application.

The instruments to be considered will range from the simplest types of scope, through TV service scopes to the laboratory scopes of a few years ago, now available to the keen amateur—but at a price!

We shall consider design principles, the basis for modifications, and calibration. This last point is rather important as manufacturers can charge a lot for recalibration of their instruments, especially if not of current manufacture.

We shall also look at some oscilloscope applications and at a few pieces of additional equipment in order to carry out an increased range of tests and measurements.

Oscilloscopes fall broadly into four main classes:-

- 1. AUDIO FREQUENCY
- 2. TELEVISION AND PULSE
- 3. LABORATORY
- 4. SPECIAL PURPOSE

Ignoring the special purpose scopes for the time being, the oscilloscopes are grouped into a convenient scale of ascending bandwidth.

BANDWIDTHS

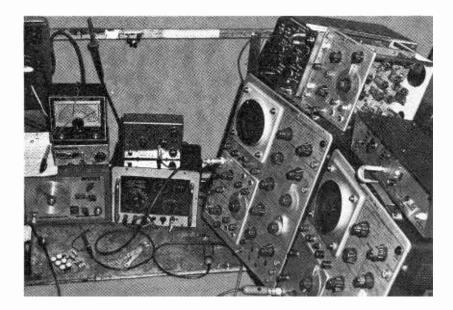
As most scopes have a low frequency limit of DC (DC coupled) or a few Hz, the bandwidth figure quoted is the upper frequency limit at 3dB down (or however else the manufacturer specifies).

The bandwidth information gives an indication of the highest frequency that the scope can predictably handle.

Considering the two curves in Fig. 1, both scopes would have a written bandwidth of 5MHz, but scope A would in fact perform quite well past this figure whilst scope B drops straight off. Scope A could be used but with loss of calibration up to perhaps 10MHz or so, scope B being totally useless at this frequency.

Incorporated in any statement concerning bandwidth is an implication of the rise time of the scope.

If we consider an oscilloscope amplifier displaying a 1MHz signal, and this signal is at the -3dB point, we can arrive at some justification for the rather mysterious equation used to express rise time in terms of bandwidth.



This imposing array of test equipment in just one corner of the author's workshop will serve to underline the fact that this series of articles on the oscilloscope contains much practical information as well as theoretical discussion.

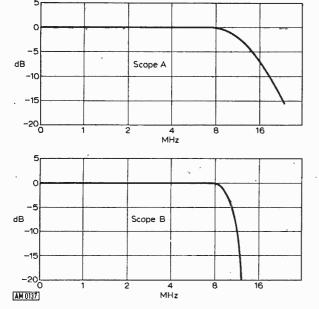


Fig. 1. The response curve of the Y amplifier in two different oscilloscopes, to illustrate the meaning of "bandwidth."

The time period of the 1MHz signal is 1μ sec. Thus for one half period the time is 500ns and for the rising portion 250ns. If now the slope of the upward going part of the cycle is taken to represent the step function applied to the scope, then the rise time of this 1MHz (3dB down) scope would appear to be 150ns.

But the 1MHz signal is not of 100% amplitude (it is 3dB down), and as rise time Tr is defined as the time to increase a step function from 10% to 90%, a correction is required, Fig. 2.

As 3dB down corresponds approximately to 30% down, i.e. the trace height at the -3dB point is only 70% of what it should be.

It is necessary to bring the 70% trace to 90% and in doing this Tr is increased by 90/70 giving a theoretical rise time of 322ns.

In practice the figure is found to be between 350 and 390ns, depending on the shape of the response. The response curve of Fig. 1, scope A would give a faster rise time than that of scope B, although both have the same bandwidth.

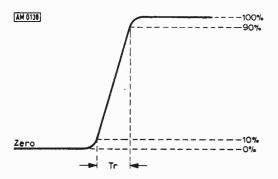


Fig. 2. First part of a response curve with a step function input to the scope. The rise time is a function of the bandwidth of the amplifier.

Taking the rise time to be 365ns for a 1MHz scope and applying the laws of proportion we get the expression:—

Rise Time (ns) \times Bandwidth (MHz) = 365

This expression holds true for the vast majority of cases, but more about that when we come to consider the Y amplifiers in more detail.

Returning to our classification of oscilloscopes it seems reasonable that the audio oscilloscope has but a limited bandwidth (1MHz or so) while the TV or pulse oscilloscope has a bandwidth of perhaps 10 or 15MHz and is capable of displaying more complex and more rapidly recurring waveforms. The laboratory scope on the other hand has a bandwidth extending from 15MHz and up and into the hundreds of MHz on the very latest real time oscilloscopes.

Using sampling techniques (imaginary or virtual time) bandwidths into the GHz region have been achieved but this type of scope belongs to the special purpose class. It is interesting to think of the real time response of say a 5GHz scope, 10~% to 90% in $7~\times~10^{-11}$ sec, quite fast!

Returning to earth, although it is convenient to classify a scope by bandwidth (or rise time) there are other, perhaps more striking, differences between the classes of scopes.

TIMEBASES

The uses of an audio oscilloscope are confined usually to periodic waveforms that can be adequately displayed by the use of a synchronised time-base without the need for complex and expensive trigger circuits. The difference between a sync or trig timebase will become clear when we come to consider more fully the numerous methods used to provide a timebase. Suffice to say that the sync timebase is a free running oscillator which is pushed along by a portion of the Y signal applied as sync, whereas the trig timebase waits for a suitable signal before commencing a sweep.

One consequence of the sync mode is that the input signal (Y) must have a repetition frequency higher than that of the timebase for a stable image to result, as in Fig. 3. If the timebase is run faster than the repetition rate of the waveform, in order to view detail the trace folds up into a jumble.

Applied to the audio scope this latter effect is not of too great a consequence as there is usually little detail lurking in a signal repeating at 10kHz. However in TV work we immediately become faced with complex waveforms to lock and also the possibility that the waveform may be required to be investigated more closely.

The triggered timebase becomes a necessity together with the improved Y amplifier bandwidth. The timebase speed ranges are also increased for greater versatility and various modes of timebase operation are employed, including the important addition of an "EXTERNAL TRIG" connection enabling the timebase to be controlled externally. This facility is invaluable in TV work as it enables the frame generator in the receiver to work as a delay timebase generator, the trig level control on the scope selecting the lines to be viewed in isolation on the screen.

This sort of facility necessitates yet another improvement to be made to the simple audio scope, namely the trace brightness.

Fig. 3. The top display occurs when the timebase runs faster than the repetition rate of the input waveform. The consequence of a timebase running slower than the repetition rate is shown in the lower display.

A recurring 1kHz sine wave may be bright enough, but when the trace is scanning say 10cm in 64/sec, and then only 25 or 50 times a second, the trace brilliance falls to almost vanishing point unless high CRT potentials are employed. Usually between 2 and 5kV are used on oscilloscopes of this nature, as opposed to possibly less than 1kV for the audio scope.

The TV or pulse oscilloscope then has, apart from an improved bandwidth, a fairly sophisticated timebase system and an improved

system and an improved display mechanism, together with a few other improvements such as DC coupling and the provision of calibrators.

Oscilloscopes intended for reasonably accurate measurement, but that are built to a price, usually incorporate some method of generating standard waveforms of precise voltage and/or time, this being cheaper than trying to stabilise the Y amplifier gain and timebase against variations.

A fairly typical example of the type of calibration provided is the Cossor 2000 oscilloscope, a 5MHz double beam scope suitable for general TV service and measurement.

The Y amplifiers are calibrated against an internally generated signal of 300mV. The Y amplifier control is set to give 3cm deflection with the input attenuator set at 0.1V/cm.

The 300mV signal is obtained from 50Hz from the scope mains transformer and a small neon is used to provide a reference level of about 70V from this high voltage AC. The resulting 70V square wave is then attenuated and is available as the 300mV calibration signal.

Time calibration is available as a 20MHz oscillator providing intensity modulation of the beam. This means that a display brightens up at every 50ns enabling accurate time measurements at the higher sweep speeds.

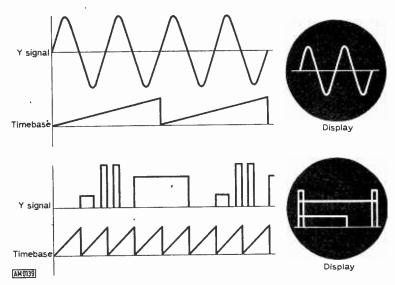
LABORATORY SCOPES

The final class of scope that we shall consider is the laboratory scope and in this class we can conveniently consider the special purpose oscilloscopes.

In general one expects to find that a laboratory scope has a good bandwidth, versatile timebase with fast sweep speeds, high tube voltage and is capable of long lasting calibration to within a few per cent, depending on the measurement methods employed.

Intended for use in research and for the investigation of complex waveforms, the laboratory oscilloscope needs to be versatile and has therefore rather a lot of controls and tends to be physically large.

As we shall see later, wide bandwidth deflection systems require a large number of valves passing



fairly high currents. This, together with the number of valves in the timebase (usually two are provided) and the supply regulator needed to maintain calibration, means that the valve count is sometimes over a hundred and a power consumption of almost 1kW is not uncommon. These big scopes are usually trolley mounted with a fan to keep the operating temperature at a reasonable level.

TEKTRONIX TRENDS

Pioneers in this field of scopes were undoubtedly the American firm Tektronix and many other manufacturers have done a lot of copying from the Tektronix design. The Tektronix format of tube in the top left corner, Y amplifier below, and timebase down the right-hand side is now familiar to users of laboratory scopes.

With the advent of Tektronix styling came another innovation, perhaps conceived initially by the same company and now copied by many, that of plug-in Y amplifiers, followed by plug-in almost everything! This means that a wideband (33MHz for Tektronix) main frame can be used for a number of special purposes just by changing plug-in units.

The main frame houses the CRT, power supplies, Y drive amplifier, X amplifier and the timebase if this is not plug-in. A range of Y plug-ins would then be used with the scope, providing double beam operation, differential inputs, very high sensitivity or a special function such as a spectrum analyser or four channel display. If plug-in timebases are provided these could be normal timebase, delay plus normal, very slow, or a straightforward amplifier plug-in for XY display.

Whilst appreciating that these plug-ins can cost a great deal of money it is fairly obvious that a selection of plug-ins is cheaper than a selection of scopes! The user is also able to keep in touch with current technology by the purchase of recent plug-ins offering such facilities as sampled inputs giving very high apparent bandwidths, although not in real time. One other advantage of plug-ins is that the Y amplifier controls probably get the hardest use on a scope and it is an easy matter to remove the plug-in for maintenance without having to disembody the whole scope.

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1 °. °				1 1	126	2 · 25	0.38
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9-0-9		100		13	0 - 95	0.10
0-9	0-9	330	330	235	1 · 28	0.10
0-8-9	0-8-9	500	500	207	1.70	0.22
0-8-9	0-8-9	1000	1000	208	2 - 30	0 · 30
15-0-15	_	40	_	240	1 · 28	0.10
0-15	0-15	200	200	236	1 · 28	0.10
20-0-20		30		241	1.09	0 · 10
0-20	0-20	150	150	237	1.28	0.10
0-15-20	0-15-20	800	500	205	2.16	0.38
0-20	0-20	300	300	214	1.36	0.22
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0-15-27	0-15-27	1000	1000	204	2 · 40	0.38

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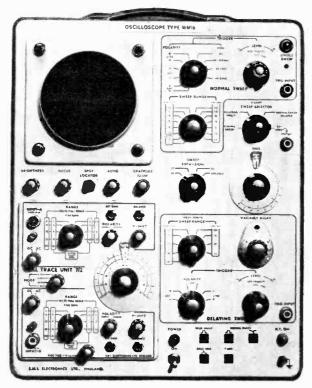


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SAMPLING TECHNIQUES

The group of scopes classed as "special purpose" can be extended to virtually any scope not corresponding to the norm, and, in a way, most scopes have a little something special since they have to appeal to buyers, just like motor cars.

