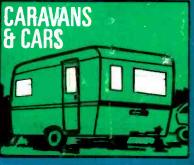
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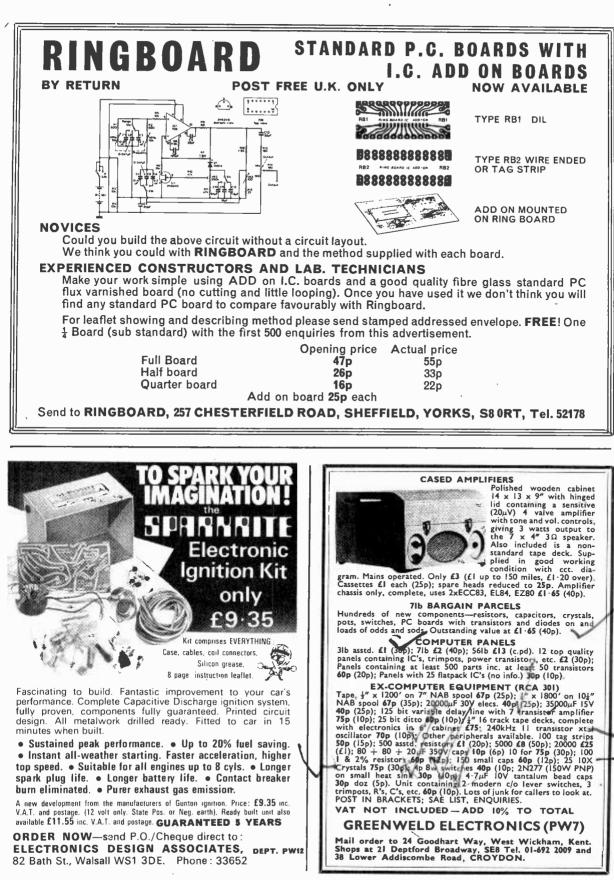
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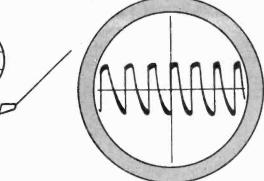
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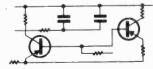
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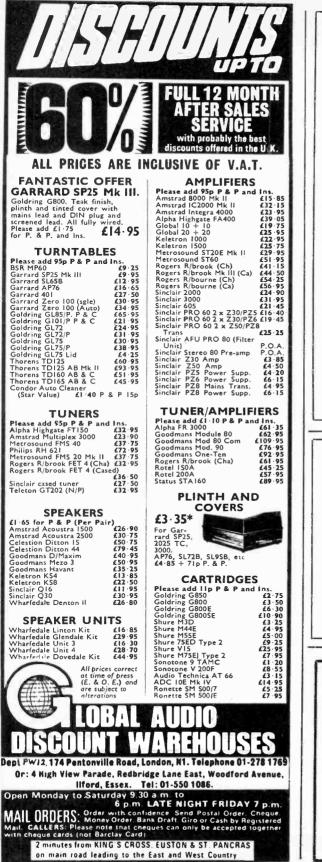
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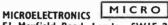
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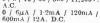
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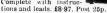
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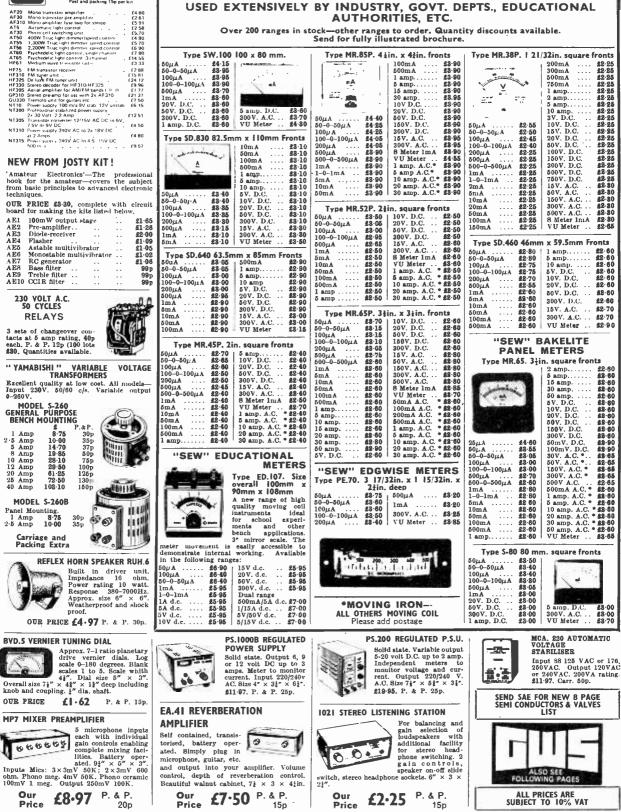
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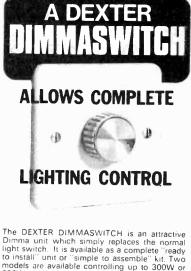
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19	RAND NEW AND FUL	69p:1N4004	7p:2N6027(D1	371)	CAPACITORS ELECTROLYTIC AXIAL LEADS Mld. Working Price Mld. Working Price
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AC126 20p BCY71 AC127 25p BCY72	26p CA3044 £1-28 NKT773 14p CA3046 70p NKT781	29p 1N4007	9p 3N128	73 p 92 p	10 100v 8p 100 25v 9p 2·2 25v 10p 100 40v 10p
AC128 24p BD124 AC128/AC176 BD131	75p CA3048 £2 11 NTGD10 40p CA3052 £1 62 OA10	40p 1N4148 40p 1N5400	4p 3N140 14p 3N152	92p £1.50	2-2 63v 8p 100 63v 13p 4 7 40v 8p 220 25v 11p
44pBD132 AC151 20pBD131/132	40 p CA3065 £1 28 O A47 80 p CA3088E £1 24 O A79	8p 1N5404 8p 1N5408	18p 3015F 25p 3015G	£2.00	10 25v 8p 220 40v 12p 10 63v 9p 470 25v 14p
AC152 25p BDY20 AC153 26p BF115	91p CA30895 £1-96 OA90 23p CA3090Q £4-23 OA91	6p1544 5p15920	4 p 7400 7 p 7401	20 p 20 p	22 25v 9p 1000 25v 21p
AC176 20p BF163 AC153/176K 52p BF167	35p CD4001AE 55p OA95 25p CD4009AE £1 16 OA200	50 15940 60 2N404	6p:7402 23p:7403	20 p 20 p	47 25v 9p 4700 16v 46p
AC187K 17p BF173 AC188K 23p BF177	29p CD4011AE 55p OA202 25p CD4012AE 54p OC25	7p12N696 45p12N697	15p 7404 17p 7405	25p 25p	47 40v 9p
AC187/188K 40p BF178 ACY17 27p BF180	31p CD4013AE £1 11 OC28 35p CD4015AE £2 92 OC29	78p 2N698 79p 2N706	30p 7408 10p 7409	25p 25p	CAPACITORS-METALLISED POLYESTER Stock values: MFD Price each
ACY18 20p BF194 ACY19 20p BF195	15p CD4017AE £2-9210C35 15p CD4018AE £2-9210C36	66 p 2 N 706 A 69 p 2 N 708	12p 7410 16p 7413	20p 30p	0·01, 0·015, 0·022, 0·033 4p 0·047, 0·068, 0·10 5p
ACY20 20p BF196 ACY21 19p BF200	15p CD4020AE £3 25 OC41 35p CD4024AE £2 09 OC42	40p 2N911 40p 2N914	50p 7420 20p 7425	20 p 30 p	0·150, 0·220 6p 0·33 8p
ACY22 10p BF254 AD140 60p BF255	14p CR1/051C 54p OC44 15p CR1/401C 71p OC45	20p12N918 20p12N929	42 p 7430 25 p 7440	20 p 24 p	0-47 9p 0-68 12p
AD149 60p BFX13 AD161 44p BFX29	25p CRS3/05AF OC71 32p £1:08 OC72	20p 2N930 20p 2N1131	28p 7442 24p 7443	£1-16 £1-45	1.0 15p 1.5 22p
AD162 44p BFX84 AD161/162 88p BFX85	25p CRS3/40AF OC75 34p £1:53 OC76	25p 2N1132 25p 2N1302	24p 7444 17p 7445	£1-45 £2-06	2-2 26p Order as "Polyesters" + Capacitance.
AF106 32p BFX86 AF114 27p BFX87	25p CZ6 17p OC77 30p D10 (NTGD10) OC81	40 p 2N1303 20 p 2N1304	17p 7446 24p 7447	£1-45 £1-25	CAPACITORS-POLYSTYRENE
AF115 27p BFX88	24p 40p OC81D 22p IRT84 £2.90 OC83	20p 2N1305 23p 2N1306	24p 7450 30p 7451	20 p 20 p	Axial leads, Clear encapsulation, 5% Tolerance, 160 volt working. Stock values Price
AF117 25p BFY51	19 p R2160 95 p O C 84	25p 2N1307	30 p 7453 34 p 7454	20 p 20 p	10pF, 15pF, 22pF, 33pF, 47pF, 68pF, 100pF, 150pF, each 220pF, 330pF, 470pF, 560pF, 680pF, 820pF,1000pF, 1500pF.
AF118 44p BFY52 AF124 25p BFY53 AF125 24p BFY90	20p IRC20 46p OC139 17p JA424 £2:08 OC170 £1:20 LIC709C/5 42p OC171	25p 2N1308 25p 2N1309 30p 2N1559 (CF	34p 7460	20p 45p	2200pF, 3300pF, 4700pF, 5600pF, 6800pF 400pF 4p Order as: "Polystyrenes" + Capacitance.
AF126 24p BP101	£1-20 LIC/09C/5 420 OC1/1 £1-40 LIC709C/8 420 OCP71M £1-50 LIC723C/5 £1-02 ORP12	42p 401C)	71 p 7472 15p 7473	32p 45p	NEW LOW PROFILE IC HOLDERS
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AF279 58p BSX20	16P LIC741C/8 34P ORP69	50p 2N1893 50p 2N2218	54p 7475 33p 7476	45p 67p	NYLON NUTS AND BOLTS
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PRICES : SYSTEM I

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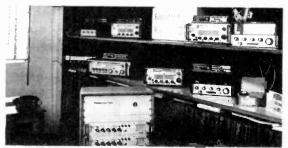
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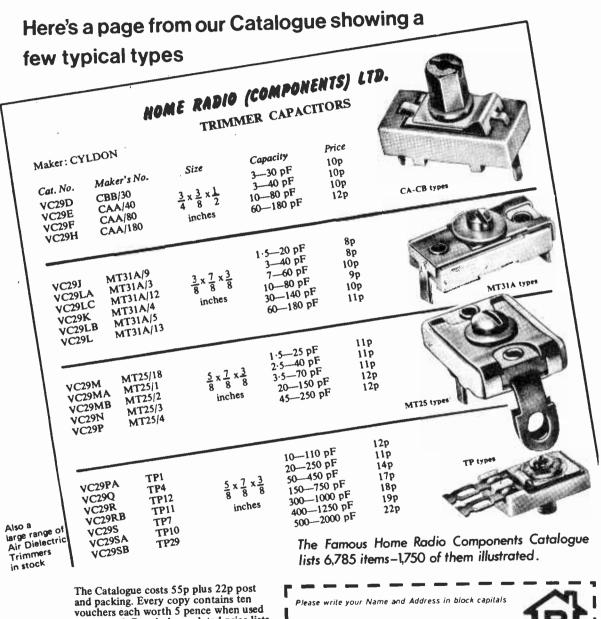
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		232 18·30 226 28·70	1 · 00 1 · 10	0-15-20	0-15-20	500	500	200	2.16	0.38
The safe, quick, con nector for electrical		20 20 10	1.10	0-20	0-20	300	300	214	1.86	0.22
appliances, 13 Ann				20-12-0-1	2-20	700(D/C 1000	³	221 206	1.21	0.30
rating, fused, will	Prim:- 200-24 Amps 7	40V. Sec:- 12, 15, 20 Type Price), 24, 30V. P& P	0-15-20	0-15-20	500	1000	206	3·10 2·88	0 · 38 0 · 38
connect a number		1 ype Frice	0.22	0-15-27	0-15-27	1000	1000	204	2.40	0.38
of appliances quickly and	1	79 1.64	0.38							
safely to	2	3 2·45 20 3·00	0.38	PLASTIC	CASED	SILICON BRI	DGE RE	CTIFIERS		
the mains.		20 8.00 21 8.55	0.42	One Amp	Two Am			Amp		A
ideal for testing, den:-		51 4-40	0.52	50 Volt 2	5p 50 Vol	t 85p 100 Volt	55p 50	Volt 65p		
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window dis-		88 6·80 89 8·86	0.67	600 Volt 8				Volt 80p Volt 90p		-
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connecting when live.	PLEAS	E ADD 10%	FOR	VAT	1	ADD 10p F	P & P			
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BA1 51" × 92" × 11" 40-		4.7K, 10K, 22K, 47K, 100K, 220K, 470K, 1M, 2M	assorted into the following groups:			
BA3 4" > 21" × 11" 41p	C16 20 Assorted Tag strips & Panels 0.55	VC 1 Single less Switch 0-14	R1 50 Mixed 100 ohms-820 ohms 40p R2 50 Mixed 1K ohms-8:2K ohms 40p			
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9 part car, 9,13*3,30	and sign supprox until / Fil. Del. 61593 1	4K7. 100K, 220K, 470K, 1M, 2M, 4-7M	C60, 32p C90, 41p C120, 52p			

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ideal for use in record players, tape recorders, stereo amplifiers and cassette and cartridge tape players in the car and at home.

Parameter	Conditions	Performance	
HARMONIC DISTORTION	Po = 3 WATTS f=1KHz	0.25%	
LOAD IMPEDANCE		$8 - 16 \Omega$	
INPUT IMPEDANCE	f=1KHz	100 k Ω	
FREQUENCY RESPONSE OF 3dB	Po=2 WATTS	50 Hz - 25KH	
SENSITIVITY for RATED O/P	$V_8 = 25V$. $R_l = 8\Omega$ $f = 1KHz$	75mV. RMS	
DIMENSIONS	_	3" × 21" × 1"	

The above table relates to the AL10, AL20 and AL30 odules. The following table outlines the differences their working conditions.

Parameter	AL10	AL20	AL30 30 10 watts RMS Min.		
Maximum Supply Voltage	25	3:0			
Power output for 2% T.H.D. (RL = $\delta \Omega f = 1 \text{ KHz}$)	3 watts RMS Min.	5 watts RMS Min.			
AL 20. 5 watts RMS #	PRE- PA 12. PA 100. 22-59 3-01	AMPLIFIER (Use with ALI (Use with AL3	25 0 & AL20) £4-35 0 & AL50) £13-15		
FRONT PANELS SP 12 with Knobs	88p) T461 (U 3.95 T538 (U	TRANSFORMERS T461 (Use with AL10) £1.38 P & P 15) T538 (Use with AL20) £1.98 P & P 15) BMT80 (Use with AL30 & AL50) £2.15 P & P 25) P & P 25)			

PA 12. PRE-AMPLIFIER S

The PA 12 pre-amplifier has been designed to match into | Fr most budget stereo systems. It is compatible with the AL 10, AL 20 and AL 30 audio power amplifiers and it can be supplied from their associated power supplies. There are two stereo inputs, one has been designed for use with *Ceramic cartridges while the auxiliary input will suit most †Magnetic cartridges. Full details are given in the specification table. The four controls are, from left to Volume and on/off switch, balance, bass and treble. right Size 152mm × 84mm × 35mm

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± 12dB at 60Hz
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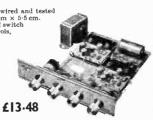
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The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and tested on a one-piece chassis measuring 20 cm \times 14 cm \times 5.5 cm. This compact unit comes complete with on/off switch This compact unit comes complete with on/off swi volume control, balance, bass and treble controls, Transformer, Power supply and Power ampa. Attractively printed front panel and match-ing_control knobs. The 'Bkerco 20' has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively, into a separate cablact. Output power 20w peak. Input 1 (Cer.) 300mV into 1M. Freq. res. 26Hz-25kHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Bass control ± 12dB at 60Hz typically 0.25% at 1 watt. Treble con. **£1**



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THE AL50

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bass and treble controls.



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<u>"STEAM" ROLLING</u>

ANNUAL Reports and Accounts of major organisations do not usually make exciting reading, but the latest from the IBA is different because of the entries describing the planning of independent commercial radio under the IBA banner.

Most of the information we are either aware of already, or we took for granted as being necessary minimum standards that are laid down to match the existing performance by the BBC. However, one or two interesting points emerge that have an important bearing for the listening audience.

The IBA, with very good reason, intends to encourage the major proportion of listening on v.h.f. The International Telecommunication Union is due to review the allocation of m.f. bands, under the present Copenhagen Convention and Plan, in 1974-5. Any proposed revisions are expected to take effect from 1976 and both the BBC and the IBA are expecting a reduction in the m.f. allocation largely due to "overcrowding". In the meantime both organisations continue to operate sound broadcasting on m.f. as a back-up for v.h.f.

The crunch is in sight for the listeners because it looks as if they must expect, after nearly twenty years of v.h.f. broadcasting, to convert to v.h.f. reception or go without. We have heard the pros and cons of v.h.f. and m.f. so many times that we will not pursue the matter here. Suffice it to say that the IBA are looking ahead to the "day of judgement" by planning in force for circular polarised transmitting aerials to compromise between horizontal and vertical polarised receiving aerials.

The m.f. transmitting aerials will be directional systems using three or four mast radiators so that several stations can transmit over a restricted area on 1151kHz. The radiated power will vary from one station to another, depending on local conditions, but in London it will be 0.5 to 1kW; elsewhere up to 5kW, with an 8kW mf1 and 30kW mf2 signal from Saffron Green (not until later next year) for London, when the IBA have finished with the installations at Lots Road Power Station.

The method of m.f. transmission adopted is not commonly used in Europe and it makes one wonder why not, even if large sites are necessary.

The other disturbing thought is the increasing availability of stations broadcasting on v.h.f. With the undesirable side-effects (such as "birdies" and inter-modulation distortion) and the greater sensitivity of tuner front-ends, we forecast a congestion (or indigestion!) problem on v.h.f. in the U.K. within the next five years. Some serious thinking and re-appraisal is therefore going to be needed with a view to extending the broadcast v.h.f. range below 88MHz; although we understand that a clash has occurred in Hertfordshire and the police service is expected to be moved to another frequency, it would be wishful thinking to expect the emergency services to be transferred out of their present 97MHz-plus domain. M. A. COLWELL-*Editor*

The January issue, on sale 7th December, will include an Ultrasonic Remote Control Unit to switch on the television, radio, lamps, or almost any electrical device or appliance, without moving out of your armchair; a practical way of housing plug-in circuit boards; a signal generator for testing and fault finding in radio and audio equipment; an article dealing with radio interference problems in audio equipment; and first details of our plans for some of the spring issues of Practical Wireless, including some superb new ideas to help you make the most of d.i.y. radio and electronics.

Further details on page 751.



Mid-Lanark A.R.C.

THE above club has sent us some details of the future programme. There will be a bring-and-buy sale on Nov. 9, a demonstration of stereo radio and quadraphonic sound by GM3UCI on the 23rd and the A.G.M. on December 7th. December 21st is called "Oklahoma" and GM3BVU will give a talk on Amateur radio in the U.S.

Meetings are held at 7.30 in the Wrangholm Hall Community Centre, Jerviston Road, Motherwell.

Sonex 74

THE venue for Sonex 74 European High Fidelity Exhibition will be The Post House Hotel, London Airport and the dates March 29th to March 31st.

WIRELESS TELEGRAPHY ACT

Readers and advertisers are reminded of the requirements laid down by the Wireless Telegraphy Act. It is an offence in the U.K. to install or operate wireless telegraphy apparatus except under the provisions of the Act and, except in the case of broadcast sound-only receivers, a licence must be obtained from the Minister of Posts and Telecommunications.

Included within the provisions of the Act are any apparatus transmitting deliberate signals for any purpose such as "walkie - talkies", radiocontrolled models or servos and some types of metal detectors. Apparatus radiating interference signals are subject to controls which also come under the administration of the same Ministry. If you require full information, please write to the Ministry of Posts and Telecommunications, Waterloo Bridge House, Waterloo Road, London, SE1 8UA.

CRATA IS COMING Watch P.W. for details



Open University Course

E LECTROMAGNETICS and Electronics, a Post-experience course by the Open University, aims to provide an understanding of the scientific basis of electronics and electronic circuit design.

The course is intended for those preparing for higher level university study in science and technology and for those who need a knowledge of electronics but who do intend to study at a higher level.

It assumes little prior knowledge of electronics or electromagnetics but does assume a background of scientific or technical education beyond GCE "O" Level.

The first part deals with the basic ideas of electricity, magnetism and electromagnetism, semiconductors and the properties of simple circuits. The remainder deals with electronic circuits, stressing the need to design circuits to meet specifications of noise, distortion, output voltage as well as gain and input and output impedance.

Applications are now invited for the course which starts next February and lasts until November. As with all Post-experience courses, no formal academic qualifications are needed. They are self-contained courses designed to teach new developments or update knowledge of a subject.

The course consists of 17 written correspondence units linked to 17 television and five radio programmes. Students are required to attend a one week residential summer school and encouraged to attend evening or Saturday tutorial sessions. There are 12 assignments to complete and an examination at the end of the course.

A home experiment kit, including a cathode-ray oscilloscope and a signal generator, is sent to students who are expected to design and build circuits for checking at summer school.

Some elementary mathematics is required for the course. Students should know elementary calculus, the meaning of sine, cosine and imaginary numbers. A preparatory booklet is issued at the beginning.

The course tuition fee is £45 plus £37 for the residential summer school. Application forms are available from The Post-experience Student Office, P.O. Box 76, Milton Keynes, MK7 6AA.

