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OCTOBER 1972

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AUDIO REFERENCE SOURCE
'LOGIPROBE' FOR DIGITAL IC's

HIGH-FIDELITY STEREO PACKAGE

Four fully wired units ready to

★ SUPER 30 AMPLIFIER (15 + 15

★ SUPER 30 AMPLIFIER (15 + 15 watt) in veneered housing
★ GARRARD SP25 MK III Turntable on Plinth with cover
★ GOLDRING G850 Magnetic cartridge with diamond stylus
★ PAIR OF STANWAY II Speaker Units
Special Total Price
Carr. £1:50

Terms: Deposit £12.77 and 9 monthly payments £9:39 (Total £97:28).

payments £9.39 (Total £97.28).

Super 30 Amplifier (15 +

repeated housing Transcription
Turntable on Plinth as illustrated
Goldring Magnetic P.U. Cartridge.
Pair of Stanway Il
Speaker units.
Special Total Price



Special Total Price

Terms: Deposit £13.63 and 9 monthly payments £10.62 (Total £109.21).

Matching as recommended for optimum performance. Package prices apply providing all individual units are purchased from any branch within 3 months. See leaflet.

* TA12 AMPLIFIER

6.5 watt in veneered

★ GARRARD SP25 MK III Player

unit on Plinth

SONOTONE 9TAHC Ceramic P.U

Cartridge with diamond stylus

* PAIR OF DORCHESTER

Loudspeaker Units Special Total Price £59.00 Or Deposit £8-40 & 9 nithly payments £6:32 (Total £65:28). Carr. £1:25 Trans. Plastic Cover £3:15 extra.

PACKAGE AS ABOVE but with Garrard 3000 Autochanger and Sonotone 9TA Ceramic Cartridge in lieu of SP25 Carr. £1-25 Carr. £1-25 Or Deposit £7-50 and 9 monthly payments £5-64 (Total £58-26) Trans. Plastic cover £3-15 extra.

'YORK' HIGH-FIDELITY 3 SPEAKER SYSTEM

* Moderate size only 25×14×10in. approx.

Response 30-20.000 c.p.s. COMPLETE KIT £23 Response 30-20.000 c.p.s. Impedance 15 ohms

Impedance 15 ohms

Performance comparable with units costing considerably more.
Onsista of (1)12in. 15 watt Bass unit with cast chassis. Roll rubber cone urround for ultra low resonance, and ceramic magnet. (2) 3-way quarter ection series cross-over system (3) 85 km, high that middle range speaker. (4) High efficiency tweeter. (5) Appropriate quantity acoustic damping aterial. (6) Handsoner Teak veneered cabinet. (7) Creati and full instructions. Terms: Dep. 24-60 and 9 monthly payments 22-47 (Total 228-83).

DEMONSTRATIONS AT ALL BRANCHES

RSC G66 MkII 6+6 WATT high quality STEREO AMPLIFIER

Individual Ganged Controls: Bass, Treble, Volume and Balance. Printed circuit construction employing 10 Transistors plus Diodes. Output rating I.H.F.M. Frequency range 20-20,000 c.p.s. Bass Control ± 12db. Treble Control ± 13db. Selector switch for



P.U. or Tape/Radio. For loudspeaker output impedances of 3 to 15 ohms. For standard 200-250v. A.C. mains operation. Attractive Black and Silver finished metal facia plate and matching control knobs. COMPLETE KIT OF PARTS INCLUDING CONTROLLY WIRED CONTROLLY W

omprenensive wiring £11.50 Carr. digram and instructions £11.50 Carr. digram and instructions class control of the control of

AUDIOTRINE HI-FI SPEAKER SYSTEMS

Consisting of matched 12in. 11,000 line 15 watt 15 onnihing high quality speaker, cross-over unit and tweeter. Smooth response and extended frequency range ensure surprisingly realistic reproduction. CR SENIOR 15 WATT INCLUDING Carr. 30p CR SENIOR 15 WATT INCLUDING 46.95 Carr. 35p



AUDIOTRINE HIGH FIDELITY SPEAKERS

Heavy construction. Latest high efficiency ceranic mar Plasticised Cone surround. "D" indicates Tweeter Cone pro-Plasticised Cone surround. "D" indicates Tweeter Cone providing extended frequency range up to 15,000 c.p.s. Impedance 3 or N.15 ohng PLESCE STATE GROUPS.

extended frequency range up to 15,000 c.p.s. Impedance 3 8.15 ohms. PLEASE STATE CHOICE.

Exceptional performance at low cost. Exceptional performance at low cost. 8 100 22.88 HF120D 12 15W 24.99 HF102D 10 10W 23.40 HF128 12 15W 25.75 HF120 12 15W 24.50 HF120 12 15W 24.50 HF120 12 15W 24.50 HF120 12 15W 26.50 Exceptional Processing States of the Processing States of th

FANE 807T HIGH FIDELITY SPEAKER

A full range 8in. 10 watt unit for excellent sound quality, in suitable enclosure. Cast chassis Roll P.V.C. cone surround and long throw voice coil to achieve very low fundamental resonance of 30 c.p.s. Tweeter cone is fitted to extend high note response. Frequency range 25 Hz to 15 KHz. Gauss 10.000. Impedance 5 or 8-15 Q. 15 KHZ, Gauss 10,000, impedance 3 or 5-10-52. PLEASE STATE IMPEDANCE WHEN ORDERING

HIGH FIDELITY LOUDSPEAKER UNITS

Cabinets latest style Satin Teak veneer. Acoustically lined or filled acoustic damping. Ported where appropriate. Credit terms available.

DORCHESTER (Illustrated) Size 19x11x9in. appr. Range 46-15,000 c.p.s. Rating 8-10 watts. Fitted litiph thus 13x8in. 49-45 Carr. 40p.

STANWAY II Size 20x 101x91jin. approx. Rating 10 watts. Inc. 13x8in. speaker with highly flexible cone surround, long throw voice coil and 10,000 line magnet. High flux tweeter. Handsome Scandinavian design cabinet. Hange 53:20,000 c.p.s. Inp. 8 ohms. Gives smooth realistic sound output. See 'package offers' for 419-35 cillustration.

R.S.C. TAI2 MKIII 6.5+6.5 WATT STEREO AMPLIFIER

R.S.C. [AIZ MKIII 6.5+6.5 WAITS STREO AMPLIFIER PULLY TRANSISTORISED, SOLID STATE CONSTRUCTION HIGH FIDELITY OUTPUT OF 6.5 WAITS PER CHANNEL Designed for outnum, performance with any crystal or ceramic Grain. P.U. cartridge, Railo tuner, Tape recorder etc. \$\frac{1}{2}\$ separate savitched input sockets on each clannel \$\frac{1}{2}\$ Separate Bass and Treble controls \$\frac{1}{2}\$ Slide Switch for mono use \$\frac{1}{2}\$ Speaker Output 3.16 ohms \$\frac{1}{2}\$ For 200-250 V. A.C. mains \$\frac{1}{2}\$ Frequency Reaponse 20-20,000 c.p.s. \$-28B \$\frac{1}{2}\$ Harmonic Distor 10.0 3.9 \$\frac{1}{2}\$ at 1,000 c.p.s. \$-100 \$\frac{1}{2}\$ M Harmonic Distor 10.0 3.9 \$\frac{1}{2}\$ at 1,000 c.p.s. \$-100 \$\frac{1}{2}\$ M Harmonic Distor 10.0 \$\frac{1}{2}\$ Substitution (1) 50mV (2) 400mV (3) 100mV. Output rating I.H.F.M. \$\frac{1}{2}\$ Harmonic Distor 10.0 \$\frac{1}{2}\$ Substitution 10.0 \$\frac{1}{2}\$ S

HI-FI SPEAKER ENCLOSURES MODERN DESIGN

Teak veneer finish. Acoustically lined. Sizes approx. Carr. 35p. per enc.

SEID FOR OUTSIAN WITH THE SPEAKER AND THE SPEA





R.S.C. BATTERY/MAINS CONVERSION UNITS

TYPE BMI. An all-dry battery eliminator. Size 54×44×2lin. approx. Completely replaces batteries supplying 1.5v and 30v, to battery radio where A.C. mains 200/250v. Sole/s is available. COMPLETE KIT 43-25 FOR USE FALLY 43-75

R.S.C. TA6 6 Watt HI-FI AMPLIFIER

200-250v. AC mains operated. Frequency Response 30-20,000 c.p.s. —2dB. Harmonic Distortion 0.3% at 1,000 c.p.s. Separate Base and Treble 'lift and cut' controls. 3 input sockets for Mike, Gram, Radio or Tape. Input selector switch. Output for 3-15 ohm spkrs. Max. sensitivity 5mV Output raing I.H.F.M. Fully enclosed enamelied case, 94-221×51m. Attractive brushed silver finish facia plate 102×32m. and matching knobs.

Complete kit of parts with full wrine diagrams and instructions. £7.75 Carr 40p OR FACTORY BUILT WITH 12 MONTHS' GUARANTEE £10.95

R.S.C. MkIII SUPER STEREO AMPLIFIER 30 FIDELITY

COMPLETELY NEW DESIGN **FURTHER IMPROVED IN BOTH** APPEARANCE and PERFORM-ANCE. REPRESENTING VALUE FAR HIGHER THAN THE

PRICES SUGGEST.

Only high grade components by 165p.

Carr.

Complete Kit of Parts

Or FACTORY BUILT with 12 months guarantee. Dep. £5.75 and 9 monthly payments £3.50 (Total £37:25).

Or FACTORY BUILT in cabinet as fillustrated. Dep. £7 and 9 monthly payments £3.99 (Total £42:91)

TECHNICAL DETAILS (Applying to each channel where appropriate)

CONTROLS: PUSH-BUITON SELECTOR (1) Disc (2) Radio (3) Tape (4) Mono L (5) Mono R (6) SPEAKER DIS. (7) Mains on/off. Bass, Treble and Balance. Plus Ceramic Mag P.U. Switch.



PRINTED CIRCUITRY TWENTY SILICON TRANSISTORS. FOUR DIODES. FOUR RECTIFIERS

SATIN SILVER METAL FACIA with black lettering. Black edged knobs with bright silver centre
PUSH-BUTTON SELECTOR SWITCHING

PUSH-BUTTON SELECTOR SWITCHING NEON INDICATOR JACK SOCKET FOR HEADPHONES CABINETED MODEL VENEERED IN SATIN TEAK, SUITABLE FOR ANY MODERN PICK-UP CARTRIDGE CERAMIC OF MAGNETIC, REGARDLESS OF PRICE WE RECOMMEND USE WITH THE BEST ANCILLARY EQUIPMENT THAT CAN BE AFFORDED.

OUTPUT: 15 watts R.M.S. (Continuous) Into 8 ohms.
10 watts R.M.S. (Continuous) into 15 ohms.
HUM & NOISE —75dB Min. Vol. —65dB Full Vol. HARMONIC DISTORTION
FREQUENCY RESPONSE: —3dB 7Hz to 70kHz
0-1% at 1000 Hz 10 Watts
TREBLE CONTROL: +16dB to —12dB at 14kHz
BASS CONTROL: +17dB to —16dB at 40Hz
SENSITIVITIES: Disc Mag. 2:5 mV. Ceramic 35m V. Radio 120mV. Tape 120mV.
REAR P ANAL SOCKETS ARE FOR 3 PAIRS OF INPUTS (1) P.U. (2) Radio.
(3) Tape Amp. Plus pair for tape recorder signal take off and 2 pairs for speaker connections.

RSC STEREO HI-FI TUNER NOW AVAILABLE. Visually matches Super 30 MkIII £44.95



TYPE C4100 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN

TYPE C48S 25-30 WATTS
Fitted four 8' high flux 8 watt speakers
Overall size approx. 48×10×56n. £17.75
Terms: Dep 23 and 9 monthly by monthly payments £2 (Total £21)

Carr. 50p.

TYPE C412S 50 WATTS
Fitted four 12" 11,000 line 15 watt speakers: Overall size approx. 56×14×9in mems: Dep. 24 and 9 monthly pay- 23 mems: £2:37 (Total £34·33) Carr. 75p £31

All types 15 Ohms covered in Regine and Vynair

(a) 100w POWER AMPLIFIER (b) PAIR OF HI-FI HEAD-

PHONES MATCHING DYNAMIC 'MIKE' (c) (attached to headphones)
(d) PAIR 50 WATT SPEAKERS
Black Rexine covered Cabinets

Size approx.
18"×18"×8"
(a) (b) (c) & (d)

18"×18"×8" Terms on Amps. Speakers and Head-phone/Mike. Deposit £15 and 18 monthly payments of £3.95 (Total

R.S.C.TDI DISCOCO NSOLE

R.S.C. TDI DISCOCO NSOLE
Incorporating twin Garrard SP25
ML.III turnitables and Geramic
Cartridges with diamond stylii.
Separate Vol. controls for each
turnitable. Also MONITORING
FACILITIES, plns Treble and Bass
Controls. Separate input for 'mike'
with vol. control switch. Black
Bexine covered Cabinet with lid.
see illus. on left
Carr. £1.25
C Dr. Dep. £13.25 and 9 mthly paymis £6.76
(Total £74) or Dep. £15 and 18 mthly
paymis £5.56 (Total £79.03).

FANE ULTRA HIGH POWER LOUDSPEAKERS ower ratings are R.M.S. continuous. 2 YEARS' GUARANTEE igh flux ceramic magnets. ALL CARRIAGE FREE. POP' 100 | 'POP' 50 | 'POP' 50

'POP' 100 18" 100 Watt 14,000 gauss 8/15Ω

£22.95 Dep. 26 and 9 nithly payments 22.20 (Total 225.80)

Dep. 23.30 and 9 ponthly payments. 21.30 (Total 215). Dep: £6 and 9

14,000 gauss 8/15Ω £12.90

15" 60 Watt

12" 50 Watt 13,000 gauss 15Ω £10.90

Dep £2 and 9 monthly payments £1.20 ments £1.20 (Total £12.80) PAIR SUITABLE ALL PURPOSES

TYPE C4100 100 WATTS Inc. four 12° 50 watt speakers for conservative rating. Extra heavy construction. Size approx. 58 × 16 × 10° Acoustically filled and pressurised. Terms: Dep. 511 and 9 mthly, pyts. \$67 °C (Total \$71.76). Carr. £1 R.S.C. A10 30 WATT ULTRA LINEAR

AND PUBLIC ADDRESS

HI-FI AMPLIFIER
Highly sensitive. Push-Pull high output, Hum level -70dB. Response Dept. Sensitive. Push-Pull high output, Hum level -70dB. Response Dept. Sensitive. Push-Pull high output, Hum level -70dB. Response Dept. Sensitivity 36 millivoits. For High Impedance microphones. For Clubs, Schools, Theatres, Dance Halls, Outdoor Functions, etc. For Electronic Organ, Guitar, String Bass, etc. Gram, Radio or Tape. Two separate inputs with vol. controls permit such as "mike" and Flek-up etc. to be used for mixing purposes, 200-250v. 50 c/s A.C. mains. For 3 and 15 ohm speakers. Complete Kit of parts with wring diagram and instructions. Twin-handled perforated cover 21-90. Or factory built with EL34 output valves and 12 months' guarantee for 219-75

Car. 55p
TERMS: Deposit 24 and 9 monthly payments of £2:10 (Total 222-90). Send SA.E. for leastle. TERMS: Deposit £4 and 9 monthly payments of £2:10 (Total £22:90). Send S.A.E. for leaflet.

CREDIT TERMS AVAILABLE ON PURCHASES OVER £8 (Kits Excepted)
INTEREST CHARGES REFUNDED ON CREDIT SALES Settled in 3 months

R.S.C. TRANSFORMERS, L.F. CHOKES & RECTIFIERS

FULLY GUARANTEED, Impregnated and Interleaved where necessary. ### HIDGET CLAMPED TYPE 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 2 | x 250mA, 6.3v. 4a c.t., 5v. 3a. £5.50 TOP SHROUDED DROP-THRO' TYPE 250-0-250v. 70mA, 6.3v. 2r., 0-5-6 3v. 2a.

vod where necessary.

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Types 6.3v. 1.5a. 49p; 6.3v. 2a. 54p; 6.3v. 3a. 78p;
6.3v. 6a. £1 30; 12v. 1a. 55p; 12v. 3a. or 24v.
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bot watts, ET 80 200 watte 22 75, 5000 watts 25 76 OUTPUT TRANSFORMERS Standard Pentode 5,000 Ω or 7,000 Ω to 3 Ω 509 Push-Pull 18 watts EL84 to 3 Ω or 15 Ω . 83p Push-Pull 10 watte 6V6, ECL86 to 3, 5, 8 of 15 Ω .

300-0-300v, 130mA, 6:3v. 4a., ct. 6:3v. 1a.
Suitable for Mullard D10 Amplifer. £2:60
350-0-350v, 100mA, 6:3v. 4a., 0:5-6:3v. 3a. £2:60
350-0-350v, 150mA, 6:3v. 4a., 0:5-6:3v. 3a. £2:60
1a. £5p. 2a. 55p. 3a. 55p. 4a. 65p. 6a. 55p.

FOR BASS GUITAR, ELECT. ORGAN, ETC.

FANE SPEAKERS 'POP' 25/2 12 in. 25 WATT Dual Cone 15 Ω (for uses £6.75 Carr. or Dep. £1 and 9 mthly other than Bass Guitar or Electronic Organ).

GROUP/DISCO EQUIPMENT PACKAGE OFFERS

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F.A.L. PHASE 100 AMPLIFIER 4 FANE POP 50 L/SPEAKERS Terms: Deposit £15.95 and 9 month payments of £10.50 (Total £110.45) nthly £34.95 £13.50 PACKAGE PRICE £45 carr. £48.45 PACKAGE PRICE 424.95 £52 carr. £56.75 PACKAGE PRICE £34.95 £23.90

£56 E1.25 £58-85 PACKAGE PRICE £61.95 £43.60

£99.95 CATT.

HIGH QUALITY LOUDSPEAKER UNITS ALL TWO TONE REXINE AND VYNAIR FINISH L125 50 WATT Fitted pair of 12" 50 watt high flux speakers for conservative

L125 50 WATT Fitted pair of 12" 50 watt high flux speakers for conservative rating. Impedance 8-15 ohms. Carr. £1:50 Or deposit £4:50 and 9 monthly payts. of £3:62. Total £37:08

L12/25 12" 25 WATT L13 13" × 8" 10 Watt 10,000 lines 3 or 15 ohms. Carr. 50p. L13 13" × 8" 10 Watt impedance required. Carr 40p £5:25

£105-55



FAL PHASE 50 MkIII AMPLIFIER 50W

Solid state. 4 Separately controlled inputs Plus master vol. control. Ind. Bass and Treble Controls. Protective circuit to guard against damage from accidental shorts. Output for damage from accidental shorts. Output for Spaker/s 3 to 30 ohms. Size 17×77×71, Or deposit £7-25 & 9 monthly payments £3-50. Total £38-76.

R.S.C. Branches listed below open all day Saturdays

BRADFORD 10 North Parade (Half-day Wed.). Tel.25349 BLACKPOOL (Agent) O & C Electronics 277 Church Street BIRMINGHAM 30/31 Great Western Arcade, Tel. 021-236 179 (Half-day Wed.). DERBY 26 Osmaston Rd., The Spot (Half-day Wed.). DARLINGTON 18 Priestgate (Half-day Wed) Tel. 41361

EDINBURGH

Hold Lothlan Rd. (Half-day Wed.). Tel. 229 9501
GLASGOW 326 Argyle St. (Half-day Tues.).
Tel. 248 4158
HULL 91 Paragon Street (Half-day Thurs.). Tel. 20505.
LEICESTER 32 High Street (Half-day Thurs.). Tel. 20505.
LEEDS 5-7 County (Mecca). Arcade. Briggate (Half-day Wed.). Tel. 28252
LIVERPOOL 73 Dale Street (Half-day Wed.).
Tel. 236 3573

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MANCHESTER 60A Oldham Street, (Half-day Wed.).
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HOSPITALS, HM. FORCES ETC.
MAIL ORDERS MUST NOT BE SENT TO SHOPS

RSC BASS-REGENT 50 WATT AMPLIFIER

A powerful high quality all-purpose unit for lead, rhythm, bass guitar, vocalists, gram, radio, tape. Peak Output rating. Loudspeaker unit optional horizontal or vertical

mounting.

*Two extra heavy duty 12in. 80w L'spkrs.

*Four Jack inputs and two Volume Controls for instant use of up to four pick-ups or "mikes". Bass and Treble controls.

Credit Terms; Deposit

215 & 9 monthly pyts of £6.25 (Total £71-25) £2 £65 Send S.A.E. for



RSC GP30 HI-FI AMPLIFIER

For Guitar, Vocal or Instrumental Group.

A 4 input, 2 vol. control Hi-Fi 30 watt unit with Separate Bass and Treble controls. Current valves. Peak output rating. Strong Rexine covered cabinet with handles. Attractive black/gold P.V.C. facia. Neon indicator. For 200-250v. A.C. mains. For 3 or 15 ohm speakers. Send S.A.E. for leaster. Terms: Deposit 24-40 and 9 monthly payments of 22-360 (Total 289-00). ents of \$2.40 (Total £28.00).





ORGAN KITS

Build your own Electronic Organ, if you want the best value for your money. Yes you really save over 50% and get the best and up-to-date designs. There are four models to choose from.

- ★ Portable—4 octave keyboard with 10 voices, 3 pitches—vibrato, at £103.00, P/P £1.50.
- Console—5 octave keyboard with 10 voices, 3 pitches. Keyboard can be split into solo and accompaniment. Vibrato built in amplifier and 50 watt 12" Goodmans speaker at £167.00, 50 watt P/P £5.00.
- Console—2 x 4 octave keyboards and 13 note pedal board, 29 voices, Vibrato, Delay Vibrato, Sustain Reverberation, Precussion, Wah Wah, etc. at £406 00. Carr. paid on complete kit U.K. only.
- ★ Console—2 x 5 octave keyboards and 32 note pedal boards, 32 voices. Vibrato, Delay Vibrato, Sustain Reverberation, Precussion, 3 Couplers, etc., at £572·55 carr, paid on complete kit U.K. only

We regret H.P. facilities are not available, but components can be bought separately. Trade and overseas enquiries can be bought separately. Trade and welcomed. Send 25p for latest catalogue.

Please call in for demonstration. Business hours: 10 a.m. to 7 p.m. Monday to Saturday. Thursday closed.

ELVINS ELECTRONIC MUSICAL INSTRUMENTS 8, PUTNEY BRIDGE RD., LONDON S.W.18 TEL: 01-870 4949

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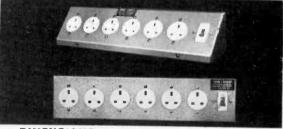
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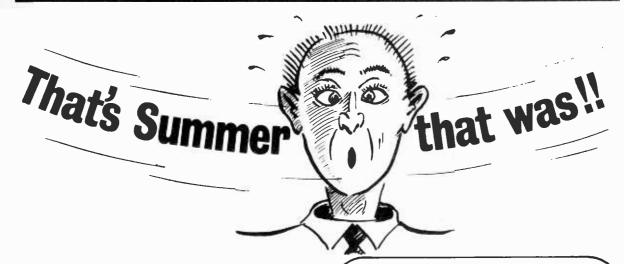
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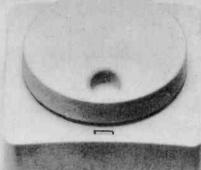
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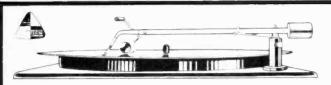
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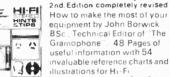
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Identical in style to

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818

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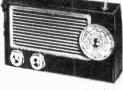
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3



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MILFI STREEO SYSTEMS COM HILFI STREEO SYSTEMS COM ALBA UA552 BUSH A1005 DANSETTE Consort Stereo DANSETTE CONSORT DECCA Sound 613 DECCA SOUND 613 DECCA SOUND 613 DECCA COMPACT 3 DECCA COMPACT 3 DECCA COMPACT 3 DECCA COMPACT 3 DECCA 403 DECCA 40	PLETE 47.75 69.89 34.43 71.45 Ial Pric 58.33 136.35 74.20 101.70 43.50 100.00 38.50	29 · 95 53 · 25 53 · 25 6 · 95 6 · 95 6 · 95 6 · 96 76 · 95 6 · 96 6 · 96 6 · 96 6 · 96 6 · 97 79 8 · 96 8 · 97 9 · 95 9 · 96 9
L/S). HMV 2451 HMV 2455 HMV 2450 HMV 2450 HMV 2450 MITH 657 speakers KB 2250 with 658 speakers KB 2010 with 658 speakers MARCONI 4452 MCDONALD MP60 complete with base, cover and Goldring 6800 cartridge, Amstrad IC 2000	165 · 00 122 · 00 66 · 00 138 · 00 48 · 25 124 · 00 101 · 50 77 · 00	125 · 75 95 · 95 48 · 95 106 · 95 37 · 95 95 · 95 77 · 95 56 · 95
amplifier. 2 Wharfedale Denton speakers MURPHY 902 Studio 1, AM/VHF	114-96	74 - 40
MURPHY 902 Studio 1, AM/VHF Radio MURPHY 903 PHILCO FORD M1500 PHILIPS 808 PHILIPS GF824	84 · 50 84 · 42 97 · 96 93 · 50 65 · 30	65 · 95 66 · 75 71 · 95

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AC107 AC113	0·20 0·20	AD162 AD161 &	0.38	BC148 BC149	0·10 0·12	BD137 BD138	0.45	BF188 BF194	0·40 0·12	OC19 OC20	0·35 0·63	2G371 2G371B	0·16 0·12	2N2219 0.2 2N2220 0.2	0 2N3054 2 2N3055	0.46	2N4059 2N4060	0·10 0·12
AC115	0.28	AD162 (M	(P)	BC150	0.18	BD139	0.55	BF195	0.12	OC22	0.38	2G373	0.17	2N2221 0 · 2		0.14	2N4061	0.12
AC117K	0.20		0.55	BC151	0.20	BD140	0.60	BF196	0.14	OC23	0 · 42	2G374	0.17	2N2222 0 2			2N4062	0.12
AC122 AC125	0.12		0.50	BC152 BC153	0 17	BD155 BD175	0.80	BF197 BF200	0.14	OC24 OC25	0.56	2G377 2G378	0.30	2N2368 0 1 2N2369 0 1		0.14	2N4284 2N4285	0.17
AC126	0·17 0·17	AF114 AF115	0.24	BC154	0.30	BD176	0.60	BF222	0.95	OC26	0.25	2G370	0.16	2N2369A 0-1		0.14	2N 4286	0.17
AC127	0:17	AF116	0.24	BC157	0.18	BD177	0.65	BF257	0.45	OC28	0.50	2G382	0.16	2N2411 0 · 2	4 2N3395	0.17	2N4287	0.17
AC128	0.17	AF117	0.24	BC158	0-12	B D178	0.65	BF258	0.60	OC29	0.50	2G401	0.30	2N2412 0 · 2		0.21	2N4288	0.17
AC132	0.14	AF118	0.35	BC159	0.12	BD179	0.70	BF259	0.85	OC35	0.42	20414	0.30	2N2646 0 4		0.21	2N4289 2N4290	0·17 0·17
AC134 AC137	0·14 0·14	AF124 AF125	0.30	BC160 BC161	0 - 45	BD180 BD185	0·70 0·65	BF262 BF263	0 · 55	OC36 OC41	0·50 0·20	2G417 2N388	0.25	2N2711 0 · 2 2N2712 0 · 2		0.42	2N4290 2N4291	0.17
AC141	0.14	AF126	0.28	BC167	0.12	BD186	0.65	BF270	0.85	OC42	0.24	2N388A	0.55	2N2714 0 2		0.15	2N4292	0.17
AC141K	0-17	AF127	0.28	BC168	0.12	BD187	0.70	BF271	0.30	OC44	0.15	2N404	0.20	2N2904 0·1	7 2N3415	0.15	2N4293	0.17
AC142	0.14	AF139	0.30	BC169	0.12	BD188	0-70	BF272	0.80	OC45	0.12	2N404A	0.28	2N2904A 0 2		0.28	2N5172	0.12
AC142K	0.17	AF178	0.50	BC170	0.12	BD189 BD190	0·75 0·75	BF273 BF274	0.35	OC70 OC71	0.10	2N524 2N527	0 - 42	2N2905 0 2 2N2905A 0 2		0·28 0·75	2N5457 2N5458	0.32
AC151 AC154	0.15	AF179 AF180	0.50	BC171 BC172	0.14	BD190	0.85	BFW10	0.60	OC72	0.14	2N598	0.42	2N2906 0·1		0.09	2N5459	0.40
AC155	0.20	AF181	0.45	BC173	0.14	BD196	0.85	BFX29	0.27	OC74	0.14	2N599	0.45	2N2906A 0 · 1		0.10	28301	0.50
AC156	0.20	AF186	0.45	BC174	0.14	BD197	0.90	BFX84	0.22	OC75	0.15	2N696	0.12	2N2907 0-2	0 2N3703	0.10	28302A	0.42
AC157	0.24	AF239	0 · 37	BC175	0 22	BD198	0.80	BFX85	0.30	OC76	0.15	2N697	0.13	2N2907A 0 · 2		0/11	28302	0.42
AC165	0.20	AL102	0.65	BC177	0.19	BD199 BD200	0·95 0·95	BFX86 BFX87	0.22	OC77 OC81	0.25	2N698 2N699	0·24 0·35	2N2925 0·1 2N2924 0·1		0.10	28303 28304	0.55
AC166 AC167	0.20	AL103 ASY26	0·65 0·25	BC178 BC179	0·19 0·19	BD200	0.80	BFX88	0.22	OC81D	0.15	2N706	0.08	2N2925 0 · 1		0.11	28305	0.84
AC168	0.24	ASY27 .	0.30	BC189	0.24	BD206	0.80	BFY50	0.20	OC82	0.15	2N706A	0.09	2N2926 (G)	2N3708	0.07	28306	0.84
AC169	0.14	ASY28	0.25	BC181	0.24	BD207	0.95	BFY51	0.20	OC82D	0.15	2N708	0.12	0 · 1	2 2N3709	0.08	28307	0.84
AC176	0.20	A8¥29	0 25	BC182	0.10	BD208	0.95	BFY52	0.20	OC83	0.20	2N711	0.30	2N2926 (Y)	2N3710	0.09	28321 28322	0·56 0·42
AC177	0.24	ASY50	0.25	BC182L	0.10	BDY20 BF115	1·00 0·24	BFY53 BPX25	0·17 0·85	OC84 OC139	0.20	2N717 2N718	0.35	0·1 2N2926 (O)	1 2N3711 2N3819	0.09	28322A	0.42
AC178 AC179	0.28	ASY51 ASY52	0.25	BC183 BC183L	0.10	BF115	0.45	B8X19	0.15	OC139	0.20	2N718A	0.50	0.1		0.50	28323	0.56
AC180	0.17	ASY54	0.25	BC184	0.12	BF118	0.70	B8 X 20	0.15	OC169	0.25	2N726	0-28	2N2926 (R)	2N3821	0.35	28324	0.70
AC180 K	0.20	ASY55	0.25	BC184L	0 12	BF119	0.70	B8Y25	0.15	OC170	0.25	2N727	0.28	0 · 1		0.28	28325	0.70
AC181	0.17	ASY56	0.25	BC186	0.28	BF121	0 - 45	B8 Y26	0.15	OC171	0.25	2N743	0.20	2N2926 (B)	2N3903 0 2N3904	0.28	28326 28327	0.70
AC181 K	0.20	ASY57 ASY58	0.25	BC187	0.28	BF123 BF125	0.50	BSY27 BSY28	0.15	OC200 OC201	0·25 0·28	2N744 2N914	0.20	2N3010 0 7		0.30	28701	0.42
AC187 AC187 K	0.22	A8Z21	0.25	BC207 BC208	0·11 0·11	BF127	0.50	BSY29	0.15	OC202	0.28	2N918	0.30	2N3011 0 1		0.27	40361	0.40
AC188	0.22	BC107	0.09	BC209	0.12	BF152	0.55	BSY38	0.18	OC203	0.25	2N929	0.21	2N3053 0·1	7 2N4058	0.12	40362	0 · 45
AC188K	0 - 20	BC108	0.09	BC212L	0.11	BF163	0.45	BSY 39	0.18	OC204	0.25	2N930	0.21					
ACY17 ACY18	0.25	BC109 BC113	0·10 0·10	BC213L BC214L	0-11 0-14	BF154 BF155	0.45	BSY41	0.28	OC205 OC309	0.35	2N1131 2N1132	0 · 20 0 · 22		0		*****	
ACY19	0.20	BC114	0.15	BC225	0.25	BF156	0.48	B8Y95	0.12	P346A	0.20	2N1302	0.14	Di	ODES AND	RECTI	TERS	
ACY20	0.20	BC115	0.15	BC226	0.35	BF157	0.55	BSY95A	0.12	P397	0.42	2N1303	0.14	AA119 0.0		0.21	OA10	0.35
ACY21	0.20	BC116	0.15	BCY30	0:24	BF158	0.55	Bu105	2.00	OCP71	0 - 43	2N1304	0.17	AA120 0-0		0.50	OA47	0·07 0·07
ACY22	0.16	BC117 BC118	0.15	BCY31 BCY32	0 · 26 0 · 30	BF159 BF160	0.60	CILLE C400	0.50	ORP12 ORP60	0.43	2N1305 2N1306	0·17 0·21	AA129 0.0 AAY30 0.0		0.42	OA70 OA79	0.07
ACY27 ACY28	0·18 0·19	BC118	0.10	BCY32 BCY33	0.22	BF162	0.40	C407	0.25	ORP61	0.40	2N1307	0.21	AAZ13 0-1		0.35	OA81	0.07
ACY29	0.35	BC120	0.80	BCY34	0.25	BF163	0.40	C424	0.20	ST140	0.12	2N1308	0.23	BA100 0·1	0 BYZ11	0.30	OA85	0.09
ACY30	0.28	BC125	0.12	BCY70	0.14	BF164	0.40	C425	0.50	ST141	0.17	2N1309	0.23	BA116 0.2		0.30	OA90	0.06
ACY31	0.28	BC126	0.18	BCY71	0.18	BF165	0.40	C426	0.35	T1843	0.30	2N1613	0.20	BA126 0 · 2 BA148 0 · 1		0.25	OA91 OA95	0.06
ACY34 ACY35	0·21 0·21	BC132 BC134	0·12 0·18	BCY72 BCZ10	0 · 14 0 · 20	BF167 BF173	0 22	C428 C441	0.20	UT46 2G301	0 - 27	2N1711 2N1889	0.20	BA154 0-1		0.35	OA200	0.06
ACY36	0.21	BC134 BC135	0.18	BCZ11	0.25	BF176	0.35	C442	0.30	2G301	0.19	2N1890	0.45	BA155 0 · 1		0.35	OA202	0.07
ACY40	0 17	BC136	0.15	BCZ12	0.25	BF177	0.35	C444	0.85	2G303	0.19	2N1893	0.87	BA156 0·1		0.28	8D10	0.05
ACY41	0.18	BC137	0.15	BD12I	0.60	BF178	0.30	C450	0.22	2G304	0.24	2N2147	0.72	BY100 0.1		0.1	8D19 1N34	0 - 05
ACY44	0.35	BC139	0.40	BD123	0.65	BF179 BF180	0.30	MAT100 MAT101	0.19	2G306 2G308	0.40	2N2148 2N2160	0.57	BY101 0-1 BY105 0-1	2 (Eg) OA	0.05	IN34A	0.07
AD130 AD140	0·38 0·48	BC140 BC141	0.80	BD124 BD131	0.60	BF181	0.30	MAT120	0.19	2G309	0.35	2N2192	0.35	BY114 0-1	2 CG651		1N914	0.08
AD142	0.48	BC142	0.30	BD132	0.60	BF182	0 - 40	MAT121	0.20	2G339	0.20	2N2193	0.35	BY126 0:1			1N916	0.06
AD143	0:38	BC143	0.30	BD133	0 - 65	BF183	0.40	MPF102	0.42	2G339A	0.16	2N2194	0.35	BY127 0-1		0.06	IN414B 18021	0·06 0·10
AD149	0.50	BC145	0.45	BD135	0.40	BF184 BF185	0.25	MPF104 MPF105	0·37 0·37	2G344 2G345	0·18 0·16	2N2217 2N2218	0.22	BY128 0-1 BY130 0-1		0.35	18951	0.10
AD161	0.33	BC147	0 · 10	BD136	0 - 40	DL 100	0.00	MIFIO	0.07	20340	0.70	2142210	0 20	21100 0.1	O GHOOD	0 01		3 00

