

## RSB HIGH-FIDELITY STEREO PACKAGE


$\star$

* TA12 AMPLIFIER housing * GARRARD SP25 MK III Player * SONOTONE 9TAHC Ceramic P.U Cartridge with damond stylus Loudspeaker Units Special Total Price Or Deposit $\mathbf{£} 8 \cdot 40$ \&
£59:00 $\mathbf{5 6 . 3 2}$ (Total $\mathbf{£ 6 5 \cdot 2 8 \text { ). Carr. } £ 1 . 2 5}$ Trans. Plastic Cover $£ 3 \cdot 15$ extra. PACh AGE AS ABOVE but with Garrard 3000 Antochanger and Sonotone 9TA Ceramic Car-
tridge in lieu of SP25
Sh

Matching as recommended for optimum performance
Package prices apply providing all individual units are purchased from any branch within 3 months. See leatlet Or Deposit $£ 7.50$ and 9 monthily Terms: Deposit $£ 13.63$ and 9 monthly payments $£ 10 \cdot 62$ (Total $£ 109$ 21). payments $\mathbf{f 5} 64$ (Total $\mathbf{f 5 8} \mathbf{2 6}$ )
'YORK' HIGH-FIDELITY 3 SPEAKER SYSTEM
 * Performance comparable with units costing considerably more Consists of (1)12in. 15 walt Bass unit whts cast chassis. Roll ruthber cone

 ions. Terns: De1, $£ 4 \cdot 60$ and 9 monthly paytuents $£ 2.47$ (Total $£ 26.83$ ).
DEMONSTRATIONS AT ALL BRANCHES

Individual Ganged Controls: Bass, Trehle, Volume and Balance. Printed circuit construction employing 10 Transistors plus Diodes. Output rating I.H.F.M. Frequency range $20-20,000$ c.p.s. Bass Control $\pm 12 \mathrm{db}$. Treble Control 13 dtb . Selector switch for P.U. or Tane/Radio. For loudspeaker output impedances of 3 to 15 ohms. For standard $200-250 \mathrm{v}$. A.C. mains operation. Attractive Black and Silver finished metal facia plate and matching control knobs
COMPLETE KIT OF PARTS INCLUDING COMPLETE KIT OF PARTS INCLUDING
FULLY WIRED PRINTED CIRCUIT ANA

Or FACTOKY BUILT IN TEAK VENEERED CABINET as illustrated $£ 1488$ or

## AUDIOTRINE HI-FI SPEAKER SYSTEMS

Consisting of matcled 12 in . 11,000 line 15 Watt 15 ohm high quality speaker, cross-over unit and tweeter. Smooth response and extended frequency range response and extended frequency range OR SENIOR 15 WATT INCLUDING $£ 5.95$ HF126 15,000 LINE SPEAKER
£6.95 Carr


HF126 15,000 LINE SPEAKER AUDIOTRINE HIGH FIDELITY SPEAKERS
 Plasticised Cone surrounth. "D" indicates Tweeter Cone provjding
extentid frequencr range up to 15,000 c.p.s. Impedance 3 or extended frequency range up to 15,00
8.15 ohnns. PLEASE STATE CHOICE. 8. 15 ohns. PLEASE STATE CHOICE.
Exceptional performance at low cost. Exceptional performance at low cost.
10 W
$12.88 \quad \mathrm{HF} 120 \mathrm{D} \quad 12^{\prime \prime} \quad 15 \mathrm{~W}$
\&4. 89 $\begin{array}{lccccccc}\text { HF808T } & 8^{\prime \prime} & 10 \mathrm{~W} & £ 2 \cdot 88 & \text { HF120D } & 12^{\prime \prime} & 15 \mathrm{~W} & £ 4.89 \\ \text { HF102D } & 10^{\prime \prime} & 10 \mathrm{~W} & £ 3.40 & \text { HF126 } & 12^{\prime \prime} & 15 \mathrm{~W} & £ 5.75 \\ \text { HF120 } & 12^{\prime \prime} & 15 \mathrm{~W} & £ 4.50 & \text { HF126D } & 12^{\prime \prime} & 15 \mathrm{~W} & £ 6.25\end{array}$ FANE 807T HIGH FIDELITY SPEAKER enclosure. Cast chassis Koll P.V.C. cone surround anil long throw voice
coil to achicse very low findanental resonance of 30 c.l.s. Tweeter
cone is tited to cone is fited to extend
15 KHz Gauss 10.000 .
PILEASE STATE 1 MI
$\$ 3.85$

## HIGH FIDELITY LOUDSPEAKER UNITS

Cabinets latest style Satin Teas veneer. Acoustically lined or filled acoustic damping. Ported where appropriate. Credit terms available. DORCHESTER (IIlustrated) Size $16 \times 11 \times 9$. appr. Range $50-16,000$ STANWAY with highly flexille cone surround, long throw roice coil and 10,000 linc magnet. High 8 ohms, (ives smooth realistic somnd output. See 'packnge offers' for $\mathbf{1} 19.35$
R.S.C. TAI2 MKIII $6.5+6.5$ WATT STEREO AMPLIFIER
 HIGH FIDELITY OUTPUT OF 6.5 WATTS PER CHANNEL Designed for optimum performance with any crystal
or ceramic (?ram. P.U. cartridge, Radio tuner, Tape recorder etc. $\star 3$ reparate suitched input socketa on each channel * Separal.e Rass and Trebte controls $\star-15$ ohms $\star$ For $200-250$ v. A.C. mains $\star$ Frequency Response $20-20,000$ c.p. . . $\quad 2 d \mathrm{H} \rightarrow$ Harmonic Distor


 WIRING DIAGRAMS ARTS WITAFUNL $£ \mathbf{1 5} 50$ Carr. Factory built with $£ 19.50$ Deposit $£ 3$ and 9 mithly pyints $£ 2.15$ (Total $£ 22.35$ ). Or it Teak vencer housing $\mathbf{4 3}$

HI-FI SPEAKER ENCLOSURES MODERN DESIGN Teak reneer finish. Acoustically lined. Sizes approx. Carr. 35 p . per enc
JE8 Size $16 \times 11 \times 9 \mathrm{in}$. SE8 For ontimum nerformPresurrised Gives Dlesing ance with anesm
 8 in . Hi-Fispeaker. $\leq 5.35 \times 15 \times 9 \mathrm{in}$.
 with loin. Hi-Fi spkr. Size $24 \times 15$ \&6.74


## R.S.C. BATTERY/MAINS CONVERSION UNITS

 TYPE BM1. An all-dry battery eliminator. Size $5 \frac{k}{} \times 4 \times 2 \mathrm{in}$.approx. Completely replaces batteries supplying 1.5 v and 90 v , to hattery radio where A.C. mains 200/250r, $50 \mathrm{c} / \mathrm{s}$ is available.
COMPLETRK1T $\mathbf{E 3 . 2 5}$ ASMEBIBLED READY $\mathbf{E 3 . 7 5}$
WITH DIAGRAM

## R.S.C. TA6 6 Watt HI-FI AMPLIFIER

200-250v. AC mains operated. Frequency Response $30-20.000$ c.p.s.
2!1B. Jarmonic Distortion $0.3 \%$ at 1,000 c.j.s. Separate Bass abil Treble 'lift and cut' colltrols. 3 input sockets for Mike, liram, Kadio
 Complete kit of parts with tull wiring dising and instructions Complete kit of parts with full wiring diagrams and instructions.
OR FAGTORY BUILT WITH 12 MONTHS' GUARANTEE flo ${ }^{\prime} 95$


## R.S.C. MkIII SUPER 30 HIGH FIDELITY STEREO AMPLIFIER

 A completelv new desigen FURTHER IMPROVED IN BOTH APPEARANCE and PERFORMANCE. REPRESENTING VALUE FAR HIGHER THAN THE PRICES SUGGEST. Only high grade components by $\mathrm{C}_{4}$ leading manufacturers.COMPLETE KIT OF PARTS Or FACTORY BUILT with 12 months $\mathcal{O}\{2.75$ payments $£ 3.50$ (Total £37-25.) monthly LUU 10 Or FACTORY BUILT in cabinet as $\mathbf{P} 20.75$ illustrated. Dep, $£ 7$ and 9 monthly f30.75
payments $£ 3.99$ (Total $£ 42.91$ )
 SATIN SILVER METAL FACIA with black letter ing. Black edged knobs with bright silver centres * NEON INDICATOR * JACK SOCKET FOR HEADPHONES - CABINETED MODEL VENEERED IN SATIN TEAK. SUITABLE FOR ANY MODERN PICK. UP CARTRIDGE CERAMIC WI RECOMMEND USE WITH THE BEST ANCILLARY EQUIPUSE WITH THE BEST ANCILLA
MENT THAT CAN BE AFFORDED.

PRINTED CIRCUITRY TWENTY SILICON TRANSISTORS
FOUR DIODES. FOUR DIODES,
FOUR RECTIFIERS

OUTPUT : 15 watts R.M.S. (Continuous) Into 8 ohms. HUM \& NOISE -75 dB Min. Vol. 10 watts R.M.S. (Continuous) into 15 ohms. FREQUENCYRESPONSE:-3dB 7 Hz to $70 \mathrm{kHz} \quad 0.1 \%$ at 1000 Hz 10 Watts TREBLE CONTROL: +16 dB to -12 dB at 14 kHz
BASS CONTROL: +17 dB to -16 dB at 40 Hz CROSS TALK -58 dB SENSITIVITIES: Disc Mag. 2.5 mV . Ceramic 35 mV . Radio 120 mV . Tape 120 mV . REAR PANEL SOCKETS ARE FOR 3 PAIRS OF INPUTS (1) P.U. (2) Radio.
(3) Tape Amp. Plus pair for tape recorder signal take off and 2 pairs for speaker (3) Tape Amp Bass, Treble and Balance. Plus Ceramic MagP.U. Switch. $\quad$ Connections.
RSC STEREO HI-FI TUNER NOW AVAILABLE. Visually matches Super 30 Mklll £44.95


R.S.C. AIO 30 WATT ULTRA LINEAR
 $\pm 3 \mathrm{~dB} 30-20,000 \mathrm{c} / \mathrm{s}$. All high grade components. Vaives EF80,
 Sensitivity 36 millivolts. For High Impedance microphones. For Cinbs, Schools, Theatres, Dance Halla, Outdoor Functions, etc. For Electronic Organ, Guitar, String Bass, etc. Gram, Radio or Tape. Two separate Inputs with vol. controls permit such as "mike" and Pick-1pp etc. to be used
for miling purposes, $200-250 \mathrm{v} .50 \mathrm{c} / \mathrm{s}$ A.C. malns. For 3 and 15 ohm speakers. Com. plete Kit of parts with wiring diagram and instructions. Twin-handled perforated cover有-80. Or factory built with EL34 output Falves and 12 months' guarantee for 819.75

## Car

## TERMS: Deposit $£ 4$ and 9 monthly payments of $£ 2-10$ (Total $£ 22.90$ ). Send S.A.E. for leaf

## R.S.C. TRANSFORMERS, L.F. CHOKES \& RECTIFIERS

Primat inanin
 $230 \mathrm{v} ., 60 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{~s}$..
260-0-250v. 80 mA 6 3v 2 a 250-0-280v. 60 ODA 6 UPRIGHT MOUNTI 3 v . $2 \mathrm{~m}, 0-5-6 \cdot 3 \mathrm{v} .2 \mathrm{~s}$. $250-0.200 \mathrm{v}$. 60mA, $6.3 \mathrm{~V} .2 \mathrm{~m} ., 0-6-6 \cdot 3 \mathrm{~V} .2 \mathrm{~s}$. $300-0-300 \mathrm{v}$. $100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}, 4 \mathrm{a}, 0-5-6.3 \mathrm{v} .3 \mathrm{~s}$. $300-0-300 \mathrm{v} .130 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}$. c.t. 6.3 v . 1 a For mullard 610 Ampliffer $350-0-350 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a}, 05 \mathrm{~s}-6.3 \mathrm{v} .3 \mathrm{~m}$
 $425-0-425 \mathrm{v}-200 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} .$, c.t., 5 v.
$425-0-425 \mathrm{v} .200 \mathrm{~mA}, 6$
6
$450-0-450 \mathrm{v} .250 \mathrm{~mA}, 6-3 \mathrm{v} .48 .$, ct., 5 v TOP SHRODDED DEOP-THRO' TYPE $250-0-260 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .3 \cdot 6 \mathrm{a} . \ldots \ldots$. $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v}$. $28 . .63 \mathrm{v} .1 \mathrm{a}$. $350-0-350 \mathrm{v}$. $80 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{v}$. $250-0-250 \mathrm{v} .100 \mathrm{~mA} .6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., 0-6-6 \cdot 8 \mathrm{v} .3 \mathrm{a}$
$300-0-300 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .48 ., 0-5-6.3 \mathrm{v} .3$ $300 \cdot 0-300 \mathrm{v} .130 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}$. 4 a ., c.t. 6.3 v . 1 a Suitable for Mollard 510 Amplifter $350-0-350 \mathrm{v}, 100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}, 4 \mathrm{a} ., 0-5-6.3 \mathrm{v} .3 \mathrm{a}$


## FILAMENT of TRANSISTOR POWER PACK




 AUTO (8tep UP/step DOWN) TRANSFORHERS

 OUTPUT TRANSFORMER\& | Standard Pentode $5,000 \Omega$ or $7.000 \Omega$ to $3 \Omega$ |
| :--- |
| Push-Pull 8 watta EL 84 to $3 \Omega$ or $16 \Omega$. | Push-Pull 8 watts EL84 to $3 \Omega$ or $16 \Omega$.

Push-Pull 10 watts $6 \mathrm{~V} 6, ~ E C L 86$ to $3,5,8$ o

$$
\text { Push } 18
$$ $15 \Omega$

Push-Pr \&5-10 Push-Pull EL84 to 3 or $15 \Omega 10-12$ watts.. 25-50 $\begin{aligned} & \text { Push-Pull Ultra Linear for Mullard } 510 \text {, etc. } \\ & \text { Pash-Pull } 15-18 \text { watts, sectionslly wound }\end{aligned}$
 Push-Pull 20 watt high quality sectionally
wonnd EL34, 6L6, KT66 etc. to 3 or 15 SMOOTHING CHOKES $150 \mathrm{~mA} .7-10 \mathrm{H} .283 .30$ $70 \mathrm{p}: 100 \mathrm{~mA}, 10 \mathrm{H}, 200 \Omega 80 \mathrm{~m} ; 80 \mathrm{~mA}, 10 \mathrm{H}$, $70 \mathrm{p} ;$
$350 \mathrm{~m}=\mathrm{m} ; 60 \mathrm{~mA}, 10 \mathrm{H}, 400 \Omega \Omega 5 \mathrm{p}$.
£2.60 SELENIUM KECTHFIRFS $F$, W. (Bridged)

CREDIT TERMS AVAILABLE ON PURCHASES OVER E8 (Kits Excepted)

## PACKAGE OFFER <br> Units listed below

(a) 100 w POWER AMPLIFIER (b) PAIR OF HI-FI HEADPHONES
(c) MATCHING DYNAMIC'MIKE' (attached to headphones) (d) PAIR 50 WATT SPEAKERS Black Rexine
Cabinets Cabinets
Size approx.
$18^{\prime \prime} \times 18^{\prime \prime} \times 8^{\prime \prime}$
(a) (b) (c) 8 (d)
579.05 Terms on Amps. Speakers and Head phone/Mike. Deposit $£ 15$ and 18 monthly payments of $£ 3.95$ (Total £8610).

## FANE ULTRA HIGH POWER LOUDSPEAKERS ${ }^{\mathbf{E}}$

$15 \Omega \in \mid 0.90$
Dep 22 and 9
monthly pay-
ments 81.20 ments Total $^{2} 1 \cdot 20$ PAIR SUITABLE
ALL PURPOSES



 |  |
| :--- | :--- | :--- |
| $18^{\prime \prime} 100$ Wate |
| 14000 gauss |$\quad 15^{\prime \prime} 60$ Watt $12^{\prime \prime} 50$ Watt 14,000 gauss

$8 / 150$

14,000 gauss
$8 / 150$
$\pm 12.90$
$\$ 22.95$
Dep: 86 and 9

Dep. $23 \cdot 30$ and 9 | nithly payments |
| :---: |
| 20 (Total $£ 25 \cdot 80$ ) |
| 1.30 (Total £15). | FOR BASS GUITAR, ELECT. ORGAN, ETC

FANE SPEAKERS 'POP' $25 / 212 \mathrm{in} .25$ WATT Dual Cone $15 \Omega$ (for uses $\notin 6.75$ Carr. or Dep. 21 and 9 mithly other than Bass Guitar or
Electronic Organ). or Dep. 11 and 9 mithly
payments 75 p (Total

GROUP/DISCO EQUIPMENT PACKAGE OFFERS P.A.L. PHASE 50 ME. III AMPLIFIER
PR. FANE POP $25 / 205$ L/SPEAKERS Ternus: Deposit 86.50 and 9 monthly payments of $£ 4.72$ (Total $£ 48.98$ ) F.A.L. PHASE 50 MK III AMPLIFIER Cerms: Deposit 810 and 9 monthl payments of 85,25 (Total 257.25 ) F.A.L. PEASE 50 ME.III AMPLIFIER PAIR L12/25 25 W L/S in cabinets Terms: Deposit 810 and 9 monthly payments of 25.76 (Total 261.75 ) F.A.L. PHA8E 100 AMPLIFIER
4 FARE POP 50 L/SPEAKER8 Terms: Deporit 815.95 and 9 montbly

payments of 810.50 (Total 8110.45 ) | 834.95 | PACKAGE PRICE |
| :--- | :--- |
| 813.50 |  |
| 48.45 | $\mathbf{E 4 5} \underset{\varepsilon 1}{\text { carr. }}$ |

## HIGH QUALITY LOUDSPEAKER UNITS

ALL TWO TONE REXINE AND VYNAIR FINISH L125 50 WATT Fitted pair of $12^{\prime \prime} 50$ rating. Impedance $8-15$ ohms. Carr. $£ 1 \cdot 50$ £33:50 ating. Impedance $8-15$ ohms. Carr. 1 L12/25 $12^{\prime \prime} 25$ WATT L13 13" $\times 8^{\prime \prime} 10$ Watt
 Carr. 50p.

R.S.C.TDI DISCOCO NSOLE Incorporating twin Garrard SP25 My.II turntables and Ceramic Cartridges with dismond styli. Separate Vol. controls for each turntable. Also MONITORING FACLITIEs, plas Treble and Bass Controls. Separate input for 'mike' wexine covered Cabinet with lid see illus on lett
Or Dep. $£ 13.25125$
PR7.10 9 mop. 13125 and mihly pymis 56.76 HU Lotal 274 ) or Dep. 215 and 18 mthly

PACKAGE PRICE ¢52 ${ }^{\text {car }}$

PACKAGE PRICE 656 :9125 PACKAGE PRICE $£ 99.95{ }^{\text {and }}$

FALPHASE 50 MkIIIAMPLIFIER 50W Solld state. 4 Separately controlled Inputs Plus master vol. control. Ind. Baas and Treble damage from accidental shorts. Output for Speaker/s

00-250v. A.C. maine. Output
Or dopoait en 25 mains. Outpue
NOW THREE NEW BRANCHES 19/19A MARKET STREET NOTTINGHAM ALSO 5 MARKET SQUARE SUNDERLAND 8 LTtLL UNOERBANK STOCKPORT
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TERMS C.W.0. or O.O.D. No C.O.D. ander 11. POSTAGE 25D EXTRA URDER \&2. 30D EXTRA OVER I2 OR AS GUOTED. TRADE SUPPLIED. 8.A.E. PLEASE WITH EAQUIRIES.

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MALL ORDERS MUBT NOT BE SENT TO SEOPS

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 50 WATT AMPLIFIERA powerful high quality all-purpose unit for lead, rhythm, bass guitar, vocalists, gram, radio, tape. Peak Output rating. Loudspeaker unit optional horizontal or vertical mounting.

* Two extre heavy duty 12 ln . 50 w L'spkrs. \& Four Jack inputs and two Volume Controls for instant use of up to four pick-ups of "mikes". Bass and Treble controls. Credit Termis: Depostt
\&15 \& 9 monthly
Drts of $\& 6.25$ $\begin{array}{ll}\text { pyts of } £ 6.25 \\ \text { (Total } 871.25 \text { ) } & \text { Carr. } \\ \text { £2 }\end{array}$


## RSC GP30 HI-FI AMPLIFIER

For Guitar, Vocal or Instrumental Group.
A 4 input, 2 vol. control Hi - Fi 30 watt unf with Separate Bass and Treble controla Current valves. Peak output rating. Strong
Rerine covered cabinet with handles. Rerine covered cabinet with handles.
Attractive black/gold P.V.C. facia. Neon Attractive black/gold P.V.C. facia Neon or 15 ohm speakers. Send S.A.E. for leaflet. or 15 ohm speakers. Send S.A.E. for leaflet
Terms: Depoeit 44.40 and 9 monthly pay Terms: Deposit $44 \cdot 40$ and 9
ments of 28.40 (Total $£ 28.00$ ).


## R.S.C. Branches listed below open

 all day SaturdaysBRADFORD 10 North Parade (Half-day Wed.). Tel. 25349 BLACKPOOL (Agent) O\& C Electronics 227 Church Street BIRMINGHAM 30/31 Great Western Arcade, DERBY 26 Osmaston Ra., The Spot (Hall-cay wed DARLINGTON 18 Prilestgate (Hall-day Wed) Teil 68043 EDINBURGH

101 Lothlan Rd. (Half-day Wed.). Tel. 2299501 GLASGOW 326 Argyle St. (Halt-day Tues.). Tel. 248415 HULL 91 Paragon Street (Half-day Thurs.). Tel. 20505. LEEDS 5-7 County (Mecca) Arcade. Brlggate LIVERPOOL 73 Dale Street (Half-day Wed.).
LONDON 238 Edgware Road, W.2. (Half-day Thurs.). MANCHESTER 60A Oldham Street, (Half-day Wed.) MIDDLESBROUGH 106 Newport Rd. (Half-day Wed.)

## NEWCASTLE UPON TYNE

24 Newgate Shopping Centre (Half-day Wed.). Tel. 21469 NOTTINGHAM 19/19A Market Street (Hzlf-day Thurs.). SHEFFIELD 13 Exchange Street (Castle Market Blds.) SUNDERLAND 5 Market Square Tel. 70573


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Improved one-valve model "DX" mark 2
Complete kit-price 3 \$30 (pont in panking 20 p .)
Costomer writes: "Australs, Indie and America at loud volume." -'I am 14 jears of age and have logged over 130 atations, plus countless Amatours from all over the world."

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This ift containa all genoine short-wave components, drilled chanals, valve, acceasorien and full instructions. Ready to samemble, and of course, as all our prodacts-fully guaranteed. Foll range of other $\mathbf{S . W .}$. kits, Including the tamous model despatched by return. (Mall ordes only.) Bend now for tree deacriptive catalogue a onder form.
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PW JUNE 11


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| PHILIPS RH580 | 52．00 | 36.50 20.50 |
| PIONEER SA500A | 45.50 | 32.95 |
| PIONEER SA600 | 89.60 | 57.50 |
| EER SA | 119.85 |  |
| PIONEER SA |  |  |
| PIONEER QL600 Quadraphonlc con－ |  |  |
|  |  |  |
| ni | $42 \cdot 85$ | 29.95 |
| QA 800 Quadraphon | 179.05 | 113.66 |
| QC 800 Quadraph | $123 \cdot 50$ | $71 \cdot 95$ |
| QM 800 Qusdr | 152.88 | 96.95 |
| verberation 202 | 51.05 | $33 \cdot 95$ |
| RANK Rotel 210 | 34.90 | 23.95 |
| RANK Rotel 310 | 47.50 | 31.95 |
| ANK Rotel 610 | 74.50 | 48.95 |
| ROGERS Ravens | 64.50 | 45.50 |
| GERS Ravensbourne（ca | $69 \cdot 50$ | 49.50 |
| ROGERS Ravensbrook Mk | 50.50 | 35.95 |
| ROGERS Ravensbrook（cased） | 55.50 |  |
| NCLAIR 2000 | 35.00 | 22.95 |
| Prolect 60／2 $\times 230$ | 23.90 | 15.95 |
| Project 60／2 $\times \mathbf{Z 5 0}$ | 34.86 |  |
| Prolect 605 | 29.95 | 18.90 |
| AFU |  | 4.50 |
|  | $61 \cdot 95$ | 2．93 |
| 3000 | 45.00 | 29.50 |
| ELETON SAQ | 33.00 | 20.50 |
|  | 33.00 | 20.50 |
| WHAR202 15 watt RMS Per C | 45.75 | 28.95 |
| WHARFEDALE Linton Amplif | 65.00 | 39.95 |
| TUNERS |  |  |
|  |  |  |
|  |  |  |
| ARMSTRONG 523 AM | $52 \cdot 68$ | 39．95 |
|  | 40.97 | 31.25 |
| NG M8 Dec |  |  |
|  | $24 \cdot 43$ | 17.50 |
| DULCIFMT | 32－89 | 24.50 |
| OODMAN | $75 \cdot 74$ |  |
| dVC Nivico |  |  |
| MCT V5E AM／FM |  |  |
| MCT V7E AM／FM Quadra | $122 \cdot 42$ | 99. |
| LEAK Delta FM |  | 53.95 |
| LEAK Delta AM／F | 89.50 | 65.95 |
| PHILIPS RH 690 | $44 \cdot 15$ | 31.95 |
| PIONEER TX500 AM／F | 70.93 | 49.95 |
| PIONEER TX600 AM | $100 \cdot 37$ | 68.95 |
| RANK ROTEL 320 | 53.38 | 38.50 |
| RANK ROTEL 620 | 86.33 | 63.95 |
| ROGERS Ravens bou | 57.95 |  |
| ROGERS Ravenabourne In | 62．63 | 47.95 |
| ROGERS Ravensbrook chas | $42 \cdot 14$ | 31.95 |
| ROGERS Ravens b | 48.00 |  |
| SINCLAIR 2000 | 45.00 | 31.95 |
| SINCLAIR 3000 | 45.00 | 31.95 |
| SINCLAIR Project 60 tuner | 25.00 | 17－50 |
| TELETON GT202 | 46. | 30 |
| All above Tuners are complete Stereo Decoder excent where | with MP |  |
| TUNER／AMPLIFIERS <br> AKAI CR80T FM／AM Tuner Ampll－ <br> fler with built in Elght Track Tape <br> Recorder |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
| AKAI AA 8500 | 228.34 | 175．00 |
| AKAI 6600 | $145 \cdot 2610$ | 109.00 |
| KA1 6300 |  |  |
| AKAI 6200 | 197.09 | 74. |
| ARENA 2600 | 111.30 |  |
| ARMSTRONG M8 |  |  |
| ARMSTRONG 525 | 90.14 |  |
| ARMSTRONG 526 |  |  |
| CARLTONE M4000 AM／FM with $\begin{array}{llll}8 \text { track player and speakers．．．．．．．} & 69.95 & 39.95 \\ \text { GOODMANS Module } 80,35 \mathrm{w} \text { ．RMS } & 89.02 & 67.95\end{array}$ GOODMANS Module 80 Compact $160.38 \quad 122.95$ GOODMANS Module 110 FM／MW／ LW／SW 100W RMS |  |  |
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TUNER／AMPLIFIERS－continued SX828
Pre Pric $224.61 \quad 157.9$ ROGERS Ravenshrook（cased） ROTEL R×200
ANDBERG 1171 MPX
TANDBERG TR200 MPX
TANDBERG TR1000 FM MPX（teak） TELETON F2001
TELETON R8000 AMM／FM
FM．．．．．．

All include MPX Stereo which take ceramle only． of Armstrong where M8 decoder is extra exception
TURNTABLES
GARRARD SP25 Mk III
GARRARD SL65B
GARRARD SL95B
GARRARD 401
GARRARD SL72B
GARRARD Zero 100 A
GARRARD WB4 base Mk IIZ to fit

10.25
13.95

| 25 |
| :--- |
| 95 |

Zero 100 \＆Zero 100 S
The following Turntables are complete with
base，plinth，perspex cover and cartridoe． base，plinth，perspex cover and cartridge．
Fully wired and ready for use．All at speclal ices．
GARRARD SP25 Mk III
With Goldring G． 800 Special Price $£ 18 \cdot 50$ with Goldring G800 Special Price $£ 18$ ． 50
McDONALD MP60 MCDONALD MP60
McDONALD MP60 $44 / 7$ Speclal Price £19．50
with SHUREM
with Goldring G800 Special Price £28－25
GARR Shure M55E
with Shure M75EJ
GARRARD 2025 with
Sonotone $9 T$ AHC
Sonotone 9TAHC
GOLDRING 705／P
with G850
GL75
with G800
THORENS 150 AB with TXII cover 36.75
Shure M55E cartridge
Base and Cover to fit GARRARD
SP25，SL55，SL65B
SP25，SL55，SL65B．
GARRARD $40 \mathrm{~B} . . . .$.
GARRARD AP76
GL69P Mk．II
GL75
Covers for 69 P and 72 P
Cover for 75P Deluxe
C99 plinth and cover for G99
GOLDRING G101P
GOLDRING GL72 Chassis
GOLDRING GL72F
GOLDRING GL85P
LEAK Delta
Including SRP 473 Quadraphonic． McDONALD MP60

## 610 HT $70^{\circ}$

HT70 inc plinth and cover
Base and Cover for MP60 and 610
PHILIPS 308 transcription
plete with base and cover $\ldots .$. ．
PHILIPS GA 105 with base，cover
PIONEER PL12AC with base \＆cover
THORENS TX25 cover
HORENS TO125
THORENS TD125 Mk．I
THORENS TD 125AB Mk．II with TP
THORENSTDI50 Mk．II
THORENS TD 150 M Mk．ii
THORENS TD150AB Mk．
WHARFEDALE Linton with base．
and cover and Shure M44－7 cartridge
AKAI SW 155
AMSTRAD 138 （pair） $13^{\circ} \times 8^{\circ}$ twin
cone teak
B \＆W DM2
\＆W DM3

Speclal Price £ $\mathbf{3 0} \mathbf{0} 95$
Special Price £33．50
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0.95
7.95
8.50

