## PRAGTIGAL Wilitless FEBRUARY 1973 20p

3-RANGE GBYSTAL MARKER - 9 VOLT BATTERY ELIMINATOR



FANE 'MODE ONE' HIGH FIDELITY SPEAKER KIT


Incorporating a model $8038^{\prime \prime} 13,000$ Gauss Bass Speaker with ultra low resonance. P.V.C. surround cone. Printed circuit cross-over assembly with ferrite cored coils. Model 303 Pressure Tweeter, Acoustic damping material, Screws, Panels Tremendous $\mathbf{4 9 . 9 5}$ post etc., and Instructive diagrams, Frequency Value at $\leq 7.10$ free Response $25 \mathrm{~Hz}-2 \mathrm{KHz}$. Impedance 8-15. RSC 666 Mkill 6 +6 WATT high qualisy STEREO AMPLIFIER Individual Ganged Controls: Bass, Treble, Yolume and Balance. Printed circuit construction employing 10 Transistors plus Diodes. Output rating I.H.F.M. Frequency range $20-20,000 \mathrm{c}$. p.s. Bass Control $\pm 12 \mathrm{db}$. Treble Control $\pm 13 \mathrm{db}$. Selector switch for P.U. or Tape/Radio. For loudspeaker output impedances of 3 to 15 ohms. For standard 200-250v. A.C. mains operation. Attractive Black and Silver finished metal fascig plate and matching control knobs. FULIT WIRED PRINTED CIRCUIT AND COMPREHENSIVE WIRING DIAGRAMS \& INATRUCTIONS $4 \| .50$ CaIt. as illustrated $\mathbf{5 1 4 \cdot 9 9}$ or dop. $82 \cdot 20$ and 9 monthly payments $21 \cdot 70$ (Total $\mathbf{2 1 \%} 50$ ). AUDIOTRINE HI-FI SPEAKER SYSTEMS
Consisting of matched 12 in . 11,000 line 15 Watt 15 ohm high quality speaker, cross-over unit and tweeter. Smooth response and extended frequency range ensure surprisingly realistic reproduction. OR SENIOR 15 WATT INCLUDING HF126 15,000 LINE SPEAKER $\qquad$


## AUDIOTRINE HIGH FIDELITY SPEAKERS

Heavy congtruction. Latest high efficiency ceramic magnets. Plasticised Cone surround. "D" indicates Tweeter Cone providing extended frequency range up to 15,000
$8-15$ ohma. PLEASE STATE CHOICE.
 $\begin{array}{llllllll}\text { HF102D } & 10^{\circ} & 10 \mathrm{~W} & 28 \cdot 40 & \text { HF126 } & 12^{\circ} & 15 \mathrm{~W} & 55 \cdot 75 \\ \text { HF120 } & 12^{\prime} & 15 W & 84 \cdot 60 & \text { HF126D } & 12^{\prime} & 15 \mathrm{~W} & 56.25\end{array}$
FANE 807T HIGH FIDELITY SPEAKER A full range 8in. 10 -watt unit for excellent aound quality, in suitable enclosure. Cast chassis Roll P.V.C. cone surround and long throw voice coll to achieve very low fundamental resonance of 30 c.p.s. Tweeter 15 KHz , Gauss 10,000 . Jmpedance 3 or $8-15 \Omega$.
PLEARE STATE TMPFDANCE WHRN ORDERING 3.85 ODEFL 803
$£ 4.95$

## HIGH FIDELITY LOUDSPEAKER UNITS

Cabineta latest style Satin Tear veneer. Acoustically lined or filled
2countic damping. Ported where appropriate. Credit terma available. DORCHESTFR (Illustrated) Size $16 \times 11 \times 9 \mathrm{in}$. appr. Range $45-15,000$ c.p.s. Rating $8-10$ watts, Fitted High finx $13 \times 8$ in. $\mathbf{~} 9.45$ Dual Cone qpeaker. Imp, 3 or 15 ohmas. Rating 10 Fatts. Carr. 40 p. MONARCH 8 Sizo $19 \times 10 \times$ 9in. approx. Rating 10 watts. Inc. $13 \times 8$ in. speaker with highly fexible P.V.C. cone surround, long throw voice coil and 10,000 line magnet. 8 ohms, Gives smooth realistic sound output.
see 'package ofers' for illustration.
Carr. 50p
E19.35

Carr. 50 p

## HI-FI SPEAKER ENCLOSURES MODERN DESIGN

Teak veneer fnish. scousticaily lined. Bizes approx. Carr. 35 p . per enc. JE8 Size $16 \times 11 \times$ Yin. SE8 For optimum performPressurised. Gives pleasing ance with any 8in. results with any
8in. Hi-Fi speaker.

SE10 For outstanding results with $10 \mathrm{in} . \mathrm{Hi}-\mathrm{Fi}$
$\underset{\substack{\text { spkr. Size } \\ \times 10 \text { in. P'td. }}}{ } \times 15$ ⑥.74 Hi-Fi spkr. Size 22 £6. 47 $\times 15 \times 9$ in.
SE12 For excellent
performance with 12in.
Hi-Fi speaker and tweeter ${ }_{25}^{\text {Size }} \times$
$16 \times 10_{1} \mathrm{in}$.
$£ 7.87$

R.S.C. BATTERY/MAINS CONVERSION UNITS

TYPE BMI. An all-dry battery eliminator. Size $51 \times 4 \frac{1}{4} \times 2 \mathrm{in}$. approx. Completely replaces batteries supplying $1 \cdot 5 \mathrm{v}$ and 90 v .
to battery radio where A.C. mains $200 / 250 \mathrm{v}$. $50 \mathrm{c} / \mathrm{s}$ is avallabla COMPLETE KIT
WITH DIAGRAM 3.25 ASSEMBLED READY $\{3.75$
R.S.C. TA6 6 Watt HI-FI AMPLIFIER

200-950\%. AC mains operstod. Frequency Response $30-20,000$ c.p.s. Treble 'lift and cut' controls. 3 input sockets for Mike, Gram, Radio or Tape. Input selector switch. Output for 3-15 ohm spkrs. Max. sengitivity 5 mV Output rating I.H.F.M. Fully enclosed ensmelled case, $9 \frac{1}{2} \times 2 \frac{1}{2} \times 5 \frac{1}{2} \mathrm{in}$. Attractive brushed sitver finish lacis plate $10 \pm \times 3$ in. and matching knobs. Complete kit of parts with full wiring diegrams and instructions.


## NOW IN STOCK! FANE 'CRESCENDO’ GROUP/DISCO LOUDSPEAKERS

Send S.A.E. for leaflet on this range of extraordinarily efficient units including the very latest BASS CRESCENDO ' 12 '. 100 WATTS
FULL DISCOUNT to Genuine Trade Customers. CARR. FREE.
 MIDGET CLAMPED TYPE $2 \mathrm{~F} \times 25 \times 2 \% \mathrm{in}$. $260 \mathrm{v}, 60 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}, 2 \mathrm{a}$

FULLY BEROUDFD UPRIGET MOUNTT
250-0-250\% 60 DFD UPRIGHT MOUNTING $250-0-250 \mathrm{v}$. $60 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a} ., 0-5-6-3 \mathrm{v} .2 \mathrm{a}$. $81-40$ $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{z}, 0 \cdot 5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$. 82.20
 For Mullerd 510 Amplifier $\cdots \ldots \ldots . .$. $350-0 \cdot 350 \mathrm{v}$. $100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}$. $4 \mathrm{a} ., 05-6.3 \mathrm{v}$. 3 a . 2820 $350-0-350 \mathrm{v} .150 \mathrm{~mA}, \mathrm{~B}-3 \mathrm{v} .4 \mathrm{a} ., 10-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$. $£ 2-65$ $425-0-425 \mathrm{v} .200 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a}$, , c.t., 5 v .3 a . $425-0-425 v .200 \mathrm{~mA}, 6-3 \mathrm{v} .4 \mathrm{a} ., 63 \mathrm{v} .3 \mathrm{a}$., 5 v

## $50-0-450 \mathrm{v} .250 \mathrm{~mA}$, 6.3 v .4 a ., c.t., 5 v . 3a. $85-50$

R.S.C. MkIII SUPER 30 HIGH FIDELITY STEREO AMPLIFIER

## BUILD AN AMPLIFIER WORTH APPROXIMATELY

DOUBLE THE KIT PRICE INCLUDING CABINET
Only high grade components by leading manufacturers

* Push Button Selector Switching
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* Satin Silver Finish Metal Fascia
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Send S.A.E. for full descriptive leaflet.
R.S.C. STEREO FM TUNER. Visually matches Super 30 Mk . III a

TOP SHROUDED DROP-THRO' TYPE
 $250.0 \cdot 250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .3 .5 \mathrm{a} .7 \ldots . \mathrm{c}$
$250.0 .250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a} .6 .3 \mathrm{v}$. $350-0.350 \mathrm{v}$.
80 mA,
$6.3 \mathrm{v} .2 \mathrm{a} ., 1$
0.556 .3 v

 $300-0.300 \mathrm{v} .130 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}$., 0 o.t. $8-3 \mathrm{vv} .1 \mathrm{a}$. Suitable for Mullard 610 Amplifer $350-0-350 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}$, $10-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$. ${ }_{52} 2.2$ $350-0-350 \mathrm{v}$. $150 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a} ., 0-5.6 .3 \mathrm{v} .3 \mathrm{a}$. 22.60
FLLAMENT OF TRANSISTOR POWER PACK


 ADTO (Step UP/step DOWN) TRANSFORMERS
$0-110 / 120 \mathrm{v}$. $200-230-250 \mathrm{~F}$. $50-80$ watts \&1.10
 OUTPUT TRANSFORMERS
OUTPUT TRANSFORMERS
昭 $15 \Omega . . \quad$ or 15 Pull 10 watts 6V6, ECL86 to $3,5,8$ or

Push-Pull Ultra Linear for Mullard 510, etc.
Push.Pull 15-18 watts, sectionally wound 616, KT66, etc., for 3 or $15 \Omega$. Push-Pull 20 watt high quality gectionally
found EL $34,6 L 6, \mathrm{KT} 66$ etc. to 3 or 15

SELENTUM RECIIFIERS F. W. (Bridged) All 6/12v. D.C, output. Max. A.C. anput $25 \mathrm{p} .2 \mathrm{v}, 35 \mathrm{p}$ $1 \mathrm{a}, 25 \mathrm{p} .2 \mathrm{a}, 35 \mathrm{p}$.
$3 \mathrm{a}, 50 \mathrm{p} .4 \mathrm{a}, 65 \mathrm{p}$.
 SMOOTEINC OHGKES $50 \mathrm{~mA}, 7-10 \mathrm{H}, 250$ $\Omega$ 70p; 100 mA , $10 \mathrm{H}, 200, \Omega 60 \mathrm{p} ;$ $50 \mathrm{p} ; 60 \mathrm{~mA}, 10 \mathrm{H}$, $400 \Omega 25 \mathrm{p}$.

## 'YORK' HIGH-FIDELITY 3 SPEAKER SYSTEM

 $\star$ Moderate size only $25 \times 14 \times 10 \mathrm{in}$. approx. $30-20,000$ c.p.s. COMPLETE KIT$\star$ Response 30-20,000 c.p.s. Impedance 15 ohms
$\star$ Performance comparable with units costing co:siderably more

Carr. 65p Consists of (1) 12 in . 15 watt Bass unit with cast chassis, Roll rubber cone surround for ultra low resonance, and ceramic magnet. (2) 3-way quarter section series cross-over system: (3) $8 \times 5$ in. high flux middle range speaker. (4) High efficiency tweeter. (5) Appropriate quantity acoustic damping material. (6) Handsome Teak veneered cabinet. (7) Circuit and full instructions. Terms: Dep. $£ 4 \cdot 60$ and 9 monthly payments $£ 2.47$ (Total $£ 26.83$ ).

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 MICROPHONE
R.S.C. COLUMN SPEAKERS IDEAL FR VOCALISTS All types 15 Ohms covered in Rexine and Vynair AND PUBLIC ADDRESS TYPE C4100 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN TYPE C3I2 30-40 WATTS Fitted two TYPE C4I2S 50 WATTS exceptionally efficient, low feedback howl char- Fitted four $15^{\prime \prime} 11,000$ line 15 watt acteristic high flux $13^{*} \times 8^{\prime \prime} 20$ watt $\boldsymbol{1} \mathbf{1 9 . 9 5}$
 TYPE C4I00 100 WATTS inc. four 12" 50 watt speakers for conserva-


465

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## 4 H \% \%

 R.S.C. AID 30 WATT ULTRA LINEAR HIFF AMPLIFIER Highly sensitive. Push-Pull high $+3 \mathrm{AB} 30-20,000 \mathrm{c} / \mathrm{s}$. All high grade components. Valves EFS6 Controls. Sensitivity 36 millivolts. For High Impedance micro phones. For Clubs, Schools, Theatres, Dance Halls, Outdoor FundRadio or Tape. Two separate inputs with vol, controls permit such as "mike" andPick-up etc. for mixing purposes, $200-250 \mathrm{v}$. 50 chs i. C mains. For 3 and 15 ohm sperms: Dens and
LINEAR T40/60D 50W GROUP/DISCO AMPLIFIER

* FULL MONITORING FACILITIES
* Twin jack output sockets for speaker
$\star$ Input sockets for medium or high impedance
Microphones or Guitar PUs and Crystal o
Ceramic Gram. PUs
末 Frequency response $30 \cdot 20,000 \mathrm{~Hz}$
* Output overload protection plus double fusing FRONT PANEL (Jack inputs)
Gram, Gram, Microphone/Guitar P.U; plus monitoring CONTR Master Vol Vol. (1) (2) (3) and (4). Bass, Treble, Master Vol., Monitor Selection Switch Gram (1) or (2), Mains Switch

PAL PHASE 50 Mk. III AMPLIFIER 50 WATT. Solid state. 4 Separately controlled inputs Plus master vol. control, Tad. Bass and Treble Controls. Protective circuit to
guard against damage from accidental shorts. Output for guard against damage from accidental shorts. Output for Speaker/s 3 to 30 ohms. Size 1
mains. Ont put 50 waits music mains. Output 50 wats music rating.
Or deposit $£ 7.25 \& 9$ monthly payOr deposit $25 \cdot 25$. 9 mon

RSC PHANTOM '50' Combined SOw Amplifier and 12in. Loudspeaker. For Bass instruments). Inc. 3 inputs and 2 vol. controls plus Treble Bass and Presence. Output Jack for additional 150 hm Speaker. Attractively finished ins and Presence. Out fascia and trimmings. Compact size. Fitted carrying handle. Available early February

PACKAGE OFFER
(a) 100w POWER AMPLIFIER
(b) PAIR OF HIFH HEAD. PHONES
(c) MATCHING DYNAMIC 'MIKE' (attached to headphones)
(d) PAIR 50 VAT SPEAKERS Black Rexine covered Cabinets fr? $18^{\prime \prime}<18^{\prime \prime}$ : $8^{\prime \prime}$ LG DO (a)(b)(c)\&(d) Carr. $£ 1 \cdot 25$ Terms on Amps. Speakers and Head monthly payments of $£ 4.00$ (Total monthly
$\mathbf{8 7} \cdot 00$ ).

Incorporating twin Gerard SP25 Mk. III turntables and Sonotone or Aces Cartridges with diamond stylii. Separate Fo., controls for each turntable. Also MONITORING FACILITIES, plus Treble and Bass Controls. Separate input for 'mike'
with vol. control switch. Black exine covered Cabinet with lid. see illus. on left Or $\operatorname{Dec}$ Carr. £1.25 Or Dep. 813 - 25 and mothy payments $93 \cdot 62$. 18

## FANE ULTRAHIGH POWER LOUDSPEAKERS



FANE SPEAKERS 'POP' 25/2 12 in 25 WATT Dual Cone $15 \Omega$ (for uses $\cap$ Raf 7 or Dep. 81.25 and 9 other than Bass Guitar or Electronic Organ). Carr. free (Total parma

## GROUPPIISCO EOUPMENT

F.A.L. PHASE 50 MK.III AMPLIFIER PR. FANE POP $25 / 225 W$ L/SPEAKERS Terms: Deposit $£ 6.50$ and o monthly payments of $£ 4.92$ (Total $£ 50.78$ ) F.A.L. PHASE 50 MK.III AMPLIFIER TR. FANE POP 50 L/SPEAKERS Terms: Deposit 810 and 9 monthly
payments of $£ 5.37$ (Total $£ 58.33$ ) P.A.L. PHASE 50 MK.III AMPLIFIER PAIR Li2/25 25 W L/S in cabinets Terms: Deposit flo and 9 monthly payments of 55.88 (Total $262 \cdot 92$ ) LINEAR T40:60D AMPLIFIER Parr L12/20 L/S in cabinets Terms: Deposit f9.95 and 9 monthly payments of 87.67 (Total 278.98) F.A.L. PHASE 100 AMPLIFIER 4 FANE POP 50 L/SPEAKERS


PACKAGE OFFERS £34.95 PACKACE PRICE $\underset{213.50}{25}$ \& PACKAGE PRICE £52 ${ }^{\text {and }}$

PACKAGE PRICE $\left\{56{ }^{\text {ararriz }}\right.$

PACKAGE PRICE £69.95 PACKAGE PRICE $499.955_{a z}^{\text {car }}$
£55.95 and 9 monthly pymts, $\approx 6$ (Total £62-95

RS BASS-REGENT 50 WATT AMPLIFIER
A powerful high quality all-purpose unit for lead, rhythm, bass guitar, vocalists, gram, radio, tape. Peak Output rating Loudspeaker unit
vertical mounting.
$\star$ Two extra heavy duty 12in. 50 w - Four Jack in Controls fork inputs and two Volume pick-ups or "mikes". Bass and Treble controls.
Credit Terms: Deposit 815 \& 9
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## RSC GP 30 HI-FI AMPLIFIER



For Guitar, Vocal or Instrumental Group A 4 input. 2 vol. control Hi-Fi 30 watt unit with Separate Bass and Treble controls, Current valves. Peak output rating.
Strong Rexine covered cabinet with handles. Attractive black/gold P.V.C. fascia. Neon indicator
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50.45 52.45 (Total $£ 26-45$ ).




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rejection and noise ratio.
 months Guarantee
 MULTIBAND-6

SOLID STATE SHORT WAVE RECEIVER KIT

All transistor T.R.F. Receiver tunes 550 KHz to 30 MHz ( 540 to 10 metres) complete coverage-no gaps. Medium waves-Trawlers-Ship/Shore Telephone-All Six Amateur Bands 160-10 metres-International Broadcast from Australia, Far East, Russia, USA etc. using 4 miniature plug in Coils. Hi-Gain FET Regen. Det./AF/AF Module giving full loudspeaker output to any external $2 / 3$ ohm speaker. Receives AM/CW/SSB.
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It tunes from 540 metres medium through to 10 metres with no gaps Covers shipping, coastguard and distress frequencies, all six amateur bands $160-10$ metres, International broadcast, Met. stations etc. etc. giving world-wide reception. Exclusive features include Air-spaced CODAR-COIL Hi-"Q" Aerial input, illuminated Meter and Slide Rule Scale, Two Speed vernier tuning, Switched B.F.O. for CW/SSB signals. Separate output for Tape recorder.
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Complete ready built $£ 27 \cdot 50$, Carriage 70 p.

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READY BUILT UNIT

## GUARANTEED 5 YEARS

Patents pending.
12 volt only-state pos or Pe \& Capacitive discharge ignition is recognised as being the most efficient system and will give you:

* Continual Peak-Tuned Performance
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Kit includes absolutely everything for assembly: Case, Cables, Coil Connectors, Silicon Grease, etc. 8 page illustrated instructions cover fitting of all Types of Tachometers. Call in for a Workshop Demonstration. S.A.E.

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Complete with baseplate and screws

At direct from manufacturer prices with return of post

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ype No
$7^{*}$
$6^{*}$
$\hat{3}^{*}$
$10^{*}$
11
12
13
14
15
18
*THESE SIZES ACCEPT STANDARD VEROBOARD RANGE

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SAME DAY SERVICE NEW! TESTED! GUARANTEED!

SETS $\begin{aligned} & \text { 1R5, 1S5, 1T4, 3S4, 3V4, DAF91, DF91, DK91, DL92, DL94. } \\ & \text { Get of } 4 \text { for £1.12. DAF96, DF96, DK96, DL96, } 4 \text { for \&1.55. }\end{aligned}$

| 1R5 | -28 | 30 Cl 5 | -58 | SABC80 | . 32 | EL500 | -62 | PCF808 | -68 | U801 | 75 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 155 | $\cdot 22$ | $30 \mathrm{C17}$ | . 78 | EAF42 | . 50 | EM80 | . 86 | PCL82 | - 30 | UABC80 | . 31 |
| 1T4 | $\cdot 18$ | $30 \mathrm{C1} 18$ | -58 | EB91 | -10 | EM81 | -36 | PCL83 | -55 | UAF42 | 50 |
| 354 | $\cdot 26$ | $30 \mathrm{F5}$ | -64 | EBC33 | . 40 | EM84 | - 82 | PCL84 | . 33 | UBC41 | 45 |
| 3V4 | . 47 | 30 FL 1 | -65 | EBC41 | $\cdot 49$ | EM87 | . 50 | PCL85 | - 88 | UBF80 | . 85 |
| 5 U 4 G | . 31 | 30 FL 12 | -68 | EBC81 | $\cdot 30$ | EY51 | - 36 | PCL86 | . 37 | UBF89 | -82 |
| $5 \mathrm{5V} 4 \mathrm{G}$ | $\cdot 35$ | 30 FL 14 | -68 | EBC90 | -22 | EY86 | -29 | PCL88 | . 68 | UCC84 | - 32 |
| 6Y3GT | . 30 | 30L1 | . 29 | EBF80 | -32 | EY87 | . 29 | PCLS00 | . 89 | UCC85 | -85 |
| 5Z4G | . 35 | 30L15 | $\cdot 70$ | EBF83 | . 39 | EZ40 | -38 | PCL805 | -38 | UCF80 | . 80 |
| 6/30L2 | - 54 | 30 L 17 | -67 | EBF89 | -29 | EZ41 | - 39 | PENA4 | . 77 | UCE42 | - 58 |
| 6AL5 | -11 | 30 P 4 | $\cdot 65$ | ECC81 | $\cdot 17$ | Ez80 | . 21 | PEN36C | -70 | UCH81 | . 80 |
| 6AM6 | $\cdot 13$ | 30 P 12 | -69 | ECC82 | . 20 | EZ81 | . 22 | PFL200 | . 51 | UCL82 | -38 |
| 6AQ5 | -22 | 30719 | -65 | ECC83 | . 35 | Ez90 | -25 | PL36 | $\cdot 48$ | UCL83 | . 68 |
| 6AT6 | . 20 | 30PL1 | -60 | ECC85 | - 34 | GZ30 | $\cdot 84$ | PL81 | -43 | UF41 | - 62 |
| 6AUG | -20 | 30 PL 13 | . 89 | ECC804 | - 54 | GZ32 | . 40 | PL81A | $\cdot 47$ | UF89 | -80 |
| 6BA6 | $\cdot 20$ | 30 PLL 4 | .80 | ECF80 | . 30 | KT41 | $\cdot 77$ | PL82 | . 31 | UL41 | . 58 |
| 6BE6 | . 21 | 35L6GT | . 45 | ECF82 | -28 | KT61 | - 55 | PL83 | -33 | UL84 | - 80 |
| 6BJ6 | $\cdot 41$ | 35W4 | . 25 | ECH35 | . 55 | KT66 | . 78 | PL84 | - 30 | UM84 | -28 |
| 6BW7 | - 50 | $35 \mathrm{Z4GT}$ | . 25 | ECH42 | . 59 | LN319 | -63 | PL600 | . 63 | UY41 | -89 |
| 6 F 14 | . 35 | 50CD6G | -68 | ECH81 | . 29 | LN329 | . 72 | PL504 | . 68 | UY85 | -25 |
| 6F23 | -68 | 807 | . 49 | ECH83 | $\cdot 38$ | LN339 | . 65 | PM84 | -80 | VP4B | $\cdot 77$ |
| 6F25 | . 53 | AC/VP2 | $\cdot 77$ | ECH84 | .35 | N78 | $\cdot 87$ | PX25 | . 95 | W77 | -48 |
| 6J7G | $\cdot 24$ | B349 | $\cdot 70$ | ECLS0 | -30 | P61 | - 40 | PY32 | - 62 | 277 | -22 |
| 6K7G | . 12 | B729 | -54 | ECL82 | -29 | PABC80 | - 31 | PY33 | - 52 | Trandi |  |
| 6 K 8 G | -36 | CCH35 | . 67 | ECL86 | . 35 | PC86 | . 47 | PY81 | .25 | AC107 | $\cdot 17$ |
| 697G | -35 | CY31 | $\cdot 28$ | EF39 | . 38 | ${ }^{\mathrm{P} C 88}$ | . 47 | PY82 | -25 | AC127 | -18 |
| 6SL7GT | -30 | DAF91 | -22 | EF41 | - 57 | PC96 | - 42 | PY83 | $\cdot 26$ | AD140 | -37 |
| 68N7GT | . 30 | DAF96 | . 36 | EF80 | . 23 | PC97 | -36 | PY88 | -33 | AF116 | -20 |
| 6V6G | -28 | DF91 | . 16 | EF85 | -28 | PC900 | . 29 | PY800 | -31 | AF116 | -20 |
| 6V6GT | -28 | DF96 | . 36 | EF86 | .30 | PCC84 | . 29 | PY801 | . 31 | AF117 | -20 |
| 6X4 | . 23 | DH77 | . 20 | EF89 | -26 | PCC85 | . 23 | R19 | - 30 | AF125 | -17 |
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$14+14$ watts r．m．s． 40 Hz to $\mathbf{4 0 k H z} \pm 3 \mathrm{bB}$ ．Total distortion at 10 watts at $\mathbf{1 k H z}$ － $0.1 \%$
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This compact and reliable unit operates from amptifiers with outputs from 5-100 watts. Does not impose a heavy load on the amplifier, or, if connected in the wrong polarity, cause any damage, as with some units.
Operation is simplicity itself and the unit is fully fused. The unit is supplied to function from bass notes but may easily be addition of components costing less than $\mathbf{5 p}$.