Perhaps the most important special purpose scope, to be found in few amateur labs, is the sampling oscilloscope.



A close-up of the front panel of one of the author's scopes. This EMI WM16 has plug-in facilities, dual timebases and a bandwidth of better than 40MHz

Considered on a real time basis the sampling scope has a bandwidth of a few tens of MHz. However, a special input circuit, usually contained in the probe, samples the instantaneous level of the signal at a rapid rate and the probe output when fed through the Y amplifier produces a display that builds up in a very short space of time to a continuous display.

Various manufacturers use different sampling techniques but the results obtainable represent bandwidths well into the hundreds of MHz and beyond.

A useful result of the development of sampling techniques has been the production of a circuit which when connected to an oscilloscope deflection amplifier's outputs, enables the trace on the screen, perhaps a 5MHz pulse, to be drawn by a mechanical plotter which takes about 10secs to complete one accurate scan. The technique used is similar to sampling oscilloscopes, the input to the XY plotter being sampled over say 10 seconds. The resulting XY plot is a faithful reproduction, within the plotter resolution, of the trace that was on the scope face, although not in real time as it takes 10 seconds to draw a signal of, say, 100ns width.

Other special oscilloscopes are designed to do specific jobs and there are such things as spectrum analyser scopes produced. In this scope the Y channel is narrow band, the precise band being determined by the X deflection voltage. Thus as the timebase sweeps, usually fairly slowly, the Y amplifier sweeps a certain range of frequencies, the Y deflection being proportional to the signal at that frequency. The X axis can be calibrated in frequency and such a scope can be used for investigating modulation sidebands etc.

Storage scopes also fall into the category of "special purpose" if only by virtue of the very high price. We shall consider storage tubes in the next section dealing with displays, but suffice it to say here that a special tube is employed which enables a trace to be retained after the scan is completed. These scopes are very useful for low speed Servo work and in conjunction with spectrum analyser facilities, as mentioned above, flicker can be completely eliminated.

To be continued



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Trio 9RS9DS must be In good condition with handbook and working.—C. H. Brain, 7 Elverlands Close, Ferrinn, Susser BNI2 SPL.

Urgently required, Mazda valve, type AC(VP): also any info. on massive, old Murphy set type A20, Info. or price required for that ancient valve to:—N. Penny, "Nanook". The Creek, Sunbury-on-Thames, Middx.

"Tape head cover for Grundig Portable Battery TKE Tape Recorder and circuit diagram.—Lal Sai Klew, 65A Union-Flats, Jalan Sentul, Kuala Lumpur, Malaysia.

"Codar PR40 Pre-Selectorin good condition wanted.—P. Dimpleton, 37 Mountview Avenue, Dunstable, Beds.

INFORMATION WANTED

... Technical details of, or the actual coil for the Mini Four, appearing in the March and April Issues of P.W. for 1952. I have all the components except the coil type CT9 which was originally made by Stern Radio.—d. Cull, Sunnyside, 10 Ashdene Rcad, Southampton, Hants.
... Info wanted on Rr type 103A, RF unit 24 and circuit diagram of Rx type BC-453-B a U.S. Army job.—M. Bracewell, 26 Selwyn Crescent, Hatfield, Herts.
... barrow or buy circuit diagram for an Armstrong receiver Type A5105.—John King, 4 Eastbourne Road, Polegate, Suseex.
... Detailed instructions required for fitting new belt to Akai 4000D tape deck.—T. Fieldhouse, 100 Wortley Heights, Leeds LS12 19F.
... Anv Info on BUSH EBS 4 RADIO all replies answered.—K. Eskriett, 63 Paley Road, Bradford, Yorks, BD4 7EL.
... For, AP61335 Freq. Swept Generator, CT202. Handbook BR1771(14) or circuit diagram. Buy loan of copy, any info welcome.—T. E. Wicks, 12 Kensington Ave, Watford, Herts. WD1 TRY.
... ang een on the U.S.N. transceiver Type CR1-4344—a unit of Model TBY-8 made by Colonial Radio Corporation, Buffalo, N.Y. Even band-coverage gen would help.—H. W. Boyett, G86ZG, 66 Freshbrook Road, Lancing, Sussex BN15 8DA.
... can you please sugniv me with data and servicing instructions also circuit diagram for the Grundig TK120 Tape Recorder.—G. E. Simkin, 20 Wensleydale Drive, Forest Hall, Newcastle upon Type, NE12 0JH.
... Can you please sugniv me with data and servicing instructions also circuit and required reading the Recorder.—G. E. Simkin, 20 Wensleydale Drive, Forest Hall, Newcastle upon Type, NE12 0JH.
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No. 58 GRIP TESTER

A series of simple transistor projects, using not more than twenty components.

THE objective when using this piece of equipment is to hold a probe (made of aluminium foil folded round a piece of wooden broom handle) in each hand and squeeze the probes as hard as possible. The tighter the grip the more the lamps will become illuminated. But more than this; the lamps come on in a set sequence. A weak grip will make only one lamp glow faintly but a very strong grip could make all three lamps glow brightly. An intermediate grip may only illuminate two lamps. The circuit shown in Fig. 1 is designed to operate three lamps this way but can be extended to operate as many as are required if the instructions are followed.

is reached when it might be more economic to use a zener diode. For more than four indicating stages R2 ought to be reduced to 220 ohm. The sensitivity of the unit is controlled by VR1. Reducing its value lowers the sensitivity and requires a stronger grip to get the lamps to light up.

* components list

R1 1kΩ 4W R2 470Ω ↓W R3-5 1kΩ ↓W

VR1 200kΩ linear potentiometer

D1-6 1N4148 Tr1-4 BC108 LP1-3 6V 40mA

Battery 9V Probes Veroboard

Circuit

Trl is an emitter follower and the potential at its emitter is set by the potential divider effect of R1, VR1 and the body's resistance plus contact resistance between the palms of the hands and the probes. The lower the skin and body resistance the higher will be the emitter potential. Skin contact resistance can, to some extent, be controlled by the pressure of grip on the probes and affects the emitter this potential.

This potential is used to provide base current into each of the following grounded emitter drivers but the silicon diodes in series with each of the bases ensures that in the case of Tr2 the output from Trl must be higher than 1.2V while for Tr3 it must be 1.8V and for Tr4 should exceed 2.4V. Thus, when the grip is weak the potential from Trl might only be 1.6V and in this case LP1 will be the only lamp illuminated but if it is 2.2V Tr3 will be starting to conduct and LP2 * will start to glow while LP1 glows even more brightly. The diodes are there simply to provide potential increments for consecutive stages and the technique of adding one extra to each stage could be continued until some point

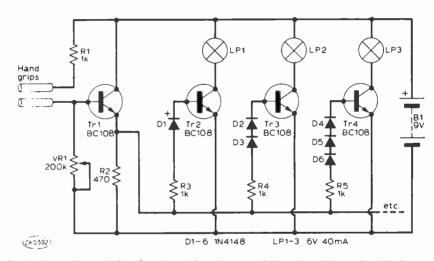
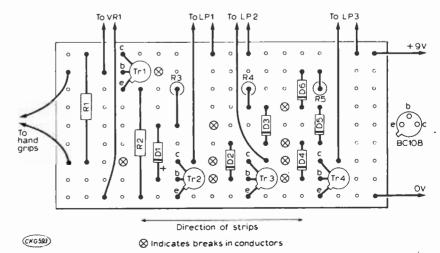


Fig. 1, above, is the circuit for a four stage tester and a suggested layout on plain veroboard is shown in Fig. 2, below.



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appii	ıcaı	uon.		PC86	0.75	PL84	0.66	30C15/	
• •				PC88	0.75	PL504	0.88	PCF800	1.05
DM70	0.63	FF80	0.46	PC97	0:45	PL508	1.05	30C17	1.00
D Y 51	0-85	EF83	1.03	PC900	0.56	PL509	1.55	30C18/	
DY86/7	0.42	EF85	0.43	PCC84	0.52	PL802	0.96	PCF805	0.90
DY802	0.45	EF86	0.90	PCC88	0.80	PY33	0.66	30F5/PF	818
EABC80	1.00	EF89	0.81	PCC89	0.65	PY81/800	0.50	,	1.10
EB91	0.88	EF91	1 30	PCC189	0.65	PY82	0.55	30FL1/	
EBC81	0.75	EF92	1.40	PCF80	0.51	PY88	0.60	PCE800	0.75
EBF80	0.60	EF95	1.35	PCF82	1.80	PY500A	1.05	30FL2	0 75
EBF83	0.62	EF183	0.60	PCF86	0.65	PY800	0.50	30FL12	1.05
EBF89	0.58	EF184	0.60	PCF200	0.85	PY801	0.50	30FL14	0.85
EC86	0.75	EH90	0.56	PCF201	0.87	U26	1 00	30L1/PC	194
EC88	0.77	EL34	0.95	PCF801	0-65	U191	1.00	0021710	0.52
ECC81	0.45	EL36	1.05	PCF802	0.71	U193	0.50	30L15/P0	
ECC82	0.48	EL81	0 90	PCF806	0.66	UABC80	0.90	SULIBIFE	1.05
ECC83	0.45	EL84	0.47	PCH200	0.88	UBC81	0.70	lass to	
ECC84	0.55	EL85	0.55	PCL82	0.54	UBF89	0.60	30L17	0.90
ECC85	0.53	EL86	0.95	PCL83	0.66	UCC85	0.60	30P4MR	1.30
ECC88	0.75	EL95	0.70	PCL84	0.59	UCH81	1.00	30P12/P0	1085
ECC189	0.71	EL91	1.81	PCL85	0.63	UCL82	0.70		1.05
ECF80	0.56	ELL80	1.30	PCL86	0.63	UCL83	0.70	30P19/P0	
ECF82	0.78	EM84	1.18	PCL805/8	35	UF89	0.80	002 20/2 0	1 00
ECF86	0.71	EM87	1.18		0.63	UL84	0.95	30PL1/P0	
ECH81	1.00	EY51	0.88	PD500	1.55	UY85	0.50	301 11/11	0.95
ECH83	1.00	EY86/87	0.42	PFL200	0.80	6/30L2/		00717 101	0.83
ECH84	0.78	EY88	0.64	PL36	0.88	ECC804	1.00	30PL13/	1 00
ECL80	0.53	EZ80	0.51	PL81	0.75	6F23/EF8	12	PCL800	1 20
ECL82	0.61	EZ81	0.40	PL81A	0.88		1.05	30PL14/	
ECL83	0.68	G Y 501	0.90	PL82	0.50	30C1/PCF	80	PCL88	1.25
ECL86 .	0.63	GZ34	0.78	PL83	0.98	1	0.51	30PL15	1.05

