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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 125 | 419 | BLI 9／6 | 25 LGGT 31 | ECEF9 | 79 | K＇ 61 | 121－ | TDD4 | 71 |
| 184 | 419 | 6L6G 876 | 2524 G \％－ | ECF82 | 76 | K「63 | 519 | $014 / 18$ | $7 / 6$ |
| 1.55 | $4 / 8$ | 6L18 7／9 | 30 F 5 9／－ | ECE 21 | 101－ | KT66 | $18 / 6$ | U25 | $9 / 6$ |
| 174 | 8\％－ | 6LD20 8／8 | 30 LI 8819 | ECH85 | 11／－ | K788 | $27 / 6$ | U26 | $9 / 6$ |
| 2 D 21 | $5 / 8$ | 6P25 12／－ | 30515 11／61 | ECE42 | $10 / 6$ | KTW61 | 5／8 | U85 | 12／6 |
| 3A5 | $6 / 4$ | 6P28 9／8 | 30F4 11／6 | ECHS1 | 6／9 | KTW63 | 5／－ | U37 | 11／－ |
| 364 | $5 / 3$ | $6976{ }^{71}$ | $30 \mathrm{P12}$ 9／－ | ECE88 | 218 | KTZ63 | 71－ | U107 | $12 / 6$ |
| 5U4G | $61-$ | 697GT 819 | $30 \mathrm{PL1} 11 /-$ | ECLSO | $5 / 9$ | MD14 | $71-$ | U191 | 1218 |
| 5YBGT | 6） 6 | 68L7GT 619 | 35A5 0／8 | ECL 82 | 76 | N37 | $8 / 6$ | $\bigcirc 281$ | $9 / 6$ |
| 5Z4G | 8／8 | 6SN7GT B／9 | 35L6GT 816 | ECL88 | 1016 | N78 | 13／－ | 0282 | 15／－ |
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| 830 L 2 | $9 / 6$ | 6VEG 4／9 | 35Z4GT 5／9 | ［［13 36 | $4 / 9$ | PG86 | 818 | U801 | 19／6 |
| 6A8G | 716 | 8VgGT 6／9 | 30L6GT 8／6 | EF38 | 71. | PC97 | $7 / 6$ | पABC8 | 818 |
| 6AK5 | $4 / 9$ | 6X4 4／6 |  | PF40 | 10）－ | Pcces | 616 | UAF42 | 719 |
| 6AQ5 | $5 \mathrm{j}=$ | 6X5G 5／－ | 185BTA 19／6 | EF41 | $9{ }^{1}$ | FCC85 | 716 | URA1 | 616 |
| 6ATG | 51－ | 6X5GT 6／9 | 807 9／6 | EF50 | 818 | Fecss | $11 / 9$ | UBC41 | $8 / 9$ |
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Mains operation. Ready built on plated heavy gauge

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$300-0-300 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 0-5-6.3 \mathrm{v}, 3 \mathrm{a}$
 $350-0-850 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 a, 105-6.3 \mathrm{v}, 9$
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# PRACTIGAL WIRELESS 

## TOPIC DF THE MONTH Troubled Waters

THE first blow was struck against the radio 'pirates' on Friday, 25th November, 1966, when Radio 390 were fined $£ 100$ for using a transmitter without a licence, at Red Sands Tower on 16th August, 1966. Mr. Edward Allbeury and Mr. David Beresford Lye, directors of Radio 390, who were found guilty of the same offences, were each given an absolute discharge.

The second blow came just five days after the Radio 390 case, when Mr. Roy Bates, proprietor and operator of Radio Essex (now known as Radio BBMS) was fined the maximum of $£ 100$ at Rochford Magistrates' Court, Southend. Both 'pirate' radio stations are to appeal against the findings.

Radio City who also operate from one of the war-time forts in the Thames Estuary have not so far been prosecuted under the Wireless Telegraphy Act of 1949 for illegal broadcasting. On the findings of the Canterbury and Rochford Magistrates (court reports inside), Radio City is within territorial waters and it would appear that the Crown could get a conviction. So why have they been missed? Could it be something to do with ownership, or is it that they are not big enough to worry about?

Radio BBMS has openly defied the Government by continuing to broadcast from Knock John Tower in the Thames Estuary, and Radio 390 admits that it will broadcast from another country on the Continent if it loses the pending High Court appeal.

The Marine and Broadcasting (Offences) Bill will give the Government powers to silence all the 'pirates' in one swoop when it becomes an Act of Parliament. But, how long is this going to take? The Government have many Bills on the Statute Book, a number of which they consider to be of more importance. However, even this legislation cannot prevent commercial operators setting-up high power stations on the Continent, which could be beamed to this country.

Realising that the Marine and Broadcasting (Offences) Bill is already in the pipeline, was it worth prosecuting Radio 390 and Radio Essex? The first case took two days to hear and the second one a full day, and cost us-the tax-payer-hundreds, if not thousands, of pounds sterling.
W. N. STEVENS, Editor.
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[^0]
## Imported Communications Receivers

It has come to our notice that a letter appeared in the December 1966 issue of Practical Wireless stating that service and spares were not available for imported communication receivers.

We sell considerable amounts of imported communication receivers, many through the medium of advertisements in this magazine, for all of which we carry spares and have full servicing facilities. $\begin{array}{ll}\text { G. W. Smith \& Co. } & 3 \text { Lisle Street, } \\ \text { London, W.C. } 2,\end{array}$
[As you are probably aware, these servicing and spares facilities are not always available from radio dealers, which inspired the letter from a reader. We are glad, therefore, to hear that at least one company is able to offer such facilities.]-Editor.

## Buy British?

I have a Lafayette catalogue which shows several models of the H.E. range of receivers and all are quoted as being "imported" into the U.S. So that those on the U.K. market are presumably reexports from the U.S.

1 have also been called upon to repair a Sharpe radio of Japanese manufacture which was purchased in Hong Kong and have found that the valves used cannot be purchased in the U.K., there are no equivalents and that letters to agents in Japan and Germany have not produced any results.

I agree with Mr Pryse, one must by very careful what one buys. But beggars cannot be choosers; after all, what British sets are available at such moderate cost as the Jap jobs with the same specifications?

## A. Parry.

South Oxhey, Hertfordshire.

## Transistor Terminology

I used to use valves. However, I have now graduated to transistors. What an utterly wretched mess. Every manufacturer has his own numbering system and, it would appear, his own set of notations. One maker's Ico is another's Alpha dash, and mistaking one manufacturer's beta for another's hybrid pi can cause a very nasty accident. How about all the "big-boys" sitting round a table and settling on a simple standard notation we can all understand?

## Martin Jessopp.

Leyton,
London, E10.

# NEWS AND 

## A.A. MEMBERS GO ON THE AIR

 The world's first $\mathbf{2 4}$-hour two-way v.h.f. car radio link between a motoring organisation and its members on the road-the A.A. Linkline Service-has been introduced. Under the new service, A.A. members in and around London and Birmingham and travelling up the M1 will be able to keep continuous twoway contact with A.A. operations rooms and will be able to radio direct for the breakdown service, pass urgent messages to and receive messages from anyone, receive warnings of traffic jams etc., obtain weather reports and even find out the correct time. Linkline rental of $£ 180$ per year includes all equipment and installation costs, set hire, licence fees, servicing, all radio calls and certain emergency calls connected with a breakdown or accident.
## COURSE ON AMATEUR RADIO THEORY AND PRACTICE

Interested persons are invited to find out more about a proposed course on Amateur Radio and Electronics, to begin shortly. The course will be held in the London Borough of Waltham Forest, and is designed for those who missed the beginning of the normal courses, or who find the location of the R.A.E. courses difficult to reach.
The scheme should be suitable for persons wishing to try the Winter 1967 Radio Amateurs' Exam and for persons who would like to brush up on the subject. Young people and beginners will be made very welcome. K. L. Smith, G3JIX, 82 Granville Road, Walthamstow, E.17.

## NEW LOW PRICED F.M. PORTABLE


H. O. Thomas Electronics announce two new models, bringing their total range of Wien radios up to six. They are the Wien "Sport" retailing at $7 \frac{1}{2}$ guineas and a mains/transistor am/fm set-the M1-at 16 guineas.

The M1 is a table model in teak cabinet, embodies 8 transistors, covers medium and f.m. bands. The "Sport" (see photograph) covers f.m. and medium waves, has 9 transistors and comes complete with earpiece, strap and batteries. Further information from H. O. Thomas Ltd., 4 Vernon Place, London, W.C.1.

## SCHOOLBOYS AND GIRLS EXHIBITION

Opened in the Empire Hall, Olympia on December 27 this exhibition features among its exhibits a TV videotape studio presented by Ampex Ltd., where children are able to mime an action or play a charade and see their performance played back immediately on a TV monitor screen.

# ...COMMENT 

GRUNDIG A.F. SIGNAL TRACER


Among the new Grundig range of test instruments is the SV2 a.f. signal tracer. The use of transistors and battery operation make the instrument ideal for lab. or field work. The test probe type UK2 supplied is switchable between a.f. and r.f. In the r.f. position, it operates as a demodulator for frequencies between $100 \mathrm{kc} / \mathrm{s}$ and $300 \mathrm{Mc} / \mathrm{s}$ whilst the low capacity ensures no detuning of the circuit under test.

Frequency response is $200 \mathrm{c} / \mathrm{s}$ to $8 \mathrm{kc} / \mathrm{s}-3 d B$. Input for 160 mW output in the $O d B$ position is 1 mV and in the $-40 d B$ position 100 mV . Input imperance is $50 \Omega$ on the OdB position and $5 \mathrm{M} \Omega$ in the -40 dB position. Output voltage is 0.9 V and output impedance is $1 \mathrm{k} \Omega$. For further details contact Grundig (Great Britain) Ltd., Newlands Park, Sydenham, S.E. 26.

## SANSUI PRODUCTS

Lasky's Radio Limited have now been appointed sole distributors in the U.K. for Sansui High Fidelity equipment.

The range comprises a complete selection of high quality stereo amplifiers, tuners and combined tuner/amplifiers.

Price list and details are available on application to Lasky's Radio Limited, 3/15 Cavell Street, London, E.1. Demonstrations can be provided at 42 Tottenham Court Road, London, W.1.

## 10,000 POLICEMEN TO HAVE POCKETPHONES

A major contract worth $£ 500,000$ has been awarded by the Home Office to Pye Telecommunications for the supply of Pocketphone u.h.f transceivers. One hundred police forces will shortly be using these units.

TWO ADDITIONS FOR LEKTROKIT
A.P.T. Electronic Industries Ltd., Chertsey Road, Byfleet, Surrey, announce the availability of Chassis Plate No. 7 and Insulator Leadthrough No. 2 in the Lektrokit Chassis Construction System.

Lead-through insulators are connection devices for insertion into
 the Lektrokit No. 7 chassis plate for circuit wiring. They are made of PTFE high grade insulant and the Sealectro "Clover Leaf" connection insert, which provides a multiaperture insulated terminal point for use in circuit wiring on metal chassis and provides five connection wires. Price of No. 7 Chassis Plate is 12s. per pack of 2 and No. 2 Insulators, 3s. per pack of 6 .

## Way-Out Style

As a young boy I was always being caught out by my elder sister. She would plague the life out of me with a series of classic "When is a so-and-so not a so-and-so". As the years drifted merrily by I came to be free of these irritating conundrums, and indeed I had forgotten all about the wretched things until I started to read Practical WireLEsS and then, bless me, there they were again. I refer to these drifting standards. which never seem quite what they are supposed to, and vary from one designer or advertiser to another. Take signal to noise ratio. Now there's plain signal-tonoise, or there's signal-to-noise-plusnoise and so it goes on with a few handfuls of dB's thrown in for good measure. Audio amplifiers are notorious for this sort of treatment. Not only do we have noise figures (no mention of the signal now, only the noise), we have hum, input sensitivity, outputs, impedances and Uncle Tom Cobley ad infinitum. Of course all this information may be very useful but the standard references to which all these figures are referred seem to alter with each item one reads about. One manufacturer assures that his amplifier will supply 12 watts output. Now a friend of mine bought one of these and, as he worked as an apprentice in an electronics laboratory, took the unit in for a test. It was found that the unit actually provided four watts output. These results were checked by a senior member of the staff, and I have no doubt that the tests were valid. So how about a definite standard rating on these things to whichall units are related. Then when we buy a ten watt audio amplifier we will get ten watts and not five or two. These glowing adjectives beloved by advertising agents should be made to be accurate. Could not the magazine accepting the advert check first? If you raise anything with the advertisers they invariably blind you with science. "Ah, that's under quiescent conditions, and assuming that the signal does not exceed one millivolt, of course you could calculate for the input transistor bottoming but then the hum level will be up by about, Ooh let's see now 25 , yes about 25 dB so you can't have it both ways can you?" So how about some standards and every one sticking to them. At the moment I'm back in my childhood memories again. When is a 12 watt amplifier not a 12 watt amplifierwhen it's advertised as such?

## R. Farjohn.

Kettering,
Northants.

## More News and Comment on Page 760

# 3 3 3 3 3 0 0 0 0 <br>  

THE practical preselector design to be described is continuously tunable over the frequency range $14-30 \mathrm{Mc} / \mathrm{s}$ thereby embracing the three high frequency Amateur bands, viz., 10, 15 and 20 metres.

The prototype preselector is used primarily in c.w. connections; it is attractive physically and may be powered from the station receiver. Tuning is carried out via a slide-rule type drive with ' 10 ' and ' 20 ' occupying the scale ends. Ample space does exist for the inclusion of a small mains transformer plus rectifier circuit capable of supplying 200-250V d.c. at 20 mA and 6.3 V a.c. at 1 A .

It is desirable to be able to mute the preselector when an associated transmitter is to be used nearby, and a self-shorting jack-socket is fitted via which a muting circuit may be introduced. The preselector may be muted very conveniently, either fully or partially, by arranging for a $50 \mathrm{k} \Omega$ variable resistor
to be automatically switched in and out of circuit by the transmitter 'Send/Receive' switch. No provision is made for bypassing the unit-by means of a switch perhaps-since this is carried out manually.

Some communications-type receivers used at Amateur and SWL stations use valves that are considered to be 'noisy' by modern standards: by using a preselector between the aerial and the receiver a considerable improvement results particularly on the higher frequency bands. This is understandable since when a strong signal is fed to a 'noisy' receiver the a.v.c. system is loaded adequately and the valves are biased back heavily; the received signal then sounds clean and 'punchy'. It should be noted however that a preselector should not be considered as an alternative to a good aerial but merely an addition.

The complete circuit diagram is shown in Fig. 1 where V1 functions as a high-gain r.f. amplifier with V2 operating as a conventional cathode-follower output stage. The station aerial is plugged in at socket Sk1, either direct or via the transmitter/receiver change-over switch or relay, and a short screened lead from socket Sk3 is connected to the receiver aerial socket. Band coverage is effected by means of VCl , the shaft of which is in connection with the panel-fitted drive and scale. Variable r.f. gain results from fitment of VR1. Amp-

Fig. 1: The theoretical circuit diagram.
lified r.f. appearing at pin 7, V1 'sees' considerable opposition from the r.f. choke whereupon it passes more readily to the cathode-follower output stage via capacitor C5 to re-appear at socket Sk3. Normally the anode circuit of V1 is operated in a non-resonant state, grid circuit tuning being adopted. Extra gain may be obtained however by resonating the anode circuit close to the operating frequency and to this end coil L1 and panel-fitted VC2 are provided. Although, in theory, maximum gain occurs when both grid and anode circuits are


Fig. 2: Above-chassis layout and dimensions.
tuned to the same frequency such exact tuning is rarely practical since oscillation takes over. Under certain conditions-maladjustment of VC2 for example-oscillation can be instigated; it becomes very important therefore to include adequate screening. In the prototype the grid and anode circuits of V1 are well screened from each other; a 'can' is fitted to Tl and the chassis box is also made use of. Screening is indicated by the broken lines in Fig. 1.

Normally VC2 is set to minium capacitance and is used only under difficult copying conditions. The circuit is useful c.w.-wise for as VC2 is manipulated tuning tends to sharpen due to positive feedback. The benefits are somewhat less apparent on 'fone' for the extra gain secured is at the cost of an increased noise level. In this part of the circuit it should be noted that capacitor C9 is a d.c. 'blocker' and it must on no account be omitted!
The layout and most of the wiring is shown in Figs. 2 and 3. No chassis drilling diagram is given since constructors may vary things to suit items to hand. The type of capacitor used for VC1 for example is not over-critical and any small singlegang item of about 150 pF maximum capacitance is suitable. Note in Fig. 2 that the lugs of the can
associated with T1 are bent outward (not inward) to permit the can to be removed without disturbing the coil itself.

