PRACTICAL FEBRUARY 1973 20p 3-RANGE CRYSTAL MARKER • 9 VOLT BATTERY ELIMINATOR

General Coverage RECEIVER

23 05

PW







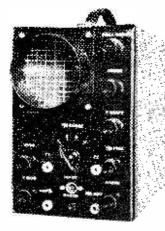
Minimum post/packing on 1 valve 7p., on each additional valve, (3p. per. valve extra) Any parcel insured against damage in transit 3p extra.

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BUILD, SEE AND LEARN step by step, we take you through all the fundamentals of electronics and show how easily the subject can be mastered. Write for the free brochure now which explains our system.

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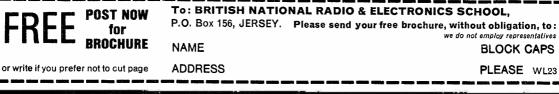
amplifiers, oscillators, signal tracer, pho-

to electric circuit, computer circuit, basic

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Build yourselfa TRANSISTOR RADIO

ROAMER 10 WITH VHF INCLUDING AIRCRAFT

10 TRANSISTORS. 9 TUNABLE WAVEBANDS, MW1, MW2, LW, SW1, SW2, SW3, TRAWLER BAND. VHF AND LOCAL STATIONS ALSO AIRCRAFT BAND

BARD LOCAL STATIONS ALSO AIRCRAFT BAND Built in Ferrite Rod Aerial for MW/LW. Retractable, chrome plated 7 section Telescopic Aerial, can be angled and rodated for peak short wave and VHF listening. Push Pull output using 600mw Transistors. Car Aerial and Tape Record Sockets. 10 Transistors plus 3 Diodes. Fine tone moving coil speaker. Ganged Tuning Condenser with VHF section. Separate coil for Aircraft Band. Volume ouloff. Wave Change and tone Control. Attractive Case in black with sliver blocking. Size $9^{\circ} \times 7^{\circ} \times 4^{\circ}$. Easy to follow instructions and diagrams. Parts price list and easy build plans 800 pt GFREE with parts). Earpiece with plug and switched socket for private listening 80p extra.

-

Total building cost £8.50

> P. P. & Ins. 50p (Overseas P. & P. £1)

ROAMER 40) (A) (3) EIGHT Mk I NOW WITH

VARIABLE TONE CONTROL

POCKET

FIVE

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7 Tunable Wavebands: MWI, MW2, LW, SWI, SW2, SW3 and Travier Band. Built in Ferrite Rod Aerial for MW and LW. Retractable chrome plated Tele-scopie aerial for Short Waves. Pub pull output using 600mW transistors. Car aerial and Tape record ockets. Selectivity avrich. 8 transistors plus 3 dods. Fine tone moving coll speaker. Air spaced ganged tuning con-denser. Volume(on)off, tuning, wave change and tone controls. Attractive case in rich chestnut shade with pold blocking. Size $9 \times 7 \times 4$ in, approx. Easy to follow instructions and diagrams. Parts Price List and Easy Build Plans 259 (FREE with parts). Earplece with plug and switched socket for private listening 309 extra.

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3 Tunable Wavebands: MW, LW, Trawler Band with extended M.W. band for easier tuning of Luxenbourg, etc. 7 stages—5 transistors and 2 diodes, supersensitive ferrite rod aerial, fine tone moving coil apeaker. Attractive black and gold case. Size of x 11 x 34 in. Easy build plane and parts price list 10p (FREE with parts).

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J Addisone Traver bandis: NWI, MWZ, LW, SWJ, BWZ, BW3 and Trawie Band. Extra Medium waveband provides easier tuning of Radio Luxembourg, etc. Built in ferrite rod aerial for MW and LW. Retractable 4 section 24 in. chrome plated telescopic.aerial for SW. Bocket for Car Aerial. Powerlui push-pull output. 7 transfors and 2 diodes, fane tone moving coll speaker. All: spaced ganged tuning condenser. Volume/on/of, tuning and wave change controls. Attractive case with carrying handle Size 9 × 7 × Min. approx. Easy to follow instructions and diagrams. Parts price list and easy build plans: 20 (FRES) with parts). Earplece with plug and switched socket for private listening 30 extra. Total building costs O 5.000 P. P.4

Total building costs £5-98 P. P. & (Overseas P. & P. £1) LIS. 45p.

3 Tunable Wavebands: MW, LW and Trawler Band. 7 stage-5 transistors and 2 diodes, territe rod aerial. tuning condenser volume control, fine tone moving coil speaker. Attractive case with red speaker grille. Size $6\frac{1}{5} \times 4\frac{1}{5} \times 1\frac{1}{5}$ in. Easy build plans and parts price list 10p (FREE with parts).

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AND 2 DIODES

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BUILD RADIOS, AMPLIFIERS, ETC., FROM EASY STAGE DIAGRAMS, FIVE UNITS INCLUDING MASTER UNIT TO

SIX

ROAMER

6 Tunable Wave-bands: MW, LW, SW1, SW2, SW3, SW1, SW2, SW3, Trawler, bandplus an extra Medium waveband for easier tuning of Luxembourg etc. Sensitive ferrite rod aerial and telescopic aerial for Short Waves.



for Blort Waves. Sin. Speaker. 8 stages-6 transistors and 2 clodes Attractive black. case with red grille, dlal and black knobs with pollshed metal inserts. Size 9 × 51 × 21 n. approx. Easy build plans and parts price list **25** (FREE with parts).

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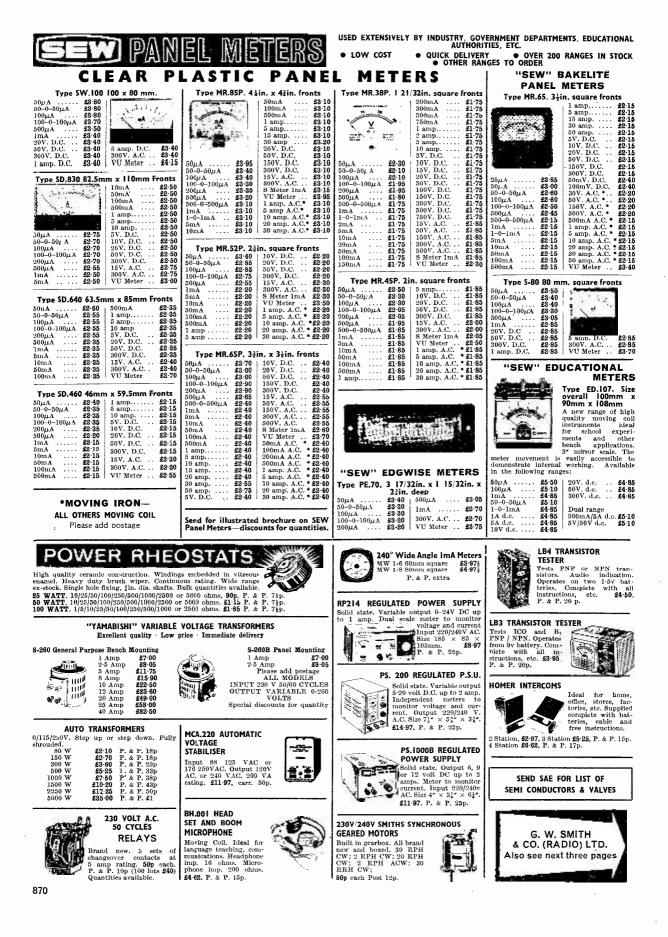
6 Tunable Wave-bands: MW, LW, SW1, SW2, SW5 and Trawier Band. Sensitive ferrite rod aerial for M.W. and L.W. Tele-scopic aerial for Short Waves. 3in. Speaker. 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with polished metal inserts. Bize 9 x 51 x 21 in. approx. Push pull output. Battery economisers switch for extended battery life. Ample power to drive a larger speaker. Parts price list and easy build plans 250 (FREE with parts).

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	CONSTRUCT. COMPONENTS INCLUDE: Tuning Condenser: 2 Volume Controls: 2 Slider Switches: Fine Tone Moving Coll Speaker: Terminal Strip: Fertite Rod Aerial: 3 Plugs and Sockets: Battory Clips: 4 Tag Boards: Balanced Armature Unit: 10 Transistors: 4 Diodes: Resistors: Capacitors: Three 4' Knobs. Units once constructed are detachable from Master Unit, enabling them to be stored for future use. Ideal for Schools, Educational Authorities and all those interested in radio construction. Parts price list and easy build plans 25p (FREE with parta).	I enclose £ please send items marked. ROAMER TEN C ROAMER SEVEN ROAMER EIGHT TRANS EIGHT TRANSONA FIVE ROAMER SIX POCKET FIVE EDU-KIT Parts price list and plans for	
seas P. & P. £1)	All parts including £5.50 P.P. & Case and Plans	Name	
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πč D.C. 0/2-5/10/50/250/1000 V. A.C. 0/10/250µA/2-5/25/250 MA/ 10 Amp. D.C. 10 Amp A.C. 0/20K/200K/ 2MEG/20 MEG. - 20 + 62db. **£12-50.** P. & P. 25p.

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DC Current $100wA_1/10/$ $100mA_1A.$ Resistance 300 ohms/3/30/300K/3m $\Omega.$ Complete with batteries. test leads, instructions and stardy steel carrying case. OUR PRICE **£5**:97. P. & P. 25p

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BRIDGE A new portable bridge offering ex-cellent range and accuracy at low cost. Ranges: R. $1\Omega = 11\cdot1 \mod \Omega$ 6 Ranges $\pm 1\%$ L.1 μ H -111



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+ 10 dB. (10 K o ohnwi Operation in ternal batteries Attractive 2-tone case $7\frac{3}{5''} \times 2^{*}$. Price £17.50 £17.50.



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MODEL AT201 DECADE

Frequency range 0-200KHz. Attenuator 0-111db, 0.1db step. Impedance 600 ohms. Max. input power 30dbm. Size 180×90×55mm.







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4 Bands covering 550 Kc/s - 30 Mc/s. B.F.O. Built-in Speaker 220/240v A.C. Brand new 0.0 A.C. Brand new with instructions. £15-75. Carr. 374p.



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4 Bands covering 550Kc/s-30Mc/s. FET 8 Meter. Variable BFO for SSB, Built-in Speaker, Bandspread, Sensitivity Control. 220/240v. A.C. or 12v. D.C. 12² × 44" × 7" Brand new with instructions, **\$25**. Carr. 37¹/₂ p.

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Model 350, 13" × 8" with single tweeter/crossover. 20-20,000 Hz. 15 watt RMS. Available 8 or 15 ohms. **27:25** each P. & P. 37D. Model 450, 13" × 8" with twin tweeter/crossover. 55-18,000 Hz. 8 watt RMS. Available 8 or 15 ohns. **23:62** each. P. & P. 25D.

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71^{**}. 8 ohms. 8 watt RMS. 16 watt peak. Complete with DIN lead. **\$12.95** pr. Carr. 50p.



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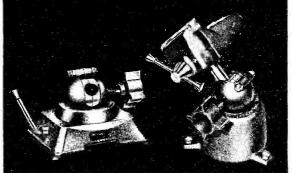
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TOTAL COST OF COMPLETE COMPONENTS ONLY £27.85-POST FREE !

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SPECIAL CONTEMPORY STYLE SLIMLINE METAL SPECIAL CONTEMPORY STYLE SLIMLINE METAL CASE WITH WOODEN END CHEEKS IS NOW AVAILABLE FOR THIS AMPLIFIER-DETAILS IN-CLUDED WITH ALL LISTS, OR AVAILABLE ON RECEIPT OF S.A.E.

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30 Watts (R.M.S.) per Channel into 8 Ohms !! Total Harmonic Distortion 0.02% !!

Frequency Response (-3 dB) 20Hz-100kHz !! This high quality Stereo Amplifier for the Home Constructor was described in a series of articles in "Practical Electronics", from November 1970 to March 1971. It is now recognised as practically the ultimeter in High Electronic the ultimate in High Fidelity and is certainly equal to anything one can buy, no matter what the cost, but it is well within the capabilities of the ambitious constructor.

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SK.1 KI1

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contains 15 Watt miniature iron fitted

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7 - 3

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CENTRIFUGAL BLOWER Miniature mains driven blower centrifugal type blower unit by Woods, powerful but specially built for quiet running-driven by cushloned induction motor with specially built low noise bearings. Overrall size of blower is approx. 4%" × 44" × 4", When mounted by its flange air is blown into the combinent but to avoid air out month if from the X 4. When invited by its lange an issue of the continued by the centre using a clamp, ideal for cooling electrical equipment, or fitting into a cooker hood, film drying cabinet or for removing flux smoke when soldering etc. etc. A real bargain at 21-35.

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This is a fully screened intermediate frequency module for amplification and detection of 1.m. signals at 10^o TMHz and a.m. signals at 470K Hz. The first stage is used as an i.f. amplifier for 1.m. and a self oscillating mixer for a.m. operation, in conjunction with an external oscillator coil 35p each. 10 for 27.85.

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HONEYWELL THERMOSTAT Made by Honeywell for normal air temperatures 40°-s0°F (5-29°C). This is a precision instrument with a differential which can be adjusted to better than 1-9°F. A mercury switch breaks on temp. rise—the witch is clear plastic windows thermometer above and on conduit box or directly on wall. Price \$1.25 each or ten for \$11.25.

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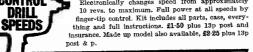
RADIO STETHOSCOPE Easiest way to fault find—traces signal from serial to speaker—when signal stops you've found the fault. Use it on Radio, TV. amplifier, anything—com-plete kit comprises two special transistors and all parts inclu-tions where tuba and constal ding probe tube and crystal earpiece. £2--twin stetho-7

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3 PIN REVERSE PLUG & SOCKET Our Ref. PSO2. For bringing live leads to equip-ment. All brown bakelite construction, rated 10A 250v. Pirce 35p per pair. 13 AMP JUNCTION BOXES

Ref. No. 803. Again a flat ended toggie. Made by Arrow. A 3 position double pole changeover switch. centre off for auto aerials, reversing motors etc. **30p** each.

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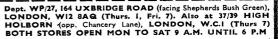
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SA1000 QD 210 Quadraphonic decoder. A 800 Quadraphonic pre-amp. QC 800 Quadraphonic pre-amp. M 800 Quadraphonic pow. amp. Reverberation 202w. RANK ROTEL 210	42 · 85 188 · 60	29 · 95 122 · 95
QC 800 Quadraphonic pre-amp	129 · 98 160 · 84	84 · 95 104 · 95
CM 800 Quaraphone pow, amp. Reverberation 2020 RANK ROTEL 210 RANK ROTEL 210 RANK ROTEL 610 RANK ROTEL RA 1210 RANK ROTEL RA 1210	54 · 95 34 · 90	35-95
RANK ROTEL 210	34 90 52 00 78 50	23 50 34 95
RANK ROTEL 610 RANK ROTEL RA 810	105.50	51 · 95 72 · 95
RANK ROTEL RA 1210	129.00	89 95 49 25
ROGERS Ravensbourne Ravensbourne (cased) Ravensbrook Mk. II	64 · 50 69 · 50 50 · 50	49 · 25 53 · 95 38 · 95
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SINCLAIR 2000	35∙00 45∙00	28·95
BROJECT 605 SOLARVOX 20. 10 watts. RMS per	29.95	18 - 90
SOLARVOX 30, 15 watts RMS per	39-95	24 - 95
channel SOLARVOX AM106 2 x 8 watts. RMS plus MATRIX 4 channel. SOLARVOX AM318 2 x 18 watts. plus MATRIX 4 channel TANDBERG TA300 TELETON SAQ 2068	49-95	32.95
SOLARVOX AM318 2 x 18 watts.	28·45	
TANDBERG TA300	41 · 38 69 · 90	26 · 95 54 · 95
307		20 50 20 50
GA 202 15 watt. RMS per channel WHARFEDALE Linton amplifier.	45 · 75 65 · 00	28 95 41 95
All take both ceramic and magne	etic carl	ridges.
TUNERS AMSTRAD Multiplex 3000 FM *ARMSTRONG 523 AM/FM ARMSTRONG 524 FM PULCI FMT 7 FM DULCI FMT 7 FM MCT VTE AM/FM LEAK DULCI FM DULCI FM DULCI FMT 7 FM DULCI FM DU	39-95	28 · 95
*ARMSTRONG 523 AM/FM *ARMSTRONG 524 FM	52 · 68 40 · 97	40 · 95 31 · 95
ARMSTRONG M8 Decoder *DULCI FMT 7 FM	9 · 50 24 · 43	6-95 17-50
DULCI FMT. 7S Stereo	32 · 89 75 · 74	24 · 50 35 · 95
JVC Nivico MCT V5E AM/FM	86 · 89 122 · 42	69 95
LEAK Delta FM	79.50	99-95 57-95
METROSOUND FMS 20	89 · 50 54 · 92	69 · 95 38 · 75
METROSOUND FMS 20 PHILIPS RH 690 PHILIPS RH 621	48 · 50 109 · 00	31 · 95 89 · 95
PIONEER TX500A AM/FM	75 · 52 104 · 57	50 · 95
PHILIPS RH 621 PIONEER TX500A AM/FM PIONEER TX600 AM/FM RANK ROTEL 320 RANK ROTEL 620	59 . 50	73 · 95 42 · 95
RANK ROTEL 620 ROGERS Ravensbourne Chassis Ravensbourne in Teak Case	93 · 50 57 · 95	67 · 95 43 · 95 47 · 95
Ravensbrook Chassis	62 63 42 14	31.95
Ravensbrook (case)	48.00 45.00	36 · 95 29 · 95
	45.00	29 95 17 50
Project 60 Tuner (stereo) All above Tuners are complete wir Decoder except where starred	th MPX	Stereo
TUNER/AMPLIFIERS AKAI CR80T FM/AM Tuner Ampli- fier with built in Eight Track Tape	140.04	80.07
Recorder AKAI AA8500 AKAI 6200	149 ·84 249 · 00	89 · 95 179 · 85 75 · 95
AKAI 6300	105.00 137.50	79 95
AKAI 6600 ARENA 2600	159-00 111-30	108 95 59 95
ARMSTRONG M8 Decoder	9.20	6 · 95 69 · 95
ARAI 8200 AKAI 8600 ARENA 2600 ARENA 2600 ARMSTRONG 525 ARMSTRONG 525 CARLTONG 526 CARLTONG 526	90·14 102·72	77.95
track player and speakers GOODMANS Module 80, 35w. RMS	69·95	39 95
	93-00 168-00	69 95 127 95
Module 110 FM/MW/LW/SW/	119.00	91 - 95
100w. RMS	139.00	105-95