What of D.N.L.?

PHILIPS Ltd. will be using the Dolby-B noise reduction system!!

Scottish show cancelled

B ECAUSE of lack of interest, the Scottish International Hi-Fi Exhibition has been cancelled. Only 12 of the expected 27 firms confirmed their bookings for the show.

The organisers feel that the reason for the lack of interest is that many companies have stretched their budgets by representation at the Harrogate and Olympia shows.

Tyne/Wear radio contract

A FTER interviewing the six applicant groups for the Tyne/Wear radio contract, and giving full consideration to the written applications, the Independent Broadcasting Authority has announced that it has formed the view that Metropolitan Broadcasting is the leading contender.

The Authority now proposes, subject to contract, to offer the franchise to Metropolitan, the chairman of which is Sir John Hunter.

The company's programme plans will be published when it begins broadcasting — probably during the summer of 1974.

More for SQ

MORE manufacturers are getting onto the quadraphonic bandwagon by building SQ decoders into their equipment. Companies like Braun, Grundig, Korting, Philips, Revox, Saba, Sharp, Siemens have taken out SQ licences with CBS.

Physics Exhibition

THE Council of the Institute of Physics has decided that the Physics Exhibition should now be discontinued, and the show arranged for 1975 will now not take place.

In recent years the number of visitors to the exhibition has decreased considerably as have the number of industrial firms and other concerns that used to have exhibits there.

The very first Physics exhibition was held by the Physical Society in 1905. The one held in 1973 was the fifty-seventh in this series.

New 4-channel system

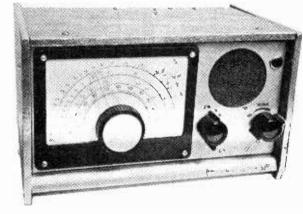
A NEW quadraphonic sound system devised by Duane Cooper and developed by Nippon Columbia was demonstrated at the Berlin Radio Show. The new system is called New Discrete or Discrete Matrix. It is said to have certain advantages over other quadraphonic systems because of its dual nature. A typical set-up would use a twochannel matrix for surround sound named BMX. This involves 45° phase shifts between the speakers rather than conventional 90° ones.

If increased definition in image placement should be required, a demodulator for the carrier channels on the records would be added, giving the set-up a potential 20dB separation between channels at midfrequencies.

The Discrete Matrix system allows the two extra channels contained on the gramophone record to be of a narrow bandwidth resulting with the maximum frequency of the record being 36kHz compared with 45kHz on the CD-4 records.

Noise reduction techniques are not employed with this system, so making demodulators potentially cheaper.

F. G. RAYER G30GR



\ECEIVER

THIS receiver employs two transistors and two IC's, one of the latter in the intermediate frequency amplifier section and the second in the driver and output stages. It has band switching and covers all the important short wave ranges, including the low frequency bands, which are not included in some short wave or "all-wave" receivers.

 $\Box \Delta F$

The receiver has a very inexpensive but quite attractive cabinet and operates an internal loudspeaker, a jack allowing headphones to be plugged in when preferred.

MIXER STAGE

The mixer section is shown in Fig. 1 and uses six miniature coils, the appropriate coils being selected by the 3-way 6-pole rotary switch. Each range is separate from the others and two coils are in circuit for each range. L1, L2 and L3 are the aerial coils, and L4. L5 and L6 the oscillator coils.

The six poles of the switch are numbered from S1 to S6. Pole S1 takes the aerial circuit to the aerial coupling windings of the aerial coils and S2 transfers the aerial tuning section of the gang capacitor, VC1, to the correct coil, for aerial tuning purposes. Pole S3 connects the base of Tr1 to the base coupling windings, as necessary. The earthed ends of all aerial coupling windings (pin 9) and tuned windings (pin 1) are permanently connected to the chassis, while all the base coupling windings are returned to the base bias network R1/R2.

In a similar manner, switch section S4 selects the collector coupling windings of the oscillator coils L4, L5 or L6, while S5 connects the emitter of Tr1 to the appropriate emitter winding. S6 selects the tuned windings of the oscillator coils which are tuned by the second section of the ganged capacitor, VC2.

All the emitter windings (pin 7 of each coil) are returned to the emitter bias circuit, C2 and R3. In the same way, each collector winding (pin 8) goes to the IF amplifier. In order to secure proper coverage and tracking, oscillator coil L5 has a padder capacitor CP1 of 3000pF from pin 4 to chassis. L6 has a 1000pF capacitor CP2 from pin 3 to chassis while L4 requires no padder, pin 6 being wired to the chassis.

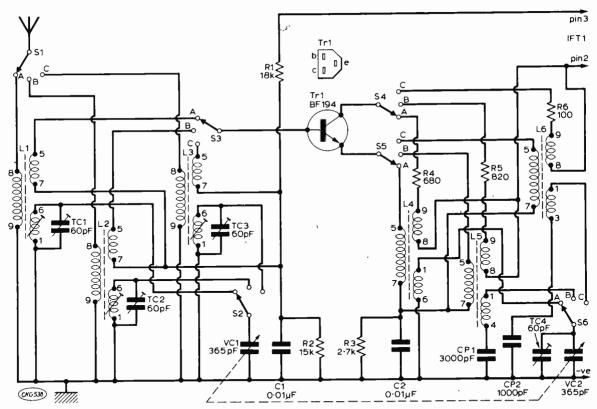
If the circuit in Fig. 1 appears difficult to follow. it is suggested that the switch is set at its middle position and L2 and L5 wired in. The receiver can then be tested on this band. When it is found to be in order L1 and L4 can be added and wired and a check made that this works correctly, before adding L3 and L6. This is much better than wiring in all the coils, then perhaps finding that a mistake has been made with the switch contacts or the operation of the switch, so that some wiring error is difficult to locate and correct. To avoid any possible confusion here, the bands, approximate coverage, and maker's range numbers are as follows:—

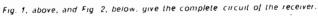
Band	Coverag	e Ma	iker's Range No.
Α	30—10·5MHz	10— 28m	5T
В	15— 5 MHz	20— 60m	4 T
С	5— 1 7MHz	60—180m	3T

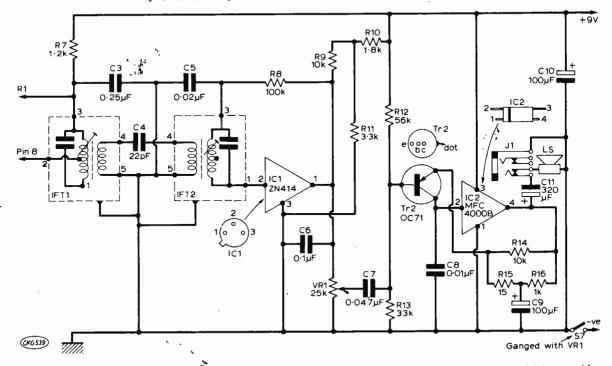
L1 and L4 are for Band A, L2 and L5 for Band B and L3 and L6 for Band C.

In order to avoid squegging, or spurious oscillation and hissing spoiling reception, resistors R4, R5 and R6 are included in the individual collector circuits to L4, L5 and L6. The best values for these resistors depend on Tr1. Gain is maximum when these resistors are of the lowest values which allow proper working of this stage. The values shown should certainly be satisfactory, but it is an easy matter to have on hand a few resistors of various values between about 100 Ω and 1k Ω (say about half a dozen different values) and try these in series with the circuit to pin 9 of each range, while tuning over the range. Excess oscillation is most likely at the high frequency end of any one band (VC2 nearly fully open).

Trimmers TCl, TC2 and TC3 are for aerial circuit trimming and each is adjusted on the appropriate band.







IF AMPLIFIER

Fig. 2 is the circuit of the intermediate frequency amplifier and audio amplifier, which are constructed on one small circuit board. The IF filter consists of two loosely coupled units, IFT1 and IFT2, tuned to 470kHz. Output from IFT2 goes to IC1 which provides three stages of amplification at 470kHz and includes automatic gain control and detection circuitry, giving an audio output which is taken to the volume control VR1.

Resistors R10 and R11 form a potential divider across the 9V supply and current is taken by IC1 and VR1 through R9. This means that the circuit should not be operated with VR1 disconnected and that this potentiometer should be of the value given.

The mixer stage is fed from its own positive supply point at the junction of C3 and R7.

AF AMPLIFIER

Tr2 is a high gain pre-amplifier, followed by IC2 which has 6 transistors and 3 diodes in a driver-pushpull output circuit which delivers approximately 250mW to a 16 Ω speaker. This IC is very economical on battery current and the output is easily adequate for normal loudspeaker reception. The load impedance is not too critical, so that speakers of higher impedance may be used. R14, R15 and R16 provide direct current feedback to stabilise the whole audio amplifier.

CIRCUIT BOARDS

The mixer board is approximately $1^{1}_{4} \times 1^{3}_{16}$ in, Fig. 3, with a bracket fixed as shown and a tag serving as a return point for C1, C2, R2 and R3. This bracket must be bolted tightly to the metal chassis so that the board is connected to the negative line.

External connections will be required to a few points. These can be made by providing Veropins, or by leaving a projecting wire, so that leads can be soldered on as necessary.

The small pins of Trl project from the underside of the board and connecting wires are soldered directly to them which will run to the sections of the bandswitch, as indicated in Fig. 3.

Both sides of the IF/AF board are shown in Fig. 4 and it is approximately 3_{4}^{5} x 1_{4}^{1} in. Holes should first be drilled to clear the pins and can tags of the two IF transformers. If any small error is made when drilling these, they can be enlarged or elongated as necessary with a very small round file. Drill holes for two 6BA bolts, one marked MC is fitted with a tag which forms the negative return

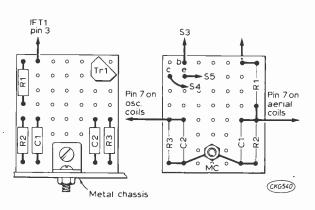


Fig. 3: Layout of components on the mixer board.

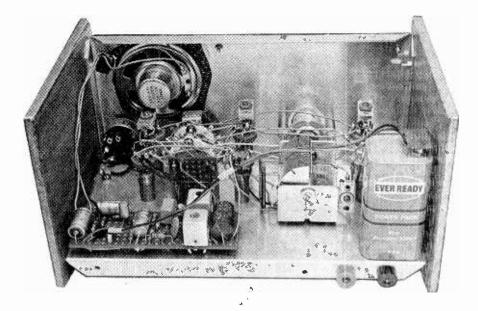
to the metal chassis. These bolts should be at least $^{1}2in$. long so that spacers or extra nuts will allow the board to be clear of the metal chassis.

C4 is underneath, directly from pin 4 of IFT1 to pin 4 of IFT2, but all other items are on top \Im f the board. Position these as shown, noting the polarity of electrolytic capacitors.

In most places the wire ends of the resistors and other items are long enough to reach the connecting points. Elsewhere, 24 s.w.g. tinned copper or similar connecting wire can be used. Sleeving is put on all leads which cross other wires and anywhere else where this appears necessary.

Two thin flexible leads are soldered on to connect to the speaker. A red flexible lead, with a positive battery clip, is also provided, as shown.

Colour coded leads also run from R9 and the base of Tr2. C7 is soldered directly on the centre tag of the volume control, VR1. Fit a colour-coded lead from C3, to run on to R1 on the mixer board. A further, lead is taken from pin 2 of IFT1, up through the board as in Fig. 4, and will be soldered to the circuit which connects pins 8 on the oscillator coils.



Rear view of receiver showing position of IF/AF board at front left with mixer board immediately behind.

★ components list

Contractions of the second sec
Resistors R1 18kΩ R7 1 2kΩ R13 33kΩ
R2 15kΩ R8 100kΩ R14 10kΩ
R4 680Ω* R10 1.8kΩ * R16 1kΩ
R5 820Ω* R11 3·3kΩ
R6 100Ω* R12 56kΩ VR1 25kΩ log ·
with switch, S7
Resistors 1W 5%. * See text ,
Capacitors
C1 • 0·01µF C9 100µF 10V
C2 0.01µF C10 100µF 10V
C3 0 25µF C11 320µF 10V
C4 22pF CP1 3000pF
C5 0 02µF CP2 1000pF
C6 0-1µF VC1/2 2 x 365pF (Jackson
C7, 0.047/JF Type O. Cat. No. 5250/2)
C8 0.01µF TC1-4 60pF pre-set trimmers
1
Semiconductors
Tr1 BF194 IC1 ZN414) S.C.S. Components
Tr2 OC71 IC2 MFC4000B POB 26, Wembley,
Middx.) 🔅 📉
Miscellaneous
IFT1/2 (Denco IFT13). L1, Blue 5T: L2, Blue 4T
13 Ripe 3T. L4, Red 51, L5, Red 41, L0, Red 01,
(All Denco). Tuning drive (Jackson Type 6/35 Cat.
No. 4103). S1-6, 2 wafer switch, each 3 pole 3 way.
Speaker, 21in, 25 to 400. Universal chassis mem-
bers, 8 x 4in (2) (Home Radio). Switched output Jack
socket. Aerial and earth sockets. Veroboard 0 15in
matrix, 11 x 13/16 in approx and 31 x 11 in approx.
Wood for cabinet. Knobs
TTOOL OF BUDHICK THISBS

IC1 has three leads, positioned as in the underside view of this component, in Fig. 4. IC2 has four spills, 2 and 3 being longer, as in Fig. 4. If this IC is located as shown, the tags will fit the Veroboard holes correctly and connections being soldered on underneath. Both ICs should be soldered without undue heating. It should only be necessary to keep the soldering iron in contact with the joint for a second or two. Lengthy heating may damage these items

This circuit board should not be tested without VRI and the loudspeaker being connected.

If a signal generator is to be used to adjust the circuits, couple this loosely to the lead running to pin 2 of IFT1. It is only necessary to place the generator lead near this lead with no actual connection. The cores of IFT1 and IFT2 should then be adjusted, with a proper tool, for best output.

When no generator is available, adjustment should prove quite easy as the IFTs are pre-aligned by the maker. It is then only necessary to tune in a stable signal and adjust each core for best volume. The cores should have a sharp resonance peak. Again, it should be stressed that a properly shaped tool must be used, as a wedge-shaped blade may easily break the cores so that they cannot be rotated, while inserting a steel or similar screwdriver will upset correct alignment.

The audio section should be found to provide good amplification and adequate loudspeaker volume. The small internal speaker will give quite reasonable audio quality, for SW listening purposes. A larger, external speaker may be plugged in (as well as phones) and this will naturally give some improvement. It should be of suitable impedance, about 16 to 25Ω . Though a small speaker can give satisfactory results, it cannot be expected to be quite as good as a larger unit operating with its own cabinet or baffle.

CONSTRUCTION

The chassis is a "universal chassis" flanged member 8 x 4in. with a second similar member used for the panel. The front edge of the chassis is set back ${}^{1}_{2}$ in. from the panel, as in Fig. 5, using two ${}^{1}_{2}$ in. spacers and two ${}^{3}_{4}$ in. countersunk 6BA

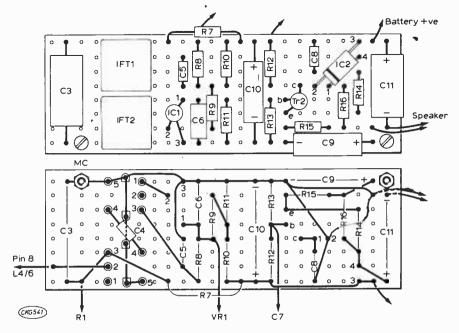


Fig. 4: The two sides of the IF/AF board and connections to the remainder of the circuit.

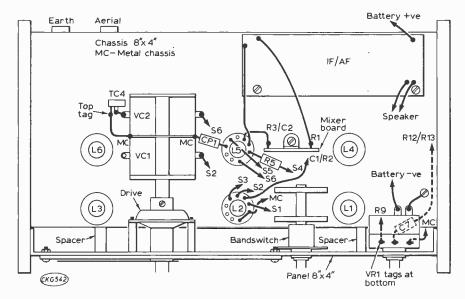


Fig. 5: Layout of major components on top of the chassis and interconnections.

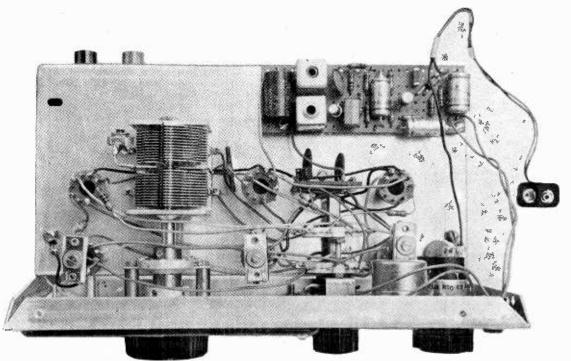
bolts, which run through the panel and the front flange of the chassis. (These two bolts with spacers are not absolutely essential, as chassis and panel are held in position by the case sides. However, with the bolts securing these parts together, assembly and testing can be completed before fitting the sides in position, and wiring is thus more easily reached.)

Locate the drive template on the panel and drill the fixing holes for it and for the dual-speed ball drive. A large hole is also punched for the projecting part of the drive which carries the cursor.

Position the bandswitch and VR1 as in Fig. 5,

keeping these as low as possible to leave room for the speaker. The speaker opening is made with a large chassis punch or adjustable washer or tank cutter, or by drilling a ring of small holes and clearing up the edge with a half-round file.

Check that the panel and chassis are correctly fixed and at right angles, then fit the ganged capacitor into the drive and drill the fixing holes for the capacitor. Washers are placed under the capacitor to bring it level with the drive. The position of the drive and capacitor should be carefully adjusted as necessary so that they are in line and turn smoothly.



General view of receiver from above to assist in locating components shown in Fig. 5.

Holes ${}^{1}_{4}$ in. in diameter are drilled for the six coils, which are located as in Fig. 5. Their fixing nuts should be tightened with the fingers only. Pins are counted in a clockwise direction from the space, from 1 to 9, and wiring is simplified if all the coils are positioned so that their pins are approximately in the same direction.

The IF/AF amplifier board and mixer board are fixed as in Fig. 5, but it is easier to leave these off until most of the wiring has been done to the lower tags of the switch. which are otherwise difficult to reach.

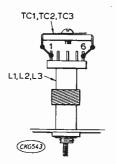


Fig. 6: Method of mounting trimmers on top of the coils.

Trimmers TC1, TC2 and TC3 are mounted directly across the coils L1, L2 and L3 as in Fig. 6. Short, stout wires are soldered to pins 1 and 6 of each coil, for this purpose, when wiring the receiver. It is preferable to take the upper plate tag of the trimmer to the earth side of the circuit (pin 1) in each case.

The single oscillator trimmer, TC4, is soldered to the ganged capacitor as in Fig. 5, the top tag being connected to the capacitor frame by a stout wire. A check should be made that the tuning capacitor fixing bolts are not too long, or they may touch the fixed plates of the capacitor.

A bandswitch with two wafers was used. The front wafer switches the aerial, base and VC1 circuits while the rear wafer is employed for the oscillator coils.

It is not essential to use a two-wafer switch provided the required number of poles are available and the switch is small enough to be accommodated.

Fig. 7 shows connections to the switch. It will be found very helpful to use colour-coded leads here. With the aerial coils, yellow may be used for aerial and S1 circuits, with red for base and S3 circuits, and green for S2, VC1 and associated circuits. For the back wafer, red can be used for S4. yellow for S5, and green for S6. Chassis returns to the coils can be black and the base bias circuit to C1/R2 may be blue. Whatever colours are used. employ them exclusively for one circuit.

It is also helpful to solder on lengths of wire, before mounting the switch, where the tags will be near the chassis, and hard to reach later. These wires can then be cut to length and taken to the various coils.

If the contacts of the switch cannot be seen, and its operation is not wholly clear, test it for continuity with a meter, in each position. Also it is advisable to wire in the coils for one band only, to confirm that no error is being introduced here, before proceeding with the other ranges. Pressure should not be imposed on the coil pins when these are hot, so a little care is required when soldering these to prevent them moving when the insulation softens.

The volume control is mounted as in Fig. 5. Connect the lower tag to S7 and to the metal chassis. Run a lead from the other outer tag, under the chassis and up through a hole near the AF amplifier, where it is soldered to R9, Fig. 4. Solder C7 to VR1 slider and take a further insulated lead under the chassis and up through to the junction of R12 and R13.

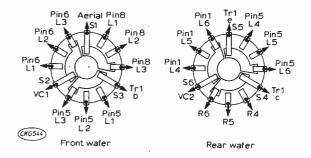


Fig. 7: Details of the wiring on the bandchange switch wafers.

ALIGNMENT

Alignment of the IFTs has been described. To align the aerial and oscillator coils, deal with one band at a time. Adjust the coil cores at a low frequency in the band (VC1/2 nearly closed) and the appropriate trimmer at a high frequency in the band (VC1/2 nearly open).

TC4 is initially set about half closed. If it is subsequently found that TC1, TC2 or TC3 is fully open for best volume, TC4 should be screwed down slightly. Provided TC1, TC2 and TC3 each have a definite peak giving best volume, there is no need for a separate trimmer for each oscillator coil.

Coverage is primarily determined by the settings of the oscillator coils and TC4. If a signal generator is available, set VC1/2 5° from the fully closed position and adjust the core of L4 for reception on 10.5MHz; similarly adjust L5 for reception on 5MHz, and L6 for reception on 1.67MHz.

L1 should then be adjusted at 11 \cdot 5MHz for best volume. L2 is similarly adjusted at 5 \cdot 5MHz, and L3 at 1 \cdot 83MHz. VC1/2 is then opened to tune to 28 \cdot 5MHz, and TC1 is adjusted. TC2 is adjusted at 13 \cdot 5MHz, and TC3 at 4 \cdot 5MHz.