## Coil Details

Both T1 and L1 are home-brew dust-cored items. Considering T1, and assuming approximately 30 pF for circuit 'strays', a tuned circuit inductance of some $0.9 \mu \mathrm{H}$ used in conjunction with a 150 pF variable capacitor will enable the desired band coverage to be obtained. Ti consists of 10 turns 28 s.w.g. enamelled copper wire close wound on a 0.3 in . former, and 6 turns of 36 s.w.g. d.s.c. copper wire close wound, for the aerial winding. The two windings are separated from each other by 0.05 in . L1 is 12 turns of 28 s.w.g. enamelled copper wire, turns close. Later, a turn per coil may need to be removed to ensure correct band coverage, coils being tested either by using a g.d.o. when they are in situ, or via received signals. When finding the frequency range afforded by the $\mathrm{T} 1 / \mathrm{VC1}$ combination with a g.d.o. it will normally be necessary to remove the screening can although it should be remembered that re-fitment of this will cause the circuit to resonate at a slightly different frequency to that measured. Fortunately the dust cores permit considerable inductance variation.

The size of the chassis used is also shown in Fig. 2 but when self-powering items are to be used this should be made 2 in . longer.

Details regarding the front panel are given in Fig. 4, matters being so arranged that when the completed assembly is placed on the table the front panel slopes backwards slightly to assist operation of the controls; the appearance also benefits.


Fig. 3: Wiring and layout below chassis.

Casing details are given in Fig. 5 to agree with the prototype which is fashioned from faced hardboard and held together with pins and impact adhesive.
When the preselector is not self-powered a suitable power pick-up socket should be fitted to the main receiver. An international-octal (I.O.) valve holder is ideal for the purpose rigidly situated so


Fig. 4: Panel details.
Fig. 5: Dimensions of the main casing.

that plug P11 carrying the 3 -core supply cable from the preselector can be engaged.

Tests should then be carried out, using an ohmmeter, to ensure that no b.t.-chassis short circuit exists after which a short screened lead from socket Sk3 may be connected to the receiver aerial socket. The receiver may have separate aerial/earth sockets in which case the braid of the screened cable should be connected to the earth socket and the lead associated with capacitor C7 connected to the aerial socket. The receiver is then switched on and this will bring the preselector warning lens to life.

## Alignment

A weak signal is now sought around $14 \mathrm{Mc} / \mathrm{s}$ and the preselector pointer moved fully right to completely enmesh the vanes of VCl . The vanes of VC 2 should be fully disengaged and the dust core of L1 removed. The core of T1 should next be carefully adjusted to increase the strength of the signal tuned using the receiver ' $S$ ' meter as a visual guide.

The receiver is now tuned to the 15 -metre band and a weak signal sought, after which the scale
pointer of the preselector is moved toward mid-scale-or to where the signal sounds strongest. The same procedure is adopted on the 10 -metre band when the preselector pointer should be almost fully to the left of the scale for maximum received signal strength.

Should it seem however that the preselector cannot be tuned down far enough to peak the signal then too much inductance is in circuit and the core of Ti -or the number of turns-requires adjustment. Without the aid of frequency measuring gear some experimenting is inevitable but the aim should be to get ' 10 ' and ' 20 ' peakable at the opposite ends of the preselector scale. VC1 plays a major part in the band coverage and an electrically over-large item is undesirable. Where a good quality variable capacitor is to hand but which possesses excess capacitance, a fixed-value item may be wired in series with it. For example a 250 pF variable may be suitably 'reduced' by including a 470 pF capacitor in series with it-or, alternatively, vanes may be removed.

When the T1/VC1 combination has been dealt with attention may be given to the 'Peaking' circuit, L1/VC2. The core should be lightly inserted in the coil and first tests made on ' 20 ' as before. The normally weak signal, already being amplified by the preselector should be further peakable as VC2 is carefully rotated when L1 is of the correct inductance value.

Although signals are likely to be heard at almost any time of day or night on ' 20 ' none may materialise on ' 10 ', or even ' 15 ' for lengthy periods solely due to unfavourable propagation conditions.

## $\star$ components list

| Resistors: | Capacitors: |
| :---: | :---: |
| R1 $39 \mathrm{k} \Omega$ | C1 10,000pF ceramic |
| R2 $6.8 \mathrm{k} \Omega$ | C2 10,000 pF ceramic |
| R3 $27 \Omega$ | C3 2000 pF ceramic |
| R4 $100 \Omega$ | C4 10,000 p ceramic |
| R5 100k $\Omega$ | C5 50pF silver mica |
| R6 220 2 | C6 2000 pF ceramic |
| VR1 $5 \mathrm{k} \Omega$ pot. (Lin.) | C7 5000 pF ceramic <br> C8 $4 \mu \mathrm{~F}$ electrolytic, 350 V |
|  | C9 2000pF ceramic |
| Valves: | VC1 150 pF variable (see text) |
| V1 EF183 | VC2 100pF variable |
| V2 EF80 | Jackson 'Air tune' |

## Sockets:

Sk1, Sk3-Coaxial type, surface mounting
Sk2-Miniature closed-circuit jack type

## Dial and Drive:

Jackson type SL. 165191 complete

## Miscellaneous:

R.F. choke, 2.6 mH (Denco type RFC5), 0.3 in . Bakelite coil former with dust iron core and screening can (Denco Ref. $5000 \mathrm{~A} / 4 \mathrm{PL}$ ), Coil former with dust iron core (Denco-Ref. 351/8BA), Miniature panel lamp (Eagle PL), Octal plug, Knobs (3), Valveholders B9A (2), Chassis $7 \times 3 \frac{1}{2} \times 1 \frac{1}{2}$ in. etc. and casing materials.

## EXPERIMENTERS CORNER



## TRANSISTORISED COMPUTER

THIS computer uses 20 transistors and 30 diodes. It adds and subtracts, the number input being fed in by a 'phone dial. The answer is read off 10 light-bulbs, which are mounted on top of the case. The answer is of course in binary form, with which the constructor should become familiar. The unit is small compared to anything else of similar function.

## Theory

The computer consists of 10 bi -stable circuits called flip-flops, and the circuit of one is shown in Fig. 1. The circuit works in the following way.

Suppose that Trl is conducting and therefore $\operatorname{Tr} 2$ is cut off, almost all the supply voltage will be across R1 and B. This means that the collector of Trl is nearly at earth potential. However the collector of Tr 2 is nearly 12 volts negative. This means that D1 has only a small negative voltage across it in the reverse direction, but that D2 has


Fig. 1: (Above) Circuit diagram of one flip-flop.
Fig. 2: (Below) Pulses at points in Fig. 1.


## S. BENDA

nearly 12 volts across it in the reverse direction.
Now suppose that a positive pulse appears across the input bar. The pulse will not overcome the 12 volts across D2, but it will overcome the small negative voltage across D1. Thus D1 will conduct


Fig. 3: (Above) Block schematic of "Adding".
Fig. 4: (Below) Block schematic of "Subtracting".

and since the pulse is positive it will reduce the base current of Trl.

This will reduce the collector current of Trl which will make its collector more negative. This increases the base current of Trl. Thus the collector current of Tr2 increases making the negative voltage on it decrease. This decreases the base current of $\operatorname{Tr} 1$, until it is cut off and $\operatorname{Tr} 2$ is conducting. Fig. 2 shows the voltage wave forms in the flip-flop.
N.B.: Negative pulses at the input of a flip-flop have no effect upon it, since they reinforce the reverse negative voltage across D1 and D2. In Fig. 2.

To begin with, the bulb B , which is connected to Tr 1 , is not conducting. A pulse in the base switches it on. Another pulse switches it off and so on. The collector of $\operatorname{Tr} 2$ is, of course, always in the opposite state to the collector of Trl. So it can be seen that a flip-flop can be represented by a little box with a bulb on top of it.

It needs two pulses to switch the bulb through a whole cycle. This shows that the number of pulses which can be obtained from either of the collectors of a flip-flop is exactly half those appearing at the input. This can be verified from Fig. 2. Because each flip-flop divides the number of pulses by two, in the computer each flip-flop will represent twice the number of the preceding one.

So if F.F. 1 represents one, F.F. 2 will represent two, F.F. 3 will represent four and so on. In the actual computer there are ten flip-fiops so that the last flip-flop will represent 512. In Fig. 3 there are, for the sake of simplicity, only three flipflops. The input of each flip-flop (except for the


Fig. 5: Block schematic of the computer. Each box represents one flip-flop as in Fig. 1.
first one) is connected to the preceding collector corresponding to Tr 2 in Fig. 1.

Suppose we start with all the bulbs off, in other words nought. If we dial a pulse into F.F. 1 this will switch on B1. A negative pulse will be sent to F.F. 2 (since the input of F.F. 2 is connected to Tr 2 ) and nothing will happen to F.F.2. We have added nought plus 1 . Now if we dial another pulse into F.F. 1 we will switch B1 off. However a positive pulse will be sent to F.F. 2 and this will switch on B2 which represents 2 . We have added 1 plus 1.

The reader will then be able to work out for himself, that it is possible to add up to 7 on this circuit, but upon adding 7 plus 1 , he will get the answer of nought. The actual explanation of this is that if there were a fourth flip-flop a positive pulse would be sent to this, registering the number 8.

Fig. 4 is similar to Fig. 3 except that it is connected for subtracting. The input of each flip-flop is connected to the pre-


Fig. 6: Suggested power supply. ceding collector corresponding to Tr1 in Fig. 1. Suppose we start with the number 7, that is all the three bulbs on. If we dial a pulse to F.F.1, B1 will be turned off and a negative pulse will be sent to flip-fiop 2, B2 and B3 will be left on corresponding to 2 plus 4 which is 6 . We have subtracted 1 from 7.
If we dial in another pulse we will switch on B1. This will send a positive pulse to F.F.2. This will switch B2 off which will send a negative pulse to F.F.3. So B3 and B1 will be left on corresponding to 4 plus 1 , which is 5 . We have subtracted 1 from 6. Thus, to sum up, we have seen that:
(1) A flip-flop is a circuit which can only be in two states, on and off.
(2) A flip-flop effectively divides the number of pulses appearing at its input by two.
(3) If a number of flip-flops are connected together, the number of each flip-flop is twice that of the preceding one. The total on the computer is of course obtained by adding together the corresponding value of all the bulbs which are on.
(4) The flip-flops can be connected in an adding circuit or a subtracting circuit depending upon whether the input of each flip-flop is connected to the collector corresponding to Tr 2 or Tr 1 , in Fig. 1 of the preceding flip-flop.

## Construction

Details of construction are left to the individual constructor since there are numerous variations and these are simple enough to work out. The recommended order of construction is as follows: the case is built, the power-pack is made, the flipflops are constructed.

Note: A reset bar is included. This makes it possible to set the computer to zero just by pressing a switch. D3, in Fig. 1, is included in each flip-flop so that the flip-flops do not interfere with each other.

## The case

It is clear from the size of the bits which ones fit on top of each other. The first step is to glue and nail A, B, C and G together. A, B and C are all made from $\frac{3}{8}$ in ply, $A$ and $B$ being identical. When these have been assembled, D, E and F are


Fig. 7: Constructional details of the case.
bracketed together by aluminium strips to the shape which they will have when screwed to the sides.

Next, two flip-fiops are constructed on a single printed circuit board. The lay-out of the flip-flops is left to the constructor. The printed circuit board is divided roughly in half and each flip-flop is constructed in it. The earth bar, the negative supply, the output to the two bulbs, and the reset bar are connected to the connections which go to the sockets.

The sockets which are the mechanical suspensions for the flip-flops are screwed to the back $F$ about an inch apart from each other, starting an
inch inside the left side. The bulbs are then mounted on the top E . The connections to the appropriate bulbs are made from the plugs connecting the extreme right plug to the extreme right bulb. This will be the first flip-flop, so that the numbers will go up from right to left as is conventional. All the bulbs are connected to the negative bar. Switch $S$ is a push to test switch, used to reset to zero.

Fig. 5 is a schematic diagram of the computer. When the five plugs have been wired together and to their appropriate bulb connections, only the negative and positive bars which go to the power pack will be left. There will also be the connections to the switch which will be wired later.

The reset switch $S$ and the phone dial circuit are wired in as shown in Fig. 6. The phone dial circuit is so designed that it feeds positive pulses into the first flip-flop by breaking the negative line from the input. (The phone dial is normally shorted but when dialling, it opens.) The reset switch is mounted roughly in the middle of D in Fig. 5.

## components list



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Photograph of the completed prototype computer.
The next thing to do is to construct the power pack in the right hand corner of the case.
The first printed circuit (the first two flip-flops) is plugged in and the input to the first flip-fiop is wired up. The power supply is connected and switched on. The bulb of the first flip-flop ought to switch on and of alternately as each pulse is dialled jn. If it does not work, the flip-flop should be checked, especially for such things as the polarity of the diodes. When this is working, the second flip-flop should be connected to the first through the switch checking that this works. We should now be able to subtract and add up to two. The rest of the flip-flops are made, plugged in and wired to the switch in a similar fashion. It is important to check that when the switch is in one position all the inputs of the flip-flops are connected to the collectors of the preceding flip-fiops corresponding to Tr 2 and when it is in the other position all are connected to $\operatorname{Trl}$ (see Fig. 1).

## Conclusion

The computer should function well. The phone dial gave a little trouble and the constructor is advised to be careful in the type which he buys. The wiring should be of thin single core type wire.

The uses of this computer are mainly demonstrational and educational. It can be used as a counter of pulses, it being able to count up 2,000 pulses a second. However, when it is used as a counter of low repetition frequency pulses, a "squarer" has to be inserted before the input.

PRACTICAL ELECTRONICS
FEBRUARY ISSUE

## AUTO CALENDAR CAR BURGLAR ALARM DOORBELL REPEATER

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# RADIO 390 

 RADIO ESSEX
## Both fined $£ 100$ for illegal broadcasting

## 390 switched-off pending appeal

Essex (BBMS) carry-on

0N Friday, 25th November, Nineteen Hundred and Sixty Six, Estuary Radio Ltd., who up to that time operated Radio 390 from a fort in the Thames Estuary, were fined the maximum of $f 100$ at St. Augustine Magistrates' Court, Canterbury, Kent, for unlawfully "using apparatus for wireless telegraphy, namely a transmitter without a licence, at Red Sands Tower on 16th August, 1966". Estuary Radio's managing director, Mr. Edward Allbeury, and company secretary, Mr. David Beresford Lye, were found guilty of the same offences, but were each given an absolute discharge.

## BROADCAST ON. 773KC/S

The Post Office had no difficulty in proving that Radio 390 had broadcast on approximately $773 \mathrm{kc} / \mathrm{s}$ on 16th August, 1966, without a licence. Four Post Office engineers were called upon to give evidence: one to substantiate no licence had been allocated, and three to give evidence of monitoring the station and making tape recordings of the transmissionfrom Shoeburyness in Essex, Morden Point on the Isle of Sheppey and Herne Bay in Kent.

## UNDER BRITISH JURISDICTION

Establishing whether the former anti-aircraft tower on Red Sands, from which Radio 390 operates, came under British jurisdiction was an extremely complex matter. Sir Peter Rawlinson, Q.C., representing the defendants, told the court that Radio 390 is situated at least six nautical miles off the Kent coast and is thus well outside British territorial waters. John Newey, prosecuting for the Post Office, in this criminal case, did not agree and gave two main reasons to substantiate his claim.

Firstly, under the terms of the Geneva International Convention of Sea, 1958, which was ratified in September 1964 by the British Government the Thames Estuary may be considered as a bay. But only if the amount of water (in area) within the bay exceeds that in a semi-circle drawn-with a 24 -

mile base-line-across the indentation in the coast. Lieutenant-Commander P. B. Beasley, head of Territorial Waters in the Hydrographic Department of the Ministry of Defence, told the court that in his capacity as a naval surveyor he had calculated the amount of water in the bay, with a base-line drawn across the indentation from Walton-on-theNaze to North Foreland, and found that there are 683 sq. miles in the "bay' and five less in the semicircle. His calculations, however, took in water in the Thames up to Greenwich and to Rochester Bridge in the Medway. Defence was not satisfied that this was permissible and laughter accompanied Sir Peter's suggestion of using Greenwich-on-Sea as a holiday attraction for a town situated in Greater London.

The other factor, also based on the Geneva Convention, concerned low-tide elevations, which includes all islands that are un-covered at normal low water. Prosecution claimed that Middle Bank, one of the sandbanks off the Isle of Sheppey, is one and as such forms the inner limit of territorial waters. Although it is marked on Admiralty charts, Mr. V. Davis, master of the Mallard which has been supplying the forts for some time, stated that he had not seen Middle Sands uncovered for at least twelve months and is only uncovered after an abnormal tide.

## CUSTOMS AND EXCISE

Appearing upon a subpoena to give evidence for Radio 390 , Mr. R. Stiff, a customs and excise officer based at Whitstable, Kent, told the court that his superiors had ordered the master of the supply ship Mallard to report before and after visiting the forts in the Thames Estuary. This order, he told the court, had been withdrawn in May 1966; under instructions from the Commissioners of Customs and Excise. He also told the court, under cross-examination, that no duty was levied on the transmitting equipment brought to Red Sands Tower from Rotterdam, and that the customs only require masters' to visit them and fill up a form when they are leaving for the high seas.

## MARINE \& BROADCASTING BILL

Sir Peter Rawlinson, the former Solicitor-General, made reference to the Marine and Broadcasting Offences Bill, which has been introduced by the Goverment to suppress broadcasting from ships, aircraft and certain marine structures. It has not been through all the necessary stages to become an Act, he told the court, but it is a provision to deal with the problem you are faced with today. "If the present laws satisfy you that you have powers to deal with this case, what is the point of wasting the time of the Parliamentary draftsmen?"

