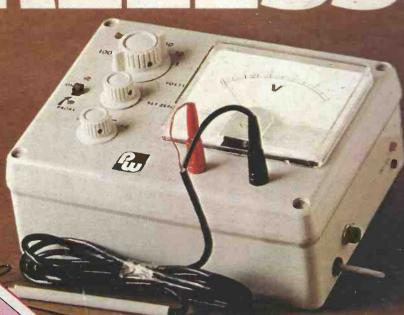
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#### **News and Views** EDITORIAL-Perseverance 484 485 NEWS...NEWS...NEWS... 494 PRACTICAL WIRELESS-Pre-view of our next issue 511 READERS PCB SERVICE—Prices and details of the PCBs available 514 KINDLY NOTE—Further information on the Inductor for the Atomic Time Receiver, August 1977 518 519 ON THE AIR—Amateur Bands......Eric Dowdeswell G4AR SW Broadcast Bands ... ... Charles Molloy G8BUS MW Broadcast Bands ... ... Charles Molloy G8BUS VHF Bands..... Ron Ham BRS15744 For our Constructors A WIDE RANGE VOLTMETER for AC, DC and RF 486 An input impedance of 11M $\Omega$ enables this voltmeter to be used on just about any circuit without upsetting the circuit conditions. Six ranges to 1000V plus probes permits measurement of AC or DC voltages M. Tooley BA, G8CKT 490 ALL BAND SHORT WAVE CONVERTER—1 This converter can be aligned for the amateur bands or the SW broadcast bands and provides an IF output 497 RF RESONANCE INDICATOR With the aid of an external signal source this very useful indicator can be used to find the resonant frequency of a tuned circuit or to select values of inductance and capacitance for a given frequency D. H. E. King G3TQN 505 THE PW 'JUBILEE' ELECTRONIC ORGAN-3 Details this month on the operation and adjustment of the melody, drum and rhythm, and accompaniment 512 DESIGN YOUR OWN PROJECTS-3 This Car Courtesy Light project will give you another 15 seconds of light inside your car when the door **General Interest** 501 SO YOU WANT TO PASS THE R.A.E?-3 Ohm's Law is translated into some practical transistor circuits and the very important principles of magnetism are discussed in this part...... John Thornton Lawrence GW3JGA and Ken McCoy GW8CMY IC OF THE MONTH 516 The ZN1304E is used in timing circuits to provide accurate delays of up to one year! Several circuits are shown

24 PAGE 'COMPONENT SOURCE DIRECTORY'

for different applications of the IC.

Free This Month!

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AMBIT announce a new addition to the catalogue - information on TOKO's new ceramic ladder filters, 2.4kHz SSB filters etc. HF coils, new flat faced low cost panel meters. Catalogue 45p.

#### DETECKNOWLEDGEY

Metal locator principles and practise, including some of the facts that the manufacturers of £100+ metal locators wouldn't like you to know !! £1.00 The Bionic Ferret 4000 - A little detector technology of our own. The VCO based metal locator for the electronics constructor, including platsic moldings for housings of electronics and search coil, tubing etc. Can be set up using just a test meter. 'All in' price £34.26 inc PP and 8% VAT.

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TBA120	FM IF	0.75	BF274	.7GHz	0.18	EF5800 6 varicap FM £14.00
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SN76660N	FM IF	0.75	ZTX213	30v/.3W	0.16	8319 4varicap mos mix £11.45
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HA1197	AM radio		ZTX551	60v/1W	0.18	7020 cer. filt. fm if £6.95
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uA753	FM gain	1.80	BD535	60v/50W		nbfm if filter/amp/detector
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CA3130T	mos oa	0.85*	BA121	••	0.30	940k as above with tca 940E
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LM3900	op amps	0.68*	BB105	uhf varic		NB All our audio ICs are
7805uc	5v/1A	1.55*	mvam2	dual, am	1.48	"short circuit" protected as
tda1412	12v/.6A	0.95*	mvam115		1.05	defined by the manufacturer
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NE561B	hf pll	3.50*	7mm IFs	for RC	0.33	33/42pF swing 7.5 0.26
NE565k	If pll	2.50*	CFS10.7		0.50	60pF swing 10mm dia 0.24
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11C90	650MHz	14.001	BBR3132	6nole fm	2.25	trimpots for varicaps 0.45
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ZTX108	30v/.3W	0.14	MEHT 4/	5/7 kHz	1.65	10000uF/63v 1.15
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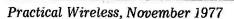
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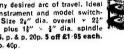
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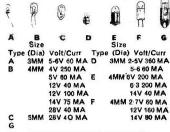


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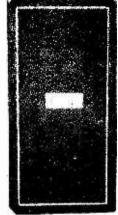
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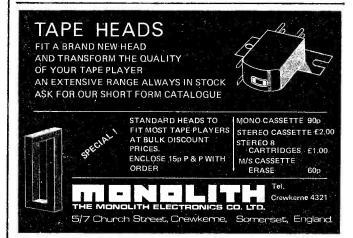
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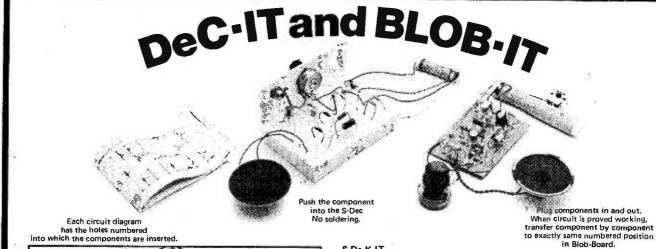
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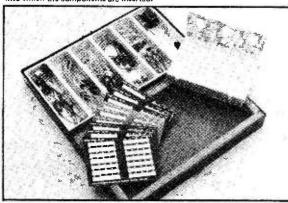
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4019 57p 4020 140p 4021 120p	4081 30 p 4082 30 p 4093 104 p	TRIACS Plastic	BRIDG RECTI- FIERS	OA91	15p 9p 9p	BSX19 20p BSX20 20p BU105 200p	2N5485 45p 2N6107 70p
4022 140p 4023 23p 4024 90p	4510 140p 4511 140p	3A 400V 85p 6A 400V 107p 6A 500V 120p	1A 50V 1A 100\		9p 9p 10p	BU108 312p MJE340 70p MJ481 175p	2N6027 60p 2N6247 200p 2N6254 140p
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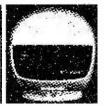
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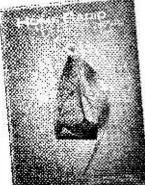
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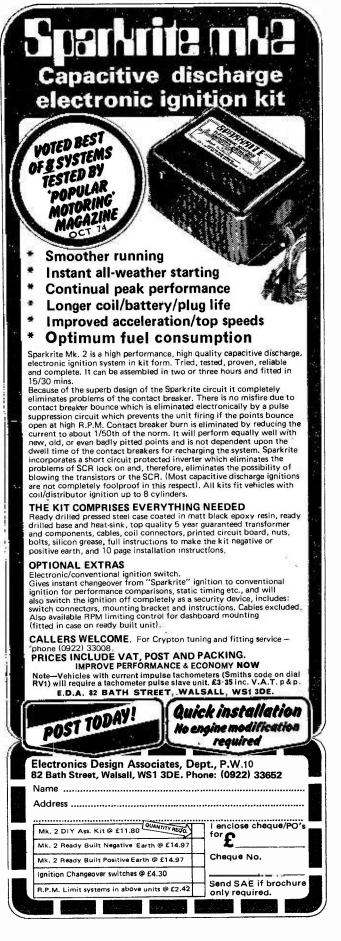
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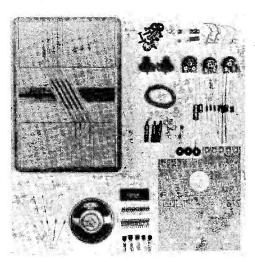
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		All	7p eacl	1	
	BLOW 1	in			
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## Perseverance

AWAY from any technicalities this month. Just the story of a PW reader's perseverance. Charlie M. is nearly 78. He was a Marconi marine operator in World War 1 and in his latter years has long cherished the idea of joining the radio amateur fraternity and talking to other folk around the world. He'd done all the swotting but a couple of problems confronted him. His wife is a chronic invalid requiring constant attention, and they live in a remote part of Wales, with but one equally lonely neighbour. How could he leave his wife and go anywhere to take the RAE and the code test?

Following up a couple of suggestions Charlie was able to get the nearest technical college, some 20 miles away, to make the necessary arrangements for him to sit the exam last May. His sole neighbour came round for a few hours and off went Charlie to college, the only candidate! The result? A "distinction" in Part 1 of the paper and a "credit" in Part 2. So far, so good, but taking the code test wasn't quite so simple!

A trip to the nearest testing centre would have meant too long away from home and his wife. He contacted the centre, at Cardiff, and eventually the Marine Radio Surveyor there telephoned Charlie to say that he would call round the next time he was in the area on duty. Eventually he turned up and "they did the necessary test on the kitchen table" A few days later a "pass" certificate arrived. Charlie writes "prompt and willing service like this, in these days of 'couldn't care less' is really most heart-warming".

A lovely story, isn't it? A GW4 call ought to be on its way very soon. Another not-so-young amateur has loaned Charlie an AR88 receiver plus a 50 watt transmitter so at long last a dream is about to be fulfilled. Charlie has been reading PW since 1952, "a valuable wireless encyclopaedia that I wouldn't part with for all the tea in China". With the present price of tea, that values PW very highly indeed!

Due to increased production costs, the cover price of your copy of *Practical Wireless* has been increased to 45p. The price for new binders has also been increased, as from the 1st October to £2·85. These price increases have been approved by the Price Commission.

#### PLEASE NOTE

We do not operate a Technical Query Service except on matters concerning constructional articles published in PW. We do not supply service sheets or information on commercial radios, TV's or electronic equipment.

All queries must be accompanied by a stamped self-addressed envelope otherwise a reply cannot be guaranteed.

## A Century of Recorded Sound

As previewed in the September issue of PW, the City of London Phonograph and Gramophone Society recently held an exhibition of early reproducers and associated items at the British Institute of Recorded Sound, Exhibition Rd., Kensington, which celebrated one hundred years of recorded sound.

1877 was in fact a year of universal significance for the sound recording industry, seeing the parallel but independent emergence of two versions of a world-shattering device-the sound reproducer, or "talking machine". Charles Cros in France and Thomas Edison in the United States had almost simultaneously arrived at the same answer to an interesting problem, and while Edison's was a practical working model, the Cros version although restricted to a set of detailed plans, was every bit as brilliantly conceived. It was largely lack of funds and his failure to convince a prospective backer which prevented Cros from seeing his machine emerge as a reality.

#### Edison v Cros

The exhibition itself naturally displayed an emphasis upon Edison's machines, although Cros was in a sense acknowledged by the inclusion of an Emile Berliner hand-cranked gramophone; it was Berliner who had eventually developed the reality from the plans Cros had deposited at the Academie Francaise in April 1877.

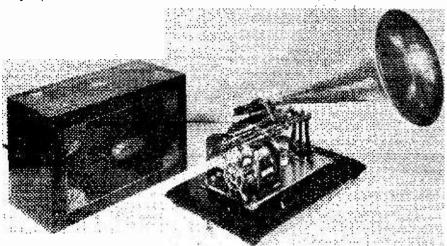
Whatever the arguments about origins, however, a stroll around this display evoked an atmosphere of warm, pre-electric nostalgia. Delicate cylinder phonographs rubbed shoulders with bluff, aristocratic console gramophones in select veneers. Splendid wooden horns balanced at the end of strange foil contraptions with worm gear drives and irresistible cranking handles peered out at an utterly changed world.

Surprisingly, in spite of their great age, most of the machines on view were still playable, in fact, at the height of its popularity, the gramophone was capable of very good reproduction, even though little scientific investigation of basic principles had accom-

panied its development. The HMV "Re-entrant" model (console gramophone of about 1930) proved very pleasant to listen to in spite of a relatively narrow audio range.

Perhaps a good deal of the interest evident at the exhibition may be dismissed as pure sentimentality, for the machines are somewhat crude by modern standards, but they do represent the beginnings of an immense extension of the range of human experience, and as such they will remain vital informational pieces of equipment. They are additionally interesting as a group of acoustic dinosaurs—they represent the visible and audible

exhibition was not restricted to the purely acoustic devices, and a selection of early "radio-gramophones" and electrically operated record players was in evidence, including the well-known Decca "Deccalian" with interchangeable heads for 78 or LP. Long-playing records were the "coming thing" in the fifties, and also included in the display was a range of earlier attempts to produce longer playing times, among which was a variable-speed type, designed to exploit the higher speeds at the perimeter of the disc, although this had the disadvantage that a complex device was needed for replay-one which pro-



One of the reproducers in the display—a Thorens phonograph circa 1905.

end of an era, their electrical counterparts proving unequally effective and competitive in the ensuing conflict.

On the other hand, they had, and still retain, real beauty; a combination of satisfying mechanical symmetry and the atavistic flesh-and-blood appeal of real wood, the voices of Melba and Caruso, and above all, an aura of magic and mystery which characterised an age of real discovery.

#### Past successes

In terms of the eventual establishment of enterprise in the reproducer field, there was plenty of evidence of the developing "names" in audio devices. Thorens, for example, now heavily committed to quality hi-fi, were represented by an early piece of acoustic precision engineering in the shape of a particularly attractive motor design for a phonograph.

The chronological span of the

duced a differential slowing towards the centre. Edison's attempts were more practical and saleable—a long player at 78rpm, which clearly necessitated a remarkably close-cut groove, a good deal closer than a modern LP cut on vinyl.

Another century on may well see an exhibition of 1977's music centres and cassette recorders, languishing in chrome and plastic bowers filled with surround sound, but it is questionable whether they will stimulate the imagination or convey as much of the character of the age as these quaint works of wood, metal and mica. They are important because they stirred up the ripples which led to a gigantic tidal wave in human affairs—the crude boxes which paved the way for the world-wide recording industry, and in so doing, opened up one of the most creative extensions of human commercial and artistic endeavour.

**Ted Parratt** 

485

## VOLIMETER

#### M.TOOLEY BA G8CKT

FOR AC.DC.RF

A reliable high-impedance DC and AC voltmeter is an invaluable asset in any enthusiast's workshop. The circuit described is simple to use, exhibits excellent linearity and has a constant input impedance of  $11 M\Omega$  on all ranges. The basic voltmeter is provided with six DC ranges from 1V to 1000V full-scale. A variety of probe designs is included in order to facilitate further DC, AC and RF measurements. The unit is portable and operates from the mains or alternatively it may be powered from an external DC supply. An automatic diode switch is included for changing over from internal to external power.

#### **Circuit Description**

A simplified circuit of the DC voltmeter is depicted in Fig. 1. This shows the basic bridge configuration formed by Tr2, Tr3, R9 and R10. A constant voltage is developed across R10, the emitter resistor of Tr3. The input voltage, less approximately 0 6V which is the base-emitter voltage drop for Tr2, is effectively developed across R9, the emitter resistor of Tr2. The difference between these two voltages produces a

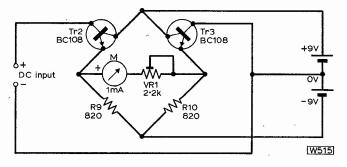


Fig. 1: Simplified circuit of the voltmeter.

### **★** specifications

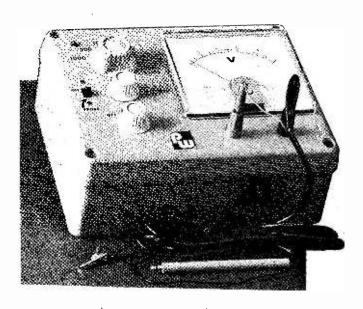
Functions: D.C. positive, DC negative,
AC (by means of suitable probe).

Ranges: 1V (full-scale DC) 180V
10V 580V
50V 1000V

Input Resistance: 11MΩ without probe or 10MΩ with 1MΩ in probe (DC).

Supply Voltage: 220/240V 50Hz
external DC 18 to 24V at 40mA.

Typical Accuracy: DC ±2% AC ±5%



current in the milliammeter, M. The calibration of the instrument is set by the variable resistor, VR1.

The voltage to be measured is applied to the potential divider formed by resistors R2 to R7, see Fig. 2. The voltage division ratio is selected by means of the Range Switch, S2. A fixed resistor, R1, is provided in the input lead. To ensure correct calibration this resistor is bypassed by means of S3 when a probe is fitted. The output from the potential divider is fed to the FET transistor, Tr1. This transistor is connected as a source follower and provides a very high input resistance and a voltage gain of very slightly less than one.

Transistors Tr2 and Tr3 operate as a balanced emitter follower pair. This symmetrical arrangement ensures good linearity and a high degree of temperature stability. The base voltage for Tr3 is fixed at approximately half the DC supply by means of the potential divider formed by R11 and R12. The circuit may be balanced by means of VR3 which sets the DC potential at the gate of Tr1 and in turn the potential at the base of Tr2.

The meter connections are reversed to facilitate positive and negative voltage measurements without the necessity of altering the input lead connections. For AC measurements the instrument is effectively used on the DC negative range and a suitable probe must be employed. The probe is designed to produce a negative DC output using a simple half-wave diode rectifier arrangement. The value of probe resistor, R, is chosen so that the instrument is calibrated for RMS AC voltages, see table.

#### Construction

The transistors, Tr1, Tr2, Tr3 and associated components are mounted on a 150 x 115mm 0·1in matrix board, Fig. 3. Components and connecting leads are located and soldered on this board by means of pressfit terminal pins. Wire links between pins are made using insulated solid wire. The completed board assembly is mounted below the lid of the plastic box and secured by means of the two meter terminals.

Resistors R2 to R6 are wired directly to the contacts of the Range Switch, S2. Resistor R1 is wired across the contacts of the Probe Switch, S3. Care should be taken to keep wiring as short and neat as possible. The mains transformer is secured to the base of the box, Fig. 4, preferably in such a way as to distribute the weight evenly over the base area of the instrument whilst ensuring adequate clearance when the lid and associated components are fitted in place. The external supply sockets are also located in the base of the box, adjacent to the fuseholder. The bridge rectifier and capacitor are fitted to the main circuit board.

#### **Probes**

Various probe designs are given in Fig. 5 together with suitable component values as given in the table. The DC probe of Fig. 5a is intended for use when DC voltage measurements are to be made in the presence of AC and RF signals. The  $1M\Omega$  probe resistor provides an extra degree of isolation for the circuit under investigation and minimises reactive loading effects. The construction of this probe is shown in Fig. 6. The

Table of components for probe designs

Probe	Figure	Component values	Useful voltage range	Useful frequency range
DC	5a	R—1MΩ 0-52% high stability metal oxide	0 to 1000V	DC only
AC low voltage	<b>56</b>	R—3·3 MΩ 2% high stability. C—1μF polyester tubular 250VDC. D—OA91	0·5 to 30∨	15Hz to 100kHz
AC medium voltage	5c	R—3·3 MΩ 2% high stability. C—1μF polyester tubular 250VDC D1, D2, D3 OA91	1-5-to 100 <b>V</b>	15Hz to 100kHz
RF	5d	R—3·3 MΩ 2% high stability. C—1nF poly- styrene 160VDC. D—OA91	0·5 to 30V	100kHz to 100MHz

probe circuit is housed in the barrel of a discarded felt-tip pen. The tip contact of the probe makes use of the body of a 3.5mm jack plug which is inserted in the barrel of the felt-tip pen and held in place by means of epoxy adhesive. Only the tip electrical

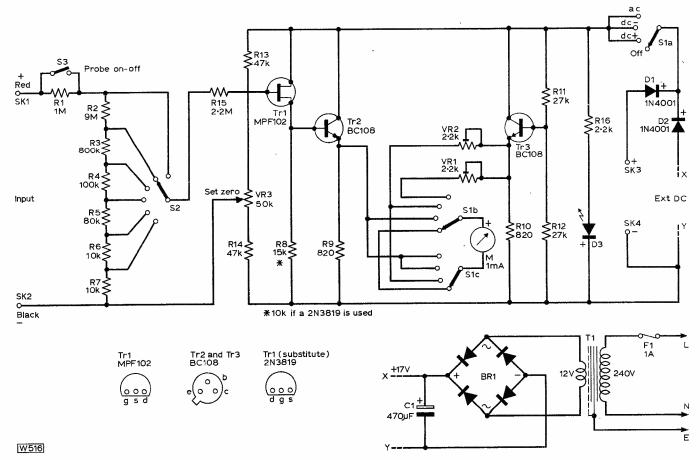


Fig. 2: The detailed circuit diagram, including transistor base connections and optional power supply circuit.

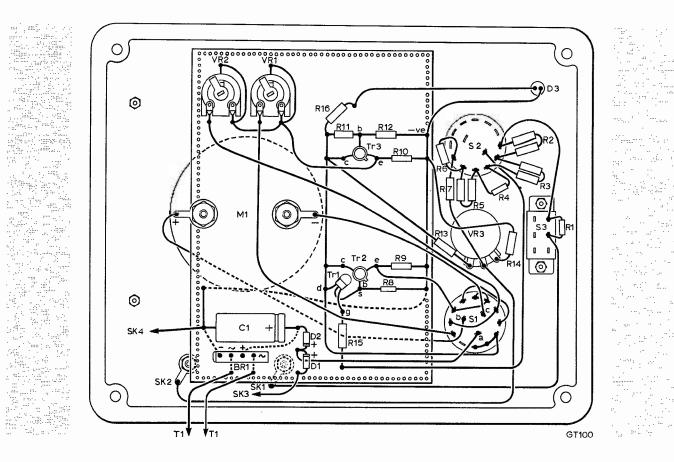
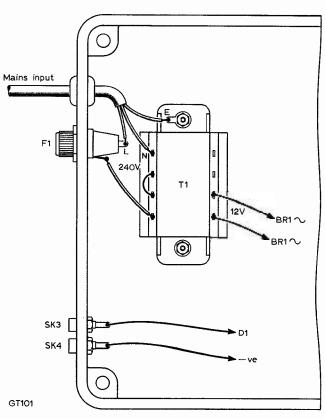
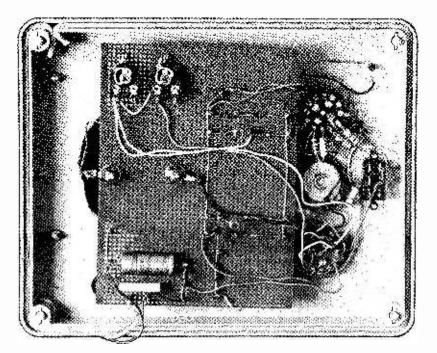


Fig. 3 : (above) showing internal layout, and Fig. 4 (below) indicating mains input and transformer details:



#### \* components

			and the same of th
Resisto	rs IMΩ	Do	***
	transfer to the second of the second	R9	820Ω
	$M\Omega$ (2.2M $\Omega$ + 6.8M $\Omega$ )		820Ω
	$800$ k $\Omega$ (470k $\Omega$ + 330k $\Omega$ )		<b>27</b> kΩ
	100kΩ	R12	27kΩ
		R13	47kΩ
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	/0kΩ  0kΩ	R14	47kΩ
	10κ32  5kΩ	R15	2 2MQ
		R16	2·2kΩ
DO L. I	R7 ½W metal oxide hi	gn sta	ibility 2%
No to r	R16 4W carbon film hi	gn sta	ibility 5%
V.R.1/2	2·2kΩ horizontal pre-s	et	
V rt3	50kΩ linear carbon		
<b>6</b>	nductors		
Tri	MPF102	n.	4 51 4004
Tr2/3	BC108		1N4001
BR1	8 T T 6 T 5 T 5 T 5 T 5 T 5 T 5 T 5 T 5 T	D3	LED (pushfit)
	Bridge rectifier 100PIV		
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	500mA. Fuse 1A and		
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outher'	epending on readout	accur	acy required, the
Diantia	s meter was 117 $ imes$ 100	amm (	42 × 4in. approx.). □
Flastic	case approx. 225 $ imes$ 175	× 851	$\min_{i} (\mathfrak{s} \times I \times \mathfrak{s}_{2}^{*} \mathfrak{i} \mathfrak{n}_{s}).$



A view of the inside of the voltmeter, to be used in conjunction with Fig. 3, in which the method of connecting resistors in series to form R2, R3, and R5 is clearly shown.

connection of the jack plug is used, the outer connection is ignored.