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						UCH42	0.75		0.50
SAE	tο	r list:	S .			UCH81	0.40		0.75
			٠.			UCL82	0 85		0.40
AZ1	0.60	EF80	0.25	PC86	0.80	UCL83	0.70	6V6GT	0.45
AZ31	0.55	EF85	0.85	PC88	0.80	UF41	0.75	6X4	0.40
CBL31		EF86	0.80	PC97	0.50	UF89	0.40	6X5G	
CL33	1.50	EF89	0.28	PC900	0.48	UL41	0.85	6X5GT	0.45
CY31	0.50	EF91	0.37	PCC84	0.40	UL84	0.48	7B6	0.75
DAF91	0.80	EF92	0.50	PCC88	0.55	UY41	0.48	7B7	0.70
DAF96	0.50	EF95	0 40	PCC89	0.50	UY85	0.40	7C5	1.30
DCC90	1.35	EF98	0.75	PCC189	0.60	VR105-30			0.75
DF91	0.80	EF183	0.30	PCF80	0.30	VR150-30 OA2			0.70
DF96	0.50	EF184	0.35	PCF82	0.35	OB2	0.40	7R7	0.75
DK91	0.45	EL32	0.60	PCF86	0.60	1R5	0.40	787 7¥4	2.25
DK92	0.70	EL33	1.75	PCF801	0.50	185	0.45	12AT6	0.75
DK96	0.60	EL34	0.50	PCF802	0.50	1T4		12AT7	0.40
DL92	0.40	EL36	0.50	PCF805	0.90	384	0 40	12AU6	0.45
DL94	0.48	EL37	2.50	PCF806	0.75	3V4	0.70	12AU7	0.83
DL96	0.55	EL41	0.90	PCF808	0.90	5R4GY	0.80	12AX7	0.88
DY86/7	0.36	EL42	0.90	PCL82	0.35	5U4G	0.40	12BA6	0.45
DY802	0.37	EL84	0.28	PCL83	0.66	5V4G	0.50	12BE6	0.50
	0.38	EL95	0.40	PCL84	0.45	5Y3GT	0.45	30C1	0.80
EAF42	0.75	ELL80	1.00	PCL85	0.50		0.45	30C15	1.05
EB91	0.22	EM80	0.45	PCL86	0.45	6/30L2	0.90	30C17	1.10
EBC33	1.00	EM81	0.60	PCL805/8			0.40	30C18	0.90
EBC41	0.75	EM84	0.35		0.50	6 A M 5	0.90	30 F5	1.10
EBC81	0.88	EM85	1.00	PD500	1.80	6AQ5	0.45	30FL1	0-80
EBF80	0.40	EY51	0.40	PEN45	0.75		0.85	30FL2	0.75
EBF83	0.40	EY86	0.40	PL36	0-55	6AT6	0.45	30FL14	0.90
EBF89	0-82	EZ40	0.75	PL81	0.50		0.80	30L15	1.05
EBL31	1.50	EZ41	0.75	PL82	0.45		0.28	30L17	0.95
ECC81	0.40	EZ80	0.28	PL83	0.45		0.35		
ECC82	0.38	EZ81	0.29	PL84	0.40		0.75	30P4MR	1 30
ECC83 ECC84	0.38	G Y 501	0.80	PL500	0.75	6BJ6	0.55	30P12	1.05
ECC85	0.80	G Z 30	0.45	PL504	0.75		0.55	30P19	1-00
ECC88	0-40	GZ32	0.50	PL508	0.90		1.00	30PL1	0.95
ECH35	1.25	GZ34 GZ37	0.65	PL509	1.55		1.35	30 PL13	1.20
ECH42	1.00	HN309	1.25	PL802 PX4	0.95		0.90	30PL14	1.25
ECH81	0.30	K T61	1.75	PX25	3.50		0.90		
	0.45	KT66	2 50	P X 25 P Y 33	3·50 0·63		0.35	35 W 4	0.50
ECL80	0.55	KT81 (7C		PY81	0.80		1.30	35Z4GT	0.70
ECL82	0.85	WIOI (IC	1.30	PY82			1.40	50CD6G	1.20
ECL83	0.70	KT81	1.75	PY83	0.35		1.00	807	0.50
ECL86	0.40	K T88	2.90	PY88	0.38		1.05	813 ITT	
ECLL800		KTW61	1.00	PY500	1.00		1·00 0·70	813 USSI	
	1.20	MU14	1.00				0.65		£5:76
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AC188	0.20	BF195	0.13	OC20	2:00	ZTX 500	0·15 0·15	2N2646 2N2904	0.50
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ACY39	0.65	BFS61	0.25	OC25	0.40	ZTX531	0 25	2N2905	0.32
AD140	0.50	BF898	0.25	OC28	0.70	ZTX 550	0 18	2N 2905 A	0.25
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AD162	0.39	BFY50	0.20	OC42	0.40	IN4002	0.8	2N2926 2N3053	0.10
AF115	0.25	BFY51	0.20	OC44	0.18	IN4003	0.8	2N3055	0.60
AF116	0.25	BFY52	0.20	OC45	0.18	IN4004	0.8	2N3525	0.80
AFILT	0.20	BFW10	0.81	0071	0.15	IN 4005	0 10	2N3614	0.59
AF186 AF239	0.40	BY100 BY126	0·15 0·14	OC72 OC76	0·25 0·30	IN4006 IN4007	0.12	2N3615 2N3702	0.65
A8 Y27	0.30	BY127	0.15	0077	0.55	1N4009	0.08	2N3702 2N3703	0.11
A8Y28	0.25	BZX61 A	eries	OC81	0.28	IN4148	0.08	2N 3704	0.14
BA102	0.25		0.20	OC81D	0.28	18921	0.07	2N 3705	0.12
BA115 BC107	0.10	BZY88 s		0C81Z	0.45	182033	0.20	2N3706	0.10
BC107 BC108	0·12 0·12	CR81-05	0.10	OC83 OC140	0- 25 0-65	182051A 182100A	0 10	2N3707	0.13
BC109	0.12	CR81-40	0.45	OC170	0.25	183010	0.20	2N3708 2N3709	0-07 0-10
BC113	0.16	CR83-05	0.40	OC171	0.30	2N696	0.15	2N3710	0.11
BC117	0.21	CR83-40	0.55	OC200	0.55	2N697	0.15	2N3711	0.11
BC143	0.30	MJE340	0.50	OC201	0.80	2N706	0.10	2N3819	0.35
BC147 BC148	0·12 0·10	MJE370 MJE520	0.68 0.65	OC202 OC203	0.90 0.55	2N706A 2N1131	0.12	2N3820	0.50
BC169C	0.14	MJE2955		0CP71	1.00	2N1131 2N1132	0·25 0·25	2N3823 2N3903	0·50 0·15
BC182	0.12	MJE3055		ORP12	0.55	2N1302	0.18	2N3904	0.20
BC182L	0.12	MPF102	0.40	ORP60	0.45	2N1303	0.18	2N3905	0.25
BC184L	0.13	MPF103	0.36	T1005	0.20	2N1304	0.22	2N3906	0.16
BCY32	1.20 0.38	MPF104 MPF105	0·35 0·46	TIC44 TIC22611	0.29	2N 1305	0.22	2N 4058	0.15
BCY33 BCY34	0.45	NKT404	0.60	TIL209	0.25	2N1306 2N1307	0·28 0·28	2N4059 2N4060	0.10
BCY70	0.15	OAS	0.60	T1843	0.26	2N1308	0.28	2N4061	0.13
BCY71	0.20	OA10	0 40	ZTX 107	0 12	2N1309	0.30	2N4062	0.14
BCY72	0.15	OA79	0.10	ZTX108	0 10	2N 1613	0.20	3N141	0.81
BCZII BD121	0.65 1.00	OA81 OA91	0.10	ZTX300 ZTX301	0·14 0·14	2N 1614	0.45	40360	0.40
BD124	0.80	OA200	0.08	ZT X 301	0.20	2N2147 2N2160	0·75 1·00	40361	0.45
B D 131	0.45	OA202	0.10		0.24	2N2369A		40362 40430	0·40 0·85
	_								0 00
8N7400	0.20	8N7425	0 37	BN7473	0.44	8N74107	0.51	BN74157	1.09
8N7401 8N7402	0.20	8N7427 8N7428	0·37 0·43	8N7474 8N7475	0·48 0·59	8N74110	0.57	BN74170	2.88
8N7403	0.20	8N7430	0.20	8N7476	0.45	8N74111 8N74118	0.86 1.00	8N74174 8N74175	1.80
BN7404	0.20	BN7432	0 37	BN7480	0.80	BN74119	1.92	BN74176	1.44
BN7405	0.20	BN7433	0.43	8N7482	0.87	BN74121	0.57	BN74190	2.30
8N7406 8N7407	0.40	8N7437 8N7438	0·43 0·43	8N7483 8N7484	1.20	BN74122	0.80	BN74191	2 30
SN7408	0·40 0·25	8N7440	0.20	8N7486	0.50	8N74123 8N74141	1·44 1·00	BN74192 BN74193	2.30
BN7409	0.33	6N7441A1		8N7490	0.75	BN74145	1.44	BN74193	2:30
BN7410	0.20		0.85	8N7491A	N	8N74150	2.30	8N74195	1.44
BN7411	0.28	8N7442	0.85	GN77400	1.10	8N74151	1 15	BN74196	1.58
8N7412 8N7413	0.28	8N7450 8N7451	0.20	BN7492 BN7493	0.75	BN74154 SN74155	2 30	BN74197	1.58
BN7416	0.30	BN7453	0.20	BN7494	0.85	8N74156	1.15	BN74198 BN74199	3·16 2·88
8N7417	0.30	BN7454	0.20	BN7495	0.85		4 10	2111138	2.00
BN7420	0.20	BN7460	0.20	SN7496	1.00	DIL		14 pin	15p
BN7422	0.28	BN7470 BN7472	0.33 0.38	8N7497 8N74100	4·32 2·16	SOCKET	27	16 pin	170
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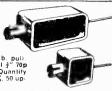
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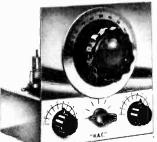
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SHORT WAVE DX by MALCOLM CONNAH

THE receivers used by Broadcast Bands listeners vary enormously; they may be ex-government sets or brand-new commercial units; but all receivers have one thing in common: They will not give their best performance until they are used with a good aerial system.

When we talk of an aerial system we include any devices, such as aerial tuning units, which are placed

between the aerial and the receiver.

In order to get optimum reception the aerial system must be resonant at the frequency of reception. Amateur Bands listeners, and operators, have an advantage here because their bands, with the exception of 15 metres, are closely related. These bands are 10, 20, 40, 80 and 160 metres. If an aerial system is resonant on 80 metres it is a relatively simple matter to get it to resonate on 40, 20 and 10 metres.

The Broadcast Bands, however, are completely unrelated being 11, 13, 16, 19, 25, 31, 41, 49, 60, 75, 90 and 120 metres. If one of these bands is of particular interest a half-wave dipole may be erected for that band. The only practical solution for all band reception is to use some form of end-fed aerial. It should be noted that the term 'long-wire' is often used incorrectly, a misuse of which I have been guilty, as this is strictly an end-fed aerial which is long in relation to the wavelength being received.

The length of aerial that can be erected depends on the amount of space available, but the usual compromise is between 50 and 100 feet long. Theory dictates that the aerial should be straight, but many people have had very good results with aerials that have been bent in order to fit them into the space available.