These adjustments are repeated until no further improvement is possible. These frequencies are the most effective tracking points for the low frequency and high frequency end of each band and result in best tracking throughout the whole range.

CALIBRATION

The tuning drive listed has a scale marked $0-100^{\circ}$, in addition to scales for individual calibration. Set the cursor to 100° with the tuning capacitor fully closed. If calibrated as described the following points, read against the 0-100 scale, may be used as a guide to intermediate frequencies: —

733

Range A		Range B		Range C	
30MHz	12°	15MHz	7°	5.0MHz	8
28MHz	15°	14MHz	10°	4.5MHz	12°
26MHz	170	13MHz	13°	4.0MHz	17
24MHz	19	12MHz	16°	3.5MHz	22
20MHz	27°	11MHz	19°	3.0MHz	29
18MHz	32°	10MHz	23°	2.5MHz	410
17MHz	36°	9MHz	28°	2.0MHz	62°
16MHz	40°	8MHz	35°	1.9MHz	70°
15MHz	45°	7MHz	44°	1-8MHz	79
14MHz	52°	6MHz	59°	1·7MHz	89°
13MHz	60°	5.5MHz	71°		
12MHz	70°	5MHz	85°		
11MHz	81°	States and		New York	

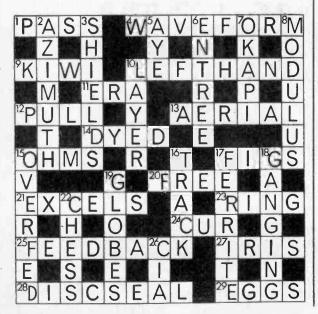
CABINET

Each side of the cabinet is 6mm plywood, approximately 5^{1}_{4} in. deep, to give a front projection. The sides are 4^{1}_{2} in. high at the back, and 5in. high at the front, to tilt the panel backwards slightly. (Note, however, that panel and chassis remain at right angles to each other.)

A strip of wood 8 x 1 x ${}^{1}2$ in. with a rounded front edge is fitted under the panel by means of two self-tapping screws run into the lower flange of the panel.

The cabinet top is $8 \times 5^{1}_{4}$ in. and it is screwed to the back, which is 8×4 in., by means of an inner strip about $8 \times 1 \times {}^{1}_{2}$ in. in size. This completed part (top and back) is secured with two self-tapping screws into the front flange, and two bolts at the back, so that it can be removed to renew the battery. The bottom of the chassis itself may be left open, or closed with a sheet of hardboard.

PW TECHNICROSS PUZZLE Solution to No. 1 presented last month



TELEVISION

IN THE DECEMBER ISSUE

VISION MIXER

This easily built unit enables the outputs from two CCTV cameras—or more if extra channels are added—to be faded, switched or mixed. The unit produces a constant sync signal by taking the pulses from the "camera 1" channel and adding them to whichever video signal is selected.

ADDITIONAL I.F. AMPLIFICATION

There are several situations in which additional i.f. amplification can be useful. Simple transistor stages can also make it economically worth while. This article shows how.

SERVICING TV RECEIVERS

The next chassis to be dealt with is the GEC Series 1 single-standard chassis. We shall also be resuming the Philips G6 colour chassis.

DX RECEIVER SYSTEM

Following the recent article on varicap tuning units last month this article describes some receivers for DX operation.

COLOUR BRILLIANCE CONTROL

With the three c.r.t. drives necessary in a PAL colour receiver the traditional simple brightness control system is no longer suitable. An examination of the technique used instead provides a valuable insight into video circuit arrangements.

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TBA 651	ALL	1uV - 6dB	54p	2-00
TBA 120 A	FM inc.det.	15uV-limiting begins-10·7MHz	23 p	1-07
CA 3088E	AM inc.det.	200uV for 20 dB SN/N	16 p	1-50
CA 3089E	FM inc.det.	12uV for 3dB limiting AFC-SQUELC	H-	2-20
		AGC-TUNING METER DRIVER.	25p	
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токо	BLOC	K FILTER SELE	CTOR	
TYPE	FREQUENCY	BANDWIDTH kHz	USAGE	PRICE
CFT 455 B	455 kHz	8 at -6 dB+±10 at -22dB	nbfm	50p
CFT 455 C		6 27dB	am	50p
CFU 455 C		4-8 28 dB	am	55p
MFH mechanica	l series	4,5 or7 at −6 dB ±5 at −50 dB	ssb am nbfm	1-40
CFS 10·7	10.7 mHz	300 at -3 dB 600 at - 20 dB	wbfm	40p CFS
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HIGH FIDELITY LOUDSPEAKER KIT

Consisting of a Fane Model 803 ultra-low resonance 8" speaker unit with PVC cone surround, and a Fane Model 303 high frequency pressure tweeter together with a printed circuit cross-over assembly with ferrite cored coils.

SPECIFICATION OF UNITS					
	Model 803	Model 303			
Overall Diameter	8″	3″			
Natural resonance	30Hz	_			
Main resonance	*35Hz	1200Hz			
Magnet Pole Diameter	1″	2"			
Magnet Flux Density	13,000 gauss	10,000 gauss			
Frequency response	30Hz-8kHz	2kHz-17kHz			
Impedance	8-15 ohms	8-15 ohms			
Power Handling	*15 watts	*15 watts			

Very easy to assemble, this boxed kit comes with acoustic foam damping material, panels, screws, wire, wiring diagrams and instructions to provide a remarkable loudspeaker assembly-a pair is ideal for stereo.

CABINETS for the 'Mode One' are available in Teak veneer finish. SIZE $15\frac{3}{2}$ x $10\frac{3}{2}$ x 9".

Manufactured by

*When used with above cabinet.

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9

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THERE are a number of integrated circuit audio power amplifiers available at the present time One of these, the LM380N device, has a number of features which make it attractive to the amateur experimenter. In particular, it is very useful in circuits requiring the minimum number of components. The device is manufactured by the National Semiconductor Company, and is available from Ambit International, 37 High Street, Brentwood, Essex, or Athena Ltd., 140 High Street, Egham. Surrey.

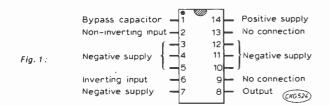
ADVANTAGES

The LM380N automatically 'centres' its output at one half of the power supply voltage. This eliminates the need for additional circuitry (including a pre-set potentiometer) which is required with some other types of amplifier for adjusting the bias so that maximum voltage swing (and hence a maximum power output) can be obtained.

The LM380N device also incorporates internal protective circuits. If the silicon chip becomes too hot (above about 150°C) owing to incorrect operation, the circuit automatically becomes inoperative for a time until the chip has cooled. Protection is also incorporated against excessive current in the output stage; such currents will occur if the output is accidentally short-circuited. The limiting current in the output stages is about 1.3A.

The LM380N can feed up to 2.5W to an 8 Ω loudspeaker when operated from an 18V supply. The absolute maximum permissible supply voltage is 22V, but it is wise to use a somewhat lower value to allow a margin for error. The writer has found that satisfactory loudspeaker volume can be obtained using the minimum recommended supply voltage of 8V. The total harmonic distortion is 0.2% at 2W output using an 18V supply.

It is normally convenient to use the LM380N in a standard 14 pin dual-in-line socket so that it can



be removed easily from the circuit. However, one can solder directly to the terminals of the device.

CONNECTIONS

The connections of the LM380N are shown in Fig. 1. The input signal can be fed either to the non-. inverting input or to the inverting input. Generally it is more convenient to feed the signal to the noninverting input and to leave the inverting input unconnected.

If, however, the signal is fed to the inverting input, the non-inverting input should be returned to earth through a capacitor or a resistor or directly earthed. This will prevent positive feedback from the output to the non-inverting input causing instability. A capacitor is preferable when the signal source has a high impedance, but with a source of moderate impedance a resistor approximately equal in value to this source impedance is preferable to maintain the balance of the differential stage. When the source impedance is low, the non-inverting input may be earthed.

GAIN

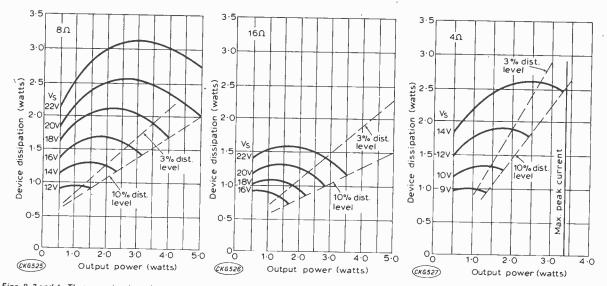
The voltage gain of the LM380N is fixed at 50 (or 34dB) by the internal circuitry of the device. Although this fixed gain limits the versatility of the amplifier, it does result in a minimum number of external components being required for its use.

HEAT SINK

The LM380N device itself can dissipate up to 1.25W when operated without any heat sink at ambient temperatures of up to 25°C; this is adequate for many applications. For example, Fig. 2 shows that the power does not exceed 1.25W at supply voltages up to 14V when an 8 Ω speaker is employed. Even if a higher supply voltage is used, it is not likely that the dissipation will exceed 1.25W for an appreciable time.

Fig. 3 shows that there is still less chance of overheating when a 16 Ω speaker is employed. In this case, the supply voltage would have to exceed 20V for the dissipation to exceed 1.25W.

In the case of a 4 Ω speaker, however, Fig. 4 shows that the dissipation can reach 1.25W when a 10V supply is used. If a much higher supply voltage is employed, the pins 3, 4, 5, 10, 11 and 12 of the device should be soldered to a copper heat sink of



Figs. 2, 3 and 4 : These graphs show dissipation of the LM380N against output power for various values of supply voltage and loudspeaker impedance

area about six square inches.

The three per cent total harmonic distortion line shown in Figs. 2 to 4 is approximately the onset of clipping.

POWER SUPPLY

If there is hum or noise on the power supply line, a hum rejection of about 38dB can be obtained by connecting a 5μ F capacitor from pin 1 to earth. A smaller capacitor will also provide some measure of hum reduction.

If the power supply leads from a battery or filter capacitor are longer than two or three inches, a 0 1μ F capacitor should be connected between pin 8 and earth to prevent oscillation.

In addition, a $2 \cdot 7\Omega$ resistor in series with a $0 \cdot 1\mu F$ capacitor may be connected between pin 8 and earth to suppress any high frequency oscillations.

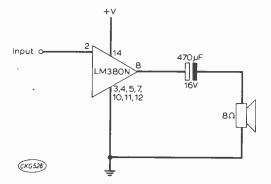
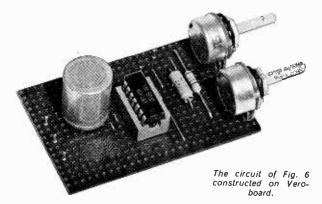


Fig. 5: A simple circuit using the LM380N.

SIMPLE CIRCUIT

The simplest circuit using the LM380N is shown in Fig. 5. The 470μ F capacitor must be placed in series with the loudspeaker to prevent a steady current from flowing through the speaker from pin 8. A smaller capacitor than that shown will result in inferior bass response.



The input pin operates with a mean potential equal to the earth potential. A capacitor in series with the input pin is therefore required only if the

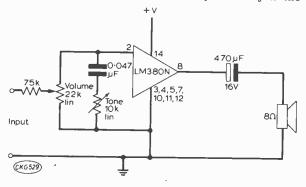
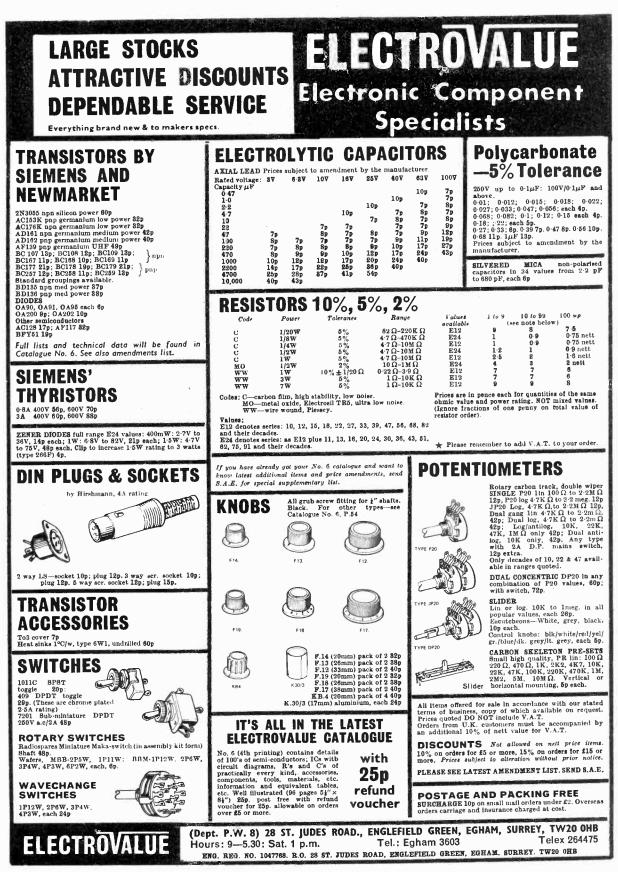


Fig. 6: A record player amplifier suitable for use with a crystal or ceramic pick-up cartridge.

mean potential of the signal source is not also at earth potential.

The writer has used the circuit of Fig. 5 in a radio receiver. Fig. 6 shows how a similar circuit may be used as a record player amplifier with volume and tone controls. The input impedance of the LM380N is about $150 k\Omega$.





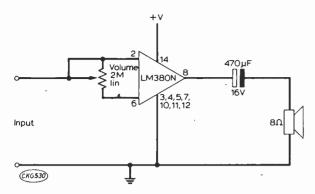


Fig. 7: A high input impedance achieved by use of a common-mode volume control.

HIGH IMPEDANCE INPUT CIRCUIT

An amplifier with a high impedance input is shown in Fig. 7; it is suitable for use with high impedance signal sources such as a crystal microphone. This circuit employs a 'common mode' volume control. When the potentiometer slider is at the bottom of its travel in Fig. 7, the input signal is fed to both the inverting and the non-inverting inputs. In this case the signals will almost cancel in the device and the output will be small. When the potentiometer is at the top of its travel, however, only pin 2 will receive an appreciable input voltage and maximum volume will be obtained.

The circuit of Fig. 8 shows how a common mode volume control circuit may be used with a common mode tone control to maintain the high input impedance.

A very high input impedance amplifier can be made using the field-effect transistor input circuit shown in Fig. 9. At low frequencies the input impedance is 22 megohms, but at high frequencies the input impedance is reduced by the gate to drain capacitance of the field effect transistor

INTERCOM SYSTEM

Listen

S1a

Talk

8Ω

(CKG533)

A simple circuit for an intercom system is shown in Fig. 10. The transformer ratio of 25:1 multiplied by the gain of the LM380N produces a loop gain of 1250. The roles of the input and output speech transducers are reversed when the switch is operated.

Volume

- Master unit

2M lin.

25:1

Repanco

T53

_M380N

3,4,5,7,

16

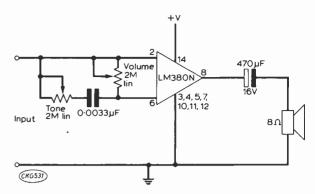


Fig. 8: This circuit features common-mode controls for both volume and tone.

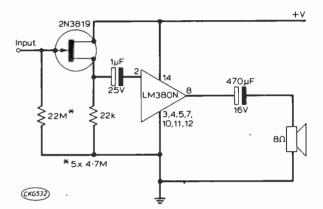
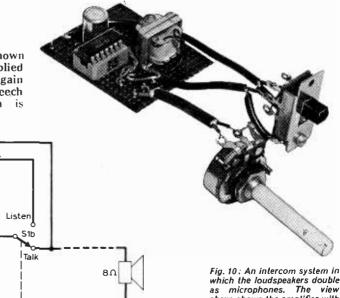


Fig. 9: The addition of a FET input stage gives a very high input impedance.



above shows the amplifier with controls attached.

Remote unit

DUAL POWER SUPPLY

Another simple circuit using the LM380N is shown in Fig. 11; it provides a dual voltage supply balanced with respect to ground from a single supply. If the input is 20V, outputs of +10V and -10V can be obtained. The potentiometer can be used to balance the outputs relative to ground, but may be omitted if exact balance is not required.

An advantage of this circuit is that a high quiescent current is not taken when little current flows in the outputs.

EXTRA GAIN

Although the gain of the LM380N is fixed at 50 by the internal components, higher gain can be obtained by using additional positive feedback. For example, Fig. 12 shows how a gain of 200 can be obtained.

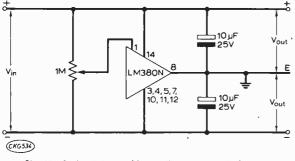


Fig. 11 : A circuit to provide a split power supply from a single source.



Microwave distance Record

On Thursday, 13th September a 3cm (10GHz) contact was made between GW8CKT/P on Snowdon and GM8AZU/P on the Cairnsmore of Fleet. We believe that, at 212.5km, this is a new British distance record.

Weather conditions were far from ideal, with gale force winds and both ends of the link well above the cloud base. Visibility

on Snowdon at 3560 feet was only 15 yards, and on the Cairnsmore of Fleet at 2300 feet was only 20 yards. The high wind on Snowdon made it impossible to use a dish aerial and so a 10dB horn was used. At the Scottish end a 32in. dish was used, and a considerable amount of luck was in evidence when the beam heading, estimated using a cheap plastic compass, turned out to be correct to better than 0.5° . Earlier attempts to find a signal using a 10in. dish at the Scottish end had failed. Signal reports exchanged were readability 5 and strength 6/7.

Equipment used at GM8AZU/P: Tx, Mullard CXY19 Gunn device, output approximately 100mW; Rx, Mixer CS10B, Local Oscillator, Mullard CL8370; i.f., 70MHz; ANT, 32 inch dish with horn feed.

Equipment used at GW8CKT/P: TX, Mullard CXY19 Gunn device, output approximately 120mW; RX, Mixer, balanced pair of Mullard BAW95, Local Oscillator,

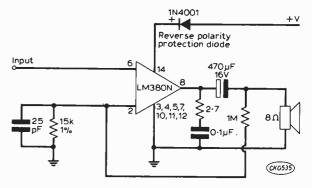


Fig. 12 : Increased gain may be obtained by the use of positive feedback.

The maximum gain is around 300, since attempts to obtain still higher gain may merely result in oscillation.

SUPPLY POLARITY

As in the case of most integrated circuit audio amplifiers, if the power supply to the LM380N is applied with the polarity reversed, a large current will flow and the device will almost certainly be destroyed within a few milliseconds.

Readers may therefore wish to incorporate a diode in one of the power supply lines (normally the positive line). If a supply of reverse polarity is accidentally applied to the circuit at any time, the diode will prevent any appreciable current from flowing and will thus protect the LM380N. It is, of course, essential that the diode is connected with the correct polarity, see Fig. 12.

> Mullard CL8380; i.f., 70MHz; ANT, Small horn.

The equipment, which was all solid state, was carried to the summits of the two mountains concerned. Pundits who ask why the GW team did not use the train, may be interested to know that the train was not running due to the bad weather so it's just as well that they bargained on climbing!

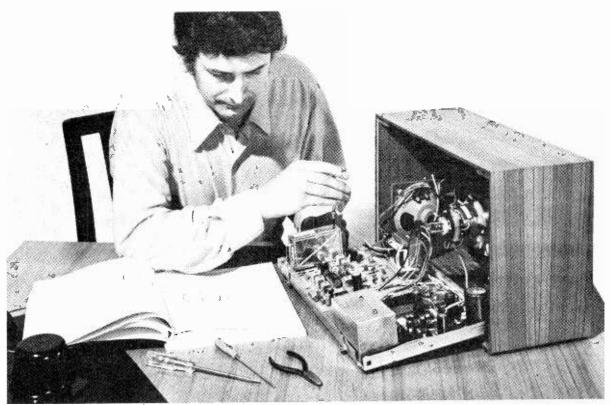
80m talkback was used between the two base camps in order to co-ordinate the departure for the climb to the summit.

2m talkback was used from summit to summit.

Those involved were:—

At the GM end: G3VUQ, G3YCQ, G8AMG, G8APZ, G8AZU, G8DKK. At the GW end: G3XSO, G3YMV, G8BPN, G8CKT, G8ENX, G8FTB, G8HCO.—Michael H. Tooley, G8CKT, (Weybridge, Surrey).

---continued on page 762



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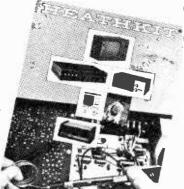
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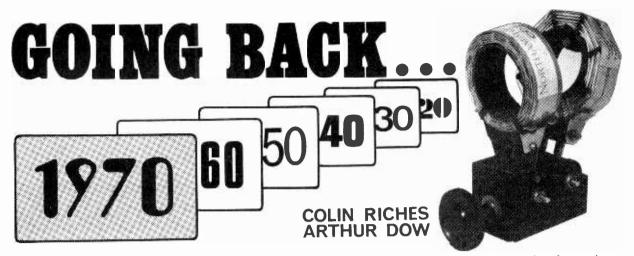
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Letter from America

F OR several years I have read your column religiously and at long last decided to write to you. Needless to say I have an avid interest in Vintage Radio. However, I have had to content myself with vintage parts, valves, radio books and magazines. Additionally I construct simple vintage radios out of antique parts using my own circuits or those from Hugo Gernsback publications from the early '30's. My valve collection fortunately contains many good useable valves. At present I am constructing a short wave receiver (semi-antique) using types '35 and '27 (U.S. tubes) and meant for mains operation.

I started my radio hobby in 1928 with a commercial crystal set (Vario Couple Type). I made crystal sets until 1932 when I started on valve short wave and medium wave receivers. My hobby continued through 1935 and 1936. It was interrupted in 1937 by my joining the U.S. Army. I did only occasional short wave listening thereafter until 1946 when I went back to radio construction.