A short length (approximately 1m) of coaxial cable is used to couple the probes to the voltmeter. This should preferably be a substantial RF type cable with a copper braided screen. The braid terminates in a short length of stranded wire fitted with a crocodile clip. This ensures a low-resistance contact with the chassis or common rail of the circuit under investigation. The voltmeter end of the connecting cable is fitted with two 4mm plugs. The AC and RF probes use a similar construction technique, Fig. 7.

#### Calibration

Calibration on the DC and AC ranges is carried out by means of VR1 and VR2 respectively. Calibration on the DC ranges may be checked either by the application of an accurately known DC voltage or by reference to another DC voltmeter. If neither is avail-

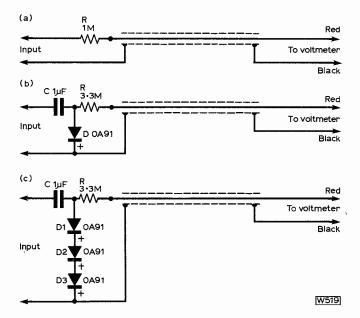


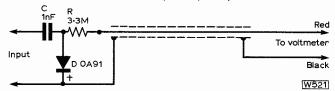
Fig. 5: Suitable probe designs for the unit.

3-5mm jack plug Resistor Screen connection Coaxial cable

R

Black insulated stranded wire W520

Fig. 6: The construction of the DC probe, (above) and the circuit of the AC and RF probes (below).

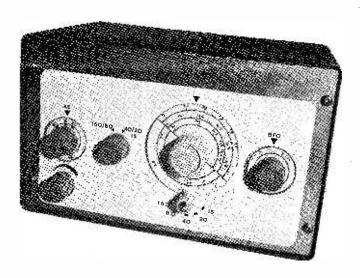


able a new 1.5V cell may be connected to the instrument and VR1 accurately set for a reading of 1.5V, after first remembering to set the Probe Switch "off" and zero the meter! Repeat the calibration procedure for the DC negative and AC ranges (but without a probe connected). Calibration can be checked on the AC range if a known source of AC is available. This may conveniently be a low-voltage transformer of known output supplied from the mains. Do not attempt to calibrate the instrument using AC mains voltage directly since this may cause damage to the probe and to the instrument. The AC probes are suitable only for relatively low AC voltages.

#### **Operation**

The voltmeter is switched to the desired Function and the Set Zero control is then adjusted in order to accurately zero the meter. The Range Switch is set to the 1000V range. The input leads are then connected to the circuit under test and the Range Switch is then progressively advanced to the range which produces an easily measurable indication. Note that, for the sake of simplicity, a separate mains switch is not fitted to the instrument. Thus, when the unit is not required for use, it is advisable to disconnect the instrument from the AC supply by removing the mains plug.

# all band Short wave ERAYER G30GR CONVERTER



The controls are, left to right, RF Tune, Bandswitch, main tuning and BFO Tune. The RF Attenuator/on-off switch is below the RF Tune control at the left.

With a receiver intended particularly for multi-band reception individual coils with parallel and series capacitors are often provided for each range, values being arranged to secure suitable coverage. A band-spreading capacitor suitable for the LF bands is too large in value for the HF bands, so that some ranges need series padders. The number of coils, trimmers and padders for a multi-band receiver of this type becomes large and careful adjustment is needed to track aerial and oscillator tuning.

The converter described here avoids these difficulties, and is in line with the trend to use a high intermediate frequency, to eliminate second channel interference. It is suitable for operation with a receiver tuned to about 5.5MHz, which will be available with many general coverage receivers, and allows 1.8 to 21MHz to be covered with a single converter oscillator coil.

Although this article describes a converter intended for use on the amateur bands there is no reason why it should not be aligned for the SW broadcast bands, since most of these bands are adjacent, in terms of frequency, to the amateur bands.

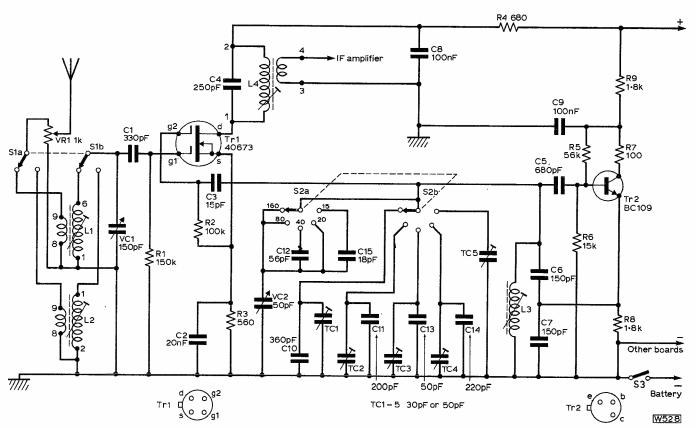


Fig. 1: Circuit diagram showing the mixer and oscillator sections of the converter, together with the lead-outs for the transistors.

#### Circuit Description

Fig. 1 shows the mixer and oscillator stages. The ganged switch S1a/S1b brings into circuit either L1 or L2 for aerial tuning, L1 covering the 15, 20 and 40m bands, and L2 the 80 and 160m bands. Each band is peaked by the panel control VC1. This provides five bands with two coils, with no trimming or similar alignment difficulties.

L3 is the oscillator coil, tuned by VC2, with the switch S2a/S2b. This switch has five positions, operating as follows:—

160m VC2 has C10 and TC1 in parallel, so that the oscillator coverage is  $7 \cdot 25$  to  $7 \cdot 5$ MHz. With the  $5 \cdot 5$ MHz IF, this gives reception over the  $1 \cdot 75$  to  $2 \cdot 0$ MHz range.

80m C11 and TC2 are in parallel with VC2, giving an oscillator coverage of 9 to 9.5MHz, or 3.5 to 4.0MHz on reception.

40m C13 and TC3 are across L3, and C12 is in series with VC2. Oscillator coverage is  $12 \cdot 5$  to 13MHz, giving reception of signals in the 7 to  $7 \cdot 5$ MHz band.

20m C14, TC4 and VC2 are in parallel, so that L3 tunes 8.5 to 9MHz and reception is from 14 to 14.5MHz.

15m TC5 is across L3 and C15 is in series with VC2, giving an oscillator range of 15·5 to 16MHz, for reception over 21 to 21·5MHz.

VC2 is operated by a ball drive and is the main tuning, with VC1 peaking signals as mentioned. VC1 is calibrated to avoid tuning to second channel frequencies, which arise at about 11, 13, 15 and 18MHz in the usual way with a 5.5MHz IF. VR1 is an

#### \* components

Resistors	100	No.	marti (il	
R1 150kΩ	R6	15042	RII	2-2kΩ
- R2 100kΩ	R7	19000	R12	68012
R8 560Ω	RB	1 202	R13	300603
R4 680Ω	R9	128002	R14	6-840
R5 56kΩ		1:2M0	R15	2:761
VR1 1kΩ linea	CONTRACTOR OF THE CANADA AND AND AND	and the second of the control of	58	4 files de para
All resistors	are # or #VV	5%		Barthagas (A. A. Tapad arting
Capacitors	15 - 17 10 year 100			
C1 330pF	C9	100nF		10nF
C2 20nF	C10	360a F*	C18	100pF*
C3 15pF	C11	2006F*	C19	1 95 97 5 550 (500)
C4 250pF*	C12	589F.	C20	10nF
C5:: 680pF:::	C13	ACCOMPANY OF THE PARTY OF THE P	C21	220pF*
C6 150pF*	C14		C22	220pF*
C7 150pF*	C15	6 6000 6 60	C23	470 oF 12V
C8: 100nF	C16	220pE		
*24, sliver rui			N. P. 63	0000
TCt/5 50pFtsimmer VC2 50pF(C804)		VC1 150pF (Jackson C804) VC3 20pF (C804)		
	(scourity)	Y DU EV	pr (Coor	
Semiconducto	rs			
Tr1 40673			5459	
Tr2 BC109	715577461	Tr4 2N	2926	
Miscellaneous	400000000000000000000000000000000000000			
St. f-pole 2-	vas water :	witch S2	2-pole	5-way wafei
switch, Li, Y	official, Ran	go 4, velv	e type (	Denco), L2
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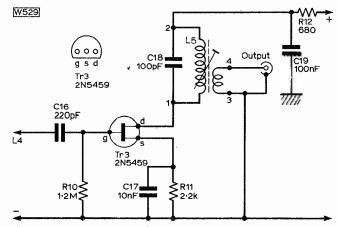


Fig. 2: The optional IF amplifier stage which works at 5·5MHz. This is a separate unit, and may be fitted if the main receiver is relatively insensitive.

attenuator or aerial input control, enabling the strength of signals to be kept down so that satisfactory CW and SSB reception can be obtained, also preventing the overloading of the receiver with strong AM transmissions. Tr1 is the mixer, with the signal input to gate 1, and the oscillator input to gate 2. Tr2 is the oscillator stage, operating as described. L4 is tuned to approximately 5.5MHz and is followed by an optional FET 5.5MHz stage. This can be omitted with a reasonably sensitive main receiver, or can be added later. A BFO is included to allow CW and SSB reception with the popular type of receivers which may have no beat frequency oscillator incorporated.

Fig. 2 is the circuit of the 5.5MHz optional stage. Signal input is taken from Tr1 coupling coil L4 pin 4, to C16. L5-C18 is a further 5.5MHz coil connected in the drain circuit of Tr3, and coupled to the output socket. This stage is assembled as a separate unit, fitted to the chassis later.

#### **BFO**

The beat frequency oscillator is designed for a centre frequency of 5.5MHz and uses the circuit in Fig. 3. It is also assembled as a separate unit. Without the BFO, only AM signals can be received, unless a suitable BFO is present in the receiver itself. As AM reception may be required, provision is made to switch off the BFO for this purpose. To do this, the corner of the back moving plate of VC3 is bent so that it contacts the fixed plate when VC3 is fully closed. The stage is then not operative and current is limited to about 1mA by R14 and R15. An on-off switch in series with R15 could be used if preferred.

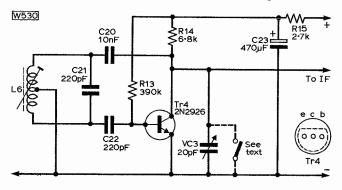
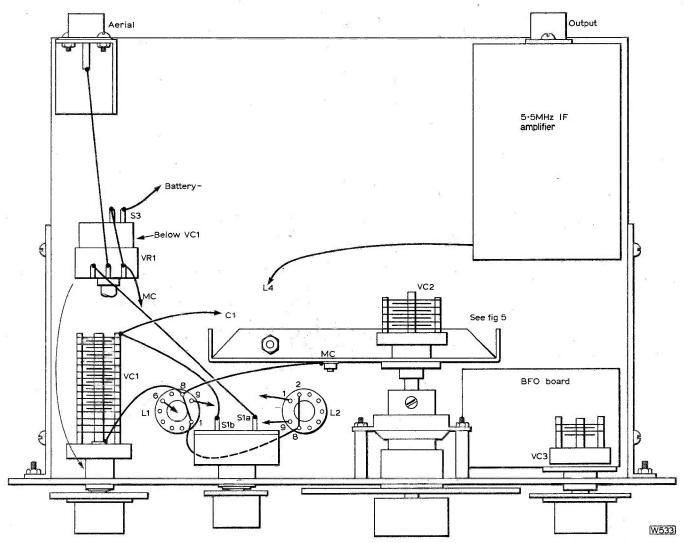


Fig. 3: Another optional unit is the beat frequency oscillator which also operates at about 5·5MHz. If the main receiver has a BFO then this unit is not required.





Metal bracket 100 x 90mm (4 x 3<sup>1</sup>/<sub>2</sub>") approx

W532

Trimmers mounted on paxolin strip

MC

TC5

TC4

TC3

TC4

TC3

TC4

TC3

TC4

TC1

Chassis

Fig. 5: Details of the assembly mentioned in the photograph. It can be finished completely as shown before mounting on the main chassis.

The positions of components and wiring can be seen from Fig. 4. The chassis returns MC are <sup>1</sup>2in 6BA bolts, with extra nuts and tags, so that the board can be mounted later with clearance for connections and leads. Insulated leads are provided to go to S2a/b, VC1, positive, and output socket or IF stage. Leads of Tr1 and Tr2 are shown in Fig. 1.

Fig. 6: Layout of the units and main components on the chassis. After the main tuning dial has been fitted to the panel the remaining panel components can be mounted in the same line.

#### Osc/Mixer assembly

VC2 and S2a/b are fitted to a bracket approximately  $100 \times 90 \text{mm}$  (4in x  $3^{1}2\text{in}$ ) as in Fig. 5. The five trimmers are mounted on a strip of paxolin, which is spaced from the bracket by a long bolt, or similar, to clear the switch. Connect C10 to TC1, C11 to TC2, C13 to TC3, and C14 to TC4 before mounting the trimmer strip, including leads to take to the switch tags on that side.

The board is mounted by the bolts described earlier. The switch requires a spindle 2in long, so that it can project through a \$1\_4\$ in hole in the panel, when the assembly is bolted in place approximately \$1\_2\$ in behind the panel. Alternatively, a shaft coupler can be added, with a length of rod. The exact distance from bracket to panel is arranged so that the spindle of VC2 engages correctly with the ball drive bush.

Fig. 6 shows the positions of components on the chassis, and connections for L1 and L2. VR1 fits directly below VC1. The aerial lead runs direct to VR1, away from the 5.5MHz circuits to avoid unnecessary 5.5MHz breakthrough. The BFO board fits to the right, as shown.

Part 2 next month will deal with the construction of the BFO and final alignment of the converter plus a few hints on using the converter. NEXT MONTH IN.

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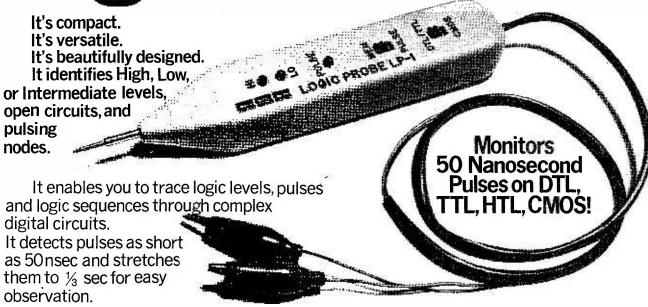
dependently or linked together from the front panel. Both are adjustable and fully metered. Finally, adequately stabilised. V DC to 0 SA PL also: TRAFFIC LIGHT CONTROLLER **SOLID-STATE TUNING INDICATOR** 



We were delighted to hear from Albert Hedges of Ramsgate, long time reader of PW, that he still has in use a tool set that was announced in Practical Wireless for September 23, 1933 as a "Great Birthday Offer" on the occasion of PW's first birthday. A special voucher was issued on which 11 gift stamps were stuck, taken from consecutive issues of PW. This completed voucher plus 3s 6d (1712p) got the complete tool set in an attractive metal case. The set comprised a steel rule, steel scriber and chuck, scribing and cutting trammels, set square, viewing mirror, screwdriver plus a set of BA spanners. Since PW was published weekly at that time, at a cover price of 3d (1p and a bit!) it didn't take long or cost very much to acquire the tool set. We wonder if there are any others still around! If only we could make such a splendid "special offer" today!

Practical Wireless, November 1977

## Logic Probe LP-1



#### Try the LP-1 and you won't know how you ever managed without it!

#### How it works

You just clip the probe leads to the circuit power supply, setting the 'Logic Family' switch to DTL, TTL or CMOS. (CMOS position also covers HTL.).

Touch the probe's tip on the node you're investigating and the LP-1 lights up to show you exactly what you've got. The LED marked 'HI' comes on for logic state 1 (High) and 'LO' comes on for logic state 0 (Low).

The third LED, marked 'PULSE', shows the dynamic signal activity at the node under test. Set the switch to 'PULSE' and pulses as narrow as 50 nanoseconds are stretched to ½ second. Single-shot and low rep. rate pulses are clearly shown—you can't do that even with a fast CRO! High frequency pulses up to 10MHz will make the 'PULSE' LED blink continuously at 3Hz; and with assymetric signals the 'LO' LED will come on for duty cycles under 30%, and 'HI' for those over 70%.

Another useful feature is 'Pulse Memory'.

Put the probe tip on to a node, switch to 'MEM' and the next logic change-positive or negative—or the next pulse edge, will cause the 'PULSE' LED to come on and stay on, until reset. Meanwhile, 'HI' and 'LO' LEDS continue to function as usual. No other probe or logic checking device gives you all that!

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Alternatively, ask for our latest catalogue, showing all CSC time-and-cost-saving products for the engineer and the home hobbyist.

#### **Brief Specification:**

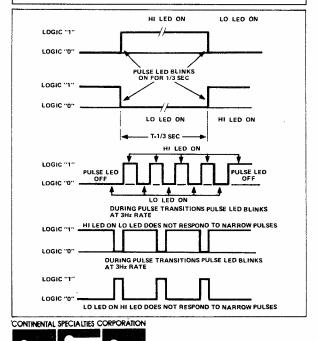
Input Impedance: 100,000 Ohms, 10MHz
constant for all functions. Power r
DTL/TTL Thresholds: 5 Volt\*
logic 1, 2.25V ± 0.15 15 Volt\*
logic 0, 0.80V ± 0.10 36 Volts
HTL/CMOS Thresholds: Size: 6.
logic 1, 1,70% Vcc (155 x 2

logic 0, 0,30% Vcc Min. detectable pulse: 50 nanoseconds

#### Max. input signal frequency: . 10MHz

Power requirements: 5 Volt Vcc, 30mA 15 Volt Vcc, 40mA 36 Volts max. Size: 6.1 x 1.0 x 0.7 inches (155 x 25 x 18 mm)

Weight: 3oz (85g) Power leads: 24 inches (610mm), colour coded.



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A superb solid state audio ampli-

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E3.15.7-F. &F. 35p.

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When designing, building or servicing RF equipment it is sometimes necessary to know the frequency at which a particular coil resonates or tunes. A recent example involved a radio IF stage with very low gain; one of the IFTs seemed suspect and this was removed from the printed circuit and dismantled to expose a small ferrite-enclosed coil and an even smaller capacitor with unreadable markings. Using an RF signal generator and the apparatus described here it was found that a 470pF capacitor tuned the coil to the correct IF; an 'outboard' capacitor was then fitted across the IFT, bringing the radio back to 100 per cent performance, and the test apparatus was returned to the shelf to await the next emergency.

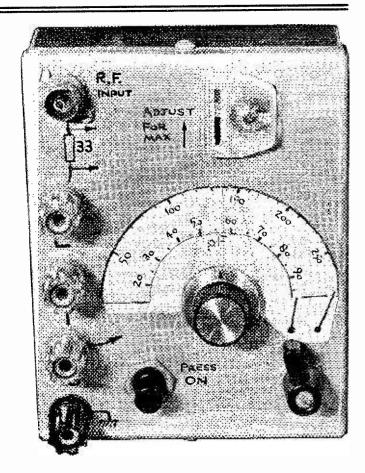
This resonance indicator is not intended to replace more accurate (and more expensive!) apparatus, but rather to provide a rapid method of checking unknown tuned circuits in the range 100kHz to 28MHz. With a given inductor in circuit, the values of unknown capacitors may be found within the range of VC1a and b by resonating the inductor at the same frequency, first with and then without the unknown capacitor between terminals N and M. The change in the value of VC1a or VC1b needed to re-establish resonance is therefore the value of the unknown capacitor.

#### **Circuit operation**

In a series tuned circuit maximum current flows at resonance and in Fig. 1 this current through R1 feeds the emitter of Tr1 with an increased RF voltage compared with the voltage at other frequencies. The emitter and base of Tr1, just biased on by R2, VR1, form a detector circuit and the boosted RF thus acts to increase the emitter-base current. The resulting increase in collector current is indicated by the meter so that the resonance of a particular coil with a selected capacitance and frequency is now known.

#### Construction

Because a variable capacitor usually has the frame earthed, this has to be fitted at the 'bottom' of the circuit and the operational electronics are therefore at the 'live RF' end, as is the push-button on-off switch. All components apart from R1, S1, S2, VC1 and M1 may be fitted to a piece of Veroboard; VR1 is adjusted to give a small (about 20 per cent) pointer deflection when S1 is closed. R1, a carbon type, is fitted directly from the coaxial RF input socket to terminal O to limit excess inductance; the circuit board could be attached across R1 by short stiff wires if one wishes to avoid making additional fixings to the chassis or panel. See Figs. 2 and 3.



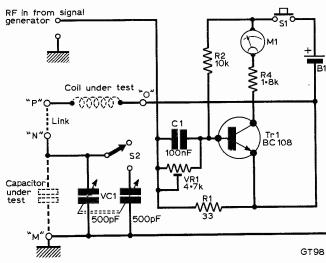


Fig. 1: The circuit diagram of the RF Resonance Indicator.

VC1 is bolted direct to the case. A metal case is recommended rather than a plastic one. A short pointer on the shaft traverses over a card scale glued to the outside of the box. During construction ensure that the link between terminal N and P is easily removed for ease of calibration.

The single Mallory cell (in its holder) may be glued into place, and should last for several years.

Piece of veroboard mounted on stiff wires between meter and R1

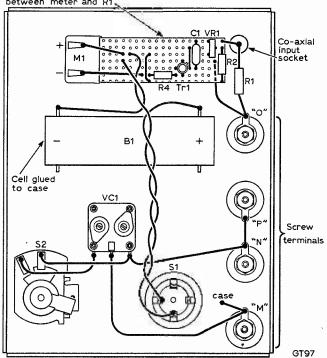


Fig. 2: General wiring inside the aluminium case.

#### **Calibration**

Connect a coil (fifteen turns of plastic or enamel covered wire close-wound and taped securely to a ferrite aerial rod will do) between terminals P and O. Temporarily unsolder the link N-P. Connect a close-tolerance 50 or 100pF silver mica or polystyrene capacitor between terminals N and M, keeping S1 closed. Then vary the tuning of the RF signal generator connected to the RF input socket while looking for a peak in meter deflection. Without changing the RF generator frequency, remove the external capacitor, connect N-P and vary VC1 until the meter reading again peaks.