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TIMPO AND IFIEDO		Price	Price
TUNER/AM PLIFIERS-c GOODMANS Module 110,	continued Compact	245.00	187.50
JVL NIVICO VK 5500/5503 /	AM/FM	96 96	81 . 95
VR 5521L AM/FM and SE 4VR 5414 Quadraphonic KYOTO 1000 AM/FM Tune fier with built in Stereo	EA	175.00 212.00	146 · 95 179 · 95
KYOTO 1000 AM/FM Tune	r/Ampli-	212.00	119.95
fier with built in Stereo	Cassette		
Recorder. Complete w	han two	85.00	61 - 95
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PHILIPS RH 790		134.00	74 95
PHILIPS RM /20	•••••	215 · 00 140 · 53	179 · 95 98 · 95
SX626 SX727		192.49	134 35
		231 · 74 297 · 20	162 · 95 208 · 95
QX 8000 Quadraphonic ROGERS Ravensbrook Ch		286.24	199 95
ROGERS Ravensbrook Ch	assis	96·57	73·95
ROGERS Ravensbrook (cas	sed)	105 · 35 67 · 93	78 · 45 45 · 95
ROTEL RX 150A		69 90	50 · 95 65 · 95
ROTEL RX200A		89·50 107·50	65-95 78-95
ROTEL RX 600A		149 00 189 50	109 · 95 139 · 95
ROTEL RX 800A			139 · 95 94 · 95
ROGERS Ravensbrook (cas ROTEL RX 150 ROTEL RX 150A ROTEL RX200A ROTEL RX 400A ROTEL RX 600A ROTEL RX 600A ROTEL RX 800A SOLARVOX TAM 1105 2) PMS AW/EM Multiplas	5 watts	129.50	34.30
Audital maniples	c comp		
		38.50	29.95
TANDBERG 1171 MPX		103.03	84.95
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TANDBERG TR1000 FM ME	MPY	156 · 00 169 · 00	129 · 60 139 · 95
With 2 speakers and 1 Matrix 4 channel TANDBERG 1171 MPX TANDBERG TR1000 MPX TANDBERG TR1000 FM Mi TANDBERG TR101 AM/FM WHARFEDALE LINTON V TELETON R8000 AM/FM TELETON R8000 AM/FM	VE40	115-00	95-95
TELETON CR55	•••••	125·26 42·16	68 · 50 21 · 95
TELETON R8000 AM/FM All the above take mag	netic car	tridaes	excent 1
Teleton R8000 which takes MPX Stereo Decoder with	ceramic o	nly. All i	nciude
MPX Stereo Decoder with strong where M8 decoder i	the exce	eption o	r Arm-
TUDNTABLES			
CONNOISSEUR BD1 kit		13.34	10.95
CONNOISSEUR BD1 kit CONNOISSEUR BD2 Cha CONNOISSEUR BD2 P/C/3 GARRARD SP25 Mk. III	ssis	32.71	25.95
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GARRARD AP76		28 • 44	17.25
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GARRARD Zero 100A GARRARD Zero 100S GARRARD WB4 Base Mk. Zero 100 and Zero 100S	11Z to fit	57.42	38-95
The following Turntah		57 · 42 52 · 83 6 · 55	38-95 36-95 4-95
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The following Turntab basc, plinth, plastic of Fully wired and ready	les are co cover and for use, A	57 · 42 52 · 83 6 · 55	38-95 36-95 4-95
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The following Turntable base, plinth, plastic of Fully wired and ready f prices. GARRARD SP25 Mk. 1 with Goldring G800 McDONALD MP60 with SHURE M 44/2 McDONALD MP60 with SHURE M 44/2 McDONALD MP60 with SHURE M 44/2 McDONALD HT70	les are co cover ani for use, A 111 Special Special Special	57.42 52.83 6.55 mplete t d cartriu li at spe Price £1 Price £1 Price £1	38-95 36-95 4-95 with dge. cial 8-50 7-50 8-95 9-95
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The following Turntables, base, plinth, plastic of Fully wired and ready 9 prices. GARRARD SP25 Mk.1 with Goldring G800 McDONALD MP60 with SHURE M 44/7 McDONALD MP60 with SHURE M 44/7 McDONALD MP60 with SHURE M 44/8 McDONALD HT70 with GOLAND 580 GARRARD AP76 with Shure M75E1 GARRARD AP76 with Shure M75E1 GARRARD 2025 with Sonotone 9TAHC GOLDRING GL 75 with G800 THORENS 159 AB con	les are co cover anni for use. A Special Special Special Special Special Special Special Special Special	57:42 52:83 6:55 mplete d cartrid d cartrid Price £1 Price £1 Price £2 Price £2 Price £3 Price £3 Price £3 Price £3 Price £3 Price £3	38-95 36-95 with fige. icial 8-50 7-50 8-95 9-95 55-50 8-50 2-50 2-50 2-75 99-50
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SPEAKERS 26:00 13:95 AMSTRAD 138 (pair) Teak 26:00 13:95 AKAI SW 155. 64:50 44:95 B and W Model 70 159:50 109:95 B and W DM2 69:96 77:96 B and W DM2 69:96 77:96 B and W DM3 (pair) 47:94 39:95 CELESTI'IN COUNTY (pair) 47:94 39:95 Ditton 10: (pair) 57:60 26:00 Ditton 12: 57:00 26:00 Ditton 44 56:00 39:96 GOODMANS Minister Pair 49:20 39:95 GoODMANS Minister Pair 57:92 39:40 Magitser 67:40 48:90 Magitser 67:40 48:90 Magitser 57:0 22:950 Goodwood 55:00 38:95 Dimension 8 22:44 44:495 Dimonsion 8 22:44 44:495 Dimension 8 22:44 44:495 Dimension 8 22:44 44:495	SME 3012 With S2 Shell SME 3012 HE with S2 S	Shell	35.81	26 50
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AKAI SW 155. 64 *50 44 *95 B and W Model 70 159 *50 109 *95 B and W DM2 69 *99 47 *50 B and W DM3 69 *99 47 *50 B and W DM4 69 *66 37 *95 B and W DM5 (pair) 59 *48 43 *95 Ditton 120 (pair) 56 *40 38 *50 Ditton 15 37 *40 26 *00 Ditton 14 55 *50 04 *3 *55 Ditton 44 55 *00 42 *50 Ditton 44 55 *00 70 *35 *60 Ditton 44 57 *40 38 *50 Double Maxim 67 *40 48 *00 Magitster 65 *63 42 *50 Double Maxim 67 *40 48 *00 Magitster 57 *60 33 *85 Dimension 8. 21 *44 48 *95 Dimension 8. 21 *44 48 *95 Dimension 8. 21 *44 48 *95 Dimension 8. 22 *95 56 *10 *37 57 *50 Stopeaker system (pair) 37 *60 38 *50 18 *55 KN900 3-speaker system (pair)		Teak	26.00	13.95
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Magnister 65:83 42:90 Double Maxim 67:40 48:40 Mezzo 3 35:70 23:45 Magnum K2 62:00 36:95 Goodwood 55:00 36:95 Dimension 8 72:44 44:95 KN800 3-speaker system (pair) 15:86 11:93 KN800 3-speaker system (pair) 31:86 15:95 KN1000 3-speaker system (pair) 30:60 37:55 EAA K 150 (pair) 50:00 37:55 EAA K 150 (pair) 50:00 37:55 Duplex 15 32:00 21:95 Duplex 15 55:04:67:22:95 SiNCLAIR Q16	Havant (pair)	Pair	57.12	35.95
Goodwood 50 00 30 32 Dimension 8			67.40	48.00
Goodwood 50 00 30 32 Dimension 8	Mezzo 3	•••••	35.70	23 · 45 29 · 50
System (pdf) 25 bit 25 bit 25 bit 26 bit 27 bit KN800 3-speaker system (pair) 31 60 18 65 27 65 KN100 3-speaker system (pair) 31 60 18 65 27 65 KN1100 3-speaker system (pair) 27 50 14 65 47 65 KN1100 3-speaker system 25 00 37 50 46 55 LEAK 150 (pair) 50 60 37 55 56 56 60 37 55 LINEAR 10 weit Teak (Pair) Sp. Price 38 50 47 65 50 MARSDEN HALL Annexe 100 30 00 77 95 50	Goodwood		55.00	36 95
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202 21-50 14-75 Duplex 15 32-00 21-95 Duplex 15 56-00 37-50 DUPLEX 15 56-00 37-50 DINEER CS53 46-72 29-95 SINCLAIR Q16 8-98 6-50 TANDBERG Tan 7 29-50 23-60 Tan 11 (pair) 40-00 31-95 TL 12 teak (pair) 71-50 56-95 TL 12 teak (pair) 71-50 56-95 TL 25 Teak (pair) 71-50 56-95 TELETON 8000 (pair) 21-95 11-95 TG300 (pair) 55-95 29-95 WHARFEDALE Denton Mark II 55-00 23-75 Iriton 111 (pair) 55-00 23-75 Dovedale 3 Mark II 47-50 22-95 Unit 3 speaker kit 12-70 8-95 Unit 3 speaker kit 12-70 8-95 Unit 3 speaker kit 12-00 8-95 Unit 3 speaker kit 12-95 9-12 CHASSIS SPEAKERS 9-12 6-95	KN1100 4-speaker sys KN1600 3-speaker sys	tem (pair) stem	40 · 80 25 · 20	23 · 95 14 · 95
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Tail 1 (Gail) 500 44.53 TL 12 Teak (pair) 71.50 56.95 TL 25 Teak (pair) 71.50 56.95 TELETON 8000 (pair) 21.08 11.95 THORPE GRINVILLE TG100 (pair) 21.08 11.95 TG200 (pair) 41.95 24.95 TG200 (pair) 41.95 24.95 TG200 (pair) 41.95 24.95 TG300 (pair) 41.95 24.95 TG300 (pair) 41.95 24.95 TG300 (pair) 55.95 29.95 WHARFEDALE Denton Mark II 20.08 41.95 Linton Mark II (pair) 52.00 37.50 Dovedale S Mark II 46.95 22.95 Unit 3 speaker kit 19.00 12.95 Unit 3 speaker kit 19.00 12.95 Unit 3 speaker kit 27.50 87.75 CHASSIS SPEAKERS 600DMANS Twin-axiom 8 9.12 6.95 Twin Axiom 10 5.97 24.64 41.93 Audiom 15P 21.00 14.60 32.04 Audiom 16P 5.97 4.50 3.20	202		21.50	14 . 75
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(pair) 42:00 28:95 Linton Mark II (pair) 52:00 37:50 Triton 111 (pair) 65:00 46:95 Meiton Mark II 35:00 23:75 Dovedale 3 Mark II 47:50 32:25 Rosedale 69:00 44:95 Unit 3 speaker kit 12:50 8:95 Unit 3 speaker kit 12:50 8:95 Unit 4 speaker kit 27:50 18:75 CHASSIS SPEAKERS GOODMANS Twin-axiom 8 9:12 6:95 Twin Axiom 10 10:06 7:50 Audiom 12P 13:00 9:15 Audiom 10P 5:97 24:45 Audiom 14P 3:570 24:45 Audiom 100 40 watts din. 12:00 4:60 3:20 Axent 100 6:90 Audiom 16P 3:59 9:50 3:20 3:260 Crossover network X0/950 7:77 5:45 WHAPEFEDALF IF NERVERS 13:50 9:50 3:30 3:30			41 95 55 95	24 · 95 29 · 95
Melton Mark II 35:00 23:75 Dovedale 3 Mark II 47:50 32:25 Rosedale 69:00 44:95 Unit 3 speaker kit 12:50 8:95 Unit 4 speaker kit 19:00 12:95 Unit 5 speaker kit 19:00 12:95 Unit 5 speaker kit 19:00 12:95 Unit 5 speaker kit 19:00 12:95 CHASSIS SPEAKERS 60:00 MANS Twin-axiom 8 9:12 6:95 Twin Axiom 10 10:06 7:50 18:75 Audiom 10P 5:97 4:15 Audiom 12P 13:00 9:15 Audiom 12P 13:00 9:15 4:05 3:20 4:45 Audiom 18P	(pair)	on Mark II	42·00	28 · 95
Melton Mark II	Linton Mark II (pair)		52 00 65 00	37 · 50 46 · 95
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CHASSIS SPEAKERS 9-12 6-95 GOODMANS Twin-axiom 8 9-12 6-95 Twin Axiom 10 10-06 7-50 Axiom 401 17-68 11-95 Audiom 8P 5-49 4-15 Audiom 10P 5-97 4-60 Audiom 12P 13-00 9-15 Audiom 15P 21-00 14-60 Audiom 16P 35-70 24-45 Audiom 100 6-90 8-35 Audiom 16P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 100 6-90 4-80 Audiom 160 40 8-35 Audiom 160 40 8-35 Audiom 170 3-20 77 Audiom 100 6-90 4-80 Midax 650 13-59 9-50 Midax 650 7-77 5-45 WHAPEFEDAL FE N. Ranzer/RS/NDP 777	Rosedale		69.00	44 . 95
CHASSIS SPEAKERS 9-12 6-95 GOODMANS Twin-axiom 8 9-12 6-95 Twin Axiom 10 10-06 7-50 Axiom 401 17-68 11-95 Audiom 8P 5-49 4-15 Audiom 10P 5-97 4-60 Audiom 12P 13-00 9-15 Audiom 15P 21-00 14-60 Audiom 16P 35-70 24-45 Audiom 100 6-90 8-35 Audiom 16P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 100 6-90 4-80 Audiom 160 40 8-35 Audiom 160 40 8-35 Audiom 170 3-20 77 Audiom 100 6-90 4-80 Midax 650 13-59 9-50 Midax 650 7-77 5-45 WHAPEFEDAL FE N. Ranzer/RS/NDP 777	Unit 3 speaker kit		19.00	12 95
Axióm 401	Unit 5 speaker kit	••••••	27.50	18.75
Axióm 401	CHASSIS SPEAKER GOODMANS Twin-axi	SI	9 · 12	6.95
Audiom 10P 5-57 4-50 Audiom 12P 13:00 9-15 Audiom 12P 35:70 24-45 Audiom 12P 4:50 3:20 ARU 172 4:50 3:20 Axent 100 6:90 4:80 Midax 650 13:59 9:50 Attenuator 3:73 2:60 Crossover network X0/950 7:77 5:45 WHAPEFEDALF IF NETWORK X0/950 3:30		• • • • • • • • • • • • •	10-06 17-68	7.50
Audiom 12P 13-60 9-13 Audiom 12P 14-60 Audiom 13P 12-00 14-60 Audiom 13P 12-00 14-60 Audiom 100 40 watts din. 12-00 8-35 ARU 172 44-65 ARU 172 6-90 4-80 Midax 650 13-59 9-50 Attenuator 3-73 2-60 Crossover network X0/950			5.49	4.15
Axent 100	Audion 10F		13.00	9.15
Axent 100	Audiom 18P		35.70	24.45
Axent 100 6:90 4:80 Midax 650 3:59 9:50 Attenuator 3:33 2:60 Crossover network XO/950 7:77 5:45 WHA PEFFDAJ E Sin Ronze/RS/DD 4:75 3:30	Audiom 100 40 watts ARU 172		4.50	8·35 3·20
WHARFEDALES in Bronze/RS/DD 4.75 3.30	Axent 100		6.40	4 80
WHARFEDALES in Bronze/RS/DD 4.75 3.30	Attenuator	1/050	3.73	2.60
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THE HY41

The HY41 supersedes the popular HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically 0.05% at 1KHz into 8 ohms!) and is electronically and mechanically compatible with the HY40.

With this important improvement the HY41 retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi-Fi but also for public address systems and industry.

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent years.

OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts

R.M.S. continuous. LOAD IMPEDANCE: 4–16 ohms. INPUT IMPEDANCE: 30K ohms at 1KHz. VOLTAGE GAIN: 30db at 1KHz

TOTAL HARMONIC DISTORTION: less than 0.15% (typical 0.05%)

at 1KHz FREQUENCY RESPONSE: 5Hz-50KHz + 1db. SUPPLY VOLTAGE: + 22.5volts D.C. SUPPLY CURRENT: 0.8 amps maximum.

PRICE: inc. comprehensive manual, P.C. board, five extra components and P. & P .:-MONO: £4.90 STEREO: £9.80

UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an integrated pre-amplifier circuit

Supplied with the HY5 are two stabilizing capacitors and by the addition of volume, treble and bass potentiometers it is ready for use. Internally the HY5 provides equalization for almost every conceivable input, the

desired function is achieved by use of a multi-way switch or by direct interconnection, Two distinctive features of the HY5 are its inbuilt stabilization circuit, allowing it to be run off any unregulated power supply from 16–25 Volts and a balance circuit

which, when linked by a balance control to a second HY5, forms a complete stereo pre-amplifier.

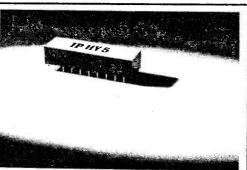
Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in con-junction with the HY41 and PSU45 forms a completely intergrated system.

INPUTS

 $\begin{array}{c} \mbox{Magnetic Pick-up (within \pm 1db R1AA curve)} \\ \mbox{2mV. 47K } \Omega \\ \mbox{Tape Replay (external components to suit} \\ \mbox{head}). \ \mbox{4mV. 47K} \Omega \end{array}$

Microphone (flat) 10mV. 47K Q

OUTPUTS Main Pre-amp output 500mV. Direct tape output 120mV. ACTIVE TONE CONTROLS (Bexendall) Treble + 12db. Bass + 12db. INTERNAL STABILIZATION Enables the HY5 to share an unregulated supply with the Power Amplifier. SUPPLY VOLTAGE



SUPPLY CURRENT 6mA approx. OVERLOAD CAPABILITY better than 26db on most sensitive input infinite on tuner and auxl. OUTPUT NOISE VOLTAGE: 0.5mV.



POWER SUPPLY PSU45

MONO: £3.60

The versatile P.S.U.45 is designed to supply your HY41's +HY5's in stereo or mono format.

STEREO: £7.20

Specification

16-25 volts PRICE:

> Input: 200-240 Volts. Output: ± 22.5 Volts at 2 amps. Overall Dimensions: L. 7"; D. 3.8"; H. 3.1"

PRICE: £4.50 inc. P. & P.

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FEBRUARY 1973

Letter from your new Editor

T the time of going to press we have seen the last of A the Apollo series of manned space flights to the moon. Fifteen years ago when the USSR launched Sputnik 1, followed by the U.S. launching of Explorer 1, little did many people imagine what space research could do to provide further knowledge and skills for everyday living. One could comment in depth on this, but rather than indulging yet again in retrospect, let us look to the future.

RACTICAL

NASA space programmes are to be directed towards space laboratories in which man can examine the influences of near sterile conditions on terrestrial activities. Already it is expected that crystal growth in a space laboratory will be tried, so perhaps we who have a particular interest in semiconductor technology will again reap the benefits of such an exercise.

On a more domestic note, following the celebrations of 50 years broadcasting, further progress is being made to improve communications: The IBA have now used their colour programmes digital converter in service; stereo is established on Radio 2 (v.h.f.), although there is apparently some unexplained mono material intruding; the planning of commercial radio is well underway; the third Goonhilly dish has increased the international telephone capacity to handling almost half of Britain's 60 million calls by satellite; the first UK i.c. radio chip receiver design for home con-structors has been published; the BBC has announced the CEEFAX news service for television.

We shall be taking a closer look at the world of communications inside and outside the home; giving you up-to-date information on components and equipment; extending our popular ranges of simple-to-build projects; encouraging readers to participate with us in do-it-yourself communications.

Many of you will have followed the writings of your new editor elsewhere. To PW newcomers we welcome you to the club; we hope to provide plenty to stimulate your interest in future issues. In the meantime, we are always interested to hear your views on matters appropriate to the magazine. We are also convinced that a great deal of talent exists among the readership in designing projects, as is evident from our correspondence. If you feel that you would like to show others what you do, drop us a line; better still, how about writing it up into an article.

M. A. COLWELL—*Editor*

THE MARCH ISSUE WILL BE **PUBLISHED ON FEBRUARY 2nd**

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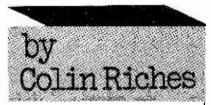
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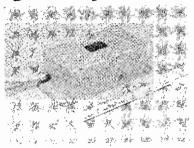
NHWS

KW catalogue

A new catalogue has just been released by KW Electronics Ltd., Specifications and pictures of KW transmitters, receivers and associated equipment are shown and a price-list is included.

Free copies of this catalogue may be obtained by writing to KW Electronics Limited, Dartford, Kent.

Ignition system



Future Techmatics announce a new low-cost capacitive discharge ignition system, named "Highwayman" and designed for both the fleet owner and the private motorist. The unit priced at £9.90 plus 35p postage is claimed to give fuel economy, improved performance and excellent starting under adverse conditions.

Fitting is simple with only three wires to connect. Using the conventional coil and contact breakers, "Highwayman" produces well over 30,000 volts to the spark plugs with a rise time of 2-6 microseconds. Maximum operating rate is 600 pps. Battery drain is 1.5 amps. The contact breaker resistance limit is 25 ohms and current and voltage at contact breakers is 0.15 amps at 12V.

Further information on the range of electronic ignition systems and other devices, may be obtained from Future Techmatics Limited, Waldeck House, Waldeck Road, Maidenhead, Berks.

Solder feed

The Mark 3 Anextra includes several improvements to simplify its main function of eliminating the need for "three hands" when soldering. The reel of solder, 18 to 22 gauge is contained in the pistol grip which is easily attached to most types of soldering iron.

The maximum 4oz. reel of solder is easily changed. The amount of solder fed by each pressing of the trigger is quickly adjusted to suit the joints being made. The operator thus holds

Working /MDS

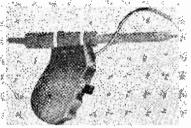
Who ever heard of a radio Amateur going mobile on a dogsled?

I didn't believe it at first but here's the full story:

Having supplied quantities of radio equipment to the South African Antarctic Expedition, Racal Electronics is naturally in fairly close touch with events and told us of the claim by one of the Expedition's members to have effected the world's first radio contact (QSO) by an amateur from a dog-sled mobile installation. The QSO was achieved on 7MHz between the sled in Antarctica and a station in South Africa. Racal has supplied the Expedition with a number of TR.28 h.f. transceivers which it uses for mobile applications.

The Expedition's base station (call sign ZS1ANT) which is equipped with Racal transmitter and receiver, is in the charge of Frank Schneider, a radio ham who operates most evenings between 1600 and 1900 GMT on s.s.b. at about 14.30MHz (call sign ZS6GE). As Antarctica is classed as a separate continent for many amateur radio certificate awards. a contact with Frank is considered a rare achievement and so his QSL cards confirming radio contact are in great demand among the world's radio amateurs.

If any U.K. hams manage to contact ZS1ANT, the address for QSL cards is 5 Prinshof Street, Pretoria, South Africa, or via the SAARL QSL Bureau.

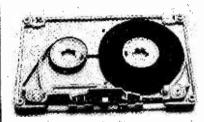


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both the iron and solder in one hand, being free to hold the work with the other hand.

Supplied with a loz. reel of 60/40 22 s.w.g. solder, with simple instructions, the Anextra is £3.75 post free U.K., direct from the makers. If you send an s.a.e. you can obtain a leaflet on the unit. Anextra Ltd., Chiltern Works, Rear of 77/78 Chiltern View Road, Uxbridge, Middx.

New Mechanics



The range of "LH" (low, noise high output) ferric oxide compact cassettes from BASF is available with the patented Special Mechanics (SM) developed by BASF technicians in West Germany.

The Mechanics comprise two plastic tusks and a roller system which together guide the tape on and off the spools. They ensure constant free running of the tape and eliminate jerking caused by static.

The improvement in tape running is most noticeable with C120 cassettes which, because of their extreme tape length of over 56 feet and thinness, are prone to running difficulties.

Recommended retail prices, including purchase tax, of the LH SM cassettes are 81p (C60), £1·11 (C90) and £1·51 (C120). BASF United Kingdom Limited, P.O. Box 473 Knightsbridge House, 197 Knightsbridge House, London, S.W.7 ISA.



Ronson Blowtorch



Ronson Products Ltd., the people that make the lighters and shavers recently let me have a look at their blowtorch.

It's hardly the sort of unit you would use on a transistor p.c. board or anything requiring delicate soldering but for heavy soldering jobs, it's ideal.

With its micro-adjustment to give a precision choice of flame size and heat intensity, the Blowtorch when used with its copper soldering tip can undertake relatively fine soldering jobs on metal, wire splices, pipes and tubing, etc. It's ideal, too, for bending or fashioning glass, metal tubing and rod and for all types of hand forging, shrink fitting, enamelling or light brazing.

The range of Ronson Blowtorches is made up of three models. All are supplied complete with the large capacity Hi-Heat butane refill. The standard pack costs just £2.45 or with copper soldering tip at £2.79. The complete Blowtorch kit-at £3.99comes with three handy attachments (soldering tip, flame spreader and diffuser head) all neatly contained in a packaway case, as can be seen in the photograph. Ronson Products Ltd., Leatherhead, Surrey.

"Texan" Reprints

Reprints of the "Texan" 20+20W Stereo Amplifier are available.

They may be obtained by sending 35p (30p+5p postage/packing) to "TEXAN" REPRINT, c/o Chief Cashier, Practical Wireless, Tower House, Southampton Street, London WC2E 9QX.

Electrovalue cat.

Electrovalue have sent me their catalogue No. 6—already in its third printing. Including i.c. circuit and connection diagrams as well as semiconductor outlines and technical gen, the catalogue contains many other interesting items plus a purchase refund voucher for the 25p it costs to buy.

Copies can be obtained from Electrovalue Limited, 28 St. Judes Road, Englefield Green, Egham, Surrey.

Bib test cassette

Bib recently let me hear their Hi-Fi Stereo Test Cassette which is entitled, "How to get the best stereo and mono reproduction and recording".

The tape, devised by Richard Arbib, managing Director of Bib Sales is recorded by Decca using the Dolby system.

The Max Harris Jazz Trio play some specially composed pieces, illustrating tests including balance control, channel identification speaker phasing, reducing tape hiss and adjusting record volume controls.

Members of the Trio, playing six instruments are used to check cassette recorder reproduction over a wide frequency range.

Side 1 of the cassette deals with reproduction and side 2 with recording. Other advice and tests include wow and flutter, movement between channels and how to clean tape heads.

To illustrate various points, excerpts from Bach's Toccata and Fugue in D minor and Khachaturian's Spartacus are given together with excerpts from Vivaldi's "The Four Seasons" and some Gilbert and Sullivan operas to illustrate high quality sound.

This cassette represents a very useful addition to those who like me suffer from "cassette-itus" and a none too perfect stereo system.

The Bib reference for the cassette is "53" and the price $\pounds 2 \cdot 25$. The tape plays for 50 minutes, which represents an extra 25% of playing composed with a standard Musicassette. Bib Division, Multicore Solders Ltd., Hemel Hempstead, Herts.

Litesold's latest

Light Soldering Developments inform us that they have marketed two new devices. Both are for use with their ETC/1 temperature controlled and Conquerer irons.' The De-Soldering Unit (priced at \pounds .75) slips onto the iron and converts it to a selfcontained de-soldering tool.

The i.c. De-Soldering Head, at $\pounds 2.25$, slips on in place of the soldering bit to give simultaneous de-soldering of all leads of 14 and 16 way dual-in-line i.c.'s. Light Soldering Developments Ltd., 28 Sydenham Road, Croydon, CR9 2LL.



De-soldering unit

Digital Clock

The 24 hour digital clock shown on the cover this month is mains driven and incorporates an alarm buzzer. It can be obtained from Sternway Electrical Ltd., 111 Fleet Street, London EC4, for £7.95 plus 25p post and packing.

The "CQ" Column

Just a little reminder about the CQ Column. As readers write in, I put all their letters in strict order so that it is a case of "first come, first served." Requests for entries in this column now number many dozens a week and as we cannot always include a "CQ Column" in every issue of P.W. there is often some delay before the items appear.

Should there be any immediate urgency for a mention to appear, our Advertising Department will be pleased to accept "small ads" for a small charge.



E ACH issue of both *Practical Wireless* and *Television* carries articles of a constructional nature. With any hobby or interest, the greatest pleasure and reward comes from participation, having a go oneself rather than just reading about or examining the work of others. Thus these constructional features fill a very necessary need and are widely appreciated.

However, modern radio and television techniques are of a complex nature, and it is understandable, that in spite of the clear description, circuit and layout diagrams, readers sometimes get into difficulties, resulting in a written plea for help to the Editor, who in many cases refers it back to the writer of the original article. Many of these difficulties and queries though, would not arise if certain basic principles and precautions were observed. This article is designed to assist constructors prevent problems before they arise.

COMPONENTS

First we will consider the components. It is always best to obtain **all** the components at the start, if at all possible. If any are left out, to be obtained later, it means that the tags or print where they would be connected are left unsoldered and therefore adjoining components are left high and dry. If the omitted component is used as an anchoring point such as a transformer or can electrolytic, then it will not be possible to fit the associated components at all. Where a number of parts are deferred in a complex circuit it is very likely that one or more may be overlooked altogether, and considerable trouble caused in trying to get the circuit to work before the omission is discovered.

Having gathered the components together it is wise to check them for faults. Unfortunately, there is always a percentage of new parts that are defective, as each one cannot be individually checked by the maker. Small though the percentage may be, it means that somebody is going to get one, and that could be you!

Transformer windings should be checked for continuity, and then with the ohmeter switched to its highest range, check for leaks between windings, and between windings and core.

Capacitors are the most likely source of faults especially the miniature electrolytics used in transistor circuits. These should be checked for leaks; some leakage may be found using the high resistance range of the meter, but it should not be very much. If in doubt compare with other electrolytics. Any giving a substantially lower reading than the others should not be used. Of course, a lower reading will be obtained with the meter polarity connected the wrong way round; usually, the polarity on the ohms ranges is **opposite** to that for the voltage and current ranges.

While leaky capacitors are more common than open-circuit ones, the latter condition can be tested for by observing the meter needle kick when the capacitor is connected across it. The larger the value of the capacity the greater the kick, so with low values a response may not be observed. It will not be necessary to check the values on a bridge; if it is not leaky or o/c, the value will probably be right.

Assuming the colour code markings are clear it is very rare for a resistor to be of incorrect value or o/c so these can be taken for granted, especially if there is a large number and checking them all would be rather tedious. However, circuits where close tolerances are necessary such as measuring and test equipment, may demand the individual checking of appropriate resistor values. Also very high values are worth checking as these are generally less reliable than the lower ones. Resistors with dubious markings should be checked.

TOLERANCES

Sometimes queries are received about tolerances and capacitor voltage ratings showing that these limitations are not always understood.

The tolerance means the amount by which the value may deviate from that stated. Thus a 100Ω 10% resistor may be anything from 90 to 110Ω in value. Resistors may be obtained in 1%; 2%; 5%; 10% and 20% tolerances, the 5% ones being indicated by a gold ring and the 10% ones by a silver one. In most practical circuits values of resistance are worked out and then taken to the nearest preferred value, so in most cases the values are not very critical. Unless otherwise stated, the 20% tolerance will be satisfactory, but of course if closer tolerance resistors happen to be available they can be used. The closer the tolerance, the higher the cost, so it is a waste of money using close tolerance components where they are not needed.

If close tolerance is specified in the components list, then the circuit is more critical and the stated tolerance should be used. If for some reason a close tolerance component of the value required cannot be obtained, but there are some of that value with larger tolerance to hand, check these with a meter. It may be that they could fall within the required tolerance. A 20% resistor does not mean that it is **bound** to be 20% outside the stated value, only that it **may** be. The error is guaranteed to be less than 20%. Thus it is often possible to select by measurement a 20% resistor that is spot-on in value, or nearly so.

Critical circuits often contain a preset control which must be set to give a specified voltage or current. Thus the resistors associated with that part of the circuit need not be of close tolerance. In fact, different values that are near to those specified can be used at a push, because the preset will compensate.

The same thing applies to capacitors. Many electrolytics are rated at -20% + 100% which means that they may be up to 20\% less or 100% more than the stated value. It is usually better to have a little more capacity than less, especially where decoupling circuits are concerned. Some capacitors are available that are -20% + 50% if a closer tolerance is required. It can be seen from this that the average electrolytic is likely to be rather higher than its stated capacity. It is also obvious that values are not too critical, so if the required value is not available, the next highest can generally be used. Thus 50μ F can be used in place of 25μ F, and 16μ F in place of 8μ F.

Paper and polyester capacitors are usually 20% or 25% tolerance, although for special purposes where accuracy is important 5% tolerance or better can be obtained. As with resistors, if a bridge is available, it is often possible to select from a number one that is quite close to the required value.

Ceramic capacitors are usually made with wide tolerance ratings; -25% + 50% is common where value is not too important but a little more rather than a little less is preferred. Such can be used for r.f. decoupling purposes, 1000pF. to 3000pF. being common values. Ceramics can be obtained in the lower values at 10% tolerance or better and these or mica capacitors should be used for tuned circuits and similar r.f. applications.

