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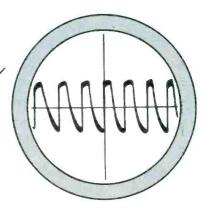
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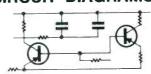
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VOL. 49 NO. 1 ISSUE 795 MAY 1973

BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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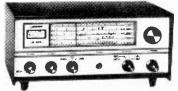
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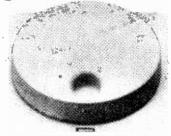
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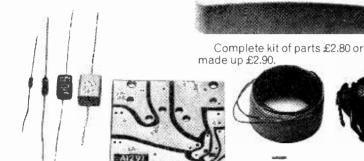
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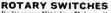
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1.0						7p		2 p
2.2					7p	-	7p	7p 7p
4-7			_	7p		7p	7p	7p
10			\ 7p	_	7p	7p	7p	7p
22	_		7p	2p	_	7p	7p	8р
47	7p	_	7p	7p	7p	7p	8p	12p
100	7p	7p	7p	7p	7p	8p	12p	18p
220 470	7p 7p	7p	7p	8p	9p	10p	17p	26p
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4700	28p	26p	37p	40p	SOP	40p		
10,000	87p	40p	0.0	109				

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250V up to 0.1µF: 100V/0.1µF and above.
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c	1/8W	5%	4-7 Ω-470Κ Ω
Ċ	1/4W	10%	4-7 Ω-10M Ω
C	1/2W	5%	4·7 Ω-10M Ω
C	1W	10%	4-7 Ω-10M Ω
MO	1/2W	2%	10 Ω-1 Μ Ω
WW	1W	$10\% \pm 1/20 \Omega$	0-22 Ω-3-9 Ω
ww	3W	5%	1 Ω-10 Κ Ω
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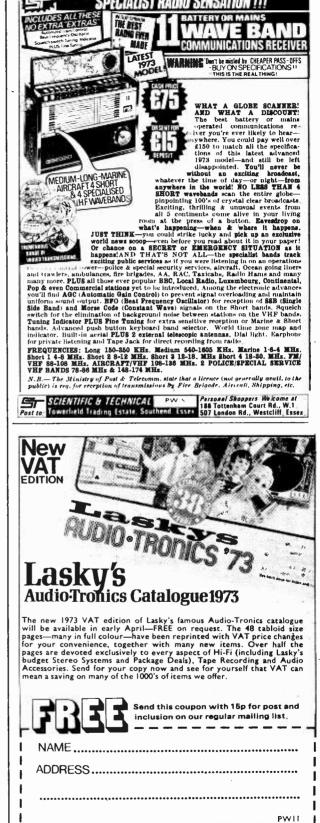
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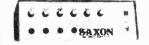
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OM800A Pow. amp	š	p. Price	135 95
RANK ROTEL 210		38 - 39	
RAVE ROTEL 210. RANK ROTEL 310. RANK ROTEL 310. RANK ROTEL 610. RANK ROTEL RA 810. RANK ROTEL RA 1210 ROGERS Ravensbourne Ravensbourne (cased) Ravensbrook Mk. II. Ravensbrook (cased) Mk. II. SINCL AIR 2000	::	57·20 86·35	39 95 56 95
RANK ROTEL RA 810	• •	116 · 05	83 · 50 101 · 95
ROGERS Ravensbourne		77·00 82·50 57·75	59 · 50 64 · 95
Ravensbourne (cased)		57 - 75	44 95
Ravensbrook (cased) Mk. II		63 · 25 38 · 50	48 50 27 75
SINCLAIR 2000		49 · 50 32 · 95	34 - 95 23 - 75
3000PROJECT 605 SOLARVOX 20. 10 watts RMS r	er		
COLADVOV 20 15 watta PMS	205	43-95	
channel	tte	51 · 65	35 · 95
RMS plus MATRIX 4 channel		42 - 30	29 · 75
plus MATRIX 4 channel	us	56 · 52	42 - 95
TANDBERG TA300		76 · 89 87 · 45	59·95 72·50
WHARFEDALE Linton amplifier Amplifiers listed all take both cer	r	71 - 50	50 95
cartridges.	antil	. u./u ill	
TUNERS AKAI AT550 AM/FM/MPX/FET		84 · 10	61 - 95
AKAI AT580 AM/FM/MPX/MC)5.	424 00	96 - 95
FET AMSTRAD Multiplex 300 FM ARMSTRONG M8 Decoder *DULC! FMT 7 FM JVC Nivico MCT V5E/VT500 AN MCT V7E AM/FM. LEAK Delta FM		131·09 37·55	26-95
*DULC! FMT 7 FM		10·45 22·96	7·75 14·90
JVC Nivico MCT V5E/VT500 AN	//FN	1 80 96	62 · 95 94 · 95
LEAK Delta FM			52 95
LEAK Delta FMLEAK Delta AM/FM		83 · 79 51 · 70	62 · 25 36 · 95
PHILIPS RH 690		45·66 102·61	33 · 50 78 · 80
METROSOUND FMS 20. PHILIPS RH 691. PIONEER TX500A AM/FM PIONEER TX500 AM/FM. RANK ROTEL 320. RANK ROTEL 620. RANK ROTEL 620. RANK ROTEL 620. SIGNEAR Ravensbourne in Teak Ravensbrook (cased) SINCLAIR 2000.		72 - 47	48 · 95 68 · 95
RANK ROTEL 320		55.91	20.05
RANK ROTEL 620	Cas	87·86 e 61·05	
Ravensbrook (cased)		46 · 75 42 · 44	34 · 95 28 · 95
SINCLAIR 2000		42 44 23 57	28 95 16 95
Project 60 Tuner (stereo) All Tuners listed are complets	 wi	23-57 th MPX	16·95 Stereo
All Tuners listed are complete Decoder except where starred.			
TUNER/AMPLIFIERS AKAI CR80T AM/FM Tuner Am	pli-		
fier with built in Eight Track To Recorder	ape	140 · 78	84-95
AKAI AA8030		131 · 09 178 · 07	96 · 95 131 · 95
AKAI AS8100S Quadraphonic.		243 - 85	181 - 95
fier with built in Eight Track T. Recorder AKAI AA8030. AKAI AA8080. AKAI AS8100S Quadraphonic. AKAI AA8500. AKAI 6300. ARAI 6300.		235 97 130 31	166 · 95 74 · 95
ARENA 2600		104 · 62 10 · 45	55·95 7·75
ARENA 2600 ARMSTRONG M8 Decoder ARMSTRONG 525ARMSTRONG 526		84 - 96	66 50
		96 · 81 87 · 55	66 · 95
Module 80 Compact		158 · 16 112 · 04	119 95 85 95
Module 110 FM/MW/LW/S	w/		
100w. RMS		130 · 86 230 · 65	99·95 175·95
	-		

These prices are effective April 1st, 1973 and are calculated assuming a V.A.T. rate of 10%. Should the V.A.T. rate differ, please check prices before ordering.

Rec	. Retail	Comet
	Price	Price
TUNERS/AMPLIFIERS—continued	1 £ p	£ p 124⋅95
JVC Nivico 4MM 1000 Quadraphonic JVC Nivico VR 550/5501 AM/FM	149.93	75.95
JVC Nivico VR 550/5501 AM/FM VR 5521L AM/FM and SEA	164 - 74	135-95
VR 5521L AM/FM and SEA	211 - 82	176 - 95
4VR 5414 Quadraphonic KYOTO 1000 AM/FM Tuner/Ampli-	211.02	110.93
KYOTO 1000 AM/FM Tuner/Ampli-		
fier with built in Stereo Cassette		
Recorder. Complete with two	79 - 90	57 - 95
speakers and two microphones	163 83	123 95
CHILDE DU 700	202 · 41	154 95
LEAK Delta 75 PHILIPS RH 720 PIONEER SX525	134 - 86	92.95
CYCOC SAS23	184 - 72	126 - 95
\$X626	222 - 39	152 - 95
SX727 SX828	285-21	196 - 95
3 x 020	216 - 81	150 95
OX 9000 Quadraphonic	274 - 69	190 - 95
QX 4000 Quadraphonic QX 8000 Quadraphonic ROTEL RX 150A	65 - 68	47 95
ROTEL RX 150A ROTEL RX 400A ROTEL RX 600A ROTEL RX 800A ROTEL RX 154A Quadraphonic	84 · 10	61 - 95
ROTEL RY 400 A	101 - 12	74 - 95
POTEL BY 600A	140 01	103-95
ROTEL BY 800A	178 07	131 - 95
POTEL RY 154A Quadranhonic	121 - 68	89 95
SOLARVOY TAM 1105 2 x 5 watts		
SOLARVOX TAM 1105 2 x 5 watts RMS AM/FM Multiplex comp.		
with 0 cooplers and featuring		
Matrix 4 channel	36 · 28	28 · 95
TANDRERG TR200 MPX	99 - 79	83.95
TANDRERG TRIONO EM MPX (teak)	146 - 86	124 95
TANDRERG TRIGIO AM/FM MPX	159 09	133 - 95
TELETON CR55	118 - 06	64 - 95
What 2 speaned ANDBERG TRI000 MPX TANDBERG TRI000 FM MPX (teak) TANDBERG TRI010 AM/FM MPX TELETON CR85 TELETON CR85 TELETON CR85 WHARFEDALE LINTON WE40 WHARFEDALE LINTON WE40	39 - 74	20.95
WHARFEDALE LINTON WE40	107 - 66	81 - 95
All Tuner/Amplifiers listed take mag	netic car	tridaes
except Teleton R8000 and Kvoto 1	000 whi	ch take
	a Dagge	tor with
ceramic only. All include MPX Stere	O Decou	
All Tuner/Amplifiers listed take mag except Teleton R8000 and Kyoto 1 ceramic only. All include MPX Stere	M8 dec	oder is
the exception of Armstrong where	M8 dec	oder is
the exception of Armstrong where extra.	M8 dec	oder is
the exception of Armstrong where extra.	wa dec	oder is
the exception of Armstrong where extra.	12·65	10·50
the exception of Armstrong where extra.	12 · 65 31 · 02	10·50 24·95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2	12·65 31·02 39·16	10·50 24·95 32·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARPARD SP25 Mk. ii	12 · 65 31 · 02 39 · 16 15 · 25	10·50 24·95 32·25 9·75
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARPARD SP25 Mk. ii	12·65 31·02 39·16 15·25 12·85	10·50 24·95 32·25 9·75 9·50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis CONNOISSEUR BD2 P/C/SAU2 GARPARD SP25 Mk. ii	12·65 31·02 39·16 15·25 12·85 18·78	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. GARRARD SP25 Mk. ii GARRARD 40B GARRARD 5L55B. GARRARD SL55B.	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. GARRARD SP25 Mk. ii GARRARD 40B GARRARD 5L55B. GARRARD SL55B.	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43	10·50 24·95 32·25 9·75 9·50 12·95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD 5155B. GARRARD 5175B.	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73	10·50 24·95 32·25 9·75 9·50 12·95 30·60 27·50 20·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD 5155B. GARRARD 5175B.	12·65 31·02 39·16 15·25 12·85 18·78 46·40 40·43 30·73 26·82	10·50 24·95 32·25 9·50 12·95 30·60 27·50 20·25 16·95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD 5155B. GARRARD 5175B.	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57	10·50 24·95 32·25 9·75 9·50 12·95 30·60 27·50 20·25 16·95 37·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. ii GARRARD 40B GARRARD 5L65B GARRARD SL65B GARRARD SL65B GARRARD SL72B GARRARD SL72B GARRARD AP76 GARRARD AP76 GARRARD Zero 100S	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44	10·50 24·95 32·25 9·75 9·50 12·95 30·60 27·50 20·25 16·95 37·25 34·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. il GARRARD 40B. GARRARD SL55B. GARRARD SL55B. GARRARD SL55B. GARRARD SL75B. GARRARD SL75B. GARRARD SL72B. GARRARD AP76. GARRARD Zero 100A. GARRARD Zero 100A. GARRARD Zero 100A. GOLDRING G101P/C.	12·65 31·02 39·16 15·25 12·85 18·78 46·40 40·43 30·73 26·82 51·57 47·44	10·50 24·95 32·25 9·75 9·50 12·95 30·60 27·50 20·25 16·95 37·25 34·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 40B GARRARD SL55B GARRARD SL55B GARRARD 501 GARR	12.65 31.02 39.16 15.25 12.85 18.78 46.40 40.43 30.73 26.82 51.57 47.44 28.05 29.70	10·50 24·95 32·25 9·75 9·50 12·95 30·60 27·50 20·25 16·95 37·25 34·25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. il GARRARD SB58. GARRARD SB58. GARRARD SL958. GARRARD SL958. GARRARD SL958. GARRARD SL728. GARRARD SB58. GARRARD GB58. GOLDRING GB58. GOLDRING GB58. GOLDRING GB58.	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60 27 · 50 20 · 25 16 · 95 37 · 25 34 · 25 19 · 50 20 · 25
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. il GARRARD SB58. GARRARD SB58. GARRARD SL958. GARRARD SL958. GARRARD SL958. GARRARD SL728. GARRARD SB58. GARRARD GB58. GOLDRING GB58. GOLDRING GB58. GOLDRING GB58.	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 12 · 95 30 · 60 27 · 50 16 · 95 37 · 25 16 · 95 37 · 25 19 · 50 20 · 25 26 · 50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. ii GARRARD 40B GARRARD 540B GARRAR	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61 39 · 60 48 · 84	10 · 50 24 · 95 32 · 25 9 · 75 9 · 75 12 · 95 30 · 60 27 · 50 20 · 25 16 · 95 37 · 25 34 · 25 19 · 50 20 · 26 · 50 26 · 50 33 · 50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. ii GARRARD 40B GARRARD 540B GARRAR	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61 39 · 60 48 · 84 82 · 54	10 · 50 24 · 95 32 · 25 9 · 75 12 · 95 30 · 60 27 · 50 20 · 25 34 · 25 19 · 50 20 · 25 34 · 25 35 · 50 20 · 25 56 · 50 33 · 50 55 · 55
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. ii GARRARD 40B GARRARD 540B GARRAR	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61 39 · 60 48 · 84	10 · 50 24 · 95 32 · 25 9 · 75 9 · 75 12 · 95 30 · 60 27 · 50 20 · 25 16 · 95 37 · 25 34 · 25 19 · 50 20 · 26 · 50 26 · 50 33 · 50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. II GARRARD 40B. GARRARD 5L95B. GARRARD SL95B. GARRARD SL95B. GARRARD SL95B. GARRARD SL75B. GARRARD SL72B. GARRARD SL72B. GARRARD ZETO 100A. GARRARD ZETO 100A. GARRARD ZETO 100A. GOLDRING G101P/C GOLDRING G172P GOLDRING G172P GOLDRING G175P GOLDRING G175P GOLDRING GL85P/Cover LEAK Delta. JVC Nivico SRP 473 Quadraphonic,	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 38 · 61 39 · 60 48 · 84 82 · 50 65 · 07	10 · 50 24 · 95 32 · 25 9 · 50 12 · 95 30 · 60 27 · 50 20 · 25 16 · 95 37 · 25 19 · 50 20 · 25 19 · 50 20 · 25 34 · 25 19 · 50 20 · 25 33 · 34 25 · 50 26 · 50 33 · 50 49 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. ii GARRARD 40B. GARRARD 40B. GARRARD SL65B. GARRARD SL65B. GARRARD SL72B. GARRARD SL72B. GARRARD SL72B. GARRARD Zero 100A. GARRARD ZERO 100	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 518 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 65 · 07 65 · 88	10 · 50 24 · 95 32 · 25 9 · 50 12 · 95 9 · 50 12 · 95 30 · 60 27 · 50 16 · 95 37 · 25 16 · 50 20 · 25 34 · 25 19 · 50 20 · 25 56 · 50 26 · 50 27 · 50 33 · 50 55 · 50 49 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. ii GARRARD 40B. GARRARD 40B. GARRARD SL65B. GARRARD SL65B. GARRARD SL72B. GARRARD SL72B. GARRARD SL72B. GARRARD Zero 100A. GARRARD ZERO 100	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 518 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 65 · 07 65 · 88	10 · 50 24 · 95 32 · 25 9 · 50 12 · 95 9 · 50 12 · 95 30 · 60 27 · 50 16 · 95 37 · 25 16 · 50 20 · 25 34 · 25 19 · 50 20 · 25 56 · 50 26 · 50 27 · 50 33 · 50 55 · 50 49 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. ii GARRARD 40B. GARRARD 40B. GARRARD SL65B. GARRARD SL65B. GARRARD SL72B. GARRARD SL72B. GARRARD SL72B. GARRARD Zero 100A. GARRARD ZERO 100	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 518 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 65 · 07 65 · 88	10 · 50 24 · 95 32 · 25 9 · 50 12 · 95 9 · 50 12 · 95 30 · 60 27 · 50 16 · 95 37 · 25 16 · 50 20 · 25 34 · 25 19 · 50 20 · 25 56 · 50 26 · 50 27 · 50 33 · 50 55 · 50 49 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. ii GARRARD 40B. GARRARD 40B. GARRARD SL65B. GARRARD SL65B. GARRARD SL72B. GARRARD SL72B. GARRARD SL72B. GARRARD Zero 100A. GARRARD ZERO 100	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 518 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 65 · 07 65 · 88	10 · 50 24 · 95 32 · 25 9 · 50 12 · 95 9 · 50 12 · 95 30 · 60 27 · 50 16 · 95 37 · 25 16 · 50 20 · 25 26 · 50 20 · 25 55 · 50 49 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. ii GARRARD 40B. GARRARD 40B. GARRARD SL65B. GARRARD SL65B. GARRARD SL72B. GARRARD SL72B. GARRARD SL72B. GARRARD Zero 100A. GARRARD ZERO 100	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 518 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 65 · 07 65 · 88	10 · 50 24 · 95 32 · 25 9 · 50 12 · 95 9 · 50 12 · 95 30 · 60 27 · 50 16 · 95 37 · 25 16 · 50 20 · 25 26 · 50 20 · 25 55 · 50 49 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. ii GARRARD 40B. GARRARD 40B. GARRARD SL65B. GARRARD SL65B. GARRARD SL72B. GARRARD SL72B. GARRARD SL72B. GARRARD Zero 100A. GARRARD ZERO 100	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 518 · 78 46 · 40 40 · 43 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 65 · 07 65 · 88	10 · 50 24 · 95 32 · 25 9 · 50 12 · 95 9 · 50 12 · 95 30 · 60 27 · 50 16 · 95 37 · 25 16 · 50 20 · 25 26 · 50 20 · 25 55 · 50 49 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. ii GARRARD 40B GARRARD 540B GARRAR	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 33 · 61 39 · 60 48 · 84 82 · 50 65 · 07 65 · 88 13 · 96 65 · 07 67 · 89 17 · 71 19 · 49 64 · 95 er 47 · 19	10 · 50 24 · 95 32 · 25 33 · 50 9 . 5
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. ii GARRARD 40B GARRARD 540B GARRAR	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 12 · 85 · 18 · 78 · 46 · 40 · 40 · 43 · 30 · 73 · 26 · 82 · 51 · 57 · 47 · 44 · 42 · 8 · 05 · 65 · 07 · 65 · 88 · 13 · 96 · 17 · 71 · 19 · 49 · 95 · 64 · 17 · 71 · 19 · 49 · 95 · 64 · 77 · 53 · 77 · 50	10 · 50 24 · 95 32 · 25 9 · 75
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 P/C/SAU2 GARRARD SP25 Mk. ii GARRARD 40B GARRARD 540B GARRAR	12 · 65 31 · 02 39 · 16 15 · 25 12 · 85 18 · 78 46 · 40 30 · 73 26 · 82 51 · 57 47 · 44 28 · 05 29 · 70 33 · 61 39 · 60 48 · 84 82 · 50 65 · 07 65 · 88 13 · 96 65 · 07 67 · 89 17 · 71 19 · 49 64 · 95 er 47 · 19	10 · 50 24 · 95 32 · 25 33 · 50 9 . 5
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD3 Chassis. GARRARD SU595 GARRARD 401 GARRARD SU595 GARRARD ZETO 100A GOLDRING GU17C GOLDRING	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 12 · 85 · 18 · 78 · 46 · 40 · 40 · 30 · 73 · 26 · 82 · 51 · 57 · 47 · 44 · 42 · 05 · 29 · 70 · 38 · 61 · 39 · 60 · 48 · 84 · 82 · 50 · 65 · 07 · 117 · 11 · 19 · 49 · 65 · 07 · 170 · 53 · 70 · 109 · 04	10 · 50 24 · 95 32 · 25 9 · 77 · 95
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD3 Chassis. GARRARD SU595 GARRARD 401 GARRARD SU595 GARRARD ZETO 100A GOLDRING GU17C GOLDRING	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 12 · 85 · 18 · 78 · 46 · 40 · 40 · 43 · 30 · 73 · 26 · 82 · 51 · 57 · 47 · 44 · 42 · 8 · 05 · 65 · 07 · 65 · 88 · 13 · 96 · 17 · 71 · 19 · 49 · 95 · 64 · 17 · 71 · 19 · 49 · 95 · 64 · 77 · 53 · 77 · 50	10 · 50 24 · 95 32 · 25 9 · 75
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 CP/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 5495B GARRARD 5495	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 18 · 78 · 46 · 40 · 40 · 43 · 30 · 73 · 26 · 82 · 51 · 57 · 74 · 44 · 28 · 05 · 29 · 70 · 38 · 61 · 39 · 60 · 48 · 84 · 82 · 65 · 07 · 65 · 88 · 13 · 96 · 17 · 71 · 19 · 49 · 17 · 53 · 77 · 00 · 109 · 04 · 116 · 05	10 · 50 24 · 95 32 · 25 9 · 75 9 · 75 9 · 75 9 · 75 30 · 60 27 · 50 20 · 25 37 · 25 26 · 50 26 · 50 49 · 95 52 · 95 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 17 · 95 95 · 50
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Kit CONNOISSEUR BD2 CP/C/SAU2 GARRARD SP25 Mk. II GARRARD 40B GARRARD 5495B GARRARD 5495	12 · 65 · 31 · 02 · 39 · 16 · 16 · 15 · 25 · 12 · 85 · 18 · 78 · 46 · 40 · 43 · 30 · 73 · 326 · 82 · 51 · 57 · 47 · 44 · 28 · 05 · 65 · 04 · 48 · 25 · 65 · 07 · 65 · 88 · 13 · 96 · 49 · 56 · 67 · 77 · 00 · 109 · 04 · 116 · 05 · 65 · 04	10 · 50 24 · 95 32 · 25 9 · 75 9 · 50 0 20 · 25 52 · 55 33 · 50 0 20 · 25 52 · 55 53 · 55 53 ·
the exception of Armstrong where extra. TURNTABLES CONNOISSEUR BD1 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 Chassis. CONNOISSEUR BD2 P/C/SAU2. GARRARD SP25 Mk. II GARRARD 40B. GARRARD 40B. GARRARD SL95B. GARRARD SL95B. GARRARD SL95B. GARRARD SL7B. GARRARD SL7B. GARRARD SL7B. GARRARD SL7B. GARRARD ZETO 100A. GARRARD ZETO 100A. GARRARD ZETO 100A. GARRARD ZETO 100A. GOLDRING GI19/C. GOLDRING GI19/C. GOLDRING GI72P. GOLDRING GI75P. GOLDRING GL75P. GOLDRING GL75P. GOLDRING GL75P. GOLDRING GL75P. GOLDRING GL85P/Cover. LEAK Delta. JVC Nivico SRP 473 Quadraphonic, including plinth and cover. MCDONALD 4P60. MCDONALD 4P10. MCDON	12 · 65 · 31 · 02 · 39 · 16 · 15 · 25 · 18 · 78 · 46 · 40 · 40 · 43 · 30 · 73 · 26 · 82 · 51 · 57 · 74 · 44 · 28 · 05 · 29 · 70 · 38 · 61 · 39 · 60 · 48 · 84 · 82 · 65 · 07 · 65 · 88 · 13 · 96 · 17 · 71 · 19 · 49 · 17 · 53 · 77 · 00 · 109 · 04 · 116 · 05	10 · 50 24 · 95 32 · 25 9 · 75 9 · 75 9 · 75 9 · 75 30 · 60 27 · 50 20 · 25 37 · 25 26 · 50 26 · 50 49 · 95 52 · 95 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 12 · 25 17 · 95 95 · 50

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	(Fig. 1)	
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Earpiece with plug and switched socket for private
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Total building costs PR-50 P. P. 8

Total building costs **£6-58** P. P.&



bands: MW, LW, SW1, SW2, SW3 Trawler, bandplus an extra Medium waveband for tuning easier tuning of Luxembourg etc. Sensitive fer rite rod aerial and telescopic aerial for Short Waves.

Speaker. sin. speaker. of stages—6 transistors and 2 diodes. Attractive black case with red grille, dial and black knobs with polished metal inserts. Size 9 x 5½ x 21n. approx. Easy build plans and parts price list 25p (FREE with parts).

Total building costs £4.38 P. P. & Inc. 31p

POCKET FIVE

3 Tunable Wavebands. MW, LW, Trawler Band with extended M.W. band for easier tuning band for easier tuning of Luxembourg, etc.
7 stages—5 transistors and 2 diodes,
supersensitive ferrite rod acrial, the
tone moving coll speaker. Attractive black and gold
case. Size 5 i × 1 × 3 in. Easy build plans and
parts price list 10p (FREE with parts).

Total building costs £2.50 P.P. & Orrange as P. & P. 65n)

TRANSONA FIVE

5 TRANSISTORS AND 2 DIODES

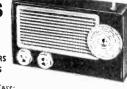


3 Tunable Wavebands: MW, LW and Trawler Band. 7 stage 5 transistors and 2 diodes, ferrite rod aerial. retuning condenser volume control, fine tone moving coil speaker. Attractive case with red speaker grille. Size 6½ × 4½ × 1½in. Easy build plans and parts price list 10p (FREE with parts).

Total building costs £2-75 P. P. &

TRANS EIGHT

8 TRANSISTORS and 3 DIODES



6 Tunable Wave-bands: MW, LW, 8W1, 8W2, SW3 and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves, 3in. Speaker, 8 improved type transiators plus 3 diodes. Attractive case in black with red grille, dial and black knobs with poliahed metal Inserts. Size 9 × 5½ × 2 jin. approx, Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and easy build plans 25p (FREE with parts).

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reference	Type P AC107 AC113 AC115 AC115 AC115 AC1126 AC126 AC126 AC126 AC126 AC134 AC134 AC134 AC134 AC134 AC134 AC136 AC161 AC161 AC161 AC161 AC166 AC166 AC166 AC166 AC166 AC167 AC177 AC188 AC177 AC188 AC179 AC180 AC180 AC180 AC181 AC181 AC181 AC181 AC181	rice p 22 25 22 25 22 25 26 26 27 27 28 28 2	AD162 AD161 & AD162 (MI AD162 (MI AD1140 AF114 AF115 AF116 AF117 AF118 AF124 AF125 AF128 AF128 AF128 AF128 AF128 AF128 AF128 AF128 AF128 AF128 AF128 AF128 AF139 AF130 AF180 A	364 364 360 360 360 360 360 360 360 360	Type P BC145 BC147 BC148 BC148 BC148 BC149 BC150 BC150 BC151 BC152 BC157 BC158 BC157 BC158 BC160 BC160 BC167 BC168 BC167 BC170 BC171 BC172 BC177 BC172 BC177 BC178 BC178 BC178 BC178 BC177 BC178 BC188	rice p 40; 111 11 113 20 222 18; 31 32 20 13 13 20 13 13 20 13 20 21 22 24 21 21 21 21 21 11 11 11 11 13 13 13 13 13 13 13 13 13	Type BD138 BD135 BD136 BD137 BD138 BD140 BD140 BD176 BD177 BD177 BD188 BD177 BD188 BD186 BD186 BD186 BD187 BD188 BD186 BD187 BD188 BD186 BD187 BD188 BD188 BD187 BD188 BD188 BD187 BD188 BD188 BD187 BD188 B	Price p 714 44 44 44 44 44 45 55 66 66 67 77 77 71 47 77 77 71 47 77 77 82 82 83 81 80 10 41 10 26 47 77 77 77 77 77 77 77 77 77 77 77 77	BF182 BF183 BF184 BF185 BF188 BF194 BF195 BF196 BF197 BF200	rice p 444 441 133 444 113 115 115 115 115 115 115 115 115 115	Type P MAT121 MAT121 MAT121 MAT121 MAT121 MAT121 MAT102 MAT121 MAT102 CC19 CC29 CC29 CC29 CC29 CC29 CC29 CC2	21 46 40 40 40 42 42 42 46 42 27 55 55 55 55 55 55 55 55 16 11 15 16 16 16 16 16 16 16 16 16 16	2G308 2G309 2G339A 2G345 2G371B 2G371B 2G3774 2G3774 2G3774 2G3774 2G3774 2G378 2G381 2G38	cice p 38 48 22 17 13 18 17 18 18 17 18 18 17 18 17 18 17 18 18	2N2160 2N2192 2N2193 2N2194 2N2217 2N2218 2N2218 2N2220 2N2220 2N2222 2N2369 2N2369 2N2369 2N23612 2N2411 2N2711 2N2711 2N2711 2N2711 2N2711 2N2906 2N2906 2N2906 2N2906 2N2906 2N2907 2N2907 2N2907 2N2907 2N2907 2N2907 2N2907 2N29097 2N29097 2N29097 2N2923	82 82 83 84 84 85 85 85 85 85 85	2 N 3 0 0 3 2 N 3 0 3 2 N 3 0 3 2 N 3 0 3 2 N 3 0 3 2 N 3 0 3 2 N 3 0 3 2 N 3 0 3 4 2 N 3 0 3 4 N 3 0 3 3 2 N 3 0 3 4 N 3 0 3 4 N 3 0 3 3 2 N 3 0 3 4 N 3 0 3 4 N 3 0 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	ice P 18\(\frac{1}{2}\) 18\(\frac{1}{2}\) 15\(\frac{1}{2}\) 15\(\frac{1}{2}\) 15\(\frac{1}{2}\) 15\(\frac{1}{2}\) 15\(\frac{1}{2}\) 23 31 46\(\frac{1}{2}\) 16\(\frac{1}{2}\) 10 11 12 7\(\frac{1}{2}\) 10 10 10 10 1555 331 31 31 31 333	2N 4059 2N 4060 2N 4061 2N 4061 2N 4061 2N 4061 2N 4081 2N 4285 2N 4286 2N 4286 2N 4286 2N 4286 2N 4286 2N 4281 2N 428	rice p 113 13 13 184 184 184 184 184 184 184 184 184 184
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50 0.26							
100 0 28							
200 0 39	0.41	0.54	0.54	0 63	0.67	0.83	1.76
400 0 48							
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800 0 . 70	0.77	0.88	0.88	0.99	$1 \cdot 32$	1.65	4.40

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PIV	300mA	750 mA	1 A	1.5 A	3 A.	10A	30A
50	0 04	0.06	0.06	0.08	0:16	0.23	0.66
100	0.04	0.07	0.06	0.15	0.18	0.26	0.83
200	0.06	0.10	0.07	0.16	0.22	0.27	1.10
400	0.07	0 · 15	0.08	0.22	0.30	0.41	1.38
600	0.08	0.18	0.11	0.26	0.38	0.50	2.05
800	0.11	0.19	0.12	0.28	0.41	0.61	$2 \cdot 20$
1000	0.12	0.28	0.16	0.33	0.51	$0 \cdot 70$	2.75
1200		0.37	-0000	0.42	0.63	0.83	_

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I.C.=10 amps. Ptot=
30W. hfe=30-170.
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0.47; 0.44 0.39;

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also electrically equivalent to 2N2646
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115 WATT SIL POWER NPN

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$\frac{021}{U23}$		MADT's like MHz Series PNP Transistors	0 - 5
U24		Germanium 1 Amp Rectifiers GJM Series up to 300 PIV	0 - 51
U25		300 MHz NPN Bilicon Translators 2N708, BSY27	0 - 68
U26		Fast Switching Silicon Diodes like IN914 Micro-Min.	0 - 5
U27		NPN Germanium AF Translators TO-1 like AC127	0.6
U29		1 Amp SCR's TO-5 can, up to 600 PIV CRS1/25-600	1.10
U30	15	Plastic Silicon Planar Trans. NPN 2N2926	0 - 50
U31		Silicon Planar Plastic NPN Trans. Low Noise Amp 2N3707	0.5
U32		Zener Djodes 400mW DO-7 case 3-18 volts mixed	0.66
U33		Plastic Case 1 Amp Silicon Rectifiers IN4000 Series	0.60
U34		Silicon PNP Alloy Trans. TO-5 BCY26 28302/4	0.50
U35		Silicon Planar Transistors PNP TO-18 2N2906	0.6
U36		Silicon Planar NPN Transistors TO-5 BFY50/51/52	0.85
U37		Silicon Alloy Transistors SO-2 PNP OC200, 28322	0.68
U38		Fast Switching Silicon Trans. NPN 400 MHz 2N3011	0.6
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U45		3A SCR. TO66 up to 600PIV	1.10
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Code No's, mentioned above are given as a guide to the type of device in the pak. The devices themselves are normally unmarked.