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SPEAKERS－continued CELESTION County CELESTION Ditton 120 （pair）． CELESTION DItton 15 CELESTION Ditton 25 CELESTION DItton 44
FERROGRAPH S1 inc，stand
GOODMANS Mavant（pair） GOODMANS Minister（ GOODMANS Double Maxim GOODMANS Mezzo 3
GOODMANS Magnum K2
GOODMANS DImension 8
GOODMANS DIN 20NT klt．
tem（pair）
N600 3－speaker System（pair）
KN1100 4－speaker System
KN1600 3－speaker System
KN2100 3－speaker System
LEAK 150 （pair）
LEAK 600
LINEAR 10 watt teak（pair）
METROSOUND HFS 103 （pair）
METROSOUND 202
METROSOUND Duglex 25
PHILIPS RH 402 （pair）
PHILIPS 406.
SINCLAIR Q16
STE－MA 450
TANDBERG TAN 7
ANDPERG Tan 11 （palr）
ANDBERG Tan 25 teak（palr）
TANDBERG Tan 50 teak
THORPE Grenville TG 100 （pair） Grenville TG 200 （palr）
WHARFEDALE
Denton Mark II（palr）．
Linton Mark II（pair）
Dovedale 3 Mark i
Rosedale
Triton III（palr）
Unit 4 Speaker K
Unlt 5 Speaker KIt

| 20 |  |
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| 56.40 | 39.95 |
| $37 \cdot 40$ | 27．95 |
| 65.00 | 45－95 |
| 54.00 | 38.95 |
| 99.00 | 70.95 |
| $95 \cdot 00$ | 89.95 |
| 54.42 | 39．95 |
| $50 \cdot 62$ | 35.95 |
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| 32.07 | 24.75 |
| 35－70 | 23.95 |
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| $26 \cdot 46$ | 17.50 |
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| $56 \cdot 00$ | 37.95 |
| 44．70 | 33.95 |
| $34 \cdot 00$ | 25.95 |
| $44 \cdot 25$ | 28.95 |
| 8.98 | $6 \cdot 75$ |
| 25.00 | 18.95 |
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| $48 \cdot 82$ | 41.40 |
| $66 \cdot 08$ | 55.95 |
| 65.00 | 49.95 |
| $21 \cdot 08$ | 11.95 |
| 28－95 | 17.95 |
| $41 \cdot 95$ | 25.95 |
| $55 \cdot 95$ | 31.95 |
| 42.00 | 27.95 |
| 52.00 | $35 \cdot 95$ |
| 35.00 | 23.95 |
| 47．50 | $30 \cdot 50$ |
| $65 \cdot 00$ | 44.25 |
| 65.00 | 44.95 |
| $12 \cdot 50$ | $8 \cdot 75$ |
| －00 |  |

6.95
6.95
7.50
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WHARFEDALE BIIn．Bronze／RS／DD Super 8／RS／DD
WMT1 MatchIng Transtormer．．．．．．．．．．．．．．．．．．．．

## CARTRIDGES

AMSTRAD 900C
AMSTRAD 900 EX A．．．．
GOLDRING G850
GOLDRING G800E
GOLDRING G800 Super E
GOLDRING CS90 Stereo
EMPIRE 1000 ZEIX．
EMPIRE 999VE／X．
EMPIRE 999TE／X．
EMPIRE 999E／X
EMPIRE 909E／X
ORBIT Magnetle NM
SHURE M3DM．．
SHURE M31E
SHURE M32E
SHURE M44－G
SHURE M44－7
SHURE M－44C
SHURE M44E
HURE M75E

7.50
1.95
4.5
4.50
9.25
4.95
4.95
8.95
3.20
4.90
9.50
2.70
5.45
3.40
6.25
9.95
0.70
is
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$3 \cdot 50$
5.50

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\begin{array}{ll}
15 \cdot 69 & 93 \cdot 95 \\
33 \cdot 64 & 26 \cdot 95 \\
43 \cdot 09 & 32.95
\end{array}
$$ ． 50

50
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$55 \quad 28$ 95

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$\begin{array}{ll}37 \cdot 50 & 25.95\end{array}$
$59 \cdot 50$ 595
$26 \cdot 00$
$159 \cdot 50$
$63.00 \quad 45 \cdot 50$
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CARTRIDGES - continued

## SHURE M75-6 <br> SHURE M75E

SHURE M75 ED
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SHURE M75ED
SHURE V15-11
*SONOTONE 9TAHC Diam/Saph.
$\begin{array}{rr}3.75 & 1.45\end{array}$
Starred cartridges above are ceramic. All othera ar magnetlc.
BABES AND COVERS GARRARD WB1 Base

WBA Base
SPC1 Cove
SPC4 Cove
$\begin{array}{ll}3.78 & \mathbf{3 . 2 0} \\ \mathbf{5} .60 & \mathbf{4} 70 \\ 3.68 & \mathbf{2} .90 \\ \mathbf{4 . 3 8} & \mathbf{3 . 5 0}\end{array}$
Speclat offer of Base and Cover to
W84 base Mk IIZ to fit Zero 100
and Zero 100 S .
GOLDRING PIInth 75
GOLDRING PIInth 69
GOLDRING Covers for 69P and 72 P
Cover for 75P De luxe TO125AB)
THORENS TX25 (for TD125A
THORENS TX11 Cover.

## lal Price 3-60

 $\begin{array}{ll}6.55 & 4.95 \\ 8.37 & 7.00\end{array}$ SME PIInth System 2000 with motor-MOTORBOAROS only
$\begin{array}{rr}8.37 & 7.00 \\ 8.37 & 7.00 \\ 4.36 & 3.70 \\ 4.88 & 3.85 \\ 8.26 & 3.60 \\ 4.13 & 3.50 \\ 12.39 & 10.50 \\ 46.20 & 34.50 \\ 5.85 & 4.45 \\ 0.98 & 0.75\end{array}$
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## C90

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$5^{7 \prime} 2^{\prime \prime}$ L.P. 1200
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FIDELITY UA2 Music Master
UA1 Music Master with Radio. OODCMANS
GOODMANS Module 80 compac
lystem FM/35 watts. RMS (Less HMV 2451
HMV 2450 with Stereo Radio KB1025 with 657 speakers.
KB 2250 with 658 speakers
KB 2010 with 658 speakers
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McDONALD MP60 complete with
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speakers 902 Studio i, AM/VHF Radio
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PHILCO FORD M1500
PHILIPS 808
PHILIPS GF82

Rec. Retail
Price $\begin{gathered}\text { Comet } \\ \text { Price }\end{gathered}$

## MI-FI STEREO SYSTEMS-coninu

 PHILIPS 825PHILIPS 826
PHILIPS 835
PHILIPS 836
PYE Biack Box unit stereo 1022 RIGONDA Party TIme
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79.50
$75 \cdot 00$ coder. Garrard 2025 Telon
ULTRA 6028.
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AKAI 4000D 4 -track stereo deck

AKAI CR80D 8-track stereo tape deck 85.02 | 54.95 |
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| 8.45 |

$\begin{array}{llll}\text { AKA } & \text { CRBO 8-track stereo recorder } & 106.39 & 74.00\end{array}$ AKAI CR80T 8-track stereo recorder
and tuner/amplifier.
AKAI $\times 200 \mathrm{D}$
AKAI $G \times 220 \mathrm{D}$
AKAI 1800SD
AKAI 2000SD
FERGUSON 3247 4-track
FERGUSON 32484 -rack
FERGUSON 3252 4-track
FERROGRAPH $702 / 4$ Dolby
FERROGRAPH 702H Dolby
FERROGRAPH 722/4 Dolby
FERROGRAPH 722H Dolby
FERROGRAPH 702 2-t rack tape deeck
FERROGRAPH 704/W 4-track deck
FERROGRAPH 722
FERROGRAPH 724
FIDELITY BRAEMAR 4-track
GRUNDIG TK 121 twin track
GRUNDIG TK 146 4-track Auto
GRUNDIG TK 147 4-track Auto
GRUNDIG TK 148 (4-track auto
PHILIPS 4303 TwIn-track
1308 De luxe 4-track


TANDBERG 1841 4-track stereo
TANDBERG $3021 \times$ twin track stereo TANDBERG $3041 \times 4$-track stereo.. TANDBERG $4021 x$ twin track stereo TANDBERG $4041 \times 4$-track stereo. TANDBERG 6041X 4 -track stereo. TANDBERG 6021X twin track stereo TAPE RECORDERS (CASSETTES) AKAI CS 350 recorder ......
AKAI CS $50 D$ Deck........
AKAI GXC 40D Tape Deck. AKAI GXC 40 D Tape D AKAI GXC 40 Recorder...........
APCO Batt./Malns with AM/FM APCO
Radio BUSH Dİ
SH TPG0 sette DC70
USH TP 66 8att/Mains
BUSH TP 70 battery/malns
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DANSETTE DCT105.
DECCA 2000 (batt./mains)
LIA VRF Radlo
WKCO 350 Bt./Mns. VHF/MW Radio EKCO 351 Battery/Malns.
FERGUSON 3240 with case
ERGUSON 3262
FERGUSON 3262 Battery/Mains
GRUNDIG C210 batt./malns
GRUNDIG C410 with AM/FM radio
HARVARD Elite with AM/FM radlo
JVC NIVICO 9420 L/ S with AM/FM radio batt./mains. . 3 with MWiVHF
PHILIPS R.R. 392 wir Radlo Cassette
2202
204 battery/mains
3302
PYE 9109
PYE 9116 Stereo
TELETON TRC 130 with VHF/AM
radio battery/mains
TC110 battery/mains
$\begin{array}{rr}108.50 & 73.95 \\ 189.75 & 139.95\end{array}$
$\begin{array}{lr}08 \cdot 50 & 73.9 \\ 89.75 & 139.9\end{array}$

| 24.30 | $91 \cdot 65$ |
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| 103.95 |  |


$\begin{array}{ll}66.09 & 48.75 \\ 104.00 & 80.85 \\ 104.00 & 80.85\end{array}$ $\begin{array}{lr}.00 & 80-85 \\ 12 & 135.50\end{array}$ | 12 | 135.50 |
| :--- | :--- |
| 73 | 135.50 | $\begin{array}{ll}73 & 145 \cdot 25 \\ 73 & 145.25\end{array}$

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\begin{aligned}
& 125 \cdot 83 \\
& 104.46
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$$ 104.46

$92 \cdot 26$ 92.95
77.95
68.25
 35.00
20.62 $\begin{array}{ll}35 \cdot 00 & 22.95 \\ 20 \cdot 62 & 15.95\end{array}$ $20 \cdot 6$
27 $\begin{array}{cr}28 \cdot 13 & 19.95 \\ 11.95\end{array}$ $\begin{array}{cr}\text { D. Price } & 11.95 \\ 20.62 & 14.95\end{array}$

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$28-75$
18.45
23
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$30-15$
$37 \cdot 55$ 37.55
48.75
$42 \cdot 00$
23.95
$61.45 \quad 42.95$
49.95 $49 \cdot 95$
$22 \cdot 85$
$29 \cdot 10$ 20.10
66.10 $20 \cdot 37$
$66 \cdot 10$ $66 \cdot 10$
29
$\begin{array}{ll}42.50 & 28.00 \\ 27.50 & 18.50\end{array}$


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H.L. Audio Phoenlx 707 amp. McDonald MP60 turntable, complete with base, cover and Shure M44/7 cartridge. Fully wired plus 2 Thorpe Grenville 100 loudspeakers
ROTEL RA 210 amplifier with McDonaid MP60, bas cover and Goldring G800 magnetic cartridge. Plus two Linear 10 watts speakers (Teak)
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PIONEER SA500A amp with McDonald MP60 IONEER SA500A amp.. with McDonald MP60 Plus two Wharfedale Denton speakers

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PHILIPS RH802 Stereo Tuner/ Amplifler/Player. 2 15 watts. LW/MW1/MW2/SW/FM. MPX. with GP400 magnetic cartridge. Speakers extra
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ARMSTRONG 525 FM Tuner/Amplifler. 25 watts RMS per channel, teak case, with M8 MPX Decoder. Goldring GL75 turntable, pilnth, cover and G800 cartridge, plus two Whartedale Dovedale III
speakers speakers
$\qquad$
ARENA 2600 Tuner/Amplifier. FM/MW/LW 49 m Band. Marine Band. 15 watts. RMS per channel. Flve pre set F.M. Stations and manual tuning with Garrard AP76 pilinth, cover and Gars
Plus two Goodmans havant speakers
POTEL R×150 Tuner/Amplifler, AM/FM MPX
OTEL RX150 Tuner/Amplifler, AM/FM. MPX with McDonald MP60 plinth, cover and G800 cartid
plus two Wharfedale Denton Mk. II spealkers plus two Whariedale Denton Mk. $139.94 \quad 96.40$ AKAl CR80T Tuner Amplifler. AM/FM. MPX with -track stereo Recorder/Player, wlth McDonald MP60, plinth, cover and G800 cartridge. Plus two Wharfedate L'Inton Mk. II speakers $231.85 \quad 144-40$ TELETON CR55 Tuner/Ampllfler. AM/FM MPX with Garrard AP76 Turntable, plinth, cover and Shure M75EJ magnetic cartridge. Plus two Whartedale Dovedaie 111 speakers............ $266 \cdot 10 \quad 163.00$ PIONEER SX525 Tuner/Amplifler, Inciuding MPX Decoder with Pioneer PL12AC turntable, Including plinth, cover and Shure M55E cartridge. Plus two Ploneer CS53 speakers.
$28 \cdot 15 \frac{191.75}{\text { LEAK }}$
LEAK Delta 75. AM/FM tuner/amplifler, with LEAK Delta transcrlption deck, complete with plinth, cover and cartridge. Plus two Leak 600 speakers $\begin{array}{r}239 \cdot 80 \\ 326 \cdot 50\end{array}$

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| 8 | 203827 | OC82 | $\begin{array}{ll}820344 \mathrm{~B} & \mathrm{OC}_{8} \mathrm{O}_{4} \\ 8 \mathrm{G} 345 \mathrm{~B} & \mathrm{OC} 45\end{array}$ $\begin{array}{ll}82 \mathrm{G378} & \mathrm{OCCA}^{\text {OC78 }}\end{array}$

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U26 30 Fbst Switching Bilicon Diodes Ilize IN914 Micro-Min
12 NPN Germanlum AF Transistors TO-I like ACl 27
$\begin{array}{lll}\text { U29 } & 10 & 1 \text { Amo SCR's TO-5 can, up to 600 PIV CRs } \\ \text { U30 } & 15 & \text { Plastle Bilicon. Planar Trans. NPN 2N2926. }\end{array}$
$\begin{array}{llll}U 31 & 20 & \text { silicon Planar Plastle NPN Trans. Low Nolse Amp 2N } 3707 & 0.50\end{array}$
U32 25 Zener Dlodes 400 mW DO-7 case $3-18$ volth mired
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U34 30 sllicon PNP Alloy Trans. TO-5 BCY 26 28302/4
U35 25 sllicon Planar Tramelatore PNP TO-18 2N2906
U3f 25 Ellicon Planar NPN Transistors TO-5 BFY50/51/52
U37 30 Eillicon Ailoy Transintors 80-2 PNP OC200, 28322.
$\begin{array}{lll}1038 & 20 \text { Fast Switching Billcon Trank. NPN } 400 \mathrm{MHz} & 2 \mathrm{~N} 3011\end{array}$
U39 30 RF. Germ. PNP Transistors 2N1303/5 TO-5
U40 10 Dual Transistors 6 lead TO-5 2N2060

| $\mathbf{U} 41$ | 25 |
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| RF Germanlum Transiators TO-5, OC45, NKT72 | $\ldots .$. |


| U42 | 10 VHF Gernuanlum PNP Transistors TO-1 NKT687, AF 117 | 0.50 |
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U43 25 Sil. Trans. Plastic TO-18 A.F. BCil13/114
04420 8il. Trans. Plastic TO. $\delta$ BClIS/NPN U45 7 3A BCR. TO66 up to 600PIV

Code No's. mentloned above are glven as a gulde to the type of device in the pak. The devices themselves are normally unmarked.

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16 White apot R.F. transistors PNP OC 77 type transiators Matched transistora $0 \mathrm{C} 44 / 45 / 81 / 81$ OC 75 transistors
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Q24 8 OA 81 diode
Q25 is IN914 sllicon diodes 75 PIV 75 mA
Q26 8 OA95 Germanium diodea sub-min
Q27 2 10A PIV slicon rectifiers I8425R
Q28 2 Bilicon power rectifiers BYZ $13 \ldots .$.
Q29 $\quad 4$ sillcon transistors ${ }^{2} \quad \times \quad 2$ N696,
Q30 7 Sillcon switch transistors 2 N706
Q31 6 gilicon awitch transistors $2 N 708$
Q32 3 PNP gllicon translators $2 \times 2 N 1181$
Q33 3 Silicon NPN tranalatora 2 Ni71i...
Q34 7 Billcon NPN tranalstors 2Na369,
Q35 3 Silticon PNP TO-6. $2 \times 2$ N2904
Q3A 7 2N 3646 TO-18 plastic 300 MHz NPN
Q37 3 2N3053 NPN Sillicon transiators. 2N3702

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$20 \mathrm{~Hz}-20 \mathrm{KHz} \pm 1 \mathrm{~dB}$ better than $0.1 \%$
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[^0]
## Wires and Waves

ASKED what type of aerial he uses, an enthusiast of the new generation might well reply "What's an aerial?". Apart from those multi-rod devices on the roof associated with television, the aerial is usually just another component fitted snugly inside the case of a transistor radio.

DX enthusiasts and amateur transmitters are, of course, alive to the importance of the external aerial, but there must be thousands of would-be DX-ers battling against the odds by trying to find exotic stations on ordinary transistor radios and relying only on the pickup capabilities of the internal ferrite rod assembly or at best a diminutive pull-out rod. While some success is possible under these conditions, experienced listeners will testify as to the vastly improved results obtained by using a well-designed external system, perhaps terminated in an aerial tuning unit.

It is not, however, just a matter of throwing out a random piece of wire and hoping for the best. Some thought must be given to the wavebands on which peak performance is wanted and the directions from which optimum reception is needed. In fact, devising an aerial can be quite as absorbing as the building of active equipment.

The erection of an aerial system is more an art than a science, because the siting and lengths of wire are somewhat empirical. Formulae for dimensions and directions are based on the ideal conditions obtained in "free space" but the average amateur is rarely fortunate enough to have unrestricted space and a clear open site. The immediate terrain and features (hills, large buildings, etc.) may modify the ideal calculations and so there is a fruitful field here for experimentation.
Once embarked on the subject of aerials, it is a short step to begin thinking about what happens between the transmitter and the receiver. Here again is a complete field for exploration. One of the first things that an embryo DX-er has to learn is how the various phenomena associated with radio wave propagation are going to affect his listening activities. A good aerial system coupled with a knowledge of propagation are the foundations for successful long distance listening.

That there is a need for information on aerials is borne out by the many letters we have received asking for help in this direction. The wall chart enclosed with this issue should provide all the basic material for those wishing to install a good aerial system, or improve their existing set-up, and it is complementary to the DX Data Chart supplied with the March issue.

We have also included in this issue, an introductory article on radio wave propagation, which it is hoped will provide a further stimulus to investigation into this somewhat neglected, yet vital, sphere of interest.
W. N. STEVENS-Editor

## NEWS AND COMMENT

| Leader |  |
| :--- | :--- |
| News... News ... News... | 487 |
| MW Column by Charles Molloy | 488 |
| Electronotes by S. Ginsberg | 502 |
| Letters | 505 |
| Practically Wireless by Henry | 506 |
| CQ! CQ! CQ! | 510,540 |
| On the Short Waves by Malcolm |  |
| Connah and David Gibson, G3JDG |  |
|  | 527 |

## CONSTRUCTIONAL

## Audio Reference Source by E. Buckland <br> 494 <br> The "Logiprobe" by Laurence Cook <br> ..... 501 <br> Take 20, No. 41, Frost Alarm by Julian Anderson <br> ..... 509 <br> Pre-Tuned Car/Portable Radio by R. H. Longden <br> ..... 512 <br> Transmitter for Two Metres, Part 2 by F. G. Rayer, G3OGR <br> ..... 516 <br> Experimenters Corner, IntercommCalling System and 25 W a.c. tod.c. inverter <br> 518

OTHER FEATURES
Principles of Propagation by Henry Hatch ..... 490
Transistor Circuitry for Beginners, Part 11 by H. W. Hellyer and Michael Hollier ..... 520
Going Back by Colin Riches and Arthur Dow ..... 524
Gas Filled Valves, Part 2by I.R. Sinclair531
IC of the Month, Motorola MFC 6040Electronic Attenuatorby L. A. J. Ireland540
FREE-AERIAL DATA WALLCHART
Some Readers may be aware of a slight loss of quality in printing. This is due to a shortage of our usual paper whic $h$ has been brought about by the Dock Strike.
THE NOVEMBER ISSUE WILL BE PUBLISHED ON OCTOBER 6th

[^1]
## Nip-E-Board

Remember some time ago we mentioned Nippiboard - the etched P.C. Board? Well now NIP Electronics, the manufacturers have announced additions to their range.

The Nip-E-System provides for a number of basic etched printed circuit board arrangements that can be used in many circuit applications immediately. The user then goes ahead with the component layout assembly and wiring, knowing that he does not need to worry about special designs or messy etching procedures. The basic layout design


STANDARDISED P.CB. FOR TRANSISTORS procedures and photographic image transference have been done for the constructor. All the user needs to do is apply the standardised pattern to his circuit and assemble the components. Connectors are available as part of the Nip-E-System for single row and double row pattern arrangements of discrete or integrated circuits or both.

With the boards you get a choice of ready-made paper base laminate or epoxy glass fibre board $1_{16} \mathrm{in}$. ( 1.58 mm .), a hole matrix $0 \cdot 1 \mathrm{in}$. $(2 \cdot 54 \mathrm{~mm}$.) $\times 0 \cdot 15 \mathrm{in}$. ( 3.81 mm .) and a choice of drilled or undrilled boards. A choice of board for discrete components only or a mixture of integrated circuits and discrete components is available and there is a choice of board size to take up to about

> P.C.B. FOR I.C.


## Gas igniter



No. it's not a device for "doingin" Editors-it's a piezo electric gas igniter! It's guaranteed for ten years, does not need any batteries or flints, you don't have to plug it in the mains or hold it under a hot tap! While you pause for breath, we'll explain:

The device, made in Germany by Junkers, operates on the principle that if a sudden force is applied to the interfaces of various crystals, an electric charge results. In practice, when the trigger on this igniter is pressed, it releases a "firing" pin which deforms the piezo crystal and causes a discharge voltage in the region of 20 kV to appear at the end of the pistol "barrel". The end of the barrel is designed like a car

sparking plug so that the spark (of $50 \mu \mathrm{~S}$ duration) jumps from the centre electrode to the barrel wall thus igniting the gas it is held near.

In the sketch (a) is the crystal mounting and housing unit. (b) and (c) are the points the spark jumps from and (d) is the plastic housing of the complete unit.

The Junkers Piezo Electric Gas Igniter is priced at $£ 2 \cdot 25$ plus 15 p postage and packing and may be obtained from Servitronix Limited, 572 Kingston Road, Raynes Park, London, S.W. 20.

26 transistors (possibly more) in the 11 E to 18 E series or up to eight integrated circuits plus 16 transistors in the 21 E to 28 E series.

Constructors can have plug-in contacts for 14 -way or 30 -way gold-plated edge connectors (as supplied) for single row or double row boards, contact pitch 0.1 in. ( $2 \cdot 54 \mathrm{~mm}$.).

The customer choses the size most suitable to his application and the Company supplies a ready-made Nip-E-Board.

The boards are reasonably priced and they certainly help to make construction much easier and far neater.

If you would like further details of prices, accessories and layouts, drop a line to NIP Electronics, P.O. Box 11, St. Albans, Herts. They will be pleased to send readers their comprehensive free booklet on the Nip-E-System.

## Anyone help?

Our squadron has recently started a radio section, and all projects are of a self help basis, thus you may understand that supplies and money are very limited. The boys' ages vary from 13 years to 16 years.

I would be most obliged if through your column, I might request any radio hams etc who have surplus to requirements any books, components or radio equipment, to contact us.

All expenses for postage and packing would be refunded, and all communications acknowledged.

Please address all letters, parcels, etc. to: -Mr . G. H. Barker, "Training Officer", 2380, A.T.C. Dartmouth Sqdrn., "The Lodge", Longcross Cemetery, Townstal Road, Dartmouth, South Devon.

## BI-PRE-PAK LTD.

Due to a printer's error in our August issue an incorrect price was quoted for the Complete Telephone as offered for sale by the above Company. The correct price should have read $95 p$. We offer our apologies to BI-PRE-PAK LTD. and to any readers who may have been inconvenienced by this error.

## Decoder

Motorola Semiconductors have announced the type MC1310 monolithic f.m. broadcast receiver stereo decoder which requires no external tuning inductors. Stereo channel separation is stated to be 40 dB at 1 kHz , with $0.3 \%$ total harmonic distortion.

## Dymo Star 1710

We recently had the opportunity to try out the Dymo Star 1710 labelling machine. This machine is ideal for stamping out the wording for the front panels of equipment.

Letter selection is made by turning the dial wheel until the required character appears in the letter slot.

Technical symbol and character wheels may be fitted to this machine quite simply and different colour tapes are available.

Full instructions are provided with each Dymo Star.


## IC power amp




The HY4l is a linear integrated circuit, power amplifier with an output of 20 Watts r.m.s. into 4-16 having a total harmonic distortion of less than $0.15 \%$ (typical $0.05 \%$ ) at 1 kHz into 8 ohms.
P.C. board, resistor, capacitors, hardware mountings and comprehensive manual are all included in the basic kit, no further components being required in constructing a complete power amplifier of high performance.

Internally the HY41 is based on proven circuit techniques developed over recent years and is sufficiently versatile to provide power not only for $\mathrm{Hi}-\mathrm{Fi}$ but for public address systems and industry.

Supplied by the Canterbury Company I.L.P. (Electronics) Ltd., the HY4l requires no adjustment whatsoever and can be assembled without recourse to sophisticated measuring equipment or electronics know how. I.L.P. (Electronics) Ltd., Crossland House, Nackington, Canterbury, Kent.

## Rover-point

Nettle Accessories Limited, a member of the Aerialite Group of Companies, announce the introduction of a portable extension lead to their range of electrical accessories, known as the "Roverpoint".

It consists of a 15 metre length of white $0.65 \mathrm{sq} . \mathrm{mm} .3$ core, P.V.C. cable, contained in a moulded plastic reel. A flush 13A socket is incorporated into the reel, and the cable is supplied complete with 13A plug.

The reel has a handle that can be utilised for carrying or hanging, and its rotating section is provided with two projections to facilitate easy rewinding.

Suitable for feeding loads of up to 1 kW , with the cable fully extended and 500W with the cable coiled on the reel, "Roverpoint" sells at a recommended retail price of £3.99. Nettle Accessories Limited, Warren Street, Stockport. Cheshire.


## Sonex 73

Sonex 73 , the high fidelity equipment exhibition organised by British Audio Promotions, will be held at the Excelsior Hotel, London, from March 30 to April 1.

## Erie calalogue

Erie Electronics have published a new comprehensive catalogue of their electronic components. It covers all product ranges, and catalogue contains specifications on all Erie distributor sales, Erie Electronics and Erie Controls products, as well as information on Erie thick film devices and 'Toshiba semiconductors. Copies are available from Erie Electronics Ltd., South Denes, Great Yarmouth, Norfolk.

## Chadacre Electronics

Please note their new address: 63 Stratford Broadway, London, E.15. Telephone 01-534 1207.

DESPIME The lise of high power Jfansmitters, used in comjunction with aerial systenis of cone siderable gain and directivity, as well as exThemely sensitive reeciver techníques to accomplish a high standard of world-wide $t$.f-communication, the final merit of reecption is controlled ty many betural causés and variations:

## The Pioneers.

The medium theough which a radio wave must propagate termed the Tonosphere, determines this final pattern of reception including field strength, fading and even "black outs." The early pionecrs Nere well aware of the electro-matenetic wave with its effects though proof of its wast potential only came when Gugliélono Marcont established contact between Bournemouth and the liste of Wight in 1898. This was followed by an even greater breakthrough in 1901 When he transmitted the first telegraph signat from Poldhn, Copnwah to be intercepted, at St Jotns, Nen foundand.
Kesearch in this fleld by thany workers-revealed great discoveries. The name of mathematician Oliver Heaviside in England, who propounded the existence of a Conducting Laver in the upper atnosphere in 1892 as well as the worl catried out by Kennelly in the U.S.A. as early os 1902 can never escape mention. Sir E. V/Appleton and M. A. W. Bancti, who delermined the position of the Hedviside Cayer in
on the atmosplice with show considerable variations when we consider the changes from day to night, the four seasons of the year and the eleven year cycle of the sun's regutar variation. This solar cyele appears to follow an average change of 11.4 years; from one of minimum activity to maximum in 4 years and falling from maximum to the next minimum in 7 years. (The last inaximum occurred in 1968 and present predictions are estimating the next minimum will occur in 1975). Differences of this kind affect the conditions of the atmosphere and as a result have considerable influence on the propagation of radio waves. The solar radiations affect the atmosphere and cause it to assume a "mirror-like" reftecting surface which return adio waves to earth

## Ionization

The radiation from the sun unsetties and excites the-normal arrangements of the atanas and molecules of gas. This brings abont a cendition known as lonization; the atqus of gas become incomplete having lost some or thetir electronts

The regiom of ionization will therefane consist partly of free etectrons and this process will continue sa long as the earth's rotation permits that region of the afmosphere $t 0$ be exposed to the sun

After sumset this frocess ceases and the fred elect Irons rejoin their mother" atoms, a pradess known as recombinakion and this region will fall in iomized

1925 are also grat names that we associate with early radio experiments

The many effects acting in diferent vays on radio. signals during their passage from transmiter in receiver is indeed a great scientific subject-yet pethaps to the ynajority of readers the fascination lies in the fact that, even by using only simple equipment, signals may be intercepted from the other side of the world

## Sun and Atmosphere

Let us consider how transmission of this kind is possible. A mode of propagation of This kind requires two ossential and indispensible components, the atmosphere and the sun, The atmosphere, forming a gaseous envelope surrounding our planet, consists mainly of two gases, ditrogen and oxygen. This atmosphere is subjected to the full exposure and effect of the stu's rays, not only those of heat and visible light but of ather radiations, inctuding ultraviolet, gamma and X-1ays, all bombarding our atmosphere after a journey of some 93 million miles. The effect of these rays falling on our atmosphere-permits long distanceradio colmmunication

## The Solar Cycle

The difference in the amount of sunlight falling
density. The ionized fegion is coalled a Luyer and is able to reflect the wave back (of earth though it must be remembered that radio (like dight waves) travel onty in straight lines. To mate use of this reflecting property the transmifted signal must be beamed in a skyward direction, as well as towards that part of the earth where it is to be heard. For long distance communication the radiated signal must leave the eacth at a low angle so that the first encounter with the ionosphere witl be as far away as possible. In the same way a signal with a high angle of elevation will reach the layer at a much claser distance and may be regarded as being nore suitable for reception in a nearby area

## Bending

It should be mentioned at thiswstage that the vars of the sun will be first absorbed by the upper part of the atmosphere so that the overall density of the laver will strow some variation. The radio signal coming-up from the earth's surface will first enter an area of comparatively low density but as it enténs decper into the ionized region it will encounter an area of greater free electron density. The wave will meet an adverse force, presenting some opposition to its progress. It is convenient to think of the radio wave behaving in a simitar way to light when con sidering tow it is furned in the ionosptiere to be
returned to earth (both travelling at a speed of 186,000 miles per second).