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ì	PIV 1A	3 A	5A	5A	7A	10A	16 A	30A	
	TO5	TOS	6TO6	8TO6	4 TO 4	8T04	BTO4	8TO48	
	50 0 23	0.25	0.35	0.35	0.47	0.50	0.53	1.15	
	100 0 - 25	0.33	0.47	0.47	0.50	0.58	0.63	1.40	
	200 0 - 35	$0 \cdot 37$	0.49	0.49	0 57	0.61	0.75	1.60	
	400 0 - 43	0.47	0.56	0.56	0.67	0.75	0.93	1.75	
	600 0 - 53	0.57	0.68	0.68	0.77	0.97	1.25	winter	
	800 0.63	0.70	0.80	0.80	0.90	$1 \cdot 20$	1.50	4.00	

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П	PIV	300mA	750mA	1.A	1-5A	3 A	10A	30 A
		0.04	0.05				0.21	
		0.04	0.06	0.05	0.13	0.16	0.23	0.75
	200	0.05	0.09				0.24	
	400	0.06	0.13				0.37	
	600	0.07	0.16				0 · 45	
	800	0.10	0.17				0.55	
	1000	0.11	0.25				0.63	
	1200	-	0.33				0.75	

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T4	8	2G381T	OC81
T5	8	2G382T	OC82
T6	8	2G344B	OC44
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Q25	15 IN914 Silicon diodes 75 PIV 75mA	0.20
Q26	8 OA95 Germanium diodes sub-min	
Q27	IN69	0.50
Q28	2 10A PIV Silicon rectifiers IS425R 2 Silicon power rectifiers BYZ 13	0.50
029	A Silloon transistors 0 w nNege	0.50
4.0	4 Silicon transistors 2 × 2N696, 1 × 2N697, 1 × 2N698	0-50-
Q30	7 Silicon switch transistors 2N706	0 00
	NPN	0.50
Q31	6 Silicon switch transistors 2N708	
	NPN	0.50
Q32	3 PNP Silicon transistors 2 × 2N1131,	
~~~	1 × 2N1132	0.50
Q33 Q34	3 Silicon NPN transistors 2N1711	0.20
434	7 Silicon NPN translators 2N2369, 500MHz (code P397)	
Q35	3 Silicon PNP TO-5. 2 × 2N2904 &	0.50
200	1 × 2N2905	0 - 50 -
Q36	7 2N3646 TO-18 plastic 300 MHz NPN	
Q37	3 2N3053 NPN Silicon transistors	0.50
Q38	7 NPN transistors 4 × 2N3703, 3 ×	
	2N3702	0.50
		-

# ELECTRONIC SLIDE-RULE

The MK Slide Rule, designed to simplify Electronic calculations features the following scales:—Conversion of Frequency and Wavelength. Calculation of L. C. and fo of Tuned Circults. Reactance and Belf Inductance. Area of Circles. Reactance and Belf Inductance. Area of Circles. Weight of Conductors. Decibel Calculations. Weight of Conductors. Decibel Calculations. Multiplication and Division. Squaring, Cubing and Square Roots. Conversion of kW and Hp. A must for every electronic engineer and enthusiasts. Size: 2 cm × 4cm. Complete with case and instructions.

### INTEGRATED CIRCUIT PARK

Manufacturers "Fail Onts" which include Functional and Part-Functional Units. These are classed as 'out-of-spec' from the maker's very rigid specifications, but are ideal for learning about I.C's and experimental work.

Pak No.	Contents	Price	Pak No.	Contents	Price	Pak No.	Contents	Price
	12×7400	0.50	UIC46-		0.50	UIC86=	5 × 7486	0.50
	$12 \times 7401$	0.50	UIC47 =		0.50	UIC90 =	5×7490	0.50
	$12 \times 7402$	0.50	UIC48 =	5×7448	0.50	UIC91 ==	5 × 7491	0.50
	$12 \times 7403$	0.50	UIC50 ==	12×7450	0.50	UIC92 =		0.50
	12×7404	0.50	UIC51 =	12×7451	0.50	UIC93=		0-50-
	12×7405	0.50	UIC53 =	12×7453	0.50	UIC94=		0.50
UIC06 -		0.50	UIC54=	12×7454	0.50	UIC95 =		0.50
UIC07 =	8×7407	0.50	U1C60 ==	$12 \times 7460$	0.50	UIC96 =		0.50
UICIO =	$12 \times 7410$	0.50	UIC70 =		0.50		5 × 74100	0.50
UIC13 = 8	8×7413	0.50	UIC72 =	8 × 7472	0.50		5 × 74121	0.50
UIC20	12×7420	0.50	UIC73-		0.50		5 × 74141	0.50
UIC30 =	$12 \times 7430$	0.50	UIC74 =		0.50		5 × 74151	
UIC40 =	12 × 7440	0.50	UIC75 = 1		0.50		5 × 74154	0.50
UIC41 = 8	5 × 7441	0.50	UIC76		0.50		5 × 74194	
UIC42 = 1		0.50	UIC80=		0.50			
UIC43-		0.50	UIC81 =			010199=	5×74199	0.20
UIC44=		0.50			0.50			
UIC45 = 5			UIC82-		0.20	UICXI ==	25 Assorte	d
01040=	7 X /440	0.50	UIC83 = 5	×7483	0.50		74°s	1.50

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BN7403	0.15	0.14	0.12	BN7473.	0.37	0.35	0.32	
BN7404	0.15	0.14	0.12	8N7474	0.87	0.35	0.42	
8N7405	0.15	0.14	0.12	BN7475	0 · 45	0.43		
BN7406	0.35	0.31	0.28	8N7476	0.40	0 39	0.38	
8N7407	0 35	0.31	0.28	BN7480	0.67	0.64	0.58	
BN7408	0.18	0.17	0.16	8N7481	£1 · 20	£1·15	£1 · 10	
8N7409	0.18	0.17	0.16	BN7482	0.87	0.86	0.85	
8N7410	0.15	0.14	0.12	BN7483	#1 10	£1 · 05	0.95	
BN7411	0.25	0.24	0.23	BN7484	£1 · 00	0.95	0.90	
BN7412	0.35	0.31	0.28	BN7485	£3 · 60	£3·50	£8 40	
BN7413	0.29	0.28	0.24	BN7486	0.82	0.31	0.30	
SN 7416	0.43	0.40	0.38	8N7489	£5·50	25 25	£5·00	
567417	0.43	0.40	0.38	8N7490	0.67	0.64	0.58	
SN7420	0.15	0.14	0.12	SN7491	#1.00	0.95	0.90	
SN7422	0.50	0.48	0.45	SN7492	0.67	0.64	0.98	
BN7423	0.50	0.48	0.45	BN7493	0.67	0.64	0.58	
BN7425	0.50	0.48	0.45	8N7494	0.77	0.74	0.68	
8N7427	0.45	0.42	0.40	BN7495	0.77	0.74	0.68	
8N7428	0.70	0.65	0.60	8N7496	0.87	0.84	0.78	
BN7430	0.15	0.14	0.12	BN74100	£1·65	£1 · 60	£1·55	
BN7432	0.45	0.42	0 - 40	8N74104	0.97	0.94	0.38	
8N7433	0-80	0.75	0.70	8N74105	0.97	0.94	0.88	
8N7437	0.64	0.82	0.60	8N74107	0 · 40	0.38	0.36	
BN7438	0.64	0.62	0.60	BN74110	0.55	0.53	0.50	
8N7440	0.15	0.14	0.12	8N74111	£1 25	£1·15	\$1.10	
8N7441	0.67	0.64	0.58	8N74118	£1 · 00	0.95	0.90	
8N7442	0.67	0.84	0.58	BN74119	£1·85	£1 · 25	\$1.10	
8N7443	#1 - 30	£1.25	21.20	8N74121	0 · 40	0.37	0.34	
8N7444	\$1.30	£1.25	\$1.20	8N74122	£1·40	£1 · 30	£1·10	
BN7445	#1.80	\$1.77	81 - 75	8N74123	\$2.80	£2·70	£2·60	
8N7446	0.97	0.94	0.88	8N74141	0.67	0.64	0.58	
8N7447	£1.00	0.97	0.95	8N74145	£1 · 50	<b>81 · 40</b>	£1·80	
BN7448	\$1.00	0.97	0.95	8N74150	£3 · 00	\$2.70	£2·50	
BN7450	0.15	0.14	0.12	BN74151	£1 · 00	0 - 95	0.80	
BN7451	0.15	0·14	0.18	BN74153	£1·20	£1·10	0.95	
BN7453	0.15	0.14	0.12	BN74154	\$1.80	£1·70	£1 · 60	
8N7454	0.15	0.14	0.12	8N74155	\$1.40	£1·30	£1 · 20	
8N7460	0.15	0.14	0.12	8N74156	£1 · 40	£1·30	£1 ·20	
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D441410	0.59	V 20	0 22	2411 1801				

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BP 709P-µA70	9C 86p	34 p	30p
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BP930	12p	11p	10p
BP932	13p	12p	11p
BP933	18p	12p	11p
BP935	13p	12p	11p
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BP944	18p	12p	11p
BP945	25p	24p	22p
RP946	12p	11 p	10p
BP948	25p	24 p	22p
BP951	65p	60p	550
BP962	12p	11p	10p
BP9093	40p	88p	85p
BP9094	40p	88p	359
BP9097	40p	38p	359
BP9099	40p	38p	85p

Devices may be mixed to qualify for quantity price. Larger quantity prices on application. (DTL 930 Series only).

# NUMERICAL INDICATOR TUBES



MODEL	CD66	GR116	3015F Minitron
Anode voltage (Vdc)	170min	175min	5
Cathode Current (mA)	2.3	14	8
Numerical Height (mm)	16	. 13	9
Tube Height (mm)	47	32	22
Tube Diameter (mm)	19	13	12 wide
I.C. Driver Rec.	BP41 or 141	BP41 or 141	BP47
PRICE EACH	\$1.70	£1:55	#1-90

All indicators
0.9 + Decimal
point. All side
viewing. Full
data for all
types available
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### RTL MICROLOGIC CIRCUITS

Price each

Epoxy TO-5 case	1-24	25-99	100 up
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nL923 J-K flip-flop	50	47	45p

Date and Circuits Booklet for IC's Price 7p.

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0.1% DISTORTION! HI-FI AUDIO AMPLIFIER

# THE AL50

* Frequency Response 15Hz to ONLY 100,000-1dB.

★ Load-3, 4, 8 or 16 ohms.

★ Distortion—better than 1% at 1KHz.

★ Signal to noise ratio 80dB.

105mm × 13mm. Tailor made to the most stringent specifications using top quality components and incorporating the latest solid state circuitry and ALSO was conceived to fill the need for all your A.F. amplification needs. FULLY BUILT — TESTED — GUARANTEED.

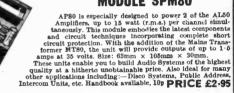
Volts.

STABILISED POWER **MODULE SPM80** 

£3.25p each

★ Supply voltage 10-35

★ Overall size 63mm ×



TRANSFORMER BMT80 £1.95 p. & p. 25p.

# STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit tecnniques. Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon planar transitiors, two of these are specially selected low noise NPN devices for use in the input stages. Three switched stereo inputs, and rumble and scratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable has a not replace controls.

bass and treble controls.

SPECIFICATION



Frequency Response Harmonic Distortion Inputs: 1. Tape Head
2. Radio, Tuner
3. Magnetic P.U.

All input voltages are for an output of 250mV. Tape and P.U. inputs equalised to RIAA curve within ± 1dB, from 20Hz to 20KHz. Bass Control

Bass Control
Treble Control
Filters: Rumble (High Pass)
Scratch (Low Pass)
Signal/Noise Ratio
Input overload Supply Dimensions

20Hz - 20KHz  $\pm$  1dB better than  $0\cdot1\%$  $1\cdot25$  mV into 50K  $\Omega$ 35 mV into 50K  $\Omega$  $1\cdot5$  mV into 50K  $\Omega$ 

± 15dB at 20Hz ± 15dB at 20KHz 100Hz

8KHz better than - 65dB better than + 26dB + 35 volts at 20mA + 35 volts at 20mA 292mm × 82mm × 35mm ONLY £11 95

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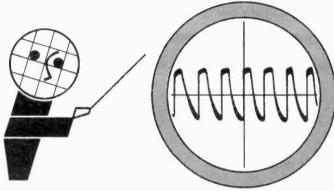
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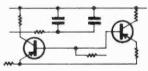
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RAPY

# RACTICAL RELESS

VNI 48 NN 6

Issue 788

OCTOBER 1972

# Wires and Waves

A SKED what type of aerial he uses, an enthusiast of the new generation might well reply "What's an aerial?" Apart from those multi-rod devices on the roof associated with television, the aerial is usually just another component fitted snugly inside the case of a transistor radio.

DX enthusiasts and amateur transmitters are, of course, alive to the importance of the external aerial, but there must be thousands of would-be DX-ers battling against the odds by trying to find exotic stations on ordinary transistor radios and relying only on the pickup capabilities of the internal ferrite rod assembly or at best a diminutive pull-out rod. While some success is possible under these conditions, experienced listeners will testify as to the vastly improved results obtained by using a well-designed external system, perhaps terminated in an aerial tuning unit.

It is not, however, just a matter of throwing out a random piece of wire and hoping for the best. Some thought must be given to the wavebands on which peak performance is wanted and the directions from which optimum reception is needed. In fact, devising an aerial can be quite as

absorbing as the building of active equipment.

The erection of an aerial system is more an art than a science, because the siting and lengths of wire are somewhat empirical. Formulae for dimensions and directions are based on the ideal conditions obtained in "free space" but the average amateur is rarely fortunate enough to have unrestricted space and a clear open site. The immediate terrain and features (hills, large buildings, etc.) may modify the ideal calculations and so there is a fruitful field here for experimentation.

Once embarked on the subject of aerials, it is a short step to begin thinking about what happens between the transmitter and the receiver. Here again is a complete field for exploration. One of the first things that an embryo DX-er has to learn is how the various phenomena associated with radio wave propagation are going to affect his listening activities. A good aerial system coupled with a knowledge of propagation are the foundations for success-

ful long distance listening.

That there is a need for information on aerials is borne out by the many letters we have received asking for help in this direction. The wall chart enclosed with this issue should provide all the basic material for those wishing to install a good aerial system, or improve their existing set-up, and it is complementary to the DX Data Chart supplied

with the March issue.

We have also included in this issue, an introductory article on radio wave propagation, which it is hoped will provide a further stimulus to investigation into this somewhat neglected, yet vital, sphere of interest.

W. N. STEVENS—Editor

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# FREE-AERIAL DATA WALLCHART

Some Readers may be aware of a slight loss of quality in printing. This is due to a shortage of our usual paper which has been brought about by the Dock Strike.

THE NOVEMBER ISSUE WILL BE PUBLISHED ON OCTOBER 6th

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# NEWS...

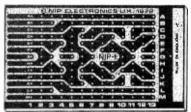
# NEWS...

# NEWS...

# Nip-E-Board

Remember some time ago we mentioned Nippiboard — the etched P.C. Board? Well now NIP Electronics, the manufacturers have announced additions to their range.

The Nip-E-System provides for a number of basic etched printed circuit board arrangements that can be used in many circuit applications immediately. The user then goes ahead with the component layout assembly and wiring, knowing that he does not need to worry about special designs or messy etching procedures. The basic layout design



STANDARDISED P.CB. FOR TRANSISTORS

procedures and photographic image transference have been done for the constructor. All the user needs to do is apply the standardised pattern to his circuit and assemble the components. Connectors are available as part of the Nip-E-System for single row and double row pattern arrangements of discrete or integrated circuits or both.

With the boards you get a choice of ready-made paper base laminate or epoxy glass fibre board  $^{1}_{16}$ in. (1·58mm.), a hole matrix 0·1in. (2·54mm.)×0·15in. (3·81mm.) and a choice of drilled or undrilled boards. A choice of board for discrete components only or a mixture of integrated circuits and discrete components is available and there is a choice of board size to take up to about

P.C.B. FOR I.C.

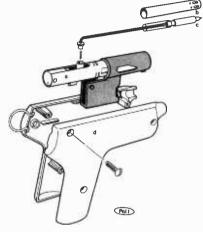


# Gas igniter



No. it's not a device for "doingin" Editors—it's a piezo electric gas igniter! It's guaranteed for ten years, does not need any batteries or flints, you don't have to plug it in the mains or hold it under a hot tap! While you pause for breath, we'll explain:

The device, made in Germany by Junkers, operates on the principle that if a sudden force is applied to the interfaces of various crystals, an electric charge results. In practice, when the trigger on this igniter is pressed, it releases a "firing" pin which deforms the piezo crystal and causes a discharge voltage in the region of 20kV to appear at the end of the pistol "barrel". The end of the barrel is designed like a car



sparking plug so that the spark (of  $50\mu S$  duration) jumps from the centre electrode to the barrel wall thus igniting the gas it is held near.

In the sketch (a) is the crystal mounting and housing unit. (b) and (c) are the points the spark jumps from and (d) is the plastic housing of the complete unit.

The Junkers Piezo Electric Gas Igniter is priced at £2·25 plus 15p postage and packing and may be obtained from Servitronix Limited, 572 Kingston Road, Raynes Park, London, S.W.20.

26 transistors (possibly more) in the 11E to 18E series or up to eight integrated circuits plus 16 transistors in the 21E to 28E series.

Constructors can have plug-in contacts for 14-way or 30-way gold-plated edge connectors (as supplied) for single row or double row boards, contact pitch 0·lin. (2·54mm.).

The customer choses the size most suitable to his application and the Company supplies a ready-made Nip-E-Board.

The boards are reasonably priced and they certainly help to make construction much easier and far neater.

If you would like further details of prices, accessories and layouts, drop a line to NIP Electronics, P.O. Box 11, St. Albans, Herts. They will be pleased to send readers their comprehensive free booklet on the Nip-E-System.

# Anyone help?

Our squadron has recently started a radio section, and all projects are of a self help basis, thus you may understand that supplies and money are very limited. The boys' ages vary from 13 years to 16 years.

I would be most obliged if through your column, I might request any radio hams etc who have surplus to requirements any books, components or radio equipment, to contact us.

All expenses for postage and packing would be refunded, and all communications acknowledged.

Please address all letters, parcels, etc. to:—Mr. G. H. Barker, "Training Officer", 2380, A.T.C. Dartmouth Sqdrn., "The Lodge", Longcross Cemetery, Townstal Road, Dartmouth, South Devon.

# NEWS...

# NEWS...

# NEWS...

# BI-PRE-PAK LTD.

Due to a printer's error in our August issue an incorrect price was quoted for the Complete Telephone as offered for sale by the above Company. The correct price should have read 95p. We offer our apologies to BI-PRE-PAK LTD. and to any readers who may have been inconvenienced by this error.

# Decoder

Motorola Semiconductors have announced the type MC1310 monolithic f.m. broadcast receiver stereo decoder which requires no external tuning inductors. Stereo channel separation is stated to be 40dB at 1kHz, with 0.3% total harmonic distortion.

# Dymo Star 1710

We recently had the opportunity to try out the Dymo Star 1710 labelling machine. This machine is ideal for stamping out the wording for the front panels of equipment.

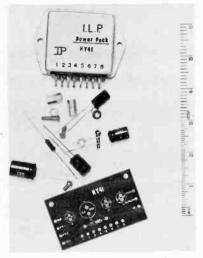
Letter selection is made by turning the dial wheel until the required character appears in the letter slot.

Technical symbol and character wheels may be fitted to this machine quite simply and different colour tapes are avail-

Full instructions are provided with each Dymo Star.



# IC power amp



The HY41 is a linear integrated circuit, power amplifier with an output of 20 Watts r.m.s. into 4-16 $\Omega$  having a total harmonic distortion of less than 0·15% (typical 0·05%) at 1kHz into 8 ohms.

P.C. board, resistor, capacitors, hardware mountings and comprehensive manual are all included in the basic kit, no further components being required in constructing a complete power amplifier of high performance.

Internally the HY41 is based on proven circuit techniques developed over recent years and is sufficiently versatile to provide power not only for Hi-Fi but for public address systems and industry.

Supplied by the Canterbury Company I.L.P. (Electronics) Ltd., the HY41 requires no adjustment whatsoever and can be assembled without recourse to sophisticated measuring equipment or electronics know how. I.L.P. (Electronics) Ltd., Crossland House, Nackington, Canterbury, Kent.

# **Rover-point**

Nettle Accessories Limited, a member of the Aerialite Group of Companies, announce the introduction of a portable extension lead to their range of electrical accessories, known as the "Roverpoint"

It consists of a 15 metre length of white 0.65 sq. mm. 3 core, P.V.C. cable, contained in a moulded plastic reel. A flush 13A socket is incorporated into the reel, and the cable is supplied complete with 13A plug.

The reel has a handle that can be utilised for carrying or hanging, and its rotating section is provided with two projections to facilitate easy rewinding.

Suitable for feeding loads of up to 1kW, with the cable fully extended and 500W with the cable coiled on the reel, "Roverpoint" sells at a recommended retail price of £3.99. Nettle Accessories Limited, Warren Street, Stockport. Cheshire.



# Sonex 73

Sonex 73, the high fidelity equipment exhibition organised by British Audio Promotions, will be held at the Excelsior Hotel, London, from March 30 to April 1.

# Erie catalogue

Erie Electronics have published a new comprehensive catalogue of their electronic components. It covers all product ranges, and catalogue contains specifications on all Erie distributor sales, Erie Electronics and Erie Controls products, as well as information on Erie thick film devices and Toshiba semiconductors. Copies are available from Erie Electronics Ltd., South Denes, Great Yarmouth, Norfolk.

# **Chadacre Electronics**

Please note their new address: 63 Stratford Broadway, London, E.15. Telephone 01-534 1207.

ESPITE the use of high power transmitters, used in conjunction with aerial systems of considerable gain and directivity, as well as extremely sensitive receiver techniques to accomplish a high standard of world-wide h.f. communication, the final merit of reception is controlled by many natural causes and variations.

# The Pioneers

The medium through which a radio wave must propagate, termed the Ionosphere, determines this final pattern of reception including field strength, fading and even "black outs." The early pioneers were well aware of the electro-magnetic wave with its effects though proof of its vast potential only came when Guglielmo Marcom established contact between Bournemouth and the 1sle of Wight in 1898. This was followed by an even greater breakthrough in 1901 when he transmitted the first telegraph signal from Poldhu, Cornwall to be intercepted at St. Johns, Newfoundland.

Research in this fleta by many workers revealed great discoveries. The name of mathematician Oliver Heaviside in England, who propounded the existence of a Conducting Layer in the upper atmosphere in 1892, as well as the work carried out by Kennelly in the U.S.A. as early as 1902 can never escapemention. Sir E. V/Appleton and M.A.F. Barnett, who determined the position of the Heavistee Layer in

on the atmosphere will show considerable variations when we consider the changes from day to night, the four seasons of the year and the eleven year cycle of the sun's regular variation. This solar cycle appears to follow an average change of 11-4 years; from one of minimum activity to maximum in 4 years and falling from maximum to the next minimum in 7 years. (The last maximum occurred in 1968 and present predictions are estimating the next minimum will occur in 1975). Differences of this kind affect the conditions of the atmosphere and as a result have considerable influence on the propagation of radio waves. The solar radiations affect the atmosphere and cause it to assume a "mirror-like" reflecting surface which return adio waves to earth

# Ionization

The radiation from the sun unsettles and excites the normal arrangements of the atoms and molecules of gas. This brings about a condition known as lonization; the atoms of gas become incomplete, having lost some of their electrons.

The region of ionization will therefore consist partly of free electrons and this process will continue so long as the earth's rotation permits that region of the almosphere to be exposed to the sun.

After souset this process reases and the free electrons rejoin their "mother" atoms, a process known as recombination, and this region will fall in ionized

# PRINCIPLES OF PR

1925, are also great names that we associate with

The many effects acting in different ways on radio signals during their passage from transmitter to receiver is indeed a great scientific subject—yet pethaps to the majority of readers the fascination lies in the fact that, even by using only simple equipment, signals may be intercepted from the other side of the world.

# Sun and Atmosphere

Let us consider how transmission of this kind is possible. A mode of propagation of this kind requires two essential and indispensible components, the atmosphere and the sun. The atmosphere, forming a gaseous envelope surrounding our planet, consists mainly of two gases, ditrogen and oxygen. This atmosphere is subjected to the full exposure and effect of the sun's rays, not only those of heat and visible light but of other radiations, including ultraviolet, gamma and X-rays, all bombarding our atmosphere after a journey of some 93 million miles. The effect of these rays falling on our atmosphere-permits long distance cadio communication.

# The Solar Cycle

The difference in the amount of sunlight falling

density. The ionized region is dalled a Eayer and is able to reflect the wave back to earth though it must be remembered that radio (like light waves) travel only in straight lines. To make use of this reflecting property the transmitted signal must be beamed in a skyward direction, as well as towards that part of the earth where it is to be heard. For long distance communication the radiated signal must leave the earth at a low angle so that the first encounter with the ionosphere will be as far away as possible. In the same way a signal with a high angle of elevation will reach the layer at a much closer distance and may be regarded as being more suitable for reception in a nearby area.

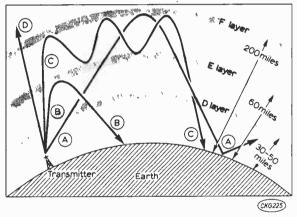
# Bending

It should be mentioned at this stage that the rays of the sun will be first absorbed by the upper part of the atmosphere so that the overall density of the layer will strow some variation. The radio signal coming up from the earth's surface will first enter an area of comparatively low density but as it enters deeper into the ionized region it will encounter area of greater free electron density. The wave will meet an adverse force, presenting some opposition to its progress. It is convenient to think of the radio wave behaving in a similar way to light when considering how it is turned in the jonosphere to be

returned to earth (both travelling at a speed of 186,000 miles per second).

# Hop and Skip

The word Refraction or Deflection explains this particular point in that a ray is changed in its course after entering a medium differing in density from one through which it has already passed. In this way the wave will be turned away from its original path and, providing the density of the medium and the frequency of the vibration are suitable, a point will be reached where the wave will be turned from its original route so as to follow a parallel course with the layer. Eventually it will be completely turned and leave the ionosphere at a similar angle as that of entry. The wave will return to earth having accomplished its first Hop-leaving a Skip distance between the sending and receiving points suggesting an area of silence existing between them. This is not so because the width of the transmitting beam will usually cover a considerable angle and the random scatter of the downcoming wave due to irregularities of the ionosphere tends to fill in this void. The second hop is made possible by an



Representation of the various methods by which radio waves are propagated. The main layers (D, E and F) are shown with their approximate heights above the earth's surface; the F layer is shown simplified—see text. The wave A is the normal long hop transmission; further reflection may take place when it meets the earth's surface. For reception in nearby areas the signal is beamed at a higher angle and is reflected by the E Layer.

C shows a form of propagation that is thought to occur at times. A number of reflections take place between the upper layers before the signal is returned to earth. If the angle of radiation is too high (and the frequency unsuitable) the waves will be lost in space as shown by D.

upward reflection from the earth's surface but the effectiveness of this is somewhat variable. It will depend upon the texture of the particular area of the earth's surface. Sea water is excellent, next comes pastoral land, while at the lower end of the scale desert areas may be regarded as poor; all have different conduction values. There is no rigid limit as to how many hops may take place since these are governed by the height of the layer at the time of transmission, the radiation pattern given by the aerial and the distance to be covered as well as the original transmitted power.

Some idea of a professional mode of transmission may help to make this point clear; the path from the United Kingdom to India needs three such hops and that to Australia six or seven. It will now be clear that although the wave will follow only a straight line, the curvature of the earth has been overcome by each individual hop although so far the ionosphere has been considered as one reflecting region. This is not so and it does in fact consist of several parts, each playing a different role and each one having a profound effect upon the wave.

# D Layer

The basic structure of the ionosphere starts with that area known as the  $D\ layer$ , situated between 30 and 50 miles above the earth; this becomes very dense by day but falls to a very low level—almost non existent—at night. During the hours of daylight it will cause considerable attenuation of the signal due to absorption, particularly to the lower frequencies. This effect is well known to the medium wave DXer as long distance reception on this band is virtually confined to the 'locals' until after sunset when the D Layer will begin to fail.

# E Layer

The *E Layer* (sometimes known as the *Kennelly-Heaviside Layer*) lies about 60 miles above the earth and although not the most important part of the ionosphere, it is responsible for the reflection of both medium and short waves.

A particular development of the E region, which at times can produce really sensational forms of propagation, is that known as *Sporadic E*. As the term implies this condition is irregular and cannot be forecast with any accuracy. An increase in ionization takes place usually around noon in our latitude. These abnormal conditions permit the reflection of very high frequencies and even enable TV signals to be observed from distant stations.

# F Layer

The topmost layer is that known as the *Appleton* or F Layer. The height varies from about 200 miles upwards and ionization is mainly confined to nitrogen as at this height oxygen becomes rare. The F Layer is frequently considered as the most important. It becomes divided into two parts during daylight, the upper part designated as  $F_2$  and the lower portion  $F_1$ . After sunset, and prior to dawn, it assumes the form of only one layer.