The scale-card may then be marked with its first 50 or 100pF calibration point. Close S2, retune VC1 for peak reading and calibrate the other scale. Depending upon the particular type of variable capacitor available it is possible that the minimum capacitance of both gangs in parallel is more than 50pF and that 100pF will be the first calibration.

Now with VCI set to the 50pF calibration point, add the external capacitor and vary the input frequency to obtain a peak meter reading. Remove the external capacitor and increase the value of VCI to regain the peak meter reading, marking this new calibration point on the scale. In this way calibration points may be located at 50 or 100pF intervals around the scales.

It will also be possible to confirm the basic frequency formula that if the 15-turn coil resonates at about 5 to 6 MHz with 50pF, then at 450pF, nine

#### **★** components

Resistors: R1 33Ω, R2 10kΩ, R4 1 8kΩ, VR1, 4 7kΩ preset.

Capacitors: C1 100nF polycarbonate. VC1, 500/500pF gang capacitor

Transistor: BC108

Switches: S1, push-to-make switch, S2, SPDT wafer

Miscellaneous: Screw-type ferminals, Co-axial socket, Metal case, 5½" × 4½" × 1½" (140mm × 105mm × 45mm). (AB10) B1: 1 2V to 1+5V cell (mercury), Piece of Veroboard, 2" × 1" (50mm × 25mm).

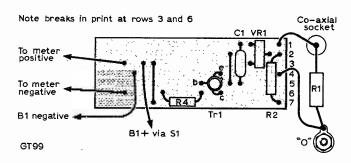
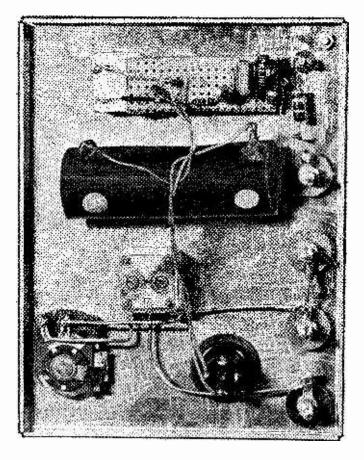
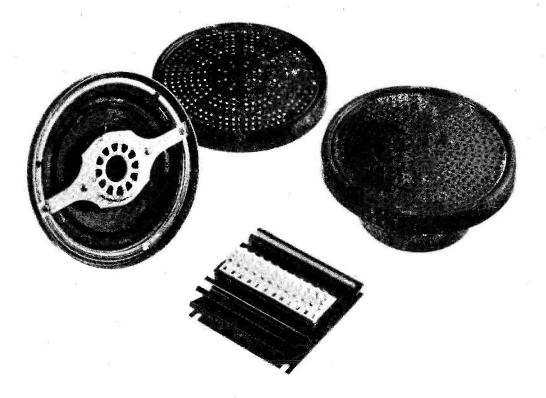


Fig. 3: Showing the component positions on the Veroboard, and meter and battery interconnections.



times the original capacitance, the resonant frequency becomes **one-third** of its value at about 1.8MHz. This is because resonance is proportional to the **square-root** of the ratio of capacitance change.

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The C15/15 is a unique Power Amplifier providing Stereo 15 watts per channel or 30 watts Mono and can be used with any car radio/tape unit. It is simply wired in series with the existing speaker leads and in conjunction with our speakers S15 produces a system of incredible performance.

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Thermal protection
Size  $4 \times 4 \times 1$  inches

Data on S15
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2" Active Tweeter
20oz Ceramic magnet
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## So you want to pass the R.A.E. (Radio Amateurs' Examination)?

John Thornton Lawrence GW3JGA & Ken McCoy GW8CMY

The passing of the Radio Amateurs' Examination, set by the City and Guilds, requires a certain level of theoretical technical knowledge. Whether one considers that this level is too high or too low is beside the point. The course that follows is intended, with the help of certain external aids, to prepare the reader to pass the examination. It will not teach him all about electronics!

#### **Practical Ohm's Law**

Before we move off Ohm's law and resistance, let us see how it can be applied to calculating the resistor values in a practical circuit. We are going to use an audio frequency amplifier as an example and this is shown in Fig. 1a. As we are only concerned with the DC conditions and how they are set up, we can forget about all the AC components, the coupling and de-coupling capacitors, leaving only the DC components as shown in Fig. 1b. Most modern small signal transistors have a beta (DC gain) of 100 or more, this implies a very small base current, sufficiently small

Fig. 1: The application of Ohm's Law to a simple transistor circuit.

that it may be ignored altogether if certain "rule-of-thumb" conditions are observed.

In a small signal audio frequency transistor amplifier stage, the collector current for optimum gain, noise performance, etc., would be about 1 to 2mA, so for simplicity we will choose 1mA  $(10^{-3}A)$ . Now for the current flowing down the base potential divider, R1 and R2. As a rule-of-thumb guide this should be a tenth of the collector current, so in our circuit it would be  $0 \cdot 1$ mA  $(10^{-4}A)$ . This ensures that this current is large compared with the small bias current of the transistor. The two currents are shown in Fig. 1b.

Now for the voltages in the circuit. First we must know the supply voltage, so for our example we will make this 9V. The emitter resistor R4 provides stabilisation of the operating conditions for Trl. A typical voltage drop across this would be 0.5 to 1V. So again for simplicity we will choose 1V. The collector voltage should sit midway between the emitter voltage +1V and the supply voltage +9V, that is at +5V. This will allow a signal voltage swing on the collector to go positive by 4V to the supply voltage and negative by 4V to the emitter voltage. Remember, up the page is more positive and down the page is more negative (away from positive)! Finally, the voltage drop across the emitter-base of a silicon transistor is 0.6V so if the emitter is at +1V the base will be at +1.6V.

Now for the sums to work out the value of the resistors, these are taken in reverse order.



. . . some practical experience is desirable!

$$R4 = \frac{V}{I} = \frac{1V}{10^{-3}A} = 10^3 \Omega = 1k\Omega$$

$$R3 = \frac{V}{I} = \frac{4V}{10^{-3}A} = 4 \times 10^3 \Omega = 4k\Omega$$

$$\text{R2} = \frac{\text{V}}{\text{I}} = \frac{1 \cdot 6\text{V}}{10^{-4}\text{A}} = 1 \cdot 6 \times 10^{4} \,\Omega = 16\text{k}\Omega$$

R1 = 
$$\frac{V}{I} = \frac{9-1.6V}{10^{-4}A} = \frac{7.4V}{10^{-4}A} = 7.4 \times 10^{4} \Omega = 74k\Omega$$

In a practical circuit the value of each resistor would have to be chosen from the list of "preferred" values. There are 12 "preferred" values in each decade of the 10% tolerance range of resistors and 24 "preferred" values in the 5% range.

10% (E12) range:— 
$$1 \cdot 0$$
,  $1 \cdot 2$ ,  $1 \cdot 5$ ,  $1 \cdot 8$ ,  $2 \cdot 2$ ,  $2 \cdot 7$ ,  $3 \cdot 3$ ,  $3 \cdot 9$ ,  $4 \cdot 7$ ,  $5 \cdot 6$ ,  $6 \cdot 8$ ,  $8 \cdot 2$ .

5% (E24) range. All the above values plus: — 
$$1 \cdot 1$$
,  $1 \cdot 3$ ,  $1 \cdot 6$ ,  $2 \cdot 0$ ,  $2 \cdot 4$ ,  $3 \cdot 0$ ,  $3 \cdot 6$ ,  $4 \cdot 3$ ,  $5 \cdot 1$ ,  $6 \cdot 2$ ,  $7 \cdot 5$ ,  $9 \cdot 1$ .

To complete our exercise let us now specify the preferred values for our circuit.

	R1	R2	R3	R4
Calculated value	$74 \mathrm{k}\Omega$	$16 \mathrm{k}\Omega$	$4k\Omega$	$1 \mathrm{k} \Omega$
5% range (E24)	$75 \mathrm{k}\Omega$	$16 \mathrm{k}\Omega$	$3 \cdot 9 k\Omega$	$1 \mathrm{k} \Omega$
10% range (E12)	$68k\Omega$	$15k\Omega$	$3 \cdot 9 k\Omega$	$1 \mathrm{k} \Omega$

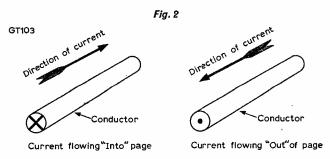
#### Magnetism

We are not proposing to spend any time on permanent magnets except to say that a permanent magnet has a "north seeking" pole and a "south seeking" pole and that imaginary lines of magnetic field or force run from the north to the south pole of the magnet. If two magnets are brought close together then the poles attract one another if they are dissimilar, N-S or S-N, and repel one another if they are similar, N-N, S-S. (See Radio Amateurs' Examination Manual, page 9).

If you are a family man, perhaps you could borrow your son's copy of the Ladybird Book, "Magnets, Bulbs and Batteries"! Seriously though, it's an excellent little book and illustrates pictorially the effects we are going to discuss.

#### **Magnetic Effect of an Electric Current**

In the following section we shall look at the magnetic effects produced by currents flowing in conductors. When illustrating these effects in diagrams it is essential to know the direction in which



the current is flowing and the way this is done is shown in Fig. 2. A cross on the conductor relates to the flight of the arrow and indicates that the current is flowing away from the observer and a dot on the conductor represents the point of the arrow and indicates that the current is flowing towards the observer.

Now, let's get down to business and look at a conductor in cross section as shown in Fig. 3. The conductor is surrounded by button compasses, no current is flowing and the compasses are taking up a position in line with the earth's magnetic field. When current flows through the conductor away from you, as shown in Fig. 4a, a magnetic field is produced and the compasses align themselves with the lines of this field, in a clockwise direction. When the current flows in the reverse direction, towards you, as shown in Fig. 4b, you can see that the direction of the magnetic field is also reversed. Remember, reversal of the current produces a reversal of the field.

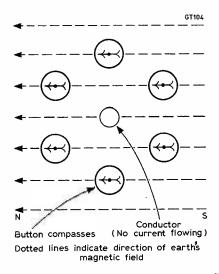


Fig. 3

▼ Fig. 4

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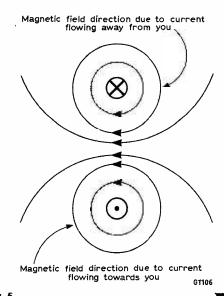
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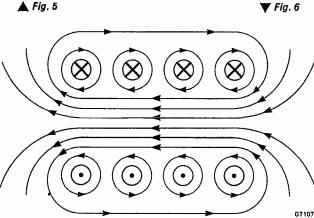
## the conductor The Solenoid

If a conductor is formed into a single turn coil, a cross-section view would appear as shown in Fig. 5. You will now notice that the magnetic fields produced in the centre of the coil are in the same direction and are, therefore, more concentrated. The solenoid is a coil comprising a number of turns, as shown in section in Fig. 6. Here you can see the overall effect of the lines of magnetic field around each conductor, combining to produce a concentrated field in the centre of the solenoid, with an overall magnetic field similar to that produced by a permanent bar magnet

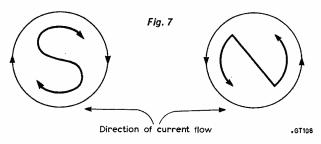
Practical Wireless, November 1977

the conductor





with its "north seeking" pole and "south seeking" pole. The magnetic polarity of the solenoid can be deduced by observing the direction of the current flow when viewing the coil at one end, as shown in Fig. 7. The arrows on the letters indicate the direction of the current and make a useful memory aid.



Now, suppose we place a conductor in a magnetic field, with no current flowing, as shown in Fig. 8a, there is no disturbance to the field. When a current flows through the conductor, its resultant magnetic field reacts with the existing field, as shown in Fig. 8b. You will see that on one side of the conductor the lines of magnetic field are in the same direction as those produced by the current and tend to reinforce the field on that side whilst on the other the fields tend to cancel out. This causes a force to be exerted on the conductor resulting in its moving in the direction indicated. A reversal of current produces a reversal in the direction of movement, as shown in Fig. 8c.

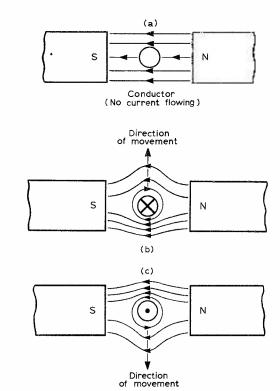


Fig. 8: Physical effect of current flowing in a conductor situated in a magnetic field.

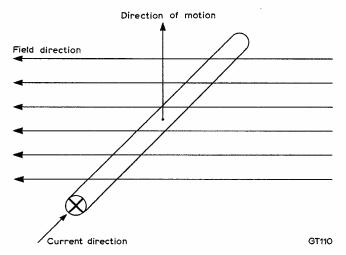


Fig. 9: Effect on a conductor when it is moving in a magnetic field.

Finally, let us look at the converse of this effect where the conductor is moving at right angles to a magnetic field, as shown in Fig. 9. Here a flow of current is INDUCED in the conductor and its direction depends on the direction of the motion. The memory aid for this, which is Fleming's Left Hand Rule, is illustrated in Fig. 10.

#### The Left Hand Rule

If the thumb, forefinger and second finger of the Left hand are placed at right angles to one another,

- (i) The Forefinger indicates Field direction.
- (ii) The ThuMb indicates Motion direction.
- (iii) The SeCond finger indicates Current direction.

So that, if we know any two of the three directions, the third can be found.

To summarize what we have seen in this section,

- (i) If we pass current through a conductor a magnetic field is set up around it.
- (ii) The direction of the field depends on the direction of the current flow.
- (iii) If the conductor is in a magnetic field and a current is made to flow in it, the conductor will move, the direction of motion being dependent on the direction of current flow.
- (iv) If a conductor is moved in a magnetic field, then a current will be induced in the conductor, the direction of which is dependent on the direction of motion.

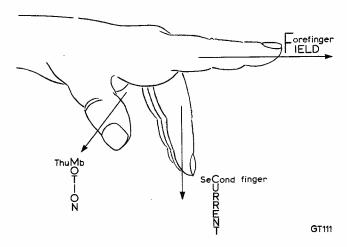


Fig. 10: Illustration of Fleming's Left Hand Rule. The importance of memorising this rule cannot be stressed too strongly.

You may begin to wonder what on earth all this has to do with amateur radio, so we will explain that the relationship between the direction of the current flowing in the conductors and the resulting magnetic field, together with the rate at which a conductor is moved in a magnetic field, are all basic ideas related to the generation of Alternating Current (AC).

## **Electromagnetic Induction**

In the previous section you will have noticed the term INDUCED current, or a current produced by electromagnetic induction. This effect can best be demonstrated by means of the interaction of a bar magnet and a solenoid, Fig. 11. If the bar magnet is moved into the solenoid a deflection will be noticed in the meter connected between the ends of the windings. When the bar magnet is removed a deflection will be noticed again, but this time in the opposite

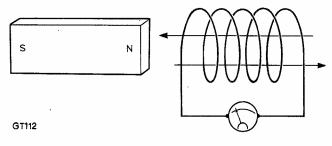
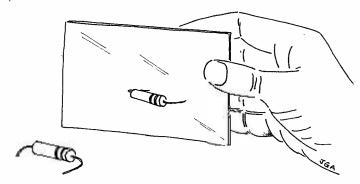


Fig. 11: A practical experiment which will show that a current is generated when a bar magnet is inserted into or removed from a solenoid. Remember:—No movement, no current!

direction. Whilst the magnet is stationary, no deflection will be observed. As an aside, you will also notice the fact (and by no means an insignificant one) that the faster you move the magnet, the greater the meter deflection.

As we have said before, some practical experience is very desirable, so why not wind yourself a solenoid, 50 to 100 turns of insulated wire on a toilet roll tube, connect it to a milliammeter, push in a magnet and see what happens!

The meter deflections indicate the presence of a potential difference between the ends of the solenoid conductors, giving rise to INDUCED current. If we think about this for a minute we will remember that, while current is flowing in the solenoid, that current will produce a magnetic field. Now, the direction of that field will be such as to oppose the motion of the magnet which induces it. Thus, if the north pole of the magnet is pushed inside the solenoid the current flow induced will produce an apparent north pole at that end of the solenoid, thus tending to oppose the magnet's motion. As the magnet is withdrawn the induced current will produce an apparent south pole at that end of the solenoid, again opposing the extraction of the magnet, since a north pole will attract a south pole.



... what is meant by "reflected impedance"?

The German physicist Lenz formalised this in his Law in 1834. Basically it means that the direction of the induced potential difference tends to set up a current opposing the motion or change of magnetic field producing that potential difference. Now the magnetic field which is used to induce currents in a solenoid need not come from a permanent magnet. It could come from another solenoid placed in close proximity to the first. In this we have the bones of the TRANS-FORMER, but, before we look at that subject, the question of the nature of ALTERNATING CURRENT (AC) arises. Again, the previous sections will be of assistance since AC is best understood when reference is made to the facts relating to conductors moving in a magnetic field.

#### To be continued next month

Readers are asked to note that the publications mentioned already in this series as recommended reading have recently been increased in price. They are "A Guide to Amateur Radio" and "The Radio Amateurs' Examination Manual" which now cost £1·38 and 86p respectively. They are obtainable from the Radio Society of Great Britain, 35 Doughty Street, London WCI. The prices are inclusive of postage.

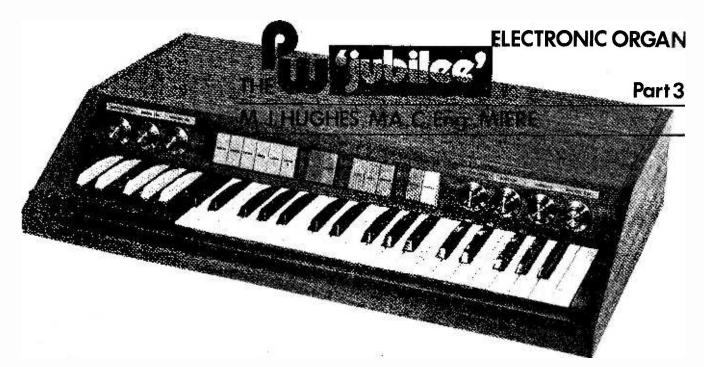


Fig. 1 shows the melody keying, percussion, sustain and tone forming circuits in their entirety. ICs 7, 8 and 9 are the priority encoders described in Part 1. They receive the 37 tones from the generators on pins 16 to 27 in the case of ICs 7 and 8, and 15 to 27 for IC9. There are 13 inputs to the latter to allow for bottom C. Single lines to each keyboard contact can be seen clearly. When one of these lines is pulled to ground through the respective switch, the note associated with that key is latched and fed out at pin 9. The links between the ICs give priority to the highest note played.

# **Melody Circuits**

The high level signals generated at the outputs of the priority encoders are fed to potential divider (R11 and R12) which reduces them to a level less than Vbe for Tr3 which is connected as an emitter follower. If there is no bias at the base of this transistor the audio signal will not appear at the emitter; the rate of application and removal of bias at this point controls the envelope of the output signal—thence the duration of sustain. If S1 and S2 are closed the priority output from IC9 (pin 31) is routed through the three cascaded gates of IC11b, c and d, and eventually appears, at reduced level, across VR5. A proportion of this is fed through D2 to the base of Tr3 providing the bias necessary to allow the audio signal to appear at its emitter. C6 creates a slight time constant, in conjunction with the setting of VR5, to introduce attack in the envelope.

When the selected key is released the priority signal falls immediately to zero but D2 becomes reverse biased allowing a charge to remain on C6. This charge keeps Tr3 (which can be considered to be an analogue gate) open and the audio continues to appear at its emitter. Over a short period the DC charge on C6 leaks away through Tr3 as base current and the bias is slowly lost. As this happens the audio signal at the emitter dies away. Because the signal is a square wave to start with there is no distortion in this operation. The period of charge leakage sets the sustain duration and this can be controlled by adjustment of VR6 which sets the base current for

the transistor. This latter control is brought out to the front panel.

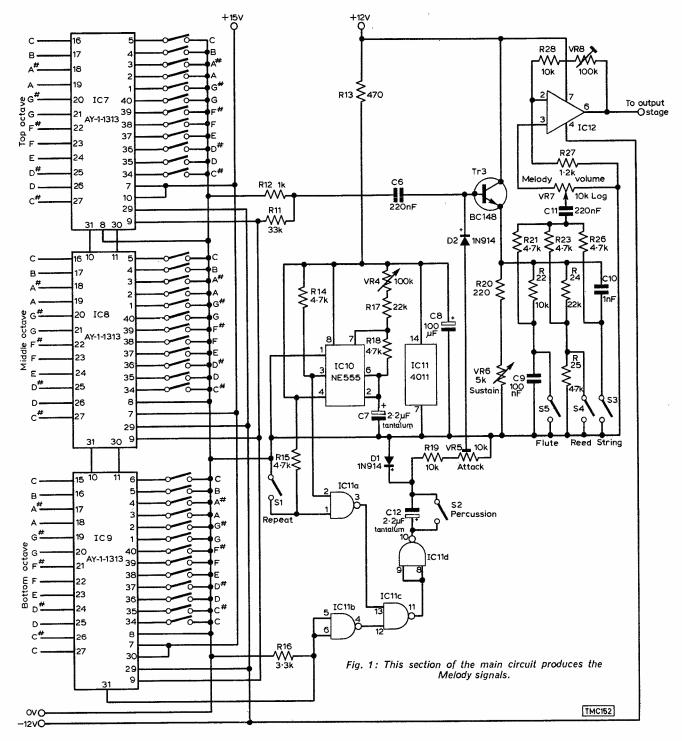
S2 introduces a low-leakage tantalum capacitor into the path of the keying strobe. This differentiates the control signal for Tr3; this opens the analogue gate momentarily allowing a short burst of audio through. The sustain setting controls the rate at which this percussive burst dies away. The burst of audio occurs on the depression of the key and will not sound again until the key is released and pressed again.

IC10 is the repeat percussion oscillator, frequency controlled by VR4 (again a front panel control). When S1 is open the low-frequency pulses of this oscillator are fed through IC11a and pass through the following gate when a key is depressed. Instead of getting a steady DC level at pin 10 of IC11d, the keying signal is now chopped by the repeat signal. This creates note repetition. Using this in conjunction with the sustain control produces effects such as banjo or xylophone sounds. Note that C7 should be a tantalum capacitor.

The RC circuitry following Tr3 creates the voicing. Normally S3, 4 and 5 are closed which shorts the signals to ground. Opening one or more of these switches introduces a particular tone colour. The signals of these three options are mixed by R21, 23 and 26 before being fed to the front panel "Melody Volume" control and thence to the melody buffer amplifier with gain set by VR8. This signal is then fed to the power amplifier or phono output stage.