## Hop and Skip

The word Refraction or Deflection explains this particular point in that a ray is changed in its course after entering a medium differing in density from one through which it has already passed. In this way the wave will be turned away from its original path and, providing the density of the medium and the frequency of the vibration are suitable, a point will be reached where the wave will be turned from its original route so as to follow a parallel course with the layer. Eventually it will be completely turned and leave the ionosphere at a similar angle as that of entry. The wave will return to earth having accomplished its first Hop-leaving a Skip distance between the sending and receiving points suggesting an area of silence existing between them. This is not so because the width of the transmitting beam will usually cover a considerable angle and the random scatter of the downcoming wave due to irregularities of the ionosphere tends to fill in this void. The second hop is made possible by an


Representation of the varlous methods by which radio waves are propagated. The main layers ( $D, E$ and $F$ ) are shown with their approximate heights above the earth's surface; the $F$ layer is shown simplifled -see text. The wave A is the normal long hop transmission; further reflection may take place when it meets the earth's surface. For reception in nearby areas the signal is beamed at a higher angle and is reffected by the E Layer.
C shows a form of propagation that is thought to occur at times. A number of reflections take place between the upper layers before the signal is returned to earth. If the angle of radlation Is too high (and the frequency unsuitable) the waves will be lost in space as shown by D.
upward reflection from the earth's surface but the effectiveness of this is somewhat variable. It will depend upon the texture of the particular area of the earth's surface. Sea water is excellent, next comes pastoral land, while at the lower end of the scale desert areas may be regarded as poor; all have different conduction values. There is no rigid limit as to how many hops may take place since these are governed by the height of the layer at the time of transmission, the radiation pattern given by the aerial and the distance to be covered as well as the original transmitted power.

Some idea of a professional mode of transmission may help to make this point clear; the path from the United Kingdom to India needs three such hops and that to Australia six or seven. It will now be clear that although the wave will follow only a straight
line, the curvature of the earth has been overcome by each individual hop although so far the ionosphere has been considered as one reflecting region. This is not so and it does in fact consist of several parts, each playing a different role and each one having a profound effect upon the wave.

## D Layer

The basic structure of the ionosphere starts with that area known as the $D$ layer, situated between 30 and 50 miles above the earth; this becomes yery dense by day but falls to a very low level-almost non existent-at night. During the hours of daylight it will cause considerable attenuation of the signal due to absorption, particularly to the lower frequencies. This effect is well known to the medium wave DXer as long distance reception on this band is virtually confined to the 'locals' until after sunset when the D Layer will begin to fail.

## E Layer

The E Layer (sometimes known as the KennellyHeaviside Layer) lies about 60 miles above the earth and although not the most important part of the ionosphere, it is responsible for the reflection of both medium and short waves.

A particular development of the E region, which at times can produce really sensational forms of propagation, is that known as Sporadic E. As the term implies this condition is irregular and cannot be forecast with any accuracy. An increase in ionization takes place usually around noon in our latitude. These abnormal conditions permit the reflection of very high frequencies and even enable TV signals to be observed from distant stations.

## F Layer

The topmost layer is that known as the Appleton or $F$ Layer. The height varies from about 200 miles upwards and ionization is mainly confined to nitrogen as at this height oxygen becomes rare. The F Layer is frequently considered as the most important. It becomes divided into two parts during daylight, the upper part designated as $\mathrm{F}_{2}$ and the lower portion $\mathrm{F}_{1}$. After sunset, and prior to dawn, it assumes the form of only one layer.

## Frequency Choice

Having examined the structural and reflecting arrangements which affect the wave, let us now consider how these various parts are put to practical use. Most of us are aware of the general rule that high frequencies are most useful by day and the lower ones give the best performance by night, although the exact choice of frequency used is critical if reception is to be of a standard worthy of being termed a service. Indeed, numerous observations are needed to formulate the vast number of short wave schedules published in advance which have to take into account the many factors already mentioned.

## lonosphere Sounding

Such information is compiled by "sounding" the ionosphere. A radio wave with an adjustable frequency is sent vertically upwards to a layer so that it is able to engage it at right-angles and then the

frequency is adjusted so that it can be observed to either penetrate the ionosphere or be reflected back to earth. When this frequency is found-the highest limit to which the frequency can be raised and retain its reflection-it is known as the Critical Frequency.

Having obtained this frequency it may be increased up to three or even five times, provided the wave is radiated in such a manner and angle that it will meet the layer at a slanting or oblique angle. Such arrangements may appear straightforward but in the case of a multi-hop circuit-perhaps one crossing the equator or a dusk and night period-the requirements become complex, requiring many calculations and even some compromises to meet the variations over the path. The wave for reflection from the F Layer will, even during its first hop, need to be strong enough not only for reflection but to overcome losses through absorption when it passes through the $D$ and E regions. It will, in fact, have to pass through these lower layers on two occasions even during its first hop.

## S.I.D.

We often hear on the amateur bands comments such as "Conditions aren't too good today". Such remarks refer to changes in propagation which can broadly be placed in two categories, one type of disturbance is referred to as a Dellinger or SID (Sudden Ionospheric Disturbance). This is often of a sensational effect happening in a very short timeso suddenly that the receiving equipment is often suspected. The effect is brought about by solar action
which causes an overwhelming ionization of the $D$ Layer leading to almost complete absorption.

The lower frequency end of the shortwave band is most affected and signals in this part may even become inaudible. The higher frequencies are less affected and will be the last to suffer losses and the first to return to normal. The duration of such disturbance is usually short lived.

When the face of the sun looking towards the earth is subjected to an eruption, solar flare (often called a sun spot) this brings about the emission of numerous kinds of radiation. These vary in their intensity but when of a great magnitude, may persist for a long period. For these reasons this kind of unsettled condition may reoccur with a complete rotation of the sun in approximately 28 days. The Dellinger or SID will normally only effect that side of the earth facing the sun.

## Ionospheric Disturbance

A more prolonged type of disturbance known as an Ionospheric Disturbance-or Storm-may also be associated with solar conditions and often occurs some 30 hours after observation of changes on the surface of the sun. The general merit of reception falls considerably with deep and sometimes rapid flutter fading due to a lower and variable density of the F Layer.

Having described such adverse conditions, the reader may begin to wonder how a wave survives for so many thousands of miles, and especally as variations in the signal strength may be as much
as 1000 to 1 , yet so much in modern receiver design is included to bring these variations to a stable and acceptable listening quality. The information given in the chart headed "Radio Propagation Characteristics" should be of value in helping to choose the correct wave bands.

## Reception Reports

Considering the complexities and variations in propagation it is not surprising that all broadcasting organisations giving a service in the international broadcasting bands welcome accurate reception reports from listeners.

Considerable sums of money are spent each year to inform the listener of recommended frequencies and times of operation. Even after a schedule is published, the broadcaster is still in need of accurate information regarding the level of interference, as the shortwave bands are so congested-a situation which will become worse as we move to solar minimum conditions and the higher frequency bands become less useful.

## Medium Waves

Most of these remarks have concerned the short waves or high frequencies as these are the ones most used for long distance reception. However, reception of distant stations is also possible in the medium wave band $(525-1605 \mathrm{kHz})$. MW Dxing is made especially difficult due to the large number of high powered stations operating in Europe. This wave band is basically designed for local reception and there are far fewer opportunities for long distance listening, even after midnight. Owing to so many broadcasters extending their hours of broadcasting such services frequently include an aerial system designed to avoid the sky wave and emphasise the ground wave. This reduces after dark interference and at the same time permits an economy by the sharing of frequencies. Listening to stations operating in the MW band is in any case confined to the hours of darkness if reception from a great distance is the aim. After dark these frequencies are reflected by the E Layer; the D Layer at night being almost non-existent. There are cases, however, when frequencies approaching 2 MHz find reflection from the $F$ Layer, having penetrated the E region.

## Other Bands

Other bands are subjected to other influences; remarkable reception due to tropospheric propagation in the VHF and UHF bands occurs occasionally. An outstanding example of the abnormal mode of propagation is that in earlier sunspot maximum periods, BBC Television pictures have been resolved as far away as the West Indies and South Africa.
Many listeners appear to associate bad weather, such as rain and fog, with either good or bad reception but there is no real evidence to substantiate this, at least not as far as the medium and shortwave bands are concerned. As the frequency is increased towards the microwave portion of the spectrum, that above 1000 MHz , these and other factors have to be taken into account.
At a recent press conference given by the GPO Telecommunications Department, many interesting facts were disclosed concerning the adverse effects of rainfall over even short path transmissions on these channels.

# your PRACTICAL 1 ci 1 . D月TВ WALL CHART 

WE expect rather a lot of our receivers don't we? In the early days of radio most homes sported a beautiful long wire aerial but with the tremendous improvement in receiver design and the vastly improved sensitivity we seem to have forgotten just how important a decent aerial is. Some receivers now being marketed claim that the silly little telescopic aerial which is an integral part of the set is all that is needed-rubbish!

For good DX results three things are needed, all of about equal importance: the receiver, the skill of the listener and the aerial. The receiver will cost quite a bit of money and the skill can only be learned with time; on the other hand an aerial will cost very little-wire isn't all that expensive after all-and the erection will take only a few hours.

The type of wire is far from critical. Hard drawn copper is possibly the best, it doesn't stretch, but it is expensive. One of the best, and cheapest forms is aluminium garden binding wire. 250ft. reels cost only about 30p.

Ex-Government aerial wire is still available on the surplus market and this is excellent; it is usually made up from one strand of copper surrounded by steel wires for strength.

On the Wall Chart we have tried to deal with practical types; it is all very well to read about wonderful professional arrays but few of us have the room or the money to pay for the tall masts required. Instead we have dealt with the types that readers are likely to have space for. Even if you live in a small flat you will usually be able to find room for a pretty good Whip Type, or even an Inverted L.

The chart deals with aerials but of course any signals induced into them will only be with respect to earth and a good earth should be used. One always used to see comments such as ". . . the earth wire can be taken to a cold water pipe . . ." but in these days of plastic plumbing this will not always work. A good earth can be made by soldering a wire to a piece of copper clad board-such as is used for making printed circuits; this should be buried as deep in the ground as can be managed and a bucket of water should then be poured over it to make the earth resettle around it. The size of the board is not critical but the larger the better. The wire from this earth to the receiver should be of very low resistance and as short as possible.


## E. BUCKLAND

NO one would deny that a full-range, full-facility audio signal generator is not useful. The author has a good one (built from a design published in Practical Wireless some years ago) and it is continually in use for designing, testing and trouble shooting but only a few of the facilities account for 95 per cent of the usefulness. Most of the time the frequency is left on 1 kHz and only the calibrated output is used. When the frequency is varied it is nearly always at the spot frequencies of $100 \mathrm{~Hz}, 1 \mathrm{kHz}$ and 10 kHz . Nearly all signal generators have a switch to give either a sine-wave or squarewave output. This is frequently used but it is rare that the type of wave-form matters very much. Where it does matter, it is nearly always the square-wave that is required.
The main signal generator was found to be so useful that the author decided on building another, this time to be battery operated for portability. Bearing in mind the points made above it was also decided to make a far simpler and less expensive version, incorporating only the most useful facilities.

This unit gives a constant square-wave outputirrespective of battery voltage and other factors-at three spot frequencies: $100 \mathrm{~Hz}, 1 \mathrm{kHz}$ and 10 kHz . The output is continuously variable over a wide range. To simplify the switching, the on-off switch is incorporated with the frequency selector and the decade outputs are provided from separate output sockets.

The complete unit is very small, fitting nicely into a small aluminium box, $4 \mathrm{in} . \times{ }^{2}{ }_{2} \mathrm{in} . \times 2 \mathrm{in}$. and the total cost is only a fraction of that for a full facility audio signal generator.

This makes an excellent "back-up" unit but even by itself it should be useful for those without an a.f. signal generator.

## THE CIRCUIT

The signal oscillator is a basic multivibrator, made up from $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$. Both halves of this are identical, with similar base bias resistors and the same collector load, although for $\operatorname{Tr} 2$ this is a variable potentiometer and not a fixed resistor as that for Trl.

The values of the coupling capacitors are altered by the main switch, SWl, and one of three capacitors can be selected. This balance in the two sections ensures a square wave output with a $1: 1$ mark space ratio, not vital but easy to incorporate and occasionally useful. The values of the bias resistors etc., ensure that the transistors are driven on hard when they are turned on, this ensures that the output will be constant.

The output is taken from the collector load of Tr2, the slider of VR1 is connected via C2 to the base of the emitter-follower Tr3. The high value of C 2 is deliberate, this will ensure no degradation of the tops and bottoms of the square wave at 100 Hz . $\operatorname{Tr} 3$ was found necessary to isolate the output from the


Internal view of the prototype.


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Fig. 1 : Complete circuit of the Audio Reference Source.
multivibrator. As this stage contributes no gain it may be thought that the output network could be connected directly to the slider of VR1 but this would vary the load at the collector of Tr2 and affect the frequency and level. The inclusion of Tr3 makes certain that this interaction is minimal.

The output from the emitter of $\operatorname{Tr} 3$ is taken via the d.c. blocking capacitor C 3 to a decade attenuator. At each of these output sockets the output is one tenth that of the previous one.

Because of the operation of a multivibrator, we can always be sure that the output will be constant, irrespective of frequency as long as the supply voltage is constant. This is done by including a zener diode with a rating of $7 \cdot 5 \mathrm{~V}$ in the positive supply line, the voltage drop taking place across the resistor R11. SW1 is a three-pole, four-way switch; three of the sections are used to alter the frequency of operation of the multivibrator, the fourth section acts as the on-off switch.

The whole circuit is very simple as can be seen from Fig. 1. BC107 transistors are specified but BC108, BC109 or their plastic versions (BC168 and BC169) can also be used, as can a 2 N 2926 . None of


Fig. 2: The component layout on Veroboard. The only breaks in the copper strip are those near the mounting holes.

## $\star$ components list

|  <br> All resistors $\frac{1}{6}$ W; 5 per cent types. VR1 $1 \mathrm{k} \Omega$ linear pot., catbon track holes, 0.15 in . matrix; small aluminium case with lid. * |
| :---: |

these changes will affect the constant output which is controlled by the supply voltage and nothing else.

VR1 should of course be a linear control and the associated knob can be calibrated if required.

The capacitors in the multivibrator may not give the exact frequency specified, this will depend on their tolerance, but it should be close enough for all practical purposes.

The unit takes only a small current and this is adequately provided for by a PP3 battery.

## CONSTRUCTION

The component layout of such a unit is far from critical but that used in the prototype is both simple and neat. The majority of the components are mounted on a small piece of 0.15 in . matrix Vero-
board, 16 holes by 9 holes; this can be cut from a standard $2^{1}{ }^{1}$ in. width. The component layout is shown in Fig. 2. Various take-off points are letter coded R to Z to tie up with the main wiring diagram in Fig. 3.

No breaks are necessary in the copper conducting strip of the Veroboard other than those near the mounting screws. The battery negative is taken to the board by a wire running from a small solder tag which fits under one of these mounting screws.

The frequency determining capacitors are mounted directly onto the switch SW1, this can be seen from the photograph of the prototype.

The output sockets are mounted next to each other and the attenuating resistors are wired directly to these, the chassis connections being taken to solder tags under the mounting screws. Coax output sockets were used on the prototype mainly to continue standardisation in the author's test equipment but other types-such as phono sockets-can be used.

The component board is held onto the chassis by means of a short length of aluminium angle bracket.


Fig. 3: The wiring diagram. The retters R-Z match up with those in Fig. 2.

## CALIBRATION

It is not possible to say what the exact output will be for any particular version, this depends on the saturation of the individual transistors, but what can be said is that it will not vary with frequency or battery voltage. If a highly accurate output is required this is best measured on a 'scope. The output can also be reduced to a reference figure by wiring in an extra resistor between the collector of Tr2 and VR1. If the output is say 2 V and the maximum output wanted is 1 V then a $1 \mathrm{k} \Omega$ resistor will be required. The output from the prototype is 1.8 V and this level has been found sufficient. The output from the other decade outputs is 180 mV and 18 mV at maximum output.

## BACK NUMBERS

We regret that the back numbers department of P.W. has now closed and consequently we are unable to supply these. Requests for specific back issues can usually be included In our ' 'CQ' section; there is no charge for this but It is a sorvice between readers and P.W. is unable to meet any of these requests.

NEWCOMERS to the medium waves are often surprised at the number of West African countries that can be heard on this band. La Voix de la Revolution located at Conakry in the Republic of Guinea, is a conspicuous signal on 1403 kHz after 2300 hrs GMT. Programming is African in style with announcements in French. The new high power broadcaster at Bissau, Portuguese Guinea can be logged on 1070 kHz between 2300 hrs and 0100 hrs GMT with pop music, announcements and news being in Portuguese. From the Canary Islands, the high power Radio Nacional Espana outlet in Tenerife is a strong signal on 620 kHz after 2300 hrs . Programmes are in Spanish and there is interference at times from Batra in Egypt. Dakar, Senegal on 764 kHz can be heard on weekdays with African music and French announcements after Sottons, Switzerland closes down. From the Republic of Zaire (Congo) the station at Kinshasa on 692 kHz is on the air all night and is audible, with African programming after the East German station on this frequency signs-off, usually at 0100 hrs GMT on weekdays. Radio Nigeria at Enugu is on 1320 kHz until sign-off at 2300 hrs GMT. Programmes are in English and can be found during the last half hour of transmission, as a weakish signal between the European channels 1313 kHz and 1322 kHz . Another English speaking broadcaster is occasionally heard on 629 kHz . This is ELBC at Monrovia, Liberia which closes down at 0045hrs GMT and is usually logged towards the end of its transmission.

A new broadcaster in North Africa has appeared on the Long Waves. It is located in Algeria and is audible in the UK during the evening on 254 kHz (1181m); a channel it shares with Lahti, Finland. Programmes are in French and reception reports, which are requested over the air, should be sent to Radio Television Algerienne, 21 Boulevard des Martyrs, Algiers, Algeria. This is the second North African to appear on the LWs in recent years: Azilal, Morocco is on 209 kHz with programmes in Arabic and can be logged after dark with some interference from Kiev on the same channel. The range of long wave stations increases considerably at nightEuropeans fade-in regularly along the eastern seaboard of North America after local sunset. Stations heard in the UK by the writer include Reykjavik, Iceland on 209 kHz at 0100 hrs GMT; Ashkhabad, Turkmenia on 200 kHz after Droitwich signs-off; Ankara, Turkey 182 kHz with sign-off at 1930 hrs GMT; Baku, Azerbaijan on 218 kHz at 0100 hrs GMT; Novosibirsk 272 kHz at 0130 hrs and Omsk 394 kHz at 1900 hrs . In Europe, the long waves covers 151 kHz to 282 kHz buit in Asiatic Russia the band extends to 400 kHz . Regulars to be heard in the "hf" section are Orenburg 300 kHz ; Kharkov 384 kHz and. Minsk 400 kHz .
Please send logs and information about the medium waves to the author at 132 Segars Lane, Southport PR8 3JG.

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## LAURENCE COOK

THE circuit to be described was designed to fulfil the need to see what was going on in TTL logic systems without having to use a voltmeter to determine whether a "l" or " 0 " existed at any point. To give a positive indication of the presence of a logic level it was decided at the outset to have two lamps, corresponding to a " 0 " or " 1 ". Neither lamp would light with the probe either floating or at an inadmissible voltage (e.g. $1 \cdot 2$ volts).
Since the probe has been completed, it has proved extremely useful to me (and to those who have borrowed it!) and will doubtless soon repay its cost in time saved tracking down faults. It may even encourage people to "have a go" at logic circuitry, since it quashes the familiar cry, "I can't see what's going on inside those bugs".

## CIRCUIT

Only four transistors, four resistors, two diodes and two bulbs are used (see Fig. 1). A few moments spent studying the circuit should enable one to spot


Fig. 1. Circuit of the Logiprobe.
the fact that it is really two circuits, one the inverse of the other; that is, $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$ are arranged in a similar fashion to Tr 1 and Tr 2 but "upside down". The reason for this is simple.

With the probe on a logic " 0 " the voltage at Tr base, determined by the divider chain and probe voltage ( $>0.8 \mathrm{~V}$ ) causes Tr 1 to turn on. Trl collector goes towards +5 V and Tr 2 emitter does the same, since Tr 2 operates in common collector mode. LP1 therefore lights, indicating a logic " 0 ". Similarly a logic " 1 " at the probe causes the voltage at $\operatorname{Tr} 3$ base to turn $\operatorname{Tr} 3$ on, and so $\operatorname{Tr} 4$ drives LP2, which lights up.

The resistors in the divider chain are of such values as to keep both lamps off when the probe is either floating or between 0.8 V and 2.4 V with respect to earth. Should the probe be accidentally touched on a voltage below earth or above +5 V , then D2 or D1 respectively conduct to prevent the reverse base-emitter voltages of Tr 3 or Tr 1 being exceeded. Resistors R2 and R3 limit this current, but it is inadvisable to deliberately look for trouble by touching the probe onto higher voltage rails for long periods.

## CONSTRUCTION

The logiprobe is assembled on a piece of 0.15 in . matrix veroboard (see Fig. 2.), with flying leads for supply and lamps. This enables it to be housed in any convenient small plastic box. The probe may be made from an old ball-point pen. It is largely a matter of choice how one terminates the supply leads, but since the supply must be the same as that of the TTL circuitry to be tested, then small insulated crocodile clips would be handy.


Fig. 2. Layout of the Logiprobe on a small piece of veroboard. Note that transistor leadout connections are shown as seen from on top. Compare this layout with photograph of completed unit.

Start by cutting a piece of veroboard to the right size for the box, then solder flying leads as shown. Next solder in the resistors, diodes and transistors. Use a heatsink and a small well-tinned iron just in case the resistor values are altered by overheating them, since these determine the levels at which LP1 and LP2 light. For this reason R1 to R4 should be $5 \%$ or better, and not nasty old things out of that TV set recently butchered! Finally solder LP1 and LP2 onto their respective leads.


The lid of the box carries the two lamps which should be of differing colours, representing " 0 " or " 1 ". The lamp terminals are insulated to prevent short circuits when the lid is filted to the box.

## TESTING

Connect the logiprobe to a 5 V supply. If all is in order both lamps will be off. If not, either the supply is wrong, or a mess has been made of the board. Look for blobs of solder bridging the copper strips and get rid of them! If both or either of the two lamps are still on, make sure that everything is connected the right way round; we all make mistakes!


Fig. 3. Test set-up using an integrated circuit.
Touching the probe to earth or +5 V should light LP1 or LP2; just to make sure all is well try the probe on an i.c. output with a voltmeter as a temporary check. (See Fig. 3).

Finally, a word of warning. Unless one is prepared to fiddle for hours with stacks of resistors, use the components specified. If you can't resist trying different transistors, at least use silicon of a similar type.

When your logiprobe is finished you'll wonder how you managed without it. But keep it hidden or people will borrow it from you!

## BINDERS/INDEX for PW

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S.GINSBERG

ONE so often reads about the amazing advances and research programmes which take place in other parts of the globe. It is, therefore, refreshing to hear of some work which is being done in this country. This is particularly so since the establishment in question is the Post Office Research Department at Dollis Hill.

Workers at Dollis Hill are experimenting with those intriguing things called magnetic bubbles. A new generation of words is now fast coming into being. For example, a "bubble eater" and a "keyhole generator" are commonplace.
Basically, one method of employing magnetic bubbles is to lay down a series of minute conductive elements in the form of " T " shapes. These are typically formed of nickel-iron and are of the order of $1 \mu \mathrm{~m}$ thick. The idea is that a tiny magnetic bubble can be transferred from one " T " to the next and even annihilated. Thus the bubbles can be used as a means of storing data. The bubbles themselves are only some $10-18 \mu \mathrm{~m}$ in diameter.
The workers at Dollis Hill have developed, and I kid you not, a bubble detector bridge (see what I mean about the terminology?). The idea is an extremely clever one. Four minute resistive arms of a-bridge circuit are formed by a deposition of a very thin nickel-iron alloy which is less than $1000 \AA$ thick. The resistivity of this alloy changes whenever it is subjected to a magnetic field. Thus, when a magnetic bubble arrives at the bridge, its magnetic field will affect, say, two of the "resistors" effectively altering their resistances and thus unbalancing the bridge.

This work is impressive and follows closely on the heels of a previous announcement of work done here on transistors rated at around 1.5 Watts in the 4 GHz region. These transistors were reported to have base widths of only 0.14 microns. Truly it is a small world.
Occasionally one hears news which is disturbing. Not only because of the actual content and what it implies, but also because of the reliable source from which is comes. This piece of news concerns lasers. One can use a laser beam and modulate it, thus using it to convey communications. If you "shine" a laser beam down a light fibre you can carry it from one place to the next. Again, it is possible to get quite a few "channels" on a laser beam, far more than you can on a single, comparable coaxial cable, for example. The thought now goes that for all communications work, land lines etc., lasers plus light fibres will be used. If this is true, then it could mean our old friend the coaxial cable is on the way out!

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BRITISH INSTITUTE OF ENGINEERING TECHNOLOGY

## CQ complaint

I wish to make a complaint regarding an advertisement in your CQ column of June 72.
I supplied a S.A.E. and requested lists of issues especially Nov. 71 from a reader.
This was over a month ago and as yet have received no word from him. I think he must be collecting 3 p stamps!
Would you please put an advert in your CQ column for me? I require Nov. 71 Practical Wireless or a copy of the article on the organ.-M. F. Longmore, ( 31 Kent Ave., Larne, Co. Antrim, $N$. Ireland).

## Construction award

The 2nd G3XBF Constructors Award, sponsored by the Barking Radio and Electronics Society G3XBF-Affiliated to the Radio Society of Great Britain will be held on Thursday, November 9th, 1972 at the new BRES HQ: Westbury Recreation Centre, Westbury School, Ripple Road, Barking, Essex, at 7.45 pm .
Talk-in facilities are: $160 \mathrm{~m}-$ G3XBF, on 2 m -G8EAY/A, (TX $145 \cdot 0$ ). Judges: G. M. C. Stone, CEng, MIEE, MIERE, G3FZD, Council Member and v.h.f. Manager RSGB. D. A. Findlay, DFC, FCA, G3BZG, General Manager and Secretary RSGB. R. S. Hewes, G3TDR, Region 7 Representative RSGB.

There will be an award for each section and an overall winner. Each award will consist of a hand produced certificate and a worthwhile cash prize.

A film will be shown during the judging and refreshments will be available. Closing date for entries Wednesday, October 25th, 1972. Entry forms and further information may be obtained from Alan P. Foss, G8EAY, 73, Coolgardie Avenue, Chigwell, Essex. (01-500 6034).

## VHF hope

So interesting is your August editorial on "Hope for VHF" that I could write sufficient about it to fill another!

VHF has not "caught on" for several reasons, and I will list a
few technical ones first. A v.h.f. radio costs $1^{1}{ }_{2}$ to 3 times as much as a comparable type for m.w. Invariably it uses at least two more transistors, which, so far as batteries are concerned, raise the quiescent current by about 10 per cent, and this is aggravated by the fact that v.h.f. oscillators are not only less stable in the face of falling voltage, but in fact actually cut out completely when the battery has still an appreciable amount of "life" in it usable on m.w. With battery manufacturers seemingly not knowing where to stop with their price-rises, and many of the receivers being of the "pocket" type, the matter speaks for itself.
But away from technical aspects, the BBC HAS something to answer for. As an example, take Sundays on Radio 4.

At 8.20 a.m., v.h.f. and m.w. part company, and unless one wants a Pakistani programme, he scraps his m.w. and goes v.h.f. But some 45 minutes later he is assailed by "Open University", so, out has to come his trusty m.w. I have always said that v.h.f. and m.w. should never part course, and neither should have Radios 1 and 2, because in the latter case the 247 m . transmission was to fill up locally the areas not well served by Droitwich on 1500 m . Since the service areas of the v.h.f. stations more nearly coincide with the centres of Pakistani population this would be the more logical frequency for that service, but better still these should be on the "Local" stations, since for a large part of their time they just repeat BBC programmes available at better quality on the regional stations a little along the dial. In North-Northumberland, listeners have to rely upon m.w. because v.h.f. is not reliable there, and there is no Pakistani population either!

I run a v.h.f. tuner to Mr. Cameron's excellent design a year or two ago in "P.W." and it does enable me to hear the broadcast distortion more clearly, for the programmes are either full of badly received telephoned matter, or of the "popular" type to which a bit of distortion makes little difference anyway.-James $\mathbf{w}$. Robson, (Newcastle Upon Tyne).

## Thanks

In the issue August 1972 your contributors H. Hellyer and M. Hollier continue with Part 9 of their excellent series "Transistor Circuitry for Beginners".

Their style is lucid and most readable, and in this issue we were particularly gratified to note their suggestion, page 341, "if Mullard Ltd. didn't exist, they would have had to be invented".