Sir Peter explained that territorial waters could be extended by an Act of Parliament. However, The Territorial Waters Order in Council of 1964 had been made under the Queen's prerogative and is not an Act of Parliament. "If you accept that the Order in Council is not good law and is to be treated as if it were in the wastepaper basket, I suggest that you look at the International Convention which says the same thing."

## CHANGING THE BOUNDARIES

Summing-up, Sir Peter Rawlinson said that it was a remarkable thing that this matter which affects the sovereignty of the realm should turn on the evidence of a distinguished officer (Lt.-Cdr. Beasley), but who only held the rank of a LieutenantCommander in the Royal Navy. He also made reference to the fact that no official map or chart indicated changes in territorial waters, concerning this case, and that under the terms of the Geneva Convention the general public must be informed of such changes.

## VERDICT

After a second adjournment of thirty minutes (recall for further technical evidence from Lt.-Cdr. Beasley), Mr. Donald Andrews, Chairman of the Bench, read from a prepared statement: "We find that Red Sands is situated in territorial water. The Wireless Telegraphy Act of 1949 is silent on the question of local jurisdiction, but the territorial waters in question join the coast of Kent and for that reason we are of the opinion that the justices of the County of Kent have jurisdiction in this matter. On the evidence before us, we find the evidence proved."

## EQUIPMENT NOT CONFISCATED

The Post Office made application to the court to confiscate the transmitting equipment, worth approximately $£ 12,000$, and for costs. John Newey, prosecuting for the Post Office told how easy it is to form a new company and start all over again.

After a third retirement, the Bench passed sentence and refused the Post Office the right to confiscate the equipment, and their application for costs.

## NOT GIVEN UP

Immediately after the case had been heard, the Mallard supply ship carried a pre-record tape to Red Sands, on which Mr. Allbeury gave the station's reasons for shut down and notice of appeal. "If we win the appeal", Mr. Allbeury told reporters, "we shall start broadcasting immediately. If it goes against us, we shall operate from another country on the

Continent." He would not say which, but indicated the suggestion to be a last resort.

Radio 390 was founded in September 1965 and was not a 'pop pirate', but broadcast-to quote Mr. Allbeury-"sweet music" for housewives. It had a claimed audience of four million and its profits were said to be in the region of $£ 15,000$ monthly.

## RADIO ESSEX

On Wednesday, 30 th November, just five days after the Radio 390 case, Mr. Roy Bates the owner and operator of Radio Essex was summoned under the Wireless Telegraphy Act of 1949 for using a transmitter without a licence at Knock John Tower in the Thames Estuary. He was also found guilty and fined a maximum of $£ 100$ at Rochford Magistrates' Court, Southend.

Mr Bates, who now calls his station Radio BBMS (Britain's Better Music Station), appeared without council and pleaded that the court has no jurisdiction over the Knock John Tower, since it is more than three nautical miles off the coast of Essex. John Newey, prosecuting for the Post Office, followed the same lines as he used in the Radio 390 case over the Thames Estuary being a 'bay'. He also introduced low-tide elevations, claiming that West Barrow is one. This lies within three nautical miles of Knock John Tower and is marked as a low-tide elevation on Admiralty Charts.

Mr. R. H. Dalton, Mr. J. F. Woods (Assistant Executive Engineers in the Post Office) and Mr. J. H. Ainley (an Executive Engineer in the Post Office) gave evidence of monitoring Radio Essex on 222 metres and locating the station on 16th August 1966, from Herne Bay in Kent, Shoeburyness in Essex and Morden Point on the Isle of Sheppey respectively. The same three men gave evidence in the Radio 390 case. Also as in the Radio 390 case, Mr. W. Goldsmith, a Higher Executive Officer in the Radio Service Department of the Post Office, stated that although application for a licence had been made, no licence had been issued.

Mr. Bates did not cross-examine any of the witnesses and before the magistrate retired told the court "I do not wish to make any statement at all." He did, however, after the decision (and the Post Office's application to confiscate the equipment and for a portion of the costs), state that he wished to make an appeal against the decision and that the question of forfeiture should not be considered until after the appeal. The court made no order about costs or forfeiture.

## STILL ON THE AIR

After the case was heard, Mr. Bates told Practical Wireless that he could not accept the jurisdiction of the court and that he planned to carry on broadcasting from Knock John Tower with his 25 kW Medium Wave transmitter.

> APPEAL
> It is possible that during the interval between going to press and publication of this issue, one or both of these cases will come up before a higher court. Details will, of course, be published in a later issue.

## THE

MWCOLUMN


A$S$ an experiment, we are going to run this column for the next few months, during the main MW DX season.
Over the last few weeks conditions have been good for North America, with occasional West Coast openings-notably KING Seattle on $1090 \mathrm{kc} / \mathrm{s}$ and KOMO Seattle $1000 \mathrm{kc} / \mathrm{s}$. Best times for West Coast is from 0300-0700. As these notes are written, North America is going through a poorer patch, but the South Americans are more prominent and numerous.

Asia has been quite good in the afternoons and late evening periods, examples being Voice of America, Hue (Vietnam), and Lucknow (India) both on 760 between 1600-1700, Kaifeng (China) on 930 and Anwhei (China) on 940 (together with the Brazilian PRF4) around 2130, and Hanoi (North Vietnam) on 1010 at 2200. The best times to listen for Asia are 1330-1730 and 2030-2300 from October to March.

One interesting aspect of MW DX is that you have the opportunity to hear countries you would not normally hear on short waves, such as Bermuda, Bahamas, Gibraltar, Greenland, Jamaica, British Honduras, Liberia, Surinam, Okinawa, and others.

One word of warning to newcomers.. Identification of stations is generally more difficult (apart, of course, from Canadian, USA stations, etc.) since English is not usually employed at all. And since "openings" to certain areas and the reception of particular stations are far less consistent than on short waves, and are therefore far more important in a serious study of propagation, it is essential to be absolutely positive when claiming reception from a particular station. Should any doubt exist, it is important to state that the reception claim is tentative.

As in all hobbies there are occasional black sheep. We get them in short-wave listening-the spasmodic appearance of a reporter who claims reception of difficult or virtually impossible stations. Such antics usually betray the "reporter" but in MW work fictitious claims are much more readily apparent. Fictitious reporting is usually obvious to the experienced DX'er and the culprit is made unwelcome in clubs or asked to leave. Equally true is the fact that an innocent reporter making an improbable claim may easily find himself viewed with suspicion. The answer is easy: make sure of the facts and if doubt exists add the word "tentative".

Most MW DX enthusiasts use some form of loop, which has the great advantage of high directivity. Such a loop was described in the November issue of Practical Wireless, but readers without this issue may obtain details of my own loop on request. All I ask is for return postage to be included (or where applicable overseas, an IRC).

Next month we will give details of recent station changes which have come to hand. In the meantime I would like to hear from readers interested in MW activity and in particular from Asia, the Pacific area or Latin America not only in stations heard but news of any important changes or new stations on the air.

Alastair Woodland


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Constructional details of a low cost variable voltage transistor power supply unit. Range $0-18 \mathrm{~V}$ at currents up to 1 amp . An ideal unit for the amateur workshop.

## STEREO BALANCE

How to use stereo balance control systems to obtain optimum results. Various types of controls are discussed to enable the designer to make the most of existing listening conditions.

MARCH ISSUE ON SALE FEB. 3rd

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WHEN using a dynamic microphone with a valve amplifier often it is necessary to convert the low impedance signal from the microphone into one suitable for feeding the high impedance valve input circuit. This can be done with a transformer, but good microphone transformers are expensive. The device to be described, however, renders a microphone transformer unnecessary, provides extra amplification, and is both cheap to construct and compact in its construction.

## The circuit

The basic circuit of the device is shown in Fig. 1, and consists of a single transistor in grounded-base configuration. A signal from a low-impedance source is applied to the emitter circuit via Cin and the amplified signal, at high impedance, is taken from the collector circuit via Cout.

It is the configuration's ability to function as an impedance transformer which is of particular interest here: the low impedance input is eminently suitable for dynamic microphones, whilst the high output impedance (in the


Fig. 1: Simple impedance converter. region of a megohm) makes the circuit suitable for connection to the high impedance input circuitry of valve amplifiers. Additionally, the configuration is capable of developing significant and useful power gain when so connected. Since, in the grounded case, the current gain is slightly less than unity, the configuration derives its power gain from the high voltage gain. For driving valve amplifiers, it is voltage gain which is particularly required, since valves are voltageoperated devices.
The complete circuit (see Fig. 2) is conventional, and required little original thought on the author's part. The device


Fig. 2. Circuit diagram of the complete unit.
appears to have a fairly flat a.f. response, and an additional point in its favour is its low battery consumption: about $600 \mu \mathrm{~A}$ from the 9 -volt battery.
The choice of Trl does not appear to be particularly critical; an OC71 was used in the prototype simply because it happened to be immediately available. Several different a.f. transistors have been tried in this circuit, all with equal success; a few r.f. types have also been tried, but on the whole, these tended to be noisier. Red spot surplus types are not recommended for the same reason.

It is feasible that some improvement in quality would result if a low-noise transistor such as ACl07 was to be used in this circuit. However, the expense involved would not necessarily be justified by the slight improvement so obtained.

## Construction

The wiring shown is perfectly straightforward and should present no difficulties; details are given in Fig. 3. The transistor is wired into circuit last of all, and its leads must be covered with PVC sleev-


Fig. 3: Component layout on the paxolin board.
ing. This is so that when the whole unit is finally assembled, the transistor may be bent across the tagboard without fear of causing short circuits.
The case of the prototype unit was a discarded 2 oz . tobacco tin measuring approximately $3 \frac{3}{4} \mathrm{in}$. $x 2 \frac{1}{4} \mathrm{in}$. $\times 1 \mathrm{in}$. This tin was found to be particularly suitable, although any available tin of comparable size may be used and drilled accordingly. The drilling details for the prototype are shown in Fig. 4.


Piece of plastic foam wedged between
battery plugs and tin, keeps battery in position

## Final assembly

Layout of the major components within the case are shown in Fig. 6. The tagboard is mounted by means of a $6 \mathrm{~B} . \mathrm{A}$. . nut, bolt and shakeproof washer. A piece of paxolin, the same size as the tagboard ( $1 \frac{1}{2} \mathrm{in} . \times 1 \frac{1}{2} \mathrm{in}$.) is suitably drilled to receive the 6 B.A. bolt, and is placed immediately between the tagboard and the tin so as to act as an insulator (see Fig. 5). It may be found that the centreconductor of SK1 requires shortening by about $1 / 8 \mathrm{in}$. in order to prevent it fouling the tagboard.

Once the tagboard has been secured within the tin, the final wiring details shown in Fig. 6 may be completed. Earthing connections to the tinplate casing are easily made by soldering direct. Finally, the transistor is bent across the tagboard (see Fig. 6). Care is essential here to ensure that the leads are not bent too near the transistor envelope.

## Testing

Having checked all wiring, and ensured that the battery polarity is correct, a low impedance microphone (between 50 and 2002) is connected to SK1 via screened cable (coaxial type), and a similar connection is made from SK 2 to the valveamplifier high impedance input. For those new to the principles of amplifying microphone signals, a loud howling sound may result if the gain control is advanced too far, or if the microphone is too near the loudspeaker. This is known as acoustic feedback, and can be arrested by retarding the main amplifier gain control. However, this is not an altogether satisfactory solution, since to prevent feedback it may be necessary, in extreme cases, to turn the control to such a position that gain is so low as to be of little use. Alternatively, and if space is available, the microphone can be kept well away from the loudspeaker. This is the most generally used solution. The most reliable method of all is to employ a uni-directional microphone which will not pick up signals from the loudspeaker when directed away from it. This, however, is a rather more costly solution.

It will be found that long input leads to the unit will give no trouble, but since the output is at high impedance, the lead joining the unit to the main amplifier should be no longer than is absolutely necessary. Hum troubles may arise if this precaution is not taken.


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THIS article is intended for the beginner, who needs some idea of how to set out his space and equipment before actually beginning to build, and for the established amateur who feels that perhaps he isn't using the area at his disposal as well as he might, and yet does not quite know where to start. The actual layout is, in the end, dependent on the floor and wall space available, but the ideal is a room apart from the rest of the family, in the interests of peace and quiet, this also offers complete freedom from danger to the rest of the family and any visitors. If a separate room is not available, then half a room, a shed in the garden, or a

doing some home building, and consequently deals with power, tools, equipment, light and space.

## Power

Power may be broadly divided into three groups: (1) A.C. mains; (2) D.C., filtered and smoothed; and (3) Low voltage power, ( $9-12$ volts).

First A.C. mains, 15 amps should be enough for most workshops, but make sure the house wiring can stand the load. If the amateur decides to wire his own sockets and distribution board (see Figs. 1 \& 2), it should be tested by the local Electricity

Board before being connected

Fig. 1: Suggested layout for the constructor.
fold-out bench, built into the wall or an old cupboard. It should offer reasonable comfort all the year round, being neither too warm, too cold, or too damp. It all depends on what use the workshop will get. An amateur using commercial equipment will need less space than one who is building his own, or seeking to improve existing equipment.

This article assumes that the enthusiast will be
becase gas pipe, or to a water pipe, because many houses now have plastic water pipes, and this plastic will render the water-pipe earthing circuit useless.

To obtain a good and reliable earth, obtain a length of motor car ignition cable, and bolt and solder the wire to a copper spike. This joint is then painted over with bituminous paint to prevent corrosion, and the spike buried in three to four feet of
damp soil. The wire is then taken into the workshop in the normal way. It is best not to use the electricity mains earth at all, as it can be dangerous. Instead connect all station equipment to this earth, except the receiver and transmitter, if any. Give this a separate earth as far as possible from the first earth, as the earth for a transmitter or receiver can form a part of the aerial system, and thus carry radio frequency power.
A power unit supplying d.c. filtered and smoothed can be provided for equipment without a built-in power pack. Suggested ratings are $250-300$ volts and 6.3 volts, at 200 mA and 4 Amps respectively. All wiring should be kept neat and tidy. Mains wiring should be as far removed as possible from aerial and earth wires for minimum hum pickup, and test equipment leads should not be left dangling, or one day you may be a test meter short! Wire should be of adequate current carrying capacity, and run underneath shelves where possible.
Lastly, low voltage supplies. These should be completely isolated from the mains, and be suitably fused.
(1) A miultirange testmeter. Here, ranges offered is a secondary consideration to the input resistance. No less than 20,000 ohms/volt for accurate readings: better still 50,000 or 100,000 ohms/volt. Best of all is an accurate valve voltmeter, with an input resistance of many megohms/volt.
(2) A signal source. If possible a signal generator with outputs at a.f., r.f. and i.f.- frequencies. If not, a microphone for a.f., and an aerial for r.f. will suffice.
(3) A signal tracer, which can be used in con= junction with the above for fault finding is a good (and cheap) piece of equipment.
(4) A gramophone turntable, arm, and loud, quiet, fast and slow music records could be provided for testing audio amplifiers.
(5) Last, but by no means least, a soldering iron. The author uses a 25 watt instrument soldering iron costing 25 s . and having interchangeable bits, and a replaceable element. In the author's opinion a "quick-heat" iron rated at about 250 watts is not a good bargain, especially when using it with transistors, and, of course the price is much higher. If a 25 watt iron is thought too light as in the case of

## Tools

Buy the best tools available; not only will they last longer and keep their edge longer, but will not slip or become loose fitting in their handles. Multiple screwdrivers are not to be recommended, as the quality is sacrificed for the novelty, and the separate blades are soon lost. A basic tool kit could be as follows:-one 8 in . screwdriver $\frac{1}{4}$ in. blade; one 4 in . screwdriver $\frac{1}{8} \mathrm{in}$. blade; one neon screwdriver 500 , volt rating; three Phillips (crossed head) screwdrivers, small, medium and large tips; one pair insulated electricians' heavy duty pliers; one pair long nose pliers; one pair side cutters; one pair "Bib" wire strippers; one good pocket knife; one set B.A. spanners. These tools should have a rack made for them and should be returned to this rack immediately after use, to stop them rolling under equipment being used, tested or constructed. (See Fig. 1.) An excellent rack can be made from a strip of wood and some Terry clips.

## Equipment

Here again buy the best available. However in this section price alone is not a good guide to the equipment's quality. Buy a well-known make, and the quality will speak for itself. The actual equipment will depend on what the enthusiast decides to concentrate, so only a basic list is given.


Fig. 2: Possible arrangement for the SWL or "Ham".
constructors making up their own chassis, then a 65 watt iron will be large enough.
The best position is with the light on one side of the bench to avoid glare, especially with a window. Lighting should not be fluorescent, as this type of lighting can cause severe radio interference. The author considers that a light of the "Anglepoise" type is almost as good as the fluorescent light, as the fact that it will throw a shadow is offset by its "manouvrability". A window along the adjacent wall will give a good light during the
day, and, perhaps more important, aerial and earth leads can be taken straight outside instead of trailing round the room to the window, picking up hum on the way. The proximity of a window will be very helpful when trying new aerials.