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Handing the total of 3000 watt ( 3 kw ) this unit is unique for its price in that not onily bass, middle and treble but also master controls are provided. Two amplifier sockets eliminate the need for split leads, etc. Supplied In lough white steel case with a blue stelvetite hooded cover. Fully guaranteed.
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MONO VERSION $£ 6 \cdot 50$ carr. 20 p (As iltustrated left S.A.E. details 9 volt operation) Outputs up to I volt RMS

£15-80
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## SAXON STEREO

 CONTROL UNITTwo decks, and full headphone monitoring. The unit is mains operated and measures $17 \frac{1^{\prime \prime}}{} \times 3^{\prime \prime} \times 4^{\prime \prime}$ deep and is finished with a smart white on black facia. The controls are: Left/Right deck fader, volume, bass, and is finished with a smart white on black facia. The controls are: Left/Right deck fader, volume, bass,
trebie, Headphone Selector and volume, Microphone volume, bass, treble, mains onfoff. THHIS IS A MUST FOR THE HOME QUILT HIGH OUALITY GISCOTHEQUE AND IS COM PARAELE TO UNITS AT OVER TWICETHEPRICE. (N.B.-Stereo only has mic Input.)

## COMPLETE AMPLIFIERS

The CSE 100. £34.90 carr. free
This versatile unit is now avallable in a black vynide case and so represents even better value than ever delivering speech and music powers of up to 100
 watts RMS and continuous signal outputs of 70 watts. Two Individually controlled inputs with wide range bass and treble controls. Ideal for small groups D.J.S., ete

The SAXON $100 £ 48 \cdot 50$ carr. free


With an RMS output of 120 watis speech and music, 100 watts continuous power, four individually controlled FET Input stages and wide range bass and treble controls, this amplifler has established itself as a unit offering quality and reliability at low cost.

LOUDSPEAKERS British made bargainsII
$12^{\prime \prime} 25$ watt $8 / 15$ ohms $£ 5 \cdot 95$ carr. 30 p. $15^{\prime \prime} 50 \mathrm{~W} .8 / 15$ ohm $£ 44 \cdot 50$ carr. 50 p.
$12^{4} 40$ watt 15,000 gauss magnet system $8 / 15$ ohm $\mathfrak{E} 11 \cdot 50$ carr. 40 p
A.K.G. MICROPHONES suitable for disco, group or general P.A. use D11DHL rrp £11-00 our price £9.45 post free
D190C High Z ro $£ 21 \cdot 50$ our price $£ 17.45$ post free
D1000C 24 ct gold plate rrp $£ 37 \cdot 00$ our price $£ 32 \cdot 00$ post free
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TRADE \& EXPORT enquiries invlted.

## (IP) IL.P. (Estationes be

## THE HY41



The HY41 supersedes the popular HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically $0.05 \%$ at 1 KHz into 8 ohms! , and is electronically and mechanically compatible with the HY40.

With this important improvement the HY41 retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi-Fi but also for public address systems and industry

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier.

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent vears.
OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts R.MI.S. continuous.

LOAD IMPEDANCE: 4-16 ohms.
INPUT IMPEDANCE: 30 K ohms at 1 KHz
VOLTAGE GAIN: 30 db at 1 KHz
TOTAL HARMONIC DISTORTION: less than $0.15 \%$ (typical 0.05\%)
at 1 KHz .
FREQUENCY RESPONSE: $5 \mathrm{~Hz}-50 \mathrm{KHz}+1 \mathrm{db}$.
SUPPLY VOLTAGE: +22.5 volts D.C.
SUPPLY CURRENT: 0.8 amps maximum.

PKICE: inc. comprehensive manual, P.C. board, five extra components and P. \& P.:-
MONO: $£ 4.90$
STEREO: $\mathfrak{f} 9.80$

## UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an integrated pre-amplifier circuit.

Supplied with the HY5 are two stabilizing capacitors and by the addition of volume, treble and bass potentiometers it is ready for use.

Internally the HY5 provides equalization for almost every conceivable input, the desired function is achieved by use of a multi-way switch or by direct interconnection, Two distinctive features of the HY5 are its inbuilt stabilization circuit, allowing it to be run off any unregulated power supply from $\mathbf{1 6 - 2 5}$ Volts and a balance circuit which, when linked by a balance control to a second HY5, forms a complete stereo pre-amplifier.

Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely intergrated system.

## INPUTS

Magnetic Pick-up (within $\pm 1 \mathrm{db}$ RIAA curve) $2 \mathrm{mV} .47 \mathrm{~K} \Omega$
Tape Replay lexternal components to suit headi). $4 \mathrm{mV} .47 \mathrm{~K} \Omega$
Microphone (flat) $10 \mathrm{mV} .47 \mathrm{~K} \Omega$
Ceramic Pick-up lequalized and compensatable) $20-2000 \mathrm{mV}$. variable.
Tuner (flat) 250 mV . $100 \mathrm{~K} \Omega$
Auxiliary $1250 \mathrm{mV} .47 \mathrm{~K} \Omega$
Auxiliary $22-20 \mathrm{mV}$. $100 \mathrm{~K} \Omega$

## OUTPUTS

Main Pre-amp output 500 mV .
Direct tape output 120 mV .
ACTIVE TONE CONTROLS (Bexendall)
Treble $\pm 12 \mathrm{db}$.
Bass +12 db .
INTER̄NAL STABILIZATION
Enables the HY5 to share an unregulated
supply with the Power Amplifier.
SUPPLY VOLTAGE
16-25 volts
PRICE: MONO: $£ 3.60$ STÉREO: $£ 7.20$


SUPPLY CURRENT
6 mA approx.
OVERLOAD CAPABILITY
better than 26 db on most sensitive input infinite on tuner and auxl.
OUTPUT NOISE VOLTAGE: 0.5 mV .

## POWER SUPPLY PSU45

The versatile P.S.U. 45 is designed to supply your HY41's + HY5's in stereo or mono format.

## Specification

Input: 200-240 Volts.
Output: $\pm 22.5$ Volts at 2 amps .
Overall Dimensions: L. $7^{\prime \prime}$; D. $3.8^{\prime \prime}$; H. 3.1"
PRICE: $\mathbf{E 4 . 5 0}$ inc. P. \& P.

## Letter from your new Editor

$\mathrm{A}^{\top}$$T$ the time of going to press we have seen the last of the Apollo series of manned space flights to the moon. Fifteen years ago when the USSR launched Sputnik 1, followed by the U.S. launching of Explorer 1, little did many people imagine what space research could do to provide further knowledge and skills for everyday living. One could comment in depth on this, but rather than indulging yet again in retrospect, let us look to the future.

NASA space programmes are to be directed towards space laboratories in which man can examine the influences of near sterile conditions on terrestrial activities. Already it is expected that crystal growth in a space laboratory will be tried, so perhaps we who have a particular interest in semiconductor technology will again reap the benefits of such an exercise.

On a more domestic note, following the celebrations of 50 years broadcasting, further progress is being made to improve communications: The IBA have now used their colour programmes digital converter in service; stereo is established on Radio 2 (v.h.f.), although there is apparently some unexplained mono material intruding; the planning of commercial radio is well underway; the third Goonhilly dish has increased the international telephone capacity to handling almost half of Britain's 60 million calls by satellite; the first UK i.c. radio chip receiver design for home constructors has been published; the BBC has announced the CEEFAX news service for television.

We shall be taking a closer look at the world of communications inside and outside the home; giving you up-to-date information on components and equipment; extending our popular ranges of simple-to-build projects; encouraging readers to participate with us in do-it-yourself communications.

Many of you will have followed the writings of your new editor elsewhere. To PW newcomers we welcome you to the club; we hope to provide plenty to stimulate your interest in future issues. In the meantime, we are always interested to hear your views on matters appropriate to the magazine. We are also convinced that a great deal of talent exists among the readership in designing projects, as is evident from our correspondence. If you feel that you would like to show others what you do, drop us a line; better still, how about writing it up into an article.

> M. A. COLWELL-Editor.

## THE MARCH ISSUE WILL BE PUBLISHED ON FEBRUARY 2nd

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[^1]

## KW catalogue

A new catalogue has just been released by KW Electronics Ltd., Specifications and pictures of KW transmitters, receivers and asso ciated equipment are shown and a price-list is included.

Free copies of this catalogue may be obtained by writing to KW Electronics Limited, Dartford, Kent.

## Ignition system



Future Techmatics announce a new low-cost capacitive discharge ignition system, named "Highwayman" and designed for both the fleet owner and the private motorist. The unit priced at $£ 9 \cdot 90$ plus 35 p postage is claimed to give fuel economy, improved performance and excellent starting under adverse conditions.
Fitting is simple with only three wires to connect. Using the conventional coil and contact breakers, "Highwayman" produces well over 30,000 volts to the spark plugs with a rise time of $2 \cdot 6$ microseconds. Maximum operating rate is 600 pps. Battery drain is 1.5 amps . The contact breaker resistance limit is 25 ohms and current and voltage at contact breakers is 0.15 amps at 12 V .

Further information on the range of electronic ignition systems and other devices, may be obtained from Future Techmatics Limited, Waldeck House, Waldeck Road, Maidenhead, Berks.

## Solder feed

The Mark 3 Anextra includes several improvements to simplify its main function of eliminating the need for "three hands" when soldering. The reel of solder, 18 to 22 gauge is contained in the pistol grip which is easily attached to most types of soldering iron.

The maximum 4oz. reel of solder is easily changed. The amount of solder fed by each pressing of the trigger is quickly adjusted to suit the joints being made. The operator thus holds

## Working /MDS

Who ever heard of a radio Amateur going mobile on a dogsled?

I didn't believe it at first but here's the full story:
Having supplied quantities of radio equipment to the South African Antarctic Expedition, Racal Electronics is naturally in fairly close touch with events and told us of the claim by one of the Expedition's members to have effected the world's first radio contact (QSO) by an amateur from a dog-sled mobile installation. The QSO was achieved on 7 MHz between the sled in Antarctica and a station in South Africa. Racal has supplied the Expedition with a number of TR. 28 h.f. transceivers which it uses for mobile applications.

The Expedition's base station (call sign ZSIANT) which is equipped with Racal transmitter and receiver, is in the charge of Frank Schneider, a radio ham who operates most evenings between 1600 and 1900 GMT on s.s.b. at about 14.30 MHz (call sign ZS6GE), As Antarctica is classed as a separate continent for many amateur radio certificate awards, a contact with Frank is considered a rare achievement and so his QSL cards confirming radio contact are in great demand among the world's radio amateurs.

If any U.K. hams manage to contact ZSIANT, the address for QSL cards is 5 Prinshof Street, Pretoria, South Africa, or via the SAARL QSL Bureau.

both the iron and solder in one hand, being free to hold the work with the other hand.

Supplied with a loz. reel of $60 / 4022$ s.w.g. solder, with simple instructions, the Anextra is $£ 3 \cdot 75$ post free U.K., direct from the makers. If you send an s.a.e. you can obtain a leaflet on the unit. Anextra Lid., Chiltern Works, Rear of 77/78 Chiltern View Road, Uxbridge, Middx.

## New Mechanics



The range of "LH" (low, noise high output) ferric oxide compact cassettes from BASF is available with the patented Special Mechanics (SM) developed by BASF technicians in West Germany.

The Mechanics comprise two plastic tusks and a roller system which together guide the tape on and off the spools. They ensure constant free running of the tape and eliminate jerking caused by static.

The improvement in tape running is most noticeable with Cl20 cassettes which, because of their extreme tape length of over 56 feet and thinness, are prone to running difficulties.

Recommended retail prices, including purchase tax, of the LH SM cassettes are 81 p (C60), £1•11 (C90) and $£ 1.51$ (Cl20). BASF United Kingdom Limited, P.O. Box 473 Knightsbridge House, 197 Knightsbridge House, London, S.W. 7 1SA.

# Ronson Blowtorch 



Ronson Products Ltd., the people that make the lighters and shavers recently let me have a look at their blowtorch.

It's hardly the sort of unit you would use on a transistor p.c. board or anything requiring delicate soldering but for heavy soldering jobs, it's ideal.

With its micro-adjustment to give a precision choice of flame size and heat intensity, the Blowtorch when used with its copper soldering tip can undertake relatively fine soldering jobs on metal, wire splices, pipes and tubing, etc. It's ideal, too, for bending or fashioning glass, metal tubing and rod and for all types of hand forging, shrink fitting, enamelling or light brazing.

The range of Ronson Blowtorches is made up of three models. All are supplied complete with the large capacity Hi-Heat butane refill. The standard pack costs just $£ 2.45$ or with copper soldering tip at $£ 2 \cdot 79$. The complete Blowtorch kit-at $£ 3$.99comes with three handy attachments (soldering tip, flame spreader and diffuser head) all neatly contained in a packaway case, as can be seen in the photograph. Ronson Products Ltd., Leatherhead, Surrey.

## "Texan" Reprints

Reprints of the "Texan" $20+20 \mathrm{~W}$ Stereo Amplifier are available.
They may be obtained by sending 35 p ( $30 \mathrm{p}+5 \mathrm{p}$ postage/packing) to "TEXAN" REPRINT, c/o Chief Cashier, Practical Wireless, Tower House, Southampton Street, London WC2E 9QX.

## Electrovalue cat.

Electrovalue have sent me their catalogue No. 6-already in its third printing. Including i.c. circuit and connection diagrams as well as semiconductor outlines and technical gen, the catalogue contains many other interesting items plus a purchase refund voucher for the 25 p it costs to buy.

Copies can be obtained from Electrovalue Limited, 28 St. Judes Road, Engiefield Green, Egham, Surrey.

## Bib test cassette

Bib recently let me hear their HiFi Stereo Test Cassette which is entitled, "How to get the best stereo and mono reproduction and recording".
The tape, devised by Richard Arbib, managing Director of Bib Sales is recorded by Decca using the Dolby system.
The Max Harris Jazz Trio play some specially composed pieces, illustrating tests including balance control, channel identification speaker phasing, reducing tape hiss and adjusting record volume controls.
Members of the Trio, playing six instruments are used to check cassette recorder reproduction over a wide frequency range.

Side 1 of the cassette deals with reproduction and side 2 with recording. Other advice and tests include wow and flutter, movement between channels and how to clean tape heads.

To illustrate various points, excerpts from Bach's Toccata and Fugue in D minor and Khachaturian's Spartacus are given together with excerpts from Vivaldi's "The Four Seasons" and some Gilbert and Sullivan operas to illustrate high quality sound.

This cassette represents a very useful addition to those who like me suffer from "cassette-itus" and a none too perfect stereo system.

The Bib reference for the cassette is " 53 " and the price $£ 2 \cdot 25$. The tape plays for 50 minutes, which represents an extra $25 \%$ of playing composed with a standard Musicassette. Bib Division, Multicore Solders Ltd., Hemel Hempstead, Herts.

## Litesold's latest

Light Soldering Developments inform us that they have marketed two new devices. Both are for use with their ETC/1 tem-perature-controlled and Conquerer irons.' The De-Soldering Unit (priced at $£ \cdot 75$ ) slips onto the iron and converts it to a selfcontained de-soldering tool.

The i.c. De-Soldering Head, at $£ 2 \cdot 25$, slips on in place of the soldering bit to give simultaneous de-soldering of all leads of 14 and 16 way dual-in-line i.c.'s. Light Soldering Developments Ltd., 28 Sydenham Road, Croydon, CR9 2LL.


De-soldering unit

## Digital Clock

The 24 hour digital clock shown on the cover this month is mains driven and incorporates an alarm buzzer. It can be obtained from Sternway Electrical Ltd., 111 Fleet Street, London EC4, for $£ 7.95$ plus 25 p post and packing.

## The "CQ" Column

Just a little reminder about the CQ Column. As readers write in, I put all their letters in strict order so that it is a case of "first come, first served." Requests for entries in this column now number many dozens a week and as we cannot always include a "CQ Column" in every issue of P.W. there is often some delay before the items appear.

Should there be any immediate urgency for a mention to appear, our Advertising Department will be pleased to accept "small ads" for a small charge.

# Guide for Constructors 

## V.CAPEL

EACH issue of both Practical Wireless and Television carries articles of a constructional nature. With any hobby or interest, the greatest pleasure and reward comes from participation, having a go oneself rather than just reading about or examining the work of others. Thus these constructional features fill a very necessary need and are widely appreciated.

However, modern radio and television techniques are of a complex nature, and it is understandable, that in spite of the clear description, circuit and layout diagrams, readers sometimes get into difficulties, resulting in a written plea for help to the Editor, who in many cases refers it back to the writer of the original article. Many of these difficulties and queries though, would not arise if certain basic principles and precautions were observed. This article is designed to assist constructors prevent problems before they arise.

## COMPONENTS

First we will consider the components. It is always best to obtain all the components at the start, if at all possible. If any are left out, to be obtained later, it means that the tags or print where they would be connected are left unsoldered and therefore adjoining components are left high and dry. If the omitted component is used as an anchoring point such as a transformer or can electrolytic, then it will not be possible to fit the associated components at all. Where a number of parts are deferred in a complex circuit it is very likely that one or more may be overlooked altogether, and considerable trouble caused in trying to get the circuit to work before the omission is discovered.

Having gathered the components together it is wise to check them for faults. Unfortunately, there is always a percentage of new parts that are defective, as each one cannot be individually checked by the maker. Small though the percentage may be, it means that somebody is going to get one, and that could be you!
Transformer windings should be checked for continuity, and then with the ohmeter switched to its highest range, check for leaks between windings, and between windings and core.

Capacitors are the most likely source of faults especially the miniature electrolytics used in transistor circuits. These should be checked for leaks; some leakage may be found using the high resistance range of the meter, but it should not be very much. If in doubt compare with other electrolytics. Any giving a substantially lower reading than the others should not be used. Of course, a lower reading will be obtained with the meter polarity connected the wrong way round; usually, the polarity on the ohms ranges is opposite to that for the voltage and current ranges.

While leaky capacitors are more common than open-circuit ones, the latter condition can be tested for by observing the meter needle kick when the capacitor is connected across it. The larger the value of the capacity the greater the kick, so with low values a response may not be observed. It will not be necessary to check the values on a bridge; if it is not leaky or o/c, the value will probably be right.

Assuming the colour code markings are clear it is very rare for a resistor to be of incorrect value or o/c so these can be taken for granted, especially if there is a large number and checking them all would be rather tedious. However, circuits where close tolerances are necessary such as measuring and test equipment, may demand the individual checking of appropriate resistor values. Also very high values are worth checking as these are generally less reliable than the lower ones. Resistors with dubious markings should be checked.

## TOLERANCES

Sometimes queries are received about tolerances and capacitor voltage ratings showing that these limitations are not always understood.

The tolerance means the amount by which the value may deviate from that stated. Thus a $100 \Omega$ $10 \%$ resistor may be anything from 90 to $110 \Omega$ in value. Resistors may be obtained in $1 \% ; 2 \% ; 5 \%$; $10 \%$ and $20 \%$ tolerances, the $5 \%$ ones being indicated by a gold ring and the $10 \%$ ones by a silver one. In most practical circuits values of resistance are worked out and then taken to the nearest preferred value, so in most cases the values are not very critical. Unless otherwise stated, the $20 \%$ tolerance will be satisfactory, but of course if closer tolerance resistors happen to be available they can be used. The closer the tolerance, the higher the cost, so it is a waste of money using close tolerance components where they are not needed.

If close tolerance is specified in the components list, then the circuit is more critical and the stated tolerance should be used. If for some reason a close tolerance component of the value required cannot be obtained, but there are some of that value with larger tolerance to hand, check these with a meter. It may be that they could fall within the required tolerance. A $20 \%$ resistor does not mean that it is bound to be $20 \%$ outside the stated value, only that it may be. The error is guaranteed to be less than $20 \%$. Thus it is often possible to select by measurement a $20 \%$ resistor that is spot-on in value, or nearly so.

Critical circuits often contain a preset control which must be set to give a specified voltage or
current. Thus the resistors associated with that part of the circuit need not be of close tolerance. In fact, different values that are near to those specified can be used at a push, because the preset will compensate.
The same thing applies to capacitors. Many electrolytics are rated at $-20 \%+100 \%$ which means that they may be up to $20 \%$ less or $100 \%$ more than the stated value. It is usually better to have a little more capacity than less, especially where decoupling circuits are concerned. Some capacitors are available that are $-20 \%+50 \%$ if a closer tolerance is required. It can be seen from this that the average electrolytic is likely to be rather higher than its stated capacity. It is also obvious that values are not too critical, so if the required value is not available, the next highest can generally be used. Thus $50 / \mu \mathrm{F}$ can be used in place of $25 \mu \mathrm{~F}$, and $16 / \mathrm{F}$ in place of $8, \mu \mathrm{~F}$.
Paper and polyester capacitors are usually $20 \%$ or $25 \%$ tolerance, although for special purposes where accuracy is important $5 \%$ tolerance or better can be obtained. As with resistors, if a bridge is available, it is often possible to select from a number one that is quite close to the required value.
Ceramic capacitors are usually made with wide tolerance ratings; $-25 \%+50 \%$ is common where value is not too important but a little more rather than a little less is preferred. Such can be used for r.f. decoupling purposes, 1000 pF . to 3000 pF . being common values. Ceramics can be obtained in the lower values at $10 \%$ tolerance or better and these or mica capacitors should be used for tuned circuits and similar r.f. applications.
It may be felt that these tolerances are rather wide, but remember that they are the maximum permissible deviations for the category. Most components will be found to be well within the tolerance rating.

## VOLTAGE RATINGS

The voltage rating of capacitors seems to be something with which some readers have difficulty. For d.c. circuits it means simply that the applied voltage must not exceed that for which the capacitor is rated. The minimum rating then, must be the applied voltage plus a safety margin. Thus with a 200 volt h.t. line all h.t. capacitors should be 250 volt working minimum. Lower voltage working capacitors can be used elsewhere such as for cathode bias bypass. For the earlier stages this may be a few volts but output stages run at up to 20 volts bias normally, so 25 volt working capacitors should be suitable. With some stages the bias is higher, and 50 volt capacitors must be used, but these are also often used with lower bias voltages to give a higher safety margin.

The miniature capacitors used with transistor equipment come in various low-voltage ratings. Again, the rating can be selected by considering the supply voltage and circuit position. If the battery voltage is 9 volts, then a rating of say 12 volts or higher would do for any circuit position. Lower voltage ratings can be used for emitter capacitors, usually 6 volt being ample here. Coupling capacitors in both valve and transistor equipment can be rated at about half the supply voltage but it must be remembered that a fault condition may put the
whole of the supply voltage across the capacitor, so it is best to use one rated for the full supply voltage.

With one make of record-player, the designers slipped up on this point. It was valved, but with a silicon rectifier. A 150 volt coupling capacitor was used which was amply rated for normal running. When the player was first switched on the supply voltage was instantly available, before the valves had warmed up. This meant that around 250 volts appeared across the capacitor during this period. Needless to say a number of these players found their way into the workshop with short circuited coupling capacitors!