Use Soldercon sockets for ICs 7 to 9 but do not insert the integrated circuits. Complete the assembly of the rest of this section by reference to Fig. 2. To facilitate testing, solder temporary links across the pairs of pins which will eventually go to S1 and S2. At the same time, temporarily wire in VR4, VR6 and VR7. Set the potentiometers and presets as follows to start with: VR4 Midway, VR5 To bottom (ground) end, VR6 To bottom end, VR7 Midway, VR8 Midway.

Insert the tone generator ICs. With a couple of lengths of wire fitted with clips, select one of the tone lines (see last month's circuit) and hook it tem-



porarily to the end of R11 which goes to the priority encoders. This will provide a test signal. The other wire should have one end clipped to pins 5 and 6 of IC11 (the end of R16 going to this point will do). The other end of this wire simulates keying by touching it to the +12V rail (at the positive end of C8).

Connect the power supply as described last month plus a loudspeaker. When you apply power you should hear nothing. Next hook the keying wire to +12V and you should still hear nothing. Gently adjust the wiper of VR5 away from the bottom end of its track to produce a tone in the loudspeaker. Adjust VR5 until the tone just reaches a stable level (ie does not get louder with increase of the setting). If, at this stage the volume is uncomfortably loud or is distorting, reduce the value of VR8. Remove the keying wire

from the 12V source and the tone should stop immediately. Slowly advance VR6 and tap the keying wire on and off the 12V point. The sustain effect should get greater as VR6 is increased in value. If you get an unpleasant click at each contact with the keying point, you have probably advanced VR5 too much—this setting is fairly critical.

Remove the link across the pins for S2 and try the keying test. You should get the single burst of sound when the keying contact is made. Finally remove the link across the pins for S1. This time, when you key, you should hear repeated percussive bursts of sound—rate adjustable by VR4.

Turn off the power and remove all temporarily connected potentiometers and also remove IC12 or it will be impossible to test following stages.

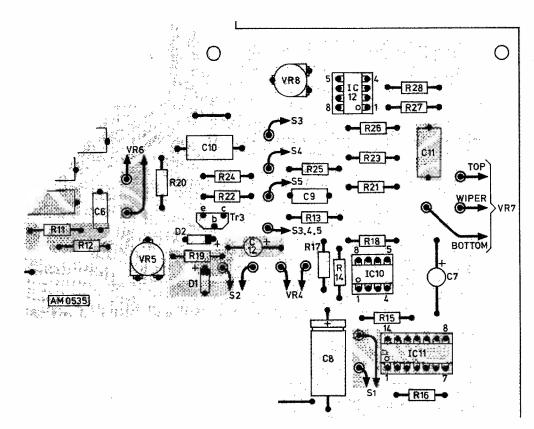
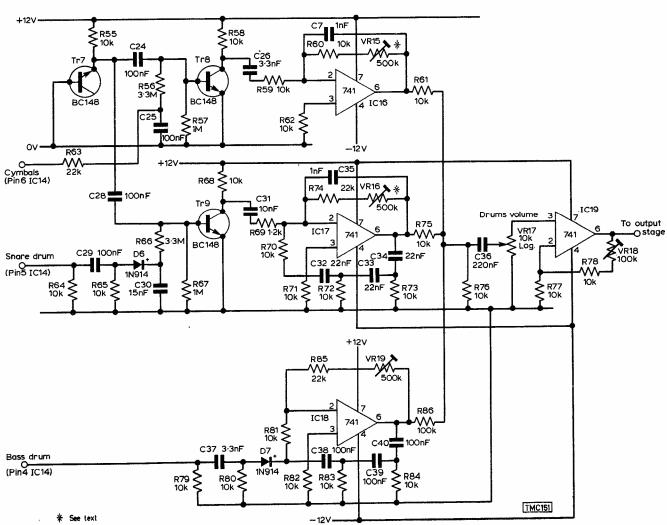


Fig. 2: left, assembly and interwiring diagram for the part of the main circuit shown in Fig. 1.

Fig. 3: below, is the circuit for the Drum and Rhythm part of the organ.



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# **Drum and Rhythm Section**

Fig. 3 shows the drum and cymbal voicing circuits. Tr7 is used as a white noise generator and feeds the cymbals and snare drum stages. Cymbal pulses from the rhythm generator IC are used to gate white noise through Tr8. The envelope of the gate is set by C25 with R63 and R56. The noise is filtered at top and bottom by C26 and C27 respectively. VR15 is used to balance the cymbal level with that for the other instruments.

The snare drum circuit is a little more complex. A sharp burst of white noise is generated at the collector of Tr9 when the trigger is received from the rhythm generator. This is fed to IC17 which is connected as a low-frequency phase-shift oscillator. VR16 is set so that the circuit is just NOT oscillating. When the white noise burst arrives it triggers a decaying oscillation in this stage and mixes with the frequency so produced. Some care is needed in setting VR16 for optimum results but the sound is quite realistic. The bass drum sound is produced by using

the rhythm pulse to trigger a similar phase shift oscillator which is tuned to a lower frequency. VR19 controls the oscillation point.

Assembly details are shown in Fig. 4. Do not insert the rhythm generator chip (IC14) at this stage. Note that this is an 18-pin package. When everything apart from IC14 has been correctly inserted, temporarily connect VR17 to its pins and set the controls as follows: VR15 Minimum resistance, VR16 Minimum resistance, VR17 Midway, VR18 Midway, VR19 Minimum resistance.

Connect the power supply. Slowly increase the value of VR19 until oscillation just starts then turn it back slightly so that it just stops again. With a flying lead, momentarily touch +12V to the top end of R79. You should hear a "thump" similar to that from a bass drum. Adjust VR19 for the correct amount of decay. Use VR18 to preset the level.

Now test the snare-drum circuit. Apply +12V pulses to the top end of R64 and adjust VR16 for best results. Try to achieve a reasonable balance with the bass drum. A  $100k\Omega$  component for VR16 would make for

easier adjustment. After building several models it was found that the best setting is very close to the bottom end if the original  $500k\Omega$  potentiometer is used.

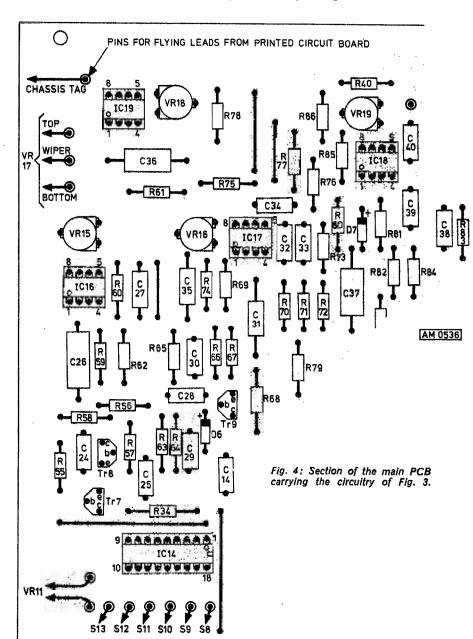
Finally, test the cymbals by applying +12V to the end of R63 going towards the rhythm generator and adjust VR15 until the sound is realistic. As with the snare drum circuit, adjustment may be easier with VR15 as a  $100k\Omega$  component.

The quality of the cymbals is to some extent controlled by Tr8. There is a large variation in gain for this device and a very high gain might saturate the device with the trigger pulse. This can be detected by a kind of "hesitation" at the beginning of the cymbal sound. It is remedied by reducing the value of R58 from  $10k\Omega$  to  $4.7k\Omega$ .

# Accompaniment Circuits

The Accompaniment circuits are shown in Fig. 5 and the assembly details of this stage in Fig. 6. IC14 is the rhythm generator the speed of which is controlled by VR11. Rhythms are selected by the switches S8 to S13 singly or in any combination. The switches couple the rhythm select inputs with the "Any Key Down" signal produced by the chord generator. This ensures a synchronised start of rhythm at the instant an accompaniment key is depressed.

The chord waveform is different from the simple square



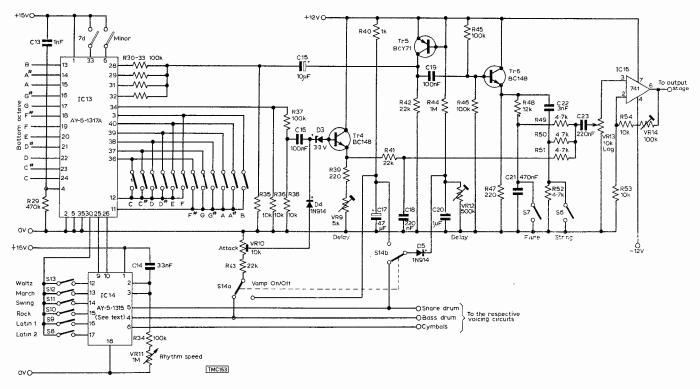


Fig. 5: The last part of the circuit to be described is for the Accompaniment.

# **★** components

Melody	/ Section	in the state		R68	10kΩ	C30	15nF
R11	33kΩ	VR8	100kΩ sub miniature	R69	1·2kΩ	C31	10nF
R12	1kΩ	a and a	preset	R70/73		C32/34	
R13	470Ω	C6	220nF	R74	22kΩ	C35	inE
R14/15		C7	2-2µF 15V tantalum	R75/84		C36	220nF
R16	3·3kΩ	C8	100μF 25V	R85	22kΩ	C37	3-3nF
R17		C9	100nF	R86	100kΩ	C38/40	100nF
R18	4.7kΩ	C10	1nF	VR15	500kΩ sub miniature	D6/7	1N914
R19	10kΩ	C11	220nF		preset but see text	Tr7/9	BC148
R20	220Ω	C12	2·2μF 15V tantalum			IC16/19	741
R21	4.7kΩ	D1/2	1N914		Pinne Talline of the Carlotte		
R22	10kΩ	Tr3	BC148	Qsee a	nd Accompanimen	C	
R23	4.7kΩ	IC7/9	AY-1-1313	R29	470kΩ	C16	100nF
R24	22kΩ	IC10	555	R30/34		C17	47μF 25V
R25/26	4·7kΩ	IC11	4011	R35/36		C18	220nF
R27	1·2kΩ	IC12	741	R37	100kΩ	C19	100nF
R28	10kΩ	S1/5	single pole one way	R38	10kΩ	C20	1 <i>u</i> E
VR4	100kΩ linear		toggles (5 off).	R39	220Ω	C21	470nF
VR5	10kΩ sub-miniature	April 1985	Rocker Tabs for	R40	220A2 1kΩ	C22	3nF
	preset		conventional kev-	R41/43		C23	220nF
VR6	5kΩ linear	· · · · · · · · · · · · · · · · · · ·	board version. Key-		22ΛΩ 1MΩ	D3	3·3V 400mW zener
VR7	10kΩ log. (ganged	e in the second	board switches	R45/46	100kΩ	D4/5	1N914
anta a si	with mains switch if		(depending on	R47	220Ω	Tr4	BC148
A TOTAL STREET	conventional key-		version being built).	R48	22042 12kΩ	Tr5	BCY71
eler i itiilik	board version is	voltali (*)		R49/52		Tr6	BC148
	constructed)	ada oʻzeri. Ta	, Berstua (1777) (1 <u>a) (Jap</u> atili	R53/54		IC13	AY-5-1317A
		n ya ja		VR9	5kΩ sub miniature		
i i i de la filla di di La granda	CROW, Spannaminch from 1. Mercy and 1997. The Committee Analysis of Marcy Committee.	e de la companya de				1014	AY-5-1315 (pattern
	and cymbals section	3fi 3m46	control to market	VOXO	preset	1000	004-Jubilee)
		VR16	500kΩ sub miniature	VR10	10kΩ sub miniature	S6/13	741
R56	3·3MΩ	14545	preset but see text	12542	preset	20/19	single pole one way
R57			10kΩ log		1MΩ linear	1111	toggles (8 off)—
R58	10kΩ* See text; this		100kΩ sub miniature	VR12	500kΩ sub miniature		rocker tabs for
	resistor might need		preset	and the second second	preset	Arrilla	conventional key-
	reducing to 4·7kΩ	VK19	500kΩ sub miniature	VR13	10kΩ log		board version
R59/62		There is the common of the com	preset	VR14	100kΩ sub miniature	514	double pole change-
R63	22kΩ	C24/25		e coman, 2004	preset		over toggle or rocker
R64/65		C26	8-3nF	C13	1nF		tab with similar pole
R66	3-3MΩ	C27	Inf Control of Control	C14	33nF		configuration
R67	TMΩ	C28/29	100nF	C15	10µF 25V	arii tara	رامل المراج البارات والإين ومعاصمته

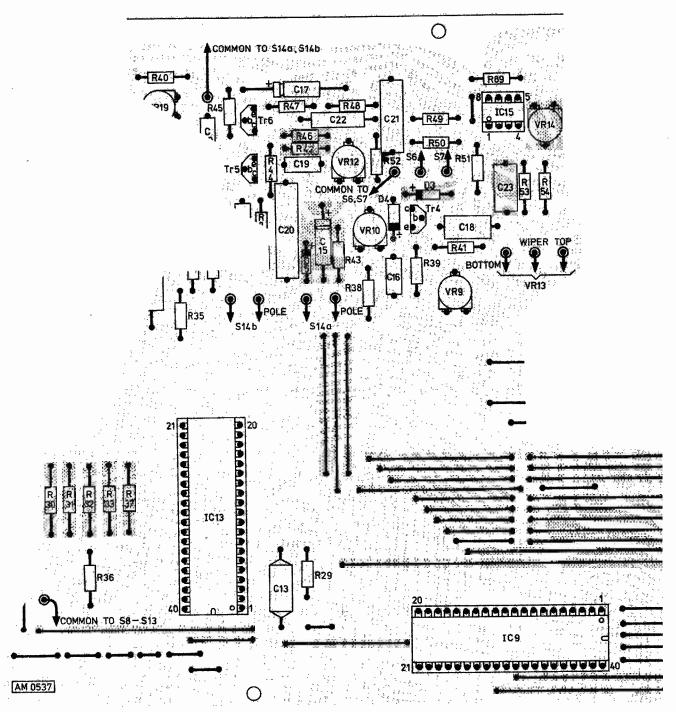


Fig. 6: Assembly details for the circuit shown in Fig. 5.

wave produced in the melody circuits in that it is more akin to a staircase which constantly changes its shape (depending on the harmonic relationships between the three or four elements it comprises). The simple emitter follower type of envelope shaper would introduce asymmetric distortion. Tr5 in conjunction with R42 acts as a voltage controlled attenuator. The mixed chord signal is applied to its collector via C15 and taken from this same point via C19 for further processing. If Tr5 is "turned on" the signal is shunted to the positive rail and its amplitude falls to nearly zero. The transistor is biassed so that this is the usual condition. When it is turned off—by means of the snare-drum pulse—the signal momentarily rises at the collector and then dies away as

the charge on C20 is shunted to ground through VR12. This gives a percussive attack and a reasonable sustain; the latter being preset by VR12. If S14b is in the "Vamp OFF" position a steady DC level is maintained on C20 and this holds Tr5 permanently off. In this condition any signals from the chord generator are unaffected by the envelope shaper.

The envelope shaper for the alternating bass is similar to the emitter follower circuit used for the melody rail except that it produces a slightly larger signal (to allow for losses in the heavier filtering which is applied to it). A zener diode (D3) is used to back off the transistor's Veb so that larger signals can be applied without them appearing at the emitter prematurely.

## Last Assembly

Complete the assembly of this stage by reference to Fig. 6. Insert Soldercon sockets for IC13 and IC9 but do not insert these ICs yet. Wire in temporary links between the pole pins of S14a and b to the DC level (at the pin adjacent to R45)—this disables the Vamp and will make initial testing easier. Temporarily short out R35 to inhibit chords. Refer to Fig. 4 which shows the position of IC14 and connect a temporary link between the pin labelled "S13" and "Common". This selects the waltz rhythm. Wire VR11 and VR13 to their respective pins. Set all controls as follows: VR9 to minimum resistance, VR10 to "ground" end of track, VR11 midway, VR12 to maximum resistance, VR13 midway, VR14 midway.

Connect the power supply and loudspeaker but before turning on insert ICs 13 and 14. Take great care not to damage the pins. Double check the orientation of these two ICs (they are expensive!).

You can now apply power and should, initially, hear nothing from the loudspeaker. Depress the key marked for the chord of C or, alternatively, use a piece of wire with clips to bridge the contacts in the position of this switch. Slowly move the wiper of VR10 away from ground to produce the bass note. It will be alternating and its speed should be adjustable with VR11. There should be no percussion or sustain at this stage. Set VR10 so that there is no further increase in volume as it is adjusted. If necessary adjust VR14 for correct level.

# Final Steps

Switch off the power and remove the link between the pole of S14a and the DC level pin. Now insert a link between the pole and its adjacent pin (which carries the bass drum pulses).

Re-apply power to hear the alternating bass with percussion and sustain. Adjust VR10 to remove undesirable clicks and then set VR9 for sustain period. Try different chord selections by pressing other keys and you should find that the pairs of bass notes change accordingly.

Removing the shorting link across R35 should produce static chords—depending on the key you are depressing. Try the 7th and Minor select keys in conjunction with the selected chord.

Switch off the power and re-connect the pole pin for S14b to its immediately adjacent neighbour (carrying the snare-drum pulses). Re-apply power and you should now hear rhythmic chords interspersed with the alternating bass. Adjust VR12 for the best duration of chord sustain.

Insert IC9 and then refer to Fig. 2 in Part 2 and insert ICs 7 and 8—at the same time checking all the top side wiring links.

Board assembly is now complete and all the stages have been tested and initially adjusted. Remove all temporary leads. Remember to replace IC12 and IC19.

Next month—the final stages—assembly into the cabinet.



# To:-READERS PCB SERVICES LTD, PO BOX 11, WORKSOP, NOTTS

Issue	Project	Ref	Price P/I	P
Dec 75	Sound-To-Light Display	DN0798	1·15+12	
Dec 75	Disco System, Amp. (2 reg'd) each	AM0421	4.40+22	
Dec 75	Disco System, Light Modulator	AM0423	3.50+22	
Mar 76	CMOS Crystal Calibrator	AM0438		
Apr 76	Wobbulator	AM0443		Ē
Apr 76	Auto. Slide Synchroniser	AM0441	2.33+15	Ē
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Nov 76	Electronic Thermostat	A017		Ē
Nov 76	Cirtest Probe	A018		Ē
Nov 76	Burgiar Alarm	A019		_
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Jan 77	Icelert	A020		Ē
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<b>.</b>	Polyphon, tune disc blank, (SRBP			Ē
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Apr 77		A029/030		_
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June 77		A032		Ē
	Versatile AF Generator	A033		Ē
June 77	Tele-Games	D029		E
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July 77	Digital Clock Timer	A036		_
Aug 77	Shoot (Telegames)	D035		Ē
Aug 77	Atomic Time Receiver	D036		Ē
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Sept 77	Jubilee Electronic Organ		19.00+75	Ē
Sept 77	Electronic Car Voltage Regulator	D037	1.25+12	Ē
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Oct 77	Sine-Square Wave Generator	D040		Ē
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to READERS PCB SERVICES and not to the Editorial offices.

# DESIGN YOUR OWN PROJECTS

# CAR COURTESY LIGHT

Courtesy lights in cars can be very annoying. You get into your car at night, sit down, shut the door and the light goes out; leaving you fumbling in the dark trying to insert the ignition key! Most, if not all, of these problems can be solved by an appropriate circuit which keeps the light on for a few seconds after the door is closed—besides, this provides us with an interesting design exercise!

# **Specification**

Assuming that the car has a negative earth power supply, the circuit in the car before modification will consist of a 12V supply driving the light bulb, with a switch, operated by the door, in the positive line. We want our circuit to supply current to the light for about fifteen seconds after the switch is opened. This arrangement is shown in Fig. 1.

# Design

Well then, how are we going to set about doing this? The only way that springs readily to mind (ours at any rate) is to charge up a capacitor when the switch is on and to let it discharge when the switch is turned off. After all, most timing circuits are based on this principle! Unless we are going to become involved with relays and the like we will need a series pass transistor in parallel with the switch to turn on the light after the switch is turned off. The arrangement will be something like that in Fig. 2.

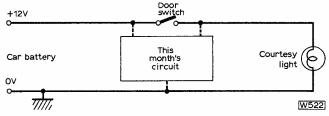
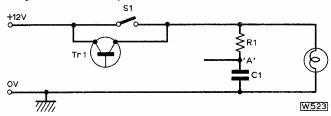


Fig. 1: Above, the normal car courtesy light plus our circuit gives a worthwhile advantage. Fig. 2: below, is the germ of the idea. Don't worry about the incomplete transistor! All will be revealed later.



RI is the resistor through which we charge up capacitor CI. We haven't drawn an emitter on the pass transistor yet, this is because we've not decided whether it's going to be PNP or NPN! Anyway, there's a slight problem with the circuit as it stands. We want

# TOBY BAILEY & BOB WHITAKER

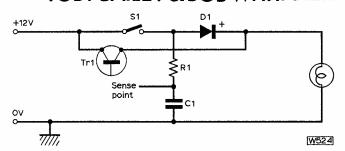


Fig. 3: The diode D1 turns out to be the critical component in this month's circuit.

Tr1 to turn on when the voltage at point 'A' reaches a sufficiently high value: we then want C1 to discharge slowly when S1 is turned off. However, C1 will charge up just as effectively through Tr1 as through the switch, so there's no way that we can discharge C1 when S1 is turned off again. Hence, with the present arrangement, the light will never turn off. Somehow we have to isolate the effects of the switch and the transistor for the purpose of charging up C1.

A small amount of thought produced the following simple modification: we insert a diode between the switch and the light, so that the transistor is in parallel with both. We then take the charging resistor from the switch side, Fig. 3. Now when the switch is closed C1 will still charge up and we can use the voltage at the sense point to hold Tr1 on. The difference now is that when S1 is off and Tr1 is on, D1 will be reverse biased and hence no current can pass through R1. This allows us to discharge C1, in some manner yet to be specified!

Having solved that problem, how are we going to fit those two 'dangling wires' in Fig. 2 together? It's fairly obvious that we're going to need another transistor and that we want it to turn off when the voltage at the sense point becomes low enough. We can then

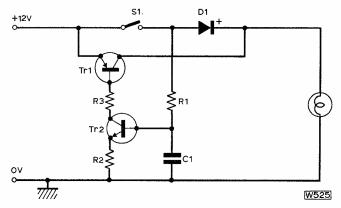


Fig. 4: A second transistor and a working circuit at last.

Practical Wireless, November 1977

# \* components

R1  $100k\Omega$  R2  $6\cdot 8k\Omega$  both  $\frac{1}{4}$  or  $\frac{1}{3}W$  carbon C1  $2\cdot 5\mu$ F 25V electrolytic C2  $0\cdot 68\mu$ F Tr1 OC35 Tr2 2N3702 Tr3 2N3704 D1 1N4001 The lamp and the switch S1 are part of the car wiring

use this transistor to control Tr1. If we use an NPN transistor here then Tr1 will have to be PNP to make them fit together sensibly, as in Fig. 4.