## Space

The efficient use of space requires much thought, and as everyone's taste is different, again only a basic idea is presented. With today's miniature transistor equipment, it may be possible to operate a transceiver from a floor-standing ashtray, but most of us will need more space. Two suggested layouts are in Figs. 1, 2 and 3. Fig. 1 is for the home constructor, and Fig. 2 for the licensed amateur, or, without the transmitter, for the s.w.l. If commercial only gear is used, then the drawers and shelves can be left out, except those needed for books, etc, and the rig placed on a small table against the wall, with enough space for books and charts.
If the bench is to be made from scratch, the best height will be determined by the chair with which it is intended to be used. The chair should be comfortable without causing backache when used for considerable periods! The bench should be well made, as it will have to support a lot of weight, and a few shillings saved now may be pounds spent later when the bench collapses with costly equipment on it. The main point in most stations is the receiver, and this should be placed so that it can be operated for long periods without eye or arm strain. To this end, the receiver tuning dial should be directly in front of the eyes, to avoid parallax error, and should be evenly lit, to avoid eyestrain. The tuning knobs should be about four inches from the bench, and operated with the elbow resting flat on the bench, this position being much less tiring than any other. To make the best of this the receiver should be about one to two feet back on the table. Space should be left for the log, microphone, key, etc., without being cramped. All dials and meters should be within reach while sitting at the bench, and all readable. To achieve this try to get the radio equipment in the right angle of the joint of two walls (see Fig. 3). The bench top should be covered with hard rubber to guard against shock, and should be jointless, to stop dust, bits of solder, and small bolts and screws being lost.

Storage space is most important, and one soon accumulates parts such as nuts, bolts, springs, washers, resistors, coils, switches, etc., and a way must be found to keep them tidy. Small boxes can be stacked on a shelf, a nest of component drawers
bought, and stood on the floor or a table, or if the bench is home made, a number of shallow drawers ( 4 in . - 6 in .) should be constructed. This last method is the method used by the author, and if compartments are added to some drawers, then almost anything can be kept within reach. If the floor space is available, by all means expand outwards, but the only way for many amateurs is up, so make sure all shelving is really safe to carry what is placed on them. Oscilloscopes are cheap compared to the price of human life and limb! Keep the heavy stuff down near the floor, and put only the lighter equipment and boxes on the higher shelves. There is no point in wasting space by having deep shelves and then stacking only at the front, so make the shelves about 6 in . wide, bearing in mind what is written above. Some wall space should be left free for charts, maps (great circle maps are best for "DX'ers"), and QSL cards.

## Surplus

Spare components can be obtained very cheaply by cannibalising old receivers and ex-Government equipment. Chassis and old parts such as resistors and small capacitators can be re-used, but beware of re-using old electrolytics, these are best bought new. If a use can be found for 3 -phase $400 \mathrm{c} / \mathrm{s}$ motors, all the better, but the experience gained in dismantling old equipment is much more valuable, especially with regard to component layout. If receivers and other equipment are repaired, space


Fig. 3: Layout for a "shack" in the house.
should be left in the workshop for these also. Note to the beginners, now. Don't work on a live or even plugged in set, either with soldering iron or screwdriver, it can be dangerous to the extent of killing you!

Secondly, don't be too miserly with cannibalised equipment, or the workshop will look more like a wholesalers than a place for one of the most interesting hobbies there is.

## RUSH NEON DRVER <br> \author{ A. J. BASSETT 

}SINCE publication of the "Low Voltage Neon Indicator" article in the June, 1966 issue of Practical Wireless, several readers have enquired as to the feasibility of a more powerful push-pull transistor circuit whose output would be sufficient to drive a neon bulb. A further suggestion from one reader was that the device should cause a glow around


Fig. 1:Complete circuit of the push-pull neon driver. both electrodes of the neon tube. One or two readers sent along their own suggestions for such a circuit and these were quite good, but unlike that submitted here, used capacitive cross-coupling of the transistors, and were thus more expensive to build.

The device consists of an inductance/ resistance tuned oscillator, whose circuit is shown in Fig. 1; no capacitors are necessary for tuning purposes. This type of oscillator is sometimes used for "battery-to-mains" transistor inverters, for which purpose the components used have larger powerhandling capacities than those specified in this article.

The output waveform is a square-wave with plenty of overshoot as Fig. 2a depicts. Fig. 2b shows the waveform after it has been "clipped" by the firing of the neon. The small "pip" on the leading edge is due to the fact that the neon does not fire until a voltage is reached which is slightly higher than the steady burning voltage of the lamp.

In comparison with the device described in the June issue, this push-pull neon driver is more powerful, and so consumes a lot more current; 20 to 50 mA or more according to the load and other operating conditions. This is sufficient to light
several neon indicators in parallel if series resistors are used, or one neon without a series-resistor will light up quite brilliantly, with illumination provided at both electrodes. By using the circuit of Fig. 3 it is possible to light two neon tubes, each at one electrode. The peak voltage available from the oscillator when off load is over 150 volts; more


Fig. 2a: Output waveform showing clearly the overshoot on both peaks.

Fig. 2b: The same waveform after clipping.

Fig. 3: Modification allowing the use of two neons.
than adequate to fire most of the miniature neon bulbs which are available.

As with the previous article, component layout is left to the ingenuity of the reader, and should present few problems. Due to the simplicity of the circuit, the small size of the components, and the fact that the layout is not critical, the neon driver may be built into quite a small space.

## RECEIVING THE BBC STEREO PROGRAMMES

For some inexplicable reason, the grid of the triode of the circuit in Fig. 7 and the collector of Tr4 in Fig. 8 (article of the above title, December, 1966 issue, page 857) are labelled respectively "from collector of Tr4" and "to triode grid of ECF80".

These markings are, of course, incorrect, and the corresponding points relate to suitable connections
for a stereo indicator, which in the article are referred to as points " $A$ ".

While the error will be obvious to most readers, some may be confused and think that, perhaps, the valve circuit must be partnered with the transistor circuit. This, of course, is not true as the two circuits are entirely separate.-K. Royal.


IN a super-regenerative receiver regeneration is advanced far beyond the point where oscillation commences, but is interrupted at a frequency above audibility. This provides very high sensitivity. The super-regenerative receiver described here uses easily obtainable valves, and tunes approximately $142-150 \mathrm{Mc} / \mathrm{s}$ with the coils employed. Coverage can readily be modified by altering the coils.

A 954 acorn valve is used for r.f. amplification, and to help isolate the oscillating stage from the aerial. Output is coupled to L4 by L3. V2 is the detector. Grid rectification causes a negative grid potential which stops oscillation until the charge has leaked away through R3, when oscillation recommences. The values of R3 and C4 allow this to happen at above audible frequency.

VR1 adjusts regeneration by varying the h.t. voltage applied to V2. In a super-regenerative detector a loud hiss is heard when no signal is present, but this almost ceases when a signal is tuned in. V3 is an audio amplifier, and V4 the output stage.

For smooth regeneration and lack of various feedback effects, a separately decoupled h.t. supply was found necessary for V1 and V2. This is prefer-

## F.G. RAYER G3OGR

ably obtained from a voltage regulator, but satisfactory results are possible by voltage dropping from the 250 V line as shown in Fig. 6.

## Chassis layout

The prototype chassis was $6 \times 6 \times 3 \mathrm{in}$. deep. The panel is supported by large brackets, and these also brace the vertical screen carrying V1, V2 and VC2 (see Fig. 2). This provides a front section with V1 grid and other circuits, while V1 anode and V2 holder tags are behind. The audio stages V3 and V4 are on the chassis.

The vertical screen can be largely wired in advance. Punch holes for VC2, V2 holder, and a clearance hole for V1 (Figs. 3 and 4). The connections in Fig. 3 are when viewing the acorn valve from its shorter or grid end (also see Fig. 2). Care must be taken when soldering, or the valve seal will be broken by heat. Leads are shaped and cut so that there will be no strain on the valve pins, and they are tinned with solder. C 1 and C 2 have


Fig. 1: Circuit diagram of the receiver section.


Fig. 2: Top view of chassis layout. Note the positioning of the components. At these high frequencies the shortest possible leads should be used.
the shortest possible wires. Clean the valve pins, if necessary, and tin the extreme ends with cored solder and a hot iron, which is removed immediately the solder flows. The valve is then soldered in as in Fig. 3, with equal care.

Fig. 4 shows the rear of the screen, leads to V2 and the items in the tuned circuit are kept as short as possible. Fit soldering tags so that tags 4 and 7 of V2 holder may be soldered to them without wire, (Fig. 2). Tag 1 goes to VC 2 at its nearest point (Fig. 2).

## Capacitor modification

VC2 has four moving plates, and two fixed plates, isolated from each other. It was made from a 75pF short wave variable capacitor. The spindle retaining clip was pulled out with a pointed tool, and the spindle and moving plates withdrawn. Unwanted plates were removed from the spindle by bending them from side to side with small flat nosed pliers. If the capacitor has plates assembled on threaded rods, with spacers, it should be taken apart to remove the plates. The rotor had nine moving plates. Counting from the back, leave plates $1,3,6$ and 8 , and remove the others. Remove all the fixed plates one at a time, and note that the capacitor is not a type with the two fixed plates supports joined by a metal strip in front. Replace the spindle. Prepare two fixed plates by cutting off one lug of each. Put one such plate between the front pair of moving plates, and solder it to one support. Put the other plate between the rear moving plates, and solder it to the other support. Each section of VC2 is thus a single fixed plate between two moving plates, double spaced. The capacity is approximately 5 pF each section.

The screen is bolted as in Fig. 2. A coupling and piece of $\frac{1}{4} \mathrm{in}$. rod couples VC2 to the ball
drive, which occurpies a hole in the pand The latter was varnished hardboard backed by fluminium sheet. VCl hasino reduction drive.

Details of winding the coils are as follows: L1; 2 turns of 18 or 20 s.w.g. insulated wire, and placed between the turns of $\mathrm{L} 2 . \mathrm{L} 2$; $4 \frac{1}{2}$ turns of 16 s.w.g. enamelled or bare wire, spaced to $\frac{3}{4} \mathrm{in}$. long. L3; 2 turns of insulated wire at the centre of L4. L4; 5 turns of 16 s.w.g. wire spaced $\frac{7}{8} \mathrm{in}$. long. All coils are $7 / 16 \mathrm{in}$. outside diameter.
To make L2 and L4, straighten the wire and wind turns side by side on a suitable object. Run a small tool round and round between turns, or stretch the coil to the required length. Shape and cut the ends and solder them to the appropriate points. L1 and L3 are made in the same way and fitted as in Fig. 2.

RFC1 is 70 turns of 34 s.w.g. enamelled wire, close wound on a $5 / 16 \mathrm{in}$. diameter former. It was a push fit on a bolt attached to the artical screen. Adhesive is applied to the ends of the winding only.

RFC2 is wound on a $2 \frac{1}{2} \mathrm{in}$. piece of $\frac{1}{4} \mathrm{in}$. diameter insulated rod. Secure 34 s.w.g. enamelled wire near the top. Wind 70 turns side by side and again secure with adhesive or tape. Bind the extreme bottom of the rod with a few turns of bare wire, and solder on a tag bent at right angles. This tag is bolted to the chassis, and is an earthing point for C5 (Fig. 2). Solder the top choke lead to the centre of L4. Other v.h.f. type chokes should be satisfactory.

## Audio amplifier

The audio and output stages are wired as in Fig. 5. Any slight leakage in C7 or C9 will upset the audio stage grid voltages, therefor these capacitors should be tested if not new. A tag strip anchors the two h.t. positive supply leads. Insulated leads for power supplies and speaker pass through a


Fig. 3 (above): Top chassis screen viewed from the front. Fig. 4 (below): Top chassis screen viewed from the rear.

hole in the chassis. If the speaker transformer is separate, and not attached to the speaker, the transformer could be bolted to the chassis underneath, near V4. When using a speaker with transformer attached, remember that the h.t. voltage is present on connections from receiver to transformer primary.

Current can probably be taken from an existing power pack. The heaters require 0.9 A at 6.3 V . The audio stages draw approximately 60 mA at 250 V . Current required at the $130-150 \mathrm{~V}$ point is small, depending on the setting of VR1, and averages about $4-6 \mathrm{~mA}$.

## Power supply

A suitable power supply circuit is shown in Fig. 6 , and can be modified in some cases to suit items to hand. The 6.3 V winding may be rated at more than 1A. If this winding can supply 2A or more,


Fig. 5 (above): Under chassis wiring of the receiver.
Fig. 6 (below): Circuit of a suitable power supply.


## components list

## Capacitors:

C1 2000pF 150 V disc ceramic
C2 2000 pF 150 V disc ceramic
C3 2000pF 250 V disc ceramic
C4 50 pF mica
C5 2000 p 250 V disc ceramic
C6 $0.25 \mu \mathrm{~F} 250 \mathrm{~V}$ paper tubular
C7 $\quad 0.01 \mu \mathrm{~F}$ ceramic or mica
C8 $25 \mu \mathrm{~F} 12 \mathrm{~V}$ or similar electrolytic
C9 $0.01 \mu \mathrm{~F}$ ceramic or mica
C10 $25 \mu \mathrm{~F} 25 \mathrm{~V}$ or similar electrolytic
C11 $0.01 \mu \mathrm{~F} 350 \mathrm{~V}$
C12 $8 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic
C13 $16 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic
C14 $8 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic
VC1 15 pF variable
VC2 $5+5$ pF variable (see text)
TC1 30 pF air spaced concentric trimmer
VR1 $50 \mathrm{k} \Omega$ linear pot.
VR2 $500 \mathrm{k} \Omega$ log pot.

## Resistors:

| R1 | $100 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R6 | $100 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ |
| :--- | :--- | :--- | :--- |
| R2 | $1 \cdot 2 \mathrm{k} \Omega \frac{1}{2} W$ | R7 | $470 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ |
| R3 | $8.2 \mathrm{M} \Omega \frac{1}{2} \mathrm{~W}$ | R8 | $270 \Omega 1 \mathrm{~W}$ |
| R4 | $33 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R9 | $6 \cdot 2 \mathrm{k} \Omega 3 \mathrm{~W}$ |
| R5 | $2 \cdot 2 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ | R10 | $10 \mathrm{k} \Omega 3 \mathrm{watt}$ |

## Valves:

| V1 | 954 acorn | V4 | 6BW6 |
| :--- | :--- | :--- | :--- |
| V2 | 6 C 4 | $\cdot$ | V5 |
| V3 | 6 C 4 |  |  |

## Miscellaneous:

Two B7G holders, One B7G screen, B9A holder, L1, L2, L3 and L4, RFC1 and RFC2, see text, Ball drive, Co-axial socket, 10 H 80 mA choke, Mains transformer $250-0-250$ at $80 \mathrm{~mA}, 5 \mathrm{~V}$ at $2 \mathrm{~A}, 6.3 \mathrm{~V}$ at 1 A, Switch 1 pole 2 way, 4 -sided chassis $6 \times 6 \times 3$ in., $6 \times 3$ in. flanged runner (Home Radio), $6 \times 6$ in. panel, Two panel brackets about $5 \times 5$ in;, Knobs, tag strip, etc.
and there is no 5 V winding, a 6.3 V rectifier such as the EZ81 can be used, in which case the rectifier cathode is taken to the h.t. smoothing choke only, and all heaters are then in parallel.
H.T. drain can be kept down to a suitable level for a 60 mA transformer by using $12 \mathrm{k} \Omega$ and $20 \mathrm{k} \Omega$ resistors instead of $6.2 \mathrm{k} \Omega$ and $10 \mathrm{k} \Omega$, and by increasing R8 to $330 \Omega$. Smoothing capacitors need not be the values shown, and can be 350 V or 450 V . The choke is any small 60 mA or 80 mA smoothing type. The power supply is built on a separate chassis, size to suit individual components.

## Receiver adjustment

With L4 wound as described, TC1 is almost completely open for the $144 \mathrm{Mc} / \mathrm{s}$. band. A very small adjustment of TCI has considerable influence on waveband coverage. Later, it can be rotated

NIDE

## 95 K디s - 85 M 디s

THIS generator is suitable for receiver calibration and alignment, and for quick stage-by-stage checks of r.f., i.f. and audio circuits. Unmodulated (c.w.) or modulated r.f. output is available on fundamentals through all frequencies from $100 \mathrm{kc} / \mathrm{s}$ to $80 \mathrm{Mc} / \mathrm{s}$, and harmonics may be used up to $160 \mathrm{Mc} / \mathrm{s}$.
Figure 1 shows the circuit, which is for a.c. mains operation. The 6 -way switch S1A and S1B selects any of six coils (L1 to L6) which are tuned by VCl . The coverage obtained by the author was as follows, but the extreme ends of each band are unused: Band 1, $95-360 \mathrm{kc} / \mathrm{s}$; Band 2, 280-1050 $\mathrm{kc} / \mathrm{s}$; Band 3, $890 \mathrm{kc} / \mathrm{s}-3 \cdot 3 \mathrm{Mc} / \mathrm{s}$; Band 4, $2 \cdot 4-$ $10.5 \mathrm{Mc} / \mathrm{s}$; Band $5,7.25-36 \mathrm{Mc} / \mathrm{s}$; and Band $6,30-$ $85 \mathrm{Mc} / \mathrm{s}$. All ranges are with the full 180 -degrees rotation of VCl , except for Band 6, which is covered by approximately half-capacity ( 90 -degrees rotation). All the coils are of fixed inductance, to avoid possible loss of calibration.
One triode section of the 12AU7 acts as r.f. oscillator, with output from the cathode via C3 to the 6BA6 amplifier and mixer. The remaining triode section functions as an audio oscillator, with injection to the 6BA6 suppressor grid; VR1 allows control of the output. The 3-way switch S2A and S2B provides oscillator switching.