Note from what has been said before, that the capacitor voltage rating must not be exceeded. This means that one with a higher rating than is necessary can be used if the desired rating is not available. The higher the voltage, the more bulky the capacitor and with some exceptions, more costly. Generally though, size is the main consideration. If the equipment is small and the space limited use the lowest voltage rating consistent with requirements, but if space is not at a premium, higher ratings can be used if desired.

For a.c. or pulse circuits, the capacitor must be considerably uprated. The peak value of an a.c. sine wave is 1.4 times that of the r.m.s. voltage. The peak-to-peak voltage then will be $2 \cdot 8$ times, so a capacitor should be rated at three times its d.c. working voltage. Thus for 250 volts a.c., a 750 volt working capacitor would be the minimum. Usually, 1000 volt capacitors are used to give a good safety margin.

## CONSTRUCTION

Having selected and obtained our components, there are a number of points to watch for when fitting them. First, check the colour coding of resistors and that you are reading them the right way round. For example, a $270 \mathrm{k} \Omega$ (red-violet-yellow) can be mistaken for a $4.7 \mathrm{k} \Omega$ (yellow-violet-red) if the coding is read from the wrong end of the resistor. Also, a $1 \cdot 2 \mathrm{k} \Omega$ (brown-red-red) resistor can be mistaken for a $220 \Omega$ (red-red-brown) one. With the preferred values now in use, these are the only "back-to-front" mistakes that can be made, so be careful when handling resistors. With many resistors, especially in the smaller wattages, mistakes can easily be made. Make sure too, that the colours are what you think they are. Some markings in orange are quite deep in tone and can be mistaken for red, particularly when viewed in artificial light.

Another mistake that can easily be made is to wire in polarised components incorrectly. We all know that electrolytic capacitors should only be connected one way round, but when fitting a large number of parts to a printed board it is easy for the odd one to go in the wrong way round. Double checking is the only answer. Similarly, diodes have to be watched. It anything, it is easier to make a mistake here as the markings and shape of the very small ones are not easy to identify. The ring and rounded end with Mullard diodes indicates the cathode, but often the ring is indistinct, and the other end appears rounded as well.

It is best to work to a system in construction. Do all the mechanical operations first, drilling, cutting
circuit boards and fitting components such as transformers, controls and sockets. It is easy to have a mishap and damage some of the smaller components if any of this work is left to later. Wiring of the circuit can now begin. This should be done stage by stage, and when a stage is completed, go back and check component values, electrolytic and diode polarity, and trace through the connections (it is easy to solder a lead to the adjacent tag or printed strip to the one intended). Having satisfied oneself that the stage is wired correctly, then pass on to the next. If the construction has to be left (constructors have been known to go to bed at times!), try to complete a stage. This is a danger-time when errors and omissions can easily be made.
When re-starting it is prudent to check the previous stage again. All this checking may seem tedious and time-consuming, but even experienced engineers can and do make mistakes when constructing things and it is better to check and double-check rather than spend hours trying to correct baffling faults found when the equipment is first switched on.

Modern transistors are less heat-conscious than their predecessors, but they still can be damaged by too much heat. It is a good idea to leave the transistors in any particular stage as the last component to be fitted, then they cannot be affected by heat when soldering in adjacent components. When actually soldering the transistors, leave the iron on the connection only long enough to make a good joint. If for any reason it is not satisfactory and needs re-doing, leave it to cool for a few seconds before tackling it again. It is good practice to use a heat-sink whenever possible.

## SOLDERING

When making a large number of joints it is possible that even the expert will make one or two "dry" joints. The only remedy is to be painstaking with each one and not to rush it. Wire-ended components are supposed to be ready tinned, but often solder will not take readily, and if they are soldered into print or to a tag, the solder will flow around the wire but take on the print and appear to make a good joint, but it will be bad inside.


Fig. 1 : Many dry joints exhibit an inward curve where the solder meets the wire (top). A smooth contour from wire to solder is usually the sign of a good joint (bottom).

Always tin the wire initially and see that the solder has taken all around before attempting to make a joint. This may mean that the wire must be scraped first. It is sometimes possible to tell a bad joint by the way the solder meets the wire. Reference to Figure 1(a) shows the solder curving inward where it meets the wire. This is due to surface tension in the solder when it was molten and shows that it has not taken on the wire because the solder had a separate surface. Often there will be traces of
resin from the solder core at the junction. In Figure 1(b) the solder has bonded itself to the wire and has no separate surface, hence there is a smooth flow from the wire to the bulk of the solder. This is not an infallible way of judging joints as the solder may have taken just at the point where the wire leaves the joint but not inside; or it may have taken inside, as in the first example, but not at the edge; but at least it does give a clue. A further check can be made by gently pulling or twisting the wire to see if there is any movement between it and the joint.

Excess solder must be guarded against, especially on printed circuits where there is a danger of it shorting over to adjacent print. A golden rule which should be observed at all times is never to interrupt the making of a joint. If the wire is pushed through the print or wrapped around a tag, and then one is called away without soldering the joint, more likely than not one will proceed with the next joint on returning. Time and again joints have been left unsoldered because of interruptions. If the house is burning down, let it, but make sure you finish your joint!
More could be said on the important art of soldering but it is hoped to make this the subject of a complete future article.

## CIRCUIT BOARDS

There are several printed circuit methods available to the constructor. Veroboard is a popular one because it is versatile and ready to use. When cutting across a section of print to isolate it, remove a complete segment. Just cutting across with a biade may permit the solder to later bridge the cut, or the cut may not be complete to start with. Fig. 2 shows the right and wrong way.
Better still, use the proper spot-face cutter sold for this purpose. The physical mounting of the printed board may pose problems as it is desirable to have access to both sides for servicing. One successful method is to solder a tag board to a strip of unused print at the edge. The tags can then be mounted


Fig. 2 (a) A narrow cut in a copper rail can is easily bridged with solder or dirt so a wide cut (b) is much preferred.
with nuts and bolts where required. This gives a vertical mounting with access to both sides the tags being bent to give the printed board any desired angle. Fig. 3 illustrates this arrangement.

Wiring should be done with solid rather than stranded wire, because it stays put and can be formed to give a much neater appearance. Bare copper wire can be used with sleeving, or as the usual plastic-covered wire. Whichever is chosen, it
is good to use different colours for different parts of the circuit. Quite a range of colours can be obtained. Red can be used for positive supply circuits, black for earth or negative; green for grid or base circuits; grey for a.g.c.; orange, unsmoothed h.t. and so on. This enables future testing to be so much easier, but stick to the coding once it has been decided upon.


Fig. 3: Method of mounting Veroboard in a vertical position allowing access to both sides of the board.

It is a good practice to earth all appropriate components to one point in each stage. Furthermore, these points can then be linked and earthed to the chassis or frame at one point. This prevents h.f. chassis currents, in the case of radio equipment, leading to common impedance coupling and instability. With audio equipment it reduces the possibility of hum from the same cause. It is true that in many cases it may prove unnècessary, but like providing adequate decoupling, it is good preventive practice and difficult to carry out once the circuit has been wired.

## TESTING

Having completed the building of the project, the time eventually comes for the first switch-on. It is not unknown for this action to be accompanied by a blinding flash, smoke or other disquieting phenomena! A simple precaution is to take a resistance reading across the power supply circuits before switching on. The initially low resistance reading should quickly rise as electrolytics charge up from the meter battery. (Remember, the positive side of the test meter is negative battery polarity). Any permanent low resistance must be investigated. Then, wire the meter, switched to a high current range, in series with the supply and switch on. An abnormally high current should prompt an immediate switch-off and examination.

It may be that in spite of all these precautions, the equipment constructed fails to work satisfactorily. Normal fault-finding techniques must now be applied to find the cause of the trouble. Voltage measurements find the majority of faults, so go to work with the meter, and with the aid of the published circuit diagram check to find if there are volts where they should be. Check too, as to whether the voltages are approximately correct. This will depend on the equipment and its function. As a very general rule with transistor stages, the collector voltage should be about half that of the supply, emitter voltage should be about 1 volt and the base should be about $0 \cdot 1$ volt higher than the emitter for germanium and about $0 \cdot 6$ volts higher for silicon transistors. With oscillators, emitter followers
and similar stages, voltages will be different from the above.

Directly coupled stages can be confusing and a fault in one can affect the voltages in another. Note though, that the base/emitter voltage difference is present as this forward bias is essential for the transistor to conduct, in normal circuits. Some lowcurrent circuits, as used in the input stages of audio amplifiers, may use a high value resistor of $3 \mathrm{M} \Omega$ or so from base to collector, to supply bias, and the meter current will cause a much lower reading. This must be allowed for, or if available a valve-voitmeter should be used. Incidentally, when the equipment is working satisfactorily, it is a good idea to take all the voltages and note them down on the circuit, for future reference.

If there are still no results and the voltages seem right, then check through the signal circuits using some form of signal injection. However, by following some of the tips outlined here, construction will not be such a hit-or-miss affair, but one reasonably certain of immediate success.

## MODIFICATIONS

Now we come to the question of modifications. Some readers may wish to add extra facilities or to tailor the equipment to their own particular needs. This sometimes leads to letters to the Editor or author requesting modification design details. Now while we try to help as far as possible, producing designs to order is something that cannot be undertaken. Not only is a good deal of time involved, but any theoretical design must be built and development work carried out before it can be passed as workable. Obviously this is not possible.

Minor modifications should be within the capabilities of most readers if they have read carefully the various theoretical and practical articles that regularly appear in radio magazines. More ambitious modifications could provide a subject for private research and experiment; really, with this hobby, there is more satisfaction and pleasure to be derived by experimenting and trying out one's ideas than there is by following a tried and tested circuit. A recommendation though, is to get the unit working as first planned, and then introduce the modifications. If they prove unworkable, one can then revert to the original.

## Back Numbers Important Announcement

We regret to inform readers that owing to the closure by the Company of the department concerned it will no longer be possible to supply back numbers of Practical Wireless and Television.

To ensure obtaining regular copies of these magazines readers are strongly urged to place a regular order with their local newsagent, or to take out an annual postal subscription.

Reference to past issues of the magazines may sometimes be obtained at certain public libraries who may hoid bound volumes. A few libraries are said to offer a photostat service. Alternatively, we are always willing to insert a free request for specific back numbers in our "CQ" column which appears in most issues.

# VHEignalGenerator <br> <br> R.H.LONGDEN 

 <br> <br> R.H.LONGDEN}

WHEN it is necessary to adjust a VHF receiver or converter such as may be used for the 144 MHz amateur band, a signal generator covering the required frequency is extremely useful. As an example, even a straightforward unit such as the 144 MHz converter in the July 1972 issue of Practical Wireless has four circuits which must be tuned to about 144 MHz . With such equipment, if all of the circuits are initially considerably off tune, it may not be easy to peak them for maximum noise or reception of signals which are not very strong. On the other hand, when a suitable signal is available, it is easy to trim all the circuits for maximum efficiency.
The generator described here is intended particularly for the frequencies from 105 MHz to 170 MHz , thus including the 2-Metre Band, but it can be used at frequencies outside these limits, and particularly for checking the coverage and alignment of converters and the simpler types of VHF receivers. It is a small, self-contained solid state unit, providing a modulated r.f. output.

## GENERATOR CIRCUIT

In Fig. 1, Trl is the audio tone generator or modulator. The transformer T1 is connected in the correct phase to obtain audio oscillation and this modulates the r.f. oscillator, which is supplied through the winding 3-4 of T1. .
Tr 2 is the r.f. oscillator. L 1 is tuned to the required r.f. frequency by VC1, which has a dial for logging frequencies. An adequate signal is generally obtained by having the generator near the equipment being adjusted, but output can be taken to an external lead by the loop L2, if desired.
With a crystal controlled converter such as that mentioned, reception must be at the correct frequency, because VHF signals can only come out at a particular lower frequency. In this particular converter, 144 MHz is tuned at 4 MHz on the receiver.


145 MHz at 5 MHz , and 146 MHz at 6 MHz on the receiver scale. So for adjusting such equipment there is no real need for VCl to be calibrated. Instead, VCl is merely tuned until the VHF signal comes through the converter, which can then be adjusted. In other cases, it is helpful to calibrate VCl , in the way described. This will allow the frequency range of fully tunable equipment to be checked.

## CONSTRUCTION

VC1, Tr2 and the associated items are assembled on a tag board about $1^{11_{2}} \times 2 \mathrm{in}$. as in Fig. 2. As an alternative to the tag or group board, plain Veroboard with 10 pins inserted could be used, or eyelet board, or $l_{16}$ in. thick paxolin drilled to take the leads. Veropins will have to be snipped off nearly

## components list

| Resistors |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | $4 \cdot 7 \mathrm{kS}$ | R4 | $10 \mathrm{k} \Omega$ |
| R2 | $10 \mathrm{k} \Omega$ | R5 | 10kS |
| R3 | 47 k / | R6 | $1 \mathrm{k} \Omega$ |
| All resistors 10\% $\frac{1}{4}$ W |  |  |  |
| Capacitors |  |  |  |
| C1 $0.02 \mu \mathrm{~F}$ dis |  |  |  |
| C2 1000 pF disc or tubular ceramic |  |  |  |
| C3 | $4 \cdot 7 \mathrm{pF}$ |  |  |

## Transistors

Tr1 NKT214 or AC128
Tr2 BF200 or similar VHF planar epitaxial transistor

## Miscellaneous

VC1 Jackson C804 10pF
T1 T/T3, 3.6:1 +1 (R.S. Components)
On-off switch
Two small sockets
Tag and insulated board
Case about $4 \frac{3}{4} \times 3 \frac{3}{4} \times 2 i n$, deep
$0-100$ knob dial, KN1, Home Radio (Mitcham)
flush, as if this is not done the spindle of VCl may not project enough to take the numbered dial.

The board is drilled for VCl. A washer is later put between this board and the panel, on the bush of VCl and the bush nut then holds the whole assembly to the panel.

All connections in this section should be short, though the wires from $\operatorname{Tr} 2$ need not be cut down to less than ${ }^{1} 2 \mathrm{in}$. Solder these rapidly after other wiring is taken to the tags, and use a heat shunt such as a pair of flat-nosed pliers on the leads while soldering.

Ll is chosen from the details given, for the coverage which is required. L2 is a single turn, some $3_{8}$ in. to ${ }^{1} 2$ in. from L1, and is the same for all coils.

This section can be tested by connecting the S1 lead to negative on a 9 V battery and the lead which runs from Cl to 3 on Tl to a meter, which is clipped on the battery positive terminal. If the circuit is oscillating, current falls slightly when VCI is shorted by placing a metal tool from moving to fixed plates. Actual current was 4 mA , falling to about $3 \cdot 8 \mathrm{~mA}$ but this figure is not very important, and will depend on the particular transistor used. However, it is important that this change in current is found. If it is not, the circuit is not oscillating and no r.f. is produced.


Fig. 2: The component layout.
With particular transistors in the $\operatorname{Tr} 2$ position, an upper frequency limit will be found, where oscillation grows weak and ceases. No particular difficulty arises in obtaining oscillation up to 180 MHz or so. In fact, a number of transistors will work, and if the one fitted oscillates up to the highest frequency wanted, this is satisfactory. There is no point in using a transistor which could operate at a much higher frequency than required, as these cost considerably more than the popular types suitable for up to 180 MHz . On the other hand, some cheap transistors which are supposed to be suitable for this frequency will cease to oscillate or become very inefficient. Should some particular VHF transistor be to hand, and not work with the values given, then the values at R 4 (or R 5 ), C 3 , and R 6 may be changed to find if oscillation can be obtained.
$\mathrm{T}, \mathrm{Tr} 1$ and the three resistors are mounted on a piece of eyelet or other insulated board about $1_{3}{ }_{4} \mathrm{x}$ $1^{3_{4}}$ in. as in Fig. 2. Leave flying leads for the battery positive, Sl (battery negative) and from tag 3 of Tl to go to Cl.


An internal view of the prototype.
This part of the circuit may be tested by connecting phones to $3-4$ and applying 9 V . With the components listed, a clear audio tone should be obtained.

Two countersunk 8BA bolts fix the board as shown. Spacers, nuts or washers are put between the panel and board.

The front panel should be made of parolin. If it is metal, the bush of VCl should be isolated from it with insulated washers. VC1 is fitted with a $0-100$ degree dial, or with a control knob allowing markings to be made on a paper scale fixed to the panel.

The case was a die-cast box $4^{3}{ }_{4} \times 3^{3}{ }_{4} \times 2$ in. deep, but a small plastic lunch-box or other case will do equally well. L1 is placed so that it is well clear of metal when the panel is fitted to the box.

## L1, FREQUENCY AND CALIBRATION

Exact coverage will naturally depend on individual layout and the length of leads, but should be reasonably close to the figures given. The frequency is lowered by using more turns on L1, by winding Ll to a larger diameter, or by compressing L1 so that its turns are closer together. Fewer turns, smaller diameter, or stretching raises the frequency. In all cases L1 is of 20 s.w.g. tinned copper wire, selfsupporting. Details of LI are:
$105-125 \mathrm{MHz}$ : 5 turns, ${ }_{2}$ in. outside dia. and $5_{8} \mathrm{in}$. long. Ends ${ }_{3} \mathrm{in}$. and ${ }_{8} \mathrm{in}$. long.
$125-148 \mathrm{MHz}: 5$ turns, $3_{8 i n}$. outside dia. and lin. long. Ends ${ }^{1}{ }_{8}$ in. and ${ }^{1}{ }_{2}$ in. long.
$148-170 \mathrm{MHz}: 4$ turns, ${ }_{3}{ }_{32} \mathrm{in}$. outside dia. and ${ }_{4} \mathrm{in}$. long. Ends each ${ }_{2}$ in. long.
Where a crystal controlled converter is available, or a VHF receiver, these will furnish calibration marks through the ranges they cover. This may prove handy when building other, fully tunable VHF equipment.

The VHF enthusiast can calibrate the oscillator by using a Lecher line and measuring the length of this to find the wavelength in metres. This is practical at these frequencies as the line will only be up to three metres or so long, and resonance produces a dip in battery current.

For some lower frequencies it may be possible to pick up the signal when the generator is tuned so that a harmonic is heard in the receiver. Second harmonic reception will arise when the generator is tuned to one-half the receiver frequency.

When some calibration points have been obtained, these can be entered on a scale or list, or on a graph which will give intermediate frequency readings.

## EXPERIMENTERE CORNEA



## NOVEL 'SCOPE CALIBRATOR

THE instrument to be described will work well with virtually any oscilloscope and facilitates the voltage calibration of both the $X$ and $Y$ axes in one simple operation. It is easy to build and use and the total outlay, including a suitable case, should not exceed £2.

## CIRCUIT

The circuit is basically a conventional phase-shift network with the addition of resistors R2 and R3, and zener diodes D1 and D2. The values of C1 and R1 were found by experiment to give an almost perfect circle output from the phase-shift network. Addition of the zener diodes clips the alternative half cycles and produces the rather novel square display as shown in the photograph. Resistors R2 and R3 simply limit the zener current to an acceptable level and eliminate any chance of loading the phase-shift network. Provision of the ganged potentiometers allows the amplitude of the display to be varied from zero volts to the maximum zener voltage which in the prototype was set to be 5 V .

Although a matched pair of zener diodes is to be preferred, odd diodes can be matched by inclusion of series resistance at points marked A and B on the circuit diagram. Indeed the constructor could use virtually any zener diodes that happen to be at hand as long as the nominal zener voltage is equal to, or in excess of, the maximum required for display. It will be found that the polarity of the zener diodes is of no consequence in this circuit, it will operate whichever way the diodes are connected. The prototype used Mullard OAZ201 $5 \cdot 1 \mathrm{~V}$ types adjusted as above to provide exactly 5 V . The rating of the diodes should be at least 250 mW .

The constructor is not hindered in any way in the construction of this instrument as the layout is by no means critical and there is considerable flexibility in the selection of components. Any transformer supplying $12-20 \mathrm{~V}$ will suffice as the current required is negligible. A type MT98 9-0-9V available from


Fig. 1: The circuit of the 'scope calibrator.


Henry's Radio is ideal as it is small enough for Veroboard or printed circuit board mounting. The ganged potentiometer should be a good quality type with a resistance between $500 \mathrm{k} \Omega$ and $1 \mathrm{M} \Omega$. If the reader wishes, separate potentiometers, individually calibrated for each axis, could be used. Resistors R2 and R3 should not be reduced in value or the zener diodes may be damaged. The outputs can be taken via any type of terminals convenient to the constructor. No further constructional notes are considered necessary as the reader is free to use whatever form of construction that he (or she!)* finds most convenient. Of course there is no reason why the unit could not be incorporated as an integral part of an oscilloscope provided sufficient space is available.

## CALIBRATION

Having constructed the instrument with an established 5 V maximum output, the first step in calibration is to set the potentiometers for maximum amplitude and mark this point as 5 V . Then adjust the oscilloscope gain controls until the display is ten divisions of the oscilloscope graticule on each side. This gives a display of 0.5 V per division. Then, without touching the scope gain controls, gradually reduce the calibrator output by one division at a time marking the dial at 0.5 V steps. You then have a reasonably accurate instrument capable of voltage calibration of both axes of your oscilloscope in a single operation.

There is ample scope for the constructor to tailor the unit to suit his own needs and for this reason constructional details have been cut to a minimum.

* Concession to Women's Lib.-Ed.


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#  <br>  <br> L.A.J. IRELAND 

## Number 35

THE SGS TBA23I i.c. reviewed this month follows along the fairly well established lines of high performance quality audio preamplifiers set by the RCA3052 which has already been reviewed in this column (May 1970). Low noise and high gain coupled with low power consumption are features being demanded more and more both by industry and the discerning audio enthusiast and the tight specifications associated with the TBA231 (noise figure less than 70 dB , flat frequency response gain of 29 dB ) should make this i.c. meet the requirements of any amateur seeking a good quality audio preamp.

In Fig.1, a complete circuit diagram of one of amplifiers in the TBA231 is given. It is not intended to analyse the circuit in detail but a number of the more unusual features in the design will be pointed out. First a string of diodes D1 to D6 accurately control the constant current transistors $\operatorname{Tr} 3$ and $\operatorname{Tr} 6$ which also act as active bypass elements. In addition provision is made for limiting the output current in the event of a short circuit at pin 1. In this instance, the voltage increase developed across R6 automatically biases off $\operatorname{Tr} 7$ and $\operatorname{Tr} 8$ thereby preventing damage to the chip from an excessive current flow.


Fig. 1: Circult of the TBA231. Numbers in brackets are pin connections of second identical amplifier.


Fig. 2: Amplifier incorporating RIAA equalisation and active tone control circuits.

Also, even though the two amplifiers are fabricated and electrically connected on the same monolithic chip, channel separation of 140 dB results from careful design and layout. So any interchannel inter-action will more than likely be caused by poor external bias decoupling or power supply fluctuations.

A typical application of the TBA231 as a hi-fi preamplifier utilising the first section for RIAA equalisation and the second amplifier section as an active tone control unit is illustrated in Fig.2. Typical performance specifications of this design are associated usually only with the more expensive hi-fi amplifier units.

The TBA231 is available from any SGS distributor such as Quarndon Electronics Ltd., Slack Lane, Derby.

## EIS again . . .

Further development work carried out on the Electronic Ignition System has indicated that the output voltage of the original circuit was a little high and resulted in an increased possibility of crossfire and distributor cap flashover in damp conditions. As a result the output voltage has been reduced and it is now recommended that for optimum operation the value of the capacitor be increased from $0.47 \mu \mathrm{~F}$ to $1 \cdot 0 \mu \mathrm{~F}$.

Because of the arduous operating conditions imposed on this capacitor it is recommended that a triple foil type with at least 440 V a.c. or 1000 V d.c. rating be used. A suitable capacitor has been developed specifically for C-D ignitions and these are available from Magtor Ltd., 68 Dale Street, Manchester, at a cost of 35p including post and package. -Stephen Soar, (Manchester).

## . . . and again

Just a brief note on the $P W$ Electronic Ignition System. I found that the unit caused interference on my car radio so I bought a filter kit from Magtor Ltd., as advertised in PW. I fitted the three components inside a cylindrical aluminium can taken from an old vibrator unit and wired it into the E.I. box. In some cases it might be possible to fit the components into the E.I. box itself.

The filter kit is actually intended to decouple E.I. circuits when a tachometer is also fitted but it certainly proved effective against interference to my radio. -P. Beaman, (Bridgnorth, Shropshire).
(The decoupling kit can be obtained from Magtor Ltd., 68 Dale Street, Manchester, MI 2 HS , price £1 including $p$ and p.)-Editor.