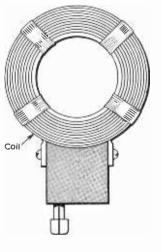
My recent vintage radio construction includes a one tube SW receiver (using a transmitting type '30). The coils (plug-in) are my originals from 1932. These are about the only parts surviving from that era. While I was in the army in pre-World War 2 days, a relative threw the rest away! I also have two surviving books.

The other receivers are a Short Wave Portable which is a good copy (including original vernier dial) from an article in a 1933 Short Wave Craft Magazine. I had been planning to build it for decades and only made it last year. Also I have a breadboard type Medium Wave receiver using a type '99. (A very good performer with one modern part—a ferrite rod aerial in it). I use it mostly for a quick test of old tubes. Much better than the tube tester!

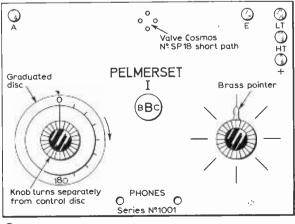
I possessed one vintage radio in recent years (an RCA Radiola) but an avid collector got it away from me. All I have at the moment is a vintage tube tester, Signal Generator and Output meter (Weston, circa 1929). The trouble is that some collectors in this country possess 100 to 300 radios leaving none for us pickers.—Chester A. Beck, K6DFP, (9045 Margaret Street, Downey, California, 90241, U.S.A.)

Mr. W. H. Quick tells us that he has been given an old one-valve radio which he would like to get going. He would like to know what the L.T. and H.T. voltages are. There is a 1.5A fuse fitted and we show in the diagram the front panel and a plug-in coil which fixes to the side of the set.

If anyone can help Mr. Quick, they can contact him at 15 Beechwood Grove, Horbury, Wakefield, Yorkshire.



Mr. Quick's plug-in coil and the front panel of his vintage receiver.



🕘 = Brass terminals



AST month we saw that there is, at least, one circuit which is sensitive to the rate of voltage change, i.e. the divider circuit would only respond correctly if we caused rapid changes in lighting level at the photo cell; slow changes would not make the divider work. There are other circuits

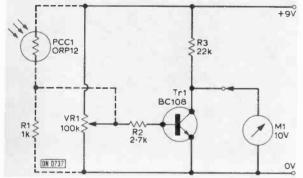


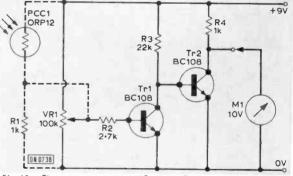
Fig. 14a If PCC1 and R1 are used as alternatives, omit VR1 and link in PCC1 on the "left-hand" end of R2.

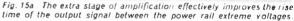
out for Fig. 14a.

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which like to see what are known as "fast going edges" to signals; as a result, a range of circuits has been developed which will accept slow changing inputs and convert these into signals having fast rise and fall times.

These circuits are called triggers because their





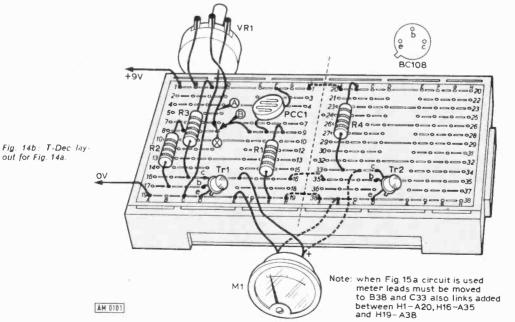


Fig. 15b: T-Dec layout for Fig. 15a.

output will always be in a certain state (say zero volts) until the input signal rises to a certain level and, irrespective of the time it takes the input to get to this level, when the critical voltage has been reached the output changes to a higher level (say +9V) instantaneously.

In practice everything takes a certain amount of time to happen, so "instantaneously" is, perhaps, too strong a term to use. Nevertheless, as you will see if you do some of the following experiments, we can make extremely slow voltage changes trigger a circuit to give edges to waveforms that change from one level to another in a few millionths of a second.

Fast and slow "edges"

First of all we had better look at what we are calling an "edge" so that we can compare the difference between fast and slow edges. Fig. 14a is a very simple transistor amplifier stage which gives an output inversely proportional to the voltage at the wiper of VR1 (or, if you are using the photocell alternative, the junction of PCC1 and R1).

Measure the voltage at the collector of Tr1 with VR1 set to the bottom of the track (Alternatively completely shade PCC1). You should read about +9V because the transistor, in the absence of base current, is not conducting. Slowly increase the voltage at the wiper of the potentiometer by rotating it (or slowly increase the amount of light falling on PCC1); base current will start to flow and the voltage at the collector will start to fall.

The thing to notice is that you can control the level of the measured voltage quite easily and get any value you like by careful adjustment of VR1 or the amount of light falling on PCC1. Try and get a "feel" for the rate at which the measured voltage changes for given rates of moving the potentiometer or illuminating the cell.

You can use the wires A or B in the layout and transfer one, or other, of them to point X—depending on whether you were using the cell or the potentiometer. Fig. 15a shows an extra stage of amplification. Carry out the same experiment but now measure the voltage at the collector of Tr2. Obviously the extra stage gives us inversion so when the potentiometer is down the measured voltage is low.

Now slowly increase VR1 until the voltage starts to rise and then try and control it in the same way as before. It should be very apparent that, for the same rate of change in position of the wiper of

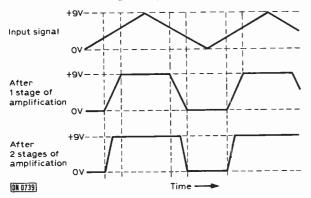


Fig. 16: Note the increased amplification appears to enhance the signal's rise time between the supply voltage limits.

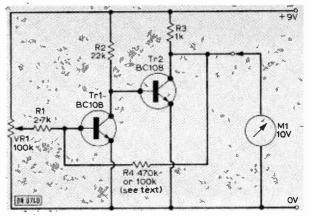


Fig. 17a. True trigger action is obtained by using positive feedback via R4.

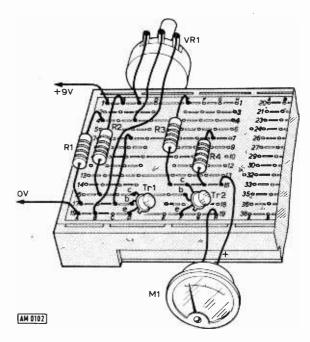


Fig. 17b : T-Dec layout for Fig. 17a.

the potentiometer, the voltage at Tr2 goes from zero to +9V very much quicker than it did before.

It is, however, still possible to set it mid-way between the two extremes by careful adjustment. The effect is even more pronounced using the photocell and you should start to appreciate the increase in the rate of change of the signal at the output.

Amplification

The signals we have been talking about can be described as waveforms as shown in Fig. 16. The portion of the signal between the low and high voltages of the output is called an edge and you can see that it has become much steeper with the extra amplification.

Simple amplification thus increases a signal's rise time but there is still the possibility of getting a mid-rail voltage during the transition—especially if the input signal was unusually slow. Ideally we



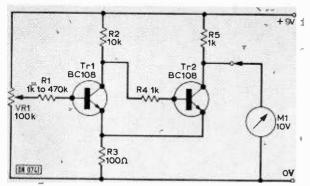


Fig. 18a: Schmitt trigger circuit. The trigger level can be controlled over small limits by changing R1 in the range 1kΩ to 470kΩ.

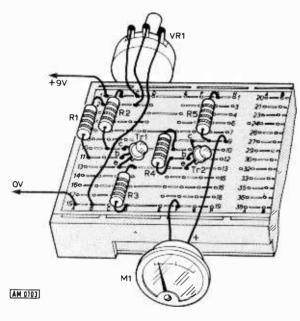


Fig. 18b: T-Dec layout for Fig. 18a.

would like to have a circuit that gives a fast change irrespective of the rate of change of input. The circuit in Fig. 15a has been modified in Fig. 17a with a resistor coupling the output back to the input. We have introduced a positive feedback loop.

If VR1 is slowly increased the voltage at Tr2 collector will, at some time start to rise; when this happens current starts to flow through R4 back into the base of Tr1 and effectively increases the base current we are already applying from the potentiometer. The effect is to make the voltage at Tr2 rise even more enhancing the effect until eventually Tr2 is totally non-conducting. All we needed to do was set the operation in motion by initiating base current into Tr1; once that was started the voltage at Tr2 collector would move from zero to +9V without any further movement of the potentiometer—the feedback loop did the rest.

The feedback cycle occurs extremely rapidly (the speed is limited only by certain internal parameters of the transistors) so the output changes level at a speed set by the circuit and no longer by the rate at which we turn the knob on VR1. Try it for yourself and you will find it impossible to set a mid rail voltage at the output.

When VR1 is at the limit of its travel, try turning it down; the same thing happens on the downward going edge of our input signal. Notice that there is a sort of "no-mans-land" between the positioning of the wiper for upward going triggering and downward triggering. This is known as "hysteresis" and is very useful in differentiating between the two levels we are considering.

Hysteresis

In this circuit, you can control the amount of hysteresis by means of the value for R4. A 470k Ω resistor will give the smallest differential between upward and downward triggering levels but by reducing it to 100k Ω you can widen the gap between the levels. This circuit is operating as a true trigger and the feature to take note of is the use of positive feedback to speed up the edge. If you think about the circuit a bit you will find it is not very different from the bistable described last month.

Schmitt trigger

Probably the best known trigger circuit is the Schmitt trigger shown in Fig. 18a. When the voltage

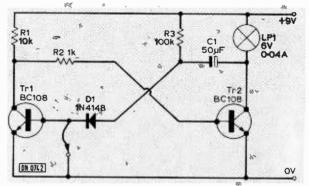


Fig. 19a : Basic monostable multivibrator. Capacitor C1 can be increased to $3,000\,\mu\text{F}$ to extend the dwell time.

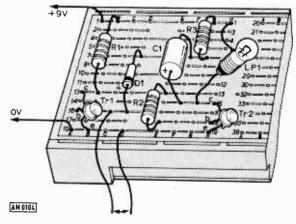


Fig. 19b: T-Dec layout for Fig. 19a.

at the wiper of VR1 has reached a certain level base current will start to flow in Tr1 and the voltage at its collector falls slightly; this reduces the base current into Tr2. The two emitters are, however, connected together and as Tr1 starts to conduct the voltage at the "top" end of R3 starts to rise.

Because this is connected to the emitter of Tr2 we reduce—even more—the potential difference between Tr1 collector and Tr2 emitter thus the base current into Tr2 becomes less. Here again we have a positive feedback loop caused by emitter coupling and the effect of this is to accelerate Tr2 going out of conduction and the output voltage drops very rapidly.

Again this occurs independently of the rate we are applying signal at the input and the speed is limited only by the transistors' parameters. Reduce the input voltage slowly and the opposite happens.

Monostable multivibrator

Another circuit which often comes into the category of trigger circuits is the "monostable multivibrator" shown in Fig. 19a. Unlike the Schmitt trigger it is a little bit more complicated to initiate triggering but it offers a useful bonus. It has a "short term memory". We can design it so that it will trigger rapidly on the receipt of a suitable signal but the output from it stays at the new level for a fixed period of time before rapidly returning to its original state.

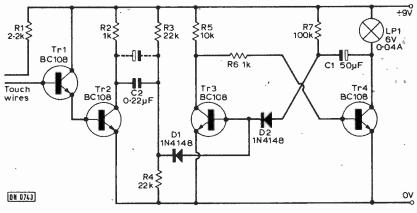


Fig. 20a: Touch-sensitive child's room-light. Supply current is approximately 1mA rising to about 80mA when the lamp is on. Duration of 3½ minutes can be obtained by making C1 3,000μF and C2 50μF. The capacitor shown dotted, across C2, indicates how it is connected—plus to R2.

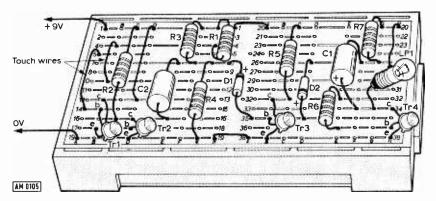


Fig. 20b : T-Dec layout for Fig. 20a.

Make up Fig. 19a on T-Dec and follow this brief description of how it works. Initially let us state that D1 serves no purpose in the circuit except to protect the emitter base junction of Tr1 from a high reverse voltage that is generated during the switching operation.

When the circuit is switched on the lamp may go on for a few moments until things have settled down. When the lamp has gone off we should arrive at a stable state of affairs in that base current is provided for Trl through R3—hence its collector is at near zero volts; because of this Tr2 will be cut off and the potential at its collector will be high (about $\pm 9V$); consequently the lamp will be off.

If we deliberately knock Trl out of conduction, by rapidly short-circuiting its base to ground with the flying leads, we can momentarily establish base current in Tr2 and it conducts. The light goes on and the voltage at its collector drops to about zero. However the capacitor transmits this negative-going voltage excursion to the base of Trl and the potential at the junction of R3 and Cl falls to about -8V(it was previously $\pm 1.2V$ caused by the forward voltage drops of D1 and the base emitter junction of Trl).

Assuming we have immediately removed our short-circuit link Tr1 will stay out of conduction because no base current can flow until the potential at the anode end of D1 has regained its level of $\pm 1.2V$ and this will take time because the negative end of C1 has to charge back to this value through R3. This takes quite a few seconds and during this

period the lamp stays alight.

When this has been reached. Trl starts to go back into conduction and the potential at its collector falls giving rise to an increase in voltage at Tr2 collector; this is fed back momentarily through C1 and enhances the base current into Tr1 (positive feedback again). As a result of all this the lamp switches off very rapidly. If you have a $3,000\mu$ F capacitor you can substitute it for Cl and get a "dwell" time of about 312 minutes. The dwell time can be calculated as $0.7 \times C1 \times R3$ (C in Farads R in ohms and the time will be in seconds).

Touch switch

The monostable thus gives us trigger action and a timing function which can be put to many uses. A novel circuit for a safe child's bedside light is shown in Fig. 20a. It is a touch sensitive switch coupled to a monostable that switches on a lamp for a pre-determined period of time (Warning: the novelty is more likely to keep a child awake than get him off to sleep!).

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THE YEN

AVE you ever had a yen to do something?-the Japanese have. My ageing eyeballs have recently scanned a report which comes from the Orient from an "impeccable source". In February of this year, the Electronic Industries Association of Japan found that the total sales of electronic parts and components from Japan amounted to 101,079 million yen-which is a lot of yen for just one month's effort. It is interesting to see how this figure breaks down. For example, electron tubes (that's valves in English or Toobs in American) in February amounted to 17,841 million ven and showed an increase in February 1972 of over 10%. Integrated circuits accounted for 8,483 yen and showed an increase over the same month last year of a staggering 92%. On these figures, the Western comics who chant "Ha so?" might easily find the answer to be "Velly well thank you".

Other news from Japan is equally interesting. One snippit from spies is that Sony are to withdraw from the electronic calculator market altogether. Another is that Government approval (Japanese) has been given for the joint enterprise between Alps Electric and Motorola for the manufacture and sale of ICs. This American / Japanese Company is aiming to sell 3,000 million yen's worth of ICs in 1974.

KEEPING A WATCH!

Still in yen land, the Japanese watch industry is claiming that some 200,000 watches using piezo-electric crystals, will be produced there this year. Production lines are eagerly being set up to manufacture C-MOS ICs and there is a hive of activity in the liquid crystal readout sector. If all this activity goes through, then clearly now is the time to watch Japan.

MINI FREQ. COUNTER

What other interesting things are happening in Japan? Well, quite apart from the considerable amount of electronics business that's taking place (would you believe that this country sold 83,349 million yen's

worth of communications equipment in 1972?) there is always the neatness, the preciseness of some of the products. Perhaps an excellent example is in the field of frequency counters-feed a signal in and the frequency is flashed up on a digital readout. Well, one Company (and I'm talking about a production item. not a prototype laboratory wonder) is marketing a miniature but professional standard frequency counter. It gives a digital readout of frequency from 15Hz to 50MHz although there is an optional pre-scaler which extends this to 220MHz at the upper limit. It's completely portable and uses internal rechargeable cells. The internal oscillator is accurate for the majority of applications having a stability of + 0 0005 at 25 C. The size is particularly impressive-120 x 175 x 25 millimetres. Just grab yourself a ruler or do a quick mental conversion and you'll see that this slips into your pocket (there's 25.4 millimetres to the inch!).

LASER TELEVISION

One could hardly look at the Japanese electronics scene without taking in the television industry. Latest thing in this sector to catch my eye is a large screen laser colour television projector. This beasty is a considerable improvement over its younger sister which made a debut at the World Exposition in Osaka in 1970. The earlier model had a resolution of 525 lines. The latest version has a resolution of 1,125 scanning lines. A krypton ion laser is used to generate the red, while an argon ion laser emits the green and blue spectrums. Perhaps we're not at the home use stage yet, but maybe the time will come when an entire wall will light up with a full colour, 3D life-size TV screen-so real you'll be able to step through your kitchen wall and join in a quick romp with Noddy or a punch-up with Ena Sharples: the mind boggles.

In serious terms, the new laser colour television projector has some very real advantages. The image is very clear and sharp. It is also very bright and there is very little divergence, too. One feature which my Japanese contact did not highlight but which is of interest is that the

ON RECENT DEVELOPMENTS

polygonal mirror used for horizontal scanning rotates in magnetic bearings. These have certain advantages over conventional bearings, notably reductions in noise and vibration.

CHINESE PUZZLE?

How many characters or words do you think there are on this page? How about a page in a Chinese newspaper then? No, I haven't nipped across on the Kowloon ferry, I'm still in Japan where a leading electronics manufacturer has just launched a very high-speed printer which prints out the Chinese language. It will produce some 600 lines of Chinese in 60 seconds which, as I'm sure you know, works out at 12,000 Chinese characters every minute. A computer is used to hold information prior to printout but manual over-ride can be used. The printout can be in either lateral or vertical rows so it doesn't matter which way you want to read it-the machine can oblige. Damn clever, those Chinese, or should that be Japanese? I'll have to get myself properly orientated.

EARTH STATIONS

In the early days, the Japanese electronics industry suffered (rightly or wrongly) from a "cheap goods" brand. It is now no longer possible to regard all its products as in this category. An earth terminal is no small thing, neither is there any room for sub-standard effort. In this field, one Japanese Company alone has built, supplied and/or installed very nearly 50 (fifty) earth stations.

GET ORGANISED!

A little gem from England to finish with. In a church at the Royal Naval Air Station Yeovilton, Somerset, an electronic organ began to play itself—a radar beam was being picked up by some of the internal components. About time the Navy got itself organised!



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AF/HF/VHF TROUBLE-TRACER

Our Trouble-Tracer will provide you with a test signal ranging from audio to VHF. Test probes pick up signals from the equipment under test and feed them into an amplifier and speaker. All in the one cabinet—What else could you want?



Curing Radio Interference in Audio Equipment

EXT MONTH'S

1.1.1.1

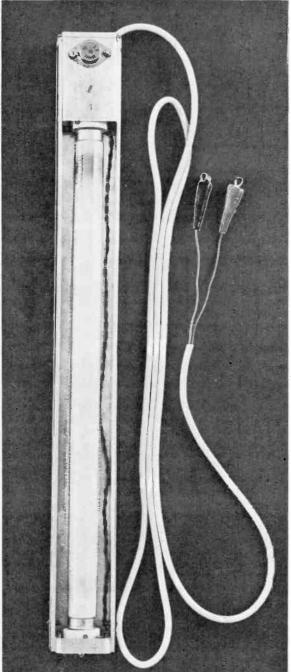
Interes

Do you suffer interference on your tape recorder or HI-FI from nearby radio transmitters? This feature tells you how to cope with this ever-increasing problem.

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JANUARY ISSUE ON SALE 7th DECEMBER

PORTABLE FUORESCENT LAMPU FROM YOUR 12V BATT



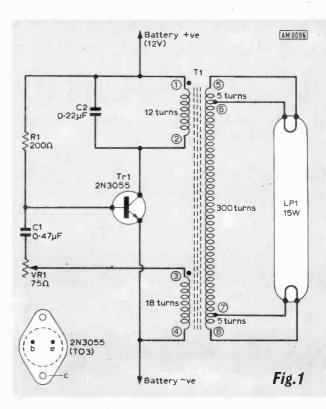
FOR: EMERGENCY LIGHTING, CARA

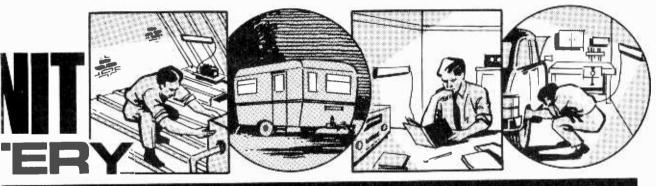
THE battery operated 15W fluorescent lamp unit described here is of simple construction, being designed around readily available components. The whole assembly is made up in aluminium, consisting of a framework which supports the tube and houses the oscillator module. A cover plate acts as reflector and dust cover.

CIRCUIT DESIGN

Fig. 1 shows the circuit. A 2N3055 silicon power transistor operates as a transformer coupled class 'C' oscillator. The fluorescent tube is supplied from a third winding on the transformer. Satisfactory operation is obtained from 10 to 15V.

A variable resistor provided in the base circuit of the transistor ensures correct operation with devices having any gain within normal spreads. The





VANS & CARS, LOFTS, SHEDS, GARAGES, MOBILE RALLIES, ETC...

transformer is designed around Mullard FX2242 pot cores. The collector winding is tuned by a 0.22 F capacitor. Bias for the transistor is provided by a 200 Ω resistor from the positive supply rail.