# Frequency Choice

Having examined the structural and reflecting arrangements which affect the wave, let us now consider how these various parts are put to practical use. Most of us are aware of the general rule that high frequencies are most useful by day and the lower ones give the best performance by night, although the exact choice of frequency used is critical if reception is to be of a standard worthy of being termed a service. Indeed, numerous observations are needed to formulate the vast number of short wave schedules published in advance which have to take into account the many factors already mentioned.

# Ionosphere Sounding

Such information is compiled by "sounding" the ionosphere. A radio wave with an adjustable frequency is sent vertically upwards to a layer so that it is able to engage it at right-angles and then the

# Radio Propagation Characteristics

Frequency	Day	Night	
A. 100kHz-400kHz	Reception very dependent reception possible at distance		
B. 400 kHz-1·5MHz	Ground wave reception only, usually no more than 200 miles but certain winter conditions can increase this to 1000 miles.	'Skip' takes place and reception of stations up to 1000 miles is common with not infrequent reception of stations at much greater distances.	
C. 1·5MHz–3MHz	Similar to B but distant reception more common.	Varies with conditions but similar to, and usually better than, B.	₹
D. 3MHz–8MHz		tations much easier and more al thousand miles especially at	
E. 8MHz–15MHz	Generally the best frequencies for DX but ground wave absorption limits local reception.	Often good for long distance reception but depends on conditions and time of year.	
F. 15MHz–25MHz	As for E but DX, although often better, is more dependent on conditions.	Usually poor for long distance reception but dependent on time of year and conditions.	<b>*</b>
G. 25MHz-45MHz	Highly dependent on conditions—sometimes excellent DX is possible but more often unsuitable.	Local reception only.	\$* ^{\$}
H. 45MHz-120MHz		occasional 'freak' conditions, pressure areas—when stations y can be received.	*
I. 120MHz-250MHz J. 250MHz-1GHz		more than 30 miles. Signals occasional freak conditions give	. 3*

frequency is adjusted so that it can be observed to either penetrate the ionosphere or be reflected back to earth. When this frequency is found—the highest limit to which the frequency can be raised and retain its reflection—it is known as the *Critical Frequency*.

Having obtained this frequency it may be increased up to three or even five times, provided the wave is radiated in such a manner and angle that it will meet the layer at a slanting or oblique angle. Such arrangements may appear straightforward but in the case of a multi-hop circuit—perhaps one crossing the equator or a dusk and night period—the requirements become complex, requiring many calculations and even some compromises to meet the variations over the path. The wave for reflection from the F Layer will, even during its first hop, need to be strong enough not only for reflection but to overcome losses through absorption when it passes through the D and E regions. It will, in fact, have to pass through these lower layers on two occasions even during its first hop.

# S.I.D.

We often hear on the amateur bands comments such as "Conditions aren't too good today". Such remarks refer to changes in propagation which can broadly be placed in two categories, one type of disturbance is referred to as a Dellinger or SID (Sudden Ionospheric Disturbance). This is often of a sensational effect happening in a very short time—so suddenly that the receiving equipment is often suspected. The effect is brought about by solar action

which causes an overwhelming ionization of the D Layer leading to almost complete absorption.

The lower frequency end of the shortwave band is most affected and signals in this part may even become inaudible. The higher frequencies are less affected and will be the last to suffer losses and the first to return to normal. The duration of such disturbance is usually short lived.

When the face of the sun looking towards the earth is subjected to an eruption, solar flare (often called a sun spot) this brings about the emission of numerous kinds of radiation. These vary in their intensity but when of a great magnitude, may persist for a long period. For these reasons this kind of unsettled condition may reoccur with a complete rotation of the sun in approximately 28 days. The *Dellinger* or *SID* will normally only effect that side of the earth facing the sun.

# Ionospheric Disturbance

A more prolonged type of disturbance known as an *Ionospheric Disturbance*—or *Storm*—may also be associated with solar conditions and often occurs some 30 hours after observation of changes on the surface of the sun. The general merit of reception falls considerably with deep and sometimes rapid flutter fading due to a lower and variable density of the F Layer.

Having described such adverse conditions, the reader may begin to wonder how a wave survives for so many thousands of miles, and especally as variations in the signal strength may be as much

as 1000 to 1, yet so much in modern receiver design is included to bring these variations to a stable and acceptable listening quality. The information given in the chart headed "Radio Propagation Characteristics" should be of value in helping to choose the correct wave bands.

# Reception Reports

Considering the complexities and variations in propagation it is not surprising that all broadcasting organisations giving a service in the international broadcasting bands welcome accurate reception

reports from listeners.

Considerable sums of money are spent each year to inform the listener of recommended frequencies and times of operation. Even after a schedule is published, the broadcaster is still in need of accurate information regarding the level of interference, as the shortwave bands are so congested—a situation which will become worse as we move to solar minimum conditions and the higher frequency bands become less useful.

# Medium Waves

Most of these remarks have concerned the short waves or high frequencies as these are the ones most used for long distance reception. However, reception of distant stations is also possible in the medium wave band (525-1605kHz). MW Dxing is made especially difficult due to the large number of high powered stations operating in Europe. This wave hand is basically designed for local reception and there are far fewer opportunities for long distance listening, even after midnight. Owing to so many broadcasters extending their hours of broadcasting such services frequently include an aerial system designed to avoid the sky wave and emphasise the ground wave. This reduces after dark interference and at the same time permits an economy by the sharing of frequencies. Listening to stations operating in the MW band is in any case confined to the hours of darkness if reception from a great distance is the aim. After dark these frequencies are reflected by the E Layer; the D Layer at night being almost non-existent. There are cases, however, when frequencies approaching 2MHz find reflection from the F Layer, having penetrated the E region.

# Other Bands

Other bands are subjected to other influences; remarkable reception due to tropospheric propagation in the VHF and UHF bands occurs occasionally. An outstanding example of the abnormal mode of propagation is that in earlier sunspot maximum periods, BBC Television pictures have been resolved as far away as the West Indies and South Africa.

Many listeners appear to associate bad weather, such as rain and fog, with either good or bad reception but there is no real evidence to substantiate this, at least not as far as the medium and shortwave bands are concerned. As the frequency is increased towards the microwave portion of the spectrum, that above 1000MHz, these and other factors have to be taken into account.

At a recent press conference given by the GPO Telecommunications Department, many interesting facts were disclosed concerning the adverse effects of rainfall over even short path transmissions on these channels.

# PRACTICAL MERIAL DATA WALL CHART

E expect rather a lot of our receivers don't we? In the early days of radio most homes sported a beautiful long wire aerial but with the tremendous improvement in receiver design and the vastly improved sensitivity we seem to have forgotten just how important a decent aerial is. Some receivers now being marketed claim that the silly little telescopic aerial which is an integral part of the set is all that is needed—rubbish!

For good DX results three things are needed, all of about equal importance: the receiver, the skill of the listener and the aerial. The receiver will cost quite a bit of money and the skill can only be learned with time; on the other hand an aerial will cost very little—wire isn't all that expensive after all—and the erection will take only a few hours.

The type of wire is far from critical. Hard drawn copper is possibly the best, it doesn't stretch, but it is expensive. One of the best, and cheapest forms is aluminium garden binding wire. 250ft. reels cost only about 30p.

Ex-Government aerial wire is still available on the surplus market and this is excellent; it is usually made up from one strand of copper surrounded by

steel wires for strength.

On the Wall Chart we have tried to deal with practical types; it is all very well to read about wonderful professional arrays but few of us have the room or the money to pay for the tall masts required. Instead we have dealt with the types that readers are likely to have space for. Even if you live in a small flat you will usually be able to find room for a pretty good Whip Type, or even an Inverted L.

The chart deals with aerials but of course any signals induced into them will only be with respect to earth and a good earth should be used. One always used to see comments such as "... the earth wire can be taken to a cold water pipe..." but in these days of plastic plumbing this will not always work. A good earth can be made by soldering a wire to a piece of copper clad board—such as is used for making printed circuits; this should be buried as deep in the ground as can be managed and a bucket of water should then be poured over it to make the earth resettle around it. The size of the board is not critical but the larger the better. The wire from this earth to the receiver should be of very low resistance and as short as possible.

# reference Source DUTPUT SOURCE E. BUCKLAND

O one would deny that a full-range, full-facility audio signal generator is not useful. The author has a good one (built from a design published in Practical Wireless some years ago) and it is continually in use for designing, testing and trouble shooting but only a few of the facilities account for 95 per cent of the usefulness. Most of the time the frequency is left on 1kHz and only the calibrated output is used. When the frequency is varied it is nearly always at the spot frequencies of 100Hz, 1kHz and 10kHz. Nearly all signal generators have a switch to give either a sine-wave or square-wave output. This is frequently used but it is rare that the type of wave-form matters very much. Where it does matter, it is nearly always the square-wave that is required.

The main signal generator was found to be so useful that the author decided on building another, this time to be battery operated for portability. Bearing in mind the points made above it was also decided to make a far simpler and less expensive version, incorporating only the most useful facilities.

This unit gives a constant square-wave output—irrespective of battery voltage and other factors—at three spot frequencies: 100Hz, 1kHz and 10kHz. The output is continuously variable over a wide range. To simplify the switching, the on-off switch is incorporated with the frequency selector and the decade outputs are provided from separate output sockets.

The complete unit is very small, fitting nicely into a small aluminium box, 4in. x 2¹2in. x 2in. and the total cost is only a fraction of that for a full facility audio signal generator.

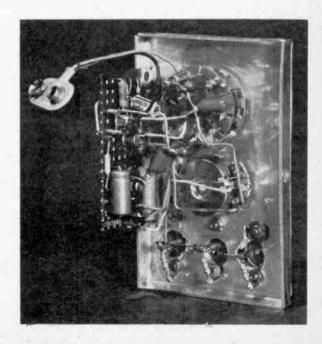
This makes an excellent "back-up" unit but even by itself it should be useful for those without an a.f. signal generator.

# THE CIRCUIT

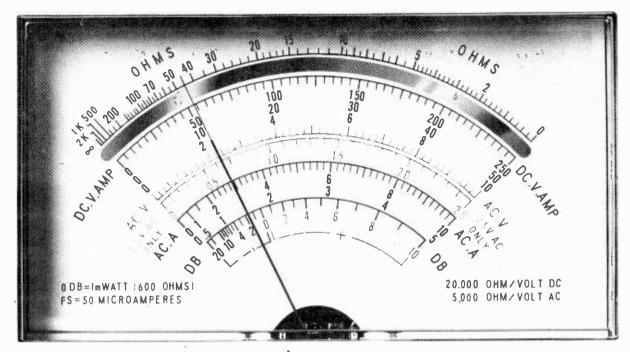
The signal oscillator is a basic multivibrator, made up from Tr1 and Tr2. Both halves of this are identical, with similar base bias resistors and the same collector load, although for Tr2 this is a variable potentiometer and not a fixed resistor as that for Tr1.

The values of the coupling capacitors are altered by the main switch, SWI, and one of three capacitors can be selected. This balance in the two sections ensures a square wave output with a 1:1 mark space ratio, not vital but easy to incorporate and occasionally useful. The values of the bias resistors etc., ensure that the transistors are driven on hard when they are turned on, this ensures that the output will be constant.

The output is taken from the collector load of Tr2, the slider of VR1 is connected via C2 to the base of the emitter-follower Tr3. The high value of C2 is deliberate, this will ensure no degradation of the tops and bottoms of the square wave at 100Hz. Tr3 was found necessary to isolate the output from the



Internal view of the prototype.



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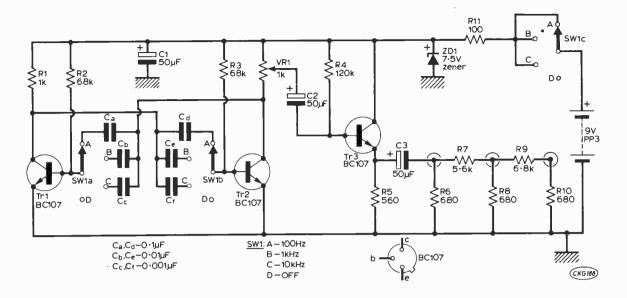


Fig. 1: Complete circuit of the Audio Reference Source.

multivibrator. As this stage contributes no gain it may be thought that the output network could be connected directly to the slider of VR1 but this would vary the load at the collector of Tr2 and affect the frequency and level. The inclusion of Tr3 makes certain that this interaction is minimal.

The output from the emitter of Tr3 is taken via the d.c. blocking capacitor C3 to a decade attenuator. At each of these output sockets the output is one tenth that of the previous one.

Because of the operation of a multivibrator, we can always be sure that the output will be constant, irrespective of frequency as long as the supply voltage is constant. This is done by including a zener diode with a rating of 7.5V in the positive supply line, the voltage drop taking place across the resistor R11. SW1 is a three-pole, four-way switch; three of the sections are used to alter the frequency of operation of the multivibrator, the fourth section acts as the on-off switch.

The whole circuit is very simple as can be seen from Fig. 1. BC107 transistors are specified but BC108, BC109 or their plastic versions (BC168 and BC169) can also be used, as can a 2N2926. None of

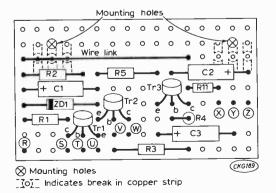


Fig. 2: The component layout on Veroboard. The only breaks in the copper strip are those near the mounting holes.

# * components list

<b>D</b>		· ` [	^ , 4
Resistors		. E	ş
R1, $1k\Omega$	™R7 5		± ,
R2 ₃ 68kΩ	R8 68		
R3 68kΩ - ×			`\$ .
R4 120kΩ	R10 68		
′. R5 ຶ <b>560</b> Ω	~. R11 10	200Ω	
R6 680Ω	å . · ./a	Cambra .	* *
,	**		* *
All resistors #W, 5 p			* .
$\sim$ VR1 1k $\Omega$ linear pot.	, c <b>arbo</b> n tra	ack 👢	laite. 🖎
40		< 1 - T	A 75
Capacitors ·	,	₿`, * ' E *	, , , , , , , ,
C1 50µF 10V min.	Ca,Cd 0	1 F Mylar o	r ceramic
C2 50µF × ,,**	Cb,Ce 0	-01μF	99
ČC3 50μF ,,	Cc,Cf 0	·001μF ,,	
		***	
Semiconductors	*	·	* * ,
Tr1 BC107 see te	xt Tr3 B	C107 see tex	ts 🥫 🤺
Tr2 BC107	-ZD1 7-	5V, 50mW ze	ner diode
	*	į.	
Miscellaneous	·* *	\ F	3 8
SW1, three-pole, for	ur-way rote	rv switch:	off coax
sockets-see text;	battery clir	· Veroboar	d. 16 x 9
holes, 0.15in. matrix;	small alun	ninium case	with lid.
Hores, o Tolli, matria,	, omign aran		38%

these changes will affect the constant output which is controlled by the supply voltage and nothing else.

VR1 should of course be a linear control and the associated knob can be calibrated if required.

The capacitors in the multivibrator may not give the exact frequency specified, this will depend on their tolerance, but it should be close enough for all practical purposes.

The unit takes only a small current and this is adequately provided for by a PP3 battery.

# CONSTRUCTION

The component layout of such a unit is far from critical but that used in the prototype is both simple and neat. The majority of the components are mounted on a small piece of 0.15in. matrix Vero-

board, 16 holes by 9 holes; this can be cut from a standard 212in, width. The component layout is shown in Fig. 2. Various take-off points are letter coded R to Z to tie up with the main wiring diagram in Fig. 3.

No breaks are necessary in the copper conducting strip of the Veroboard other than those near the mounting screws. The battery negative is taken to the board by a wire running from a small solder tag which fits under one of these mounting screws.

The frequency determining capacitors are mounted directly onto the switch SW1, this can be seen from

the photograph of the prototype.

The output sockets are mounted next to each other and the attenuating resistors are wired directly to these, the chassis connections being taken to solder tags under the mounting screws. Coax output sockets were used on the prototype mainly to continue standardisation in the author's test equipment but other types-such as phono sockets-can be used.

The component board is held onto the chassis by means of a short length of aluminium angle bracket.

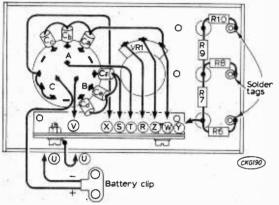


Fig. 3: The wiring diagram. The letters R-Z match up with those in Fig. 2.

# **CALIBRATION**

It is not possible to say what the exact output will be for any particular version, this depends on the saturation of the individual transistors, but what can be said is that it will not vary with frequency or battery voltage. If a highly accurate output is required this is best measured on a 'scope. The output can also be reduced to a reference figure by wiring in an extra resistor between the collector of Tr2 and VR1. If the output is say 2V and the maximum output wanted is 1V then a 1kΩ resistor will be required. The output from the prototype is 1.8V and this level has been found sufficient. The output from the other decade outputs is 180mV and 18mV at maximum output.

# **BACK NUMBERS**

We regret that the back numbers department of P.W. has now closed and consequently we are unable to supply these. Requests for specific back issues can usually be included in our 'CQ' section; there is no charge for this but it is a service between readers and P.W. is unable to meet any of these requests.



EWCOMERS to the medium waves are often surprised at the number of West African countries that can be heard on this band. La Voix de la Revolution located at Conakry in the Republic of Guinea, is a conspicuous signal on 1403kHz after 2300hrs GMT. Programming is African in style with announcements in French. The new high power broadcaster at Bissau, Portuguese Guinea can be logged on 1070kHz between 2300hrs and 0100hrs GMT with pop music, announcements and news being in Portuguese. From the Canary Islands, the high power Radio Nacional Espana outlet in Tenerife is a strong signal on 620kHz after 2300hrs. Programmes are in Spanish and there is interference at times from Batra in Egypt. Dakar, Senegal on 764kHz can be heard on weekdays with African music and French announcements after Sottons, Switzerland closes down. From the Republic of Zaire (Congo) the station at Kinshasa on 692kHz is on the air all night and is audible, with African programming after the East German station on this frequency signs-off, usually at 0100hrs GMT on weekdays. Radio Nigeria at Enugu is on 1320kHz until sign-off at 2300hrs GMT. Programmes are in English and can be found during the last half hour of transmission, as a weakish signal between the European channels 1313kHz and 1322kHz. Another English speaking broadcaster is occasionally heard on 629kHz. This is ELBC at Monrovia, Liberia which closes down at 0045hrs GMT and is usually logged towards the end of its transmission.

A new broadcaster in North Africa has appeared on the Long Waves. It is located in Algeria and is audible in the UK during the evening on 254kHz (1181m); a channel it shares with Lahti, Finland. Programmes are in French and reception reports, which are requested over the air, should be sent to Radio Television Algerienne, 21 Boulevard des Martyrs, Algiers, Algeria. This is the second North African to appear on the LWs in recent years. Azilal, Morocco is on 209kHz with programmes in Arabic and can be logged after dark with some interference from Kiev on the same channel. The range of long wave stations increases considerably at night-Europeans fade-in regularly along the eastern seaboard of North America after local sunset. Stations heard in the UK by the writer include Reykjavik, Iceland on 209kHz at 0100hrs GMT; Ashkhabad, Turkmenia on 200kHz after Droitwich signs-off; Ankara, Turkey 182kHz with sign-off at 1930hrs GMT; Baku, Azerbaijan on 218kHz at 0100hrs GMT; Novosibirsk 272kHz at 0130hrs and Omsk 394kHz at 1900hrs. In Europe, the long waves covers 151kHz to 282kHz but in Asiatic Russia the band extends to 400kHz. Regulars to be heard in the "hf" section are Orenburg 300kHz; Kharkov 384kHz and Minsk 400kHz.

Please send logs and information about the medium waves to the author at 132 Segars Lane, Southport PR8 3JG.

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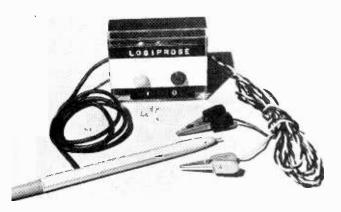
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## logiprobe



#### **LAURENCE COOK**

THE circuit to be described was designed to fulfil the need to see what was going on in TTL logic systems without having to use a voltmeter to determine whether a "1" or "0" existed at any point. To give a positive indication of the presence of a logic level it was decided at the outset to have two lamps, corresponding to a "0" or "1". Neither lamp would light with the probe either floating or at an inadmissible voltage (e.g. 1·2 volts).

Since the probe has been completed, it has proved extremely useful to me (and to those who have borrowed it!) and will doubtless soon repay its cost in time saved tracking down faults. It may even encourage people to "have a go" at logic circuitry, since it quashes the familiar cry, "I can't see what's going on inside those bugs".

#### CIRCUIT

Only four transistors, four resistors, two diodes and two bulbs are used (see Fig. 1). A few moments spent studying the circuit should enable one to spot

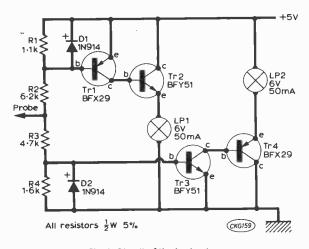


Fig. 1. Circuit of the Logiprobe.

the fact that it is really two circuits, one the inverse of the other; that is, Tr3 and Tr4 are arranged in a similar fashion to Tr1 and Tr2 but "upside down". The reason for this is simple.

With the probe on a logic "0" the voltage at Tr1 base, determined by the divider chain and probe voltage (>0.8V) causes Tr1 to turn on. Tr1 collector goes towards +5V and Tr2 emitter does the same, since Tr2 operates in common collector mode. LP1 therefore lights, indicating a logic "0". Similarly a logic "1" at the probe causes the voltage at Tr3 base to turn Tr3 on, and so Tr4 drives LP2, which lights up.

The resistors in the divider chain are of such values as to keep both lamps off when the probe is either floating or between 0.8V and 2.4V with respect to earth. Should the probe be accidentally touched on a voltage below earth or above +5V, then D2 or D1 respectively conduct to prevent the reverse base-emitter voltages of Tr3 or Tr1 being exceeded. Resistors R2 and R3 limit this current, but it is inadvisable to deliberately look for trouble by touching the probe onto higher voltage rails for long periods.

#### CONSTRUCTION

The logiprobe is assembled on a piece of 0.15 in matrix veroboard (see Fig. 2.), with flying leads for supply and lamps. This enables it to be housed in any convenient small plastic box. The probe may be made from an old ball-point pen. It is largely a matter of choice how one terminates the supply leads, but since the supply must be the same as that of the TTL circuitry to be tested, then small insulated crocodile clips would be handy.

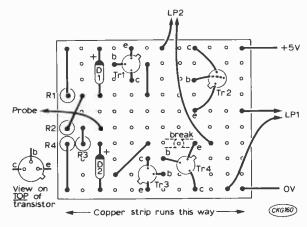
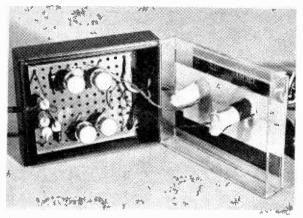


Fig. 2. Layout of the Logiprobe on a small piece of veroboard. Note that transistor leadout connections are shown as seen from on top.

Compare this layout with photograph of completed unit.

Start by cutting a piece of veroboard to the right size for the box, then solder flying leads as shown. Next solder in the resistors, diodes and transistors. Use a heatsink and a small well-tinned iron just in case the resistor values are altered by overheating them, since these determine the levels at which LP1 and LP2 light. For this reason R1 to R4 should be 5% or better, and not nasty old things out of that TV set recently butchered! Finally solder LP1 and LP2 onto their respective leads.



The lid of the box carries the two lamps which should be of differing colours, representing "0" or "1". The lamp terminals are insulated to prevent short circuits when the lid is fitted to the box.

#### TESTING

Connect the logiprobe to a 5V supply. If all is in order both lamps will be off. If not, either the supply is wrong, or a mess has been made of the board. Look for blobs of solder bridging the copper strips and get rid of them! If both or either of the two lamps are still on, make sure that everything is connected the right way round; we all make mistakes!

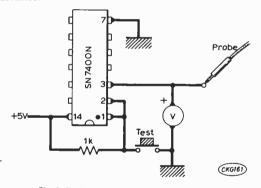


Fig. 3. Test set-up using an integrated circuit.

Touching the probe to earth or +5V should light LP1 or LP2; just to make sure all is well try the probe on an i.c. output with a voltmeter as a temporary check. (See Fig. 3).

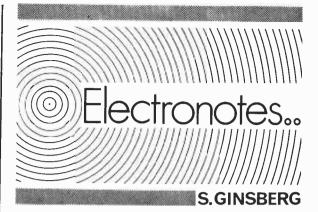
Finally, a word of warning. Unless one is prepared to fiddle for hours with stacks of resistors, use the components specified. If you can't resist trying different transistors, at least use silicon of a similar type.

When your logiprobe is finished you'll wonder how you managed without it. But keep it hidden or people will borrow it from you!

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NE so often reads about the amazing advances and research programmes which take place in other parts of the globe. It is, therefore, refreshing to hear of some work which is being done in this country. This is particularly so since the establishment in question is the Post Office Research Department at Dollis Hill.

Workers at Dollis Hill are experimenting with those intriguing things called magnetic bubbles. A new generation of words is now fast coming into being. For example, a "bubble eater" and a "keyhole generator" are commonplace.

Basically, one method of employing magnetic bubbles is to lay down a series of minute conductive elements in the form of "T" shapes. These are typically formed of nickel-iron and are of the order of  $1\mu$ m thick. The idea is that a tiny magnetic bubble can be transferred from one "T" to the next and even annihilated. Thus the bubbles can be used as a means of storing data. The bubbles themselves are only some  $10\text{-}18\mu\text{m}$  in diameter.

The workers at Dollis Hill have developed, and I kid you not, a bubble detector bridge (see what I mean about the terminology?). The idea is an extremely clever one. Four minute resistive arms of a bridge circuit are formed by a deposition of a very thin nickel-iron alloy which is less than 1000Å thick. The resistivity of this alloy changes whenever it is subjected to a magnetic field. Thus, when a magnetic bubble arrives at the bridge, its magnetic field will affect, say, two of the "resistors" effectively altering their resistances and thus unbalancing the bridge.

This work is impressive and follows closely on the heels of a previous announcement of work done here on transistors rated at around  $1\cdot 5$  Watts in the 4GHz region. These transistors were reported to have base widths of only  $0\cdot 14$  microns. Truly it is a small world.

Occasionally one hears news which is disturbing. Not only because of the actual content and what it implies, but also because of the reliable source from which is comes. This piece of news concerns lasers. One can use a laser beam and modulate it, thus using it to convey communications. If you "shine" a laser beam down a light fibre you can carry it from one place to the next. Again, it is possible to get quite a few "channels" on a laser beam, far more than you can on a single, comparable coaxial cable, for example. The thought now goes that for all communications work, land lines etc., lasers plus light fibres will be used. If this is true, then it could mean our old friend the coaxial cable is on the way out!

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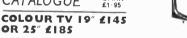
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#### **CQ** complaint

I wish to make a complaint regarding an advertisement in your CO column of June 72.

I supplied a S.A.E. and requested lists of issues especially Nov. 71 from a reader.

This was over a month ago and as yet have received no word from him. I think he must be collecting 3p stamps!

Would you please put an advert in your CQ column for me? I require Nov. 71 Practical Wireless or a copy of the article on the organ.—M. F. Longmore, (31 Kent Ave., Larne, Co. Antrim, N. Ireland).