The aerial should, preferably, be an outdoor one erected at a reasonable height and located as far away as possible from such obstructions as buildings and trees. A very simple aerial tuning unit (such as that described by David Gibson in the January 1974 issue) should then be constructed in order to make the aerial system resonant on the desired bands.

Readers' Logs

David Kernick of Prescot, Lancashire used his Grundig TR600A portable with only just the built-in telescopic antenna to hear the following.

6070 R. Sofia, Bulgaria at 1930.

7145 R. Kiev in English at 0030.

7215 All India Radio in English at 2000.

9550 R. Finland noted at 1805.

9670 Adventist World Radio at 0930.

9695 V. of Saudi Arabia, Arabic at 0405.

9745 R. Baghdad, Iraq noted at 1945.

9770 R. Australia, English at 1605.

9833 R. Budapest, Hungary at 1615.

11920 R. Algiers noted at 1900.

11970 R. Tunis in Arabic at 0920.

15140 R. Havana, Cuba in French at 1935.

15165 R. Denmark in Danish at 1850.

15240 R. Belgrade, Yugoslavia at 1530.

15410 United Nations Radio at 1600.

17755 HCJB, Quito, Ecuador at 1930.

17780 RSA, South Africa noted at 1600.

17845 WYFR noted in English at 1730.

17865 WINB, Red Lion, music at 1930.

21630 V. of Saudi Arabia, testing at 1110.

Richard Staples has found an Eddystone 680X in the loft (excuse me whilst I return my ladder to garage) and the addition of a 100 foot end-fed aerial produced:

3999 R. Godthab, Greenland in Danish at 0840.

4820 Voz Evangelica, Honduras at 1805.

4940 R. Yaracuy, Venezuela, Spanish at 1740.

5920 R. Kiev, news in English at 1800.

9590 R. Australia noted in English.

9610 R. Canada in English at 2115.

11720 R. Nacional, Brazil, Portuguese at 0705.

11935 R. Pakistan, news in English at 1715.

15200 RSA, South Africa in English at 0840.

21695 Greek Military Radio, Athens at 0905.

Christopher Hodgson of Sunderland reports that Radio WYFR (Family Radio Inc.) broadcasts in English to Europe at 1810 GMT on 15130kHz. The station replied to his report in about two weeks and the address for reports is: WYFR, 290 Hegenberger Road, Oakland, California 94621, U.S.A.

With his usual equipment; Codar Multiband 6, P.W. A.T.U. and 50 foot end-fed; Christopher also heard:

7080 Voice of Vietnam, Hanoi at 1820.

7210 Red Cross Broadcasting at 1700.

9505 VOA, Tangier, in Rumanian at 1930.

9525 All India Radio at 2010.

9540 Radio Tashkent noted at 1210.

9545 Radio Ghana, s/off at 2215.

11805 WYFR—Family Radio at 2100.

15130 WYFR—Family Radio at 1810.

15175 RSA, South Africa, s/off at 1850.

15185 R. Finland noted at 1830.

15290 ORTF, Paris, s/off at 1115.

15415 Radio Kuwait, s/on at 1730.

15420 BBC, East Med. relay noted at 1600.

17820 R. Canada, s/on in Polish at 1530.





VHF/FM

by SIMON DAVID

HOGMANAY was celebrated in Scotland in a different way than usual. No doubt the timing was deliberate for Radio Clyde, Scotland's first commercial radio station, broadcast on 95·1MHz on December 31st. The station started at 10.30 p.m. with news and introductions to the staff. The 4kW transmitter is at Black Hill.

The criticisms and doubts surrounding London Broadcasting, the London news stations, resulted in the resignations recently of the Managing Director and Chief Editor. Former Lord Mayor of London, Sir Charles Trinder, also walked out issuing an admission that the finances had not lived up to expectations. One thing evident is the difference between some commercial and BBC local radio broadcasts from a technical standpoint and although both have severe financial restrictions, it is only to be expected that the latter has the advantage of drawing on the resources of its "great-auntie".

I have been informed that BBC Radio Derby is still operating on $96\cdot5MHz$ from Sutton Coldfield using slant polarisation. The $94\cdot2MHz$ transmitter that I mentioned recently is installed at the studio to fill-in the town centre area because of surrounding high ground. It uses a vertically polarised aerial and 10 watt transmitter.

The Radio Derby aerial at Sutton Coldfield is a 5-element Yagi array 500 feet above ground level. It provides a maximum e.r.p. of 5kW in the Derby direction.

Also from Derby, **Roy Patrick** reports that the Lichfield IBA transmitter for the Birmingham area is due on the air on 94·8MHz in February; the Manchester commercial station is due on 97·0MHz (2kW) in March; the Swansea station is expected to start transmitting on 95·1MHz (1kW), using the circular type of aerial, later on in the summer of 1974.

Last month I reported on the results of using the Antiference FM264T six-element aerial. Results since then have been repeated with the addition of Rouen on 96.6MHz. Unfortunately conditions have not favoured reception from Rheims.

MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

AVE KERNICK (Prescot, Lancs) has a Grundig TR600A transistor portable with a built-in ferrite rod antenna, which he has found to be an excellent receiver for pulling-in distant stations. He reports hearing programmes in English from AFN Frankfurt 872kHz; Deutschlandfunk, West Germany 1268kHz at 1745hrs; Radio Norway 1578kHz at midnight; Radio Sweden 1178kHz at 2245hrs; Radio Tirana, Albania 1457kHz (additional frequency for the English Service) at 0330hrs; together with Sud Radio, Andorra in French at 2245hrs on 818kHz and Tripoli, Libya in Arabic at 0025hrs on 1250kHz. Dave asks if it is possible to hear North America on the medium waves using a portable receiver. This is unlikely as a ferrite rod aerial does not have enough pick-up to receive really distant stations. DXers who want to try for North Americans should use an external aerial or a medium wave loop such as the DXers MW Loop Aerial described in the April 1973 issue of Practical Wireless.

Readers' Logs

Roy Patrick (Derby) reports hearing the new Independent Broadcasting Authority (IBA) station at Manchester testing on 1151kHz at 1100hrs on December 1st and IBA Birmingham using test tones on the same channel. IBA stations in the provinces are expected to use 1151kHz for stations at Manchester, Birmingham and Glasgow (R. Clyde); 1169kHz for Swansea and 1546kHz for Liverpool and Edinburgh.

R. B. Callwood (Munich, West Germany) reports hearing BBC Radio 1 (1214kHz) at 1300hrs on his

car radio while driving on the autobahn between Munich and Frankfurt. Reception was on a single occasion only and he wonders if any other reader has received BBC Radio 1 in Germany.

Bill Thorne (London) asks for information about the French broadcasts on 584kHz (513m) which he listens to regularly. The station on this frequency produces programmes for the Paris area for the greater part of the day and has a power of only 5kW. The address is O.R.T.F., 116 Avenue du President Kennedy, Paris 16eme France.

Brian Murray has heard IBA Radio Clyde testing on 1151kHz at 1345hrs and he reports that this station is due on the air on December 31st, 1973. Brian has been busy again with his Astrad VEF 204 receiver using an old band 1 TV aerial as a medium wave antenna. His log includes programmes in English from Radio Warsaw 1502kHz at 0115hrs; Radio Sweden 1178kHz at 0025hrs; Manx Radio, Isle of Man 1295kHz at 1350hrs; Radio Eireann 1250kHz at 2120hrs; Trans World Radio, Montecarlo 1466 kHz at 2325hrs and Radio Portugal 755kHz at 2312hrs.

A last-minute phone call from **T. McCann** (Belfast) reports reception of Newfoundland on 930kHz (CJON in St. John's) with the comment "I was surprised at the strength of this station." Propagation on the North American path is rather variable with periods of a week or more when nothing can be heard. At other times, many stations in Canada and the United States can be heard, the limiting factor being interference from Europeans. During the winter listen around midnight on 600kHz, 640kHz, 710kHz, 930kHz, 940kHz, 950kHz, 1070kHz, 1130kHz. North Americans are easy to identify as all stations are allocated callsigns which are used frequently together with the name of the town or city where the studios are located.

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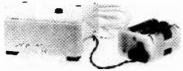
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SHORT WAVES

by DAVID GIBSON, G3JDG

thank you to the many sharp-eared r.f. sleuths who sent in logs. Everyone seems to have bagged far more DX than I did—well done.

John Powell (Essex) sends in some useful information regarding "who's where and when". John says look out for VQ9HCS on Astove Island (look it up; I had to!). New Ham on Campbell Island is ZL4NJ/A.

A listening MUST. Havering Amateur Radio Club are running a station in Rutland from Saturday, March 30 to Monday April 1 1974. Listen on topband, eighty and v.h.f. Why? Because after that date there will be no County of Rutland, its being absorbed into the surrounding counties so this is your very last chance. Full marks for initiative to the Havering A.R.C.

Michael Watson (Kent) tells that a station in Teheran, EP2BQ, has put up an inverted V for topband. Listen for the EP2 callsign in the bottom 5kHz of 160 metres. Who will hear him first?

Several people have written taking me to task for omitting the list of Happenings in the radio world. It appears that we have a number of keen Contest types among us. The calendar for February is as follows: 9-10, 1-8MHz contest; 16-17, ARRL Contest (c.w.); 23-24, REF contest (phone); March 3-4, 144MHz Open and s.w.l. contest; March 3-4, ARRL DX contest (phone). National Field Day this year will be on June 1-2.

Robert Beebe (Derby) reports hoards of G stations on topband. He tells that members of the Derby club have worked some juicy DX around 1830kHz and quotes calls like W1, KV4, DJ and OK etc.

Vice Chairman (wonder what sort of vice?) David Andrews writes to tell of the Droitwich High School Radio Club. Ten members so far and all going in for the R.A.E. The Club has both Rx and Tx but no antenna up as yet. (How about a base-loaded Maths Master—a sure sine of success).

Keith Rowlings (Herts) has a UR1A, PR40, 75ft. long wire—and a problem. He's heard N20 and L50 on 7MHz and wants to know where they are (and so do I). Anyone any information on these or are they Japanese postal districts?

Graham Nicholls (Oxon) has a homebrew 70cm converter feeding a homebrew 144MHz converter which feeds an R107 (not homebrew). His 15 element 70cm Parabeam rests in his bedroom, but it still heard the following; F1CTH, G3BA, G3COJ, G3DAH. G3YXN, G3KEQ, G3UHT, G3WSN, G3ZFP, G3ZMD. G3YC, G4ABF, G4AHU, G4BEL, G4BMP, G6XM, G8ADC. G8FMK. GW8AWS/P, HW6BOH/P. HW7FY, ON5FF, ON5HN. On two metres with a hamebrew 6-ele Yagi (also in the bedroom) Graham logged: GW8HEZ, HW1CS, HW5SY, PA0ADY, PA0CIO, PA0EZR/A, PA0FHV, PA0PEP, PAOPRY, PAOTAR, SM7DT.

Ye fantastic logge has been sent in by Stanley Sharred. I note that it's on IBM paper—it's cheating if you get the computer to listen and log. No gear is mentioned (bet it's a regenerative cats whisker feeding a 100 Watt light bulb) but the following are claimed for 160 metres; GM3ANO, GM4ALK. GM4ASY, GW3UCB, DK3BJ, EI8H, K2ANR. K3RUQ, KV4FZ, OE5KE, OK1AXD, OK1FCW. OK1KRS, OK1KPU, OK2BKT, OK5KWA, OL6AQJ. OL8CCS, VE1CD. PA0HIP. VEIMX. VEIASJ. VOIKE, WIDX, WIMX, W2DED, W2LWI, W2UEZ. WA2WLN/2, WA8IJI, WB8APM. On Stanley excelled with; CT1ADV, CT2BG, EL7D. K2BT, VE1AIH, V01FG, 7X2MD, 9Y4HR. An excursion to 7MHz revealed DX like; C3IMO, CR4BS. CR6TP, EP2TW, K4DX, PY4MA, PY6WF, PY6AOV, SV1CH, TY1ABE, YV1BI, 5U7BB, 9G1HE.