## Padding out

I write with reference to the many designs of receiver appearing in $P W$ using Denco Miniature plug-in coils.

On reading through the manufacturer's literature on these coils it came to may notice that no padder was required for range five (red) coils. To satisfy my
curiosity, I drew a graph of mid range frequency against padder value for each of the five coils. This came out as a straight line, and gave the range five padder to be $6,000 \mathrm{pF}$. This value was then tried in my receiver, which uses these coils, and it gave a marked improvement at the l.f. end of the band. On mentioning this to a friend who has built a receiver along similar lines to mine, he also tried it and got results similar to mine.

I would like to know what other readers, and maybe even Denco Ltd., think on the subject.-P. Richards, (Manchester).

## A bit tight

I am sure many readers, at some time or another, have been frustrated to find that they have been unable to remove the bits from their 25 Watt Henley Solon soldering irons when they are due for replacement.

Having purchased a new iron some time ago, I slightly reduced the diameter of the bit with emery cloth and fitted a sleeve made from aluminium foil to come between bit and the body of the iron. Thus the binding between bit and iron is eliminated.

The foil I used was obtained from a cup containing a mince pie and if other readers follow my example, they can eat the byproduct with their coffee whilst doing a soldering job!-R. H. Roling, GW6WM (Glamorgan).

## What do you get?

Please will you tell me what a man who pays $£ 10$ plus for a tone arm actually gets for his money?

I have recently constructed a pair of tone arms using standard 'Meccano' parts throughout. Both are heavy, but due to the screwadjusted counter weight, tracking weights of much less than that of a Meccano nut are easy to arrange. They are about 13 in long from pivot to head. Tracking error should not be too great if it is set correctly, which I suppose would involve setting the stylus to point along the groove while the arm is about one-half of the way across the track of the record. I have
been unable to test it as yet due to the lack of a cartridge and stylus, which I am not allowed to remove from our Record Player for testing purposes (or any other), therefore, I used a dummy weight to simulate this.

The cost of the arm with the screw adjusted counterweight would be less than $£ 1$ if all the parts were bought new.-S. Sellick, (Devon).

## Aerial problem

May I enquire through the columns of $P . W$. for help.

I have a portable receiver which is for use on the 108-136 MHz and $145-175 \mathrm{MHz}$ bands. The set is equipped with the usual telescopic aerial, and this is ideal for reception from airborne aircraft or when within sight of an airport control tower.

I would like to build an aerial which I can place on the housetop (40ft above ground) which I am sure would give me better reception from the local airport, which is 5 miles from my home.

I have written to 3 major aerial manufacturers for either details or purchase of a suitable aerial. but they do not seem to be interested in the problem.-J. Stirzaker, (4 Maitland Avenue, Anchorsholme, Blackpool, Lancs). (The lack of interest may be explained by the fact that the Ministry of $P \& T$ has repeatedly pointed out that a Licence [not generally available to the public] is required for the reception of transmissions by Fire Brigade, Aircraft, Shipping, etc.)-Editor.

## Help!

At the moment $I$ am having difficulty in obtaining a diagram and aligning instructions for a Ferdio wireless PR41 "Town and Country" with trawler band.

I have the service sheet for PR41 but this is the older one and has 8 coils, but the one $I$ want has 9 coils, which must have been the last model made. It has a tone control on the side and tape DIN socket on the back of the case. Can anyone help please?-Richard Cowley, Kerrowglass, Kirk Michael, Isie of Man.

# - $\%$ SणUNDELHTIIN EOUPMEN from 4 SPECHILSED DISED STUDIOS 

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SOVEREIGN. 100 watt $\mathrm{mms}. 18^{\circ}$ Bass, $12^{\prime \prime}$ Full SOVEREIGN. 100 watt $\mathrm{rms.}_{\text {. }}$ I
range. Size $50^{\prime \prime} \times 26^{\prime \prime} \times 14^{\prime \prime}$.

FULL RANGE OF MICROPHONES, STANDS, ETC. ALWAYS IN STOCK

## SOUND CONTROLLED AND SOUND TO LIGHT UNITS

Mid, Treble and Bass Channels. up to 1 kw of lamps per channel plus override switching. DJsoL. Sound to light. Takes output from most amplifers. Adjustable levels.
DJ40L. Sound controlled version. Built in microptrone, no connections required.

ASSEMBLED DISCOTHEQUES
DISCO-PLINTH. Consists of 2 turntables fitted with high quality ceratruc cartridges. The unit has a built in cross-fade rotary controt for transferring the oound from left to right decks. The unit has no amplification as the D.J. 105 S or D.J. 70 . Size $32 \times \times$ $142^{*} \times 7^{*}$ (incl. lif).
DISCO-IMP. The latest addition to the Discosound Range of discotheques, Even smaller and more compact than the Disco-Mini, it contains all the necessary features for the smooth runaing of a mobile unit. Size $29^{\circ} \times$ DISCO-MITT
DIsCo-MINI. Complete portable Disco with
built-in full function built-in full function preamplifier/mixer. Fo use with any power amplifier such as "Disc-
master". size $300^{*} \times 20^{"} \times 8$ " DISCO STAMBARD Has all
the Disco-Mini wifh the addition facilities of the Disco-alini wifh the addition of a built-in pletely self contained disco unit. A V.U. meter gives risual indication of output levels. Size $32^{\prime \prime} \times 27^{\prime \prime} \times 7 \frac{1}{2}^{\prime \prime}$.
DISCO SUPER. Disco-Standard. Fitted individual controis for both mic. and deck inputs plus a cross-fade for deck to deck transifer. A built in P.F.L. cuetng system, mic. over-ride, also a V.U. meter gives visual indication of output levels.
DJ. 30L (3000w) 3-channel psychedelic DJ. 30L (3000w) 3-channel psychedelic light are also featured for ease of cueing. Size sre also featured for ease of cueing, Size
$38^{*} \times 27^{\circ} \times 10^{\prime \prime}$. Super plus a third used for Jingles or other effects without using the main deck system. Flexi lights are also
fitted. Size $50^{\prime \prime} \times 27^{\prime \prime} \times 10^{\circ}$.

## Discoscene

536, Sutton Road, Southend, Essex. (0702) 611577

Discosound
122, Balls Pond Road. London, N. 1. (01) 2545779

Discosound (Birnningham) Ltd.
494, Bristol Road,
Selly Oak, B'ham 29. (021) 4721141

EFFECTS PROJEGTORS
 DISCO COLT. 150 watt. LIQUIMATIC MINL, 50 watt Q1 with $\mathrm{f}^{\prime \prime}$ wheel DISCOWHEEL, 50 watt Q1 with quick change Cassette
GNOME 150,150 watt $Q 1$ with Cassette. LICOIMATIC, 150 watt Q1 with $6^{\pi}$ wheel. PLUTO TUTOR-2, 250 watt Q1 with Cagsette and $6^{x}$ wheel.
TUTOR-2, With Liquisplode Tank.
KALEIDOSCOPE LENS (for Titor-2) 6* Liquid Wheel and Crystail Wheel Liquid Cassette and Moire ( 24 different types to choose from). Portable Hi-Power Strobes. YOU WILL BE SURPRISED BY THE LOW PRICES \& PERFORMANCE

## SDL POWER SPEAKERS

High efficiency $12^{\prime \prime}$ speakers. Ferrite magnets, Heavy duty voice coils and cones for Disco and Group use,
$12^{\prime \prime} 50$ watt rms. 8 ohm Full range.
$12^{*} 95$ watt fms. 15 ohm Mid-Treble. $15{ }^{n} 50$ watt rms. 15 ohm. Full range.
$15^{\prime \prime} 100$ watt rma. 15 ohm. Bass. $15^{\prime \prime} 100$ watt rma. 15 ohm. Bass.

## DISCO SPOT BANK



Designed to take three E/S Type spot or colour bulbs up to 150 watts each. The unit is of all metal construction and has one 3-pin mains input socket plus one 3 -pin mains output socket for connecting more than one bank together if requirerl. The unit can be left free-standing or wall mounted if needed. Black crackle finish gives the unit a wery professional appearance.
Size $18^{\prime \prime} \times 6^{+} \times 7^{*}$ (excluding bulbs)
Also in stock: Vltra Violet Spot Lamps and Fluorescent Lamps, Standard and Colour Spiot Lamps and Fittings. Rotating Colour Displays, Flexilights, Fibre Optics, Dimmers, Flashers Effects Foils, etc. Your enauiries invited.

## MIXER UNITS

DJ.101. Battery powered, 6-channel, variable levels, $8 \times 50 \mathrm{k}$ mic., $1 \times 100 \mathrm{mV}$. aux., $3 \times$ 100 mV p.u. Output 250 mV .
DJ.102. Mains operated, 4 -channel, variable evels. $2 \times 50 \mathrm{k}$ mic., $2 \times 100 \mathrm{mV}$ p.u. PFL control, master volume, mic. over-ride, outpht variable $0-500 \mathrm{mF}$.
DISCO 40. Pre amp part of Disco amp (see above). All facilities. Output will drive up to ten 100 watt amplifiers.

## DISCO MINI

Hardly larger than a suitcase yet contains for a necessary features bile unit. The pre-amp bas separate tone and trols for both mic. and deoks,
and each input has its own indi-
plus the addition ontrols and inputs,
built in P.F.L. system for cueing, together to deck sound transfer. A are standard on all units, Response $20-20,000 \mathrm{~Hz}$. Mic. input 5 mV 50K. Output 1 volt.
McDonald M.P. 60 Turntables are used with high quality ceramic cartridges, and each deck has its own individual cut out switch fitted This unit is suitable for Discos or Clubs having a power amplifier, or for use with the 'Discmaster' 100 watt power amplifier as above.

309, Edgware Road, London, W.2. (01) 7236963

## CHECK WITH YOUR NEAREST STUDIO FOR LATEST PRICES AND DETAILS (TRADE and retail

 SUPPLIED)WE SUPPLY NEARLY ALL THE COMPONENTS FOR PROJECTS ADVERTISED IN THIS MAGAZINE

| TRANSISTORS |  |  |  | 2N | 2. | AF116 | 0.25 | ${ }^{8 C 307}$ | 0.1 | BF271 | 0.21 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 29301 | 0.1 | 2N | 0.12 | 2N6174 | 0.22 | AF118 |  | BC307VI | 0.10 | BrF273 | ${ }_{0}^{0.83}$ |
| 2G302 | 0.15 | 2N2925 | 0.12 | 2N5175 | 0.28 | $\mathrm{AF}^{\text {P1 }} 121$ | 0.22 | BC308 | 0.09 | BF274 | 0.28 |
| 24303 | 0-85 | 2N2926 |  | 2N5176 | 0.32 | AF124 | 0.24 | BC. 08 A | 0.09 | B $\mathrm{H}_{4} 457$. | 0.48 |
| 2 C 306 | 0.30 | Green | 0.10 | 2N5245 | 0.43 | AF125 | 0.20 | BC308B | 0.09 | BF458 | 0.57 |
| $2 \mathrm{G309}$ | 0.80 | Yellow | 0.10 | 2N5190 | 0.92 | AF126 | 0.19 | BC309 | 0.10 | BF459 | $0 \cdot 57$ |
| 2ar344A | 0.25 | Orange | $0 \cdot 10$ | 2N5191 | 0.96 | AF127 | $0 \cdot 80$ | BC309A | 0.10 | BFS21 | $2 \cdot 10$ |
| 2G345R 0 | 0.25 | 2N3053 | 0.31 | 2N6192 | 1.24 | AF139 | 0.38 | BC909B | 0.10 | BFS21A | 2.30 |
| 20371 | 0.15 | 2 N 3054 | 0.47 | $2 \mathrm{NS193}$ | 1.01 | AF170 | 0.25 | BC313 | 0.30 | BFS28 | $0-92$ |
| 2G974 | 0.15 | 2N3054 | 0.46 | 2N5194 | 1.10 | AF172 | 0.25 | BC327 | 0.24 | BFS61 | 0.27 |
| 2G381 | 0.22 | 2N3055 | 0.50 | 2N5195 | 1.46 | A ${ }^{1} 178$ | 0.55 | BC328 | 0.22 | BFSG8 | 0-28 |
| 2G417 | 0.20 | 2N3390 | 0.29 | $2 \times 5245$ | 0.48 | AF179 | 0.85 | BC337 | $0 \cdot 19$ | BFW10 | 0.81 |
| 2N109 | 0.48 | 2N 3391 | 0.20 | 2NS457 | 0.30 | AF180 | 0.50 | BC338 | 0.19 | BFW11 | 0.81 |
| 2N174 | 1.40 | 2N3391A | 0.28 | 2N5458 | 0.38 | AF186 | 0.40 | BCY30 | 0.35 | BFW15 | 0.35 |
| 2N176 | 0.75 | 2N3392 | 0.18 | 2N5459 | 0.38 | $\mathrm{AF}^{2} 00$ | 0.35 | BCY3I | 0.40 | BFX13 | 0.28 |
| 2N274 | 0.75 | 2N3393 | $0 \cdot 12$ | 3N128 | 0.63 | A F239 | 0.41 | BCY32 | 0.60 | BFX29 | 0.25 |
| 2N335 | 0.75 | 2N3394 | 0.12 | 3N138 | 1.37 | AF240 | 0.72 | RCY32 | 0.76 | BFX 30 | 0.25 |
| 2N351 | 0.95 | 2N3402 | 0.17 | $3 \times 199$ | 1.38 | AF279 | 0.54 | BCY33 | 0.34 | BFX 37 | 0.30 |
| 2 N 376 | 1.00 | 2N3403 | 0.18 | 3N140 | 0.76 | AF280 | 0.54 | BCl 34 | 0.35 | BFX44 | 0.38 |
| 2 N 384 | 0.03 | 2N3404 | 0.24 | 3N141 | 0.69 | AFY42 | 0.74 | BCY38 | 0.40 | BFX63 | 2.48 |
| 2 N 388 A | 0.40 | 2N3405 | 0.27 | 3N142 | 0.54 | AF211 | 0.65 | BCY39 | 1.05 | RFX 68 | 0.30 |
| 2N404 | 0.23 | 2N3414 | 0.10 | 3 N 143 | 0.64 | AL102 | 0.76 | BCY40 | 0.50 | BEX84 | 0.24 |
| 2N404 | 920 | 2N3415 | $0 \cdot 10$ | 3N152 | 0.79 | ALI 103 | 0.70 | BCY 42 | 0.15 | BPX85 |  |
| 2N456 | 0.75 | 2N3418 | 0.15 | 3N153 | 0.74 | A8Y26 | 0.30 | BCY43 | 0.15 | BFX86 | 0.24 |
| 2N456A | 0.75 | 2N3417 | 0.21 | 3N154 | 0.74 | A8Y27 | 0-88 | BCY58 | 0.21 | BFX87 | 0.25 |
| 2N457A | 0.80 | 2N3570 | 1.25 | 3 N 159 | 1.00 | ASY28 | 0.28 | BCY59 | 0.22 | BFX88 | 0.20 |
| 2N491 | $8 \cdot 25$ | 2N3571 | 1.12 | 3N187 | 1.30 | AsY 29 | 930 | BCY66 | 0.86 | BFX89 | 0.45 |
| 2N584 | 0.28 | 2N3572 | 0.97 | 3N200 | 8.07 | Asyso | 0.20 | ${ }^{\text {BCY }} 67$ | 0.94 | BFY10 | 0.35 |
| 2N591 | $0 \cdot 84$ | 2N3702 | $0 \cdot 10$ | 3N201 | 1.05 | ASY55 | 0.85 | BCY70 | 0.17 | BFY11 |  |
| 2N696 | 0.15 | 2N3703 | 0.10 |  |  | A8Z21 | 0.55 | BCY71 | ${ }_{0}^{0.22}$ | BFY17 | 0.8 |
| 2N697 | 0.15 | 2N3704 | 0.10 | 40050 | 0.78 | AU103 | 0.25 | BCY72 | 0.18 3.47 | ${ }_{\text {BFY }}$ BFY 18 | 0.85 |
| 2N698 | 0.25 | 2N3705 | 0.10 | 40251 | 0.81 | ${ }_{\text {BC108 }}$ | 0.14 | BCY88 | 2.40 | BFY29 | $0-50$ |
| 2N899 | 0.29 | 2N3706 | 0.90 0.10 | 40309 | 0.33 | BC109 | 0.14 | BCY89 | 0.80 | BFY29 | 0.40 |
| ${ }^{2 N} 708$ | 0.10 | $\begin{aligned} & \text { 2N3707 } \\ & \text { 2N } 3708 \end{aligned}$ | 0 | 40310 | 0.50 0.92 | $\mathrm{BClIS}^{\text {a }}$ | 0.13 | BCZ10 | 0.85 | BFY 37 | 0.20 |
| $2 \mathrm{N708}$ | 0.13 | 2N3709 | 0.80 | ${ }_{40316}$ | 0.92 | RC114 | 0.12 | BCZ11 | 0.50 | BFY41 | 0-43 |
| 2N 709 | 0.38 | ${ }^{2}$ N3710 | 0.80 | ${ }_{40318}^{4036}$ | 0.92 | BC115 | 0.15 | BD115 | 0.75 | BFY43 |  |
| 2N711 | 0.30 | ${ }^{2} \times 13711$ | 0.80 | 40322 | 0.92 | ${ }_{\text {BC116A }}$ | 0.18 | ${ }_{\text {BDIE1 }}$ | 0.75 | ${ }_{\text {BFY }}{ }^{\text {BF }}$ | 0.18 |
| 2N718 | 0.81 | ${ }_{2}^{2 N 3712}$ | 0.85 1.08 | 40360 | 0.48 | ${ }_{\text {BC117 }}$ | 0.21 | BD123 | 0.82 | VFY52 | 0.18 |
| 2N718A | 0.30 0.50 | $\begin{aligned} & \text { 2N3713 } \\ & \text { 2N3714 } \end{aligned}$ | 1.68 1.15 | ${ }_{40381}^{40361}$ | 0.48 | RC118 | 0.11 | BD124 | $0 \cdot 67$ | BFY53 | 0.15 |
| 2N721 | 0.55 | 2N3715 | 1.28 | ${ }_{43063}$ | 0.88 | RC119 | 0.27 | BD130 | 0.57 | BFY56 | 0.84 |
| 2N914 | 0.15 | 2N3716 | 1.30 | 40389 | 0.46 | RC121 | 0.83 | BD181 | 0.40 | BFY64 | 41 |
| 2N916 | 0.17 | 2N3773 | $2 \cdot 35$ | 40394 | 0.56 | ${ }^{\mathrm{BC1} 23}$ | 0.29 | BD132 | 0.50 | BFX75 | 20 |
| 2N938 | 0.30 | 2N3774 | $8 \cdot 38$ | 40395 | 0.50 | ${ }_{\text {BC12 }}$ | 0.15 0.20 | ${ }_{\text {BD135 }}$ | 0.48 | ${ }_{\text {BFY }}{ }^{\text {BF }}$ | . 24 |
| 2N919 | 0.20 | $2 \mathrm{~N}^{2775}$ | 4.19 | 40406 | 0.44 | ${ }_{-\mathrm{BC} 132}$ | 0.20 0.80 | BD137 | 0.55 | BFY78 | 0.36 |
| 2N929 | 0.14 | 2N3776 | $5 \cdot 95$ 4.84 | 40407 | 0.38 | ${ }_{\text {BCl34 }}$ | 0.11 | ${ }^{\text {BDD138 }}$ | 0.63 | BFY90 | 0.60 |
| ${ }_{\text {2N9 }}$ | 0.14 | 2N3777 | 2.84 | 40408 | 0.5 | BC135 | 0.11 | BD139 | 0.71 | BRY39 | 0.30 |
| 2N1091 | 0.24 | 2N3779 | 8.15 | 40409 | 0.6 | BC136 | 0.15 | BD140 | 0.88 | R8X19 | $0 \cdot 18$ |
| 2N1131 | 0.20 | 2N3780 | 4.50 | 4 | 2.00 | ${ }^{\text {BC137 }}$ | 0.15 | BDY10 | 1.25 | $\times 20$ |  |
| 2N1132 | 0.20 | 2N3781 | 8.67 | 40414 | 9.55 | BC138 | 0.20 | BDY11 | 1.60 | B8X21 |  |
| 2N1184 | 1.27 | 2N3782 | 3.87 | 40438 | 1.44 | ${ }_{\text {BCl }}$ | 0.89 0.89 | BDYY ${ }^{\text {BDY }}$ | 1.50 | ${ }^{\text {BSXX27 }}$ | -84 |
| ${ }_{2}{ }^{\text {N1302 }}$ | 0.18 | 2N3789 | 1.76 1.90 | 40467 A | 0.69 | BC142 | 0.24 | BDY19 | 1.97 | B8X28 | -25 |
| 2N1303 | 0.16 | 2N3790 | 1.90 2.06 | 40488 A | 0.44 | ${ }_{\text {BCl4 }}$ | 0.21 | BDY 20 | 0.92 | B8X29 | 0.47 |
| 2N1304 | 0.20 0.20 | ${ }_{2} \mathbf{2 N 3 7 9 1}$ | 2.06 | 40600 | 0.69 | BC144 | 0.24 | BDY38 | 0.65 | BsX 30 | $0 \cdot 68$ |
| 2N1306 | 0.22 | 2N3794 | 0.10 |  | 0.6 | BC145 | 0.21 | BDY60 | 0.80 | B8X 59 | 0.78 |
| 2N1307 | 0.22 | 2N3819 | 0.26 | 40603 | 0.58 | BC147 | 0.11 | BDY | 0.85 | B8x60 | 42 |
| 2N1303 | 0.25 | 2N3820 | 0.47 | 40604 | 0.68 | ${ }_{8 C 148}$ | 0.10 |  | 0.78 | B8X615 | 0.15 |
| 2N1309 | 0.25 | 2N3323 | 0.50 | 40836 | 1.10 | ${ }_{\text {BC153 }}$ | 0.13 0.18 | ${ }_{\text {BFF117 }}$ | 0.48 | BSX77 | 0.20 |
| 2N1483 | 0.80 | 2N3824 | 0.75 | 40673 | 0.68 | ${ }_{\text {BC154 }}$ | 0.18 | BF119 | 0.68 | Asx78 |  |
| 2N1507 | 0.24 | 2N3826 | 0.23 | AC107 | 0-35 | ${ }_{\text {BC157 }}$ | 0.14 | ${ }_{\text {BFIL }}$ | 0.25 | BSW70 | 0.28 |
| 2N1613 | 0.20 | ${ }_{2}^{2 N 3854}$ | ${ }_{0}^{0.18}$ | AC113 | $0 \cdot 18$ | BC158 | 0.13 | BF123 | 0.27 | BEY24 | 0.20 |
| 2N1631 | 0.35 0.30 | 2N3954A | 0.18 0.16 | ${ }^{\text {AClis }}$ | 0.16 0.20 | BC159 | 0.14 | BF125 | 0.25 | BSY25 | $0 \cdot 15$ |
| 2 N 1638 | 0.27 | 2 N 3855 A | 0.16 | $\mathrm{ACl27}^{\text {A }}$ | 0.20 | BC160 | 0.37 | BF127 | 0.27 | B8Y26 | 0.20 |
| 2N1671 | 1.00 | 2N3856 | 0.18 | ${ }_{\text {ACl26 }}$ | 0.20 0.20 | BC167B | 0.11 | BF152 | 0.20 | BSY27 | 0.15 |
| 2N1701 | 1.10 | 2N3856A | 0.16 | AC127 | 0.20 | BC168B | 0.18 |  | 0.2 | BSY 28 | 0.15 |
| 2N1702 | 2.15 | 2N3858 | 0.18 | ${ }_{\text {AC128 }}$ | 0.20 | $\underset{\text { BCIf }}{\text { BCOC }}$ | ${ }_{0}^{0.11}$ | ${ }_{\text {BFILS }}$ | 0.1 | ${ }_{\text {BSTY39 }}$ | ${ }_{0}^{0.15}$ |
| 2N1711 | 0.17 | ${ }_{2} \mathrm{~N}^{\text {N } 388888}$ | ${ }_{0}^{0.18}$ | AC415 | 0.30 | ${ }_{\text {BG169C }}$ | ${ }_{0}^{0.13}$ | ${ }^{\text {BF159 }}$ | ${ }_{0}^{0.27}$ | ${ }^{\text {BSY }}$ (51 | 0.25 |
| 2N1893 | 0.34 0.30 | ${ }_{2}{ }_{2} \mathrm{~N} 38859 \mathrm{~A}$ | ${ }_{0}^{0.16}$ | AC142K | 0.25 | ${ }_{\text {BC170 }}$ | 0.11 | BF160 | 0.23 | BSY52 | 0.25 |
| 2N2147 | 0.70 | 2N3860 | 0 0-16 | ${ }_{\text {ACl }}$ | 0.1 | BC171 | 0.13 | BF161 | 0.35 | BSY53 | 0.25 |
| 2N2148 | 0.60 | 2N3806 | $0 \cdot 70$ |  | 0.22 | BC172 | 0-11 | BF163 | 0.20 | RSY54 | 0.30 |
| 2N2192 | 0.40 | 2N3877 | $0 \cdot 25$ | ${ }_{\text {AClis3K }}$ | ${ }_{0.25}$ | ${ }^{\text {BC182 }}$ | 0.10 | ${ }^{\text {BF166 }}$ | 0.35 | BEY56 | 0.79 |
| 2N2192A | 0.40 | 2N3877A | 0.28 | AC154 | 0.20 | ${ }_{\text {BC182 }}$ | ${ }_{0}^{0.1}$ | ${ }^{\text {BF167 }}$ | 0.18 | B8Y65 | ${ }_{0}^{0.45}$ |
| 2N2193 | 0.40 | 2N3878 | 1.28 | ${ }_{\text {ACl7 }}{ }^{\text {a }}$ | 0.18 | ${ }_{\text {BCl83L }}$ | ${ }^{6} \cdot 09$ | ${ }_{8 F 177}$ | 0.25 | BSY79 | 0.40 |
| ${ }_{2}^{2 N} 2193 \mathrm{~A}$ | 0.42 | ${ }_{\text {2N }}$ | ${ }_{0}^{1.91}$ | AC176K | 0.20 | ${ }_{\text {BC184 }}$ | 0.11 | $3 \mathrm{BF178}$ | 0.25 | BSY790 | 0.45 |
| $\begin{aligned} & 2 N R 194 \\ & 2 N 2194 A \end{aligned}$ | 0.27 | 2N3900 2 N 3900 A | 0.20 0.21 | ${ }_{\text {ACl87K }}$ | 0.20 | BC184L | 0.11 | ${ }^{8} \mathrm{~B} 179$ | 0.80 | BSY95A | 0.09 |
| 2 N 2195 | $0 \cdot 37$ | 2N3901 | 0.32 | ${ }_{\text {ACY17 }}$ | ${ }_{0.25}^{0.26}$ | BC186 | 0.25 | BF180 | 0.35 | BU104 | 1.42 |
| 2N2195A | 0.18 | 2N3903 | 0.20 | ACY18 | 0.15 | ${ }^{\text {BC187 }}$ | 0.25 | BF181 | 0.32 | 8U105 | 5 |
| 2N2918A | $0 \cdot 30$ | 2N3904 | 0.17 | ACY19 | 0.20 | ${ }^{\mathrm{BC} 204}$ | 0.11 | ${ }_{\text {BF182 }}$ | 0.30 | ${ }^{\text {Cl }} 11$ | ${ }_{0}^{0.53}$ |
| 2N2219 | 0.37 | 2N3905 | 0.21 | Acy20 | 0.20 | $\mathrm{BC205}$ BC 206 | 0.11 | BFF184 | 0.17 | GETIII. | 0.45 |
| $2 \mathrm{~N}^{22104}$ | 0.51 | ${ }^{2 N 3406}$ | ${ }_{0}^{0.282}$ | ACY 21 | 0.18 | ${ }_{\text {BC207 }}$ | 0.10 | BF185 | 0.17 | GET113 | 0.20 |
| ${ }_{2}^{2 N} 22220$ | 0.20 0.20 | 2N4036 | 0.68 0.42 | ACY2 | 0.18 | BC208 | 0.09 | BF194 | 0.14 | GET114 | 0.20 |
| ${ }_{2} \mathrm{~N}^{2} 2221 \mathrm{~A}$ | 0.33 | ${ }_{2} \mathbf{N} 4058$ | 0.12 | $\mathrm{ACY}^{\mathrm{ACY}} \mathbf{3 0}$ | 0.18 | $\mathrm{BCP29}^{\text {b }}$ | 0.10 | Br199 | 0.15 | GET 1 | 0.50 |
| 2 N 2222 | 0.31 | 2N3059 | 0.90 | ACY39 | 0.55 | ${ }_{\text {BC2 }}$ | 0.80 | ${ }_{\text {BF196 }}$ | 0.15 | GET] | 0.35 |
| ${ }^{2 N 2922 A}$ | 0.41 | 2 N 4060 | 0.11 | ACY40 | 0.17 | ${ }_{\text {BC2 }}$ | 0.12 | ${ }_{\text {Brig8 }}$ | 0.15 | GET12 | 0.25 |
| ${ }_{2}^{2 N 2368}$ | 0.11 | 2N4061 | 0.11 | ACY41 | 0.17 | BC214L | 0.14 | BF199 | 0.18 | GET635 | 0.20 |
| 2N2369 2N2369A | ${ }_{0}^{0.39}$ | ${ }^{2 N} 4062 \mathrm{~N}$ | 0.11 | ACY44 | ${ }_{0}^{0.31}$ | BC236 | 0.16 | BF200 | 0.85 | QET53 | 0.20 |
| ${ }_{2} \mathrm{~N}_{2646}$ | 0.41 | 2N4303 | 0.32 | ${ }_{\text {ADI }}{ }^{\text {AD }} 140$ | 0.98 0.50 | ${ }^{\text {BCP237 }}$ | 0.09 | ${ }^{\text {BF224J }}$ | 0.14 | (7ET53 | 0.20 |
| 2N2647 | 1.20 | 2N4913 | 0.80 | AD140 | 0.55 | ${ }_{8}$ | 0.09 0.09 | ${ }_{\text {BF235J }}$ | 0.19 | GRT87 | 0.12 |
| 2N2741 | ${ }^{0.12}$ | 2N4914 | 0.87 | $\mathrm{AD} 142^{\text {d }}$ | 0.50 | ${ }_{\text {BC251 }}$ | 0.20 | ${ }_{\text {BF238 }}$ | 0.22 | GET880 | 0.30 |
| - 2N2712 | 0.12 | 2N4915 | 0.95 | AD143 | 0.45 | ${ }_{\text {BC252 }}$ | 0.18 | B ${ }^{\text {2 }} 244$ | 0.16 | GET883 | 0.20 |
| 2N2713 2N2714 | ${ }_{0}^{0.17}$ | ${ }_{2}^{2 N 4916}$ | 0.11 0.17 | ${ }^{\text {AD1 }}$ A 149 V | 0.66 1.26 | ${ }^{\text {RC25 }}$ | 0.23 | ${ }_{\text {BF } 245}$ | 0.83 | GET887 | 0.20 |
| $2 \times 2904$ | 0.18 | 2N4918 | 0.50 | AD150 | ${ }_{0}^{1.63}$ | ${ }^{3 C 257}$ | 0.09 0.09 | $\mathrm{BF} 246^{\text {BF247 }}$ | 0.43 | GET88 | 0.22 |
| 2 N 2904 A | 0.25 | 2N4919 | 0.53 | AD161 | 0.37 | BC258 BC259 | ${ }_{0}^{0.09}$ | BF247 | 0.48 0.14 | GET | 0.25 |
| 2N2905 | 0.26 | 2N4920 | 0.60 | AD162 | 0.37 | ${ }^{\text {BC2681 }}$ | 0.20 | BF254 | 0.14 |  |  |
| 2N2905A | 0.23 | 2N4941 | 0.50 | AD161 | PR | ${ }^{\text {BC262 }}$ | ${ }_{0}^{0.18}$ | BF255 | 0.15 | RET | R |
| 2N2906 | 0.18 | ${ }^{2 N} 492 \mathrm{~L}$ | 0.55 | AD162 $\}$ | 0.69 | ${ }_{\mathrm{BC} 263}$ | ${ }_{0}^{0.28}$ | BF257 | 0.41 |  |  |
| 2N2906A | - 0.28 | 2N4923 | 0.60 0.90 | ADZ11 | 1.50 | ${ }^{\text {BC3 }}$ O 0 | 0.42 | BF258 | 0.48 |  |  |
| 2N2907 | 0.18 | 2N4926 | 1.00 | ${ }_{\text {AP106 }}$ | 1.75 0.27 | BC. 01 | 0.34 | BF259 | 0.48 |  |  |
| 2N2907A | - 0.25 | 2N4928 | 1.80 | ${ }_{\text {A A }}{ }^{\text {A } 1096}$ | 0.27 0.40 | BC302 | 0.27 | BF261 | 0.23 |  |  |
| 2N2913 | 0.75 | 2 N 4949 | 2.23 | ${ }^{\text {AF }}$ F114 ${ }^{\text {a }}$ | 0.25 | RC303 | 0.54 | BF264 | 1.45 | E | C |
| 2N2923 | 0.12 | 2N4930 | 2 | AF115 | 0.24 | BC304 | 0.43 | BF270 | 0.25 |  |  |