#### **Construction** award

The 2nd G3XBF Constructors Award, sponsored by the Barking Radio and Electronics Society G3XBF—Affiliated to the Radio Society of Great Britain will be held on Thursday, November 9th, 1972 at the new BRES HQ: Westbury Recreation Centre, Westbury School, Ripple Road, Barking, Essex, at 7.45 pm.

Talk-in facilities are: 160m-G3XBF, on 2m—G8EAY/A, (TX 145·0). Judges: G. M. C. Stone, CEng, MIEE, MIERE, G3FZD, Council Member and v.h.f. Manager RSGB. D. A. Findlay, DFC, FCA, G3BZG, General Manager and Secretary RSGB. R. S. Hewes, G3TDR, Region 7 Representative RSGB.

There will be an award for each section and an overall winner. Each award will consist of a hand produced certificate and a worthwhile cash prize.

A film will be shown during the judging and refreshments will be available. Closing date for entries Wednesday, October 25th, 1972. Entry forms and further information may be obtained from Alan P. Foss, G8EAY, 73, Coolgardie Avenue, Chigwell, Essex. (01-500 6034).

#### VHF hope

So interesting is your August editorial on "Hope for VHF" that I could write sufficient about it to fill another!

VHF has not "caught on" for several reasons, and I will list a

few technical ones first. A v.h.f. radio costs 112 to 3 times as much as a comparable type for m.w. Invariably it uses at least two more transistors, which, so far as batteries are concerned, raise the quiescent current by about 10 per cent, and this is aggravated by the fact that v.h.f. oscillators are not only less stable in the face of falling voltage, but in fact actually cut out completely when the battery has still an appreciable amount of "life" in it usable on m.w. With battery manufacturers seemingly not knowing where to stop with their price-rises, and many of the receivers being of the "pocket" type, the matter speaks for itself.

But away from technical aspects, the BBC HAS something to answer for. As an example, take Sundays on Radio 4.

At 8.20 a.m., v.h.f. and m.w. part company, and unless one wants a Pakistani programme, he scraps his m.w. and goes v.h.f. But some 45 minutes later he is assailed by "Open University", so, out has to come his trusty m.w. I have always said that v.h.f. and m.w. should never part course, and neither should have Radios 1 and 2, because in the latter case the 247m, transmission was to fill up locally the areas not well served by Droitwich on 1500m. Since the service areas of the v.h.f. stations more nearly coincide with the centres of Pakistani population this would be the more logical frequency for that service. but better still these should be on the "Local" stations, since for a large part of their time they just repeat BBC programmes available at better quality on the regional stations a little along the dial. In North-Northumberland. listeners have to rely upon m.w. because v.h.f. is not reliable there, and there is no Pakistani population either!

I run a v.h.f. tuner to Mr. Cameron's excellent design a year or two ago in "P.W." and it does enable me to hear the broadcast distortion more clearly, for the programmes are either full of badly received telephoned matter, or of the "popular" type to which a bit of distortion makes little difference anyway.—James W. Robson, (Newcastle Upon Tyne).

#### **Thanks**

In the issue August 1972 your contributors H. Hellyer and M. Hollier continue with Part 9 of their excellent series "Transistor Circuitry for Beginners".

Their style is lucid and most readable, and in this issue we were particularly gratified to note their suggestion, page 341, "if Mullard Ltd. didn't exist, they would have had to be invented".

We especially appreciate their acknowledgement of (sic), "a direct crib from Chapter 3 of the Mullard Transistor Handbook". It is perhaps carping to indicate that reference should be made to the end of Chapter 2, and that the title used is ambiguous, in connection with other Mullard publications. For the benefit of readers wishing to supplement the information provided by your contributors the correct title should be "Transistor Audio and Radio Circuits".

L. W. Owers, Manager—Educational Service, Mullard Ltd.

#### **VHF** services

With regard to your editorial column in the August *Practical Wireless*, I would, as a newcomer to the arts of practical electronic work, like to make one comment.

Although your column makes a fair general statement, I feel that one reason for the lack of use of v.h.f. services is the fact that reception in many areas (for example the Pennine valley in which I live) is very difficult. This problem may, I suppose, be overcome by the erection of a dipole aerial but the average radio listener is still faced with the fact that very few of the popular battery operated portables are equipped to take a coaxial or twin feeder from an external aerial (idea for a future article?). The so-called "v.h.f. telescopic aerials" fitted to these sets are virtually useless in these sheltered areas.

Of course, when one writes to the BBC commenting on the problems of receiving Radio 3 on Medium Wave, they in turn refer one to the v.h.f. services! Do they realise that v.h.f. is not easily available to all?—T. D. Jackson (Lancashire).

## practically wireless

No. 92 what you mean is...

commentary by HENRY

PICTURE, if you can, the telepundits squaring-off across the studio table, dissembling when flummoxed, leaping eagerly into the subject when a question slots into their pigeon-hole of knowledge. The scene is familiar.

But have you ever been exasperated by the overbearing type who listens with evident impatience to his opposite number's bumblings, then thrusts in with the verbal pike off: "What you mean is . . ." and proceeds to expound his own meaning?

I think we could do with a few of those pikers in the hushed rooms and holy corners where Users' Manuals, Operating Handbooks and Service Instructions are compiled. In one classic example of the dismantling instructions for a Japanese radio-cumportable tape recorder, sequence of nearly a dozen operations had to be made to get the chassis from the cabinet. Following the quaint orders was bad enough, but after action 3 one reached an impasse. The next stop in the sequence could only be taken if you tugged, pulled, shoved, wrenched and twisted the loudspeaker mounting. plastics break with a gut-rending "Crack", don't they?

The solution comes, after one failure, at about Stage 12, when



Leaping eagerly into the subject.

we are told: "Before unloosing the regulator board, take off the two clips marked A and B in diagram."

But even when meanings are explicit there can be an embarrassing contretemp. Five times in a fortnight, soon after Garrard brought out their SP25 Mark III autochanger, we had to explain patiently to new users that rejecting during Manual Play required one to flick the lever to Auto and then bring it back to Manual. If you left it in the Auto position, the pickup arm would rejectsure-but cycling commenced and the record would be replayed in the selected size position. The instructions are there, plainly enough on Page Nine of the handbook issued with the gramophone deck, but who reads handbooks?

Not so good are those handbooks, usually printed in several expensive colours and all sorts of languages from Serbo-Croat to Sanskrit, which have such convoluted language that the English version is as ambiguous as the hieroglyphics.

Henry has whiled away many hours cross-referencing the English with adjacent columns of French and German, which deluded tutors were under the impression he had learned in his younger days.

Instructions in some strange Scandinavian tongue translate curiously if one attempts to be literal. Take the phrase: "Nun das Stromkabel in eine Steckdose anschliessen." That comes near the beginning of the Bedienungsanleitung (which everybody knows is the manual de Instrucciones) for the Sanyo STD-100 stereo cassette recorder.

Well, if we have to cope with the Common Market, let's have a go. Looks like a tale about this nun who climbs some mountain to get more living room. And lower down we see . . ." reglers so einstellen, dass optimale Aufnahmequalität erzielt wird." That one



Who reads handbooks?

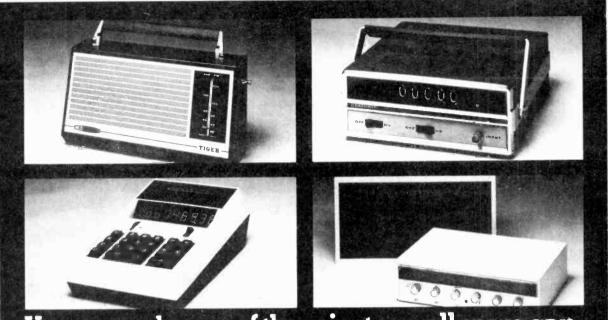
is obvious: "if you've go to instal it regularly, cheer up and do not use that naughty word."

It becomes quite deflating to learn that the first phrase tells you to plug the power cord into an a.c. outlet, while the second is about adjusting the input level for optimum recording quality.

The section in Japanese was most intriguing, especially as English words like ON, OFF and EJECT larded the text like plums in a pudding.

Henry has campaigned for years to make suppliers add at least a circuit diagram to their equipment, and to put the specifications where they can be seen. In the June issue of Hi-Fi News, the B & O publicity boys mention that they always include a circuit diagram in a cute little pocket inside each piece of their equipment. In the same issue, a reader tells us he could not get a service manual with his tape recorder. He received, instead, a courteous letter pointing out that it was not Company policy to supply service manuals to the consumer public.

He answers that he, too, has a policy, which stated quite simply says: "No Manual—No Machine." Henry feels that more people should wield that pike.



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Maybe radio is more in your line. Well, you could make our new version of the successful Tiger transistor portable – the Tiger FM. Designed specifically for the high-quality sound of VHF broadcasts (BBC radio 2, 3, 4 and local stations), it's particularly easy to build. Ideal for beginners.

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## **TAKE 2 ③**

#### **JULIAN ANDERSON**

A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

T this time of year the nights are closing in and unless something miraculous occurs, winter will follow shortly. As a nation we are supposed to ignore that season until it actually happens; iced points on the railways and the resulting chaos is just one example. However Take 20 is going to set an example to the nation with this month's circuita Frost Alarm. You may think that such a project has few uses, but think about it. Freezing pipes in the loft can be prevented, the greenhouse heating can be turned on and the fruit growers can take the necessary precautions if you are given some warning that the air temperature is approaching 0°C. The circuit falls within our £1 limit but if it is to become a permanent fixture, rather than built up for interest, a mains operated power supply must be used, batteries are quite unsuitable unless you are prepared to keep switching the unit on and off.

We are calling the circuit a Frost Alarm but it can be made to operate over a wide range of temperatures, it is simply a matter of adjustment. The alarm device is a bulb which will light as soon as the temperature falls below the preset level. The warning device can be situated in any convenient position where it will be seen easily with the temperature sensor up to 100 yards away. This is the main advantage; you don't have to go out in the cold to look at a barely readable mercury thermometer.

#### The Circuit

The circuit of the frost alarm is shown in Fig. 1. The temperature sensing device is a thermistor. This is a device whose ohmic resistance varies with the temperature. At  $25^{\circ}\text{C}$  the resistance of the one specified is about  $4^{\circ}7k\Omega$ . Above this the resistance falls to a low level but below it the resistance increases. On the one used for the prototype this was measured as  $8k\Omega$  at  $0^{\circ}\text{C}$ .

The thermistor is wired in series with a variable resistor, VR1, and the junction of these is taken to the Schmitt Trigger circuit which comprises Tr1 and Tr2. The voltage at the junction of TH1 and VR1 will depend on two factors; the temperature and the setting of VR1. We can easily arrange for this voltage to be just sufficient to bias Tr1 into conduction and set VR1 so that when the temperature falls, and TH1 increases in value, that Tr1 will have insufficient voltage at the base to maintain conduction.

While Tr1 is switched on, Tr2 will be held switched off since the saturation voltage (which is that voltage between the emitter and the collector when the transistor is fully conducting) is below that necessary to bring Tr2 into conduction. The connection of these two transistors is such that when one is conducting, the other is off and vice versa. The switching action is very rapid and very positive. We have explained

### No. 41 FROST ALARM

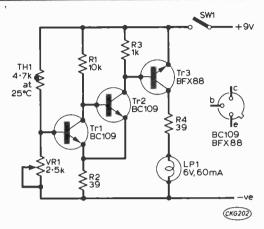


Fig. 1: The circuit of the Frost Alarm.

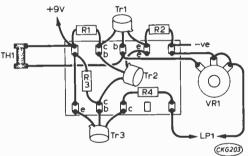


Fig. 2: Suggested component layout on tag-board.

#### **★** components list

TH1 Tr1 Tr2 Tr3 LP1	BC109 BC109 BFX88 6V, 60mA bulb	thermistor (Henry's	10p 10p 20p 5p
	holder I On-off switch		11p 7p
		-	99p

Prices are those recently advertised and may have changed. No allowance is made for minimum order costs or for postage and packing and these points should be checked carefully before ordering.

the operation of this circuit before in this series in more detail. When Tr2 is off there will be no voltage drop across R3 and so Tr3 will be off. When Tr2 is on, this will turn on Tr3 and current will pass through the bulb. The reason for R4 is only because 9V bulbs

do not seem widely available, unlike 6V versions, and this resistor prevents the bulb being overloaded. A switch is shown only for convenience. If a mains operated power supply is used, as it should be, the switch should be on the input to this. As we mentioned before the thermistor can be connected to the circuit by a long length of wire, as the resistance of this will be negligible compared to that of the device itself.

#### Calibration

It is not too difficult to calibrate VR1. Put the thermistor with its leads into a small plastic bag and put this into a bowl of water and melting ice. The temperature among the melting ice will be 0°C but this may mean that the warning will come too late. If a decent sized bowl is used, it is better to calibrate using the water temperature at the bottom of the bowl, here the temperature will be 4°C. Once calibrated the unit can be tested by putting it into a fridge, checking the switch-on temperature against a mercury thermometer. The inside of a fridge should be just above freezing, say 3°C or so.

A suggested layout on a small tagboard is shown in Fig. 2.

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#### Fractical Wireless Designer's Trophy

To encourage new authors, entries for the 1972 Trophy will be restricted to readers who have not previously had an article published in PW. This leaves the field wide open for those wanting to try their hand at writing technical constructional articles. Contestants will not be in competition with well-known authors, only with other newcomers, so the cup can only be won by a new writer. It Could Be You.

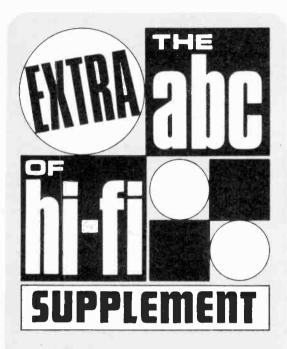
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- 3. The competition is open only to authors who have not previously had any work published in PW.
- 4. Articles submitted for the competition should conform to the general style of material published in PW and must describe the operation and construction of a piece of radio, audio or test equipment that has been designed and built by the author.
- 5. Articles should, preferably, be typed using double spacing, leaving wide margins, on one side only of each sheet. Circuit diagrams and any other drawings must be separate and numbered to agree with the text. Author's roughs must be clear enough to permit re-drawing. Components list must also be separate and laid out to the standard PW format.
- Photographs of the equipment are desirable and should be in black and white, sharp and clear. Photographs may be identified by sticking a label on the reverse instead of writing on the back of the photograph itself.
- 7. Components used in the design must be readily available from retail sources.
- Articles should be sent to the Editor, Practical Wireless, Old Fleetway House, Farringdon Street, London, E.C.4. Authors will be advised as soon as possible of the acceptance or rejection of their articles. Equipment, the subject of an article, must not be sent to the Editor until advised to do so
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### INNEXTMONTH'S

## WIRELESS



The prospective buyer of hi-fi equipment can rightly feel a little bemused as he attempts to make sense of the welter of technical literature showered on him by manufacturers. With the audio 'season' now upon us we thought readers would like hi-fi expert Gordon King to explain and comment on the confusion of hi-fi jargon that now besets the man-in-the-street. Hi-fi is not cheap. A study of our ABC will ensure that your money is well spent.

#### 8 WATT SILICON AUDIO AMPLIFIER

The falling cost of silicon output transistors now makes them an attractive alternative to germanium types. This article describes a high specification, all-silicon, 8W power amplifier with a suitable power supply. In addition a circuit is given for a matching high quality preamplifier.

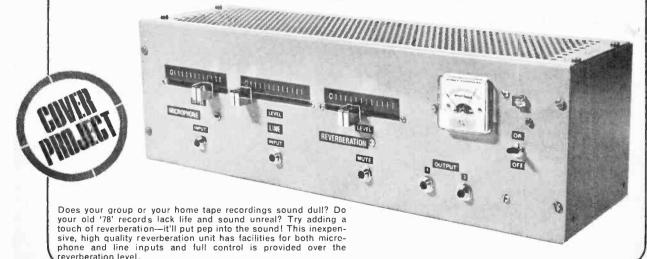
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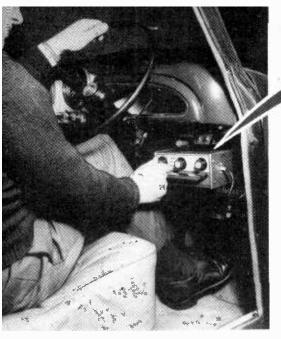
One of the problems in building test gear is range switching. This project uses plug-in coils (no switching) meaning, of course, that these are not permanently 'tied-up' in the circuit. The signal generator has wide coverage with outputs of r.f. modulated r.f. and audio.

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#### THE



## CAR PORTABLE RADIO

OR general use it is an advantage to have a receiver with a number of pre-selected stations available so this receiver is pre-tuned to four frequencies with provision for adding two more stations, or variable tuning, if wanted later. Three m.w. stations are available, with one l.w. station for reception of the BBC on 1500m. This is very convenient for day to day use and reception of a variety of programmes.

Reception normally is on the loudspeaker but there is provision for plugging in a personal earphone or headset, when this is more convenient for listening. A car aerial connector socket is provided, so that the receiver can be placed in a car where the use of pre-set station selection is a decided advantage. The receiver shape allows it to rest on a parcel shelf with its speaker upwards, or suspended under a shelf with the speaker downwards.

A diode output socket is fitted which is of advantage when a tuner is required for a tape recorder or other audio equipment. The receiver audio stages may then provide a signal for monitoring purposes.

R.H.LONGDEN

The circuit is shown in Fig. 1 and is a straightforward and reliable one using easily obtained components. L1 is the ferrite aerial rod, and section S1a of the 6-way switch selects TC1, TC2, TC3 or TC4 pre-set trimmers, to give automatic tuning of the wanted stations. L1, TC4 and the parallel capacitor C1 provide l.w. reception, no additional winding being required.

Switch S1b similarly selects one of four oscillator trimmers, TC5 to TC8, and these tune the oscillator coil L3 to the required frequency. In practice, it is sometimes found that changes in battery voltage, temperature or slight changes in oscillator capacitor values, throw some pre-set stations slightly off tune. This is avoided by using a small panel control VC1, which can if necessary be adjusted to compensate. In use, the trimmers are set with VC1 half closed, then it is only necessary to adjust VC1 if signals are heard to be off-tune.

It will be noted that alignment between L1 and L3, throughout one or more fully variable tuning ranges, is not necessary, as when ordinary tuning is used. There are thus no ganging difficulties here, as it is only necessary to adjust pairs of capacitors TC1/TC5, TC2/TC6 etc., for the wanted stations.

As the ferrite rod aerial is unsatisfactory in a vehicle, coil L2 allows a car aerial to be coupled to the receiver.

The 2-stage i.f. amplifier has three single-tuned i.f.t.'s, and a.g.c. via R9 from the detector diode D1. Audio signals may be taken directly from the diode circuit by the outlet provided. VR1 is then turned to zero, unless audio signals for monitoring are wanted from the receiver.

The remaining outlet is for a personal earphone or headset, when required, inserting the plug silencing the receiver speaker. A large external speaker can also be plugged into this socket.

#### SWITCHED CAPACITOR ASSEMBLY

This consists of the switch, with eight pre-sets and C1, wired on a paxolin panel 4 x 2in., as in Fig 2. TC1 and TC5 are both 60pF max as are TC2 and TC6. These were set for 1214kHz, Radio 1 and

1088kHz, Radio 4. TC3 is 50-450pF, and TC7 is 20-250pF, for 647kHz, Radio 3. For 200kHz, Radio 2 TC8 is 450pF and TC4 is 1250pF with C1 1000pF in parallel.

It is unlikely that other values will be wanted for TC1 and TC5. TC2 and TC6 can be 100pF if a lower frequency than about 1088kHz is needed here, or may have small fixed capacitors in parallel. In some parts of the country Radio 2 on 200kHz may not be required when TC4 and TC8 can then be 100-400pF, for an additional m.w. station in which case C1 is omitted. Ranges with the pairs of pre-sets overlap considerably. The oscillator circuit requires less capacitance than the aerial circuit.

Washers on the switch keep leads and tags clear of the metal panel of the receiver and when the assembly is wired, it is fixed with the selector switch

#### CIRCUIT BOARD

This is 5 x 3in., a piece 1³4 x 1³4in. being cut out to accommodate the speaker, as in Fig. 3. Wiring will be simplified if the perforated board is cut so that there are 19 rows of holes one way, and 32 rows the other. Components can then be placed with their

wire ends exactly as shown, and wiring will closely follow the diagram of the underside of the board.

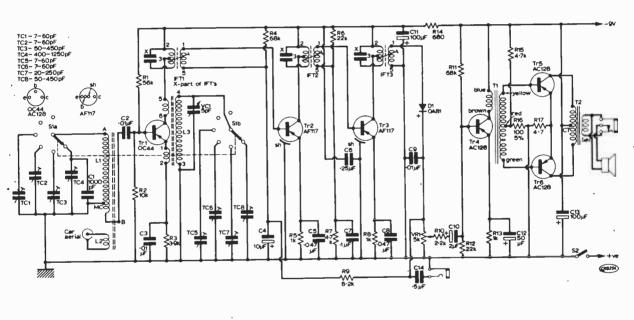
Holes have to be drilled for L3 and the i.f.t.'s. A very small round file will be found useful to obtain a fit if any holes prove to be out of position. The identification spot on L3 falls between pins 1 and 6, and these pins should come as in Fig. 4.

Check resistor values as they are inserted, and note also the polarity of the electrolytic capacitors and diode D1. When some components are in position, turn the board over and connect as in Fig. 4, snipping off excess wire.

If each item and its leads are marked in coloured ink or pencil on the drawing as inserted and connected, it is unlikely that anything will be overlooked, or wrongly connected. It may prove helpful to use red 1mm sleeving on positive circuits, black on negative and some other colour for remaining connections.

Pieces of coloured sleeving about 38 in. long can be put on the transistor wires. This will identify them, and also hold these at a suitable height from the board.

Transformer T1 is held by its leads plus a little adhesive. Other driver transformers of similar type will give the same results, but connections must be



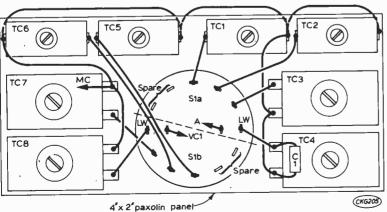


Fig. 1: above, shows the complete circuit diagram for the PW pre-tuned radio, together with the base data for the transistors. Values of pre-set trimmers TC1-8 are tabulated separately. Fig. 2: left, gives the layout of the trimmer capacitors and connections to station selector switch, all mounted on a separate paxolin panel.

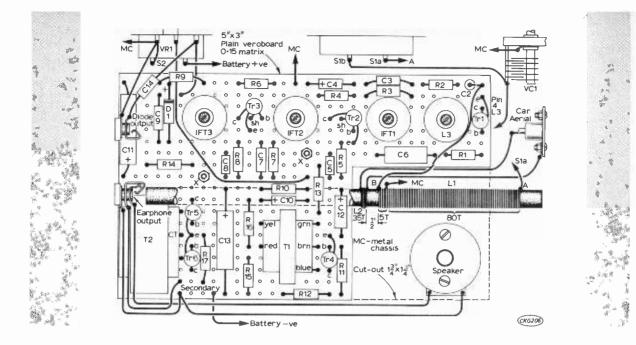


Fig. 3: above, layout of components on the front of the veroboard panel. For clarity the framework of the speaker has been omitted Fig. 4: right, shows the component wiring on the reverse side of the board. Note polarity of electrolytic capacitors and diode D1.

The photograph at the bottom of the page is a general view inside the receiver which may be compared with Fig. 3 above.

taken from the maker's data or leaflet. T2 has fixing lugs which pass down through slots made by drilling small holes close together.

Leave flying leads from D1, R10, pin 4 of L3, earth (positive) line, C2, and battery negative, as shown in Fig. 3. Two leads from the secondary of T2 are anchored on the board and run to the speaker circuit.

#### FERRITE AERIAL

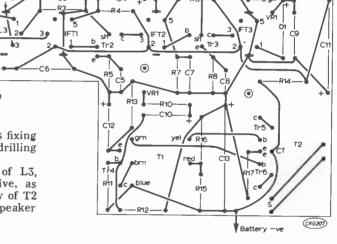
L1 is wound with 24 s.w.g. enamelled wire, with turns side by side, on a 6 x  3 8 in. diameter rod. Anchor the wire  1 2 in. from one end, at A, Fig. 3, with tape or adhesive. Wind on 80 turns and form loop of wire at MC. Continue for a further 5 turns in the same direction and finish off at B. A lead runs from MC on the aerial winding to MC at TC7, Fig. 2, A runs to S1a, and B to C2.

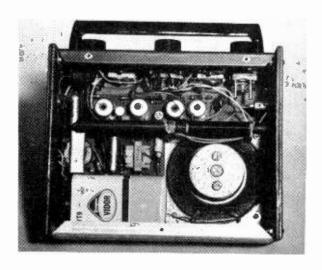
The aerial is mounted by cutting two strips of paxolin about 2 x  $^{1}2$ in. and mounting these with small brackets held under bolts that secure the speaker. A "V" is cut in the end of each strip, and the rod held by thin string round it and through small holes in the strips.

L2 is 35 turns of any thin insulated wire, placed on the rod about  $^{1}\mathrm{_{2}in.}$  from B.

The car aerial socket is mounted on the right side of the case, viewing the receiver from behind, Fig. 3.

The diode output socket is near VR1, on the side of the case, and C14 is for d.c. isolating purposes.





#### * components list

Resist	ors				
R1	56kΩ	R7	4.7kΩ	R13	1kΩ
R2	10kΩ	R8	1kΩ	R14	680Ω
	3.9kΩ	R9	8·2kΩ	R15	4 · 7kΩ
	68kΩ	R10	2-2kΩ	R16	100Ω 5%
R5		R11	68kΩ	R17	4.7Ω
	22kΩ	R12	22kΩ		0% ±W
		potentiom	eter with		

Capa	citors
C1	1000p

C1 1	1000pF SM	C8	0.047µF
C2 (	0.01µF	C9	0.01µF
	0·01μF	C10	2μF 6V
C4 1	10μF 6V	C11	100µF 12V
	)·047μF	C12	50µF 6V
	0.25µF	C13	100μF 12V
	)·1μF	C14	0·5μF 150V
TC1	7-60pF	TC5	7-60pF
TC2	7-60pF	TC6	7-60pF
TC3	50-450pF	TC7	20-250pF
TC4	400-1250pF	TC8	50-450pF
All c	ompression trimmers	6	
VC1	5pF variable (Jacks	on C8	04)

#### Semiconductors

Tr1	OC44	Tr4	AC128
Tr2	AF117	Tr5	AC128
Tr3	AF117	Tr6	AC128
D1	OA81		

#### Miscellaneous

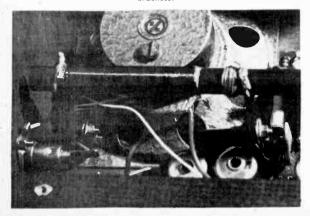
L1-2, see text. L3, oscillator coil (Osmor PW/01). IFT1 (Weyrad P51/1). IFT2 (Weyrad P51/2). IFT3 (Weyrad P50/3V). T1, driver transformer (Osmor QXD1). T2, output transformer 6.2:1 CT (Henrys MOP). Switch S1a-b, rotary water switch, 2 pole 6 way. Speaker 3½in. 3Ω. Universal chassis flanged members, 7 x 3in. (2) (Home Radio). Knobs (3). Handle. Veroboard, plain, 0.15in. 5 x 3in. Coaxial aerial socket. Output jacks (2, 1 shorting type). Battery PP9 and clips.

The a.f. output jack socket is below this, and has contacts which open when the plug is inserted. It is connected as in Fig. 3, so that inserting a plug breaks the internal speaker circuit.

#### CABINET

The receiver can be tested out of its case, by wiring the circuit board to VR1, VC1, and S1a-b, as in Fig. 3.

Close-up shot of the method of attaching the ferrite rod to paxolin brackets



The leads MC from VR1 and VC1 go to tags bolted to the panel flanges.

The parts of the cabinet are quite easily prepared, and holes should of course be drilled before fitting the speaker or any other items.

Top and Bottom These are 7 x 3in. flanged universal chassis members. Punch the top for VR1, Sla-b and VCl, and drill holes for the handle fixing bolts. Drill the front flanges for 6BA bolts or selftapping screws (to secure the front) and the back flanges for self-tapping screws. Cover the top with self-adhesive material of the required colour.

Each side is 3-ply,  $6^{1}_{8}$  x  $3^{5}_{8}$ in., to allow overlapping the front and back, with a small projection at the top and front. The end flanges of the top and bottom are secured to the sides by two bolts in each position.

These are 3-ply, each 7 x 6in. Front and Back Place the speaker to the bottom right, mark its fixing holes, and cut an aperture to match the speaker cone. Put the circuit board in place, and drill the two holes X-X in Fig. 3, through board and front, so that the board can later be fixed in this position.

Speaker Fitting Pass two countersunk headed 6BA bolts through from the front, to hold the speaker and also the brackets for the ferrite rod supports. Use other bolts or small wood-screws for the remaining speaker fixing holes.

Circuit Board Two countersunk bolts are put through the holes which match with X-X, and held with nuts. Extra nuts are then put on, so that when the circuit board is on these bolts, a clear space of 38in. or so remains between it and the case front, to clear the wiring. Nuts at X-X then hold the board in place.

A piece of fabric about 8 x 8in. of the Finishing required colour has its top edge placed between the plywood front and the top flange. Temporarily fold this fabric over the knobs, so that the screws holding the front to the flange can be tightened. Also spread Bostik 1 or other adhesive along the top edge of the front. Screw the case bottom to the front. The fabric is then drawn taut over the whole front, and is folded over and fixed with adhesive at the case bottom, and front edges. The two sides are then fitted with bolts or screws.

#### TUNING ADJUSTMENTS

The receiver is tested and tuned before fixing it in the case, as mentioned. If no signal generator is available, the i.f.t. cores are adjusted for best volume, any transmission being tuned in by means of a pair of trimmers. Once this has been done, the cores need no further adjustment.