Eighty metres found Martin Ward listening with a JR500S and 60ft. end fed plus an "L-match device" (Oh L). Squeaks of s.s.b. reported from; CT1GC, LX1GC, KG4CB, VE1AIH, VO1FG, 9H1CE. 9J2AE, and a late arrival—CN8CG. Martin reports hearing the Panama City Radio Club on 21MHz with the callsign 3E1KC.

Stephen Day (Suffolk) made an "adjustment" to his R1155 and claims the signals went up by some 20dB. (You can come and make the same adjustment to my receiver—anytime). Antenna is 50ft. end fed and main interest is eighty metres. Stephen bagged mostly G stations but managed foreign signals from; ZK5AFZ and 9H4L.

John Turner says, "I have been giving the Pye Cambridge a rest". What a thoughtful lad. This compassion for a trusty friend has not prevented John from listening with his homebrew t.r.f. (P.W. November 1963). The bandspread is the small tuning capacitor from the 235MHz section of an Ex 19 set. The t.r.f. 85ft, end fed and lots of patience produced; CT2BK, EA6CK, EA8IH, EL7C, HB0LL. HI3XCP, HK3AVK, HR1RSP, HZ1SH, JX4GN JY6UMS, K4PWC/AM, KP4BBW, PY2ELV, PY4LW. TF5TP, TG8KT, VE1AF, VE3AII/SU. PZ1DR, VK2AHM, VK2LW, VK2SG, VK3AD, VK3XJ, VK5FH, VK6SB, VS9MJ, VK3AX. VK5FH, VU2GBG. YV4AGT, ZB2CS, ZB2DL, ZD7SD, ZD7SS, ZM3FO. 3A2CP, 4Z4MQ, 5B4F, 7X2MD. Think what could have been received if Stephen Day (above) had made an "adjustment"!

BROADCAST BANDS

Short Wave Reports by 15th of the month to Malcolm Connah, 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.

Medium Waves Logs to Charles Molloy, 132 Segars Lane, Southport, PR83JG. VHF/FM Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

AMATEUR BANDS

Short Wave/VHF

Logs in alphabetical order please by 15th of the month to David Gibson, G3JDG, 12 Cross Way, Harpenden, Hertfordshire.



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MODEL THIS



HIOKI Model 720X VOM

A versatile, accurate measur accurate measuring instrument. 20,000 opv. 0/ 5/25/100/500/ 1000V DC. 0/10. 50/250/1000V AC. 0-50uA/ 250mA. 0-20k/ OUR PRICE

P&P 20p



TMK MODEL TW50K

TMK MODEL TW50K
46 ranges, mirror
scale, 50k/V DC
50k/V AC.
DC Volts: 0, 125/
0,25/1,25/25/5/10/
25/50/125/25/0/
1000, DC current
150/125/25/0/
1000, DC current
104/100k/104/104/
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U4323 MULTIMETER

U4323 MULTIMETER
20,000opv. Simple
unit with audio/15
cosillator. Suitable
for general receiver
tuning. Ranges:
0.5/2.5/10/50/250/
500/1000V DC.
2.5/10/50/250/
DC. Resimence 5/
Resimence 5/
Resimence 5/
Resimence 5/
Admm. Supplied in carrying case complete with test leads.

DUR PRICE £7.00

MODEL TE300

MUDEL 1 E 3 UI
30,000 pp., Mirror
sale. Overload
protection. 0/0.8/3/1560/300/1200V DC.
0/6/30/120/900/
1200V AC. 0/30 uA/
6mA/60mA/300mA/
600mA. 0/8k/80k/
800k/8 Meg ohms.
-20 to +63dB. **OUR PRICE £7.50**



P&P 15p

P&P 20p

U4324 MULTIMETER

U4324 MULTIMETER
High sensitivity, overload protected.
20,000opv. Ranges:
0,6/1.2/31/2730/
60/120/600/1200V
00/36/5/60/156/
300/600/900V AC.
Current: 0,6/10.6/16/
6/6/6/6/000mhod.AC.
25/500 ohms/0.6/16/
AA AC. Resistence:
25/500 ohms/0.6/16/
Mohms. Decibels: -10 to +12d8. Size
167 x 98 x 63mm. Supplied complete with test leads, spare diode and instructions.

OUR PRICE £8.00

U435 MULTIMETER U435 MUL TIMETER 20,000pt, Overload protected, Ranges: 75mV/2.5/10/25/100/250/500/10000 C. 25/10/25/100/25/100/25/100/25/100mA/15/25/100mA/0.5/2.5A DC. 5/25/100mA/15/25/100mA/0.5/2.5A AC. Resistance: 0.3/3/30/3006 complete such assistance: 0.3/3/

OUR PRICE £8.75

U4312 MULTIMETER

U4312 MULTIMETER

extremely sturby
instrument for
general electrical
use. 667 cpv.
0/0.3/1.5/7.5/30/
60/150/300/600/
900V DC & 75mV.
0/0.3/1.5/7.5/306
0/150/300/600/
900V AC, 0/300uA/
1.5/6/15/150/60/
150/150/60/15/
15/6/15/150/60/
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OUR PRICE £9.75 P&P 25p

U91 Clamp VOLT AMMETER

AMMETER
For measuring AC voltage and current without breaking circuit. Ranges. 300/600V AC. Current: 10/25/100/250/500A. Accuracy 4%. Size 283 x 94 x 36mm. Complete with carrying case, leads and fuses. **OUR PRICE £10.50**



P&P 20p

MODEL C7080EN

MUUEL L/UBBEN Giant 6" mirror sala, 20,000 opv 0/0,25/11/2.5/10/ 50/250/1000/ 5000V DC. 0/2.5/10/50/250/ 1000/5000V AC. 0/50uA/11/0/ 100/500mA/10A 20 Meg. –20 to +50d8. 20 Meg. - 20 to +50dB. OUR PRICE £13.95



P&P 35p

II4317 MULTIMETER MOOEL 500

MUUEL 500 30,000 opv with overload protect-tion. Mirror scale. 0/0.5/2.5/10/25/ 100/250/500/ 1000V DC. 0/2.5/10/25/100/ 250/500/1000V AC. 0/50uA/5/50/ 500mA. 12A DC. 0/60k/6 meg/60 me

OUR PRICE £10.95 Carr. paid Leather case for above £1.75

KAMOOEN 360 MULTIMETER

High sensitivity. DC 100kohm/V AC 10kohm/V 5" mirror scale. AC 10kehm/V
C 10kehm/V
C mirror szele
overload protect
ed. Ranges: 0.5/
2.5/10/50/250/
1000V DC 5/10/
50/250/1000V
AC. Current:
0.01mA/0,5/5/50/
500mA/10,6/
Resistance: 0.1/
1/10/100k ohms/
1/10/100k ohms/
10/100k ohms/
Decibels –20 to
62d8. Battery op

10/10/m o.m... Decibels – 20 to +62dB, Battery operated. Size: 180 x 140 x 80mm, Supplied complete with, test leads etc.

80

80

OUR PRICE £13.95

HIOKI MODEL 700X



OUR PRICE £14.95 KAMOOEN HM720B FET VOM

KAMUUEN HM/2 Input impedence 10 Megohms. Ranges: 0/.25/1/2.5/10/50/ 1000V DC. 0/2.5/10 50/250/1000V AC 0/25u A/2.5/25/250 mA DC. 0/5k/50k/500k/5 M 500 Megohms

OUR PRICE





TMK MODEL 117 FET **ELECTRONIC VOLTMETER**



OUR PRICE £17.50 P&P 20p KAMODEN 72200 Multitester



OUR PRICE £16.95 P&P 30p

370WTR MULTIMETER

370W1H MULTIME! Features AC current ranges. 20,000cpv 0/0.5/2.5/10/50/ 250/500/1000V DC 0/2.5/10/50/250/ 500/1000V AC. 0/50u.A/1/10/100 mA/1/10A DC. 0/100mA/1/10A AC. 0/5k/50K/500k/ 5 Meg/50 Meg. Decibels: -20 to 46 2d8.



U4317 MULTIMETER
High sensitivity
instrument for field
and laboratory work
Knife edge pointer.
Ranges: 100mV/ 0/100/250/500/1000
500-1000 / 525-5/102/550/100/250
500/1000V AC. Current: 50uA/0.5/
1/5/10/5250mA/1/5A DC. 0.25/
0.51/15/10/5250mA/1/5A DC. 0.25/
0.51/15/10/50/250mA/1/5A DC. 0.25/
0.51/15/10/50/250/
0.51/15/10/50/250/
0.51/15/10/50/250/
0.51/15/10/50/250

OUR PRICE £15.00 P&P 20n

TE40 HIGH SENSITIVITY

AC VOLTMET 10 Mag input. 10 ranges: 0.001/ 0.03/0.1/0.3/ 1/3/11/30/100/ 300V RMS. 5cps-1.2MHz. -40 to +50dB supplied brand new complete with leads and instructions.



TE65 VALVE VOLTMETER

28 ranges. DC volts 1.5-1500V. AC volts 1.5-1500V. Resistance up to 1000 Megohms, 200/240V AC operation. Com-plete with probe and instructions

OUR PRICE £17.50 Additional probes available RF £2.12, HV £2.50

TMK LAB TESTER

TMK LAB TESTER
100,000 opv. 6.8"
scale. Buzzer
short circuit check.
Sensitivity 100,000
opv DC. 5k/V AC
DV Votes 15/2.5"
AC 3/10/50/250
100/10000 DC.
current 10/100 AD,10/
10/100/500 AD,25/10A, Resistence:
1k/10k/100k/10 Meg/100 Meg ohms.
Decibets: -10 to +498. Plastic case
with carrying handle. Size: 190 x 172
x 99mm.

DUR PRICE £19.95 P&P 25c

MODEL U4311 Sub-standard
Multi-range Volt-Ammeter
Sensitivity 330
Ohms/Volt AC
and DC.
Accursey 0.5%
DC. 1% AC.
Scale length:
10/2300/750wA1.
15/317.5/15/30/75/515/30/75/515/30/75/15/30/75/50WD/1.
15/317.5/15/30/75/50V DC. 0/75/mW/
1.5/317.5/15/30/75/50V DC. 0/75/mW/
0/75/150/300/750V DC. 0/75/mW/
1.5/317.5/15/30/75/50V DC. 0/75/mW/
0/75/150/300/750V DC. 0/75/mW/
0/75/150/30/

OUR PRICE £49.00

LB3 TRANSISTOR TESTER

Tests ICO and B. PNP/NPN. Operates from 9V battery. Complete with all instructions etc. **OUR PRICE** £3.95 P&P 20p

LB4 TRANSISTOR TESTER Tests PNP or NPN

Tests PNP or including transistors. Audio indication. Operates on two 1.5V batteries. Complete with instructions etc. OUR PRICE £4.50 P&P 20p



TRANSISTOR TEST 27 ranges. 16,700.pp; Verload protected. Ranges: 03,15,56/30/50/300/900V DC. 1.5/7.5/30/150/300/900V DC. 1.5/7.5/30/150/300/750V AC. Current: 0,06/0.6/6/50/500mA DCA AC. Resistances: 0.06/0.6/26/26/20/60/200k ohms/2 Mohms Battery operated. Supplied complete Rattery operated. Supplied complete of the protection of the control of the c Battery operated. Supplied complete with probes, leads and steel carrying case. Size: 115 x 215 x 90mm.