You can see that two additional resistors have appeared as well as Tr2. We've included R3 to limit the base current in Tr1—it should stop anything nasty happening! If we don't include R2 then C1 will be discharged very rapidly. This is because Tr2 will saturate and then pass a large current through the forward biased diode of its base-emitter junction. With R2 in the circuit the emitter of Tr2 will just float up to about 0.5V below the capacitor voltage: the current drawn from the capacitor is just the current through the emitter resistor divided by the gain of the transistor. On further consideration, what on earth do we need R3 for? The current that flows in the base of Tr1 is just Tr2's collector current; since R2 will limit this anyway we don't need R3 as well. Also, R3 would be a bit of an embarrassment if it caused Tr2 to saturate so, on second thoughts, let's dispense with it.

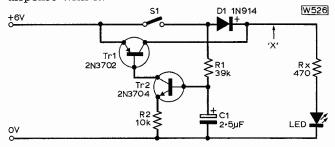


Fig. 5: The test circuit for the idea, using an LED instead of the car's lamp bulb. Note the use of a 6V supply here.

At this stage it's probably a good idea to play with the circuit on S-Dec to make sure that it works. Fig. 5 shows the circuit we assembled; the 6V supply and the LED were used merely because they were nearest to hand. This arrangement gives a good idea of the feasibility of the circuit so far developed.

 $10k\Omega$  seems a reasonable sort of value for R2, although we could have used any of a wide range of values equally well. It should keep the current drawn from C1 small and prevent excess base current in Tr1. The choice of  $39k\Omega$  for R1 is also fairly arbitrary-it charges C1 quite quickly. Rx limits the current in the LED to around 10mA. With these values the circuit works with a delay of about five seconds: so far so good. However, the light turns off rather slowly, taking a couple of seconds after the light starts dimming before it is completely extinguished. The problem is that at the turn-off point the current being drawn from C1 is very small and so everything happens very slowly. We could try sticking a resistor across C1 to increase the current drawn at turn-off but then we'd need a much larger capacitor, since it would discharge very quickly to start with. We must be able to do better than this!

Surely the way to get fast switching is to use positive feedback, i.e. regenerative switching. The only way to produce positive feedback here is somehow to connect the point marked 'X' in Fig. 5 to the base of Tr2. We don't want to use a resistor since this will mess up our biasing and the whole business then becomes very confused. What happens if we use a capacitor to provide the feedback? It certainly should speed up the switching in the critical region: as soon as the light starts to turn off the voltage at point 'X' will start to drop and since the voltage drop across a capacitor can't change instantaneously, the voltage at the base of Tr2 will also be forced down. For our first try the use of a  $0.68\mu F$  capacitor produced rather a strange result—the LED flashed a few times as it turned off. Perhaps something like that was to be expected; after all we have very nearly constructed an oscillator! With further trials we found that a  $0 \cdot 1 \mu F$  capacitor had little effect, that 0.47 produced a vast improvement in switching speed without any untoward effects and that larger values (about 2μF electrolytic) also speed up switching with no hint of oscillation. Having reached this stage it's now time to design the complete circuit for a proper light bulb; we can find the optimum value of 'speed-up' capacitor by trial and error.

A quick attack on the car produced the information that the interior light is rated at 12V 6W. From this it doesn't require much mental strain to work out that we will need to supply about 0.5A to keep the bulb alight. Of the selection of power transistors that we possess an OC35 seems to be the most suitable—

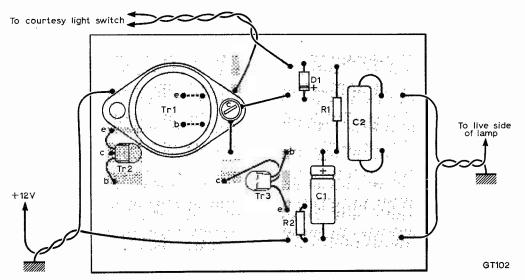


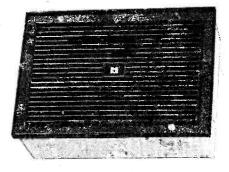
Fig. 7: The final circuit can be bullt up on a piece of stripboard as shown here. In the author's unit the board was stuck in the bottom of an aluminium die-cast box with flexible leads coming out for the switch, supply and lamp.

Practical Wireless, November 1977

# PRODUCTION bill tull

#### **Protection racket**

Not a lot to look at is it? but then a burglar alarm should be fairly unobtrusive in order that it can perform its task to the best of its ability. This latest one from ADE (Security) Co. is called the Maxi-guard Mk 4, and is designed around ultrasonics with an operational range of between 6ft and 30ft. When the device is properly set up it transmits a frequency of 40kHz, and provided there is no movement within the room the same frequency is returned to the units built-in re-



ceiver. However, if there is something in the room that moves, the frequency of the returned signal is altered (Doppler effect), activating the alarm.

The Maxi-guard operates from a 12V DC source and draws approximately 100mA. Measuring  $181 \times 126 \times 64$ mm, it can be obtained from the manufacturers for £35.00 plus  $12\frac{1}{2}\%$  VAT.

ADE (Security) Co., 217 Warbreck Moor, Aintree, Liverpool. Tel: 051-525 3440.

#### **Quartz** controlled

A rather smart looking digital clock has recently been announced by those wizards of miniaturisation—Sinclair Radionics. Finished in matt black, the Microquartz GT is primarily designed for use in the car, although it's equally effective fixed on a desk, bedside table or workbench. Fixing is by means of adhesive pads.

All time settings are adjusted by the

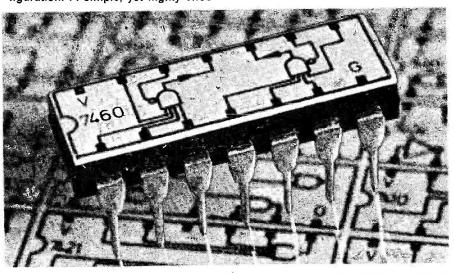
## So simple

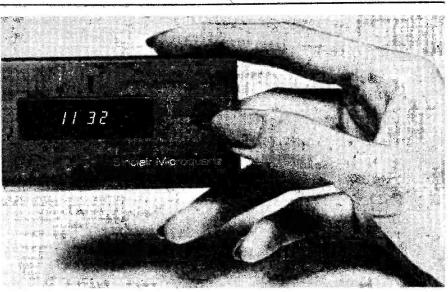
Unless you happen to possess a photographic memory, the constructor using TTL IC's almost always has to refer to data books for correct pin configuration. A simple, yet highly effec-

tive idea from Concept Electronics, is IC-size self-adhesive printed labels showing pin-outs for the 61 most popular 14 and 16 pin ICs. Aptly named Stickies, they are attached to the top of ICs and can be used for constructing and fault finding in prototypes, designing PCB layouts, fault finding on production circuits, and are invaluable as a teaching aid.

Available in sets of 450, they are packed in a re-usable plastic folder complete with comprehensive instructions. Also included in the pack is a list of equivalents which extends the range of Stickies to cover 86 ICs. Priced at £2.80 for the pack, further details can be obtained from:—

Concept Electronics, 8 Bayham Road, Sevenoaks, Kent. Tel: 0293 514110.





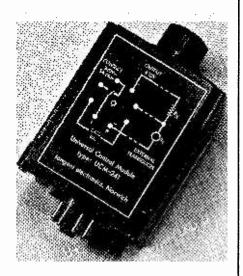
touch of a button, and as the unit is quartz controlled, it is claimed to operate for up to two years on two pen light batteries. The black anodised alloy case measures 90 x 45 x 16mm and weighs in at 3oz.

Available from the normal retail shops, the price is £12.95. If trouble is encountered in getting one, then apply direct to Sinclair Radionics, London Road, St. Ives, Huntingdon, Cambs. Tel: 0480 64646.

Practical Wireless, November 1977

#### 5-way controller

Plug it in, connect an external transducer and 240V AC and what've you got? Well you've got a temperature controller; a light controller; a variable time delay; a liquid level sensor or a touch switch. To perform any of these control functions it is only necessary to connect a transducer between terminals 5 and 6 (thermistor for temperature control, capacitor for timing control, light dependent resistor for lighting control etc.) and a resistor of similar resistance to the transducer between terminals 6 and 8. Also as this



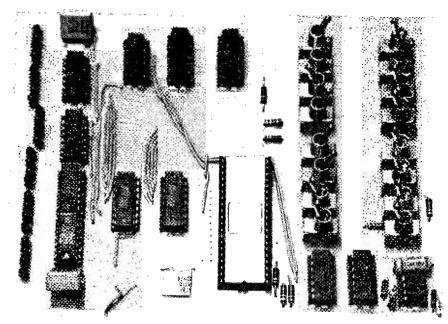
5 in 1 module operates from the mains it generates its own internal isolated supply of +10V DC at terminal 5. Called the Universal Control Module, it contains its own internal comparator and the level required is obtained by adjusting the knob at the top of the module. The internal single pole/change over contact is rated at 240V 5A AC or 30V 5A DC.

For one-off the price is £14.95 plus VAT, and for an extra £4.80 a kit containing resistors, capacitors, a light sensitive resistor, thermistor etc. can be obtained.

Tangent Electronics, 136 Whitehall Road, Norwich, Norfolk. Tel: 0603 28015.

#### **Master meter**

A new arrival from Alcon Instruments is a 20kΩ/V multimeter with claimed accuracy figures of 1.5% on DC and 2% for AC. Called the Master 20 it is available in two versions—standard



## Legal "Scrumping"?

Mention the words Microprocessor system to the average enthusiast and he'll draw in his breath and mention things like the cost of petrol going up, and food isn't getting any cheaper and that he'd like to indulge but just can't afford it. If that person is you—then read on because Bywood Electronics have launched a system, which at £55 is claimed to be more price competitive than any other system available. With the rather unusual and mnemonic name "Scrumpi" it has nothing to do with apples, but is designed for the engineer or student who wishes to obtain

experience of using and designing with microprocessors.

All parts are supplied in the Scrumpi kit, which incidentally is based on the National Semiconductor SC/MP eightbit microprocessor. The switches are soldered to the PCB by their terminals while the circuit needs a power supply of +5V and -7V and these can be derived from a single 12V supply with a five volt Zener diode. Comprehensive instructions and operating data are provided with Scrumpi along with details for the SC/MP microprocessor. Bywood Electronics, 68 Ebberns Road, Hemel Hempstead, Herts. Tel: 0442 62757

and USI. The latter model derives its name because it incorporates a Universal Signal Injector capable of supplying a 1kHz-modulated 500kHz 20V output, rich in harmonics and detectable up to 500MHz.

Both models feature a DC range capable of measuring from 100mV to 1kV and currents from  $50\mu A$  to 3A; an AC range which measures from 10V to 1kV and currents from 1mA to 3A and resistance ranges from 200 ohms to 20M ohms.

Optional extras include a 30kV probe which extends the DC voltage range for servicing TV's, 'scopes etc.

The Master 20 measures 170 x 140 x 62mm and is supplied with leads, prods and instructions. For the standard model the price is £37·15 and for the USI model £41·90. The 30kV probe is £16·95.

Alcon Instruments Ltd., 19 Mulberry Walk, London SW3. Tel: 01-352 1897.



Quite a number of monolithic timer devices are now on the market, the "555" being one of the best-known types. Although the economical 555 can provide a very wide range of delay times from about 5µs up to some minutes, it is not suitable for a long delay time of the order of an hour or a week. The problem of using an analogue timer to obtain very long delays is that the product of the timing resistor value and of the timing capacitor value must be very large. However, one cannot employ a large value electrolytic capacitor if one requires an accurate delay time, since this type of capacitor has a large tolerance in its value and the value can change with time. In addition, the leakage current of such capacitors makes it impossible to employ a large value of timing resistor.

#### The ZN1034E

A recent device from Ferranti employs an analogue timer, but the same chip also incorporates a 12-stage frequency divider. Thus the basic oscillator must pass through 4095 cycles before the timing period is terminated. One can therefore employ moderate values of the timing components and multiply the oscillator period by a large factor.

It is not usually necessary to employ an electrolytic capacitor to control the timing of the ZN1034E oscillator. Successive timing periods can therefore be repeated very accurately, to within about 0.01 per cent. Similarly the change of the timed period with temperature can be as low as 0.01 per cent per °C if the temperature coefficients of the timing resistor and capacitor are very low.

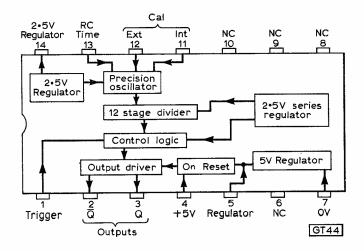


Fig. 1: Connections for the ZN1034E timer IC together with the internal circuit shown in block form.

The ZN1034E device is supplied in a 14-pin dual-inline package with the connections shown in Fig. 1, but electrically similar devices are available in an 8-pin dual-in-line and in a 10-lead circular metal can under the type numbers ZN1034P and ZN1034T respectively.

# **Power supply**

If a 5V regulated supply (as used with TTL circuits) is available, pin 4 should be connected to the +5V line and pin 7 to the 0V line. A  $0\cdot1\mu$ F capacitor should be connected directly between these pins to provide high frequency decoupling. Alternatively a supply of 6V up to 450V can be used in the type of circuit shown in Fig. 2. The positive line is connected through a dropping resistor  $R_D$  to pins 4 and 5. The internal regulator connected to pin 5 ensures that the correct voltage of +5V is applied to pin 4.

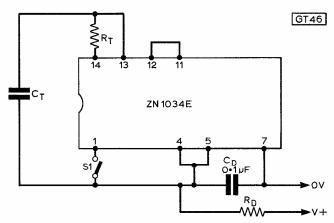


Fig. 2: The ZN1034E with its input and timing circuits and power supply connections.

The value of  $R_D$  in  $k\Omega$  is given by the equation:—

$$R_D = \frac{(V^+ - 5)}{(I+7)}$$

where I is the load current in mA. Additional decoupling may be required if the supply voltage should exceed 50V. The current consumption of the ZN1034E is about 5mA plus any current taken from either of the outputs.

# **Timing**

The timing resistor ( $R_T$  in Fig. 2) should have a value of between  $5k\Omega$  and  $5M\Omega$ , but for optimum linearity and performance, the value should be between  $50k\Omega$  and  $1M\Omega$ . The product of the values of

 $R_T$  and  $C_T$  sets the period of the internal oscillator. If the value of C<sub>T</sub> exceeds 68nF, the delay period is 2700 multiplied by R<sub>T</sub>C<sub>T</sub> if pins 11 and 12 are joined so as to bring the internal calibrating resistor of  $100k\Omega$ into circuit. Typical values of R<sub>T</sub> and C<sub>T</sub> and the time delays which can be obtained by multiplying R<sub>T</sub>C<sub>T</sub> by a large factor are shown in Table 1.

The value of  $C_T$  should exceed  $0.01\mu F$  for optimum performance; although smaller values may be employed when the timed period must be short, the period is then not linearly related to R<sub>T</sub>C<sub>T</sub>. The minimum recommended value of C<sub>T</sub> is 3·3nF. For very long delays, electrolytic capacitors are convenient, but they do not provide such accurate timing.

	MING ONENTS		2736R <sub>T</sub> C <sub>T</sub>	PERIOD 7500R <sub>T</sub> C <sub>T</sub>
C <sub>τ</sub> (μF)	R <sub>T</sub> (Ω)	R <sub>T</sub> C <sub>T</sub>	(Pins 11 and 12 joined)	(300Ω from pin 12 to earth)
0·01 0·1 1 1 10 10	39k 220k 100k 1·2M 1·2M 3·3M 2·2M	0·39ms 22ms 100ms 1·2 sec 12 sec 33 sec 220 sec	1 sec 1 min 5 min 54 min 10 hours 1 day 1 week	2·91 sec 2·74 min 12·5 min 2·5 hours 27 hours 2·7 days 2·7 weeks

Table 1: Giving various values of R and C that can be used with the timing circuit of the ZN1034E.

An internal calibration resistor of  $100k\Omega$  in value is connected in circuit when pins 11 and 12 are joined; the delay time is then equal to about 2736R<sub>T</sub>C<sub>T</sub>. If, however, an external calibrating resistor of  $300k\Omega$  is connected between pin 12 and earth (pin 7), the timed period is 7500R<sub>T</sub>C<sub>T</sub>. The multiplying factor can also be fixed at 2500 by the use of a  $50k\Omega$  resistor between pin 12 and ground or at 4100 with a  $150k\Omega$ resistor.

# Measuring the period

The basic oscillator period can be measured by connecting a probe to pin 13, but the probe impedance should not be less than 10R<sub>T</sub> or it will cause a considerable change in the period of oscillation. For short

times the output from this pin should be viewed on an oscilloscope, but for long times a stop watch is convenient. The total delay time is 4095 times the period of the oscillator. The measurement of the period of the basic oscillator is much quicker than the measurement of the whole of a long timed period at the output of the frequency divider circuit, but the measurement of the total timed period at the output will normally provide a more accurate value of this period.

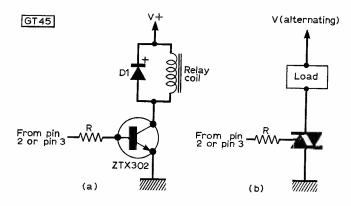


Fig. 3: Two types of output circuit suitable for the timer.

## Starting up

The timing in a ZN1034E circuit may be started by joining pin 1 to earth by closing the switch S1 in Fig. 2 for a moment. The timing process is then unaffected by any further operation of S1. Alternatively, if pin 1 is earthed, timing will begin immediately the power is first applied to the circuit.

# Output circuit

Two complementary outputs are provided from the ZN1034E. The output at pin 2 is normally at a low voltage, but rises to +3.6V at the end of the complete timed period. On the other hand, pin 3 is normally at a 'high' voltage, but this voltage falls from about +3.0V to a 'low' value at the end of the

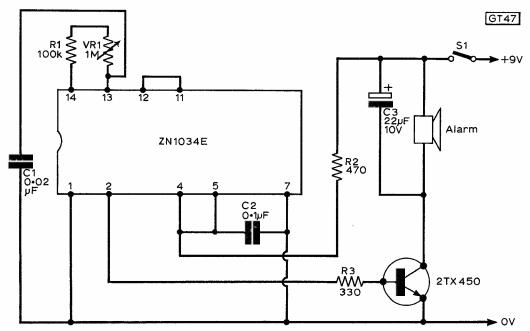


Fig. 4: Here the timer is used in an alarm circuit which can provide delays from 1 to 11 minutes. The transistor type should be shown as ZTX450.

is Phinone

W. Jordan

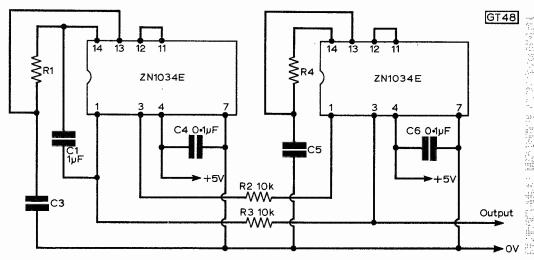


Fig. 5: Two ZN1034E chips are used here to extend the timed period to a week or more.

timed period. Either output can deliver or accept up to 25mA.

A typical output circuit for the operation of a relay is shown in Fig. 3(a). At the end of the timed period, the output from pin 2 rises in voltage and this causes the ZTX302 NPN transistor to conduct. A current therefore flows from  $V^+$  through the relay coil and the relay closes. The  $V^+$  supply in Fig. 3(a) is chosen to suit the relay used. The diode D1 suppresses transient voltages developed in the relay coil and hence protects the ZTX302 transistor.

If the resistor R of Fig. 3(a) is connected to pin 3 of the ZN1034E instead of pin 2, the relay will be closed during the timed interval and will open at the end of the interval. The resistor R of Fig. 3(a) must limit the current flowing from the ZN1034E output to a value no greater than 25mA. A value of a few hundred ohms is suitable with a minimum value of about  $150\Omega$ . Fig. 3(b) shows how the output from a ZN1034E can be used to control a triac device which itself switches the power to a load on or off. As before, R must limit the ZN1034E output current to 25mA.

#### Minute timer

In Fig. 4 the product  $R_{\rm T}C_{\rm T}$  can be varied from  $0\cdot02$  to  $0\cdot22$  second by increasing VR1 from 0 to  $1M\Omega$ . When multiplied by the 2700 factor, times of 1 to 11 minutes can be obtained. Timing starts when S1 is closed and power is applied to the circuit. The alarm sounds at the end of the timed period and continues to sound until S1 is opened. A suitable alarm is obtainable from Doram Electronics Ltd.

# Repetitive timer

The circuit of Fig. 5 shows how a second ZN1034E can be started at the end of the timed period of the first device. At the end of the period timed by the second device, the timing process is started again in the first device. Thus this timer circuit continues to operate with each device working in turn. The output from pin 3 of either device provides the signal through R2 or R3 which begins the timing in the other device. Thus one has an oscillator with a period which can exceed a week!

A wide selection of other circuits is included in the ZN1034E data sheet including (i) a battery charger

which can accurately charge nickel-cadmium cells for a known period at a known current (ii) a metronome (iii) a timer for periods of 1 minute to 1 hour (iv) a 0 to 1 hour industrial timer with suppression against noise pulses (v) a delayed windscreen wiper motor control for vehicles (vi) the use of two ZN1034E devices in cascade to obtain a very large pulse division factor and hence delays of up to a year with an accuracy of 6 minutes after calibration. Other applications include the use of the device on farms for watering, etc, at the required times.

# KINDLY NOTE!

# ATOMIC TIME RECEIVER August 1977

The author has kindly supplied further information on the coil assembly T1. An alternative to the one specified can be obtained from Hawnt Electronics Ltd., 112 Pritchett Street, Birmingham B6 4EN. This is the 10mm Vinkor LA2936 comprising parts: LA1421 pair of cores, LA1383 adjuster, DT2169 coil former, DT2341 ring, DT2342 clip (4 off) and DT2344 tag board.

The windings required are, Primary: 110 turns of 40 SWG enamelled copper wire. Secondaries: two of 20 turns each centre tapped. There are suitable holes in the PCB for this alternative assembly.

# PLEASE MENTION PRACTICAL WIRELESS WHEN REPLYING TO ADVERTISEMENTS





#### by Eric Dowdeswell G4AR

Not too many reports this month, with just about everyone away on holiday I suppose. With the appalling weather we are having in the south I thought that a lot of you would have been tied to your sets instead of looking after the leeks! Weather or not, it seems that quite a few of you have been doing the rounds of the rallies and other "do's".

Tom Learmonth of Cwmbran, Gwent, tells me in his first letter to the column that he has now passed his RAE. Congratulations Tom, but I have to remark that it is usually the other way round! Letters first, pass the RAE, and not another word! Tom is not too keen to get the code test over and done with although I have advised him otherwise. He is anxious to get hold of a secondhand transceiver for the 2m band, possibly for mobile work, so any offers to Tom at 10 Glade Close, Coed Eva, Cwmbran, Gwent. Incidentally, Tom studied entirely on his own for the RAE and now his Dad is thinking of having a go!

From Hastings, **Brian Harrison** has stuck to the job in hand and covered 10, 15 and 20m on SSB while **Robin Bayley** A9203, up in Kemberton, Shropshire, patiently awaits his RAE course to begin so that he can take the exam next May. In the meantime he is using his EC10 and Marconi R1475 to good advantage from 15 to 80m.