It may be felt that these tolerances are rather wide, but remember that they are the maximum permissible deviations for the category. Most components will be found to be well within the tolerance rating.

VOLTAGE RATINGS

The voltage rating of capacitors seems to be something with which some readers have difficulty. For d.c. circuits it means simply that the applied voltage must not exceed that for which the capacitor is rated. The minimum rating then, must be the applied voltage plus a safety margin. Thus with a 200 volt h.t. line all h.t. capacitors should be 250 volt working minimum. Lower voltage working capacitors can be used elsewhere such as for cathode bias bypass. For the earlier stages this may be a few volts but output stages run at up to 20 volts bias normally, so 25 volt working capacitors should be suitable. With some stages the bias is higher, and 50 volt capacitors must be used, but these are also often used with lower bias voltages to give a higher safety margin.

The miniature capacitors used with transistor equipment come in various low-voltage ratings. Again, the rating can be selected by considering the supply voltage and circuit position. If the battery voltage is 9 volts, then a rating of say 12 volts or higher would do for any circuit position. Lower voltage ratings can be used for emitter capacitors, usually 6 volt being ample here. Coupling capacitors in both valve and transistor equipment can be rated at about half the supply voltage but it must be remembered that a fault condition may put the whole of the supply voltage across the capacitor, so it is best to use one rated for the full supply voltage.

With one make of record-player, the designers slipped up on this point. It was valved, but with a silicon rectifier. A 150 volt coupling capacitor was used which was amply rated for normal running. When the player was first switched on the supply voltage was instantly available, before the valves had warmed up. This meant that around 250 volts appeared across the capacitor during this period. Needless to say a number of these players found their way into the workshop with short circuited coupling capacitors!

Note from what has been said before, that the capacitor voltage rating **must not be exceeded.** This means that one with a higher rating than is necessary can be used if the desired rating is not available. The higher the voltage, the more bulky the capacitor and with some exceptions, more costly. Generally though, size is the main consideration. If the equipment is small and the space limited use the lowest voltage rating consistent with requirements, but if space is not at a premium, higher ratings can be used if desired.

For a.c. or pulse circuits, the capacitor must be considerably uprated. The peak value of an a.c. sine wave is 1.4 times that of the r.m.s. voltage. The peak-to-peak voltage then will be 2.8 times, so a capacitor should be rated at three times its d.c. working voltage. Thus for 250 volts a.c., a 750 volt working capacitor would be the minimum. Usually, 1000 volt capacitors are used to give a good safety margin.

CONSTRUCTION

Having selected and obtained our components, there are a number of points to watch for when fitting them. First, check the colour coding of resistors and that you are reading them the right way round. For example, a $270k\Omega$ (red-violet-yellow) can be mistaken for a $4.7k\Omega$ (yellow-violet-red) if the coding is read from the wrong end of the resistor. Also, a $1 \cdot 2k\Omega$ (brown-red-red) resistor can be mistaken for a 220Ω (red-red-brown) one. With the preferred values now in use, these are the only "back-to-front" mistakes that can be made, so be careful when handling resistors. With many resistors, especially in the smaller wattages, mistakes can easily be made. Make sure too, that the colours are what you think they are. Some markings in orange are quite deep in tone and can be mistaken for red. particularly when viewed in artificial light.

Another mistake that can easily be made is to wire in polarised components incorrectly. We all know that electrolytic capacitors should only be connected one way round, but when fitting a large number of parts to a printed board it is easy for the odd one to go in the wrong way round. Double checking is the only answer. Similarly, diodes have to be watched. It anything, it is easier to make a mistake here as the markings and shape of the very small ones are not easy to identify. The ring and rounded end with Mullard diodes indicates the cathode, but often the ring is indistinct, and the other end appears rounded as well.

It is best to work to a system in construction. Do all the mechanical operations first, drilling, cutting circuit boards and fitting components such as transformers, controls and sockets. It is easy to have a mishap and damage some of the smaller components if any of this work is left to later. Wiring of the circuit can now begin. This should be done stage by stage, and when a stage is completed, go back and check component values, electrolytic and diode polarity, and trace through the connections (it is easy to solder a lead to the adjacent tag or printed strip to the one intended). Having satisfied oneself that the stage is wired correctly, then pass on to the next. If the construction has to be left (constructors have been known to go to bed at times!), try to complete a stage. This is a danger-time when errors and omissions can easily be made.

When re-starting it is prudent to check the previous stage again. All this checking may seem tedious and time-consuming, but even experienced engineers can and do make mistakes when constructing things and it is better to check and double-check rather than spend hours trying to correct baffling faults found when the equipment is first switched on.

Modern transistors are less heat-conscious than their predecessors, but they still can be damaged by too much heat. It is a good idea to leave the transistors in any particular stage as the last component to be fitted, then they cannot be affected by heat when soldering in adjacent components. When actually soldering the transistors, leave the iron on the connection only long enough to make a good joint. If for any reason it is not satisfactory and needs re-doing, leave it to cool for a few seconds before tackling it again. It is good practice to use a heat-sink whenever possible.

SOLDERING

When making a large number of joints it is possible that even the expert will make one or two "dry" joints. The only remedy is to be painstaking with each one and not to rush it. Wire-ended components are supposed to be ready tinned, but often solder will not take readily, and if they are soldered into print or to a tag, the solder will flow around the wire but take on the print and appear to make a good joint, but it will be bad inside.

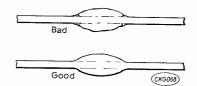


Fig. 1 : Many dry joints exhibit an inward curve where the solder meets the wire (top). A smooth contour from wire to solder is usually the sign of a good joint (bottom).

Always tin the wire initially and see that the solder has taken all around before attempting to make a joint. This may mean that the wire must be scraped first. It is sometimes possible to tell a bad joint by the way the solder meets the wire. Reference to Figure 1(a) shows the solder curving inward where it meets the wire. This is due to surface tension in the solder when it was molten and shows that it has not taken on the wire because the solder had a separate surface. Often there will be traces of resin from the solder core at the junction. In Figure 1(b) the solder has bonded itself to the wire and has no separate surface, hence there is a smooth flow from the wire to the bulk of the solder. This is not an infallible way of judging joints as the solder may have taken just at the point where the wire leaves the joint but not inside; or it may have taken inside, as in the first example, but not at the edge; but at least it does give a clue. A further check can be made by gently pulling or twisting the wire to see if there is any movement between it and the joint.

Excess solder must be guarded against, especially on printed circuits where there is a danger of it shorting over to adjacent print. A golden rule which should be observed at all times is never to interrupt the making of a joint. If the wire is pushed through the print or wrapped around a tag, and then one is called away without soldering the joint, more likely than not one will proceed with the next joint on returning. Time and again joints have been left unsoldered because of interruptions. If the house is burning down, let it, but make sure you finish your joint!

More could be said on the important art of soldering but it is hoped to make this the subject of a complete future article.

CIRCUIT BOARDS

There are several printed circuit methods available to the constructor. Veroboard is a popular one because it is versatile and ready to use. When cutting across a section of print to isolate it, remove a complete segment. Just cutting across with a blade may permit the solder to later bridge the cut, or the cut may not be complete to start with. Fig. 2 shows the right and wrong way.

Better still, use the proper spot-face cutter sold for this purpose. The physical mounting of the printed board may pose problems as it is desirable to have access to both sides for servicing. One successful method is to solder a tag board to a strip of unused print at the edge. The tags can then be mounted

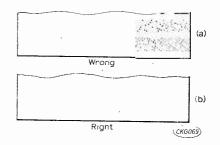


Fig. 2 (a) A narrow cut in a copper rail can is easily bridged with solder or dirt so a wide cut (b) is much preferred.

with nuts and bolts where required. This gives a vertical mounting with access to both sides the tags being bent to give the printed board any desired angle. Fig. 3 illustrates this arrangement.

Wiring should be done with solid rather than stranded wire, because it stays put and can be formed to give a much neater appearance. Bare copper wire can be used with sleeving, or as the usual plastic-covered wire. Whichever is chosen, it is good to use different colours for different parts of the circuit. Quite a range of colours can be obtained. Red can be used for positive supply circuits, black for earth or negative; green for grid or base circuits; grey for a.g.c.; orange, unsmoothed h.t. and so on. This enables future testing to be so much easier, but stick to the coding once it has been decided upon.

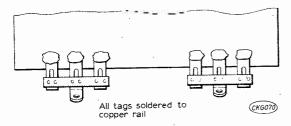


Fig. 3: Method of mounting Veroboard in a vertical position allowing access to both sides of the board.

It is a good practice to earth all appropriate components to one point in each stage. Furthermore, these points can then be linked and earthed to the chassis or frame at one point. This prevents h.f. chassis currents, in the case of radio equipment, leading to common impedance coupling and instability. With audio equipment it reduces the possibility of hum from the same cause. It is true that in many cases it may prove unnécessary, but like providing adequate decoupling, it is good preventive practice and difficult to carry out once the circuit has been wired.

TESTING

Having completed the building of the project, the time eventually comes for the first switch-on. It is not unknown for this action to be accompanied by flash, smoke or other disquieting blinding а phenomena! A simple precaution is to take a resistance reading across the power supply circuits before switching on. The initially low resistance reading should quickly rise as electrolytics charge up from the meter battery. (Remember, the positive side of the test meter is negative battery polarity). Any permanent low resistance must be investigated. Then, wire the meter, switched to a high current range, in series with the supply and switch on. An abnormally high current should prompt an immediate switch-off and examination.

It may be that in spite of all these precautions, the equipment constructed fails to work satisfactorily. Normal fault-finding techniques must now be applied to find the cause of the trouble. Voltage measurements find the majority of faults, so go to work with the meter, and with the aid of the published circuit diagram check to find if there are volts where they should be. Check too, as to whether the voltages are approximately correct. This will depend on the equipment and its function. As a very general rule with transistor stages, the collector voltage should be about half that of the supply, emitter voltage should be about 1 volt and the base should be about 0.1 volt higher than the emitter for germanium and about 0.6 volts higher for silicon transistors. With oscillators, emitter followers

and similar stages, voltages will be different from the above.

Directly coupled stages can be confusing and a fault in one can affect the voltages in another. Note though, that the base/emitter voltage difference is present as this forward bias is essential for the transistor to conduct, in normal circuits. Some low-current circuits, as used in the input stages of audio amplifiers, may use a high value resistor of $3M\Omega$ or so from base to collector, to supply bias, and the meter current will cause a much lower reading. This must be allowed for, or if available a valve-voltmeter should be used. Incidentally, when the equipment is working satisfactorily, it is a good idea to take all the voltages and note them down on the circuit, for future reference.

If there are still no results and the voltages seem right, then check through the signal circuits using some form of signal injection. However, by following some of the tips outlined here, construction will not be such a hit-or-miss affair, but one reasonably certain of immediate success.

MODIFICATIONS

Now we come to the question of modifications. Some readers may wish to add extra facilities or to tailor the equipment to their own particular needs. This sometimes leads to letters to the Editor or author requesting modification design details. Now while we try to help as far as possible, producing designs to order is something that cannot be undertaken. Not only is a good deal of time involved, but any theoretical design must be built and development work carried out before it can be passed as workable. Obviously this is not possible.

Minor modifications should be within the capabilities of most readers if they have read carefully the various theoretical and practical articles that regularly appear in radio magazines. More ambitious modifications could provide a subject for private research and experiment; really, with this hobby, there is more satisfaction and pleasure to be derived by experimenting and trying out one's ideas than there is by following a tried and tested circuit. A recommendation though, is to get the unit working as first planned, and then introduce the modifications. If they prove unworkable, one can then revert to the original.

Back Numbers Important Announcement

We regret to inform readers that owing to the closure by the Company of the department concerned it will no longer be possible to supply back numbers of **Practical Wireless** and **Television**.

To ensure obtaining regular copies of these magazines readérs are strongly urged to place a regular order with their local newsagent, or to take out an annual postal subscription.

Reference to past issues of the magazines may sometimes be obtained at certain public libraries who may hold bound volumes. A few libraries are said to offer a photostat service. Alternatively, we are always willing to insert a free request for specific back numbers in our "CQ" column which appears in most issues.

VHSignal Generator R.H.LONGDEN

WHEN it is necessary to adjust a VHF receiver or converter such as may be used for the 144MHz amateur band, a signal generator covering the required frequency is extremely useful. As an example, even a straightforward unit such as the 144MHz converter in the July 1972 issue of *Practical Wireless* has four circuits which must be tuned to about 144MHz. With such equipment, if all of the circuits are initially considerably off tune, it may not be easy to peak them for maximum noise or reception of signals which are not very strong. On the other hand, when a suitable signal is available, it is easy to trim all the circuits for maximum efficiency.

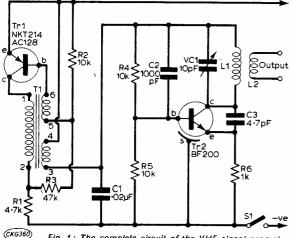
The generator described here is intended particularly for the frequencies from 105MHz to 170MHz, thus including the 2-Metre Band, but it can be used at frequencies outside these limits, and particularly for checking the coverage and alignment of converters and the simpler types of VHF receivers. It is a small, self-contained solid state unit, providing a modulated r.f. output.

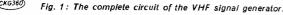
GENERATOR CIRCUIT

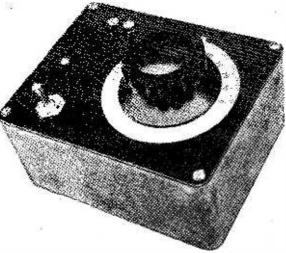
In Fig. 1, Tr1 is the audio tone generator or modulator. The transformer T1 is connected in the correct phase to obtain audio oscillation and this modulates the r.f. oscillator, which is supplied through the winding 3-4 of T1.

Tr2 is the r.f. oscillator. L1 is tuned to the required r.f. frequency by VC1, which has a dial for logging frequencies. An adequate signal is generally obtained by having the generator near the equipment being adjusted, but output can be taken to an external lead by the loop L2, if desired.

With a crystal controlled converter such as that mentioned, reception must be at the correct frequency, because VHF signals can only come out at a particular lower frequency. In this particular converter, 144MHz is tuned at 4MHz on the receiver.







145MHz at 5MHz, and 146MHz at 6MHz on the receiver scale. So for adjusting such equipment, there is no real need for VCl to be calibrated. Instead, VCl is merely tuned until the VHF signal comes through the converter, which can then be adjusted. In other cases, it is helpful to calibrate VCl, in the way described. This will allow the frequency range of fully tunable equipment to be checked.

CONSTRUCTION

VC1, Tr2 and the associated items are assembled on a tag board about $1l_2 \ge 2$ in. as in Fig. 2. As an alternative to the tag or group board, plain Veroboard with 10 pins inserted could be used, or eyelet board, or l_{16} in. thick paxolin drilled to take the leads. Veropins will have to be snipped off nearly

★ components list

+9V

(
Res	istors .		
			1010
3	4·7kΩ	R4	
	10kΩ	R5	10kΩ
R3	47kΩ	R6	1kΩ
Allı	resistors 10% #W		
6	-		
	acitors		
	0.02µF disc cera		
C2	1000pF disc or tu	bular cera	mic
C3	4.7pF silver mica	1	
TransistorsTr1NKT214 or AC128Tr2BF200 or similar VHF planar epitaxial transistorMiscellaneousVC1Jackson C804 10pFT1T/T3, 3·6: 1 + 1 (R.S. Components)On-off switchTwo small socketsTag and insulated board			
Case about 4 ³ / ₄ x 3 ³ / ₃ x 2in. deep 0-100 knob dial, KN1, Home Radio (Mitcham)			

flush, as if this is not done the spindle of VC1 may not project enough to take the numbered dial.

The board is drilled for VCl. A washer is later put between this board and the panel, on the bush of VCl and the bush nut then holds the whole assembly to the panel.

All connections in this section should be short, though the wires from Tr2 need not be cut down to less than 1_2 in. Solder these rapidly after other wiring is taken to the tags, and use a heat shunt such as a pair of flat-nosed pliers on the leads while soldering.

L1 is chosen from the details given, for the coverage which is required. L2 is a single turn, some ${}^{3}_{8}$ in. to ${}^{1}_{2}$ in. from L1, and is the same for all coils.

This section can be tested by connecting the SI lead to negative on a 9V battery and the lead which runs from Cl to 3 on Tl to a meter, which is clipped on the battery positive terminal. If the circuit is oscillating, current falls slightly when VCl is shorted by placing a metal tool from moving to fixed plates. Actual current was 4mA, falling to about $3 \cdot 8mA$ but this figure is not very important, and will depend on the particular transistor used. However, it is important that this change in current is found. If it is not, the circuit is not oscillating and no r.f. is produced.

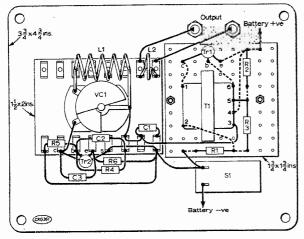
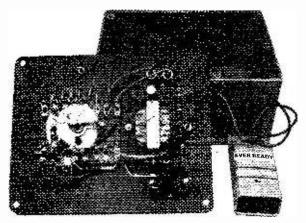


Fig. 2: The component layour.

With particular transistors in the Tr2 position, an upper frequency limit will be found, where oscillation grows weak and ceases. No particular difficulty arises in obtaining oscillation up to 180MHz or so. In fact, a number of transistors will work, and if the one fitted oscillates up to the highest frequency wanted, this is satisfactory. There is no point in using a transistor which could operate at a much higher frequency than required, as these cost considerably more than the popular types suitable for up to 180MHz. On the other hand, some cheap transistors which are supposed to be suitable for this frequency will cease to oscillate or become very inefficient. Should some particular VHF transistor be to hand, and not work with the values given, then the values at R4 (or R5), C3, and R6 may be changed to find if oscillation can be obtained.

T1, Tr1 and the three resistors are mounted on a piece of eyelet or other insulated board about 1^{3}_{4} x 1^{3}_{4} in. as in Fig. 2. Leave flying leads for the battery positive, S1 (battery negative) and from tag 3 of T1 to go to C1.



An internal view of the prototype.

This part of the circuit may be tested by connecting phones to 3-4 and applying 9V. With the components listed, a clear audio tone should be obtained.

Two countersunk 8BA bolts fix the board as shown. Spacers, nuts or washers are put between the panel and board.

The front panel should be made of paxolin. If it is metal, the bush of VCl should be isolated from it with insulated washers. VCl is fitted with a 0-100 degree dial, or with a control knob allowing markings to be made on a paper scale fixed to the panel.

The case was a die-cast box $4^{3}_{4} \times 3^{3}_{4} \times 2in$. deep, but a small plastic lunch-box or other case will do equally well. L1 is placed so that it is well clear of metal when the panel is fitted to the box.

L1, FREQUENCY AND CALIBRATION

Exact coverage will naturally depend on individual layout and the length of leads, but should be reasonably close to the figures given. The frequency is lowered by using more turns on L1, by winding L1 to a larger diameter, or by compressing L1 so that its turns are closer together. Fewer turns, smaller diameter, or stretching raises the frequency. In all cases L1 is of 20s.w.g. tinned copper wire, selfsupporting. Details of L1 are:

105-125MHz: 5 turns, ${}^{1}_{2}$ in. outside dia. and ${}^{5}_{8}$ in. long. Ends ${}^{3}_{8}$ in. and ${}^{5}_{8}$ in. long.

125-148MHz: 5 turns, ³8in. outside dia. and lin. long. Ends ¹8in. and ¹2in. long.

148-170MHz: 4 turns, ${}^{9}_{32}$ in. outside dia. and ${}^{1}_{4}$ in. long. Ends each ${}^{1}_{2}$ in. long.

Where a crystal controlled converter is available, or a VHF receiver, these will furnish calibration marks through the ranges they cover. This may prove handy when building other, fully tunable VHF equipment.

The VHF enthusiast can calibrate the oscillator by using a Lecher line and measuring the length of this to find the wavelength in metres. This is practical at these frequencies as the line will only be up to three metres or so long, and resonance produces a dip in battery current.

For some lower frequencies it may be possible to pick up the signal when the generator is tuned so that a harmonic is heard in the receiver. Second harmonic reception will arise when the generator is tuned to one-half the receiver frequency.

When some calibration points have been obtained, these can be entered on a scale or list, or on a graph which will give intermediate frequency readings.



NOVEL 'SCOPE CALIBRATOR

THE instrument to be described will work well with virtually any oscilloscope and facilitates the voltage calibration of both the X and Y axes in one simple operation. It is easy to build and use and the total outlay, including a suitable case, should not exceed £2.

CIRCUIT

The circuit is basically a conventional phase-shift network with the addition of resistors R2 and R3, and zener diodes D1 and D2. The values of C1 and R1 were found by experiment to give an almost perfect circle output from the phase-shift network. Addition of the zener diodes clips the alternative half cycles and produces the rather novel square display as shown in the photograph. Resistors R2 and R3 simply limit the zener current to an acceptable level and eliminate any chance of loading the phase-shift network. Provision of the ganged potentiometers allows the amplitude of the display to be varied from zero volts to the maximum zener voltage which in the prototype was set to be 5V.

Although a matched pair of zener diodes is to be preferred, odd diodes can be matched by inclusion of series resistance at points marked A and B on the circuit diagram. Indeed the constructor could use virtually any zener diodes that happen to be at hand as long as the nominal zener voltage is equal to, or in excess of, the maximum required for display. It will be found that the polarity of the zener diodes is of no consequence in this circuit, it will operate whichever way the diodes are connected. The prototype used Mullard OAZ201 5·1V types adjusted as above to provide exactly 5V. The rating of the diodes should be at least 250mW.

The constructor is not hindered in any way in the construction of this instrument as the layout is by no means critical and there is considerable flexibility in the selection of components. Any transformer supplying 12-20V will suffice as the current required is negligible. A type MT98 9-0-9V available from

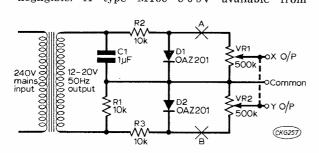


Fig. 1: The circuit of the 'scope calibrator.

J. A. NEKREWS

Henry's Radio is ideal as it is small enough for Veroboard or printed circuit board mounting. The ganged potentiometer should be a good quality type with a resistance between 500k Ω and 1M Ω . If the reader wishes, separate potentiometers, individually calibrated for each axis, could be used. Resistors R2 and R3 should not be reduced in value or the zener diodes may be damaged. The outputs can be taken via any type of terminals convenient to the constructor. No further constructional notes are considered necessary as the reader is free to use whatever form of construction that he (or she!)* finds most convenient. Of course there is no reason why the unit could not be incorporated as an integral part of an oscilloscope provided sufficient space is available.

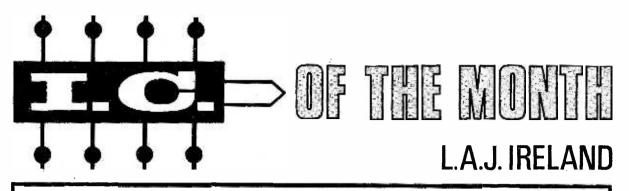
CALIBRATION

Having constructed the instrument with an established 5V maximum output, the first step in calibration is to set the potentiometers for maximum amplitude and mark this point as 5V. Then adjust the oscilloscope gain controls until the display is ten divisions of the oscilloscope graticule on each side. This gives a display of 0.5V per division. Then, without touching the scope gain controls, gradually reduce the calibrator output by one division at a time marking the dial at 0.5V steps. You then have a reasonably accurate instrument capable of voltage calibration of both axes of your oscilloscope in a single operation.

There is ample scope for the constructor to tailor the unit to suit his own needs and for this reason constructional details have been cut to a minimum. * Concession to Women's Lib.—Ed. HOME RADIO (Components) LTD , Dept. PW, 234-240 London Road, Mitcham, CR4 3HD. Phone 01-648 8422

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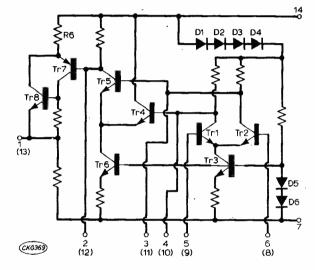




Number 35

THE SGS TBA231 i.c. reviewed this month follows along the fairly well established lines of high performance quality audio preamplifiers set by the RCA3052 which has already been reviewed in this column (May 1970). Low noise and high gain coupled with low power consumption are features being demanded more and more both by industry and the discerning audio enthusiast and the tight specifications associated with the TBA231 (noise figure less than 70dB, flat frequency response gain of 29dB) should make this i.c. meet the requirements of any amateur seeking a good quality audio preamp.

In Fig.1, a complete circuit diagram of one of amplifiers in the TBA231 is given. It is not intended to analyse the circuit in detail but a number of the more unusual features in the design will be pointed out. First a string of diodes D1 to D6 accurately control the constant current transistors Tr3 and Tr6 which also act as active bypass elements. In addition provision is made for limiting the output current in the event of a short circuit at pin 1. In this instance, the voltage increase developed across R6 automatically biases off Tr7 and Tr8 thereby preventing damage to the chip from an excessive current flow.



SGS TBA231 Audio Preamplifier

Fig. 1 : Circuit of the TBA231. Numbers in brackets are pin connections of second identical amplifier.

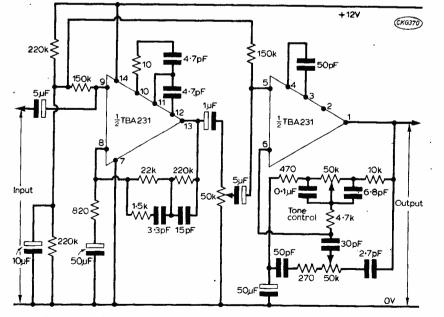


Fig. 2: Amplifier incorporating RIAA equalisation and active tone control circuits.