HA341 MIII TIMETER TRANSISTOR TEST

OUR PRICE £10.50 P&P 20m

KAMOOEN HM350 TRANSISTOR TESTER

TRANSISTOR 1
High quality
instrument to
test reverse leak
current and DC
current. Amplification factor of
NPN, PNP, diodes,
transistors, SCR's
etc. 4" square
clear scale meter.
Operates fromes.
Instructions, leads
carrying handle.



P&P 30p

OUR PRICE £12.50

STOOTE MULTIMETER-TRANSISTOR TESTER

THANSISTUR TI 100,000opv. Mirror scale. Overload protection. 0/0.12/ 6.6/3/12/30/120/ 600V DC. 0/6/30/ 120/600V AC. 0/12/600uA/12/ 300mA612A DC. 0/10k/1 Meg/ 100 Meg. -20 to +50dB. 0.01-0.2 MFD. Transistor tester mei



ransistor tester measures Alpha, Beta nd ICO, Complete with instructions, atteries and leads. OUR PRICE £14.95

Model 449A In Circuit TRANSISTOR TESTER

Checks true AC, Beta in/out. Checks ICO, Checks diodes in/out. Checks SCR etc. Beta HI 10-500 LO 2-50. ICO 0-5000uA. 220/ 240 V AC operation.



3

OUR PRICE £17.50 P&P 25p

KAMOOEN HMG500 insulation resistance tester

IRSUIZATION TESISTATIVE TESTATION AND TESTAT

OUR PRICE £19.95 P&P 30p

TE16A TRANSISTORISEO SIGNAL GENERATOR

5 ranges, 400kHz to 30 MHz. An inexpensive instrument for the handy-man. Operates on 9V battery. Wide easy to read scale. 800kHz



modulation.
Size: 149 x 149 x 92mm Complete with instructions and leads OUR PRICE £8.97 P&P 250

TE22 SINE SQUARE WAVE AUDIO GENERATOR



OUR PRICE £17.50 P&P 37p

ARF 300 AF/RF SIGNAL GENERATOR

GENEHATUR
All transistorised
compact fully
portable. AF sinewave 18Hz to 220
kHz. AF square
wave 18Hz to 100k
Hz. Output Square/
Sine wave 10V.
P-P RF 100kHz to
200MHz. Output
IV maximum



OUR PRICE £29.95

1102



Send s.a.e. for 8 page list of Semi-Conductors & Valves

NEW SINCLAIR PROJECT 80

UI-LI MODOFES & LYCKAGES
Z40 Power Amplifier £5.45
Z60 Power Amplifier£6,95
Stereo 80 Pre-Amplifier £11.95
Active Filter Unit £6.95
Project 805 £26.95
PZ5 Power Supply £4.98
PZ6 Power Supply £7.98
PZ8 Power Supply£7,98
2 x Z40/Stereo 80/PZ5£25.00
2 x Z40/Stereo 80/PZ6£27.75
2 x Z60/Stereo 80/PZ8£30.45
Transformer for PZ8£4.05
POST & PACKING 35p each

AT201 Decade ATTENUATOR

Frequency range 0-200k Hz. Attenuator 0-111dB, 0.1dB steps. Impedence 600 ohms. Input power maximum 30dBm, Size: 180 x

OUR PRICE £12.50 P&P 37p

BELCO Sine Square Wave CR OSCILLATOR, Sine 18 x 20,000 Hz. Maximum output +10dB (10k ohms) Operates from internal batteries. Attractive tv tone case. Size: 196 x 127 x 50mm

OUR PRICE £17.50 P&P 17p

SWR METER Model SWR3

NWH METER Model S
Handy SWR meter for
transmitter entenna alignment, with built-in field
strength meter. Accuracy
5%, Impedence 52' Indicator 100uA DC, Full
scale 5 section collapsible
antenna. Size 145 x 50 x
60mm.

OUR PRICE £4.25

P&P 25

3

MODEL TE15 GRID DIP METER GRID DIP METER
Transistorised. Operates as Grid Dip,
Oscillator, Absorbtion Wave Meter and
Oscillating Detector.
Frequency range
440kHz – 280MHz
in six coils. 500uA
meter. 9V battery
operation. Size:
180 x 80 x 40mm.



OUR PRICE £15.00

BVD5 Vernier TUNING DIAL App, 7:1 ratio planetary drive vernier dial. Log scale 0–180 degrees.
Blank scales 1–50.
Blank scales 1–52.

OUR PRICE £1.62

YAMABISHI VARIABLE **VOLTAGE TRANSFORMERS**

Excellent quality at low cost.
All models—Input 230V 50/60Hz.
Variable output 0–260V
MODEL S260 GENERAL PURPOSE
BENCH MOUNTING
PR.P

		rar	
1A 2.5A	£8.75 £10.00	30p 35p	
5A	£14.70	37p	al Oh
8A	£25.50	50p	A HILLIAN
10A	£28.10	75p	100
12A	£29.50	100p	
20A	£72.50	125o	
25A	£72.50	130p	SHILL
40A	£103.10	150p	S. I
MODE	EL S260B		1
2.5A	£8.75	30p	
1A	£10.00	350	

POWER RHEOSTATS

High quality ceramic construction, Wind-

construction. Windings embedded in vitreous enamel. Heavy duty brush wiper. Continuous rating. Wide range available ax-stock. Single hole fixing. %" diameter shafts. Bulk quantities available. 25 WATT 10/25/50/100/250/500/ 1000 Ohms. £1.15 P&P 10p

50 WATT 10/25/50/100/250/500/ 1000/2500/5000 Ohms.

P&P 10p 100 WATT 1/5/10/25/50/100/250/ 500/1000/2500 Ohms. £2.34

RUH6 Reflex Horn Speaker

Built-in driver unit. Impedence 16 ohms. Power rating 10W, Response 380—7000Hz. Size app. 6" x 6". Weather and shock protected. **OUR PRICE £4.97**

EW CLEAR PLASTIC PANEL METERS

USED EXTENSIVELY BY INDUSTRY, GOVERNMENT DEPARTMENTS, EDUCATIONAL AUTHORITIES ETC. Over 200 ranges in stock-other ranges to order. Quantity discounts available. Send for fully illustrated brochure.

CLEAR PLASTIC MODEL SD640 Size: 85 x 64mm

£3.35 £3.30 £3.35 £3.25 £3.20 £3.20 £3.20 £3.20 £3.20 £3.20 £3.20 £3.20 £3.20



CLEAR PLASTIC MODEL SW100 Size: 100 x 80mm

£4.55 £4.35 £4.10 £4.35 £4.30 £3.95 £3.95 £3.95 £3.95 £3.95



EDGWISE MODEL PE70 Size: 90 x 34mm



MODEL ED107 EDUCATIONAL METER Size: 100 x 90 x 150mm including terminals

A range of high quality moving coil instruments ideal for school experiments and other bench applications. 3" mirror scale. The meter movement is easily accessible to demonstrate internal working.





OV DC £6.55 1A/15A DC £7.70

CLEAR PLASTIC MODEL 85P Size: 120 x 110mm

£4.85 £4.70 £4.40 £4.70 £4.70 £4.30 £4.30 £4.30 £4.30 £4.30 £4.30 £4.30 £4.30 £4.30 £4.30 £4.30 £4.30 £4.30 £4.30



300V DC £4.3 15V AC £4.3 300V AC £4.3 S Meter 1mA £4.3 VU Meter £5.0 1A AC £6.3	

..

CLEAR PLASTIC MODEL SD460 50uA 100uA 200uA 500uA 50-0-50uA £3.10 £3.05 £3.00 £2.80 £3.10 £3.05 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 £2.85 A 10V DC ... 50V DC ... 300V DC ... 15V AC ... 300V AC ... VU Meter ... £2.85 £2.85 £2.85 £3.00 £3.00 £3.20

POSTAGE & PACKING 15p

*Items with asterisk are Moving Iron type, all others are Moving Coil

CLEAR PLASTIC MODEL SD830 Size: 110 × 83mm 50µA ... : 23,75 100µA ... : 23,75 200µA ... : 23,65 50µA ... : 23,65 50µA ... : 23,65 50µA ... : 23,65 50µA ... : 23,75 £3.75 £3.70 £3.65 £3.45 £3.70 £3.40 £3.40 £3.40 £3.40 £3.40 £3.40 £3.40 £3.40 £3.40 £3.40 £3.40 100-0-10 1mA ... 5mA ... 10mA ... 100mA ... 100mA 500mA 1A DC 5A DC 10A DC 5V DC



10V DC 20V DC 50V DC 300V DC 15V AC 300V AC VU Meter

CLEAR PLASTIC MODEL 45P Size: 50 x 50mm Size: 50 x 50mm
50x A ...
100x A ...
100x A ...
200x A ...
500x A ...
500x A ...
100x 100x A ...
100x 100x A ...
100x 100x A ...
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(SHIII)	100
300V AC	£2.70
S Meter 1mA.,	£2.75
VU Meter	£3.00
1A AC	* £2.65
5A AC	* £2.65
10A AC	* £2.65
20A AC	* £2.65
30A AC	* £2.65

CLEAR PLASTIC MODEL 38P Size: 42 x 42mm

£2.80 £2.765 £2.565 £2.500 £2. 2mA ... 5mA ... 10mA ... 20mA ... 100mA 150mA 200mA 300mA 750mA 1A DC 2A DC 15A DC 15A DC 20A DC 20A DC 3V DC 10V DC



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0	15V DC	£2.50
0	20V DC	£2.50
0	50V DC	£2.50
0	100V DC	£2.50
0	150V DC	£2,50
0	300V DC	£2.50
0	500V DC	£2.50
0	750V DC	£2.50
0	15V AC	£2.55
0	50V AC	£2.55
Ō	150V AC	£2.55
0	300V AC	£2,55
Ō	500V AC	£2.55
ŏ	S Meter 1mA	£2.55
0	VU Meter	£2.90

CLEAR PLASTIC MODEL 65P Size: 86 x 78mm

1mA 5mA 10m/ 50m/ 100m 500m 1A D 5A D 10A I 15A I 20A I



1mA		£2.85	10111
		£2.85	Hilling and Final
10m A		£2.85	ALL III
50mA		£2.85	William Control
100mA		£2.85	
500mA		£2.85	50V AC £3.10
1A DC		£2.85	150V AC £3.10
5A DC	•••	£2.85	300V AC £3.10
10A DC	•••	£2.85	500V AC £3.10
15A DC	••	£2.85	S Meter 1mA £3.15
20A DC	••	€2.85	VU Meter £4.10
30A DC	••	£3.10	14 40
	••		
50A DC		£3.20	5A AC £2.85
5V DC		£2.85	10A AC * £2.85
10V DC		£2.85	20A AC * £2.85
20V DC		£2.85	30A AC * £2.85
50V DC		£2.85	50m A AC • £2.85
150V DC		£2.85	100mA AC * £2.85
300V DC		£2.85	200mA AC * £2.85
15V AC		£3.10	
	••	20.10	500mA AC • £2,85
DAKELITE			80 Enlarged Window
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BAKELITE MO Size: 80 x 80mm

50uA 100uA 500uA 50-0-50uA .. 100-0-100uA .. 1mA 1A DC ... 5A DC ... 20V DC ... 50V DC ... 300V DC ... VU Meter



CLEAR PLASTIC MODEL 52P Size: 60 x 60mm

50uA 100uA 500uA 50-50uA 100-0-100uA ... 1mA 5mA £3.85 £3.30 £2.35 £3.35 £2.75 100-0-100uA 1mA ... 5mA ... 10mA ... 500mA ... 100mA ... 500mA ... 1A DC ... 1A DC ... 1A DC ... 10V DC ... 20V DC ... 20V DC ... 50V DC ...