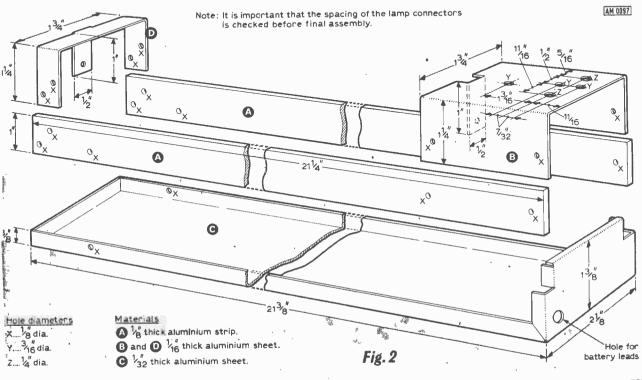
The operating frequency is determined by the 0.47μ F base timing capacitor C1, the variable resistor, the tuning capacitor and the load conditions. Since the load (the fluorescent tube) is a high resistance until alight, the circuit has a "soft" start, the oscillations starting at low frequency and amplitude and building rapidly 'over a few seconds until settling down at steady amplitude and high frequency once the tube 'strikes'.

construction method allows assembly with the tools normally available in a small workshop. The cover plate is the most complicated piece, but being fabricated from ${}_{32}$ in, sheet this makes the work quite easy. Cutting is accomplished with a Stanley knife using a laminate cutting blade (Stanley No. 5194). The cut edges should be filed smooth. The original cover plate made by the author was bent up in a normal small metalwork vice, extra long 'jaws' being made up from 2 x lin, hardwood.

The oscillator housing is bent up from "hein. sheet as is the tube mounting bracket. The power transistor is mounted on the oscillator housing so that the base and emitter pins are inside the casing, directly above the circuit board. One bi-pin tube connector is also firmly mounted to a bracket bent up from this housing. Two side struts are bolted on to this oscillator housing. The smaller 'U' bracket supports them at the far end and also holds the

CONSTRUCTION

The tube and oscillator housing is made up from aluminium strip and sheet as shown in Fig. 2. This



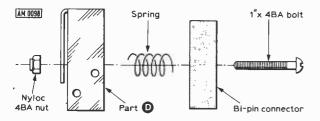


Fig. 3: Details of the spring-loaded tube connector.

other bi-pin tube connector. This connector is mounted on a lin. 4BA bolt and spring, Fig. 3, to facilitate easy fitting of the fluorescent tube by pulling back the connector and then pushing it over the tube pins.

OSCILLATOR PCB

Fig. 4 shows full size layouts for both the component and the copper side of the circuit board. The board can be made by laying the drawing over a piece of copper clad board ready cut to size, and drilling through all the holes. It is essential that the drawing does not move during this operation. The layout can then be copied on to the board using a fine brush or mapping pen and cellulose paint. The board can then be etched off in ferric chloride (strong) solution. (A 500ml bottle is adequate and may be obtained from most chemists to order.) After etching the board should be washed thoroughly in warm water. The paint can be removed with thinners or rubbed off with scouring powder. The components can them be mounted in place and soldered. Flying leads are required for the three transistor connections. Veroboard terminal pins are used for the four connections to the fluorescent tube.

VARIABLE RESISTOR

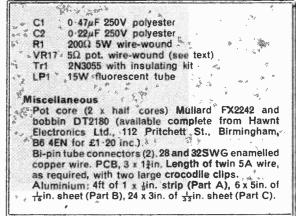
The variable resistor VR1 used here is primarily intended for use as a convergence control in Colour TV receivers. If difficulty is experienced in obtaining this control, it should be ordered from a TV dealer as a spare part (e.g. Decca CTV25 Part No. 535167). This control is mounted near the edge of the board so that adjustment may be made by turning the knob edge with a forefinger from the end of the lamp unit.

THE TRANSFORMER

The transformer is wound on a Mullard DT2180 bobbin. Enamelled copper wire is used throughout and all windings are wound in the same direction.

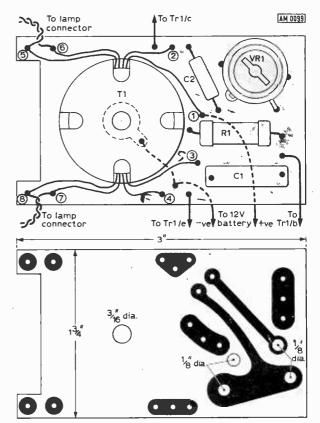
The collector winding is put on first and consists of 12 turns of 28SWG wire, the start labelled (1) and the finish (2). The turns should be wound close together. The base winding is wound directly on top of the collector winding and consists of 18 turns of 28SWG wire, also closely wound. Label the start (3) and the finish (4). Next a single turn of insulating tape is put round the bobbin to isolate the low voltage windings from the tube supply winding.

Finally the high voltage winding is put on consisting of 310 turns of 32SWG wire with taps brought out after 5 and 305 turns. This winding is layer \star components list



wound, with a turn of insulation put right round the finished bobbin. The start, tap 1, tap 2 and finish should be labelled (5) (6) (7) and (8) respectively. The two ferrite cores can then be placed around the bobbin and the transformer loosely bolted on to the circuit board.

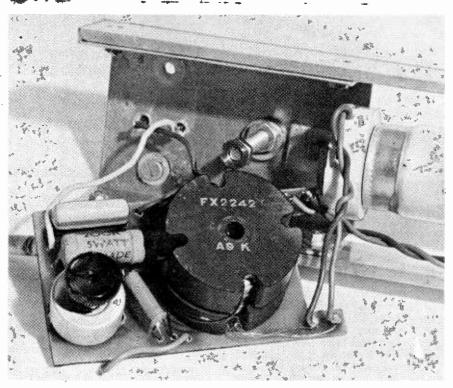
The leadouts can now be cut to length, scraped clean at the ends and soldered to their respective points on the circuit board. Once this has been



All holes drill No.55 unless otherwise stated.

Fig. 4: Full size layout of printed circuit board and component location





A view of the oscillator assembly at one end of the lamp unit.

americanradiohistory com

done, the fixing bolt may be removed and the top ferrite core taken off. A small piece of Sellotape should be stuck on to the centre pole-piece of the core. This provides a small gap which ensures that the core cannot be saturated by the primary magnetic flux. The upper core is then replaced and held into place with a further piece of Sellotape around the join (the cores are finally held together by the module mounting bolt).

An 'exploded' view of the transformer is shown in Fig. 5 which also shows the method of mounting the module.

TESTING

The power transistor should be mounted on the module housing with a mica washer and two nylon bushes, usually supplied with the transistor. A smear of silicone grease should be applied to each side of the mica washer to ensure good thermal contact. The flying leads should be connected to the transistor, ensuring that the base and emitter leads are not reversed. The supply lead should also be connected to the copper side of the circuit board. Do not fit the tube or module into the framework yet.

Connect the power leads to a 12V supply, ensuring correct polarity. The oscillator should 'whistle' loudly, since without a load the operating frequency is, lower. If the circuit does not oscillate it is probable that the phasing between the collector and base windings is incorrect. Reversing either winding should ensure correct operation.

ASSEMBLY

Once it is established that the oscillator is functioning correctly, the fluorescent tube connectors

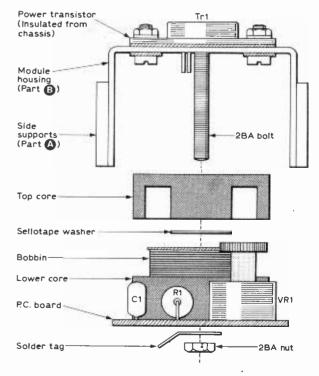


Fig. 5: An exploded diagram of the oscillator transformer and mounting.

may be wired up and the module bolted into the framework. Care must be taken not to overtighten the mounting bolt as the ferrite cores are very brittle and easily fractured. The nut can be sealed with a drop of paint or varnish. The tube can now be fitted into place and final adjustments made. Reconnect the 12V supply, ensuring correct polarity. The oscillator should start up at a medium frequency, increasing rapidly in pitch until the tube strikes and lights. The oscillator should then be inaudible. Adjust VR1 for maximum brightness. At one end of its travel the light will be dim and at the other extreme excessive base drive will cause squegging with consequent flickering of the lamp. Once the oscillator is correctly set operation should be satisfactory over the range 10 to 15V. The current consumption should be between 1.3 and 1.5A at 12V input.

The cover plate should now be clipped on at the oscillator end and pressed home. Two self tapping screws hold the cover in place.

- NOTE 1 Connecting the lamp to the battery with reverse polarity will not cause any damage since the transistor is reverse biased and cut-off, resulting in practically zero current flow.
- NOTE 2 The metal framework has been left completely isolated. Slight radio interference may be caused in the immediate vicinity of the lamp unit. To reduce this interference to a negligible level (field localised to within 4ft.) the frame should be • connected to either the positive or the negative supply line. Connect a short lead from either to the soldering tag on the module mounting bolt.

EXPERIMENTAL WORKSHOP—Part 3— Trigger Circuits—continued from page 749

If the gap between the touch wires is bridged with the fingers a minute current flows into the base of emitter follower Tr1. This produces a considerably larger current into Tr2 and its collector falls to zero. The junction of R3 and R4 is momentarily pulled down by C2 from about +4.5V to -4.5V. This negative going signal is coupled to the base of Tr3 of the monostable through D1 and this switches off Tr3 starting the monostable cycle.

The lamp goes on for the period set by C1 and R7. Capacitively coupling the touch-sensitive switch with C2 allows the user to keep his finger on the touch wires without interfering with the monostable action.

The values shown in the circuit only give a dwell time of a few seconds—for experimental purposes—but a reasonable period of time of 3^{1}_{2} minutes can be arrived at by increasing C1 to $3,000\mu$ F, and C2 must be increased to about 50μ F.

Next month we shall look at a development of the monostable; the astable multivibrator.



Multimeter Competition

In our June "Multimeter" Competition readers were invited to place eight features of the new Sinclair Radionics multimeter DM1 in order of appeal to the average P.W. reader.

Having considered all entries, the judges decided that the best received were a large number of identical attempts which had placed features in the following order:

1st-E; 2nd-D; 3rd-L; 4th-J; 5th-K; 6th-B; 7th-A; 8th-C.

In accordance with the rules, these tying competitors then participated in a postal eliminating contest from which the eventual winners were judged to be Mr. J. Bertram, of Fenham, Newcastle-upon-Tyne; Mr. R. Harris, Knowle, Bristol; Mr. J. R. Mann, Knaresborough, and Mr. G. Rider, Hythe, Southampton.

These four readers each win a Sinclair digital multimeter and 12 months' free copies of Practical Wireless.

The tying competitors who entered the final postal eliminating contest, and were subsequently unsuccessful, each receive a consolation prize and 12 months' free copies of Practical Wireless.



The next series of special issues of P.W. will be in the Spring 1974.

In the coming months we shall be giving advance information on our new

EXCLUSIVE P.W. PROJECTS

COMING IN THE SPRING ISSUES. ORDER YOUR COPIES NOW W ITHOUT a doubt one of the most important tools for either professional engineer or amateur hobbyist is the soldering iron. Nearly every component has to be soldered, so whether constructional work or repairs are being carried out, the iron has to be called into use. There are a considerable number of soldering instruments of all sorts and sizes available, so in this article we will take a look at some of them to see which are most suitable for particular applications, and their respective advantages and disadvantages.

ccess

BASIC REQUIREMENTS

We will start off with what could be called the basic workshop instrument. This is an iron with the element operating at mains voltage and a wattage of between 25 and 40 watts. The size allows for most printed-circuit and general component soldering, but the bit may be rather large for some of the finer printed boards. For this reason, most irons have a variety of interchangeable bits so that a thinner one can be fitted for fine work.

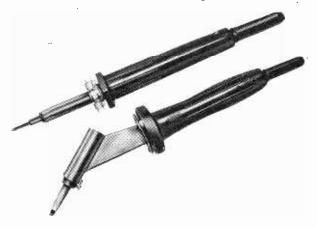
In practice though, bits are not often changed according to the requirements of the job. For one thing they have a habit of getting seized-up and difficult to remove. They should really be loosened from time to time to facilitate changing, but in practice this precaution is usually neglected. Also, most workshop irons are kept on continually in order to be instantly available, so to change the bit for a particular job would mean allowing the iron to cool down and waiting for it to warm up again after the change, plus of course a repeat performance for the re-fitting of the normal bit. Going to the other a limited heat output and so cannot tackle large jobs.

The difference between temperature and heatvolume must be noted here. All soldering irons attain a temperature which exceeds the melting point of solder (168°C for the high-quality 60/40 grade) otherwise they would be useless for their purpose, but some deliver a greater quantity or volume of heat than others. This is determined largely by the wattage of the instrument. Hence, a soldered joint to a punched-out chassis tag may be impossible with some smaller irons because the chassis conducts the heat away faster than the element can produce it, and so the bit cools rapidly to below the required temperature. Any large area of metal will have the same effect.

Another factor is the size of the bit. The bit effectively stores heat and so acts as a reservoir. Heat flows out of the bit when the iron is used and more heat is supplied by the element. However, the outflow can be greater than the input for a short period until the stored heat is exhausted. Thus larger areas can often be soldered than would be feasible with a particular element-wattage, if the iron is fitted with a large bit. When the iron has been thus used, it will take longer for the bit to return to correct operating temperature than would a smaller bit because it has what is termed, a slow heat recovery time.

IDLING TEMPERATURE

A further consideration is the heat loss when the iron is switched on but is not in use, as is the case in most workshops for the greater vart of the time. While the iron may get hotter than needed because there is no heat conduction by application to a work area, it must not get so hot as to damage the element or cause premature deterioration of the bit. Hence the physical size of the iron barrel and bit must not be too small for the element size so that heat losses by convection and radiation are insufficient to keep the temperature to a safe limit. It follows then, that physical size is closely related to element rating and should not be too small or too large.



Stiron 20W and 60W irons, made in Sweden and featuring ironcoated bits.

In order to keep the temperature of an iron down when it is not being used for long periods, it is the practice in some workshops to operate a half-heat arrangement, whereby a lamp is switched in series with the iron. The temperature will gradually rise to not far short of the correct operating level, then when the iron is needed, the lamp is switched out and the temperature comes up within a few seconds. Another method is to stand the iron on a large chunk of metal which keeps it from overheating by conduction. An old speaker magnet is sometimes used for the purpose, as this also attracts the iron and keeps it in place.

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 - with constant on all four. *Constant acts as last entry in a calculation.
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Assembly time is about 3 hour

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- 6. Printed circuit board
- 7. Keyboard panel.
- Electronic components pack (diodes, resistors, capacitors, transistor)
- Battery clips and on/off switch.
- 10. Soft wallet,

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But if you want to get even more out of it, you can go one step further and learn how to unlock the full potential of this piece of electronic technology.



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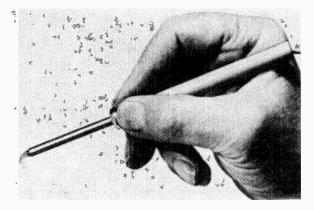
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Because of the limitations of the 25 to 40 watt iron, most workshops have at least one or two other types and sizes of iron available. For larger jobs, an iron with a rating of 60 to 100 watts is required. These irons are similar to their smaller counterparts in general construction and appearance except for the size and element rating. The bit may be square instead of the usual pencil-type. As only occasional use would be expected, the iron would not normally be left on for long periods, so there would be no overheating problems.



Work on integrated circuits requires a very small iron such as the Micro Soldering Pencil, shown here.

For the smaller and more intricate jobs, there are irons that are little bigger than pencils with element ratings of 10 to 15 watts. These are ideal for some of the tiny printed circuits that are now encountered and for the wiring of I.C.'s where the connections are close and damage could be caused by excessive heat. Heat output is obviously limited and many larger jobs could not be tackled. The element wire for these mains-operated low-wattage irons is necessarily very fine and so they are less reliable than the higher-rated ones. They should not be run continuously but only when a particular job calls for their use. Because of their small bit size, they are also makes them suitable for outside service work.

LOW VOLTAGE IRONS

Another type which has achieved a measure of popularity is the low-voltage iron. While these can be run from a low-voltage source such as a car battery, the more common method is to operate them from a mains transformer. The main feature is a very quick heating time, just a matter of seconds, and a rapid heat-recovery time. This means that the iron can be used for outside service work where delays waiting for a conventional iron to warm up are thus eliminated.

One type of low-voltage iron is constructed very similarly to the normal iron and fed from a separate transformer, which also serves as an iron-rest. Other types have the transformer built-in, either over the top of a pistol-grip handle, or in one make, actually inside the handle. With these the element is also the bit, consisting of a loop of wire connected across the transformer secondary, Fig. 1. In either of these low-voltage types, the bit can very quickly become overheated, even when being used on large areas, so a switch is incorporated in the iron so that the operator can keep switching it on and off and thereby maintain the tool at about the

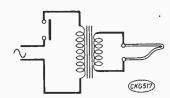


Fig. 1: Circuit of a transformer iron with element/bit consisting of a wire loop.

right temperature. In one make that uses a separate transformer, a thumb ring is used as a switch on the handle; while most of the built-in types, being pistol-like in construction, use a trigger switch.

This need for constant switching can be a drawback, especially if the switches are stiff as some are, and need considerable finger pressure. The danger of overheating due to switching on for too long can also be a hazard for transistors and other semiconductor devices.

A yet further drawback of the built-in transformer type is their weight. This is of little consequence for occasional use, but when used continuously, as in the professional workshop, they can be very tiring. The wire-loop bits are not very durable and need frequent replacement; while owing to their flexibility they cannot be used to unpick joints as can the conventional bit.



A pistol-grip soldering gun with integral transformer. The Welwyn KL3000.

The separate transformer type of low-voltage iron is therefore the more convenient, but for outside work the built-in type is probably the best. Neither though, really is as suitable as the mains-voltage type for workshop use.

CONTROLLED TEMPERATURE

Of recent years we have seen several thermostatically controlled irons which overcome some of the snags inherent with the uncontrolled types, whether high or low voltage. One, rather ingeniously, uses the Curie effect of iron. Iron, when it is heated beyond a certain point loses its magnetic properties. A small iron disc is fixed to the base of the soldering-iron bit and this has an attraction for a bar magnet which holds a switch in the 'on' position by means of a push-rod, Fig. 2. When the iron temperature reaches the Curie point of the disc, it loses its attraction, the magnet is released and the switch is opened. As the temperature drops to below the Curie point, attraction is re-established and the switch returns to the 'on' position.

Each bit has its own iron disc, which can be made with different Curie points, hence with its own temperature setting. This particular iron is a low voltage model and is operated from a separate transformer. It has a very rapid warm-up time and good heat recovery, but, because of being thermostatically controlled, does not overheat nor need switching attention by the operator. The barrel is a little short though, for some types of work.

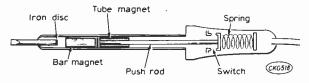


Fig. 2: Mechanism of a heat-controlled iron using the Curie effect.

Another thermostat iron is called the 'Litestat.' This is a mains-operated instrument, hence it is not encumbered with a transformer, either built-in or attached by lead. It has a 70 watt rating, but is only little larger than the average 25 to 40 watt instrument, the thermostat preventing it overheating. As with other thermostat irons, when there is a heavy outflow of heat from the bit due to working on a large heat conductive area, any loss of temperature is compensated by the switch remaining on longer than usual, and the larger element quickly supplies the extra heat volume. Thus we have the best of both worlds, a moderate sized iron that will handle reasonably small jobs (quite small if the extra-small bit is used) and will also tackle the big ones. Although the occasional user will probably get on quite well with a normal uncontrolled iron, the advantages of the thermostat control really make this type of iron a 'must' for professional workshops.

These then are the basic types of soldering instrument and their respective features. Within each category there are many makes and models and engineers and hobbyists alike often have a particular favourite that handles well and seems to produce good work for them.

SOLDERING BITS

Bits are available in several types. There are of course the various shapes and sizes that are produced for specific applications, most irons having a number of alternative bits obtainable as extras. There are though, differences in material. The most common is copper, which because of its high heat conduction is the best material (excluding precious metals) for the purpose. When clean it can be tinned quickly and easily, another great advantage. A disadvantage with copper bits is their deterioration with use. Prolonged periods of operation at high temperatures causes oxidization and flaking of the metal. In addition, at the bit face where the solder is melted, cavities begin to form due to the chemical affinity of solder for copper, which absorbs it each time the bit is used.

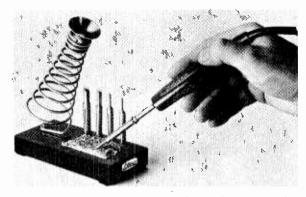
Little can be done to stop the flaking other than running the iron at a lower temperature during standby periods, but the cavities can be almost eliminated by using the Savbit solder developed by Multicore. This contains minute traces of copper which satisfies the affinity of the solder without it taking more from the bit.

Other types of bit are made from alloys, or are nickel or chromium plated to achieve longer life. One method used by some manufacturers is to clad the copper bit with iron which is harder and more durable than copper, yet has the copper core for its thermal properties. A disadvantage with all these bits is that they cannot be filed without ruining them, thus once the plating or cladding has gone the bit must be discarded, whereas a copper bit can be filed flat at its face many times before filing and flaking reduces the size to inoperative proportions.

The superior thermal qualities and ease of tinning. make the copper bit still the favourite, especially since its life can be prolonged with special solders.

USING THE IRON

Now just a point or two on using the iron. It is surprising the number of people who are technically well qualified, professional engineers included, who cannot seem to produce a good soldered joint. It is very important to do so, as all sorts of faults can arise from poor soldering. It is noteworthy that all candidates for the RTEB servicing exams had to undergo soldering tests and failure led to automatic disqualification for the whole of the practical and theoretical examinations.



Litesoid Conqueror iron and stand with bit-cleaning sponge and , range of interchangeable bits.