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2N3819	31p	2N 5458	35p
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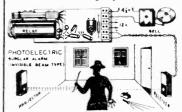
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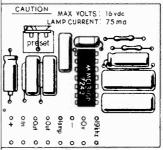
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WHY did you buy this copy of *Practical Wireless?* Were you influenced by advanced publicity or advertising; are you a regular reader with a devotion to follow our activities month by month; or are you one of many thousands who pick up this magazine to seek guidance on what makes radio and electronics tick? It has been said that people read *Practical Wireless* to learn something about the subject. After all, it is a technical field that demands some education and understanding and it is really this aspect that makes most people read.

To supplement professional career requirements there is a growing band of people who are bank clerks, clergymen, accountants, businessmen, as well as students and technicians who are seeking part time courses on the practical side of radio and electronics. Some colleges are able to offer facilities, subject to minimum class size, but we have heard of cases where they cannot find enough qualified engineers who are willing to spend extra time in the evenings to instruct these students. It is a pity because it often means that a course has to be dropped because of this.

So we come back to magazines; Practical Wireless is used in schools and colleges to a great extent because it provides an excellent support service to instructors, many of whom cannot always find sufficient time in addition to their everyday jobs to make full preparation for classes. Practical Wireless is a leader because its articles and designs are "down-to-earth" and, in spite of competition from elsewhere, we still offer the greatest constructional project support to instructors, technicians and engineers, while encouraging the confidence of newcomers.

This month we have rubber-stamped this policy by giving you for the first time a unique supplement containing eight extra straightforward constructional projects for the home, attractively presented with abundant illustrations and a full colour cover picture. To make it easier for you to find this supplement and worthwhile to keep for reference, we have printed it on a pleasant shade of "apple-green" coloured paper—another first for *Practical Wireless*.

Don't let this divert your curiosity too far from our other usual features because you will also find much more to interest you in this issue. For the benefit of quick and easy reference you will also find our contents list just inside the front cover, together with information on many aspects of our service. And watch out for next month's issue too for more special attractions, some of which are mentioned in this issue.

M. A. COLWELL—Editor

The June issue, on sale May 4th, will include a new easy competition to win a Digital Multimeter, a special feature on what to look for when buying Hi-Fi Equipment, and "Special Valves in Electronics", plus the usual abundance of constructional projects.

Further details on page 48.

NEWS...

B.R.C. change their name

British Radio Corporation Limited announced on the 1st April that it has changed its name to Thorn Consumer Electronics Limited. It continues to manufacture and market audio and TV products under the Ferguson, HMV, Ultra and Marconiphone brands and remains a wholly-owned subsidiary of Thorn Electrical Industries Ltd.

VAT

To the best of our knowledge, the prices quoted in this issue were correct at the time of going to press.

time of going to press.

As from April 1st, 1973, there is no purchase tax but a large number of goods carry Value Added Tax.

The "N.F.A.C."

HE National Federation of Aerial Contractors Limited is making an attempt to "clean up" the aerial contracting industry.

The Ministry of Posts and Telecommunications listed 55,000 complaints of bad reception in their recent annual report. Out of 32 listed causes of complaints. the largest numbers were for "inefficient aerial installations' and the N.F.A.C. feels that it can help this state of affairs by alerting the consumer and all who employ aerial contractors that there are in existence a very "Rooftop large number of Racketeers".

Plans currently being considered by the Federation include random inspections of members' installations and a system whereby new companies applying for membership will have their work inspected in addition to the trade references that are already required. A special Standards Committee will hear reports of faulty workmanship.

By this system, the N.F.A.C. hopes to assist in narrowing the field of consumer complaints and possibly convince dealers that they mean to play their part in cleaning up the aerial contracting industry.

NEWS...

NEWS...

NEWS...

Mullard film on I.C. design

WLLARD Ltd. have announced a new 16mm colour film lasting 18 minutes. It's called The Computer-Aided Design of Integrated Circuits and is available on free loan from the Mullard Film Library, 269 Kingston Road, Merton Park, London, SW19 3NR.

The film, which was shot mainly on location at the Mullard semiconductor plant at Southampton, describes in detail the use of the computer and its peripheral equipment in such functions as IC design and layout, mask-making and testing at every stage of production.

Tandberg in the jungle

Sergeant J. Murtagh of the Royal Signals is seen in the picture using a Tandberg Series 11 portable tape recorder. This machine and a TP4-1 portable radio accompanied a recent British Trans-Americas expedition which took in 18,000 gruelling miles from Alaska to the tip of South America. The purpose of the journey was to survey a road through the uncrossed 300 miles of swamp and jungle bordering the Panama canal which blocks the Pan American highway system.

During the trip, the expedition kept in touch with the outside world with the TP4-1 receiver, picking up BBC news broadcasts and weather reports.

In the jungle and swamps, the electrical equipment was carried in man-packs or by ponies and although it was partially immersed in water, rolled on several times by the ponies and carried through thick mud, it continued to function without a fault.



Sgt. Murtagh of the Royal Signals.

Signals "piped" through waveguide

THE core of a system which, when fully implemented, will transmit 300,000 phone conversations or 200 colour TV signals at the same time through a waveguide "pipe" is now operating at the GEC-Marconi works at Great Baddow.

This equipment will be used by Post Office engineers in a field trial system to be installed between the Post Office Research Station at Martlesham, Suffolk and a Post Office site at Wickham Market, 15 kilometres away.

The new "pipe" is a 50mm diameter circular waveguide capable of supporting signals throughout the frequency band from about 32 to 110GHz. The photograph shows 32-50GHz channel separating filters and band-branching assembly.

÷ (**)

Texan reprints

R EPRINTS of the "Texan" 20+20W Stereo Amplifier are available.

They may be obtained by sending 35p (30p+5p) postage/packing to "Texan" Reprint, c/o Chief Cashier, Practical Wireless Tower House, Southampton Street, London WC2E 9QX.

World Radio Club

FURTHER to the item on the World Radio Club in the March issue, we have been informed by the programme Producer that an extra broadcast in the BBC World Service will be made each week at 20.30 GMT on Thursdays.

The midday edition has now been moved to 13·30 GMT on Wednesdays. The other Friday and Sunday transmissions remain unaltered. BBC, Bush House, P.O. Box 76, Strand, London WC2B 4PH.

Some S.E.R.T. meetings

THE Society of Electronic and Radio Technicians, Faraday House, 8-10 Charing Cross Road, London, W.C.2. will be holding the following meetings:

April 11: "Test Equipment" by B. Ellison from Tektronix. Venue is The Conference Theatre, I.B.A., 70 Brompton Road, London, S.W.3 and the lecture commences at 7.00 p.m.

April 5: "Colour TV Forum and Exhibition". This will be held in the Byng Kendrick Suite, University of Aston, Birmingham, commencing at 7.00 p.m.

April 24: "The CVC5 Colour Receiver" by A. E. Thomas from ITT. This will be held in the Cleveland Scientific Institution, Corporation Road, Middlesborough. Meeting starts at 7.30 p.m.



THIS is a self-contained receiver which may be used over the range 115-150MHz, or 140-190MHz, according to the coil fitted. It was actually found to maintain good efficiency even up to 210MHz. A vertical telescopic aerial or improved aerial system will provide reception on the internal speaker, an outlet being present for headphones when required. An optional preamplifier is also described.

The receiver has a superregenerative detector, which is a great advantage from the point of view of simplicity. This type of detector is highly sensitive, and it should be possible to copy a signal of under $1\mu V$. There is also only one tuned circuit, so no alignment or ganging difficulties arise. The bands include the 2-metre amateur band (144-146MHz). In terms of sensitivity, most signals which can be well received with the simpler type of converter-communications receiver combination can also be received satisfactorily with this receiver.

A disadvantage sometimes encountered with this type of receiver is tricky tuning and hand-capacity

effects. These do not arise here, due to sound construction and a metal case and so actual use of the receiver is easy.

Circuit Details

Fig. 1 is the circuit, employing a junction f.e.t. in the first stage. The rod or other aerial is coupled by L1, and L2 is tuned by VC1. The network R2, C4, R3 and C5 gives a suitable quench frequency and regeneration is controlled by VR1. To modify the tuning range, L2 only need be changed.

A three-stage audio amplifier assembled on a separate circuit board follows. Tr2 is the first audio amplifier, Tr3 the driver, and Tr4/5 the output pair, operating a small speaker in the case. The outlet takes a jack plug for an external speaker or phones, if wanted, and VR2 is the volume or audio gain control. R12 is a small pre-set potentiometer, which allows working conditions for the output pair to be suitably adjusted.

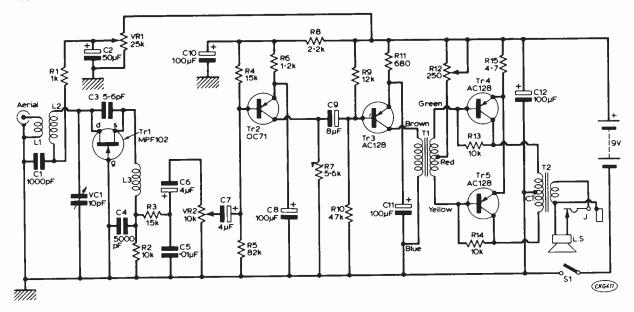


Fig. 1 : Circuit of the main receiver. The circuit of the pre-amplifier is shown in Fig. 4. The heading photograph shows the two units bolted together.

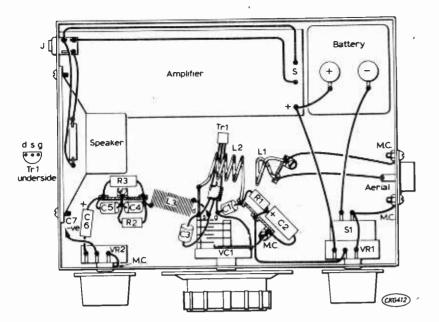


Fig. 2: Layout of the main components and audio amplifier board within the cabinet. When the preamplifier is fitted the coaxial aerial socket is removed and used on the preamplifier box.

Photograph looking into the top of the receiver which may help when locating components as in Fig. 2 above.

Cabinet Construction

Flanged universal chassis members 7×3 in form the front and back, and similar parts 5×3 in are the sides. The top and bottom are 7×5 in flat plates.

The front member is drilled for VC1, VR1 and VR2, as in Fig. 2. Also punch or drill holes for a co-axial socket on the right hand side, or for an insulated terminal or socket, if a co-axial feeder is not required here.

An opening is cut in the left member for the speaker, taking care that this will clear the amplifier and other parts. Perforated zinc or expanded metal is placed over the aperture, and the speaker is bolted on. The jack outlet is placed as shown.

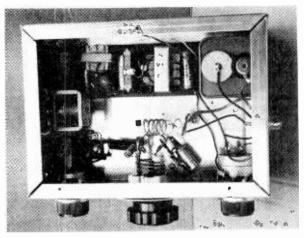
The four flanged members are then assembled by bolts through the holes present in them. Four holes are drilled in one 7×5 in plate, these are marked through so that the flanges can be drilled to suit. The case bottom can then be attached. Two rubber feet were placed on the front bolts, to raise the front of the receiver slightly.

It is easier to assemble the receiver if the sides and back are left off until later. When all construction is finished, the top 7 x 5in flat plate is fixed with four self-tapping screws.

Detector Stage

This is wired as in Fig. 2. A 3-lead holder is used for Trl. This avoids possible damage from heating while soldering, and also allows the transistor to be changed, if necessary. The MPF102 is listed as having a top frequency of 200MHz. Some were found to perform satisfactorily at well above this, but others, not up to specification, would only operate at relatively low frequencies.

The holder drain tag is soldered directly to the lower fixed plates pillar of VC1. The leads of C3 are cut short, and this item is soldered from the source tag, to the top pillar of VC1. A stout wire is also soldered to this pillar, projecting back about ¹2in so that L2 can be changed without unsoldering other items.



A stout lead from the *gate* tag goes to the moving plates contact of VC1, just clearing the moving plates. The tag strip holding R1 and C2 is raised on a long bolt, so that wires from C1 are as short as possible. A wire projects upwards about ¹2in to take the other end of L2.

L1 is a single turn of insulated wire. Coupling can be adjusted by rotating this small tag strip slightly on its fixing bolt, but it is not very critical.

L3 is self-supporting, and is 30 turns of 26swg enamelled wire, wound on a ¹4in diameter object which is afterwards removed. Turns are closewound. One end is soldered to the tag supporting R2, C4 and R3, and the other end is soldered to the source tag of Tr1 holder.

The potentiometers and other parts can then be wired as in Fig. 2. A lead will run from VR2 under the speaker to the input pin of the audio amplifier.

Audio Amplifier

This is assembled on Veroboard 5×1^3 4in, as in Fig. 3. First drill two holes for the chassis bolts, position the board in the case, and mark and drill

matching holes in the metal bottom. Tags held with the bolts form earthing points, Fig. 3. The bolts are 1 ₂in long, so that extra nuts hold the assembly clear of the metal case, lock-nuts underneath securing the amplifier. A piece of card 5×1^{3} ₄in may be put between the amplifier and case bottom, though shorts to the metal will not arise if joints are kept close to the board.

Coils

These are self-supporting, wound with 18swg, 20-swg or other stout wire, with spaced turns. A coil having 4 turns, $^{1}_{2}$ in outside diameter, and $^{7}_{8}$ in long, was found to tune 115-150MHz. This is suitable for 2 metre reception.

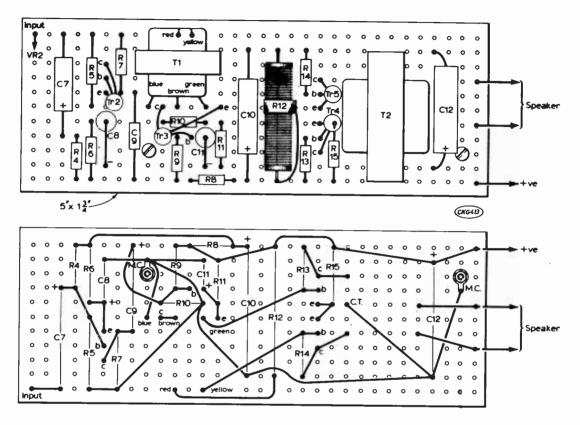


Fig. 3: Diagrams of the component layout and wiring of the audio amplifier board.

Take care to fit the electrolytic capacitors as indicated. With a unit of this kind, it is helpful to place black 1mm sleeving on the negative line leads, and red sleeving on positive leads. With another colour for other wiring, it will be easy to check connections if this should prove necessary.

The amplifier may be tested before fixing it. Place the slider of R12 at about the central position. Connect the speaker and a 9V battery, negative to one of the chassis tags. Either place a meter in one battery lead and move the slider of R12 for a current of 10mA, or adjust R12 to place just enough resistance in circuit for speech to sound normal. If R12 is at a very low value, current drawn will be small but cross-over distortion will be present.

For this test, input can be from any convenient source; a signal generator, diode tuner, pick-up, or from the first stage of the completed receiver. If VR2 is not in circuit, avoid overloading the amplifier by the test signal.

The amplifier is fitted as shown, negative return being through the metal case. Connect the speaker leads and amplifier to the jack so that the contacts which open silence the speaker, when phones or an external speaker are in use. A coil $^{1}2$ in long and $^{7}16$ in in diameter, having three turns, tuned 192-150MHz, while a similar coil having two turns allowed 216MHz to be reached.

Stray circuit capacitances and the length of connecting leads influence the frequencies tuned. The frequency can be raised by reducing the number of turns, or by stretching the coil to separate turns, or by reducing the overall diameter.

Operating notes

When VR1 is advanced, a position should be found where a strong hiss begins. This is roughly the correct setting for VR1, though it will be found that further slight adjustment may be helpful, depending on the strength of the signal tuned in.

The hiss should cease when any signal of sufficient strength is tuned in, provided VR1 has not been turned too far. VR2 adjusts volume in the usual way, and can probably be advanced about half way, for the internal speaker.

If superregeneration is impossible on some part of the band, move L1 a little further from L12. This

* components list

Resis	tore				
			-	12kΩ	
R1	1kΩ		R9		
R2	$10k\Omega$		R10	$47k\Omega$	
R3	15k Ω		R11	680Ω	
R4	15kΩ		R12	250Ω	miniature slide pot.
R5	82kΩ		R13	$10k\Omega$	
	1 · 2kΩ	,	R14	10kΩ	
	5 · 6kΩ		R15	4.7Ω	Alf ±W, 5%
	• • • • • • • • • • • • • • • • • • • •		1110	7 ,	V
R8	2 · 2kΩ				
VR1	25k Ω	linear	pot. w	rith sv	vitch
VR2	10kΩ	log. p	ot.		

C	_	-	_	:	\$ _	~	

	,,,,,,,		
C1	1000pF disc ceramic	C7	4μF 4V
	50μF 10V	C8	100μF 10V
		C9	8μF 6V
C3	5.6pF		
C4	5000pF		100μF 10V
	0 · 01µF	C11	100μF 10V
			100μF 10V
C6	4μF 4V		100με εσν
VC1	10pF variable Jackson	C804	

Transistors

Tr1	MPF102		Tr3	AC128
	OC71	•	Tr4/5	2xAC128

Miscellaneous

Case: Two 5x3in. and two 7x3in. flanged universal chassis members, and two 5x7in. flat plates (Home Radio, Mitcham); KN2 2½in. dial and knob (Home Radio); Two 1in. knobs; tag strips, etc.; T1 Osmor driver transformer; T2 Output transformer, 2xAC128 type to 2/3 ohms; 2½in. 3Ω speaker; Jack socket with break contacts; 3-lead transistor holder, coaxial socket.

is not critical, but tight coupling will tend to prevent regeneration, while very loose coupling will reduce signal strength.

Aerials

There is room for considerable experiment here. Some local transmissions (range about 10 miles) were received with about 6in of wire projecting from the socket, which shows how sensitive this type of circuit can be.



This view of the receiver shows the positioning of the internal loudspeaker and the socket for an external loudspeaker or headphones.

With a telescopic aerial extending to three feet, a considerable number of transmissions were received, including amateurs over 50 miles away. This aerial performed poorly with the receiver and aerial near a metal window, but was better in the centre of a downstairs room, and even better in an upstairs room. Reducing the length to about two feet made almost no difference, and sliding the sections up and down did not give any notably best or critical resonant length.

Best results of all on 2 metres were obtained with a dipole made from \$^1_4\$ in aluminium tubing, \$38^1_2\$ in overall, with a centre co-axial feeder. This aerial was mounted out of doors on a light pole. A long or lossy feeder would tend to lose much of the advantage such an aerial can give.

The angle and slope (polarisation) of all these aerials had some influence on results. No doubt an improved VHF aerial would increase signal strength, but some means of rotating it would be needed, and this was not felt justified.

Pre-amplifier

The receiver has high sensitivity, but in some circumstances there are advantages to be obtained by adding an r.f. stage. This stage will materially reduce radiation from the superregenerative detector, and also help isolate the aerial to avoid dead spot or damping effects on some frequencies. In fact, these are the most important advantages, and much gain must not be expected from the r.f. stage at frequencies over 150MHz or so.

Fig. 4 is the circuit, the f.e.t. being used in a grounded-gate arrangement which does not need neutralising. L1 is peaked by the small capacitor VC1. Tuning is flat, and needs no adjustment over a small band.

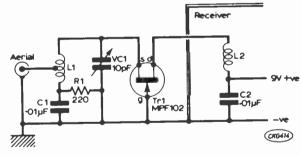


Fig. 4: Circuit of the pre-amplifier and connections to the input circuit of the main receiver.

The f.e.t. drain circuit is to the coupling loop L2, which was originally used for aerial coupling in the receiver. Alternatively, a broadly resonant winding can be used here, resulting in better gain over a narrow band of frequencies.

Cabinet

The box is $3 \times 2 \times 2$ in and is bolted on the metal side of the receiver case. It is made from a flat piece of aluminium 7×2 in and one 7×3 in flanged "universal chassis" member.

The long flanges are cut 2in from each end, a 90° piece being removed. A piece of wood about

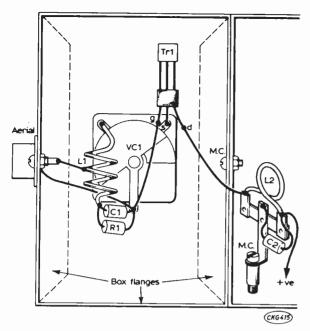


Fig. 5: Positioning of the few components within the preamplifier box.

 3×2 in and $^{1}2$ in or so thick is then placed between the flanges, and another piece of wood is placed level with this, and the whole gripped tightly in a vice. The 7×3 in member is then bent into a $3 \times 2 \times 2$ in box, with the flanges inwards. Fig. 5 shows this part from behind. The front is drilled for VC1, and one side for the co-axial or other aerial socket. Three holes are also drilled in the other side, to match up with the holes which are exposed when the co-axial socket is removed from the receiver.

The 7 x 2in piece is bent at 2in from each end, in the same manner, so will fit on to enclose the box. It is held with a number of self-tapping screws.

Pre-amplifier Wiring

The transistor holder (or transistor) is soldered directly to VC1, as in Fig. 5. All leads are as short as possible.

L1 is wound with 18 or 20swg copper wire, and is similar to the coil in the receiver, but will generally have to be stretched somewhat, or have

★ components list

R1 220 Ω ½W, 5% C1 0.01 μ F

C2 0·01μF

VC1 10pF or similar miniature variable, or pre-set.
Tr1 MPF102 Holder optional

Universal Chassis flanged side 7x3in. (Home Radio) Aluminium 7x2in. Knob, tag-strip, etc.

The components listed above for the pre-amplifier are additional to those required for the main receiver.

about one less turn. If maximum volume is with VC1 fully open, this shows that L1 should be changed, by removing a turn, spacing turns further apart, or winding a new coil of smaller diameter.

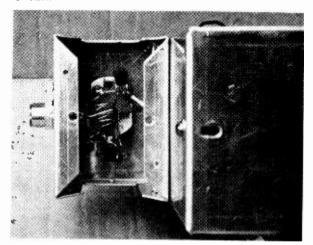
The position of the aerial tapping depends somewhat on the use of a co-axial fed dipole or similar aerial, or a short vertical rod type aerial. This tapping can usually be about one-quarter to one-third the total number of turns from the C1 (earthed) end.

Two bolts fix the r.f. stage to the side of the receiver, and a lead from Trl drain passes through the original aerial socket hole to L2.

Receiver Changes

The tag strip holding L2 is replaced by one having two insulated tags. A lead from one tag is run to a positive pin on the a.f. amplifier and C2 is connected from this tag to the chassis tag, as in Fig. 5. The drain lead is taken to the other tag. L2 is one turn of insulated wire, positioned near

L2 is one turn of insulated wire, positioned near the detector coil. Coupling is adjusted for best regeneration, by bending the loop L2 to adjust the distance to the detector coil, as with the original circuit.



Rear view of the completed pre-amplifier bolted to the receiver.

It was found that results were better with coupling in one phase. To check for this, twist L2 180°, to change its sense with relation to the detector coil.

As mentioned, L2 can be resonant over a narrow band. This increases gain, but makes it a little more troublesome to change coils or cover a wide band of frequencies. If this method is to be tried, wind L2 with one or two extra turns, compared with the detector coil, using insulated wire to avoid shorts. It is then necessary to stretch or compress L2, or change the number of turns, until it is found to peak up signals in the wanted frequency range. The resonant effect is quite flat, but these adjustments, and the degree of coupling with the detector coil, and position of the aerial tapping, can make quite a difference to reception.

Because superregenerative receivers are notorious for their radiation it is strongly recommended that the pre-amplifier be fitted as an essential part of the receiver. Complete screening, as described by the author, is very important.



FETRONS

HE field effect transistor (FET) is currently being used in the front end of a.f. and r.f. circuits, as well as being developed into simplified forms of logic circuitry for micro-miniature applications such as wrist watches and pocket calculators. Aside from the manufacturers of such luxury items, our attention is turned here to more domestic matters such as television receivers, radio transmitters and receivers. Where thermionic valves are still being used, there is some reluctance to effect a total conversion to semiconductor techniques. We can have the best of both worlds because we can now replace valves in some circumstances with direct equivalent improved performance transistors. Particular areas of application also include unattended relay stations, and telecommunications terminals, as well as domestic receivers.

TRIODE EQUIVALENT

These transistors, called "fetrons," have emerged from the military applications stable and are being made available for other applications, although very little is generally known about the performance so far. The fetron is basically an arrangement of two n-channel field effect transistors (Fig. 1) connected to provide the equivalent working characteristics of a triode valve but with a much better frequency response at both ends of the spectrum. This is because the fetron has an extremely low channel resistance and inter-electrode capacitance. Furthermore, since there are no heaters, operation is immediate on switch-on.

OTHER FEATURES

The life of the fetron is likely to be much greater than the thermionic valve under normal working conditions and the degradation of operational characteristics is minimal. Other important features include a higher amplification factor (almost ten times that of a valve) and a lower noise figure. Since no heaters are used, power requirements are simplified to just one high tension supply.

PENTODE CHARACTERISTIC

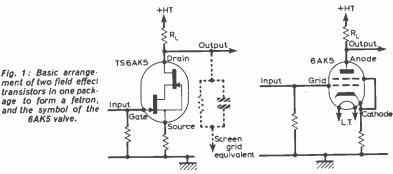
Both the thermionic valve and the FET are voltage controlled devices, hence design equations are virtually the same. Although the pentode anode voltage-current characteristics are similar to the drain characteristics of the fetron, the latter are more clearly defined at the cut-off region

or "knee" and exhibit stable current drain for various drive conditions (Fig. 2).

Since the main purpose of the fetron is to act as a direct replacement for the triode valve, it is essential that it should withstand high voltages and have a matched gm. The single junction FET cannot do this, but when two specially selected FETs are cascaded the problem is overcome. It is also possible to reduce the Miller (gate to source capacitance) effect by using a low capacitance, small signal, high gm FET at the input circuit, coupled with a high voltage output FET.

With the arrangement shown in Fig. 1, the output FET acts as a voltage dropper for the input FET and the Miller effect capacitance of each is in series. The output impedance is also greater than in a valve pentode, resulting in the excellent characteristics shown in Fig. 2. Since the input gate circuit is effectively a reversed bias junction, it presents a very high resistance load to the signal source.

Fig. 3 shows the transfer characteristic of a fetron which has been made



29

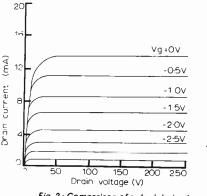
TYPICAL PENTODE D	EVICE CHARA	CTERISTICS-
PARAMETER	6AK5	TS6AK5
Plate voltage breakdown	350V	350V
Plate resistance	0·5MΩ	5·0MΩ
Transconductance	5,000µmhos	4.500µmhos
Plate current (Rk=200Ω)	7·5mA	7 · 0m A
Grid voltage for Ib=10µA	-8·5V	-5·0V
Amplification factor	2.500	22,500
Input capacitance	4·0pF	6.5pF
Output capacitance	0 · 02 p F	0.02pF
Useful frequency limit	400MHz	600MHz

TABLE 2:

TYPICAL TRIODE DEVI (EACH SIDE)—Rk	CE CHARACT =2-70 Ω, Eb=1	ERISTICS 30V
PARAMETER	12AT7	TS12AT7
Plate voltage breakdown	400 + V	350V
Plate resistance	15kΩ	250kΩ
Transconductance	$4,000\mu$ mhos	3,000µmhos
Plate current (Rk=240Ω)	5.0mA	9·0mA
Grid voltage for lb=110µA	-7·0V	-7·0V
Amplification factor	60	750
Input capacitance	2 · 2pF	25pF
Output capacitance	1 · 5pF	3.5pF

up from selected FETs to approximate closely that of a particular valve (shown dotted) operating within the same limits. If special requirements include partial operation beyond this FET cut-off then clearly a more appropriate FET device must be selected for this, perhaps providing a higher current for the same control voltage. The gm or transconductance ratio of the fetron gives a true square law property with consequent harmonic distortion figures of an extremely low order. In fact, harmonics beyond second order are claimed to be negligible.

Although the simulation of the "screen grid" principle can be effected within the fetron package, the similarity of the transfer curves to those of a pentode must not be taken as an assumption that the fetron is an ideal replacement for the pentode, even though the noise figure may be lower. The fetron has a markedly improved performance over the triode due to square law operation.



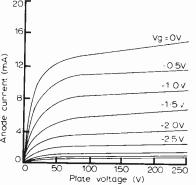
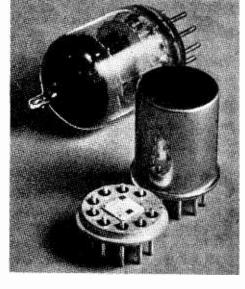
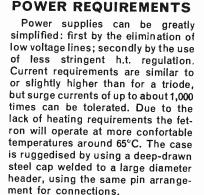


Fig. 2: Comparison of output drain characteristics with those of the 6AK5 anode.