A small convertor type mains transformer supplies h.t., the drain being about 20 mA at 165 V . The two heaters need $6.3 \mathrm{~V}, 0.6 \mathrm{~A}$. The h.t. line voltage is not too important, but oscillation may cease on Range 6 if this is much under 160 V .

## Case

A neat, strong and inexpensive aluminium case was made by the author from "Universal Chassis" members; using two 10 in . x 3 in . runners, two $8 \mathrm{in} . \times 3 \mathrm{in}$. runners and two 10 in . $x 8 \mathrm{in}$. plates. Assembled, these provide a cabinet measuring 10 in . x 8 in . $\times 3 \mathrm{in}$. A further 10 in . x 3 in . runner acts as chassis.

A different cabinet or case already to hand could probably be used and the layout is not likely to prove critical except for the r.f. oscillator.

The 10 in $\times 3$ in. runner has its corners cut so that the case sides will fit (Figs. 2 and 3) and it is bolted to the panel so that its surface is $2 \frac{3}{4}$ in. from the lower edge. The valveholders and mains transformer are fixed as in Fig. 2. VCl is attached to the panel with three countersunk bolts; spacers being placed between panel and capacitor. A well insulated lead is soldered to the lower fixed plates tag before mounting the capacitor, and this passes directly through a hole in the chassis. A short lead also connects the rotor contact tag to another bolted to the chassis. Nearly all wiring is done before fixing the case sides.

## Under the chassis

Wiring and components are shown in Fig. 3. Place the bandswitch so that the shortest possible leads may be used from S1A to R1, C1, and tag 7 of the valveholder. Leads to C2 should be very short, and also from tag 8 (cathode) to S1B.


## GENEAATO

R. F. GRAHAM

Heater and h.t. lines can run against the chassis. A tag strip was used as anchor points for C7 and the leads from L7. All wiring should be rigid, the coils being left until last.

The function switch can be wired from Fig. 4. Section S2A applies h.t. to the r.f. oscillator in both "CW" and "MOD" positions. Section S2B supplies the audio oscillator with h.t. in both "MOD" and "AF" positions.

## Audio choke

L7 is an audio choke, the capacitors C6 and C7 providing an effective centre-tap. A small transistor receiver output coupling transformer was used by the author, whilst almost any transistor driver transformer or other small audio choke or transformer could be employed. The winding carries no direct current.

If the component has more than one winding, each winding can be tried separately, or both can be used in series, reversing connections to one if necessary. This allows the tone produced to be modified. It is also possible to lower the pitch by increasing the values of C6 and C7, or raise it by reducing these values. When first testing the generator, it is best to listen to the audio output with headphones.

## Coils

In view of the large number of turns, ready. made coils were used for Bands 1 and 2. The coils for Bands 3 to 6 were home wound. Each coil has a single winding (or easily-arranged equivalent) with A going to S1A, tapping B to S1B, and the end to chassis (see Fig. 5).


As it is difficult to tap small ready-made coils, extra turns were added for Bands 1 and 2. These extra turns can be looked on as a continuation of the main winding, and are in the same direction. Therefore the earth end of the original winding is now joined to the beginning of the extra coil, and forms the cathode tap B. The end of the new winding C goes to chassis.

Band 1 ( $100-350 \mathrm{kc} / \mathrm{s}$ ) This was a surplus long wave aerial type coil, with 6 turns added to provide a tapping, as already described. A piece of ferrite $\operatorname{rod} 3 / 8 \mathrm{in}$. in diameter and $1 \frac{1}{2} \mathrm{in}$. long was pushed into the coil and cemented. Another coil was also found suitable, with tuned and coupling windings connected in series to increase the inductance. An unmodified l.w. coil can be expected to give coverage to about $150 \mathrm{kc} / \mathrm{s}$.

Band 2 ( $300-1,000 \mathrm{kc} / \mathrm{s}$ ) This was also an old long wave aerial coil with the coupling winding and core removed, and some turns unwound until suitable coverage was obtained. Five turns are re-wound to give a tapping five turns from earth.

Band 3 (Calibrated $0.9 \mathrm{Mc} / \mathrm{s}$ to $3.3 \mathrm{Mc} / \mathrm{s}$ ) This is 74 turns of 32 s.w.g. d.s.c. wire, found in a compact pile on a $\frac{1}{2}$ in. diameter former (Fig. 3); tapping B is six turns from C.

Band $4(2 \cdot 5-10 \mathrm{Mc} / \mathrm{s})$ This coil has 50 turns of 32 s.w.g. enamelled wire, side by side on a $\frac{1}{2} \mathrm{in}$. diameter former, with tapping B two turns from ${ }^{2}$.

Band $5(7 \cdot 5-34 \mathrm{Mc} / \mathrm{s})$ This is also on a $\frac{1}{2}$ in. former, and has seven turns of 24 s.w.g. enamelled wire side by side, with tapping $B$ one turn from $C$.

Band $6(32-80 \mathrm{Mc} / \mathrm{s})$ This is $3 \frac{1}{2}$ turns of 16 s.w.g. wire $\frac{1}{2} \mathrm{in}$. outside diameter and $\frac{5}{8} \mathrm{in}$. long. End A

Fig. 1: (Left) Complete circuit diagram of the wide range signal generator.

Fig. 2: (Right) Top view of the chassis.

is $\frac{1}{4} \mathrm{in}$. long and end C is $\frac{1}{2} \mathrm{in}$. long, soldered directly to switch and a tag bolted to the chassis (Fig. 5); tapping B is $1 \frac{1}{2}$ turns from C.

All the coils, except that for Band 1, are aircored. Various ready-made coils are likely to be satisfactory. If those with cores are employed, it makes it easier to obtain correct coverage, but the cores must be sealed before calibrating the generator.

## Bandswitching

Connections are shown in Figs. 3 and 4. Leads to the Band 5 coil should be as short as possible. For Band 6, the coil is placed and connected as shown in Fig. 5. The switch has two wafers, and should be connected as in Fig. 4 so that the shortest possible circuit is obtained for Band 6 .

It was found that with a smaller coil for Band 6, giving coverage up to $100 \mathrm{Mc} / \mathrm{s}$, r.f. oscillation tended to cease towards the top end. Oscillation was maintained up to over $85 \mathrm{Mc} / \mathrm{s}$ with the coil shown and thus the second harmonic allows output up to $170 \mathrm{Mc} / \mathrm{s}$.

Each coil is electrically separate from the others, so can be checked or modified individually, if necessary. No changes should be made after calibration, of course, and the whole instrument should be kept in its case.

## Scales and cursor

A semicircular scale of thin white card (73 in. in diameter) cemented to the panel was used by the author. The cursor was cut from perspex and fixed to a large knob by three self-tapping screws. A hair-line was scribed along the underside of the cursor and six equally-spaced $1 / 16$ th in. holes drilled on this line, so that calibration marks could be made by placing a pencil point in them.

The knob, with cursor, is locked to the capacitor spindle. The six semicircles can then be drawn by pplacing a pencil or "Uno" type pen in the appropriate holes. Mark with dots maximum and minimum settings on the outer scale, so that the cursor can be replaced correctly if removed.

The holes were also found very helpful when calibrating the generator. Markings were made in
pencil, then in ink after a final check. With care, the accuracy should be at least equal to that of the popular type of "off-the-shelf". generator: There are several methods of providing calibration, depending on the equipment to hand.

## Use of harmonics

Calibration of the generator (or a receiver) may be aided by employing generator harmonies, multiples of frequency. If a receiver is tuned to the long wave Light Programme, this is $200 \mathrm{kc} / \mathrm{s}$. With the switch at CW , tune the generator until its output heterodynes with the Light Progamme signal. This is easily done by using Range 1, closing VCl from minimum position. The heterodyne whistle on the receiver falls in pitch towards the correct generator tuning point, rising again as this point is passed. This will also happen with harmonics. The receiver merely compares the generator and Light Progamme (or other frequency standard) sienals. The generator can thus be calibrated at $200 \mathrm{kc} / \mathrm{s}$. Further rotation of VCl will produce a similar heterodyne. This is $100 \mathrm{kc} / \mathrm{s}$ (VC1 nearly closed) and can be marked.

With the generator returned to $200 \mathrm{kc} / \mathrm{s}$ (zero beat with Light Programme) its output can be tuned in on the receiver at multiples. That is, 400 , $600,800 \mathrm{kc} / \mathrm{s}$, and so on. If the generator is tuned to $100 \mathrm{kc} / \mathrm{s}$ as described, its harmonics appear at $200,300,400,500,600,700 \mathrm{kc} / \mathrm{s}$, and so on. This allows accurate calibration of a receiver at $100 \mathrm{kc} / \mathrm{s}$ points.

By tuning the generator to $200 \mathrm{kc} / \mathrm{s}$ (zero beat with Light Programme) 1Mc/s can be found accurately on the receiver (5th harmonic, 300 metres on medium waves). If receiver tuning is then left untouched, the generator can be tuned to $1 \mathrm{Mc} / \mathrm{s}$ in Ranges 2 and 3. This can be marked. So can generator frequencies providing harmonics on $1 \mathrm{Mc} / \mathrm{s}$. That is, $500 \mathrm{kc} / \mathrm{s}, 250 \mathrm{kc} / \mathrm{s}$ and $125 \mathrm{kc} / \mathrm{s}$. The receiver can also be tuned to harmonics $1 \mathrm{Mc} / \mathrm{s}$, allowing calibration at $2,3,4,5,6 \mathrm{Mc} / \mathrm{s}$, and so on.

When proceeding in this way, an all-wave recejver with a large dial is very useful. A t.r.f. receiver with regeneration just sufficiently advanced to cause a heterodyne is perfectly satisfactory. A superhet should have some form of tuning indicator, or a b.f.o.


Fig. 3: This drawing shows the underside wiring.

1


Fig. 4: S1A \& S1B switch connections.
To avoid errors, calibrate the generator by beating its output (at a harmonic, if necessary) with a known signal. Working from $200 \mathrm{kc} / \mathrm{s}$ as described will locate $2.5 \mathrm{Mc} / \mathrm{s}$ so that M.S.F. on this frequency can be heard (most of the transmission is one second pulses). This allows $2.5 \mathrm{Mc} / \mathrm{s}$ to be confirmed on the generator, and with its tuning untouched allows, $57.5,10 \mathrm{Mc} / \mathrm{s}$ and other harmonics to be found on the receiver with great accuracy.

## Crystal marker

A $100 \mathrm{kc} / \mathrm{s}$ or $1 \mathrm{Mc} / \mathrm{s}$ crystal marker is used by many short wave enthusiasts, and permits quick calibration. Adjust the receiver to marker pips in turn, tune the generator, and mark its scale. By beating generator harmonics with marker harmonics, the scale can be sub-divided as necessary. For example, $50 \mathrm{kc} / \mathrm{s}$ markings may be found with

## $\star$ components list

Resistors: ( $\frac{1}{2}$-watt except where stated)

| R1 | $47 \mathrm{k} \Omega$ | R5 | $22 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- |
| R2 | $100 \mathrm{k} \Omega$ | R6 | $2.2 \mathrm{M} \Omega$ |
| R3 | $22 \mathrm{k} \Omega$ (1-watt) | R7 | $1 \mathrm{k} \Omega$ |
| R4 | $47 \mathrm{k} \Omega$ | R8 | $390 \Omega$ |
| VR1 | $50 \mathrm{k} \Omega$ |  |  |

VR1 $50 \mathrm{k} \Omega$ potentiometer

## Capacitors:

C1 100pF
C7 $0.01 \mu \mathrm{~F}$
C2 2000pF
C8 $0.01 \mu \mathrm{~F}$
C3 20pF
C9 $0.01 \mu \mathrm{~F}$
C4 $1000 \mathrm{pF}, 1 \mathrm{kV}$
C5 1000 pF

## VC1 500pF air spaced

## Switches:

S1A/S18 2-wafer, 2-pole 6-way
S2A/S2B 2-pole 3-way C10/C11 $16 / 8 \mu \mathrm{~F}$ or similar 350 V electrolytic

Valves:
$12 \mathrm{AU7}$ (or ECC82) and 6BA6

## Miscellaneous:

L1-L7 as described, B9A holder, B7G holder, coaxial socket, mains on/off switch, 250 V 25 mA contact cooled or similar rectifier ( $\frac{1}{2}$-wave), mains transformer ( 220 V 20 mA HT $\frac{1}{2}$-wave, 6.3 V 0.6 A ), Universal Chassis box $10 \times 8 \times 3$ in., $10 \times 8$ in. back plate, $10 \times 3 \mathrm{in}$. extra runner, mains cord, tag strip, etc.

a $100 \mathrm{kc} / \mathrm{s}$ crystal if the receiver is tuned to the generator's 2 nd harmonic. Then $150 \mathrm{kc} / \mathrm{s}$ on the generator is $300 \mathrm{kc} / \mathrm{s}$ on the receiver, while 250 $\mathrm{kc} / \mathrm{s}$ on the generator is $300 \mathrm{kc} / \mathrm{s}$ on the receiver, while $250 \mathrm{kc} / \mathrm{s}$ on the generator is $500 \mathrm{kc} / \mathrm{s}$ on the receiver, and so on, the $100 \mathrm{kc} / \mathrm{s}$ multiples being from the crystal.
To avoid counting off $100 \mathrm{kc} / \mathrm{s}$ intervals over high frequency bands if a $1 \mathrm{Mc} / \mathrm{s}$ crystal is not available, the $1 \mathrm{Mc} / \mathrm{s}$ point can be found from the $100 \mathrm{ke} / \mathrm{s}$ crystal, then used to mark $1 \mathrm{Mc} / \mathrm{s}$ points, later confirmed if necessary with the $100 \mathrm{kc} / \mathrm{s}$ harmonics.

## Accuracy

Any equipment should be switched on for 20 minutes or so, before using it to calibrate the generator, which should have also thoroughly warmed up. As the calibration procedure only has to be done once, care should be exercised. There is usually no need to rely on visual re-setting of the receiver or generator, during calibration, because settings are found by heterodyning the signal or its harmonics.

## Wavemeter or G.D.O.

Various surplus and other wavemeters of good accuracy are available. If one is to hand, and has a milliammeter indicator, it can be used by coupling it as loosely as possible to the generator coil. This gives a quick method of calibrating the scales lightly in pencil, as a useful guide to subsequent more accurate calibration as previously described.

A grid dip oscillator can be used in the same way, the signal generator being switched off. Couple the g.d.o. lightly to the appropriate coil. If this is done carefully, with an accurate g.d.o., results will agree very nearly with final calibration, and are thus a useful guide to avoid counting harmonics.

## Calibrated generator

If a calibrated generator of sufficient accuracy can be brought into use tune it in on a receiver, and tune the home-built generator to the same frequency, marking the scale. Remember that the

## Imported Receivers

With reference to Mr. Pryse's letter on page 564 of the December issue of Practical Wireless, I should like to clarify a few points.
Lafayette receivers are NOT manufactured in New York, they are made in Tokyo, Japan, for their own subsidiary in New York which merely acts as an outlet to the trade. However, I do feel that the retailers in the U.S. could have replied though Mr. Pryse states to the contrary. This may be due to his letter having been referred to Japan.

Further to the above remarks, I think that the British dealers who sell knowingly Japanese products under the guise of American ones deserve exposure, and do not accept ignorance of facts as an excuse. No self-respecting dealer buys from an unknown source-though with what I think is junk being offered in the way of so-called kits, I do not believe that there can be many self-respecting radio component dealers in this country. Cpl. T. K. Offord. Shrewsbury, Shropshire.

## Communications through the ground

Some time ago I made some experiments with 4 watt amplifiers for ground communications. I found that 200 yards was about the limit of these amplifiers. I then tried using a pair of AC2PEN DD valves in push-pull; this being little better. When I added a d.c. bias to the signal, I was received slightly more than half a mile away. (My earths are about 30 yards apart.)

I then thought of discarding my equipment which was made up of bits and pieces from the junk box and investing in some new components with which to build a somewhat more powerful circuit suited better to ground communications.

Before taking this step, I thought it wise to make sure that the use of highpower transmitters would not contravene any of the GPO licensing laws, so I wrote to the GPO at St. Martin's-LeGrand, who informed me, and I quote, "that this particular system is licensable under the Wireless Telegraphy Act of 1949. Before we could consider an application for a licence authorising its use, we should need to know the purpose of the installation and the type of messages you would propose to pass."

I hope that this information may be of use to those readers who may dabble in the fascinating subject of Ground Communication.
A. J. Clapton.

Trowbridge,
Wiltshire.