We especially appreciate their acknowledgement of (sic), "a direct crib from Chapter 3 of the Mullard Transistor Handbook". It is perhaps carping to indicate that reference should be made to the end of Chapter 2, and that the title used is ambiguous, in connection with other Mullard publications. For the benefit of readers wishing to supplement the information provided by your contributors the correct title should be "Transistor Audio and Radio Circuits".
L. W. Owers, Manager-Educational Service, Mullard Ltd.

## VHF services

With regard to your editorial colunn in the August Practical Wireless, I would, as a newcomer to the arts of practical electronic work, like to make one comment.

Although your column makes a fair general statement, I feel that one reason for the lack of use of v.h.f. services is the fact that reception in many areas (for example the Pennine valley in which I live) is very difficult. This problem may, I suppose, be overcome by the erection of a dipole aerial but the average radio listener is still faced with the fact that very few of the popular battery operated portables are equipped to take a coaxial or twin feeder from an external aerial (idea for a future article?). The so-called "v.h.f. telescopic aerials" fitted to these sets are virtually useless in these sheltered areas.

Of course, when one writes to the BBC commenting on the problems of receiving Radio 3 on Medium Wave, they in turn refer one to the v.h.f. services! Do they realise that v.h.f. is not easily available to all?-T. D. Jackson (Lancashire).

# practically Wireless commentary by HENRY 

PICTURE, if you can, the telepundits squaring-off across the studio table, dissembling when flummoxed, leaping eagerly into the subject when a question slots into their pigeon-hole of knowledge. The scene is familiar.

But have you ever been exasperated by the overbearing type who listens with evident impatience to his opposite number's bumblings, then thrusts in with the verbal pike off: "What you mean is . . ." and proceeds to expound his own meaning?

I think we could do with a few of those pikers in the hushed rooms and holy corners where Users' Manuals, Operating Handbooks and Service Instructions are compiled. In one classic example of the dismantling instructions for a Japanese radio-cumportable tape recorder, a sequence of nearly a dozen operations had to be made to get the chassis from the cabinet. Following the quaint orders was bad enough, but after action 3 one reached an impasse. The next stop in the sequence could only be taken if you tugged, pulled, shoved, wrenched and twisted the loudspeaker mounting. Some plastics break with a gut-rending "Crack", don't they?
The solution comes, after one failure, at about Stage 12, when


[^2]we are told: "Before unloosing the regulator board, take off the two clips marked $A$ and $B$ in diagram."

But even when meanings are explicit there can be an embarrassing contretemp. Five times in a fortnight, soon after Garrard brought out their SP25 Mark III autochanger, we had to explain patiently to new users that rejecting during Manual Play required one to flick the lever to Auto and then bring it back to Manual. If you left it in the Auto position, the pickup arm would reject-sure-but cycling commenced and the record would be replayed in the selected size position. The instructions are there, plainly enough on Page Nine of the handbook issued with the gramophone deck, but who reads handbooks?

Not so good are those handbooks, usually printed in several expensive colours and all sorts of languages from Serbo-Croat to Sanskrit, which have such convoluted language that the English version is as ambiguous as the hieroglyphics.

Henry has whiled away many hours cross-referencing the English with adjacent columns of French and German, which deluded tutors were under the impression he had learned in his younger days.

Instructions in some strange Scandinavian tongue translate curiously if one attempts to be literal. Take the phrase: "Nun das Stromkabel in eine Steckdose anschliessen." That comes near the beginning of the Bedienungsanleitung (which everybody knows is the manual de Instruc ciones) for the Sanyo STD-100 stereo cassette recorder.

Well, if we have to cope with the Common Market, let's have a go. Looks like a tale about this nun who climbs some mountain to get more living room. And lower down we see . . ." reglers so einstellen, dass optimale Aufnahmequalität erzielt wird." That one


Who reads handbooks?
is obvious: "if you've go to instal it regularly, cheer up and do not use that naughty word."

It becomes quite deflating to learn that the first phrase tells you to plug the power cord into an a.c. outlet, while the second is about adjusting the input level for optimum recording quality.

The section in Japanese was most intriguing, especially as English words like ON, OFF and EJECT larded the text like plums in a pudding.

Henry has campaigned for years to make suppliers add at least a circuit diagram to their equipment, and to put the specifications where they can be seen. In the June issue of Hi-Fi News, the $B$ \& $O$ publicity boys mention that they always include a circuit diagram in a cute little pocket inside each piece of their equipment. In the same issue, a reader tells us he could not get a service manual with his tape recorder. He received, instead, a courteous letter pointing out that it was not Company policy to supply service manuals to the consumer public.

He answers that he, too, has a policy, which stated quite simply says: "No Manual-No Machine." Henry feels that more people should wield that pike.


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## A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

A$T$ this time of year the nights are closing in and unless something miraculous occurs, winter will follow shortly. As a nation we are supposed to ignore that season until it actually happens; iced points on the railways and the resulting chaos is just one example. However Take 20 is going to set an example to the nation with this month's circuita Frost Alarm. You may think that such a project has few uses, but think about it. Freezing pipes in the loft can be prevented, the greenhouse heating can be turned on and the fruit growers can take the necessary precautions if you are given some warning that the air temperature is approaching $0^{\circ} \mathrm{C}$. The circuit falls within our $£ 1$ limit but if it is to become a permanent fixture, rather than built up for interest, a mains operated power supply must be used, batteries are quite unsuitable unless you are prepared to keep switching the unit on and off.

We are calling the circuit a Frost Alarm but it can be made to operate over a wide range of temperatures, it is simply a matter of adjustment. The alarm device is a bulb which will light as soon as the temperature falls below the preset level. The warning device can be situated in any convenient position where it will be seen easily with the temperature sensor up to 100 yards away. This is the main advantage; you don't have to go out in the cold to look at a barely readable mercury thermometer.

## The Circuit

The circuit of the frost alarm is shown in Fig. 1. The temperature sensing device is a thermistor. This is a device whose ohmic resistance varies with the temperature. At $25^{\circ} \mathrm{C}$ the resistance of the one specified is about $4.7 \mathrm{k} \Omega$. Above this the resistance falls to a low level but below it the resistance increases. On the one used for the prototype this was measured as $8 \mathrm{k} \Omega$ at $0^{\circ} \mathrm{C}$.

The thermistor is wired in series with a variable resistor, VR1, and the junction of these is taken to the Schmitt Trigger circuit which comprises Trl and Tr2. The voltage at the junction of TH1 and VR1 will depend on two factors; the temperature and the setting of VR1. We can easily arrange for this voltage to be just sufficient to bias Trl into conduction and set VR1 so that when the temperature falls, and TH1 increases in value, that Trl will have insufficient voltage at the base to maintain conduction.

While $\operatorname{Tr} 1$ is switched on, $\operatorname{Tr} 2$ will be held switched off since the saturation voltage (which is that voltage between the emitter and the collector when the transistor is fully conducting) is below that necessary to bring Tr2 into conduction. The connection of these two transistors is such that when one is conducting, the other is off and vice versa. The switching action is very rapid and very positive. We have explained

No. 41
FROST ALARM


Fig. 1: The circuit of the Frost Alarm.


Fig. 2: Suggested component layout on tag-board.

## * components list

|  | 10k 3 \% +W | 1p |
| :---: | :---: | :---: |
|  | 39, $5 \%$, ${ }^{\text {d }}$ W | 1p |
|  | $1 \mathrm{k} \Omega 5 \%$ \% W | 1p |
|  | $39 \Omega 5 \%$ iW | 1p |
| VR1 | $2 \cdot 5 \mathrm{k} \Omega$ lin. pot | 12p |
| TH1 | VA1066S, $4.7 \mathrm{k} \Omega$ thermistor (Henry's | Radio) 20p |
|  | BC109 | 10p |
| Tr2 | BC109 | 10p |
|  | BFX88 | 20p |
|  | $6 \mathrm{~V}, 60 \mathrm{~mA}$ bulb | 5p |
| Bult | holder | 11p |
| SW | On-off switch | $7 p$ |

Prices are those recently advertised and may have changed. No allowance is made for minimum order costs or for postage and packing and these points should be checked carefully before ordering.
the operation of this circuit before in this series in more detail. When Tr2 is off there will be no voltage drop across R3 and so $\operatorname{Tr} 3$ will be off. When $\operatorname{Tr} 2$ is on, this will turn on $\operatorname{Tr} 3$ and current will pass through the bulb. The reason for R 4 is only because 9 V bulbs
do not seem widely available, unlike 6 V versions, and this resistor prevents the bulb being overloaded. $A$ switch is shown only for convenience. If a mains operated power supply is used, as it should be, the switch should be on the input to this. As we mentioned before the thermistor can be connected to the circuit by a long length of wire, as the resistance of this will be negligible compared to that of the device itself.

## Calibration

It is not too difficult to calibrate VR1. Put the thermistor with its leads into a small plastic bag and put this into a bowl of water and melting ice. The temperature among the melting ice will be $0^{\circ} \mathrm{C}$ but this may mean that the warning will come too late. If a decent sized bowl is used, it is better to calibrate using the water temperature at the bottom of the bowl, here the temperature will be $4^{\circ} \mathrm{C}$. Once calibrated the unit can be tested by putting it into a fridge, checking the switch-on temperature against a mercury thermometer. The inside of a fridge should be just above freezing, say $3^{\circ} \mathrm{C}$ or so.

A suggested layout on a small tagboard is shown in Fig. 2.

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## Practical Wireless

 Designer's Traphy1972

To encourage new authors, entries for the 1972 Trophy will be restricted to readers who have not previously had an article published in PW. This leaves the field wide open for those wanting to try their hand at writing technical constructional articles. Contestants will not be in competition with well-known authors, only with other newcomers, so the cup can only be won by a new writer. It Could Be You.

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## INNEXTMONTH'S

## PRAGTIGAL miallas



The prospective buyer of hi-fi equipment can rightly feel a little bemused as he attempts to make sense of the welter of technical literature showered on him by manufacturers. With the audio 'season' now upon us we thought readers would like hi-fi expert Gordon King to explain and comment on the confusion of hi-fi jargon that now besets the man-in-the-street. Hi-fi is not cheap. A study of our ABC will ensure that your money is well spent.

## 8 WATT SILICON AUDIO AMPLIFIER

The falling cost of silicon output transistors now makes them an attractive alternative to germanium types. This article describes a high specification, all-silicon, $8 W$ power amplifier with a suitable power supply. In addition a circuit is given for a matching high quality preamplifier.

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 phone and line inputs and full control is provided over the reverberation level.


# THE <br>  

# PRE-TUNED  RADIO 

FOR general use it is an advantage to have a receiver with a number of pre-selected stations available so this receiver is pre-tuned to four frequencies with provision for adding two more stations, or variable tuning, if wanted later. Three m.w. stations are available, with one l.w. station for reception of the BBC on 1500 m . This is very convenient for day to day use and reception of a variety of programmes.

Reception normally is on the loudspeaker but there is provision for plugging in a personal earphone or headset, when this is more convenient for listening. A car aerial connector socket is provided, so that the receiver can be placed in a car where the use of pre-set station selection is a decided advantage. The receiver shape allows it to rest on a parcel shelf with its speaker upwards, or suspended under a shelf with the speaker downwards.

A diode output socket is fitted which is of advantage when a tuner is required for a tape recorder or other audio equipment. The receiver audio stages may then provide a signal for monitoring purposes.

## R.H. LONGDEN

The circuit is shown in Fig. 1 and is a straightforward and reliable one using easily obtained components. L1 is the ferrite aerial rod, and section Sla of the 6 -way switch selects TC1, TC2, TC3 or TC4 pre-set trimmers, to give automatic tuning of the wanted stations. L1, TC4 and the parallel capacitor Cl provide l.w. reception, no additional winding being required.

Switch Slb similarly selects one of four oscillator trimmers, TC5 to TC8, and these tune the oscillator coil L3 to the required frequency. In practice, it is sometimes found that changes in battery voltage, temperature or slight changes in oscillator capacitor values, throw some pre-set stations slightly off tune. This is avoided by using a small panel control VC1, which can if necessary be adjusted to compensate. In use, the trimmers are set with VC1 half closed, then it is only necessary to adjust VC1 if signals are heard to be off-tune.

It will be noted that alignment between L1 and L3, throughout one or more fully variable tuning ranges, is not necessary, as when ordinary tuning is used. There are thus no ganging difficulties here, as it is only necessary to adjust pairs of capacitors TC1/TC5, TC2/TC6 etc., for the wanted stations.

As the ferrite rod aerial is unsatisfactory in a vehicle, coil L2 allows a car aerial to be coupled to the receiver.

The 2-stage i.f. amplifier has three single-tuned i.f.t.'s, and a.g.c. via R9 from the detector diode D1. Audio signals may be taken directly from the diode circuit by the outlet provided. VR1 is then turned to zero, unless audio signals for monitoring are wanted from the receiver.

The remaining outlet is for a personal earphone or headset, when required, inserting the plug silencing the receiver speaker. A large external speaker can also be plugged into this socket.

## SWITCHED CAPACITOR ASSEMBLY

This consists of the switch, with eight pre-sets and Cl , wired on a paxolin panel $4 \times 2 \mathrm{in}$., as in. Fig 2. TC1 and TC5 are both 60 pF max as are TC2 and TC6. These were set for 1214 kHz , Radio 1 and

1088 kHz , Radio 4. TC3 is $50-450 \mathrm{pF}$, and TC7 is $20-$ 250 pF , for 647 kHz , Radio 3 . For 200 kHz , Radio 2 TC8 is 450 pF and TC4 is 1250 pF with Cl 1000 pF in parallel.

It is unlikely that other values will be wanted for TC1 and TC5. TC2 and TC6 can be 100 pF if a lower frequency than about 1088 kHz is needed here, or may have small fixed capacitors in parallel. In some parts of the country Radio 2 on 200 kHz may not be required when TC4 and TC8 can then be $100-400 \mathrm{pF}$, for an additional m.w. station in which case Cl is omitted. Ranges with the pairs of pre-sets overlap considerably. The oscillator circuit requires less capacitance than the aerial circuit.

Washers on the switch keep leads and tags clear of the metal panel of the receiver and when the assembly is wired, it is fixed with the selector switch nut.

## CIRCUIT BOARD

This is $5 \times 3$ in., a piece $1^{3_{4}} \times{ }^{3}{ }_{4}$ in. being cut out to accommodate the speaker, as in Fig. 3. Wiring will be simplified if the perforated board is cut so that there are 19 rows of holes one way, and 32 rows the other. Components can then be placed with their
wire ends exactly as shown, and wiring will closely follow the diagram of the underside of the board.

Holes have to be drilled for L3 and the i.f.t.'s. A very small round file will be found useful to obtain a fit if any holes prove to be out of position. The identification spot on L3 falls between pins 1 and 6, and these pins should come as in Fig. 4.

Check resistor values as they are inserted, and note also the polarity of the electrolytic capacitors and diode D1. When some components are in position, turn the board over and connect as in Fig. 4, snipping off excess wire.
If each item and its leads are marked in coloured ink or pencil on the drawing as inserted and connected, it is unlikely that anything will be overlooked, or wrongly connected. It may prove helpful to use red lmm sleeving on positive circuits, black on negative and some other colour for remaining connections.
Pieces of coloured sleeving about ${ }^{3}$ in. long can be put on the transistor wires. This will identify them, and also hold these at a suitable height from the board.
Transformer T 1 is held by its leads plus a little adhesive. Other driver transformers of similar type will give the same results, but connections must be


Fig. 1: above, shows the complete c/rcuit dlagram for the PW pre-tuned radio, together with the base data for the transistors. Values of pre-set trimmers TC1-8 are tabulated separately. Fig. 2: left, gives the layout of the trimmer capacitors and connections to. station selector switch, all mounted on a separate paxolín panel.


Fig. 3: above, layout of components on the front of the veroboard panel. For clarity the framework of the speaker has been omitted. Fig. 4: right, shows the component wiring on the reverse side of the board. Note polarity of electrolytic capacitors and diode D1.
The photograph at the bottom of the page is a general view inside the receiver which may be compared with Fig. 3 above.


## FERRITE AERIAL

L1 is wound with 24 s.w.g. enamelled wire, with turns side by side, on a $6 \times{ }_{8}$ in. diameter rod. Anchor the wire ${ }^{1} 2 \mathrm{in}$. from one end, at A, Fig. 3, with tape or adhesive. Wind on 80 turns and form loop of wire at MC. Continue for a further 5 turns in the same direction and finish off at B . A lead runs from MC on the aerial winding to MC at TC7, Fig. 2, A runs to Sla, and B to C2.

The aerial is mounted by cutting two strips of paxolin about $2 \times{ }^{1}{ }_{2} \mathrm{in}$. and mounting these with small brackets held under bolts that secure the speaker. A " $V$ " is cut in the end of each strip, and the rod held by thin string round it and through small holes in the strips.
L2 is 35 turns of any thin insulated wire, placed on the rod about ${ }^{1}{ }_{2}$ in. from $B$.

The car aerial socket is mounted on the right side of the case, viewing the receiver from behind, Fig. 3.

The diode output socket is near VR1, on the side of the case, and C14 is for d.c. isolating purposes.


| Resistors |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | 56k $\Omega \quad$ R7 | 4.7k | R13 $1 \mathrm{k} \Omega$ |
| R2 | 10k | $1 \mathrm{k} \Omega$ | R14 680 |
| R3 | 3.9k』 R9 | 8.2k $\Omega$ | R15 4.7kn |
| R4 | 68k $\quad$ R10 | $2 \cdot 2 \mathrm{k} \Omega$ | R16 100 5\% |
| R5 | $1 \mathrm{k} \Omega \quad \mathrm{R} 11$ | 68k $\Omega$ | R17 4.78 |
| R6 | 22k $\quad$ R12 | $22 \mathrm{k} \Omega$ | All $10 \%$ + W |
|  | $5 \mathrm{k} \Omega \log$ potentio | eter wit | switch, S2 |
| Capacitors |  |  |  |
| C1 | 1000pF SM | C8 | $0.047 \mu \mathrm{~F}$ |
| C2 | $0.01 \mu \mathrm{~F}$ | C9 | $0.01 \mu \mathrm{~F}$ |
| C3 | $0.01 \mu \mathrm{~F}$ | C10 | $2 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C4 | $10 \mu \mathrm{~F} 6 \mathrm{~V}$ | C11 | $100 \mu \mathrm{~F} 12 \mathrm{~V}$ |
| C5 | $0.047 \mu \mathrm{~F}$ | C12 | $50 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C6 | $0.25 \mu \mathrm{~F}$ | C13 | $100 \mu \mathrm{~F} 12 \mathrm{~V}$ |
|  | $0.1 \mu \mathrm{~F}$ | C14 | $0.5 \mu \mathrm{~F} 150 \mathrm{~V}$ |
| TC | $17-60 \mathrm{pF}$ | TC5 | 7-60pF |
| TC | 2 7-60pF | TC6 | 7-60pF |
| TC | 50-450pF | TC7 | 20-250pF |
| TC | 4 400-1250pF | TC8 | 50-450pF |
|  | compression trimm | mers |  |
|  | 15 pF variable (Ja | ckson C8 |  |
| Semiconductors |  |  |  |
|  | OC44 | Tr4 | AC128 |
| Tr2 | AF117 | Tr5 | AC128 |
| Tr3 | AF117 | Tr6 | AC128 |
| D1 | OA81 |  |  |
| Miscellaneous |  |  |  |
| Li-2, see text. L3, oscillator coil (Osmor PW/01) |  |  |  |
|  | 1 (Weyrad P51/1). | IFT2 | Weyrad P51/2). |
| (Weyrad P50/3V). T1, driver transformer (Osmor |  |  |  |
| QXD1). T2, output transformer 6-2:1 CT (Henrys |  |  |  |
| MOP). Switch S1a-b, rotary water switch, 2 pole |  |  |  |
| 6 way. Speaker $3 \frac{1}{3} \mathrm{in}$. $3 \Omega$. Universal chassis flanged |  |  |  |
| Handle. Veroboard, plain, $0.15 \mathrm{in} .5 \times 3 \mathrm{in}$. Coaxial |  |  |  |
|  |  |  |  |
| Battery PP9 and clips. | aerial socket. Output jacks ( 2,1 shorting type). |  |  |

The a.f. output jack socket is below this, and has contacts which open when the plug is inserted. It is connected as in Fig. 3, so that inserting a plug breaks the internal speaker circuit.

## CABINET

The receiver can be tested out of its case, by wiring the circuit board to VR1, VC1, and S1a-b, as in Fig. 3.

Close-up shot of the method of attaching the ferrite rod to paxolin brackets.


The leads MC from VR1 and VC1 go to tags bolted to the panel flanges.

The parts of the cabinet are quite easily prepared, and holes should of course be drilled before fitting the speaker or any other items.
Top and Bottom These are $7 \times$ 3in: flanged universal chassis members. Punch the top for VR1, Sla-b and VCl, and drill holes for the handle fixing bolts. Drill the front flanges for 6BA bolts or selftapping screws (to secure the front) and the back flanges for self-tapping screws. Cover the top with self-adhesive material of the required colour.

Sides Each side is 3 -ply, $6^{1}{ }_{8} \times 3^{5}{ }_{8}$ in., to allow overlapping the front and back, with a small projection at the top and front. The end flanges of the top and bottom are secured to the sides by two bolts in each position.

Front and Back These are 3-ply, each $7 \times 6$ in. Place the speaker to the bottom right, mark its fixing holes, and cut an aperture to match the speaker cone. Put the circuit board in place, and drill the two holes X-X in Fig. 3, through board and front, so that the board can later be fixed in this position.

Speaker Fitting Pass two countersunk headed 6 BA bolts through from the front, to hold the speaker and also the brackets for the ferrite rod supports. Use other bolts or small wood-screws for the remaining speaker fixing holes.

Circuit Board Two countersunk bolts are put through the holes which match with X-X, and held with nuts. Extra nuts are then put on, so that when the circuit board is on these bolts, a clear space of $3_{8}$ in. or so remains between it and the case front, to clear the wiring. Nuts at X-X then hold the board in place.

Finishing A piece of fabric about $8 \times 8 \mathrm{in}$. of the required colour has its top edge placed between the plywood front and the top flange. Temporarily fold this fabric over the knobs, so that the screws holding the front to the flange can be tightened. Also spread Bostik 1 or other adhesive along the top edge of the front. Screw the case bottom to the front. The fabric is then drawn taut over the whole front, and is folded over and fixed with adhesive at the case bottom, and front edges. The two sides are then fitted with bolts or screws.

## TUNING ADJUSTMENTS

The receiver is tested and tuned before fixing it in the case, as mentioned. If no signal generator is available, the i.f.t. cores are adjusted for best volume, any transmission being tuned in by means of a pair of trimmers. Once this has been done, the cores need no further adjustment.

When setting the trimmers for the wanted stations, deal with each pair of trimmers in turn, according to the position selected by the rotary switch. 'The position of the core of L3 has considerable influence on frequency, so needs to be left alone once a suitable setting has been located. VCl is half closed while adjusting the trimmers.

Pre-sets having a range of $7-60 \mathrm{pF}$ will cover about $1500-1000 \mathrm{kHz}$ in aerial and oscillator positions. For oscillator tuning, $20-250 \mathrm{pF}$ trimmers will cover the remainder of the m.w. band, with $50-450 \mathrm{pF}$ trimmers for aerial tuning. For 200 kHz , extra capacitance is necessary, up to about 450 pF for oscillator, and $2,000 \mathrm{pF}$ for aerial circuits.

# TRAMSMIITTER for 2 metres <br> <br> PART 2 <br> <br> PART 2 F.G.RAYER G30GR 

 F.G.RAYER G30GR}

## POWER SUPPLY/MODULATOR

This power-supply/modulator was made for use with the 2 -metre Transmitter described last month, for which it will provide all power requirements, and adequate modulation. It is only necessary to insert an octal plug from the transmitter into the modulator. The modulator is designed to have other uses, to increase its utility, as follows:-
(1) It will supply approximately 12 to 15 W of audio for one or more speakers.
(2) It will modulate a transmitter of up to about 25W d.c. input where the transmitter has its own power supply.
(3) It will supply power and modulation for a transmitter in the 10 W power range.
(4) The modulator can be switched off, leaving 300 V at 120 mA available for, say c.w. working.
(5) Optional choke input drops the supply to about 240 V for receiving equipment and similar uses.
An h.t. current meter is included to check working of the modulator and associated equipment, and an h.t. "ON" switch allows the modulator and a transmitter used with it to be switched on and off.

## CIRCUIT

The circuit is shown in Fig. 1. The first section of the double triode 12 AX 7 is an amplifier for the usual type of crystal microphone, with contact potential
bias from R1. Potentiometer VR1 is the audio gain or modulation level control. The triode 6C4 is a phase-splitter, driving the two 6 BW6's of the output stage, V3 and V4. This is a very straightforward and troublefree circuit.

The h.t. circuit is well smoothed, by C10, Cll and L1 while R16 is a safety bleeder resistor. Some modification to working conditions can easily be made, if better suited to other associated equipment.

HT Voltage. With the values given, the h.t. supply is 300 V when loaded to 120 mA . If R14 and R15 are each $270 \Omega$, the supply obtained is 280 V when loaded with 100 mA . A terminal board with pairs of small terminals is fitted under the chassis, so that the positive connection to C 11 can be interrupted. The power supply then works as a choke input circuit, giving a reduced supply of about 240 V at 120 mA .

Output Stage. Operating conditions with cathode bias provide about 9 watts of audio with 250 V , and about 12 watts with 285 V . For modulating a transmitter the audio output required is about half the d.c. input of the transmitter, say 7 to 8 watts, for a 15 watt d.c. input. If wished, it will be found that R12 can be considerably increased in value, to reduce the current taken by the 6BW6's, without loss of audio quality.

Modulated HT. This is derived from the h.t. line and secondary of T 1 , the fixed ratio transformer being intended for a p.a. load of about 3 to $8 \mathrm{k} \Omega$.


516

## Resistors

| Resistors |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | $2.2 \mathrm{M} \Omega+\mathrm{W} 10 \%$ | R9 | $47 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 5 \%$ |
| R2 | 270k $\Omega \frac{1}{2} \mathrm{~W} 10 \%$ | R10 | 220k $\Omega \frac{1}{2} W$ W |
| R3 | $270 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 10 \%$ | R11 | $220 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 5 \%$ |
| R4 | $1 \cdot 5 \mathrm{k} \Omega \frac{1}{2} W \mathrm{~W} 10 \%$ | R12 | 270』 2W 10\％ |
| R5 | $47 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 10 \%$ | R13 | $5 \cdot 6 \mathrm{k} \Omega 1 \mathrm{~W} 10 \%$ |
| R6 | $1 \mathrm{M} \Omega \frac{1}{4} \mathrm{~W} 10 \%$ | R14 | 120』 $2 \mathrm{~W} 10 \%$ |
| R7 | 1．5k $\Omega \frac{1}{2} W 10 \%$ | R15 | 120』 2W 10\％ |
| R8 | $47 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W} 5 \%$ | R16 | $220 \mathrm{k} \Omega 1 \mathrm{~W} 10 \%$ |

VR1 $500 \mathrm{k} \Omega$ log．potentiometer
Capacitors

| C1 | $8 \mu \mathrm{~F} 450 \mathrm{VW}$ | C7 | $0.01 \mu \mathrm{~F} 750 \mathrm{VW}$ |
| :---: | :---: | :---: | :---: |
| C2 | $0.01 \mu \mathrm{~F} 350 \mathrm{VW}$ | C8 | $0.01 \mu \mathrm{~F} 750 \mathrm{VW}$ |
| C3 | $0.01 \mu \mathrm{~F} 350 \mathrm{VW}$ | C9 | $16 \mu \mathrm{~F} 450 \mathrm{VW}$ |
| C4 | $0.01 \mu \mathrm{~F} 350 \mathrm{VW}$ | C10 | $32 \mu \mathrm{~F} 450 \mathrm{VW}$ |
| C5 | $0.01 \mu \mathrm{~F} 350 \mathrm{VW}$ | C11 | $8 \mu \mathrm{~F} 450 \mathrm{VW}$ |
| C6 | $50 \mu \mathrm{~F} 50 \mathrm{VW}$ |  |  |
| Valves |  |  |  |
| V1 | 12AT7 | V3 | 6BW6 |
| V2 | 6 C 4 | V4 | 6BW6 |

MISCELLANEOUS
Valveholders，B9A with skirt and screening can（1）， B9A plaln（2）B7G with skirt and screening can（1）． Meter M1， 150 mA ．Toggle switches（2）．Microphone socket．Octal valveholder，for power outlet．Mains neon indicator．Fuse， 250 mA and holder．D1／D2 sillcon rect／fiers， 1000 p．i．v． 1 A or better．Chassis $10 \times 7 \times 2 \mathrm{in}$ ．L1，about 10 H at 120 mA ．T1，modulation transformer Type 223 （Garex，Chinnor，Oxon）T2， mains transformer to provide $300-0-300 \mathrm{~V}$ at 120 mA ， 6.3 V at 2.5 A and 6.3 V 2 A twice（Douglas，Parmeko etc．）．

A multi－ratio transformer may be used for other load impedances．The transmitter d．c．input is VxI， for example， 300 V at 40 mA or 12 watts．So the transmitter p．a．modulating impedance is approxi－ mately $V / I$ or $300 / 0 \cdot 04=7 \cdot 5 \mathrm{k} \Omega$ ．（For the impedance calculation，remember to add the p．a．screen grid current to the p．a．anode current．）

Unmodulated HT．This is derived from the h．t． line，after the switch，to allow metering of the total h．t．drain，and control of h．t．to the transmitter． When using the 2 －metre transmitter described，more grid current that required was available，so h．t．to the


General view of the prototype chassis．


Underneath the chassis．Suggested layout of the major components should be followed．Otherwise component positioning is not particularly critical．
earlier stages was reduced to about 260 V by placing a $1 \mathrm{k} \Omega / 2 \mathrm{~W}$ resistor in series with pin 7 of the octal socket，Fig． 1.