When setting the trimmers for the wanted stations, deal with each pair of trimmers in turn, according to the position selected by the rotary switch. The position of the core of L3 has considerable influence on frequency, so needs to be left alone once a suitable setting has been located. VC1 is half closed while adjusting the trimmers.

Pre-sets having a range of 7-60pF will cover about 1500-1000kHz in aerial and oscillator positions. For oscillator tuning, 20-250pF trimmers will cover the remainder of the m.w. band, with 50-450pF trimmers for aerial tuning. For 200kHz, extra capacitance is necessary, up to about 450pF for oscillator, and 2,000pF for aerial circuits.

## TRANSMITTER for 2 metres

#### PART 2 F. G.RAYER G30GR

#### POWER SUPPLY/MODULATOR

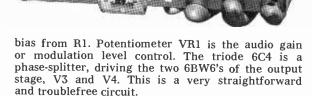
This power-supply/modulator was made for use with the 2-metre Transmitter described last month, for which it will provide all power requirements, and adequate modulation. It is only necessary to insert an octal plug from the transmitter into the modulator. The modulator is designed to have other uses, to increase its utility, as follows:—

- (1) It will supply approximately 12 to 15W of audio for one or more speakers.
- (2) It will modulate a transmitter of up to about 25W d.c. input where the transmitter has its own power supply.
- (3) It will supply power and modulation for a transmitter in the 10W power range.
- (4) The modulator can be switched off, leaving 300V at 120mA available for, say c.w. working.
- (5) Optional choke input drops the supply to about 240V for receiving equipment and similar uses.

An h.t. current meter is included to check working of the modulator and associated equipment, and an h.t. "ON" switch allows the modulator and a transmitter used with it to be switched on and off.

#### CIRCUIT

The circuit is shown in Fig. 1. The first section of the double triode 12AX7 is an amplifier for the usual type of crystal microphone, with contact potential

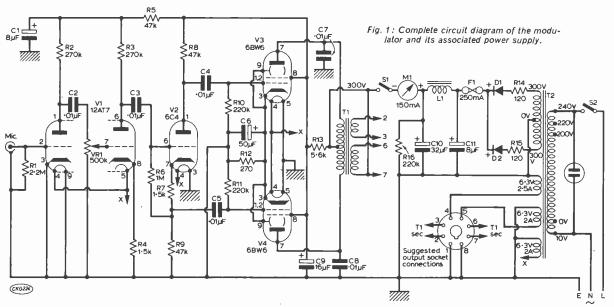


The h.t. circuit is well smoothed, by C10, C11 and L1 while R16 is a safety bleeder resistor. Some modification to working conditions can easily be made, if better suited to other associated equipment.

HT Voltage. With the values given, the h.t. supply is 300V when loaded to 120mA. If R14 and R15 are each  $270\Omega$ , the supply obtained is 280V when loaded with 100mA. A terminal board with pairs of small terminals is fitted under the chassis, so that the positive connection to C11 can be interrupted. The power supply then works as a choke input circuit, giving a reduced supply of about 240V at 120mA

Output Stage. Operating conditions with cathode bias provide about 9 watts of audio with 250V, and about 12 watts with 285V. For modulating a transmitter the audio output required is about half the d.c. input of the transmitter, say 7 to 8 watts, for a 15 watt d.c. input. If wished, it will be found that R12 can be considerably increased in value, to reduce the current taken by the 6BW6's, without loss of audio quality.

Modulated HT. This is derived from the h.t. line and secondary of T1, the fixed ratio transformer being intended for a p.a. load of about 3 to  $8k\Omega$ .



#### * components list

270kΩ ½W 10%	R10	220kΩ ½W 5%
270kΩ ½W 10%	R11	220kΩ ½W 5%
1.5kΩ ½W 10%	R12	270Ω 2W 10%
47kΩ ‡W 10%	R13	5.6kΩ 1W 10%
1MΩ ½W 10%	R14	120Ω 2W 10%
1.5kΩ ½W 10%	R15	120Ω 2W 10%
47kΩ ½W 5%	R16	220kΩ 1W 10%
500kΩ log, poten	tiometer	
	270kΩ ½W 10% 1·5kΩ ½W 10% 47kΩ ½W 10% 1MΩ ½W 10% 1·5kΩ ½W 10% 47kΩ ½W 5%	270kΩ ½W 10% R11 1·5kΩ ½W 10% R12 47kΩ ½W 10% R13 1MΩ ½W 10% R14 1·5kΩ ½W 10% R15 47kΩ ½W 5% R16

Capac	itors
C1	8µF

C1	8μF 450VW	C7	0·01μF 750VW
C2	0·01μF 350VW	C8	0·01μF 750VW
C3	0·01μF 350VW	C9	16μF 450VW
C4	0·01μF 350VW	C10	32μF 450VW
C5	0·01μF 350VW	C11	8μF 450VW
C5 C6	0· 01μF 350VW 50μF 50VW	C11	8μF 450VW

#### Valves

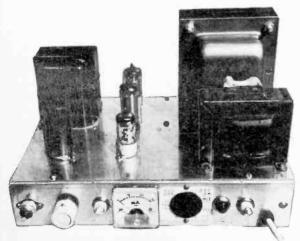
V1	12AT7	V3	6BW6
V2	6C4	V4	6BW6

#### MISCELLANEOUS

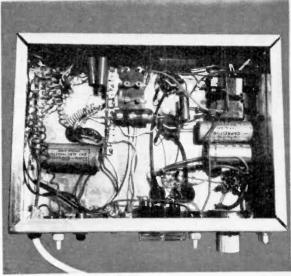
Valveholders, B9A with skirt and screening can (1), B9A plain (2) B7G with skirt and screening can (1). Meter M1, 150mA. Toggle switches (2). Microphone socket. Octal valveholder, for power outlet. Mains neon indicator. Fuse, 250mA and holder. D1/D2 silicon rectifiers, 1000 p.i.v. 1A or better. Chassis 10 x 7 x 2in. L1, about 10H at 120mA. T1, modulation transformer Type 223 (Garex, Chinnor, Oxon) T2, mains transformer to provide 300-0-300V at 120mA, 6.3V at 2.5A and 6.3V 2A twice (Douglas, Parmeko

A multi-ratio transformer may be used for other load impedances. The transmitter d.c. input is VxI, for example, 300V at 40mA or 12 watts. So the transmitter p.a. modulating impedance is approximately V/I or  $300/0.04 = 7.5 \text{k}\Omega$ . (For the impedance calculation, remember to add the p.a. screen grid current to the p.a. anode current.)

Unmodulated HT. This is derived from the h.t. line, after the switch, to allow metering of the total h.t. drain, and control of h.t. to the transmitter. When using the 2-metre transmitter described, more grid current that required was available, so h.t. to the



General view of the prototype chassis.



Underneath the chassis. Suggested layout of the major components should be followed. Otherwise component positioning is not particularly critical.

earlier stages was reduced to about 260V by placing a  $1k\Omega/2W$  resistor in series with pin 7 of the octal socket, Fig.1.

#### CONSTRUCTION

This is on a 10 x 7 x 2in. "universal chassis" so that the front runner can be prepared for the meter, etc., before it is fixed in position. Securing bolts for the mains transformer and modulation transformer also pass through the side and back flanges for additional strength and rigidity.

In the layout adopted, the microphone socket and VR1 are to the left, adjacent to the 12AX7 holder. Grid leads here are screened, and clear of heater wiring. The 6C4 is towards the centre, and the two 6BW6's in line towards the back, with the modulation transformer to the left, and the mains transformer to the right. This leaves the front right of the chassis for the smoothing choke. The only live circuits above the chassis are leads to the choke, and these were covered with tape.

The front runner carries the following, left to right: -microphone socket, VR1, h.t. switch, meter, octal socket, AC "ON" neon indicator, AC switch, and outlet for the mains lead. Transmitters, speakers or other associated equipment employ octal plugs wired to match.

The small terminal board mentioned has two terminals wired to the modulation transformer secondary, so that it can be shorted in a few moments with a wire link for c.w. when the same equipment is also used for a.m. If frequent changes are made from c.w. to a.m. in this way a switch can be placed across the secondary.

The modulator should never be used without a load connected to the modulation transformer.

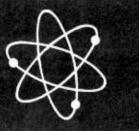
#### **AERIALS**

The output of the transmitter can be matched into any of the usual aerials requiring a low impedance feed.

A simple dipole will give good results over local

-continued on page 540

#### **EXPERIMENTERS CORNER**



#### INTERCOMM CALLING SYSTEM R. A. BUTTERWORTH

OST intercomms use three wires or a complicated relay/switch system. The system described here uses only two wires and can be adapted to any amplifier already available providing it has both input and output transformers. The two wire cables connecting the units can be any cheap twin type. A bonus in this system is that only one *Slave* unit is necessary because by paralleling several pairs at a convenient junction point, communication can be had from any two points.

In the author's arrangement the Master unit is usually in the shack at the bottom of the garden but

the Slave can be in the lounge (telephone) hall (door bell) and bedroom or kitchen. By moving the units and plugging in, communication can be had between any two locations. Another bonus is that the units consume current only when communication/calling is made.

#### OPERATION

Figure 1 is the full schematic of the author's unit to enable the reader to follow the way in which the unit operates. With SW3 "OFF", when SW1 or SW2, which are spring loaded, are pressed it causes a loud bleep in the other unit's loudspeaker in the following manner. If the master wishes to call the remote unit, SW1 is pressed, shorting contacts 5 and 6, thus completing the positive line through the primary of the input transformer/switch/speech coil of the loudspeaker to the common line. The amplifier is

in operation and at the same time the current through the primary winding induces a low frequency note in the secondary which is amplified. Contacts 2 and 3 have been connected at the same time so that the Slave speaker is connected to the output of the amplifier so the resultant amplified audio note (generated in the input transformer) is heard in the Slave's speaker. Switch 3 is now operated to await the reply, if no response, put SW3 "OFF" and press SW1 again. Once contact is established, the Master controls all Speak/Listen operations and switches "OFF" SW3 ready for the next call. A similar operation takes place when the Slave wishes to call the Master. The 50µF electrolytic blocks what would otherwise be a direct d.c. connection but not the audio signal. It will become obvious that the Master

can monitor the *Slave* by simply switching "ON" SW3 and so act as a baby alarm, telephone/door bell warning.

Any pair of miniature  $3\Omega$  speakers can be used and the transformers are a pair of miniature transistor single ended output (3 $\Omega$ ) types. The potentiometer VR1 is a preset skelton type, the required volume, once set, does not require further adjustment. As will be seen from Fig. 1, SW1 is a DP/DT type, SW2 is a SP/ST, and SW3 a simple ON/OFF type. Switches 1 and 2 are, of course, biased types (spring loaded); there are many varieties on the

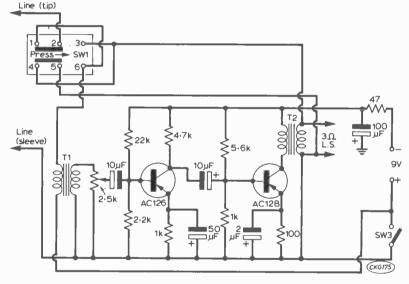


Fig. 1: The circuit of the Master unit—see text for an explanation of the unusual calling system.

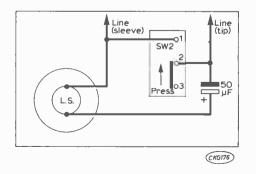


Fig. 2: The circuit of the Slave unit.

market, the most easily available is the toggle type; but the constructor has a choice.

As stated at the beginning, the main reason for offering yet another intercomm unit is the novel method of calling and the use of only two wires. This gives a versatile and flexible installation, well worth

the few hours needed to construct. It may interest the reader to know that this method of calling was developed as a result of a mistake made when making up a conventional system and to the best of the writer's knowledge has never been used before.

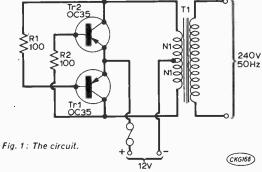
#### 25W D.C. to A.C. INVERTER

S. SOAR

THE inverter described here will operate 240V 50Hz appliances of up to 25W consumption. It was originally built to drive an electric shaver or a 25W soldering iron from a car battery.

The circuit is a simple resistance coupled inverter with a square wave output of 240V 50Hz.

Considering the circuit in Fig. 1, assume that Tr1 starts to conduct; voltage induced in N1 rapidly drives Tr1 into saturation and biases Tr2 off. Flux increases in the transformer core until saturation is reached which results in a sudden rapid increase in current in Tr1. This current exceeds the current which Tr1 can supply with the available drive, Tr1, therefore, comes out of its saturated state. Voltage induced in N1 falls to zero as the transformer core saturates and Tr1 is returned to the "off" state, this ends the first half cycle. Flux collapse in the transformer core results in an induced voltage in such a direction as to turn Tr2 on so initiating the start of the second half cycle.



#### **Performance**

No Load .....Input current 700mA (8-4W)

Load 15W ....Input current 2-0A, efficiency 62-5%

Load 25W ....Input current 2-8A, efficiency 75%,

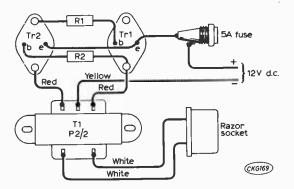


Fig. 2: Wiring of 25W inverter

#### * components list

R1, R2 100Ω, 2W
Tr1, Tr2 OC35
Fuse 5 Amps
Transformer: Type P2/2 available from Magtor
Limited, 68 Dale Street, Manchester 1.

Construction is straightforward and operation is little affected by position of components. However, it is advisable to keep interconnections as short as possible to reduce inductance.

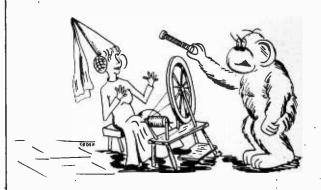
Since transistors Tr1 and Tr2 are not operating at maximum load, large heat-sinks are not necessary and the entire unit can be inserted in a metal case measuring only 3in x 3in x 4in. Care must be taken to ensure that the collectors of both transistors are isolated from each other, this can most easily be done by mounting these in the side of the case on insulating washers, alternatively a plastic case can be used.

If a d.c. output is required, this can be easily obtained by connecting a bridge rectifier to the secondary, since the output is square wave, smoothing represents no problem and a capacitor of  $2\mu F$  will suffice for most requirements.

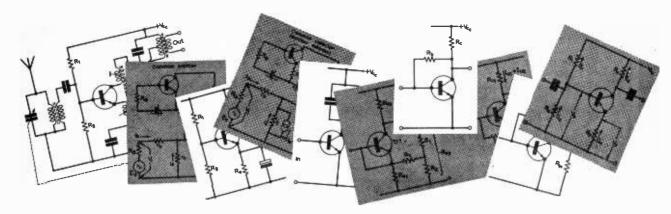
It is not recommended that half wave rectification be used as this will tend to saturate the transformer core in one polarity only and this may cause malfunction of the inverter.

#### MAXWELL

by G8DSH



'-about eighty turns tapped ten turns up, please!"



## TRANSISTOR CIRCUITRY for beginners

PART 11

#### A breather

Before we can progress with our look at transistor circuits, we must halt, survey the battlefield of some of our illusions, and reconnoitre the lines of our next advance.

In other words, having taken single stage circuitry and combinations of stages, we must now consider the effect of the sub-circuits on those before and those after. The more we delve into transistor circuitry, the less we can regard each "block" as an entity unto itself. Black boxes, so beloved of the academic, are seldom darker than a shade of mottled grey when we come to put them into practice.

One such circuit concept, that seems primarily to make hay of basic theory, is the so-called "virtual earth".

We have reached a stage in our talk about circuits where we can see, without the aid of equivalent transistor circuits or little arrows showing electron flow, that the d.c. conditions and the a.c. conditions in any given configuration will be different, though interdependent.

As an example, consider the plain problem of decoupling. In your humble transistor radio you have a perfect example. As you bothered your neighbours on the beach with Bach's Partita and Fugue while all they wanted was to be Woganised (how I've longed to do that!) the signal current in the power supply circuits were being bypassed from the battery by a relatively hefty electrolytic capacitor. Fig. 55 illustrates this, and shows that the h.t. line

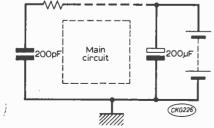


Fig. 55: Simple decoupling. The capacitors represent a virtual shortcircuit to signal currents.

is, as far as the a.c. signals are concerned, at the same potential as the chassis.

From there, it is a small step to think in terms of impedance and frequency rather than resistance and direct current when considering a signal-handling circuit.

Why, for instance, do we need that hefty capacitor back there, across the supply, when the decoupling of the tuner section is efficiently performed by a fraction of a microfarad? The answer lies in the frequency. At the supply, signal currents at audio frequencies are having to be bypassed, and  $2000\mu F$  to a 100 Hz signal is an impedance (a.c. resistance) of 0.81 ohm.

At the front end, taking the FM radio that you, of course, will be using, despite the BBC's recent retrograde step to duplicate local radio on medium waves, the frequency you want to bypass is somewhere near a million times as great and so the capacitance need only be a millionth of the former, that is 2 picofarad against 2,000 microfarad, to have the same effect. Of course, to safeguard over a wider bandwidth, the actual value will be a couple of hundred picofarad,

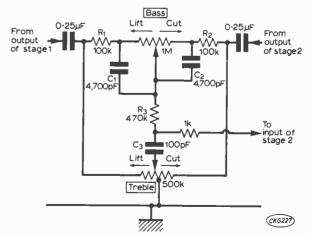


Fig. 56: The original Baxandall tone control circuit, to suit an input of less than  $10k\Omega$ , for use with an SP61 valve.

but the comparison—and the point—remains. When considering circuits, you must consider the effect of the a.c. signals they will be handling as well as the d.c. conditions that provide basic biassing, etc.

#### Virtual earths

Which brings us back to the concept of the virtual earth. Fig. 56 shows a simple circuit, again a practical one, and very familiar, that of the Baxandall tone control circuit, widely used in all sorts of constructions, and not always completely understood. If it serves no other purpose, it should remind us that Peter Baxandall dreamed this one up in 1952, based on an SP61 valve (or, in war surplus terms, a VR65).

The underlying reason for choosing such an example is (a) to make the opportunity of talking a bit more about feedback, (b) to introduce tone control circuitry, which will feature in our next constructional project and (c) to get over as well as we can, to satisfy a number of enquirers, the concept of the "virtual earth".

Feedback has featured already in our potted circuits, d.c. feedback to bring bias conditions to the operating state we require and a.c. feedback to regulate the signal flow through a stage, and, as we shall have to consider later, to make a stage nonlinear in an especially controlled way (as, for example, in designing an RIAA corrected magnetic pickup pre-amplifier).

The whole point about the Baxandall tone control circuit, first considered in a Wireless World article of October 1952, is that its action depends on negative feedback and that it requires an understanding of the virtual earth concept to grasp its principles of operation. Having once got hold of this, we can step forward briskly into the world of "closed-loop gain" and "variable feedback control", which scares so many students away from what is really quite elementary circuitry. Incidentally, the virtual earth concept preceded Baxandall by quite a few years and he was quick to give credit to Professor F. C. Williams for the coining of the term.

#### Feedback

Enough waffling: Feedback is the principle of taking part of the output from a stage, or stages, and applying it to the input. If it is positive feedback, the signal you re-apply to the input is in phase, and thus aids the input, eventually driving the stage beyond its working limits. Control this positive feedback and you have a simple oscillator—the more output it delivers, the more it wants to deliver, until it blocks the stage off, things revert to normal, and away we go again.

But we are more concerned at this juncture with negative feedback. If you are audio-oriented (as you must have guessed by now that Mike and I are!) you will have read all manner of attributions for negative feedback. In the late Forties and early Fifties there were so many articles on negative feedback, interlaced with symbolic formulæ, that one would have imagined it could cure all amplifier ills from operator's twitch to the galloping parasitics!

In fact, the principle is simple: take off a portion of the output signal from a stage (or stages) and apply it to the signal in such a way as to oppose the input, i.e., in antiphase, and you have a method of

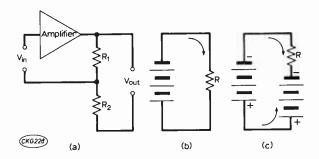


Fig. 57: (a) Negative feedback in series with the input signal. If R1 = R2 the gain is unity. (b) a battery analogy, with no feedback. (c) with feedback equal to the drive, voltage across R is virtually zero.

exercising control that depends on the nature of the input—it is to some extent, and within certain limits, self-regulating.

When we take a brief recap. of some previous articles in this series, we shall also appreciate that negative feedback from the output to the input of an amplifier stage effectively changes the impedance as well as reducing the gain.

This is important, and I am not going to insult regular readers by going, chapter and verse, over our earlier chats about  $R_{\rm IN}$  and  $R_{\rm in}$ , etc. But to summarise a few points, take a look at Fig. 57(a). Here we have an amplifying stage with a signal voltage applied and negative feedback in series with that input signal. (Again, this is important).

Let's assume, for easy figuring that the amplifier has an open-loop gain of 100. That's to say, it would increase its applied signal 100 times if there was no extra circuitry to consider. Then, commonsense tells us that if the values of R1 and R2 are the same, the gain will be unity, not 100 times, because the feedback is in series with the input. To get the hang of this, we have to look at things in terms of the impedance that the signal "sees". Fig. 57(b) shows a battery driving a current through a resistor. The battery "sees" the impedance of the resistor. But what if, Fig. 57(c), we put another battery of the same sort in series with R? We haven't changed the value of R but little or no current flows-so the effective impedance seen by the source voltage, the prime battery, is now high.

#### Back to the amplifier

Let's now get back to our amplifier with its feedback and instead of applying the feedback in series as before, we shall apply it in parallel, Fig. 58(a). Again, R1=R2. But as the feedback is now in parallel with the input signal, we can see, applying the battery analogy, in Fig. 58(b) that it effectively shorts out the signal. In other words, adding V1 to V2 produces an effective zero.

Sorry about that repetitious word "effective", but if I say "this is zero", some pedant is going to hurl a wad of mathematical treatises at me to prove that Isaac Newton never went near the orchard, or something!

Go back to that mini-circuit of Fig. 58(a) and you can now see that the voltage at the junction X of R1 and R2 is very low indeed. Not zero, for we have to take into account the voltage across the amplifier, and the best we can say is that the voltage at this junction, R1/R2, is very low, virtually at

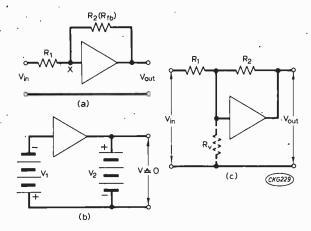


Fig. 58: (a) Parallel feedback, point X is virtual earth point. (b) battery analogy repeated. (c) choice of amplifier gain and resistors gives virtual impedance, dotted, between virtual earth point and true earth.

earth potential. Hence the term, virtual earth. From this, it follows that the input impedance of the circuit is low at this point.

Here, we have one of the bones of contention over which audio pundits have worried, and with which we shall not concern ourselves now—suffice to say, the source signal "sees" an impedance equal to RI in parallel with whatever the virtual resistance Rv in Fig. 58(c) may be, while the amplifier sees an impedance of about Rv. And the beauty of this arrangement is that by juggling with amplifier gain and feedback component values, we can make the input match our source exactly, for best signal energy transfer conditions, while making our amplifier "see" a source resistance (impedance) that is just right for its job. In many audio applications, an impedance of around  $600\Omega$  would do us very nicely for lowest noise conditions, and this case can be met quite easily.

The important factor to remember is that the imaginary resistor we produce by the virtual earth application is approximately equal to the value of R2 divided by the amplifier gain. Its value is not affected by R1. There is no need for R1 and R2 to be equal in all cases, although we have chosen this circumstance for ease of explanation—the performance depends on the ratio between resistor values.

#### Back to Baxandall

So now back to Baxandall, and a circuit that originated from valved techniques.

This time we shall split the circuit into its "Lift" and "Cut" conditions first, showing the virtual earth points. Forget, at the moment, the tapped potentiometer of Fig. 56 and consider the treble lift circuit. This, shorn of all extraneous detail, could be redrawn as Fig. 59(a). If V_R is made low enough so that the voltage at the slider when in the middle of its travel is not affected by the current supplied by C (even at higher frequencies) then the total current flowing toward the virtual earth point, X, is  $I_1 + I_2$ .  $I_1$  is approximately equal to  $V_{in}/R_{in}$  and I2 depends on the value of capacitance. If we make R_{fb} equal to R_{in}, merely to simplify combination of lift and cut control, and call this simply R, then the output voltage has one component independent of frequency, for a constant value of V_{in} while the other one, leading in phase by  $90^{\circ}$  is both proportional to frequency and to k which is the fraction of the potentiometer setting.

What this means, in practical terms, is that for any particular potentiometer setting the response of the cut circuit will be down by the same number of decibels as the lift circuit is up. As we know from Baxandall tone controls published many times before, the curves are a mirror image of each other. This is one of the virtues of the control.

The tapped control is just a convenience and it can be seen that there is actually a small voltage between the centre point of the practical circuit (Fig. 56) and virtual earth, across the capacitor. But its value makes this voltage practically negligible.

A look at the combined bass control in its simplified layout of Fig. 59(c) may help to understand better the working of the tone control. To give level

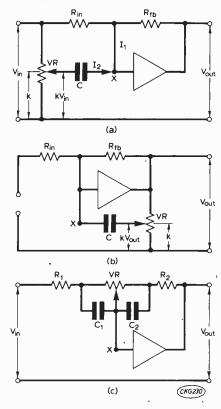


Fig. 59: Fundamental Baxandall treble lift circuit. (b) treble cut circuit. (c) bass lift and cut section of combined circuit.

response at mid-setting, R1 and C1 are the same as R2 and C2. At middle and high frequences the potentiometer,  $V_{\rm R}$  is almost shorted out by the low reactances of C1 and C2, so we are back to Fig. 58(a) with  $R_{\rm in} = R_{\rm rb}$  and unity gain. As the frequency of the signal falls, the gain rises (or, if the potentiometer setting is changed, falls to the level determined by the response curve), and, just as with the treble circuit, the curves are mirror images.

The symmetrical beauty of the finished control, with components calculated to suit Baxandall's original case, the VR65 valve, a high-gain pentode, can be seen in Fig. 56. One of the interesting points about its chosen values is that the treble response will be up or down 3dB at full lift or cut settings of the control when the reactance of C3 is numerically

equal to R1+2R3. The values of C1 and C2 must be equal, as are R1 and R2, for reasons already stated, and values are chosen to give the correct bass response.

#### In practice

Coming to the present time, we can see an example of virtual earth circuitry used in the much-vaunted input stage of the Cambridge P40 amplifier, Fig. 60, where the aim was to get a high-gain, low-noise input amplifier, controlled so that the local feedback loop alters the gain, and thus provides a volume control right at the front of the circuit, in a low-signal level stage—just where we are told never to put it! The aim succeeded to some extent, because there was indeed a very low-noise result, and the overload capability, where most input amplifiers fall down badly, was a phenomenal 60dB.

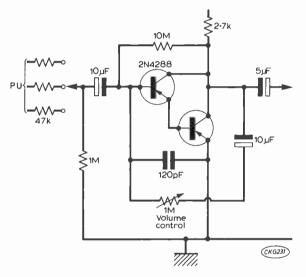


Fig. 60: Virtual earth input stage used in Cambridge P40 and P50 amplifiers.

But later versions of Cambridge amplifiers reverted to an uncontrolled input stage and put the virtual earth amplifier in the second stage, mainly because the original design gave a peculiar volume control "law". You see, the accepted use of a control is a 20dB attenuation when the knob is half-way from maximum (or the slider half retarded). By putting a twin-gang  $1M\Omega$  log law potentiometer in the virtual earth feedback circuit, Cambridge limited the attenuation to between 3 and 6dB for the same movement, with its action accelerating as it was turned farther down.

To get the range of input levels, the control had to be shunted with a  $47k\Omega$  resistor, except in the Pickup 1 mode, so except in this mode, only about three-quarters of the control action was effective. Later versions use a  $50k\Omega$  linear potentiometer to get the approximate log law (using the fixed resistor,  $22k\Omega$ , across part of it).

So we have now considered practical ways of using virtual earth circuitry, and can go on to the even more practical matter of building a circuit whose action may not seem quite so mysterious.

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## GOING BACK... 1970 60 50 40 30 20 COLIN RICHES

ARTHUR DOW

EVOTEES of this column will be highly delighted at the publicity currently being given by the Post Office to the 50th. anniversary of broadcasting in this country by issuing a set of three postage stamps to commemorate the event. Since we mentioned the subject in the last issue details of the stamps have been released by the Post Office and they are reproduced here.

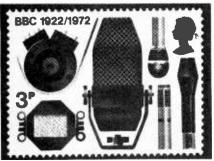
The 3p stamp depicts six of the many types of microphones used in broadcasting since 1922. Observant old-timers will recognise the Marconi-Sykes electromagnetic microphone of 1924 as well as the Marconi-Reisz carbon microphone of 1926 among the collection. On the 5p stamp a typical domestic wooden horn loudspeaker of the 1920's is illustrated. Some readers may recall the S.G. Brown conical horn speaker and the Amplion horn of the same period.