## NEWS AND..



The UA7O is a new auto/manual unit designed by BSR. The 11in. diameter turntable is driven from a dynamically balanced, four pole induction motor located on butyl rubber mountings. The low mass pickup arm, supported on horizontal ball bearing pivots, is of lightweight tubular aluminium and is counter-balanced vertically and laterally. After balancing, the stylus pressure is set by a rotary stylus pressure control calibrated from 0-6 grammes. A mechanical cueing device allows the pickup to be raised or lowered at any selected point on a record when it is played manually.

Another feature is the automatic pickup lock which secures the arm to its rest when a record has been played.

Any standard mono or stereo cartridge may be fitted but the BSR C1 ceramic cartridge is ideally suited to this unit. Wow is below $0.2 \%$ r.m.s. Flutter, below $0.06 \%$ r.m.s. and rumble is $-29 d B$ at $1 \mathrm{kc} / \mathrm{s}$. Finish is in satin black with black turntable mat inlaid with brushed aluminium rings. Price is $£ 12.18 \mathrm{~s}$. 3 d. without cartridge.

## "BUYING SECONDHAND"

"Buying Secondhand" is one of the newest in the Consumers" Association paperback Consumer Publications series. It suggests where to look and what to look for when you are buying anything from a camera to a sewing machine and from a television set to a golf club. The section that deals with the buying of secondhand radios and TV's is of great value to the non-technical as it points out all the snags and pitfalls that one may fall into. It makes clear all the points that one may not at first look for and think of when making a purchase and we think that this book would be an invaluable addition to most people's bookshelves. The price is 8 s . and it is obtainable from any bookseller or from the Consumers' Association, 14 Buckingham Street, London, W.C.2.

## COMMENT

## THE EXHIBITION THAT WASN'T!

Britain's first National Hobbies Fair opened at the Royal Horticultural Society's Hall in London on November 12th. The-exhibition terms of reference was hobbies in general-collecting of. coins, stamps, models, etc., stands for the do-it-yourself enthusiast; boat building; pottery; marquetry; orchid growing-and amateur radio.

Fired with enthusiasm we went along, principally to have a look at two exhibits of particular interest-the British. Amateur Television Club and the Paddington Amateur Radio Society. When we arrived, on the afternoon of November 16, we found that the BATC had fled the scene due, so we were told to "lack of interest by visitors", leaving behind nothing but an empty stand. Shaken but philosophical we looked in on the display of the Paddington radio club. The stand was there all right, complete with the club transmitting station G3PAD/A, but the stand was unattended and draped in a shroud!

Instead we went to see a demonstration of hand-operated printing machines which, if not of radio or TV interest, was at least still alive and kicking.

## A NOTE FROM MARTIN ELECTRONICS

Martin Electronics Ltd., regret that they have fallen rather behind with replying to letters from customers.

They apologise for any inconvenience that this may have caused readers and hope the delay will not be too long.

## NAVAL OFFICER WINS FOURTH PLACE



Sub. Lt. D. Davies, R.N. won fourth place in an international amateur radio contest organised by the Certificate Hunters Club. In addition to winning fourth place, he won the European title in the contest, open to amateur radio operators throughout the world. During the 54 hours of the contest, Sub. Lt. Davies made contact with 348 stations. The photograph shows Sub. Lt. Davies operating his radio station at his home in Msida, Malta.

## S.W. Broadcast Stations

I refer to Mr. R. Ronai's letter in the December issue on page 588 attacking my letter.

In my opinion he appears to have got hold of the wrong end of the stick. I was not talking about non-broadcast assigned frequencies when referring to Radio Moscow and the like.

The point is that Radio Moscow and others are deliberately filling up the Broadcast Bands with distorted modulation jammers which instantly wipe out stations on at least two adjacent channels-in Cyprus, for, most of the time the 25 m band was completely useless.

I do not care what frequency a s.w. broadeast station uses so long as it is not in any Amateur Band and in this respect I boycott the $7 \cdot 0-7 \cdot 1 \mathrm{Mc} / \mathrm{s}$ frequencies of Radio Pakistan, Radio Peking, Cairo Radio and any others who have the nerve to use Amateur Band frequencies.

As for the 18150 and $12095 \mathrm{kc} / \mathrm{s}$ frequencies of the BBC, I immediately spring to their defence as $I$ find in winter that these are the only channels usable.

I am not demanding that you should stop mentioning these stations, but I feel that if you really cared you would.
N. D. Mugford, $\mathbf{A 4 7 1 3}$ (ex ZC4)

## Ancient and Modern

I would be interested to learn if any other readers have successfully fitted a modern pickup to an early cylinder-type gramophone. I have an Edison model circa 1890 with a number of wax cylinders, most of which are in mint condition.
A.W. Jenner.

53 Clifford Way, Hounslow, Middlesex.

## Wireless Set 31

I will shortly be getting a 31 set, and I would like to ask other readers if they have any useful data on this unit that they could lend me. These sets are advertised as breakdown units, but I would like to get one working rather than break it down for spares.
Charles Cawley. 15 Willow Walk, Dog In Tree Estate, Huntington Cannock, Staffordshire.

# practically wireless commentary by ILINII 

THE prime advantage of sitting on a fence is the allround view one gets. A service mechanic who is also an inveterate spare-time dabbler treats with greater sympathy the customer bringing electronic oddments for repair after having had a go-and failing. He knows too well the pitfalls and frustrations of kitchen-table surgery.

Not so sympathetic the superprofessional, with his spotchecks, stock faults and instant diagnosis. Between him and the amateur there is a constant lovehate relationship. From his position on the rails, like a cowpoke at the rodeo, Henry watches them react with an air of detachment.

The pathetic, defunct receiver lands on the workshop bench


Like a cowpoke at the rodeo.
and $A$. sniffs around it like a mongrel who scents an unwelcome visitor. He removes the back as if expecting some popeyed golliwog to spring up and surprise him. He glares at the works then: "Someone's been at it," he yells.

True enough. Very often someone has; the unfortunate owner, in an attempt to circumvent the crippling charges that
service carries in these times. Without test equipment, spares and experience he is handicapped. While he may make his preliminary tests with confidence, there comes a stage when he is beaten. It is easy enough in a well-equipped workshop to whip a valve from the rack to make a proving test-not so simple for the chap who has to justify the inroads into the family budget. And then discover the fault lies a lot deeper and the expense was not justified after all!

It sometimes seems that the chief enemy of A. is the bloke who ultimately pays his wages, the customer. He is angered by the substitute component dangling precariously from a tagstrip, affronted by an obviously "surplus" valve, offended by crystalline solder joints while one of those emergency circuit alterations (which may even be an improvement on original design) he regards as a personal insult.

But while A. is aggrieved at the outsider's attempts, B. is almost apoplectic. He has the "Whobody did it?" complex developed to a fine degree. At the first sign of tampering, he is likely to threaten to down tools. Something of a perfectionist himself, he cannot bear the sight of someone else's bungling. It takes all the Service Manager's diplomatic guile ("Get at it, mate!") to make him deal with a radio set that has "bounced".

For the benefit of innocent readers who imagine that the radio workshop is a magic cave whence issue perfectly rejuvenated receivers it should be explained that the "bouncer", the "reject", the "comeback" the "second complaint" or "twicer" is the repair job that has been delivered and subsequently fails.

It does happen-yes, really, even in the best organised department. Knowing the bits and pieces that go into the average item of electronic equipment, it is not surprising that the occasional failure crops up. But the customer whose precious tunebox develops apparently similar symptoms is likely to be querulous when bringing the bouncer back.


Listening to B. argue that the trouble is an Act of God is a treat the rest of the workshop rarely likes to miss. But hearing his remarks afterwards, when he discovers that the knobs are screwed on askew, the fastening bolts cross-threaded and maybe the valves plugged into the wrong sockets is a banquet of outraged invective. "The blighter isn't getting this done for nothing," he fumes.

Again for the benefit of the innocent, remember that repairs carry a limited guarantee. Limited, that is, to the work that has actually been done. When you take your car to the garage for a carburettor job and get a puncture as you drive home, you would hardly expect a sympathetic response if you rang up the mechanic to complain.

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# THE BROADCAST BANDS 

IF you want the real DX contact you will have to work for it this month, especially after dark. From 1900/2000 onwards you can forget the $13,16,19 \mathrm{~m}$. bs. If you wait for the late evening the $49 \mathrm{~m} . \mathrm{b}$. can produce surprising results with low-powered South Americans breaking through the strong European signals. If your ears can stand straining through c.w. the $90 \mathrm{~m} . \mathrm{b}$. is providing some rare catches.

## MIDDLE EAST

Israel: Kol Israel (Broadcasting House, Jerusalem), has dropped its Sunday morning English transmissions. The evening transmission to the U.K. has been retimed to 2115-2i20 on 9,009/9,725. The African English transmission remains 2015-2030 on 9,009.
Turkey: Radio Ankara (Ankara), has been heard signing on at 2330 on 9,745 in an unidentified language.

## ASIA

Afghanistan: Afghan Broadcasting System (Ansari Wat, Kabul), has restarted its evening English transmission after a lapse of several years. The transmission from 1900-1930 has been reported on 15,225 and 11,865 although some say the $25 \mathrm{~m} . \mathrm{b}$. outlet is 11,760 . Other reports say the $19 \mathrm{~m} . \mathrm{b}$. has been replaced by one in the 31 m.b.

Indonesia: Radio Republik Indonesia (P.O. Box 157, Djakarta) now appears to use only 9,865 between 1615 and 2000. English is at 1900-2000.
Korea (P.D.R.): Radio Pyongyang (Pyongyang), has replaced 6,650 by 6,480 for its $1100-1200$ and 1400-1500 English transmissions. The other frequency for these transmissions remains 7,580 . The station's home service may be faintly heard during the evening on 6,290/ 6,600.
Malaysia: BBC Far Eastern Relay Station (P.O. Box 716, Johore Bahru), now has its own QSL card which is far superior to that issued by the BBC, London. Indeed this BBC relay outlet will give full verification details on the card if asked, something that London will not do.
Philippines: Far East Broadcasting Company (Box 2041, Manila), now using 11,855 instead of 15,385 from 2330-0030. In the morning DZH8 has been heard signing on in English before 0900 on 11,855 .

## NORTH AMERICA

U.S.A.: Voice of America (U.S. Information Agency, 330 Independence Avenue, S.W., Washington 20547, DC), now has the following English schedule to Europe: 0300-0730 3,980/5,965/5,995/7,200/7,250/9,540/ $9,635 / 9,740 / 11,790 ; \quad 0500-0730 \quad 6,040 / 15,295 / 1,196 ;$ 1400-2330 $3,980 / 7205 / 9,760 ; 1500-2215 \quad 5965 ; 1900-$ $22159,710 / 11,760 ; 1830-233011,805 ; 1400-221515,205 ;$ $1400-200015,290 ; 1400-183017,780 ; 1600-1800,2100$ -$2130,2200-23301,196$. On Sundays read 2345 for 2330.

A new programme format is being used by the V.O.A.
U.S.A.: Radio New York Worldwide ( 485 Madison Avenue, New York, N.Y., 10022), now uses the following frequencies to Europe in English: $1200-1400$ 15,265/ 17,$845 ; 1400-1600 \quad 15,440 / 17,845 ; 1600-2100 \quad 15,440 /$ 17,755; 2100-2130 15,440/11,970; 2130-2330 (-0030 Sundays) $9,655 / 11,970 ; 0030-0100$ Sundays 9,655 .

## CENTRAL AMERICA

Cuba: Radio Habana Cuba (Apartado Postal 7026, Habana), now transmits in English as follows: 20102140 (Northern Europe) 6,015; 2050-2150 15,270/ 15,300; 0100-0600 11,760/6,170; 0330-0600 6,135; 0630-0800 9,655; 1800-1900 15,340.
Netherlands Antilles: Trans World Radio (SC Zoutpannenweg, Bonaire) has English as follows: 00350105, 0230-0400, 1105-1235 (-1530 Sundays) on 11,815 or 11,820; 2100-2130 (Europe) 15,130 or 15,245 or 11,815 or 11,820 .
Windward Islands: Windward Islands Broadcasting Service (St. George's, Grenada). The European frequency used from $2000-2145$ has been variously reported as 11,895 or 11,920 .

## SOUTH AMERICA

Brazil: Radio Ailtina de Bahia (Avenue 7 de Setembro 311, Salvador, Bahia), has reactivated ZYN30 on 15,225 . Has been heard from around 2300-0130.
Ecuador: La Voz de los Andes (HCJB), (Casilla 691, Quito), is again using 15,115 during its $1845-2000$ and 2100-2130 English transmissions. The parallel frequency is 17,890 .

## EUROPE

Austria: Osterreichischer Rundfunk (Wien IV, Argentinierstrasse 30a). Frequency schedule valid to 0100 on 5th March is as follows: on 6,000 0430-2300; $6,1550500-1100,1700-2200,2300,0430 ; 7,2450500-$ 1300, 1800-2000; 9,525 0000-0300; 9,610 1700-1900; $9.7700500-0800,1100-1700,2300-0400 ; 11,7600300-$ $0400 ; 11,895 \quad 1200-1400 ; 11,900 \quad 1100-1400 ; 15,210$ 1900-2100; 15,410 0600-0900; 15,430 0000-0200; 17,730 1400-1600; 17,750 1600-1800; 17,755 1000-1200; 17,855 0400-0500, 0800-1000.
Belgium: Belgian National Broadcasting System (Overseas Service, 18 Place Eugene Flagey; Brussels 5), has replaced 17,860 by the new outlet of 11,715 from 1600-1715. At this time 9,740 is also in use. Another new outlet heard is 9,660 from $1830-2100$.
Thanks go this month to the Swiss Broadcasting Corporation, A. B. Thompson, the World Communications Club of G.B., B. Bunting, Roy Patrick, A. E. Roxburgh, the International Short Wave Club, B. Lowe, J. D. Ashworth, J. W. Smith, B. Garvey and D. G. Hobro.

AUSTRALIAN and New Zealand hams at 5 and 9 plus on topband or just a few local G stations? Well, your guess is as good as mine for the coming year. Theoretically $28 \mathrm{Mc} / \mathrm{s}$ should be really something and 21 should also provide hoards of DX. Fourteen will doubtless continue to provide most distant signals at one time or another, and of course $7 \mathrm{Mc} / \mathrm{s}$ will seem noisier than ever. Topband and Eighty may well go down into the doldrums with the seasonal changes and the sunspot activity increase.
What about those New Year resolutions? All those not making any are banished to $7 \mathrm{Mc} / \mathrm{s}$. Still stuck for ideas? How about the station itself. Does your antenna go to ground when you switch off? How about fuses, and those mains plugs, are they $100 \%$ ? Has the earth lead corroded? This can be a source of noise. First resolution then, check the entire installation from mains right through to the aerial itself. If you do this just once a year it will avoid your wondering why you don't hear the DX too well, only to find when you do check, that the antenna wire broke off at the window, giving you an effective length of $3 \frac{1}{2} \mathrm{ft}$. (Pauses, titters behind fan, and remembers case of the '3JDG "Iongwire" which wouldn't load.) This month there appears to be a mass migration to ten metres. Certainly the band has been wide open most days although it does fall off at night. If things continue we will doubtless end up with the spottiest sun for decades. In view of the many very fine logs which arrived I propose to move on to my New Year resolution-cutting of the cackle.

## TEN

Reports from all over, from Scotland to Worcestershire, all reporting the same story, DX on Ten. All modes, all continents too, with the best time to listen still during daylight hours.
C. Clarke (Surrey), 12 valve single conversion s/het, phased verticals logged - K2RFZ/MM, K3BEQ, K8ERD, LU7ABV, MP4BBA, MP4TBO, OD5CN, PY2ARV, SV1AN, SV $\emptyset W L, ~ U A 1 A V M$, UA3AJT, UA6LIV, UA9FFB, UB5APK, UW9CR, VE3FIT, VK3AHT, VK3HW,VK6CF, VP9FB, VS9AJC, WIFQA, W8CNC, W9ARK, WøGYM, ZC4MO, ZS4OI, ZS5DC, $4 \mathrm{X} 4 \mathrm{HJ}, 9 \mathrm{~J} 2 \mathrm{BK}$. Chris reckons it won't be long before we start hearing JA and UA $\emptyset$ on ten metres. Anyone been lucky yet?
P. Baker (South Wales), HE30, 45ft. l.w. raisedCR4BC, many CR6's, CR7DS, CT3AM, EA6BH, EA8AE, JA1TRD (sorry I spoke!), K2GL, MP4BBA, OD5BU, PY1LW, SV1AL, UA9FB, UF6DV, UG6AZO, UY5HF (Ukraine-new prefix issue), VO1HB, VS9APW, W5GQG, WØIMC, XE2BM (Mexico), ZB2AJ, ZC4KF, ZEIJA, ZS1JH, ZS8L, ZS9G, 5AITK, 5N2AAF, $9 \mathrm{H} 1 \mathrm{~A}, 9 \mathrm{Q} 5 \mathrm{~EB}$.

George Owen (Somerset), GC1U, Joystick, heardCR4BC, CT3AM, CX1AAM, EA8EV, IT1ALD, K3AAG, LU2DED, PY8MA, PZ1BK, VE2BT, WICLP, W5GQG, ZE1BP, ZSIBS, 9 Y4VS, all these on a.m.