## CONSTRUCTION

This is on a $10 \times 7 \times 2 \mathrm{in}$ ．＂universal chassis＂so that the front runner can be prepared for the meter， etc．，before it is fixed in position．Securing bolts for the mains transformer and modulation transformer also pass through the side and back flanges for addi－ tional strength and rigidity．
In the layout adopted，the microphone socket and VR1 are to the left，adjacent to the 12AX7 holder． Grid leads here are screened，and clear of heater wiring．The 6C4 is towards the centre，and the two 6BW6＇s in line towards the back，with the modula－ tion transformer to the left，and the mains trans－ former to the right．This leaves the front right of the chassis for the smoothing choke．The only live cir－ cuits above the chassis are leads to the choke，and these were covered with tape．
The front runner carries the following，left to right：－microphone socket，VR1，h．t．switch，meter， octal socket，AC＂ON＂neon indicator，AC switch， and outlet for the mains lead．Transmitters，speakers or other associated equipment employ octal plugs wired to match．

The small terminal board mentioned has two ter－ minals wired to the modulation transformer secondary，so that it can be shorted in a few moments with a wire link for c．w．when the same equipment is also used for a．m．If frequent changes are made from c．w．to a．m．in this way a switch can be placed across the secondary．

The modulator should never be used without a load connected to the modulation transformer．

## AERIALS

The output of the transmitter can be matched into any of the usual aerials requiring a low impedance feed．

A simple dipole will give good results over local

MOST intercomms use three wires or a complicated relay/switch system. The system described here uses only two wires and can be adapted to any amplifier already available providing it has both input and output transformers. The two wire cables connecting the units can be any cheap twin type. A bonus in this system is that only one Slave unit is necessary because by paralleling several pairs at a convenient junction point, communication can be had from any two points.

In the author's arrangement the Master unit is usually in the shack at the bottom of the garden but the Slave can be in the lounge (telephone) hall (door bell) and bedroom or kitchen. By moving the units and plugging in, communication can be had between any two locations. Another bonus is that the units consume current only when communication/calling is made.

## OPERATION

Figure 1 is the full schematic of the author's unit to enable the reader to follow the way in which the unit operates. With SW3 "OFF", when SW1 or SW2, which are spring loaded, are pressed it causes a loud bleep in the other unit's loudspeaker in the following manner. If the master wishes to call the remote unit, SWl is pressed, shorting contacts 5 and 6, thus completing the positive line through the primary of the input transformer/switch/speech coil of the loudspeaker to the common line. The amplifier is in operation and at the same time the current through the primary winding induces a low frequency note in the secondary which is amplified. Contacts 2 and 3 have been connected at the same time so that the Slave speaker is connected to the output of the amplifier so the resultant amplified audio note (generated in the input transformer) is heard in the Slave's speaker. Switch 3 is now operated to await the reply, if no response, put SW3 "OFF" and press SW1 again. Once contact is established, the Master controls all Speak/Listen operations and switches "OFF" SW3 ready for the next call. A similar operation takes place when the Slave wishes to call the Master. The $50, \mathrm{~F}$ electrolytic blocks what would otherwise be a direct d.c. connection but not the audio signal. It will become obvious that the Master
can monitor the Slave by simply switching "ON" SW3 and so act as a baby alarm, telephone/door bell warning.

Any pair of miniature $3 \Omega$ speakers can be used and the transformers are a pair of miniature transistor single ended output ( $3 \Omega$ ) types. The potentiometer VR1 is a preset skelton type, the required volume, once set, does not require further adjustment. As will be seen from Fig. 1, SW1 is a DP/DT type, SW2 is a SP/ST, and SW3 a simple ON/OFF type. Switches 1 and 2 are, of course, biased types (spring loaded); there are many varieties on the


Fig. 1: The circuit of the Master unit-see text for an explanation of the unusual calling system.
market, the most easily available is the toggle type; but the constructor has a choice.
As stated at the beginning, the main reason for offering yet another intercomm unit is the novel method of calling and the use of only two wires. This gives a versatile and flexible installation, well worth
the few hours needed to construct. It may interest the reader to know that this method of calling was developed as a result of a mistake made when making up a conventional system and to the best of the writer's knowledge has never been used before.

## 25W D.C. to A.C. INVERTER

THE inverter described here will operate 240 V 50 Hz appliances of up to 25 W consumption. It was originally built to drive an electric shaver or a 25 W soldering iron from a car battery.

The circuit is a simple resistance coupled inverter with a square wave output of 240 V 50 Hz .

Considering the circuit in Fig. 1, assume that Tr 1 starts to conduct; voltage induced in N1 rapidly drives Tr1 into saturation and biases Tr2 off. Flux increases in the transformer core until saturation is reached which results in a sudden rapid increase in curreat in Tr1. This current exceeds the current which $\operatorname{Tr} 1$ can supply with the available drive, $\operatorname{Tr} 1$, therefore, comes out of its saturated state. Voltage induced in N 1 falls to zero as the transformer core saturates and Tr1 is returned to the "off" state, this ends the first half cycle. Flux collapse in the transformer core results in an induced voltage in such a direction as to turn $\operatorname{Tr} 2$ on so initiating the start of the second half cycle.


## Performance

> No Load...... Input current $700 \mathrm{~mA}(8.4 \mathrm{~W})$ Load 15 WW Load 25 W .....Input current 2.0 A , efficiency $62.5 \%$ Lourrent 2.8 A , efficlency $75 \%$,


Fig. 2: Wiring of 25W inverter

## components list

|  |  |  |
| :--- | :--- | :--- |
| R1, R2 |  | $100 \Omega, 2 \mathrm{~W}$ |
| Tr1, Tr2 | OC35 |  |
| Fuse | 5 Amps |  |
| Transformer: | Type P2/2 available from Magtor |  |
| Limited, 68 Dale Street, Manchester 1. |  |  |

Construction is straightforward and operation is little affected by position of components. However, it is advisable to keep interconnections as short as possible to reduce inductance.

Since transistors Trl and Tr2 are not operating at maximum load, large heat-sinks are not necessary and the entire unit can be inserted in a metal case measuring only $\operatorname{3in} \times \operatorname{3in} \times 4$ in. Care must be taken to ensure that the collectors of both transistors are isolated from each other, this can most easily be done by mounting these in the side of the case on insulating washers, alternatively a plastic case can be used.

If a d.c. output is required, this can be easily obtained by connecting a bridge rectifier to the secondary, since the output is square wave, smoothing represents no problem and a capacitor of $2 \mu \mathrm{~F}$ will suffice for most requirements.

It is not recommended that half wave rectification be used as this will tend to saturate the transformer core in one polarity only and this may cause malfunction of the inverter.

## maxwell

by G8DSH




#  PART 11 

## A breather

Before we can progress with our look at transistor circuits, we must halt, survey the battlefield of some of our illusions, and reconnoitre the lines of our next advance.

In other words, having taken single stage circuitry and combinations of stages, we must now consider the effect of the sub-circuits on those before and those after. The more we delve into transistor circuitry, the less we can regard each "block" as an entity unto itself. Black boxes, so beloved of the academic, are seldom darker than a shade of mottled grey when we come to put them into practice.

One such circuit concept, that seems primarily to make hay of basic theory, is the so-called "virtual earth".
We have reached a stage in our talk about circuits where we can see, without the aid of equivalent transistor circuits or little arrows showing electron flow, that the d.c. conditions and the a.c. conditions in any given configuration will be different, though interdependent.

As an example, consider the plain problem of decoupling. In your humble transistor radio you have a perfect example. As you bothered your neighbours on the beach with Bach's Partita and Fugue while all they wanted was to be Woganised (how I've longed to do that!) the signal current in the power supply circuits were being bypassed from the battery by a relatively hefty electrolytic capacitor. Fig. 55 illustrates this, and shows that the h.t. line


Fig. 55: Simple decoupling. The capacitors represent a virtual shortclrcuit to signal currents.
is, as far as the a.c. signals are concerned, at the same potential as the chassis.

From there, it is a small step to think in terms of impedance and frequency rather than resistance and direct current when considering a signal-handling circuit.

Why, for instance, do we need that hefty capacitor back there, across the supply, when the decoupling of the tuner section is efficiently performed by a fraction of a microfarad? The answer lies in the frequency. At the supply, signal currents at audio frequencies are having to be bypassed, and $2000 \mu \mathrm{~F}$ to a 100 Hz signal is an impedance (a.c. resistance) of $0 \cdot 81 \mathrm{ohm}$.

At the front end, taking the FM radio that you, of course, will be using, despite the BBC's recent retrograde step to duplicate local radio on medium waves, the frequency you want to bypass is somewhere near a million times as great and so the capacitance need only be a millionth of the former, that is 2 picofarad against 2,000 microfarad, to have the same effect. Of course, to safeguard over a wider bandwidth, the actual value will be a couple of hundred picofarad,


Fig. 56: The original Baxandall tone control circuit, to suit an input of less than 10k』, for use with an SP61 valve.
but the comparison-and the point-remains. When considering circuits, you must consider the effect of the a.c. signals they will be handling as well as the d.c. conditions that provide basic biassing, etc.

## Virtual earths

Which brings us back to the concept of the virtual earth. Fig. 56 shows a simple circuit, again a practical one, and very familiar, that of the Baxandall tone control circuit, widely used in all sorts of constructions, and not always completely understood. If it serves no other purpose, it should remind us that Peter Baxandall dreamed this one up in 1952, based on an SP61 valve (or, in war surplus terms, a VR65).
The underlying reason for choosing such an example is (a) to make the opportunity of talking a bit more about feedback, (b) to introduce tone control circuitry, which will feature in our next constructional project and (c) to get over as well as we can, to satisfy a number of enquirers, the concept of the "virtual earth".

Feedback has featured already in our potted circuits, d.c. feedback to bring bias conditions to the operating state we require and a.c. feedback to regulate the signal flow through a stage, and, as we shall have to consider later, to make a stage nonlinear in an especially controlled way (as, for example, in designing an RIAA corrected magnetic pickup pre-amplifier).

The whole point about the Baxandall tone control circuit, first considered in a Wireless World article of October 1952, is that its action depends on negative feedback and that it requires an understanding of the virtual earth concept to grasp its principles of operation. Having once got hold of this, we can step forward briskly into the world of "closed-loop gain" and "variable feedback control", which scares so many students away from what is really quite elementary circuitry. Incidentally, the virtual earth concept preceded Baxandall by quite a few years and he was quick to give credit to Professor F. C. Williams for the coining of the term.

## Feedback

Enough waffling: Feedback is the principle of taking part of the output from a stage, or stages, and applying it to the input. If it is positive feedback, the signal you re-apply to the input is in phase, and thus aids the input, eventually driving the stage beyond its working limits. Control this positive feedback and you have a simple oscillator-the more output it delivers, the more it wants to deliver, until it blocks the stage off, things revert to normal, and away we go again.
But we are more concerned at this juncture with negative feedback. If you are audio-oriented (as you must have guessed by now that Mike and I are!) you will have read all manner of attributions for negative feedback. In the late Forties and early Fifties there were so many articles on negative feedback, interlaced with symbolic formulæ, that one would have imagined it could cure all amplifier ills from operator's twitch to the galloping parasitics!

In fact, the principle is simple: take off a portion of the output signal from a stage (or stages) and apply it to the signal in such a way as to oppose the input, i.e., in antiphase, and you have a method of


Fig. 57: (a) Negative feedback in series with the input signal. If R1= R2 the gain is unity. (b) a battery analogy, with no feedback. (c) with feedbach equal to the drive, voltage across $R$ is virtually zero.
exercising control that depends on the nature of the input-it is to some extent, and within certain limits, self-regulating.

When we take a brief recap. of some previous articles in this series, we shall also appreciate that negative feedback from the output to the input of an amplifier stage effectively changes the impedance as well as reducing the gain.

This is important, and I am not going to insult regular readers by going, chapter and verse, over our earlier chats about $R_{1 N}$ and $R_{i n}$, etc. But to summarise a few points, take a look at Fig. 57(a). Here we have an amplifying stage with a signal voltage applied and negative feedback in series with that input signal. (Again, this is important).

Let's assume, for easy figuring that the amplifier has an open-loop gain of 100 . That's to say, it would increase its applied signal 100 times if there was no extra circuitry to consider. Then, commonsense tells us that if the values of R1 and R2 are the same, the gain will be unity, not 100 times, because the feedback is in series with the input. To get the hang of this, we have to look at things in terms of the impedance that the signal "sees". Fig. 57(b) shows a battery driving a current through a resistor. The battery "sees" the impedance of the resistor. But what if, Fig. 57(c), we put another battery of the same sort in series with $R$ ? We haven't changed the value of $R$ but little or no current flows-so the effective impedance seen by the source voltage, the prime battery, is now high.

## Back to the amplifier

Let's now get back to our amplifier with its feedback and instead of applying the feedback in series as before, we shall apply it in parallel, Fig. 58(a). Again, $\mathrm{R} 1=\mathrm{R} 2$. But as the feedback is now in parallel with the input signal, we can see, applying the battery analogy, in Fig. 58(b) that it effectively shorts out the signal. In other words, adding V1 to V2 produces an effective zero.

Sorry about that repetitious word "effective", but if I say "this is zero", some pedant is going to hurl a wad of mathematical treatises at me to prove that Isaac Newton never went near the orchard, or something!

Go back to that mini-circuit of Fig. 58(a) and you can now see that the voltage at the junction $X$ of R1 and R2 is very low indeed. Not zero, for we have to take into account the voltage across the amplifier, and the best we can say is that the voltage at this junction, R1/R2, is very low, virtually at


Fig. 58: (a) Parallel feedback, point $X$ is virtual earth point. (b) battery analogy repeated. (c) choice of amplifier gain and resistors gives virtual impedance, dotted, between virtual earth point and true earth.
earth potential. Hence the term, virtual earth. From this, it follows that the input impedance of the circuit is low at this point.
Here, we have one of the bones of contention over which audio pundits have worried, and with which we shall not concern ourselves now-suffice to say, the source signal "sees" an impedance equal to R1 in parallel with whatever the virtual resistance $R_{r}$ in Fig. 58(c) may be, while the amplifier sees an impedance of about $R_{r}$. And the beauty of this arrangement is that by juggling with amplifier gain and feedback component values, we can make the input match our source exactly; for best signal energy transfer conditions, while making our amplifier "see" a. source resistance (impedance) that is just right for its job. In many audio applications, an impedance of around $600 \Omega$ would do us very nicely for' lowest noise conditions, and this case can be met quite easily.
The important factor to remember is that the imaginary resistor we produce by the virtual earth application is approximately equal to the value of R2 divided by the amplifier gain. Its value is not affected by R1. There is no need for R1 and R2 to be equal in all cases, although we have chosen this circumstance for ease of explanation-the performance depends on the ratio between resistor values.

## Back to Baxandall

So now back to Baxandall, and a circuit that originated from valved techniques.
This time we shall split the circuit into its "Lift" and "Cut" conditions first, showing the virtual earth points. Forget, at the moment, the tapped potentiometer of Fig. 56 and consider the treble lift circuit. This, shorn of all extraneous detail, could be redrawn as Fig. 59(a). If $V_{R}$ is made low enough so that the voltage at the slider when in the middle of its travel is not affected by the current supplied by $C$ (even at higher frequencies) then the total current flowing toward the virtual earth point, $X$, is $I_{1}+I_{2} . I_{1}$ is approximately equal to $V_{i n} / R_{i n}$ and $I_{2}$ depends on the value of capacitance. If we make $\mathrm{R}_{\mathrm{rb}}$ equal to $\mathrm{R}_{\mathrm{ta}}$, merely to simplify combination of lift and cut control, and call this simply $R$, then the output voltage has one component independent of frequency, for a constant value of $\mathrm{V}_{\mathrm{ta}}$ while the
other one, leading in phase by $90^{\circ}$ is both proportional to frequency and to $k$ which is the fraction of the potentiometer setting.

What this means, in practical terms, is that for any particular potentiometer setting the response of the cut circuit will be down by the same number of decibels as the lift circuit is up. As we.know from Baxandall tone controls published many times before, the curves are a mirror image of each other. This is one of the virtues of the control.

The tapped control is just a convenience and it can be seen that there is actually a small voltage between the centre point of the practical circuit (Fig. 56 ) and virtual earth, across the capacitor. But its value makes this voltage practically negligible.

A look at the combined bass control in its simplified layout of Fig. 59(c) may help to understand better the working of the tone control. To give level


Fig. 59 : Fundamental Baxandall treble lift circuit. (b) treble cut circult. (c) bass Iff and cut section of combined circuit.
response at mid-setting, Rl and Cl are the same as R2 and C2. At middle and high frequences the potentiometer, $\mathrm{V}_{\mathrm{R}}$ is almost shorted out by the low reactances of Cl and C 2 , so we are back to Fig. 58(a) with $\mathrm{R}_{\mathrm{in}}=\mathrm{R}_{\mathrm{tb}}$ and unity gain. As the frequency of the signal falls, the gain rises (or, if the potentiometer setting is changed, falls to the level determined by the response curve), and, just as with the treble circuit, the curves are mirror images.

The symmetrical beauty of the finished control, with components calculated to suit Baxandall's original case, the VR65 valve, a high-gain pentode, can be seen in Fig. 56. One of the interesting points about its chosen values is that the treble response will be up or down 3 dB at full lift or cut settings of the control when the reactance of C3 is numerically
equal to $\mathrm{Rl}+2 \mathrm{R} 3$. The values of Cl and C 2 must be equal, as are R1 and R2, for reasons already stated, and values are chosen to give the correct bass response.

## In practice

Coming to the present time, we can see an example of virtual earth circuitry used in the muchvaunted input stage of the Cambridge P40 amplifier, Fig. 60, where the aim was to get a high-gain, lownoise input amplifier, controlled so that the local feedback loop alters the gain, and thus provides a volume control right at the front of the circuit, in a low-signal level stage-just where we are told never to put it! The aim succeeded to some extent, because there was indeed a very low-noise result, and the overload capability, where most input amplifiers fall down badly, was a phenomenal 60 dB .


Fig. 60: Virtual earth input stage used in Cambridge P40 and P50 amplifiers.

But later versions of Cambridge amplifiers reverted to an uncontrolled input stage and put the virtual earth amplifier in the second stage, mainly because the original design gave a peculiar volume control "law". You see, the accepted use of a control is a 20 dB attenuation when the knob is half-way from maximum (or the slider half retarded). By putting a twin-gang $1 \mathrm{M} \Omega \log$ law potentiometer in the virtual earth feedback circuit, Cambridge limited the attenuation to between 3 and 6 dB for the same movement, with its action accelerating as it was turned farther down.

To get the range of input levels, the control had to be shunted with a $47 \mathrm{k} \Omega$ resistor, except in the Pickup 1 mode, so except in this mode, only about three-quarters of the control action was effective. Later versions use a $50 \mathrm{k} \Omega$ linear potentiometer to get the approximate log law (using the fixed resistor, $22 \mathrm{k} \Omega$, across part of it).

So we have now considered practical ways of using virtual earth circuitry, and can go on to the even more practical matter of building a circuit whose action may not seem quite so mysterious.


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DEVOTEES of this column will be highly delighted at the publicity currently being given
by the Post Office to the 50 th. anniversary of lighted at the publicity currently being given
by the Post Office to the 50th. anniversary of broadcasting in this country by issuing a set of three postage stamps to commemorate the event. Since we mentioned the subject in the last issue details of the stamps have been released by the Post Office and they are reproduced here.
The 3p stamp depicts six of the many types of microphones used in broadcasting since 1922. Observant old-timers will recognise the MarconiSykes electromagnetic microphone of 1924 as well as the Marconi-Reisz carbon microphone of 1926 among the collection. On the 5p stamp a typical domestic wooden horn loudspeaker of the 1920's is illustrated. Some readers may recall the S.G. Brown conical horn speaker and the Amplion horn of the same period.

No doubt there are many of these speakers still hidden away in attics and cupboards so let us hope that this invaluable publicity will cause the public at large to appreciate the value and significance of
these treasures from the early days of wireless and thus prevent their needless destruction.

The third stamp, for $7^{1} 2 \mathrm{p}$, brings us right up to date with a fine illustration of one of the latest colour TV cameras as used by both the BBC and the independent TV companies.

The fourth stamp, to be issued at the same time as the other three, is for $9 p$ and shows an early form of spark transmitter as used by Marconi in establishing wireless contact between Lavernock Point, Glamorgan, and Brean Down, Somerset, in May 1897. On the 75th. anniversary of this historic event the name of George Kemp is coupled with that of Marconi. Kemp was a Post Office engineer loaned to Marconi as a senior assistant. Their experiments resulted in the first successful tests over water and, incidentally, the first between two countries.

All four stamps are the work of David Gentleman who was also the designer of the Philympia series of stamps issued in 1970. The anniversary stamps described will be on sale on September 13th.


The $3 p$ stamp is printed in several shades of grey with black, brown and yellow while the 5 p stamp is grey, belge, red, brown, black and umber. The $7 \frac{1}{2} \rho$ stamp featuring the TV camera also has several shades of grey combined with black and red. The $9 p$ Marconi-Kemp commemoratlve issue combines light and blue grey with black, yellow and brown. A special first-day cover and two pictorial handstamps are being provided by the Post Office.

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# THE BROADCAST BANDS Malcolm Connah 

## Frequencies in kHz - Times in GMT

FOR a change this month I think it will be useful to all readers if we start with some news of DX stations around the world. The source of the information is Sweden Calling DXers and my own listening efforts.
BOLIVIA: The Bolivian station on 4845 is CP-72, Radio Fides de La Paz. This station is scheduled to broadcast from 1030 to 0330 GMT only but has been heard on an extended schedule. The station has also been heard in Europe on 4875 kHz .
CP-103, Radio 27 de Diciembre, listed on 3350 kHz is pres;ently operating on 3439 kHz with sign-off at 0215 GMT or later.

BRA.ZIL: The new European service from Radio Nacional de Brasilia has been noted on 15450 kHz with weak signals and splash from VOA, Monrovia, on $15 \not 445 \mathrm{kHz}$ at 2245 . The programme consists of Brazilian music and short talks in English, reports are requested.
MOINGOLIA: Radio Ulan Bator has introduced a Russian service which is on the air on Tuesdays at 1030 and on Fridays at 1040. These broadcasts have been heard on 7260 kHz , the station announces $41 \cdot 3$, 48 and 1321 metres.

PAFiAGUAY: ZPA-1, Radio Nacional, Asuncion can be occasionally logged on 4615 kHz with special sports newscasts in Spanish after 2200 hours.

SWEDEN: Due to heavy interference on 15105 kHz during: the broadcasts in English and Swedish to the Far East at 1230-1330, Radio Sweden has moved this transnission to 17815 kHz as from Thursday 22 nd June. Reports will be much appreciated. A change of frequency for South Asia at 1400-1530 is also being considered.
The first report this month comes from Mervyn Winters of Greenisland, Co. Antrim who used an AR88 with a 12 foot whip antenna to pull in several interesting stations including:

4930 Ecos del Torbes in Spanish at 2350
4995 R. Brazil Central, LA music at 2340.
6030 RSA, South Africa noted at 2355.
$61 \cdot 40$ RNE, Spain, English to NA at 0110.
9570 R. Australia noted at 0714.
11620 AIR, Delhi, India at 1930 .
11720 R. Nacional de Brazilia at 2307.
15018 R. Hanoi, N. Vietnam in English at 2015.
15190 R. Ankara, Turkey in English at 2200.
21570 R. Japan in English to Europe at 0800.
21605 R. Kuwait in Arabic at 0900.
Roger Hunter of Carmarthen has added a PR 30 preselector to his Codar CR-70A receiver enabling him to hear the following stations:

6025 R. Portugal in English at 2058
6080 R. Berlin International at 2145.
7235 R. Australia with Newsreel at 1000.
9009 Kol Istael, 'In the Jewish World' at 2115.

9640 TWR, Monte Carlo, DX programme at 0945.
11755 R. Finland in English at 1815.
15105 'R. Japan, news and comment at 2000.
17735 R. Free Europe, music at 1740.
21545 R. Ghana, talk in English at 1050.
21595 CBC, Canada in English at 1900.
Michael Berry of Dewsbury in Yorkshire has again used his outdoor vertical wire and Eddystone EB-35 receiver to good effect, hearing: -

3264 R.T.V. Congolaise noted at 1910.
4765 R.T.V. Congolaise in French at 2100.
4832 R. Capital, Costa Rica in Spanish at 0205.
4880 R. Once Sesenta, Peru in Spanish at 0335.
4940 R. Yaracuy, Venezuela, Spanish at 0135.
4965 R. Santa Fe, Colombia, Spanish at 0430.
4970 R. Rumbos, Venezuela, Spanish at 0435.
4980 Ecos del Torbes, Ven., Spanish at 0025.
5030 R. Reloj Continente, Ven., Spanish at 0310.
6255 Schulungssender, Austria, German at 1245.
11862 R. Lubumbashi, Zaire in French at 1655.
11865 R. Club Pernambuco, Brazil at 0330.
Nigel Knowlman of Cullompton in Devon has a Lafayette HA-600A and a 50 foot inverted $L$ anteinna, this combination enabled him to hear the following stations:-
11520 R. Bangladesh in English at 1745.
11720 R. Nacional de Brazilia in English at 0700.
11940 R. Bucharest, Romania, English at 1300.
11955 FEBA, Seychelles in English at 1730.
15170 Beirut, Lebanon in English at 1830.
15185 Voice of Nigeria, English at 0700.
17655 R. Cairo, U.A.R., English at 1800
17815 HCJB, Quito, Ecuador, English at 1945.
Next month the series of instructional articles for newcomers will continue with a discussion of the various types of aerials. This will include details of construction and the advantages and disadvantages of the various types.

Reports should arrive by the 15th of the month and be addressed to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex.

## OUR "CQ" COLUMN

If you wish to have a "CQ" request in Practical Wireless, we would be grateful if you could write it out in the same style we print it. This helps us to help you by saving time trying to take extracts from long letters and declphering names and addresses.


IT'S September already and the summer has almost gone. This is sad news for the sun bathers but good news of the l.f. enthusiasts. How about having a really good "go" at topband this year? Once the leaves turn and the darker evenings arrive you can be sure of hearing a few interesting tweets on 160 metres. Quite a number of European countries are active as are stations from further afield. You only need to monitor the bottom 50 kHz of the band (i.e. from 1800 kHz to 1850 kHz ) to hear quite a bit of topband d.x. The American stations are usually active at the very edge of the band and usually on c.w. Stewart, W1BB, is a good one to listen for and a few VO and VE stations have put in an appearance from time to time.

Czechoslovakia is a country well represented on 160 metres. Apparently, novice licences are awarded and OL stations are limited to 10 W on 160 and 2 metres. What a splendid idea. There was a time when the British Post Office exercised its wisdom and imposed a 10 W limit plus c.w.-only for the first year -Ah, happy days. Rumour has it that LU (Argentine) EL and ZS will be in evidence on 160 metres which should offer a challenge from sitting comfortably on 14 MHz and just letting the d.x. drop into ones lap.
Letter from Peter Martin (Nottingham) informs that KR6 stations are now signing KA6 and that 7P8AM is on from Lesotho-anyone heard him yet? He also mentions the RSGB news Bulletin Service. The latter is broadcast on Sundays on both eighty metres and two metres and is put out from various parts of the country, so you should have no problems in receiving all the latest information on Amateur radio, both for licensed operators and s.w.ls. Time depends on which area you're in. However, try listening on $3 \cdot 6 \mathrm{MHz}$ at 0930 for transmissions from Bromley in Kent.

Speaking of the RSGB, don't forget that many of its members put out special slow morse transmissions to help those trying to get up to the magic twelve words/minute. These stations are on from all over the country and at many different times. There is almost certainly somebody on in your localityusually on topband. The RSGB will give you all the information (you get this and many other things all the time if you become a member).

Alan Smith (Nelson) took "one of my rare trips down on to eighty metres". Reward was ZD8RR at 5 and 7 but Alan queries the authenticity of this station. Any offers? Gear in use is a JR310 and a twiddle on twenty revealed squirts of s.s.b. from;; CE3AIU, CO2FA, CX2AL, CX2BR, EL2GY, FC9VN, FM7WN, HClHV, HC1SS, HC2HM, HK3COC, HK6CBS, HV3SJ, LU3FAQ, LX1DV, OD5HD, PY2BCQ, PY4EP, PZ6AA, SL2ZZM, TI2FCD, TI8PE, TR8GD, VE1RB, VE2WY, VE3BYI, VE5AZ, VE7MT, VE7YF, VK2AVA, VK2BHR, VK3MO, VK4SD, VK5DK, VK6TW, VK7RX, V05GJ, VP1TB, VP2GB, VP2MZ, VP7NO, VP9HA, VQ9MC, VQ9R, VR1FL, VU2HLU, W8JXM, W9YRA, XE1D0, XE1EH, ZD3D,

# THE AMATEUR BANDS David Gibson, G3JDG 

## Frequencies in kHz - Times in GMT

ZD7SD, ZE1CS, ZE6JS, ZL1GY, ZL2FA, ZL4CO, ZM2TG, ZP5CF, 4X4NJ, 4X4VB, 8P6EK, 9J2DT, 9K2CA, 9K2CI, 9M2CP, 9M2CW, 9V1QJ. Antenna was a sneaky sixty foot end fed.
R. Dickens (Shepherds Bush) has a "modified" R1155 and a 20ft. aerial. He reports signals from many EU stations on 3.5 MHz but also includes a couple of goodies heard in the form of M1B and 6 W8DY. Best on 7 MHz was 4U1ITU.
G. Benson (G8FBL) tells gleefully of contacts made by special station GB3CRC run by the Chad Radio Club, Lichfield. Over 300 contacts were made including chats on 21 MHz with CT2BG, CX4CR, HC1RF, 7Q7BQ, 9H1DL, 9J2TB and 9Q5RA-no mention of mode. (Don't tell me, brightly coloured flags and it was a clear day!)
"I wonder how much of the inside is original", says an unsigned letter from Nicholas Dean of Loughborough. The antenna is a 20 metre bow tie (bet it suites you and, of course, you'll get d.x. in necks to no time) at 20 ft and fed into an a.t.u. It is then pressed into service on $3 \cdot 5 \mathrm{MHz}$. Signals received from; CE8AA, CN8BQ, CT1HE, CT2BG, PY2FYQ, ZB2A, ZL6MP, ZS1MH, 4X4UF, 7X0GF, 9Q5BJ.

Graham Armstrong (Jedburgh) reports hearing some good EU d.x. on topband; DL5XF, GI3GRD, GW3UPK. He reports a station on c.w. signing 2LO which will doubtless raise a smile. (LO LO, what's all this then?). Anyone else hear this character? Apparently he was on for at least a week.