Also, even though the two amplifiers are fabricated and electrically connected on the same monolithic chip, channel separation of 140dB results from careful design and layout. So any interchannel inter-action will more than likely be caused by poor external bias decoupling or power supply fluctuations.

A typical application of the TBA231 as a hi-fi preamplifier utilising the first section for RIAA equalisation and the second amplifier section as an active tone control unit is illustrated in Fig.2. Typical performance specifications of this design are associated usually only with the more expensive hi-fi amplifier units.

The TBA231 is available from any SGS distributor such as Quarndon Electronics Ltd., Slack Lane, Derby.

LETTERS... The Editor does not necessarily endorse the views expressed by correspondents

EIS again . . .

Further development work carried out on the Electronic Ignition System has indicated that the output voltage of the original circuit was a little high and resulted in an increased possibility of crossfire and distributor cap flashover in damp conditions. As a result the output voltage has been reduced and it is now recommended that for optimum operation the value of the capacitor be increased from 0.47μ F to 1.0μ F.

Because of the arduous operating conditions imposed on this capacitor it is recommended that a triple foil type with at least 440V a.c. or 1000V d.c. rating be used. A suitable capacitor has been developed specifically for C-D ignitions and these are available from Magtor Ltd., 68 Dale Street, Manchester, at a cost of 35p including post and package. -Stephen Soar, (Manchester).

... and again

Just a brief note on the PW Electronic Ignition System. I found that the unit caused interference on my car radio so I bought a filter kit from Magtor Ltd., as advertised in PW. I fitted the three components inside a cylindrical aluminium can taken from an old vibrator unit and wired it into the E.I. box. In some cases it might be possible to fit the components into the E.I. box itself.

The filter kit is actually in-tended to decouple E.I. circuits when a tachometer is also fitted but it certainly proved effective against interference to my radio. -P. Beaman, (Bridgnorth, Shropshire).

(The decoupling kit can be obtained from Magtor Ltd., 68 Dale Street, Manchester, M1 2HS, price £1 including p and p.)-Editor.

Padding out

I write with reference to the many designs of receiver appearing in PW using Denco Miniature plug-in coils.

On reading through the manufacturer's literature on these coils it came to may notice that no padder was required for range five (red) coils. To satisfy my

902

curiosity, I drew a graph of mid range frequency against padder value for each of the five coils. This came out as a straight line, and gave the range five padder to be 6.000pF. This value was then tried in my receiver, which uses these coils, and it gave a marked improvement at the l.f. end of the band. On mentioning this to a friend who has built a receiver along similar lines to mine, he also tried it and got results similar to mine.

I would like to know what other readers, and maybe even Denco Ltd., think on the subject.-P. Richards, (Manchester).

A bit tight

I am sure many readers, at some time or another, have been frustrated to find that they have been unable to remove the bits from their 25 Watt Henley Solon soldering irons when they are due for replacement.

Having purchased a new iron some time ago, I slightly reduced the diameter of the bit with emery cloth and fitted a sleeve made from aluminium foil to come between bit and the body of the iron. Thus the binding between bit and iron is eliminated.

The foil I used was obtained from a cup containing a mince pie and if other readers follow my example, they can eat the byproduct with their coffee whilst doing a soldering job!-R. H. Roling, GW6WM (Glamorgan).

What do you get?

Please will you tell me what a man who pays £10 plus for a tone arm actually gets for his money?

I have recently constructed a pair of tone arms using standard 'Meccano' parts throughout. Both are heavy, but due to the screwadjusted counter weight, tracking weights of much less than that of a Meccano nut are easy to arrange. They are about 13in long from pivot to head. Tracking error should not be too great if it is set correctly, which I suppose would involve setting the stylus to point along the groove while the arm is about one-half of the way across the track of the record. I have

been unable to test it as yet due to the lack of a cartridge and stylus, which I am not allowed to remove from our Record Player for testing purposes (or any other), therefore, I used a dummy weight to simulate this.

The cost of the arm with the adjusted counterweight screw would be less than £1 if all the parts were bought new .--- S. Sellick, (Devon).

Aerial problem

May I enquire through the columns of P.W. for help.

I have a portable receiver which is for use on the 108-136 MHz and 145-175MHz bands. The set is equipped with the usual telescopic aerial, and this is ideal for reception from airborne aircraft or when within sight of an airport control tower.

I would like to build an aerial which I can place on the housetop (40ft above ground) which I am sure would give me better reception from the local airport, which is 5 miles from my home.

I have written to 3 major aerial manufacturers for either details or purchase of a suitable aerial but they do not seem to be interested in the problem.-J. Stirzaker, (4 Maitland Avenue. Anchorsholme, Blackpool, Lancs). (The lack of interest may be explained by the fact that the Ministry of P&T has repeatedly pointed out that a Licence [not generally available to the public] is required for the reception of transmissions by Fire Brigade, Aircraft, Shipping. etc.)—Editor.

Help!

At the moment I am having difficulty in obtaining a diagram and aligning instructions for a Perdio wireless PR41 "Town and Country" with trawler band.

I have the service sheet for PR41 but this is the older one and has 8 coils, but the one I want has 9 coils, which must have been the last model made. It has a tone control on the side and tape DIN socket on the back of the case. Can anyone help please?-Richard Cowley, Kerrowalass, Kirk Michael, Isle of Man.



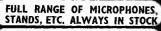
HIGH POWER SPEAKER SYSTEMS

DISCO

Strong leather cloth finish 4" board, fully lagged. Fitted high efficiency 8 or 16 ohm speakers.

PRINCE, 50 watt rms. 12". Size 24" × 16" ×

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SOUND CONTROLLED AND SOUND TO LIGHT UNITS

Mid, Treble and Bass Channels, up to 1kw of lamps per channel plus override switching. DJ30L. Sound to light. Takes output from most amplifiers. Adjustable levels

DJ40L. Sound controlled version. Built in microphone, no connections required

ASSEMBLED DISCOTHEQUES

DISCO-PLINTH. Consists of 2 turnitables fitted with high quality certain cartridges. The unit has a built in cross-fade rotary control for transferring the sound from left to right decks. The unit has no amplification built in and nust be used with amplifiers such as the D.J. 105S or D.J. 70S. Size 32" × 145" × 7" (hel. 11d).

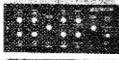
14 $f^* \times 7^*$ (incl. lid). DISCO-IMP. The latest addition to the Disco-sound Range of discotheques. Even smaller and more compact than the Disco-Minl, it contains all the necessary features for the smooth running of a mobile unit. Size 29" × 16 $f^* \times 7^*$.

184" \times 7". DISCO-MIRI. Complete portable Disco with built-in full function preamplifier/mizer. For use with any power amplifier such as "Disc-master". Size 30" \times 20" \times 8" DISCO-STANDARD. Has all the facilities of the Disco-Mini with the addition of a built-in 100 watt power amplifier making it a com-pletely self contained lisco unit. A V.U. meter view wimal inductive counts. A V.U. meter gives visual indication of output levels. Size $32'' \times 27'' \times 71''$

gives visual indication of output levels. Size $32^{\prime\prime} \times 27^{\prime\prime} \times 74^{\prime\prime}$. DISCO-SUPER, A slightly larger version of the Disco-Standard. Fitted individual controls for both mic. and deck inputs plus a cross-fade for deck to deck transfer. A built in P.E.L. cueing system, mic. over-ride, also a V.U. meter gives visual indication of output levels. DJ. 30L (3000w) 3-channel psychedelic light unit is a standard fitting. Deck cut out switches are also featured for ease of cueing. Size $38^{\prime\prime} \times 27^{\prime\prime} \times 10^{\prime\prime}$.

are also reactived for ease of cueing, Size $38^{-} \times 21^{-} \times 10^{\circ}$. DISCO-SUPREME, All facilities of the Disco-Super plus a third turntable which can be used for Jingles or other effects without using the main deck system. First lights are also atted. Size $50^{\circ} \times 27^{\circ} \times 10^{\circ}$.

PA-DISCO AMPLIFIERS





DJ.70S MIXER/AMPLIFIER. 70 watt rms. output for 8-16 ohms. 2-mic, 2-aux/decks. Master volume/Bass/ Treble. Size $15\frac{1}{2}$ " \times 5" \times 6".

DJ.105S. 30 watt rms. version. Size $11\frac{3}{4}'' \times 5'' \times 6''$. DISCMASTER SLAVE AMPLIFIER. 100 watt rms. for 8-16 ohms.

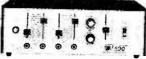
NEW D.J. 500 SERIES P.A. AMPLIFIERS 50 WATT, 70 WATT & 100 WATT MODELS

This new range incorporates many features that make them ideal for the professional user, clubs, discotheques, factories etc. Fibre glass P.C. Boards are used throughout with low noise eilicon transistors, high stability resistors, generously rated components and hand wired assembly to ensure reliability and quality.

* Exclusive "Fail Safe" Electronic Protection circuit.

* Fault Condition

arning lamp. 🛨 Built in bass boost below 30 Hz.



* 4 channel mixer with slider controls.

All three amplifiers have a built in emitter follower output socket for connecting a slave amplifier to enable the power output to be increased up to 1000 watts or more if required. A matching range of slave power amplifiers and a separate matching 100v line transformer is available SPECIFICATION

Frequency Response 50-20,000 Hz ± 3db (10dB Bass Boost at 10 Hz Signal/Noise Ratio better than =50db. Harmonic Distortion less than 1% Speaker Impedance 8-16 ohms. Inputs: Mic 1 & 2 Aux 3 & 4 5mV at 50K ohms (50 or 600 ohm to order) 100mV at 1 meg ohm. Size (all models) 15^{*} × 5" × 6". Power Output: Model D.J.500

50 watts R.M.S. 70 watts R.M.S. 100 watts R.M.S. (at 8 ohms) Model D.J.700 Model D.J.1000

DISCO MINI

Hardly larger than a suitcase yet contains all the necessary features for a high quality mo-bile unit. The pre-amp has separate tone con-

bile unit. The pre-samp has separate tone con-trols for both mic. and decks, and each input has its own indi-vidual volume controls and inputs, plus the addition of a cross fade for deck to deck sound transfer. A bull in P.F.L. system for cueing, together with mic-over-ride facility are standard on all units. Response 20-20,000 Hz. Mic. input 5mV, 50K. Output I volt. McDonaid M.P.60 Turntables are used with high quality ceramic cartridres, and each deck has its own individual cut out switch fitted

activities and each deck has its own individual cut out switch fitted. This unit is suitable for Discos or Clubs having a power amplifier, or for use with the Discmaster' 100 watt power amplifier as above. Size $32^{"} \times 20^{"} \times 8^{"}$.



DISCO-AMP. 100 watt rms output for 8-16 ohms, 4 channel inputs, 2-mic, 2 decks. Separate volume control plus masters. Response 30Hz -30KHz, distortion less than 1%. Treble/Bass/ PFL/Mic over-ride etc. Panel size $16\frac{1}{2}'' \times 7''$.

Cassette. GNOME 150, 150 watt Q1 with Cassette. LIQUIMATIC, 150 watt Q1 with 6" wheel. PLUTO TUTOR-2, 250 watt Q1 with Cassette PLUTU TUTUR-2, 200 watt Qt wint Cassette and 6° wheel. TUTOR-2, with Liquisplode Tank. KALEDOSCOPE LENS (for Tutor-2) 6° Liquid Wheel and Crystal Wheel Liquid Cassette and Moire (24 different types to choose from). Portable Hi-Power Strobes. YOU WILL BE SURPRISED BY THE

DISCO COLT. 150 watt. LIQUIMATIC MINI, 50 watt Q1 with 6" wheel. DISCOWHEEL, 50 watt Q1 with quick change

EFFECTS PROJECTORS

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A small selection from our vast stock.

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LOW PRICES & PERFORMANCE

SDL POWER SPEAKERS

High efficiency 12" speakers. Ferrite magnets, Heavy duty voice coils and cones for Disco High efficiency 12[°] speakers. retrite n Heavy duty voice coils and cones fo and Group use. 12[°] 50 watt rms. 8 ohm Full range. 12[°] 25 watt rms. 15 ohm Mid-Treble, 15[°] 30 watt rms. 15 ohm. Full range. 15[°] 100 watt rms. 15 ohm. Bass. 18[°] 100 watt rms. 15 ohm. Bass.

NHI

DISCO SPOT BANK



Designed to take three E/S Type spot or colour bulbs up to 150 watts each. The unit is of all metal construction and has one 3-pin mains input socket plus one 3-pin mains output socket for connecting more than one bank together if required. The unit can be left free-standing or wall mounted if needed. Black crackle finish gives the unit a very professional appearance.

Size $18'' \times 6'' \times 7''$ (excluding builds) Also in stock: Ultra Violet Spot Lamps and Fluorescent Lamps, Standard and Colour Spot Lamps and Fittings. Rotating Colour Displays, Flexilights, Fibre Optics, Dimmers, Flashers Effects Foils, etc. Your enquiries invited.

MIXER UNITS

DJ.101. Battery powered, 6-channel, variable levels, 8 \times 50k mic., 1 \times 100mV. aux., 2 \times 100mV p.u. Output 250mV.

DJ.102. Mains operated, 4-channel, variable levels. 2 \times 50k mic., 2 \times 100mV p.u. PFL control, master volume, mic. over-ride, output variable 0-500mV.

DISCO 40. Pre amp part of Disco amp (see above). All facilities. Output will drive up to ten 100 watt amplifiers.





stereo amplifier

PART TWO

PREAMPLIFIER

Construction is on the same lines as the driver amplifier, on a group board with common earth busbar, and is shown for one channel, Fig. 6a and circuit diagram Fig. 6b. Decoupling components R10, R24 and C2 and C12 are common to both channels. Screened leads are used from the input sockets to the selector switch, and from the switch to the input tags and also from the volume control to the driver amp inputs. The switch wiring is shown in Fig. 7a. Note that the equalising components are mounted directly on the switch (Sections c

and d).

It is at the input sockets where the only earth connections to chassis are made (apart from mains earth) this is important as hum and distortion can easily occur if earth loops are formed by connecting more than one point to the chassis.

The modular construction of the preamp with its earth bus-bar ensures that its own earth returns are all common to itself. (This applies also to the driver module.)

It will be seen that the chassis earth at the input is carried via the screened leads to the preamp, and then to the earthy side of the volume control, thence to the driver amp, through to the common point on the power supply, where the return from the power amps via the speakers are also returned. This is made clear in the layout drawing Fig. 8. The preamplifier has a number of connections to the controls, and it will be found easiest to solder connecting wires in place on the module before fitting to chassis. Leads of different colours would be a further aid. The leads should then be trimmed to length and taken to their control terminations in pairs. Driver and power amplifier can be treated in a similar manner.

Note that with all the transistors, the collector and case are common, so care must be taken to ensure that the case does not come in contact with other component or earth connections.

Output sockets for "Record" can be fitted if required. These are fed from each channel via a 100k Ω resistor from the negative side of C7, and will provide a signal of 100mV at high impedance, or 1mV per 1k Ω for impedances less than 100k Ω . Connections are shown in Fig. 6b.

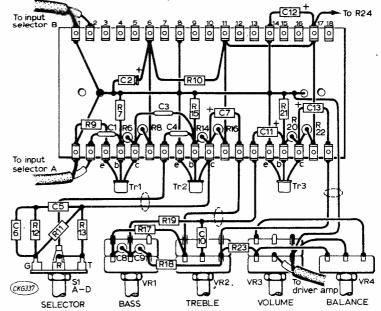


Fig. 6a: The wiring of the preamplifier section, only the components for the R.H. channel are shown; those for the other are mounted on the other side of the board and on the rear section of the pots.

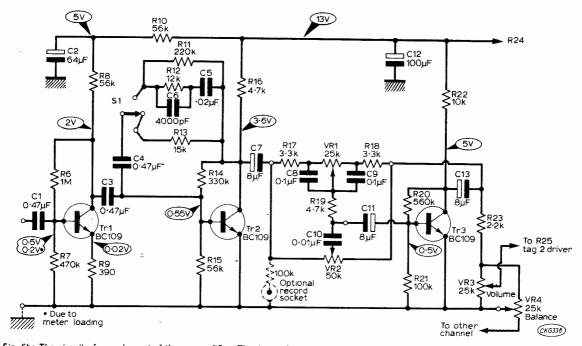


Fig. 6b: The circuit of one channel of the preamplifier. The decoupling components in the positive line are common to both channels.

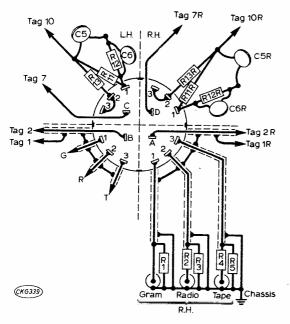


Fig. 7a: The wiring of the selector switch S1.

If the gram input is intended for a ceramic cartridge, this input must be attenuated with a divider of $33k\Omega$ and $6 \cdot 8k\Omega$, in the same manner as the radio and tape inputs. This will provide a sensitivity of 100mV and loading to give the pickup similar characteristics to a magnetic type, to suit the equalisation.

If the radio or tape recorder to be used is mono only, the appropriate input sockets should be linked together so that the single input plug is connected to both channels.

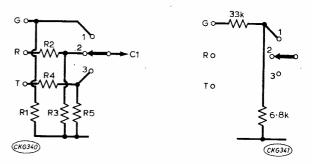


Fig. 7b (left) : The circuit of the input selector section. Fig. 7c (right) : Modification for a ceramic pickup.

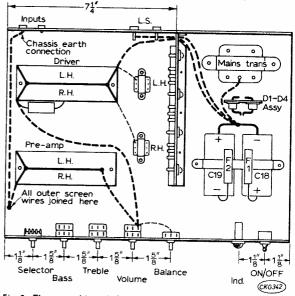


Fig. 8: The general layout showing the connection of the earth line to avoid earth loops.

POWER SUPPLY

The layout and circuit diagram are shown in Fig. 9 and need little comment. The rectifiers are "tophat" types mounted on a piece of lin. x 1_2 in. paxolin. A 2A bridge rectifier can be used here if desired; the symbols shown correspond to the bridge connections.

Capacitors C18 and 19 are held in place with an aluminium strip, to which the fuseholders are also secured.

The mains earth can be made to any convenient chassis point. A useful addition would be a 2-pin mains outlet on the rear panel to feed the gram motor or other ancillary equipment. This would be taken from the 240V connections on the mains transformer, to operate via the amplifier on-off switch. Note that the earth connections to any ancillary equipment comes automatically from the amplifier, and should not be connected to a separate mains earth, which would invariably result in excessive hum.

TESTING

Switching on any equipment for the first time always gives one a little concern, wondering if a mistake has been made somewhere, and if something is going to blow up, knowing that fuses do not always blow quickly enough to prevent damage.

Anyone feeling this concern can alleviate it in this case, simply by removing the fuses, and soldering 0.5W resistors of 4.7Ω to 10Ω in their place. Switch on; the resistors will only become warm, particularly the one in the positive line, if everything is well, but will immediately burn if a serious fault exists. One can then switch off before any damage is done, locate the fault and try again, replacing the fuses when satisfied that all is well.

A check can now be made on the voltage readings, starting at the fuses and working forward. The voltages shown are approximate, small variations can occur due to component and transistor tolerances. During this check the volume control should be at minimum, and resistors of 15Ω (or thereabouts) connected in place of each speaker. The resistors need only be ${}^{1}_{2}W$ or 1W as the amplifier is not delivering any power (or shouldn't be).

Switch the meter to a.c. (25V) and check that no voltage appears across the speaker sockets at any position of the volume control, tone controls, and selector switch. An a.c. reading of 10-15V would indicate r.f. instability, and the resistor across the speaker sockets would overheat. This would only occur if the layout or wiring differed from that shown

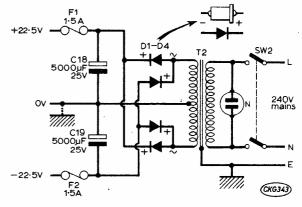


Fig. 9a: The circuit of the power supply.

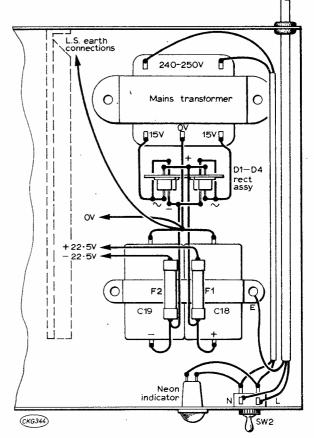
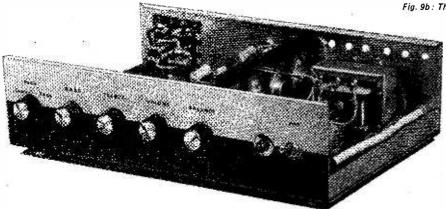


Fig. 9b : The layout of the power supply.

to create stray coupling and hence r.f. feedback. The cure would be to connect a by-pass capacitor of 100-250pF from collector of Tr2 to Tr3 to chassis.

The amplifier is now ready to go, and speakers and inputs can be safely connected. Choosing loudspeakers and a record player deck can present a problem to some people. The short answer is to pay as much as one can afford.



No. 96 Protection Racket



THE nearest approach Henry ever made to the Grim Reaper—in the course of duty—was when some well-meaning idiot omitted to remove the short-circuit from the safety switch of the supply unit of a high-powered transmitter

True, it was impossible to work on the Army's '10-set' once any of the rack-mounted units had been slid from its rails. A link of wire across the safety-switch contacts became routine test procedure. But lying there, while the petrol-driven generator pumped futile fumes across Breedon Moor, and the Naafi wagon was miles away was no recommendation, for a trust in protective devices.

Hence, perhaps, my present suspicion that regulation, control and 'protection', when not forced upon an electronics manufacturer by



"Oh, but it shouldn't!" cry the makers.

law, is usually a kind of gimmick, spawned from convenience, nurtured in wrath, weaned by ingenuity and matured in advertisement.

In particular, the curious convolutions of audio circuit producers (not designers, for Henry is painfully aware that these gentlemen languish in a limbo, surveying the prostitution of their ideas by the pimps of commercialism) result in tinselly circuits with curious protection gadgets, tweaked to safeguard the precious output devices against the hamfisted handling of the common herd. It causes a budding circuit maker to wonder where expediency leaves off and practicality takes over.

Often quite passable output stages are ruined by utter instability when the supply voltage wanders a touch or two. 'Oh, but it shouldn't', cry the makers. 'The British mains supply system is the best in the world.'

O.K. Henry goes along with that. But, even so, when, on Sunday morning, all the pinafored aspirants to Womens Lib are chickening in; or on Saturday evenings, when the great British publick (sorry, public) is tuning in to David Coleman and that travesty of human behaviour we laughingly call 'Sport'; then, and during those episodes of televisual dramuck that bring a paler shade of Whitehouse to the cheek, the mains supply voltage drops to a level where a Tandberg tape recorder refuses to rewind, a Quad amplifier forgets its steep transfer curve has certain advantages and ninety-nine from a hundred average radios rampage into avid crossover distortion.

For some reason connected with out insular arrogance, British designers expunge the idea of true regulation, protection and control. At the very least, we find a series regulator in the American (well then, Japanese) importations.

Henry is always amused by those models with cut-outs, which pop off dramatically when the impedances of loudspeakers (usually Scandinavian in origin) hit them below the belt. There are others, more genteel, which choke themselves into silence with a strangulated burp, waiting for you to light a cigarette, apologise to the dollybird you were hoping to impress, and switch on againhoping the fault has now disappeared.

Protection circuits, *per se*, bring trouble. For every attempt by a well-meaning designer to cherish his brain-child, there will be one or two electronic catastropes.

For protection *in excelcis* we turn to the Whichdogs of the Consumer Council (past, present or future—what's in a name?) and some Naderish fumings from across the Atlantic. If you spent an evening, or, God Help You, a cocktail half-hour, in the presence of George Darling, M.P., who steered the Trades Description Act through Parliament, you



... the dolly bird you were hoping to Impress.

would come away believing that every maker of electronic equipment conspires to do you down.

I don't think that is quite true. Seems more like the maker of electronic equipment fearing the user will do *him* down. Why else would Sony label their cassette cutout feeler a 'miserase protect-, ing lever'?

There's a famous amplifier with a delicious FET protection circuit, with a diode from gate to source. The driver stage is wonderfully protected, yes? But when things go wrong, the mid-rail flies up to 55 volts and that driver is only rated at 40V. It goes up in smoke, taking its 47-ohms emitter resistor with it, and often the 2N3055 output transistor as well.

It's about time we constructors were protected from the misborn circuitry and afterthought mods of manufacturers. What about it lads? Join UPESCO—the Union for the Protection and Encouragement of Suffering Constructors.



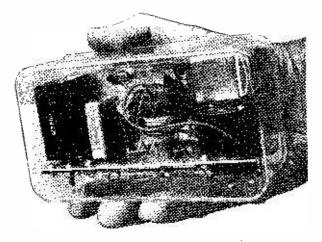
A CRYSTAL marker is used to calibrate receivers, signal generators, transmitter v.f.o.'s and similar equipment or to check their calibration. The marker described here is self-contained and requires few components. Details of typical uses are given later.

CIRCUIT

Fig.1 is the circuit, the single BFY51 transistor operating as a crystal controlled oscillator having three fundamental frequencies selected by a 3-pole 4-way switch. S1a and S1b select one of the three crystals, 100kHz, 1MHz or 3.5MHz. The remaining switch position is "Off."