Fetrons that have been made so far include replacements for the 6EW6, 6JC6, 6AK5 and 12AT7 but with ready made FET junctions currently available it is expected that the majority of common types can be simulated. More familiar types such as 6V6 and 6AQ5 are next on the list. The type number given to fetrons consists of the equivalent valve number but prefixed TS. Hence the

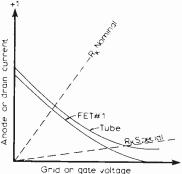


Fig. 3: Transfer characteristic of a fetron compared with a valve,

fetron for replacing the 12AT7 is TS12AT7.

The manufacturer who has announced these activities in fetrons is the American company Teledyne Semiconductors, who are selling in the U.K. via the distributors GDS Sales Ltd. of Slough. Prices are higher than for valves but this is offset by the long term performance advantages described. GDS Sales quotes £8 for the TS12AT7 and £6.50 for the TS6AK5 for orders of 1 to 99, these being the first available in the U.K. Although this price is high the long term advantages of reliability and performance are compensatory.Small orders for these devices are being handled by the subsidiary company Best Electronics (Slough) Ltd, Michaelmas House, Salt Hill, Bath Road, Slough, Bucks, SL1 3UZ.

Elsewhere in this issue we are taking a closer look at some of the valves that still have a unique role to play in radio and electronics. Look out for our special feature "Special Valves for Communications".

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2N2906

2N2907 0.18

2N2923 2N2924 0.12

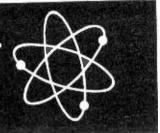
2N2904A 0.25

2N2905A 0.28

2N2906A 0.28

2N2907A 0.25

EXPERIMENTERS CORNER



6-9V STABILISED SUPPLY

THIS inexpensive unit will enable cassette recorders, portable radios, portable record players and the like requiring 6 to 9V to be run from a 12V car battery, in or out of the car. This not only saves their internal batteries but ensures that they run at peak efficiency.

CIRCUIT

In the basic circuit, Fig. 1, the reference voltage is determined by a zener diode ZD which controls the output voltage. Tr1, a power transistor, takes a small current from the zener diode, amplifies it, and feeds the resulting current to the output circuit.

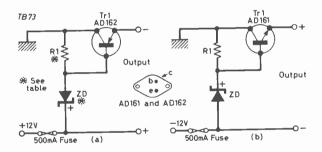


Fig. 1: Basic stabilising circuits for a) negative and (b) positive "earth".

With the output circuit left open Tr1 remains off, but as soon as a load is connected the current will increase until the voltage at the output is a little less than that of the zener diode. If for any reason the output voltage increases the voltage across Tr1's base-emitter decreases causing the collector current to drop. Conversely, if the output voltage decreases the base-emitter voltage will increase, raising the collector current. The overall effect being that the output voltage will remain constant despite varying load currents.

OVERLOAD

Although the basic circuit will work quite satisfactory, if the output leads are accidentally shorted together a heavy current will flow which may damage the transistor before the fuse can blow. To insure against this the circuit can be modified to the form shown in Fig. 2. Here, no matter what the load, even a short circuit, no more than 330mA will flow. Under normal loads the voltage across R2 will be less than the 500mV or so required to start Tr2 conducting, so the circuit will work as in Fig. 1.

J. ROWLEY

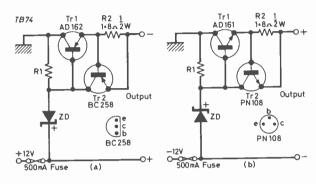


Fig. 2: Protected circuits for negative or positive "earth".

However when the current exceeds 280mA this will no longer obtain and Tr2 will start to draw current from the zener diode. At first this will have no effect, but if the voltage across R2 increases further Tr2 will draw more and more current until finally the zener will stop conducting, thus enabling the output voltage to fall to a level where no more than 330mA flows.

Output Voltage	ZD (400mW)	R1 (¼W)
6V 7·3V 9V	6·2V 7·5V 9·1V	$\begin{array}{c} 680\Omega \\ 390\Omega \\ 220\Omega \end{array}$

CONSTRUCTION

The unit is built into an aluminium box approx. $3\times2\times2$ in. (Type AB12) the power transistor being bolted to the box after applying silicone grease. The few components are connected directly to the pins of the power transistor. Since the quiescent current is only about 13mA no on-off switch is fitted.

BACK NUMBERS

We regret that the back numbers department of P.W. has now closed and consequently we are unable to supply these. Requests for specific back issues can usually be included in our 'CQ' section; there is no charge for this but it is a service between readers and P.W. is unable to meet any of these requests.

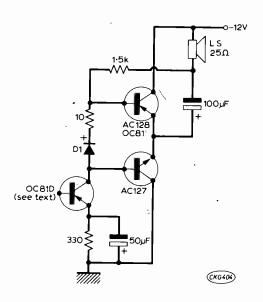
TWO VERSATILE TRANSISTOR AMPLIFIERS

As an independent service engineer one is often called on to repair car radios whose age, or foreign origin, make it difficult, if not impossible, to obtain spares. Quite often there is a burntout output or driver transformer which would normally result in the set involved being scrapped. To avoid this it has been possible, over a period of time, to evolve two output stages which employ no transformers or "difficult" components. The transistors used are easily obtained and cheap. In fact, one aspect of the design was to take advantage of the excomputer panels now widely on sale, which contain large numbers of suitable transistors, etc.

CIRCUIT No.1

The first design is intended to take the place of the relatively low-powered output stage used by several firms in hybrid car radios. A typical set employed two "12 volt h.t." valves and three transistors, an OC81d driving a pair of OC81's. The original OC81d is retained, but with a slightly different emitter resistor, and feeds directly into a complementary pair, AC127 and AC128.

The actual construction is so simple that it may be done on a seven-way tag strip. It will usually be possible to use the heat sinks previously fitted to the OC81's. The sole drawback, if such it be, is that the loudspeaker has to be changed to a high impedance type.

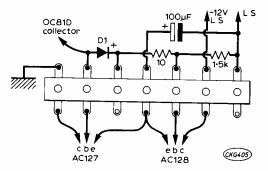


Two transistor output stage added to existing OC81D stage in receiver.

CIRCUIT No.2

It was to provide more power than the AC127/128's could give, and also to avoid having to use special loudspeakers, that the second circuit was evolved. It consists of an amplifier, a driver, and a complementary stage, which in turn drives the output transistors. In this circuit the computer panels really came into their own. Those used contained mainly

C. E. MILLER



Suggested layout of Circuit No. 1 using a tag strip.

2G302's (p.n.p.), 2N1091's (n.p.n.), OC23's (p.n.p. output) and OA10 diodes. There were also some anonymous devices which looked, and behaved, like OC81's. The alternatives for the various transistors, etc., in the design are as follows:—

Trl. AC128, OC81, 2G302.

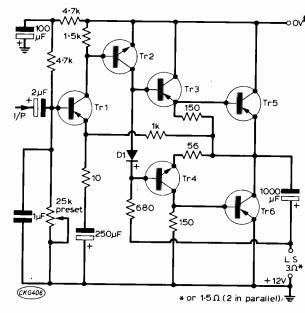
Tr2. AC127, AC176, 2N1091.

D1. AA119, OA10, AC128 with base/collector strapped.

Tr3, as Tr1.

Tr4, as Tr2.

Tr5, Tr6. AD149, OC23. (Etc.—any large output type).



Higher powered output stage of Circuit 2.

As a final construction point, the output transistors should be mounted on a piece of aluminium of some 30 sq. in. This may conveniently be shaped to act as a screen for the rest of the amplifier. The prototype was deliberately mounted in the worst possible place, in a confined space close to the vehicle heater, but no overheating has been observed.



There are 195 other good reasons for buying AMTRON electronic kits

Apart from the five items shown above, there are another 195 kits to choose from in the vast AMTRON range of electronic kits.

A few examples of equipment you can construct from AMTRON kits are: Power supplies, preamplifiers, amplifiers, L.F.instruments, accessories for musical instruments, amateur and radio control transmitters and receivers, battery chargers, electronic car accessories, psychedelic lighting equipment, measuring instruments, tuners, receivers, I.C.digital equipment.

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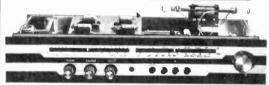
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1R5	-28	30C17	-76	EAF42	-50	EM80	-36	PCF808	-68	U801	-75
185	.22	30C18	-57	EB91		EM81	-36		+30		31
1T4	.16		-64	EBC33	-40	EM84	-32		.55		-50
384	-26		-85		-49	EM87	-50		-33		-45
3V4	-47		-69	EBC81	-80		-36		-38		-34
5U4G	.31	30FL14	-68	EBC90	-22		-29		.37		-32
5V4G	+35		-29		-32		-29		-80		-82
bY3GT	-30		.70		-39	EZ40	.39		-89		-85
5Z4G	-35	30L17	.70	EBF89	-29	EZ41	-39	PCL805	-38		-30
6/30L2	-54	30P4	-54		.17	EZ80	-21	PENA4	.77	UCH42	-58
6AM6	-13	30P12	-69	ECC82	-20	EZ81	-22	PEN36C	-70	UCH81	-80
6AQ5	-22	30P19	-54	ECC83			-25		-51		-82
6AT6	.20	30PL1	-56	ECC85	-34		-84	PL36	-48		-55
6AU6	-20	30PL13	-89	ECC804	-54	GZ32	-40	PL81	-43		-62
6BA6	-20	30PL14	-80	ECF80	+30		.77	PL81A	.47	UF89	-80
6BE6	-21	35L6GT	.45	ECF82	-26	KT61	-55	PL82	-31	UL41	-58
6BJ6	-41	35W4	-25	ECH35	.55	KT66	-78	PL83	-38	UL84	.80
6BW7	-50	35Z4GT	-25	ECH42	-59	LN319	-56	PL84	-30		.22
6F14	-35	50CD6G	-68	ECH81			-80	PL500	-63	UY41	-89
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6J7G	-24	B729		ECL82	-29	PABC8		P¥32	- 52		- 22
6K7G	.12	CCH35		ECL86	-85	PC86	-44		-52	Transist	aro:
6K8G	-36	CY31		EF39	.38	PC88	-44		-25	AC107	.17
6Q7G	.35	DAF91		EF41	-57				-25	AC127	-18
68L7GT	.32	DAF96		EF80	-23	PC97	-38		-26	AD146	.87
68N7GT	-32	DF91		EF85	-28	PC900	-29	PY88	.33	AF115	.20
6V6G	.28	DF96		EF86		PCC84	-29	PY800	-31	AF116	.20
6V6GT		DH77		EF89	-26	PCC85	-23	PY801		AF117	-20
6X4		DK32		EF.31		PCC88	-38	R19		AF125	-17
6X5GT		DK91		EF92	-27	PCC89		R20		AF127	.17
10P13		DK93		EF98		PCC189		U25		OC26	-25
12AT7		DK96		EF183		PCC805				OC44	-12
12AU7		DL35		EF184		PCF80				OC45	-12
12AX7		DL92		EH90		PCF82				OC71	.12
19BG6G		DL94		EL33		PCF86				OC72	-12
20F2		DL96	.00	EL34	-48	PCF800				OC75	-12
20P3	-75	DY86		EL41	-54	PCF801				OC81	-12
25L6GT	-19	DY87	0.4	EL84	-23	PCF802				OC81D	-12
25U4GT	.07	DY802	1	ET30	.20	PCF805				OC82	.12
30C1	.50			EL95						OC82D	.12
30C15	-58	EABC80	-32	EL500	-62	PCF806	-56	U329	-66	OC170	.28

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practically wireless HENRY commentary by

Age cannot wither them

HERE wireless engineers foregather, talk inevitably veers toward: 'I remember...'

It is either a model with such idiosyncracies that a catalogue of 'common faults' would have called for an appendix to the service manual, a manufacturer whose crass perfidy extended to an invoice before the goods arrived —or worse, so long afterwards that one had to guess at the cost of the spares before one dared complete the repair—or a customer.

But my subject today is not so much the trials and tribulations of the working engineer as this 'harking back' tendency we all evince, once we converse with fellows of like mind. Go to a meeting of the RSGB, the SERT, the BARTG or even your local Gramophone Society and before the last strains of the demonstration or mutters of the lecture have died away, everybody is avidly recounting his or her personal experiences.



. . . a donkey-driven gramophone.

Watching two members of the Royal Television Society taking coffee last week reminded me of Ralph Richardson and John Gielgud in the Royal Court Theatre production of Home. Parallel tracks of reminiscence, meeting rarely at some way-station. From the few words I caught in that BBC Hospitality Room, member A was waffling on about videotape while the other had some bee in

his bonnet about phase-lock loop and pulse-code-modulation.

Henry was dying to know how Mr. B allied the two subjects, but couldn't find out because the charming production assistant he was trying to chat up with his memories of Marconi would insist on relating her opinions of Arthur Negus every time I had to pause for breath.

All this is brought on by hearing about the Fetron.

The Fetron is a genuine solid state substitute, mounted in a case like a valve, with pin formation and characteristics of the valve it is meant to replace.

You can read the ins and outs of it in the "Special Product Report" elsewhere in this issue, if it grips your curiosity like it did mine. Suffice it to say on this page that all those "everlasting" relay stations, built around valves designed to run forever, could not die without putting up a fight first.

Use of the Fetron saves major circuit modification when a valve-change is needed. Ain't science wunnerful?

Trouble is, Henry took a look at the types available and found there listed the dear old 12AT7. Now the TS12AT7 sounds a good idea until you remember some of those old 'universal' radiograms, and one or two series-heatered television sets that used them.

What happens if you plug in a Fetron? Have they made a resistive heater 'bridge', or do we have to solder a resistor across the socket? And, if we do, shouldn't there be a thermistor provided? Should we not also protect the h.t. line because the Fetron is operative immediately?

So many questions...reminds Henry of that unfortunate chap in an electronics magazine who offered a simpler way of getting over some stabiliser problems. Only snag was, somebody had to remember to turn the control back to zero after use unless the

next chap along blew the thing up—you know, the way your loudspeaker creases when you have left the amplifier gain up high and a 'friend' flicks your stylus!

Well, the upshot of this poor chap's sensible economy was that



. . . and the inevitable happened.

electronic geniuses wrote in, both calling him gormless and detailing complicated protection circuits that would automatically switch off, from any given function. I wonder if Mrs. Mary W. would like one built into every TV?

I remember one TV we could never switch 'Off' because the maker had fitted too-substantial suppressors across the contacts.

We all tend to hark back. You should see the glee with which Colin Riches unearths a donkey-driven gramophone. At the wedding of a friend's daughter, hardly out of her teens, one of the speakers, Marketing Director of a worldwide Telecommunications company, had to remind the reception that his first acquaintance with the charming Sally was when she sat in his lap—at eighteen months—and the inevitable happened.

He might, at least, have reminded them of the days when he was hawking cheap radios round the council estates. It is just as funny a story. Remind me to tell it to you, one day . . .

Special Valves

PART1 COMMUNICATION TYPES

M.K.TITMAN B. Sc(Eng), C. Eng, MIEE.

HERMIONIC devices still have a wide range of applications in modern electronic circuits and, despite the semiconductor takeover, they remain essential components in a variety of applications from high power r.f. amplifiers to electro-optical transducers.

The requirement for valves for u.h.f. and s.h.f. has led to the development of special techniques. The following valves were all developed from the necessity to exploit new ways to enable communication systems to use the wide bandwidths available at u.h.f. and microwave frequencies. The principles used are mathematically complex but their operation can be readily understood.

DISC SEAL VALVES

The form of construction used for both triode and tetrode configurations is illustrated in Fig. 1. The structure consists of a thimble-like cathode, spaced from a parallel wire grid further separated from a disc anode. The structures are very rigidly held by the ceramic space discs and because of the annular configuration co-axial input and output terminations can be used. The advantage of this system is that high power operation with reasonable efficiency in the GHz region is possible.

Disc scal triodes are used for amplifier and oscillator applications from $0.5 \, \text{GHz}$ to $4 \, \text{GHz}$ frequencies, at power levels of $1 \, \text{W}$ to $600 \, \text{W}$. Typical values of g_m are $6 \, \text{mA/V}$ to $25 \, \text{mA/V}$. At lower power levels

(<25W) the envelope is designed for convection cooling but forced air cooling is used for the higher power levels. Examples of this valve type are the ES157 at 2W, and TDO4-20 at 12W.

KLYSTRONS

Klystrons are also essentially microwave valves which operate as oscillators in the frequency range from u.h.f. to more than 100GHz. Generally they are available for discrete commercial frequencies such as 6, 7, 8 or 9GHz and mechanical tuning by micrometer adjustment is possible.

The klystron consists of a cavity (or for power devices, multiple cavities) through which a stream of electrons is beamed from a normal electron gun assembly, as shown in Fig. 2. The electrons are velocity modulated by a field produced by a toroidal modulating structure known as a rhumbatron. The electrons therefore become bunched in regions of high electron density and rarified in low density regions, as they travel through a further section known as the drift space. Consequently if critical frequencies are utilised the bunching allows resonant oscillation to occur in a mode controlled by the rhumbatron.

Power levels for high frequencies are in the region of 1kW with special u.h.f. power devices operating at 460 to 1000MHz at levels of 20kW. The electronic tuning range for such devices is from 30 to 100MHz,



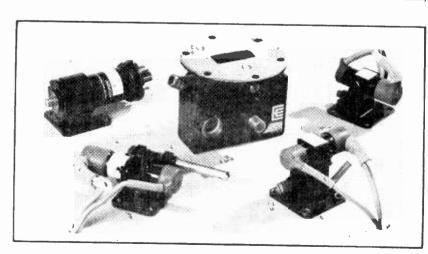


Fig. 1: at left, shows the general configuration of a disc seal valve. The picture shows a collection of oscillator klystrons, the centre one being used in communications relay equipment. The others are used in radar local oscillators.

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AC127 25p BCY72 15p CA3048 £2:34 0 A95	5p 1N5404 10 3N128 6p 1N5408 25p 3N140	92p	2:2 25v 7p 100 40V 10p 2:2 63v 5p 100 63v 10p			
AC128/AC176 BD131 75p CA3065 £1 42 0 A202	97p1S920 7p3015F	62.00 A	4.7 40v 5p 220 40v 9p			
AC151 20p BD131/132 £1 50 CA3090Q £4-70 OC25	70 1 5 5 0 0 9 1 3 0 1 5 G 1 5	£2 00] .	10 63v 6p 470 25v 12p			
AC153 26p BF115 23p CD4009AE £1.16 OC29	76p 1\$5012 80p 7401 60p 1\$5015 75p 7402	20p	22 40v 6p 2200 25v 30p 22 47 25v 6p 4700 16v 33p			
AC153/176K 62P BF16/ 25P CD4012AE 34P OC36	63p 1S5018 75p 7403 40p 1S5024 75p 7404	20p	47 40v 6p			
AC187K 17p BF173 39p CD4013AE £111 OC41 AC188K 23p BF177 25p CD4015AE £2.92 OC42	40p 1S5047 /5p 7405	25 p	CAPACITORS—METALLISED POLYESTER Price each			
ACY17 27p BF180 35p CD4018AE £2.92 OC45	20p 2N696 15p 7409 20p 2N697 17p 7410	25p	0·01, 0·015, 0·022, 0·033			
# A CV10 20m RE105 15n CD4024 A E £2 U9 CC70	20p 2N698 30p 7413	30p	0·047, 0·003, 0·10 0·150, 0·220			
# ACY21 19p BF200 35p CR1/401C 60p OC76	25p 2N706 10p 7420 25p 2N706A 12p 7425 46p 2N708 16p 7430	30 p	0.33 0.47			
A D140 550 BF255 150 £1 08 0 C01	20p 2N911 50p 7440	24p	0·68 1·0 20p			
AD161 49p BFX29 25p £1.53 OC83	23p 2N918 42P 7443	£1 45	1-5 2-2 Order as "Polyesters" + Capacitance.			
A D161/162 £1 04 BF X85 34P D10 (N 1 GD10) (OC 139	25 p 2 N 9 3 0 28 p 7 4 4 5	£2.06 £1.45	CARACITORS_POLYSTYRENE			
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BC109/BC179 BZY88C6V8 13p MJ491 £1 35 TIL112 24p BZY88C7V5 13p MJ802 £4 12 TIL209	35p 2N2925 20p 74151 60p 2N2926 10p 74153	£1:10 £1:35	Probably the best test probes ever made. When you push a plunger a spring steel forked tongue pushes out and holds the components,			
BC109C 11pBZY88C8V2 13pMJ802/MJ4502 11P31A	70p 2N3053 27p 74154 85p 2N3054 50p 74155	£2:00 £1:55	wires etc., while you take readings etc. it won't let go ditte you			
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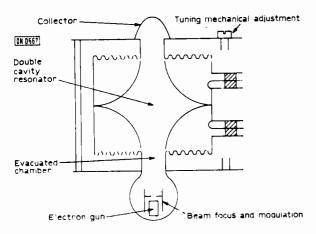


Fig. 2: Internal arrangement of a klystron valve.

whilst the mechanical range is considerably more. Typical device types are the KS6, 7, 9 family and YK1010 to 1090. Most of these utilise waveguide outputs but some have coaxial probes. The higher power devices require forced air cooling, whilst the u.h.f. power units need a cooling water supply.

TRAVELLING WAVE TUBES

These are microwave power amplifier valves used extensively in communication systems particularly for microwave links. The basic construction is shown in Fig. 3 and consists of an electron gun assembly, a modulating helix structure and a collector electrode. The electron gun forms a narrow electron beam focused by means of the grid and anode. The beam passes along the axis of an accurately formed helix structure and is continually focussed by a magnet system. The modulating microwave frequency is passed along the helix and travels at approximately the same speed as electrons in the beam. Thus the r.f. field produces an electric field which velocity modulates the electron beam as it travels along the helix axis. After modulation the electron beam bombards the collector electrode which is often water cooled.

For low power valves the helix is of wire but for power devices a ring bar structure is used. As the helix is in a long glass envelope, heat dissipation is by radiation and thus the power is limited, especially since the mechanical helix structure must be very accurate. For very high power devices a ring-bar helix system is used and is a development of the

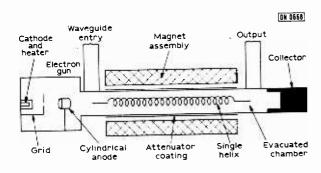


Fig. 3: Diagram to illustrate the construction of a travelling wave tube.

cross-wound opposite band helix system. Where very high power is necessary the ring bar structure is supported by annular beryllium insulators of high thermal conductivity.

Travelling wave tubes are very efficient microwave amplifiers which produce amplitude modulated output signals. The frequency range is determined by the mechanical structure and the helix in particular and, for the simple helix, it is roughly an octave about the centre frequencies from 1 to 9GHz.

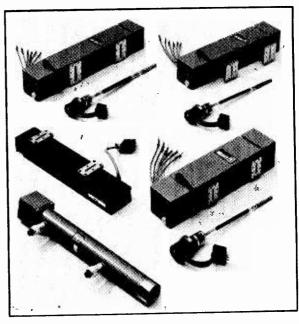
Power levels for continuous operation are usually 1 to 10W but kilowatts are possible while operation in pulsed modes can result in peak power levels in the megawatt region. The band-width at high power levels is usually reduced to as low at 10% or 400MHz at 4GHz.

Both forward and backward wound helices are used and typical gains in the X band are in the region of 30 to 40dB, with noise factors of 20 to 28dB. Generally they are designed to fit into special mountings which incorporate the permanent magnet systems. The input and output are usually taken directly from waveguide connections, with the forward wave tubes operating as amplifiers and the backward wave tubes as oscillators. Typical forward wave types are LB4-20 and 30, at 4GHz and LB6-15 to 25 at 6GHz, with backward wave oscillators like the YH1100 and BA16.

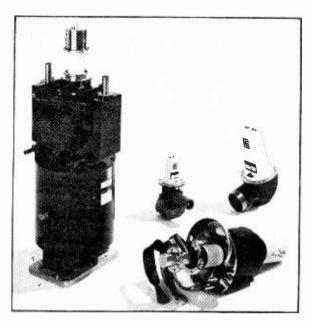
MAGNETRONS

These are essentially high efficiency oscillator valves and are used for producing fixed frequency, fixed amplitude oscillations and, in a pulsed mode, are widely used in radar equipment. The normal frequency is in the X band $(5\cdot 2 \text{ to } 10\cdot 9\text{GHz})$ although other bands are covered.

The magnetron, as illustrated in Fig. 4, consists of one or more very carefully machined cylindrical cavities with a cathode adjacent to the cylinder and formed of a thin wire. A permanent magnet provides



A selection of travelling wave tubes used for communications in the S, C and X-bands. Three are replaceable types, shown beside their mounts.



In this collection of magnetrons the large one is an L-band 2·3MW tunable pulse magnetron intended for high power surveillance radar. In the foreground is a 25kW CW model for industrial use. The remaining two magnetrons are rated at 50kW and 900kW pulse operation in the S-band.

a magnetic flux at right angles to the cylinder and thus at right angles to the electric field formed by the diode. Electrons released from the cathode travel in a circular path and at a given frequency just graze the anode. The oscillation frequency is determined by the physical characteristic of the cylinder and therefore is often fixed. Slight tuning is however provided with some magnetrons.

Continuous-wave magnetrons are available in the frequency range 8 to 9.5GHz at power levels of 6W to 20W. Typical operating conditions are Va=1kV, Ia=50mA, Vh=6.3 and Ih starting at 1A. Typical types are JPT 9-01 and JPG 8-01.

Pulsed magnetrons are designed for short pulse durations in the region 1 to $5\mu s$ for X band devices at approximately 9GHz. Power outputs range from 25W to 50kW with devices such as JPT9-02 and YJ1050. The lower frequency $1\cdot 25$ GHz (L Band) and $5\cdot 5$ GHz (C Band) devices operate at higher power levels up to 1,000kW.

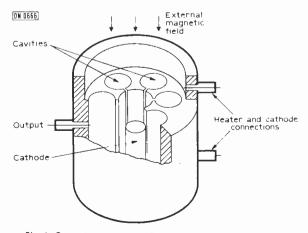


Fig. 4: General arrangement of a multiple cavity magnetron.

FUTURE TRENDS

Although trends continue towards the use of semiconductor devices, the power transmitter valve at all frequencies cannot yet be replaced directly. Thus power valves at all frequencies are still of very considerable use and development continues to improve all these designs.

A trend which undoubtedly will continue is the replacement of high power microwave transmitters by low power solid state components such as varactor chains. This has been made possible by improved receiver and aerial design.

We are indebted to the English Electric Valve Co. of Chelmsford for permission to reproduce the photographs in this article.

TO BE CONTINUED

TELEVISION

MAY ISSUE

THE LID OFF VARICAPS

What exactly is a varicap tuner, how does it work and what goes wrong with it? This month Keith Cummins looks at all aspects of varicap tuners and sums up the pros and cons. Including an insight into the tricky servicing problems that can arise with their use.

TRANSISTOR IF PREAMPLIFIER

It is often worthwhile converting dualstandard sets to single-standard operation and fitting a modern transistor u.h.f. tuner. When this is done it is convenient to remove the v.h.f. tuner, but this usually means the need for extra gain between the u.h.f. tuner and the i.f. strip. A simple transistor i.f. preamplifier that has been used in converting sets such as the BRC 850 chassis is featured this month.

ASSESSING COLOUR RECEIVER PERFORMANCE

In the concluding article in his series E. J. Hoare provides a detailed account of how to assess the colour performance of receivers—purity and convergence etc. and the operation of the colour circuits.

SERVICE NOTEBOOK

Amongst the items in George Wilding's Service Notebook this month is a detailed procedure for tackling that common condition, lack of e.h.t.

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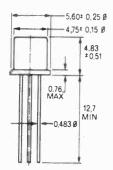
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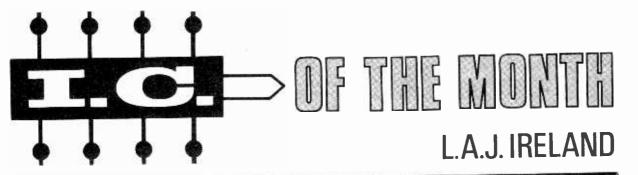
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EF183	20p	18Y9	10p	30F5	l2p
EF184	20p	PY801	17p	30FL1	20p
		PVPAA	170		



Number 37

SGS NE555 Precision Timer

highly stable timing device, type NE555, recently released by SGS, is the topic for this month's article. It allows precision timing from microseconds to hours with a mere handful of components; its uses however are not limited solely to the timing field as it can also find wide application in such diverse spheres as pulse generation, frequency division, pulse-width modulation, etc., to mention but a few. Such versatility coupled with low cost should make it an attractive i.c. to the amateur experimenter and a few of its more interesting features and applications will be outlined in the following notes.

Applications

A block diagram of the NE555 is shown in Fig. 1 and the first application to be considered is its use as an accurate timer, Fig. 2. The timing period is set by one additional resistor capacitor network with additional terminals allowing control over the triggering and resetting of the device. The external

Control voltage 5 Şĸ Threshold o Comparator 2 o Trigge Comparator 4_{o Reset} Discharge o Flip-flop Output stage Įз ļ١ CKG407) Farth Output

Fig. 1: Block diagram of the NE555 timing device.

capacitor connected between pin 7 and earth is initially held discharged by the short circuit path of the saturated transistor Trl. When a negative trigger

pulse is applied to pin 2 the flip-flop changes state and biases off Tr1 thereby allowing C1 to charge via R1. The time constant associated with R1C1 determines the rate at which C1 charges and when its voltage reaches 2 ₃ $V_{\rm cr}$ the threshold comparator

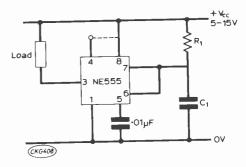


Fig. 2: Typical application of the NE555. The values of R1 and C1 for a delay of 1 second would be 1M Ω and 1 μ F.

resets the flip-flop and discharges C1 in addition to providing an output pulse at pin 3. One of the great advantages of this type of circuit is that the timing rate, for all practical purposes, is independent of the supply voltage. Timing periods from as short as 1 microsecond to as long as 1 hour may be obtained with this rather simple arrangement.

Multivibrator

Another interesting application of the NE555 is obtained when pins 2 and 6 are joined together as illustrated in Fig. 3. Here the device is operated as

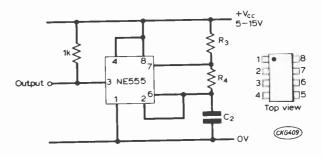


Fig. 3: In this circuit the NE555 is used as a free-running multivibrator.

a free-running multivibrator with the frequency and duty-cycle set by the R3-R4-C2 arrangement. The combined value of R3 and R4 in conjunction with C2 determines the frequency while the duty cycle is set by the ratio R3/R4. As the transistors fabricated in the silicon chip are of the highest quality excellent square waves are obtained from the output at pin 3. Once again, in this arrangement the operating frequency is independent of the power supply voltage.