## PART TWO

## PREAMPLIFIER

Construction is on the same lines as the driver amplifier, on a group board with common earth busbar, and is shown for one channel, Fig. 6a and circuit diagram Fig. 6b. Decoupling components R10, R24 and C2 and C12 are common to both channels. Screened leads are used from the input sockets to the selector switch, and from the switch to the input tags and also from the volume control to the driver amp inputs. The switch wiring is shown in Fig. 7a. Note that the equalising components are mounted directly on the switch (Sections c and d).

It is at the input sockets where the only earth connections to chassis are made (apart from mains earth) this is important as hum and distortion can easily occur if earth loops are formed by connecting more than one point to the chassis.
The modular construction of the preamp with its earth bus-bar ensures that its own earth returns are all common to itself. (This applies also to the driver module.)
It will be seen that the chassis earth at the input is carried via the screened leads to the preamp, and then to the earthy side of the volume control, thence to the driver amp, through to the common point on the power supply, where the return from the power amps via the speakers are also returned. This is made clear in the layout drawing Fig. 8. The preamplifier has a number of connections to the controls, and it will be found easiest to solder connecting wires in place on the module before fitting to
chassis. Leads of different colours would be a further aid. The leads should then be trimmed to length and taken to their control terminations in pairs. Driver and power amplifier can be treated in a similar manner.

Note that with all the transistors, the collector and case are common, so care must be taken to ensure that the case does not come in contact with other component or earth connections.

Output sockets for "Record" can be fitted if required. These are fed from each channel via a $100 \mathrm{k} \Omega$ resistor from the negative side of C 7 , and will provide a signal of 100 mV at high impedance, or 1 mV per $1 \mathrm{k} \Omega$ for impedances less than $100 \mathrm{k} \Omega$. Connections are shown in Fig. 6b.


Fig. 6a: The wiring of the preamplifier section, only the components for the R.H. channel are shown; those for the other are mounted on the other side of the board and on the rear section of the pots.


Fig. 6b: The circuit of one channel of the preamplifler. The decoupling components in the positive line are common to both channels.


Fig. 7a: The wiring of the selector switch S1.

If the gram input is intended for a ceramic cartridge, this input must be attenuated with a divider of $33 \mathrm{k} \Omega$ and $6.8 \mathrm{k} \Omega$, in the same manner as the radio and tape inputs. This will provide a sensitivity of 100 mV and loading to give the pickup similar characteristics to a magnetic type, to suit the equalisation.

If the radio or tape recorder to be used is mono only, the appropriate input sockets should be linked together so that the single input plug is connected to both channels.

fig. $7 b$ (/eft): The circuit of the input selector section.
Fig. 7c (right): Modification for a ceramic pickup.


Fig. 8: The general layout showing the connection of the earth line to

## POWER SUPPLY

The layout and circuit diagram are shown in Fig. 9 and need little comment. The rectifiers are "tophat" types mounted on a piece of $1 \mathrm{in} . \times{ }^{1}{ }_{2} \mathrm{in}$. paxolin. A 2A bridge rectifier can be used here if desired; the symbols shown correspond to the bridge connections.

Capacitors C18 and 19 are held in place with an aluminium strip, to which the fuseholders are also secured.

The mains earth can be made to any convenient chassis point. A useful addition would be a 2 -pin mains outlet on the rear panel to feed the gram motor or other ancillary equipment. This would be taken from the 240 V connections on the mains transformer, to operate via the amplifier on-off switch. Note that the earth connections to any ancillary equipment comes automatically from the amplifier, and should not be connected to a separate mains earth, which would invariably result in excessive hum.

## TESTING

Switching on any equipment for the first time always gives one a little concern, wondering if a mistake has been made somewhere, and if something is going to blow up, knowing that fuses do not always blow quickly enough to prevent damage.

Anyone feeling this concern can alleviate it in this case, simply by removing the fuses, and soldering 0.5 W resistors of $4 \cdot 7 \Omega$ to $10 \Omega$ in their place. Switch on; the resistors will only become warm, particularly the one in the positive line, if everything is well, but will immediately burn if a serious fault exists. One can then switch off before any damage is done, locate the fault and try again, replacing the fuses when satisfied that all is well.

A check can now be made on the voltage readings, starting at the fuses and working forward. The voltages shown are approximate, small variations can occur due to component and transistor tolerances. During this check the volume control should be at minimum, and resistors of $15 \Omega$ (or thereabouts) connected in place of each speaker. The resistors need only be ${ }^{1} 2 \mathrm{~W}$ or 1 W as the amplifier is not delivering any power (or shouldn't be).

Switch the meter to a.c. (25V) and check that no voltage appears across the speaker sockets at any position of the volume control, tone controls, and selector switch. An a.c. reading of $10-15 \mathrm{~V}$ would indicate r.f. instability, and the resistor across the speaker sockets would overheat. This would only occur if the layout or wiring differed from that shown


Fig. 9a: The circuit of the power supply.


Fig. 9b: The layout of the power supply.

to create stray coupling and hence r.f. feedback. The cure would be to connect a by-pass capacitor of $100-250 \mathrm{pF}$ from collector of $\operatorname{Tr} 2$ to $\operatorname{Tr} 3$ to chassis.

The amplifier is now ready to go, and speakers and inputs can be safely connected. Choosing loudspeakers and a record player deck can present a problem to some people. The short answer is to pay as much as one can afford.

# raaticially wirless commenavaratiENiY 

THE nearest approach Henry ever made to the Grim Reaper-in the course of duty-was when some well-meaning idiot omitted to remove the short-circuit from the safety switch of the supply unit of a high-powered transmitter

True, it was impossible to work on the Army's ' 10 -set' once any of the rack-mounted units had been slid from its rails. A link of wire across the safety-switch contacts became routine test procedure. But lying there, while the petrol-driven generator pumped futile fumes across Breedon Moor, and the Naafi wagon was miles away was no recommendation, for a trust in protective devices.

Hence, perhaps, my present suspicion that regulation, control and 'protection', when not forced upon an electronics manufacturer by

"Oh, but it shouidn't!" cry the makers. law, is usually a kind of gimmick, spawned from convenience, nurtured in wrath, weaned by ingenuity and matured in advertisement.

In particular, the curious convolutions of audio circuit producers (not designers, for Henry is painfully aware that these gentlemen languish in a limbo, surveying the prostitution of their ideas by the pimps of commercialism) result in tinselly circuits with curious protection gadgets, tweaked to safeguard the precious output devices against the ham-
fisted handling of the common herd. It causes a budding circuit maker to wonder where expediency leaves off and practicality takes over.

Often quite passable output stages are ruined by utter instability when the supply voltage wanders a touch or two. 'Oh, but it shouldn't', cry the makers. 'The British mains supply system is the best in the world.'
O.K. Henry goes along with that. But, even so, when, on Sunday morning, all the pinafored aspirants to Womens Lib are chickening in; or on Saturday evenings, when the great British publick (sorry, public) is tuning in to David Coleman and that travesty of human behaviour we laughingly call 'Sport'; then, and during those episodes of televisual dramuck that bring a paler shade of Whitehouse to the cheek, the mains supply voltage drops to a level where a Tandberg tape recorder refuses to rewind, a Quad amplifier forgets its steep transfer curve has certain advantages and ninety-nine from a hundred average radios rampage into avid crossover distortion.

For some reason connected with out insular arrogance, British designers expunge the idea of true regulation, protection and control. At the very least, we find a series regulator in the American (well then, Japanese) importations.

Henry is always amused by those models with cut-outs, which pop off dramatically when the impedances of loudspeakers (usually Scandinavian in origin) hit them below the belt. There are others, more genteel, which choke themselves into silence with a strangulated burp, waiting for you to light a cigarette, apologise to the dollybird you were hoping to impress, and switch on againhoping the fault has now disappeared.

Protection circuits, per se, bring trouble. For every attempt by a well-meaning designer to cherish
his brain-child, there will be one or two electronic catastropes.

For protection in excelcis we turn to the Whichdogs of the Consumer Council (past, present or future-what's in a name?) and some Naderish fumings from across the Atlantic. If you spent an evening, or, God Help You, a cocktail half-hour, in the presence of George Darling, M.P., who steered the Trades Description Act through Parliament, you

would come away believing that every maker of electronic equipment conspires to do you down.

I don't think that is quite true. Seems more like the maker of electronic equipment fearing the user will do him down. Why else would Sony label their cassette cutout feeler a 'miserase protecting lever'?
There's a famous amplifier with a delicious FET protection circuit, with a diode from gate to source. The driver stage is wonderfully protected, yes? But when things go wrong, the mid-rail flies up to 55 volts and that driver is only rated at 40 V . It goes up in smoke, taking its 47 -ohms emitter resistor with it, and often the 2 N3055 output transistor as well.

It's about time we constructors - were protected from the misborn circuitry and afterthought mods of manufacturers. What about it lads? Join UPESCO-the Union for the Protection and Encouragement of Suffering Constructors.


ACRYSTAL marker is used to calibrate receivers, signal generators, transmitter v.f.o.'s and similar equipment or to check their calibration. The marker described here is self-contained and requires few components. Details of typical uses are given later.

## CIRCUIT

Fig. 1 is the circuit, the single BFY51 transistor operating as a crystal controlled oscillator having three fundamental frequencies selected by a 3-pole 4 -way switch. Sla and Slb select one of the three crystals; $100 \mathrm{kHz}, 1 \mathrm{MHz}$ or $3 \cdot 5 \mathrm{MHz}$. The remaining switch position is "Off."

When the 100 kHz crystal is in use C2 is across L 1 , and the core is adjusted to approximately this frequency. For the higher frequency crystals C2 is not connected, the windings of Ll acting as an r.f. choke. Output is taken from a coupling winding and isolating capacitor C3.

With the unit operating at 100 kHz this frequency and its harmonics or multiples will be heard on a receiver. Harmonics such as $500,600,700 \mathrm{kHz}$ up to

1500 kHz allow easy calibration of a receiver or tunable signal generator in the medium wave band.

Higher harmonics of this frequency are used for general short wave calibration, or the calibration of a transmitter v.f.o. For example, 1.8, 1.9 and $2 \cdot 0 \mathrm{MHz}$ harmonics for Top Band and $3 \cdot 5,3 \cdot 6,3 \cdot 7$ and $3 \cdot 8 \mathrm{MHz}$ for the 80 m band.

When tuning, especially on higher frequencies, a quick indication of 1 MHz points is useful and harmonics of the 1 MHz crystal will be found at multiples of this frequency- $2,3,4,5 \mathrm{MHz}$ and so on.

For amateur band reception, in particular, a bandedge crystal is extremely useful. That fitted here is $3 \cdot 5 \mathrm{MHz}$, its. harmonics appearing at $7 \cdot 0,14 \cdot 0,21 \cdot 0$ and $28 \cdot 0 \mathrm{MHz}$ as well as the fundamental at $3 \cdot 5 \mathrm{MHz}$ and harmonics $10.5,17.5$ and 24.5 MHz which are, of course, remote from amateur bands.

## CONSTRUCTION

A piece of sheet aluminium $5 \times 4 \mathrm{in}$. is bent as in Fig.2. The whole unit is assembled on this and will afterwards fit in a plastic box approximately $51_{2} \mathrm{x}$ $3 \times 2^{3}{ }_{8} \mathrm{in}$.


Fig. 1: Circuit diagram of the crystal marker.

Crystal holders to suit the particular crystals used are bolted as in Fig.2. The box lid is also drilled for the switch, output socket and a small bolt to hold a battery clamp. Heavy pressure during drilling may crack the plastic, so a little care is required.
The transistor and most other small components are supported by soldering their leads directly on to the switch tags. Run leads X-X down through a hole to one crystal holder, leads Y-Y to the second holder and connect Z-Z similarly to the remaining holder. A card marked with the switch positions is placed between the case top and metal panel and held together by the switch nut and output socket. A hole is drilled to fix a piece of metal shaped to secure the 9 V battery to the left of the switch.


Fig. 2 : Layout of components on chassis with details of switch connections.

## $\star$ components list

| Resistors |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| R1 270ks |  |  | $47 \mathrm{k} \Omega$ | 10\% |
| Capacitors |  |  |  |  |
| C1 350pF |  | $1200 p F$ | C3 | 22pF |
| Crystals |  |  |  |  |
| $100 \mathrm{kHz}, 1 \mathrm{MHz}$ and 3.5 MHz surplus types with holders to suit. |  |  |  |  |
| Miscellaneous |  |  |  |  |
| Tri, BFY51. L1, 'Yellow" Range 1 (Denco valve type), |  |  |  |  |
| S1, 3 -pole, 4 way wafer switch. Aluminium $5 \times 4$ in. |  |  |  |  |
| Plastic box $5 \frac{1}{2} \times 3 \times 2 \frac{3}{8} \mathrm{in}$. approx. Knob. Insulated socket. |  |  |  |  |
| Battery 9V with terminal clips. |  |  |  |  |

## ADJUSTMENT

Rotation of the core of L1 allows the second harmonic of 100 kHz crystal to be moved slightly in frequency to secure zero beat with the BBC on 200 kHz or MSF on 2.5 or 5 MHz . When the marker signal and received transmission are about the same strength, the frequency error of the harmonic will be heard as a low pitched growl, falling to a repetitive swishing sound, or flutter, or seen as a rise and fall of the receiver tuning meter, as the error is reduced. In any case at frequences of 1 MHz and higher the error will be only a few parts in a million and accuracy is higher than necessary for any ordinary purpose.

## IN USE

The output can be coupled to a receiver by a short lead plugged into the socket and placed near the receiver, or near a short wire in the receiver aerial socket or plugged into the receiver, depending on the


Another view of the crystal marker. The transistor is wired directly on to the switch tags.
strength required. Harmonics grow progressively weaker and the limit to which they can be detected depends on receiver sensitivity. The marker signal is unmodulated, so the receiver b.f.c. should be on and set to zero.
To calibrate a tunable generator or v.f.o., couple its output to the receiver and tune the v.f.o. or generator to zero beat with the appropriate crystal harmonic. The receiver is tuned to the wanted frequency, but receiver tuning has no effect on calibration in this case. The b.f.o. is not in use in this instance.

VFO calibration at 50 kHz points can be achieved by tuning the receiver to the second harmonic of the v.f.o., and 100 kHz points provided by the crystal will then fall at 50 kHz points on the v.f.o. scale. The 10 kHz points can be estimated from the v.f.o. scale.

Harmonics can be used to adjust r.f., mixer or i.f. stages for best results, using a meter to read cathode or emitter current of an a.g.c. controlled stage. <br> \title{
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## inside


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THIS receiver features modular construction, easy accessibility of units, and complete coverage from 150 kHz to 30 MHz . It will thus provide reception on long, medium and all the short wave bands from about 200 to 10 metres.

To facilitate construction, wiring and testing the receiver is built as three units-a mixer-oscillator assembly using a dual-gate field effect transistor mixer with separate f.e.t. oscillator; a high gain 2-transistor intermediate frequency amplifier; and a 4-transistor audio amplifier and output section. These units are then assembled into a case which carries the panel and a chassis with coils, etc.

## MIXER-OSCILLATOR

The circuit for this unit is shown in Fig. l. Tre, a $3 N 141$, is the mixer, with the signal fed to G1 and oscillator input to G2. Output from this stage is from the drain to the lst i.f.t. of the i.f. unit.

Tr2, an MPF102, is the oscillator with injection to G2 of the mixer via C4. The feedback windings $8-9$ of the oscillator coil L2 provide feedback from the drain to the gate of Tr2, to enable this stage to oscillate.