When the 100kHz crystal is in use C2 is across L1, and the core is adjusted to approximately this frequency. For the higher frequency crystals C2 is not connected, the windings of L1 acting as an r.f. choke. Output is taken from a coupling winding and isolating capacitor C3.

With the unit operating at 100kHz this frequency and its harmonics or multiples will be heard on a receiver. Harmonics such as 500, 600, 700kHz up to



Rear view of the finished unit mounted in a plastic box.

1500kHz allow easy calibration of a receiver or tunable signal generator in the medium wave band.

Higher harmonics of this frequency are used for general short wave calibration, or the calibration of a transmitter v.f.o. For example, 1.8, 1.9 and 2.0MHz harmonics for Top Band and 3.5, 3.6, 3.7 and 3.8MHz for the 80m band.

When tuning, especially on higher frequencies, a quick indication of 1MHz points is useful and harmonics of the 1MHz crystal will be found at multiples of this frequency—2, 3, 4, 5MHz and so on.

For amateur band reception, in particular, a bandedge crystal is extremely useful. That fitted here is $3 \cdot 5$ MHz, its harmonics appearing at 7.0, 14.0, 21.0 and 28.0MHz as well as the fundamental at $3 \cdot 5$ MHz and harmonics 10.5, 17.5 and 24.5MHz which are, of course, remote from amateur bands.

CONSTRUCTION

A piece of sheet aluminium 5 x 4in. is bent as in Fig.2. The whole unit is assembled on this and will afterwards fit in a plastic box approximately 5^{1}_{2} x $3 \times 2^{3}_{8}$ in.

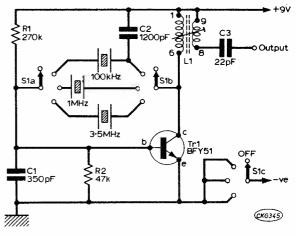


Fig. 1 : Circuit diagram of the crystal marker.

Crystal holders to suit the particular crystals used are bolted as in Fig.2. The box lid is also drilled for the switch, output socket and a small bolt to hold a battery clamp. Heavy pressure during drilling may crack the plastic, so a little care is required.

The transistor and most other small components are supported by soldering their leads directly on to the switch tags. Run leads X-X down through a hole to one crystal holder, leads Y-Y to the second holder and connect Z-Z similarly to the remaining holder. A card marked with the switch positions is placed between the case top and metal panel and held together by the switch nut and output socket. A hole is drilled to fix a piece of metal shaped to secure the 9V battery to the left of the switch.

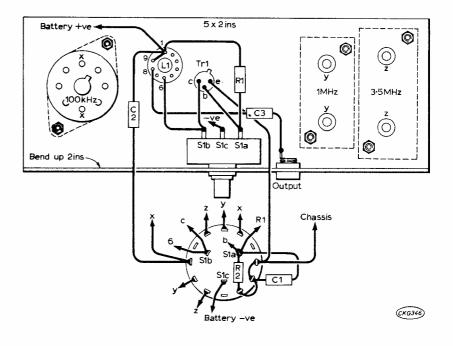


Fig. 2: Layout of components on chassis with details of switch connections.

\star components list

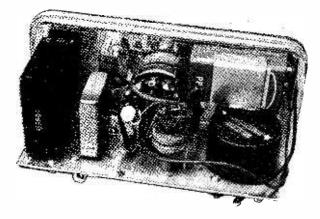
istors 270kΩ	R2 47kΩ +₩ 10%	
acitors 350pF	C2 1200pF C3 22pF	
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ADJUSTMENT

Rotation of the core of L1 allows the second harmonic of 100kHz crystal to be moved slightly in frequency to secure zero beat with the BBC on 200kHz or MSF on $2 \cdot 5$ or 5MHz. When the marker signal and received transmission are about the same strength, the frequency error of the harmonic will be heard as a low pitched growl, falling to a repetitive swishing sound, or flutter, or seen as a rise and fall of the receiver tuning meter, as the error is reduced. In any case at frequences of 1MHz and higher the error will be only a few parts in a million and accuracy is higher than necessary for any ordinary purpose.

IN USE

The output can be coupled to a receiver by a short lead plugged into the socket and placed near the receiver, or near a short wire in the receiver aerial socket or plugged into the receiver, depending on the



Another view of the crystal marker. The transistor is wired directly on to the switch tags.

strength required. Harmonics grow progressively weaker and the limit to which they can be detected depends on receiver sensitivity. The marker signal is unmodulated, so the receiver b.f.o. should be on and set to zero.

To calibrate a tunable generator or v.f.o., couple its output to the receiver and tune the v.f.o. or generator to zero beat with the appropriate crystal harmonic. The receiver is tuned to the wanted frequency, but receiver tuning has no effect on calibration in this case. The b.f.o. is not in use in this instance.

VFO calibration at 50kHz points can be achieved by tuning the receiver to the second harmonic of the v.f.o., and 100kHz points provided by the crystal will then fall at 50kHz points on the v.f.o. scale. The 10kHz points can be estimated from the v.f.o. scale.

Harmonics can be used to adjust r.f., mixer or i.f. stages for best results, using a meter to read cathode or emitter current of an a.g.c. controlled stage.



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PHONES BALANCE BALANCE AUX AUX

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THIS receiver features modular construction, easy accessibility of units, and complete coverage from 150kHz to 30MHz. It will thus provide reception on long, medium and all the short wave bands from about 200 to 10 metres.

To facilitate construction, wiring and testing the receiver is built as three units—a mixer-oscillator assembly using a dual-gate field effect transistor mixer with separate f.e.t. oscillator; a high gain 2-transistor intermediate frequency amplifier; and a 4-transistor audio amplifier and output section. These units are then assembled into a case which carries the panel and a chassis with coils, etc.

MIXER-OSCILLATOR

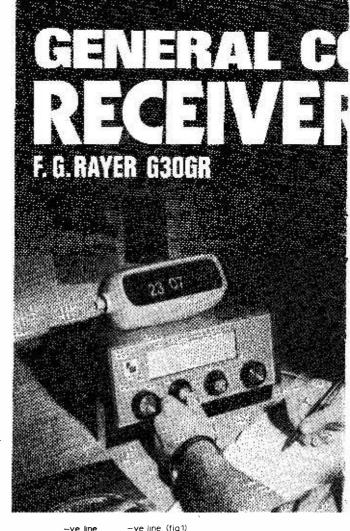
The circuit for this unit is shown in Fig. 1. Tr1, a 3N141, is the mixer, with the signal fed to G1 and oscillator input to G2. Output from this stage is from the drain to the 1st i.f.t. of the i.f. unit.

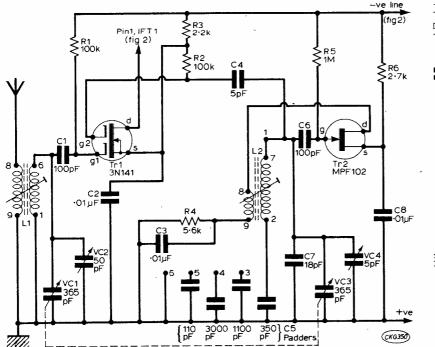
Tr2, an MPF102, is the oscillator with injection to G2 of the mixer via C4. The feedback windings 8-9 of the oscillator coil L2 provide feedback from the drain to the gate of Tr2, to enable this stage to oscillate.

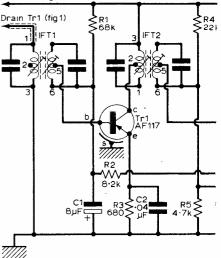
Coils are fitted in pairs, "Blue" in the L1 position and "Red" for L2. Coverage is approximately as follows:

Range 1	150-500kHz	2000-750 metres
Range 2	515-1545kHz	580-194 metres
Range 3	$1 \cdot 67 \cdot 5 \cdot 3 MHz$	180-57 metres
Range 4	5-15MHz	60-20 metres
Range 5	$10 \cdot 5 \cdot 31 \cdot 5 MHz$	28-9 · 5 metres

Range 1 is for long waves, but in this circuit the i.f. is 470kHz so coverage has had to be curtailed from that listed above or instability arises at the h.f. end of this band. This is easily done by marking the scale for Range 1 to suit. An alternative is to solder

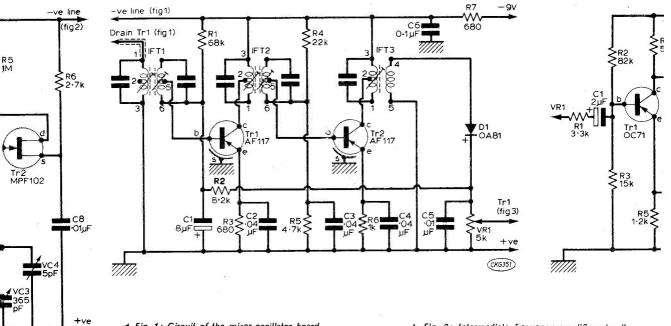






◄ Fig. 1: Circuit of the mixer-oscillator board.





◄ Fig. 1: Circuit of the mixer-oscillator board.

▲ Fig. 2: Intermediate frequency amplifier circuit.

CKG350



a 50pF capacitor directly across the tuned section of Range 1 coils. Such capacitors must not be fitted at the holder because of their effect on other ranges.

Range 2 is for medium waves, while the remaining ranges are for the higher frequencies. Actual coverage can be modified somewhat by adjusting the cores.

Plug-in coils as used at L1 for aerial tuning and at L2 for the oscillator have several advantages. Construction and wiring are simplified when compared with the permanent fitting of all coils and a multiway bandswitch. With plug-in coils, it is also a simple matter to obtain only those coils for the bands required. Coils for other bands can always be obtained later and no changes have to be made to the receiver to allow them to be used.

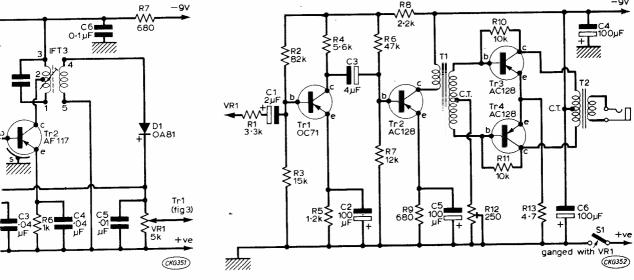
A panel aerial trimmer VC2 is fitted which has the advantage that the aerial circuit can be peaked up for best results with any aerial, on any frequency. Tuning on the higher frequencies becomes critical, so the bandspreading capacitor VC4 is provided for fine tuning. No additional bandspreading capacitor is necessary for the aerial coils.

Ranges 1, 2, 3 and 4 have their own oscillator coil padders, 110pF for Range 1, 350pF for Range 2, 1100pF for Range 3, and 3000pF for Range 4. No padder is used for Range 5. These padders go respectively to tags 5, 2, 3, 4 and 6, as in Fig. 1. The coils are so made that the correct padder is automatically in circuit when a coil is inserted.

IF AMPLIFIER

Fig. 2 shows the intermediate frequency amplifier which has two double-tuned i.f.t.'s and one single tuned i.f.t. This results in good selectivity and gain.

Diode D1 is the demodulator which also provides automatic gain control bias through R2 for Tr1. Audio signals are taken from the volume control VR1 to the a.f. amplifier.



▲ Fig. 2: Intermediate frequency amplifier circuit.

[▲] Fig. 3: Circuit of the audio amplifier and output stages.

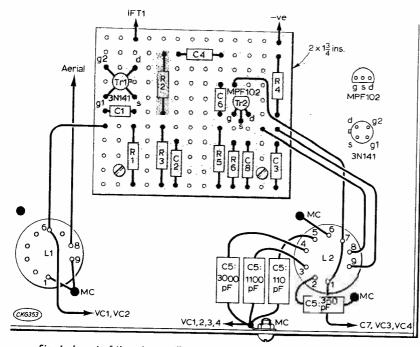


Fig. 4: Layout of the mixer-oscillator board and wiring of padding capacitors.

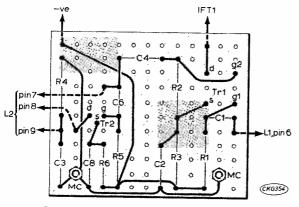


Fig. 5: Underside wiring of board shown in Fig. 4.

AF AMPLIFIER

The circuit for this section is shown in Fig. 3. Trl is the 1st a.f. amplifier, followed by the driver Tr2. The driver transformer Tl couples to the push-pull output pair Tr3 and Tr4 and T2 is the output transformer for a 2 or 3-ohm speaker. The pre-set R12 is adjusted for proper operating conditions in the output stage.

This type of circuit gives plenty of amplification and output. Its great advantage lies in the fact that the d.c. operating conditions of each stage are isolated from other stages, so it is not necessary to use matched sets of transistors. Some simplification would be possible by omitting Tr1 and taking C1 to the base of Tr2, though the extra stage of amplification is useful with weak signals.

MIXER-OSC BOARD

This section is wired on a piece of plain Veroboard $2 \ge 1^{3}_{4}$ in. Do not remove the shorting ring from Tr1 until the transistor is fitted in the way explained.

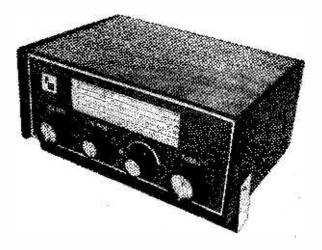
Two ¹₂in. 6BA bolts with tags are secured in the positions in Figs. 4 and 5. Extra nuts on these space the board from the metal chassis to clear wiring. These bolts also provide a chassis return when the board is fixed to the chassis.

Resistors and capacitors are positioned as in Fig. 4. The board is turned over and wired as in Fig. 5. Place sleeving on leads where necessary. Veropins can be inserted for external connections, or flying leads can be left for this purpose and cut down to length later. Leads run from C1 to pin 6 of L1, from Tr1 drain to pin 1 of i.f.t.1, from C6 to pins 1 and 7 of L2, from Tr2 drain to pin 8 on L2 and from C3 and R4 to pin 9 on L2. These pins or leads are identified by locating them as in Fig. 4. A pin or black lead is also required for the negative

connection, which runs to a pin provided on the i.f. board.

Tr1. This should be supplied with a shorting collar, spring or ring, which is left in position until Tr1 is fitted. With an insulated gate transistor, static charges from the fingers, or a metal or plastic tool, can damage the unprotected transistor. Spread the wires with a matchstick or piece of wood so that they can be inserted in the holes shown in Figs. 4 and 5. Solder drain and source leads. Solder the G1 lead by keeping the iron in contact with the R1 side of the joint, and the G2 lead by keeping the iron against the R2 side of the joint.

Once the transistor is fitted, it is protected by R1, R2 and R3, and the shorting spring can be pulled off. If it is necessary to unsolder this transistor, bind thin wire round the leads in advance. Do not touch the



General view of completed receiver with metal strap fitted to lift front edge.

unprotected G1 or G2 wires with the soldering iron, fingers or metal plastic tools.

Tr2. This transistor can be soldered in the usual way. A 3-lead holder was fitted for it primarily as a simple means of testing various transistors in the oscillator position.

When this section is finished, it is fixed with extra nuts as in Fig. 4, and the leads for L1 and L2 are cut and soldered. The 1_2 in bolts should leave enough clearance between the chassis and joints, but a piece of card or other insulating material about $2 \times 1_4^3$ in. in size can be put under the board.

Fig. 4 also shows how the padders are wired. Do not forget the lead 6 to chassis for Range 5. Leads from pin 8, L1 and the chassis run to sockets at the back of the case for aerial and earth.

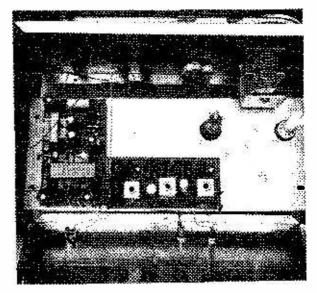
IF AMPLIFIER BOARD

This is $3^{7}_{8} \ge 1^{3}_{4}$ in. and the components are placed as in Fig. 6. Holes are drilled for the pins and screening can tags of the i.f.t.'s with a central hole so that the lower cores can be reached with an adjusting tool. A very small round file is useful here if some of the holes are not in quite the correct positions.

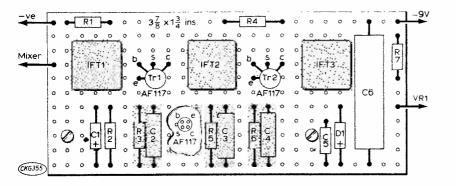
Two bolts MC with tags are fitted in the same way as with the mixer-oscillator board, to mount the i.f. amplifier and provide the positive chassis return.

When fitting the transistors bring them down to within about ${}^{3}_{8}$ in. of the board so that leads are reasonably short. Wires can be identified and short circuits prevented by putting ${}^{3}_{8}$ in.-pieces of sleeving on them—green for emitter, blue for base and red for collector. Connections underneath are shown in Fig. 7. It may be found helpful to put red sleeving on positive circuits, black on negative circuits and some other colour on other wires. Pins are inserted for the external connections--negative supply from R1 to the mixer-oscillator; mixer to i.f.t.1, pin 1; from R7 to negative on the a.f. amplifier and battery; and from D1 positive to VR1.

The i.f. amplifier is fixed 3^{1}_{4} in. from the end of the chassis, level with the back of the chassis, with i.f.t.1 towards the mixer-oscillator section. Fig. 4 is the underside of the chassis, but i.f. and a.f. sections are on top of the chassis.



View of receiver with sides and back removed to show placement of the i.f. and audio boards.



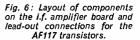
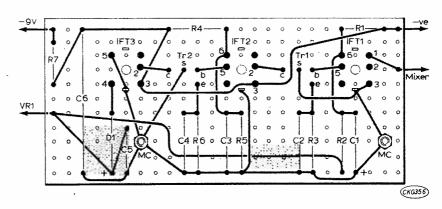


Fig. 7 : Wiring details under the i.f. amplifier board. Points marked MC are the bolts fixing the board to the chassis.



AF AMPLIFIER BOARD

Components are placed as in Fig. 8, using a board $3^{3}_{4} \times 2^{1}_{4}$ in. in size. Bolts with tags are again used for chassis return and mounting with pins fitted for the junction of R1 with C1, for battery negative and for leads which will run from the secondary of the output transformer T2 to the loudspeaker.

Wiring should be straightforward as shown in Fig. 9. Coloured sleeving can be used to identify transistor and other leads, as already mentioned.

When this board is complete, it can be mounted in the space to the right of the chassis. Joints must be clear of the metal, or protection provided against shorts by placing card under the board, as described earlier.

CHECKING THE AF

The **a.f. section** may be checked by connecting a loudspeaker and providing a signal to R1 from a radio tuner, audio oscillator, pick-up or other source. VR1 should be in circuit to avoid overloading.

Initially set R12 so that little resistance is in circuit. With a 9V battery connected and the amplifier working, increase the value of R12 by moving the slider until the current is some 8mA to 10mA or so with no signal. Current peaks will be very much higher than this, increasing as the volume is increased.

★ components list

Alternatively, R12 can be set to a position which results in clear reproduction with plenty of volume, though battery drain is increased if R12 is too high in value.

IF ALIGNMENT

The **i.f. amplifier** can be checked and aligned by itself or in conjunction with the a.f. section. VR1 must be connected and R1 of the a.f. section is connected to VR1; or phones may be connected to VR1, with an isolating capacitor in one lead to avoid upsetting the a.g.c. circuit.

As the i.f.t.'s are supplied pre-aligned, only a little adjustment of the cores should be necessary. If a signal is being obtained from the mixer-oscillator section, tune in a medium wave BBC or other stable transmission. Keep signal strength low by using a short piece of wire as an aerial, or by looping an insulated wire round the lead from pin 8 of L1. A proper tool is then used to rotate each core in turn, for best results. VR1 should be at maximum. A strong signal is avoided because it will operate the a.g.c. circuit and so make the correct core settings less precise. In any case, little or no adjustment of the cores may be needed, as explained.

If a signal generator is used, proceed in the same way, but couple the generator to the primary of i.f.t.1 by placing an insulated lead near pins 2 or 3. In this case, the mixer-oscillator section need not be in use.

MIXER/OSCILLATOR	Semiconductors Tr1 AF117 Tr2 AF117 D1 0A81
Resistors R1 100kΩ R3 2·2kΩ R5 1MΩ	Tr1 AF117 Tr2 AF117 D1 OA81
R2 100k Ω R4 5.6k Ω R6 2.7k Ω	Miscellaneous
Capacitors C1 100pF SM C5 *	IFT1/2 (Denco IFT18/465). IFT3 (Denco IFT14/465) Veroboard, plain, 0-15in. matrix 37 x 1%in.
C2 0·01μF C6 100pF SM C3 0·01μF C7 18pF SM C4 5pF SM C8 0·01μF	AF AMPLIFIER
* Padders:	Resistors R1 3·3kΩ R6 47kΩ R11 10kΩ
All silver mica	R2 82kΩ R7 12kΩ R12 250Ω pre-set
VC1/3 2 x 365pF gang (Jackson Type 02) VC2 50pF variable (Jackson Type C804) VC4 5pF variable (Jackson Type C804)	R3 15kΩ R8 $2\cdot 2k\Omega$ R13 $4\cdot 7\Omega$ R4 $5\cdot 6k\Omega$ R9 680Ω R5 $1\cdot 2k\Omega$ R10 $10k\Omega$
Semiconductors Tr1 3N141 Tr2 MPF102	Capacitors C1 $2\mu F$ 6V C4 $100\mu F$ 10V C2 $100\mu F$ 6V C5 $100\mu F$ 6V C3 $4\mu F$ 6V C6 $100\mu F$ 10V
Inductors L1. Denco "Blue" valve type for ranges required L2. Denco "Red" valve type for ranges required	Semiconductors Tri OC71 Tr2-3-4 AC128
Miscellaneous Valveholders B9A (2). Veroboard, plain, 0·15in. matrix 2 x 1 ^a / _s in.	Miscellaneous T1, driver transformer 3 · 5 : 1 + 1. T2, output transformer 3 + 3 : 1. Veroboard, plain, 0:15in. matrix 3 ² / ₃ x 2 ¹ / ₃ in.
IF AMPLIFIER	All Resistors 1W 10%
ResistorsR1 $68k\Omega$ R4 $22k\Omega$ R7 680Ω R2 $8\cdot 2k\Omega$ R5 $4\cdot 7k\Omega$ VR1 $5k\Omega$ pot.R3 680Ω R6 $1k\Omega$ with switch S1Capacitors	Cabinet, etc. Universal chassis sides, flanged 10 x 4in, (3), DL44 23in. drum, DL34 Type G cord drive. DL31 tension spring.
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	DL36A pulley wheels (2) drive cord. (All Home Radio). Perspex 10 x 4in. 3-ply wood, 10 x $7\frac{1}{2}$ in., 10 x 7in., $7\frac{1}{2}$ x $4\frac{1}{2}$ in. (2), knobs, etc.

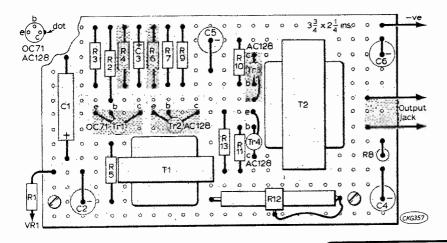


Fig. 8: Components on the audio stages board are placed as shown. Observe correct polarity of the several electrolytic capacitors.

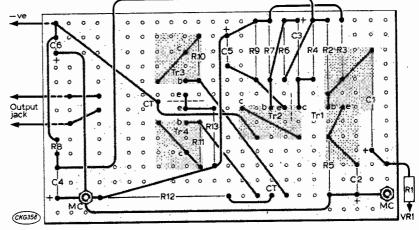


Fig. 9: Wiring underneath the audio amplifier board. Again points MC are "earth" returns, via the fixing bolts, to the chassis.

MIXER-OSC ADJUSTMENT

The **mixer-oscillator** is most easily tested and aligned when the receiver is otherwise completed. The coil adjusting screws are screwed in by the makers so that the coils can be placed in the cans in which they are supplied so initially all the cores have to be unscrewed several turns from this position.

Deal with each pair of coils separately. The cores can be locked with 6BA nuts when they are correctly adjusted.

Band coverage at the low frequency end of the band is adjusted by moving the core of L2. The core of L1 is adjusted so that near the low frequency end of the band signals peak up with VC2 nearly half closed. In these circumstances, it should be found that VC2 can be peaked for best results throughout the whole band. If it becomes necessary to close VC2 more and more, as the receiver is tuned from the h.f. end of the band towards the l.f. end, this shows that the core of L1 needs screwing in slightly. On the other hand, if when tuning in this way VC2 has to be opened more and more for best results, the core of L1 is too far in.

With the tuning capacitor VC1/3 fully closed, the frequency reached is lowered by screwing in the core of L2 and raised by unscrewing this core. This allows ranges to be adjusted so that there is some overlap between bands. A corresponding adjustment has to be made to the core of L1. It should be found that alignment is not difficult, either by tuning in transmissions, or by using a signal generator. Maximum results will in any case be obtained if VC2 can be peaked for best volume throughout the whole of any range and is then seen not to be either fully open or fully closed.

R4 on Tr2 is the lowest value which does not result in strong spurious oscillations marring reception. The best value depends somewhat on Tr2 and is likely to be between about $1 \cdot 2k\Omega$ and $8 \cdot 2k\Omega$.

CASE ASSEMBLY

Three $10 \times 4in$. flanged universal chassis members are used, one as the case front, one as the back and the third as a chassis to carry the three circuit boards and coil holders.

The sides are 3-ply, sanded and varnished, each $7_{12} \ge 4_{2}$ in. The top is similar 3-ply, $10 \ge 7_{2}$ in. while the bottom is $10 \ge 7$ in.

A piece of 1 sin. perspex, 10 x 4in. backed by card, except for a window over the tuning scales, is also required for the front.