David Lawley (Gravesend) sends in some interesting sigs heard on 160 metres. Among the c.w. offerings are; DL9KR, EI9J, EL2CB, GC3ZES/A, GM2HCZ, GW3UCB, OK1HBT, OL1AOH, OL1APC, OL5APO, PA0PN (on s.s.b.).
B. Spencelayh (Enfield) has got his version of the Deluxe $9 / 12$ receiver ( $P W$ April/May 1972) perking. First attempts on 21 MHz brought sigs from; EA3SA, HB9AJO, JA4BLY, OD5LX, VQ9MC, WA1JTT, W9YFV, 4X4HK, 4Z4MO, 5H3JL, 9J2SS, 9M2DQ.

Happenings for September include the Harlow Mobile Rally on September 24 at Magdalen Laver, near Harlow. Contests in my little black book inculude: September 9-10, WAE phone contest; 10, $3 \cdot 5 \mathrm{MHz}$ field day; 17, final d.f. round at Oxford.

## ELECTRONICA 72

Electronica 72, recognised by many as the most important trade fair in the electronics industry, will take place this year at Munich, Germany, from November 23-29. Included in the exhibits will be components and assemblies, production facilities, testing apparatus, information and training. Running at the same time as the exhibition will be the conference Mikroelektronic consisting of some 40 lectures.

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## PART TWO

## Trigger tubes

TThe discharge between the anode and cathode in a gas-filled tube can be started in ways other than that of raising the voltage to striking voltage. One of these ways is to use a trigger electrode to generate ions which will then carry the current of the main discharge. The trigger electrode is a pointed wire very close to the unheated cathode and pointed to the cathode surface. Because of the close spacing, it is easy to start ionisation with a small voltage applied between trigger and cathode, as the creation of ions is dependent on field strength (volts per metre spacing).

In addition to this effect, ions are discharged at high speed from a pointed wire due to the particularly high field strength around points. The old electrostatic experiment of blowing out a candle with a point discharge from an electrostatic generator is an illustration of this effect (Fig. 9). With the voltage between anode and cathode less than the striking voltage but above the running voltage, current will start to flow only when the discharge is triggered by the injection of ions from the trigger circuit. This is achieved by applying a small positive pulse at the trigger electrode. The amplitude and width of this trigger pulse must be above certain critical values (depending on the shape and spacing of the electrodes) to start the main discharge. Once the main
discharge has started, it cannot be stopped by any voltage applied to the trigger electrode, only by dropping the anode-to-cathode voltage below a level called the "sustaining voltage." Fig. 10 shows the characteristics of a typical trigger tube, the HIVAC XC23.

## Applications

Figure 11 shows a trigger tube used as a pulse amplifier. The trigger pulse causes current to flow,


Fig. 9: The high concentration of electric charge around a point causes Jonisation of the alr. The movement of lons of the same slgn away from the point creates a wind capabie of blowing out a candle.


Fig. 10: Characteristics of the Hivac XC23. With bias at OV, pulse amplitude for transfer equals $91-98 \mathrm{~V}$; with bias of +80 V , pulse required Is 20 V min.; trigger resistance equals $47 \mathrm{k} \Omega$. Deionisation time is 2 mS (time for which $V a=0$ to switch off tube).
so that a negative voltage pulse is generated in the anode load resistor and a positive pulse in the cathode load resistor. The voltage drop can be designed to be sufficient to cause the tube to extinguish at the peak of the pulse, so that the tube is ready to fire again at the next trigger pulse. The repetition rate which can be used is limited by the time which must be allowed for all the ions created in the first discharge to recombine before the full voltage is again applied between anode and cathode. For this reason, trigger tube circuits working at rates greater than 4 kHz are seldom found, and the circuits are notable for the use of capacitors to spread pulse widths out rather than to sharpen them, as is usually the case.

Figure 12 shows a ring counter circuit using gas trigger tubes. This type of counter circuit is not so familiar to constructors as the binary counters used in transistor circuits, and a description of its opera-


Fig. 11: If the negative pulse is not needed, a capacilor can be connected from anode to earth. The discharge of this will then provide the cathode pulse and the anode load can be ralsed so that the anode recovers slowiy and the tube has ample time to switch off.

Fig. 12 (right): Ring counter circuil working at 500 Hz .

tion might be of interest. The basic principle of any ring counter is that a set of bistable elements is connected in a closed ring in such a way that each trigger pulse fed to a common point turns on the element next to the one previously on, and also turns off that previous element. In the circuit of Fig. 12, imagine that V2 is passing current and that the rest of the tubes are not. Because of the current in V2, there will be a voltage positive to earth developed across the resistor in the cathode lead of V2, and this voltage will bias the trigger electrode of V3 (not shown, but wired in exactly the same way as V2) positive, not enough to fire the tube but enough to make certain that a trigger pulse of about 50 V will fire V3. This value of trigger pulse is not sufficient to fire any tube whose trigger electrode is not raised in voltage already, so when a pulse is received at the common input terminal and applied to all the trigger electrodes, V3 is the only tube to fire. When V3 fires, however, the voltage in the common anode line drops, and this drop of voltage is sufficient to extinguish the discharge in V2. The result is that the discharge has moved one tube on with the receipt of one trigger pulse. This action continues from tube to tube as each pulse is received, until the last tube in the set, Vn , is glowing. In a ring-of-ten counter, this would be the tube indicating number nine, and wired to the number nine indicator of a display. This tube is connected to a transfer tube, Vt , and when the next trigger pulse is received, Vt will fire, causing a positive pulse to appear at its cathode load resistor. Vt will extinguish immediately after, however, as the value of its anode load is far too high to permit a continuous discharge, and the current which does flow is due to the capacitor between anode and earth discharging through the tube. The positive pulse at the cathode switches on V1, which has a positive bias on its trigger electrode already, and is also the zero indicator. The same positive pulse is also used as the output pulse of the counter stage, carrying to the next counting ring or to some other output.

## Counting tubes

The action of a trigger tube, in which the trigger


FIg. 13: On the left is shown the princlple of construction of a Dekatron; the symbol of the Dekatron GC10B is shown right).
electrode starts off a discharge path which can then spread to the nearest anode, can be used in a tube in which the discharge is passed from one cathode to another, and which also makes use of the fact that the glow in a gas discharge is concentrated at the cathode. The best-known example of this technique is the well-known DEKATRON counting tube in which a central anode rod is surrounded by ten cathode rods (see Fig. 13). The structure of different types of Dekatrons differs in detail, but the type GC10B can be taken as an example of the way in which these fascinating tubes work. In the GC10B, the cathode pin which is used to indicate zero is taken to a base connection ( $\mathrm{k}_{0}$ ), and all the other cathodes are connected together and taken to another base connection, $\mathrm{k}_{\mathrm{c}}$. At the opposite end, the pins are visible through the glass end of the tube, and the glow round any particular cathode can be clearly seen. Escutcheon plates with the numbers $0-9$ can be fitted against the end of the tube and lined up so that the zero of the escutcheon is adjacent to the zero pin of the tube, and the other numbers line up with successive cathodes.

To transfer the discharge from one electrode to another, guide electrodes are used. These are pins located in pairs between the cathodes; all the first pins of each pair in clockwise order are connected together and taken to base connection $G_{1}$, and the second pins of each pair are brought together to the $\mathrm{G}_{2}$ base connection.

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The action is as follows (Fig. 14): with about 475V applied to the anode through an $820 \mathrm{k} \Omega$ resistor, and other details as shown in Fig. 14, a discharge must exist between the anode and one cathode. Since all the cathodes are joined together, and since the running voltage of a gas discharge is well below the striking voltage, once one cathode has started a discharge it cannot spread to any other cathode except by the action of the guides which will be described, unless one cathode is made more negative than any other. The only cathode with which this can be done is the zero cathode which is taken to a separate pin, so that the Dekatron can be made to read zero when power is first applied, or when a fresh count is wanted.
If now all the first guides ( $\mathrm{G}_{1}$ ) are pulsed negative, the glow will shift from the cathode to the nearest guide 1 and stay there. If the second guides are now pulsed negative just as the first guides are rising again in voltage, the discharge will shift to the nearest $\mathrm{G}_{2}$, which will again be one step clockwise. When this guide's voltage rises again, the glow transfers to the next cathode, which is one cathode on from the starting point. The result is that every time a set of pulses is applied to the guides, the glow shifts clockwise from one cathode to the next, and so counting has been achieved. This process continues until the glow lands on the zero cathode, which is taken to the -20 V line through a $150 \mathrm{k} \Omega$ load resistor, so that a positive pulse is obtained across the resistor whenever the glow lands on zero. This can be used to transfer the count to the next stage, as the positive pulse can be inverted by a valve or trigger tube and processed to provide the double pulse needed for the next stage.
The Dekatron system is at present the most economical method of counting and displaying, since both operations are achieved in one tube. It is, however, essential that the circuits published by HIVAC should be adhered to exactly. Any variation in the pulse width and amplitude, or in the time lag between the pulses applied to guides 1 and 2 can cause misfiring, and most of the problems ancountered in Dekatron circuits are easily cured by attention to the pulse system. Fig. 14 shows the circuits which should be used for driving with single pulses, double pulses and sine waves respectively. The sine wave circuit is of particular interest, as the 50 Hz mains provide an accurate frequency standard for digital clocks, the design of which is particularly easy using Dekatrons.

Not every count is to ten, however, particularly in the case of digital clocks, and the Dekatron Selector tubes such as the type GS10C are designed with this in mind. Each cathode is taken to a separate pin on the 12 -pin base, with the anode as a centre pin, and can be wired as a counter or as a transfer cathode. A transfer cathode is one which passes the count as a pulse to the next stage, and also acts as the zero to which some other cathode will reset. This enables us to have any count up to nine followed by a zero, and the range has been extended by tubes which count to 12. Another advantage of the selector type of tube is that it no longer ties us to the Dekatron type of display, but enables us to display on a Digitron type of tube, described later.

The standard range of Dekatrons includes counters and selectors working at rates up to 4 kHz , but another range or Dekatrons using a third set of guides connected to the reset line through a $220 \mathrm{k} \Omega$ resistor, and an output cathode guide connected to


Fig. 14a: Integrated pulse drive. The value of $C$ depends on the pulse width and repetion rate being used.


Fig. 14b: Double puise drive for the GC10B.


Fig. 14c: Sine-wave circuit (left)
Frequency $50 \mathrm{~Hz} \quad 100 \mathrm{~Hz} \quad 200 \mathrm{~Hz} \quad 500 \mathrm{~Hz} \quad 1 \mathrm{kHz} \quad 2 \mathrm{kHz} \quad 4 \mathrm{kHz}$

| $C 1(\mu F)$ | 1.5 | 0.82 | 0.33 | 0.15 | 0.082 | 0.033 | 0.015 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $C 2(\mu F)$ | 0.1 | 0.05 | 0.02 | 0.01 | 0.005 | 0.002 | $6800 F$ |

Reset circuit is shown on right. To reset, S1 is opened, taking cathode Kc and guides to +120 V and so transferring the glow to Ko.
the output cathode by a $220 \mathrm{k} \Omega$ resistor, can be operated at speeds up to 20 kHz .

## Alpha-numerical indicators

As we have seen earlier, when a voltage is applied between the anode and the cathode of a gas-filled tube, a glow appears round the cathode. When a.c. is applied, of course, both electrodes are seen to glow.


A typical gas filled read-out tube. When a voltage is applied between the anode and cathode a glow appears around the cathode. By making the cathode in the shape of numbers or letters, it will glow when the voltage is sufficiently negative to cause str/king.

The glow is due to the recombination of ions which have been formed by collisions and is most noticeable at the cathode because this is the place where electrons are being rapidly accelerated in the face of negative ions moving in the opposite direction. The glow exactly surrounds the shape of the cathode, and does not extend to more positive electrodes.

If the cathode is made in the shape of a letter or a number, this figure or number will be seen as a glowing shape whenever the cathode is sufficiently negative to the anode to strike and run. If a number of separately connected wires are shaped in the form of numbers $0-9$, each number will display only when the wire forming it is sufficiently negative to the anode to form a gas discharge.

The Hivac Numicators are tubes of this type, and the range of types is large. Tubes may be viewed end-on or side-on according to the type of construction of the tube. Numicators can be driven from Dekatrons, provided that trigger tubes or other invertor stages are used to change the positive pulses at the cathodes of the Dekatron to the negative pulses used at the cathodes of the Numicator. Perhaps "pulse" is a misleading word in this application, because the top of the pulse will be as long in the time sense as the figure is to be displayed.

Most Numicators are designed for steady operation, but some are intended to be used in what is called the "anode stroking technique," often used in connection with digital counters.

Digital counters can readily be arranged to give a readout whenever a clock pulse is received, and the readout can be converted to decimal form and used to drive Numicators. Considerable economy in circuitry can be arranged if the decimal readout is attached to all the Numicator cathodes; for example, in a five figure readout, there would be one decimal converter with the zero output connected to all the five Numicator zeros, the "one" output to all the Numicator "ones", the "two" to all the "twos" etc. The decimal output and the tubes are then switched in sequence, so that the units tube has its anode volts pulsed just as the decimal output gives the unit figure pulse to all the Numicator cathodes, with the result that only the units tube displays a figure. On the next pulse, the tens tube is activated to display
the decimal output from another store, so that each tube flashes a digit in sequence. Because of the clock pulse rate used, the display looks continuous. This is not a technique which would be used in small counters, but it is extremely useful in small computers, particularly in conjunction with integrated circuit counters.

## Thyratrons

Thyratrons are the big brothers of trigger tubes. Like trigger tubes, they are made to conduct by the application of a positive pulse to a third electrode; unlike trigger tubes, they use hot cathodes and can operate at very high voltages indeed-one type listed by English Electric quotes a peak forward voltage of 120 kV and with large currents, up to several thousand amps, flowing. Small thyratrons are made in glass envelopes and resemble output valves at first sight, the larger types have ceramic casings.

The small type of Thyratron has a heated cathode, a grid similar to the control grid of an output valve, and an anode which is often finned and connected to a thick pin set in the glass bulb for maximum heat dissipation. In operation, the heaters must be switched on before high voltage is applied, this is usually done automatically by means of a thermal delay circuit, since failure to observe the correct delay period would be fatal to the thyratron. When the heaters have reached full temperature, the grid voltage can be applied, this is a negative bias sufficient to prevent any electrons passing the grid, enough, in fact, to prevent electrons from being emitted to any noticeable extent from the cathode. The positive anode voltage can then be applied.

If the grid is now pulsed positive, the tube conducts strongly due to the ionisation of the gas by the electrons from the cathode, and this current will continue until the voltage at the anode is reduced to a low value. After a short "recovery time", the tube can be fired again if the anode voltage has also recovered to its previous value. What makes the thyratron unique is its ability to switch very high currents very rapidly and at a high forward voltage. By very rapidly, we mean delay times of around 20 120 nanoseconds in the most advanced types.

Thyratrons are used to control spot welders, to pulse radar transmitter magnetrons, and to operate other short time, high energy devices such as the Kerr Cell used in high speed photography. They also find extensive use in large invertors (converting a.c. to d.c.) such as are used at each end of the crosschannel d.c. cable. One intriguing use is as "electronic crowbars". In modern electronic equipment, protection against faults by means of fuses is not very effective because of the time which a fuse needs to blow. Even if this time is measured in milliseconds, much damage can be done, and the idea of the electronic crowbar is a device which will come into operation much more quickly than a fuse, shorting out the voltage across the circuits and taking the current which will eventually blow the fuse. This use demands a device which can be switched into conduction very quickly and which will take a large current in the time before a fuse blows--the Thyratron is ideal, though for the smaller sizes thyristors are taking over.

The Author gratefully wishes to acknowledge the help of HIVAC LTD. in the preparation of this article.

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Number 33

## Motorola MFC6040 Electronic Attenuator

ACOUSTIC feedback--that deafening howl which occurs when a microphone picks up the sound from the loudspeakers of a public address system and thereby completes a feedback loop, setting the whole system into oscillation-will be familiar to readers. It is particularly embarrassing when, for example, an announcer is using a microphone with a considerable length of cable, and by moving to a new location initiates this response from a previously well-behaved system. It would therefore be convenient if, in addition to his microphone, the announcer could have to hand the gain control of the amplifier, so that it could be adjusted for best results from his own position, without having an assistant constantly at the amplifier controls.
However, it is not a practical proposition to remove the volume control of the amplifier to the end of a long cable for such remote operation. There would be a considerable increase in the noise level of the system, despite the best efforts to screen the cable; there is also the consideration that the audio signal may have been amplified prior to the volume control, and at the higher level, may itself produce some feedback effects due to the stray capacitance of the cable.

It may be suggested that a volume control could be incorporated in the microphone case, to control the signal level before it is applied to the amplifier; however, the microphone may not be the sole signal source. It is common practice to use several inputs to a public address system, with part of the preamplifier stages acting as an audio mixer, so it would be desirable for the remote unit to control the gain of the "mixed' signal, rather than just that of the microphone channel.

What is required, therefore, is a method of remote control of amplifier gain which does not involve long signal-carrying cables, is therefore impervious to noise and does not introduce feedback or degrade signal quality. It is just this requirement which is satisfied by the new Motorola Electronic Attenuator integrated circuit, type MFC6040.

## Operation

In operation, the device is inserted in series with the master gain control of the mixer section of the preamplifier, and, depending on the setting of a remote potentiometer, attenuates the signal applied to its input terminal. Only a d.c. potential appears on the leads to the remote potentiometer; capacitative
effects are therefore irrelevant. The leads may be of any desired length and need not be screened. All the difficulties visualised above are therefore avoided.

## Practicalities

It is possible to obtain microphone cable in which two conductors are incorporated within the braiding. One of these may then be used in the conventional fashion, applying the microphone signal between it and the screening. The other can then be used for the remote control potentiometer, with the screening as an earth return. There is no question of capacitative crosstalk as the control connection is decoupled at the i.c. by a $50 \mu \mathrm{~F}$ capacitor.


Wiring for an amplifier remote gain control system using the Motorola MFC6040 integrated circuit.

The circuit indicates the connections and components required for the provision of the remote control facility outlined. A beginner should find little difficulty in assembling it on a piece of veroboard, and it can easily be accommodated close to the master gain control inside even the most compact amplifier. A d.c. supply of 20 V max. is required to
operate the i.c.; this is commonly available in modern transistor amplifiers and for mobile operation the 12 V car battery supply is adequate. The i.c. itself is presented in a miniature 6-pin epoxy package with pin 1 indexed.

## Alternatives

Alternative applications will be evident to the experimenter. The unit can clearly be employed as an audio automatic gain control by rectifying part of the output of the unit and applying it to pin 2 as a control voltage. Similarly, feedback systems can be designed which produce a control voltage dependent on signal frequency, for pre-emphasis or deemphasis operations, or to investigate Dolby effects. A suitable low-frequency signal applied to pin 2 could be used for tremolo. It is clear, then, that the field for experiment with the MFC6040 is extremely wide, and we are likely to hear much more of it.

## TELEVISION

## OCTOBER ISSUE

## COLOUR TV DELAY LINES

Why are delay lines necessary in a colour receiver, what do they do and how do they do it? We have not previously taken a close look at this aspect of colour television but we shall be doing so this month, in particular to see how the PAL delay line acts as a comb filter to separate the $U$ and $V$ components of the transmitted chrominance signal.

## RECEIVER-MONITOR

A simple conversion of a domestic receiver to act as a monitor, not only to accept CCTV signals-from a camera or videotape recorder-but also to provide demodulated off-air signals to drive other monitors, for mixing in a CCTV studio or to feed to a videotape recorder.

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## SERVICING TV RECEIVERS

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## COLOUR RECEIVER PROJECT

Details this month of cabinet construction.

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2 METRE TX -continued from page 517


Fig. 2 : Construction of a simple half wave dipole for 2 metres.
ranges. One can easily be made, using ${ }^{1} 4 \mathrm{in}$. aluminium tubing, as shown in Fig. 2, the elements being bolted to a piece of insulating material. A more weatherproof aerial can be made on the same lines, but using a closed box as fitted to TV and similar aerials. This aerial is easily raised on a light mast or post, with the co-axial feeder running down to the transmitter.

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笑む ${ }_{2}^{2 N 23694}$ 2 N 2647
2 N 2711
 2N2904A 2N2904A
2N2905
2N2905A 2N2906 2N2906A 2N2907 2N2907A
2N2913 $\begin{array}{lllllll}\text { 2N2923 } & 0.12 & 2 N 4929 & 2 \text { 2．83 } 4930 & \text { AF109R } & 0.35 \\ \text { 2．AF114 } & 0.25 \\ \text { 2N15 } & 0.25\end{array}$
Post Packin 13 per AF304 2N4931 $\begin{array}{ll} & 2 \mathrm{~N} \\ 0.12 & 2 \mathrm{~N} \\ 0.12 & 2 \mathrm{~N} \\ \end{array}$

| 8.70 | AF116 | 0.25 | BC307 | 0.09 | BF271 | 0.21 |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.09 | AF117 | 0.20 | BC307A | 0.09 | BF272 | 0.68 |  |  |
| 0.82 | AF118 | 0.50 | BC307VI | 0.09 | BF273 | 0.25 |  | 1－24 |
| 0.28 | AF121 | 0.28 | BC308 | 0.08 | BF274 | 0.28 |  | ${ }^{2} 8$ |
| 0.82 | AF124 | 0.24 | BC． 08 A | 0.08 | BF457 | 0－46 | SN7400 | 0.80 |
| 0.48 | AF125 | 0.20 | BC308B | 0.08 | BF458 | 0.57 | SN7401 | 0.20 |
| 0.82 | AF126 | 0.20 | BC309 | 0.09 | BF459 | 0.57 | SN7402 | 0.80 |
| 0.98 | AF127 | 0.20 | BC309A | 0.09 | BFS21 | $2 \cdot 10$ | SN7403 | 0.80 |
| 1.24 | AF139 | 0.88 | BC309B | 0.09 | BF821A | $2 \cdot 80$ | 8N7404 | 0.82 |
| 1.01 | AF170 | 0.25 | BC313 | 0.30 | BFS28 | 0.92 | 8N7405 | 0.28 |
| 1.10 | AF172 | 0.25 | BC327 | 0.21 | BF861 | 0.27 | gN7406 | 0－58 |
| 1.46 | AF178 | 0.65 | BC328 | 0.19 | BF898 | 0.80 | GN7407 | 0.56 |
| 0.48 | AF179 | 0.65 | BC337 | 0.17 | BFW 10 | 0.61 | 8N7408 | 0.22 |
| 0.85 | AF180 | 0.50 | BC338 | 0.17 | BFW 11 | 0.61 | gN7409 | 0.82 |
| 0.88 | AF186 | $0 \% 0$ | BCY30 | 0.35 | BFW 15 | 0.85 | GN7410 | 0.20 |
| 0.88 | A F200 | 0.35 | BCY31 | 0.40 | BFX13 | 0.88 | GN7411 | 0.22 |
| 0.68 | A F239 | 0.86 | BCY32 | 0.60 | BFX 29 | 0.25 | 8N7412 | 0.48 |
| 1.87 | AF240 | 0.68 | BCY32 | 0.50 | BFX30 | 0.25 | SN7413 | 0.35 |
| 1.86 | AF279 | 0.47 | BCY33 | 0.30 | BFX 37 | 0.38 | SN7416 | 0.45 |
| 0.76 | AF280 | 0.47 | BCY 34 | 0.85 | BFX44 | 0.88 | GN7417 | 0.45 |
| $0 \cdot 69$ | AFY 42 | $0 \cdot 65$ | BCY38 | 0.40 | BFX63 | 2.48 | gN7420 | 0.20 |
| 0.54 | AF211 | 0.55 | BCY39 | 0.80 | BFX68 | 0.80 | GN7421 | 0.28 |
| 0.64 | AL102 | 0.75 | BCY40 | 0.50 | BFX 84 | 0.24 | 6N7422 | 0.48 |
| 0.79 | AL103 | 0.70 | BCY42 | 0.15 | BFX85 | 0.29 | 8N7423 | 0.62 |
| 0.74 | ASY26 | 0.25 | BCY 43 | 0.15 | BFX86 | 0.24 | 8N7425 | 0.48 |
| 0.74 | A8Y27 | 0.80 | BCY58 | 0.18 | BFX87 | 0.27 | EN7428 | 0.32 |
| 1.00 | ASY28 | 0.26 | BCYE9 | 0.18 | BFX88 | 0.25 | 8N7427 | 0.48 |
| 1.80 | A8Y29 | 0.80 | BCY 66 | 0.88 | BFX89 | 0.45 |  |  |
| 2.07 | A8Y50 | 0.20 | BCY 67 | 0.82 | BFY 10 | 0.85 |  |  |

TTL．LOGIC I．C．NEW PRICES






1－24 25

## SUB－MIN ELECTROLYTIC

Axial lead $\begin{array}{rr}1-24 & 2 p \\ 0.20 & 0.18 \\ 0.38 & 0.84 \\ 0.86 & 0.81 \\ 0.45 & 0.89 \\ 0.45 & 0.39 \\ 0.60 & 0.55 \\ 0.47 & 0.48 \\ 0.70 & 0.65 \\ 1.45 & 1.27 \\ 1.26 & 1.00 \\ 1.30 & 1.05 \\ 1.10 & 1.00 \\ 2.50 & 8.30 \\ 0.45 & 0.40 \\ 12.40 & 11.80 \\ 4.97 & 4.40 \\ 0.80 & 0.75 \\ 1.20 & 1.00 \\ 0.80 & 0.75 \\ 0.80 & 0.75 \\ 0.85 & 0.79 \\ 0.85 & 0.79 \\ 1.00 & 0.90 \\ \end{array}$

Values：$(\mu \mathrm{F} / \mathrm{V})$－ $6.64 / 64$ ： $1 / 40$ ．1．6／05： $2.5 / 16$ ． $0.2 / 63$ ． 4.716 6p oach $6.4 / 6 \cdot 4 ; 6 \cdot 4 / 25 ; 10 / 16 ; 10 / 25 ; 10 / 64 ; 12 \cdot 5 / 25 ; 16 / 40 ; 20 / 16 ; 20 / 64,35 / 25$ ； $25 / 25 ; 32 / 10 ; 32 / 40 ; 40 / 16 ; 50 / 6 \cdot 4 ; 50 / 25 ; 50 / 40 ; 64 / 10 ; 80 / 16 ; 80 / 25 ;$ 100／6－4；125／10；125／16； $200 / 10$

| SILICON RECTIFIERS |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PIV | 50 | 100 | 200 | 400 | 600 | 800 | 1000 | 1200 |
| 1 A | 8p | 9p | 10 p | 11p | 19p | 150 | 20p | － |
| 3A | 150 | 17p | 20p | 881 p | 259 | 970 | 800 | 85 p |
| 6A |  | － | 25p | 80 p | 32tp | 85 |  |  |
| 10A | 80p | 35p | 400 | 47p | 589 | 66p | 75p | － |
| 15A | 86 p | 46p | 48p | 55 p | 65 p | 750 | 87 p |  |
| 35A | 70 p | 809 | 000 | 81．00 | $81 \cdot 40$ | \＄1．70 | 42－75 | － |
| 1 amp and 3 | 3 mmp | e pla | ence | ulation |  |  |  |  |


| IN34A | 10p |
| :---: | :---: |
| IN914 | 7p |
| IN916 | 7p |
| IN4007 | 20 p |
| I844 | 7D |
| 19113 | 15p |
| 18120 | 18p |
| 19121 | 14p |
| I8130 | 8p |
| 18131 | 10p |
| 18132 | 12p |
| J8920 | 7 p |
| 18922 | 8 p |
| IS923 | 12p |
| 18940 | 8 D |

## OPTOEFECTRONICS

MINITRON 3015F 7－8EGMENT INDICATOR（ 16 PIN DIL） $82 \cdot 00$ | May be driren by SN7447 |
| :---: |
| GNP．7AH COLD CATHODF | TUBE SIDE VIEWING． 0.9 and TWO DECIMAL POINTB．Mas be driven by gN744］AN．769

TIL 209 LIGHT EMITTING MODE．Made by TEXAS INST， （Red）． 85 p
B9900 PHOTORESTSTOR 88p

## VEROBOARD

|  | 0.15 | 0.1 |
| :---: | :---: | :---: |
|  | Matrix | Matrix |
| $27 \times 34 \mathrm{n}$ | 17p | 28p |
| $24 \times 8 \mathrm{~m}$ | 25 p | 25p |
| 3t $\times$ 3in | 250 | 25p |
| $31 \times 81 n$ | 80 p | 29p |
| $5 \times 17 \mathrm{in}$（Plain） | 82p |  |
| Vero Pins（Rag o | 36） 20 p |  |
| Vero Cutter 45p |  |  |
| Pin insertion $T$ matrix）at 50p． | ools（•1 | and $\cdot 15$ |

＂SCORPIO＂CAP
DISCHARGE IGNITION
SYSTEM
（As published in P．E．Nov．
＂7I）．Complete kit $£ 10 \cdot 00$
P．\＆P．50p．

## RESISTORS

$\begin{array}{ll}\text { Carbon Film } & \\ \text { \＄watt } 5 \%, 1 p . & \text {＋W，1W \＆} 2 \mathrm{~W} \\ \text { t watt } 5 \%, 1 p \\ \text { Ei2 Series }\end{array}$



| BAX 16 | 121p | F8973／4 | $221 p$ |
| :---: | :---: | :---: | :---: |
| BAY18 | 1710 | OAS | 17p |
| BAY31 | 7 P | OA10 | 20y |
| BAYF8 | 250 | 0 A9 | 10p |
| BY100 | 15p | 0447 | 8p |
| BY103 | 22p | 0.470 | 78 |
| BY122 | 47t | OA73 | 10 p |
| BY124 | $15 \%$ | OA79 | 70 |
| BY128 | 150 | OA81 | 80 |
| BY127 | 170 | OA82 | 10 p |
| BY164 | 57 p | OAgo | 7 |
| BYX10 | 829 | OA91 | 79 |
| BYZ10 | 85p | OA95 | 7 |
| BYZ11 | 820 | OA200 | 7 p |
| BYZ12 | 809 | OA202 | 10p |
| BYZ13 | 25p | TIV307 | 50p |

## SLIDE POTENTIOMETERS

SINGLE 58 mm ，TRACK
TWIN GANGED．LOG or LIN
1k to 500k 60p each
MULLARD C280 M／FOIL
$0.01,0.022,0.033,0.047$ 3p each $\begin{array}{llll}0.068,0.10 & \cdots & \cdots & \text { ip each } \\ 0.15,0.22,0.33 & \cdots & \cdots & 8 p \text { each }\end{array}$ 0.15
0.47
0.68
0.68
$1 \mu \mathrm{~F}$
$1-5 \mu \mathrm{~F}$

WIRE－WOUND RESISTORS
2.5 watt $5 \%$（up to 270 ohma 5 watt $5 \%$（up to $8 \cdot 2 \mathrm{k} \Omega$ only）， 9 p
10 watt $5 \%$（up to $26 \mathrm{~K} \Omega$ only）， 101

POTENTIOMETERS
Carbon：
Log．or Lin．，leas switch， 16 p
Log．or Lin．，with switch． 2 p Wire－wound Pots（3w）， 88 p Twin Ganged Stereo Pota，Log．
or Lin． 40 p ．

PRESETS（CARBON）
0.1 Watt 6 p VERTICAL
0.3 Watt 7ip HORIZONTAL

SPECIAL OFFER
TOSHIBA TH9013P


# Sinclair Project 60 <br> Project 60 Stereo FM Tuner 



Amongst the many advanced electronic features to be found in this remarkable stereo tuner, use of the phase lock loop principle ensures standards of audio quality better than from any other method of detection yet used. Varicap diode tuning, accurately formed printed circuit coils, an I.C. in the special stereo decoder section and switchable squelch circuit for silent tuning between stations contribute to the unsurpassed performance of this tuner, irrespective of price consideration. But the Project 60 FM Stereo Tuner is far from expensive - indeed, it offers fantastic value for money and will bring the thrill of stereo radio to many who previously. may not have been able to afford it. The tuner may be used with any good system as well as Project 60, but if you use it with other Project 60 modules, you will find the matching front panels particularly impressive in appearance as well as function.