John Tye G4BYV writes from Dereham, Norfolk, concerning the lads who work continental stations via repeaters and then ask for a QSL! Frequently they have only worked over a couple of miles! John spreads his time over a wide range of bands from 2m down to 23cm where he has worked 107 different stations in 9 countries! A very creditable achievement that really means something, and all with home-made equipment.

From Trowbridge, Wiltshire, comes a complaint from David Birch, aged 13, who is fed up with QRM from TV sets, pointing out that according to the TV licence the "apparatus" is not supposed to interfere with other "wireless telegraphy" equipment. You are quite right Dave, but just try to get someone to do something about it! I read recently that there is a possibility of legislation in the US on this matter but I hate to think how long it will take to get it into law and then to implement it. Pity it wasn't done at the beginning, but there, it costs money! Only hope is to try screened twin feeders properly matched and to keep the set and the aerial as far from the source of QRM as possible.

J. Hodgson of Morpeth, Northumberland, comments on some strange calls heard in the "10m" band but I fear that these are rubbish from the adjacent 11m band! Unfortunately, with the improving conditions on the

higher frequencies, we shall be able to hear more and more of the overseas Citizens Band stuff.

The organisers of the Worked All Britain Award have now introduced the WAB Counties Award which is also available to listeners. It is issued in two classes, depending upon the number of counties worked/heard. QSLs are not required. A record book to facilitate the "book-keeping" is really a must for this sort of award. Full details from Alec Brennend G4AVA, 76 Deneley Avenue, Todmorden, Lancs. Incidentally, as an added incentive to have a go, all profits from WAB activities go to the Radio Amateur Invalid and Bedfast Club.

Club News. The newly formed Brighton and District Radio Society is well under way and forthcoming events include a talk on Computers by G3XJG on October 12 and on the 26th G3OEM will discourse on Aeronautical Radio matters. Info from the Hon. Sec. Nigel Hewitt G8JFT, 74 Carlyle Street, Brighton.

The Cheltenham ARS and the local RSGB group have investigated the possibility of forming a single club and the likely date for the first combined meeting is November 3. Let's hope the move will be beneficial to all concerned. Further info from **Derek Lively** G3KII, 26 Priors Road. Cheltenham.

The very active Wessex AR Group has its AGM on October 7 and on the 21st they will be reviewing the results of their efforts in the VHF NFD. Several members were successful in the last RAE. It is expected that at least a dozen will start the new course at the Bournemouth College. Further info on the Club from Geoff Cole G4EMN, 6 St. Anthony's Road, Bournemouth. Meetings in the Club Room at the Dolphin Hotel, Holdenhurst Road, Bournemouth, 7.30 p.m.

Several readers have queried the new prefix P28 now being heard on the bands. This is the Republic of Djibouti previously using FL8 as a French colony. The series starts with J28AA so it's a bit difficult to tie up old calls in use with the new ones.

From Adlington, Lancs, comes a letter from Paul Farnworth who is listening and working for the RAE, "then I will leave school and try to get a job". Paul is 15 so let us hope that his plans work out. John Overton writes from Glasgow with some nice log entries on CW. He is very frustrated at not being able to answer back but perhaps it will not be for much longer as he is taking the RAE in December. His BC348 only goes to 18MHz so he's thinking of making another set for the 10 and 15m bands. Once again I must point out that a converter is the proper answer. Why not use all the other facilities you have in the 348, John? No point in duplicating them, and you are not likely to get hold of a better dial movement!

Radial, the journal of the RAIBC, reports a healthy growth in the Club membership and activities and a few volunteers are needed for jobs such as Equipment Secretary, Shows and Rallies Manager, Tapes Manager and a Transport Manager. It is not generally appreciated just how much work is involved in the transporting of gear to and from the invalid and bedfast members of the Club, apart from the odd servicing and maintenance chore.

Anyone interested in helping a most deserving cause can contact Harry Boutle G2CLP at 14 Queen's Drive, Bedford MK41 9BQ.

A report from Alan Doherty BRS34968 in Portrush, Co. Antrim, just made the dateline. A rare call these days logged by Alan was Libya in the form of K5CO/5A. Not much activity there since the Forces moved out. Alan says not to be fooled by those CY calls, just read VE instead! Two other nice ones that one can go for many years without hearing were VR4DX and VR6TC, Tom Christian on Pitcairn.

Log extracts

- J. Hodgson:— 20m FG7XL JW7BK J29AI OJ0MA YB2SV 5W1AU 15m HK3AMV HR6SWA
- J. Tye:— (G4BYV) worked on 23cm (1296MHz) DF8QK DK3UC PA0FWS PA0VTW PA0EZ ON6AT SM6ESG
- R. Bayley:— 80m A2GCO CT2AP KP4EJA VE4BC 40m HK0COP JA4AKU 15m VE7DIY 7P8BC
- HK0COP JA4AKU 15m VE7DIY 7P8BC

  B. Harrison:— 20m F0CH/FC 15m HM2JV JA1PPC 10m
  7X2DG
- A. Doherty:— 80m FG7AN ZS5LB 20m K5CO/5A TU2GA-VR4DX VR6TC W60KJ/KS6 ZD7SD 3D2AN, 5W1AU 15m WA4RQK/VQ9 ZD8RR 5N2AAX
- J. Overton:— 20m A9XBC C31A SV1GR TG9DF VP2AA VP1WS

All calls are SSB except those in italic which are CW.



# SHORT WAVE BROADCASTS by Charles Molloy G8BUS

Solar activity is on the increase according to the Swiss Shortwave "Merry-go-round" which regularly broadcasts the latest sunspot number and gives predictions, which are obtained from the Zurich Observatory. Forecasts of the number of sunspots for the coming months show a gradual rise from 27 in October to 33 in January 1978 and this upward trend is reflected in reports of DX on the higher frequencies. The writer has been listening recently on Sunday mornings at 0840 to the DX programme from Radio Australia on the new frequency of 21570kHz in the 13m band. Although beamed to Asia this transmission comes in better in the UK at this time than the frequencies in the 25m and 31m bands that are beamed to the UK.

Harold Emblem who DXes in Mirfield, in Yorkshire, reports hearing the afternoon transmission of "Sweden Calling DXers" on a new frequency of 21690kHz. HCJB in Quito Ecuador is also on a new 16m channel of 17755kHz, Radio Australia is on 15140 and 15410 in the 19m band and Radio South Africa is on 17780. Harold asks what sort of information should go into reports to this column. The exact frequency (if known) plus the date and time of reception will help readers to search for the station and some information of the gear used and the aerial will help those who intend purchasing or building a receiver or are thinking of putting up an aerial.

An interesting report comes from **Derek Taylor** of Preston in Lancashire who uses a Realistic DX160 receiver, a calibrator and a 30ft. loft aerial when operating on the shortwaves. He reports hearing the International Service of Radio Nacional de Venezuela in English at 2200 on 15400 and he received a confirmation letter from them after one month. Radio Korea (Seoul) was heard in English at 1330 on 11860kHz and the Voice of Nigeria outlet at Benin on 4932 in the 60m band was logged at 2100.

A newsletter has been received from the Bristol Path-

finder DX-Group. This club has about 20 members, mostly in the Bristol area, but DXers from anywhere in the UK are welcome. Enquiries should go to Lawrence Bennett, 7 Maple Avenue, Fishponds, Bristol BS16 4HJ. D. M. Tinker is a keen DXer who would like to know if there is a DX club in the Rotherham or Sheffield areas. Reply please to 20 Croft Road, Brinsworth, Rotherham, S Yorks S60 5AP.

Roger Fitzpatrick of Roscrea, Co. Tipperary and his friend Sean Keevey recovered a couple of old Pye 5-valve receivers from their respective lofts and were surprised, after blowing away the dust, to pull-in between them the following DX:—The Voice of Vietnam on 10040kHz at 1807, Nigeria on 15220 at 1615, Radio Australia on 9570 at 0800. "Have you any information on Radio Rodina?" asks Roger. Radiostantsia Rodina (Radio Station Homeland according to the World Radio Handbook translation) is not a radio station but a radio programme. It is in Russian and is carried by the external service of Radio Moscow and is intended for Russians living abroad.

Michael Walker (BRS 38836) has been listening to Radio Baghdad and he would like to know the address of this station. Write to:—Iraqi Broadcasting and TV Establishment, Salihiya, Baghdad, Iraq. Frank Hannam sent in a log from Colne in Lancashire. Using a Fidelity Rad 21 and a 35ft inverted-L aerial he heard the Voice of Turkey on 9515kHz at 2210 (there is a DX programme nightly at 2230), Radio Australia on 21570 at 0815 and Radio South Africa on 21535 at 1400. Frank has just been given a big box of valves and he is looking for details of a valve receiver to build.

Can you suggest a good aerial for indoor use, asks Ian Radford (Derby) who reports hearing Radio Australia on 9570 at 0800 and RSA on 21535 at 1700 with his Eddystone EC10 and whip aerial. You seem to be doing very well at the moment, Ian! Why not try the TV aerial? Unplug it from the TV and connect the co-ax lead to the EC10. If results are good then you can get hold of a 2-way outlet with switch from a TV dealer and switch the aerial to either the TV or the EC10 as required. Do not join all three, the TV the EC10 and the aerial together, they may not get on with one another!

"Just received a QSL card from Radio South Africa (on 21535) so it looks like the high bands are coming back" writes **W. G. Holmes-Jones** from Abergavenny, in Gwent. He uses a R209 and a home-brew 16-transistor receiver for the broadcast bands together with the choice of a Joystick, 84ft loft aerial or 45ft longwire plus an ATU and a tunable notch filter. The highlights of a very comprehensive log are Radio 4VEH Haiti on 9779 at 1130, Radio Finland 15260 at 1300 in English, Radio Australia 9570 each day at 0700 but it gets lost before scheduled sign-off at 0900 (try 21570), Radio Iran 17730 at 1930 in English, The Voice of Greece 9760 at 2200, Radio Mozambique on 6115 at 1800. Radio South Africa was heard on 15220 at 1345 with its weekly Wednesday DX programme

"I have acquired an ex-RAF R1155 receiver which I know you are familiar with" says Alan Spencer who lives at Ryhall, in Lincolnshire. When connected to a 45ft long wire it produced ELWA Monrovia, Liberia, on 4770 at 2230 and Radio Nacional Espejo, Ecuador, on 4680 at 0355. Two resistors have now burnt out and Alan is unable to get hold of a circuit or manual. A. J. Brooks, 5 Farrant House, Winstanley Road, London SW11 2EJ can supply diagrams and manuals for most ex-WD and some other communications receivers. An SAE will bring a list, The paper decoupling capacitors in the R1155 are liable to leakage and it is worth doing what the writer did with his and replace the lot with modern  $0 \cdot 1 \mu F$  350VW capacitors. If a decoupler does short circuit then a burnt out resistor may follow. An old dodge for testing decouplers is to connect the positive lead of a voltmeter to the HT line, disconnect the wire from the live side of the decoupler and tap-on the negative probe from the voltmeter in place of the wire just removed. A good capacitor will give a kick on the meter as it charges and the needle will then go back to zero. A leaky capacitor may give a kick and the needle will return slowly to some intermediate reading

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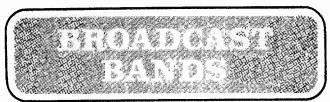
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Practical Wireless, November 1977

caused by the current leaking through it. A steady reading on the meter equal to the HT volts indicates that the capacitor is short-circuit and will have to be replaced. Be careful to have the meter switched to the appropriate voltage range (to measure the HT volts) or it will have to be replaced as well!

A large mailbag this month has meant that some letters are being held over to next month. My apologies to those concerned.



#### MEDIUM WAVE DX

## by Charles Molloy G8BUS

"Readers will think I am mad, from your remarks about me in the July issue" writes Harold Brodribb from St Leonards-on-Sea, who has taken up the challenge of DXing with vintage radio receivers. "I am getting good results with pre-war sets provided they are maintained well and used on this high site with an outdoor aerial and ATU." Harold mentions that his CR100 has many advantages over vintage equipment. He has changed the RF valves for quieter types (the writer used 6BA6) and fitted an Smeter and a stabilised voltage supply for the oscillator. He has adapted the BFO valve to perform a dual function as BFO and product detector. The writer used the CR100, also known as the B28, for MW DXing for a number of years. Even unmodified it is a very good receiver though it too, could now almost be classified as vintage. A large number of CR100s came on the surplus market after the last war and they can still be obtained privately for quite a modest sum. They have an internal power pack and can be run direct from 240V mains. They are not too bulky, rather heavy, like most ex-WD equipment. An external speaker is required though there is space to fit one inside the metal cabinet.

A useful report of Spanish DX comes from Declan O'Dea who lives in Ballinasloe, Co. Galway. With a 10-transistor domestic portable he logged La Voz de Madrid on 1097kHz, R. Espana Madrid on 917, Radio Madrid on 800, R. Zaragoza 872, R. Valencia 1259, R. Sevilla 809, R. San Sebastian 1025, R. Centro Madrid 1385, R. Popular de Jerez 1385, R. Reloj Barcelona 1124 and La Voz de Gerona on 1385. From North America WINS on 1010 was logged at 0300 and there was an unidentified VOA transmission on 1295 which would be from the 600kW BBC transmitter at Crowborough in the UK. Declan would like to contact other PW readers in his area. The address is c/o Bank of Ireland, Society Street, Ballinasloe, Co. Galway.

John Little writes from Sunninghill, Berks, to say he was interested in the reference in the July issue to DXing the Middle East. He has just spent two years in Iran where DXing Europe prior to going to work at 0430 was great fun! With local stations not yet on the air, being 3½ hours ahead of London, the BBC frequently came through on 200kHz, 647kHz and 908kHz both on the built-in rod aerial and on an outside inverted L. A further illustration that it is interference (QRM) rather than distance that limits the range of DX on the medium waves.

A Realistic DX160 receiver, a MW loop and a 250ft long wire from the house to a 25ft pole at the bottom of the garden is used by Martin Liezers who lives in Newport, in Gwent. DX heard with this set-up between midnight and 0300 included La Voix de la Revolution, Conakry, Guinea, very strong on 1403kHz; CJON St John's, Newfoundland on 930; WNEW New York City on 1130 and an unidentified with the call KB Radio on 1520. The latter is WKBW in Buffalo NY and the complete call will be used in the formal identifications on the hour and the half-hour. Many

stations try to form slogans out of their call signs and some of these will mislead the newcomer. KLOK is "Clock Radio," WIOD is the "Wonderful Island of Dreams" (Miami), KYAK is in Alaska, and there used to be a KOLD in the same territory at one time! Some call signs may help the DXer. WNEW is in New York, WBAL is in Baltimore, WBOS in Boston, WCBS is owned by the Colombia Broadcasting System, WNBC by the National Broadcasting Company and WINS was the International News Service. There are no prizes for guessing what can be heard from WPOP and WFUN!

Martin raises a couple of interesting points in his letter. He mentions "a lot of crackles which disappear at dawn" and he asks what precautions can be taken to protect the house if his long wire is struck by lightning! Static, QRN, atmospherics, are the names given to the noise heard by Martin and each crackle is caused by a lightning discharge. Since the static disappears at sunrise it must, like DX, have been propagated for quite some distance. During the summer, thunderstorms in the tropics create a considerable amount of static which travels as far as the UK after dark and, although not loud enough to interfere with local reception, it can be troublesome to the DXer. A loop will reduce static provided that the DX and the static are not coming from the same direction. Summer static is usually from the south of the UK but it can come from other directions as well.

The advice about lightning protection usually offered in radio books is that the aerial should terminate at the point of entry to the building, on the moving contact of a knife switch. The upper contact goes to the receiver and the lower to a good, short, outside earth.

Summertime ends on October 23 this year in the UK and the return to GMT will mark the start of the winter season for North American DX. It will then be possible to listen to Canada and the USA before midnight and on nights when conditions are good some DX should be heard as early as 2300. The nearest, most consistent and earliest station to appear is CJON, located in St John's Newfoundland, which transmits with a power of 25kW on 930kHz. It can be found just on the low frequency side of AFN Berlin on 935. DXers who have never heard North America on the medium waves should try for CJON. Another regular is WINS in New York City on 1010kHz which is reasonably clear of QRM once the Dutch station on 1007 leaves the air, usually around 2300.

All North American medium wave stations use call signs which are mentioned over the air frequently. The prefix C is used on Canada and either a W or a K in the United States. All stations are on channels which are multiples of 10kHz. The best DX is often heard after midnight but quite a number of stations appear earlier whenever conditions are good. Tune slowly, as all these broadcasters suffer from slow fading and are easily missed. If unsuccessful, try again a few days later. If conditions are poor one night they will probably pick up again before long.



#### by Ron Ham BRS15744

Several contributors have expressed their pleasure at our journal's new format and the start of a series about taking the RAE. Nigel Golds BRS36910 West Chiltington, Sussex, leads his report with "I am pleased that there is a series which will help me with my studies for the RAE". Like many others, Nigel is a keen listener on 10m and has heard the DLs, OKs, Fs, and Gs as well as the German beacon, DL0IGI, during the periodic short skip openings in August.

While on a "junk" crawl, in aid of my early wireless

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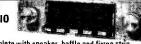
(£34 PER PAIR + p & p £6.50 Duo III, 20 watts rms, 40 watts peak,  $27" \times 13" \times 11\frac{1}{2}"$  (approx.) (£52 PER PAIR



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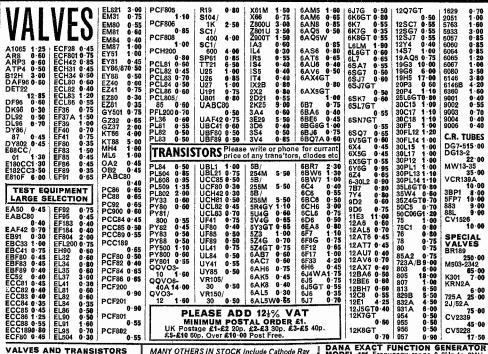
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collection, I met Vic Elliott BRS37850 Midhurst, Sussex, who emphasised his delight about the RAE series and explained, that as an ex-RN morse instructor, he is now brushing up his basics for the next exam and plans to become active on the HF bands. Later, I called on Gordon Goodyer BRS37345 Petworth, Sussex, a PW reader for many years, who said that he likes the new format but the increase in size upsets his very tidy bookshelves! Gordon spends a lot of time listening on 10m with his CR100 and dipole and on 2m with his home-brew frontends, indulging in his special interest of making and testing VHF ground plane aerials.

A period of solar activity began on July 23rd and ended on August 5th during which time our extra-terrestrial observers monitored the event. John Smith, Cranleigh, Surrey, recorded two definite peaks in the solar noise output at 142MHz, the first started on the 23rd, reached it's peak on the 28th, and returned to normal on August 2 when it rose again to a climax on the 5th and down again by the 10th. In both cases the maximum was about four times the normal level. While the noise was fluctuating, both John and I recorded a host of individual solar bursts, each lasting between one and five minutes, throughout the event. Cliff Ranft, Chilworth, Surrey, found evidence of ionospheric disturbance on July 29th and 30th and he recorded a moderate SCNA (Sudden Cosmic Noise, Absorption) between 1410 and 1510 on August 5th.

Although cloudy skies prevented systematic use of the optical instruments, John Smith did manage to see a sunspot group on July 26th, and Cmdr. Henry Hatfield, Sevenoaks, using his spectrohelioscope, observed a variety of sunspots between August 1st and 4th, in addition to several small filaments and plages. On August 1st and 2nd Henry saw a bright prominence on the sun's east limb and his records show that each time he sees one of these events we all record some form of radio noise at metre waves. Henry counted five sunspots, plus two plages on the 9th, I received bursts of radio noise at 136MHz on the 10th and on the 13th John Smith noted that the solar noise level was up, and Cliff Ranft again found evidence of an ionospheric disturbance.

According to my observations the cause of the disturbed conditions on the 4th was due to a mixture of tropo, due to the falling pressure noted by both Ciaran and myself, and sporadic-E which manifested itself for most of the morning. At 0913 I received a 599 signal from the 70cm beacon at Sutton Coldfield GB3SUT, a strong picture from Lichfield on Ch. 8 and good signals from ten continental broadcast stations in Band II. At the same time, the influence of sporadic-E ranged from 40 to 73MHz, bringing a host of continental signals into the UK in Band I plus 14 east-European broadcast stations between 66 and 73MHz.

Although the tropo-lift was waning I received 59 signals from F1ENH and G8FAS in Somerset, via the London repeater, GB3LO. Sporadic-E occurred again on the 5th and was most intense at 0910 when I received very strong signals from 46 east-European stations between 66 and 73MHz in addition to sync. pulses on R1, 49·75MHz and a crop of continental stations in Band I.

The falling barometer indicated another tropo opening on August 10 and 11th. At 2300 on the 10th Alan heard a GM station just above the noise on 2m and at 2355 he worked G8JJR near Doncaster on SSB and while he, at the east end of Sussex, listened to a mobile north of Darlington, via the Cambridge repeater, GB3PI. Your scribe, located at the west end of the county, listened to the Bristol Channel repeater GB3BC and it's "Bing-Bong" code, which must be familiar to our GW readers under normal conditions. I am told that the original aerial at the Brighton 70cm repeater GB3BR 433·15MHz has been changed for an improved colinear. G8LGQ who lives to the east of the repeater, with 400ft of chalk in the way, is getting a much better signal than before. Further reports to me or to G8HVV, QTHR.

I received a reasonable signal from GB3SUT from 0050 on the 10th to midday on the 11th, and at 0740 on the 11th I heard the Emley Moor beacon GB3EM 432.910MHz

at 559. Slight tropo-lifts produced signals from GB3SUT on 70cm during the early mornings of the 13th and 16th; more reports about 70cm activity would be welcome.

Interest in our microwave reports is growing and a most welcome letter from Sam Jewell G4DDK, Stone, Staffs, who says there is some dozen stations active on 10GHz from Birmingham in the south to Manchester in the north and that there is some activity most weeks between various stations in that area. A typical path recently covered was Mow Cop on the Staffordshire-Cheshire border to Winter Hill in Greater Manchester, a line-of-sight distance of 59km. On this occasion G4DDK, G8ANZ and G8BHH were at Mow Cop and G8AXE with G8AFC on Winter Hill.

The type of equipment being used in the Midlands is typical of modern wideband FM gear for 3cm; a 12mW Gunn diode transmitter to a 16in dish and a separate tunable Gunn diode/Sim-2 mixer as receiver with a 106MHz IF, resolved on an FM broadcast receiver. I know just how good this equipment has to be because I spent part of Sunday, August 21st on the Trundle, a hilltop some 675' ASL, just north of Chichester, Sussex, with Colin Boys G8BCO, Peter Kerry G8ARO and David Bookham G8JNI to see their respective 10GHz stations as they prepared to take part in the RSGB's 10GHz Cumulative contest.