There is nothing really difficult in making a good joint, just observing a few straightforward rules. The first one is to make sure that both surfaces are clean. In the case of wires, this can be done by pulling the wire a couple of times through the blades of a pair of side-cutters, as though one were stripping insulation. Terminals and tags can be scraped with a screwdriver blade. In most cases wires and terminals will be already tinned, but do not rely too much on it. Next both surfaces should be tinned. This is done by applying the iron to the surface for a few seconds, and then introducing the solder to bit and

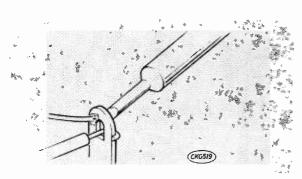


Fig. 3: The iron should heat the whole joint-not just the solder.

surface so that it runs easily over it, Fig. 3. If the solder is thick and slow to run, the bit temperature is too low, either because the iron has not been switched on long enough, or the iron is too small for the work. The solder may not run over the surface readily at first because insufficient heat has been transferred from the bit, and it is just not hot enough to melt the solder. This could be due to poor contact between bit and surface, but a little solder introduced at the junction of the two, will give a good thermal conduction, and the surface should then quickly attain sufficient temperature to itself melt solder when applied.

When both surfaces have been thus tinned, they are brought together in mechanical contact, and the iron applied again to both. More solder is then introduced so that it runs freely over both surfaces,

LETTERS—continued from page 742

Value for money

I greatly appreciated the article on 'Going Back' as it is full of nostalgia. I have taken P.W. off and on since the early beginnings, but only since 1967 have I bought it every month and J only started then because a free record of audio faults was given away, but on reading the articles on transistorised equipment, and particularly details of a transistor SW receiver by F. G. Rayer, I was astonished at the transformation in building techniques (being brought up on 38" thick breadboards and 116" dia. connecting wire!) and plunged up to the neck in transistor circuits and have been building them from P.W. projects ever since.

Though the price of P.W. has greatly increased, the contents have kept in step and I think it is still good value for money. It is improving all the time, as reference back to only a few years ago will show, and even in the last few months there have been detailed improvements, such as better layout and the contents page being put on the first page. Long may you continue!

Incidentally, radio parts seem to be one of the few things which have not greatly increased in price, and some, like transistors and i.c.s, have actually gone down.—R. A. Read (Salisbury).

A Fly in the Ointment?

Do any readers know how to build an electronic fly-catcher? We are driven crazy with flies in the summer and we are sure that it is the sheep that bring them in.

I was born in the UK and lived many years in Africa but the flies were never as bad as here. I have taken P.W. for over 20 years now but have not seen any details of fly catchers. Also, we are a bit lost out here for getting components especially as we can only get a £2 British P.O. here on demand at the Post Office.-J. S. Skeels (One Tree Point, Rukaka, Northland, New Zealand).

then the iron is withdrawn. Do not move the work until the solder has solidified otherwise a weak joint will result; this will take only a second or two. Where possible the joint should be mechanically sound before soldering. No external flux should be used as these are often corrosive and will give trouble in the future. Sufficient of the correct type of flux is contained in the cores of solders intended for electronic wiring, to do the job.

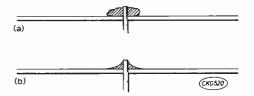


Fig. 4: (a) A 'dry' joint, showing the blob of solder due to insufficient heat or dirty surfaces.
(b) A good joint, showing smooth flow of solder over joined surfaces.

Do not use too much solder as this is not only unnecessary but could form a short to adjacent terminals. In appearance, the joint should be bright and smooth. A lumpy or pitted appearance shows the solder was not hot enough. It should also appear as a 'mound' rather than a blob. The illustration Fig. 4 shows what is meant by this. If the solder surface comes down and curls under as shown, it has not taken to the surface and we have a 'dry' joint. By observation of these points and a little practice, perfect joints can be made every time.

Short Wave Converter

I have built the Radio Nederland converter, *Practical Wireless*, September 1973, and am very pleased with the results, however. I should like to point out an error in publication which would result in disappointment to those to quote your preamble — "with little experience in electronics."

Reference page 409 figure 1 circuit diagram oscillator Tr2 AF 124 and page 410 drawing AM0022. Note the emitter and base connections are shown reversed so there could be no conduction in the collector circuit due to reverse polarity at the base.

As a note of interest I used Wearite P coils either PA4 or PHF4 which very nearly approximate the coil data given for L1 and L2, a similar coil was slightly modified to make up L3. A PHF6 coil tuned by a 200pF silver mica in parallel with a 250pF trimmer was used for L4. The unit is used with a BUSH TR130 receiver tuned to the extreme h.f. end of the m.w. band.—A. J. Birkinshaw (Telford, TF2 6RA).



THE article last month gave circuit descriptions of single and multi-system matrix decoders based on two circuit modules, Units A and B. There now follows constructional details of these two units, and of the additional units and components needed to build a multi-system decoder with infinitely variable front and back separation.

Readers are reminded that they will require, in addition to the decoder, a stereo outfit plus a pair of back amplifiers and speakers for quadraphonic reproduction from discs and tapes.

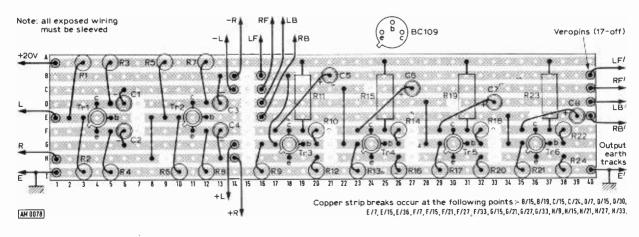
Unit A construction

Unit A is assembled on a piece of 0.1in. pitch Veroboard 0.9in. wide by 4in. long, see Fig. 16. Begin by making breaks in the copper strips, where shown, with a spot face cutter, and then insert and solder the terminal pins.

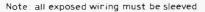
During assembly, it is important to ensure that the transistors are not overheated as this could have a detrimental effect on noise performance. A clip made of aluminium sheet should serve to conduct away heat when placed around the transistor can during soldering. Constructors who are not accus-



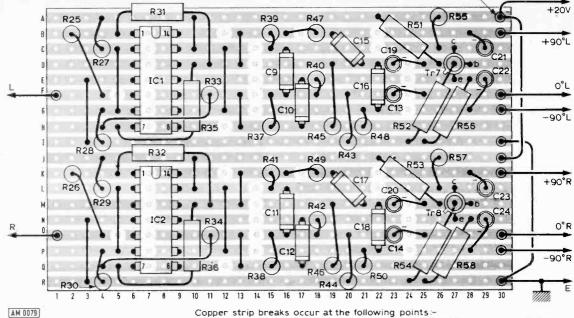
tomed to $0 \cdot 1$ in. Veroboard should also make sure that solder blobs do not bridge between the copper strips. It is a good idea to run a sharp knife blade along the gaps between strips to remove excess flux and any particles of solder. When inserting capacitors in the unit A circuit board, check that the polarity is as shown in Fig. 16.

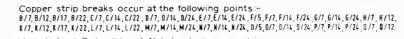


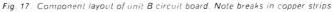


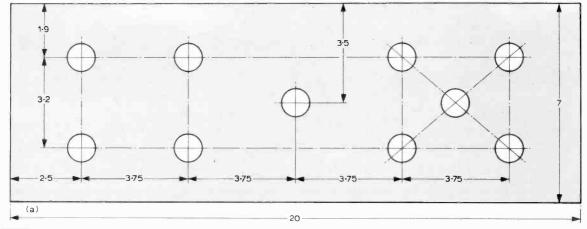




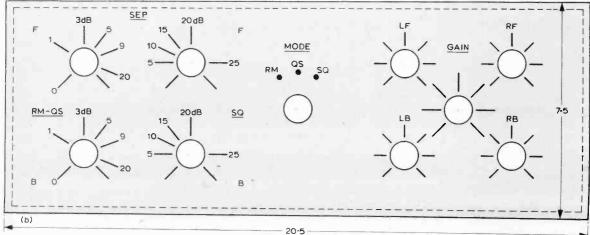




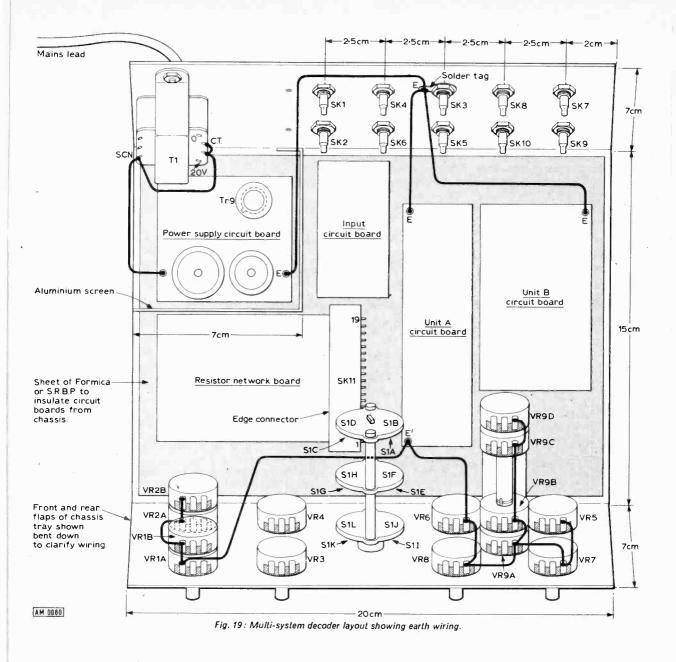


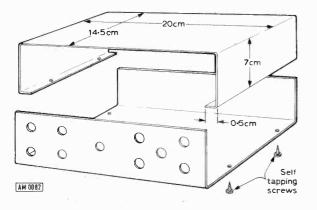












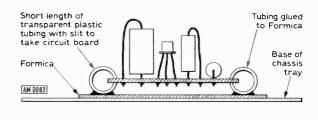


Fig. 20: Dimensions and fixing details of the chassis cover.

Unit B construction

A piece of 0.1in. pitch Veroboard 1.8in. wide by 3in. long is employed for unit B, and the layout is shown in Fig. 17. Left and right hand channels are identical and are arranged one above the other on the circuit board.

Make breaks in the copper strips according to the diagram of Fig. 17 and insert and solder all terminal pins. Commence with the ICs, leaving pins 3, 5, 8, 11, and 14 unsoldered, and then position and solder the remaining components. Use a heat clip on Tr7 and Tr8 and ensure that the polarity of the electrolytic capacitors is correct.

Checking units A and B

As a preliminary check, wire the earth and $\pm 20V$ terminal pins of unit A circuit board to an 18V battery (two PP9s in series) and with a testmeter measure the voltages between the earth terminal and the transistor cans. Tr1 and Tr2 should show a voltage of about 14V, and Tr3-Tr6 a voltage of 9V. If there is a serious discrepancy, look for a short circuit between the copper strips on the underside of the circuit board, or an error in component positioning.

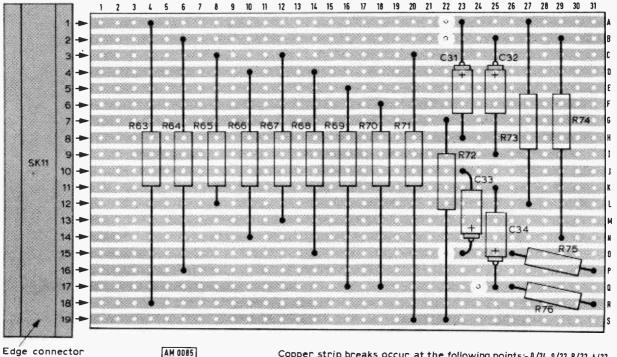
To check unit B, connect the 18V battery to earth and +20V terminals and measure the voltage at IC1 and IC2 pins 10 and 12, which should be at 9V relative to the earth terminal pins. The can voltage of Tr7 and Tr8 will be about 14V if there are no constructional faults.

Small piece of 16 swg aluminium to engage in slot at the back of the front pots, and slot in the spindle. AL Cut slot in spindle AM 0084 16 swg aluminium bracket

Fig. 22: VR9 assembly utilising two dual-gang potentiometers.

If the user intends to experiment with a singlesystem decoder, units A and B can be employed with an 18V battery, or the power supply of Fig. 15, with 22kΩ balance controls (VR5-VR8 Fig. 14) wired to the LF, RF, LB, and RB outputs of unit A. It is advisable to connect a 1000 // F 25V electrolytic capacitor across the supply rails when operating units A and B from a battery.

Where an oscilloscope with X-Y facilities is available, unit B can be tested for 90° phase shifting by injecting a signal of 2kHz into the left input, with the X input of the scope linked to the 0°L output, and the Y scope input connected to each of the 90°L outputs in turn. The resulting display should be a near perfect circular trace. Repeat the test for the right hand channel.



Edge connector

Copper strip breaks occur at the following points:- 0/24, 0/22, 8/22, A/22. Fig. 23: Component layout of resistor network board.

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TIL360	L	E	D	٦	16	DI	L		6	Т	0.1	іля	21	10	'nΑ	T	at	ho	de	Т	2.50	11	5.00
DL707	L	E	D	- 1	14				1		0.3	ins	31	30	mA		An	od			2.00		2.00
DL34	L	E	D		14	н			4		0,1	ins	51	/ 10	mΑ	c	atl	hod	de 👘		2,50	10	0.00
DL82		E			16	"			1		0,6	sins	6	/ 30	mA	1		od	-	1	6.50		6,50
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Multi-system decoder construction

Fig. 19 shows the layout of a multi-system decoder based on the circuit of Fig. 14. Additional circuit boards serve to accommodate the resistor network, input capacitors and resistors, and power supply components; these will be described later.

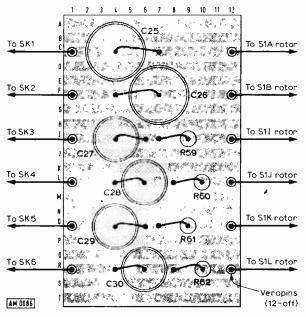
A start can be made by making up the chassis tray from 16s.w.g. aluminium sheet, to the measurements shown in Fig. 19. Allow 7cm of space for the power supply, and mark out and drill the rear of the chassis tray to take sockets SK1-SK10. Next, mark out and drill the holes to mount transformer T1, the power supply screen, and mains lead grommet.

Drilling details for the front of the chassis tray are given in Fig. 18a, and Fig. 18b shows a front panel made of 20.5cm by 7.5cm brushed aluminium or white Formica, which is drilled to match the holes in the chassis tray. The dimensions and fixing details of the chassis cover are shown in Fig. 20.

Glue a sheet of Formica or s.r.b.p. inside the base of the chassis tray to insulate the circuit boards from the chassis; this should measure 19cm by 14.5cm. A method of securing the circuit boards is shown in Fig. 21.

Make up switch S1 from three 4-pole 3-way wafers, with a three spacer gap between wafers. Mount the assembled switch on the front of the chassis tray, along with controls VR1-VR8.

In the absence of a four-gang component for VR9, this can be made up from two dual-gang potentiometers, as shown in Fig. 22. A small piece of sheet aluminium engages with the spindle slot at the rear of the front pair of pots, and with a slot in the



Copper strip breaks occur at the following points.- C/6,F/6,1/5,1/8, L/5,L/9,0/5,0/8,R/5,R/9.

Fig. 24 : Component layout of input circuit board.

spindle of the back pots. To align VR9, set the front pots to mid-track and measure the resistance between a slider and the earthed end of its track. Rotate the body of the rear pots to give a similar resistance reading on a rear pot slider and its track end, and then tighten the mounting nuts. VR9 can now be mounted on the chassis.

Resistor network board

The resistor network components are assembled on a piece of $0 \cdot \lim$, pitch Veroboard $1 \cdot \lim$, wide by $3 \cdot \lim$, long, and this is designed to plug into a 19way edge connector (SK11) to facilitate easy modification of matrix parameters. The layout of the resistor network board is shown in Fig. 23.

A suitable edge connector, such as the RS Components $0 \cdot 1$ in. 25-way, may be cut down to 19 ways with a small saw. When the resistor network board is completed it can be inserted in SK11, and the latter glued to the insulating board on the chassis tray.

Input circuit board

Fig. 24 shows the input circuit board with components mounted on $0 \cdot 1$ in. Veroboard, which measures 2in. wide by $1 \cdot 2$ in. long.

In Fig. 14 (last month) the lower unit board should have been designated unit B. We regret, that due to pressure on space, final constructional details, wiring and setting up, have had to be held over until next month.

TO BE CONTINUED





No. 55 TRIPLEX SIGNALLING UNIT

A series of simple transistor projects, using not more than twenty components.

THIS project can be used as quite a useful gadget for signalling between the house and a shed or to illuminate signs outside an office door. Signals are produced by two lamps either. or both, of which can be switched on and off. This does not, in itself, sound very clever but the circuit to be described enables one to do this with a single pair of wires. Thus, over two wires one can display three separate codes on the two lamps.

Circuit

The trick is to make use of positive going half cycles of the mains supply to switch on one lamp. In Fig.1 D6 is forward biased for positive going cycles and LP2 will light but when SW2 is switched to the centre position the polarity of these half cycles is reversed and D5 becomes forward biased, turning on LP1 (D6 becomes reverse biased and LP2 goes out).

The third code, having both lamps on at the same time, is obtained by turning SW2 into the third position which applies a.c. to the signal wire pair direct from the transformer. LP1 and LP2 will now each light up, LP2 on positive and LP1 on negative half cycles.

Variations

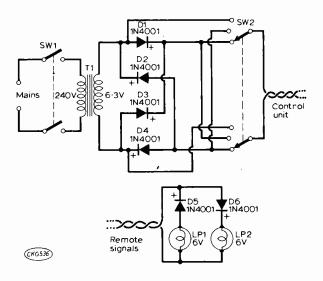
There are many variations to this circuit, and relays could be used instead of the lamps. Provided limiting resistors were inserted into the lines and the voltage reduced to below the reverse breakdown level, light emitting diodes could be used instead of the lamps, diodes D5 and D6 being omitted. For those who do not wish to bother with a.c. and a transformer one can still transmit two codes down the pair of wires by dispensing with the control unit. All that is needed in its place is a suitable battery and a reversing switch on the control end of the signal wires. One polarity will turn on one of the lamps, reverse the polarity of the supply and the other lamp will light. Apart from the diodes most of the components can be

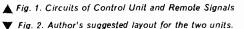
★ components list

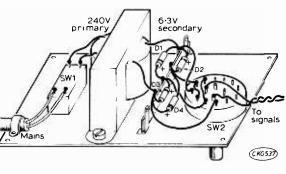
D1-6	Diodes 1N4001
LP1-2	6V Lamps
SW1	2 pole mains switch
SW2	2 pole 3 way wafer switch
T1	Mains transformer, 240/6-3V
	Mounting box, tag strip, etc.

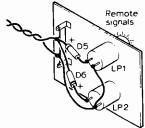
salvaged from old equipment. Any 6.3V transformer will do for T1 and probably the best source is an old valved radio.

Fig. 2 shows a suggested layout for the unit, on a metal or insulating material panel, which can be the lid of a box.













SHORT WAVE DX by MALCOLM CONNAH

A S many of you will know, propagation conditions vary according to the time of day, the time of year and the position in the 11-year sunspot cycle; as well as other minor factors. This means that, at any particular time, there is an optimum band for reception from any part of the world.

Forecasting these optimum bands is a relatively simple matter once one has collected all the necessary information. The following forecast is for reception in Western Europe and is listed by transmitter site.

North America During the late afternoon the most suitable band will be 25 metres, by 1900 GMT this will have changed to 19 metres but will return to 25 metres by 2300. During the early hours of the morning the most useful frequency will drop still further reaching 31 metres by 0300.

Central & South America The optimum frequency during the late afternoon will be 16 metres and this will drop gradually during the evening to be 19 metres at 1900; 25 metres at 2300 and 49 & 60 metres at 0300.

Middle East The late afternoon finds 19 metres as the best band dropping to 31 metres at 1900 and 41 metres at 2300.

Far East & Australasia Reception for this area will be much the same as the Middle East except that the best band will not drop below 31 metres.

Africa Late afternoon reception will be best on 16 metres dropping to 25 metres at 2000 and 31 metres at 2300.

DX News

COSTA RICA: Radio Capital de Costa Rica has been heard on 4832kHz at 0130 GMT. Reception is poor due to the low power of 1 kW.

ECUADOR: Radio Nacional del Ecuador has been noted with a programme of news and Latin-American music on 6170kHz at 0500 GMT.

EL SALVADOR: La Voz del Comercio, Colonial Sta. Lucia, Santa Ana, is asking for reception reports on 9545kHz. The best time for reception being 1600 GMT.

MEXICO: XERMX has been heard in Spanish on 15195kHz at 0330 GMT, this is a change from the usual frequency of 15125kHz.

TUNISIA: Radio Tunis has been noted on 15226 kHz at 2345 GMT and at 0910 GMT on 11970kHz. (Some of the above items by courtesy of Sweden calling DXers.)

Readers' Logs

John D. Porter of Bakewell (No jokes about Bakewell tarts—please) in Derbyshire has nine transistors and a few other components built into his superhet receiver. This, in combination with a 45 metre longwire and some attention to the higher frequency bands, produced the following results:

- 11710 R. Nacional d'Espana at 0005.
- 15110 R. Grenada, Windward Is., English at 2100.
- 15150 R. Pyongyang, N. Korea noted at 2030.
- 15375 HCJB, Quito, Ecuador at 2210.
- 15415 R. Kuwait in English at 1850.
- 15450 R. Nacional de Brasilia in English at 2355.
- 17820 R. Canada Int., in Polish at 1540.
- 17885 HCJB, Quito, Ecuador noted at 2250.