Coils are fitted in pairs, "Blue" in the Ll position and "Red" for L2. Coverage is approximately as follows:

| Range 1 | $150-500 \mathrm{kHz}$ | $2000-750$ metres |
| :--- | :--- | :--- |
| Range 2 | $515-1545 \mathrm{kHz}$ | $580-194$ metres |
| Range 3 | $1 \cdot 67-5 \cdot 3 \mathrm{MHz}$ | $180-57$ metres |
| Range 4 | $5-15 \mathrm{MHz}$ | $60-20$ metres |
| Range 5 | $10 \cdot 5-31 \cdot 5 \mathrm{MHz}$ | $28-9 \cdot 5$ metres |

Range 1 is for long waves, but in this circuit the i.f. is 470 kHz so coverage has had to be curtailed from that listed above or instability arises at the h.f. end of this band. This is easily done by marking the scale for Range 1 to suit. An alternative is to solder


4 Fig. 1: Circuit of the mixer-oscillator board.


a 50 pF capacitor directly across the tuned section of Range 1 coils. Such capacitors must not be fitted at the holder because of their effect on other ranges.

Range 2 is for medium waves, while the remaining ranges are for the higher frequencies. Actual coverage can be modified somewhat by adjusting the cores.

Plug-in coils as used at L1 for aerial tuning and at L2 for the oscillator have several advantages. Construction and wiring are simplified when compared with the permanent fitting of all coils and a multiway bandswitch. With plug-in coils, it is also a simple matter to obtain only those coils for the bands required. Coils for other bands can always be obtained later and no changes have to be made to the receiver to allow them to be used.

A panel aerial trimmer VC2 is fitted which has the advantage that the aerial circuit can be peaked up for best results with any aerial, on any frequency. Tuning on the higher frequencies becomes critical, so the bandspreading capacitor VC4 is provided for fine tuning. No additional bandspreading capacitor is necessary for the aerial coils.

Ranges 1, 2, 3 and 4 have their own oscillator coil padders, 110 pF for Range 1, 350 pF for Range 2, 1100 pF for Range 3 , and 3000 pF for Range 4. No padder is used for Range 5. These padders go respectively to tags $5,2,3,4$ and 6, as in Fig. 1. The coils are so made that the correct padder is automatically in circuit when a coil is inserted.

## IF AMPLIFIER

Fig. 2 shows the intermediate frequency amplifier which has two double-tuned i.f.t.'s and one single tuned i.f.t. This results in good selectivity and gain.

Diode D1 is the demodulator which also provides automatic gain control bias through R2 for Tr1. Audio signals are taken from the volume control VR1 to the a.f. amplifier.


A Fig. 2: Intermediate frequency amplifier circuit.
A Fig. 3: Circuit of the audio amplifier and output stages.


Fig. 4: Layout of the mixer-oscillator board and wiring of padding capacitors.


Fig. 5: Underside wiring of board shown in Fig. 4.

## AF AMPLIFIER

The circuit for this section is shown in Fig. 3. Tr1 is the 1st a.f. amplifier, followed by the driver Tr2. The driver transformer Tl couples to the push-pull output pair $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$ and T 2 is the output transformer for a 2 or 3 -ohm speaker. The pre-set R12 is adjusted for proper operating conditions in the output stage.

This type of circuit gives plenty of amplification and output. Its great advantage lies in the fact that the d.c. operating conditions of each stage are isolated from other stages, so it is not necessary to use matched sets of transistors. Some simplification would be possible by omitting $\operatorname{Tr} 1$ and taking C 1 to the base of $\operatorname{Tr} 2$, though the extra stage of amplification is useful with weak signals.

## MIXER-OSC BOARD

This section is wired on a piece of plain Veroboard $2 \times 1^{3}{ }_{4} \mathrm{in}$. Do not remove the shorting ring from Trl until the transistor is fitted in the way explained.

Two ${ }^{1} 2$ in. 6BA bolts with tags are secured in the positions in Figs. 4 and 5. Extra nuts on these space the board from the metal chassis to clear wiring. These bolts also provide a chassis return when the board is fixed to the chassis.

Resistors and capacitors are positioned as in Fig. 4. The board is turned over and wired as in Fig. 5. Place sleeving on leads where necessary. Veropins can be inserted for external connections, or flying leads can be left for this purpose and cut down to length later. Leads run from Cl to pin 6 of L1, from Trl drain to pin 1 of i.f.t.1, from C6 to pins 1 and 7 of L2, from $\operatorname{Tr} 2$ drain to pin 8 on L2 and from C 3 and R4 to pin 9 on L2. These pins or leads are identified by locating them as in Fig. 4. A pin or black lead is also required for the negative connection, which runs to a pin provided on the i.f. board.

Tr1. This should be supplied with a shorting collar, spring or ring, which is left in position until $\operatorname{Tr} 1$ is fitted. With an insulated gate transistor, static charges from the fingers, or a metal or plastic tool, can damage the unprotected transistor. Spread the wires with a matchstick or piece of wood so that they can be inserted in the holes shown in Figs. 4 and 5. Solder drain and source leads. Solder the G1 lead by keeping the iron in contact with the Rl side of the joint, and the G2 lead by keeping the iron against the R2 side of the joint.

Once the transistor is fitted, it is protected by R1, R2 and R3, and the shorting spring can be pulled off. If it is necessary to unsolder this transistor, bind thin wire round the leads in advance. Do not touch the


General view of completed receiver with metal strap fitted to lift front edge.
unprotected G1 or G2 wires with the soldering iron, fingers or metal plastic tools.

Tr2. This transistor can be soldered in the usual way. A 3-lead holder was fitted for it primarily as a simple means of testing various transistors in the oscillator position.

When this section is finished, it is fixed with extra nuts as in Fig. 4, and the leads for Li and L2 are cut and soldered. The ${ }^{1} 2 \mathrm{in}$. bolts should leave enough clearance between the chassis and joints, but a piece of card or other insulating material about $2 \times 1^{3} 4$ in. in size can be put under the board.

Fig. 4 also shows how the padders are wired. Do not forget the lead 6 to chassis for Range 5. Leads from pin 8, Ll and the chassis run to sockets at the back of the case for aerial and earth.

## IF AMPLIFIER BOARD

This is $37_{8} \times 13_{4}$ in. and the components are placed as in Fig. 6. Holes are drilled for the pins and screening can tags of the i.f.t.'s with a central hole so that the lower cores can be reached with an adjusting tool. A very small round file is useful here if some of the holes are not in quite the correct positions.

Two bolts MC with tags are fitted in the same way as with the mixer-oscillator board, to mount the i.f. amplifier and provide the positive chassis return.

When fitting the transistors bring them down to within about $3_{8} \mathrm{in}$. of the board so that leads are reasonably short. Wires can be identified and short circuits prevented by putting $3_{8}$ in. .pieces of sleeving on them-green for emitter, blue for base and red for collector. Connections underneath are shown in Fig. 7. It may be found helpful to put red sleeving on positive circuits, black on negative circuits and some other colour on other wires.

Pins are inserted for the external connectionsnegative supply from R1 to the mixer-oscillator; mixer to i.f.t.l, pin 1; from R7 to negative on the a.f. amplifier and battery; and from D1 positive to VR1.

The i.f. amplifier is fixed $3_{4}{ }_{4} \mathrm{in}$. from the end of the chassis, level with the back of the chassis, with i.f.t. 1 towards the mixer-oscillator section. Fig. 4 is the underside of the chassis, but i.f. and a.f. sections are on top of the chassis.


View of receiver with sides and back removed to show placement of the i.f. and audio boards.


Fig. 6: Layout of components on the lif. amplifler board and lead-out connections for the AF117 transistors.

Fig. 7: Wiring details under the i.f. amplifier board. Points marked MC are the bolts fixing the board to the chassis.


## AF AMPLIFIER BOARD

Components are placed as in Fig. 8, using a board $3^{3}{ }_{4} \times{ }^{1}{ }^{1}{ }_{4} \mathrm{in}$. in size. Bolts with tags are again used for chassis return and mounting with pins fitted for the junction of R1 with C1, for battery negative and for leads which will run from the secondary of the output transformer T2 to the loudspeaker.
Wiring should be straightforward as shown in Fig. 9. Coloured sleeving can be used to identify transistor and other leads, as already mentioned.

When this board is complete, it can be mounted in the space to the right of the chassis. Joints must be clear of the metal, or protection provided against shorts by placing card under the board, as described earlier.

## CHECKING THE AF

The a.f. section may be checked by connecting a loudspeaker and providing a signal to R1 from a radio tuner, audio oscillator, pick-up or other source. VR1 should be in circuit to avoid overloading.
Initially set R12 so that little resistance is in circuit. With a 9 V battery connected and the amplifier working, increase the value of R12 by moving the slider until the current is some 8 mA to 10 mA or so with no signal. Current peaks will be very much higher than this, increasing as the volume is increased.

Alternatively, R12 can be set to a position which results in clear reproduction with plenty of volume, though battery drain is increased if R12 is too high in value.

## IF ALIGNMENT

The i.f. amplifier can be checked and aligned by itself or in conjunction with the a.f. section. VR1 must be connected and R1 of the a.f. section is connected to VR1; or phones may be connected to VR1, with an isolating capacitor in one lead to avoid upsetting the a.g.c. circuit.
As the i.f.t.'s are supplied pre-aligned, only a little adjustment of the cores should be necessary. If a signal is being obtained from the mixer-oscillator section, tune in a medium wave BBC or other stable transmission. Keep signal strength low by using a short piece of wire as an aerial, or by looping an insulated wire round the lead from pin 8 of L1. A proper tool is then used to rotate each core in turn, for best results. VR1 should be at maximum. A strong signal is avoided because it will operate the a.g.c. circuit and so make the correct core settings less precise. In any case, little or no adjustment of the cores may be needed, as explained.

If a signal generator is used, proceed in the same way, but couple the generator to the primary of i.f.t. 1 by placing an insulated lead near pins 2 or 3 . In this case, the mixer-oscillator section need not be in use.

## components list




Fig. 8: Components on the audio stages board are placed as shown. Observe correct polarity of the several electrolytic capacitors.

Fig. 9: Wiring underneath the audio amplifler board. Again points MC are 'earth' returns, via the fixing bolts, to the chassis.


## MIXER-OSC ADJUSTMENT

The mixer-oscillator is most easily tested and aligned when the receiver is otherwise completed. The coil adjusting screws are screwed in by the makers so that the coils can be placed in the cans in which they are supplied so initially all the cores have to be unscrewed several turns from this position.

Deal with each pair of coils separately. The cores can be locked with 6BA nuts when they are correctly adjusted.

Band coverage at the low frequency end of the band is adjusted by moving the core of L2. The core of Ll is adjusted so that near the low frequency end of the band signals peak up with VC2 nearly half closed. In these circumstances, it should be found that VC2 can be peaked for best results throughout the whole band. If it becomes necessary to close VC2 more and more, as the receiver is tuned from the h.f. end of the band towards the l.f. end, this shows that the core of L1 needs screwing in slightly. On the other hand, if when tuning in this way VC2 has to be opened more and more for best results, the core of Ll is too far in.

With the tuning capacitor VC1/3 fully closed, the frequency reached is lowered by screwing in the core of L2 and raised by unscrewing this core. This allows ranges to be adjusted so that there is some overlap between bands. A corresponding adjustment has to be made to the core of L1.

It should be found that alignment is not difficult, either by tuning in transmissions, or by using a signal generator. Maximum results will in any case be obtained if VC2 can be peaked for best volume throughout the whole of any range and is then seen not to be either fully open or fully closed.

R 4 on $\operatorname{Tr} 2$ is the lowest value which does not result in strong spurious oscillations marring reception. The best value depends somewhat on $\operatorname{Tr} 2$ and is likely to be between about $1 \cdot 2 \mathrm{k} \Omega$ and $8 \cdot 2 \mathrm{k} \Omega$.

## CASE ASSEMBLY

Three $10 \times 4 i n$. flanged universal chassis members are used, one as the case front, one as the back and the third as a chassis to carry the three circuit boards and coil holders.

The sides are 3 -ply, sanded and varnished, each $7^{1}{ }_{2} \times 4^{1}{ }_{2}$ in. The top is similar 3 -ply, $10 \times 7^{1}{ }_{2}$ in. while the bottom is $10 \times 7 \mathrm{in}$.

A piece of $1_{8}$ in. perspex, $10 \times 4 \mathrm{in}$. backed by card, except for a window over the tuning scales, is also required for the front.

Fig. 10 shows how the case is assembled. Mark through the holes punched in the flanges of the $10 \times 4$ in. members so that the wooden sides can be drilled. The back is flush. The 10 x 4 in . member forming the chassis is set forward about $7_{8} \mathrm{in}$. and is $1^{3}{ }_{8} \mathrm{in}$. above the lower edge of the back so that there is clearance for the mixer-oscillator board below, as well as for VCl/3 above.


Fig. 10: Positioning of the major components on the chassis and front panel with details of the dial drive mechanism

The front is set in lin. from the front edges of the side pieces as in Fig. 10. Drill the front for VC4, VC2, VR1 and the cord drive bush. Mark the same hole positions on the perspex, and drill clearance holes for the operating spindles. Also drill four holes to match with those punched in the front near the flanges.

When assembly is otherwise complete, the perspex is put in place and held with four lin. 6BA bolts, each with three nuts, so that it covers the drum and cord drive. A piece of card, with a cut-out through which the scales can be seen, fits behind the perspex.

Drill the front for VC1/3, fixing this with countersunk head 4BA bolts with extra nuts or spacers behind. The two wheels for the cord run on bolts as in Fig. 10. The cord has one complete turn round the driving spindle and is held taut by the spring in the drum.

The card for the scales is brought forward by means of a piece of wood about ${ }_{4}$ in. thick fixed to the $10 \times 4$ in. member. A small piece of tinplace is cut and folded so that it can be clipped to the cord with pliers and a vertical wire pointer is soldered to this, the pointer and drum being as shown in Fig. 10 with the ganged capacitor fully closed.

The receiver can be wired and tested with the back, top and bottom completely removed, so that all units can be reached easily. The bottom is attached with three or four self-tapping screws. The top requires to be hinged, or provided with strips to hold it in place, so that it can be lifted off the case to change coils.

## CALIBRATION

Markings are made before fitting the perspex. If the scales are to be calibrated in frequency first check coverage and ganging and fix the coil cores with 6BA nuts. Calibration is then most easily done


The markings of the four controls and dial calibration can be seen in this view of the receiver.
with a signal generator. This is set to various frequencies, the signal is tuned in on the receiver, and the appropriale scale is marked. Take care to avoid harmonics and second-channel responses, in the usual way.

An alternative is to tune in various bands, such as 19 or 31 metres, and mark these. Another possibility is to fit a $0-100$ or similar horizontal scale, against which stations tuned in, or known frequencies can be logged. A rule calibrated in mm . will act as an easily obtainable ready-made scale.


Only the mixer-oscillator board and associated coil holders are mounted underneath the chassis.

## AERIAL AND EARTH

Remember that conditions on the various frequencies vary enormously according to the time of day and other factors. Quite a large number of transmissions should be received with some 5 ft . to 20 ft or so of wire as an indoor or outdoor aerial. For weak signals in the $1 \cdot 5-5 \mathrm{MHz}$ region, a longer aerial will make a great difference by improving signal strength. For good results on these frequencies, some 50 ft . to 150 ft . or so of wire as high as possible and clear of earthed objects, can be worth while.

Though many signals are sufficiently strong with no earth the use of an earth connection will give a worthwhile improvement in volume on some frequencies and often allow the reception of weak signals which cannot otherwise be received. An earth lead can be an insulated wire taken to an earth spike or other metal object buried in the ground. Where this is impossible, a counterpoise earth consisting of an insulated wire running near the ground or in an opposite direction to the aerial can be helpful.

## ISSUES WANTED

P.E. Aug. 1965, Sept. 1966. Nov., Dec., 1698, Jan., Feh., April, June, Aug., Sept., Oct., Nov. 1969. P.W. Jan., Feb,, Mar. 1967.-A. G. Hodgett, 3, Ely Way, Fellgate, Jarrow, Co. Durham Feligate, Marrow, May 1972.-G. Barraclough. Rustic Gables, Waterhill Lane, Sowerby Bridge, HX62UA.
Jun., Feb., Aug., 1970;-Dec. 71;-July 1972; of P.W. Nov. 1969;-Sept. 70:-
July 1972, P. E. Juty 72 :-E.E.-G. D. Llody, 28 Underhill, Bolham Road, Riverton July 1972, P. E. duty' 72 :-E.E.-G. D. Llody, 28 Underhill, Bolham Road, Riverton evon. EX166SF.
..buy, loan, exchange P.W. April, May, June, 1969-W. L. Brunsdon, 28 Meadfoot Road, Wallasey, Wirral, Cheshire.
. wanted-March \& April 1970 to P.W. containing articles on 'General Coverage RX' buy or loan.-C. MacAddhabhui, Machaire Gathlan, Derrybeg, Co. Donegal, Ireland . November 1971 edn. 'Everyday Electronics' Cover price and postage paid, C. Rickard, 10, Berridge Road, Sheerness, Kent. P. W. Nov. 1

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. a circuit for the construction of a simple musical rhythm unit.-G. Smith, 13 Dean Park Road, Plymstock, Piymouth, PL97NY
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## TELEVISION

## FEBRUARY ISSUE

## ASSESSING RECEIVER PERFORMANCE

How good is your set and how do you go about assessing the quality of the picture? This month we start a new series on subjective performance testing, i.e. without the need to use any test equipment.

## CRT REJUVENATOR

This simple item costs very little to build but saves pounds by prolonging the life of old tubes-cathode reactivation can often in fact be a case of new tubes from old!

## SHORT BACK-FIRE AERIAL

Here's a new one for aerial constructor enthusiasts to try out! Reg Roper reports on the excellent results he obtained recently using this type of aerial.

## SERVICING TV RECEIVERS

In response to many requests, this month L. LawryJohns deals with the Philips T-Vette/Stella Companion mains-battery transistor portables.

PLUS ALL THE REGULAR FEATURES
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# Power for Ever! 9V BATTERY ELIMIINATOR <br> <br> M.WALLIS <br> <br> M.WALLIS <br> HAVE you ever worked out how much it costs you using batteries rather than the mains supply for operating your equipment? Obviously it depends on the type of battery you use, what current you are drawing and how often the <br>  

equipment is used but a quick calculation shows that the current costs about 2,000 times as much as operating through a power supply. Certainly a power supply costs rather more than a battery but this is rapidly recovered by savings in battery costs.

The unit described here is a replacement for the popular PP9 type of battery that is fitted in a number of the larger types of transistor portable radios. This battery is also very popular with amateur constructors. Although designed to replace the PP9 type, the circuit of course holds good for any 9 V battery with a maximum current supply of about 80 mA but the size of the unit described here may be too large to act as a direct replacement.

The cost of our battery eliminator is about $£ 1$, appreciably less than the commercial units available. In addition our unit is exactly the same size as the battery that it replaces-it is built inside the old battery casing-and so it will neither be too large, or too small, when in place.

## THE CIRCUIT

The theoretical circuit is shown in Fig. 1 and is absolutely standard. The transformer (the type number and suppliers are mentioned in the components list) has a $7-0-7 \mathrm{~V}$ secondary and this is connected to the rectifier diodes D1 and D2 giving full-wave rectification; this is then smoothed by the capacitor C1. The reason for the resistor R1 is to act as a bleeder, when the unit is on it will then be drawing at least 20 mA and ensures that the peak voltage that may be present is never applied to the unit. With no load at all connected to the power supply, the voltage reaches well over 10 V and this is


Fig. 1 : The circuit of the battery eliminator.
not desirable as damage may result. As shown, with no load other than R1, the prototype measured $9 \cdot 2 \mathrm{~V}$ and with 80 mA being drawn about $8 \cdot 5 \mathrm{~V}$.

## CONSTRUCTION

As can be seen from the photographs, the unit is built inside an old battery case. This has to be taken apart as follows:-

First, using a screwdriver, prise up the bent-over metal ridge that holds the top of the battery in place and work all around this, levering it up. Straighten this metal with pliers or the top will not come out easily and reassembly will be difficult. When this is done the entire contents of the battery will fall out.

The top panel with the snap-on contacts should be cut free of the connecting wires or bands of metal and put to one side. Just enough of the original metal on the underside should be left for making the connections later.

The circuit is built on a piece of drilled s.r.b.p. board with dimensions exactly $2 \frac{1}{16} \times 2^{1}{ }_{2} \mathrm{in}$. Holes will have to be drilled in this to take the transformer mounting lugs which are then fitted through and bent over. The remaining components are "threaded" through convenient holes and soldered together as shown in Fig. 2. C1 is shown here very much smaller than it actually is to make this drawing clear; in fact Cl will be so large that it probably overlaps the diodes and RI. Both sides of the transformer have three wires coming out, the secondary is that with two brown and one blue wire, the primary has brown, blue and a green. The mains wire should be connected to the primary side to the brown and blue, unless you live in an area where the mains supply is 230 V or below in which case the mains should be wired to the brown and green.

The earth wire should be stripped back and a

## $\star$ components list




The prototype jusi before final assemb/y.


Fig. 4: How the unit fits together.

second short length of wire twisted with this and then both soldered to the case of the transformer. The reason for this is safety; this second wire will later be soldered to the battery case and if by any chance this solder joint breaks from the transformer, the battery case will still remain earthed.

Neither side of the 9 V is shown earthed since it

will depend on the design of the equipment which side requires earthing. If the equipment is negative chassis, the earth should run to the negative side and conversely for positive earth equipment.

The circuit board is held inside the battery case by means of two side fillets made up from hardboard, the dimensions for one of these is shown in Fig. 3; the other is of course identical. Three pieces are needed for each and these are then glued together.

When the side fillets are ready they should be fitted inside the case with the circuit board to ensure that everything is a tight fit and that they don't rattle about. If all is well, the bits should be taken out and one of the side pieces replaced to make the hole for the mains wire, both the piece of hardboard and case should be drilled together to ensure that the holes line up exactly.

It is important that the mains lead is fitted through one of the short sides with the hardboard fillets as this will prevent it chaffing on the sharp metal case; a grommet will be of little help as the metal sides will cut right through it in a very short while.

A knot should be made in the mains lead as close as possible to the transformer, as can be seen from the photograph, this will prevent it being pulled away from the unit with possibly disastrous results.

The unit is then reassembled as shown in Fig. 4. This should leave three wires coming out of the top: positive, negative and the earth wire from the transformer casing. The last should be soldered to the metal casing anywhere inside. The supply leads are then fitted to the snap contacts, remembering that for a battery the female contact is the negative and the male the positive. The original top can then be replaced and this should rest on the side fillets.

Before completing the assembly, the unit should be tested to ensure that it works; taking it apart again can be quite a job. If all is well the top metal, which is standing proud, should be bent down to hold the top in place.

The dimensions for the fillets are only applicable to the modern Ever Ready PP9 batteries. Other types of batteries have different inside dimensions and this will affect the length of the fillets; in this case the dimensions will have to be worked out.

## TAKE

JULIAN ANOERSON
A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

ONE of the disadvantages of being interested in radio and electronics is that you act as a magnet for faulty transistor radios and the like. Certainly you can say "No!" to requests to "have a look at it," but if you take this attitude you will not be very popular. Your author usually agrees, on the condition that mechanical troubles are not handled (broken cabinets, dial mechanisms etc) and that if replacement components are required it is up to the owner to get the bits. If you stick by these principles, repairs can be done very quickly but only if you have the right equipment. The most useful item is a multimeter-it is hopeless trying to work without one-but running a close second is a signal injector/tracer and this forms the subject of our project this month.

## Inject

The circuit of the signal injector/tracer is shown in Fig. 1; SWl alters the function and is in the "inject" mode. The circuit is a multivibrator producing a square-wave output at Cl to which a probe can be attached. The square-wave is in the audio range but it is so full of harmonics (a square wave is a fundamental frequency plus all its harmonics) that these go up to several megahertz. If you place a transistor radio on the medium wave band even near this circuit, the output will be heard all over the band. If we inject this signal at the volume control we will be able to establish if the amplifier part of the set is O.K.; if it doesn't work then we can concentrate our efforts in this direction.
If this is O.K. we can work back along the i.f. section and we shall eventually discover where the fault lies.