Fig. 10 shows how the case is assembled. Mark through the holes punched in the flanges of the $10 \times 4in$. members so that the wooden sides can be drilled. The back is flush. The $10 \times 4in$. member forming the chassis is set forward about $7_{8}in$, and is $1^{3}_{8}in$, above the lower edge of the back so that there is clearance for the mixer-oscillator board below, as well as for VC1/3 above.

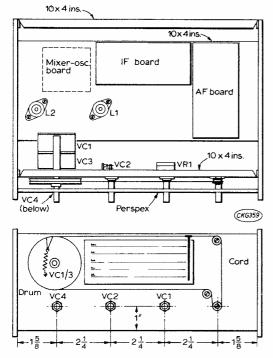


Fig. 10: Positioning of the major components on the chassis and front panel with details of the dial drive mechanism.

The front is set in lin. from the front edges of the side pieces as in Fig. 10. Drill the front for VC4, VC2, VR1 and the cord drive bush. Mark the same hole positions on the perspex, and drill clearance holes for the operating spindles. Also drill four holes to match with those punched in the front near the flanges.

When assembly is otherwise complete, the perspex is put in place and held with four lin. 6BA bolts, each with three nuts, so that it covers the drum and cord drive. A piece of card, with a cut-out through which the scales can be seen, fits behind the perspex.

Drill the front for VC1/3, fixing this with countersunk head 4BA bolts with extra nuts or spacers behind. The two wheels for the cord run on bolts as in Fig. 10. The cord has one complete turn round the driving spindle and is held taut by the spring in the drum.

The card for the scales is brought forward by means of a piece of wood about ${}^{1}_{4}$ in. thick fixed to the 10 x 4in. member. A small piece of tinplace is cut and folded so that it can be clipped to the cord with pliers and a vertical wire pointer is soldered to this, the pointer and drum being as shown in Fig. 10 with the ganged capacitor fully closed.

The receiver can be wired and tested with the back, top and bottom completely removed, so that all units can be reached easily. The bottom is attached with three or four self-tapping screws. The top requires to be hinged, or provided with strips to hold it in place, so that it can be lifted off the case to change coils.

CALIBRATION

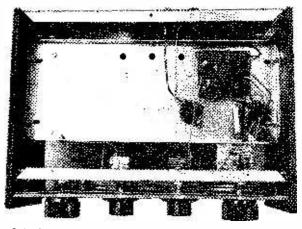
Markings are made before fitting the perspex. If the scales are to be calibrated in frequency first check coverage and ganging and fix the coil cores with 6BA nuts. Calibration is then most easily done



The markings of the four controls and dial calibration can be seen in this view of the receiver.

with a signal generator. This is set to various frequencies, the signal is tuned in on the receiver, and the appropriate scale is marked. Take care to avoid harmonics and second-channel responses, in the usual way.

An alternative is to tune in various bands, such as 19 or 31 metres, and mark these. Another possibility is to fit a 0-100 or similar horizontal scale, against which stations tuned in, or known frequencies can be logged. A rule calibrated in mm. will act as an easily obtainable ready-made scale.



Only the mixer-oscillator board and associated coil holders are mounted underneath the chassis.

AERIAL AND EARTH

Remember that conditions on the various frequencies vary enormously according to the time of day and other factors. Quite a large number of transmissions should be received with some 5ft. to 20ft or so of wire as an indoor or outdoor aerial. For weak signals in the 1.5-5MHz region, a longer aerial will make a great difference by improving signal strength. For good results on these frequencies, some 50ft. to 150ft. or so of wire as high as possible and clear of earthed objects, can be worth while.

Though many signals are sufficiently strong with no earth the use of an earth connection will give a worthwhile improvement in volume on some frequencies and often allow the reception of weak signals which cannot otherwise be received. An earth lead can be an insulated wire taken to an earth spike or other metal object buried in the ground. Where this is impossible, a counterpoise earth consisting of an insulated wire running near the ground or in an opposite direction to the aerial can be helpful.



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TELEVISION

FEBRUARY ISSUE

ASSESSING RECEIVER PERFORMANCE

How good is your set and how do you go about assessing the quality of the picture? This month we start a new series on subjective performance testing, i.e. without the need to use any test equipment.

CRT REJUVENATOR

This simple item costs very little to build but saves pounds by prolonging the life of old tubes-cathode reactivation can often in fact be a case of new tubes from old!

SHORT BACK-FIRE AERIAL

Here's a new one for aerial constructor enthusiasts to try out! Reg Roper reports on the excellent results he obtained recently using this type of aerial.

SERVICING TV RECEIVERS

In response to many requests, this month L. Lawry-Johns deals with the Philips T-Vette/Stella Companion mains-battery transistor portables.

PLUS ALL THE REGULAR FEATURES





AVE you ever worked out how much it costs you using batteries rather than the mains supply for operating your equipment? Obviously it depends on the type of battery you use, what current you are drawing and how often the equipment is used but a quick calculation shows that the current costs about 2,000 times as much as operating through a power supply. Certainly a power supply costs rather more than a battery but this is rapidly recovered by savings in battery costs.

The unit described here is a replacement for the popular PP9 type of battery that is fitted in a number of the larger types of transistor portable radios. This battery is also very popular with amateur constructors. Although designed to replace the PP9 type, the circuit of course holds good for any 9V battery with a maximum current supply of about 80mA but the size of the unit described here may be too large to act as a direct replacement.

The cost of our battery eliminator is about $\pounds 1$, appreciably less than the commercial units available. In addition our unit is exactly the same size as the battery that it replaces—it is built inside the old battery casing—and so it will neither be too large, or too small, when in place.

THE CIRCUIT

The theoretical circuit is shown in Fig. 1 and is absolutely standard. The transformer (the type number and suppliers are mentioned in the components list) has a 7-0-7V secondary and this is connected to the rectifier diodes D1 and D2 giving full-wave rectification; this is then smoothed by the capacitor C1. The reason for the resistor R1 is to act as a bleeder, when the unit is on it will then be drawing at least 20mA and ensures that the peak voltage that may be present is never applied to the unit. With no load at all connected to the power supply, the voltage reaches well over 10V and this is

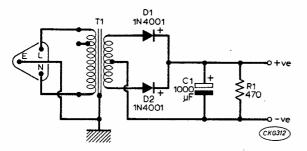


Fig. 1 : The circuit of the battery eliminator.

not desirable as damage may result. As shown, with no load other than R1, the prototype measured $9\cdot 2V$ and with 80mA being drawn about $8\cdot 5V$.

CONSTRUCTION

As can be seen from the photographs, the unit is built inside an old battery case. This has to be taken apart as follows:—

First, using a screwdriver, prise up the bent-over metal ridge that holds the top of the battery in place and work all around this, levering it up. Straighten this metal with pliers or the top will not come out easily and reassembly will be difficult. When this is done the entire contents of the battery will fall out.

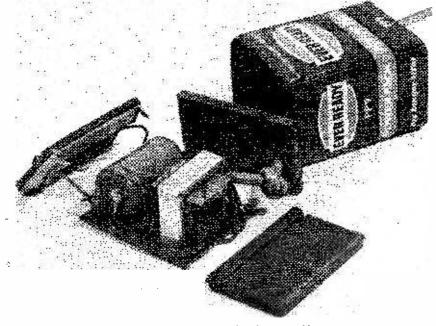
The top panel with the snap-on contacts should be cut free of the connecting wires or bands of metal and put to one side. Just enough of the original metal on the underside should be left for making the connections later.

The circuit is built on a piece of drilled s.r.b.p. board with dimensions exactly $2\frac{1}{16} \ge 2^{1}_{2}$ in. Holes will have to be drilled in this to take the transformer mounting lugs which are then fitted through and bent over. The remaining components are "threaded" through convenient holes and soldered together as shown in Fig. 2. C1 is shown here very much smaller than it actually is to make this drawing clear; in fact C1 will be so large that it probably overlaps the diodes and R1. Both sides of the transformer have three wires coming out, the secondary is that with two brown and one blue wire, the primary has brown, blue and a green. The mains wire should be connected to the primary side to the brown and blue. unless you live in an area where the mains supply is 230V or below in which case the mains should be wired to the brown and green.

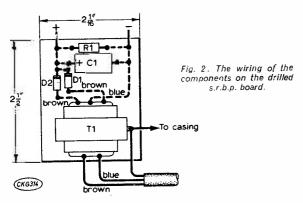
The earth wire should be stripped back and a

★ components list

R1	470Ω ±W, 10 per cent
C1	1000µF, 15V minimum
D1, I	D2 1N4001 silicon diodes
T1	Mains transformer with 7-0-7V secondary, type MT98 (Henry's Radio)
Hard	board, see text; Mains lead; Old PP9 battery;
Drille	ed s.r.b.p. board.

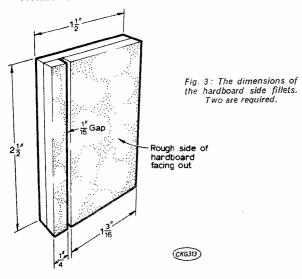


The prototype just before final assembly.



second short length of wire twisted with this and then both soldered to the case of the transformer. The reason for this is safety; this second wire will later be soldered to the battery case and if by any chance this solder joint breaks from the transformer, the battery case will still remain earthed.

Neither side of the 9V is shown earthed since it



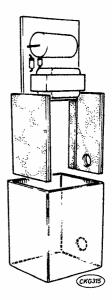


Fig. 4: How the unit fits together.

will depend on the design of the equipment which side requires earthing. If the equipment is negative chassis, the earth should run to the negative side and conversely for positive earth equipment.

The circuit board is held inside the battery case by means of two side fillets made up from hardboard, the dimensions for one of these is shown in Fig. 3; the other is of course identical. Three pieces are needed for each and these are then glued together.

When the side fillets are ready they should be fitted inside the case with the circuit board to ensure that everything is a tight fit and that they don't rattle about. If all is well, the bits should be taken out and one of the side pieces replaced to make the hole for the mains wire, both the piece of hardboard and case should be drilled together to ensure that the holes line up exactly.

It is important that the mains lead is fitted through one of the short sides with the hardboard fillets as this will prevent it chaffing on the sharp metal case; a grommet will be of little help as the metal sides will cut right through it in a very short while.

A knot should be made in the mains lead as close as possible to the transformer, as can be seen from the photograph, this will prevent it being pulled away from the unit with possibly disastrous results.

The unit is then reassembled as shown in Fig. 4. This should leave three wires coming out of the top: positive, negative and the earth wire from the transformer casing. The last should be soldered to the metal casing anywhere inside. The supply leads are then fitted to the snap contacts, remembering that for a battery the female contact is the negative and the male the positive. The original top can then be replaced and this should rest on the side fillets.

Before completing the assembly, the unit should be tested to ensure that it works; taking it apart again can be quite a job. If all is well the top metal, which is standing proud, should be bent down to hold the top in place.

The dimensions for the fillets are only applicable to the modern Ever Ready PP9 batteries. Other types of batteries have different inside dimensions and this will affect the length of the fillets; in this case the dimensions will have to be worked out.



A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

NE of the disadvantages of being interested in radio and electronics is that you act as a magnet for faulty transistor radios and the like. Certainly you can say "No!" to requests to "have a look at it," but if you take this attitude you will not be very popular. Your author usually agrees, on the condition that mechanical troubles are not handled (broken cabinets, dial mechanisms etc) and that if replacement components are required it is up to the owner to get the bits. If you stick by these principles, repairs can be done very quickly but only if you have the right equipment. The most useful item is a multimeter-it is hopeless trying to work without one-but running a close second is a signal injector/tracer and this forms the subject of our project this month.

Inject

The circuit of the signal injector/tracer is shown in Fig. 1; SW1 alters the function and is in the "inject" mode. The circuit is a multivibrator producing a square-wave output at C1 to which a probe can be attached. The square-wave is in the audio range but it is so full of harmonics (a square wave is a fundamental frequency plus all its harmonics) that these go up to several megahertz. If you place a transistor radio on the medium wave band even near this circuit, the output will be heard all over the band. If we inject this signal at the volume control we will be able to establish if the amplifier part of the set is O.K.; if it doesn't work then we can concentrate our efforts in this direction.

If this is O.K. we can work back along the i.f. section and we shall eventually discover where the fault lies.

★ components list

R1	1M Ω , $\frac{1}{4}$ W, 5 per cent	1p
R2	2.7k Ω "	1p
R3	1ΜΩ " "	1p
R4	2.7kΩ " "	1p
C1	3300pF disc ceramic	3p
C2	3300pF disc ceramic	3p
C3	3300pF disc ceramic	3p
C4	100µF, 10V minimum	5p
Tr1	BC109	10p
Tr2	BC109	10p
D1	1N914	7p
SW	I One-pole, 2-way slide switch	8p
SW	2 On-off switch, toggle type	5p
Crys	tal earpiece and jack socket	35p
	· · · · ·	93p
char	es are those recently advertised and m nged. No allowance is made for minimu s or for nostage and packing and these	m order

changed. No allowance is made for minimum order costs or for postage and packing and these points should be checked carefully before ordering.

No. 45 Signal injector/tracer

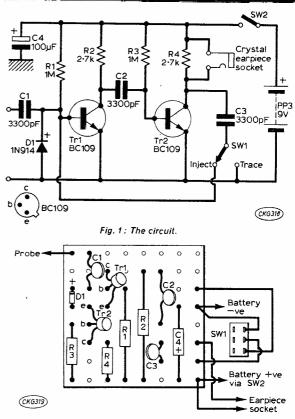


Fig. 2: Suggested layout on Veroboard.

Trace

When SW1 is switched to "trace", the circuit is no longer a multivibrator but becomes a highly sensitive amplifier. If the probe is fixed to an r.f. point the signal will be rectified by the diode D1 and amplified by both stages and fed to the crystal earpiece. It is smoothed by C3 which now, instead of coupling back to the base of Tr1, goes to the negative line.

The current drain of the unit is quite small and a PP3 battery is quite sufficient.

Two wires, fitted with crocodile clips, should be connected to the negative line and to C1 as these will be needed to couple the injector/tracer to the circuit under test. If using the injector at r.f. frequencies, the output is so high that the wire from C1 has only to be held near the aerial, it is not necessary to make a direct connection.

Construction

The components can be mounted in any convenient form but a suggested component layout is shown in Fig. 2; this is built on a small piece of Veroboard with 0.15 in matrix, 8×8 holes; no breaks are necessary in the conductor strip. SW1 can be a small slide switch wired as shown; SW2 can take any convenient form.







THE BROADCAST BANDS Malcolm Connah

Times in GMT Frequencies in kHz

ONTHLY NEWS FOR DX LISTENERS

HRISTMAS is over and here we are in another New Year. I know that many of my readers will have asked for presents of money so that they can save towards the new receiver that they want and many will write to me asking advice on the best set to buy.

Unless a second-hand purchase is anticipated the reasonably serious listener will have to pay around £50 for a good receiver. There are of course many sets on the market for much less and several which cost a lot more.

In this middle price range there are two receivers which stand out as being very good value for money and for this reason they are very popular with DXer's. The first is the Lafayette HA600 which is a general coverage receiver (550kHz to 30MHz) this set has the advantage of being all solid-state which means that it can be run from either the mains or from 12 volts d.c. The second is the Trio 9R59DS which is again general coverage but can only be operated from 240 volt mains.

Before anyone asks, my personal preference is for the Lafayette. There are two reasons for this, the first is that I have always owned Lafayettes and had no trouble with them at all. The second is that when I worked in an Electronics Laboratory, designing circuits, I only used transistors and integrated circuits, never valves. Consequently I feel more at home with a solid state receiver and if anything goes wrong I will be more able to repair it myself.

A great number of readers will, of course, not be lucky enough to afford one of these sets but they can increase their enjoyment of the hobby in many ways.

The 1973 edition of the World Radio TV Handbook has just been published and although it costs about £3 many experienced DXers will tell you that it is an invaluable text that they would never be without. The book lists all the Broadcasting Stations in the world with full details on each, including frequencies used. hours of transmission and the languages used. The book also contains a section on general information and a complete listing, by frequency, of all the stations.

A good New Year Resolution would be to erect a new and better aerial, about which much has been published in the past few months There is, however, a snag which was pointed out to me by Mr. A. W. Lewington of Bath. I also noticed the difficulty when I moved house recently and wanted to erect a new aerial. The problem is that nobody seems to sell good aerial wire any more. A few years ago Woolworths used to sell aerial wire which consisted of stranded copper wire with thick plastic insulation. This had the two important properties of being strong and flexible to withstand the ravages of our British weather. It is, however, no longer available.

If any reader knows of a good source of aerial wire

I would be pleased to hear from him so that I can pass the information on to all our readers.

Yet another way of getting more enjoyment from the hobby is by joining a reputable DX Club. These clubs publish magazines for their members and these are used to exchange news and views about all aspects of the hobby. The membership fee is usually about £1.50 and the magazines alone make this outlay very well spent. The club that I would recommend is the World DX Club and the Secretary is Clive Jenkins, 11 Wesley Grove, Portsmouth, PO3 5ER.

In a recent article I published a specimen Reception Report. Mr. A. J. Wills of Elgin wrote to me to point out that the space devoted to programme details was not long enough. This was due to an error on my part when typing out the article. The most important part of the report is the section on programme details. All the other details on the report can be obtained from such sources as the World Radio TV Handbook.

The programme details are the only way in which the station can be sure that it was in fact their transmissions that were heard. The more complete the details are the greater is the liklihood of the station confirming the report with a QSL card.

All this chat has left me with very little space for your reports so I will start straight away with one from James Pruden of Sturminster Newton in Devon. James has a Skywood CX-203 receiver with a 15 metre end-fed aerial, this combination enabling him to hear:

- 6010 RTB, Belgium in French at 1510.
- 9545 Radio Ghana in English at 2120.
- 9610 Radio Kiev, USSR, in English at 1930.
- 11650 Radio Bangladesh in English at 1715.
- 15015 Voice of Vietnam in English at 2015.
- 15165 Radio Denmark, ID in English at 1330.
- 15170 ELWA, Liberia in Arabic at 2230.
- 15345 Radio Norway in English at 1615.

21570 Radio Japan, news in English at 0800. Craig Tyson of Wembley in Western Australia used his Lafayette HA600 receiver and inverted 'L' aerial to hear the following stations:

- 6090 Phnom Penh in English at 1230.
- 7215 AFN, Taiwan in English at 1300.
- 7470 R Liberation, N. Vietnam, English at 1030.
- 9510 Lakeland Radio, Malawi, English at 1945.
- 9520 VLT9, New Guinea in English at 0730.
- 9580 Voice of the Philippines, English at 1300.
- 15170 Radio Tahiti in French at 0700.
- 15185 Voice of Nigeria in English at 0700.

Reports should arrive by the 15th of the month and be addressed to me at 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.



H APPY New Year. Now, how about a resolution to devote at least 30 per cent of your listening time to bands which you normally ignore? If you are an h.f. type, you could do no better than start off with top band transatlantics. These are tests carried out at certain times and on certain dates. The first ones in 1973 are as follows. January 14 and February 11 from 0500 to 0730 hours.

For something a little more difficult, how about the transpacific tests? These are to be held on January 13 and February 10 from 1330 to 1600 hours. The U.S. and Canadian stations will be transmitting between 1800 and 1807kHz. The D.X. stations will use 1825 to 1830kHz or 1800 to 1805kHz. It should be noted that stations in other countries are often restricted in choice of frequencies. For example, Japanese Amateurs may only use 1907 to 1912 • 5kHz while stations in New Zealand are restricted to 1875kHz. Doubtless we will get some Lid calling an endless CQ on these frequencies. How wonderful it would be for me to be proved wrong on this. How about it, Lids?

John Spacey (Devon) tells of A51PN putting in an appearance on 14MHz. He also mentions that Swan Island is active (listen for W6MTE/HR6) as is VU25FBZ on Andaman Island, both on 14MHz.

Two useful New Year presents you can treat yourself to. One is the latest countries list from the RSGB. Second is a good world atlas. For example, do you know where Swan Island or Andaman Island (mentioned above) are?

Which bands to listen on and at what time is really a matter of personal choice. However, the following remarks are based on readers' reports and personal observations by your scribe's ears.

The h.f. bands (14, 21 and 28MHz) become somewhat erratic during the winter months. By contrast, the three lower frequency bands (1.8, 3.5 and 7MHz) all improve compared to their summertime performance. Fifteen and twenty metres start to close down quite early now. Often, by 2000 hours there are no signals at all and this state of affairs remains until around 0600 hours.

On ten metres it is often a matter of luck. This band now opens at about 0800 hours and closes again at around 1700 hours. However, 28MHz is really a sort of lucky dip. If there is a high sunspot activity the band will suddenly burst into life.

Most of the winter D.X. activity migrates to 7MHz and this is particularly evident when the h.f. bands (14MHz and upwards) close down for the night. In theory, the sunspot activity should continue to decline in the coming months. This activity follows an 11-year cycle and we are currently on the way down towards a trough.

R. Kell (Northumberland) sends in a five-band log which includes earfuls of activity on 3.5 and 7MHz. Guilty parties aiding and abetting include a "modified" R109 with an a.t.u. and 150ft. end fed antenna. Goodies on 3.5MHz include; CN8HD,



Frequencies in kHz

 Times in GMT

XV5AC, ZM4PG, 9H5D. Plundering forty metres brought the following r.f. jewels; CO3GS, CN8HD, HR1RF, KZ5PW, OA4SO, PY2ELX, PY2FKZ, TF1TP, VR2DE, XE11IJ, YV4AGP.

John Hulse signing himself "Yours faithfully" and residing in Cheshire, tells of a sparkling new FR50B receiver. Duper squeaks on 28MHz from; CR6CN. CR7IC, CX2CF, ET3JH, KZ5PW, LU5DEK, LU5DTV, OY9LV, PY1AGC, ST2SA, VK6CF, VP7ND, VP9BO, XW8CN, YV4EBH, ZP5AQ, ZS6OS, 3B8CV, 3B8CZ. Down on 21MHz, the following menu was provided; CP1FU, CT2BG, EL4B, EP2TC, ET3DS, FP8DH, HI3XSJ, HK3CCO, HK3CLX, OD5FU, PZ1CU. VP1BH, VU25DK, XV5AC, YA1OS, YV5AK, ZD3X, ZE7JC. All stations using s.s.b. and the receiving aerial is described as a 66ft. dipole at 10m height.

Stefan Kaye (Oxon) made a brave attempt to break the habit. But the soulful look in the silent eyes of his AR88D got to him. Result of this joyous reunion was; CE3PY, CT2AC, LU3DTV, LU9DTQ, VQ9MC, ZS1WS—all on s.s.b. on ten metres. Down on eighty, a listen was rewarded by: FW8IA, HB0AIC, K3UQU/W1, ON0NJ, TZ2AC, VE1ADV, VE11E, VE3PT.

R. Iball (Notts.) uses a diamond aerial! Well, it's shaped like a diamond, is 7ft. long and hidden in the loft. The receiver is a JR500SE (not hidden in the loft) and the 14MHz c.w. signals were received by courtesy of: HS4AGN, UA0DV, VE7ZR, VE3ZT, ZL1ARV, ZL1MQ, ZL3GQ, ZM1AFW, ZM3ABC. Donald Duck mode of signals on the same band from: FP8DH, PZ1DR, VE6PP, VP8RA, VK1BF, VK6PG, VK6VW, VP9GA, VP9GE, VS9MB, ZL1AH, ZM4KM.

Trevor Thomsen (Bulawayo, Rhodesia) sends letters with pretty stamps and includes logs heard on his Hallicrafters S53A and 40ft. end fed. The list for s.s.b. on 21MHz reads: EL2CB, GR3NM, K3TGM, K4MQG, WA3GJZ, WB8JEY, W1AWE, W4SKO, W5RO, W8COG, 6W8AL, 6W8EM. Bernard Hughes (Worcester), JR31O, 66ft. long wire, 28MHz s.s.b.

Logs, in alphabetical order please, to arrive by the 15th of the month to 12 Cross Way, Harpenden, Herts.



AMATEUR BANDS RECEIVER DECEMBER 1972 Part 1. Fig. 2C, potentiometer (500 ohms) associated with S-meter should be marked VR2. Fig. 2D, power supply diodes should be marked D1 and D2. The OA2 voltage stabiliser should be marked V1. Amend Components List:—Fig. 2D, V1 OA2, V2 ECL86.

I.C. LINEAR CAPACITANCE METER JANUARY 1973 D3 should be a C5V6 5·6V (not 3·3V). This applies to both the circuit and the components list.

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2



with negiti-glible hum. Valve ime $up; -2 \times ECL66$ Trude Pentodes. $1 \times E260$ bas rectifier. Two dual potentioneters are provided for bass and treble control, giving bass and treble boost and ett. A dual volume control is used. Balance of the loft and right hand channels can be adjusted by means of a sepa-rate Balance' control fitted at the rear of the chassis. Input rensitivity is approximately 2600m/ for full peak output of 4 watts per channel (8 watts mono), into 3 ohm speakers. Full negative feedback in a carfully calculated distortion. Supplied complete with knobs, chassis size distortion. Supplied complete with knobs, chassis size $11''w \times 4''d$. Overall height including valves 5". Ready built & tested to a high standard. **PRICE 48-92** P.&P. 45p.

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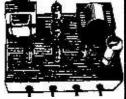
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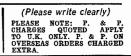
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COLIN RICHES ARTHUR DOW

M ULLARD Limited, as their 50th Anniversary tribute to the BBC, staged a two month exhibition at Mullard House in London. It was opened on November 2 by Lord Hill, chairman of the BBC.

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GOING BAC

The Post Office gave its full support and co-operation to the exhibition which was complementary to the one organised by the BBC and held at the Langham Hotel, near Broadcasting House.