No doubt there are many of these speakers still hidden away in attics and cupboards so let us hope that this invaluable publicity will cause the public at large to appreciate the value and significance of these treasures from the early days of wireless and thus prevent their needless destruction.

The third stamp, for  $7^{1}_{2}p$ , brings us right up to date with a fine illustration of one of the latest colour TV cameras as used by both the BBC and the independent TV companies.

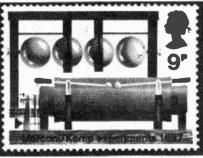
The fourth stamp, to be issued at the same time as the other three, is for 9p and shows an early form of spark transmitter as used by Marconi in establishing wireless contact between Lavernock Point, Glamorgan, and Brean Down, Somerset, in May 1897. On the 75th. anniversary of this historic event the name of George Kemp is coupled with that of Marconi. Kemp was a Post Office engineer loaned to Marconi as a senior assistant. Their experiments resulted in the first successful tests over water and, incidentally, the first between two countries.

All four stamps are the work of David Gentleman who was also the designer of the Philympia series of stamps issued in 1970. The anniversary stamps described will be on sale on September 13th.









The 3p stamp is printed in several shades of grey with black, brown and yellow while the 5p stamp is grey, belge, red, brown, black and umber. The 74p stamp featuring the TV camera also has several shades of grey combined with black and red. The 9p Marconi-Kemp commemorative issue combines light and blue grey with black, yellow and brown. A special first-day cover and two pictorial handstamps are being provided by the Post Office.

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Malcolm Connah

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## MONTHLY NEWS FOR DX LISTENERS

OR a change this month I think it will be useful to all readers if we start with some news of DX stations around the world. The source of the information is Sweden Calling DXers and my own

listening efforts.

BOLIVIA: The Bolivian station on 4845 is CP-72, Radio Fides de La Paz. This station is scheduled to broadcast from 1030 to 0330 GMT only but has been heard on an extended schedule. The station has also been heard in Europe on 4875kHz.

CP-103, Radio 27 de Diciembre, listed on 3350kHz is presently operating on 3439kHz with sign-off at

0215 GMT or later.

BRAZIL: The new European service from Radio Nacional de Brasilia has been noted on 15450kHz with weak signals and splash from VOA, Monrovia, on 15445kHz at 2245. The programme consists of Brazilian music and short talks in English, reports are requested.

MONGOLIA: Radio Ulan Bator has introduced a Russian service which is on the air on Tuesdays at 1030 and on Fridays at 1040. These broadcasts have been heard on 7260kHz, the station announces 41·3,

48 and 1321 metres.

PARAGUAY: ZPA-1, Radio Nacional, Asuncion can be occasionally logged on 4615kHz with special sports

newscasts in Spanish after 2200 hours.

SWEDEN: Due to heavy interference on 15105kHz during the broadcasts in English and Swedish to the Far East at 1230-1330, Radio Sweden has moved this transmission to 17815kHz as from Thursday 22nd June. Reports will be much appreciated. A change of frequency for South Asia at 1400-1530 is also being considered.

The first report this month comes from Mervyn Winters of Greenisland, Co. Antrim who used an AR88 with a 12 foot whip antenna to pull in several

interesting stations including:

4980 Ecos del Torbes in Spanish at 2350

4995 R. Brazil Central, LA music at 2340. 6030 RSA, South Africa noted at 2355.

6140 RNE, Spain, English to NA at 0110.

9570 R. Australia noted at 0714. 11620 AIR, Delhi, India at 1930.

11720 R. Nacional de Brazilia at 2307.

15018 R. Hanoi, N. Vietnam in English at 2015.

15190 R. Ankara, Turkey in English at 2200.

21570 R. Japan in English to Europe at 0800.

21605 R. Kuwait in Arabic at 0900.

Roger Hunter of Carmarthen has added a PR 30 preselector to his Codar CR-70A receiver enabling him to hear the following stations:

6025 R. Portugal in English at 2058 6080 R. Berlin International at 2145.

7235 R. Australia with Newsreel at 1000.

9009 Kol Israel, 'In the Jewish World' at 2115.

9640 TWR, Monte Carlo, DX programme at 0945.

11755 R. Finland in English at 1815.

15105 R. Japan, news and comment at 2000.

17735 R. Free Europe, music at 1740.

21545 R. Ghana, talk in English at 1050.

21595 CBC, Canada in English at 1900.

Michael Berry of Dewsbury in Yorkshire has again used his outdoor vertical wire and Eddystone EB-35 receiver to good effect, hearing:—

3264 R.T.V. Congolaise noted at 1910.

4765 R.T.V. Congolaise in French at 2100.

4832 R. Capital, Costa Rica in Spanish at 0205.

4880 R. Once Sesenta, Peru in Spanish at 0335.

4940 R. Yaracuy, Venezuela, Spanish at 0135.

4965 R. Santa Fe, Colombia, Spanish at 0430.

4970 R. Rumbos, Venezuela, Spanish at 0435. 4980 Ecos del Torbes, Ven., Spanish at 0025.

5030 R. Reloj Continente, Ven., Spanish at 0310.

6255 Schulungssender, Austria, German at 1245.

11862 R. Lubumbashi, Zaire in French at 1655.

11865 R. Club Pernambuco, Brazil at 0330.

Nigel Knowlman of Cullompton in Devon has a Lafayette HA-600A and a 50 foot inverted L antenna, this combination enabled him to hear the following stations:—

11520 R. Bangladesh in English at 1745.

11720 R. Nacional de Brazilia in English at 0700.

11940 R. Bucharest, Romania, English at 1300.

11955 FEBA, Seychelles in English at 1730.

15170 Beirut, Lebanon in English at 1830.

15185 Voice of Nigeria, English at 0700.

17655 R. Cairo, U.A.R., English at 1800

17815 HCJB, Quito, Ecuador, English at 1945.

Next month the series of instructional articles for newcomers will continue with a discussion of the various types of aerials. This will include details of construction and the advantages and disadvantages of the various types.

Reports should arrive by the 15th of the month and be addressed to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex.

#### **OUR "CQ" COLUMN**

If you wish to have a "CQ" request in *Practical Wireless*, we would be grateful if you could write it out in the same style we print it. This helps us to help you by saving time trying to take extracts from long letters and deciphering names and addresses.

## WITH ZO



## David Gibson, G3JDG Frequencies in kHz • Times in GMT

THE AMATEUR BANDS

T'S September already and the summer has almost gone. This is sad news for the sun bathers but good news of the l.f. enthusiasts. How about having a really good "go" at topband this year? Once the leaves turn and the darker evenings arrive you can be sure of hearing a few interesting tweets on 160 metres. Quite a number of European countries are active as are stations from further afield. You only need to monitor the bottom 50kHz of the band (i.e. from 1800kHz to 1850kHz) to hear quite a bit of topband d.x. The American stations are usually active at the very edge of the band and usually on c.w. Stewart, W1BB, is a good one to listen for and a few VO and VE stations have put in an appearance from time to time.

Czechoslovakia is a country well represented on 160 metres. Apparently, novice licences are awarded and OL stations are limited to 10W on 160 and 2 metres. What a splendid idea. There was a time when the British Post Office exercised its wisdom and imposed a 10W limit plus c.w.—only for the first year—Ah, happy days. Rumour has it that LU (Argentine) EL and ZS will be in evidence on 160 metres which should offer a challenge from sitting comfortably on 14MHz and just letting the d.x. drop into ones lap.

Letter from **Peter Martin** (Nottingham) informs that KR6 stations are now signing KA6 and that 7P8AM is on from Lesotho—anyone heard him yet? He also mentions the RSGB news Bulletin Service. The latter is broadcast on Sundays on both eighty metres and two metres and is put out from various parts of the country, so you should have no problems in receiving all the latest information on Amateur radio, both for licensed operators and s.w.ls. Time depends on which area you're in. However, try listening on 3.6MHz at 0930 for transmissions from Bromley in Kent.

Speaking of the RSGB, don't forget that many of its members put out special slow morse transmissions to help those trying to get up to the magic twelve words/minute. These stations are on from all over the country and at many different times. There is almost certainly somebody on in your locality—usually on topband. The RSGB will give you all the information (you get this and many other things all the time if you become a member).

Alan Smith (Nelson) took "one of my rare trips down on to eighty metres". Reward was ZD8RR at 5 and 7 but Alan queries the authenticity of this station. Any offers? Gear in use is a JR310 and a twiddle on twenty revealed squirts of s.s.b. from;; CE3AIU, CO2FA, CX2AL, CX2BR, EL2GY, FC9VN, FM7WN, HC1HV, HC1SS, HC2HM, HK3COC, HK6CBS, HV3SJ, LU3FAQ, LX1DV, OD5HD, PY2BCQ, PY4EP, PZ6AA, SL2ZZM, TI2FCD, TI8PE, TR8GD, VE1RB, VE2WY, VE3BYI, VE5AZ, VE7MT, VE7YF, VK2AVA, VK2BHR, VK3MO, VK4SD, VK5DK, VK6TW, VK7RX, VO5GJ, VP1TB, VP2GB, VP2MZ, VP7NO, VP9HA, VQ9MC, VQ9R, VR1FL, VU2HLU, W8JXM, W9YRA, XE1DO, XE1EH, ZD3D,

ZD7SD, ZE1CS, ZE6JS, ZL1GY, ZL2FA, ZL4CO, ZM2TG, ZP5CF, 4X4NJ, 4X4VB, 8P6EK, 9J2DT, 9K2CA, 9K2CI, 9M2CP, 9M2CW, 9V1QJ. Antenna was a sneaky sixty foot end fed.

R. Dickens (Shepherds Bush) has a "modified" R1155 and a 20ft. aerial. He reports signals from many EU stations on 3.5MHz but also includes a couple of goodies heard in the form of M1B and 6W8DY. Best on 7MHz was 4U11TU.

G. Benson (G8FBL) tells gleefully of contacts made by special station GB3CRC run by the Chad Radio Club, Lichfield. Over 300 contacts were made including chats on 21MHz with CT2BG, CX4CR, HC1RF, 7Q7BQ, 9H1DL, 9J2TB and 9Q5RA—no mention of mode. (Don't tell me, brightly coloured flags and it was a clear day!)

"I wonder how much of the inside is original", says an unsigned letter from Nicholas Dean of Loughborough. The antenna is a 20 metre bow tie (bet it suites you and, of course, you'll get d.x. in necks to no time) at 20ft and fed into an a.t.u. It is then pressed into service on 3.5MHz. Signals received from; CE8AA, CN8BQ, CT1HE, CT2BG, PY2FYQ, ZB2A, ZL6MP, ZS1MH, 4X4UF, 7X0GF, 905BJ.

Graham Armstrong (Jedburgh) reports hearing some good EU d.x. on topband; DL5XF, GI3GRD, GW3UPK. He reports a station on c.w. signing 2LO which will doubtless raise a smile. (LO LO, what's all this then?). Anyone else hear this character? Apparently he was on for at least a week.

David Lawley (Gravesend) sends in some interesting sigs heard on 160 metres. Among the c.w. offerings are; DL9KR, E19J, EL2CB, GC3ZES/A, GM2HCZ, GW3UCB, OK1HBT, OL1AOH, OL1APC, OL5APO, PA0PN (on s.s.b.).

B. Spencelayh (Enfield) has got his version of the Deluxe 9/12 receiver (PW April/May 1972) perking. First attempts on 21MHz brought sigs from; EA3SA, HB9AJO, JA4BLY, OD5LX, VQ9MC, WA1JTT, W9YFV, 4X4HK, 4Z4MO, 5H3JL, 9J2SS, 9M2DQ.

Happenings for September include the Harlow Mobile Rally on September 24 at Magdalen Laver, near Harlow. Contests in my little black book inculude: September 9-10, WAE phone contest; 10, 3.5MHz field day; 17, final d.f. round at Oxford.

#### **ELECTRONICA 72**

Electronica 72, recognised by many as the most important trade fair in the electronics industry, will take place this year at Munich, Germany, from November 23-29. Included in the exhibits will be components and assemblies, production facilities, testing apparatus, information and training. Running at the same time as the exhibition will be the conference Mikroelektronic consisting of some 40 lectures.

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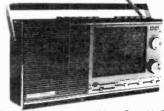
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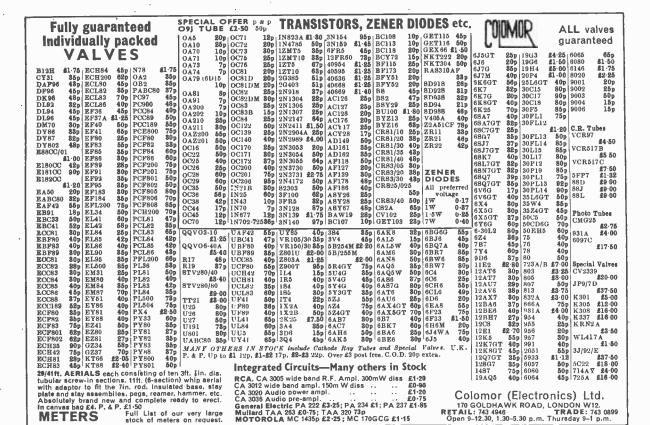
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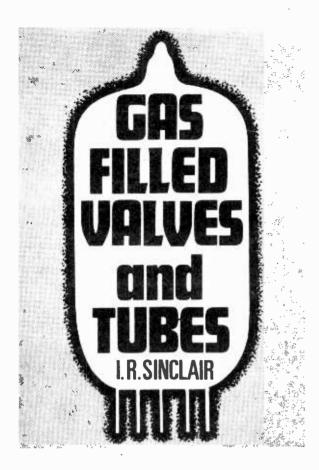
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#### **PART TWO**

#### **Trigger tubes**

The discharge between the anode and cathode in a gas-filled tube can be started in ways other than that of raising the voltage to striking voltage. One of these ways is to use a trigger electrode to generate ions which will then carry the current of the main discharge. The trigger electrode is a pointed wire very close to the unheated cathode and pointed to the cathode surface. Because of the close spacing, it is easy to start ionisation with a small voltage applied between trigger and cathode, as the creation of ions is dependent on field strength (volts per metre spacing).

In addition to this effect, ions are discharged at high speed from a pointed wire due to the particularly high field strength around points. The old electrostatic experiment of blowing out a candle with a point discharge from an electrostatic generator is an illustration of this effect (Fig. 9). With the voltage between anode and cathode less than the striking voltage but above the running voltage, current will start to flow only when the discharge is triggered by the injection of ions from the trigger circuit. This is achieved by applying a small positive pulse at the trigger electrode. The amplitude and width of this trigger pulse must be above certain critical values (depending on the shape and spacing of the electrodes) to start the main discharge. Once the main

discharge has started, it cannot be stopped by any voltage applied to the trigger electrode, only by dropping the anode-to-cathode voltage below a level called the "sustaining voltage." Fig. 10 shows the characteristics of a typical trigger tube, the HIVAC XC23.

#### **Applications**

Figure 11 shows a trigger tube used as a pulse amplifier. The trigger pulse causes current to flow,

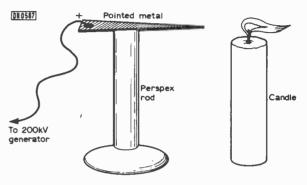


Fig. 9: The high concentration of electric charge around a point causes ionisation of the air. The movement of ions of the same sign away from the point creates a wind capable of blowing out a candle.

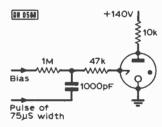


Fig. 10: Characteristics of the Hivac XC23. With bias at OV, pulse amplitude for transfer equals 91-98V; with bias of +80V, pulse required is 20V min.; trigger resistance equals  $47k\Omega$ . Delonisation time is 2mS (time for which Va=0 to switch off tube).

so that a negative voltage pulse is generated in the anode load resistor and a positive pulse in the cathode load resistor. The voltage drop can be designed to be sufficient to cause the tube to extinguish at the peak of the pulse, so that the tube is ready to fire again at the next trigger pulse. The repetition rate which can be used is limited by the time which must be allowed for all the ions created in the first discharge to recombine before the full voltage is again applied between anode and cathode. For this reason, trigger tube circuits working at rates greater than 4kHz are seldom found, and the circuits are notable for the use of capacitors to spread pulse widths out rather than to sharpen them, as is usually the case.

Figure 12 shows a ring counter circuit using gas trigger tubes. This type of counter circuit is not so familiar to constructors as the binary counters used in transistor circuits, and a description of its opera-

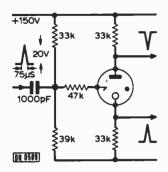


Fig. 11: If the negative pulse is not needed, a capacitor can be connected from anode to earth. The discharge of this will then provide the cathode pulse and the anode load can be raised so that the anode recovers slowly and the tube has ample time to switch off.

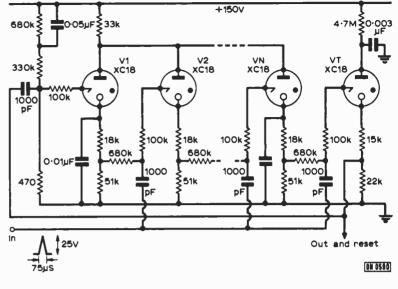


Fig. 12 (right): Ring counter circuit working at 500Hz.

tion might be of interest. The basic principle of any ring counter is that a set of bistable elements is connected in a closed ring in such a way that each trigger pulse fed to a common point turns on the element next to the one previously on, and also turns off that previous element. In the circuit of Fig. 12, imagine that V2 is passing current and that the rest of the tubes are not. Because of the current in V2, there will be a voltage positive to earth developed across the resistor in the cathode lead of V2, and this voltage will bias the trigger electrode of V3 (not shown, but wired in exactly the same way as V2) positive, not enough to fire the tube but enough to make certain that a trigger pulse of about 50V will fire V3. This value of trigger pulse is not sufficient to fire any tube whose trigger electrode is not raised in voltage already, so when a pulse is received at the common input terminal and applied to all the trigger electrodes, V3 is the only tube to fire. When V3 fires, however, the voltage in the common anode line drops, and this drop of voltage is sufficient to extinguish the discharge in V2. The result is that the discharge has moved one tube on with the receipt of one trigger pulse. This action continues from tube to tube as each pulse is received, until the last tube in the set, Vn, is glowing. In a ring-of-ten counter, this would be the tube indicating number nine, and wired to the number nine indicator of a display. This tube is connected to a transfer tube, Vt, and when the next trigger pulse is received, Vt will fire, causing a positive pulse to appear at its cathode load resistor. Vt will extinguish immediately after, however, as the value of its anode load is far too high to permit a continuous discharge, and the current which does flow is due to the capacitor between anode and earth discharging through the tube. The positive pulse at the cathode switches on V1, which has a positive bias on its trigger electrode already, and is also the zero indicator. The same positive pulse is also used as the output pulse of the counter stage, carrying to the next counting ring or to some other output.

#### **Counting tubes**

The action of a trigger tube, in which the trigger

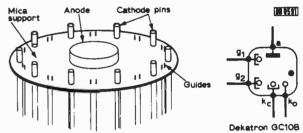


Fig. 13: On the left is shown the principle of construction of a Dekatron; the symbol of the Dekatron GC10B is shown right).

electrode starts off a discharge path which can then spread to the nearest anode, can be used in a tube in which the discharge is passed from one cathode to another, and which also makes use of the fact that the glow in a gas discharge is concentrated at the cathode. The best-known example of this technique is the well-known DEKATRON counting tube in which a central anode rod is surrounded by ten cathode rods (see Fig. 13). The structure of different types of Dekatrons differs in detail, but the type GC10B can be taken as an example of the way in which these fascinating tubes work. In the GC10B, the cathode pin which is used to indicate zero is taken to a base connection (ko), and all the other cathodes are connected together and taken to another base connection, ko. At the opposite end, the pins are visible through the glass end of the tube, and the glow round any particular cathode can be clearly seen. Escutcheon plates with the numbers 0-9 can be fitted against the end of the tube and lined up so that the zero of the escutcheon is adjacent to the zero pin of the tube, and the other numbers line up with successive cathodes.

To transfer the discharge from one electrode to another, guide electrodes are used. These are pins located in pairs between the cathodes; all the first pins of each pair in clockwise order are connected together and taken to base connection  $G_1$ , and the second pins of each pair are brought together to the  $G_2$  base connection.

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2N4289	7.7		15p		* *	 14p
2N4443	- 11		85p	BD130		65p
2N5062			42p	BD131		 77p
2N5088		- 11	46p	BD132	1.7	 81p
2N5192		- 11	77p	<b>BD</b> 135		26p
2N5195			90p	BD136		 27p
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AD142 AD149			50p			 вр
			68p	OC35		 63p
AD16			42p	82CN		 12p
AD162			40p	SD4		 9p
TO3 Trai	asistor (	Covers	, ea. 7p			

#### RESISTORS 10% - 5% - 2%

				/ 0	- /	0	-/-
Code	Power	Tolerance		Values		10 to 99	100 up
			in ohms		(see	note belo	w)
C	1/8W	5%	4·7-470K	E24	1	0.8	0.7
C	1/4W	10%	4.7.10M	E12	ī	0.8	0.7
C	1/2W	5%	4·7-10M	E24	1.2	ī	0.9
C	1W	5%	4-7-10M	E12	2.5	2	1.9
MO	1/2W	2%	10-1M	E24	4	3	2 nett
ww	1W	10%	0.22-3.9	E12	7	7	6
		$\pm 1/20 \Omega$				•	
ww	3 W	5%	1Ω-10K	E12	7	7	6
ww	7W	5%	1 Ω-10 K	E12	9	9	8
Codes:	C=carl	on film hig	h atability	low nois			
	MO = m	etal oxide I	electrosil 7	R5 nites	lowne	ina	
	WW = v	wire wound	Plessev	LEO MICIA	TOW III	Nec	

Values:
E12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. E24: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 82, 72, 91 and their decades. Prices are in pence each for same ohmic value and power rating, NOT mixed values. (Ignore fractions of 1p on total value of resistor order).

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FLH291	(7403)	20p	FLJ131	(7476)	45p
FLH211	(7404)	25p	FLH221	(7480)	68p
FLH271	(7405)	25p	FLH231	(7482)	87p
FLH381	(7408)	25p	FLH241	(7483)	1.32
FLH391	(7409)	25p	FLH341	(7486)	33p
FLH111	(7410)	20p	FLJ161	(7490)	80p
FLH351	(7413)	35p	FLJ221	(7491	
FLH121	(7420)	20p		AN)	1.28
FLH131	(7430)	20p	FLJ171	(7492)	85p
FLH141	(7440)	24p	FLJ181	(7493)	80p
FLL101	(7414)	1.22	FLJ231	(7494)	1.13
FLH281	(7442)	1.16	FLJ191	(7495)	87p
FLH361	(7443)	1-45	FLJ261	(7496)	1.48
FLH371	(7444)	1.45	FLJ301	(74100)	1.64
FLH151	(7450)	20p	FLJ281	(74104)	43p
FLH161	(7451)	20p	FLJ271	(74107)	52p
FLH171	(7453)	20p	FLK 101	(74121)	48p
FLH181	(7454)	20p	FLJ201	(74190)	1.80
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\( \text{A} \text{T 102} \ AT\pmod \text{T} 1 \ \ \frac{45}{24p} \ \ 3A \text{M T 108} \ AT\ \ 3.91 \ \ 41p \ \text{M T 108} \ AT\ \ 5.00 \ 32p \ 4A \text{M T 104} \ AT\ \ 5.00 \ 32p \ 6A \text{M T 107} \ AT\ \ 7.47 \ 5.0p \ 60 \ Volis. All tapped at 0-24-30-40-43-60V. \ \( \text{M T 124} \ AT\ \ 2.48 \ 32p \ 3A \text{M T 125} \ AT\ \ 3.16 \ 41p \ \text{M T 126} \ AT\ \ 2.24 \ 32p \ 3A \text{M T 125} \ AT\ \ 4.59 \ 41p \ \end{math}

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The action is as follows (Fig. 14): with about 475V applied to the anode through an 820kΩ resistor, and other details as shown in Fig. 14, a discharge must exist between the anode and one cathode. Since all the cathodes are joined together, and since the running voltage of a gas discharge is well below the striking voltage, once one cathode has started a discharge it cannot spread to any other cathode except by the action of the guides which will be described, unless one cathode is made more negative than any other. The only cathode with which this can be done is the zero cathode which is taken to a separate pin, so that the Dekatron can be made to read zero when power is first applied, or when a fresh count is wanted.

If now all the first guides (G₁) are pulsed negative, the glow will shift from the cathode to the nearest guide 1 and stay there. If the second guides are now pulsed negative just as the first guides are rising again in voltage, the discharge will shift to the nearest G2, which will again be one step clockwise. When this guide's voltage rises again, the glow transfers to the next cathode, which is one cathode on from the starting point. The result is that every time a set of pulses is applied to the guides, the glow shifts clockwise from one cathode to the next, and so counting has been achieved. This process continues until the glow lands on the zero cathode, which is taken to the -20V line through a  $150k\Omega$  load resistor, so that a positive pulse is obtained across the resistor whenever the glow lands on zero. This can be used to transfer the count to the next stage, as the positive pulse can be inverted by a valve or trigger tube and processed to provide the double pulse needed for the next stage.

The Dekatron system is at present the most economical method of counting and displaying, since both operations are achieved in one tube. It is, however, essential that the circuits published by HIVAC should be adhered to exactly. Any variation in the pulse width and amplitude, or in the time lag between the pulses applied to guides 1 and 2 can cause misfiring, and most of the problems encountered in Dekatron circuits are easily cured by attention to the pulse system. Fig. 14 shows the circuits which should be used for driving with single pulses, double pulses and sine waves respectively. The sine wave circuit is of particular interest, as the 50Hz mains provide an accurate frequency standard for digital clocks, the design of which is particularly easy using Dekatrons

Not every count is to ten, however, particularly in the case of digital clocks, and the Dekatron Selector tubes such as the type GS10C are designed with this in mind. Each cathode is taken to a separate pin on the 12-pin base, with the anode as a centre pin, and can be wired as a counter or as a transfer cathode. A transfer cathode is one which passes the count as a pulse to the next stage, and also acts as the zero to which some other cathode will reset. This enables us to have any count up to nine followed by a zero, and the range has been extended by tubes which count to 12. Another advantage of the selector type of tube is that it no longer ties us to the Dekatron type of display, but enables us to display on a Digitron type of tube, described later.

The standard range of Dekatrons includes counters and selectors working at rates up to 4kHz, but another range or Dekatrons using a third set of guides connected to the reset line through a  $220k\Omega$  resistor, and an output cathode guide connected to

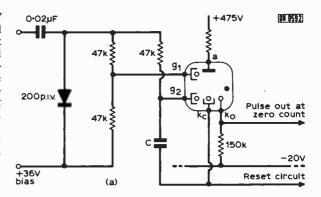


Fig. 14a: Integrated pulse drive. The value of C depends on the pulse width and repetion rate being used.

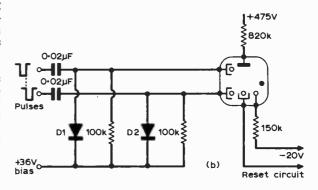


Fig. 14b: Double puise drive for the GC10B.

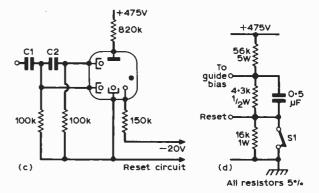
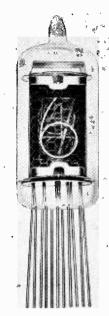


Fig. 14c: Sine-wave circuit (left) Frequency 50Hz 100Hz 200Hz 500Hz 1kHz 2kHz 4kHz  $C1(\mu F)$ 1.5 0.82 0.33 0.15 0.082 0.033 0.015 C2 (µF) 0.1 0.05 0.02 0.01 0.005 0.002 680 pF Reset circuit is shown on right. To reset, \$1 is opened, taking cathode Kc and guides to +120V and so transferring the glow to Ko.

the output cathode by a  $220k\Omega$  resistor, can be operated at speeds up to 20kHz.

#### Alpha-numerical indicators

As we have seen earlier, when a voltage is applied between the anode and the cathode of a gas-filled tube, a glow appears round the cathode. When a.c. is applied, of course, both electrodes are seen to glow.



A typical gas filled read-out tube. When a voltage is applied between the anode and cathode a glow appears around the cathode. By making the cathode in the shape of numbers or letters, it will glow when the voltage is sufficiently negative to cause striking.

The glow is due to the recombination of ions which have been formed by collisions and is most noticeable at the cathode because this is the place where electrons are being rapidly accelerated in the face of negative ions moving in the opposite direction. The glow exactly surrounds the shape of the cathode, and does not extend to more positive electrodes.

If the cathode is made in the shape of a letter or a number, this figure or number will be seen as a glowing shape whenever the cathode is sufficiently negative to the anode to strike and run. If a number of separately connected wires are shaped in the form of numbers 0-9, each number will display only when the wire forming it is sufficiently negative to the anode to form a gas discharge.

The Hivac Numicators are tubes of this type, and the range of types is large. Tubes may be viewed end-on or side-on according to the type of construction of the tube. Numicators can be driven from Dekatrons, provided that trigger tubes or other invertor stages are used to change the positive pulses at the cathodes of the Dekatron to the negative pulses used at the cathodes of the Numicator. Perhaps "pulse" is a misleading word in this application, because the top of the pulse will be as long in the time sense as the figure is to be displayed.

Most Numicators are designed for steady operation, but some are intended to be used in what is called the "anode stroking technique," often used in connection with digital counters.

Digital counters can readily be arranged to give a readout whenever a clock pulse is received, and the readout can be converted to decimal form and used to drive Numicators. Considerable economy in circuitry can be arranged if the decimal readout is attached to all the Numicator cathodes; for example, in a five figure readout, there would be one decimal converter with the zero output connected to all the five Numicator zeros, the "one" output to all the Numicator "ones", the "two" to all the "twos" etc. The decimal output and the tubes are then switched in sequence, so that the units tube has its anode volts pulsed just as the decimal output gives the unit figure pulse to all the Numicator cathodes, with the result that only the units tube displays a figure. On the next pulse, the tens tube is activated to display

the decimal output from another store, so that each tube flashes a digit in sequence. Because of the clock pulse rate used, the display looks continuous. This is not a technique which would be used in small counters, but it is extremely useful in small computers, particularly in conjunction with integrated circuit counters.