## SPECIFICIATIONS

Number of transistors: 16 plus 20 in I.C.
Tuning range: 87.5 to 108 MHz .
Sensitivity: $7 \mu \mathrm{~V}$ for lock-in over full de-
viation.
Squelch level : typicaly $20 \mu \mathrm{~V}$
Signal to noise ratio: $\ddagger 65 \mathrm{~dB}$.
Audio frequency response: $10 \mathrm{~Hz}-15 \mathrm{Khz}$
(: 1dB)
Total harmonic distortion: $0.15 \%$ for $30 \%$ modulation.
Stereo decoder operating level: $2 \mu \mathrm{~V}$.
Cross talk: 40 dB .
Outpur voltage: $2 \cdot 150 \mathrm{mV}$ R.M S max.
(typically $2,50 \mathrm{mV}$. stereo)
Operating voltage: $25-30 \mathrm{~V} D C$ at 100 mA .
Indicators: Stereo on: tuning
Size : $93 \times 40.207 \mathrm{~mm}$.

## Super IC 12 mitarace arceme high fidelity amplifier



Having introduced Integrated Circuits to hi fi constructors with the IC.10, the first time an IC had ever been made available for such purposes we have followed it with an even more efficient version, the Super IC 12. a most exciting advance over our original unit This needs very few ex ternal resistors and capacitors 10 make an astonishingly good high fitelity amplifier for use with pick-up. F M radio or small P A. set up. etc The free 40 page manual supplied, details many other applications which this remarkable IC make possible. It is the equivalent of a 22 tran

Sistor circuit contained within a 16 lead DIL package. and the finned heat sink is sufficient for all requirements The Super IC. 12 is compatible with Project 60 modutes which would be used with the $Z .50$ and $Z 30$ amplifiers. Complete with free manual and printed circuit board

## SPECIFICATIONS

Output power: 6 watts RMS contınuous (12 watts peak). $6-8 \Omega$ Frequency Response: 5 Hz to $100 \mathrm{KHz}, 1 \mathrm{~dB}$ Total Harmonic Distortion: Less than $1 \%$ (Typical $01 \%$ ) al all output powers and frequencies in the audio band (28V) Load Impedance: 3 to 15 ohmis Input Im pedance: 250 Kohms nominal Power Gain 90 dB ( $1.000 .000,000$ times) after feedback Supply Voltage: 6 to 28 V Quiescent current. 8 mA at 28 V Size: $22 \cdot 45 \cdot 28 \mathrm{~mm}$ in cluding pins and heat sink
Manual avalable separately 150 post free
With FREE printed cilcuit board and 40 page manual
£2.98 Posit tree

## Project 605

The easy way to buy and build
Project 60
Project 605 is one pack containing one PZ5 iwo Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting
 comprehensive manual, post free
Everything you need to assemble a superb 30 watt high fidelity stereo amplifier without having to solder

Sinclalr Radionics Ltd, London Road, St. Ives, Huntingdonshire PE17 4HJ. Tel: St. Ives 64311

## the world's most advanced high fidelity modules

## Z. 30 \& Z. 50 power amplifiers

The $Z .30$ and $Z .50$ are of advanced destgn using sticon epitaxial planar transistors to provide unsur passed standards of performance Total harmonic distortion is an incredibly low $002 \%$ at 15 w (8, 8 ) and all lower outputs. Whether you use $Z 30$ or $Z .50$ amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other unts in the Project 60 range Their performance and design are such. however. that $Z .50$ s and $Z .30$ may be used in a far wider range of applications.
SPECIFICATIONS ( $Z .50$ units are interchangeable with $Z .30$ s in all applications).- Power Outputs Z. 3015 watts R.M.S. into 8 ohms using 35 volts 20 watis $R$ M S into 3 ohms using 30 volts

$Z .5040$ watts R.M.S into 3 ohms using 40 volts 30 watts R M S into 8 ohms using 50 volis
Frequency response: 30 to 300.000 Hz , 1 dB Distortion: $002 \%$ into 8 ohms . Signal to noise ratio: better than 70 dB unweighted. Input sensitivity: 250 mV into 100 Kohms (for 15 w into $8 \Omega$ ) For speakers from 3 to 1 b ohms impedance. Size: $14 \times 80 \times 57 \mathrm{~mm}$

## Stereo 60 Pre-amp/control unit

Designed specifically for use on Project 60 systems. the Stereo 60 is equally sultable for use with any high quality power amplifier. Since silicon epttaxial planar transistors are used throtighout. a really high signal-to-noise ratio and excellent tracking between channels is achieved Input selection is by means of press buttons, with accurate equalisation on all input channels The Stereo 60 is particularly easy to mount.
SPECIFICATIONS-Input sensitivities; Radio - up to 3 mV Mag. pu 3mV correct to RIAA. curve $\pm 1 \mathrm{~dB} 20$ to 25.000 Hz Ceramic pu - up to 3 mV Aux - up to 3 mV Output: 250 mV Signal to noise ratio: better than 70 dB . Channel matching: within 1 dB Tone controls: TREBLE 12 to -12 dB at 10 KHz BASS $1210-12 \mathrm{~dB}$ at 100 Hz Front panel: brushed aluminum with black knobs and controls Size: $66 \times 40 \times 207 \mathrm{~mm}$


## A.F.U. High \& Low Pass Filter Unit

$£ 5.98$
For use between Stereo 60 unit and two $Z .30$ s or $Z .50$ s. The unit is very easily mounted and is unique in that the cut-off frequencies are continuously variable. As attenuation in the rejected band is rapid ( $12 \mathrm{~dB} /$ octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The AFU is sultable for use with any other amplifier system There are two filter sections - rumble (high pass) and scratch (low pass). HF. cut-off ( -3 dB ) variable from 28 KHz to 5 KHz . L.F. cut-off ( -3 dB ) variable from 25 Hz to 100 Hz Distortion at 1 KHz ( 35 V . supply) $0.02 \%$ at rated output Operating voltage from 15 to 35 V Current 3 mA Size: $66 \times 40 \times 90 \mathrm{~mm}$.

## Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use PZ.5 for normal $Z .30$ assemblies and PZ. 6 or PZ. 8 where a stabilised supply is essential.

PZ.530 volts unstabilised $\mathbf{£ 4 . 9 8}$ PZ.6.35voltssrabulised $\mathbf{5 7 . 9 8}$ PZ. 845 volts stabulised (less mannstransformer) $\mathbf{E 7 . 9 8}$ PZ.8 manstransformer E5.98


## Guarantee

If. within 3 months of purchasing any product direct from Sinclair Radionics Lid.. vou are dissatisfied with it, your money will be refunded at once. Many Sinclair appointed Stockists also offer this same giuarantee in co-operation with Sinclair Radionics Lid
Each Project 60 module is te ;ted before leaving our factory and is guaranteed to work pertectly. Should any defect arise in normal use. we will service it at once and without any charge to yous. if it is returned within two years from the date of purchase. Outside this perlad of guarantee a small charge (typically f1.00) will be made. No charge is made for postage by surface mall. AIr Mall is charged at cost.

Typical Project 60 applications

| System | The Units to use | togetherwith | Units cost |
| :---: | :---: | :---: | :---: |
| Simple battery record player | 2.30 | Crystal P.U.. 12 V battery volume control, etc | $£ 4.48$ |
| Maıns powered record player | Z.30, PZ. 5 | Crystal or ceramic P U. volume control. etc | $£ 9.45$ |
| $12 \mathrm{~W} . \mathrm{RMS}$ continuous sine wave stereo amp. for average needs | $\begin{aligned} & 2 \times 2.30 \text { s. Stereo } \\ & 60 ; \text { PZ. } 5 \end{aligned}$ | Crystal, ceramic ormag. PU.FM Tuner. etc | £23.90 |
| 25 W . RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers | $\begin{aligned} & 2 \times 2.30 \text { s, Stereo } \\ & 60 ; \text { PZ. } 6 \end{aligned}$ | High quality ceramic or magnetic $P$ U., F M. Tuner. Tape Deck. etc. | £26.90 |
| 80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms) | $2 \times 2.50 \mathrm{~s}$, Stereo 60 ; PZ.8, mains transformer | As above | ¢34.88 |
| Indoor P.A. | Z.50, PZ.8, mains transformer | Mic. guitar, speakers. etc., controls | £19.43 |
| F.M. Stereo Tuner ( $\mathbf{\Sigma 2 5}$ ) \& A.F.U. ( $\mathbf{£ 5 . 9 8}$ ) may be added as requred. |  |  |  |
|  |  |  |  |

SINCLAIR RADIONICS, ST IVES, HUNTINGDONSHIRE PE17 4H.J
Please send I enclose cash/cheque/money order Name Address

# C. HADLEY 24, WOODHILL, HARLOW, ESSEX <br> Add 5 p P. \& P. Price list S.A.E 

MINTRON DIGITAL INDICATOR TYPE 3015F

Reads $0-9$ and decimals
(Data Sheet on request)

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| TRANSISTORS |  |  |  | B1116 |  | 0 C 45 | 13p | TIP33A | ¢1.8 | 2N3711 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | BD12 | 60p | 0 C 45 | 13D | TIP34A | £1-8 |  |
| AC107 | 15p | AL102 | 880 | BD130 | ${ }^{46} \mathrm{p}$ | $0 \mathrm{C71}$ | 12p | 2N697 | 18p | 40636 |
| AC126 | 11 p | AL103 | 497 | BD131 | 59 p | OC72 | 120 | 2N1171 | 24 p |  |
| AC127 | 11p | AU103 | 850 | BF194 | 15p | $0 \mathrm{C81}$ | 18 p | 2N1304 | $25 p$ |  |
| AC128 | 110 | AT111 | $95 p$ | BFY50 | 15p | OC81D | 180 | 2N1305 | $25 p$ |  |
| AC176 | 250 | BC107 | 8 8 | BFY51 | 12p | $0 \mathrm{C83}$ | 20p | 2N2645 | 47 p |  |
| AC141K | 20p | BC108 | 8 p | BSY95A | 15p | OC170 | 84 p | 2 N 2926 | 10p |  |
| ACl42K | 200 | 3 Cl 109 | 8 p | ME0402 | 18p | OC200 | 250 | 2 N 3053 | 20 D |  |
| AD14 | 40 D | 18C154 | 20 p | ME0404 | 14p | OC201 | 25p | 2 N | 49p | 400 |
| AD150 | 440 | BC168 | 10p | ME4401 | 10p | OC25 | 25 D | 2N370 | 12 p | N4003 |
| AD161 |  | BC169 | 11p | ME4102 | 12p | OC28 | 30 p | 2N 3703 | 12 D | IN 4004 |
| AD162 |  | BC182L | 8 | ME6002 | 14] | OC29 | 88 p | 2N3704 | 12p | OA90 |
| AF114 | 15D | BC183L | 87 | ME6101 | 14p | 0 C 35 | 25 D | ${ }_{2} \mathrm{~N} 3705$ | 12 p | OA91 |
| AF115 | 15p | BC184L | 89 | ME6102 | 150 | OC36 | 88 p | 2N3706 | 10p | OA200 |
| AF116 | 150 | 13C212L | 8 p | MP8111 | 32 p | TIP29A | 48p | 2N3707 | 10p | OA202 |
| AF117 | 15p | BC214L | 8p | MP8511 | 845 | T1P30A | 55p | 2N3708 | 8 p | I844 |
|  |  |  |  | MP8513 | 45p | TIP31A | 58p | $\begin{aligned} & 2 N 3709 \\ & 2 N 3710 \end{aligned}$ | $\begin{aligned} & 100 \\ & 10 \mathrm{p} \end{aligned}$ | $\begin{aligned} & \text { IN } 414 \\ & \text { WO2 } \end{aligned}$ |
| MULLARD POLYESTER CAPACITORS C280 SERIES |  |  |  |  |  |  |  |  |  |  |
| 250 V P.C. mounting: $0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 3 \mathrm{p} .0 .033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 81 \mathrm{p} .0 .1 \mu \mathrm{~F}, 4 \mathrm{D}$ $0 \cdot 15 \mu \mathrm{~F}, 0 \cdot 22 \mu \mathrm{~F}, 5 \mathrm{p} \cdot 0-33 \mu \mathrm{~F}, 81 \mathrm{p} \cdot 0 \cdot 47 \mu \mathrm{~F}, 81 \mathrm{p} .0 .68 \mu \mathrm{~F}, 11 \mathrm{p} .1 \cdot 0 \mu \mathrm{~F}, 13 \mathrm{p} .1 \cdot 5 \mu \mathrm{~F}, 20 \mathrm{p} .2-2 \mu \mathrm{~F}, 24 \mathrm{p}$ |  |  |  |  |  |  |  |  |  |  |
| MULLARD POLYESTER CAPACITORS C296 SERIES |  |  |  |  |  |  |  |  |  |  |
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EMI $13 \times 8 \mathrm{~d} /$ cone 3,8 or 15 ohms EMI $13 \times 8$ twin tweeter 3,8 or $150 h m e$ Richard Allen $8^{\prime \prime} 3,8$ or 15 ohm Fane $8^{-}$dual cone 808T
Fane a' d/cone roll surround 807T Elac 59RM109 $9^{\prime \prime} \times 5^{\prime \prime} 15 \mathrm{ohm}$ Elac 59RM1149 958 ohm Elac $6 \frac{1}{2}$ dicone 8 ohm
Crossover tor above (post free)
Crossover tor above (post free) Geodmans $8 \mathrm{P}, 8$ or 15 ohm Goodmans 10 P, 8 or 15 ohm Goodmans 12 P, 8 or 15 ohm Goodmans 15 P, 8 or 15 ohm
Goodmans 18 P, 8 or 15 ohms $2^{\prime \prime}, 2 \frac{1}{2}^{\prime \prime}$ or $3^{-} 80$ ohm or $2 \frac{1}{2}^{-} 64$ ohm $\begin{array}{ll}7^{\prime \prime} \\ 8^{\prime \prime} & \times 4^{\prime \prime} 3 \text { or } 8 \text { ohm } \\ 8^{\prime \prime} & 3 \text { or } 8 \text { ohm }\end{array}$ $8^{\circ} \times 5^{\prime \prime} 3$ or 8 ohm $10^{*} \times 6^{\prime \prime} 3,8$ or 15 ohm
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| EBF89 | 12 pp | 30P4 | $12 \%$ p | PL81 | 1719 |
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For Ferguson 850900 chassis. Adaptable for most UHF Chassis 42.50 , p. \$ p. 50p.

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Amiths reconditioned awitchmaster MK III. Decimalized Perfect working order. 12 for $\mathbf{2} 25$ delivered. For sample rend $\mathbf{\Sigma 2} \cdot \mathbf{5 0}$ c.w.o.

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BRAND EEW HARTLET OSCILLOSCOPHS CT316 in original packing. Band wldth up to $5 \mathrm{Mc} / \mathrm{s}$. Maina supply. Price 240, p. \& p. 21-60p.

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BARGAIN PARCELS 141b at el 45 plus 32 pp p.p. ; 281 b at c8.75 plus 52 pp p.p.; 561 b at 84.50 plas 81.25 p.p. Contain pots, Res, Valves, Diodes, Tagboards, Chassia, Valveholders, ote. Good value save effa. Lacky Dip Service.

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AERLAL MAST POLES approx. fit high $2^{\prime \prime}$ dib. Inter EERIAL MAST Minimum order three New condition 01 cach sectios. Carriage 35 p each section.
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SLIDING RESIETORS. $12 \mathrm{amp}, 10 \mathrm{hm}$. Approx. 9in. long $1-4$ amp., 14 ohms. Approx. 7hn, long. As new Ex Eqp 76p, p.p. 15p. QUOTATIONS FOR QUANTITY. $^{\text {QUN }}$
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 DRILL COWTROLLER NEW IKW MODEL Electronically change apeed from approx 10 maximum．Full power 10 apeeds by finger－tip control．Kit Includes al parta．care，every hins and 13p $\underset{\text { post }}{\text { and }}$ and Map post and insurance． ble．告敃 plus 13p post \＆ p ．
MAINS OPERATED CONTACTOR $220 / 240 \mathrm{v}$ ． 00 cycle solenold With laminated core so very dient in operation，Closes dircuits each rated at 10 ampa ． Extremely well made by 0 verall $24 \times 2 \times 21 \mathrm{l}$ 1.50 each．

NEED A SPECIAL SWITCH？ Doublo Leal Contact．Very oltght preseure closes both contacts．6p each
sup doz．Plastic push－rod
each． 45 p doz．operating． 6 p
MICRO SWITCH
armp changeover contacts， $9 p$
10ph


## MINIATURE <br> WAFER SWITCHES

2 pole，${ }^{2}$ way－${ }^{2}$ pole，${ }^{2}$ way－ pole， 4 way－3 pole．\＆way－ 2 polo
6 way－ 1 pole． 12 way．All at 80 p
each， $81 \cdot 80$ for ten，your assortment．
WATERPROOF HEATHG ELEMERT 6 yard length 70 W ．Self－regulating temperature


I5A ELECTRICAL
PROGRAMMER
Learn in your zleep： Have radio playing and swake－switch on lights to ward ofl intruders－have warm house to come home to．All these and many other things you can do it you invest in an electrical programmer Clock by famous maker with 15 amp ．on／oft owitch．Switch on time can be set answhere to stay on up to 8 hours．Independent 60 minute 20 p p \＆ p or with glass front chrome bezel 75p


TREASURE TRACER MARK II battens）to make the metal detector aimilar to the circuit Practical Wireless August issue． $\$ 8.95$ plas 20 p post and insurance．

SNAP ACTION SLIDE SWITCH Rated 5a．240v．Made by Artow．Type vacuumb，etc． 5 p each， 10 for 45 p ．

## NUMICATOR TUBES

clock cocks，etc． $\mathrm{Hi-v}$
each． 10 for 813.

## － <br> 2 WAY SUB－MINIATU RE MULTI－CORE CABLE <br> 7.0076 copper cores each core P．V．C．ingulated and approz． $3 / 16 \mathrm{in}$ ．thick．Price 20 p per yard．



LIGHT CELL
Almost zero resiatant in aun－ 11 ght increases to $10 \mathrm{~K} \quad \mathrm{Ohma}$ resin sealed．size approx．Iin．dian by tin．thict Rled ORP Also ORP 12 light cell 46p．

Colled Leads．Fxtend to about 2 yards－as fitted to telephones etc．the flex conductors of these use a threakable with normal makes them virtually un $80 \mathrm{p}, 6$ core 250 per lead．All less $10 \% \mathrm{im}$ lota of or more．

## MAINS TRANSISTOR POWER

Designed to op
flers．Adjustable oute transistor seta and ampli－ to 500 mA （clasa B worklag）．Takes the place any of the following matteries：PP1，PP3，PP4，
PP6，PP7，PP9，nnd others．Kit comprises：mains transiormer rectifler，smoothing and load renistor condensers and instructions．Real snip at only
GOOD COMPANION
we can now offer these again in modular version using Modulea and Radio mobile Permeabity runer．shouldn＇t tak approx． $11^{-}$wide $\times 8^{-}$high $\times 3^{-}$deep （ize plete assembly instructions－ $\mathbf{~ 4 P 7 5}$ plins 25 p post \＆ins．

## RADIO STETHOSCOPE

Easiest way to fault find－traces signal from serial to speaker－when signal stops you＇ve found the fault． kit comprises two epecial transistors and all parts including probe tube and crystaj earplece．s8－twin stetho－set Instead of earpiece 75 pextra post and ins． 20 p

## STANDARD WAFER SWITCHES

 Standard ine $1 \neq$ wafer－allver－plated $5-a m p$ contact standard $8^{\prime \prime}$ spindie $2^{*}$ long－with locking washer and nut．No．of Poles

| 1 pole | 40p | 400 | 40p | 40p | 40p | 40 p | 40 p | 400 | 40 p |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 poles | 40 p | 408 | 40p | 40 p | 40 p | 40 p | 400 | 70 p | 70 |
| 3 poles | 40p | 40p | 10 p | 40 p | 70 p | 700 | 700 | 050 | 85 |
| 4 poles | 40p | 40 p | 40p | 70p | 70 p | 70p | 700 | 31.20 | 81．20 |
| 5 poles | 400 | 400 | 700 | 700 | 85 | 08 p | 085 | 81.45 | 21－45 |
| 6 poles | 40p | 700 | 70 D | 70p | 050 |  | 985 | 81.70 | 21．70 |
| 7 poles | 70 p | 700 | 700 | 95p | 81.20 | 81.20 | 21． 20 | 81.05 | 21．95 |
| 8 poles | 70p | 70p | 70 p | 95p | 21.80 | 21.20 | 81.20 | 28．20 | 28.20 |
| 9 poles | 70 p | 700 | 050 | 95p | 21.45 | 21.46 | 21.45 | 22－45 | 42．45 |
| 10 poles | 70 p | 70p | 950 | \＄1． 20 | 咥 $\cdot 45$ | 81.45 | 21.45 | $82 \cdot 70$ | 28．70 |
| 11 poles | 709 | 05p | 05p | E1－20 | 21.70 | 21－70 | 81.70 |  | $22 \cdot 95$ |
| 12 poles | 700 | 95p | 95p | 81.20 | 81.70 | E1－70 | 11．70 | 8880 | 28.80 |

## THYRISTOR LIGHT DIMMER

For any lamp up to 200 watt．Mounted on switch plate to fit in place of standard switch．Virtually no radio inter－ ferences．Price 28.60 plus 20 p post and inaurance．


MULLARD AUDIO AMPLIFIER MODULE Uees 4 tranaistors，and has an output of 500 mW into 8 ohma speaikers．Input suitable for crystal mic．or pick－up SPECIAL SNIP PRICE 65p each． 10 for 25.90 ．$\times$ in high

## THIS MONTH＇S SNIP

## REPEATING TIME SWITCH

1 or 2 on／ofts per 24 hours．Repeats until re－ programmed．8witches up to 15 amp．8witching Precision made with 24 hour dial．Minlature－ will fit Into $2^{\circ}$ cube．Mains operated clock but awitch may be liolated for switching battery sets．ldeal for：－bhop window lighting．anti－ thief devices，central heating control sind many other automatic
processes．Price with instructions 42 each +20 p poat and insurance．


HORSTMANN＂TIME \＆SET＂SWITCH （A30 Amp Awitch．）Just the thing if you want to come home to a warm bouse without it costing you a fortune．You can
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Made by Honeywell for normal air temperaturea
$40^{\circ}-90^{\circ} \mathrm{F}$（ $5-25^{\circ} \mathrm{C}$ ）．This is a precislon instrument with $40^{\circ}-90^{\circ} \mathrm{F}\left(5-23^{\circ} \mathrm{C}\right)$ ．This is a precislon instrument with differential which can be adjusted to better than witch is operated by a colled bi－metal element and adjustable heater is incorporated for heat anticipation． Elegantly atyled and encased ln an Ivory plaatic case with clear plastic windows thermometer above and witch aeting acale below－size approx $3.8^{\prime \prime} \times 3.2^{\prime \prime} \times 1.4^{\prime}$ deep－can be mounted on conduit box or directly on wall．Price $\$ 1.26$ each or ten for $\$ 11 \cdot \mathbf{e 5}$ ．


ZPM－MODULATION MOTOR Could also be used to open vantilators，doors，valve，damper etc．particularly suitable for remote control．Made by internal lirait switches to atop it at the end of fits travel． size approx． $6^{5} \times 6^{\prime \prime} \times 5 \frac{1}{}^{\circ}$ and welghing approx． 10 lbs． This is extremely powerful and would lift a heavy door or open a long line of ventilators．To operate thia motor you put the 50 cycle upply through a change over awitch．For instance a thermostat with change－ over contacts could automatically regulate the temperature in a growing house， chicken hatchery etc．An indicator on the motor graduated 0－10 ahows the his to a volt meter would give a remote indication of the open ar close position a very expensive motor it both direct from gatchwell our price complete with step down Transformer is $\mathbf{\$ 1 5}$ ．

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or amplification and detection of $1 . \mathrm{m}$ ．signala at 10.7 MHz
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 Brief description of each kit fa given belo sold． ith 3 kits or more we give FREE below and II piece balance kit．Price of kita 40 p each poat paid．Special price for all 7 kits ied with free balance kit．
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etc．Motor operatea from it volt bsttery．Illus－ trates and teaches how electro－magnetism operatea a motor．
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Miniature size $\ddagger^{*}$ aquare front $\times i^{\prime \prime}$ deep．Under－ stend made for Truvox．Donble wound，maybe wired in series or parallel for high or low impedance working．Each supplied with matching erase head．
2 track 50 p pair， 4 track 76 p pair．Less $10 \% 10$ or 2 track 50p pair， 4 track 76p pair．Less $10 \% 10$ or more pairs．

KA10 Morse Kay buzzer and bell kilk． 25 part hit easy to construct，aimple to operate
Instrument Motors fittod with Gear Bor．These made by Smiths Industries are as fitted into electrie clocks，chari recorders ete．Motor size spprox． $1^{t^{*}}$ dia，$\times 1^{\prime \prime}$ deep，gear box attached approx． $2^{\prime \prime}$ dismeter $\times \mathfrak{l}^{\prime \prime}$ thick with good length $x$ of spindle．Most motors are fitted with a $f^{\prime \prime}$ long $\times \frac{i^{\prime}}{} \times$ diameter drive spindle．Sultable for $200 /$ 240v msins 50 c．p．s．unless marked otherwise Following speeds available：－ 8 revs per min，
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Micro \＆witch．Made by Burgess． 15 amp onf／on－
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 2 Amp 8
2 and ${ }^{\text {surfach }}$ Switched Sockets．Oblong，brown bekelite aurface mounting－ 2 pin 8 tandard domestic Burface 8 witches． 5 smp Briti bariselite 8 oblong－1 s way Britiah make．Brown each．
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Miniature Tuben．These are approx．I＂diameter and need miniature bi－pin end connectors． All are 55 p each．Less $10 \%$ on 10 or more wat All are $55 p$ each．Less $10 \%$ on 10 or more． A．c．Maing Buzzer．These are open constructions
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4 Watt Amplifler Module．Made by Mullard Ref No．EP9000．Part of the Uniler syatem．This had an output of 4 watt speech and music into a 12－15 ohm speaker．A powerful smplifier with a
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[^4]

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## Trpe MR.85P. itin. $\times 4$ in. tronts.



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| $50 \mu \mathrm{~A}$ | 88.60 | 150 V . D.C. |
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 60 1 A . ...... 88.87 10V. D.C. . 22 -20 $100 \mu \mathrm{~A}$ $200 \mu \mathrm{~A}$ $500 \mu \mathrm{~A}$
$500-0-500$ 1 mA 6 mA
10 mA
50 mA
100 mA
500 mA
1 gmp.
10 mp .
10 gmp .
20 amp .
30 amp .
0 amp.
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M imor gcale. Mirror gerle.
$-6 / 3 / 12 / 30 / 120 / 600 \mathrm{~V}$ D.C. $3 / 30 / 120 / 600 \mathrm{~V}$ A.C. $50 / 600 \mathrm{uA} / 60 /$ $600 \mathrm{~mA} .10 / 100 \mathrm{~K}$ -20 to +46 clb . 88.971 P \& P 1210

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Reverse Swlitch.
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HIOKI MODEL 700X 100.000 O.P.V. Overlad protection. Mirror scale.
$-3 / \cdot 6 / 1 \cdot 2 / 1 \cdot 5 / 3 / 6 / 12 / 30 / 60 /$ 120/300/600/1200VDC 1.5/3/6/12/30/60/150/300/600/ $15 / 30 \mu \mathrm{~A} / 3 / 6 / 30 / 60 / 150 / 300 \mathrm{~mA}$ 6/12 AMP. DC. $2 \mathrm{~K} / 200 \mathrm{~K} /$ +63 lb 18.50 P. $\mathbf{P}$. 20


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Completel y portable, slmple
to use pocket nized tester. Ranges $0 / 3 / 30 / 300 \mathrm{~V} \mathrm{AC}$ Renjatance 0.20 K ohms TIIS KODEL 117 F.E.T. ELECTRONIC Battery operated 11 meg Input, 26 ranges. Large
mizror scale. size
 1200 V. AC VOLTS $3-300 \mathrm{~V}$ RMS. $8 \cdot 0$ R00V P-P. DCCUR Reaistance up to 2000 M ohm. Declbeis 20 to +51 db . Complete with leads/Instructhons. $217 \cdot 50$, P. \& P. 20 p

TE-200 RF SIGNAL GENERATOR


Accurste wide range alg
nal generator covering $\begin{array}{cc}\text { nal } & \text { generator covering } \\ 120 & \mathrm{Kc} / \mathrm{s}-500 \mathrm{Mc} / \mathrm{s} \text { on }\end{array}$ 6 bends. Directly call brated Variable R.F. at tenuator, muio output Xtal socket for calibration. $290 / 240 \mathrm{~V}$. A.C. tions 215. Carr. 374 D Slize $140 \times 215 \times 107$

TE22 SINE SQUARE WAVE AUDIO GENERATORS
 Sine: 20cps to 200 $\mathrm{kc} / \mathrm{s}$ on 4 bands Bquare: 20cpe to
$30 \mathrm{ke} / \mathrm{s}$. Output impedance 8.000 ohme, $200 / 250 \mathrm{~V}$ Supplled brand new and guaran
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## sl generator cover

 lng $120 \mathrm{kc} / \mathrm{s} \cdot 260$ Mc/a on 6 bands. Directly calibrated variable R.F: at 200/240V A.C. Brand new wit P. \& P. 37 ip. B.A.E for detalls.$\square$
240 Wide Apgle ImA Yeters MWl.6 60 mm square 88.07
MW1.8 80 mm square MW1.8 80 mm square P. \& P.extre


MODEL LT. 1011000 O.P.V $0 / 10 / 50 / 250 / 1000$ V. D.C. $0 / 10 / 50 / 250 / 1010$
$0 / 1 / 100$ M.A. $0 / 150 \mathrm{~K}$ ohns 21.97. P. \& P. 15 p .