The extreme neatness of each station was impressive. The aerials and the electronics are compact, mounted on sturdy tripods with provision for precise adjustments in both altitude and azimuth. At one time, Colin removed his 18in dish and demonstrated that he could just receive the 10·1GHz beacon GB3IOW St. Catherines, Isle of Wight, on open waveguide proving that he had the full 30dB gain of the dish in hand on that signal. It did not surprise me when I learnt that Colin's microwave gear won him the award at the construction contest organised by the Farnborough and District Radio Society. Peter was using a 12in dish, giving him 24dB gain on his receiver and a 14dB horn on his transmitter. At 1300 a 599 signal from GB3IOW was booming from his receiver and he demonstrated just how critical the direction is; in fact he lost the signal by moving his aerial just 112in! David's receiver consists of a balanced mixer (pair of 1N23s) into a 40673 mosfet preamp at 100MHz (IF) and then to Mullard modules. His transmitter is a 160mW Gunn diode and his aerial an 18in dish. David also received the beacon signal and a strong signal from G3KSU/P at St Catherines. Each station had two-way contacts with G8BDJ/P Chanctonbury Ring, Sussex and G3IZD/P Lynch Down, Sussex. The climax of their day came at 1800 when G8BCO/P had a 55 contact with GU3JHM/P on Alderney and G8ARO/P had a 59 contact with the Alderney station. Peter told me later that several other UK stations had made it to the Channel Islands on 3cm that afternoon.

The Microwave round table meeting held on August 7th in Winchester was very successful and well-attended in view of the short notice, which goes to show that once again the amateurs are prepared to experiment and pioneer those difficult signal paths. To help them, the 3cm beacon at Alderney GB3ALD is now active and its signals have already been received on the Trundle, a distance of 167km. I understand that several of the microwave boys are planning to get going on 24GHz and I will certainly look forward to receiving their reports for this column.

Reports on the various bands are welcome and should be sent direct, by the 15th of the month, to:-

AMATEUR BANDS Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey KT21 2TW. Logs by bands, each in alphabetical order.

MEDIUM and SW BANDS Charles Molloy G8BUS, 132 Segars Lane, Southport, PR8 3JG. Reports for both bands must be kept separate.

VHF BANDS Ron Ham BRS15744, Faraday, Greyfriars, Storrington, Sussex RH20 4HE.

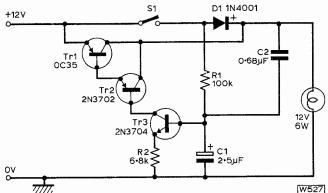


Fig. 6: The final circuit with all the snags ironed out, giving a sharp turn-off to the light, which now remains on for about 15 seconds after the car door is closed.

this is a 30W type so we shouldn't blow it if we use it as the series element. Its gain is given as 25 to 75 at 1A, so let's take a minimum of 20, which means that the base current will need to be 500/20=25mA. If we try to supply all this current from one transistor then the current drawn from C1 will be too high; the easiest way out seems to be to reduce the base current that needs to be supplied, by making the pass element a Darlington pair. The circuit will then look

The 2N3702 and 2N3704 transistors have been kept since we were using them in our experiments before. Previously the timing period was a bit short but this should go up with increased supply voltage—we can always make C1 bigger if the delay is still too small. R1 has been doubled in value since the supply voltage has been doubled, although this isn't really necessary. D1 can be any diode capable of taking 0.5A with a maximum reverse voltage of about 20V-a 1N4001

should be fine. Silicon types must be preferable here, since we don't want any problems with leakage currents through D1, keeping C1 charged. What value do we need for R2? Well we want 25mA of base current for the OC35 and a catalogue tells us that we can rely on a gain of at least 50 from the 2N3702: this means that the 2N3704 has to supply 500 µA, at least until the voltage across C1 is down to 3V or so. A  $6.8k\Omega$  resistor should be OK here; it gives a safe limit to the maximum current that Tr3 can supply.

It would be good practice normally to put a resistor from the emitter of Tr2 up to the +12V line. This stops the Darlington pair doing funny things at low currents. However, we're not involved with low currents here so we'll not bother with this resistor.

It is not entirely obvious what effect changing the load will have on the optimum value for C2, so we'll try 0.47 pF again and see what happens. We can do this final experimenting when we've built the rest of the circuit on a piece of Blob Board. With the circuit wired up we find that the courtesy light, temporarily excised from the car, stays alight for about fifteen seconds and then turns off. As for C2, the turn-off seems fast and very stable: yet again  $0.1\mu\mathrm{F}$ appears to be not quite enough but  $0.47\mu F$ ,  $0.68\mu F$ and several larger values that we tried all speed up the switching, with none of that embarrassing flickering that we had before, so let's settle for  $0.68\mu F$  as the final value for C2. A practical layout is shown in Fig. 7.

The output levels and the output impedances of things like cassette recorders don't always match the associated amplifiers so next month's design is for a simple matching circuit.

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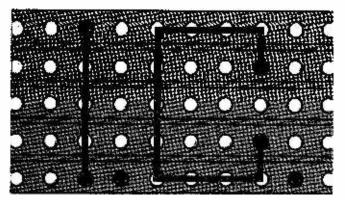
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Practical Wireless, November 1977



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November issue on sale Friday 7 October 45p

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	D63	-30	EC53	1.00	EL34	1.25	KT66	3.00	PEN45	on n	UF89	-52	AAZ13	·21	BF180	-35
	DAC32	-80	EC54	1.00	EL37	3.00	KT71	1.00	1 10140	2.00	UL41	70	AC107	18		
	DAF91	35	EC86	-84		57			DENTE						BF181	47
					EL41		KT81	5.00	PENDI		UL84	.54	AC113	-30	BF185	47
	DAF96	-60	EC88	-84	EL81	70	KT88	6.75	4020	T-00	UM80	-60	AC126	·14	BFY50	-26
	DC90	70	EC90	-50	EL83	70	KTW61		PFL20		UY41	50	AC127	-20	BFY51	.23
	DD4	-80	EC92	-55	EL84	-35		1.50	PL33	1.00	UY42	-50	AC128	26	BFY52	23
	DF33	.75	EC97	.75	EL86	-80	KTW62		PL36	-60	UY85	·35	AC132	.23	BY100	-21
	DF91	-30	ECC32	1.00	EL90	-68		1.50	PL81	∙49	U10	1.00	AC154	-30	BY114	-21
	DF92	-25	ECC33	2.00	EL95	-67	KTW63	3	PL81A	-53	U12/14	1.15	AC156	-23	BY126	-18
_	DF96	-60	ECC35	2.00	EL360	1.80		1.20	PL82	-37	U18	1.80	AC157	-30	BY127	21
	DH63	-50	ECC40	~90	EL506	1.20	L63	-65	PL83	-45	U19	4.00	AC165	-30	BYZ10	-30
00	DH76	-50	ECC81	-48		2.50	LN119	-55	PL84	-50	U25	-71	AC166	-80	BYZ11	-30
85	DH77	-50	ECC82	48	EM80	-55	LN152	-45	PL504/		U26	-60	AC168	.44	BYZ12	-30
00	DH81	-80			EM81	-60	LN309	49		.90	U33	1.75	AC176	-64	BYZ13	-30
52	DK82	-60	ECC83	.48	EM83	-60			PL508	1.30	U35	1.75	AC177	-32	FSYLLA	
70		-70	ECC84	-35			LZ319	-80		2.20	U37	2.00	ACY18	-23	FSY41A	
45	DK40		ECC85	-50	EM84	45		1.00	PL509				ACY19	.23	OA9	14
75	DK91	.50	ECC86	1.25		1.20	MHL4	1.00	PL519	2.80	U81	-80		30		
	DK92	1.00	ECC88	-72		1.10	MHLD		PT4D	1.00	U191	.50	ACY20		OA47	-12
75	DK96	·70	ECC91	-35	EMM80		MKT4		PY33/2		U251	1.00	ACY21	-30	OA70	·18
40	DL63	.70	ECC189			2.50	MU14	1.15	PY80	-50	U301	1.00	ACY22	·18	OA73	·18
90	DL82	-80	ECC804		EY51	-45	MX.40	1.00	PY81	-50	U403	-90	ACY28	-21	OA79	-11
85	DL92	.45	ECC807		EY81	·45	N150	-57	PY82	-40	U404	75	AD140	-50	OA81	·11
60	DL94	-80	ECF80	-60	EY83	-60	N308	-98	PY83	-50	U801	1.00	AD161	·53	OA85	11
50	DL96	-60	ECF82	-30	EY86/7	-87	P61	-60	PY88	-60	U4020	.75	AD162	.23	OA90	14
10	DM70	-80	ECF86	-80	EY88	-55	PABC8		PY5002		VP4 (5)	2.00	AF114	-30	OA91	-11
50	DM71	1.75	ECH35		FY91	-50	PC86	-62	PY800	-50	VP23	-65	AF115	-30	OA95	-11
00	DW4	1.15	ECH42	71	EY500	1.45	PC88	-62	PY801	-50	VP41	-90	AF117	-23		1.00
90	DY51	2.00	ECH81	-55	EZ35	-45	PC92	-55	PZ30	-50	VR105	-50	AF121	-35	OC44	18
85	DY87/6	-45	ECH83		EZ40	-52	PC95	1.00	QQV03	/10	VR150	.75	AF124	-36	OC45	·18
00	DY802	-50	ECH84	-50	EZ41	-52	PC97	-75		2.00	VU111	1.00	AF180	-56	0070	14
00	E80CC	2.50			EZ80	-35	PC900	40	QS95/1	0 .	VU120	1.00	AF186	-64	OC71	.13
00	E80CF	5.00	ECL80	-45	EZ81	-40	PCC84	89		1.00	VU133	1.00	BA115	·16	0072	·18
70	E80F	2.20	ECL82	-50	EZ90	-65	PCC85	-47	QS150/	15	W107	-75	BA116	-21	OC74	-26
00	E83F	3.50	ECL83	74	FC4	1.00	PCC88	-61		1.80	W729	1.20	BA129	·14	OC75	-13
00	E88CC	1.20	ECL84	-65	GY501	-95			QV04/7	3.00	X41	1.00	BA130	·12	OC76	18
80	E92CC	.70	ECL85	.70	GZ30	-48	PCC89	-49	QV06/9	20	X66	1.60	BA148	•20	OC77	-32
95	E180CC	-80	ECL86	-64	GZ32	-60	PCC189			4.70	Z759	5.85	BA153	-18	OC78	18
55		1.15	EF22	1.00		2.00	PCF80	-80	R10	6.50	Transis	ors	BC107	.14	OC78D	-18
45	E182CC		EF40	-78		2.00	PCF82	·45	R19	-75	& Diode		BC108	-14	OC81	18
DÓ.	E188CC		EF41	-75		2.00	PCF84	-70	UABC8		1N4744		BC109	·14		
98		5.00	EF73	1.75	HABC80		PCF86	-57	UAF42	.70	2N404	.21	BC113	-30	OC81D	-13
	E1148	-60	EF80	-29	HL13C	-60	PCF200		UBC41	-50	2N966	-61	BC115	-18	OC82	-18
00	EA50	-40	EF33	1.25	HL23	·70	PCF201		UBC81	-55	2N1756		BC116	-80	OC82D	-13
		1.30 l	EF85	-86	HL23D1		PCF801		UBF80	-50	2N2147	-99	BC118	-26	OC83	.23
00	EABC80		EF86	-50	HL41	1.00	PCF802		UBF89	-39	2N2297	-26	BCY10	.53	OC84	-28
	EAC91	-55	EF89	-42	HL41DI		PCF805		UBL21		2N2369		BCY12	-58	OC123	-26
00	EAF42	.70	EF91	.70		1.00	PCF806		UC92	-50	2N3053	-38	BCY33	-23	OC139	-50
50	EAF801		EF92	-50	HL42D1		PCH200		UCC84	-ĕŏ	2N3121		BCY34	-26	OC169	-50
00	EB34	30	EF93	.40		1.00		1.00	UCC85	·45	2N3703	-23	BCY38	-26	OC171	-40
50	EB91	20	EF94	-40	HN309		PCL82	-54	UCF80	-80	2N3709	-23	BF158	-21	OC172	41
BO :	EBC41	75	EF95	·45	HVR2		PCL83	-49	UCH21		AA119	-18	BF159	-30	OC200	-55
50	EBC81	45	EF97	-90	HVR2A		PCL84	46	UCH42	71	AA120	·18	BF163	-23	OC204	-50
50	EBC90	50	EF98	-90	HY90	-55	PCL86	-65	UCH81	-50	AA129	·18	BF173	-44		1.05
ŠŎ.	EBC91	-50	EF183	42	KT2	90	PCL805		UCL82	-55						
50	EBF80	-40	EF184	42		3.00	PEN25		UCL83	-57	MATCH	ED T	RANSIST	OR SI	ETS:-	
75	EBF83	45	EF804	1.75		1.00	PEN45		UF41	70			AC154. A			61p
50	EBF89	40	EH90	45		1.00	PEN451		UF42	-80	per paci	s. 1/0	281D & 2	OC8	1. 50p.	
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J73 Range: 2·5kHz-20kHz Power: 50w kimp: 8 ohms Size approx: 7½" × 3" × 6½"

Rec £11.75

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# 15-240 Watts!

# HY5 Preamplifier

The HY5 is a mono hybrid amplifier ideally suited for all applications. All common input functions (mag Cartridge, tuner, etc) are catered for internally. The desired function is achieved either by a multi-way switch or direct connection to the appropriate pins. The internal volume and tone circuits merely require connecting to external potentioneters (not included). The HY5 is compatible with all I.L.P. power amplifiers and power supplies. To ease construction and mounting a P.C. connector is supplied with each pre-amplifier.

FEATURES: Complete pre-amplifier in single pack—Multi-function equalization—Low noise—Low distortion—High overload—Two simply combined for stereo.

APPLICATIONS: HI-FI—Mixers—Disco—Guitar and Organ—Public address

SPECIFICATIONS:

SPECIFICATIONS: nieri—mixers—bisco—buitar and Organ—Public address
SPECIFICATIONS:
INPUTS. Magnetic Pick-up 3mV; Ceramic Pick-up 30mV; Tuner 100mV; Microphone 10mV;
Auxillary 3-100mV; input impedance 4·7κΩ at 1kHz.
OUTPUTS. Tape 100mV; Main output 500mV R.M.S.
ACTIVE TONE CONTROLS. Treble ± 12dB at 10kHz; Bass ± at 100Hz.
DISTORTION. 0·1% at 1kHz. Signal/Noise Ratio 68dB.
OVERLOAD. 38dB on Magnetic Pick-up. SUPPLY VOLTAGE ± 16-50V.
Price £5·22 + 65p VAT P&P free.

# **HY30** 15 Watts

into  $8\Omega$ 

The HY30 is an exciting New kit from I.L.P. It features a virtually indestructible I.C. with short circuit and thermal protection. The kit consists of I.C., heatsink, P.C. board. 4 resistors, 6 capacitors, mounting kit, together with easy to follow construction and operating instructions. This amplifier is ideally suited to the beginner in audio who wishes to use the most up-to-date technology available.

FEATURES: Complete Kit-Low Distortion-Short, Open and Thermal Protection-Easy to

APPLICATIONS: Updating audio equipment—Guitar practice amplifier—Test amplifier—

audio oscillator.

SPECIFICATIONS:
OUTPUT POWER 15W R.M.S. into 8 \( \Omega : \Omega

# **HY50**

25 Watts into  $8\Omega$ 

The HY50 leads I.L.P.'s total integration approach to power amplifier design. The amplifier features an integral heatsink together with the simplicity of no external components. During the past three years the amplifier has been refined to the extent that it must be one of the most reliable and robust High Fidelity modules in the World.

FEATURES: Low Distortion—Integral Heatsink—Only five connections—7 amp output transistors—No external components

SISTORS—NO external components
APPLICATIONS: Medium Power Hi-Fi systems—Low power disco—Guitar amplifier
SPECIFICATIONS: INPUT SENSITIVITY 500mV
OUTPUT POWER 25W RMS into 8Ω LOAD IMPEDANCE 4-16Ω DISTORTION 0-04% at 25W

at 1kHz SIGNAL/NOISE RATIO 75dB FREQUENCY RESPONSE 10Hz-45kHz — 3dB. SUPPLY VOLTAGE ± 25V SIZE 105 50 25mm Price £6:82 + 85p VAT P&P free

# **HY120**

60 Watts into  $8\Omega$ 

The HY120 is the baby of I.L.P.'s new high power range. Designed to meet the most exacting requirements including load line and thermal protection this amplifier sets a new standard in requirements including load line and thermal protection this amplifier sets a new standard in modular design.

FEATURES: Very low distortion—integral heatsink—Load line protection—Thermal protection—Five connections—No external components

APPLICATIONS: HI-FI—High quality disco—Public address—Monitor amplifier—Guitar and

SPECIFICATIONS
INPUT SENSITIVITY 500mV.
OUTPUT POWER 60W RMS Into 8Ω LOAD IMPEDANCE 4-16Ω DISTORTION 0·04% at 60W at 1kHz SIGNAL/NOISE RATIO 90dB FREQUENCY RESPONSE 10Hz-45kHz-3dB SUPPLY VOLTAGE

Price £15.84 + £1.27 VAT P&P free.

The HY200 now improved to give an output of 120 Watts has been designed to stand the most rugged conditions such as disco or group while still retaining true Hi-Fi performance.

FEATURES: Thermal shutdown—Very low distortion—Load line protection—Integral heatsink—No external components

APPLICATIONS: Hi-Fi-Disco-Monitor-Power slave-Industrial-Public Address

SPECIFICATIONS
INPUT SENSITIVITY 500mV
OUTPUT POWER 120W RMS into 8 Ω LOAD IMPEDANCE 4-16 Ω DISTORTION 0·05% at 100W at 1kHz.
SIGNAL/NOISE RATIO 96dB FREQUENCY RESPONSE 10Hz-45kHz-3dB SUPPLY VOLTAGE

Price £23-32 + £1 87 VAT P&P free.

# **HY400**

**HY200** 

120 Watts

into  $8\Omega$ 

240 Watts into  $4\Omega$ 

The HY400 is I L.P.'s "Big Daddy" of the range producing 240W into 40! It has been designed for high power disco address applications. If the amplifier is to be used at continuous high power levels a cooling fan is recommended. The amplifier includes all the qualities of the rest of the family to lead the market as a true high power hi-fidelity power module.

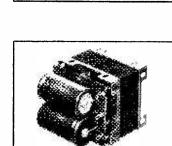
FEATURES: Thermal shutdown—Very low distortion—Load line protection—No external components.

APPLICATIONS: Public address-Disco-Power slave-Industrial

SPECIFICATIONS
OUTPUT POWER 240W RMS into 4Ω LOAD IMPEDANCE 4-16Ω DISTORTION 0·1% at 240W at 1kHz
SIGNAL NOISE RATIO 94dB FREQUENCY RESPONSE 10Hz-45kHz-3dB SUPPLY VOLTAGE

#### **POWER** SUPPLIES

PSU36 suitable for two HY30's £5·22 plus 65p VAT. P/P free. PSU50 suitable for two HY50's £6 82 plus 85p VAT. P/P free. PSU70 suitable for two HY20's £13·75 plus £1·40 VAT. P/P free. PSU90 suitable for one HY20's £13·75 plus £1·40 VAT. P/P free. PSU30 £10 + £1·85 VAT. B1 £0·48 + £0·66 VAT. B1 £0·48 + £0·66 VAT.



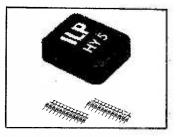
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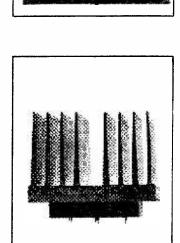
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Signature —————





# TRANSFORMERS

12	AND 24 PRIMAR	VOL1	240 VOLT	1-12V	Pri	m 220		LT RAI Sec 0-12			οV
	Amp	5			Volta	ages	availab	le 3, 4, 5	, 6, 1	8, 9, 10	0, 12,
Ref		24V	£	PAP	15. 1	8, 20,	24, 301	/ 15-0-15	V. 1	2-0-12	
111	0.5	0.2	2 20	0.45	Ref		Amps	4			& P
213	1.0	0.5	2.64	0.78	112		0.5	2.6	4	0	76
71	2	1	3 41	0.78	79		1.0	3 :	7	0	96
18	4	2	4.03	0 96	3		2.0	5 - 2	7	0	96
70	2 4 6	3	5.35	0.96	20		3.0	6.2			14
108	8	3	6.98	1-14	21		4 0	7.2			14
72	10	5	7 67	1 - 14	51		5.0	8.3			32
		6	8 99	1.32	117		6-0	9.9			45
116	12										
17	16	8	10.39	1.32	88		8-0	11			64
115	20	10	13 18	2.08	89	1	0-0	13 :	3	1	84
187	30	15 30	17 05	2.08	-	_	60 160	LT RA			
226	60	30	26 82	OA	D-1-	000		Sec 0-2			601/
								6.8.10.12			
			RANGE								
Prim 2	20/240V 3	Sec 0	-19-25-33-	40-50V				4-0-24V		1-0-301	
Voltag	es availal	ole 6,	7, 8, 10, 1	14, 15, 17,	Ref		Amps	£			& P
19, 21,	25, 31, 33	. 40, 5	OV or 25-	0-25V	124		0.5	3.1			96
Ref	Amp.	s	£	P&P	126		1.0	5 - 3			96
102	0.5		3 · 41	0-78	127		2.0	7.0			14
103	1.0		4 - 57	0-96	. 125		3.0	10 -			32
104	2.0		6.98	1 14	123		4.0	12:			84
105	3.0		8 45	1 32	40		5.0	13 -			64
106	4.0		10-70	1 50	120		6.0	15 (			84
107	6 0		14 62	1.64	121		8-0	20 -	15	C	A
118	8 0		17:05	2.08	122	1	0.0	24	13	C	A
119	10.0		21 70	OA	189		2.0	27	13	C	A
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MAIN	SISOLA	TIN	G (SCRE	ENED)		AU	TO TR	RANSFO	RM		
			C 120/240		Ref		(Watts,				P&P
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149	60		6 20	0.96	4	150		200-220-2	240	5.35	0.96
150	100		7.13	1 14	66			200-220-2		7.75	1 - 14
151	200		11-16	1 50	67			200-220-2		10 99	1-64
152	250		12 79	1.84	84			200-220-2			2 08
153				2 15	93	1500		200-220-2			QA
	350		16 28								ÕÃ
154 155	500 750		19·15 29·06	2·15 OA	95 73			200-220-2			ÖÃ

	SCREENED MINIATURES				
Ref	mA	Volts	£	P&P	
238	200	3-0-3	1 · 99	0.55	
212	1A, 1A	0-6, 0-6 9-0-9 0-9, 0-9	2 85	0.78	
13	100	9-0-9	2-14	0.38	
235	330, 330	0-9, 0-9	1 99	0.38	
207	500, 500	0-8-9- 0-8-9	2 · 59	0.71	
208	1A, 1A	0-8-9, 0-8-9	3 - 53	0.78	
236	200, 200	0-15, 0-15	1-99	0-38	
214	300, 300	0-20, 0-20	2.56	0.78	
221	700 (DC)		3 - 41	0.78	
206	1A, 1A	0-15-20-0-15-20	4 63	0.96	
203	500, 500	0-15-27-0-15-27	3 · 99	0.96	
204	1A, 1A	0-15-27-0-15-27	5 39	0.96	
239	50	12-0-12	1 . 99	0 38	
S112	500	12-15-20-24-30	2.64	0.78	
	1	PILIC			

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U4315 BUDGET METER 20K Ω/VDC 2K/VAC 1000V AC/DC 2·5A AC/DC 500K res. in robust steel case + lead etc.