#### **Thyratrons**

Thyratrons are the big brothers of trigger tubes. Like trigger tubes, they are made to conduct by the application of a positive pulse to a third electrode; unlike trigger tubes, they use hot cathodes and can operate at very high voltages indeed—one type listed by English Electric quotes a peak forward voltage of 120kV and with large currents, up to several thousand amps, flowing. Small thyratrons are made in glass envelopes and resemble output valves at first sight, the larger types have ceramic casings.

The small type of Thyratron has a heated cathode, a grid similar to the control grid of an output valve, and an anode which is often finned and connected to a thick pin set in the glass bulb for maximum heat dissipation. In operation, the heaters must be switched on before high voltage is applied, this is usually done automatically by means of a thermal delay circuit, since failure to observe the correct delay period would be fatal to the thyratron. When the heaters have reached full temperature, the grid voltage can be applied, this is a negative bias sufficient to prevent any electrons passing the grid, enough, in fact, to prevent electrons from being emitted to any noticeable extent from the cathode. The positive anode voltage can then be applied.

If the grid is now pulsed positive, the tube conducts strongly due to the ionisation of the gas by the electrons from the cathode, and this current will continue until the voltage at the anode is reduced to a low value. After a short "recovery time", the tube can be fired again if the anode voltage has also recovered to its previous value. What makes the thyratron unique is its ability to switch very high currents very rapidly and at a high forward voltage. By very rapidly, we mean delay times of around 20-120 nanoseconds in the most advanced types.

Thyratrons are used to control spot welders, to pulse radar transmitter magnetrons, and to operate other short time, high energy devices such as the Kerr Cell used in high speed photography. They also find extensive use in large invertors (converting a.c. to d.c.) such as are used at each end of the crosschannel d.c. cable. One intriguing use is as "electronic crowbars". In modern electronic equipment, protection against faults by means of fuses is not very effective because of the time which a fuse needs to blow. Even if this time is measured in milliseconds, much damage can be done, and the idea of the electronic crowbar is a device which will come into operation much more quickly than a fuse, shorting out the voltage across the circuits and taking the current which will eventually blow the fuse. This use demands a device which can be switched into conduction very quickly and which will take a large current in the time before a fuse blows-the Thyratron is ideal, though for the smaller sizes thyristors are taking over.

The Author gratefully wishes to acknowledge the help of HIVAC LTD, in the preparation of this article.



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as the D.J. 1058 or D.J. 708. Size 32" × 14½" × 7" (incl. lid.) £55-00
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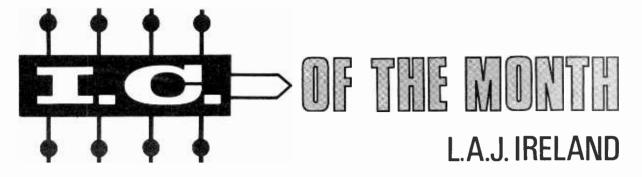
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Number 33

Motorola MFC6040 Electronic Attenuator

COUSTIC feedback—that deafening howl which occurs when a microphone picks up the sound from the loudspeakers of a public address system and thereby completes a feedback loop, setting the whole system into oscillation—will be familiar to readers. It is particularly embarrassing when, for example, an announcer is using a microphone with a considerable length of cable, and by moving to a new location initiates this response from a previously well-behaved system. It would therefore be convenient if, in addition to his microphone, the announcer could have to hand the gain control of the amplifier, so that it could be adjusted for best results from his own position, without having an assistant constantly at the amplifier controls.

However, it is not a practical proposition to remove the volume control of the amplifier to the end of a long cable for such remote operation. There would be a considerable increase in the noise level of the system, despite the best efforts to screen the cable; there is also the consideration that the audio signal may have been amplified prior to the volume control, and at the higher level, may itself produce some feedback effects due to the stray capacitance of the cable.

It may be suggested that a volume control could be incorporated in the microphone case, to control the signal level before it is applied to the amplifier; however, the microphone may not be the sole signal source. It is common practice to use several inputs to a public address system, with part of the preamplifier stages acting as an audio mixer, so it would be desirable for the remote unit to control the gain of the "mixed' signal, rather than just that of the microphone channel.

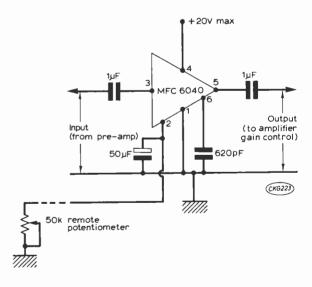
What is required, therefore, is a method of remote control of amplifier gain which does not involve long signal-carrying cables, is therefore impervious to noise and does not introduce feedback or degrade signal quality. It is just this requirement which is satisfied by the new Motorola Electronic Attenuator integrated circuit, type MFC6040.

#### **Operation**

In operation, the device is inserted in series with the master gain control of the mixer section of the preamplifier, and, depending on the setting of a remote potentiometer, attenuates the signal applied to its input terminal. Only a d.c. potential appears on the leads to the remote potentiometer; capacitative effects are therefore irrelevant. The leads may be of any desired length and need not be screened. All the difficulties visualised above are therefore avoided.

#### **Practicalities**

It is possible to obtain microphone cable in which two conductors are incorporated within the braiding. One of these may then be used in the conventional fashion, applying the microphone signal between it and the screening. The other can then be used for the remote control potentiometer, with the screening as an earth return. There is no question of capacitative crosstalk as the control connection is decoupled at the i.c. by a  $50\mu F$  capacitor.



Wiring for an amplifier remote gain control system using the Motorola MFC6040 integrated circuit.

The circuit indicates the connections and components required for the provision of the remote control facility outlined. A beginner should find little difficulty in assembling it on a piece of veroboard, and it can easily be accommodated close to the master gain control inside even the most compact amplifier. A d.c. supply of 20V max. is required to

operate the i.c.; this is commonly available in modern transistor amplifiers and for mobile operation the 12V car battery supply is adequate. The i.c. itself is presented in a miniature 6-pin epoxy package with pin 1 indexed.

#### **Alternatives**

Alternative applications will be evident to the experimenter. The unit can clearly be employed as an audio automatic gain control by rectifying part of the output of the unit and applying it to pin 2 as a control voltage. Similarly, feedback systems can be designed which produce a control voltage dependent on signal frequency, for pre-emphasis or deemphasis operations, or to investigate Dolby effects. A suitable low-frequency signal applied to pin 2 could be used for tremolo. It is clear, then, that the field for experiment with the MFC6040 is extremely wide, and we are likely to hear much more of it.

## TELEVISION

#### OCTOBER ISSUE

#### COLOUR TV DELAY LINES

Why are delay lines necessary in a colour receiver, what do they do and how do they do it? We have not previously taken a close look at this aspect of colour television but we shall be doing so this month, in particular to see how the PAL delay line acts as a comb filter to separate the U and V components of the transmitted chrominance signal.

#### RECEIVER-MONITOR

A simple conversion of a domestic receiver to act as a monitor, not only to accept CCTV signals-from a camera or videotape recorder-but also to provide demodulated off-air signals to drive other monitors, for mixing in a CCTV studio or to feed to a videotape recorder.

#### WIDEBAND BAND 1 PREAMPLIFIER

The latest Roger Bunney preamplifier gives a gain of some 25dB over channels E2-4 (48-65MHz), using five BF180 transistors and providing two separate outputs. It is extremely stable over the bandwidth and may be used for DX work or for small relay systems, especially where Band 1 channels are used for distribution after frequency translation from the higher channels.

#### SERVICING TV RECEIVERS

The next chassis we are covering is that used in the Bush/Murphy TV141/TV148/V153/V159 series.

#### COLOUR RECEIVER PROJECT

Details this month of cabinet construction.

PLUS ALL THE REGULAR FEATURES

ON SALE SEPTEMBER 18

#### 2 METRE Tx —continued from page 517

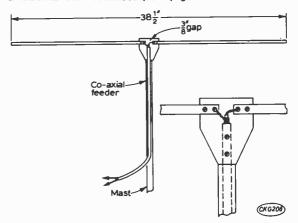


Fig. 2: Construction of a simple half wave dipole for 2 metres.

ranges. One can easily be made, using 14in. aluminium tubing, as shown in Fig. 2, the elements being bolted to a piece of insulating material. A more weatherproof aerial can be made on the same lines, but using a closed box as fitted to TV and similar aerials. This aerial is easily raised on a light mast or post, with the co-axial feeder running down to the transmitter.

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0.35

0.25

0.16

0.47

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watt	5%, lp.	↓W, 1W & 2W
	5%, 1p	E12 Series
# watt	5%, 11p	
1 watt	2%, M/O	4p
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Carbon: Log. or Lin., less switch, 16p Log. or Lin., with switch. 25p Wire-wound Pots (3W), 38p Twin Ganged Stereo Pots, Log. or Lin. 40p.

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SPECIAL OFFER TOSHIBA TH9013P 20 WATT AMP £3.50 TH9014P PRE-AMP £1.25

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Post & Packing 13p per order. Europe 25p. Commonwealth (Air) 65p. (MIN.) Matching charge (audio transistors only) 15p. extra per pair. Prices subject to alteration without prior notice.

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BF258

BF259

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0.48

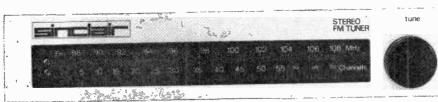
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**CALLERS WELCOME** HRS. 9-5.30 MON.-FRI. 9-5.0 SAT.

# Sinclair Project 60

## **Project 60 Stereo FM Tuner**



Built and tested. Post free. £25

## with phase lock-loop principle

Amongst the many advanced electronic features to be found in this remarkable stereo tuner, use of the phase lock loop principle ensures standards of audio quality better than from any other method of detection yet used. Varicap diode tuning, accurately formed printed circuit coils, an I.C. in the special stereo decoder section and switchable squelch circuit for silent tuning between stations contribute to the unsurpassed performance of this tuner, irrespective of price consideration. But the Project 60 FM Stereo Tuner is far from expensive – indeed, it offers fantastic value for money and will bring the thrill of stereo radio to many who previously. may not have been able to afford it. The tuner may be used with any good system as well as Project 60, but if you use it with other Project 60 modules, you will find the matching front panels particularly impressive in appearance as well as function.

#### SPECIFICIATIONS

Number of transistors: 16 plus 20 in I.C.

Tuning range: 87-5 to 108MHz.

Sensitivity: 7µV for lock-in over full de-

Squelch level: typically 20 µV

Signal to noise ratio: £65dB.

Audio frequency response: 10Hz-15Khz

Total harmonic distortion: 0.15% for

30% modulation. Stereo decoder operating level: 2 µV.

Cross talk: 40dB.

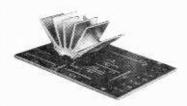
Output voltage: 2 · 150mV R.M S max. (typically 2 · 50mV, stereo)

Operating voltage: 25-30V DC at 100mA.

Indicators: Stereo on : tuning

Size: 93 x 40 · 207mm.

## Super IC.12 Integrated circuit high fidelity amplifler



Having introduced Integrated Circuits to hi-fi constructors with the IC.10, the first time an IC had ever been made available for such purposes we have followed it with an even more efficient version, the Super IC 12, a most exciting advance over our original unit. This needs very few ex-ternal resistors and capacitors to make an astonishingly good high fidelity amplifier for use with pick-up, F M radio or small P A, set up, etc The free 40 page manual supplied, details many other applications which this remarkable IC make possible. It is the equivalent of a 22 tran

sistor circuit contained within a 16 lead DIL package, and the finned heat sink is sufficient for all requirements. The Super IC.12 is compatible with Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board

#### SPECIFICATIONS

Output power: 6 watts RMS continuous (12 watts peak), 6-8Ω Frequency Response: 5Hz to 100KHz - 1dB Total Harmonic Distortion: Less than 1% (Typical 0.1%) at all output powers and frequencies in the audio band (28V) Load Impedance: 3 to 15 ohms Input Impedance: 250 Kohms nominal Power Gain 90dB (1,000,000,000 times) after feedback Supply Voltage: 6 to 28V Quiescent cur-rent: 8mA at 28V. Size: 22 · 45 · 28mm including pins and heat sink

Manual available separately 15p post free

With FREE printed circuit board and 40 page manual

£2.98 Post free

#### Project 605



The easy way to buy and build Project 60

Project 605 is one pack containing one PZ5, two Z30's, one Stereo 60 and one Masterlink This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting

Complete Project 605 pack with £29.95 comprehensive manual, post free

Everything you need to assemble a superb 30 watt high fidelity stereo amplifier without having



Sinclalr Radionics Ltd, London Road, St. Ives, Huntingdonshire PE17 4HJ. Tel: St. Ives 64311

## the world's most advanced high fidelity modules

#### Z.30 & Z.50 power amplifiers

Built, tested and guaranteed with circuits and instructions manual z.30 £4.48 z.50 £5.48

The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8\Omega) and all lower outputs. Whether you use Z 30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that Z.50s and Z.30 may be used in a far wider range of applications.

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications). — Power Outputs:

2.30 16 watts R.M.S. into 8 ohms using 35 voits 20 watts R M.S. into 8 ohms using 30 voits 2.50 40 watts R.M.S. into 3 ohms using 40 voits 30 watts R M.S. into 8 ohms using 50 voits 2.50 40 watts R.M.S. into 3 ohms using 40 voits 30 watts R M.S. into 8 ohms using 50 voits Fraquency response: 30 to 300.000Hz - 1dB Distortion: 0.02% into 8 ohms. Signal to noise ratio: better than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms (for 15w into 80). For speakers from 3 to 15 ohms impedance. Size: 14 x 80 x 57mm.





#### Stereo 60 Pre-amp/control unit

Designed specifically for use on Project 60 systems, the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxial planar transistors are used throughout, a really high signal-to-noise ratio and excellent tracking between channels is achieved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly easy to mount

SPECIFICATIONS—Input sensitivities: Radio – up to 3mV Mag. p.u. 3mV correct to RIAA. curve £1dB:20 to 25,000 Hz. Ceramic p.u. – up to 3mV. Aux. – up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE - 12 to —12dB at 10KHz: BASS + 12 to —12dB at 100Hz Front panel: brushed aluminium with black knobs and controls Size: 66 x 40 x 207mm



Built, tested and guaranteed

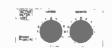
Built, tested and guaranteed

£9.98

£5.98

#### A.F.U. High & Low Pass Filter Unit

For use between Stereo 60 unit and two Z.30s or Z.50s. The unit is very easily mounted and is unique in that the cut-off frequencies are continuously variable. As attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The AFU is suitable for use with any other amplifier system. There are two filter sections – rumble (high pass) and scratch (low pass). H.F. cut-off (—3dB) variable from 28KHz to 5KHz. L.F. cut-off (—3dB) variable from 25Hz to 100Hz. Distortion at 1KHz (35V. supply) 0.02% at rated output. Operating voltage from 15 to 35V. Current 3mA. Size: 66 x 40 x 90mm.



#### **Power Supply Units**

Designed specifically for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ.6 or PZ.8 where a stabilised supply is essential

PZ.5 30 volts unstabilised £4.98 PZ.6 35 volts stabilised £7.98 PZ.8 45 volts stabilised (less mains transformer)

€7.98 PZ.8 mains transformer





#### Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc	£4.48
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P U. volume control, etc	£9.45
12W, RMS continuous sine wave stereo amp, for average needs	2 x Z.30s, Stereo 60; PZ.5	Crystal. ceramic or mag. P.U., F.M. Tuner. etc	£23.90
25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60; PZ.6	High quality ceramic or magnetic P U., F M. Tuner, Tape Deck, etc.	£26.90
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms)	2 x Z.50s, Stereo 60; PZ.8, mains transformer	As above	£34.88
Indoor P.A.	Z.50, PZ.8, mains transformer	Mic , guitar, speakers, etc., controls	£19.43
F.M. Stereo Tuner (£25) & A	A.F.U. <b>(£5.98)</b> may be	e added as required.	



#### Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, your money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sinclair Radionics Ltd

Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defect arise in normal use, we will service it at once and without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically £1.00) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.

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AC176	25p	BC107	8p	BFY51	12p	OC83	20p	2N2646	47p		
AC141K	20p	BC108	8p	BSY95A	150	OC170	24 p	2N2926	10p	DIODE	S
AC142K	20p	BC109	8p	ME0402	18p	OC200	25p	2N3053	20p	IN 4001	4 p
AD14	40p	BC154	20p	ME0404	14 _D	OC201	25p	2N3055	49p	IN4002	4 p
AD150	44p	BC168	10p	ME4401	10p	OC25	25p	2N3702	12 p	IN4003	51
	- 1	BC169	110	ME4102	120		30p	2N 3703	12p	IN 4004	71
AD162 M	P55p	BC182L	8p	ME6002	14p		36p	2N3704	120		81
AF114	15p	BC183L	8p	ME6101	14p		25p	2N3705	12p		61
AF115	15p	BC184L	8p	ME6102	15p	OC36	86p	2N3706	10p		100
		BC212L	8p	MP8111	32p	TIP29A	48p	2N3707	10p		81
AF116	15p	BC214L		MP8511	34p		55p		9p	1844	101
AF117	15p	BC214L	8p	MP8513	45p		58p		10p	IN4149	41
				OC41	18p		69p		10p		321
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0-4/μr, 13p. 160V· 0-01μF, 0-015μF, 0-022μF, 0-033μF, 0-047μF, 0-068μF, 3p. 0·1μF 3↓p. 0·15μF, 4↓p. 0·22μF, 5p. 0·33μF, 6p. 0·47μF, 7↓p. 0·68μF, 11p· 1·0μF, 13p.

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S			=8N7413		=8N7486 =8N7490	0.67
4p	301A To99	49p	= SN7416 = SN7417		= 8N7490 = $8N7491A$	
4 p	301A DIL	45p 28p	=8N7417 =8N7420	0.15	=8N7491A =8N7492	0.67
5p	709C To99	30p	=8N7430		=8N7493	0.67
7p	709C DIL		=:8N7440	0.15	=8N7494	0.77
βр	723C To99	87p	=8N7441	0.67	= 8N7495	0.77
, 6p	723C DIL 741C To99	85p	=8N7442	0.67	=8N7496	0.77
10p		34p	=8N7443	1.95	=8N74100	
8p		34p	=8N7444	1.95	=8N74104	0.97
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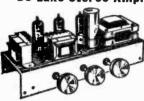
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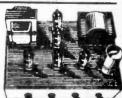
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BA102 30p	BF898 25p	OA10 35p	TIP30A 60p	2N2147 75p	28012 10.00
BA115 7p	BFX13 25p	OA81 10p	T1P31A 60p	2N2147 75p	28018 6-25 28026 8-90
BA145 15p	BFX34 75p	OA91 7p	TIP32A 70p	2N2217 25p	
BAX13 5p	BFX37 30p	OA200 7p	TIP33A	2N2221 20p	28301 50p 28303 65p
BAX16 7p	BFX88 20p	OA202 10p	1.00	2N2221 20p	28324 95p
BC107 10p	BFY50 20p	OC16 75p	TIP34A	25p	40250 50p
BC108 10p	BFY51 20p	OC20 95p	1.50	2N 2369 A	40360 40p
BC109 10p	BFY52 20p	OC23 85p	TIP35A	15p	40361 40p
	BFY64 50p	OC25 40p	2·50	2N2906 20p	40362 50p
BC109C 12p	BFY90 59p	OC28 65p	TIP36A	2N2926 (all	40408 50p
BC113 15p	BLY36 8:00	OC35 50p	3.00	cols) 10p	40486 75p
BC117 20p	B8X20 15p	OC36 65p	TIP41A 75p	2N3053 20p	40636 1:10
BC143 35p	BSY27 15p	OC42 40p	TIP42A 85p	2N3054 50p	40430 1.00
oop	20121 TOD	2042 TOP .	OOP	2710004 00h	10400 1.00

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17p





QUANTITY	DISCOU	INTS
10% 12+ : 15% 20% 100+ : 25%	25+ 250+	ANY ONE TYPE
From above sect Circuits and Spe counts are include Minimum order y Postage 7p on all	cial Offers ed. zalue £1 ple	where dis-

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25 + 20p 100 + 17p 500 + 15p	25 + 9p 100 + 8p 500 + 6p 1000 + 5p
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-		
Туре		
1 amp		re
IN4001	50	6
IN4002	100	
IN4003	200	- 8
IN4004	400	8
IN4005	600	10
IN 4006	800	12
IN4007	1000	15
1.5 amp	minia.	ture
PL4001	50	8
PL4002	100	9
PL4003	200	10
PL4004	400	10
PL4005	600	12
PL4006	800	15
PL4007	1000	16

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25 + 50p 100 + 45p 500 + 38p 1000 + 33p

2N3055

, -		,
702C	TO5	75p
709C	TO99	35p
709C	D.I.L.	35p
723C	TO99 4	1.00
723C	D.I.L.	95p
725C	TO99 4	
741C	TO99	55p
741C	D.I.L.	
747C	TO99 4	1 10
747C	D.I.L.	
		11 10
72741P		
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TUD	WITH AC	CESSORI	ES 12
Гуре	Vol ts		- E
	P.I.V	. 1-11	1
	RANGE		
3C35A	100	75p	TV TWO
3C35B	200	79p	10.00
3C35 D		85p	
	RANGE (	TO48)	
3C40A	100	85p	- 3
C40B	200	90p	2 A
3C40D	400	£1.00	3 Amp
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T048 | SC45A | 100 | 95p | SC45B | 200 | \$1.00 | SC45D | 490 | £1.25 | SC45E | 500 | £1.45 | 15 AMP RANGE (T048) | SC50A | 100 | £1.25 | SC50A | 200 | £1.25 £1.25 £1.85 £1.65 £1.85 200 400 8C50E 500 DIAC D32 25p TRIACS Types (TO66) 85p

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(Plastle)

(TO5)

8C50B 8C50D

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Additional 40430

SMALL SI	ZE AND	LOW	COST
Туре	Volts	Price	
	P.I.V.	1-11	
HALF AM			
BO5/05	50	20p	
BO5/10	100	25p	
ONE AMP		H	
TUBULAR			
B1/05	50	25p	
73.710	200	0.0	



× ♣ B2/05 50 100 200 600 1000 35p 40p 45p 50p B2/100 B2/200 B2/600 B2/1000 FOUR AMPS

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CRS 1/40 400 TCRS 1/60 600 TCRS 1/60 600 TCRS 3/05 50 80 CRS 3/10 100 30 CRS 3/10 100 45 CRS 3/40 400 45 CRS 3/40 400 60 SEVEN AMP (TO48) CRS 7/400 100 60 CRS 7/400 400 70 CRS 7/600 600 95 SIXTEEN AMP 30p 30p 35p 35p 45p 55p **6**0p 60p 65p 70p 95p SIXTEEN AMP SCR 16/100 100 SCR 16/200 200 SCR 16/400 400 SCR 16/600 600



3 Amn

T048

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Components for a 28V 0.5 Amp power unit ideal for all versions *£2.00. Also suitable Sinclair PZ5 *£3.70.

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Specially chosen for the IC12. 5"8 ohm £1.00.5" x 8"8 ohm £1.45. 10" x 6" 15 ohm °£2.00.

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19"/21" any type	£3 ·0
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All tubes add £1 carriage.	

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EB91 EBF89 ECC82 EC180 EF80 EF85 EF183 EF184 EY86 30PL13	5p 12ip 12ip 7ip 12ip 12ip 12ip 12ip 17ip 20p	30L15 30P4 PC97 PCF86 PC84 PCF80 PCC89 PCL85 PCL85 PCL86	12ip 12ip 17ip 17ip 7ip 7ip 12ip 22ip 17ip	PL36 PL81 PY81 PY800 PY82 PY33 U191 6F23 30PL1 30PL2	28 ip 17 ip 15 p 15 p 22 ip 17 ip 17 ip 29 ip 20 ip
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For Ferguson 850 900 chassis. Adaptable for most UHF Chassis 22.50, p. & p. 50p.

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GRYSTALS AS NEW: Hc 6u, 5,345; 5,030; 5,006; 4,945; 4,875; 4,840; 4,795; 4,580; 4,660; 4,520; 4,510; 2,300; 2,295 Kc/s. 50p each plus Ap. p.p.

TRIMMER BARGAINS. These are 10PF sub-min. airspaced trimmers on board with min. wire ended X1alBrand new. No details: Contents 12 trimmers, some
ceramic caps. Xtal frequency 3RD overtone 249 mc/s280 Mc/s. 255 Mc/s. No choice.
Trimmers without Xtal—80p per doz. plus 174p p.p.
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MURHEAD DECADE A.F. SIGNAL GENERATOR.
This precision instrument can be used:

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WOULD CUSTOMERS PLEASE ENSURE THAT ALL ORDERS ARE PRINTED IN BLOCK CAPITALS AND INCLUDE YOUR ADDRESS.

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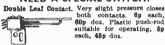
NEW IKW MODEL Electronically changes speed from approximately 10 revs. to maximum. Full power at all speeds by finger-tip control. Kit includes all parts. case, everything and full instructions. 21-50 plus 13p post and insurance. Made up model also available. \$2.25 plus 13p post & p.

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220/240v. 50 cycle solenold with laminated core so very silent in operation, Closes 4 circuits each rated at 10 amps. Extremely well made by a German Electrical Company. Overall size 2\(\frac{1}{2}\times 2\) \times 2\(\frac{1}{2}\times 2\times 2\(\frac{1}{2}\times 2\times 2\times 2\times 2\times 2\times 2\(\frac{1}{2}\times 2\times 2\times 2\times 2\times 2\times 2\times 2\(\frac{1}{2}\times 2\)



#### **NEED A SPECIAL SWITCH?**





#### MICRO SWITCH

5 amp changeover contacts, 9p each, \$1 doz. 15 amp Model 10p each or \$1.05 doz.





#### MINIATURE WAFER SWITCHES

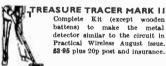
2 pole, 2 way—4 pole, 2 way—3 pole, 3 way—4 pole, 3 way—4 pole, 3 way—2 pole, 4 way—2 pole 6 way—1 pole, 12 way, All at 20p each, \$1.80 for ten, your assortment.

WATERPROOF HEATING ELEMENT 26 yards length 70W. Self-regulating temperature control. 50p post free



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Learn in your sleep; Have radio playing and kettle boiling as you to ward off intruders—have warm house to come home to. All these and many other things you can do if you invest in an electrical programmer Clock by famous maker with 16 amp. on/off switch. Switch on time can be set anywhere to stay on up to 6 hours. Independent 60 minute memory jogger. A beautiful unit. Frie £1.95 + 20p p & p or with glass front chrome bezel 78p extra.



Complete Kit (except wooden battens) to make the metal detector similar to the circuit in Practical Wireless August issue. \$3.95 plus 20p post and insurance.

#### SNAP ACTION SLIDE SWITCH

Rated 5a. 240v. Made by Arrow. Type fitted in the handles of electric drills, vacuums, etc. 5p each, 10 for 45p.



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For digital instruments, counters, timers, clocks, etc. Hi-vac XN. 3, Price £1-45 each. 10 for £13.



#### 12 WAY SUB-MINIATU RE MULTI-CORE CABLE

7-0076 copper cores each core P.V.C. insulated and of different colour. P.V.C. covered overall and approx. 3/16in, thick. Price 20p per yard.



#### LIGHT CELL

Almost zero resistant in sun-light increases to 10 K Ohms in dark or dull light, epoxy resin sealed. Size approx. Iin. dia. by \$in. thick. Bated at 500 MW, wire ended. 48p with circuit. Also ORP 12 light cell 45p.

Colled Leads. Extend to about 2 yards—as fitted to telephones etc. the first conductors of these use a tinsel wire which makes them virtually unbreakable with normal usage. 3 core 16p, 4 core 25p per lead. All less 10% in lots of 10 or more.

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PACK
Designed to operate transistor sets and amplifers. Adjustable output 6v., 9v., 12 volts for up to 500mA (class B working). Takes the place of any of the following batteries: PP1, PP3, PP4, PP6, PP7, PP9, and others. Kit comprises: main transformer rectifier, smoothing and load resistor condensers and instructions. Real snip at only 41 plus 20p poetage.



#### GOOD COMPANION

We can now offer these again in modular version using Mullard AF & IF Modules and Radiomobile Permeability Tuner. Shouldn't take more than an evening to make. Cabinet size approx. 11' wide × 8' high × 3' deep. Complete assembly instructions—24.75 plus 20p post & ins.

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Easiest way to fault find—traces signal from aerial to speaker—when signal stops you've found the fault. Use it on Radio. TV, amplifier, anything—complete kit comprises two special transistors and all parts including probe tube and crystal earpiece. \$2—twin stetho-set instead of earpiece 75p extra post and ins. 200 

#### STANDARD WAFER SWITCHES

Standard size 11 wafer—silver-plated 5-amp contact, standard \$" spindle 2" long—with locking washer and nut.

No. of Poles	2 way	3 way	4 way	5 way	6 way	8 way	9 way	10way	12way
1 pole	40p	40p	40p	40p	40p	40p	40p	40p	40p
2 poles	40p	40p	40p	40p	40p	40p	40p	70p	70p
3 poles	40p	40p	40p	40p	70p	70p	70p	95p	950
4 poles	40p	40p	40p	70p	70p	70p	70p	£1 .20	41.20
5 poles	40p	40p	70p	70p	95p	95p	95p	\$1.45	21-45
6 poles	40p	70p	70p	70p	95p	95p	95p		£1 ·70
7 poles	70p	70p	70p	95p	£1 ·20	£1 .20	£1 .20	\$1.95	\$1.95
8 poles	70p	70p	70p	95p	£1 -20	£1 ·20	£1 ·20	£2 ·20	£2 ·20
9 poles	70p	70p	95p	95p	£1 ·45	£1 ·45	£1 ·45	£2 ·45	£2 ·45
10 poles	70p	70p	95p	£1 ·20	£1 ·45	£1 ·45	£1 ·45	£2 ·70	£2 · 70
11 poles	70p	95p	95p	£1 ·20	£1 ·70	\$1.70	£1 ·70	£2 ·95	£2·95
12 poles	70p	95p	95p	£1 ·20	£1 ·70	£1·70	£1 -70	\$8 .20	£8 ·20

#### THYRISTOR LIGHT DIMMER

For any lamp up to 200 watt. Mounted on switch plate to fit in place of standard switch. Virtually no radio interferences. Price \$2.50 plus 20p post and insurance.