The Mullard exhibition was designed with a fourfold aim in mind—to show how technical innovation has contributed to the growth of broadcasting, to stress the pioneering effort that went into it, to enable the public to gain more of an insight into the technical aspects of broadcasting and to illustrate how development and research are continuing for the future.

The first part of the exhibition was entirely devoted to the development of broadcasting. It included a replica of the original Savoy Studio 1 of the early 1920s and a pictorial story showing how the microphone was evolved.

Two famous microphones exhibited were those used by Dame Nelly Melba and Sir Winston Churchill.

Visitors were also able to speak into one of the early "meat-safe" microphones and hear their voices



The lip microphone: designed by the BBC Research Department to cut out background noise. It was first introduced in 1937.



Her Majesty the Queen compares vintage and modern tape recorders.

reproduced on a tape machine. Also on display, was an early cylinder gramophone and one could, at the touch of a button, hear the kind of reproduction that could be obtained from such a machine.

An early pianola was shown and it was difficult to realise that in the earlier days of broadcasting, the announcers actually had to pedal units like these as continuity between programmes!

On the same stand there was a recording machine of the type used by BBC War Correspondents and in one of the photographs shown in this article Her Majesty the Queen can be seen comparing this with a modern cassette tape recorder.

The section of the exhibition devoted to the story of television began with the actual first Emitron TV camera. Photos showed the various outstanding developments of television and the display was climaxed by a reconstruction of a live TV studio.

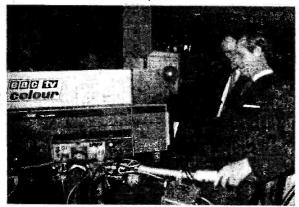
There was an audio/visual link with the BBC exhibition at the Langham, and Mullard House visitors were able to see themselves on colour TV and to read the news on closed circuit TV. From our picture it looked as though the BBC had taken on a new cameraman to demonstrate the colour camera his face looked very familiar though!

Mullard themselves had a display showing the part their components had played over the five decades of sound and TV broadcasting.

They also had a "Colour TV Look-in", a six minute



The Queen shows interest in a horn loudspeaker and the "meat safe" microphone.



Prince Philip "has a go" at being a BBC cameraman.



The "Twenties" room setting at the Langham Hotel exhibition.



This picture shows the central display feature at the Langham exhibition. It reflects the development of the BBC over the years.

presentation telling the story of the Company's contribution to colour TV development.

Exhibits were also devoted to colour TV techniques and demonstrations in which the public could take part. Visitors could experiment with a BBC Radiophonics unit and see a demonstration of 3D television together with exhibits showing what the future may hold for transmission techniques.

The BBC held their own exhibition at the Langham Hotel, formerly one of London's most luxurious hotels and now offices and studios of the BBC.

Facing visitors, in the main area of the exhibition, was a multifaceted panoramic screen consisting of 20 separate screens. Forty-two slide projectors, with a total of 3,500 slides projected onto this screen. Scenes shown were chosen from a quarter of a million original BBC pictures and gave an extremely good visual impression of broadcasting in the past. present and future. These projectors, incidentally, were controlled by a simple computer which maintain the correct picture sequences.

Underneath this screen, which stood about 9ft. above ground level, there were mock-ups of room settings of different periods of broadcasting history.

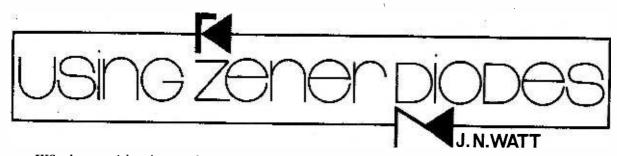
Of particular interest to "Going Back" fans was a typical room of the '20s. The man is (see photograph) depicted hearing the first BBC broadcast on his home-made receiver on November 14, 1922.

In front of the stand was a row of buttons and excerpts from 1920s' type programmes could be heard by pressing any button. Famous voices heard included Flotsam and Jetsam, Tommy Handley and Jack Hylton.

Other room settings were shown depicting the broadcasting years rolling on. A large planographical map of the British Isles provided the basis of another exhibit and showed the growth of programme coverage from 1922 onwards, achieved by many miniature "transmitter" masts that lit up. Behind this stood a 20ft. high display reflecting the growth of the BBC's services at home and abroad.

Pictures kindly supplied by Mullard Ltd. and the BBC





T HIS short article aims to bring to readers' attention some lesser known facts of zener diode operation—facts which are so useful when it comes to making the most of a voltage stabiliser or regulator.

Temperature

Almost all zener diodes, like other semiconductor diodes, have a temperature coefficient of voltage; that is, their exact voltage varies as their temperature varies. However, a study of manufacturers' literature shows that this temperature coefficient is by no means the same for all zener diodes and in fact varies with voltage as shown in Fig.1.

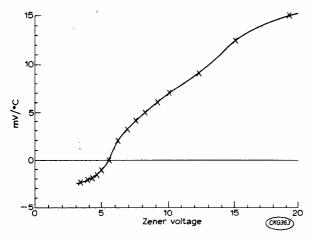


Fig. 1: Graph showing temperature coefficient for different zener voltages.

It can be seen that, at one particular zener voltage, namely 5.6V, this temperature coefficient is actually zero and that the coefficient becomes positive at higher voltages and negative at lower voltages. The values used to plot the graph were extracted from Mullard data but, in point of fact, all makes of zener diodes show this effect, which is presumably connected with the level of doping employed to obtain the various voltage ratings. Of what particular use is this information to the home experimenter?

Environment

Consider the environment in a motor-car. This could very easily range from 25° F to 85° F (-5° C to 30° C) and yet amateurs happily use a zener of any voltage thought appropriate, when, with a little further consideration, a higher performance could easily be obtained. For example, to stabilise a car battery supply at 10V for instrumentation, control or

communication purposes, the use of $6 \cdot 2V$ and $3 \cdot 9V$ zeners in series will give an almost zero temperature coefficient, so contributing to the accuracy of any measurements and to the frequency stability of receiver local oscillators etc.

A further point of interest is that a forward biased silicon diode has a temperature coefficient of about $-2 \cdot 2mV/^{\circ}C$, so that such a diode used in series with a zener diode of 6 $\cdot 2V$, see Fig.2, once again would give a zero temperature coefficient, this time with an output voltage of about 6 $\cdot 9V$. Note that the forward biased diode can be the base-emitter junction of a silicon transistor if, for any reason, this is more convenient.

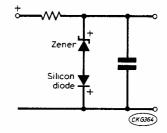


Fig. 2: Circuit illustrating the use of a forward biased diode and a zener diode in series.

So far, we have considered the effect of temperature on the actual voltage of a zener diode, using car applications as an example, but it should be remembered that almost any situation will experience temperature variations and the effect of these on any voltage regulators should not be overlooked. Steps to reduce any such voltage changes can then be taken, as described.

Stability

A further cause of disappointment in the voltage stability of zener diodes arises from the finite value of dynamic slope resistance of the zener. For example, in Fig.3a for a load of up to 20mA and a zener current of 5mA, resistance R is:—

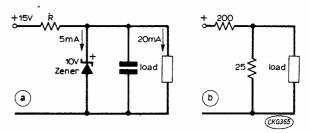


Fig. 3a : A typical zener diode application with Fig. 3b showing the effective dynamic equivalent circuit.

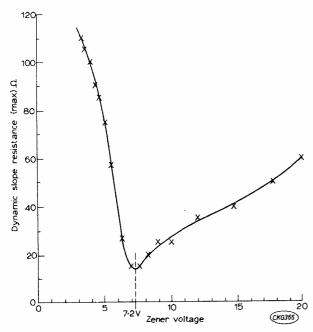


Fig. 4: Dynamic slope resistance of a range of zener diodes.

$$R = \frac{(15-10)10^3}{20+5} = 2000$$

Now, a 10V 400mW zener can have, again according to Mullard data as plotted in Fig.4, a dynamic slope resistance of 25Ω . Thus, the effective dynamic equivalent circuit is as shown in Fig.3b. This leads to the result that, for a change in supply voltage Vi of 1V, the change in output voltage, Vo, will be:—

$$V_0 = 1 \times \frac{25}{200 + 25} = 0.11V$$

which is surprisingly high. A quick measurement confirmed such a value.

Output stability

A dramatic improvement in output voltage stability, as the input voltage varies, can be brought about by the use of a constant current circuit, provided that the load current to be supplied is almost constant. This is usually so where the zener diode is used to supply a reference voltage in a voltage regulator, and in supplies to receiver local oscillators, for example.

At very low zener voltages and, to some extent at the higher voltages also, quite large values of dynamic slope resistance are noted e.g. 85Ω at 4.7Vand 60Ω at 20V so the constant current circuit of Fig.5 will greatly assist in providing voltage stability.

In this example, there is a load current of 10mA with 8mA zener current. Now, with a constant potential difference between transistor base and input voltage, due to the use of forward biased silicon diodes, and thus a constant difference between emitter and input voltage, a constant current must flow through the zener diode and load in parallel. Therefore, as the input voltage varies, the current through the zener hardly varies and we have largely eliminated the effect of its dynamic slope resistance.

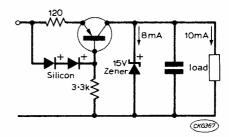


Fig. 5: In this circuit a constant current feed is provided for the zener diode.

Results

A series of measurement was made of the output voltage of the circuit of Fig.5, and of a simple resistance of 620Ω plus zener diode combination, as the input voltage was varied. The results are plotted in Fig. 6, where the remarkable improvement given by the constant current circuit is clearly seen.

A reduction of output voltage variation by a factor of about 30 over the range of 18V to 26V input voltage is surely well worth the additional complexity.

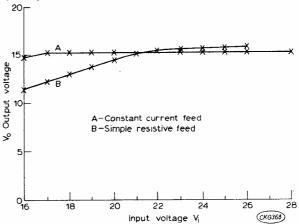


Fig. 6 : Performance of zener stabilisers with constant current feed (A) and simple resistive feed (B).

It would doubtless have been possible to have extended the flatter part of curve B down to, say, 18V input voltage, but this would have required a very much smaller value of series resistor than the 620Ω actually employed in obtaining the curve of Fig.6. This would have probably called for the use of a zener diode of greater power rating, and yet it still would not have led to as good a performance as the constant current circuit.

If the zener diode so driven is employed to supply a reference voltage in a series stabilised power supply hum rejection is also greatly improved, for the constant current transistor has a very high output resistance, and this, together with the (relatively) low impedance of the zener diode, gives attenuation of ripple. This offers the chance to use smaller smoothing capacitors. A saving of space and money is the result, as well as improved performance.

One final point. In all the circuits given here a capacitor is shown across the zener diode. This is done since zener diodes are quite effective noise generators! The capacitor also helps to lessen any hum present if a poorly smoothed mains source of power is used with the simpler zener diode circuits.

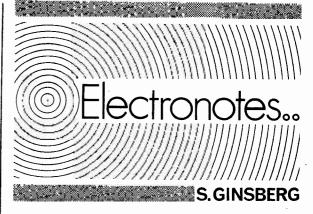
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ETER WRIGHT of Formby, Lancashire has tried his PCR2 receiver and 50ft outdoor aerial on the medium waves at 0030hrs and he logged WINS 1010kHz located in New York City. Ian Geddes who lives in Dumbarton, Scotland reports CJON 930kHz in St John's Newfoundland; CHER 950kHz in Sydney Nova Scotia; CKBW 1000kHz Bridgewater N.S; CFRB 1010kHz Toronto; WOR 710kHz New York City; WOWO 1190Hz in Fort Wayne, Indiana; WABC 770kHz New York City; WKBW 1520kHz in Buffalo N.Y; WCKY 1530kHz Cincinatti, Ohio; WWVA 1170kHz Wheeling, West Virginia; WNEW 1130kHz New York City. Ian writes "CJON is the most consistent signal from midnight until 0200hrs". Others to listen for from midnight onwards are CBM 940kHz in Montreal; CBA 1070kHz Moncton, New Brunswick; WHN 1050kHz in New York City. A weak French-speaking station can often be heard on 1375kHz after the close down of Lille, France 1376kHz at 2300hrs. This is Radio St Pierre in the French Territory of St Pierre et Miquelon which lies a few miles to the south of Newfoundland. Radio St Pierre verifies readily and is the sole broadcaster on the islands which form a 'medium waves only' DX country.

Kevin Peel (Hornchurch Essex) has an 8 transistor Astrad receiver and a 100ft outdoor aerial and he heard the following broadcasts in English on the medium waves. Radio Portugal 755kHz at 2245hrs; Radio Tirana, Albania on 1394kHz at 2030hrs and Vatican Radio 1529kHz at 2045hrs. J. Cesarczyk (South Croydon) used his Grundig Elite Boy receiver with internal ferrite aerial to hear Radio Jerusalem 737kHz at 2230hrs (with interference from Warsaw and Madrid); Radio Bucharest, Romania 755kHz at 2050hrs; the Voice of America Kavalla, Greece 791kHz (in English at 2300hrs); VOA Rhodes 1259kHz (in English at 0300hrs); BBC World Service, Berlin on 809kHz (in English at 2315hrs after the close down of BBC R4).

During the evening quite a few distant stations can be found in the gaps between European channels. Baghdad, Iraq on 760kHz can be heard between West Germany on 755kHz and Sottons, Switzerland 764kHz and is usually on the air all evening with programmes in Arabic. Riyadh, Saudi Arabia is on 588kHz between Madrid 584kHz and Frankfurt 593kHz; Ovazim, Iran 841kHz is often strong when it signs-off at 2030hrs, listen between Nancy, France on 836kHz and Rome on 845kHz; Ahwaz, Iran can be found on 1394kHz in between Radio Centro Madrid 1385kHz and Albania on 1394kHz; the BBC relay on Masirah Island in the Persian Gulf (heard in English at 2040hrs) is on 1410kHz between the French network on 1403kHz and the Spanish channel on 1412kHz.

Please send logs and information about the medium waves to the author at 132 Segars Lane, Southport, PR8 3JG.



THE calculator market is flooded with many different types, each claiming some unique feature(s). Of particular interest to the buyers —us—is the price. News has now arrived from a semiconductor manufacturer that i.c. chips are currently in production which are so cheap that an electronic calculator could easily be manufactured and sold at a market price of less than £20.

There are four versions of the chip which are fourfunction (add, subtract, multiply and divide), eightdigit units with a seven segment output circuit. The entire electronics are housed on a chip area of only 166 x 162 millimetres.

In the United States these chips are already in production and coming off the line at the rate of some 75,000 every four weeks. The Company also reports that orders for the chips in the U.K. have already exceeded £100,000.

Heat sinks are comparatively uninteresting items of electronic hardware. Usually, they consist of a piece of metal often with fins protruding. Their purpose in life is to conduct heat and to dissipate it.

A new introduction is a hollow heat sink which spreads the heat evenly. The difference in temperature between the heat-producing element (say, a power transistor) and the furthest point on the heat sink is only around 1°C.

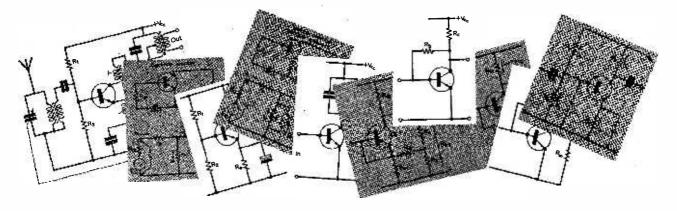
The heat sinks are fabricated rather like a hot water radiator. The hollow section is evacuated to a virtual vacuum. Water is then fed in. Because the air pressure is so low, the water boils. It then starts to lose heat and also gives off steam which condenses and turns back into water again. Eventually, equilibrium is established and the heat sink cools to room temperature.

The spread of heat on these sinks is extremely fast and the fins may be connected to the heat source by a pipe which has also been evacuated and filled with water. The fins may thus be located remotely from the heat source and the difference of 1°C holds over any part of the heat sinking system.

The cry still goes on about pollution, and electronics has come up with some useful ideas for monitoring. One research laboratory is busily engaged on producing an infra red diode which will emit radiation in the 3 to 6μ m band. Carbon monoxide, carbon dioxide and hydrocarbons all absorb radiation strongly in this band and thus the amount of absorption of the radiation gives a measure of the pollution of these chemicals. Infra red diodes already exist, but they radiate at around 0.9μ m and hence the need to design a new diode with radiation in the required region.







PART 14 TRANSISTOR CIRCUITRY for beginners

Feedback etc.

Queries have arisen about our use of the term 'feedback' and its relation to equalisation.' This month, while, at the time of writing, colleague Mike Hollier basks in holiday sunshine, seems as good a time as any to indulge myself in a little explanation of the terms we are using and why.

First, feedback. This is simply, as explained last month, a method of picking off part of the output from an amplifier and 'feeding it back' to the amplifier's input section. The feedback can be a simple resistor from collector to base of a single stage amplifier Fig. 67 (a), can be in series with the source signal (b) or in shunt with it (c).

Note that I have deliberately reverted to p.n.p. transistors in these examples. One reason is to remind you of the opening of this series of articles, where the precise examples were quoted; the other is to be able more easily to explain the action of the feedback. Here, I must insert the warning that people, like me, who were brought up on valves began to find difficulties with the revision of feedback concepts as applied to transistors, principally because the operation of transistor circuitry depends on the relationship of the 'circuit blocks' to each other. One has to consider the input and output 'loads' very much more than one did when dealing with valved circuits. So I use the germanium transistor circuits to lead into my subject---don't worry, it will get more complicated later on. . . .

The three examples of Fig. 67, are all of negative feedback. That is, the re-applied signal tends to reduce the gain of the amplifier. Its purpose, of course, is not *just* to reduce the gain but also to stabilise the circuit, help reduce noise and internally generated distortion. The feedback can be applied over several stages, not just the simple sub-circuit shown. And here it is shown as resistive feedback, i.e., effectively d.c. But we shall later be concerned with a.c. feedback, with capacitors in the loop, so that the amount of gain reduction varies as the frequency the circuit is handling also changes. Which will bring us to equalisation: which I would define as the application of frequency-dependent feedback. Taking Fig. 67 in detail, (a) combines both a.c. and d.c. negative feedback if we insert a series capacitor (shown dotted) with the collector-base resistor R_F and retain the d.c. conditions by the negative feedback across the emitter resistor R_E . Apart from the emitter resistor effectively increasing the

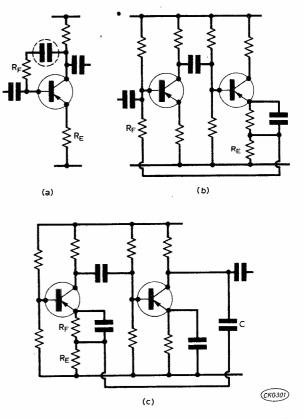


Fig. 67 (a): Simple collector/base negative feedback with d.c. blocking capacitor ringed. Change in value here affects a.c. feedback. (b) series feedback. (c) shunt feedback, from collector of second stage to emitter of first.

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input resistance to the transistor, which is an advantage, it reduces the gain by being added to the denominator of the formula for voltage gain.

In the sub-circuit (b), the voltage developed across R_E is fed back in series with the lower part of the base bias potentiometer, the latter becoming R_F , and in (c), which is voltage feedback rather than current feedback, as before, R_E does its job in the first emitter while R_F picks off a portion of the amplified signal, the amount dependent on C, and modifies the reduction of gain which R_E is already effecting.

All this has been discussed before, and the relative figures and formulæ given in detail. It does not do us any good going over the same ground, but keep the above three examples in mind as basic 'styles' of feedback when we come to consider the action of equalising circuits. In talking of the virtual resistance circuits during Parts 11, 12 and 13 the point of relative gain with and without feedback, and the change in effective resistance should have been made clear.

Corrective feedback

Why do we want equalisation? If the source itself was 'linear', there would be no need of more or less gain at special frequencies. But there are reasons of plain mechanics and basic magnetics that demand the 'tailoring' of response curves of the input circuits of an amplifier.

Consider the case of a magnetic pick-up cartridge. Because of its construction—virtually a coil in which a moving metal piece causes a changing voltage by altering a magnetic field—and is therefore an inductance, not a pure resistance. The formula for the reactance (an a.c. term for resistance, no more) of a coil is $X_L = 2\pi f L$, where X is the reactance, f the frequency the coil is handling and L its inductance. We will neglect the small resistance of its windings in the case of the pick-up cartridge.

From this, we can see that the higher the frequency, the greater the reactance. So it would seem that our corrective feedback to handle an input from a cartridge need only reduce the gain in proportion to the frequency of the signal—which, in fact, it does.

But the problem is worse than this. To get the

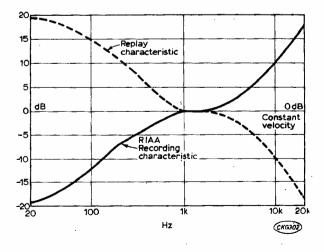


Fig. 68 : RIAA recording characteristic as practically employed. Mirror image replay characteristic dotted. Note the short 'plateau' around 1kHz.

dynamic range on to the disc and to maintain as good a signal-to-noise ratio as possible, the bass is attenuated and the treble enhanced. By international agreement, the way in which this is done conforms pretty closely to a standard. This is the RIAA characteristic, Fig. 68.

Modern discs are supposed to be recorded to this characteristic, although any enthusiast will tell you that there are some suspicious variations, difficult to prove except by comparison.

Unfortunately, a magnetic cartridge produces an output (voltage) proportional to its stylus movement. That is to say, it should. So if the characteristic is level, the output should be constant. Over a small portion of that given curve in Fig. 68 the characteristic is level, so testing only at this one frequency cannot give a true picture of the performance of either cartridge or pre-amplifier.

If we now consider how a disc is made, we shall see that the RIAA bass attenuation means that at frequencies below about 1kHz the velocity of the stylus will be reduced, although the amplitude remains constant, just as it very nearly remains constant at the higher frequencies, where the velocity now rises. In fact, the 'average' slope of the given curve is around 4dB per octave, instead of the more generally regarded 6dB per octave, which would be the ideal slope over the two nearly straight portions of the curve. (See also Fig. 71.)

To put matters in perspective, 6dB per octave means that the output voltage doubles for each octave upwards. So a bass note, say A4, the lowest of the white keys, whose frequency is 27.5Hz, giving, say, 1 millivolt at a certain loudness, would be compared with the top A on the piano 'third white note from the top, Joe', at a frequency of 3250Hz, would give 64mV if the original sound had been at the same level.

In fact, this circumstance would not so often apply, and our correction curve can be a replica of the original, mirrored, as shown dotted in Fig. 68 and the dynamic range could be left to take care of itself if the input sensitivity of the pre-amplifier and its overload characteristic are both in order. Too often, one or other is not.

As intimated in Part 11, one reason for the Cambridge style of virtual earth pre-amplifier was to achieve a very much better than usual overload performance. The average output of a magnetic cartridge is between 5 and 8mV (from a voltage output of between 1 and 1.5mV per centimetre per second of recorded velocity). But therein lies the rub.

Bass end overload

We have already seen that it is advisable in the interests of best signal handling to keep our variable controls (volume, tone and balance) after the input circuits. So our magnetic pickup circuit has to be able to handle signals from a couple of millivolts or less to 60mV or more. In practice, because there is bass boost applied during replay to make up for that attenuation during recording, the problem arises at the bass end, and we find that most preamplifiers will handle modern records if they have within a 3-30mV input sensitivity ratings. A 30dB overload rating is sometimes specified. If you consider that maximum velocity at 1kHz could be around 25cm/sec and that a cartridge with an output as



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1.5mV/cm/S would give 38mV from such a recorded groove, you can see that distortion on signal peaks would be inevitable, as this would require an overload rating of some 38dB.

So the overload safety margin diminishes toward the lower end of the frequency spectrum, and this is where mains hum, disc rumble, turntable rumble and other problems can rear their ugly heads. Hence the need, when we design our 'front-end' amplifiers to ensure that we get good gain figures before applying our feedback—and, what is more, a stable amplifier without (or with minimum) feedback, for it is precisely at this dangerously low end of the spectrum that the feedback will be least.

This is not the place to go on about cartridges, but I hope I have helped clear up a few of those queries about the need for good basic pre-amplifier design as well as the application of very precise feedback. And perhaps dropped a few hints about choice of pickup: if you have an amplifier with a sensitive magnetic pickup pre-amplifier and shove a high output cartridge into it, you can expect a bit of bass overload. As this occurs before any control you can apply, there is no real cure except correct matching.

In practice

One could quote extensively from commercial circuits to prove a point, but to combine our previous talk about virtual earth circuits and to use a design which has been proven by constructors, let me cite the modular pre-amplifier by John L. Linsley Hood, which appeared first in *Wireless World* in July 1969, and which, although parts have been modified since, happens to suit our purpose. Mr. Hood has kindly consented to allow us to quote him.

Fig. 69 shows his basic concept of a stage used to obtain the RIAA replay characteristic. Looking at it carefully, we see that it is again a virtual earth design, with point X the null point, provided the gain of the amplifier is high enough. The input impedance of the circuit will be approximately equal to that of the input network R1/C1. The load resistance of a magnetic cartridge is around $47k\Omega$ at 1kHz, and provided C2 is large enough and R2 equal

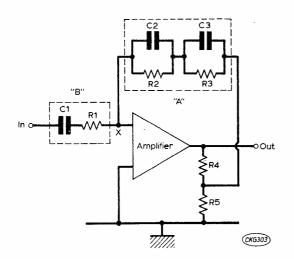


Fig. 69: Frequency selective feedback to achieve the RIAA replay characteristic, applied around a virtual earth amplifier.

to R1, C3 relatively small in relation to R2 (at 1kHz), stage gain can be given approximately by R4+R5/R5.