TKK MODEL MD. 120 Mirror geale. 20k/ Volt D.C. 600/3,000 V. D.C. 6/120/ $1,200 \mathrm{~V}$. A Current $0.60 \mu \mathrm{~A} / 0-12 / 0$ $300 \mathrm{~mA} .0 .60 \mathrm{~K} / 0-6 \mathrm{Meg} \Omega$ -20 to +63 dB .84 .621


MODEL 50030.000 0.P. With overload protection mirror ecte $0 / 5 / 2 \cdot 5 / 10 / 25$
$100 / 250 / 500 / 1,000 v . ~ D . U ~$ $0 / 2 \cdot 5 / 10 / 25 / 100 / 250 / 500 /$ $1,000 \mathrm{~V}$. A.C. $0 / 50 \mu \mathrm{~A} / 5 / 50 /$ $500 \mathrm{~mA}, 12 \mathrm{mmp}$ D.C. $0 / 60 / \mathrm{K} / 6 \mathrm{Meg} . / 60 \mathrm{Meg} \Omega$.
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$-5,2 \cdot 5,10,50,250,1,000$ $-5,2 \cdot 5,10,50,250,1,000$
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 Input imp. 2 meg $\Omega 25 \mathrm{pF}$ X amp. sensitivity 0.9 v p-p/CM. Bandwidth 1.5 cp $-800 k \mathrm{~Hz}$. Input imp. ${ }^{2}$
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 | $2 \mathrm{G306}$ | 42 D | 2 N 3564 |
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| 2 G 308 | 30 p | 2 N 3565 | $2 \mathrm{G3} 308$

2 G 309 2G309 \begin{tabular}{ll|l|}
$2 G 374$ \& 20p \& 2N3568 <br>
2G3569 <br>
2G381 \& 22 p \& 2 N 3570

 $\begin{array}{lll}2 G 381 & 22 p & 2 N 3570 \\ 2 N 388 A & 49 \mathrm{p} & 2 N 3572\end{array}$ 2N388A 49p 2N3572 

2N404 \& 20p \& 2N3805 <br>
2N69 \& 15p \& 2N3606

 2N697 15p 2N3607 

2N698 \& 25p \& 2N3638 <br>
2N699 \& 30p \& 2N3638A

 2N706 10p $2 N 3641$ $\begin{array}{lll}2 N 706 A & 18 p & 2 N 3642 \\ 2 N 708 & 15 p & 2 N 3643\end{array}$ $\begin{array}{ll}2 N 709 & 15 p \\ 2 N 3643 \\ 2 N 3644\end{array}$ $\begin{array}{ll}2 N 718 & 25 p \\ 2 N 718 A & 2 N 3645 \\ 2 N & 30 p\end{array}$ 

2N718A \& 30 p \& 2 N 3691 <br>
2N726 \& 30 p \& 2 N 3692

 

2N726 \& 30 p \& 2 N <br>
2N727 \& 30 p \& 2 N 3693

 

$2 N 727$ \& 30 p \& 2 N 3693 <br>
2N914 \& 17 p \& 2 N 3694

 

$2 N 914$ \& 17 p \& 2 N 3694 <br>
2N916 \& 17 p \& 2 N 3702

 

$2 N 918$ \& 170 \& $2 N 3702$ <br>
$2 N$ \& $2 N 3703$

 

2N929 \& 82 p \& 2 N 3704 <br>
2N 230 \& 20 D \& 2 N 3705
\end{tabular} 2N93

2N98
2N10

云云 $\begin{array}{lll}2 N 1132 & 25 p & 2 N 3709\end{array}$ 2N1302 2N1303 17p 2 N 3713
 $2 \mathrm{~N}_{1306}^{2}$云客云条 ละ

## 2

## ．

2N2147 2 N 2180 $2 N 2193$
$2 N 2193 A$ 2N2193A 2N2194 2 N 2217 2 N2218 2 N 2219 2 N 2220 2N22201 2N2297 2N2368 2N2369 ${ }_{20}^{2 N 23949 A}$ 2N2410
2N2483
2 N 2483
2 N 2484 2N2534 2N2540 2N2613 2 N 2646 2N2711 2N2713 25 2 N 2714
2 N 2904 2N2904 2N2904
2N2905 2N2905A 2N2906A $25 \mathrm{D} \mathrm{D}_{2} \mathrm{~N} 430 \mathrm{O}$

 \begin{tabular}{ll|l}
2 N 2923 \& 15 p \& 2 N 5027 <br>
2 N 2924 \& 15 p \& 2 N 5028

 2 N 2925 2 N 2926 Cl 10 2N2926Y $\begin{array}{ll}2 N 3011 & 20 \mathrm{p} \\ 2 \mathrm{~N} 517\end{array}$ 2N3014 32p｜2N5176 2N3053 18p 2N5232 2N30t4 4 AD 2N5246 2N3055 600 $2 N 5246$ 2N3133 30 p 2N5 249 2N8135 15D $2 N 5265$ 

2N8133 \& $25 p$ \& 2N6305 <br>
2N3136 \& $25 p$ \& $2 N 5306$

 

2N3136 \& 25 p \& 2N5306 <br>
2N3390 \& 250 \& 2NS 307

 

2N3390 \& 25p \& 2N <br>
2N391 \& 20 p \& 2N8 308
\end{tabular} 2N3391A 30p 2 N 5309 ${ }_{2 N} \mathrm{~N}^{2} 392 \mathrm{~A}$ 17p 2 N 5310 2N3393 15p 2N5354 2N3394 15 p 2N5355

 \begin{tabular}{ll|l}
$2 N 3403$ \& 22 p \& 2 N 5365 <br>
$2 N 3404$ \& 32 p \& 2 N 536 s

 

$2 N 3404$ \& 32 p \& $2 N 5366$ <br>
$2 N 3405$ \& 45 p \& $2 N 5367$
\end{tabular} 2N311 $29{ }^{2 N} 2{ }^{2 N 5457}$ 2N3900A

2 N 3901 2N3901 \begin{tabular}{l|l}
2 p \& $2 N 3903$ <br>
$2 N 3904$

 

D \& 2 N 3904 <br>
2 N 3905

 20 2N3906 2N4060 D 2N4081 

p \& 2 N 4062 <br>
2N 4244
\end{tabular} 2N4248 p ${ }^{2 N} 4249$

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#### Abstract

5 p BFW91 20p ${ }^{20}$ NKT223 30p 29 NK223 27p $22 \mathrm{p} \times 12242 \mathrm{p}$ 20 p BFX 30 25p NKT229 30p




VALYES

38p 252


รัธั
 28102 －位
 27 p
270
4040
8040

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300528
40600


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ci 20 25 p
$80 \mathrm{AC188}$
ACY1
 120.0819 $120 \mathrm{ACH2}$
100 ACI 2
220 12
12
47
15
15
18
18
> $12 p$
12p ACY
 15 p
$\mathbf{1 5 p}$
ACY 41 18p ACY4 $42 p$ AD149 17p AD150 17p AD162 17p
AF10．
15 p
AF11 17 p AF115㗊㫛 $15_{D}$
$\mathrm{AFPl}_{8}$
$\mathrm{AFl}_{2}$ 47p
15 p
AF12 18p AFF126 $67 p$
47 p
AF139
AF178发 $12 p$
$522_{p}$
AF18 $52 \mathrm{p} / 1 \mathrm{~N}_{18}$
45 p
$4 \mathrm{~N}_{239}$ $30 \mathrm{D} / \mathrm{AF} 279$

## 

$$
\begin{array}{r|rl}
325 p & \text { ABY } 27 \\
37 p & \text { ABY } 28
\end{array}
$$

40 p A8Y28

\section*{| 37D | A8Y50 |
| :--- | :--- |
| 37 p | ASY 51 |
| 62 p | ASY 54 |}

$$
\begin{array}{l|l}
62 \mathrm{p} & \text { ABY54 } \\
48 \mathrm{ABY} 5 \\
\text { A87 } & \text { ASY } 8 \mathrm{l}
\end{array}
$$

$$
\begin{array}{l|l}
\text { 27p } & \text { ASY88 } \\
\text { 27D } & \text { ARZ21 }
\end{array}
$$

$$
\begin{array}{ll}
210 & \text { AUC21 } \\
32 \mathrm{~A} & \text { AY10 } \\
47 \mathrm{p} & \text { BC107 }
\end{array}
$$

47 p
BC107
32p
BC108

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Decke gupplied with cartridge in ready veneered plinth with cover.
Garrard 2025TC/9TAHCD Garrard AP25 III/9TAHCD Garrard SP25 III/G800 Garrard SP25 III/M75-6 Garrard EP25 III/M44-7 Garrard GP2S III/M44-玉 3P26 III/G800 (Play-on P\&C) Garrard AP76/G80 Garrard AP76/M55E Garrard AP76/M76FJ BER McDonald MP60/a800 BGR McDonald MP60/M44-7 BER McDonald MP60/M44-E Goldring GL72/G800 oldring GLto/G800 Goldring GL75/G800
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| 3V4 | -48 | 30PL13 | -87 | ECC81 | - 17 | EL33 | -54 | PCP802 | 88 | U25 | -68 |
| 8/30L2 | - 52 | 30PL14 | -68 | ECC82 | . 18 | EL84 | . 21 | PCF805 | . 38 | U26 | . 54 |
| BAQ5 | - 21 | DAF91 | 21 | ECC83 | -21 | EY51 | . 88 | PCL82 | 28 | U191 | -57 |
| 6BW7 | -48 | DAF98 | 85 | ECF82 | . 28 | EY88 | -27 | PCL83 | 58 | U251 | -60 |
| 6 Fl | $\cdot 57$ | DF91 | -14 | ECH35 | - 58 | EZ80 | - 19 | PCL84 | . 81 | U329 | -65 |
| 6 F 23 | -67 | DF96 | . 85 | ECH42 | 56 | E281 | . 81 | PCL85 | 36 | U801 | -75 |
| 6 F 25 | . 49 | DK91 | -25 | ECH81 | . 86 | KT61 | . 54 | PCL86 | . 85 | UBF89 | -29 |
| 68N7GT | . 28 | DK92 | $\cdot 47$ | ECL80 | . 85 | LT68 | . 75 | PFL200 | . 49 | Uocss | . 84 |
| 12AU7 | -18 | DK96 | - 48 | ECL82 | . 27 | N78 | . 85 | PL88 | . 45 | UCH81 | . 28 |
| 25LAGT | . 18 | DL92 | - 24 | ECL86 | . 82 | PC86 | - 44 | ${ }^{P} \mathrm{~L} 81$ | 41 | UCL82 | . 81 |
| 30 Cl 5 | -56 | DL94 | . 48 | EF39 | $\cdot 88$ | PC88 | - 44 | PL82 | . 29 | UF89 | . 28 |
| 30 Cl 7 | $\cdot 75$ | DL96 | . 88 | EF80 | . 28 | PC97 | . 88 | PL83 | . 81 | UL84 | -27 |
| 30 Cl 8 | - 56 | DY86 | $\cdot 21$ | EF85 | . 28 | PC900 | . 28 | PL500 | . 58 | UY85 | -82 |
| 30F5 | . 68 | DY87 | $\cdot 21$ | EP86 | -28 | PCC84 | . 87 | PL504 | . 58 | W77 | . 48 |
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| 6F23 | - 88 | AC/VP2 | . 77 | ECH84 | . 86 | LN339 | -63 | PM84 | .88 | $\mathrm{VP}_{4} \mathrm{~B}$ | . 77 |
| 6 F 25 | - 58 | B349 | . 66 | ECL80 | . 85 | N78 | . 87 | PX25 | . 85 | W77 | . 48 |
| 6J7G | . 24 | B724 | . 62 | ECL82 | . 81 | P61 | . 40 | PY32 | . 62 | Z77 | . 28 |
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Bentley Acoustic Corpor.... ... 556
Bernard, Gerald
B.I.E.T.

04, cov.
Bib Sales ..
483,475
4
Boffin Projects ... ... ......$\quad 554$
British National Radio \& Electronic School

486, 546
526
Bull, J. (Electrical) Ltd.... .... .... 549
Bush \& Meissener 468
C.B.M. Electronic Components Led. ...
C.T. Electronics.

556
Carrana, C.
557
556
Colomor (Electronics) $\because \ddot{\text {.... ... } 556}$
Component Factors Ltd.
558
Comet High Fidelity Discount Warehouses

Electronics Ltd.
478, 9
D.E.W. Ltd

480
Dabar Electronic Products
DEB Chemicals (Swarfega)
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Douglas Electronics Industries L̈td.
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481
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472
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467
555 476 556
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530
5
Field Electric Ltd
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$\cdots \quad \ldots \quad . . . \quad 557$

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557 \& 558
Keytronics
55
King, J. M.
Knopp, J, F. D. ..
480
554

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Radio \& T.V. Components (Acton) Lid
Radio Society of Great Britain... 470, 47
Radionic Products Ltd .... 526
Readers Radio
Riversdale Electronics
ROC Electronics Ltd.
Rebinectronics Ltd. ... ... ... 508
RSC Hi-Fi Centres Ltd, ... ... 554
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| OB2 | 0.40 | 6 AR11 | 1.85 | 6 FraG | 0.45 | 10 C 20.60 |  |  |  |  |  |  |  | EF988 | 0.75 | GZ34 0.60 | P | 0.60 0.45 | UAPBC80 | 0.80 |
| OH3 | 0.70 | 6485 | 0.50 | 6 F 11 | 0.50 | 10D1 0.85 |  |  |  |  |  |  |  | $\begin{aligned} & \text { EF183 } \\ & \text { EF184 } \end{aligned}$ | 0.30 0.85 | HABC800.85 <br> HK90 | PL83 | 0.45 0.48 | UABC80 | 0.40 |
| OC3 | 0.40 | 6 6870 | 0.85 | $6 \mathrm{Fl3}$ | 0.50 | 10 D 20.55 |  |  |  |  |  |  |  | EFF84 | 1.25 | $\begin{array}{ll}\text { HK96 } \\ \text { KT68 } & \mathbf{2 . 3 5}\end{array}$ | ${ }^{\text {PLS84 }}$ | 0.40 | UAF41 | 0.70 |
| OD3 | 0.40 | 6ATB | 0.38 | $6 \mathrm{6F14}$ | 0.70 0.65 | $\begin{array}{ll}10 \mathrm{Fl} & 0.75 \\ 10 \mathrm{~F} 9 & 0.65\end{array}$ |  |  |  |  |  |  |  | EK90 | 0.88 | $\begin{array}{ll}\text { KT88 } & 2.25\end{array}$ | PL302 | 0.95 | UAF42 | 0.80 |
| 183GT | 0.45 | $6 \mathrm{6AU6}$ | 0.30 0.40 | ${ }_{6}^{6 F 15}$ | 0.65 0.50 | $\begin{array}{ll}\text { 10F9 } & 0.65 \\ \text { 10F18 } & 0.60\end{array}$ |  |  |  |  |  |  |  | EL34 | 0.80 | $\begin{array}{ll}\text { K788 } \\ \text { P78 } & 1.80\end{array}$ | PL504 | 0.75 | UB41 | 0.85 |
| $1 \mathrm{L4}$ | 0.25 | 6A 6 6 68 | 0.40 0.65 | 6 F 18 6 F 23 | 0.50 0.90 | $\begin{array}{ll}\text { 10F18 } & 0.60 \\ \text { 10L1 } & 0.60\end{array}$ |  |  |  |  |  |  |  | EL36 | 0.60 | PABC800.40 | PL60 ${ }^{\text {P }}$ | 0.90 | UBC41 | 0.86 |
| 1 R 4 | 0.50 | 6AW8A $613 \mathrm{~A} 6$ | $\begin{aligned} & 0.65 \\ & 0.28 \end{aligned}$ | $6 \mathrm{6F23}$ | 0.80 0.80 | ${ }^{10 \mathrm{LLI}} 110.60$ |  |  |  |  |  |  |  | EL37 | 1.70 | PC86 0.80 | PL509 | 1.10 | UBC81 | 0.46 |
| 1RS | 0.45 0.80 | $\begin{aligned} & 613 \mathrm{~A} 6 \\ & 6 \mathrm{BE} 6 \end{aligned}$ | $\begin{aligned} & 0.28 \\ & 0.38 \end{aligned}$ | ${ }_{6}^{6 F 24} 8$ | 0.80 1.00 | $10 \mathrm{P13} 110.75$ |  |  |  |  |  |  |  | EL41 | 0.75 | PC88 0.60 | PL801 | 1.00 | UBF80 | 0.40 |
| 184 186 | 0.80 0.80 | $\begin{aligned} & 6 \mathrm{BE} 6 \\ & 6 \mathrm{BF} 6 \end{aligned}$ | $\begin{aligned} & 0.32 \\ & 0.55 \end{aligned}$ | $6 \mathrm{CF}^{2} 5$ 6 F 26 | 1.00 0.35 | $\begin{array}{lll}10 \mathrm{Pl3} & 0.75 \\ 12 A B 5 & 0.70\end{array}$ |  |  |  |  |  |  |  | EL81 | 0.85 0.50 | $\begin{array}{ll}\text { PC92 } & 0.05 \\ \text { PC97 } & 0.50\end{array}$ | PL802 | 0.95 | UBF89 | 0.40 0.70 |
| 1T4 | 0.80 | 8BH6 | 0.76 | 6 F 28 | 0.70 | 12AC6 0.60 |  |  |  |  |  |  |  | EL83 | 0.50 0.25 | $\begin{array}{ll}\text { PC97 } & 0.50 \\ \text { PC900 } & 0.48\end{array}$ | PY31 | 0.60 0.35 | UBL21 | 0.70 0.70 |
| 104 | 0.40 | 6BJ6 | 0.55 | BGK6 | 0.80 | 12AD6 0.60 |  |  |  |  |  |  |  | EL85 | 0.48 | $\begin{array}{ll}\text { PC900 } & 0.48 \\ \text { PCC84 } & 0.40\end{array}$ | PY 31 | 0.88 | UC92 | 0.70 0.45 |
| 1 US | 0.75 | 6 BK 7 A | 0.75 | ${ }^{6} \mathrm{~J} / 4$ | 0.80 | 12AE6 0.80 | $\begin{array}{ll}30 \mathrm{AE} 3 & 0.40 \\ 30 \mathrm{Cl} & 0.80\end{array}$ | 50EH5 |  | DK96 | 0.65 | ECC85 | 0.80 | EL85 | 0.48 | PCC84 40.40 | PY80 | 0.40 | UCC85 | 0.45 |
| $1 \mathrm{~V}^{1}$ | 0.65 | 6BN5 6BN6 | $0.48$ $0.80$ | 6J5GT 6 J 6 | 0.40 0.80 | $\begin{array}{ll}12 A L 5 & 0.55 \\ 12 A Q 5 & 0.60\end{array}$ | $\begin{array}{ll}30 \mathrm{Cl} & 0.80 \\ 30 \mathrm{Cl5} & 1.00\end{array}$ | 85L62 | 0.80 0.55 | DL96 | 0.65 0.60 | ECCs | 0 | EL90 | 0.48 | PCC88 0.56 | PY81 | 0.30 | UGF80 | 0.70 |
| ${ }_{2 \mathrm{~A}}^{1 \times 2 \mathrm{~B}}$ | 0.65 0.50 | $\begin{aligned} & \text { 6BN6 } \\ & \text { 6BQ5 } \end{aligned}$ | 0.60 0.25 | $\begin{aligned} & 6 \mathrm{~J} 6 \\ & 6 \mathrm{~J} 7 \end{aligned}$ | 0.80 0.45 | 12ATB 0.40 | $\begin{array}{ll}30 \mathrm{Cl} 17 & 1.10\end{array}$ | 90AG | 2.40 | DM160 | 0.68 | ECC8 | 0.50 | EL95 | 0.35 | PCC89 0.55 | PY82 | 0.35 | UCH21 | 0.80 0.70 |
| 2CW4 | 0.75 | 6BRA | 0.75 | K6G | 0.75 | 12AT7 0.40 | 30 Cl 180.90 | 90 AV | 2.50 | DYE1 | 0.55 | ECC9 | 0.30 | EL821 | 0.60 | PCC189 0.60 | PY83 | 0.38 0.40 | UCH81 |  |
| 2D21 | 0.40 | 6B87 | 1.35 | 6 K 7 | 0.43 | 12AU6 0.45 | $30 \mathrm{Fs} \quad 1.00$ | 90 Cl | 0.75 | DY86 | 0.35 | ECC80 |  | EL822 | 1.40 | PCC806 0.95 | PY800 | 0.40 1.00 | UCL81 | 0.60 |
| 3A4 | 0.45 | 6BW6 | 0.90 | K8G | 0.45 | 12AU7 0.83 | $30 \mathrm{FL1} 10.80$ | ${ }_{807}$ | 2.60 0.60 | DY87 | 0.37 | ECF80 | 0.86 | EM34 | 1.00 | PCF80 0.80 | PY800 | 0.47 | UCL82 | 0.85 |
| 3A5 | 0.75 | $6 \mathrm{BW7}$ | 0.90 0.95 | ${ }^{6 \mathrm{~K} 25}$ | 0.75 0.55 | $\begin{array}{ll}\text { l2AV6 } & 0.45 \\ \text { 12AV7 } & 0.70\end{array}$ | 30 FL 12 <br> 30 FL 14 <br> 0.90 | 807 813 | 0.60 4.00 | E88CC | 0.70 | ECFP8 | 0.85 | EM71 | 0.80 | PCF82 0.35 | PY801 | 0.50 | UCL83 | 0.65 |
| 3BPl | 3.50 | 6BX6 | 0.25 | ${ }_{6 L 7}^{6 L 6 G T}$ | 0.68 | $\begin{array}{ll}\text { 12AV7 } & 0.70 \\ \text { 12AX } & 0.33\end{array}$ | $\begin{array}{ll}30 \mathrm{LL1} & 0.90 \\ \\ \\ \\ \end{array}$ | 866 A | 0.85 | E180F | 1.00 | ECF80 | 1.65 | EM80 | 0.45 | PCF84 0.60 | PZ30 | 0.38 | UF9 | 0.65 |
| 3 S 4 | 0.40 | ${ }^{68 \mathrm{BZ}} 6$ | 0.46 | ${ }_{6 L 18} 6$ | 0.48 | $\begin{array}{ll}\text { 12AX7 } & 0.33 \\ \text { 12AY7 } & 0.75\end{array}$ | $\begin{array}{ll}30 \mathrm{Ll} & 0.40 \\ 30 \mathrm{L15} & 0.95\end{array}$ | 8642 | 0.70 | E810F | 2.90 | ECH8 | 0.30 | EM81 | 0.60 | PCF86 0.60 |  | 0 | UF11 | 0.60 |
| 5 R 4 GY | 0.75 | ${ }_{6}^{6 C 4}$ | 0.35 | 6 L18 <br> 6LD20 | 0.60 | $\begin{array}{ll}\text { 12AY7 } & 0.75 \\ 1284 A & 0.65\end{array}$ | $\begin{array}{ll}30 \mathrm{L15} & 0.95 \\ 30 \mathrm{LI} 7 & 0.85\end{array}$ | 5670 | 0.60 | EABC8 | 00.38 | ECH8 | 0.45 | EM83 | 0.50 | PCF87 1-10 |  | 2.25 | UF41 | 0.65 |
| BU4G | 0.40 0.80 | 6 CbGT $6 \mathrm{CB6}$ | 0.50 | $\begin{aligned} & \text { 6LD20 } \\ & \text { 6N7GT } \end{aligned}$ | 0.50 | $\begin{array}{ll}12 \mathrm{B4A} & 0.65 \\ \text { 12BA6 } & 0.45\end{array}$ | $\begin{array}{ll}30 \mathrm{L17} & 0.95 \\ 30 \mathrm{Pl2} & 1.00\end{array}$ | 5670 6080 | 0.80 1.76 | EAP42 | 0.60 | ECH8 | 0.45 | EM84 | 0.35 | PCF801 0.50 |  | . 10 | UF42 | 0.65 |
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| 5240 | 0.45 | 6 C 47 | 0.60 | 68.7 | 0.45 | 12BH7 70.50 | 30 PL 131.10 | ${ }_{6}^{6360}$ | 1.25 | EBCF80 | 0. |  | 0.70 | EY51 | 0.40 | PCF808 0.80 | TT2 | 8.40 | UF89 | 0.40 |
| 6/30L2 | 0.90 | 6C116 | 0.80 | ${ }_{6867}$ | 0.45 | 12BY7 0.85 | 30 PLL 4 35 l $\mathbf{0 . 6 0}$ | 6939 7199 | 2.25 | EBBF83 | 0.40 | ECL8 | 0.70 | EY80 | 0.75 | PCE2000.70 | TT22 | 3.60 | UL41 | 0.65 |
| 6 AB4 | 0.45 | 6CL6 | 0.60 | ${ }^{68 K 7}$ | 0.50 |  | $\begin{array}{ll}3543 & 0.60 \\ 35 A 5 & 0.75\end{array}$ | 7199 7360 | 0.85 2.20 | EBF89 | 0.32 | ECL8 | 0.55 | EY81 | 0.40 | PCL81 0.50 | U18/20 | 0.76 | 0 L 84 | 0.48 |
| 6 AF 4 A | 0.60 | 60U6 | 0.80 | 68L-GT | T0.45 | 12K7GT0.60 | $\begin{array}{ll}35 \mathrm{A5} & 0.75 \\ 35 \mathrm{B5} & 0.65\end{array}$ | 7360 7586 | 1.50 | EbL31 | 1.50 | ECLB | 0.40 | EY83 | 0.55 | PCL82 0.85 | U25 | 0.85 | UM84 | 0.80 |
| 6 AGS | 0.25 | 6CW44 60 CY 5 | 0.70 0.50 | 68N76T 6807 | T0.45 | $\begin{aligned} & 12 \mathrm{Q} 7 \mathrm{GT} 0.45 \\ & 12 \mathrm{SR} 7 \quad 0.50 \end{aligned}$ | $\begin{array}{ll}3585 & 0.65 \\ 35 \mathrm{C5} & 0.60\end{array}$ | 7895 | 1.50 | EC53 | 0.50 | ECLL |  | EY86 | 0.40 | PCL83 0.65 | U26 | 0.85 | UYIN | 0.50 |
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| 6A38 | 0.80 | 6D3 | 0.85 | 6T8 | 0.88 | 20 Ll 1.10 | $38 \mathrm{L6GT} 0.75$ | ${ }^{\text {A2293 }}$ | 2.80 | EC88 | 0.60 |  |  | EZ | 0.48 0.60 | PCL88 0.48 | US2 | 0.40 | UY4 | 0.48 |
| 6AK5 | 0.40 | 6DC6 | 0.80 | 6U40T | 0.70 | 20 Pl 10.60 | $\begin{array}{ll}35 \mathrm{~W} 4 & 0.40 \\ 35 \mathrm{Z3} & 0.76\end{array}$ | ${ }_{\text {A } 21}$ | 0.80 0.55 | EC92 | 0.86 | EF42 | 0.70 | EZ41 | 0.76 | PCLs8 1.25 | U76 | 0.40 | UY82 | 0.60 |
| 6AK6 | 0.60 | 6DK6 | 0.60 | 6U5G | 0.75 | $\begin{array}{ll}20 \mathrm{P} 4 & 1.10 \\ \\ 2085\end{array}$ | $\begin{array}{ll}35 \mathrm{C3} & 0.76 \\ 35 \mathrm{Z} & 0.40\end{array}$ | ${ }_{\text {A } 231}$ | 0.80 | EC93 | 0.60 | EF80 | 0.80 | ERs0 | 0.28 | PCL800 1.10 | U78 | 0.40 | Y 88 | 0.40 |
| 6AL3 | 0.48 | 6DQ6 | 0.75 | 6U8A 6V6GT | 0.48 0.45 | $\begin{array}{ll}20 \mathrm{PS} & 1.20 \\ 25 \mathrm{CS} & 0.60\end{array}$ | 35Z4G 0.40 | CBL31 | 1.00 | ECC35 | 0.6 1.00 | EF8S | 0.85 | EZ81 | 0.29 | PCL801 0.95 | U191 | 0.75 | W720 | 0.75 |
| 6AMB | 0.37 | 6EH7 | 0.30 | 6X5GT | 0.45 | 2524 Cl 0.35 | $50 \mathrm{B5} \quad 0.70$ | DAF96 | 0.50 | ECC81 | 0.40 | EF89 | 0.88 | GY501 | 0.70 | PF86 0.70 | U281 | 0.55 | 2769 | 8.00 |
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| 6AQ6 | 0.70 | 6EW6 | 0.7 | 6 Y 6 G | 0.8 | 30 Ab 0. | 0CD60 | DK9 | 0.10 |  |  |  |  |  |  |  |  |  |  |  |


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