Pulse-width modulator

The final application of the NE555 to be considered is its use as a pulse-width modulator. Here an external square wave generator's output is connected to pin 2 with the modulating signal applied to pin 5 as indicated in Fig. 4. (Incidentally, another NE555 operated in the astable mode will function quite well

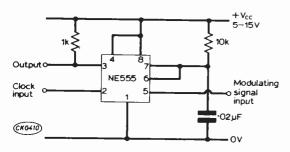


Fig. 4: Yet another application is as a pulse-width modulator.

as the clock generator.) As the control voltage on pin 5 increases, it affects the threshold voltage of the comparator resulting in an increase of the pulse width. The exact opposite occurs as the modulating voltage decreases so the output train of pulses obtained at pin 3 has a frequency identical to the clock input frequency with the pulse width controlled by the modulating signal.

A few of the more interesting applications of the NE555 i.c. have been reviewed in this article and further uses of the device are left to the ingenuity of the experimenter. The NE555 is available from Quarndon Electronics Ltd., Slack Lane, Derby.



Improving VHF Radio April PW

Although our information was taken from a normally reliable valve and transistor manual the connections for the BF200 transistor in Fig. 6 were incorrect. They should read, clockwise from the tag: emitter, base, collector and shield.

Receiver Matching Unit E.G.RAYER

AN end-connected wire of random length is often used as a short wave aerial and this can, in fact, give good results if reasonably high and clear of earthed objects. At some frequencies, when the aerial length is a half wave or multiple of a half wave, the end impedance at the receiver can be very high, over 1000 ohms. At the other frequencies (a quarter wave or odd number of quarter waves) the impedance is low, probably under 50 ohms. Therefore, for an efficient transfer of energy from the aerial to the receiver at all fre-

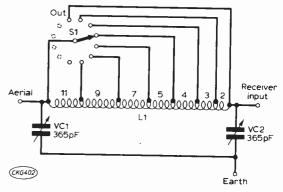


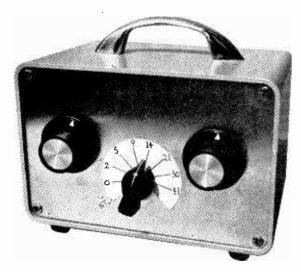
Fig. 1: above, shows the circuit of the receiver matching unit. When switched to "Out" the two variable capacitors should be turned to minimum capacity.

quencies, some matching device is needed. The one described here covers about 3.5MHz to 30MHz, and it is over this range that such an accessory is most likely to prove useful.

THE PI NETWORK

In the circuit, Fig. 1, the tapped inductor L1 has a variable input capacitor VC1 and variable output capacitor VC2. A 12 position rotary switch S1 allows turns to be selected as follows—0, 2, 5, 9, 14, 21, 30, and 41, the last four positions remaining unused. This switch and adjustment of VC1 and VC2 allows a wide range of aerials to be matched to the receiver.

Many communications receivers have a nominal aerial input impedance of about 75 ohms while others, and especially some popular older models, are 600 ohms. On some frequencies the aerial may chance to match the receiver. The Receiver Matching Unit will then give no improvement in signal strength, but can be left in circuit by setting VC1



and VC2 at minimum and the switch at "0".

At other frequencies the switch is progressively rotated to bring more turns into circuit, each time adjusting VC1 and VC2 for best results. This is merely a matter of peaking the matching unit controls for best volume, or best S-meter reading. Where the mis-match is bad, quite a significant improvement should be had. If peaking the signal by ear, switch off the receiver a.g.c. or choose a weak signal or adjust for maximum general noise picked up by the aerial.

capacitors. Solid dielectric components are not recommended. A value of 350pF or so is useful for the lower frequencies, but for the h.f. bands only 200pF or even 150pF capacitors may be suitable, if to hand.

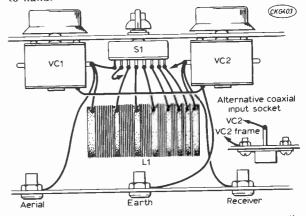
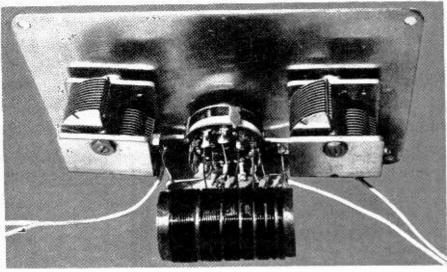


Fig. 2: Wiring diagram of the matching unit. Unused positions on the switch have been ignored.

Fig. 2 shows construction, the coil being supported by its leads. The plastic case used was $6\times4\times4$ in. but had no removable back, so flying leads were left just long enough to reach Aerial, Receiver, and Earth terminals fitted at the rear. Communication receivers often have a 75 ohm co-axial aerial input socket when a co-axial socket can be fitted to the



The photograph, right, shows the author's prototype unit. The multiple leadouts from the coil are sufficient to hold it firmly on the switch.

The coil is wound with 22 s.w.g. enamelled wire on a paxolin tube 1in. in diameter and about 2in. long. Anchor the wire through small holes near one end. Wind 2 turns side by side, and twist a small loop. Leave a space of about 116 in. and wind 3 turns, making a further loop. Continue in this way, adding 4, 5, 7, 9 and 11 turns, with a small space between each section. Scrape all the loops and solder on leads for the switch.

Solder the leads to the switch so that the first position shorts the whole coil, subsequent positions leaving 2 turns, 5 turns, 9 turns, and so on, in circuit, position 8 having no connection so that the whole coil is in use.

VC1 and VC2 are each 365pF miniature air-spaced

back of the matching unit. The inner conductor of the co-axial lead to the receiver will be the aerial lead, and the outer braiding will act as the earth connection no earth being needed on the unit.

The switch has a scale showing the number of turns in circuit. The lowest frequency reached depends on the aerial and receiver, but can extend down to 1.5MHz in some cases. On some ranges, the unit is useful in reducing second channel interference. If a numbered dial is fitted to each capacitor a very useful chart can be made up showing dial readings and switch positions for the various amateur and short wave broadcast bands, which will considerably shorten the time taken to tune the unit to any particular frequency.

INNEXTMONTH'S

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PRACTICAL WIRELESS

SIMPLE PROJECTS FOR THE HOME

8 PAGE SUPPLEMENT



This oscillator produces a pleasing tone, different in frequency for either of two doors. By using a suitable centre-tapped transformer T1, the collector circuit of each transistor can drive the base of the other transistor.

Assembly is on a perforated srbp board and wired as in Fig. 2. This board is fitted in the speaker cabinet or to a flat speaker panel fitted across the corner of the room.

One push-button switch is wired to A, and the other to B. The return leads of both switches go the common terminal C. When one switch is operated both R1 and R2 are in circuit, while with the second push R2 only is present. Wires A-C can run to the front door, and B-C to the back door.

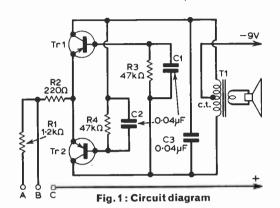
The note can be altered by changing the resistance of R1 or R2 or the capacitance of C1, C2 or C3.

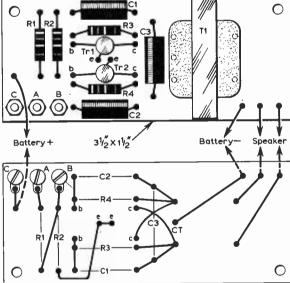
Connections for OC81, NKT271: collector wire nearest spot, then base, emitter.

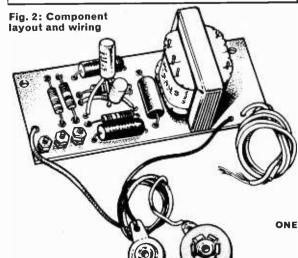
components

resistor $1.2 k\Omega \pm 10\% \ \pm w$ resistor $220\Omega \pm 10\% \ \pm w$ resistor $47 k\Omega \pm 10\% \ \pm w$ resistor $47 k\Omega \pm 10\% \ \pm w$ R₁ R2 R3 R4 capacitor 0·047μF polyester capacitor 0·047μF polyester C1 C2 C3 capacitor 0.047µF polyester Tr1 transistor OC81 or NKT271 transistor OC81 or NKT271 Tr2 transformer 9.2:1 CT primary, type T/T7 Repanco Loudspeaker 3 Ω 5in. and wooden board 12in. \times Battery 9V type PP6 or PP9 with connectors Perforated srbp component board Nuts and boits 6BA, soldering tags, pvc wire

SUPPLEMENT TO PRACTICAL WIRELESS-MAY 1973







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Ready-made amplifier module used to give press-button calling and communication in both directions. Fig. 1 is the complete circuit.

MASTER UNIT



S1 is the "push-to-call and push-to-speak" switch. When it is pressed, the circuit is completed in such a way as to cause an audio tone (R1 limits current in this condition). S2 switches the unit on so that the master position may speak to the remote position, or vice versa. S3 at the remote unit causes a tone at the master unit, to gain attention.

At the master unit, press S1 a few times to gain attention, then close S2, with S1 released to listen. Press S1 again to speak. Switch off with S2 when contact is finished. At the remote unit, press S3 a few times to call master unit and await reply. VR1 is set to a suitable volume level, and is ready wired to the 4-300 unit.

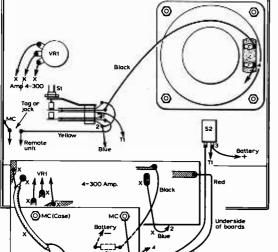
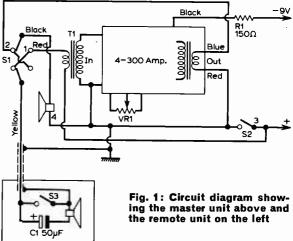


Fig. 2: Wiring of module in the master unit on the left and partly cutaway view of remote unit

Aiready on 4-300 Amp

components

resistor 150Ω ±10% ‡ watt VR₁ potentiometer supplied with amplifier module capacitor 50μF 12V electrolytic C1 **T**1 transformer 9.2:1 CT primary, type T/T7 Repanco S1 2-pole, changeover spring loaded push button, type S746 with S768 operator, or type S415 Bulgin S2 single-pole, on-off toggle switch **S3** single-pole, on-off push button Loudspeakers 3Ω 2½in. or 3½in. Battery 9V type PP6 or PP9 and connectors Amplifier module type 4-300 Component board srbp 31in. × 21in. Case 8in. \times 6in. \times 6in. (Master unit) Case 4in. \times 4in. \times 4in. (Remote unit) PVC connecting wire and knob Nuts and bolts 6BA and 4BA Soldering tags 6BA



Numbers 1 to 4 in Fig. 1 refer to connection points 1 to 4 in Fig. 2. Fig. 2 shows the master unit. Two 6BA bolts secure the 4-300 amplifier and also the srbp board for T1 and R1. Solder coloured leads to S1 as indicated before fitting this item. Input and output circuits and T1 are continued on page three

SUPPLEMENT TO PRACTICAL WIRELESS-MAY 1973

A sensor, on the end of twin flexible lead, can be placed in a water tank, swimming pool, bath or wash-boiler. A buzzer sounds when the water level reaches the sensor.

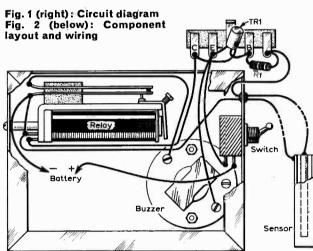
The minimum battery current drain is about 0.3mA; rises to about 400mA when water reaches the sensor.

Fig. 1 shows the circuit. The presence of water shorts the sensor probe and allows base current to flow through R1, resulting in a collector current of about 40–50mA to close the relay. The buzzer sounds until the sensor is removed from the water, or the device is switched off.

Fig. 2 shows all wiring, in a case made from aluminium. The tag strip (shown detached) is mounted vertically in the adjacent corner of the case. Space is left for a flat 3-cell 4.5 volt battery.

components

R1 resistor $10k\Omega \pm 10\% \frac{1}{2}$ watt transistor OC76 or any high gain pnp type S1 single-pole, on-off switch relay 100Ω coil, single-pole on-off contacts, 3-6V operation Battery $4\frac{1}{2}$ to 6V depending on relay obtained Buzzer $4\frac{1}{2}$ to 6V Sensor probe (see text) Case $6in. \times 4in. \times 2in.$ aluminium box or chassis with lid.



INTERCOM AMPLIFIER

continued from page two

positioned to avoid feedback which would cause instability. In addition to VR1, the 4-300 has a preset sensitivity control, which can be left at about the middle of its travel.

Easy connecting of a remote unit lead can be by a jack plug and socket, the outer conductor being the common positive return. Do not connect or disconnect while battery is switched on.

The equipment will operate as a baby alarm by placing the remote unit near the cot and closing \$2.

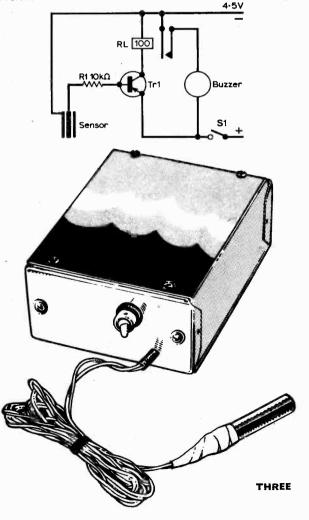
Connections to the 4-300 amplifier module are shown in Fig. 2, indicating appropriate copper pads used for connections. MC indicates connection made to the metal case by soldering tags. S1 does not necessarily need to resemble that shown in Fig. 2 but can be any style with the operation as in components list.

SUPPLEMENT TO PRACTICAL WIRELESS-MAY 1973



The sensor is made in coaxial form to avoid any accidental short (and wrong indication) by metal items. It has an outer metal tube about 2in. long by $\frac{3}{8}$ in. diameter, with a slightly shorter internal pin (actually a length of 4BA threaded rod). The inside part is fixed by a tight binding of insulating tape, or by an insulated sleeve. The sleeve and pin must not touch. Several feet of thin twin flex are soldered on, the sensor inner part going to R1.

An alternative probe can be a coaxial plug as used for TV aerial wire, although it must be kept free from corrosion.





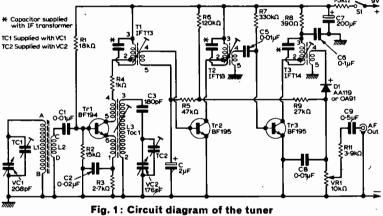
This portable medium wave tuner gives an output for a tape recorder or amplifier.

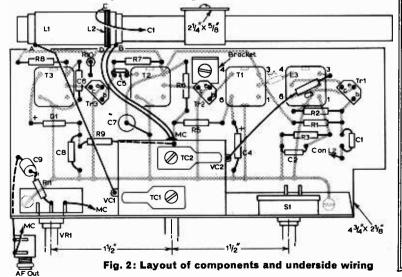
Note that the AA119 diode has a black mark to denote plus polarity; wrong polarity here will upset avc action. Components are positioned as in Fig. 2 and wired as shown in

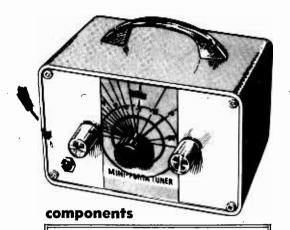
FOUR

grey. The perforated srbp board is bolted to the metal bracket carrying VR1, VC1/2 and S1. MC is the metal case connection.

A bracket, srbp strip, and strip of card wrapped round the rod and drawn tight with a







es		

R1	18kΩ	R7	330kΩ
R2	15 $k\Omega$	R8	390Ω
R3	2·7kΩ	R9	$27k\Omega$
R4	1kΩ	R10	1 · 5kΩ
R5	47k Ω	R11	3 ·9kΩ
R6	120kΩ		
ΔII	recietore	1 100/ 1	watt

All resistors ±10% ⅓ watt

Diode **Potentiometer** VR1 $10k\Omega$ log. D1 AA119 or **OA91**

Capacitors

- C1 0.01µF mica or ceramic
- C2 0.02μF mica or ceramic
- C3 180µF mica or ceramic
- C4 2µF electrolytic
- C5 0·01μF mica or ceramic
- C6 0·1μF polyester C7 200μF 9V electrolytic
- C8 0·01μF polyester
- C9 0.5μF polyester

(Note: C9 not required if used only with IC-12 audio amplifier)

Variable Capacitors

VC1 & VC2 208+ 176pF with trimmers type 00 Jackson (slow motion optional)

Preset Trimmers

TC1, TC2 fitted to VC1, 2

Transistors

Tr1 BF194 Tr2 BF195 Tr3 BF195

Coils

L1, L2 Medium wave ferrite rod aerial coil type MW/FR5 Denco

L3 Oscillator coil type TOC1 Denco

Transformers

T1 I.F. transformer type IFT13 Denco
T2 I.F. transformer type IFT13 Denco
T3 I.F. transformer type IFT14 Denco

Switch

S1 Single-pole, on-off toggle switch

Miscellaneous

Perforated srbp, 0.15in. matrix 43in. x 21in.

Control panel and bracket 43in. x 2in. aluminium

Nuts and bolts 6BA, pvc wire Case, insulated, of wood or plastic

SUPPLEMENT TO PRACTICAL WIRELESS-MAY 1973

This radio alarm is designed to awaken you at a preset time set on the clock movement, and to switch off automatically if required.

Use the "Tape Tuner" (page four of this supplement) with an integrated circuit audio amplifier. The synchronous clock runs from 250V a.c. mains and is supplied with contacts which are set by a front mounted control. A second control sets the duration, then automatically switching off. (A minute timer ringer is also provided, but is not used in this circuit.)

The master or programming switch, which is arranged as in Fig. 1 and shown in two views in Fig. 2, allows the radio to be switched on irrespective of the clock settings, or switched off separately, giving complete freedom of operation without any need to change clock settings.

components

Tape tuner as described on page four of Supplement Amplifier i.c. type "Super IC12" with heat sink (Sinclair)

Electric programmer clock as illustrated with switch contacts glass and bezel (various advertisers) Loudspeaker 8Ω to match IC12

Switch single pole, 3-way to select operation Connection block, 3-way for mains connection Fabric or expanded aluminium speaker grille Case approx. 10in × 7in. × 4½in.

A mains connector joins mains leads and clock leads.

The i.c. amplifier is mounted on brackets. The whole unit is powered by a PP9 9V battery. A mains unit could be fitted instead and several proprietary brands can be purchased or the reader can make his own. All units can be mounted in a suitable wooden case.

TAPE TUNER continued from page four nut and bolt hold the ferrite rod aerial.

The i.f. transformers T1, T2, T3 are pre-aligned but the effect of slight core adjustment can be tried. Adjust TC1 and TC2 at the high frequency (200 metres) end of the band, and the core of L3 (if necesary). The position of L1/L2 on the ferrite rod is adjusted at the low frequency end of the band.

Note that the specified case is insulated material, not metal to avoid screening the ferrite rod aerial. Audio output should be heard on high impedance phones connected to the output jack socket. The output is of high impedance and should be fed into the high impedance input of a tape recorder via screened cable (but see also the Radio Alarm Clock).

Transistor connections as indicated by top view in Fig. 2.

Alarm Clock

Radio

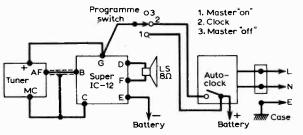
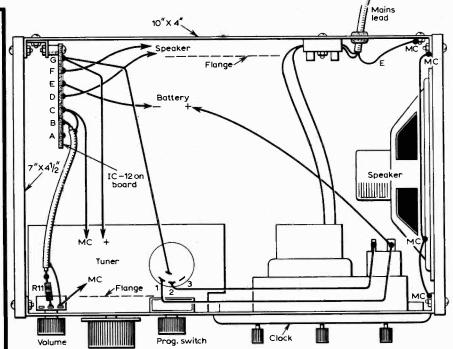
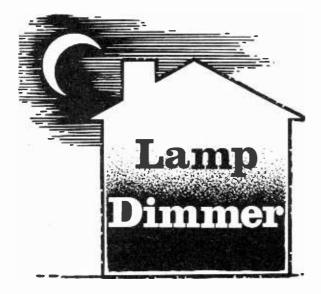


Fig. 1 (left): Circuit diagram
Fig. 2 (below): Component layout and wiring (the programme switch is shown twice for wiring detail)



SUPPLEMENT TO PRACTICAL WIRELESS-MAY 1973

FIVE



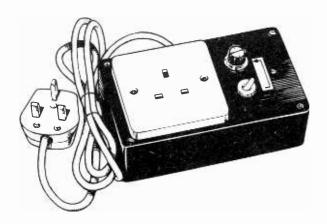
This lamp dimmer is constructed in an electrical switch box. The 40432 triac is rated at 0.5A without a heat sink, or 1A with the type 5F clip-on heat sink shown. With 240V a.c. mains, this is suitable for lamp loads of 120 watts and 240 watts respectively. An alternative triac type 40430 can also be used.

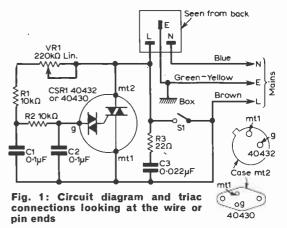
The dimmer can be fitted in place of an ordinary lamp switch. With the portable unit shown, the dimmer box and a 13A type outlet are assembled in a larger box. A table or standard lamp can be plugged into it, or it can be used for heat control of a soldering iron. This unit is not rated for power drills and is not suitable for them nor for fluorescent lamps.

Fig. 1 is the circuit, with wiring to integral 13A type outlet. The metal box, Fig. 2, provides screening. Complete closure by a metal plate was not found necessary. The triac case is connected, via a soldering tag bolted to the heat sink or case, to VR1. It must be insulated from the box and any other metal part. Flexible leads to VR1 and S1 allow these to be positioned in the front holes.

Assure proper earthing is maintained right up to any appliance controlled by the unit. The mains plug is fitted with a 3A fuse.

Triac connections shown in diagram.





components

R1 resistor $10k\Omega \pm 10\% \frac{1}{2}$ watt R2 resistor $10k\Omega \pm 10\% \frac{1}{2}$ watt R3 resistor $22\Omega \pm 10\% \frac{1}{2}$ watt VR1 potentiometer $250k\Omega$ linear C1 capacitor $0.1\mu\text{F}$ 1,000V d.c. or 300V a.c. C2 capacitor $0.1\mu\text{F}$ 1,000V d.c. or 300V a.c. C3 capacitor $0.022\mu\text{F}$ 1,000V d.c. or 300V a.c. CSR1 triac type 40432 with heat sink clip type 5F or triac type 40430 S1 Single-pole, on-off toggle switch 250V a.c. Metal electrical switch box $2\frac{3}{2}\text{in.} \times 2\frac{3}{2}\text{in.} \times 1\frac{1}{2}\text{in.}$ or $6\frac{1}{2}\text{in.} \times 3\frac{1}{2}\text{in.} \times 2\frac{3}{2}\text{in.} \times 1\frac{1}{2}\text{in.}$ or $6\frac{1}{2}\text{in.} \times 3\frac{1}{2}\text{in.} \times 2\frac{3}{2}\text{in.} \times 2\frac{3}{2}\text{in.}$

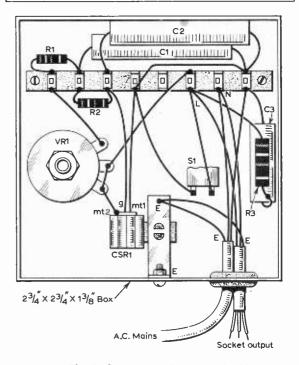


Fig. 2: Component layout and wiring
SUPPLEMENT TO PRACTICAL WIRELESS—MAY 1973

The input transducer is a small loudspeaker, followed by Tr1 and Tr2 as amplifiers. VR1 is a sensitivity control, allowing adjustment of the sound level at which the unit operates.

All components except the speaker and VR1 are mounted on the perforated srbp board in Fig. 2. Underside wiring is shown in grey. Points A, B and C carry connecting wires to VR1. Wires A and C are connected so that sensitivity increases as the control knob is rotated from the "off" position in the usual way. The case is an aluminium box or chassis.

Test by connecting a meter to the output terminals. A brief pulse of current is indicated when switching on, due to C5. The reading should then remain at zero, rising to 100-250mA while snapping the fingers or speaking quietly.

Place the unit adjacent to the source of sound. Where extraneous sounds may operate the unit, reduce sensitivity by turning back VR1 just enough to avoid this.

Twin bell wire or a long twin flexible lead run from the output terminals to the bell or relay. A diode 1N4148 should also be connected across the output terminals to suppress back e.m.f. through Tr4; diode plus to collector.

Connections for OC71, OC81: Collector nearest spot, then base, emitter.

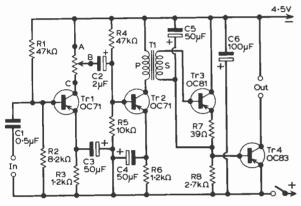


Fig. 1: Circuit diagram of the amplifier

components

Resistors		
R1 $47k\Omega$		10k Ω
R2 8·2kΩ	R6	1 ·2kΩ
R3 1·2kΩ	R7	39Ω
R4 $47k\Omega$	R8	2·7kΩ
All ±5% ¼w		
Detentionator		

Potentiometer

VR1 5kΩ with switch S1 attached

Capacitors

C1 0.5μ F polyester C4 50μ	F 6V electrolytic
	.F 6V electrolytic μF 6V electrolytic

Transistors

Tr1 OC71 Tr3 OC81 Tr2 OC71 Tr4 OC83

Transformer

T1 9.2:1, CT primary, type T/T7 Repanco

Miscellaneous

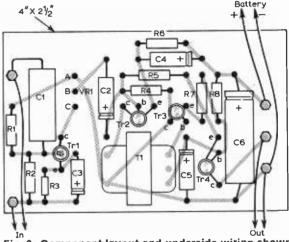
Miniature 40 ohm speaker Perforated srbp board 4in. × 2½in. Screw terminals or sockets

Case, aluminium or wood, 10in. \times 4in. \times 3in.

SUPPLEMENT TO PRACTICAL WIRELESS-MAY 1973



This alarm gives a warning by means of a bell, buzzer or lamp, so it can be used as a baby alarm, or as an extension for a door-bell or telephone bell. As it is sound operated, no direct connection is necessary to a telephone or other equipment.



in 2: Component layout and underside wiring shown



SEVEN



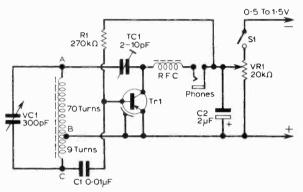


Fig. 1: Circuit diagram

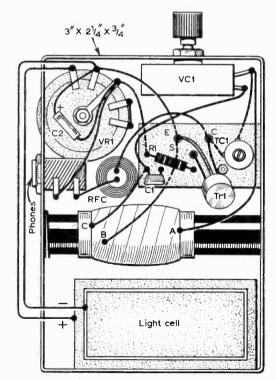
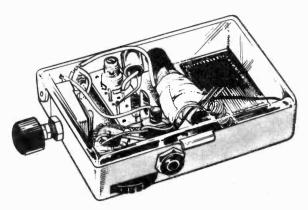


Fig. 2: Component layout and wiring

EIGHT



components

R₁

resistor 270 Ω \pm 10% $^{+}_{o}$ watt potentiometer 20k Ω miniature edge control with VR1 switch S1 C1 capacitor 0.1 µF low voltage capacitor 2µF 6V or higher electrolytic C2 VC1 variable capacitor 300pF mica dielectric

TC1 trimmer capacitor 2-10pF screw driver control Tr1 transistor AF117 or similar pnp type

RFC R.F. cored choke 5mH

> Ferrite rod &in. diameter, 2in. long Wire 26 s.w.g. enamelled copper wire for tuning coil

> Phones high impedance with jack plug and socket

Solar cell 0.5volt or dry cell 1.5V Component board 1 in. x in. and box

PVC connecting wire

Simple regenerative receiver providing headphone reception of local medium wave stations only. Power derived from a mercury cell when energised from daylight or good artificial light. A 1.5 volt dry cell can be used instead.

Tuned circuit consists of 79 turns of 26 s.w.g. enamelled copper wire (A to C) close wound on ferrite rod fin. diameter, in parallel with small tuning capacitor VC1. This coil has a tapping (B) nine turns from one end (C). Trimmer capacitor TC1 controls regeneration and is set so that oscillation is just possible with VR1 near maximum voltage setting when using a single 0.5V solar cell.

Tuning coil is wound on thin card or thick paper tube so that it can be moved along ferrite rod for best reception. A few feet of flexible wire aerial connected at A may help reception. Phones should be high impedance 2,000 ohms or more and connected via jack socket on box. Small components are mounted on perforated srbp board and wired underneath. Keep wires short. Minimum recommended box size 3in. x $2\frac{1}{4}$ in. x $\frac{3}{4}$ in. Connections for AF711: collector wire nearest spot, then screen, base, emitter.

COMPONENT SUPPLIES

Components should be readily available from several of our advertisers including the following: Arrow Electronics, Chromasonic Electronics, Electrokit, Electrovalue, Henry's Radio, Home Radio (Components), A. Marshall & Son, Trannies, J. Bull (Electrical) and others.

Sub-standard, unmarked or other components that are not as specified in components lists cannot be guaranteed as suitable substitutes. Constructors should satisfy themselves before buying.

SUPPLEMENT TO PRACTICAL WIRELESS-MAY 1973

TRICOLOUR

Mood Lighting System

PART TWO

JUREK BUDEK*



THE P.W. Tricolour provides a versatile but straightforward form of colour lighting effect that is much improved on earlier designs, due largely to the use of the principle of zero voltage switching. Last month's article explained how this was done so now it is time to do the construction and see the results.

Construction

In the *P.W. Tricolour* lighting system, the bass frequencies are 'presented' by the red lamps, middle frequencies by the green lamps and treble frequencies by the blue lamps. The control unit referred to in the following text is the *P.W. Tricolour* filter and control unit.

The construction of the control unit is not complicated if care is taken to follow the drawings and assembly notes. Before connecting any mains supply to any unit, double-check all wiring against the circuit diagrams (last month) and wiring diagrams, making quite sure that all thyristors, triacs and diodes are correctly connected.

It is recommended that sockets are used for mounting the integrated circuits. *Do* not solder the I.C.'s directly to the printed circuit board.

Assemble the eight way socket to the back panel in such a manner that when plug is inserted the five core cable to the lamps leads horizontally away from the fuse assembly.

The lights output socket is a Bulgin type P552 and the plug to fit this (for the lamps unit lead) is a Bulgin P551.

Attach the fuse holders, rubber grommets and speaker socket to the back panel. Assemble the components on to the printed circuit board, making sure that no accidental solder bridges occur across adjacent copper pads. The heat sink for the triacs is "live" and should not be connected to, or allowed to come in contact with, any metal part except the triac mountings, which are also the connections to their "main terminal 2". For safety connect this, the "zero" voltage indicated on the mains transformer, to the neutral terminal of the mains, and connect the control unit chassis to earth on the mains plug.

Insert the rubber grommet for the l.e.d. lamp

indicator into the front panel. Switches S1, S2, S3 and S4 are as used in the Texan amplifier.