The designer aimed at a gain of 10, this being deemed sufficient to deal with outputs between 4 and 10mV. The frequency response is determined by the two networks 'A' and 'B', shown in dotted 'boxes' in Fig. 69. In this idealised state, the circuit is not entirely practical, of course. Fig. 70 shows the actual circuit, drawn so that these frequency corrective components are at the front.

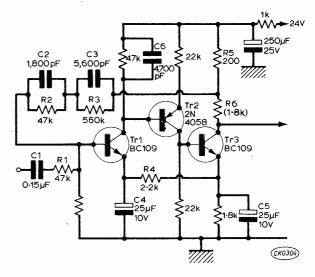


Fig. 70: The redrawn circuit of Fig. 69, part of the J. L. Linsley Hood modular pre-amplifier.

But we must also consider the effect of C4 and C5, which, in conjunction with C1 and R4, give a steepcut rumble filter (18dB/octave) with an attenuation of more than 40dB at 8Hz and a turnover point of 25Hz. The results can be seen in the RIAA replay curve, measured from the pre-amp, in Fig. 71.

Two things remain to be mentioned. C6 is put across the collector load of the first transistor to sharpen up the transient response: the dotted curve

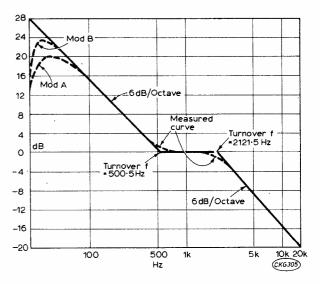


Fig. 71: Theoretical RIAA replay response curve with measured deviations. Bass roll-off is deliberately obtained by component changes.

at the bass end of this curve is in two parts. The lower is for the circuit shown; the higher, for a modified circuit. The last because the author (Mr. J. L. Linsley Hood), suspects that sufficient recording bass lift is not always given to accord with RIAA standards, and he consequently changed some values of his feedback components to get a flatter response down to 25Hz with a steeper roll-off as a protection against rumble.

These changes were as follows: $R5-470\Omega$, $R6-1.5k\Omega$, $C1-0.47\mu$ F, C3-6.800pF and C6-6.800pF.

These modifications reduce the gain, and he has thus added a sub-circuit that we can now include in our armoury—the floating emitter, collector-follower. We show his addition in Fig. 72.

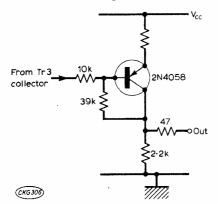


Fig. 72: A floating emitter collector-follower stage added to compensate for loss of gain.

Coping with the outputs of both magnetic and ceramic pick-up cartridges may seem a bit ambitious and, as done commercially, is not always very effective. But one can do it by switching those networks, 'A' and 'B' of our Fig. 69.

A ceramic cartridge normally likes to 'see' an impedance of a megohm or more at the amplifier input and as it is a capacitative device will suffer from low-frequency loss if this input is reduced. Hence the poor performance of many cheap record players, which have to suffer the design constric-tions of transistor amplifiers with high input impedance, while retaining the best possible gain and noise performance. By using the virtual earth configuration, one gets over this problem neatly and the three suggested sub-circuit alterations by Mr. Hood are shown in Fig. 73. Here we have (a) a network that will retain the curve sensibly level down to about 30Hz, with the bass roll-off now made better by halving the values of C4 and C5 as well. And (b), a change to network 'B', while 'A' is as in the first modification. This is a suggestion by the author to obtain a 6dB/octave rise, followed by a level response, making a 'platform' over the portion of the replay curve of Fig. 68 that is fairly level from around 1kHz to around 2kHz.

To get even more treble response, without nasty peaks, i.e., to give this same 'platform' effect to a 12dB level after about 4kHz, (c) is suggested. The reason for these changes is to equalise for the 12dB drop in voltage anticipated when an RIAA recording (having velocity characteristics) is replayed with a displacement-sensitive device, such as a piezo-electric cartridge. As you can see, the modification entails shunting part of the input resistor with a small capacitor.

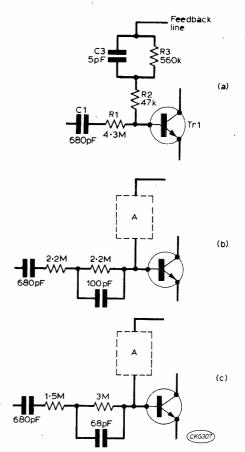


Fig. 73: Circuit changes to permit a ceramic cartridge to be fed into the same amplifier with (a) level response above 35Hz (b) a 6dB lift from 1 to 2kHz and (c) a 12dB lift at 6dB/octave, followed in each case a level response.

This, finally, brings me to the point that Mike asked me to make after last month's contribution had made its way irrevocably to the printers, viz., a capacitor shunted across the feedback resistor will give treble reduction while if it is across the input series resistor it gives treble lift, as in this previous example.

Just thought you'd like to know ... !

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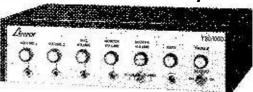
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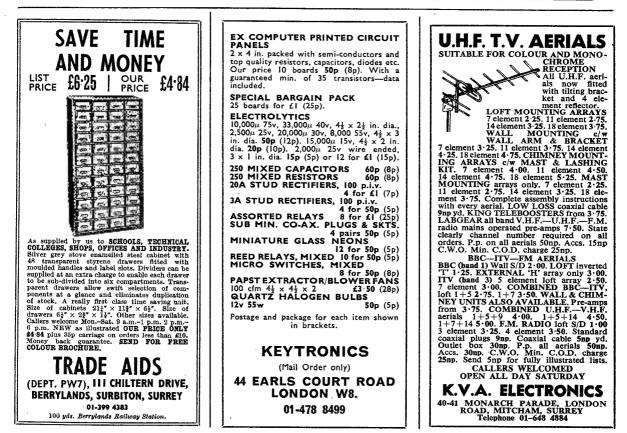
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	C141	0 14	AF125	0.28	BC161	0.50	BD185 BD186	0.65	BF263	0.55	OC41	0.20	2N388	0.82		0.21	2N3405	0.42	2N4291	0.17
	CIAIK	0.17	AF120	0.28	BC167	0 12 0 12	BD186 BD187	0.65	BF270	0.82	OC42	0-24	2N388A	0.55	2N2714	0.21	2N3414	0.15	2N4292	0.17
	C142	0.14	AF139	0.30	BC169	0.12	BD187 BD188	0 70 0 70	BF271 BF272	0.30	OC44	0.15	2N404	0.20		0.17	2N3415	0.15	2N4293	0.17
	C142K	0.17	AF178	0-50	BC170	0.12	BD189	0.75	BF272 BF273	0.80	OC45 OC70	0.12	2N404A	0.28	2N2904A		2N3416	0.28	2N5172	0.12
	C15 1	0.15	AF179	0.50	BC171	0.14	BD190	0.75	BF274	0.35	0071	0.10	2N524	0.42	2N2905	0.21	2N3417	0.28	2N5457	0.32
	C154	0.20 .	AF180	0.50	BC172	0.14	BD195	0.85	BFW10	0.60	0072	0.14	2N527 2N598	0.49	2N2905A	0.51	3N3525	0.75	2N5458	0.32
	C155	0.20	AF181	0.45	BC173	0.14	BD196	0.85	BFX29	0.27	0074	0.14	2N598 2N599	0.42	2N2906 2N2906A	0.15	2N3646	0.09	2N5459	0.40
A	C156	0.20	AF186	0.45	BC174	0.14	BD197	0.90	BFX84	0.22	OC75	0.15	2N 599 2N 696	0.12		0.18	2N3702	0.10	25301	0.50
A	C157	0.24	AF239	0.37	BC175	0.22	BD198	0.90	BFX85	0.30	OC76	0.15	2N695	0.12	2N2907A		2N3703	0.10	2S302A	0.42
	C165	0.20	AL102	0.65	BC177	0 19	BD199	0.95	BFX86	0.22	OC77	0.25	2N 698	0.24		0.14	2N3704 2N3705	0.10	28302 28303	0.42
	C166	0.50	AL103	0.65	BC178	0.19	BD200	0.95	BFX87	0.24	OC81	0.15	2N699	0.35		0.14	2N3705	0.09	28303	0-55
	C167	0.20	ASY26	0.25	BC179	0.19	BD205	0.80	BFX88	0.22	OC81D	0.15	2N706	0.08		0.14	2N3707	0.11	28304	0.90
	C168	0.54	A8Y27	0.80	BC189	0.24	BD206	0.80	BFY50	0.20	OC82	0.15	2N706A	0.09	2N2926 (G		2N3708	0.07	28306	9.84
	C169	0.14	ASY28	0.22	BC181	0.24	BD207	0.95	BFY51	0.20	OC82D	0.15	2N708	0.12		Ó·12	2N3709	0.09	28307	0.84
	C176	0.20	ASY29	0.25	BC182	0.10	BD 208	0.95	BFY52	0.20	OC83	0.20	2N711	0.30	2N2926 (Y		2N3710	0.09	28321	0.56
	C177	0.24	ASY50	0.25	BC182L	0.10	BDY20	1.00	BFY53	0.17	OC84	0.20	2N717	0.35		Ó·11	2N3711	0 09	28322	0.42
	C178	0.28	ASY51	0.25	BC1B3	0.10	BF115	0.24	BPX25	0.82	OC139	0.20	2N718	0.24	2N2926 (O		2N3819	0.28	28322A	0.42
	C179 C180	0.28	ASY52	0.25	BC183L	0.10	BF117	0.45	BSX19	0.12	OC140	0.20	2N718A	0.50		0.10	2N3820	0.50	28323	0.56
	C180K	0·17 0·20	ASY54	0.25	BC184	0.12	BF118	0.70	BSX20	0.12	OC169	0.25	2N726	0.28	2N2926 (F	()	2N3821	0.35	28324	0.70
	C180 K	0.17	ASY55 ASY56	0.25	BC184L	0 12	BF119	0.70	BSY25	0.12	OC170	0.25	2N727	0.28		0.10	2N3823	0.28	28325	0.70
	C181K	0-20	ASY57	0.25	BC186 BC187	0.28	BF121 BF123	0.45	BSY26 BSY27	0.15	OC171	0.25	2N743	0.50	2N2926 (B		2N3903	0.28	28326	0.70
	C187	0.22	ASY58	0.25	BC207	0.28	BF123 BF125	0-50	BSY28	0.15	OC200	0.25	2N744	0.20		0-10	2N3904	0.80	28327	0.70
	C187K	0.20	ASZ21	0.40	BC208	0.11	BF127	0.50	BSY29	0.15	OC201 OC202	0 · 28 0 · 28	2N914 2N918	0.14		0.70	2N 3905	0.58	28701	0.42
	C188	0.22	BC107	0.09	BC209	0.12	BF152	0.55	BSY38	0.18	OC202	0.25	2N918 2N929	0 30 0 21		0.14	2N3906	0.27	40361	0 40
	C188K	0.20	BC108	0.09	BC212L	0.11	BF153	0.45	BSY39	0.18	OC204	0.25	2N930	0 21	2N3053	0:17	2N4058	0.15	40362	0.45
	CY17	0.25	BC109	0.10	BC213L	0.11	BF154	0.45	BSY+0	0.28	OC205	0.35	2N1131	0.20						
	CY19	0.20	BC113	0.10	BC214L	0.14	BF155	0.70	BSY41	0.28	OC309	0.40	2N1132	0.22						
	CY19	0.20	BC114	0.15	BC225	0.25	BF156	0.48	BSY95	0·12	P346A	0.20	2N1302	0.14		DIOD	ES AND	RECTIF	IERS	
	CY20	0.20	BC115	0.15	BC226	0.85	BF157	0.55	BSY95A	0.12	P397	0.42	2N1303	0.14	AA119	0.08	BY133	0 21	OA 10	0.85
	CY21	0.50	BC116	0.12	BCY30	0.24	BF158	0.55	Bu105	2.00	OCP71	0.48	2N1304	0·17		0-08	BY164	0.50	0.447	0.07
	C T 22	0.16	BC117	0.12	BCY31	0.56	BF159	0.60	C111E	0.50	ORP12	0.48	2N1305	0.17		0.08	BYX 38/3		OA70	0.07
	CY27	0.18	BC118	0.10	BCY32	0.80	BF160	0-40	C400	0.30	ORP60	0.40	2N1306	0.21		0.09		0.42	OA79	0.07
	CY28	0.19	BC119	0.30	BCY33	0.22	BF162	0.40	C407	0.25	OBP61	0.40	2N1307	0.21		0.10	BYZ10	0.85	OA81	0.07
	CY29	0.35	BC120	0.80	BCY34	0.25	BF163	0.40	C424	0.20	ST140	0.15	2N1308	0.23		0.10	BYZ11	0.30	OA85	0.09
	C¥30 C¥31	0 · 28 0 · 28	BC125 BC126	0.12	BCY70	0.14	BF164 BF165	0.40	C425	0.50	ST141	0.17	2N1309	0.53		0 21	BYZ12	0.30	OA90	0-06
	CY34	0.28	BC120 BC132	0·18 0·12	BCY71 BCY72	0·18 0·14	BF165 BF167	0.40	C426 C428	0.85	TIS43	0.30	2N1613	0.20		0.22	BYZ13	0.25	OA91	0.08
	CY35	0.21	BC132 BC134	0.12	BCI12 BCZ10	0.20	BF107 BF173	0.22	C428 C441	0 20	UT46 2G301	0.27	2N1711	0.20		0.14	BYZ16	0.40	OA95	0.07
	CY36	0.28	BC135	0.12	BCZ11	0.25	BF176	0.35	C441 C442	0.30	26301	0.09	2N1889 2N1890	0.32		0.12	BYZ17	0.35	OA200	0.06
	CY40	0.17	BC136	0.15	BCZ12	0 25	BF177	0.35	C444	0.30	2G302	0.19	2N1890 2N1893	0·45 0·37		0.14	BYZ18	0.35	OA202	0.07
		0.18	BC137	0.15	BD121	0.60	BF178	0.80	C450	0.22	26304	0.24	2N1893 2N2147	0-72		0·13 0·15	BYZ19 CG62	0.28	SD10	0.05
	CY44	0.85	BC139	0.40	BD123	0.65	BF179	0.30	MAT100	0.19	2G304	0.40	2N2148	0.57		0.12	(Eg) OA9	1	8D19 IN34	0.05
	D130	0.38	BC140	0.80	BD124	0.60	BF180	0.30	MAT101	0.20	2G308	0.35	2N2160	0.60		0.17	(Lug) UAS	0.05	IN34 IN34A	0.07
	D140	0.48	BC141	0.30	BD131	0.50	BF181	0.80	MAT120	0.19	2G309	0.35	2N2192	0.35		0.12	CG651	V. 00	1N914	0.07
	D142	0.48	BC142	0.80	BD133	0.60	BF182	0.40		0.20	2G339	0.20	2N2193	0.35		0.14	(Eq) OA7	0.	1N914 1N916	0.06
	D143	0-38	BC143	0.80	BD133	0.65	BF183	0.40	MPF102	0.42	2G839A	0.16	2N2194	0.35		0.15	OA79	0.06	IN414B	0.06
	D149	0.50	BC145	0.45	BD135	0.40	BF184	0.25	MPF104	0.87	2G344	0.18	2N2217	0.22		0.15	OA5	0.35	18021	0.10
A	D161	0.33	BC147	0.10	BD136	0.40	BF185	0.30	MPF105	0.37	2G345	0.16	2N2218	0 20		0·16	OA5SL	0.21	18951	0.08
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 30
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 25
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 ORP12 43p ORP60, O RP61 40p each 1140 **U41** 10 VHF Germanium PNP Transistors TO-1 NKT667, AF117 0.50 GENERAL PURPOSE $\overline{\mathbf{U42}}$ GENERAL PORPOSE NPN SILICON SWITCH-ING TRANS. TO-18 SIM. TO 2N706/8. BSY-27/28/95A. All usable devices no open or short **Ú43** 20 Sil. Trans. Plastic TO-5 BC115/NPN 0.50 **U44** 7 3A SCR. TO66 up to 600PIV 1.00 U45

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Numerical Height (mm)	16	13	9	point. All si viewing. Fu
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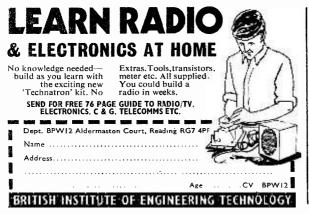
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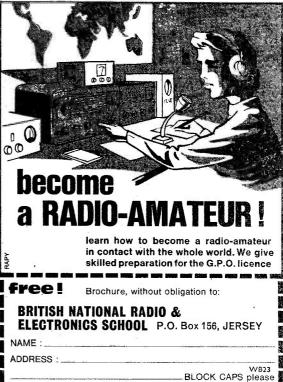
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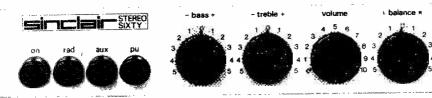
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Sinclair Project 60

Stereo 60



Built and tested post free £9.98

pre-amplifier/control unit

The versatility of Project 60 high-fidelity modules is well demonstrated in this excellent unit. It provides the facilities essential to good stereo and will enhance the quality of any system it is used with, whether Project 60 or any any other top line power amplifiers. Compact, yet robustly constructed, the unit is easily panel mounted and will operate satisfactorily from 18 to 35 volts supply. Silicon epitaxial transistors are used throughout to achieve a very high signal to noise ratio with excellent separation between channels. Distortion at maximum output is barely 0.02% with magnetic p.u. input. Accurate equalisation is provided for all inputs, which are selected by push buttons. For maximum effectiveness, the Sinclair A.F.U. is recommended for use with the Stereo 60 pre-amp/control unit. A comprehensive manual supplied with Project 60 modules makes installing and connecting easy and ensures best possible results from your system.

SPECIFICATIONS

Input sensitivities: Radio-up to 3mV. Mag. p.u. 3mV correct to R.I.A.A. curve ± 1 dB, 20 to 25,000 Hz. Ceramic p.u. -up to 3mV; Aux-up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB.

Tone controls: TREBLE ± 12 to -12dB at 10KHz; BASS +12 to -12dB at 100Hz. Front panel: brushed aluminium with black knobs and controls.

Size: $66 \times 40 \times 207$ mm.

Project 605

Super IC.12 Integrated circuit high fidelity amplifier



Hav ng introduced Integrated Circuits to hi fi constructors with the IC.10, the first time an IC had ever been made available for such purposes, we have followed it with an even more efficient version, the Super IC.12, a most exciting advance over our original unit. This needs very few external resistors and capacitors to make an astonishingly good high fidelity amplifier for uses with pick up, F,M. radio or small P.A. set up, etc... The free 40 page manual supplied, details many other applications which this remarkable IC, make possible, It is the equivalent of a 22 tran

sinclair

sistor circuit contained within a 16 lead DIL package, and the finned heat sink is sufficient for all requirements. The Super IC.12 is compatible with Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board.

SPECIFICATIONS

Output power: 6 watts RMS continuous (12 wattspeak). 6-80. Frequency Response: 5Hz to 100KHz±1dB. Total Harmonic Distortion: Less than 1%. (Typical 0·1%) at all output powers and frequencies in the audio band (28V). Load Impedance: 3 to 15 ohms. Input Impedance: 250 Kohms nominal. Power Gain at 90dB (1.000.000.000 times) after feedback. Supply Voltage: 6 to 28V. Quiescent current: 8mA at 28V. Size: 22×45×28mm including pins and heat sink. Manual available separately 15p post free.

> With FREE printed circuit board and 40 page manual **£2.98** Post free

The easy way to buy and build Project 600 Project 600 Project contains one PZ5. two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules: Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to

the Project 605 method of connecting, Complete Project 605 pack with £29.95 Everything you need to assemble a superb 30 watt high fidelity stereo amplifier without having

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Z.30 & Z.50 power amplifiers

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The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8Ω) and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that Z.50s and Z.30 may be used in a far wider range of applications.

SPECIFICATIONS (2.50 units are interchangeable with Z.30s in all applications).—Power Outputs: Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 3 ohms using 30 volts. Z.50 40 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 8 ohms using 50 volts. Frequency response: 30 to 300.000/Hz± 165. Distortion: 0.02% into 8 ohms. Signal to noise ratio: better

than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms (for 15w into 8Ω). For speakers from 3 to 15 ohms impedance. Size: 14 x 80 x 57mm.

Project 60 Stereo F.M. Tuner

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stero decoder and switchable squelch circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems.

SPECIFICATIONS—Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108MHz. Sensitivity: 7µV for lock-in over full deviation. Squelch level: Typically 20µV. Signal to noise ratio: > 66dB. Audio frequency response: 10Hz – 15KHz (±1dB). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2µV. Cross talk: 40dB. Output voltage: 2 x 150mV R.M S. maximum Operating voltage: 25–30VDC. Indicators: Stereo on; tuning. Size: 93 x 40 x 207mm.

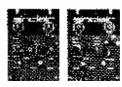
A.F.U. High & Low Pass Filter Unit

For use between Stereo 60 unit and two Z.30s or Z.50s. The unit is very easily mounted and is unique in that the cut-off frequencies are continuously variable. As attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is suitable for use with any other amplifier system. There are two filter sections - rumble (high pass) and scratch (low pass). H.F. cut-off (--3dB) variable from 28KHz to 5KHz. L.F. cut-off (--3dB) variable from 25Hz to 100Hz. Distortion at 1KHz (35V. supply) 0.02% at rated output. Operating voltage from 15 to 35V. Current 3mA. Size: 66 x 40 x 90mm.

Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 or PZ.8 where a stabilised supply is essential

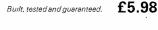
System	The Units to use	together with	Units cos
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc.	£4.48
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control, etc.	£9.45
12W. RMS continuous sine wave stereo amp. for average needs	2 x Z.30s, Stereo 60 ; PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc	£23.90
25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60 ; PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms)	2 x Z.50s, Stereo 60 ; PZ.8, mains transformer	As above	£34.88
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43
F.M. Stereo Tuner (£25) & A	.F.U. (£5.98) may be	e added as required.	





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PZ.8 45 volts stabilised

PZ.8 mains transformer

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Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defect arise in normal use, we will service it at once and without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically £1.00) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.

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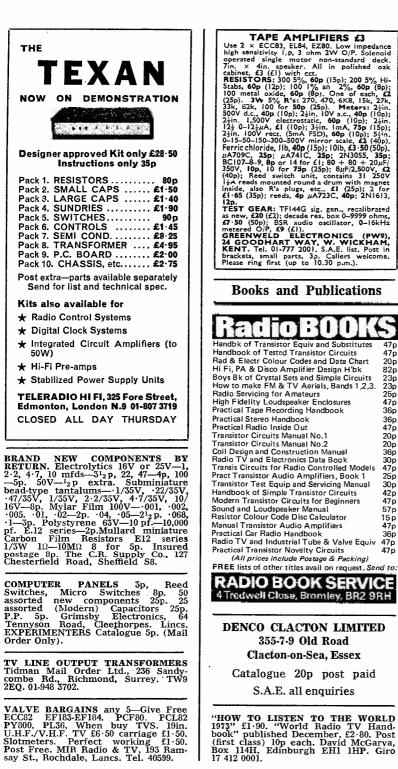
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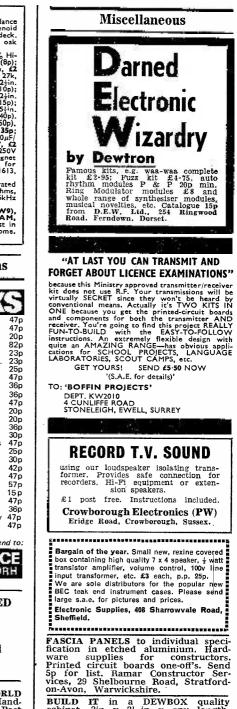
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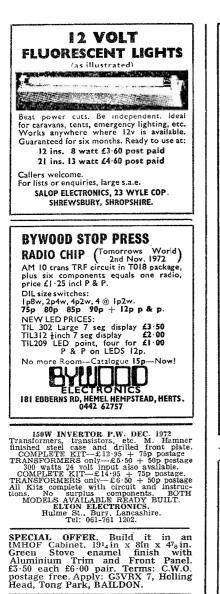


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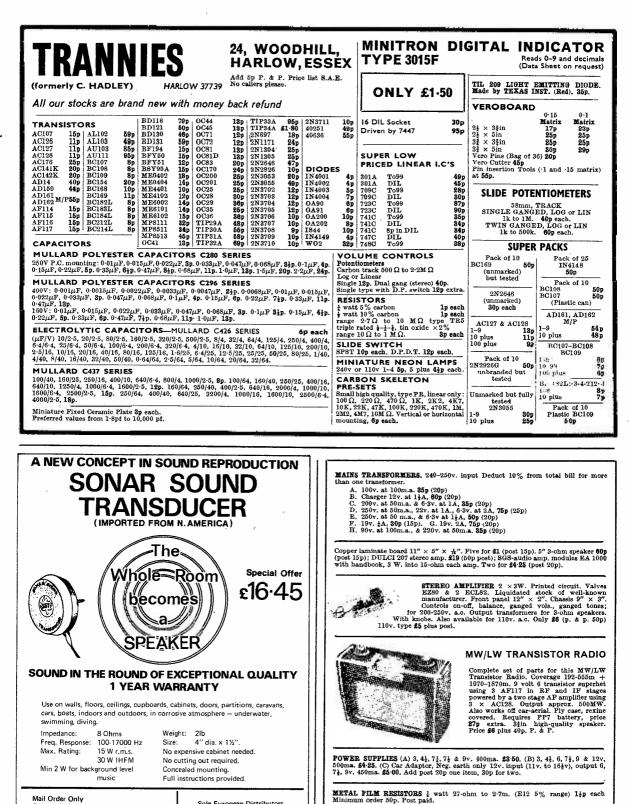
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