#### MULLARD AUDIO AMPLIFIER MODULE Uses 4 transistors, and has an output of 500mW into 8 ohms speakers. Input suitable for crystal mic. or pick-up 9V battery operated. Size 2in long ×1½in wide × lin high. SPECIAL SNIP PRICE 85p each. 10 for 25-90.

#### THIS MONTH'S SNIP .



#### REPEATING TIME SWITCH

REPEATING TIME SWITCH

1 or 2 on/offs per 24 hours. Repeats until reprogrammed. Switches up to 15 amp. Switching
time completely adjustable through 24 hours.
Precision made with 24 hour dial. Miniature—
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# HORSTMANN "TIME & SET" SWITCH (A30 Amp Switch.) Just the thing if you want to come home to a warm house without it costing you a fortune. You can delay the switch on time of your electric fires, etc. up to 14 hours from setting time or you can use the switch to give a loost on period of up or 3 hours. Equally suitable to a loost on period of up to 3 hours. Equally suitable to Special snip price \$1.40 Fort and ins. 23p.



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HONEYWELL THERMOSTAT
Made by Honeywell for normal air temperatures
40°-90°F (5-29°C). This is a precision instrument with
a differential which can be adjusted to better than
1-5°F. A mercury switch breaks on temp, rise—the
witch is operated by a colled bi-metal element and
adjustable heater is incorporated for heat anticipation.
Elegantly styled and encased in an ivory plastic case
with detting scale below-size approx 3-8' x 3-2' x 1-4' dep—can be mounted
on conduit box or directly on wall. Price \$1.25 each or ten for \$11.25.



Could also be used to open vantilators, doors, valve, damper etc. particularly suitable for remote control. Made by Satchwell. Essentially a reversible geared motor fitted with internal limit switches to stop it at the end of its travel. Size approx. 6° × 6° × 6° × 6° and weighing approx. 10 lbs. This is extremely powerful and would lift a heavy door or open a long line of ventilators. To operate this motor you put the 50 cycle supply through a change over switch. For instance a thermostat with change-over contacts could automatically regulate the temperature in a growing house, chicken hatchery etc. An indicator on the motor graduated 0–10 shows the state of open or close. Also internally fittled is a variable resistor, wires from this to a volt meter would give a remote indication of the open or close position. A very expensive motor if both direct from Satchwell, our price complete with step down Transformer is \$15.

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for money. We do not expect to be able to repeat this offer once stocks are sold. Brief description of each kit is given below and with 3 kits or more we give PREE an accurate II piece balance kit. Price of kits 40p each post paid. Special price for all 7 kits 22:50 with free balance kit.

11 piece balance kit. Price of kits 40p each post paid. Special price for all 7 kits \$2.50 with free balance kit.

KA2 Lens Kit. Eleven parts, including candle one concave lens, one convex lens, stage and alit frame, etc. Watch light rays bend as they pass through different lenses.

KA3 Water Pump Kit. Thirteen parts. Top of pump is transparent so that operating parts may be observed. Small parts are hrighly coloured to be seen easily while working. Three types of pump may be made: Lift pump, Porce Pump and Force Pump with reservoir and nozzle.

KA4 Buszer Kit. Eleven parts. Transparent covers allow the operation of buzzer to be seen. Illustrates and teaches how electromagnetism with an automatic switch results in an operating buzzer. KA5—3-Pole Motor Kit. Twenty-four parts, including enamel wire, armature and pole piece, the Motor operates from 1\(\frac{1}{2}\) volt battery. Illustrates and teaches how electro-magnetism operates a motor.

KA7 Electro-Magnet Kit. Pifteen parts, includes compass. Makes two electro-magnets, one with one layer of wire and one with several layers of wire. Picks up tacks, nails and any small parts showing how magnetism works.

KA8 Current and Resistance Kit. Twenty-nine parts, including bench and light bulb. Conduct interesting and educational projects to learn the application of "OHMS LAW" and see the difference in current and resistance with different types and lengths of wire.

KA8 Beltro and educational projects to learn the application of "OHMS LAW" and see the difference in current and resistance with different types and lengths of wire.

TAPE EIEEADS

Mintature size \(\frac{1}{2}\) equare front \(\frac{1}{2}\) deep. Understand made for Truvox. Double wound, maybe

TREE HEADS
Miniature size ‡ square front × † deep. Understand made for Truvox. Double wound, maybe wired in series or parallel for high or low impedance working. Each supplied with matching crase head. 2 track 60p pair, 4 track 75p pair, Less 10% 10 or more pairs.

Kalo Morse Key busser and bell kit. 25 part kit. casy to construct, simple to operate.

Instrument Motors fitted with Gear Box. These made by Smiths Industries are as fitted into electric clocks, chart recorders etc. Motor size approx. 1? diax. 1? deep, gear box attached approx. 2° diameter × ½° thick with good length of spindle. Most motors are fitted with a ½° long × ½° diameter drive spindle. Suitable for 200/240v mains 50 c.p.s. unless marked otherwise. Following speeds available:—8 revs per min. 20 revs per hour, 6 revs per mor. 16 revs per min. 20 revs per hour, 6 revs per doy. All £1 each or 10 for £9.

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2 Amp Switched Sockets. Oblong, brown bakelite

tiny ball.

2 Amp Switched Sockets. Oblong, brown bakelite surface mounting—2 pin Standard domestic type. 10p each or 10 for 90p. Surface Switches. 5 amp British make. Brown bakelite—oblong—1 way 10p each, 2 way 15p

bakelite—oblong—1 way 1vp each, a may averach.

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Miniature Tubes. These are approx. 1' diameter and need miniature bi-pin end connectors. 3 and need miniature bi-pin end connectors. 3 Acts available:—9' 6 watt, 12' 8 watt, 21' 13 watt Acts see Sech. Less 10'% on 10 or more colors and the second control of the second co

10 for \$2.95.

Wet Amplifier Module, Made by Mullard Ref. No. EP9000, Part of the Unilex system. This has an output of 4 watt speech and music into a 12-15 ohm speaker. A nowerful amplifier with a thousand uses—completely encased. Site approx. 3½ × 2½ × 1½. Screw down input and output terminals. Price \$1.45 each or 10 for \$13.05. Pre-Amplifier Module. 2 channel for Stereo. Input sensitivity 320mV. Part of the Mullard Unilex system and completely encased. Size 4′× 4″× 4″× 1″. Screw down input and output terminals. Price \$1.80 each or 10 for \$16.20.

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100m A



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50μA \$8·10 50-0-50μA \$2·60	10V. D.C \$2.00	þ
50-0-50µA #2-60	20V. D.C 42-00	ì

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100μA \$2.60	50V. D.C 42.00
100-0-100µA 42-50	300V. D.C. 22.00
500µA #2-80	15 V. A.C 42-10
1mA #2-00	300 V. A.C 42 10
5mA £2-00	8 Meter 1mA 42-10
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50μA £8-87	10V. D.C #2-20
50-0-50µA . #2-75	20V. D.C 82-20
100μA <b>82·75</b>	50V. D.C 42-20
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20 amp #2-20	5 amp. A.C. #2-20
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#### Two MP 28P 1 91/29in source feorie

-37	exitt. Biguare fronts.
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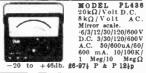
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50, 250, 500, 1,000V
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10, 100, 500mA, 2-5, 10
K. 10K. 100K. 100 MEG.

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2G374 20p 2N3569 25p 28501 2G381 22p 2N3570 125p 28502 2N388A 49p 2N3572 97p 28503	35p BC135 12p BFX85 30p NKT243 62p 27p BC136 15p BFX86 25p NKT244 17p	CA3018 84p FJH241 25p 8N7453 20p CA3018A FJH251 25p 8N7454 20p 110p FJJ101 50p 8N7460 20p	2D21 35p 30FL14 95p EZ41 50p 3Q4 50p 30L15 85p EZ80 27p
2N404 20p 2N3605 27p 3N83 2N696 15p 2N3606 27p 3N128	40p BC137 15p BFX87 25p NKT245 20p 70p BC138 20p BFX88 20p NKT261 20p	CA3019 84p FJJ111 50p 8N7472 30p CA3020 126p FJJ121 60p 8N7473 40p	384 35p 30L17 80p EZ81 29p 3V4 48p 30P12 80p GZ32 48p
2N697 15p 2N3607 22p 3N140 2N698 25p 2N3638 18p 3N141	77p BC140 35p BFX89 62p NKT262 30p 72p BC141 35p BFX93A 70p NKT264 20p 55n BC147 10p BFY11 42p NKT271 20p	CA3020A FJJ131 80p 8N7474 40p 160p FJJ141 125p 8N7475 45p	5R4 75p 30P19 85p GZ34 60p 5U4 35p 30PL1 75p KT66 22-05
2N699 30p 2N3638A 20p 3N142 2N706 10p 2N3641 18p 3N143 2N706A 12p 2N3642 18p 3N152	55p BC147 10p BFY18 25p NKT262 20p 87p BC149 12p BFY19 25p NKT274 20p	CA3021 156p FJJ181 75p 8N7476 45p CA3022 130p FJJ191 65p 8N7483 87p	5V4 45p 30PL13 93p KT88 22·00 5V3 40p 30PL14 90p MU14 75p 5Z4G 40p 35L6 50p PABC80 40p
2N706A 12p 2N3642 18p 3N152 2N708 15p 2N3643 20p 40050 2N709 62p 2N3644 25p 40250	55p BC152 17p BFY21 42p NKT275 20p 50p BC153 20p BFY24 45p NKT278 25p	CA3023 128p FJJ211 125p 8N7486 33p CA3026 100p FJJ251 125p 8N7490 87p CA3028A 74p FJL101 125p 8N7492 87p	5Z4G 40p 35L6 50p PABC80 40p 6/30L2 80p 35W4 35p PC86 60p 6AC7 40p 35Z4 35p PC88 60p
2N718 25p 2N3645 25p 40251 2N718A 30p 2N3691 15p 40309	32p BC154 20p BFY29 40p NKT281 27p 32p BC157 15p BFY30 40p NKT401 87p 45p BC158 11p BFY41 50p NKT402 90p	CA3028B FJY101 25p SN7493 87p 1C12 £1-80 SN7495 87p	6AG7 40p 35Z5 50p PC97 45p 6AK5 35p 50B5 50p PC900 48p
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2N914 17p 2N3694 18p 40312 2N916 17p 2N3702 10p 40314 2N918 30p 2N3703 10p 40315	37p BC167 11p BFY51 20p NKT405 75p 37p BC168B 10p BFY52 20p NKT406 62p	165p L923 40p SN74153 CA3030 137p LM380 122p 135p	6AM6 30p 85A2 50p PCC88 50p 6AQ5 38p 807 50p PCC89 50p 6A86 40p 1625 50p PCC189 55p
2N929 22p 2N3704 11p 40316 2N930 20p 2N3705 10p 40317	47p BC168C 11p BFY53 15p NKT451 62p 37p BC169B 11p BFY56A 57p NKT452 62p	CA3035 122p MC724P 60p SN74154 CA3036 72p MC780P 247p 200p CA3039 82p MC788P 146p SN74160	6AT6 35p 5763 70p PCF80 30p 6AU6 25p 6146 160 PCF82 34p
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2N1304 22p 2N3714 200p 40347 2N1305 22p 2N3715 123p 40348	57p BC179 20p B8X27 47p OC16 50p 52p BC182 10p B8X28 32p OC19 37p 40p BC182L 10p B8X60 82p OC20 75p	CA3048 204p MC1305P 8N74192 CA3049 160p 386p 175p	6BR8 70p DK92 55p PCF808 75p 6BW6 85p DK96 50p PCL82 35p
2N1306 25p 2N3716 130p 40360 2N1307 25p 2N3773 240p 40361 2N1308 25p 2N3791 206p 40362	40p BC183 9p BSX61 62p OC22 50p 50p BC183L 9p BSX76 15p OC23 60p	CA3050 185p MC838P 8N74193 175p	6BW7 80p DL92 35p PCL83 65p 6BZ6 40p DL94 48p PCL84 45p 6C4 33p DL96 45p PCL85 40p
2N1309 25p 2N3819 34p 40370 2N1507 17p 2N3820 55p 40406	32p BC184 11p B8X77 20p OC24 60p 57p BC184L 11p B8X78 25p OC25 40p	CA3053 46p 345p 162p	6CD6 125p DM70 40p PCL86 45p 6CL6 50p DY86 32p PFL200 65p
2N1613 20p 2N3823 50p 40407 2N1631 35p 2N3854 27p 40408	40p BC186 25p B8Y24 15p OC26 25p 52p BC187 27p B8Y25 15p OC28 60p 55p BC212L 12p B8Y26 17p OC29 60p	CA3055 240p 461p 425p CA3059 165p MC1709CG TAA243 150p	6CW4 65p DY87 33p PL36 55p 6F1 62p E88CC 100p PL81 50p
2N1632 30p 2N3854A 27p 40409 2N1637 80p 2N3855 27p 40410 2N1638 27p 2N3855A 30p 40412	62p BC213L 12p BSY27 15p OC35 50p 50p BC214L 15p BSY28 17p OC36 60p	CA3064 120p FCH101 85p MFC4000P TAA293 97p FCH111 105p TAA300 175p	6F6G 35p E180F 100p PL82 45p 6F13 45p EABC80 35p PL83 45p 6F14 70p EAF42 35p PL84 40p
2N1639 27p 2N3856 30p 40467 A 2N1701 169p 2N3856A 35p 40468 A	57p BCY10 27p BSY29 17p OC41 22p 35p BCY30 27p BSY32 25p OC42 25p	FCH111 105p SN7400 20p TAA310 125p FCH131 50p SN7401 20p TAA320 72p	6F15 65p EB91 20p PL500 75p 6F18 50p EBC41 55p PL504 80p
2N1711 24p 2N3858 25p 40528 2N1889 32p 2N3858A 30p 40600	72p BCY31 30p BSY36 25p OC44 15p 57p BCY32 50p BSY37 25p OC45 12p 50p BCY33 25p BSY38 20p OC46 15p	FCH141 105p SN7402 20p TAA435 147p	6F23 85p EBC81 30p PY32 55p 6H6 17p EBF80 40p PY33 63p
2N1893 37p 2N3859 27p 40603 2N2147 72p 2N3859A 32p AC107 2N2160 57p 2N3860 30p AC126	30p BCY34 30p B8Y39 22p OC70 15p	FCH181 105p SN7404 20p TAA521 132p	6J4 50p EBF83 40p PY80 40p 6J5 25p EBF89 32p PY81 30p 6J5GT 30p EBL21 60p PY82 35p
2N2193 40p 2N3866 150p AC127 2N2193A 42p 2N3877 40p AC128	24p BCY39 60p BSY51 32p OC72 12p 20p BCY40 50p BSY52 32p OC73 30p	FCH201 180p SN7408 20p TAA811 445p	6J6 20p EC86 60p PY83 38p 6J7 45p EC88 60p PY88 40p
2N2194 27p 2N3877A 40p AC151 2N2194A 30p 2N3900 37p AC152	22p BCY42 15p BBY54 40p OC75 22p	FCH221 130p SN7410 20p TAD100 150p FCH231 150p SN7411 23p TAD110 150p	6K8G 40p ECC40 85p PY800 40p 6L6GT 45p ECC84 30p PY801 50p
2N2217 25p 2N3900 A 40p AC154 2N2218 20p 2N3901 97p AC176 2N2219 20p 2N3903 20p AC187	20p BCY54 32p B8Y79 45p OC77 30p 25p BCY58 22p B8Y90 57p OC78 20p	FCJ101 160p 8N7412 48p 8L403D 15 p FCJ111 150p 8N7413 30p 8L702C 147p FCJ121 275p TE7416 84p UA702A 280p	6LD20 50p ECC85 40p U25 80p 6Q7 40p ECC88 40p U26 80p 6SA7 40p ECF80 35p U50 40p
2N2220 25p 2N3904 25p AC188 2N2221 25p 2N3905 80p ACY1	7 25p BCY59 22p BSY95A 12p OCS1 20p 7 27p BCY60 97p C424 15p OCS1D 20p	FCJ131 275p SN7417 84p UA702U 77p	68G7 40p ECF82 35p U52 35p 68J7 40p ECF86 65p U191 75p
2N2222 20p 2N3906 25p ACY1 2N2222A 25p 2N4058 12p ACY1 2N2297 30p 2N4059 10p ACY2	9 24p BCY71 20p GET102 30p OC82D 15p	FCJ201 100p 8N7423 51p UA709C 45p FCJ211 275p 8N7427 48p UA710C 125p	68K7 40p ECH21 57p U281 40p 68L7 35p ECH35 100p U282 40p 68N7 35p ECH42 75p U301 40p
2N2297 30p 2N4089 10p ACY2 2N2368 15p 2N4060 12p ACY2 2N2369 15p 2N4061 12p ACY2	1 20p BCY78 30p GET114 20p OC84 25p	FCK101 430p SN7428 80p UA716 187p FCL101 230p SN7430 20p UA723C 100p FCY101 102p SN7432 48p UA730C 160p	68N7 35p ECH42 75p U301 40p 68Q7 40p ECH81 30p U801 £1-80 6U4 6bp ECH83 45p UABC80 40p
2N2369A 15p 2N4062 12p ACY2 2N2410 42p 2N4244 47p ACY3	8 17p BCZ10 27p GET120 25p OC140 32p 9 47p BCZ11 40p GET873 12p OC170 25p	FJH101 25p 8N7433 80p UA741C 80p	6V6G 25p ECL80 45p UAF42 55p 6V6GT 32p ECL82 35p UBC41 50p
2N2483 27p 2N4248 15p ACY4 2N2484 32p 2N4249 15p ACY4 2N2539 22p 2N250 18p ACY4	1 15p BD116 112p GET887 20p OC200 40p	BRIDGE 50 PIV 4A 40p RECTIFIERS 100 PIV 4A 50p 200 PIV 4A 55p	6X4 35p ECL83 70p UBC81 40p 6X5G 30p ECL86 40p UBF80 40p
2N2540 22p 2N4254 42p AD14 2N2613 35p 2N4255 42p AD14	0 47p BD123 80p GET890 22p OC202 75p 9 47p BD124 80p GET896 22p OC203 40p	ENCAPSULATED 400 PIV 4A 65p 600 PIV 4A 70p	6X5GT 40p EF37A 120p UBF89 35p 10C2 50p EF39 50p UCC84 49p 10F1 75p EF40 50p UCC85 40p
2N2614 30p 2M4284 17p AD15 2N2646 40p 2N4285 17p AD16	0 62p BD131 75p GET897 22p OC204 40p 1 35p BD132 80p GET898 22p OC205 75p	600 PIV 1A 50p 50 PIV 6A 45p 50 PIV 2A 45p 100 PIV 6A 55p	10P13 60p EF41 65p UCF80 55p 10P14 41-10 EF42 70p UCH21 60p
2N2711 25p 2N4286 17p AD16 2N2712 25p 2N4287 17p AF10 2N2713 27p 2N4288 15p AF11	9 45p BDY20 105p MAT101 25p OC207 75p	100 PIV 2A 50p 200 PIV 6A 65p 200 PIV 2A 55p 400 PIV 6A 75p 400 PIV 2A 60p 600 PIV 6A 85p	12AT6 30p EF80 25p UCH42 70p 12AT7 30p EF85 35p UCH81 40p
2N2714 80p 2N4289 17p AF11 2N2904 20p 2N4290 12p AF11	5 25p BD¥62 100p MAT121 25p ORP12 50p 6 25p BF115 25p MJ400 107p ORP60 40p	SULICON RECTIFIERS	12AU7 30p EF86 30p UCL82 35p 12AX7 30p EF89 28p UCL83 60p 12AV6 40p EF91 30p UF41 60p
2N2904A 25p 2N4291 15p AF11 2N2905 25p 2N4292 15p AF11	7 20p BF117 47p M3420 80p ORF61 42p 8 60p BF152 28p MJ421 80p P346A 22p	MINIATURE WIRE ENDED PLASTIC SERIES IN PL CL 1 AMP 1.5 AMP 8 AMP	12BA6 40p EF92 35p UF80 35p 12BE6 40p EF183 35p UF85 40p
2N2905A 20p 2N4294 17p AF12 2N2906 20p 2N4303 47p AF12 2N2906A 25p 2N4964 15p AF12	4 22p BF158 15p MJ440 95p ST141 20p 5 19p BF159 35p MJ480 97p T1834 62p	4001 50PIV 7p 8p 19p 4002 100PIV 7p 9p 20p	12BH7 45p EF184 85p UF89 40p 19AQ5 85p EH90 40p UL41 65p
2N2907 28p 2N4965 18p AF12 2N2923 15p 2N5027 52p AF12	6 19p BF163 35p MJ481 125p TIS43 40p 7 16p BF167 18p MJ490 100p TIS44 10p	4003 200PIV 8p 10p 22p 4004 400PIV 8p 10p 25p 4005 600PIV 10p 12p 28p	20F2 65p EL41 60p UY41 48p
2N2924 15p 2N5028 57p AF13 2N2925 15p 2N5029 47p AF17	8 42p BF173 19p MJE340 50p 11546 11p	4006 800 PIV 12p 15p 27p 4007 1000 PIV 15p 16p 80p	20P1 50p EL81 55p VR105/30 38p 20P3 60p EL84 25p VR150/30 35p
2N2926G 10p 2N5030 42p AF17 2N2926O 10p 2N5172 12p AF18 2N2926Y 10p 2N5174 52p AF18	0 50p BF178 25p MJE371 80p TIS48 12p	50 + less 15 % 100 + less 20 % SILICON RECTIFIERS	20P4 21.10 EL85 43p 20P5 21.20 EL91 35p Add 12p in 2
2N3011 20p 2N5175 52p AF18 2N3014 32p 2N5176 45p AF23	66 39p BF180 35p MJE521 70p T1850 12p 19 30p BF181 32p MPF102 42p T1851 10p	6A 10A 17-5A 35A	25L6 50p EL96 35p for postage DIODES & RECTIFIERS
2N3053 18p 2N5232A 30p AF23 2N3054 48p 2N5245 45p AF28	79 47p BF182 30p MFF103 35p 11852 11p 30 47p BF184 20p MFF104 87p T1853 22p	100PIV — 45p 50p £1.22 200PIV 25p 50p 55p £1.42	1N34A 10p BA154 12p GJ7M 57P 1N914 7p BAX13 12p OA5 17p
2N3056 60p 2N5246 42p AFZ 2N3133 30p 2N5249 67p ASY 2N3134 15p 2N5265 325p ASY	26 25p BF194 16p MP83638 32p XC141 35p 27 30p BF195 15p NKT124 42p ZTX107 15p	400 PIV 30p 55p 62p £1.77 600 PIV 32p 60p 72p £2.12 800 PIV 35p 75p 87p £2.47	AA119 7p BAY31 7p OA10 22p
2N3135 25p 2N5305 37p ASY 2N3136 25p 2N5306 40p ASY	28 24p BF196 15p NKT125 27p ZTX108 12p 29 27p BF197 15p NKT126 27p ZTX109 15p	1000PIV 40p 85p £1.05 £2.77 50 + less 15% 100 + less 20%	AAZ13 10p BY100 15p 0A47 8p AAZ15 10p BY103 22p 0A70 7p
2N3390 25p 2N5307 37p ASY 2N3391 20p 2N5308 37p ASY	50 25p BF198 15p NKT128 27p ZTX300 12p	ZENER DIODES	BA100 15p BY122 37p OA73 10p BA102 30p BY124 15p OA79 7p
2N3391A 30p 2N5309 62p ASY 2N3392 17p 2N5310 42p ASY 2N3393 15p 2N5354 27p ASY	67 45p BF225 19p NKT210 30p ZTX303 20p 86 32p BF237 22p NKT211 30p ZTX304 25p	3.3.33 V 2.4—100 3.9—100V 10n each 25p each 40p each	BA111 27p BY127 15p OA85 7p
2N3394 15p 2N5355 27p ASZ 2N3402 22p 2N5356 32p AUY	21 51p BF238 22p NKT212 30p ZTX500 15p 10 150p BF244 23p NKT213 30p ZTX501 15p	25 + less 15% 100 + less 20% TRANSISTOR DISCOUNTS:- 12 + 10%;	BA115 7p BY210 35p OA91 7p BA141 32p BYZ11 30p OA95 7p
2N3403 22p 2N5365 47p BC16 2N3404 32p 2N5366 32p BC16	10p BFW81 47p NKT214 20p ZTX502 20p 08 10p BFW87 25p NKT215 22p ZTX503 17p 00 10p BFW88 23p NKT216 35p ZTX504 40p	25 + 15%; 100 + 20% any one type. Post- age on all Semi Conductors 7p extra.	BA142 32p BYZ12 30p OA200 10p BA144 12p BYZ13 25p OA202 10p
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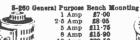
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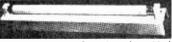
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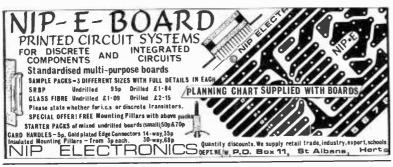
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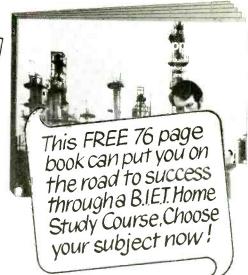
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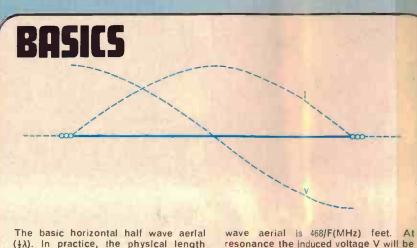
## **Aerial Data Chart**

# PRACTICAL

# CHART

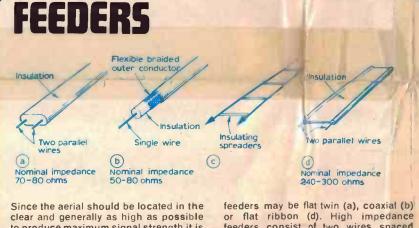


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 $(\frac{1}{2}\lambda)$ . In practice, the physical length required for resonance is reduced by a factor of  $0.95 (0.95 \times \frac{1}{2} \lambda)$  due to the effect of insulators and nearby objects. A simple formula for the practical half

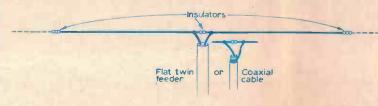
resonance the induced voltage V will be maximum at the ends of the aerial (high impedance) while the current I will be maximum at the centre



to produce maximum signal strength it is necessary to use a feeder to connect the aerial to the receiver. Low Impedance

feeders may be flat twin (a), coaxial (b) or flat ribbon (d). High impedance feeders consist of two wires spaced apart by insulators every foot or so (c).

## HALF WAVE DIPOLE

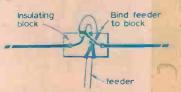


As the impedance at the centre of a half wave aerial is approximately 70 ohms feeders (a) or (b) will provide a good impedance match to the aerial ensuring maximum signal transference. The

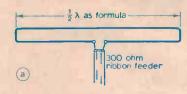
aerial, length calculated from the formula given, is cut at the centre and an insulaton inserted, the wires of the feeder being connected either side of the insulator

## CONSTRUCTION

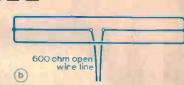
A practical method of feeding the aerial with low impedance feeder. The loop in the top of the feeder is essential to prevent the ingress of rain and dirt. The end of coaxial cable can be sealed with plastic insulating tape or compound.



## IED DIPOLE



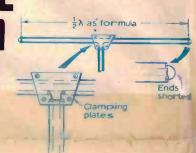
The folded dipole (a) will transform the input impedance by a factor of  $2^2$  or  $4 \times 70 = 280$  ohms so that it can be fed with a flat ribbon feeder of 300 ohms impedance, provided the wires forming



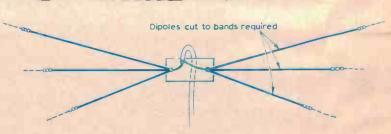
the folded dipole are the same diameter. If a three fold dipole is used the input impedance will be 70 x  $3^2 = 630$  ohms which will provide a good match to an open line feeder.

# **FOLDED DIPOLE**

practical folded dipole using 300 ohm ribbon feeder for both the aerial and the feeder. One conductor only of the aerial is cut at the centre and the feeder inserted and the joints soldered. The junction should be clamped between pleces of insulating material and properly waterproofed.



## ULTIBAND DIPOLE



If dipoles are required for optimum performance on several frequency bands they can be connected in parallel at their centres, and fed with a common feeder thus providing multiband facilities in a minimum of space. The ends of the dipoles may be tied off to any convenient

supports and the dipoles need not all be In the same plane. Note that a dipole cut for, say, the 7MHz amateur band, will be three half waves on the 21 MHz amateur band thus eliminating the need for a separate aerial for that band.

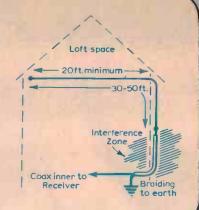
The table gives the length of a half wave aerial in the various HF amateur and broadcast bands.

Amateur
Band Length
160m 256ft 80m 128ft 40m 66ft 20m 33ft 15m 22ft 10m 16ft

A long length of copper wire, with one end connected to the receiver, is probably the most commonly used aerial. This is often fitted onto a picture rail and even gulte a small room will enable a 40ft. length to be used. One convenient form of aerial can be obtained by using the coaxial cable of a TV aerial, the outer braiding being connected to the aerial socket of the receiver. Important! disconnect the TV aerial from the TV set before using it in this form. Probably the best and only true long wire aerial is the Beverldge. This is used by many major monitoring stations. It comprises a straight wire about a mile long mounted on short poles over the ground. One end goes to the receiver and the other to earth via a resistor. It is very directional and provides excellent reception but there are few who have sufficiently long back gardens to accommodate this one!

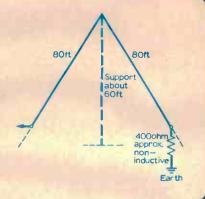
## INVERTED L

A simple, general purpose aerial which, when connected to an ATU, will give good results. The length should be between 30ft and 50ft. of which the horizontal part should be at least 20ft. A wire across the loft and running down the outside of the house is a simple method of arranging this. In areas of high local interference the vertical portion can be screened using coaxial cable, the outer braid being taken to the earth terminal on the receiver and thence to an outside earth.



## **INVERTED U**

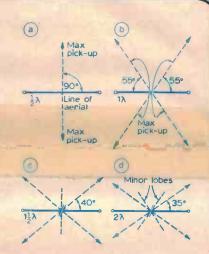
With only a single support required this form of "Inverted Vee" can be very effective. The 400 ohm resistor renders the system aperiodic i.e. not resonant at any particular frequency. It will be useful over most of the HF bands favouring signals in the plane of the aerial.



## DIRECTIVITY

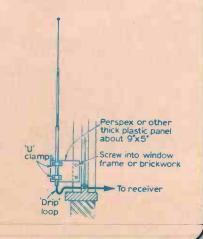
Signal pick-up of a half wave aerial is maximum at right angles to the line of the wire (a). If the wire is one wavelength long maximum pick-up is from four directions (b). By choosing the right length of aerial and adjusting its orientation the maximum pick-up lobes can be made to cover all the land areas of the world.

bonger aerials result in the appearance of minor lobes (c) and (d) which reduce directivity and improve all round coverage. With an aerial many wavelengths long maximum reception is along the line of the wire.



## WHIP TYPES

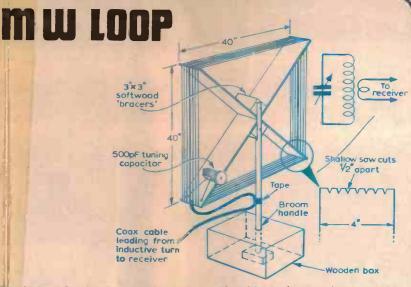
Whip aerials come in a varlety of forms, many belng ex-Government and very cheap. They can be telescopic, lengths of rod which screw into each other or several tubular sections with a single wire running through them which holds the sections rigid when tightened. In certain locations a whip aerial is about the only practical type since it can simply be mounted outside a window, as shown. The whip should be as long as possible, but very tall ones present mounting problems due to wind pressure. Generally a whip aerial will be non-resonant on the HF bands and should, ideally, be connected to an ATU. If not it may be connected to the aerial terminal directly or via a varlable capacitor.



## TV AERIALS

It is hardly worth making a TV aerial since commercial ones generally cost much less than the materials would cost to buy. Band I aerials (Channels 1-5) are nearly always cut for an individual channel and take the form of a simple dipole or an H or X arrangement. Band III aerials are available for individual channels, semi-broad-band encompassing three channels or broad-band (Channels 6-13). These aerials are generally more elaborate than Band I types due to the poorer propagation at these frequencies and incorporate one or more directors. The UHF frequencies

(Channels 21-68) are divided into groups for aerial purposes: A, B, C, D and E and the correct type must be used in a particular area. Broadband UHF aerials, usually log-periodic, are also available but their gain is rather less than with conventional types. UHF aerials are much smaller than VHF types and usually incorporate from 3 to 19 directors plus a reflector in order to increase the gain. The dimensions are falrly critical and this, together with the low cost of the commercial product, makes home construction an unrealistic proposition.



frequencies between 500kHz and 2MHz the loop aerial takes a lot of the taking. It consists of 7 turns of wire (5 of 6 turns for higher frequencies) around a wooden framework as illustrated. The ends of the wire connect to a 500pF tuning capacitor. A second wire, wound around the centre turn connects to a coax cable which goes to the aerial and earth sockets on the receiver or preferably to a balanced input.

The loop forms a tuned circuit in conjunction with the capacitor with the inductive loop providing a low impedance feed to the receiver. The capacitor has to be tuned for each frequency and the selectivity is excellent. The loop is highly directional and by rotating it, interfering stations can be virtually eliminated. The tuning is very sharp and it is advantageous to fit either a slow

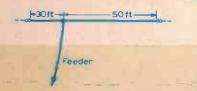
motion drive to the capacitor or to wire a small value variable trimmer in parallel with it (10pF to 20pF).

The gain is not as high as that of a long wire aerial but this is more than outweighed by the much improved signal-to-noise ratio and the directional characteristics. The direction of a station can be determined within a few degrees by nulling it out to take its bearing. The broom-handle can be fitted into a box as shown with the bottom fitting into a recessed slot to prevent it slipping.

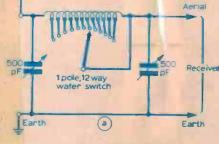
The main frame can be made of 6mm (½In.) plywood or softwood. The wires should be wound very tight and should be kept that way (under tension the wire tends to stretch slightly). The softwood blocks merely act as bracers and as supports for the broom handle.

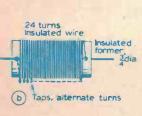
## WINDOM

A useful general coverage aerial to the HF bands is the Windom which was a single wire feeder tapped on the horizontal wire. An aerial length of out 80 feet will work especially well (The 13, 25 and 49 metre bands.



## **AERIAL TUNING UNIT**





For best results an end fed wire aerial or rod aerial should be matched to the receiver input circuit with an Aerial Tuning Unit (a). The inductor (b) is wound making a loop every other turn, the loops then being soldered to the switch tags. Fit each tuning capacitor

with a calibrated knob or dial and number the switch positions. Adjust the capacitors and switch position for maximum signal strength noting that the three adjustments are very much interdependent. Log dial and switch readings for future reference.

# FM—BAND II Twisted wire To receiver agerial socket Direction of transmitter To receiver agerial socket

The signal strength of FM broadcasting stations is quite high over most of the country and elaborate aerials are rarely necessary. Many receivers are now fitted with telescopic aerials for FM but these will be poor in some areas. A very simple FM aerial can be made from ordinary twisted bell-wire, as shown. One end should be unwound and pinned along a picture rail to form a dipole. The dimensions given are for 95MHz. If within range of a BBC local radio

station, the dipole should be modified to resonate at the frequency of this station as the signal strength is likely to be comparatively low. Length of each leg in inches = 2808 / Frequency in MHz. For DX FM reception or in difficult areas, more elaborate roof or loft mounted arrays should be used. Dimensions of a typical array are given although these aerials usually are cheaper to buy ready made.