Andrew Brown of Maidenhead in Berkshire is fourteen years of age so both his National HRO and R107 receivers are older than he is. The connection of a 10 metre long-wire antenna enabled the following stations to penetrate Andrew's shack:

- 7275 RAI, Italy in English at 1936.
- 9005 Tehran, Iran in English at 2000.
- 9560 R. Jordan, Amman in English at 1600.
- 9655 R. Damascus, Syria in English at 1930.
- 9745 R. Baghdad, Iraq in English at 1930.
- 11765 Radio Australia noted at 0710.
- 15165 R. Denmark in Danish at 0945.
- 15325 R. Pakistan, Karachi in English at 1530.
- 15520 R. Bangladesh in English at 1715.
- 17825 NHK, Japan in English at 0800.
- 21520 RSA, South Africa noted at 0755.
- 21655 R. Norway, Oslo in English at 2000.

David Thornley of Dukinfield, Cheshire has a Trio 9R59DS receiver and a Joystick antenna with ATU; which enabled him to hear:

- 7125 R. Peking in English at 0120.
- 9020 R. Iran in English at 2000.
- 9610 R. Kiev in English at 0030.
- 11672 R. Pakistan with news in English at 2000.
- 11880 Voice of Turkey in English at 2000.
- 15425 Israel with news in English at 1200.
- 17735 R. Havana, Cuba in English 2035.

21605 RSA, South Africa with quiz show at 1305.



MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

ROY PATRICK (Derby) has been busy with his National 1400 receiver on the medium waves. He reports 'good reception of Radio London on 1457kHz and the two IBA London transmitters on 557kHz and 719kHz. While on a visit to Farnborough (Hants) Roy logged Radio Brighton 1484kHz, Radio London and Radio Solent on 998kHz.

Richard Livesey (Guildford) has used his Audiotronic multiband receiver with internal ferrite aerial to hear Radio Portugal 755kHz at 2310hrs; Radio Prague 1286kHz; Trans World Radio Monte Carlo 1466kHz at 2230hrs; Radio Moscow 1493kHz at 2230hrs; Radio Warsaw 1502kHz at 2230hrs. All of these broadcast in English.

Ian Gordon (Birmingham) has a Codar CR70A receiver, a 25 metre longwire antenna and an aerial tuning unit (ATU). He reports hearing Radio Tirana 1394kHz with sign-on at 2000hrs; Radio Blackburn 854kHz; R. Leeds 1106kHz; R. Stoke 1502kHz; R. Nottingham 1520kHz; R. Bristol 1546kHz plus the American Forces Network in Germany on 611kHz (Grafenwohr / Kaiserslautern / Nürnberg), 872kHz (Frankfurt), 935kHz (Berlin), 1106kHz (Munich),

1142kHz (Bremerhaven/Stuttgart). The AFN can also be heard on 1034kHz (Karlsruhe), 1304kHz (Heidelberg), 1394kHz (Augsburg).

M. Laugharne (Didcot, Berks) reports hearing R. Solent 998kHz, R. London 1457kHz, R. Oxford 1484kHz and R. Bristol 1546kHz on his Philips portable receiver. T. D. Wilson (Hemel Hempstead) used a Grundig Mariner to hear R. Sweden 1178kHz and R. Portugal 755kHz, both in English at 2300hrs. He mentions receiving WINS, New York City on 1010kHz last February. Gary Celand (Southall, Middlesex) would like to listen to North American stations on the medium waves and when reception is possible. A path of darkness between transmitter and receiver is required for medium wave propagation. Listen for North Americans some five to six hours after sunset in the UK. From November to February they can be logged as early as 2330hrs when conditions are favourable. Those most frequently heard are CJON St. John's in Newfoundland on 930kHz; CHER Sydney, Nova Scotia on 950kHz; WINS New York City on 1010kHz; CBA Moncton, New Brunswick on 1070kHz and WNEW 1130kHz New York City.

The BBC have announced the location of the first four low power medium wave stations which will improve the Radio 4 service to the south-west of England. Torquay 854kHz (351m), Barnstaple 683kHz (439m), Plymouth 1457kHz (206m) should come into service before the end of 1973 and Redruth 755kHz (397m) by the Spring of 1974. The Barnstaple service will replace the present one on 692kHz (434m) while the others will be additional to the existing Radio 4 medium wave service.

VHF/FM DXING

by SIMON DAVID

T. J. Clamp of Cranbrook in Kent lists among other stations in the U.K., Markelo 2 on 98.4MHz and Roermond 1 on 88.3MHz, both from Holland, as well as Aalter, Belgium on 98.5MHz. He uses a Grundig Melody Boy 1,000 receiver and the in-built 86cm telescopic aerial. He also says "How about a list of BBC local radio station frequencies on f.m?" Other readers have also asked for this information, so I have included it in this month's column. The BBC Engineering Information Department issues complete lists with frequencies, powers, and polarization on Information Sheets 1034(24) and 1919(21) for any one with a technical interest. In the not too distant future I shall be giving details of some of the European frequency allocations. Details on Radio Telefis Eireann were given last month.

Igor Hájek has given me some very interesting gen on East European bands. With reference to my comments in the September issue, he points out that East European countries (including U.S.S.R.) use the 65-73MHz band, possibly with a view to making it difficult for their local population to have access to Western broadcasts. In spite of this, Czechoslovakia have tuners that cover West Europe (CCIR) and East Europe (OIRT). How long before we have this facility as commonplace in the U.K.? (see Leader article—Ed.).

This lower frequency band is in the 4 metre area of the dial and does lend itself very well to DX reception, as my colleague David Gibson will testify. Future plans for stereo on v.h.f./f.m. include Wenvoe and Kirk O'Shotts next year, Pontop Pike and Sandale (near Carlisle) in 1975. It is surprising that Norfolk and Huntingdon areas are not yet planned, especially in view of the flat terrain.

The following is a list of BBC Local Radio stations. Birmingham, Blackburn, Manchester and Teesside will have transmission powers increased. Slant polarisation is employed at Blackburn, Derby, Leeds, Leicester, Manchester, Nottingham, and Sheffield (main). All others use horizontal polarisation. Medium wave shown in brackets.

Birmingham 95.6MHz (206m) Blackburn 96·4MHz (351m) Brighton 95.3MHz (202m) Bristol 95.5MHz (194m) Carlisle 95.6MHz (397m, 206m) Derby 96.5, 94.2MHz (269m) Humberside 96.9MHz (202m) Leeds 92·4MHz (271m) Leicester 95.1MHz (188m) London 94.9MHz (206m) Manchester 95.1MHz (206m) Medway 96.7MHz (290m) Merseyside 95.8MHz (202m) Newcastle 95.4MHz (206m) Nottingham 95·4MHz (197m) Oxford 95.2MHz (202m) Sheffield 97.4, 88.6MHz (290m) Solent 96 · 1MHz (301, 188m) Stoke-on-Trent 96.1MHz (200m) Teesside 96.6MHz (194m)

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OUTPUTS Tape 100mV. Main output, Odb (0.775volts)

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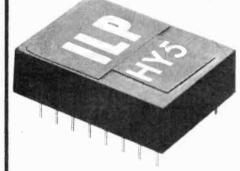
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SHORT WAVES by DAVID GIBSON, G3JDG

I T'S an interesting period for Amateur Radio. The sunspot count continues to creep lower and the longer, darker (colder) nights are making 14/21MHz less favourite for DX working. For the s.w.l. who reckons he's up to tackling something a little more difficult, then I suggest a serious DX assault on 7MHz. This will assume more and more the role of the major DX band. Further down, on 3.5MHz, more DX is becoming apparent so it could well be an l.f. DX winter.

On 3 5MHz this past month, goodies like OA4OS, ZS6TE and 9J2DT have been heard while up on 7MHz the air has been buzzing with c.w. offerings from calls like CM2JA, CR6AI, FG7XC, VK3MR, ZS5AN and 8P6DR.

Hair-raising happenings on top band. Several G stations have worked VP8KF in the Falklands. A few years back, this station would never have been thought about on $1 \cdot 8$ MHz. Even now, a VP8 would cause excited s.w.l. squeaks if heard on 14MHz. Topband sleuths are invited to lay in wait for r.f. travellers like ZL1MQ and a few JA stations who are known to be loitering. One station in Japan (JA7AO) has worked all continents (WAC) except Europe so it would be a safe bet to reckon his signal is there somewhere—who'll be first to report it?

Up on ten metres things seem to be fairly static. Long periods when one hears a noise like frying eggs (cheaper variety) and then, suddenly, an S9 plus five million dB's (well, it sounds like it) comes out of nowhere. South African stations are logged without too much effort and the South American continents comes romping in at times. Don't forget to listen first for the beacon stations since these will give a useful indication of what the bands are doing.

Before we take a peep at the logs sent in this month, let's open up the JDG little black book for contests in November. According to my crystal ball, the following are on: November 10-11, OK DX contest (c.w./phone); 10-11, topband contest; 11, four metre contest; 24-25, CQ WW (c.w./phone) contest. First event in December is on the 9th and is a two metre contest for fixed stations—you've just got time to tie that 40-element Yagi beam to the chimney pot and switch on!

Readers' Logs

Dave Gregory (Plymouth) confesses, "I have been a Broadcast Bands maniac (is there any other kind?) for some months now". Brethren will be pleased to know that my Brother Gregory has seen the light and cleansed his sins by purchasing a 9R-59DS, RA-1 and CR100. With a homebrew a.t.u. and "DX processing unit" Dave repents on 14MHz with the following log; A51PN, A6XP, AR1RSP, EA7PS (an XYL—O'lay); WA5FW, ZB2BL, 3A2EE, 4Z4MQ, 5Z4GB, 5Z4GK.

A. McNeill (Newbury), comments on the many eastern europeans loose on 14MHz. He also praises the DX'ers processing unit which was featured in P.W. and queries the callsign NI3A who keeps popping up. Are there NI takers to answer this?

Derek Harding (Godstone) says he's 23 years old and has been an s.w.l. for four days (What a waste of 22 years, 361 days). Derek asks how he can filter out the various loud whistles which beset him? Anyone got any thoughts other than the on/off switch?

John Turner sends in a 21MHz selection from a log made during his school holidays (think of all the conkers you missed). Gear in his bedroom at Doncaster includes a Pye Cambridge receiver with an 85ft end fed supplying the microvolts to the tune of; A2CCY, CE3OE, CN8CG, CP1HL, CR6AD, CT1BY, CX2CS, CX7BM, DU1FE, EA8CS, EA8HH/M, EL1G, ET3USA, HK3CDW, HS4AJL, JA4PE, JA6PIC, JA7KHZ, JH1DEV, KP4AD, KZ5EK, LU5MAO, M1C, PZ1DR, T12IO, TR8VT, TU2DO, VK4PU, VP2MF, VP8ML. VP9CB, VQ9BP, YN1AZ, YV5EED, ZD3D, ZD8MH, ZS4JW, 4Z4LM, 7X0WW, 8R1J, 9G1AF, 9H1DP. 9M2DQ, 9U5CR, 9X5VA,

Tam Large (Hassocks) lives on a farm in Sussex. His favourite animal is a 9R-59DE. Feed it a staple diet of mains electricity and put it on a 200ft. end fed lead and it yields the following twenty metre tweets; CR6LX, HP1TG, K2LZQ/OH0, M1C, PZ1DR, 4W1AF. Similar treatment brought forth the following from 21MHz; TG9CQ, XE1GR, ZD3D, 9M2CX.

Paul Davies (Blackpool) is learning to read c.w. (good lad). Meanwhile, he listens with baited breath on 14MHz to the following juicy jingle; CR6GA, EL8J, EP2SP, ET3GA, HR2WTA, IB0PV, JA4JUV/ MM, JY6HCT, KA6HQ, 9H1CQ, 9H4B, 9K2AL, 9M2DW, 9X5NA, all on s.s.b. Gear used is 5 Heath HR-10B, Joystick antenna and an a.t.u.

S. Eldridge (Crawley), has a CR70A, 132ft. end-fed looped round the bedroom and a yen to listen on 15 metres. Here's the gen on his yen; A6XB, CE3PY, CR6AG, CR6HZ, CT2AB, HI8LC, JA8ISK, JE1MUM, JF11UA, JH3EXI, JR1TAM, KA2PJ, LU6FEP, PT2JB, TI2STI, TR8VE, VQ9M, VU2DK, ZP5VO, ZS1J, ZS4JW, 5N2ESH, 5U7BA, 9X5VA.

BROADCAST BANDS

Short Wave Reports by 15th of the month to Malcolm Connah, 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.

Medium Waves Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG. VHF/FM Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

AMATEUR BANDS Short Wave/VHF

Logs in alphabetical order please by 15th of the month to David Gibson, G3JDG, 12 Cross Way, Harpenden, Hertfordshire.

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151 200 8 0 12 1 x 9 3 x 10 2 5 31 52 152 250 13 12 12 1 x 11 8 x 10 2 7 01 67 AS BELOW
153 350 15 0 14 0 × 10 8 × 11 8 9 40 82 154 500 19 8 14 0 × 13 4 × 11 8 13 55 - 156 1000 38 0 17.2 × 16 6 × 14 0 24 97 -
158 2000 60 0 21 6 × 15 3 × 18 1 41 25 -
Ref VA Weight Size cm Auto Tabs P&P
$ \begin{array}{c} \ell \\ ho_{0} \ (Watts) \ lb \ oz \\ 113 \ 20 \ l \ 0 \ 5.8 \times \ 5.1 \times \ 4.5 \ 0.115.210.240 \ l \ 0.02 \ 22 \\ 64 \ 75 \ 2 \ 4 \ 7.4 \times \ 6.7 \times \ 6.1 \ 0.115.210.240 \ 2.00 \ 30 \\ 4 \ 150 \ 3 \ 4 \ 8.9 \times \ 7.7 \times \ 7.7 \ 0.115.200.220.240 \ 2.42 \ 36 \\ \end{array} $
66 300 6 4 9 9 x 9 6 x 8 6 , 4 70 52 67 500 12 8 12 1 x 11 2 x 10 2 , 6 93 67
84 1000 19 8 14-0 × 13·4 × 14·3 ,
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Ref Amore Weight Size cm Secondary Windings P & P
111 0.5 0.25 8 4.8 x 2.9 x 3.5 0.12V at 0.25K-2 1.02 22 1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$
115 20 10 11 8 14 0 x 9 6 x 11 8 0 12 V at 10A 2 6 98 67 187 30 15 15 8 14 0 x 12 1 x 11 8 0 12 V at 15A 2 12 90 82
30 VOLT RANGE
No. 10 oz £ P 112 0.5 1 4 6.1 x 5.8 x 4.8 0-12-15-20-24-30V 1.22 22
79 1 0 2 4 7 0 x 6 7 x 6 1 ., ., 1 62 36 3 7 0 3 4 8 9 x 7 7 x 7 7 2 43 36
21 4·0 6 4 9·9 x 9·6 x 8·6 3·55 52 51 5·0 6 12 12·1 x 8·6 x 10·2 4·42 52
117 6·0 8 0 12·1 x 9·3 x 10·2 ,, , 5·28 52 88 8·0 12 0 12·1 x 11·8 x 10·2 ,, , 6·82 67
50 VOLT RANGE Ref. Ambs Weight Size cm. Secondary Tabs P & P
No. Ib oz $f = 0.5$ $1 \cdot 12$ $7 \cdot 0 \times 6 \cdot 4 \times 6 \cdot 1 \cdot 0 - 19 - 25 - 33 - 40 - 50 \vee 1 \cdot 60 \cdot 30$
104 2.0 5 8 9.9 x 8.9 x 8.6 3.25 42
106 4·0 10 0 12·1×10·5×10·2
60 VOLT RANGE
Ref. Amps. Weight Size.cm. Secondary Taps P&P No. Ib oz E P
126 1 0 3 4 8 9 x 7 7 x 7 7 , , , 2 26 36 127 2 0 6 4 9 9 x 9 6 x 8 6 3 55 42
125 3 0 8 12 12 1 x 9 9 x 10 2 ,, , 5 41 52 123 4 0 13 12 12 1 x 11 8 x 10 2 ,, 6 98 67
122 10:0 25 0 17:2 x 12:7 x 14:0 , , 16:75 *
Ref. Amps. Weight Size cm. P&P No. Ib oz Ep
5 4.0 3 4 8.9 x 7.7 x 7.7 Please note these 2.45 42
146 8.0 6 12 9.9 x 10.2 x 8.6 clude rectifiers 4.22 52 58 12.5 12 0 14.0 x 10.2 x 11.8 6.29 67
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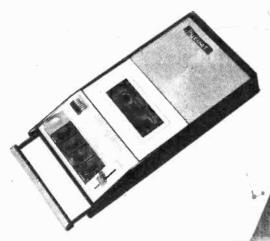
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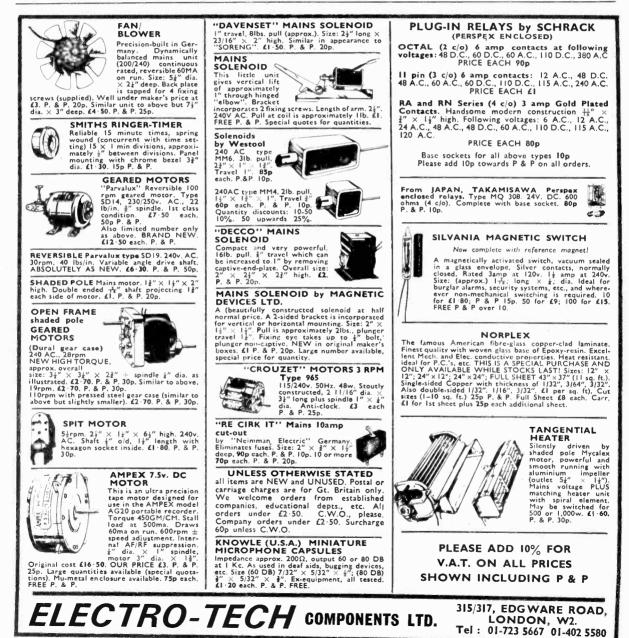
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 680.
 size 14
 x 14

 Model
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 x 14
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MAINS TRANSISTOR POWER PACK

FOWER PACK Designed to operate transistor sets and amplifiers. Adjustable output 6v., 9v., 12 volts for up to 500m A (class B working). Takes the phace of any of the following batteries: PP1, PP3, PP4, PP6, PP7, PP9, and others. Kit comprises: mains transformer rectifier, smoothing and load resistor condensers and instructions. Real snip at only \$1.10 plus 20p postage.

DESK TELEPHONES

Ex G.P.O. Black standard model with dialling dial but no internal bell. Supplied with con-nection diagram \$1 each. Ditto with bell but without dialling dial \$1.25 model as illustrated with bell and dial \$1.50 each plus 50p post for single then 65p per pair.

SMOKE WILL KILL-GAS WILL KILL-FIRE WILL KILL

But, if you install SAGA (our smoke and gas alarm) VONE family will have the latest electronic protection vainst these killers

against these killers. Saga uses a fantastic electronic sensor which "smelle" smoke and gas and sounds the alarm inimediately. In a neat case measuring approx. $\delta'' \propto 31'' \propto 21'''$, it has its own internal alarm, also a connector for addi-tional bells. You just plug it in to the mains and hang it near the celling. Saga uses so little electricity that it will hardly move the meter, leave it on always to give night and day protection. &909 plus 30p post or Kit of Paris &509. Battery Model Kit only &409.





Mains operated, turbo blower type. Freesed steel housing contains motor and impeller. Motor is 1/10th h.p. giving considerable air flow but virtually no noise. Approx. dimen-sions 10} in. wide \times 12 in. dia. outlet into trunking 10} \times 4 j. in .8565 plus £1 post and insurance.

STANDARD WAFER SWITCHES

Standard size 14" wafer-silver-plated 5 amp contact, standard #" spindle

2" long-with	locking	g wash	er and	nut.					
No. of Poles	2way	3 way	4way	- õway	6way	8way	9way	10way	12way
1 pole	44p	44p	44p	44p	44p	44p	44p	44p	44p
2 poles	44p	44p	44p	44p		44p	44p	77p	77p
3 poles	44p	44p	44p	44p	77p			£1.04	
4 poles	44p	44p	44p	77p	77p	77p	77p		\$1·82
5 poles	44p	44p	77p		£1 04			\$1·60	
6 poles	44p	77p	77p	77p	£1.04			\$1.87	
7 poles	77p	77p			£1·82				
8 poles	77p	77p			£1·82				
9 poles	77p				£1.60				
10 poles	77p				£1.60				
11 poles					£1·87		£1·87		
12 poles	-77p -	£1.04	£1·04	\$1.85	£1·87	£1·87	£1·87	£8·52	£3·52

TWENTYLITE

rvvrvrtllE Fluorescent lighting units with polyester choke and finished white enamel. 2ft. model. Ideal kitchen, bedroom, bal-way, porch. lift, etc., with tube. As-sembled ready to install. Price \$2.50 + 25p p. & p.

RADIO STETHOSCOPE

Easiest way to NADIO STELIHOSCOPP Basiest way to Ianit find-traces signal from aerial to speaker-when signal stops you've found the tault. Use it on Radio, TV, amolifar, anything-complete kit comprises two special transistors and all parts including probe tube and crystal carpiece. 82:90-with stethoset instead of carpiece 88p. extra—post and ins. 20p

TANGENTIAL HEATER UNIT This beater unit is the very latest type, most efficient, and quiet running. Is as fitted in Hoover and blower heaters costing £15 and more. We have a few only. Comprises motor, impelier, 2kW, element and 1kW. element allowing switching 1, 2 and 3kW, and with thermai safety cut-out. Can be fitted into any metal line case or cablet. Only needs control switch. **\$2** s8, 2kW. Model as above ercept 2kW. **\$2** 75. Don't miss this. Control 8witch **\$39**, P. & P. 40p.