The mains switch shown on the front panel uses detachable connecting clips, but any suitably rated mains switch is suitable. The front panel is mounted on the front of the chassis frame with spacers so that clearance of the control fixing nuts provides a neat and uncluttered appearance to the panel. The assembly

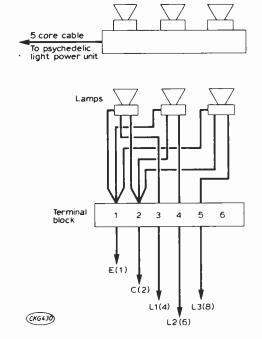


Fig. 13: The simplest arrangement in which one control unit drives three lamps, each 100 to 150 watts. E represents the earth or chassis connection via tag 1 on the Bulgin 8 pin plug|socket arrangement. The figures in parenthesis are the pin numbers. C is the common lead to the lamps—which is the 240V live lead. L1, L2 and L3 are the leads to the respective lamps shown as LP1, LP2 and LP3 (Fig. 12 last month).

^{*} TEXAS INSTRUMENTS LIMITED

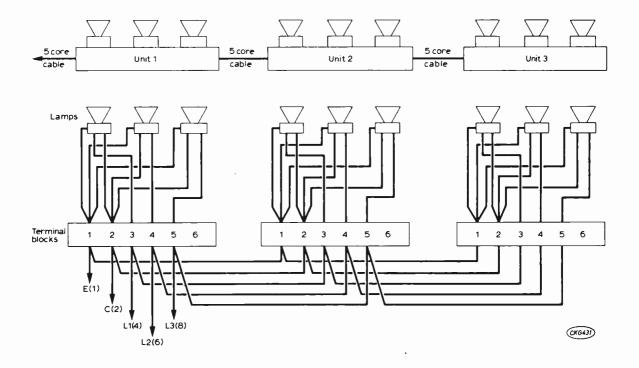


Fig. 14: Three banks of lamps, each 100w maximum, driven from one control unit.

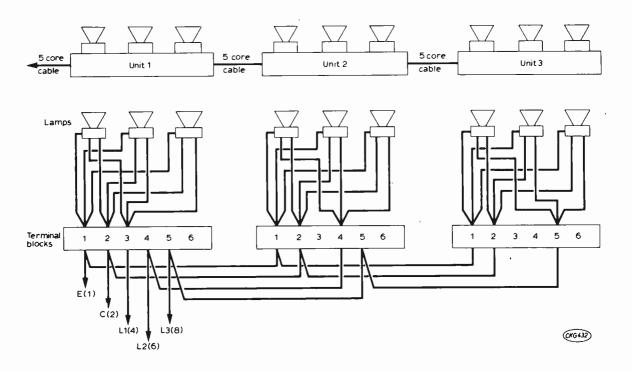


Fig. 15: Three banks of lamps, each 100W maximum, controlled by one frequency range.

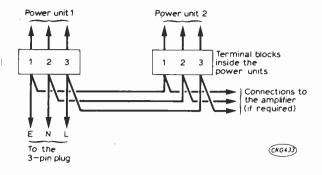


Fig. 16: Mains terminal block connections when using two control units.

uses 6BA nuts and bolts.

The three triacs and their associated heat sink uses 4BA nuts and bolts.

Fuses FS1, FS2 and FS3 are in the bass (red lamp), middle (green lamp) and treble (blue lamp) circuits respectively.

Unit Arrangement

The equipment consists of two units. One unit contains the control for the psychedelic lights, the filter circuits and the necessary power supply. It is advisable, but not essential, that this unit is located near to the 13A power socket and amplifier. The second unit is mobile and consists of three colour lamps mounted on a panel with a five core flexible cable attached to it. This unit can be hung on the wall, left on the table, or placed in some other convenient position.

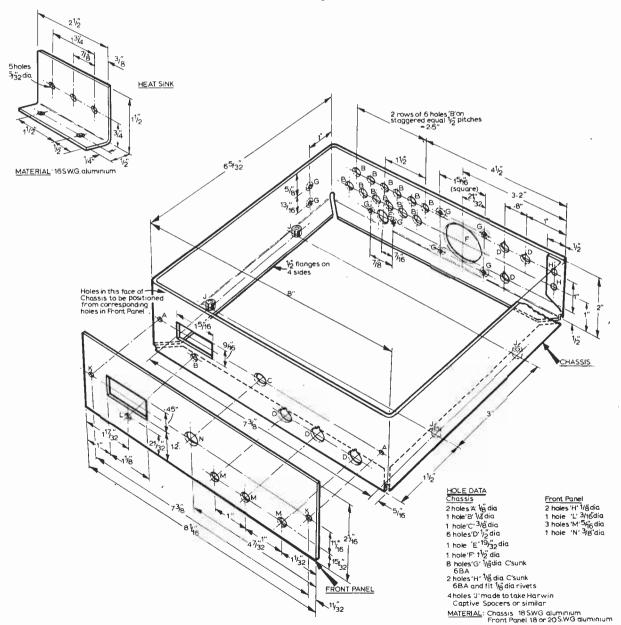


Fig. 17: Details of chassis construction and drilling with the heat sink shown top left, front panel left.

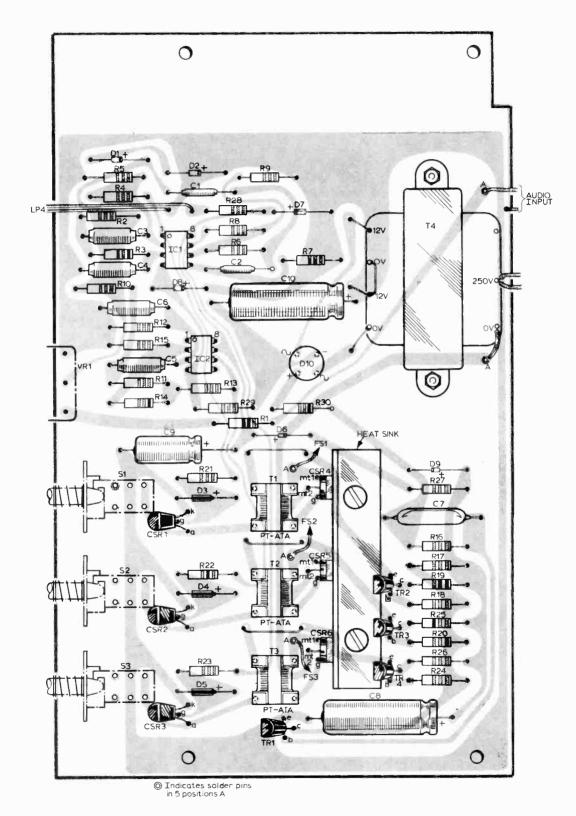
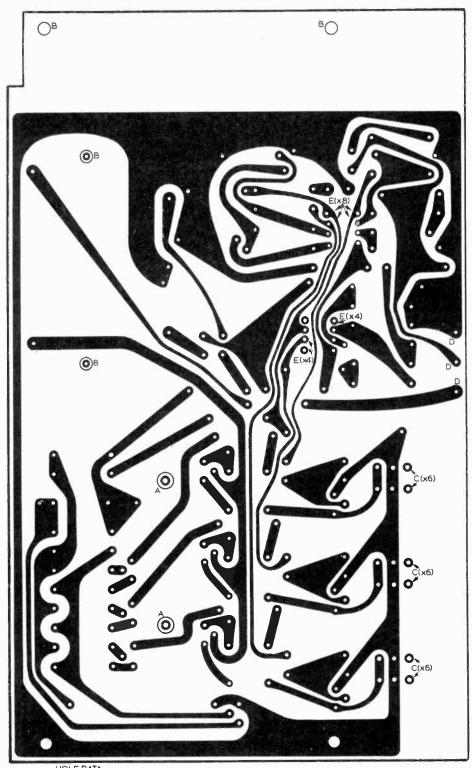


Fig. 18: Component layout and wiring to the printed circuit board. It will be observed that there are two leads from the 250V tag on T4. One lead is the live (L) lead from the mains terminal block. The other lead goes to tag 2 on the lights output socket.



HOLE DATA
2 holes 'A' ⁵/₃2' dia 3 holes 'D' 1.8 mm dia
6 holes 'B' ¹/⁸ dia 16 holes 'E' ¹/₃₂ dia
18 holes 'C' 1.3 mm dia
All other holes 1.0 mm dia

Fig 19: Full size pattern and drilling positions of the printed circuit board.

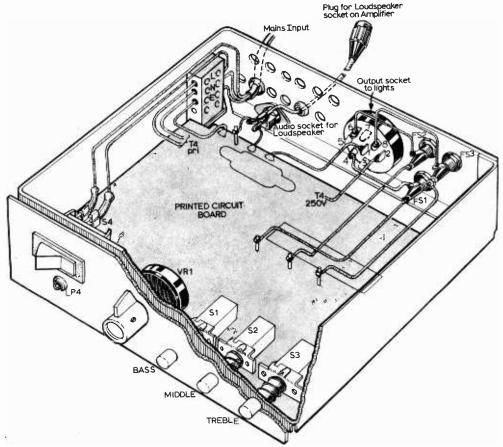


Fig. 20: Wiring of chassis mounted components to the printed circuit board. Tag 1 on the lights output socket goes to chassis (and mains earth). The live lead (L) from the mains terminal block goes to the 250V tag on T4 transformer.

The power control unit is capable of supplying three of these lamp units in parallel, each with its three coloured 100 watt lamps, i.e. a total power capability of 3×300 watts. Each lamp unit has a six way terminal block for interconnecting as shown in the diagrams.

Fig. 13 shows the connections for a single lamp unit. The five core cable is terminated with a plug suitable for connecting to the control unit. The figures in brackets show the pin numbers on the plug used. Connected thus, the three lamps will flash in accordance with frequency ranges present in the music.

Fig. 14 shows a triple unit arrangement, where each unit is connected in the same way as shown in Fig. 13. Here, however, the overall light level is increased and flexibility of lamp positioning is allowed, each lamp unit maintaining its three frequency range response.

A great deal of experimentation of lamp arrangement is worthwhile to achieve the best effect to suit your room and music. Fig. 15 gives another arrangement, using three lamp units, which is basically similar to that shown in Fig. 14, except that here each lamp unit will flash according to one frequency range.

The interconnections between speaker, amplifier and control units are also straightforward. Simply connect the speaker's DIN plug into the control unit and then plug in the cable from the control unit, now terminated with a DIN plug, into the amplifier. This should be done while all power is switched off. The amplifier should be connected via the control unit to a suitable loudspeaker before switching on.

The arrangement for a stereo system is very simple. Two control units and two lamp sets are required. A three core cable from a 13A socket is connected to the terminal board of control unit 1. From the same terminal board the second three core cable is connected to control unit 2 as shown in Fig. 16.

The advantage of this arrangement is obvious, i.e. only one 13A plug is used for both control units. If required, the power supply to the amplifier can also be taken from the terminal board of control unit 2 as shown in Fig. 16, thus achieving further simplification.

The interconnections between the control units, amplifier and speakers are similar to that described for the mono system but duplicated. Connect one speaker DIN plug into control unit 1 and then plug in the cable from it into the amplifier socket. This is repeated for the second speaker and control unit.

The effectiveness of the association of the light and music can be further improved if the lamps are placed near the speaker from which they are actuated. It is extremely effective when standing each lamp unit on or behind each speaker cabinet and projecting the lights up the walls behind.

The printed circuit board shown in this issue is for the zero voltage control version of the *P.W. Tricolour* only. A different printed circuit board, alternative components and slight alterations to the metalwork will be required for the version with lamp dimming facilities.

TO BE CONTINUED



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ADJUSTABLE SPANNER

The picture shows a self-adjusting spanner suitable for all nut sizes from $\frac{7}{6}$ in. to $\frac{13}{8}$ in. A.F.

The end of the tool is placed over the nut and turned until the "tongue" of the spanner locks onto the nut.

It is constructed from chromevanadium steel and weighs $5\frac{1}{2}$ ozs. Finish is either matt (£1·49) or polished (£1·79). Thunder Screw Anchors Ltd., Victoria Way, Burgess Hill. Sussex, RH15 9NF.

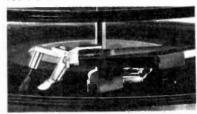


TUAC EQUIPMENT

Tuac Ltd., are marketing a new range of ready-assembled modules and complete units. They are a "waawaa" unit, fuzz box, disco "auto fade", octave doubler and a phase-splitter.

Leaflets which are issued in conjunction with Tuac kits can be obtained on receipt of a 3p stamp from: Transistor Universal Amplification, Co. Ltd., 163 Mitcham Road, London, SW17 9PG.

AUTO GROOVE-KLEEN



If you have an autochanger record playing unit, you have not been able up to now, to use a groove-cleaning brush to remove the dust and dirt from the records.

Bib seem to have solved this problem with their model 45 unit which just sticks onto the cartridge housing. Obviously to avoid any increase in stylus weight, the tone-arm should be re-balanced or the calibration control reduced by two grammes.

Due to the design, the velvet shoe and brush will not drag across the record when the tone arm moves from the end of one record to the outside of the record stack.

After the records have been played, the velvet shoe can be lifted off for cleaning with the separate brush supplied.

The price of this unit is 98p plus tax. Bib Sales, P.O. Box 78, Hemel Hempstead Herts.

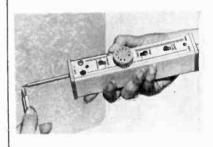
GUIDE TO SEMICONDUCTORS

Motorola Semiconductors Ltd. have published a "master selection guide". It includes in its 150 pages brief technical details of 17 dlode families from 4-layer to zener, hybrid circuits, microwave devices, optoelectronic components, rectifiers, triacs, dlodes, linear integrated circuits and much more than we can describe here. The guide, which is free of charge, may be obtained from Motorola Semiconductors Ltd., York House, Empire Way, Wembley Middlesex.

TRANSISTOR TESTER

Transistor tester type TT169 has been announced by Avo. It is designed for GO/NO-GO in-circuit testing of p.n.p. and n.p.n. signal or power transistors. The tester is battery operated and small enough to be held in the hand. Front panel lights show whether a device is faulty or OK.

The TT169 comes with all the necessary leads and connector in a plastic case. The price is £17-50 plus VAT and readers may obtain them from the usual retailers and distributors. Avo Limited, Avocet House, Dover, Kent.

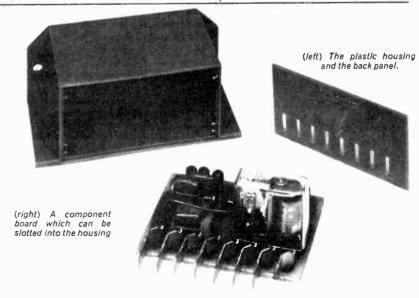


COMPONENT HOUSING TYPE LK8

Logikontrol Ltd., announce a compact component housing. It is made from high impact polystyrene and measures 90 x 50 x 37m.m. and at 25 · 4m.m. to the inch, you can work it out for yourselves! The internal volume is 10c.c. and it has facility for 2 printed circuit boards on which the components can be mounted.

Printed circuit connections and a snap-fit lid eliminate the need for a special plug and socket.

These units which are available in five different colours may be obtained from large component suppliers or in quantities of 10 upwards from Logikontrol direct, the 10 off price being 22p each. Logikontrol Ltd., 17 Little Edward Street, London, NW1 4AT.



150-80) metre CONVERTER

R.A. PENFOLD

HIS is a simple device which is easy to construct and which when placed ahead of a medium wave receiver will enable it to cover the 80 and 160 metre amateur bands. The unit is self contained, and is housed in a diecast box measuring 4^3_4 in $\times 3^5_4$ in $\times 2^5_3$ 2in. An external long wire aerial and an earth are required.

Only two transistors are used, including a fieldeffect type in the mixer stage. Frequency stability is excellent as the oscillator is crystal controlled.

Heterodyne Principle

What is required of the converter is to receive a signal in either the 160 or 80 metre band and change this signal to a frequency which lies in the MW band. This can be achieved by heterodyning.

This is a process in which two signals are mixed to produce at the output, (a) the original two frequencies, (b) the sum of the two, and (c) the difference between the two. By the use of tuned circuits in the output, whichever of the two new frequencies produced is required can be selected.

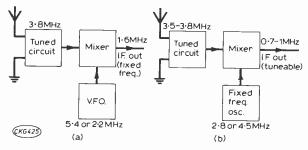


Fig. 1: Diagrams showing methods of converting a signal to a fixed or variable intermediate frequency.

The manner in which this process can be used in a converter is shown in Fig. 1. In the type of converter shown in Fig. 1a, the circuit is arranged so that the frequency to which the tuned circuit at the input is tuned is different from the operating frequency of the oscillator by the i.f. The tuning capacitors for the aerial tuned circuit and the oscillator would be ganged.

An example is given in the diagram of how a $3.8 \mathrm{MHz}$ signal is converted to a $1.6 \mathrm{MHz}$ i.f. There are two oscillator frequencies which will allow this $(3.8-1.6=2.2 \mathrm{MHz})$, or $3.8+1.6=5.4 \mathrm{MHz})$. In this type of converter the receiver is tuned to the i.f., and the tuning is carried out on the converter.

A second type of converter is shown in Fig. 1b. This type is often used in 2 and 4 metre VHF

amateur band converters. This time the tuning is carried out on the receiver, the oscillator on the converter being at a fixed frequency. The aerial tuned circuit should either be a broadband unit i.e. resonant over the entire band which is to be tuned, or should be tuneable over this range. Again there are two possible oscillator frequencies $(3 \cdot 8 - 1 = 2 \cdot 8 \text{MHz}, 3 \cdot 5 - 0 \cdot 7 = 2 \cdot 8 \text{MHz}, 3 \cdot 8 + 0 \cdot 7 = 4 \cdot 5 \text{MHz})$

This type of converter has the advantage that the oscillator can be crystal controlled, simplifying alignment and giving very good stability. This type is also very much more simple and inexpensive. The system does have drawbacks as discussed later but the author's converter, which is of this type, has proved very successful.

Practical Circuit

A circuit diagram of the converter is shown in Fig. 2. Tr2 is operated as a Pierce oscillator the crystal being used on its parallel resonant frequency. The primary winding of the oscillator r.f. transformer, L5, forms the collector load for Tr2. R2 biases the transistor, C3—C5 produce a centre tap on the crystal, this centre tap being earthed.

Tr1 is the f.e.t. mixer stage. L1 is the aerial input coupling winding and L2 the aerial tuned winding. This can be tuned over the range 70-230 metres by VC1. Tr1 is used in the common-source mode, source bias being provided by R1 and C1 is its decoupling capacitor. Tr1's source and R1 are connected via the

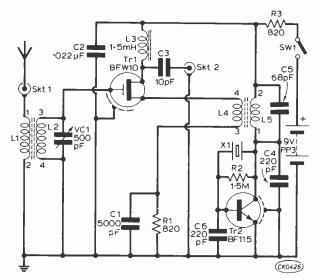


Fig. 2: Complete circuit of the converter unit.

secondary winding on the transformer, L4. The voltage across L4 modulates Trl's drain and source voltages and thus mixes the oscillator signal and the input signal. A small r.f. choke, L3, forms the drain load for Trl, the mixed output being coupled to the receiver via C3.

SW1 is the on-off switch, and R3 reduces the 9V supply to the required level. C2 is the supply de-

coupling capacitor.

The crystal frequency is chosen so that it can be used to convert signals in both the 80 and 160 metre bands to the MW band, the desired band being selected by tuning VC1—L2 to the correct frequency. Using a 2·8MHz crystal the 80 metre band will be converted to 0.7-1 MHz (3.8-2.8=1,3.5-2.8=0.7), and the 160 metre band will be converted to 0.8-1 MHz (2.8-1.8=1,2.8=1,2.8=1,3.

It is not essential for the crystal to operate exactly on 2.8MHz, as if it is a little either side of this frequency the converter will still operate but the tuning range on the receiver over which the amateur bands are covered will be slightly altered. A 2.794MHz crystal was used on the prototype.

Construction

The circuit is housed in an STC diecast box. The wiring is broken into two sections, a 5-way tagstrip on which the oscillator is constructed, and a 6-way

tagstrip on which the mixer is built.

Diagrams illustrating the wiring of these two tagstrips are shown in Fig. 3 (mixer) and Fig. 4 (osc.). These two diagrams also show all other wiring of the converter. All the wiring is quite straightforward and should present no difficulty, even to a beginner. The only point which should be noted is that the screen lead of Tr1 is too short to reach to the appropriate tag unless a short piece of insulated wire is used to lengthen it.

Figure 5 shows the interior layout of the unit and also gives details of the mounting bracket of the crystal. This bracket is constructed from 18-22 swg sheet aluminium. The two tagstrips are mounted by $^{1}2$ in 6BA bolts, a stand-off insulator $^{1}4$ to $^{3}8$ in long being used to hold them clear of the sides of the case.

The battery is held in place by being trapped between the front, and rear of the case. A pad of expanded polystyrene, foam rubber or a similar material should be glued to the rear of the case where the battery would otherwise come into contact with it. This is to make it fit more firmly and to insulate the battery terminals from the case.

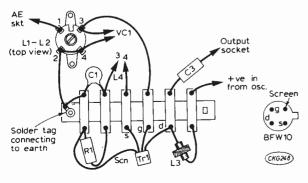


Fig. 3: Method of wiring the mixer stage components.

* components list

Resistors R1 820Ω All ‡W, 5 per cent types 1.5MΩ > R2 820Ω R3 Capacitors C1 5000pF 0.022μF polystyrene etc. C2 C3 10pF ceramic or silver mica C4 220pF polystyrene or silver mica C5 68pF polystyrene or silver mica C6 220pF polystyrene or silver mica Semiconductors Tr1 BFW10 or similar f.e.t. Tr2 BF115 Miscellaneous L1/2 Repanco RA3; L3 miniature r.f. choke, about 1.5mH; L4/5 Repanco RO3; SW1, on-off switch; STC diecast box, size 2 (4½ x 3½ x 2 ½in.); HC6U crystal, about 2 8MHz with holder (see text) (Henry's Radio); 1-off each 5-way and 6-way tag strip; 2-off coax sockets; Knob; Battery and clip.

As supplied, the exterior finish of the diecast box is rather rough and dirty. If the case is to be painted it will be necessary to thoroughly clean it first with a scouring pad. If preferred it can be cleaned in this way, and then polished to a bright natural finish.

Using the Converter

An external aerial is required; this merely consists of a length of wire which is mounted as high as possible and is as long as possible. An earth of some sort is essential for the correct operation of the circuit, although this does not necessarily have to be a very efficient one. The prototype is fitted with coaxial sockets for the aerial, earth and output connections.

Ideally the converter should be used in conjunction with a broadcast receiver which requires an external aerial. The receiver and the converter are connected by a short screened cable. In this way there is a minimum of interference picked up on the MW band directly by the receiver.

It was found possible to use the converter with an

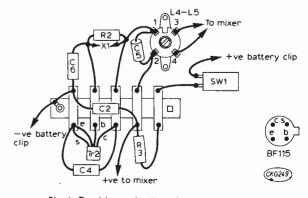


Fig. 4: Tagstrip construction of the oscillator stage.

ordinary transistor receiver. C3 should be removed, and a piece of wire connected in its place. It is then merely necessary to take a short lead from the converters output socket, and to place this alongside the receiver's ferrite aerial.

In this way it was found possible to receive a number of amateur stations on both the 80 and 160 metre bands. MW stations received directly by the receiver can prove bothersome, especially after dark.

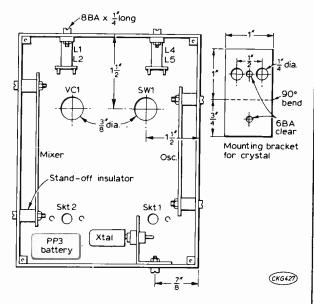


Fig. 5: Layout of components and tagstrips inside the die-cast box.

Operating the controls on the converter is very simple, as there are only two. SW1 is the on-off switch. VC1 tunes the converter to the desired band. With this control turned almost fully anti-clockwise it should be found possible to tune the 80 metre band and with it turned almost fully clockwise it should be possible to tune 160 metres.

With VCl approximately adjusted in this way, it should be possible to receive a few signals. VCl can then be peaked for maximum sensitivity. A simple dial can be marked around the control knob of VCl showing the areas over which the amateur bands are tuned.

Results

Using the converter with a 132ft. longwire aerial at about 20ft., in conjunction with a 6 transistor MW portable receiver, a large number of amateur stations have been heard. The 160 metre band is of course used mainly for local working, and a.m. is still used to a certain extent. Stations up to about 50 miles distant have been received on this band without too much difficulty.

Due to its simplicity, the circuit does have one drawback. Top Band is not only used for amateur transmissions but also for maritime ones. These transmissions are fairly powerful and occasionally when tuning the 80 metre band transmissions from ships in the nearby Thames estuary did break through. Conversely, a local amateur using a powerful SSB transmitter on 80 metres did tend to break through on the 160 metre band.

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BROADCAST BANDS

SHORT WAVE RECEIVER CHOICE by MALCOLM CONNAH

By far the largest portion of my mailbag consists of letters from readers asking my advice on the choice of a receiver. I have often said that this is a very difficult subject on which to give advice, partly because the letters give very little information and partly because "one man's meat is another man's poison".

In order to assist the less technically minded reader to select a receiver to meet his requirements I am going to devote this article to discussing the various features of receivers which are important

for good short wave reception.

1. Frequency Coverage: The most common type of receiver is the General Coverage Receiver. This type of receiver usually tunes from 540kHz to 30MHz in four bands. One of these bands covers the medium wave band leaving three bands of short wave coverage.

Due to the number of stations on the bands it is very desirable to have a separate bandspread, or fine tuning, control. This control has the effect of expanding a small portion of the tuning scale making it much easier to tune in a particular station. The much-advertised transistor portable receivers

are usually lacking in this respect.

An alternative method of frequency coverage is found in the more expensive receivers which have a number of bands each covering 500kHz of the spectrum. These receivers usually cover the Amateur bands only but can be ordered with coverage of the Broadcast bands. The tuning of these receivers is so fine that a separate bandspread control is not required.

In general the listener must ensure that the receiver covers the bands in which he is interested

and that the tuning can be finely controlled.

2. Number of Conversions: The number of conversions that a receiver has is the number of different i.f.'s (Intermediate Frequencies) that it has. The normal single conversion receiver has a single i.f. usually in the range 455-470kHz, although 1.6MHz is sometimes used. The double conversion receiver has two different i.f.'s. In general, the more i.f.'s a receiver has, the better the selectivity and image rejection will be.

3. RF Stages: Some of the simpler receivers available have no r.f. stage and the signal is passed from the aerial to the mixer stage directly. The addition of an r.f. stage will increase the sensitivity of the receiver and also improve the image rejection of a single conversion set. As mentioned last month this problem can be overcome by adding a preselec-

tor between the aerial and the receiver.

4. Operating Modes: The Broadcast Bands listener is usually only interested in amplitude modulated (a.m.) signals and this mode of operation is, therefore, essential. If the set is also to be used for reception of Amateurs provision should be made for code (c.w.) reception, this also allows reception of single sideband (s.s.b.) transmissions. However, the provision of a product detector gives much better s.s.b. reception. If the provision also exists for manual selection of the upper or lower sideband this facility can be used during the reception of a.m. signals to avoid interference and fading effects.

5. Selectivity: The selectivity of a receiver is its ability to separate stations on adjacent frequencies. It is extremely useful to have the facility of varying the selectivity of the receiver. When interference is heavy a narrow selectivity can be used to cut out the interference. Mechanical or crystal filters help to im-

prove the selectivity of a receiver.

6. Stability: It is essential for a good receiver to be stable in operation. With some valve receivers the heating effects involved caused frequency drift and other annoying effects. The introduction of transistors and, in particular, field-effect transistors has greatly improved the situation due to the low heating effects associated with these devices.

7. Valves vs. Transistors: Apart from improving stability, as mentioned above, transistors have many advantages in communication receivers. They have a longer life, require simpler power supplies and are low cost. The benefits of this are that transistor receivers tend to be smaller, lighter in weight, less expensive and also have the option of being operated from an external battery.

8. Automatic Volume or Gain Control (a.v.c. or a.g.c.) Almost every receiver has some form of a.v.c. or a.g.c. which adjusts the gain of the receiver to compensate for changes in signal strength. A receiver with variable a.v.c. or a.g.c. is to be preferred

as the optimum setting can then be used.

9. Extras: Most receivers have various extras of which the following are the most useful. (a) The provision of a headphone socket. (b) An aerial trimmer to match the aerial to the set. (c) A signal strength meter (S-meter) to assist with tuning. (d) A crystal calibrator to check the dial accuracy. (e) A noise limiter which should be variable if possible. (f) A notch filter to reduce hetrodynes.



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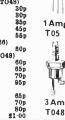
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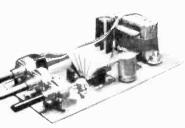


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COMMERCIAL RADIO by CHARLES MOLLOY

OMMERCIAL radio in the UK has come a step nearer with the start of medium wave tests in the London area by the Independent Broadcasting Authority. Kevin Peel (Hornchurch Essex) has heard the IBA on 557kHz with transmissions of music and announcements stating that the tests were being made by the IBA for an indefinite time. The choice of frequency is a surprise as the two IBA London stations are expected to be on 1151kHz (London News) and 1546kHz (London Entertainment). The first regular broadcasts from the IBA are scheduled to start this year with the opening of the London stations to be followed in 1974 by others in the provinces

Harold Emblem (Mirfield, Yorkshire) has logged a number of medium wave stations in the Persian Gulf area between 0230hrs and 0300hrs GMT. He reports Kuwait on 539kHz; Tabriz, Iran on 645kHz; Bagdad 760kHz; 'The Voice of the Arab Emirates' Dubai 1250kHz with an Arabic religious programme followed by pop music at 0300hrs; Teheran 1325kHz; Kuwait 1345kHz. Harold mentions that Kuwait

539kHz can be heard during the evening under Budapest, which uses the same frequency. Baghdad on 760kHz is also audible in the evening.

Commercial radio is well established in Spain where several chains of low power locals operate alongside the government owned Radio Nacional Espana networks. The commercial stations are allocated call signs and about 150 of these outlets can be found all over the band. Those most frequently heard in the UK are EAJ5 Radio Sevilla on 809kHz; EAJ1 Radio Barcelona on 827kHz; EAJ2 Radio Espana (Madrid) 917kHz; EAJ29 Radio Intercontinental 953kHz; EAJ8 R. San Sebastian 1025kHz; EFE14 La Voz de Madrid 1097kHz; EAJ15 Radio Reloj (Barcelona) 1124kHz; EFJ43 Radio Juventud Bilbao 1133kHz; ECS11 Radio Centro Madrid 1385kHz; EAJ20 Radio Sabadell 1475kHz; EFE25 La Voz de Calabria 1570kHz. The common channels 1106kHz, 1133kHz, 1394kHz, 1412kHz, 1430kHz, 1475kHz, 1502kHz, 1520kHz and 1570kHz are crowded with stations. They sign-off for the night from 2300hrs GMT onwards and at this time the DXer can hear one station after another dominate a channel only to close down and leave the frequency free for a weaker occupant. Many a rare catch can be had at this time.