S Meter 1	mA	١ ۵	£2.85
VU Meter	٠		£3.95
1A AC			* £2.75
5A AC			• £2.75
10A AC			* £2.75
20A AC			* £2.75
30A AC			* £2.75
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BAKELITE MODEL 65 Size: 80 x 80mm

£5.05 £3.30 £3.30 £3.30 £2.85

2	2011.4.0	
•	30V AC .	 * £2,85
5	50V AC .	 ° £2.85
5	150V AC .	 ° £2.85
5	300V AC .	 * £2.85
5	500V AC .	 £2.85
5	VU Meter.	 £4.00
5	1A AC .	 ° £2.85
,	5A AC	 * £2.85
5	10A AC	 * £2.85
,	20A AC	 * £2.85
5	30A AC	 * £2.85
,	50A AC	 ° £2.85
5	500mA AC	 £2.85
,	50mV DC	 £3.20
,	100mV DC	 £3.20

£3.97 P&P 15p 1-8 80×80mm £4.97 P&P 15p

1mA 1-0-1mA .. 5mA 10mA 50mA

500mA 1A DC 5A DC 15A DC 30A DC 10V DC 20V DC 50V DC



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VHM5/mm: 0.3-25 Preset triggered sweep 1-3000usec. Free running 20-200 kHz in nine ranges. Calibrator pips. 220 x 360 x 430mm, 115-230V AC OUR PRICE £39.00

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Tube. Y smp
sensitivity 0.1Vp-p/
CM. Bandwidth
1.5Hz-1.5MHz
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2 amp. sensitivity
0.9Vp-p/CM.
Bandwidth 1.5Hz
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Impedence 2 Mem base, five ranges
Ohms. 200 Hz. Superhornisation.
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220/240V AC. Supplied brand new
with handbook

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OSCILLOSCOPE
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amplifiers. Rectangular 5 = 44 CRT
Calibrated triggered sweep from 0,2usecto 100 milli-sec/cm
Free running time
base, 50Hz-1MHz.
Built in time base

A Calibrator and amplitude Calibrator. Supplied complete with all accessories and instruction manual

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Nine wave-bands covering 1.8-29.7 MHz, 144-146MHz and 10MHz WWV SSB, CW, AM and FM. AF output is more than 1 watt. S Meter. Squelch control. BFO. Variable AF and RF controls. 4-16 ohm output and jeck for phones. Power requirement 100, 240V AC, 12/14V DC. Size: 270 x 140 x 310mL

Our Price £132.50 PARP

TRIO 9R590S RECEIVER



Our Price £42.50 FARR TRID JR310 SSB RECEIVER



Covers 3.5, 7, 14, 21, 28, 28.5 end 29.1MHz bends and WWV 15MHz. SSB, AM and CW. AF output more then 1W. Crystal controlled BFO for SSB, S Meter, ANL etc. AC 110/120–220/240V. Size: 330 x 179 x 310mm. OUR PRICE £75.00 Carr. paid

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Fully transistorised portable
VHF transceiver
Will transmit and
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channels between
144—146MHz.
1 watt transmitter, 12V DC
Internal or external supply,
Bullt-in charger
for Ni-Cad cells.
Power/volume
switch, sgueloh or
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Power/volume switch, squeich control, chennel selector, mic. socket, serphone/externel speaker socket. Complete with microphone and 144,88, 144,72 & 145,72 crystate. Sizet 134 x 55 x 180mm.

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Four bands covering 860 KHz/30MHz BFO, Built-in speaker, Operates from 220/240V AC, Brand new with Instroutlone.
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Solid state mobile transceiver for 12 volt DC neg. Transmits and receives on any 1.40 28 channels between on any 1.40 28 channels between volume, squelch and channel selector. Internal 3" speaker. Complete with dynamic mic. PTT switch, three sats of crystals for 144.48, 144.6 and 146MHz, mounting bracket and instructions. Size: 150 x 70 x 220mm. OIIR PRIFF 575.00 P&P 500 OUR PRICE £75.00 P&P 500

LAFAYETTE HA600 Receiver



General coverage 150-400kHz, 550 kHz-30MHz, FET front end 2 mechanical filters, product detector. Noise limiter, variable BFO, S Metre, Bandspread and RF gain, 220/240V AC 12V DC. Brand new with instructions. OUR PRICE £50.00 P&P 50p

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Outstanding value.
With soft ear pads and adjustable headband.
8–16 ehms. 20–
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Light weight head-phones with padded ear pieces, 4/16 ohm 20—20,000Hz. Complete with 6' mplete with 6' Do **OUR PRICE** £1.97 P&P 30p

TE1018 Oeluxe Mono High Impedence Headset. Impedence readset.
Sensitive magnetic
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pads. Impedence 2,600
ohms (800 ohms DC).
Frequency response:
200—4,000Hz. 1 W

OUR PRICE £2,25 P&P 30p **DHO2S STEREO HEADPHONES**

Wonderful value and excellent and excellent performence combined. Adjust-able head band, Impedence 8 ohms 20—12,000Hz, Complete with lead and plug. OUR PRICE 62 25

P&P 30s **BH001 HEADSET and Boom**

Microphone Moving coil. Ideal for language teaching, communications etc. Headphone impederophone
dence 16 ohms. Mis se 200 ohms. OUR PRICE £5.95

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STEREUSUUM Matched peir of retereo bookshelf speakers. Delucie teak veneered finish. Size: 356 x 225 x 190mm. 6 ohms. 8 watta Paek. Complets with Din lead. OUR PRICE £12 0E £12.95





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All kits are complete with comprehensive easy to follow instructions and covered by full guarantee

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Recorder,
2 track BSR deck
with push button
controls for easy
operation. Tape;
counter and
volume control.
Complete with
hand microphone
direct recording

direct recording lead, 1,200' reel of tape and spare reel. 200/250V AC, Fully guaranteed. OUR PRICE £17.50 P&P 75p Philco Ford 5248 Mains Tape

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Plano key type controls, tape countrols, tape countrol

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Master and two sub-stations. Can be used on desk or well mounted. Complete with cable and betteries **OUR PRICE £5.25** P&P 80p

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To build yourself. Complete kit of parts with step by step instructions to build a full specification pocket sized OUR PRICE

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BSR 8 Track Player Chassis Famous BSR Strack chassis Brack chassis as used in model TD8S complete with silver and black escutcheon, ready to fit into cabinet. to fit into cabinet.
Output 125mV.
240V AC, Overell size app.

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MP7 MIXER-PREAMPLIFIER MP7 MIXER-PREAMPLIFIER
5 Microphone
inputs each with
individual gain
controls enabling
controls enabling
feelihies. Battery operated. Suze: 235
x127 x 76 mm. Inputs: Mics. 3 x 3 mV
50k; 2 x 3 mV 50k; 2 mP. hono. Mag.
am V 50k; Phono Ceramic 100mV 1
Meg. Output 250m V 100kg.

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6 transistor
high quality
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Ample output to feed most amplifiers.
Operates on 9V battery. Covers 88—
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Fantastic value for money.
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OTSSB OIGITAL CLOCK MECHANISM

with built in buzzer. On/off and successful and suc

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Clock
240V mains operation. Ivory asse with large clear numbers for hours, minutes and seconds. Size 189 a 76 x 82mm.

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AUDIOTRONIC AHA101 Stereo Headphone Amplifier All silicon, trensistor

trensistor emplifier oper ates from mag netic, ceramic or tuner inputs with twin stereo he 0 10.

headphone outputs and lume controls for each separate volume controls for each channel, Operate from 9V battery, INPUTS: 5mV and 100mV, OUTPUT: 50mV per channel.

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10 wave-bands covering AM: 535-1605kHz. LW: 150-380 kHz. MB 1.6-4MHz. SW1: 4-8MHz. SW2: 8-1.6 MHz. SW3:

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Noise Reduction Units
Reduce tape hiss by 3dB at 600Hz, 6dB at 1200Hz and 10dB for all frequencies above 3000Hz. Size: 460 x 203 x 79mm. AC 220/240V



PROCESS 4

For use with semi-professional tape recorders. Frequency response 30Hz – 20kHz ± 2dB. S/N better than 70dB. Full source/tape monitoring. Switchable multiplex filter. Supplied with

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For use with cassette and tape recorders. Frequency response 30Hz-20kHz. Switchable multiplex filter. 2 Dolby calibration meters. Off tape monitoring. S/N better than 70dB. Supplied complete with test tape or cassette. DUR PRICE £34.50 P&P 50p

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Instant recording and playing, Piano key controls. Automatic level control. Built-in speaker, Complete with rem-ots control microphone, carrying case **OUR PRICE £8.50**

AUDIOTRONIC ACO660 Stereo Cassette Deck



A beautifully styled four track stereo deck with an outstanding specification offered at a remarkable well conferred at a remarkable will be received the state of features including switchable noise filter, normal/chrome tape selector, twin VU meter sider record/playback level controls, front panel headphone socket, recording indicator lamp, phono/lin line input sockets, 3.5mm microphone insockets etc. Erequency response: 40–12kHz (40–16kHz CrOZ); S/N: 456B. Crosstalk 456B. Separation: 456B. Crosstalk 456B. Separation: 456B. Crosstalk 456B. Separation: 456B. Crosstalk

ecting leads. **OUR PRICE £39.50** P&P 50o AUDIOTRONIC LOW NOISE CASSETTES

TYPE C60 C90 C120 5 £1.37 £1.95 £2.38 10 £2.61 £3,70 £4.50 AUDIOTRONIC CrO2 CASSETTES TYPE CR60 CR90 10 £3.41 £4.63 £6.72 £9.19 £16.63 £22.80

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P&P Cassettes 3p, Cartridges 5p each OVER 10 of either FREE. WALKIE



DUR PRICE £24.95 per pair P302 Two Channel 300mW OUR PRICE £52.50 per pair P1003 Three Channel 1 Watt OUR PRICE £71.25 per pair P&P 50p per pair

NB. Licence required for use in UK

1021 Stereo Listening Station 1021 Stereo Listening undiging and gain selection of loudspeakers with additional facility for stereo switching. Two gain controls, speakers un off slide switch, stereo headphone socket.