Colin Morris (Worcestershire), double s/het home-
brew, Joystick, hooked - CR6HF, CX2CO, CX4AW, ET3AC, FH8CD, HK3AVK, KR6LL, KG6AAY, KV4CX, KP4BJM, LU1DAB, MP4TBO, OA4PQ, UL7JA, VK4HC, VK5QR, VK6GP, VKøKM (Antarctica), VP5RB, VS9AJC, all W prefixes, YV9AA, ZB2AM, numerous ZC4's and ZS's, $4 \mathrm{X} 4 \mathrm{GV}, 4 \mathrm{Z} 4 \mathrm{HQ}$, (new prefix - State of Israel), $5 \mathrm{~A} 3 \mathrm{TN}, 5 \mathrm{~N} 2 \mathrm{AAF}, 5 \mathrm{R} 8 \mathrm{CQ}, 5 \mathrm{Z} 4 \mathrm{AA}$, WøGTA/8F4 (Sumatra), 9Q5BD. Colin informs that Don Miller has permission to operate from Albania, Rio de Oro, and Annobon Island. Also reported is great activity anticipated on Easter Island (CEØ). WøGTA/8F4 is also trying topband.

Many more logs for $28 \mathrm{Mc} / \mathrm{s}$ but the picture can be seen from those quoted, so let's wander downscale to-yes, the dreaded l.f. bands, 80 and 40.

## L.F. END

C. Claydon (Scotland), $840 \mathrm{C}+$ preselector, 12 ft . vertical groped in the $7 \mathrm{Mc} / \mathrm{s}$ darkness for-EA4CR, K1HVV, SV1CX, UL7QG, 9X5MH (Rwanda), WIFJJ, WB2NDS.
D. Harvey and T. Cowpe (Salop), R107, 80ft. wire, both assure that persistent scanning of the dreaded segment brings rewards. Proof offeredHB9ABM, $1 \varnothing \mathrm{RB} / 4 \mathrm{U}$, JA4BJO (yes, Japan), JA6YB, K8ARW, KP4BRX, LX4JB, OA3KCB, OX3KV, UA3KBD, UA6KE, UD6BV, VP6KL, VK2AVA (nearly always on 40 ), VK3BM, WØGTA/A, ZC4MO.
F. Simpson (Yorkshire), claims that 40 is like someone sawing an endless plank. (I wooden be surprised!). On the other hand 80 proved very fruitful with-KG4AA. OA8V, OX3JV, TF3EA, VOIFG, VE1IE, VE2XO, VE3WV, VP1PV, VP2AA, VP7DL, VP9BO, VS9AJC, VS9ALV, WIHKK, W2ZPO, YSIDHE, YV5BOI, ZF1GC, 6 Y 5 EM . It's almost as good as my $21 \mathrm{Mc} / \mathrm{s} \log$ !
N. Henbry (Sussex), strikes again! Armed with an EA12 and a 20 metre dipole on $3.5 \mathrm{Mc} / \mathrm{s}$, Norman logged K2DXV, K8YWG, VE1ADA, VE3AYS, VS9AJC, W1AQH, W2APU, W3BMS, W4SIB, W9JLH, YV5BTS, ZB2AJ, ZL3ACJ, ZL3GS, ZL4KE, ZL4LM, 7XøAH. On 7M/cs the best were CN8AW, CR6IV, PY1BDX, VE3LZ, VK2AVA, VKøAA, VP2AA, W3BMS, W4BYB, WA8DNQ, WøGTA/8F4, 5A1TS.

## 14 AND 21

Very, very few reports for the favourites, everyone seems split into two groups. The "Iet's listen on ten" brigade, and the real expert DXers trying their skills on 3.5 and 7 .
R. Garvey, back from Cyprus (get the umbrella out of pawn again, Bob) had a quick listen with his $S 640$ and heard VK's on $14 \mathrm{Mc} / \mathrm{s}$ at 589 . His best for the session-EP2RV, JT1KAA, OY3L, TA2AC, VK2EO, VK $\varnothing$ NB, W6MQT/OX3, ZA1BB.

## CONTESTS

Sparse month for contest types. Only two down in my diary-14-15th, Affiliated Societies' Contest (quite lively this one), $29 \mathrm{th}, 144 \mathrm{Mc} / \mathrm{s}$ c.w. Contest. Many thanks for the fine logs, deadine for January is the 24th.

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maku, $80 \Omega=8 / 6 \mathrm{~d}$. P. \& P. 1/Gd. TWEETER, 2 jin. Black plastle cone, roumd on Square Frame. I.M.I. 3Q-12/6d, plus $1 / 6 \mathrm{~d}$. P. \& P. P.A. HORN Speaker, $8 \Omega 15$ watt, 9 I $9 / n$. Swivel mountag REMOTY OONTROL TWO-IN-ONE EXTENSION SPEAKER In addition to providing anextenHion spenker, two independent knobs control voinme in extension ppeaker and also in your radio, T.V., E1-FI, Grazn. eto. Btereo efteat If deslred. Complete with 2 ifit, unobtruslve cable and full instructions, Easily connected. 8ELECTED VALVE AND C. R. TUBE OFEER FEHTS MONTE:

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| 188 (DAF |  | 6АМ\% |  | ECC82 |  |  |  |  |
| 91) | 81 | 6CH6 | 519 | ECC83 | 4/8 |  | 12897 | 819888416518 |
| 1T4 (DF |  | 6 F 11 | 519 | $6 \times 4$ | 818 |  | 128K7 |  |
| 91) | 2/8 | $6 \mathrm{K8G}$ | $8 /$ | 6X5C | 4)- |  | ECC85 |  |
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Wide Range Signal Generator<br>-continued from page 759

receiver will respond if tuned to the same frequency. But there is no response if the generator is tuned to multiples of the receiver frequency. So the fundamental frequency is the first one causing a response if the generator is tuned from a high frequency downwards.

## HARMONIC STRENGTH

Harmonics grow progressively weaker. With a sensitive receiver, $1 \mathrm{Mc} / \mathrm{s}$ harmonics may be heard up to $30 \mathrm{Mc} / \mathrm{s}$ or higher, while $100 \mathrm{kc} / \mathrm{s}$ harmonics can be tuned in up to about $5 \mathrm{Mc} / \mathrm{s}$.

With a t.r.f. receiver, any response will be at
the generator frequency, or multiples of this frequency.

When using a superhet, various spurious responses arise. They can usually be identified because they are weaker. Second channel effects are heard at a frequency which corresponds to an error of intermediate frequency $x 2(940 \mathrm{kc} / \mathrm{s}$ for an i.f. of $470 \mathrm{kc} / \mathrm{s}$ ). This is likely to be moticed at high frequencies, but not at medium or low frequencies.
Weak spurious responses also arise from receiven oscillator harmonics beating with the generator signal. This is also usual.

VRI is used to adjust signal strength as required, but ceases to be wholly effective at high radio frequencies. This is unavoidable with a simple potentiometer. Enough signal is often securred merely by placing an unscreened generator output lead near the receiver aerial.

## TESTING and ALIGNMENT PROCEDURES

The wide range signal generator can be used for many purposes, such as the quick location of faulty stages in audio amplifiers, or complete receivers. If an audio amplifier gives no results, for example, the source of the fault can often be found quickly by injecting an a.f. signal. A typical two-stage amplifier is shown in Fig. 6.

With battery-operated valve receivers, or those having heater and h.t. from a transformer, a direct connection can be made to the chassis or earth line at A by clipping on a lead from the generator earth, or coaxial outer conductor. With a.c./d.c. or other sets alive to the mains, first check that the chassis goes to mains Neutral. Also include an isolating capacitor in the earth mentioned.

## AUDIO STAGES

Then set the generator to give an audio output, and feed it into point B. If the signal is not heard, the output transformer or speaker is defective or disconnected.

If the signal is heard, transfer the generator prod to C. If there is a considerable increase in volume, the output stage is obviously working. Then transfer the prod to $D$. If the signal disappears, the coupling capacitor or connections here are defective.

Should output be obtained from injecting at D, take the prod to E. Volume should again increase greatly, if the triode amplifier stage is functioning correctly. Then take the prod to $F$. If the signal disappears, the $1 \mathrm{M} \Omega$ volume control or a connection to it is suspected. If results are in order, move the prod to take in any pick-up or other lead included.

Thus, the method is to work backwards stage by stage, until results cease. The last part of the circuit just introduced is then faulty. When the faulty stage is found, a meter is generally brought in to check resistors and other items in the defective stage. Generator output is reduced as necessary with the output control. Pre-amplifier and other stages can be dealt with in the same way.

## I.F. CIRCUIT TESTS

Exactly the same method can be used to locate a faulty stage in an intermediate frequency amplifier, the generator being adjusted to deliver modulated r.f. at the intermediate frequency. With many receivers the i.f. is around $470 \mathrm{kc} / \mathrm{s}$. First test the audio amplifier as described, if necessary. Audio is also injected at points A and B, Fig. 7 , to check the anode coupling capacitor. Then inject audio at $C, D, E$ and $F$ in turn, to check the triode section of the double-diode-triode, grid capacitor, potentiometer and $33 \mathrm{k} \Omega$ diode filter resistor.

Modulated r.f. can now be injected at G, and the generator tuning swung around the i.f. Output at one frequency shows that i.f.t. 2 is in order. Lack of output shows this component, or connections to it, are faulty.

With output obtained, move to point $\mathbf{H}$, to check the i.f. stage. Output should be much increased. Taking the prod to 1 tests i.f.t.1. Results should also be obtained with a signal at the i.f. injected at J.

When a faulty stage is found, a meter test will show if normal voltages are present. If not, the connection or resistor in circuit should be checked.

## I. F. ALIGNMENT

With a new home built receiver, set the generator at the specified intermediate frequency (modulated). Should the i.f.t's. be pre-aligned or not badly off tune, inject at $\mathbf{J}$ and adjust their cores for best results.

If the cores are badly off tune, often it is necessary to inject at $G$ and tune i.f.t.2, then at ' $I$ and deal with i.f.t.1. Afterwards inject at $\mathbf{J}$ (to remove stray capacity from i.f.t.1) and re-adjust both i.f.t. 1 and i.f.t.2.

## R.F. STAGES

If a defective receiver has been tested as far as I and J, Fig. 2, this shows that the i.f. and a.f.
sections are working. Modulated r.f. of the frequency to which the receiver is tuned can then be injected at J. Lack of results shows that the mixer stage is defective. Moving the prod to K (with results from injecting at J) allows the individual coils to be checked.

When an r.f. amplifier is present, this can be checked with the appropriate r.f., exactly as with the aerial circuit of the mixer, Fig. 7.

To align aerial and oscillator circuits of a newly made receiver it is usually convenient to set band coverage, adjust the aerial circuit to agree, then trim and adjust cores for best sensitivity. For a typical medium waveband of about $550-1500 \mathrm{kc} / \mathrm{s}$ this could be done as follows:
(1) Switch to medium waves, inject $1500 \mathrm{kc} / \mathrm{s}$ at derial and adjust oscillator trimmer for correct dial reading.
(2) Roughly adjust aerial trimmer for best results.
(3) Inject $550 \mathrm{kc} / \mathrm{s}$ and adjust oscillator coil core for correct dial reading.
(4) Roughly adjust aerial core for best results.
(5) Inject at $1300 \mathrm{kc} / \mathrm{s}$, and adjust oscillator and aerial trimmers for best sensitivity.
(6) Inject at $750 \mathrm{kc} / \mathrm{s}$ and adjust oscillator core and aerial core for best sensitivity.
Steps (5) and (6) are repeated until no further improvement can be obtained. The actual trimming point (5) and tracking point (6) will vary somewhat in actual receivers, but are generally a little clear of the extreme ends of a band. At these steps the oscillator trimmer and core need not be altered unless a compromise is needed with the accuracy of dial readings.
Any r.f. stage coils can be dealt with in the same way as the mixer aerial coils, Fig. 7. With completely separate coils for each waveband, deal with each band individually, afterwards checking all bands. With long/medium wave coverage by dualband coils or ferrite aerials, it is usually necessary to adjust medium waves first.


Fig. 6: Test points on a typical audio amplifier.

## OUTPUT INDICATION

If tuning is by ear, keep the generator output as low as possible for final adjustments, with the receiver audio gain at maximum. Otherwise the any a.g.c. circuits will mask the effect of adjustments.

An audio output meter is often handy. The simplest comprises a crystal diode in series with a multi-range meter, which is connected across the output transformer primary or secondary. Set the meter to a suitable d.c. range. Some meters can be used without the diode by switching to an a.c. range.

It is sometimes convenient to adjust tuning or i.f.t's. for minimum anode current in an a.g.c. operated stage. To avoid interrupting permanent wiring, a multi-range meter can be clipped across one of the cathode resistors in Fig. 7. Either' 2-5, 5 or 10 V range is usually satisfactory, according
-continued on page 773


Fig. 7: Test points on a typical radio receiver. See text for details.

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## Wide Range Signal Generator

continued from page 770

to the valve and bias resistor. All trimming, core and i.f.t. adjustments are then directed towards minimum anode current, corresponding to minimum voltage on the meter. Unnecessarily strong signals should not be used.

When a.g.c. is from the i.f. anode, as in Fig. 7, the secondary of i.f.t. 2 does not usually peak for maximum a.g.c. voltage (minimum i.f. stage anode current). It should then be peaked for maximum audio output. With some circuits this agrees with a slight $d i p$ in a.g.c. voltage.

## COUPLING TO RECEIVER

For accurate alignment, coupling must be very loose. Enough input may be obtained for final adjustments by placing the output lead near the receiver aerial. Some receivers are supposed to be aligned with particular aerial pads or loads, such as a $400 \Omega$ carbon resistor. Or the aerial trimming can be touched up, if necessary, when the aerial is connected. The generator lead should not be taken directly to any i.f.t. or tuned circuit which is being finally adjusted because the stray capacity will cause errors. Proper trimming tools should be used, not screwdrivers having only an insulated handle.

## DIAL CALIBRATION

Tuning scales can be marked up for home built receivers by setting the generator to various frequencies, adjusting the receiver to them, and marking the dial. If the procedure detailed for calibrating the generator originally is noted, there will be little chance of errors from tuning in harmonics, or similar mistakes.

It is sometimes required to calibrate a narrow band on the receiver with great accuracy. This can be done by tuning the generator to a much lower frequency, and multiplying its output by the appropriate figure.

The 80 metre Amateur band provides an example of this method. This band is $3 \cdot 5-3 \cdot 8 \mathrm{Mc} / \mathrm{s}$. Locate $3.5 \mathrm{Mc} / \mathrm{s}$ on the receiver by setting the generator to this frequency. Some error, due to visual reading, is most likely, but this $3.5 \mathrm{Mc} / \mathrm{s}$ point is only temporary. The generator can then be tuned to $100 \mathrm{kc} / \mathrm{s}$ so that its second harmonic is at zero beat with the BBC Light Programme on $200 \mathrm{kc} / \mathrm{s}$. A transistor portable or any convenient receiver can be used for this comparison of generator harmonic and BBC. The generator is now providing $100 \mathrm{kc} / \mathrm{s}$ to a high degree of accuracy (so long as it remains at zero beat with the Light Programme) and harmonic marker pips will be tuned in at $3.5,3.6,3.7$ and $3.8 \mathrm{Mc} / \mathrm{s}$ with the Amateur band receiver, and can be written on its scale.

The upper Jimit to which low frequency harmonics may be detected depends on the receiver. For normal accuracy, harmonics need not be employed and the generator is tuned directly to the wanted frequency.

## RECEIVER FOR 144 M/cs

-continued from page 755
slowly with an insulated tool, while checking coverage.

With VR2 near maximum, slowly turn up VR1 from its minimum position. When super-regeneration commences, a loud hiss will be produced. Turning back VRI a little reduces this hiss, but if VR1 is rotated too far, super-regeneration will cease. With VR1 in the best position, VCl can be peaked for maximum noise even with no aerial connected. With an aerial on, tuning VCl should give quite a high noise level. With TC1 nearly open,


Under chassis view of the completed receiver.
resonance with VC1 can be expected around minimum capacity, increasing slightly as VC2 is closed.

When a usable signal is tuned in, the hiss should almost completely cease, and in these circumstances, peaking VCl for maximum signal strength corresponds to minimum noise. With careful adjustment, very weak signals can be resolved.

If super-regeneration is not satisfactory, it may be worth changing R 4 since surplus 6 C 4 valves seem to vary somewhat. If super-regeneration is absent, reduce R4 slightly in value. Alternatively, slightly increase the h.t. voltage by increasing the value of R10, or reduce the value of R9. On the other hand, should super-regeneration be difficult to control, slightly increase R4 in value, or reduce the h.t. voltage.
For a range of some miles, a vertical $\frac{1}{4}$-wave aerial will do. This is about 19in. long. Signal strength at other than short range will be much improved by using a dipole. It may be wire supported from convenient points, or attached to insulators on a strip of wood, or self-supporting rods. The overall length is about 38in. In view of the very small size, a simple "X" or " H " aerial is also easily constructed, but some means of rotating it will then be needed. Various ready made or adjustable aerials, and multi-element aerials giving increased signal strength, can be obtained. At first, a dipole may be preferred. This is less effective, but has little directivity, so signals can be picked up from all directions.