L. J. Hook asks for information about the MW Command receiver. Also known as the BC946 it was part of the ARC5 aircraft communications equipment used in the last war. It performs very well on the medium waves but it does require some modification as it was designed to work from a 28 volt aircraft supply.

IBA ON VHF

by SIMON DAVID

HIS new v.h.f. section will be a regular feature giving news and views on transmissions usually found on the 88 to 108MHz dial, but may be extended to include related topics. VHF is generally taken to include transmissions between 30 and 300-MHz, i.e. below 10 metres, but since this area is also covered in David Gibson's Short Wave column, this section has been specially started to provide some information more appropriate to broadcasting.

Since f.m. broadcasts began in the U.K. on a regular basis, it has been continually predicted that the medium wave band was due for banishment. This has not come about however and the medium wave is in fact still being exploited. What is expected is that the new Independent Broadcasting Authority Stations will use the upper reaches of the f.m. dial for stereo programmes, but will not necessarily use the same transmitters as the BBC. Receivers within close proximity of a BBC transmitter and collecting signals of around $100\mu V$ may find that they will be able to pick up a 20mV signal from the local IBA station.

One of the main headaches is expected to come from cross modulation effects due to emergency services being tuned in close to the commercial channels. This will undoubtedly result in a number of semi-redundant old tuners, although there is no fear of upsetting their present usefulness for BBC programmes. Whether politics come into this we are not too sure, but it is strange how the commercial side of broadcasting frequently has to accept second rate operational conditions.

In order to help find space for the new IBA com-

mercial radio stations, the BBC will be nudging its local stations along the v.h.f. tuning scale a little. changing the operating frequencies of Radios London, Medway, Oxford, Brighton, Leicester, Nottingham, Stoke, Humberside, and Sheffield. These adjustments are expected later this year when the appropriate details should be given in the local Press and Radio Times.

The new station at Carlisle is still expected to "appear" on 95.6MHz, but it looks as if Swaledale will be "lost" for want of a suitable site for a relay station.

Although some way off yet, it is not a bad idea to look into the needs and possibilities of incorporating very sharp rejection filters to suppress adjacent local transmitters. The use of a field effect transistor at the front end will also help to reduce cross modulation effects. Several tuners have automatic gain control and since this would not be helpful in this situation it is worth incorporating a switch so that it can be cut out of service as necessary.

Furthermore, the mixer stage design becomes critical and the noise generated here must be at a very low level. This will mean that the r.f. circuit will not have such a high gain as in the past but this can be made up by increasing the gain through the i.f. stages.

The use of phase-lock integrated decoders will provide tuners with lower distortion and better frequency response, both of which have become necessary for good stereo reception.

We shall always be pleased to hear of readers' experiences of v.h.f. reception, especially those who listen in to continental stations. Please be brief and confine your letters to stations received, aerial and tuner used and the effect of interfering transmissions.





SHORT WAVES by DAVID GIBSON, G3JDG

the very marked absence of 14MHz logs. It seems that the twenty-metre-only addicts are as dead as their band these days. Meanwhile, back at the eighty-metre ranch it's been a right merry r.f. square dance. The amount of DX on eighty has been quite remarkable with west coast W stations romping in at times. In fact, stations further down the globe have also put in an almost regular appearance on this band; Mexico, Brazil and Argentine, etc. Some real goodies have put in an appearance for the persistent enthusiast. Callsigns like DU1EJ and VS6DO have shown that your reciever dial need not read above 4MHz in order to log some rewarding DX signals both on phone and c.w.

News from VE land. An enthusiastic band of Canadian Amateurs are building a large oceangoing trimaran. Their object is to put the 40 most "wanted" countries on the air. I will pass on information about their ports of call as soon as I hear.

Great hopes that an Amateur station will be allowed on Clipperton Island. Callsign to listen for will probably be FO8C. Anyone heard the station reported to be located in the Spanish Sahara yet?

Time to pass on to some queries, curses and comments. Michael Green (Cheshire) uses a UR1A. The drawing of his antenna system bears a harrowing resemblance to the national grid. (Bet he's the only s.w.l who tunes topband in rubber gloves and wellies). Michael queries queer callsigns heard in the wee small hours on 80 metres s.s.b.; Rudolph, Scrooge, Virgin Mary and Snowman. Michael's problem is simply, "How do I QSL them?" (Perhaps the nearest Asylum is licensed?).

Letter from a long, long way off bears the signature of Lindsay Pennell and the post mark Hong Kong (Ah, those were the days, Chow Mein butties and cocoa on the Kowloon ferry). Lindsay wonders why so few G s.w.l.s hear the Hong Kong throng signing VS6. There are some 40 licensed Amateurs many of them being very active into Europe. Confess now, you're all logging VS6's and not telling your Auntie David.

Simon Baines (Hitchin) reports a number of W stations including W5NMA, heard on forty metres s.s.b. Gear is a five-vale receiver, transistor b.f.o. and 30ft of wire end fed.

M. Harrison (Derby) sends in a log of numerous G stations heard on topband. Incidentally, a good non-G to listen for on 1.8MHz is W1BB/1 whose stalwart support and interest in topband is well known all over the world. It is interesting to note that PY1DVG has been heard on 1.8MHz.

Kevin Smith is thirteen summers old and lives in Brighton. (Wish I was and did.) Whereas most boys of 13 are the proud possessors of pieces of string and marbles, Kevin settles for a CR100 and a 215ft long wire end fed. His best areas on topband were: DL8PC, GI3GRD, GM4BBL, GW3ZQN all on s.s.b., and OK1ATP on c.w. His log for 28MHz reads: CN8BF, CN8CF, CR4BS, CR7AF, CR7IZ, CT2AT, ET3USF, ET3USP, KV4CF, ST2SA, VP2LAF, WB4WOI/P, ZE4JW, ZS6AD, 4Z4ME, 6W8DL, 7Q7RM, 9G1HE, 9H4D, 9J2AY, 9J2DT all s.s.b.

Best times for listening on eighty metres are from midnight to around 0300 hours according to Alan Smith (Lancs). He bemoans the Lids who test incessantly by blowing into the mike (it's unhygienic but they can't touch you for it). Alan has a JR31), 60ft end fed and an a.t.u. Heard on eighty: EP2TW, KP4AN. KV4CI. PY4BTK. K2LQA, KIUAT, VEIADV, VP2LI, VP7ND, W1GEY, W2BXA, W3WGH, W4AG, ZB2CF, ZS1MH, ZS3GH, 9H1CW, VP2LI. VP7ND. WIGEY, W2BXA. 9V1RE. A cheap day excursion to 14MHz s.s.b. raised: EP2ES, HZ1AB, KG6JBE, KL7HFA, KX6BQ, LUIDAC, MP4TEE, VEIASJ, VE3MO, VK3ADR, YK1AA, ZL1KN, ZL1WE, ZL2AVE, ZL2BQC, ZL3QN.

David Sharred (Birmingham) had a quick tour of eighty metres. Main listening times were "after my paper-round", and the gear is a CR150/2 with a V-shaped antenna (60ft each leg). Goodies bagged on 3·5MHz: CN8BF, JY1, K5PFL, KV4AM, OA6NCT, PI1ROS, VE3CDP/W9, W2HCW, W4MYA, W9QLD, WA5JMK, WB4MCI/P4, ZK2BO, ZL4BT, ZL4KF, ZS3GH, 3A2EG, 5U7AX. On twenty metres David's best were VK5RN and VK6XO.

Where are all you v.h.f. types hiding? No logs at all for lonely little 70MHz and only one for 144MHz. **Michael Prescott** (Lancs.) uses a Roamer 10 receiver and a two metre dipole. He reports signals from the following: G3AHD/A, G3PVC, G3VIM, G3XIM, G3VME, G8EYO/A, G8ESU, G8GYS, G8VLE and G8XDL. Well done Michael, you've kept the v.h.f. flag flying—just.

For the contest and Rally enthusiasts, April is a busy, busy month. Jottings from my Events diary read: April 1, White Rose Mobile Rally at Leeds; 1, WAB phone contest (l.f.); 8, WAB c.w. l.f. contest; 8, eighty metre QRP (low power) contest; 15, four metre portable contest (no excuse now for not sending in a log); 21-22, Bermuda contest (phone); 29, Rugby DF qualifying round; May 5-6, two metre and 70cm open contest (another chance for the v.h.f. s.w.ls to shine); 5-6, Bermuda contest (c.w.); 6, Spalding Tulip Time Mobile Rally.

BROADCAST BANDS

Short Wave Reports by 15th of the month to Malcolm Connah, 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.

Medium Waves Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.

VHF Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4 4AD.

AMATEUR BANDS Short Wave/VHF

Logs in alphabetical order please by 15th of the month to David Gibson, G3JDG, 12 Cross Way, Harpenden, Hertfordshire.

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Operation

When a voltage is applied to the circuit, the capacitor C1 starts to charge up through R1 and VR1. Initially the emitter of Tr1 will be at negative potential but as the capacitor charges, the voltage at this point rises. When it reaches a certain point, b₁ and b₂ are virtually short circuited and current will pass through R2, R3 and Tr1. At the same time C1 will be discharged through R3 and the device will become open circuit again. The same process will start all over again so that a series of pulses appears across R3 via C2. Since the output will be a series of pulses whose rise and fall times are very rapid, only a low value capacitor is necessary despite the low value of R3. The output will be in the form of a positivegoing pulse; if a negative-going pulse is required this capacitor should be connected to b2. A sawtooth waveform is available from the emitter but it should only be connected to a high impedance load otherwise the operation of the relaxation oscillator will be affected.

The frequency of the pulses depends on the relationship of the resistance made up from VR1 and R1 and the capacitor C1. Resistor R1 limits the current

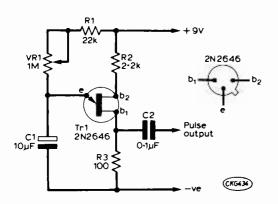


Fig. 1: Circuit and suggested valves for the pulse generator.

No. 48 PULSE GENERATOR

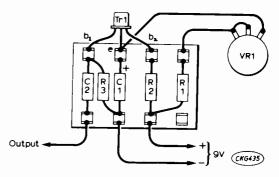


Fig. 2: Practical layout of components on a piece of tagboard.

through the emitter so that it cannot be connected directly to the positive line; this would cause damage to the device.

Experimenting

There is room for experiment here; C1 can be altered in value from $500\mu F$ down to $0\cdot01\mu F$. The high value will produce pulses with very long intervals; it is difficult to say how long as the natural leakage through the electrolytic will play a major role. If a low leakage device is used the time interval can be a minute or more. Using the low value capacitors the pulses could extend to ultrasonic frequencies.

* components list

R1 22kΩ ¼W, 5 per cent	1p	,
R2 2·2kΩ	1p	4
R3 100Ω	1p	* 1.5%
VR1 1MΩ linear pot	12p	
C1 10µF 12V	5p	* · · · ·
C2 0·1μF mylar, etc.	4p	
Tr1 2N2646	40p	
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Modifications

The output can be taken to an amplifier to act as a metronome. In fact if only a low level output is required, a high impedance loudspeaker (50Ω to 80Ω) can take the place of R3; in this case of course C2 will not be needed.

A suggested layout is shown in Fig. 2 making use of a small piece of tag board; this is far from critical and almost any layout may be used.

ON RECENT DEVELOPMENTS

o you ever have that feeling that you are being watched? Well, maybe you are at that and have been for the past 13,000 years. A theory has been put forward that we are getting intelligent messages from space. To be more precise, from an interstellar "thingy" which is buzzing round the earth—probably in an orbit which is similar to that of the moon. (Good gracious, Holmes).

LONG WAY ROUND

Before you rush out and wave your hanky at the sky, hear what the experts have done about it. It is all tied in with things called long-These echoes. observed as far back as 1928. A transmitter using 15kW on 9550kHz was radiating its Morse signal which in turn was being received by a number of receiving stations. A Morse signal was being sent and received almost instantaneously. Now a signal can go two waysdirect to the receiver by the shortest route and also in the opposite direction. This latter signal can quite easily travel right round the world before it is received by our receiver. Thus two signals are heard; the direct one, and the one which goes the "long" way round. The latter takes about one seventh of a second and is heard as an "echo" of the direct signal which, because it travels direct (therefore less distance) arrives almost instantaneously i.e., with negligible delay.

So far so good. But imagine the effect on the minds of the listeners when other echoes were heard—not delayed by one seventh of a second but at various intervals varying from about three seconds to 15 seconds! These long-delayed echoes were also noticed independently at other times, on other dates, by different receiving stations listening to a different transmitter and on a different

Then, someone plotted a graph of one of these echo sequences and another piece of the intrigueing jigsaw came to light. The plotted points bore a striking likeness to the constellation Bootis. Other echo sequences were plotted and produced patterns which were clearly

identifiable with other constellations.

The hypothesis has been put that the long-delayed echoes are being returned to Earth from a space probe; a probe which arrived from the Bootis constellation 13,000 years ago. Moreover, the probe was sent to search for evidence of intelligent life in the form of radio transmissions.

People who are in doubt about the validity of all this should bear in mind that all the evidence so far corroborates this hypothesis. So closely, in fact, that EMI engineers are to set up a high-power transmitter and high gain antenna (probably around 144MHz) in order to put the hypothesis to the test. Are they just being starry-eyed? I do not think so.

Once a complete digit is generated it is safely entrusted to the memory of a computer. Here, it is checked to see if it is eligible. If it is, then it will be stored in the computer's memory, if it is not, it will be discarded.

Ernie presses on until the memory or store has 60 numbers in its care. These are then "written" onto magnetic tape and this is then "played" to another computer for checking and finally linking the lucky numbers to the bondholders' names and addresses.

I am already making the most careful measurement of the noise generated by a pair of zener diodes—well, you never know.

ERNIE

Apart from driving the fastest milk cart in the west, Ernie has achieved fame in other ways. For example, he painstakingly avoids selecting your premium bond number every month without a single complaint or grumble. To date, his selections have paid happy punters prizes amounting to some £350 million—none of which has yet reached your scribe!

So it is with ageing joy and renewed hope that I report a new Ernie who will produce the monthly list of prizewinners in under three hours. The old Ernie used to take ten days to complete the same task.

Before we non-winners get too elated, let us examine what we are up against. Just what (or who) is Ernie and how does he choose winners?

First, Ernie comes from Ernie Harrison, Managing Director of Racal, whose idea it was. Ernie himself (the number picker) has been described as the most advanced electronic system in the world for generating numbers in a completely random fashion. How does he/it go about the task?

The first job is to monitor the noise level of a pair of zener diodes (actually, a pair for each digit). Each "pair" noise is amplified and then compared with a reference voltage. Because of the nature of noise there are peaks, and each time one of these exceeds the set reference level it is counted and used in the production of a digit.

TRANSISTORISED TED?

How about an electronic government, a big computer tucked away beneath Parliament in a Guy Fawkesproof vault? Maybe not yet, but in America the computer has managed to secure itself a small governmental foothold.

The House of Representatives is to vote by computer. Problem has been the 435-name list of members and the time wasted in correcting attendance errors. Other little hitches like finding a vote recorded from a member who wasn't even there were also proving annoying. The mind boggles.

The new system means that each member has a small plastic "card". He can use this card to vote at any one of some 50 stations located at various points about the House. Behind the Speaker's seat is a scoreboard which gives the latest updated score on how the voting is going. Electronic voting is reckoned to save at least 50 per cent of the time previously taken for such a task. The computer will also give written records of votes simultaneously plus an instant breakdown of these into States or Parties as required.

Look out members of Parliament you might be replaced by a pair of zener diodes one day—they're cheaper, smaller and generate less noise!

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H40	20	BFY50/2, 2N696, 2N1613 NPN Silicon uncoded TO-S	50p
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B63	200	Trans. manufacturers' rejects all types NPN, PNP, Sil. and Germ.	50p
B84	001	Silicon Diodes DO-7 glass equiv. to OA200, OA202	50p
B86	100	Sil. Diodes sub. min. IN914 and IN916 types	50p
888	50	Sil. Trans. NPN, PNP equiv. to OC200/I 2N706A, BSY95A, etc.	50p
BI	50	Germanium Transistors PNP, AF and RF	50p
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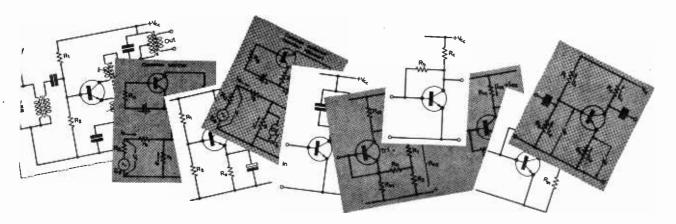
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TRANSISTOR CIRCUITRY for beginners PART 16 H.W. HELLYER & MICHAEL HOLLIER

Practicalities

A BC109 is chosen to give an open-loop gain of 260, with an input of about 30mV at 1kHz. We shall aim to keep this level constant for further tests. Connecting the two resistors of Fig. 76 to the input, we have the virtual earth type of circuitry. This has been discussed at some length in previous articles. It can now be simplified to the triangle of Fig. 77,

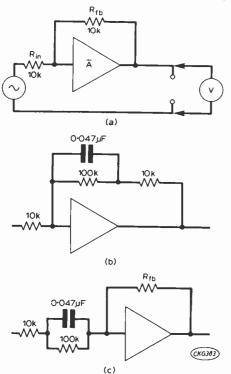


Fig. 77: (a) Simplified representation, with the symbols denoting an inverting amplifier. (b) a frequency-dependent development, and (c) the bass cut variation, with the frequency-selective portion before the feedback loop.

the input shown conventionally at the blunt end; the output at the sharp end (i.e., the 'arrow' points the way the signal is going). Fig. 77 is a simplified diagram, the letter A within its triangle denoting that it is an amplifier.

Previously you will have noted reference to an 'inverter'. By this, is meant that the input is 180° antiphase to the output. In Fig. 77, we see a bar over the A, denoting an inverter. For the benefit of old-timers like me, this can be regarded as exactly parallel to valve technology: a positive-going waveform at the grid produces a negative-going waveform at the anode.

If previous articles have been followed, it will be noted that the closed loop gain, which is the circuit gain calculated after feedback has been applied, is derived from the formula: $G_{\text{c}} = R_{\text{fb}}/R_{\text{in}}$.

If we now make R_{in} equal to $10k\Omega$ and R_{fb} also $10k\Omega$, the closed loop gain is unity, i.e., 10/10. In practice, we shall measure 0.8 rather than 1. If, with R_{in} at $10k\Omega$ and R_{fb} at $100k\Omega$, giving a theoretical gain of 10, we were again to measure, we should find the answer more like 7.7. Carrying this experiment a little further—and please do not merely take our word for this; try it and see for yourself—we find that with R_{in} at $100k\Omega$ and feedback resistors varying between $10k\Omega$ and $1M\Omega$, the closed loop gain varies between 0.1, via 0.98 (at $100k\Omega$) and 5.8. Which only goes to prove that the actual gain is always less than calculated, and, secondly, the lower the circuit impedance, the greater the error.

Practically, therefore, it would seem that our circuit was not the best. But, as it is typical of the majority of commercial designs, we make no apology. It has to be remembered that the tone control circuitry does not have to contribute a lot of gain. We do not normally need a gain at any frequency of more than 'times 10', plus a stage gain of around 4, and so a maximum gain of about 40. Refinements will be added, never fear . . .

Reverting to Fig. 77(a) and making R_{in} $10k\Omega$, with a similar value for R_{fb} , we obtain a gain of 0.98, and the virtual earth point is at the junction of the two resistors. If we insert a resistor as shown at

Fig. 77(b) we reduce the gain somewhat, 0.96, but let's return to that later, the important point being that we can arrange the gain that we require by choice of $R_{\rm in}$ and $R_{\rm fb}$.

Here I part with Mike and assert that many modern circuits are resolved and arranged (rather than designed) by what are euphemistically called 'empirical methods'; more cynically described as 'hit or miss'. With the basis of existing circuits and a mass of mathematics that go to support them, the modern designer takes for granted the previous researches, and builds upon them. Exceptions, like John Linsley Hood, who question every fact and do their own research, are as rare as gold nuggets in a leadmine.

All of which digression leads me to Fig. 77(b). Here we have $R_{\rm ln}$ at $10k\Omega$ with a similar feedback resistor $R_{\rm lb}$ in series with a $0.047\mu{\rm F}$ capacitor (itself, practically, paralleled by $100k\Omega$). The impedance of the feedback network can, if you want to be meticulous, be calculated at any point in the frequency range.

This is all very fine, but, in practice, we can say that at very high frequencies the capacitor will be an effective short-circuit. In these circumstances, the circuit becomes effectively $R_{\rm in}/R_{\rm fb}$ having unity gain. Lowering the frequency raises the reactance $X_{\rm c}$ until it eventually becomes an open-circuit, and, in comparison with the $100 {\rm k}\Omega$ previously mentioned, the gain will be nearly 11. Theory gives us 110/10, practice a little less, hence my question-begging formula. We shall settle for a gain of around 20dB, which is ten times the input voltage.

In the frequency range that C is effective we will have an impedance change in the feedback network giving us a slope of 6dB/octave. At frequencies below where unity gain is produced, the slope will flatten, so that further reduction of frequency does not change the output from unity gain. At frequencies above where the effective $R_{\rm h}$ is $110 {\rm k}\Omega$, i.e., for a theoretical gain of x11, the curve again flattens. The transitions from slope to flat are not sudden and our dotted curves show the practical results obtained.

Turnover

Reference has already been made to ft, and by this we mean the turnover frequency, (in the case of Fig. 75 we have two turnover points, at 3dB positive or negative position on the curve, depending on the way the calculations are carried out, as should become apparent).

The f_t points can be calculated from the formula $f_t = \frac{1}{2\pi CR}$ where the frequency is in hertz; the

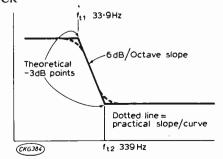


Fig. 78: The bass lift curve in theory (solid line) and in practice (dotted line).

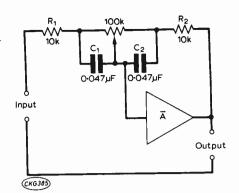


Fig. 79: A combined bass lift and cut circuit.

constant 2π can be taken as 6.28, C is in farads and R in ohms. Taking the component values of Fig. 77(b), we obtain a lower frequency turnover point of 33.9Hz while the upper frequency turnover point works out to 339Hz.

In practice, of course, the points are not definite. The plotted curve, as can be shown later, follows rather the dotted than the hard line of Fig. 78. Plotting the curve obtained from a 'hook-up' replica of Fig. 76, we get the actual curve of Fig. 78, from a generator with a 600Ω source impedance, and reading across the 'open' output with a high impedance valve-voltmeter. (Amendment, please: our habit these days is to use the battery-powered millivoltmeter so the use of the term 'valve-voltmeter' is mostly a matter of habit—although we certainly continue to use our old faithful instruments where the low value of hum and noise will not prove an embarrassment.)

One of the reasons for the smoothing of a theoretical curve is, of course, that other circuit considerations take effect. In theory, we take the two extremes, when the $0.047\mu F$ capacitor is in parallel with the $100k\Omega$ resistor and the $10k\Omega$ resistor is not effective, and when the capacitor is in series with the $10k\Omega$ resistor, the effect of the $100k\Omega$ resistor then being ignored. In practice, of course, it cannot be ignored: its real effect is to modify our $10k\Omega$ to $9k\Omega$ under these circumstances.

Taking the worked theoretical examples:

Taking the worked theoretical examples.
$$f_{\rm t} = \frac{1}{2\pi {\rm CR}} = \frac{10^6}{6\cdot28\times0.047}\times10{\rm k}\Omega \ ... \ (1)$$
 and
$$\frac{10^6}{6\cdot28\times0.047}\times100{\rm k}\Omega \ ... \ (2)$$

$$(1) = 339{\rm Hz} \ {\rm and} \ (2) = 33\cdot9{\rm Hz}$$

These figures agree very nearly with our practical measurements, This, from the curve of Fig. 78., gives us our Bass Lift circuit.

Bass cut

If we now reverse the networks $R_{\rm in}$ and $R_{\rm fb}$ as depicted in Fig. 77(c), we get an inverse of the previous curve. That is to say, we get bass cut instead of bass lift, because the feedback is now resistive, while the input circuit, up to the 'virtual earth point', is frequency-dependent.

Combining both these circuits, as in Fig. 79, we get bass cut and lift according to the position of the slider of the control. With the slider on the left, C1 is effectively short-circuited and we are left with

-continued on page 76

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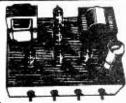
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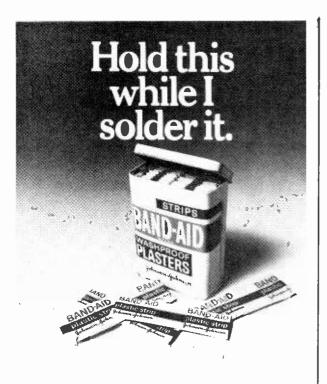
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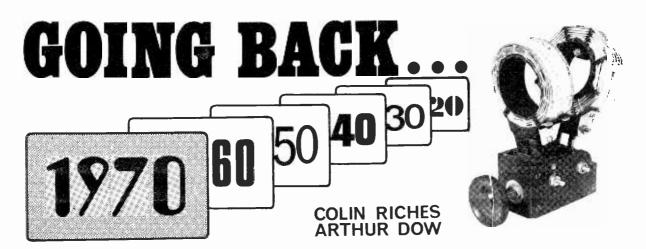
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UITE a large number of letters addressed to us involve queries or seek information on the date or origin of bits and pieces of old wireless equipment or valves. So this month we thought that we would try to give some very broad indications of the form of construction and appearance of domestic wireless sets at the interesting stage of their development. This should enable readers to date a piece of apparatus, if called upon to express an opinion, or if an interesting bit of gear is found in a junkshop.

History

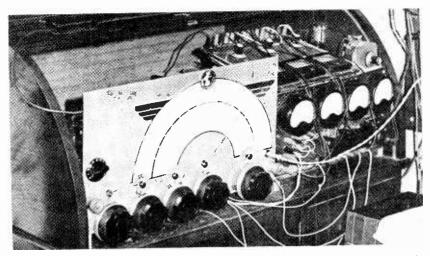
From the turn of the century when Marconi was experimenting with the first tuned spark transmitter, until 1922 when the first official broadcast was made and valve circuits had been developed to the extent that they were no longer regarded as freak, the amount of equipment produced was comparatively small and that which remains is mostly in safe hands.

Once broadcasting had begun the boom in home constructed receivers got under way very rapidly since there were few commercial receivers available at that time. It is this period from about 1922 until the mid-30's that is probably of most interest to those who specialise in collecting vintage wireless equipment and with which we will concern ourselves here.

Components

There were many firms supplying components such as coils and holders, tuning condensers, audio transformers and valves as well as ebonite panels and associated hardware. Basket-wound or wave-wound coils were frequently home-made and plugged into holders which were adjustable from the panel to vary the coupling between the coils. Resistors looked like cartridge fuses and were pushed in to clips. The grid-leak was often changed to suit the 'softness" of the detector valve or it might be a panel-mounted variable resistance.

'Spaghetti' resistors had the resistance wire wound on a flexible core and looked like a piece of string with end tags. These could be connected directly between terminals of components. Most components such as audio transformers, valveholders and condensers etc. had terminals, usually 6BA, often with a soldering tag. Sets of this period were characterised by the great effort that went into the wiring up.



We don't want to start an argument but we think that Mr. A. Rea of Hull could be our oldest reader, at 80 years plus. Wireless is still his hobby and he is very proud of the John Scott-Taggart ST900, shown above, built many years ago, probably about 1937. He can feed the output of the receiver into a tape recorder or into a valved amplifier using a pair of PX25's which feeds no less than five loudspeakers around the place.

Square sectioned copper wire was common, always arranged with neat corners or angles and straight parallel runs and neat loops under the terminals. The need for short, direct wiring was not appreciated then, and indeed, was probably of little importance where only medium and long waves were concerned and stage gains were very low.

Construction

Such receivers were built on a wooden baseboard to which the components were fixed with woodscrews and an ebonite panel was fixed to one edge of the board. Along the back edge was a row of terminals, mounted on a strip of ebonite, for connecting the set to the accumulator, high tension battery, grid bias battery, aerial and earth and headphones or speakers. Incidentally, the cabinets for these sets were also given a great deal of attention and often were works of art in themselves to ensure that they fitted in with the rest of the furniture. Indeed, the receiver was often built in to an existing piece of furniture. The panels of sets of this period were a mass of knobs and controls with possibly a rheostat for each filament, variable grid-leaks, tuning condensers for each stage, coil coupling controls and reaction controls. Later, when shorter wavelengths were in use, metal panels were employed in order to prevent 'hand capacity' effects which upset the rather critical tuning.

Valves

Valves can be dated fairly accurately from a study of their physical characteristics. At the beginning of the period we are discussing, say 1922-24, the Marconi-Osram R valve was common along with the Mullard ORA and the Cossor P1 all of which were bright emitters with tungsten filaments. Generally they had a metal sleeve base and a pinch on top of the glass envelope, formed during the evacuation process. 1924-25 saw the introduction of the dull emitter valves using oxide-coated filaments such as the MO DE5, Mullard DO6 and the Cossor WR1. These valves still had the pinch on top but the bases were the more familiar moulded type.

Between 1925 and 1927 saw the advent of the now famous Mullard PM range of valves which were dull emitters with filament voltages from two to six volts. The pinch was now concealed in the base of the valve thus eliminating a very vulnerable feature of the older valves.

The first 'mains' type valves emerged in 1927 with the heaters, usually four volts, being run from a mains transformer instead of accumulators or batteries. In the early 30's r.f. type valves appeared with sprayed-on metallic coating for screening purposes and the glass envelopes, especially for the audio amplifier valves, developed a waisted section at the top of the envelopes intended to support the mica discs of the electrode assembly and thus reduce any tendency to microphony.

For those that are really interested in these old radios there is no finer pastime than trying to get one of them to work even if it means using equivalent modern components as replacements for faulty parts. Our CQ column is open to those readers who wish to appeal to other readers for old components if it is felt that only a 100% genuine vintage receiver is acceptable.

TRANSISTOR CIRCUITRY FOR BEGINNERS-

continued from page 72

the effective bass lift circuit of Fig. 77(b). With the slider to its right we get the alternative condition, with C2 short-circuited and the bass cut circuit of Fig. 77(c).

Balance

Take the case of the slider at its middle position. Then, the input and output circuits are identical and balanced. That word, BALANCED is important. It is the basis of the Baxandall tone control circuit—one of the most elegant solutions to an audio problem yet posed, and not to be under-rated. In the full circuit, the impedance change with the slider control moved (a change in frequency-dependence, looked at in the basic way of our approach) is exactly balanced with the movement of the slider in the other

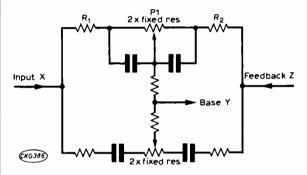


Fig. 80: The eventual network to be inserted in the feedback loop, giving bass and treble lift and cut.

section of the ganged potentiometer. It remains only that the ganged potentiometers themselves shall be within at least 1dB of linearity.