ROOM THERMOSTAT. Made by the famous Smiths Company. 15 amp. at 250v. Elegant white and beige case, size 4½ inches long by 1½ square approx. Adjustment is by slider (lockable) adjusts through range 30°--90°F. Special Snip price £1.65

CAPACITOR DISCHARGE CAR IGNITION



ELECTRONIC CONTON This system which has proved to be amazingly efficient and reliable was first described in the Wireless World about a year ago. We can supply kit of parts for an improved and even more efficient version (Practical Wireless, June). Price \$6:55 plus 20p post. When ordering please state whether for positive or negative systems. De-luxe model including printed circuit board, etc. \$7:95.

24-HOUR TIME SWITCH

Made by Smiths, these are AO mains operated, NOT CLOCK WORK. Ideal for mounting on rack or shelf or can be built into box with 13A socket. Two com-pietely adjustable time periods per 24 hours, 5A changeover contacts will awitch oircuit on or off during these periods. 52:75 post and ins. 25p. Additional time contacts 55p pair.



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With S kits or more we give FREE an accurate 11 piece balance kit. Price of kits 44p each post paid. Special price for all 7 kits \$5.00 with free balance

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KA2 Lens Kit. Eleven parts, concave lens, one convex lens, stage and slit frame, etc. KA3 Water Pump Kit. Thirteen parts. Trans-

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KA7 Electro-Magnet Kit. Fifteen parts, includes compass, showing how magnetism works.
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 KA9 Beil Kit. Eight parts, including bell and push button switch. Build a complete electric bell.
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NEW ITEMS THIS MONTH

White Rocker Switches. Four types available, all snap in fixing through oblong hole approx. $1^{\sigma} \times a_{1}^{\sigma}$, all rated at 10 a mps AC. All have white rocker except 83, which is amber. Our ref RS 81, push to make, spring return, 149.

on, 14p. Our ref RS 83, change over contacts, luminous

Our ref RS 83, change over contacts, luminous rocker, 28p. Our ref RS 84, change over contacts, normal rocker, 16p.

Rocker Switches. 15 amp Britinac panel mount-ing, hole size $l_{\frac{1}{2}} \times \frac{1}{2}$. Our ref RS S5 price 11p each. 5 amps made by Mem, their type ref 1600, our ref RS S6, price 11p each.

Miniature Hand Microphone. Dynamic, for tape recorders but equally suitable for amplifiers, good quality with lead and plug, price \$1.87.

Quality with least and plug, plue at or. Open Coll Relays. All with 10 amp change over contacts, all brand new. Our ref REL 81, 12 voit DC coll, double pole, 44p. Our ref REL 83, 210 voit AC coll, treble pole, 45p. Our ref REL 83, 250 voit AC coll, treble pole, 45p. Our ref RELES, 200 VOI AU COIL, trêblé pole, 509. Photo Transistor Bargain. First class maker but alightly reject, covered, however, by our normal six month guarantee, these respond to light or infra red. Will work a burgiar alarm system, make detector counter etc. Price 229 complete with three circuits.

Mains Flex. Padded, circular, cotton covered overall. Six amp (23-36) 100 yard coils. Price \$2.75 plus 50p post.

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Screened Cable. 70076 core suitable for pick up g or mike lead or for inter-connecting amplifiers.
10 metres, 33p.
Stereo Fre-amp Module. Mullard ref LP 7182/2—transistors and all ancillary components mounted on PC board, \$1.82 with connection dig.

GOOD COMPANION I.C. VERSION



We can now offer these again we can now oner these again in I.C. version using Ferranti ZN414 and Mullard AF Module 1172. Cabinet size approx.11" wide × 8" high × 3" deep. Complete assembly instruction. Excellent tone wood cabinet, **25**.75 plus 25p net and insurance. post and insurance

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MOTORS FOR £1-50 As used in racing cars and power models. All battery operated and reversible. RESISTANCE WIRE

RESISTANCE WIRE

RESISTANCE WIRE Mainly Nickel Chrome. (Resistances 74 ohms per metre down to 1 ohm per metre). Price 159 per os. on cach weight recla-so please send an open cheque-we will send the smallest reel over the quantity you want and make your cheque out for the quantity sent. You return the "over" amount within 1 month and we will return for the amount you return. 269 returnable charge for reel.

Special Offer. 1 yard of 1.1mm wire. This is almost exactly 1 ohm. 10p.

PC BOARD MARKER

Valve action fret tipped marking pen filled with black etch resist—it's easy with this to make a perfect PC board, just draw straight on to the copper—allow 15 mins. to dry, then immerse in ferree chioride or other etchant on removal the circuit stands in high relief, 990.

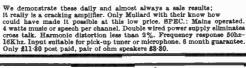
SILGED. Picesers IC, three wat amplifier which works with the Ferranti ZN414 to become prob-ably the first two IC radio in existence, the circuit and constructional details appeared in September's *Practical Wirsless*, so we can supply the SILOSD at \$1.75, the ZN414 at \$1.85 also most other items, send for PW IC radio parts list.

EDUCATIONAL KITS-all with pictorial instructions

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787



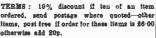
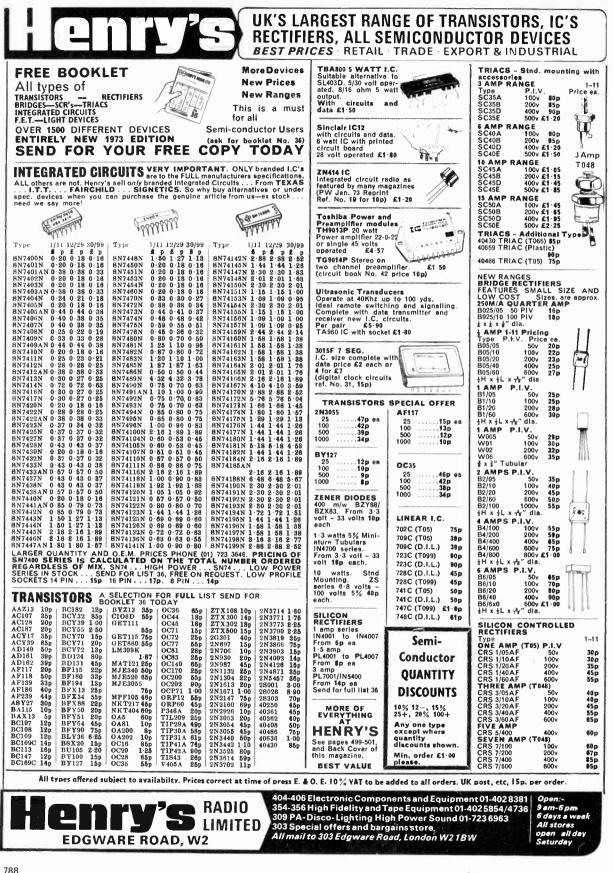






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HENELEC Stereo Buil HOWLAND WEST	t 24-9 DA1000T 25-3	5 Philips	RF839 GF829		39·9 47·7
PIONEER T) ROTEL RI		5 Philips	GF815 GF808		65 · 7 96 · 7
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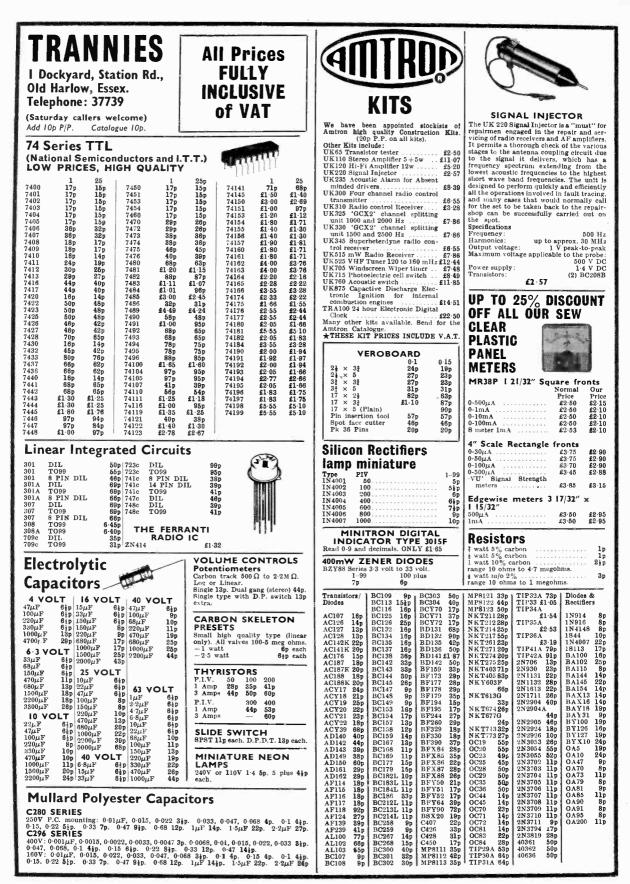
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DL94 45p EF37A 85p PCC89 45 DL96 40p EF40 62p PCC189 49	OA202 10p OC83 B 15p 2N1307 25p AC128 20p BU100 21 80 BD988 48p 5K7G 17p 30C10 70p 9003 OA202 10p OC84 25p 2N2147 64p AC176 20p BYZ13 25p V405A 40p 6K8GT 40p 30C17 85p 9004	
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EBP80 86p EL95 86p PCL86 43 EBF83 40p EL500 76p PFL200 60	QQVO3-10 UBF80 355 VR150/30 355 3V4 455 6AK8 305 6BG6G 475 6Y6G 755 75 505 6097 21-10 UBF89 345 2800U \$1-40 5B254M \$275 6AL5 185 6BJ6 455 6-30L2 855 76 555	£16-00
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500*(10) (50) (20, 1K, 1K5, 2K2, 3K3, 4K7, 6K8, 100; 100; 100; 100; 100; 100; 100; 100	PRESET SKELETON POTENTIONETERS MINIATURE 0.25W Vertical or horizontal 6p each 1K, 2K2, 4K7, 10K, et up to 1 M Ω SUB-MIN 0.05W Vertical, 100 Ω to 220K Ω 5p each (P.W.) 61 CHEDDINGTON ROAD, PITSTON
Miniature Mullard Electrolytics VEROBOARD 0.1 1 0μF 63V 6p 68μF 16V 6p 24 ± 5 th 26p 1 5μF 63V 6p 68μF 16V 6p 24 ± 5 th 26p 2 μF 63V 6p 68μF 16V 6p 24 ± 5 th 26p 3 μF 63V 6p 10μF 90μF 34 ± 5 th 32p 32p 3 μF 63V 6p 100μF 25V 6p 34 ± 5 th 32p 32	POTENTIOMETERS Carbon Track 5K 0 to 2M 0, log or lin. Single, 164p Dual Gang 46p. Log Single with switch 26p Big Carbon Track 5K 0 to 2M 0, log or lin. Single, 164p Dual Gang 46p. Log Single with switch 26p Big DiODES PLUGS DiODES PLUGS EleCTROLYTIC CAPACITORS. Tubular & Large Ca DiODES DIN 2 Pin 12p Z2/63, 457, 100/1, 500/10, 100/10, 100/25, 50/25, 10/50, 3p. 100/0, 20/27, 100/50, 9p. 1000/10, 100/25, 50/25, 10/50, 3p. 1000/10, 100/25, 50/25, 14p. 16/350, 14p. 32/3
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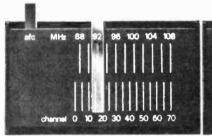
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Fun With HI-FI

In this book Gilbert Davey defines exactly what high fidelity sound is. He describes the different links in the hi-fi system-the playing deck, cartridge, tuner, amplifier, loudspeaker and loudspeaker assemblyand the part each plays in the reproduction of hi-fi sound. He tells the reader what kind of equipment is available today, and concludes with the latest developments in stereo headphones and four-track stereo-'quadraphonic sound'. Fully illustrated, £1.15.

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now... Project 80 ... exciting new thinking in modular hi-fi design

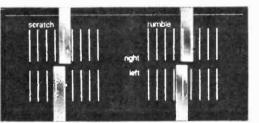


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Project 80 tuner

Stereo 80 pre-amplifier/control unit



r Stereo decoder

Project 80 Active Filter Unit (AFU)

the slimmest, most elegant hi-fi modules ever made



Living with hi-fi takes on new meaning now that Project 80 is here. These amazing new modules mark a brilliant technical advance all round; their size and presentation bring exciting new opportunities to install systems in ways hitherto only dreamed about but never before made practical. You can build a Project 80 system virtually anywhere and it is unbellevably simple to install and connect up. Everything that could possibly be wanted in a top quality do-it-yourself domestic hi-fi system will be found in Project 80 - compactness, elegantly ultra-modern styling, ease of fixing and operation, new control methods, and above all superb performance. New as well as popular established ideas on installation are featured on page four of this announcement to provide just a few examples of the system's fantastic versatility.



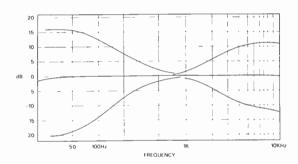
Project 80 new modules

Stereo 80 pre-amplifier and control unit

As with other Project 80 units, the Stereo 80 is mounted by means of two bolts fixed at the rear which pass through holes drilled in the wood or plastic on which modules are to be mounted. All the electronics are contained within the 3 deep front panel ! Connecting leads are taken away similarly out of sight Each channel in the Stereo 80 has its own independent tone and volume controls operated by sliders. This enables exceptionally good environmental matching to be obtained. Provision is made for magnetic and ceramic pick-ups, radio and tape in and out A virtual earth input stage forms part of the up-dated circuitry of the Stereo 80 to ensure the finest possible quality from all signal sources. Generous overload margins are allowed on all inputs. Clear instructions with template are supplied

TECHNICAL SPECIFICATIONS Size $-260 \cdot 50 \cdot 20mm (10\frac{1}{3} \times 2 \cdot \frac{1}{3} \ln s)$ Finish - Black, with white markings Inputs - Mag. P.U. 3mV RIAA corrected; Ceramic P.U. 300 mV Radio 300 mV; Tape 30 mV S/N ratio - 60db Frequency range -20Hz to $15KHz \pm 1dB$ 10Hz to $25KHz \pm 3dB$ Power requirements -20 to 35 volts Outputs -100mV + AB monitoring for tape Controls - Press button for tape, radio and P.U. selection Volume. Bass +12dB to -14dB at 100Hz, Treble+11dB to -12dB at 10KHz

For P.U., radio and tape • For P.U., radio and tape • Tape monitoring switch • Two-hole fixing B R P £11.95 - £119 VAT

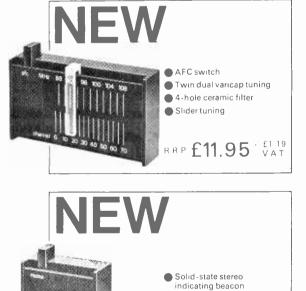


Project 80 FM tuner smaller, more efficient

A truly remarkable tuner in every way – its unbelievably compact size – its original circuitry – its dependable performance – all this in a boldly designed modern case measuring $85 \times 50 \times 20$ mm ($3\frac{1}{2} \times 2 \times \frac{1}{3}$ ins). Greater adaptability (and possibly financial convenience) results from the tuner and stereo decoder section being made available separately.

TECHNICAL SPECIFICATIONS

Size = 85 + 50 + 20mm (approx. $3\frac{1}{2} + 2 + \frac{3}{2}$ ins) Tuning range = 87 to 108 MHz Detector = 1 C balanced coincidence, for good A M rejection AFC = Switchable, with thermistor control to prevent from drift One 26 transistor LC. Twin dual varicap tuning Distortion = 0.3% at 1 KHz for 75KHz deviation Ceramic filter in LF. section Aerial impedance = 75 Ω or 240-300 Ω Sensitivity = 4 microvolts for 30dB quieting Power requirements = 12 to 45 volts



Readily adaptable

for use with other tuners

R R.P £7.45 + 0.74p

Project 80 stereo decoder

Making the Project 80 decoder separate from the F.M. tunor gives the constructor a wider choice of systems as well as saving money in cases where stereo reception may not be required. This unit gives a 40dB channel separation with an output of 150mV per channel. The gallium arsenide light emitting beacon automatically lights up to show when a stereo transmission is tuned in. Designed essentially as an integral part of Project 80 systems, this multiplex stereo demodulator may be used in many cases with existing single channel frequency modulated tuners to provide stereo reception.

Size -- 47 · 50 · 20mm (1 2 · 2 · 3ins) One 19 transistor I.C.

new constructional techniques

...and again Sinclair leads the world

- 1962 Micro-miniature power amp small enough to stand on a 10p, piece. Slimline pocket receiver smaller than a 20 cigarette pack
- 1963 Micro-6 receiver, smaller than a matchhox
- 1964 Pocket F.M. receiver, PWM amp.
- 1965 Z.12 power amplifier module; PZ.3 power supply
- 1966 Stereo 25 pre-amp/control unit
- 1967 Micromatic Q.14 loudspeaker; the first Neoteric
- 1968 IC.10, the first ever integrated circuit for constructors use

Project 80 active filter unit

This efficiently designed unit makes a highly desirable part of any worthwhile system where inputs may be from record, radio or tape. As with Stereo 80, separate controls are applied to each channel thereby making it easier to obtain ideal stereo balance in any kind of indoor environment.

 $\label{eq:constraints} \begin{array}{c|c} \textbf{TECHNICAL SPECIFICATIONS} \\ \textbf{Size} & -108 \cdot 50 \cdot 20mm (4 \downarrow \cdot 2 \cdot 1)ns) \\ \textbf{Voltage gain} & -minus 0.2dB \\ \textbf{Frequency response} & -36Hz to 22KHz, controls minimum \\ \textbf{Distortion} & -at 1 KHz - 0.03\% using 30V supply \\ \textbf{HF cut off} (scratch) & -22KHz to 55KHz, 12dB/oct slope \\ \textbf{L.F. cut off (rumble)} & -28dB at 20Hz, 9dB/oct, slope \\ \end{array}$

Z.40 & Z.60 power amplifiers totally short-circuit proof

Either of these entirely new power amplifiers is intended for use in Project 80 installations although, of course, they are readily adaptable to an even wider range of applications. Both 2.40 and 2.60 incorporate builtin protection against shortcircuiting and risk of damage arising from mis-use is greatly reduced. Comprehensive instructions are supplied with each of the modules.

Z.40 Technical Specifications Size $-55 \cdot 80 \cdot 20$ mm (2 $\frac{1}{2} \cdot 3\frac{1}{3} \cdot 3$) so y transistors Input sensitivity -100 mV Output -15 watts RMS continuous into 8 Ω (35V). 30 watts music power into 4 Ω (30V) Frequency response -10Hz-100KHz ± 1 dB Signal to noise ratio -64dB Distortion -a110 watts into 8 Ω less than 0 1% Power requirements -12-35 volts Z 60 Technical Specifications Size - 55 · 98 · 20mm (2월 · 3월 · 월ins) 12 transistors Input sensitivity - 100-250mV Output - 25 watts RMS into 8 Ω (45V). 50 watts music power into 4 Ω (50V) Distortion - typically 0 03% Frequency response - 10Hz to more than 200KHz |-1dB Signal to noise ratio - better than 70dB Built-in protection against transient overload and short circuit Load impedance - 40min; max. safe on open circuit

Sinclair power supply units PZ.8

the worlds most advanced unit in its class

Stabilised power supply unit Reentrant current limiting makes damage from overload or even direct shorting impossible, a principle never before inorporated in a commercially available constructor module. Normal working voltage (adjus table) 45V R P. £7.98+0.79p V.A.T

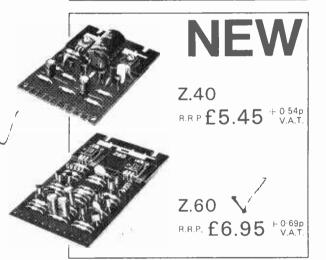
R R P. £7.98 + 0 79p V.A T Without mains transformer PZ.5 30V unstabilised R.R.P. £4.98 + 0.49p V.A T PZ.6 35V. stabilised R.R.P. £7.98 + 0 79p V.A.T



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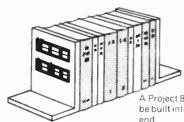
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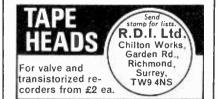
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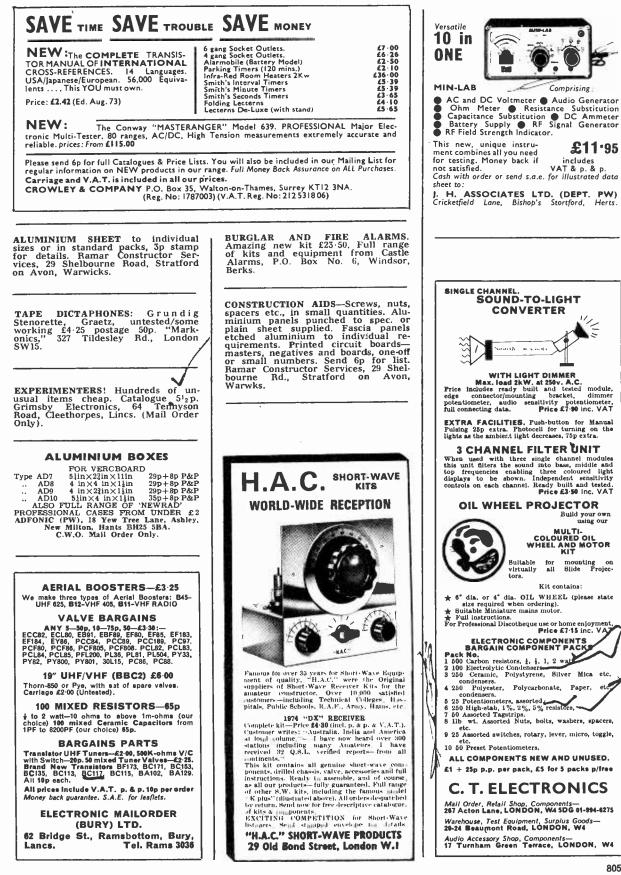
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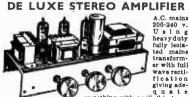


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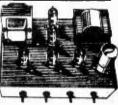


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