## $\star$ components list

| R1 1M ${ }^{\text {R }}$, $1 \mathrm{~W}, 5$ per cent | 1p |
| :---: | :---: |
| R2 $2 \cdot 7 \mathrm{k} \Omega$ " " | 1 p |
| R3 1M ${ }^{\text {R }}$, " | tp |
| R4 $2.7 \mathrm{k} \Omega$ " | 10 |
| C1 3300pF disc ceramic | 3 p |
| C2 3300pF disc ceramic | 3p |
| C3 3300pF disc ceramic | 3 p |
| C4 $100 \mu \mathrm{~F}, 10 \mathrm{~V}$ minimum | $5 p$ |
| Tr1 BC109 | 10 p . |
| Tr2 BC109 | 10 p |
| D1 1N914 | 7 p |
| SW1 One-pole, 2 -way slide switch | 8 p |
| SW2 On-off switch, toggle type | 5 p |
| Crystal earpiece and jack socket | 35 p |
|  | 93p |
| Prices are those recently advertis changed. No allowance is made costs or fof postage and packing should be checked carefully before | have order oints |

## No. 45 <br> SIGNAL INJECTOR/TRAGER



Fig. 1: The circuit.


Fig. 2: Suggested layout on Veroboard.

## Trace

When SWl is switched to "trace", the circuit is no longer a multivibrator but becomes a highly sensitive amplifier. If the probe is fixed to an r.f. point the signal will be rectified by the diode D1 and amplified by both stages and fed to the crystal earpiece. It is smoothed by C3 which now, instead of coupling back to the base of Tr 1 , goes to the negative line.

The current drain of the unit is quite small and a PP3 battery is quite sufficient.

Two wires, fitted with crocodile clips, should be connected to the negative line and to Cl as these will be needed to couple the injector/tracer to the circuit under test. If using the injector at r.f. frequencies, the output is so high that the wire from C1 has only to be held near the aerial, it is not necessary to make a direct connection.

## Construction

The components can be mounted in any convenient form but a suggested component layout is shown in Fig. 2; this is built on a small piece of Veroboard with $0 \cdot 15$ in matrix, $8 \times 8$ holes; no breaks are necessary in the conductor strip. SWl can be a small slide switch wired as shown; SW2 can take any convenient form.

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## MONTHLY NEWS FOR DX LISTENERS

CHRISTMAS is over and here we are in another New Year. I know that many of my readers will have asked for presents of money so that they can save towards the new receiver that they want and many will write to me asking advice on the best set to buy.

Unless a second-hand purchase is anticipated the reasonably serious listener will have to pay around $£ 50$ for a good receiver. There are of course many sets on the market for much less and several which cost a lot more.

In this middle price range there are two receivers which stand out as being very good value for money and for this reason they are very popular with DXer's. The first is the Lafayette HA600 which is a general coverage receiver ( 550 kHz to 30 MHz ) this set has the advantage of being all solid-state which means that it can be run from either the mains or from 12 volts d.c. The second is the Trio 9R59DS which is again general coverage but can only be operated from 240 volt mains.

Before anyone asks, my personal preference is for the Lafayette. There are two reasons for this, the first is that I have always owned Lafayettes and had no trouble with them at all. The second is that when I worked in an Electronics Laboratory, designing circuits, I only used transistors and integrated circuits, never valves. Consequently I feel more at home with a solid state receiver and if anything goes wrong I will be more able to repair it myself.

A great number of readers will, of course, not be lucky enough to afford one of these sets but they can increase their enjoyment of the hobby in many ways.

The 1973 edition of the World Radio TV Handbook has just been published and although it costs about $£ 3$ many experienced DXers will tell you that it is an invaluable text that they would never be without. The book lists all the Broadcasting Stations in the world with full details on each, including frequencies used, hours of transmission and the languages used. The book also contains a section on general information and a complete listing, by frequency, of all the stations.

A good New Year Resolution would be to erect a new and better aerial, about which much has been published in the past few months There is, however, a snag which was pointed out to me by Mr. A. W. Lewington of Bath. I also noticed the difficulty when I moved house recently and wanted to erect a new aerial. The problem is that nobody seems to sell good aerial wire any more. A few years ago Woolworths used to sell aerial wire which consisted of stranded copper wire with thick plastic insulation. This had the two important properties of being strong and flexible to withstand the ravages of our British weather. It is, however, no longer available.

If any reader knows of a good source of aerial wire

I would be pleased to hear from him so that I can pass the information on to all our readers.

Yet another way of getting more enjoyment from the hobby is by joining a reputable DX Club. These clubs publish magazines for their members and these are used to exchange news and views about all aspects of the hobby. The membership fee is usually about $£ 1 \cdot 50$ and the magazines alone make this outlay very woll spent. The club that I would recommend is the World DX Club and the Secretary is Clive Jenkins, Il Wesley Grove, Portsmouth, PO3 5ER.

In a recent article I published a specimen Reception Report. Mr. A. J. Wills of Elgin wrote to me to point out that the space devoted to programme details was not long enough. This was due to an error on my part when typing out the article. The most important part of the report is the section on programme details. All the other details on the report can be obtained from such sources as the World Radio TV Handbook.

The programme details are the only way in which the station can be sure that it was in fact their transmissions that were heard. The more complete the details are the greater is the liklihood of the station confirming the report with a QSL card.

All this chat has left me with very little space for your reports so I will start straight away with one from James Pruden of Sturminster Newton in Devon. James has a Skywood CX-203 receiver with a 15 metre end-fed aerial, this combination enabling him to hear:
6010 RTB, Belgium in French at 1510.
9545 Radio Ghana in English at 2120.
9610 Radio Kiev, USSR, in English at 1930.
11650 Radio Bangladesh in English at 1715.
15015 Voice of Vielnam in English at 2015.
15165 Radio Denmark, ID in English at 1330.
15170 ELWA, Liberia in Arabic at 2230.
15345 Radio Norway in English at 1615.
21570 Radio Japan, news in English at 0800.
Craig Tyson of Wembley in Western Australia used his Lafayette HA600 receiver and inverted ' $L$ ' aerial to hear the following stations:
6090 Phnom Penh in English at 1230.
7215 AFN, Taiwan in English at 1300.
7470 R Liberation, N. Vietnam, English at 1030.
9510 Lakeland Radio, Malawi, English at 1945.
9520 VLT9, New Guinea in English at 0730.
9580 Voice of the Philippines, English at 1300.
15170 Radio Tahiti in French at 0700.
15185 Voice of Nigeria in English at 0700.
Reports should arrive by the 15 th of the month and be addressed to me at 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.



APPY New Year. Now, how about a resolution to devote at least 30 per cent of your listening time to bands which you normally ignore? If you are an h.f. type, you could do no better than start off with top band transatlantics. These are tests carried out at certain times and on certain dates. The first ones in 1973 are as follows. January 14 and February 11 from 0500 to 0730 hours.

For something a little more difficult, how about the transpacific tests? These are to be held on January 13 and February 10 from 1330 to 1600 hours. The U.S. and Canadian stations will be transmitting between 1800 and 1807 kHz . The D.X. stations will use 1825 to 1830 kHz or 1800 to 1805 kHz . It should be noted that stations in other countries are often restricted in choice of frequencies. For example, Japanese Amateurs may only use 1907 to $1912 \cdot 5 \mathrm{kHz}$ while stations in New Zealand are restricted to 1875 kHz . Doubtless we will get some Lid calling an endless CQ on these frequencies. How wonderful it would be for me to be proved wrong on this. How about it, Lids?

John Spacey (Devon) tells of A51PN putting in an appearance on 14 MHz . He also mentions that Swan Island is active (listen for W6MTE/HR6) as is VU25FBZ on Andaman Island, both on 14 MHz .
Two useful New Year presents you can treat yourself to. One is the latest countries list from the RSGB. Second is a good world atlas. For example, do you know where Swan Island or Andaman Island (mentioned above) are?

Which bands to listen on and at what time is really a matter of personal choice. However, the following remarks are based on readers' reports and personal observations by your scribe's ears.

The h.f. bands ( 14,21 and 28 MHz ) become somewhat erratic during the winter months. By contrast, the three lower frequency bands ( $1 \cdot 8,3 \cdot 5$ and 7 MHz ) all improve compared to their summertime performance. Fifteen and twenty metres start to close down quite early now. Often, by 2000 hours there are no signals at all and this state of affairs remains until around 0600 hours.

On ten metres it is often a matter of luck. This band now opens at about 0800 hours and closes again at around 1700 hours. However, 28 MHz is really a sort of lucky dip. If there is a high sunspot activity the band will suddenly burst into life.
Most of the winter D.X. activity migrates to 7 MHz and this is particularly evident when the h.f. bands ( 14 MHz and upwards) close down for the night. In theory, the sunspot activity should continue to decline in the coming months. This activity follows an 11-year cycle and we are currently on the way down towards a trough.
R. Kell (Northumberland) sends in a five-band log which includes earfuls of activity on 3.5 and 7 MHz . Guilty parties aiding and abetting include a "modified" R109 with an a.t.u. and l50ft. end fed antenna. Goodies on $3 \cdot 5 \mathrm{MHz}$ include; CN8HD,

# THE AMATEUR BANDS David Gihson, G3JDG Frequencies in kHz - Times in GMT 

XV5AC, ZM4PG, 9H5D. Plundering forty metres brought the following r.f. jewels; CO3GS, CN8HD, HR1RF, KZ5PW, OA4SO, PY2ELX, PY2FKZ, TF1TP, VR2DE, XE1IIJ, YV4AGP.

John Hulse signing himself "Yours faithfully" and residing in Cheshire, tells of a sparkling new FR50B receiver. Duper squeaks on 28 MHz from; CR6CN. CR7IC, CX2CF, ET3JH, KZ5PW, LU5DEK, LU5DTV, OY9LV, PY1AGC, ST2SA, VK6CF, VP7ND, VP9BO, XW8CN, YV4EBH, ZP5AQ, ZS60S, 3B8CV, 3B8CZ. Down on 21 MHz , the following menu was provided; CP1FU, CT2BG, EL4B, EP2TC, ET3DS, FP8DH, HI3XSJ, HK3CCO, HK3CLX, OD5FU, PZ1CU. VP1BH, VU25DK, XV5AC, YA1OS, YV5AK, ZD3X, ZE7JC. All stations using s.s.b. and the receiving aerial is described as a 66 ft . dipole at 10 m height.

Stefan Kaye (Oxon) made a brave attempt to break the habit. But the soulful look in the silent eyes of his AR88D got to him. Result of this joyous reunion was; CE3PY, CT2AC, LU3DTV, LU9DTQ, VQ9MC, ZS1WS-all on s.s.b. on ten metres. Down on eighty, a listen was rewarded by: FW8IA, HB0AIC, K3UQU/W1, ON0NJ, TZ2AC, VE1ADV, VEIIE, VE3PT.
R. Iball (Notts.) uses a diamond aerial! Well, it's shaped like a diamond, is 7 ft . long and hidden in the loft. The receiver is a JR500SE (not hidden in the loft) and the 14 MHz c.w. signals were received by courtesy of: HS4AGN, UA0DV, VE7ZR, VE3ZT, ZL1ARV, ZL1MQ, ZL3GQ, ZM1AFW, ZM3ABC. Donald Duck mode of signals on the same band from: FP8DH, PZ1DR, VE6PP, VP8RA, VK1BF, VK6PG, VK6VW, VP9GA, VP9GE, VS9MB, ZL1AH, ZM4KM.

Trevor Thomsen (Bulawayo, Rhodesia) sends letters with pretty stamps and includes logs heard on his Hallicrafters S53A and 40ft. end fed. The list for s.s.b. on 21 MHz reads: EL2CB, GR3NM, K3TGM, K4MQG, WA3GJZ, WB8JEY, W1AWE, W4SKO, W5RO, W8COG, 6W8AL, 6W8EM. Bernard Hughes (Worcester), JR31O, 66ft. long wire, 28 MHz s.s.b.

Logs, in alphabetical order please, to arrive by the 15th of the month to $\mathbf{1 2}$ Cross Way, Harpenden, Herts.


AMATEUR BANDS RECEIVER DECEMBER 1972 Part 1. Fig. 2C, potentiometer ( 500 ohms ) associated with S-meter should be marked VR2, Fig. 2D, power supply diodes should be marked D1 and D2. The OA2 voltage stabiliser should be marked V1. Amend Components List:-Fig. 2D, V1 OA2, V2 ECL86.
I.C. LINEAR CAPACITANCE METER JANUARY 1973 D3 should be a C5V 65.6 V (not $3 \cdot 3 \mathrm{~V}$ ). This applies to both the circult and the components list.

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smothe with negri-
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| 5R4GY | 75 | 6E5 | 51.00 | 6SC7M | 75 | 12AT7 | 85 | $30 \mathrm{C18}$ | 80 | 1625 | 55 | DL94 | 48 | ECLL 8 |  | GZ30 | 40 | PCF805 | 80 | $\mathrm{SP}_{4}$ | 21.70 | UF89 | 60 |
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| 6A7 | 75 | 6F13 | 46 | 68N7GT | 35 | 12C8GT | 35 | 30 L 17 | 80 | ATP4 | 45 | E88CC | 65 | EF50 | 25 | KT66 | E2.05 | PCL 85 | 40 | SU2150 | +175 | UY41 | 48 |
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| $6 \mathrm{AU6}$ | 25 | 6J5M | 50 | 6X5GT | 40 | 128H7 | 85 | 3514 | 35 | CL33 | . 30 | EBF83 | 40 | EF183 | 30 | MSP4 | 50 | PL82 |  |  |  |  |  |
| 6B4G | 31.00 | 6J5G | 20 | 7B6 | 70 | 12857 | 40 | 35234GT | 60 | CY30 | 43 | $\begin{aligned} & \text { EBF89 } \\ & \text { EBL1 } \end{aligned}$ | 80 ¢1.00 | $\begin{aligned} & \text { EF184 } \\ & \text { EX32 } \end{aligned}$ | 55 | MU14 | 75 | PL82 | 45 | U191 | 75 | W8508 | 8.00 |
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[^3]MULLARD Limited, as their 50th Anniversary tribute to the BBC, staged a two month exhibition at Mullard House in London. It was opened on November 2 by Lord Hill, chairman of the BBC.

The Post Office gave its full support and co-operation to the exhibition which was complementary to the one organised by the BBC and held at the Langham Hotel, near Broadcasting House.

The Mullard exhibition was designed with a fourfold aim in mind-to show how technical innovation has contributed to the growth of broadcasting, to stress the pioneering effort that went into it, to enable the public to gain more of an insight into the technical aspects of broadcasting and to illustrate how development and research are continuing for the future.

The first part of the exhibition was entirely devoted to the development of broadcasting. It included a replica of the original Savoy Studio 1 of the early 1920s and a pictorial story showing how the microphone was evolved.

Two famous microphones exhibited were those used by Dame Nelly Melba and Sir Winston Churchill.

Visitors were also able to speak into one of the early "meat-safe" microphones and hear their voices


The lip microphone: designed by the BBC Research Department to cut out background noise. It was first introduced in 1937.


Her Majesty the Queen compares vintage and modern tape recorders.
reproduced on a tape machine. Also on display, was an early cylinder gramophone and one could, at the touch of a button, hear the kind of reproduction that could be obtained from such a machine.

An early pianola was shown and it was difficult to realise that in the earlier days of broadcasting, the announcers actually had to pedal units like these as continuity between programmes!

On the same stand there was a recording machine of the type used by BBC War Correspondents and in one of the photographs shown in this article Her Majesty the Queen can be seen comparing this with a modern cassette tape recorder.
The section of the exhibition devoted to the story of television began with the actual first Emitron TV camera. Photos showed the various outstanding developments of television and the display was climaxed by a reconstruction of a live TV studio.

There was an audio/visual link with the BBC exhibition at the Langham, and Mullard House visitors were able to see themselves on colour TV. and to read the news on closed circuit TV. From our picture it looked as though the BBC had taken on a new cameraman to demonstrate the colour camerahis face looked very familiar though!

Mullard themselves had a display showing the part their components had played over the five decades of sound and TV broadcasting.

They also had a "Colour TV Look-in", a six minute


The Queen shows interest in a horn loudspeaker and the "meat safe" microphone.


Prince Philip "has a go" at being a BBC cameraman.


The "Twenties" room setting at the Langham Hotel exhibition.


This picture shows the central display feature at the Langham exhibition. It reflects the development of the BBC over the years.
presentation telling the story of the Company's contribution to colour TV development.

Exhibits were also devoted to colour TV techniques and demonstrations in which the public could take part. Visitors could experiment with a BBC Radiophonics unit and see a demonstration of 3D television together with exhibits showing what the future may hold for transmission techniques.

The BBC held their own exhibition at the Langham Hotel, formerly one of London's most luxurious hotels and now offices and studios of the BBC.

Facing visitors, in the main area of the exhibition, was a multifaceted panoramic screen consisting. of 20 separate screens. Forty-two slide projectors, with a total of 3,500 slides projected onto this screen. Scenes shown were chosen from a quarter of a million original BBC pictures and gave an extremely good visual impression of broadcasting in the past. present and future. These projectors, incidentally, were controlled by a simple computer which maintain the correct picture sequences.

Underneath this screen, which stood about 9 ft . above ground level, there were mock-ups of room settings of different periods of broadcasting history.

Of particular interest to "Going Back" fans was a typical room of the ' 20 s . The man is (see photograph) depicted hearing the first BBC broadcast on his home-made receiver on November 14, 1922.

In front of the stand was a row of buttons and excerpts from 1920s' type programmes could be heard by pressing any button. Famous voices heard included Flotsam and Jetsam, Tommy Handley and Jack Hylton.

Other room settings were shown depicting the broadcasting years rolling on. A large planographical map of the British Isles provided the basis of another exhibit and showed the growth of programme coverage from 1922 onwards, achieved by many miniature "transmitter" masts that lit up. Behind this stood a 20 ft . high display reflecting the growth of the BBC's services at home and abroad.

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THIS short article aims to bring to readers' attention some lesser known facts of zener diode operation-facts which are so useful when it comes to making the most of a voltage stabiliser or regulator.

## Temperature

Almost all zener diodes, like other semiconductor diodes, have a temperature coefficient of voltage; that is, their exact voltage varies as their temperature varies. However, a study of manufacturers' literature shows that this temperature coefficient is by no means the same for all zener diodes and in fact varies with voltage as shown in Fig.1.


Fig. 1: Graph showing temperature coefficient for different zener voltages.

It can be seen that, at one particular zener voltage, namely $5 \cdot 6 \mathrm{~V}$, this temperature coefficient is actually zero and that the coefficient becomes positive at higher voltages and negative at lower voltages. The values used to plot the graph were extracted from Mullard data but, in point of fact, all makes of zener diodes show this effect, which is presumably connected with the level of doping employed to obtain the various voltage ratings. Of what particular use is this information to the home experimenter?

## Environment

Consider the environment in a motor-car. This could very easily range from $25^{\circ} \mathrm{F}$ to $85^{\circ} \mathrm{F}\left(-5^{\circ} \mathrm{C}\right.$ to $30^{\circ} \mathrm{C}$ ) and yet amateurs happily use a zener of any voltage thought appropriate, when, with a little further consideration, a higher performance could easily be obtained. For example, to stabilise a car battery supply at 10 V for instrumentation, control or
communication purposes, the use of $6 \cdot 2 \mathrm{~V}$ and 3.9 V zeners in series will give an almost zero temperature coefficient, so contributing to the accuracy of any measurements and to the frequency stability of receiver local oscillators etc.

A further point of interest is that a forward biased silicon diode has a temperature coefficient of about $-2 \cdot 2 \mathrm{mV} /{ }^{\circ} \mathrm{C}$, so that such a diode used in series with a zener diode of $6 \cdot 2 \mathrm{~V}$, see Fig.2, once again would give a zero temperature coefficient, this time with an output voltage of about $6 \cdot 9 \mathrm{~V}$. Note that the 'forward biased diode can be the base-emitter junction of a silicon transistor if, for any reason, this is more convenient.


Fig. 2: Circuit illustrating the use of a forward biased diode and a zener diode in series.

So far, we have considered the effect of temperature on the actual voltage of a zener diode, using car applications as an example, but it should be remembered that almost any situation will experience temperature variations and the effect of these on any voltage regulators should not be overlooked. Steps to reduce any such voltage changes can then be taken, as described.

## Stability

A further cause of disappointment in the voltage stability of zener diodes arises from the finite value of dynamic slope resistance of the zener. For example, in Fig.3a for a load of up to 20 mA and a zener current of 5 mA , resistance $R$ is:-


Fig. 3a: A typical zener diode application with Fig. 3b showing the effective dynamic equivalent circuit.


Fig. 4 : Dynamic slope resistance of a range of zener diodes.

$$
\mathrm{R}=\frac{(15-10) 10^{3}}{20+5}=200 \Omega
$$

Now, a 10 V 400 mW zener can have, again according to Mullard data as plotted in Fig.4, a dynamic slope resistance of $25 \Omega$. Thus, the effective dynamic equivalent circuit is as shown in Fig.3b. This leads to the result that, for a change in supply voltage Vi of 1 V , the change in output voltage, Vo, will be:-

$$
V_{0}=1 \times \frac{25}{200+25}=0 \cdot 11 \mathrm{~V}
$$

which is surprisingly high. A quick measurement confirmed such a value.

## Output stability

A dramatic improvement in output voltage stability, as the input voltage varies, can be brought about by the use of a constant current circuit, provided that the load current to be supplied is almost constant. This is usually so where the zener diode is used to supply a reference voltage in a voltage regulator, and in supplies to receiver local oscillators, for example.

At very low zener voltages and, to some extent at the higher voltages also, quite large values of dynamic slope resistance are noted e.g. $85 \Omega$ at $4 \cdot 7 \mathrm{~V}$ and $60 \Omega$ at 20 V so the constant current circuit of Fig. 5 will greatly assist in providing voltage stability.

In this example, there is a load current of 10 mA with 8 mA zener current. Now, with a constant potential difference between transistor base and input voltage, due to the use of forward biased silicon diodes, and thus a constant difference between emitter and input voltage, a constant current must flow through the zener diode and load in parallel. Therefore, as the input voltage varies, the current through the zener hardly varies and we have largely eliminated the effect of its dynamic slope resistance.


Fig. 5: In this circuit a constant current feed is provided for the zener diode.

## Results

A series of measurement was made of the output voltage of the circuit of Fig.5, and of a simple resistance of $620 \Omega$ plus zener diode combination, as the input voltage was varied. The results are plotted in Fig. 6, where the remarkable improvement given by the constant current circuit is clearly seen.

A reduction of output voltage variation by a factor of about 30 over the range of 18 V to 26 V input voltage is surely well worth the additional complexity.


Fig. 6: Performance of zener stabilisers with constant current feed (A) and simple resistive feed (B).
It would doubtless have been possible to have extended the flatter part of curve $B$ down to, say, 18 V input voltage, but this would have required a very much smaller value of series resistor than the $620 \Omega$ actually employed in obtaining the curve of Fig.6. This would have probably called for the use of a zener diode of greater power rating, and yet it still would not have led to as good a performance as the constant current circuit.

If the zener diode so driven is employed to supply a reference voltage in a series stabilised power supply hum rejection is also greatly improved, for the constant current transistor has a very high output resistance, and this, together with the (relatively) low impedance of the zener diode, gives attenuation of ripple. This offers the chance to use smaller smoothing capacitors. A saving of space and money is the result, as well as improved performance.

One final point. In all the circuits given here a capacitor is shown across the zener diode. This is done since zener diodes are quite effective noise generators! The capacitor also helps to lessen any hum present if a poorly smoothed mains source of power is used with the simpler zener diode circuits.