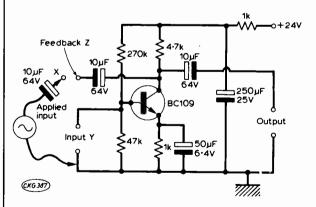


Fig. 81: The basic amplifier circuit over which the feedback is applied.

From the simple experiments we have already carried out, we know that when the input resistance, R_{in} is equal to the feedback resistance R_{fb} , then the theoretical gain is unity. In practice, findings are not far removed from the theoretical. At intermediate positions of the sliders, we shall get variations from the theoretical norm, between maximum bass and maximum cut.

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100-0-100µA £1.98		£1.75
200μA £1.95		
500μA £1.80	150V. D.C.	21.75
500-0-500μA £1.78	300 V. D.C.	£1.75
lmA £1.75		£1.75
1-0-1mA £1.75	750V. D.C.	£1.75
2mA £1.75		£1.85
5mA £1.75	50V. A.C	£1.85
10mA £1.75	150V. A.C	£1.85
20mA £1.75		£1.85
50mA £1.75		£1.85
100mA £1.75		21.85
150mA £1.75	VU Meter	£2.30

Type MR.45P. 2in. square fronts

50μA	£2·50	5 amp £1.85
50-0-50 _L A	£2·30	10V. D.C £1.85
100µA	£2.30	20V. D.C £1.85
100-0-100μA	£2-05	50V. D.C £1.85
200μA	£2-05	300V. D.C. £1.85
500μA	£1.95	15V. A.C £2.00
500-0-500µA	£1.85	300V. A.C #2-00
1mA	£1.85	8 Meter 1m A 22-05
5mA	£1.85	VU Meter £2.50
10mA	£1.85	1 amp. A.C. * £1.85
50mA	£1.85	5 amp. A.C. *£1.85
100mA	£1.85	10 amp. A.C. * £1.85
500mA	£1.85	20 amp. A.C. * 21.85
1 amp	£1.85	30 amp. A.C. * £1-85



"SEW" EDGWISE METERS Type PE.70. 3 17/32in. x 1 15/32in. x 2#in. deep

50μΑ		500μA	£3.05
50-0-50μA	£8.30	1mA	£2.70
100μA 100-0-100μA	£3.30 £3.20	300V. A.C	£2.70
200μA	£8 ⋅ 20	VU Meter	£3.75

MW 1-6 60mm square MW 1-8 80mm square

RP214 REGULATED POWER SUPPLY Solid state, Variable output 0-24V DC up to 1 amp. Dual scale meter to monitor voltage and current Input 220/240V AC. Input 220/240V AC. Bize 185 × 85 × 105mm \$28.97

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240° Wide Angle ImA Meters

P. & P. extra

£3-97 £4-97

"SEW" BAKELITE PANEL METERS

Type MR.65. 31in. square fronts

1 amp. 22-15 5 amp. 22-15 15 amp. 22-15 30 amp. 22-15



	_	l amp	22-15
CONTRACTOR OF THE PARTY OF THE	100	5 amp	£2·15
400000000000000000000000000000000000000		15 amp	£2.15
Total Control	8.0	30 amp	£2-15
0.0000000000000000000000000000000000000	9	50 amp	£2-18
200000000000000000000000000000000000000		5V. D.C	£2-15
Consideration of the last	666	10V. D.C	£2-18
	-	20V. D.C	£2-15
Name of Street	-	50V. D.C	22-15
STEEL STATE OF THE PERSON NAMED IN		150V. D.C.	£2-18
	_	300V. D.C.	£2-15
	3.85	50mV. D.C.	£2.40
	3.00	100mV. D.C.	£2-40
	08.5	30V. A.C. *	£2.20
100μA #	08.5	50V. A.C. *	€2-20
	2.50	150V. A.C. *	£2.20
	2-45	300 V. A.C. *	£2-20
	2.15	500mA A.C. *	£2·15
	2-15	1 amp. A.C. *	£2.15
1-0-1mA £2	2.15	5 amp. A.C. *	£2·15
	2.15	10 amp. A.C. *	
10mA £2	2-15	20 amp. A.C. *	
50mA #2	2.15	30 amp. A.C. *	
100m A £2	2-15	50 amp. A.C. *	
500mA £2	2.15	VU Meter	£3.40
-			

Type S-80 80 mm. square fronts

.,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
50µA	£3·50
50-0-50µA	£3.40
100μΑ	£3-40
100-0-100µA	£3.30
500μA	£3.05
1mA	£2-85
20V. D.C	£2.85
50V. D.C	£2.85
300V. D.C.	£2·85
1 amp, D.C.	£2-85



"SEW" **EDUCATIONAL METERS**

Type ED.107. Size overall 100mm x 90mm x 108mm

A new range of high quality moving cold instruments ideal for school experiments and other bench applications.

3° mirror scale. The meter movement is casily accessible to demonstrate internal working. Available in the following ranges:

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High quality ceramic construction. Windings embedded in vitreous enamel. Heavy duty brush wiper. Continuous rating. Wide range ex-stock. Single hole faxing, Jin. dia. shafts. Bulk quantities available. 25 WATT. 10/25/50/100/250/500/1000/2500 or 5000 ohms. 90p. P. & P. 10p. 50 WATT. 10/25/50/100/250/500/1000 or 2500 ohms. £1.65 P. & P. 10p. 100 WATT. 1/5/10/25/50/100/250/500/1000 or 2500 ohms. £1.65 P. & P. 15p.

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5 000 O.P.V 0/3/15/150/300/1200 V 0/3/13/130/1200 V D.C. 0/6/30/330/f900 V A C 0/300μA/300 MA 0/10K/1 meg Ω Decibels 10 to +16db £2.75 each +15p P. & P



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KAMODEN 72.200

KAMODEN 72.200
MULTITESTER
High sensitivity tester.
200,000 o.p.v Overload
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Ranges:
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600 / 1200V. D.C.
0 / 3 / 12 / 60 / 300 /
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0 / 6μA / 1.2mA / 120mA /
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0 / 2K / 200K / 2 meg /
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Features A.C. current ranges, 100,000 o.p.v. Mirror Scale, Overload protection, 0/5/2-5/10/50/250/500/1000 V

D.C. 0/2·5/10/50/250/1000 V. A.C. 0/10/250/1A/2·5/25/250 MA/ 0/2-9/10/50/2-9/10/000 V. A.C. 0/10/250/µA/2-5-9/25/250 MA/ 10 Amp. D.C. 10 Amp. A.C. 0/20K/200K/2 MEG/20 MEG. — 20 +62db. \$12.50. P. & P. 25p.



370 WTR MULTI-METER

Features A.C. current ranges, 20,000 o.p.v. 0/-5/2-5/10/50/ 250/500 1000 V. D.C. 0/2-5/10/50/250/500/1000V AC 0/50uA/1/10/100mA/1/10 Amp

0/100mA/1/10 Amp AC 0/5K/50K/500K/5 MEG/ 50 MEG.

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Model U437 10,000 0.p.v. A first class versatile in-strument manufactured in U.S.S.R. to the highest standards. Ranges: 2 5/10/ 50/250/500/1000v D.C. 2 5/ 10/50/250/500/1000v A.C. Current 100wA/1/10/ DC Current 100wA/1/10/100mA/1A. Resistance 300 ohms/3/30/300K/3m Ω. Complete with batteries test leads, instructions and sturdy steel carrying case.

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New style 20,000 o.p.v. pocket multi-meter. 5/25/50/250/ 500 / 2500 V. D.C. 10 / 500 / 100 / 500 / 1000V. A.C. 50µA / 250mA. 8K / 6 meg obms. -20 to + 22 dB.



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FUR 12/Volt D.C. 8k Ω/V Volt AC. Mirror scale. 6/3/12/39/120/690 V D.C. 3/30/120/690 V A.C. 50/800 μ A/60/690 MA.10/100K/1 Meg/10 Meg Ω -20 to +46db. 88-97 P. 20k Ω/Volt D.C. 8k Ω/ Meg $\Omega = 20$ to +46db. **86.97.** P. & P. 12p.

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suspension. Overload protection. Polarity



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Extremely sturdy instrument for general electrical use. 667 o.p.v. 0/31/5/7/53096/150/500/600/900 VDC and 75m.V.

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Full capabilities for measuring A, B and ICO. NPN or PNP. Equally adaptable for check-ing diodes. Supplied complete with instructions, battery and £7.50. Post 20p.



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| IMAMSISION TESTER | 100,000 o.p.v. mirror scale | overload protection. 0/12/ -6/3/12/30/120/600 v DC. 0/16/30/120/600. v AC. 0/12/ 600µA/1 2/800mA/12 AMP DC. 0/10 K/1 MEG/100MEG. -20 to +50db. 0-01-2 MFD. Transistor tester measures Alpha, beta and Ico. Complete with hatteries instructions with hatteries instructions. instructions batteries. and leads. \$18-50. P/P 25p.



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Checks true A.C. beta in / out. Checks Icbo. Checks diodes

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Input impedance 10 meg ohms.

ohms.
Ranges:
0 / -25 / 1 / 2·5 / 10 / 50 /
250 / 1000V. D.C.
0 / 25 / 10 / 50 / 250 /
1000V. A.C.
0 / 25 / 4 / 2·5 / 25 / 25 /
0 / 25 / 4 / 2·5 / 25 / 25 /
0 / 25 / 4 / 2·5 / 25 / 25 /
0 / 25 / 4 / 5·0 K / 5·0 K / 5·0 K /
500meg ohms.
***LaK Part 30p

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Input impedance 10 meg ohms, 0 /·3 / 1·2 / 6 / 30 / 120 / 600V. D.C. 0 / 3 / 12 / 600V. A.C. 0 / 120 μA / 120mA D.C. 0 / 11 / 100K / 10 meg /100 meg ohms \$15·97. Post 15p.



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CI-5 PULSE OSCILLOSCOPE

For display of pulsed and periodic waveforms in electronic circuits. VERT. AMP. Band-width 10MHz. Sensiwidth 10MHz. Sensitivity at 100KHz VRMS/

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3in. tube, Y amp, Sensitivity 0-1v p-p/CM. Bandwidth 1-5 cps-1-5 MHz. Input imp, 2 meg Ω 25pF X amp, sensitivity 0-9v, p-p/CM. Bandwidth 1-5cps-800kHz. Input imp, 2 meg Ω 20pF. Time base. 5 ranges 10 cps 300 kHz. Synchronization.

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5 mc/s Pass Band. Separate

5 mc/s Pass Band. Separate
Y1 and Y2 amplifiers.
Rectangular 5in. × 4in.
C.R.T. Calibrated triggered sweep from '2 u/sec.
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Free running time base 50 c/s-1 mc/s. Bulltin time base calibrator and amplitude
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accessories and instruction manual
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GENERATOR
5 ranges 400kHz-30mHz.
An inexpensive instrument for the handyman.
Operates on 9v battery.
Wide easy to read scale, wide easy to read scare, 800kHz modulation.

5½ × 5½ × 3½in.

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MEASURING BRIDGE

A new portable bridge offering excellent range and accuracy at low cost. Ranges: R. 1Ω 11:1 meg Ω 6 Ranges ± 2% C.10pF ± 1110mFd 6 Ranges ± 2% C.10pF ± 1110mFd 1: 1/100.6 Ranges ± 1%. Bridge voltage at 1,000 c.ps. Operated from 9 volts. 100μA. Meter indication. Attractive 2 tone metal case. Size 71 × 5 × 2in. \$20. p. & p. 25p.

MODEL TE.15

MODEL TE.15
GRID DIP METER
Transistorised. Operates as
Grid Dip, Oscillator, Absorption Wave Meter and Oscillating Detector. Frequency
range 440Kc/s-280Mc/s in
6 coils. 500µA Meter. 9V
battery operation. Size 180 ×
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Output max. + 10 dB.

+ 10 dB. (10 K ohms) Operation in-ternal batterles Attractive 2-tone case 7% × 5" × 2". Price £17.50. Carr. 17 p.



MODEL MG-100 SINE SQUARE WAVE AUDIO GENERATOR Range 19-220,000Hz
Sine Wave 19-100,000
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Output Sine or Square
wave 10v. P. to P.
Size 180 × 90 × 90mm.
Operation 220/240v. A.C.

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MODEL AT201 DECADE ATTENUATOR
Prequency range 0200KHz. Attenuator
0-111db, 0.1db step.

Impedance 600 ohms. Max. input power 30dbm. Size $180 \times 90 \times 55$ mm.

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VALVE VOLTMETER
28 ranges. D.C. volta
1.5-1,500v. A.C. volta
1.5-1,500v. Resistance up
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Complete with probe and
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21.750. P. & P. 30p.
Additional probes available: R.F. \$2.12\frac{1}{2}; H.V.
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MODEL U4311 SUB-STANDARD MULTI-RANGE VOLT AMMETER

Sensitivity 330 ohms/Volt

AC Dat Dr. Accuracy

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150 / 30 / 750 / 150 / 300 / 750 / 300 / 750 / 300 / 75 / 150 / 300 / 750 / 300 / 3

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High quality instrument to test Reverse Leak current and DC current current and DC current.
Amplification factor of
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Range 0-1000 Meg-ohms, 500 Volt. Battery operated. Wide range clear meter 4½" × 4". Complete with decarrying case. hatteries instruc 10-10-05 Post 30p



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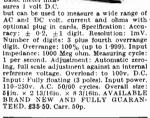


All transistorised, compact, fully port-able. AF sipe wave 18 Hz to 220 KHz. AF square wave 18 Hz to 100 KHz. Output sine / square 10v. P-P. RF 100 KHz to 200 MHz. Output 1v. maximum. Operation 220/240v. AC. Com-plete with instructions and | leads. 229-96. leads. £29.95 Post 50p.

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HONEYWELL DIGITAL VOLTMETER VT IOO

Can be panel or mounted. Basic meter mea-sures I volt D.C.



HAND HELD 2-WAY WALKIE TALKIES

Houstrial quality in robust metal cases.

Battery operation. Volume and squelch controls. Call button and press to talk button. Telescopic aerial. Complete carrying cases.

2 channel 452.50 Pair. Post 50p. 3 channel 675.50 Post 50p. Pair. Post 50p. Pair.

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each P. & P. 37P.
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Matched pair of stereo bookshelf speakers. Deluxe teak veneered finish. Size 14½" × 9" × 7½". 8 ohms. 8 watt RMS. 16 watt peak. RMS. 16 watt peak. Complete with DIN lead. £12.95 pr. Carr. 50p.

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Self contained, transistorsent contained, translatorised, battery operated.
Simply plug in microphone, guitar, etc., and output into your amplifier.
Volume control, depth of reverberation control. Beautiful walnut cabinet. 7½ × 3×4½ nt. 25–37. P. & P. 15p.

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Bands covering 550 Kc/s - 30 Mc/s. peaker 220/240v A.C. Brand new with instructions. £15.75. Carr. 37p.





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Industrial model 5A £3.



BATTERY CONDITION TESTER BATTERY CONDITION TESTER Made by Mallory but suitable for all batteries made by Ever Ready and others, most of which are zinc carbon types but also mercury manganese—nicad—eliver oxide and alkaline batteries may be tested. The tester puts a dummy load on the battery and the meter scale indicates the condition depending upon which section the pointer rests. The section reads "replace" "weak" or "good". The tester is complete in its case, size 33" × 64" × 2" with leads and prods. Price \$2.25 plus 20p postage.

SPIT MOTOR

1



200-250v Induction Motor, driving a carter gear box with 1½" of output drive shaft running at 5 revs per minute. Intended for rosating chickens, also suitable for driving models—windmills, coloured disc lighting effect, etc. etc. 21-25 plus 20p post and insurance.

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DRILL CONTROLLER NEW IKW MODEL Electronically changes speed from approxi-mately 10 revs. to maximum. Full power at all speeds by finger-tip control.

Kit includes all parts, case, everything and full instructions. 21.50. 13p post and p.

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MAINS TRANSISTOR POWER PACK

PACK
Designed to operate transistor sets and amplifiers. Adjustable output 6v., 9v., 12 volts for up to 500m Aclas B working). Takes the place of any of the following batteries: PPI, PP3, PP4, PP6, PP7, PP8, and others. Kit comprises: mains transformer rectifier, smoothing and load resistor, transformer rectifier, smoothing and load resistor, condensers and instructions. Real snip only £1.

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So thin is undetectable under carpet but will switch on with slightest pressure. For burglar alarms, shop doors, etc. 24" × 18" £1-40 13" × 10" £1-00

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Learn in your sleep: Have radio playing and kettle bolling as you awake switch on lights to ward off in-truders — have a warm house to come home to. All these and many

All these and many off you invest in an electrical programmer. Clock by famous maker with 15 amp. on/off switch to time can be set anywhere to stay on up to 6 hours. Independent 60 minute memory logger. A beautiful unit. Price 21-95 + 20pp. & p. or with glass front, chrome bezel, 79 extra.

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TELEPHONES
Complete as illustrated.
Save your legs, time and temper, simply by putting in some telephones. Ex. G.P.O. not new — but guaranteed in good condition and service able. Supplied with diagram and instructions showing how to connect. Price \$1 each + 50p post or 2 for \$2.50 post paid. Also available separately, dials and handsets 50p each + 20p post

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8ize approximately 1" × 1" 8p each, 10 for 72p.



SLIDE SWITCHES

Silde Switch, 2-pole changeover panel mounting by two 6B.A. acrews. Size approx. lin × 1hr rated 250V lanp. 6p each. 10 for 54p, 100 for £5-10, 500 for £24. Ditto as above but for printed circuit 5p each. 10 for 45p, 100 for £24.25. Sed Miniature Silde Switch. DPDT 19mm

(§in approx.) between fixing centres. 18p each or 10 for £1.08. SP Change over spring return 250v 1 amp. 10p.



SPRING COIL LEADS as fitted to telephones, 4 core 15p each, 10 for £1.35, 3 core 10p each

V.A.T. Please add V.A.T. 10% on total order after April 1st.

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Plays 12", 10" or 7" records. Auto or Manual. A high quality unit backed by BSR reliability with 12 months' guarantee. AC 200/250v. Size 18½ × 11; in. Above motor board 3½ in. Below motor board 2½ in.



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Powerful 3 watts output, 15 ohm. AG mains operated with transformer. 3-Controls, volume, treble, bass and On/off switch with knobs. Ready made on printed circuit board. Fused inputs and outputs. Famous make,

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Single play Stereo/ Mono Deram transcription ead and arm. Four speeds.

10 in. turntable.

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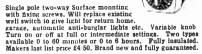
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Handbook of transistor equivalents			40p
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50/50V	10p	16+16/450V		100 + 50 +	- 50/3501	748p
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500mF 12V 15p; 25V 20p; 50V 30p.
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VOLUME CONTROLS | 80 Ohm Coax 40 yd.

BRITISH AERIALITE AERAXIAL-AIR SPACED 40 yd. £1.40; 60 yd. £2. Long spindles. Midget Size 5 K. ohms to 2 Mes. LOG or LIN. L/S 15D. D.P. 259. STERRED L/S 55p. D.P. 75p. STERRED L/S 55p. D.P. 75p. Edge 5K. S.P. 7 Transistor 25p. 1deal 025 and color. 10p, yd

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And crossover. 10 watt. State 3 or 8 or 15 ohm. As illustrated. Post 25p

With flared tweeter cone and ceramic magnet. 10 watt.

Bass res. 45-60 cps.
Flux 10,000 gauss.

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8 ohm, 10 wast, Large ceramic magnet. Special Cambric cone surround. Frequency response 30-12,000 cps. Ideal P.A. Columns, Hi-Fi Enclosure Systems, etc. Suitable cabinet 12 × 8 × 6 £4-00. Suitable cabinet 22 × 8 × 6 £4-00.



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The moving coil diaphragm gives a good radiation pattern to the higher frequencies and a smooth extension of total response from 1,000 cps to 18,000 cps. Size 3½ × 2in, deep. Rating 10 watt, 3 ohm or 15 ohm models.

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8 ohm 12 wait. Deep cone. Heavy ceramic magnet. Bass resonance 35 cps. Frequency response 30-8,000 cps.

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LOUDSPEAKERS P.M. 3 OHMS. 7. 4m. 21 25; 6:m. 21.50; 8 × 6in. 21-60; 8in. 21-78; 10 × 6in. 21-90; 10in. 22-90. SPECIAL OFFER: 80 ohm, 2; in. 23 ohm, 21:m. 35 ohm, 21:m. 28:m. 25:m. 25:m. 25:m. 25:m. 25:m. 25:m. 25:m. 25:m. 25:m. 21:m. 25:m. 25:m. 21:m. 21:m.

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New Model with new type slider volume controls. Stereo / Mono switch. 8 ohms. £10. switch. 8 ohms. £10.

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MODERN DESIGN. TEAK WOOD FINISH.



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30-14,500 c.p.s., 12in. double cone, woofer and tweeter cone together with a BAKER ceramic with a BAKER ceramic magnet assembly having a flux density of 14,000 gauss and a total flux of 145,000 Maxwells. Bass resonance 40 c.p.s. Rated 20 watts. NOTE: 3 or 8 or 15 ohms must be stated. 15 ohms must be stated

Module kit, 30-17,000 c.p.s. with tweeter. crossover. affle and £12.50 £12.50 instructions.

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WADDING 18in. wide, 15p ft

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Perrite aerial. 9 volt.

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THIN 1001 USES for every type of heating and
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ONLY 40p EACH (FOUR FOR £1 50)

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Robustly constructed to stand up to long periods of electronic power. As used by leading groups Useful response 30-13,000 cps Bass Resonance 55 cps

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4 inputs speech and music 4-way mixing. Response 10 30,000 cps. Matches loudspeakers 8/15ohm. A.C. 200/250V. Separate Treble and Bass controls Guaranteed. Details S.A.E.

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Size 3 ... 1 ... in. with knobs. 5K, 10K, 25K, 50K, 100K, 250K, 500K, 1 MEG, 2 MEG.

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HIGH QUALITY - BRITISH MADE

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12in. 15 watts

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Useful response 45-13,000cps
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use with any high fidelity system. Built-m concentric tweeter cone. Bass Resonance 30cps Flux Density 14,000gauss Useful response 25-16,000cps 8 or 15 ohms models.

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A high quality loudspeaker, its remarkable low cone resonance ensures clear its remarkable low cone
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reproduction of the deepest
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Bass Resonance 25cps
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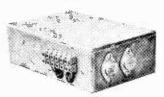
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PRACTICAL ELECTRONICS " SCORPIO" **ELECTRONIC IGNITION** SYSTEM



This Capacitor-Discharge Electronic Ignition system was described in the November and December issues of Practical Electronics. It is suitable for incorporating in any 12V ignition system in cars, boast, gockarts, etc., of either pos. or neg. earth and up to six cylinders. The original coil, plugs, points and contact-breaker capacitor fitted in the vehicle are used. No extra or special components are required. Helps to promote easier starting (even under sub-zero conditions), improved acceleration, better high-speed performance, quicker engine warm-up and improved fuel economy. Eliminates excessive contact-breaker point burning and the need to adjust point and spark-plug gaps with precision.

and the need to adjust point and sparkplug gaps with precision,
Construction of the unit can easily be
completed in an evening and installation
should take no longer than half an hour.
A complete complement of components
is supplied with each kit together with
ready-drilled roller-tinned professional
quality fibre-glass printed-circuit board,
custom-wound transformer and fully
machined die-cast case. All components are available separately. Case
size 72in x 42in x 2in approx,
Complete assembly and wring manual
25p, refundable on purchase of kit.
Price: £10-50 plus 50p P. & P.

DABAR LIGHTING EFFECTS



SINGLE CHANNEL SOUND TO LIGHT UNIT STL/I

Single channel " Sound to Light." unit with slider fader controls for audio trigger level and background load dimmer.

load dimmer.
Switchable for response to High,
Mid and Low frequency audio input
signals selected by fascia control.
D.J. Pulse-Flash push button
fitted to fascia for manual flashing
of lamp load. Neon load indicator fitted.

Constructed on glassfibre printed circuit material with attractive black anodised fascia panel, Input and load connections via Cinch printed circuit connector. Maximum Load IkW at 250V

R.F.I. filtered.

Price: £13 each post free U.K.

S.A.E. All Enquiries please



THREE CHANNEL **SOUND TO** LIGHT UNIT STL/3

Three channel " Sound to Light unit with slider fader controls for audio trigger level and back-ground load dimmer.

An attractive unit with indepen-dent control of High, Mid and Low frequency audio trigger levels Slider fader background or dimmer controls on each channel D.J. Pulse-Flash push buttons on each channel together with neon load indicators

load indicators
Constructed on glassfibre printed
circuit material with attractive
black anodised fascia panel.
Input and load connections at
rear so unit is ideally suited for
mounting into disco-console.
Maximum Load I 5kW per
channel at 250V 50Hz,
R.F.I. filters incorporated

R.F.I. filters incorporated Price: £38.50 each post free U.K.

Trade enquiries Welcome

PSYCHEDELIC LIGHTING UNIT Mk. 3



This unit represents a natural progression from our phenomenally successful Mk. I and 2 Units. As before the drive voltage is derived directly from the amplifier output or across the speakers. The unit converts the audio frequency signals into a three-coloured light display; the colour depending on the frequency of the signal and the intensity on the loudness of the audio source.

intensity on the loudness of the audio source.

The unit is constructed on professional fibre-glass printed-circuit board material and uses latest full-wave true circuitry. There is a master-level control circuitry. There is a master-level control, together with independent sensitivity controls for each channel and the sensitivity controls for each channel permitting their use as faders; allowing dimming from max. to zero at the turn knob R. F.I. suppression is provision for D. "Pulse-Flash" controls. The choice of two inputs enables operation from both high and low power amplifiers. Max. power I 5kW per channel at 240V a.c.

Complete assembly built and tested, Size 9 in × 7 in × 3 in. Price £25 carr. paid.

plete assembly built and tested 7in × 7in × 3in. Price £25 carr. paid

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66 ELMS ROAD, ALDERSHOT, Hants



F.M. TUNER AMPLIFIER for 88-102 MHz. Self-powered for 200-250v. a.c. Valves ECC55, EF59, EF80, ECC82, 2 diodes, netal rect. Chassis 10" x 6" x 6". Audio amp. nodule giving 3W. into 16-ohm. 6". Audio amp. no Price £14 (post 50p).

Kit and wiring instrs. for 12V windscreen wiper delay control: metal box 3½" 3½" × 1½" with fixing strap, relay and all compts. £1.50 (post 20p).

MAINS TRANSFORMERS, 240-250v, input Deduct 10% from total bill for more

n one transformer.

B. Charger 12v. at 1 \(\frac{1}{2} \) A, \(60p (20p) \)

E. 250v. at 50 m.a., \(\frac{1}{6} \) 6-3v at 1 \(\frac{1}{4} \), \(50p (20p) \)

H. 99v. at 100 m.a., \(220v. at 50 m.a. \) \(85p (20p) \)

J. 37v. 2A, 24-0-24v. 150m.a. \(\frac{2}{6} \) 5(50p)

K. 250-0-250v. 150m.a. 20v. \(\frac{1}{4} \) 15v. 1A. \(6-3v. 5A. \) \(\frac{2}{6} \) (50p)

L. 275-0-275v. 80m.a. \(6-3v. \) 2\(\frac{1}{4} \) A \(6-3v. \) \(\frac{1}{4} \), \(75p (25p) \)

M. 110v. input; \(200-0-200v. 50m.a. \(6-3v. \) 1\(\frac{1}{4} \), \(60p (25p) \)

N. 220v. 50m.a. \(6v. 1A. \) \(45p (25p) \)



STEREO AMPLIFIER 2 × 3W. Printed circuit. Valves
EZ80 & 2 ECL82. Liquidated stock of well-known
manufacturer. Front panel 12" x 2". Chassis 9" × 3".
Controls on-off, balance, ganged vols., ganged tones;
for 200-250v. ac. Output transformers for 3-ohm speakers.
With knobs. Also available for 110v. a.c. Only \$8 (p. & p. 50p)

110v. type £5 plus post.

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Gang capacitors. Min. 180pf+180pf 20p (8p); 150+110pf 30p (10p) 250+250pf dust cover 30p (8p); 250+250p dust cover, slow motion 20p (5p); triple 335pf direct drive with slow motion 60p (10p).

Driver transformers, 2-5 to 1+1 20p (8p); 5-7 to 1+1 20p (8p); Output trans, 2x OC81 to 3-ohm 25p (5p); 2x OC82 to 3-ohm 20p (5p); Erigewise pots (s,p.) #" dias 2-5K or 5K 15p (5p); 25 K) 1" dia 25p (5p); pots with 5/64" dias spinide 2-5K 1" dia 25p (5p); pots with 5/64" dias spinide 2-5K 2" long spinde 15p (5p) with knob; 2-5K 1; " spin. 15p (5p) with knob; all pots with s. pole switch. switch

Osc. coil & 3 i.f. trans. replacement for P50 1AC range set of 4 for 80p, post pd.

ib (min. 100) high stab resistors i W to 1W up to 2.5M 50p (10p post); ib mixed tag strips 2 to 12 way approx. 75 for £1 (10p post); spring back telephone cable; 10° coil ext. to 6tt, 4-core 15p (10p post) or 7 for £1 post pt.; AUDIO CONNECTORS, PLUGS 2-pin speaker 10p; 3-pin D1N 14p; 5-pin 17p; phono 5p; i' jack 12p; : 5-mm 6p; METAL phono 12p; i'' 12pp: 2-mm 10p; 3-5mm 12p; SOCKETS 2-pin apeaker 10p; 3 & 5 pin D1N 9p; phono single 5p; double 7ip; rebel 10p; i 4-way 12ip; i'' jack open 15p; moulded 20p; stereo open 20p; moulded 25p; LINE SOCKETS speaker, 3-pin & 5-pin D1N 17p; phono metal 12p; co-ax. T.V. plug 8p; car radio plug 6p; either socket 8p. Post 10p any order.

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This 4 digit 24 hour clock is available to readers at this special price for I month only. Parts would normally cost over £25. Kit of parts includes twelve IC's, indicators, and a smart white plastic case.