# PULSE COUNTING VHF RECEIVERS 

DURING the past few years a number of circuits have been published describing the detection of f.m. signals using pulse counter discriminators. The purpose of this article is not to go over the already well trod ground of theoretical considerations, but to put forward a practical front-end. Figure 1 shows in block form the various stages needed for a pulse counting type of v.h.f. receiver.


Fig. 1: Block schematic diagram of a pulse counting type of v.h.f. receiver.
Most of the circuits that have already been published employ crystal controlled oscillators in the front ends. These come rather expensive for the amateur-and for that matter the author. However, a circuit employing an autodyne frequency changer was located and found to be successful. This is shown in Figure 2.

## FREE RUNNING OSCILLATOR

In simple terms, the autodyne frequency changer mixes the incoming signal with oscillations generated within the valve itself to produce an intermediate frequency. One of about $150 \mathrm{kc} / \mathrm{s}$ is required and is obtained fairly easily, since the bandwidth of most f.m. transmissions is in excess of this. As far as the operator is concerned, it's

The circuit shown in Figure 2 hooked-up to a direct-coupled amplifier worked first time and gave a good account of itself on all three v.h.f. sound transmissions put out by the BBC.
A small amount of drift did occur during the initial warming-up period but subsequently the oscillator held very firmly. The degree of oscillation controlled by VR1 is critical and may require a little patience to find the optimum point of working, but


Fig. 2: Autodyne frequency changer. once set it can be forgotten.

It is possible that the oscillator could set up interference with neighbouring sets, although no trouble has been experienced in this direction by the author. Should this occur, a buffer r.f. amplifier ought to be fitted to isolate the oscillator from the aerial.

## PROTOTYPE CIRCUIT

For the sake of completeness, the original prototype circuit is shown in Figure 3. From a quick glance, one can see inexpensive EF91 valves have been used and tuned circuits have been kept to a minimum.

The inductance which may cause a little trouble is the main tuning coil. The author used a quarterinch former, with an iron dust core, upon which he wound six turns of 20 s.w.g. enamelled copper


Fig. 3: Complete circuit of a pulse counting type of v.h.f. tuner.
a matter of de-tuning to one side of the centre frequency. It is, of course, much easier to tune-in a receiver with a slow-motion drive. The reason for selecting a low i.f. is that one can employ direct coupled amplifiers and dispense with all the 'usual tuned circuits.
wire. Due to the stray capacities, which play such an important part at these frequencies, it may be necessary to experiment by adding an extra turn or subtracting one to obtain the correct coverage. The r.f. choke in the cathode of V1 has a value of 1.5 mH .
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## SEPARATE HEATER LINE

There is a limit to the voltage that can be applied to the cathode of a valve when the heater is at chassis potential. In the case of the series regulator valves, the cathodes will be several hundred volts above chassis potential, and any attempt to run the heaters of these valves from an earthed heater supply is doomed to failure as the heater to cathode insulation will break down, leading to premature, and possibly violent, valve failure. It is therefore customary to run the heaters of such valves from a separate heater winding, well insulated from chassis and all points having a PD differing from the cathode. If this separate winding is centre tapped it can be connected to the cathode of the regulator valve. If not, it can be left floating or one side connected to a potential divider across the h.t. supply so that the heater is at or near the same potential, above chassis, as the cathode of the regulator valve. The cathode of the error amplifier will be from 85 V to possibly 100 V , or fractionally higher, above earth potential, a figure that is within the heater cathode rating of most valves likely to be used in this position, so that a separate heater winding will not be required.

## E.H.T. SUPPLIES

The high e.h.t. voltages required by many oscilloscopes cannot always be supplied by voltage multiplying circuits. For instance, a common e.h.t. value is 2 kV , and a common h.t. transformer secondary voltage is 350 V , so that a X 6 voltage multiplier would be necessary. Higher e.h.t. and/or lower transformer voltages would require even more multiplying elements, an uneconomical situation both electrically and financially. Under these circumstances alternative methods have to be adopted. The use of a mains transformer having the requisite voltage output is one possibility, but such transformers are not only expensive but potentially dangerous, in more ways than one. Although the smoothing capacitors rarely exceed $1 \mu \mathrm{~F}$, they are capable of delivering a considerable amount of instantaneous power which is measured in joules, a joule being equal to $\frac{1}{2} \mathrm{CV}^{2}$ where C is capacity in farads and $V$ the voltage they are charged to. The initial shock would be severe enough, but unfortunately, in this context, the current delivered by the transformer is sufficiently high to speedily recharge the capacitors. Continued contact with such a supply would cause local burning of the flesh and possibly death. Considerable care must be exercised when dealing with such a supply, and it should be carefully discharged before
being handled. The discharging of capacitors by means of a screwdriver should be avoided if at all possible, because the resulting bang is not good for people's nerves-and it certainly isn't good for the capacitor, as it is liable to fracture the dielectric. Instead, capacitors should be discharged by means of a resistor connected across them, values from a few kohms to a few hundred kohms being suitable. It is an excellent idea to fit high resistance bleeder resistors across all high voltage capacitors to automatically discharge them when the supply is disconnected. The working voltage-not currentof such resistors must be adequate. If in doubt, a number of series connected resistors could be used.

## R.F. HIGH VOLTAGE SUPPLIES

The use of r.f. e.b.t. supplies have much in their favour, for although the voltage levels are comparable with transformer supplies, the current levels are very much lower. Although the initial shock will be as unpleasant as before, the r.f. oscillator will either cease working or, if it continues working, will do so at a much reduced efficiency. Continued contact with such a supply will therefore be far less hazardous than from a mains transformer supply. The r.f. supply will either consist of two valves, an oscillator and a power amplifier stage, or just one valve functioning as a self-oscillating power output stage, and this is the circuit shown in skeleton form in Fig. 11. The transformer for this consists of three coils, L1, L2, L3, which are usually wound on a Ferrox cube core. L1 and L2 comprise the anode to grid feedback windings which cause the valve to oscillate, L3 is the e.h.t. winding. The inductance of L 1 in conjunction with C 1 determines the oscillator frequency. The number of turns of L2 and their spacing from L1 determines the feedback voltage which should not be excessive, otherwise severe waveform deformation will occur. The number of turns for L3 determine the e.h.t. voltage. The operating frequency is a matter of compromise. The efficiency of the Ferrox cube transformer falls with decreasing frequency, whilst too high a frequency is liable to cause interference with nearby receivers. It is usual to choose a frequency in the $50 \mathrm{kc} / \mathrm{s}$ to $100 \mathrm{kc} / \mathrm{s}$ range and to enclose the e.h.t. unit in a screened box, with adequate decoupled h.t. and heater feeds. The valve must be a power type; EL84, EL34, 6L6 types being commonly used.
The components in a power supply are amongst the hardest working of any and it is therefore essential to devote care when selecting these components and assembling them together.
The smoothing capacitors are often electrolytics,
because these offer a greatly increased capacity, size for size, than paper capacitors, which makes them an attractive proposition where space is restricted. In some other respects they are inferior to paper capacitors, particularly where polarity and internal noise level is concerned. Connecting an electrolytic with reversed polarity or across an AV supply is almost certain to end in the capacitors explosive destruction. The leakage current of electrolytic capacitors is appreciably greater than paper capacitors, but even worse, from some aspects, is that the leakage current is not constant, but varies sporadically-hence the "noisy" capacitor. This current also increases with increasing voltage across the capacitor, with the result that the DV output contains not only a percentage of mains ripple, but also a percentage of capacitor noise. Capacitors that have been stored for any length of time are apt to have a low internal resistance, and will pass excessive current, which causes overheating, if connected across a source of high DV potential. This excessive current/overheating phenomenon is likely to be cumulative, culminating in another explosion. Such capacitors should be "formed" for a short while by connecting them to the DV potential via a moderate resistance of $10 \mathrm{k} \Omega$ or so. This resistor will limit the flow of current so that the capacitor cannot overheat due to passing excessive current. An interesting way of demonstrating this would be to connect a high resistance ( $20 \mathrm{k} \Omega / \mathrm{V}$ ) voltmeter across the capacitor and note the voltage across it on switching on, and then at fairly frequent intervals. At first the capacitor would pass a fairly heavy current (this could also be monitored by connecting a milliameter in series with the capacitor) and the voltage would be low. As the capacitor was "formed", its current leakage would decrease, and the voltage would increase, until a state was reached when the voltage and/or current remained constant. At this stage the capacitor could be considered to be fully formed. The practice of using an expensive multimeter to measure leakage current directly is fraught with danger, because should the capacitor suddenly go s/c or pass an excessive leakage current, the chances are that the meter movement will suffer.

## WATCH THE CAPACITOR RIPPLE RATING

One aspect of capacitors that is often overlooked is that in the process of smoothing the pulsating or raw DV from the rectifier, they have to pass what may easily be an appreciable AV current. In this respect, the reservoir capacitor, i.e. the capacitor following the rectifier, has to pass the greatest current, and the smoothing capacitor, i.e., the capacitor on the load side of the smoothing choke or resistor, the least current. This can be easily visualised if one remembers that the unwanted ripple voltage has to be "lost" somehow, and the only way of doing this is to short circuit it to earth via the reservoir and smoothing capacitors. These components must therefore possess an adequate a.c. ripple rating which will be greater than the mean DV current by a factor of $\sqrt{ } 2$.


Fig. 11: Transistor and valve e.h.t. oscillators.
In the part of the article dealing with stabilised power supplies it was stated that the series regulator valve could consist of several valves in parallel if the current capacity of a single valve was inadequate. This, of course, is perfectly true, but needs a little further elaboration. Since the combined slope of a number of valves in parallel is the sum of the individual valves' slopes, the chances of instability increase with every additional valve. Generous use of grid stoppers around $1 \mathrm{k} \Omega$ to $10 \mathrm{k} \Omega$ plus anode and screen stoppers at $10 \Omega$ and $100 \Omega$ or thereabouts respectively would minimise the chances of instability. It is essential that these stoppers are wired as close to their respective pins as possible.

## SITING COMPONENTS

The positioning of components on a chassis must also be considered. Rectifiers in common with other valves have an aversion to being in a strong magnetic field and should therefore be positioned as far from the mains transformer as is practicable. Failing this they should be positioned where the magnetic field is least, i.e. at right angles to the core. Wherever possible other inductors should be positioned with their cores at right angles so that mutual coupling is at a minimum.

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Fig. 12: Simple method showing how to measure leakage current and voltage.
much of the energy in a power pack is dissipated as heat. If the power pack is to give long and trouble free service, adequate ventilation is absolutely essential. Without it, all the care taken in the choice of components, and in their integration as a working whole, will be set at naught.

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FAREHAM'S radio club was formed, like so many others, by two or three amateurs meeting informally and "chewing the rag". Just two years ago an inaugural meeting was arranged and well over a dozen potential members crammed into the lounge of the first elected Secretary's QTH. From this encouraging response it was obvious that there was sufficient local interest to put things on a proper basis and so the Club was born.

Just one week later saw the first activity in the form of a world wide contest for which a station was set up on the stage of a disused school hall. This venture, apart from being the first introduction to "ham radio" for several members, was nearly a full scale disaster. Hooligans tore down the antenna, the weather was bitterly cold and the mains power supply all but melted. Far from being disheartening, the experience cemented all those who froze through the night into a club with spirit.

The first problem was that of accommodation and it was decided to hold monthly meetings in the back room of one of the local hostelries. With an equal membership of licensed amateurs and SWL's the pattern of these enjoyable evenings was soon established with slow morse for beginners, talks by the older hands on some of the mysteries, or perhaps a demonstration of someone's latest acquisition, followed by the inevitable natter over a "jar".

The Sunday morning net helped a good deal in the early days to catch many SWL's and others so that within a few short months the membership exceeded thirty. Biggest trouble was the provision


The club station in action. Left to right-G3VEL, G3TZM, and SWL Jack.


Club President G2OK directs operations. Left to rightG3PMM, G3VFI, Junior Op, G3VLY, G3TZM, G3VOR. SWL Brian.
of transmitting facilities and more suitable accommodation was sought by the Club's President.

After much negotiation and effort the club found its permanent QTH at the Portchester Community Association. This meant a move away from the town centre and it was decided to change the Club's name to one more in keeping with the new circumstances. Meetings were now held every Sunday and before long such was the demand that an additional evening for practical work was arranged. Once again members rallied to the cause and workshop facilities were obtained together with an adequate supply of the usual tools.

Sundays are now set aside for more organised activities and a full and varied winter programme is under way. This takes the form of a monthly lecture or demonstration, the remaining evenings being reserved for discussions, informal talks and quizzes.

Memorable occasion recently was when a new call-sign broke into the Sunday morning net. The newcomer turned out to be not only a club member but the Chairman himself.

Regular features in the club calendar are the Fareham Fair and the local Gymkhana. These give club members the opportunity to set up a temporary station, younger members looking after the usual tree climbing.

The Club now has a membership of over 40 with 16 licences, interests ranging from Top Band DX to the technicalities of u.h.f. Now with its own AR88D, a respectable antenna system almost completed and a newly acquired all band transmitter, the club is well and truly "on the air".

> 三 TAPE RECORDING YEARBOOX－1966
> 彦 Pubilshed by Print and Press Services Lid．三ㅡ 128 pages， $9 \times 5$ in．paperback．Price 7 s ． 6 d ．

FIOR those who，like the reviewer，spend their working days immersed in the technicalities of tape recording，this annual collection of facts and figures is an indispensable reference．The cur－ rent issue is no simple reprint，but has been brought as nearly up－to－date as publication times allow，thus providing current information on tape recorders，decks，mixers，microphones，radio tuners and miscellaneous accessories．In addition，the important section on manufacturers and agents has been revised and is a directory of real value．

For the ordinary enthusiast，the Yearbook offers comprehensive data on many different machines， plus articles of interest by well－known writers in this field dealing with recording，using microphones and tape－plus－cine respectively．

The catalogue section follows the same form as in previous years．The only omission we would like to see rectified is the input and output impedance and sensitivity specification－but，after all，for 7 s ．6d．，one cannot expect everything．As it is，we certainly get our money＇s worth．－HWH．


SLIMMER，neater，and two shillings cheaper， this is the latest edition of the successful volume reviewed in the September 1965 issue of Practical Wireless．
To achieve the fining down，the publishers have used a cleaner type，omitted the final chapter on Special Applications，and small parts of other chapters，whittled the less necessary diagrams and applied the blue pencil to some of the text．
One could argue with the choice of material to be omitted：Chapter 5，on Recording Level Indica－ tors，renamed Volume Indicators has some useful information expunged and five whole pages on pre－ amplifier design have been dropped from Chapter 8．It is perhaps fortunate that the excellent chapter on motors has been tidied and retained．

More serious is the information that should have found its way into a new edition to bring it more up－to－date．There is still no admission that alterna－ tive systems to NARTB exist．DIN／CCIR would seem to be a myth，and in the chapter on equalisa－ tion this error is compounded by a complete avoidance of explanation of the time－constant specification of recording characteristics；quite unforgiveable in＇a semi－technical work such as
this．Again，quarter－track recording and the various facilities it affords are not mentioned，neither is videotape，and a passing reference to head－gaps gives a limitation of 0.00025 in ．，now regarded as ＂barn－door＂dimensions by the better manu－ facturers．

This is a pity，for the book as a whole is a commendable addition to the enthusiast＇s library． Despite which，this reviewer will cling to his original copy and hanker after the book that some British authority will some day produce along the same lines．Recommended－but with reservations． $-H W H$ ．

## ＝INSTRUCTIONS TO RADIO CONSTRUCTORS．

By R．H．Warring．Second edition，published by Museum
Bress Lid． 144 pages．Size $8 \frac{1}{2} \times 5 \ln$ ．Price 159 ．

WHEREAS the first edition covered basic radio theory and the design and construction of simple receivers，the second edition is more ambitious and includes quite a lot more information．For instance，a chapter on the design and construction of home printed circuts has been added．Another new chapter deals with the design and construction of the smaller transistor receivers． The original series of circuit designs have been retained，as these are－to quote the author－well proven in performance．

Some thirty pages of this book are devoted to appendices，which range from broadcast frequency details and how to calculate circuit component values to data on the valves and transistors speci－ fied in the various circuits．An appendix is also included on receiver faults，but is not very com－ prehensive．

This book would make suitable reading for those who would like to begin constructing，yet have no knowledge whatever of the subject．－JRC．

## ㄹ TRANSISTOR ETCHED－CIRCUIT PROJECTS <br> 研 By James Kyle．Published by W．Foulsham \＆Co．Lid． 144 pages．Size $8 \frac{1}{2} \times 5 \mathrm{ln}$ ．Price 24s．

THIS novel publication deals with the use of printed circuits in home constructed gear and contains a number of actual negatives for the boards used in the various circuits given in the body of the book．These circuits range from an extremely simple potential divider network－called the volter－to an 80 metre c．w．transmitter．

The first chapter contains a lot of information on printed circuits，from which the average home constructor should be able to knock－up his own circuits at little expense．The following chapters deal with various projects，some very simple and which could be put together with a minimum of knowledge．－JRC．

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