PETER WRIGHT of Formby, Lancashire has tried his PCR2 receiver and 50ft outdoor aerial on the medium waves at 0030 hrs and he logged WINS 1010 kHz located in New York City. Ian Geddes who lives in Dumbarton, Scotland reports CJON 930 kHz in St John's Newfoundland; CHER 950 kHz in Sydney Nova Scotia; CKBW 1000 kHz Bridgewater N.S; CFRB 1010 kHz Toronto; WOR 710 kHz New York City; WOWO 1190 Hz in Fort Wayne, Indiana; WABC 770 kHz New York City; WKBW 1520 kHz in Buffalo N.Y; WCKY 1530kHz Cincinatti, Ohio; WWVA 1170 kHz Wheeling, West Virginia; WNEW 1130 kHz New York City. Ian writes "CJON is the most consistent signal from midnight until 0200 hrs ". Others to listen for from midnight onwards are CBM 940 kHz in Montreal; CBA 1070 kHz Moncton, New Brunswick; WHN 1050 kHz in New York City. A weak French-speaking station can often be heard on 1375 kHz after the close down of Lille, France 1376 kHz at 2300 hrs . This is Radio St Pierre in the French Territory of St Pierre et Miquelon which lies a few miles to the south of Newfoundland. Radio St Pierre verifies readily and is the sole broadcaster on the islands which form a 'medium waves only' DX country.
Kevin Peel (Hornchurch Essex) has an 8 transistor Astrad receiver and a 100 ft outdoor aerial and he heard the following broadcasts in English on the medium waves. Radio Portugal 755 kHz at 2245 hrs ; Radio Tirana, Albania on 1394 kHz at 2030 hrs and Vatican Radio 1529 kHz at 2045 hrs . J. Cesarczyk (South Croydon) used his Grundig Elite Boy receiver with internal ferrite aerial to hear Radio Jerusalem 737 kHz at 2230 hrs (with interference from Warsaw and Madrid); Radio Bucharest, Romania 755 kHz at 2050 hrs ; the Voice of America Kavalla, Greece 791 kHz (in English at 2300 hrs ); VOA Rhodes 1259 kHz (in English at 0300hrs); BBC World Service, Berlin on 809 kHz (in English at 2315 hrs after the close down of BBC R4).
During the evening quite a few distant stations can be found in the gaps between European channels. Baghdad, Iraq on 760 kHz can be heard between West Germany on 755 kHz and Sottons, Switzerland 764 kHz and is usually on the air all evening with programmes in Arabic. Riyadh, Saudi Arabia is on 588 kHz between Madrid 584 kHz and Frankfurt 593 kHz ; Ovazim, Iran 841 kHz is often strong when it signs-off at 2030 hrs , listen between Nancy, France on 836 kHz and Rome on 845 kHz ; Ahwaz, Iran can be found on 1394 kHz in between Radio Centro Madrid 1385 kHz and Albania on 1394 kHz ; the BBC relay on Masirah Island in the Persian Gulf (heard in English at 2040hrs) is on 1410 kHz between the French network on 1403 kHz and the Spanish channel on 1412 kHz .
Please send logs and information about the medium waves to the author at 132 Segars Lane, Southport, PR8 3JG.



THE calculator market is flooded with many different types, each claiming some unique feature(s). Of particular interest to the buyers -us-is the price. News has now arrived from a semiconductor manufacturer that i.c. chips are currently in production which are so cheap that an electronic calculator could easily be manufactured and sold at a market price of less than $£ 20$.
There are four versions of the chip which are fourfunction (add, subtract, multiply and divide), eightdigit units with a seven segment output circuit. The entire electronics are housed on a chip area of only $166 \times 162$ millimetres.
In the United States these chips are already in production and coming off the line at the rate of some 75,000 every four weeks. The Company also reports that orders for the chips in the U.K. have already exceeded $£ 100,000$.
Heat sinks are comparatively uninteresting items of electronic hardware. Usually, they consist of a piece of metal often with fins protruding. Their purpose in life is to conduct heat and to dissipate it.
A new introduction is a hollow heat sink which spreads the heat evenly. The difference in temperature between the heat-producing element (say, a power transistor) and the furthest point on the heat sink is only around $1^{\circ} \mathrm{C}$.
The heat sinks are fabricated rather like a hot water radiator. The hollow section is evacuated to a virtual vacuum. Water is then fed in. Because the air pressure is so low, the water boils. It then starts to lose heat and also gives off steam which condenses and turns back into water again. Eventually, equilibrium is established and the heat sink cools to room temperature.

The spread of heat on these sinks is extremely fast and the fins may be connected to the heat source by a pipe which has also been evacuated and filled with water. The fins may thus be located remotely from the heat source and the difference of $1^{\circ} \mathrm{C}$ holds over any part of the heat sinking system.
The cry still goes on about pollution, and electronics has come up with some useful ideas for monitoring. One research laboratory is busily engaged on producing an infra red diode which will emit radiation in the 3 to $6 \mu \mathrm{~m}$ band. Carbon monoxide, carbon dioxide and hydrocarbons all absorb radiation strongly in this band and thus the amount of absorption of the radiation gives a measure of the pollution of these chemicals. Infra red diodes already exist, but they radiate at around $0.9 \mu \mathrm{~m}$ and hence the need to design a new diode with radiation in the required region.


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#  PART 14 

## Feedback etc.

Queries have arisen about our use of the term 'feedback' and its relation to equalisation.' This month, while, at the time of writing, colleague Mike Hollier basks in holiday sunshine, seems as good a time as any to indulge myself in a little explanation of the terms we are using and why.

First, feedback. This is simply, as explained last month, a method of picking off part of the output from an amplifier and 'feeding it back' to the amplifier's input section. The feedback can be a simple resistor from collector to base of a single stage amplifier Fig. 67 (a), can be in series with the source signal (b) or in shunt with it (c).

Note that I have deliberately reverted to p.n.p. transistors in these examples. One reason is to remind you of the opening of this series of articles, where the precise examples were quoted; the other is to be able more easily to explain the action of the feedback. Here, I must insert the warning that people, like me, who were brought up on valves began to find difficulties with the revision of feedback concepts as applied to transistors, principally because the operation of transistor circuitry depends on the relationship of the 'circuit blocks' to each other. One has to consider the input and output 'loads' very much more than one did when dealing with vảlved circuits. So I use the germanium transistor circuits to lead into my subject-don't worry, it will get more complicated later on. ...

The three examples of Fig. 67, are all of negative feedback. That is, the re-applied signal tends to reduce the gain of the amplifier. Its purpose, of course, is not just to reduce the gain but also to stabilise the circuit, help reduce noise and internally generated distortion. The feedback can be applied over several stages, not just the simple sub-circuit shown. And here it is shown as resistive feedback, i.e., effectively d.c. But we shall later be concerned with a.c. feedback, with capacitors in the loop, so that the amount of gain reduction varies as the frequency the circuit is handling also changes. Which will bring us to equalisation: which I would define as the application of frequency-dependent feedback.

Taking Fig. 67 in detail, (a) combines both a.c. and d.c. negative feedback if we insert a series capacitor (shown dotted) with the collector-base resistor $R_{F}$ and retain the d.c. conditions by the negative feedback across the emitter resistor $\mathrm{R}_{\mathrm{E}}$. Apart from the emitter resistor effectively increasing thr


Fig, 67 (a): Simple collector/base negative feedback with d.c. blocking capacitor ringed. Change in value here affects a.c. feedback. (b) series feedback. (c) shunt feedback, from collector of second stage to emitter of first.
input resistance to the transistor, which is an advantage, it reduces the gain by being added to the denominator of the formula for voltage gain.

In the sub-circuit (b), the voltage developed across $\mathrm{R}_{\mathrm{E}}$ is fed back in series with the lower part of the base bias potentiometer, the latter becoming $R_{F}$, and in (c), which is voltage feedback rather than current feedback, as before, $\mathbf{R}_{E}$ does its job in the first emitter while $\mathrm{R}_{\mathrm{F}}$ picks off a portion of the amplified signal, the amount dependent on C , and modifies the reduction of gain which $R_{E}$ is already effecting.

All this has been discussed before, and the relative figures and formulæ given in detail. It does not do us any good going over the same ground, but keep the above three examples in mind as basic 'styles' of feedback when we come to consider the action of equalising circuits. In talking of the virtual resistance circuits during Parts 11, 12 and 13 the point of relative gain with and without feedback, and the change in effective resistance should have been made clear.

## Corrective feedback

Why do we want equalisation? If the source itself was 'linear', there would be no need of more or less gain at special frequencies. But there are reasons of plain mechanics and basic magnetics that demand the 'tailoring' of response curves of the input circuits of an amplifier.

Consider the case of a magnetic pick-up cartridge. Because of its construction-yirtually a coil in which a moving metal piece causes a changing voltage by altering a magnetic field-and is therefore an inductance, not a pure resistance. The formula for the reactance (an a.c. term for resistance, no more) of a coil is $X_{L}=2 \pi \mathrm{fL}$, where $X$ is the reactance, $f$ the frequency the coil is handling and $L$ its inductance. We will neglect the small resistance of its windings in the case of the pick-up cartridge.

From this, we can see that the higher the frequency, the greater the reactance. So it would seem that our corrective feedback to handle an input from a cartridge need only reduce the gain in proportion to the frequency of the signal-which, in fact, it does.

But the problem is worse than this. To get the


Fig. 68: RIAA recording characteristic as practically employed. Mirror image replay characteristic dotted. Note the short 'plateau' around 1 kHz .
dynamic range on to the disc and to maintain as good a signal-to-noise ratio as possible, the bass is attenuated and the treble enhanced. By international agreement, the way in which this is done conforms pretty closely to a standard. This is the RIAA characteristic, Fig. 68.
Modern discs are supposed to be recorded to this characteristic, although any enthusiast will tell you that there are some suspicious variations, difficult to prove except by comparison.

Unfortunately, a magnetic cartridge produces an output (voltage) proportional to its stylus movement. That is to say, it should. So if the characteristic is level, the output should be constant. Over a small portion of that. given curve in Fig. 68 the characteristic is level, so testing only at this one frequency cannot give a true picture of the performance of either cartridge or pre-amplifier.

If we now consider how a disc is made, we shall see that the RIAA bass attenuation means that at frequencies below about 1 kHz the velocity of the stylus will be reduced, although the amplitude remains constant, just as it very nearly remains constant at the higher frequencies, where the velocity now rises. In fact, the 'average' slope of the given curve is around 4 dB per octave, instead of the more generally regarded 6 dB per octave, which would be the ideal slope over the two nearly straight portions of the curve. (See also Fig. 71.)

To put matters in perspective, 6dB per octave means that the output voltage doubles for each octave upwards. So a bass note, say A4, the lowest of the white keys, whose frequency is 27.5 Hz , giving, say, 1 millivolt at a certain loudness, would be compared with the top A on the piano 'third white note from the top, Joe', at a frequency of 3250 Hz , would give 64 mV if the original sound had been at the same level.

In fact, this circumstance would not so often apply, and our correction curve can be a replica of the original, mirrored, as shown dotted in Fig. 68 and the dynamic range could be left to take care of itself if the input sensitivity of the pre-amplifier and its overload characteristic are both in order. Too often, one or other is not.

As intimated in Part 11, one reason for the Cambridge style of virtual earth pre-amplifier was to achieve a very much better than usual overload performance. The average output of a magnetic cartridge is between 5 and 8 mV (from a voltage output of between 1 and 1.5 mV per centimetre per second of recorded velocity). But therein lies the rub.

## Bass end overload

We have already seen that it is advisable in the interests of best signal handling to keep our variable controls (volume, tone and balance) after the input circuits. So our magnetic pickup circuit has to be able to handle signals from a couple of millivolts or less to 60 mV or more. In practice, because there is bass boost applied during replay to make up for that attenuation during recording, the problem arises at the bass end, and we find that most preamplifiers will handle modern records if they have within a 3 -30mV input sensitivity ratings. A 30 dB overload rating is sometimes specified. If you consider that maximum velocity at 1 kHz could be around $25 \mathrm{~cm} / \mathrm{sec}$ and that a cartridge with an output as

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$1.5 \mathrm{mV} / \mathrm{cm} / \mathrm{S}$ would give 38 mV from such a recorded groove, you can see that distortion on signal peaks would be inevitable, as this would require an overload rating of some 38 dB .

So the overload safety margin diminishes toward the lower end of the frequency spectrum, and this is where mains hum, disc rumble, turntable rumble and other problems can rear their ugly heads. Hence the need, when we design our 'front-end' amplifiers to ensure that we get good gain figures before applying our feedback-and, what is more, a stable amplifier without (or with minimum) feedback, for it is precisely at this dangerously low end of the spectrum that the feedback will be least.

This is not the place to go on about cartridges, but I hope I have helped clear up a few of those queries about the need for good basic pre-amplifier design as well as the application of very precise feedback. And perhaps dropped a few hints about choice of pickup: if you have an amplifier with a sensitive magnetic pickup pre-amplifier and shove a high output cartridge into it, you can expect a bit of bass overload. As this occurs before any control you can apply, there is no real cure except correct matching.

## In practice

One could quote extensively from commercial circuits to prove a point, but to combine our previous talk about virtual earth circuits and to use a design which has been proven by constructors, let me cite the modular pre-amplifier by John L. Linsley Hood, which appeared first in Wireless World in July 1969, and which, although parts have been modified since, happens to suit our purpose. Mr. Hood has kindly consented to allow us to quote him.

Fig. 69 shows his basic concept of a stage used to obtain the RIAA replay characteristic. Looking at it carefully, we see that it is again a virtual earth design, with point $X$ the null point, provided the gain of the amplifier is high enough. The input impedance of the circuit will be approximately equal to that of the input network R1/C1. The load resistance of a magnetic cartridge is around $47 \mathrm{k} \Omega$ at 1 kHz , and provided C 2 is large enough and R 2 equal


Fig. 69: Frequency selective feedback to achieve the RIAA replay characteristic, applied around a virtual earth amplifier.
to $\mathrm{R} 1, \mathrm{C} 3$ relatively small in relation to R 2 (at 1 kHz ), stage gain can be given approximately by R4+R5/R5.

The designer aimed at a gain of 10 , this being deemed sufficient to deal with outputs between 4 and 10 mV . The frequency response is determined by the two networks ' $A$ ' and ' $B$ ', shown in dotted 'boxes' in Fig. 69. In this idealised state, the circuit is not entirely practical, of course. Fig. 70 shows the actual circuit, drawn so that these frequency corrective components are at the front.


Fig. 70: The redrawn circult of Fig. 69, part of the J. L. Linsley Hood modular pre-amplifier.

But we must also consider the effect of C 4 and C 5 , which, in conjunction with Cl and R 4 , give a steepcut rumble filter ( $18 \mathrm{~dB} /$ octave) with an attenuation of more than 40 dB at 8 Hz and a turnover point of 25 Hz . The results can be seen in the RIAA replay curve, measured from the pre-amp, in Fig. 71.

Two things remain to be mentioned. C6 is put across the collector load of the first transistor to sharpen up the transient response: the dotted curve


Fig. 71: Theoretical RIAA replay response curve with measured deviations. Bass roll-off is deliberately obtained by component changes.
at the bass end of this curve is in two parts. The lower is for the circuit shown; the higher, for a modified circuit. The last because the author (Mr. J. L. Linsley Hood), suspects that sufficient recording bass lift is not always given to accord with RIAA standards, and he consequently changed some values of his feedback components to get a flatter response down to 25 Hz with a steeper roll-off as a protection against rumble.

These changes were as follows: R5-470 , R6-.. $1 \cdot 5 \mathrm{k} \Omega, \mathrm{Cl}-0.47 \mu \mathrm{~F}, \mathrm{C} 3-6,800 \mathrm{pF}$ and $\mathrm{C} 6-6,800 \mathrm{pF}$.
These modifications reduce the gain, and he has thus added a sub-circuit that we can now include in our armoury-the floating emitter, collector-follower. We show his addition in Fig. 72.


Fig. 72 : A floating emitter collector-follower stage added to compensate for loss of gain.

Coping with the outputs of both magnetic and ceramic pick-up cartridges may seem a bit ambitious and, as done commercially, is not always very effective. But one can do it by switching those networks, ' $A$ ' and ' $B$ ' of our Fig. 69.

A ceramic cartridge normally likes to 'see' an impedance of a megohm or more at the amplifier input and as it is a capacitative device will suffer from low-frequency loss if this input is reduced. Hence the poor performance of many cheap record players, which have to suffer the design constrictions of transistor amplifiers with high input impedance, while retaining the best possible gain and noise performance. By using the virtual earth configuration, one gets over this problem neatly and the three suggested sub-circuit alterations by Mr. Hood are shown in Fig. 73. Here we have (a) a network that will retain the curve sensibly level down to about 30 Hz , with the bass roll-off now made better by halving the values of C4 and C5 as well. And (b), a change to network ' $B$ ', while ' $A$ ' is as in the first modification. This is a suggestion by the author to obtain a 6 dB /octave rise, followed by a level response, making a 'platform' over the portion of the replay curve of Fig. 68 that is fairly level from around 1 kHz to around 2 kHz .

To get even more treble response, without nasty peaks, i.e., to give this same 'platform' effect to a 12 dB level after about 4 kHz , (c) is suggested. The reason for these changes is to equalise for the 12 dB drop in voltage anticipated when an RIAA recording (having velocity characteristics) is replayed with a displacement-sensitive device, such as a piezo-electric cartridge. As you can see, the modification entails shunting part of the input resistor with a small capacitor.


Fig. 73: Circuit changes to permit a ceramic cartridge to be fed into the same amplifier with (a) level response above 35 Hz (b) a $6 d B$ lift from 1 to 2 kHz and (c) a $12 d B$ lift at $6 d B$ loctave, followed in each case a level response.

This, finally, brings me to the point that Mike asked me to make after last month's contribution had made its way irrevocably to the printers, viz., a capacitor shunted across the feedback resistor will give treble reduction while if it is across the input series resistor it gives treble lift, as in this previous example.
Just thought you'd like to know... !

## TO BE CONTINUED

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## GENERAL PURPOSE AMPLIFIER <br> Model T80/100 70-100 Watts Output Power

Four individually controlled inputs plus Master volume control. Bass and Treble Controls providing both 'lift' and 'cut'.
Compact size, robust construction. Ideal for clubs, hotels, restaurants, schools etc. Inputs for almost any type of microphone

## GENERAL PURPOSE GROUP/DISCO AMPLIFIER Model T80/100D

## 70-100 Watts Output Power:

Three individually controlled inputs plus Master volume control. Bass and Treble Controls providing both 'lift' and 'cut'. Compact size. Robust construction. Ideal for discotheques, clubs, hotels, schools, etc. Inputs for most types of microphones. Facilities for headphone monitoring with changeover switch from input (1) to input (2).

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| 040 | 10 Dual Transistors 6 lead TO-5 2N2060 ............. |  |
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| 141 | 25 | RF Germanium Transistors TO-5, OC45, NK T72 | U42 10 VETF Gernuanium PNP Transistors TO-1 NKT667, AF11' U43 25 sil. Trans. Plastic TO-18 A. F. BC113/11 04420 sil. Trans. Plastic TO-5 BCI15/APN U45 7 3A SCR. T066 up to 600PIV $\qquad$

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SPECIFICATION Frequency Response Inputs : 1. Tape Head
$20 \mathrm{~Hz}-20 \mathrm{KHz} \pm 1 \mathrm{~dB}$ 3. Magnetic P. $\mathbf{V}$. $\cdot 25 \mathrm{mV}$ into $050 \mathrm{~K} \Omega$ 3. Magnetic P.U.
1.6 mV into $50 \mathrm{~K} \Omega$

All input voltages are for an output of 250 mV . Tape and P.U. input equalised to RIAA curve within $\pm 1 \mathrm{~dB}$. from 20 Hz to 20 KHz . Bass Control

Filters: Rumble (High Pass) cratch (Low Pass) Signal/Noise Ratio
Input overload Supply Dimensions
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## SPECIFICATIONS

Input sensitivities: Radio - up to 3 mV . Mag. p.u. 3 mV correct to R.L.A.A. curve $\pm 1 \mathrm{~dB}, 20$ to $25,000 \mathrm{~Hz}$. Ceramic p. $\mathrm{U}-\mathrm{up}$ to 3 mV : Aux - up to 3 mV . Output: 250 mV Signal to noise ratio: better than 70 dB . Channel matching: within 1 dB .
Tone controls: TREBLE $\pm 12$ to -12 dB at 10 KHz : BASS +12 to -12 dB at 100 Hz . Front panel: brushed aluminium with black knobs and controls.
Size: $66 \times 40 \times 207 \mathrm{~mm}$.

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## SPECIFICATIONS

Output power: 6 watts RMS continuous (12 wattspeak). $6-8 \Omega$. Frequency Response: 5 Hz to $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$. Total Harmonic Distortion: Less than $1 \%$. (Typical $0.1 \%$ ) at all output powers and frequencies in the audio band ( 28 V ) Load Impedance: 3 to 15 ohms. Input Impedance: 250 Kohms nominal. Power Gain: 90 dB (1.000.000.000 times) after feedback Supply Voltage: 6 to 28 V . Quiescent current: 8 mA at 28 V . Size: $22 \times 45 \times 28 \mathrm{~mm}$ inrent: 8 mA at 28 V . Size:
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The $Z .30$ and $Z .50$ are of advanced design using sificon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low $0.02 \%$ at 15 w ( $8 \Omega$ ) and all lower outputs. Whether you use $Z .30$ or $Z .50$ amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that $Z .50$ s and $Z .30$ may be used in a far wider range of applications.
SPECIFICATIONS ( $Z .50$ units are interchangeable with Z.30s in all applications).-Power Outputs: Z. 3015 watts R.M.S. into 8 ohms using 35 volts: 20 watts R. M.S. into 3 ohms using 30 volts.
$\mathbf{Z . 5 0} 40$ watts R.M.S. Into 3 ohms using 40 volts : 30 watts R.M.S. Into 8 ohms using 50 volts.
Z. 5040 watts R.M.S. into 3 ohms using 40 volts: 30 watts R. M.S. Into 8 ohms using 50 volts.
Frequency response: 30 to $300,000 \mathrm{~Hz} t 1 \mathrm{~dB}$. Distortion: $0.02 \%$ into 8 ohms. Signal to noise ratio: better than 70 dB unweighted. Input sensitivity: 250 mV into 100 Kohms (for 15 W into $8 \Omega$ ). For speakers from 3 to 15 ohms impedance. Size: $14 \times 80 \times 57 \mathrm{~mm}$.


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## Project 60 Stereo F.M. Tuner

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now. Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stero decoder and switchable squelch circuit for stient tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems.


SPECIFICATIONS-Number of transistors : 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz . Sensitivity: $7 \mu \mathrm{~V}$ for lock-in over full deviation. Squelch level: Typically $20 \mu \mathrm{~V}$. Signal to noise ratio: $>65 \mathrm{~dB}$. Audio frequency response: $10 \mathrm{~Hz}-15 \mathrm{KHz}$ ( $\pm 1 \mathrm{~dB}$ ). Total harmonic distortion: $0.15 \%$ for $30 \%$ modulation Stereo decoder operating level: $2 \mu \mathrm{~V}$. Cross talk: 40 dB . Output voltage: $2 \times 150 \mathrm{mV}$ R.M. S. maximum Operating voltage: $25-30 V D C$. Indicators: Stereo on; tuning. Size: $93 \times 40 \times 207 \mathrm{~mm}$.

## A.F.U. High \& Low Pass Filter Unit

For use between Stereo 60 unit and two Z.30s or 2.50 s. The unit is very easily mounted and is unique in that the cut-off frequencies are continuously variable. As attenuation in the rejected band is rapid ( $12 \mathrm{~dB} / o c t a v e$ ), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. There are two filter sections - rumble (high pass) and scratch (low pass). H.F. cut-off ( -3 dB ) variable from 28 KHz to 5 KHz . L.F. cut-off (-3dB) variable from 25 Hz to 100 Hz . Distortion at 1 KHz ( 35 V . supply) $0.02 \%$ at rated output. Operating voltage from 15 to 35 V . Current 3 mA . Size: $66 \times 40 \times 90 \mathrm{~mm}$.


## Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use PZ. 5 for normal $Z .30$ assemblies and PZ. 6 or PZ.8 where a stabilised supply is essential.
Typical Project 60 applications

| System | The Units to use | together with | Units cost |
| :---: | :---: | :---: | :---: |
| Simple battery record player | Z. 30 | Crystal P.U.. 12 V battery volume control. etc. | £4.48 |
| Mains powered record player | Z.30. PZ. 5 | Crystal or ceramic P.U. volume control, etc. | £9.45 |
| 12 W . RMS continuous sine wave stereo amp. for average needs | $\begin{aligned} & 2 \times 2.30 \mathrm{~s}, \text { Stereo } \\ & 60 ; \text { PZ. } 5 \end{aligned}$ | Crystal, ceramic or mag. P.U., F.M.Tuner, etc | £23.90 |
| 25W. RMS contimuous sine wave stereo amp. using low efficiency (high performance) speakers | $\begin{aligned} & 2 \times 2.30 \mathrm{~s} \text {, Stereo } \\ & 60 ; \text { PZ. } \end{aligned}$ | High quality ceramic or magnetic P.U.. F.M. Tuner. Tape Deck, etc. | £26.90 |
| 80W. ( 3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms) | $2 \times 2.50 \mathrm{~s}$, Stereo 60; PZ.8, mains transformer | As above | f34.88 |
| Indoor P.A. | Z.50, PZ.8, mains transformer | Mic., guitar, speakers. etc., controls | £19.43 |
| F.M. Stereo Tuner ( $\mathbf{( 2 5 ) ~ \& ~ A . F . U . ~ ( f 5 . 9 8 ) ~ m a y ~ b e ~ a d d e d ~ a s ~ r e q u i r e d . ~}$ |  |  |  |

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