P&P 15p OUR PRICE £2.25

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LSH20 Individual volume controls. Stereo/mono switch. 8 ohms. 40-- 19,000Hz. £3.75 P&P 30p

LSH30 Open bac type, Individual tone and volume controls, 8 ohms 30-20,000Hz DUR PRICE



volume controls. 8 ohms. 20-20,000Hz **OUR PRICE** £7.50 P&P 30p

LSH60 3" speaker units, 8 ohms, Complete with zipped carrying case, 20--20 000Hz **OUR PRICE** £8.95 P&P 30o

LSH50 Electrostatic with self powered energiser, and control unit, with headphone speaker selector. 4-32 ohrns 20-24,000Hz. **OUR PRICE** £16.95 P&P 30p

LQH400 4 channel dynamic head-phones. Each ear-peice has four drive units. 4-32 ohms 20-20,000Hz **OUR PRICE £9.95**











EA41 REVERBERATION AMPLIFIER

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Self contained, transistorised, battery operated Simply plug in microphone, guttal etc. and witput for your amplifier. Volume control and depth of reverberation control Beauwalnut cabinet, 184 x 77 x 108mm.

P&P 20p

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High quality 2 way speaker systems 25 Watts. 4-8 ohms. 40Hz-18kHz Size: 560 x 340 x 255mm. approx Wood grain finish with black fronts DUR PRICE £29.95 PR. P&P £1

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LINEAR 202 STEREO AMPLIFIER



20 Watts RMS Stereo Amplifier controls for volume, balance, bass and treble, Mono/Stereo switch, loudness and scratch filters. Uses 20 Silicon transistors. Inputs for magnetic and crystal cartridge, Aux. and tape.

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SPECIAL BARGAIN!! PHONIC 10 Two Way Speakers

Matched pair of compact book-shelf speakers of unique design Incorporating a 2" high frequency unit & 6" woofer. 8 ohms imped ence. Size: 348 x 228 x 110mm. 201 200

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LEAK TRUSPEED Mk3 RECORD DECK

PACKAGE Incorpor-ing low

low speed synchron ous hystresis motor giving constant turntable speed, 33 and 45 rpm. Cast Allumnium turntable, Fitted Goldring L75 arm and G800 cartridge, complete in plinth with perspeak cover. Size 321 x 400 x 10 mm, cover. AC100-130 and LNL 0.2 Cover. AC100-130 and LNL 0.

OUR PRICE £35.95 P&P 75p AUDIOTRONIC AMCSOE

STEREO Magnetic CARTRIOGE Made by SHURE the AMC50E offers prof-essional perf-ormance at a budget price. Frequency ~ ~

Frequency response: 20Hz-20kHz. Output voltage. 6.5mV. Compliance. 5 x 10-6 cm/dyne. Tracking force % to 2 grammes. Stylus: Efiptical diamond .0007" x .0002".

P&P 12p

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AD-76K STEREO MAGNETIC

Frequency Course: Some Source Course Course Course: Sm (11kHz 5 cm/sec). 0,7 mil conical diamond stylus. Channel separation 20dB, Tracking weight 114–2% gms. Original price 23.50 **OUR PRICE £1.95** P&P 12p

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£35.65 £40.90 £43.35 £45.65 £48.15 £23.70

6 watts per channel AM/FM Stereo tuner amplifier, Garrard 2025TC record deck with plinth, cover and stereo cartridge, and a pair of Keletron LS50 speakers. SUPER VALUE! OUR PRICE £48.50 & Ins. £1.25

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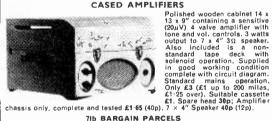
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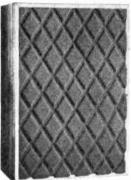
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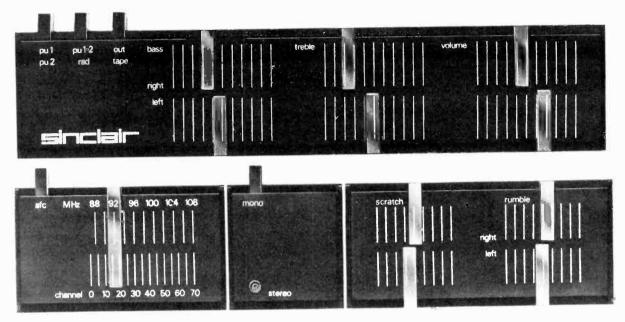
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Sinclair Project 80 exciting



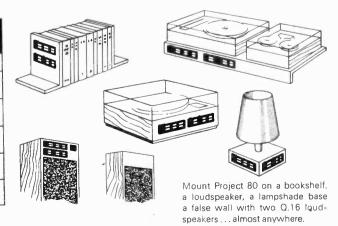
only $\frac{3}{4}$ " deep x 2" high

Living with hi-fi takes on new meaning with Sinclair Project 80. The electronics of these revolutionary new modules are all contained within elegantly designed matching cases no more than three-quarters of an inch deep. They are designed for mounting on any appropriate flat surface by means of 6BA bolts extending from the rear of each module and which pass through suitably drilled holes. Connections are taken away out of sight in a similar manner. The possibilities opened up by Project 80 are endless – superb hi-fi systems can be installed in ways hitherto only dreamed about and never before made practical. No more cutting out and shaping to put modules in position. A few holes drilled with the aid of templates supplied and the job is done. Now you need never again be faced with problems of keeping the hi-fi from clashing with carefully thought-out furnishing schemes. (That will surely please wives!) Slider controls have been introduced in place of knobs and all modules in the range incorporate new up-dated circuitry with emphasis on performance standards and built-in protection against overload and shorting. The aim was to re-think modular construction completely — to make it infinitely more versatile, even simpler and more reliable — the result — Project 80 — another triumph for Sinclair, and the most exciting construction modules ever.

the slimmest, most elegant hi-fi modules ever made

System	The Units to use	Units cost
Simple battery record player	Z.40	£5:45 ±54p V.A.T.
Mains powered record player	Z.40, PZ.5	£10·43 +£1.04 V.A.
30W. RMS continuous sine wave stereo amp.	2 × Z.40s, Stereo 80; PZ.6	£30.83 +£3.08 V.A
50W (8 Ω) RMS continuous sine wave de luxe stereo amp	2 × Z.60s, Stereo 80; PZ.8	£33 83 +£3.38 V.A
Indoor P.A.	Z.60, PZ.8	£14 93 + £1.49 V.A

Project 80 FM tuner, decoder, and A.F.U. may be added as required



new thinking in modular hi-fi

Stereo 80 pre-amplifier and control unit



Simplest ever fixing

Each channel has its own separate tone and volume controls operated by sliders, enabling ideal environmental matching to be obtained. A virtual earth input stage forms part of the up-dated circuitry that ensures the finest possible quality from all signal sources. Generous overload margins are allowed on all inputs. Clear instructions with template are supplied.

TECHNICAL SPECIFICATIONS

Size $-260 \cdot 50 \times 20$ mm $(10\frac{1}{4} \times 2 \times \frac{3}{4}$ ins)

Finish - Black with white indicators and transparent sliders

Inputs – Magnetic pick- up 3mV RIAA corrected, Ceramic pick- up 300mV Radio 300mV; Tape 30mV Signal/noise ratio – 60db Frequency range – 20Hz to 15KHz \pm 1dB, 10Hz to 25KHz \pm 3dB

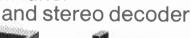
Power requirements — 20 to 35 volts

Outputs — 100mV + AB monitoring for tape

Controls — Press button for tape radio and P.U. Sliders for volume, bass (+ 12dB to - 14dB at 100Hz) treble (+ 11dB to - 12dB at 10KHz)

R.R.P. £11.95 +£1.19 V.A.T

Project 80 FM tuner







Twin dual varicap tuning: 4 pole ceramic filter: switchable A.F.C.

On the decoder, solid state stereo indicating beacon.

Making the Project 80 F.M. tuner and decoder available separately gives a wider choice of systems and saves money where stereo reception may not be required. The tuner is a triumph of electronic design and assures excellent performance. The decoder gives a 40dB channel separation with 150mV output per channel. Both units may be used with other than Project 80 systems.

TECHNICAL SPECIFICATIONS OF TUNER

Size $-85 \times 50 \times 20$ mm $(3\frac{1}{2} \times 2 \times \frac{3}{2}$ lns) Tuning range -87.5 to 108 MHz

Detector - I.C. balanced coincidence for good A.M. rejection

One I.C. equal to 26 transistors

Distortion = 0.2% at 1 KHz for 30% modulation 4 pole ceramic filter in 1.F. section Aerial impedance = 75 Ω or 240-300 Ω

Sensitivity - 4 microvolts for 30dB quieting Output - 300 mV for 30% modulation Power requirements - 23 to 33 volts

DECODER

Size $-47 \times 50 \times 20$ mm (17 × 2 × 2 ins) One 19 transistor I.C.

R.R.P. £11.95 +£1.19 V.A.T.

R.R.P. £7.45 +0.74

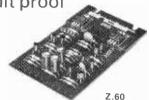
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Z.40 & Z.60 power amplifiers totally short-circuit proof





Intended for use in Project 80 installations, these modules readily adapt to an even wider range of applications. Both incorporate built-in protection against short circuiting and risk of damage from mis-use is greatly

Z.40 TECHNICAL SPECIFICATIONS

Size $-55 \times 80 \times 20$ mm ($2\frac{1}{8} \times 3\frac{1}{8} \times \frac{3}{8}$ ins) 9 transistors Input sensitivity -100mV

Output - 15 watts RMS continuous into 8 Ω (35v)

Frequency response – 10Hz – 100KHz ± 1dB Signal/noise ratio – 64dB

Distortion - at 10 watts into 8 Ω less than 0.1%

Power requirements - 12 to 35 volts

Z.60 TECHNICAL SPECIFICATIONS

Size $-55 \times 98 \times 15$ mm ($2\frac{1}{8} \times 3\frac{3}{4} \times \frac{3}{4}$ ins) 12 transistors Input sensitivity $-100 \cdot 25$ 0mV

Output - 25 watts RMS continuous into 8 Ω (45V) Distortion - typically 0.03%

Frequency response – 10Hz to more than 200KHz \pm 1dB

Signal/noise ratio - better than 70dB

Built-in protection against transient overload and short circuiting Load impedance - 4 \(\Omega \) min; max safe on open circuit

Project 80 active filter unit

Z.40 R R P. £5.45 + 0 54 V A T , Z.60 R R P £6.95 + 0 69p V.A.T.

Makes a highly desirable part of any worthwhile system where inputs may be from record, radio or tape. As with Stereo 80. separate controls applied to each channel make it easier to obtain ideal stereo balance.

TECHNICAL SPECIFICATIONS

FIGURE SPECIFICATIONS Size $-108 \times 50 \times 20 \text{mm} (4\frac{1}{4} \times 2 \times \frac{3}{4} \text{ns})$ Voltage gain - minus 0.2 dB Frequency response -36 Hz to 22 KHz controls minimum Distortion - at 1 KHz - 0.03% using 30 V supply HF cut off (scratch) -22 KHz to 5.5 KHz, 12 dB/oct, slope 1.5 mm/s (furphle) -3 dB/octL.F. cut off (rumble) - 28dB at 20Hz, 9dB/oct, slope

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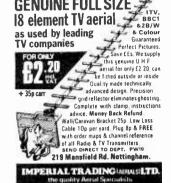
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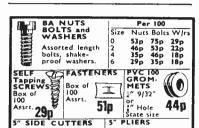
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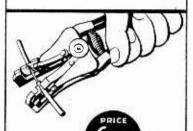
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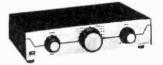
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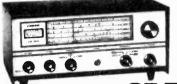
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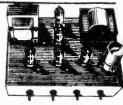
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