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2 × 8·5W rms. £24·12 inc.

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Solve your communication problems with this 4-Station Transistor Intercom system (I master and 3 Subs), in robust plastic cabinets for desk or wall mounting. Call/talk/listen from Master to Subs and Subs to Master. Ideally suitable for Business, Surgery, Schools, Hospitals and Office. Operates on one 9V battery. On/off-switch. Volume control. Complete with 3 connecting wires each 66ft. A Battery and other accessories P. & P. 979.

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Electronically changes speed from approximately. 10 revs to maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instructions. £3.45 including post & VAT. Made up model £1.00 extra.

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Designed to operate transistor sets, and amplifiers full wave and half wave working—output adjustable from 45v to 15v up to 300mA—Kit with full to 300mA—Kit with full constructional data £2.06

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A mains operated 4 + 4 stereo system. Rated one of the finest performers in the stereo field this would make a wonderful gift for almost any one in easy-to-assemble modular form and complete with a pair of Plessey speakers this should sell at about £30—but due to a special bulk this way as a invention for units.



due to a special bulk buy and as an incentive for you to buy this month we offer the system complete at only £14.00 including VAT and Postage.

#### AMPLIFIER PANEL



6 photo sockets and d.p. changeover slide switch all mounted on insulating board. Glossy black finish size 2" × 8½" approx.—silly price 35p, or £1 for six.

#### THIS MONTH'S SNIP BREAKDOWN PARCEL

four unused made for computer units containing most useful components, and these components unlike those from most computer panels, have wire ends of easily usable length. The transistors for instance have leads over 1" long, the diodes have approx. \( \frac{1}{2} \)" leads. List of the major components is as follows: 17 assorted transistors, 38 assorted diodes, 60 assorted resistors and condensers, 4 gold plated plugs in units which can serve as multipin plugs or as hook up boards for experimental or quickly changed circuits (note we can supply the socket boards which were made to receive these units). The price of this four units parcel is £1 including VAT and post (considerably less than value of the transistor or diodes alone). Don't miss this splendid offer.

#### MAINS TRANSFORMER BARGAINS



£1 · 25 £1 · 55 £1 · 39 £1 · 75 £2 · 00 £5·50 £1·25 £1·75

#### REVOLUTION COUNTER

Famous Muirhead generator: requires only a voltmeter connected to its



volumeter connected to its terminals. Voltage is exactly 3v at 1000 + rpm. Higher or lower speeds give proportional volts, therefore the motor forms the basis of a useful general purpose revolution counter. £1.25.

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Mains operated—delay can be accurately set with pointers knob for periods of up to 2½ hrs. 2 contacts suitable to switch 10 amps—second contact opens a few minutes contact opens a feafter 1st contact. 95p.

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#### IT'S FREE

Our monthly Advance Advertising Bargains List gives details of bargains arriving or just arrived—often bargains which sell out before our advertisement can appear—it's an interesting list and it's free—just send S.A.E. Below are a few of the Bargains still available from previous lines. previous lines.

Rigonda "Party Time" Stereo Record Players. A further batch has just arrived, but we have a lot of out-standing orders and so we urge you, if you want one, to call in or post your order right away. As with the first batch all are "returns under guarantee" or "service room rejects", but we guarantee them to be repairable, and will exchange any not so. Price is only £5.95 + 75p. Carriage £2.00 + 25p, this is of course less than the price of a turntable, so they are a very popular item, hence the urgency for ordering quickly.

Spares for Party Times. Circuit diagrams 50p, Cartridges £2.25, Record mats 85p, Mains transformers £3.00, Amplifiers £2.50, Gram motors

Ask about any other spares you require and when you have it working o.k. we can supply the proper Party Time speakers, £9.50 a pair. All prices include post and V.A.T.

This Months Special Offer. All our stocks of 7.029 cable with earth wire have now been sold, but we still have some of the twin left—we are offering this at about half its trade price, namely £8.50 + 72p for 100 metres, also as an extra inducement to buy, during August and September, with every coil we will give free; 100 metres of single 1.5mm which you can use as the earth wire. If not collecting, please add £3.00 carriage.

250 watt Mains Transformer—40v secondary, made up of four 10v sections, all the ends of which are brought out to the tag panel, so they can be separated if required—also the 10v coils are all a very heavy gauge wire, thick enough to take 25 amps, so any one of these coils can be loaded up to the full 250 watts, or this wattage can be spread over two or more coils. We can recommend this transformer for heavy duty hattery charging—high power amplifer plastic battery charging—high power amplifier—plastic sealing—soil heating—light welding and dozens of other jobs. Price, still only £4.50 + 36p. Post £1.50

Plex Bargain. 3 core of 14/0.006, modern coloured cores. White circular p.v.c. outer. A standard flex for appliances using up to 6 amps, or for extensions, leads etc. Special purchase enables us to offer this at £8.50 for 100mm coils (+ 68p). Post £1.50 + 12p.

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Free Gift: all who purchase 12 cells, will receive, free of charge, a mains operated ni-cad charger unit. DON'T miss this offer . . . . .

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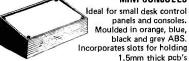
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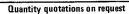


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7400 0 20 7412 0 26 7432 0 36 7472 0 35 7494 0 80 74122 0 -60 74150 1 75 17419 1 -65 7449	EBC81 1·10° EF83 1·75° KT61 3·50° EBC90 0·65 EF851 0·50° KT66 4·00° EBF80 0·45° EF881 0·50° KT66 4·00° EBF80 0·45° EF88 0·60° KTW61 1·75° EBF83 1·25° EF89 0·60° KTW61 1·75° EBL31 2·50° EF921 0·65° KTW62 1·75° ECC40 1·25° EF93 1·25° KTW63 1·75° ECC40 1·25° EF93 1·25° MU14 1·00° ECC821 0·45° EF183† 0·50° N78 7·50° ECC821 0·45° EF184† 0·50° OA2† 0·45°	PCL85† 0.80* R20 1 PCL86† 0.65* U25 1 PCL8058/5† U26 1 PD500 3.00* U26 1 PFL200 0.88* PL36† 0.92* UAF42 0 PL81 0.55* UAF42 0 PL81 0.55* UBF41 1 PL81A† 1.00* UBC4†† 0 PL82 0.60* UCC84 0	100°   584GY† 1 00°	BBA8A 3.75 6J6† 0.35* BBC4 3.71 6J7 0.75* 6BE6† 0.45* 6K4N 0.75* 6BJ6† 1.20* 6K6GT 0.75* 6BJ6† 0.80* 6K7 0.75* 6BL6 25* 6K8 0.75* 6BL7G 3.86* 6K8 0.75* 6BL7G 3.86* 6L6G 2.50* 6BQ7A 1.55* 6L6GA 1.50*	787 1.00* 30PL15 1.44 7C5 1.75* 35W4 0.60 7C6 1.25* 50C5 0.70 7H7 1.00* 85A2 1.5* 7R7 1.50* 90AG 7.2 7S7 2.25* 90AV 7.1 7Y4 0.75* 90C1 1.5* 7Z4 0.75* 90C6 5.7* 12AT6 0.45* 90CV 5.98 12AT7 0.45* 92AG 7.28	7587 12-54 7868 2-93 8088 5-50 8136 1-54
BG7 unskirted 0-15 B7G skirted 0-15 B9A	7400 0 20 7412 0 26 7432 0 36 7401 0 20 7413 0 45 7433 0 37 7402 0 20 7416 0 40 7437 0 42 7403 0 20 7417 0 40 7438 0 37 7404 0 26 7420 0 20 7440 0 22 7405 0 23 7422 0 25 7441AN 0 92 7406 0 55 7425 0 35 7442 N 8 7407 0 55 7425 0 35 7447AN 1 20 7408 0 28 7427 0 35 7450 0 20	7460 0.20 7482 7470 0.35 7493 7472 0.36 7494 7473 0.36 7495 7474 0.40 7498 7475 0.59 7497 7476 0.42 74100 7480 0.60 74107 7482 0.85 74109 7483 1.00 74110 7484 1.00 74111	0·60 74120 1-10 0 0·70 74121 0-45 0 0·80 74123 1-00 0 0·80 74123 1-00 0 0·90 74125 0-80 1 1·75 74126 0-80 1 1·75 74128 0-80 0 0·45 74132 0-80 0 0·45 74132 0-80 0 0·86 74140 0-85 0 0·86 74141 0-85 0 0·86 74142 3-00 1 0·86 74143 3-00 1	74147 2.45 74176 1.10 74148 2.00 74178 1.65 74150 1.75 74179 1.65 74151 0.90 74180 1.65 74154 2.00 74190 1.48 74156 0.90 74190 1.48 74156 0.90 74190 1.25 74157 0.90 74191 1.48 74157 0.90 74193 1.25 74159 2.50 74194 1.25 74170 2.60 74195 1.00 74172 5.00 74196 1.20 74173 1.75 74197 1.00	76013N 1 75° TBA560CQ TBA560CQ TBA560CQ TBA650C TBA760 1 52° TBA750Q TBA520Q TBA550Q TBA5301 98° TBA50Q	Sockets 8 PIN 0.15 14 PIN 0.15 16 PIN 0.17
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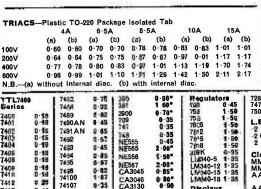
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OC170 0 -23
TIP29A 0 -54
TIP30A 0 -52
TIP41A 0 -54
TIP32A 0 -64
TIP32A 0 -64
TIP32A 0 -64
TIP41A 0 -72
ZN406 0 -20
ZN597 0 -20
ZN706 0 -15
ZN1132 0 -16
ZN1303 0 -40
ZN1303 0 -40
ZN1303 0 -40
ZN1305 0 -55
ZN1307 0 -50
ZN1307 0 -50
ZN1308 0 -60
ZN1309 0 -6 AC142 AC142K AC176 AC176K AC187K AC188K AC188K AD149 AD161 AD162 AF114 BD181 BD182 BD183 BD184 BD232 BD233 2N3705 2N3706 2N3707 2N3708 2N3709 2N3710 2N3711 0 10\* 0 10\* 0 09\* 0 10\* 0 10\* 4012BE 4013BE 4014BE 4015BE BC182 0:11" BC182L 0:12" BC183 0-10\* BC183L 0-10\* BD237 BD238 BD410 0 55 0 60 0 60 2 30 1 50 2 00 0 80 0 60 4016BE 4017BE 4018BE 4019BE BC184 0-11\* BC184L 0-12\* 2N3715 BD410 BDX32 BDY10 BDY11 BDY20 BDY38 BDY60 BDY61 BDY62 BDY95 BDY96 BC184L 0 12° BC186 0 26° BC187 0 24° BC207B 0 12° BC212 0 11° BC212L 0 12° BC213 0 12° AF114 AF115 0 20 2N3772 2N3773 2N3819 1·12 1·03 0·95 0·20 4020BE 4021BE 4022BE 4023BE 2N4347 1-10 2N4348 1-20 2N4870 0-35\* 2N4871 0-35\* 2N4871 0-35\* 2N4919 0-70\* 2N4920 0-50\* 2N4920 0-58\* 2N4923 0-46\* 1 · 70 1 · 65 1 · 15 2 · 14 4 · 96 0 · 30 0 · 30 4024BE 4025BE 4026BE 0 · 86 0 · 20 1 · 55 BC213 0-12\* BC213L 0-14\* BC214 0-15\* BC237 0-16\* BC238 0-16\* BC300 0-34 0 62 0 91 1 10 0 55 4027BE 4028BE BF179 BF180 4029BE 4030BE AL102 AL103 AU107 AU110 AU113 BC300 BC301 BC302 BC303 BCY30 BCY31 BCY32 BCY33 BCY34 BCY38 BF181 BF182 BF183 BF184 0·80 0·83 1·00 0·94 1·32 4041BE 4042BE BU108 4034BE 4044BE 4046BE BU109 BU126 MEMORIES BC107 BC107B BC108 BC108B BC109 2102A-6 3 60 2112A-4 4 75 6508 7 95 2102 2 50 2107 10 00 2112 4 50 2513 8 50 2602 2 50 BF185 BF194 BF196 0·20 0·10° 0·12° BU133 BU204 BU205 BU206 4049BE 4050BE 4069BE 4070BE 54 54 30 50 0 55 0 50 1 15 BF197 BF224J BU208 2:40° BU208 2:60° MJ480 0:80 MJ491 1:05 MJ491 1:15 MJE340 0:40° MJE520 0:45 MJE521 0:55 OC43 0:55 OC43 0:32 0·12 0·12 0·15 BC109B BC109C BF244 BF257 0.17\* 4071BE 4072BE 0 · 26 0 · 26 BCY39 BCY40 BCY42 BCY54 0·19\* 0·25 0·18\* 0·20\* 0·32 0·28 0·23 0 75 0 30 1 60 0 12 0 18 0 12 BF257 BF336 BF337 BF338 BFW30 BFW59 BFW60 4081BE 4082BE 4510BE 4511BE 20 26 42 50 35 25 BCY70 BCY71 BCY72 Resistors\* 10 OHM-10M 2N2926Y 0:09\* 2N2926G 0:10\* IWatt 1·5p 2·0p

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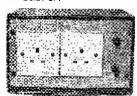
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0-033, 10p; 0-047, 0-068, 14p; 0-1, 15p; 0-15 0-22, 22p; 0-33, 0-47 39p; 0-88 45p.
180V: 0-039, 0-15, 0-22 11p; 0-33, 0-47 19p; 0-68, 1-0-22p; 1-5 28p; 2-2 32p; 4-7 38p.
DUBILIER: 1800V: 0-01, 0-015 16p; 0-022 18p; 0-047 18p; 0-1 34p; 0-47 43p.

POLYESTER RADIAL LEAD (Values in \(\mu\)1, 250V:
0.01, 0.015 8p; 0.022, 0.027 7p; 0.033, 0.047, 0.068, 0.1 8p; 0.15
12p; 0.22, 0.33 14p; 0.47 16p; 0.68 20p; 1.0 24p; 1.5 27p; 2.2 31p.

| FEED THROUGH CAPACITORS 100p; 0.015 8p; 0.15 8p; 0

ELECTRONIC CAPACITORS: Axial lead type (Values are in µF).
63V: 0·47, 1·0, 1·5, 2·2, 2·5, 3·3, 4·7, 6·8, 8, 10, 15, 22, 9p; 47, 32, 50, 12p; 63, 100, 27p;
55V: 1·0, 7p; 50, 100, 220, 25p; 470, 56p; 1000, 62p; 2200, 68p; 40V: 22, 33µF, 9p; 100,
12p; 3300, 62p; 4700, 64p; 35V: 10, 37, 7p; 330, 470, 32p; 1000, 49p; 25V: 10, 22, 47, 6p;
80, 100, 180, 8p; 220, 250, 13p; 470, 640, 25p; 1000, 27p; 1500, 38p; 2200, 34p; 3300, 52p;
4700, 54p; 16V: 10, 40, 47, 68, 7p; 100, 125, 8p; 470, 18p; 1000, 1500, 26p; 2200, 34p;
10V: 4, 100, 6p; 640, 18p; 1000, 14p.
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4700, 48p; 2000, 37p; 40V: 2000+2000, 95p; 350V: 32+32, 185p.

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# WATFORD ELECTRONICS (Continued from opposite side) \*BRIDGE SPEAKERS 80 0-3W (plastic case) 2"; 24" 65p 25; 3" 58p AA119 AAZ15 AEY11 RECTIFIERS (plastic case) (plastic case) 1A59V 20p 1A100V 22p 1A400V 29r 1A400V 29r 1A400V 34p 2A50V 35p 2A100V 45p 2A400V 53p 2A400V 53p 2A400V 53p 4A100V 75p 4A100V 75p 6A100V 73p 6A100V 55p 740V 73p 6A100V 55p 1A200V 1A400V 1A600V 2A50V 2A100V 2A200V 2A200V 2A400V 2A/600V 4A100V 4A/200V 4A/600V 4A/600V 4A/600V 6A/200V 6A/200V 6A/200V BY164 VM18 IN4001/2\* IN4003\* IN4004/5\* IN4006/7\* ZENERS Rng:3·3V-33V 400mW 9p 1·3W 17p IN4148 IS44 3A/100V\* 3A/400V\* 20p 3A/600V\* 27p VARICAPS MVAM2 135p MVAM115 95p BB104 40p BB105B 40p BB106 40p 3A/1000V\*30p SCR's\* Thyristors Noise Diode Z5J 105p 1 A50V 1 A100V 1 A200V 1 A400V 1 A600V ALUM. BOXES with lid\* 3x2x1" 45p 2½x5½x1½" 64p 4xx1½" 64p 120p 125p 5A400V 7A400V 8A400V 150p 150p 55p

BT106

TIC44

TIC45 2N4444

25p

45p 191p

10x4\frac{1}{2}x3" 12x5x3" 12x8x3"

ECTRONICS	TiL209 Red 13p	7 Segment Displays 5-LT-01 Futabe	460p	SWITCHES TOGGLE 2A SPST	
pposite side)	TIL212 Yellow 27p	TIL312·3" C.An TIL313·3" C.Cth TIL321·5" C.An TIL322·5" C.Cth	125p 125p 130p 130p	DPDT	31; 35; 58;
SPEAKERS 8Ω 0·3W 2"; 2½" 65p 0p 40Ω 2·5" 65p 5p 64Ω 2·5" 65p 5p 8Ω 5W 7" × 4" 190p	Grn, Amber 21p OCP70 40p ORP12 58p 2N5777 54p OPTO ISOLATORS TIL111/2 105p TIL114 110p	DL704 - 3" C.Cth DL707 - 3" C.Anod DL747 - 6" An	99p 99p 180g 149p 175p 225p 240p	SUB-MIN TOGGLE SP changeove	54g 85g 78g 92g
16 Ω 5 W 40 7 4" 205p 7 7 4" 205p 7 7 4" 205p 7 7 4" 205p 7 7 4 2" 205p 7 8 4 200 1 4 3p 20 8 4 400 1 4 9p 10 5 5 0 0 1 9 5 p 10 5 5 0 0 205p 10 5 1 5 4 5 0 0 205p 10 5 1 5 4 5 0 0 205p 10 5 1 5 5 5 0 0 205p 10 5 1 5 5 5 0 205p 10 5 1 5 5 5 0 205p 10 5 5 5 0 0 5 5 5 5 0 0 0 5 5 5 0 0 0 0	VOLTAGE REGU 723 DIL 45p TBA625B 95p TO3 Can Type 1A 5V 170p 1A 12V 180p 1A 18V 210p 1A 18V 210p LM309K 150p LM303K 2625p MVR5 180p MVR12 180p	Plastic Case 78L82AWC -1A 8V LM320-12 MC7805 1A 5V MC7815 1A 12V MC7815 1A 15V MC7818 1A 18V Variable Type LM325N ± 15V LM326N ± 12V	150p 115p 115p 120p 125p	PUSH BUTT Spring loaded SPST on off SPDT C over DPDT 6 Tag	55 p 65 p 85 p
P DIAC*	1A -5V 220p 1A -12V 220p	LM317K 20W 1·5A + 1·2V to 37V	350p	Bulgin DPDT Unmounted	СН 180р
LAMP HOLDE	RS AND LAMPS*	SWITCHES*	PUSI	H BUTTON:	

LAMP HOLDERS AND LAMPS* LES HOLDER Dome shaped, Red, Blue, Green, Yellow, White LES BULBS 6v and 12v 9p MES HOLDERS Chrome cover, Red or Amber, Jewelled top 10p LES OR MES Batten Holders 9p NEONS Mains, Sealed with Resistor, Sq. Top, Red or Grn. Round Top Red 24p Neon with leade, 95V AC (No resistor) 9p	Miniature Push to I ROCKE SP chant ROCKE ROCKE Iights wh ROTAR 1 pole/2 t 2 to 4 wa ROTAR
FERRIC CHLORIDE*	except K2

FERRIC	CHLOR! Anhydrou	IDE*	30p p. & p
	ETCH RI spare tip	ESIST	75
COPPE Fibre Glass 6" x 6" 6" x 12"	Single- sided 75p 130p	BOARDS Double- sided 90p 175p	* SRBP 8" x 10·5" 75p

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1	2V to 37V 350pl Unmounted	180p
	SWITCHES* PUSH BUTTON:	
, P	Push to Make 15p Push to Break	25p
P	SP changeover centre off	28p
г	ROCKER: (black) on/off 10A 250V	23p
9	ROCKER: Illuminated (white)	
,	lights when on, 3A 240V	52p
	ROTARY: (Adjustable Stop)	
; ;	1 pole/2 to 12 way, 2p/2 to 6 way, 3   2 to 4 way, 4 pole/2 to 3 way	
)	2 to 4 way, 4 pole/2 to 3 way ROTARY: Mains 250V AC, 4 Amp	41 P
)	KNOBS* fit 2" shaft with grub scr	
- 1	except K2 (push fit) & K8 (for slider	ews,
. 1	K1 Black or White pointer type	an.
2	K4 Black serrated. Metal top with liv	ne P
.	indicator 33mm dlam.	22p
,	K4A As above but 25mm diam.	20p
	K5 Black fluted metal top and skirt	
1	calibrated 0-10. 37mm diam.	26p
1	K6 PK2 as K5. pointer on skirt K7 Black, knurled, tapered. Metal	26p
	ton & skirt Calib 0-10 20mm	250
	top & skirt. Calib. 0-10, 30mm K8 Black or silvered for slider pot	10p
1	l K10 Solid Aluminium. Amniifier K	noh.
	Professional type with etch	line
	Professional type with etch indicator, tapered 18-5 × 17mm d	iam.
١.	Mar minds I il III il I	30p
: 1	K15 Black plastic ribbed body, w indicator line, 15mm diam. tap	hite
1	coloured insert tops, Red, B	erea
1		
ı	K16 As above but 23mm diam	20p

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Screened chrome 2·5mm 12p 3·5mm 15p MONO 23p STEREO 31p	Plastic body 8p 10p 15p 18p	Open metal 8p 8p 13p 15p	Moulded with break contacts 20p 24p	2½ x 3½" 36p 2 2½ x 5" 43p 3 3½ x 3½" 43p 4 3½ x 5" 48p 5	
Din	Plugs	Socket	s In line		3p 95p
2PIN Loudspeaker 3,4 & 15 pin Audio	13p	<b>8</b> p	20p	4 <sup>2</sup> / <sub>4</sub> x 17" 222p − Pkt of 36 plns Spot face cutter	- 145p 28p 69p
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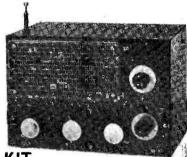
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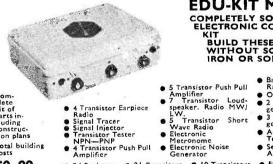
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