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SN7400	16p	15p	SN7423	55p 5	50p	8N7450	16p	15p	SN7489	6 - 05p	5 85	5 n
SN7404	16p	15p	8N7425	55p 5	50p	SN7451	16p		SN7490	74p	72	
8N7402	16p	15p	SN7427	49p 4	16p	9N7453	16p		8N7491		1 . 04	
SN7403	16p	15p	SN7428		72p	SN7454	16p		SN7492	74p	72	
SN7404	16p	15p	SN7430		l5p	SN7460	16p		SN7493	74p	72	
SN7405	16p	15p	8N7432		16p	SN7470	33p		SN7494	85p	72	
8N7406	38p	35p	SN7433		32p	8N7472	33p		SN 7495	85p	72	
SN7407	38p	35p	SN7437		39p	8N7473	41p		8N7496	95p	92	
SN7408	20p	18p	8N7438		39p	SN7474	41p		SN74100	1 - 80 p	1 . 75	
SN7409	20p	18p	SN7440		5p	SN7475	50p		8874104		1.08	
SN7410	17p	15p	887441		70p	8N7476	44p		8N74105			
SN7411	27p	25p	8N7442		70p	8N7480	73p		SN74107		42	
SN7412	38p	35p	SN7443	1 43p 1 3		8N7481	1 - 32p		8N74110		59	
8N7413	32p	29p	8N7444	1 43p 1 3		8N7482	97p	95 p	SN74111			
8N7416	47p	43p	8N7445	2 · 00p 1 · 9		8N7403		1 · 15p	8874118	1 · 10n	1.05	, P
8N7417	47p	43p	8N7446	1 · 07p 1 · 0		8N7484		1 05p	SN74119	1 · 47n	1.37	
SN7420	16p	15p	8N7447	1 10p 1 0		SN7485		3 · 85 p	SN74121	44p	41	
SN7422	55p	50p	SN7448	1 10p 1 0		SN7486	36p	35p	8N74122		1 43	
		* Dev	vices ma	y be mix	ed	to qualif	-	-		,	_ 10	

* 100 Plus less 10% off 25 plus break

Linear Integrated Circuits

301	DIL	50p	723e	DIL	99p
301	TO99				
		55p	723e	TO99	95p
301	8 PIN DIL	46p	741c	8 PIN DIL	38p
301A	DIL	69p	741c	14 PIN DIL	39p
301A	TO99	69p	7410	TO99	41p
301A	8 PIN DIL	66p	747e	DIL	46p
307	DIL	69p	748e	DIL	39p
307	TO99	69p	748c	T'O99	41p
307	8 PIN DIL	66p			
308	TO99	6 · 45p	1437	DIL	1 · 27p
30NA	TO99	6 · 40p	1458	TO99	1.27p
709c	DIL	35p	3046	DIL	84p
709e	TO99	31p	7503	DIL	1 · 27p



Electrolytic Capacitors

	4 VC	LT	16 VC	LT	40 V C	OLT
	47 _μ F 100μF 220μF 330μF 1000μF 4700μF	6½p 6½p 6½p 6½p 13p 29p	15µF 33µF 68µF 150µF 220µF 680µF 1000µF 1500µF	6½p 6½p 6½p 8p 9p 17p 17p 25p 43p	47μF 100μF 150μF 220μF 470μF 680μF 1000μF 2200μF	6 ½1 91 101 191 251 251 441
	6 3 V C	DLT	2000,21	456		
	33μF 68μF 150μF 470μF 680μF 1500μF 2200μF 3300μF	6 ½ P 6 ½ P 6 ½ P 1 1 P 1 3 P 1 8 P 1 8 P 2 6 P	25 VC 10 μF 22 μF 47 μF 100 μF 150 μF 220 μF 470 μF	6 ½ p 6 ½ p 6 ½ p 8 p 8 p 10 p 13 p	63 ∀ C IµF 2∙2µF	≻LT 6½, 6½,
-	١		680µF	20p	4 · 7 µF	6 ½ p
	10 VO 22μF 47μF 100μF 220μF	6 ½ p 6 ½ p 6 ½ p 8 p	1000μF 2200μF 5000μF	22p 39p 68p	6 8μF 10μF 22μF 68μF 100μF	6 ½ p 6 ½ p 10 p
ĵ	330µF	I Op	40 V O		150μF	135
	470μF 1000μF	10p 11p	6·8μF	6∮p	220μF 330μF	19p
	1500μF	20p	15μF	6 ¹ ⁄ ₂ P	470µF	26p
	2200μF	24p	33μF	6 1 p	1000µF	44p

BARGAIN PACKS

,	Unmarked Packs	
,	Pack of 25 1N4448 55p	
	Pack of 10 BC108 BC107	55

BC107	55
(Plastie can)	
Pack of 10	_
Plastic BC10	9
55p	
	-

1	Pack of 8C169	10	55p
	but tes		

2N264633p each

Pack of 10 unbranded but tested

Transistors

V								MULLARD
AC107 16p		BF260	29p		14p	Diodes	- 8r	250V P.C. mounti
AC126 14p AC127 13p	BC142 38		18p	OC45	14p	Rectifi	ers	0-15μF, 0-22μF, 5
AC127 13p	BC143 35		18p	OC70	23p			
AC142K 22p	BC144 36 BC145 26		37p	0C71	14p	1N914	8p	MULLARD
ACIAIK 20p		Bp BFX84 D BFX85	28p	OC72	14p	1N916 1N4148	8p	400 V: 0:00 IμV, 0
AC176 15p		p BFX86	35p 22p	OC81 OC83	14p	1844	8p	$0.022 \mu F$, 0.033μ
AC187 13p		p BFX87	28p		22p	1N4007	10p 22p	12p. 0 47µF, 141
AC187K 20p	BC153 16		26p	OC84 T1P29A	28p 53p	18113	17p	160V: 0.01μF, 0
AC188 13p	BC154 17		21 p	TIP30A		18120	17p	0.22µF, 51p, 0.3
AC188K 20p	BC157 13		17p	TIPSIA		18121	15p	VOLUME C
ACY17 24p	BC158 12		17p	TIP32A		18130	9p	Potentiometers
ACYIN 21p	BC159 14		39p	TIP33		18131	11p	Carbon track 500
ACY19 25p	BC167 18		72p	TIP34A		18132	13p	Log or Linear
ACY20 22p	BC168 11		19p		1.54	18920	8p	Single 13p. Due
ACY21 23p	BC169 11		220	TIP35A		18922	9p	Single type with
ACY22 18p		p C426	33p		2.53	18923	13p	
ACY39 68p		p C428	31p	TIP36A	-	18940	бр	SLIDE POT
AD140 40p		p C450	17p		3 19	AA119	11p	58mm, TRACK
AD142 44p		p MP8111	35p	TIP41A	79p	AA129	11p	SINGLE GANG
AD143 39p		p MP8112	42p	TIP42A	91 p	AAZ13	11p	45p each
AD149 38p		3p MP8113		2N706	13p	AAZ15	14p	TWIN GANGEI
AD150 60p	BC515F 11	p MP8121		2N930	23p	AAZ17	14p	66p each.
AD161 29p	BC213L 11			2N1131	22p	BA100	16p	CARBON S
AD162 29p	BC214L 11	p MP8123		2N1132	28p	BA102	25p	Small high quali
AD M/P 50p	BC258 8	p NKT21		2N1613	22p	BA115	8 p	All valves 100-2
AFII4 14p		p NKT21:		2N1711	26p	BA144	14p	-1 watt 5
AF115 14p	BC267 14			2N2904	40p	BA145	22p	-2.5 watt
AF116 14p		p NKT21		2N2904.		BA154	14p	
AF117 14p		p NKT26			44p	BAX13	14p	VEROBOAR
AF118 92p		P NKT27		2N2905	46p	BAX16	14p	
AF124 27p		Dp NKT27-		2N2924	18p	BAY18	19p	21in × 31in
AF139 39p AF239 41p		p NKT27		2N2926	10p	BA Y 31 B Y 100	9p	2∤in × 5in
AF239 41p AL100 77p		p NKT40:		2N3053	26p	BY126	19p 16p	3∄in × 3∄in
AL102 66p				2N3054	55p			3‡in × 5in
AL102 00p		7p NKY60	66p	2N3055 2N3405	52p	BY127	19p	5in × 17in (plair
ASY26 31p		Bp NKT61:		2N3663	44p 57p	BYXIO	24p	Vero Pins (hag o
ASY27 40p		Op AK 101.	33p	2N3702	9p	OA5	19p	Vero cutter, 50p;
AU 103 99p		Bp NKT67		2N3702	9p	OA9	11p	0.15 matrix) at
AU 110 £1.10		p NKT67		2N3704	9p	0A10	24p	SLIDE SWIT
AUTH 77p		20	24p	2N3705	9p	OA47	9p	SPST 11p each.
BC107 9p		D NKT71		2N3706	9p			
BC108 9p	BD141 £1-8			2N3707	9p	OA70	8p	MINIATUR
BC109 9p		p O(19	55p	2N3708	9p	OA73	11p	240V or 110V 1-
BC113 15ap		3p OC20	55p	2N3709	9p	OA79	8p	MINITRON
BC116 16p		D OC23	33p	2N3710	90	0.481	9p	INDICATO
BC125 16p		3p OC25	28p	2N3711	95	OAR5	11p	
BC126 25p		9p OC28	33p	2N3794	17p	OA90		Reads 0-9 and
BC132 16p		5p OC29	33p	2N3819	28p		8p	(Data Sheet o
BC134 16p		5p OC35	38p	40361	50p	OA91	8p	ONLY EL 5
BC135 16p		7p OC36	38p	40362	50p	0.495	8p	16 DIL Socket
BC137 16p		7p OC41	14p	40636	50p	OA200	11p	Driven by 7447

MULLARD POLYESTER'S

MULLARD POLYESTER CAPACITORS C280 SERIES

Carbon track 500 Ω to 2-2M Ω
Log or Linear
Single 13p. Dual gang (stereo) 44p
Single type with D.P. switch 13p extra.
CLUDE BOTENTIOMETERS

Small high quality type (linear only). All valves 100-5 meg ohms.

-2.5 watt	6 p each		
VEROBOA	RD 0	15	0.1
	M	atrix	Matrix
21in × 31in	14	9°D	26p
21 in × 5in		8p	28p
3fin × 3fin		8p	28p
3∮in × 5in		3 p	32p
5in × 17in (pl		4p	
Vero Pins (hag		,	
Vero cutter, 50	n: Pin inse	rtion Te	bols (0.1 and
0.15 matrix) a			

MINIATURE NEON LAMPS

MINITRON DIGITAL INDICATOR TYPE 3015F Reads 0-9 and decimals

(Data Sheet on request)
ONLY £1 50 33p £1.05

 $250 \rm V.P.C.$ mounting: $0.01 \mu F, 0.015 \mu F, 0.22 \mu F, 3 jp, 0.33 \mu F, 0.047 \mu F, 0.068 \mu F, 4 p.0.1 \mu F, 4 jp, 0.15 \mu F, 0.22 \mu F, 5 jp, 0.33 \mu F, 7 p, 0.47 \mu F, 0 jp, 0.68 \mu F, 12 p, 1.0 \mu F, 14 p, 1.5 \mu F, 22 p, 2.2 \mu F, 27 p, 0.47 \mu F, 12 p, 1.0 \mu F, 14 p, 1.5 \mu F, 22 p, 2.2 \mu F, 27 p, 0.47 \mu F, 12 p, 1.0 \mu F, 14 p, 1.5 \mu F, 12 p, 1.0 \mu F, 12$

MULLARD POLYESTER CAPACITORS C296 SERIES 400 V: 0-001μF, 0-0015μF, 0-0012μF, 0-0013μF, 0-0012μF, 0-0013μF, 0-0015μF 0-0022μF, 0-0047μF, 21p, 0-0068μF, 0-01μF, 0-015μF 0-022μF, 0-033μF, 31p, 0-047μF, 0-018μF, 0-1μF, 41p, 0-15μF, 61p, 0-122μF, 81p, 0-33μF, 12p, 0-47μF, 14p, 0-15μF, 0-01μF, 0-01μF, 0-01μF, 0-033μF, 0-047μF, 0-01μF, 0-01μF, 0-01μF, 0-033μF, 0-047μF, 0-047μ

800

VOLUME CONTROLS

Potentiometers	RECT	TIFIERS
Carbon track 500 Ω to 2-2M Ω Log or Linear	P.1.V.	1 AMP
Single 13p. Dual gang (stereo) 44p Single type with D.P. switch 13p extra.	100	IN4001 4 IN4002 4
CLUDE BOTENTIOMETERS	200	IN4003 5

SLIDE POTENTIOMETERS 58mm, TRACK SINGLE GANGED, LOG or LIN 1k to 1M. 45p each TWIN GANGED, LOG or LIN 1k to 500k.

CARBON SKELETON PRESETS

-1 watt 54pe 2-5 watt 64pe			50	33p	53p
VEROBOARD	0·15 Matrix 19p 28p 28p 33p	0·1 Matrix 26p 28p 28p 28p 32p	100 200 400 600 800	35p 37p 40p 44p 49p	57p 60p 64p 66p
Sin × 17in (plain) Vero Pins (hag of 36)	94p , 22p		THY	rRIST	ORS

SLIDE SWITCH SPST 11p each. D.P.D.T. 13p each.

240V or 110V 1-4 5p, 5 plus 41p each

RESISTORS

1 Amp 28 3 Amps 44

7 Amps

PIV

i watt 5% carbon 1p each i watt 10% carbon 1p each 1 watt 10% carbon 2ip each Range 10 ohns to 4.7 meg. i watt m/o 2% 3p each Range 10-1 meg ohns

50 100

IN4001 4±p IN4002 4±p IN4003 5±p IN4004 6±p IN4005 8p

IN4006 9p IN4007 10p

BRIDGE RECTIFIERS

P.I.V. 1 AMP 2 AMP 5 AMP 10 AMP

200 300 400

53n

Umnarked	but fully
2 N 30	
1-9	າລວ 33 ໘
10 plus	27

FULLY MARKED TYPES

1:5 AMP

PL4001 8p PL4002 9p PL4003 10p PL4004 10p PL4005 13p

PL4006 15p

£1.76p £2.20p £1 98p £2 15p £2 42p

£2 31p £2 42p £2 75p

1-9	59p
10 plus	53p
BC107-B	C108
BC10	
1-9	9p
10-99	8p
100 24226	Rin

AD161, AD162 M/P

BC	182L:-3-	4-212-4
1-9		91
101	lus	81

AC127	OF	AC128
1 -9		131
10 plus		121
100 plus		111

ZENER DIODES

400 M/W 5% Miniature BZY 88 Range

All voltages 3 3 - 33 Volt 9p rach

I watt 5% All voltages 6-8-200 Volts 14p each

10 watt 5% All Voltages 7:5-100 Volts 51p each

Sinclair Project 60

Now-the Z.50 Mk.2

with built-in automatic transient overload protection

When originally introduced, the Sinclair Z.50 proved how it was possible to design and produce a popularly priced modular power amplifier having characteristics to challenge the world's costliest amplifiers. Many thousands of Z.50's are now giving excellent service day in, day out. But we have also learned that constructors do not always use their Z.50's ideally. That is why we have introduced modifications whereby risk of damage through miss-use is greatly reduced and performance further enhanced. The Z.50 Mk.2 has improved thermal stability, more accurately regulated D.C. limiting to ensure more symetrical output voltage swing and clipping and still less distortion at lower power. Z.50 Mk.2 is compatible with all other Project 60 modules, and may be incorporated to advantage in existing systems. Eleven silicon epitaxial planar transistors are now used, two more than in the original Z.50; circuitry has been re-designed, making this versatile high performance amplifier better than ever.



manual £5.48

Z.30 the power amplifier for quality and economy



with free manual

The Z 30 provides excellent facilities for the constructor requiring a high fidelity audio system of less power than that available from Z.50's. Using a power supply of 35 volts, Z 30 will deliver 15 watts RMS into 8 ohms, or 20 watts RMS into 3 ohms using 30 volts. Total harmonic distortion is a fantastically low 0.02% at 15 watts into 8 ohms with signal to noise ratio better than 70 dB unweighted. Input sensitivity 250mV into 100K ohms. Size 80 x 57 x 13 mm ($3\frac{1}{8}$ x $2\frac{1}{8}$ x $\frac{1}{2}$ J Z 30, Z 50 and Z.50 MK.2 modules are compatible and interchangeable

Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, you money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sinclair Radionics Ltd.

Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defect arise in normal use, we will service it at once and without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically E1.00) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.



Brilliant new technical specifications

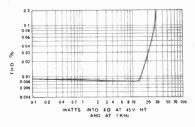
Input impedance 100 K Ω Input (for 30w into 8 Ω) 400mV Signal to noise ratio, referred to full o/p at 30v HT 80dB or better

Distortion 0.02% up to 20W at 8Ω . See curve Frequency response 10Hz to more than 200 KHz \pm 1dB

Max. supply voltage 45v (4Ω to 8Ω speakers) ($50v15\Omega$ speakers only)

Min. supply voltage 9v

Load impedance — minimum; 4Ω at 45v HT Load impedance — maximum; safe on open circuit



Typical Project 60 applications

System	The Units to use	together with	Units cost	
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc.	£4.48	
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control, etc.	£9.45	
12W. RMS continuous sine wave stereo amp. for average needs	2 x Z.30s, Stereo 60; PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£23.90	
25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60; PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90	
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms)	2 x Z.50s, Stereo 60; PZ.8, mains transformer	As above	£34.88	
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43	

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+12 to -12dB at 100Hz. Front panel: brushed aluminium with black knobs and controls. Size: 66 x 40 x 207mm.

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Project 60 Stereo F.M. Tuner



The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stero decoder and switchable squelch circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems

SPECIFICATIONS—Number of transistors: $16 \, \text{plus} \, 20 \, \text{m} \, 1 \, \text{C.}$ Tuning range: $87.5 \, \text{to} \, 108 \, \text{MHz}$. Sensitivity: $7 \, \mu \text{V}$ for lock-in over full deviation. Squelch level: Typically $20 \, \mu \text{V}$. Signal to noise ratio: $> 65 \, \text{dB}$. Audio frequency response: $10 \, \text{Hz} \, - 15 \, \text{KHz} \, (\pm 1 \, \text{dB})$. Total harmonic distortion: $0.15 \, \text{m} \, \text{for} \, 30 \, \text{m}$ modulation. Stereo decoder operating level: $2 \, \mu \text{V}$. Cross talk: $40 \, \text{dB}$. Utular voltage: $2 \, \text{x} \, 150 \, \text{mV}$ R.M.S. maximum Operating voltage: $25 \, - 30 \, \text{VDC}$. Indicators: Stereo on ; tuning. Size: $93 \, \text{x} \, 40 \, \text{x} \, 207 \, \text{mm}$.

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SPECIFICATIONS

Output power: 8 watts RMS continuous (12 watts peak). $6-8\Omega$. Frequency Response: 5Hz to 1C0KHz \pm 1dB. Total Harmonic Distortion: Less than 1%. (Typical 0-1%) at all output powers and frequencies in the audio band (28V). Load Impedance: 3 to 15 ohms. Input Impedance: 250 Kohms nominal. Power Gain: 90dB (1,000,000,000 times) after feedback. Supply Voltage: 6 to 28V. Quiescent current: 8mA at 28V. Size: 22 × 45 × 28mm including pins and heat sink

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\text{each or 100 for \$\frac{2}{1}\text{N} \text{ \$\frac{5}{2}\text{ \$\frac{7}{2}\text{D}_1}\$ \\
\text{VEROBOARD} \quad 0-1 \quad 0-15 \\
\text{24" \times 6" 25p 25p 5k-2M Log and Lin 2\psi'* \text{34" 23p 17p single 15p, single 13p, studied 3\psi'* \text{ \$\frac{7}{2}\text{ \$\frac{ VEROBOARD 0-1 0-16 CARBON POTS 24" × 6" 25p 5 5×2M Log and Lin 24" × 34" 23p 17p single 15p, studied 34" × 5" 25p 30p with SW. 24p, dudied 34" × 34" 25p 25p 30p with SW. 24p, dudied 34" × 34" 25p 25p 42p. STREEP WIRE 2 Pin DIN Plug 12p, 8kt. 10p 9, stereo 9p, quad 5 Pin DIN Plug 18p 6t. 10p 9p, stereo 9p, quad 5 Pin DIN Plug 18p 6t. 10p 9p, stereo 9p, quad 5 Pin DIN Plug 18p 6t. 10p 9p, stereo 9p, quad 5 Pin DIN Plug 18p 6t. 10p 9p, stereo 9p, quad 5 Pin DIN Plug 18p 6t. 10p 9p, stereo 9p, quad 5 Pin DIN Plug 18p 6t. 10p 9p, stereo 9p, quad 5 Pin DIN Plug 18p 6t. 10p 9p, stereo 9p, quad 5 Pin DIN Plug 18p 6t. 10p, p

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1 R.5	0.45	6BE6 0.32	6F25 1.00	0 10LD11 0.70		aerv			EL37	1.70	PC86 0.60	PL504 0.75	
		6BF6 0.55	6F26 0.8		Access				EL41	0.75	PC88 0.60	PL508 0.90	UBC81 0.45
184	0.80		6F28 0.70				10 MA	LVEC	EL81	0.55	PC92 0.05	PL509 1.10	UBF80 0.40
185	0.30				FLEC	TRON	IC VA	LVES	EL83	0.50	PC97 0.50	PL801 1.00	UBF89 0.40
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1 V 2	0.55	6BN6 0.60	6J6 0.80		30C15 1.00	85A2 0.55	DY51 0.55					PY33 0.68	UCC85 0.45
1X2B	0.55	6BQ5 0.25	6J7 0.4	5 12AT6 0.40	30C17 1.10	90AG 2.40	DY86 0.35	ECC91 0.30	EL90	0.42	PCC88 0.55		
2021	0.40	6BR8 0.75	6K477 0.60	0 12AT7 0.40	30C18 0.90	90 A V 2.50	DY87 0.36	ECC189 0.65	EL360	1.15	PCC89 0.55	PY80 0.40	
		6BS7 1.35	6K 6GT 0.7		30F5 1.00	90C1 0.75	DY802 0.37	ECC807 1.00	EL821	0.60	PCC189 0.60	PY81 0.30	UCH21 0.60
3A4	0.45		6K7 0.4		30FL1 0.80	90CV 2.40	E80F 1.10	ECF80 0.35	EL822	1.40	PCC805 0.95	PY82 0.35	UCH42 0.70
3 A 5	0.75	6BW6 0.90			30FL12 1.10	807 0.50	E88CC 0.70	ECF82 0.35	ELL80	0.75	PCC806 0.95	PY83 0.38	UCH81 0.40
3BP1	3.50	6BW7 0.90			30FL14 0.90	813 4.00	E180F 1.00	ECF8041.65	EM34	1.00	PCF80 0.30	PY88 0.40	UCL81 0.60
384	0.40	6BX6 0.25	6K25 0.7				E810F 2:90	ECH42 0.75	EM71	0.80	PCF82 0.35	PY800 0.47	UCL82 0.85
3 \ 4	0.65	6BZ6 0.45	6L6GT 0.5		30L1 0.40	866A 0.85		ECH81 0.30	EM80	0.45	PCF84 0.60	PY801 0.50	UCL83 0.65
5R4GY	0.75	6C4 0.35	6L7 0.4		30L15 0.95	5642 0.70	EABC800.38			0.60	PCF86 0.60	PZ30 0.38	UF9 0.65
5U4G	0.40	6C5GT 0.55	61.18 0.5	0 12B4A 0.65	30L17 0.95	6080 1.75	EAF42 0.60	ECH83 0.45	EM81			QQVO2-6	UF11 0.60
5 V 4 G	0.50	6CB6 0.40	6LD20 0.5	0 12BA6 0.45	30P12 1.00	6146 1.60	EBC33 0.60	ECH84 0.45	EM83	0.50	PCF87 1·10	QQ102-0	
5Y3GT		6CD6GA	6N7GT 0.5		30P19 0.95	6146B 2.50	EBC41 0.65	ECL80 0.50	EM84	0.35	PCF801 0.50	2.25	
		1.80	6P28 0.69		30PL1 0.95	6360 1.25	EBC81 0.33	ECL81 0.50	EM85	1.00	PCF802 0.50	QQVO3-10	
523	0.75	6CG7 0.60	697 0.5		30PL13 1.10	6939 2.25	EBF80 0.40	ECL82 0.35	EM87	0.70	PCF805 0.90	1.25	UF43 0.65
5Z4G	0.45		68A7 0.4		30PL14 1.25	7199 0.85	EBF83 0.40	ECL83 0.70	EN91	0.40	PCF806 0.75	QQV03-20A	UF80 0.35
6/30 L2	0.90	6CH6 0.60			35 A3 0.60	7586 1.50	EBF89 0.32	ECL84 0.55	EY51	0.40	PCF808 0.90	5.25	UF85 0.40
6.4 B.4	0.45	6CL6 0.60	6SG7 0.4		35A5 0.75	7895 1.50	EBL31 1.50	ECL85 0.55	EY80	0.75	PCH2000.70	TT21 3.40	UF89 0.40
6AF4A	0.60	6CU6 0-80	68K7 0.5			A2293 2:20	EC53 0.50	ECL86 0.40	EY81	0.40	PCL81 0.50	TT22 3.50	UL41 0-65
6AG5	0.25	6CW4 0.70	68L7GT0.4		35B5 0.65		EC86 0.60		EY83	0.55	PCL82 0.35	U18/20 0.75	UL84 0.48
6AG7	0.45	6CY5 0.50	68N7GT0.4		35C5 0.60	AZ1 0.60		EF37A 1.00	EY86	0.40	PCL83 0.65	U25 0.85	UM84 0.80
6.1116	0.60	6CY7 0.75	68Q7 0.50		35 D5 0.75	AZ31 0.55	EC88 0.60	EF40 0.50				U26 0.85	UYIN 0.50
6AJ8	0.30	6D3 0.55	68R7 0.5	0 20L1 1.10	35 L6GT 0.75	CBL1 0.90	EC90 0.35	EF41 0.65	EY87	0.43	PCL84 0.45		UY11 1.00
	0.40	6DC6 0.80	618 0.3		35 W 4 0.40	CBL31 1.00	EC92 0.45		EY88	0.43	PCL86 0.45	U31 0.70	
6AK5		6DK6 0.60	6U4GT 0.70		3573 0.75	CY1 0.50	EC93 0.60	EF42 0.70	EZ40	0.50	PCL88 1.25	U37 6.50	UY41 0.48
6AK6	0.60		6U5G 0:7		35Z4G 0,40	CY31 0.50	ECC35 1.00	EF80 0.30	EZ41	0.75	PCL200 0.75	U52 0.40	UY82 0.50
6AL3	0.43	6DQ6B 0.75	6U8A 0.4		35Z5GT0.70	DAF96 0.50	ECC40 0.70	EF85 0.85	EZ80	0.28	PCL800 1.10	U76 0.40	UY85 0.40
6 A L5	0.22	61)84 1.25			50 A5 0.80	DF96 0.50			EZ81	0.29	PCL801 0.95	U78 0.40	W729 0.75
6A M5	0.40	6EA8 0.65	6V6GT 0.4			DK92 0.70	ECC81 0.40	EF86 0.30	GTIC	3.00		U191 0.75	
6AM6	0.37	6EH7 0.80	6X4 0.4				ECC82 0.33	EF89 0.28	G Y 501	0.70	PCL805 0.50	U201 0.50	Y63 0.75
6AQ5	0.42	6EJ7 9.35	6X5GT 0.4		50C5 0.60	DK96 0.60	ECC83 0.83	EF91 0.37	GZ30	0.45	PD500 1.80	U281 0.55	Z759 8.00
6AQ6	0.70	6EW6 0.70	6X8 0.6		50CD6G1.20	DL96 0.55			GZ31		PF86 0.70	U282 0.55	Z803U 1.35
6AR5	0.55	6F1 0.75	6Y6G 0.8	0 30 A E3 0.40	50EH5 0.65	DM70 0.60	ECC84 0.80	EF92 0.85	GZ31	0.40	11700 0.70	0.202 0.30	(2000 0 1.00
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IKM				BD121	0.65
2N696	0.15	AC128	0.15	BD123	0.80
2 N 697	0.15	AC132	0.35	BD124	0.60
2N698	0.30	AC153	0.20	BD131	0.75
2N705	0.70	AC154	0.15	BD132	0.80
2N706	0.10	AC157	0.17	BF115	0.20
		AC169	0.10		
2N708	0.15			BF167	0.18
2N753	0.25	AC176	0.17	BF173	0.20
2N929	0.20	AC187	0.25	BF179	0.80
2N930	0.20	AC188	0.25	BF180	0.80
2N997	0.80	ACY17	0.25	BF181	0.80
2N1131	0.25	ACY18	0.20	BF184	0.20
2N1132	0.25	ACY19	0.25	BF185	0.20
2N1184	1,25	ACY20	0.20	BF194	0.14
2N1302	0.17	ACY21	0.20	BF195	
	0.17	ACY22	0.10		0.14
2N1303	0.17	AD140	0.60	BF196	0.12
2N1304	0.20	AD149	0.45	BF197	0.12
2N1305	0.20			BF200	0.35
2N1306	0.25	AD161	0.85	BFW87	0.25
2N1307	0.25	AD162	0.35	BFW88	0.20
2N1308	0.25	ADZ11	1.25	BFW89	0.20
2N1309	0.25	ADZ12	1.25	BFW91	0.20
2N1613	0.17	AF114	0.17	BFX88	0.20
2N1711	0.20	AF115	0.17	BFY17	0.40
2N1756	0.75	AF116	0.17		
		AF117	0.17	BFY19	0.25
2N2147	0.75	AF118	0.17	BFY50	0.20
2N2160	0.60		0.80	BFY51	0.20
2N2217	0.25	AF125	0.20	BFY52	0.20
2N2218	0.20	AF127	0.20	B8 Y 26	0.17
2N2219	0.20	AF180	0.35	BSY27	0.15
2N2369A	0.15	AF181	0.35	BSY28	0.17
2N2477	0.65	AF186	0.40	B8Y65	0.20
2N2646	0.40	AF239	0.86	BSY95A	0.12
2N2905	0.25	AFZ11	0.45	OC16	0.50
2N2923	0.12	AFZ12	1.00		0.50
2N2924	0.12	A8¥26	0.25	OC22	
2N2924 2N2926	0.10	ASY27	0.30	OC23	0.60
	0.10	ASY28	0.25	OC24	0.60
2N3053	0.20	ASY29		OC25	0.85
2 N 3054	0.50		0.80	OC26	0.25
2N 3055	0.60	ASY54	0.25	OC29	0.60
2N3133	0.25	ASZ15	0.70	OC35	0.50
2N3134	0.25	ASZ16	0.70	OC36	0.45
2N3391	0.17	ASZ17	0.75	OC42	0.20
2N3392	0.17	ASZ18	0.75	OC44	0.15
2N3393	0.15	ASZ20	0.25	OC45	0.12
2N3394	0.15	ASZ21	0.40	OC70	0.10
2N3395	0.20	AUY10	1.00		
2N3402	0.15	BC107	0.10	OC71	0.12
		BC108	0.10	OC72	0.12
2N3403	0.15	BC109		OC73	0.30
2N3404	0.32		0.10	OC75	0.15
2N3414	0.20	BC113	0.10	OC76	0.15
2N3415	0.15	BC118	0.20	OC78	0.25
2N3417	0.25	BC134	0.20	OC78D	0.20
2N3702	0.10	BC147	0.10	OC81	0.20
2N3703	0.10	BC148	0.10	OC81D	0.20
2N 3704	0.12	BC149	0.12	OC83	0.20
2N3707	0.12	BC152	0.15		
2N3707		BC158	0.15	OC139	0.30
	0.10	BC175	0.20	OC140	0.85
2N3710	0.10			OC141	0.60
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