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| 7404 | ${ }^{14} \mathrm{p}$ | 7420 | 15p | 7441 | ${ }_{65}^{65}$ | 7473 | 30 p | 7495 | 60p | 74126 | 50p | 74144 | 275p | 74162 | 90p | 74178 | 140 p | 74192 | 820p |
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Details this month on the operation and adjustment of the melody, drum and rhythm, and accompaniment sections.
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## General Interest

SO YOU WANT TO PASS THE R.A.E?-3
Ohm's Law is translated into some practical transistor circuits and the very important principles of magnetism are discussed in this part

John Thornton Lawrence GW3JGA and Ken McCoy GW8CMY IC OF THE MONTH
The ZN1304E is used in timing circuits to provide accurate delays of up to one year! Several circuits are shown for different applications of the IC.

## Free This Month !

24 PAGE 'COMPONENT SOURCE DIRECTORY'

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FAIRCHILD TIMEBAND MAINS DIGITAL ALARM CLOCKS
C500 (left) black or white £14-35. C6110 (centre) £15.90 C590 (rlght) £24.95


NEW FROM IBICO. Siim 6-digit 6-function watch plus backlight and CHRONOGRAPH 1/100 second to 1 hour, Lap and Net times. in the all Stainless Steel 402ES Water Resistant case. 451 ES $£ 49 \cdot 95$. On leather strap 451 ELB $£ 48 \cdot 50$.
I.C. New low cost 6 -digit watch with $1 / 100$ second stopwatch. $£ 32 \cdot 50$. Solar powered version with Tritium "Beta Light" night light £ 44 -50.
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| MiniATURE MAINS Primary 240 V with two independent secondary windings |  |  |  |
| No. 2024 2025 |  | KMS |  |
|  |  |  |  |
| 1 AM No 2066 2027 2028 2023 2030 | $\begin{gathered} \text { AINS Primary } 240 \mathrm{~V} \\ \text { Secondary } \\ 6 \mathrm{~V}-0-6 \mathrm{~V} 1 \mathrm{amp} \\ 9 \mathrm{~V}-0-9 \mathrm{~V} 1 \mathrm{amp} \\ 12 \mathrm{~V}-0-12 \mathrm{~V} 1 \mathrm{amp} \\ 15 \mathrm{~V}-0-15 \mathrm{~V} 1 \mathrm{amp} \\ 30 \mathrm{~V}-0-30 \mathrm{~V} 1 \mathrm{amp} \end{gathered}$ |  |  |
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|  |  |  |  |
| $\begin{aligned} & \text { Noo } \\ & 2031 \\ & \text { 2032 } \\ & 2032 \end{aligned}$ | Rating1 <br> 1 <br> 1 <br> 2 mp <br> 2 amp | Price <br>  |  |

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 S132 2 pin DIN plug to 2 pin DIN socket length $10 \mathrm{~m} \quad 98 \mathrm{p}^{*}$ S133 5 pin DIN plug to 2 phone plugs connected to pins 3 \& 5 S134 5 pin DIN plug to 2 phono sockets connected to pins 3
$\& 5$ length 23 cm S135 5 pin DiN socket to 2 phono plugs connected to pin 3 \& $\mathbf{S 1 3 6}$ Coiled stereo headphones extension cord extends to 7 m S124 3 pin DIN plug to 3 pin DIN plug length $1.5 \mathrm{~m} \quad$ 75p* 81255 in DIN plug to 5 pin DIN plug length $1.5 \mathrm{~m} \quad 75 p^{*}$ S113 3.5 mm Jack to 3.5 mm Jack length $1.5 \mathrm{~m} \quad \mathbf{7 5 p}{ }^{*}$ S114 5 pin DIN plug to 3.5 mm Jack connected to pins $\begin{aligned} & 3 \\ & \text { length } 1.5 \mathrm{~m}\end{aligned}{ }^{5} 5 \mathrm{p}^{*}$

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SWITCHES

| SWITCHES |  |  |  |
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| DPDT miniature slide | 1973 |  | Sc-10* |
| DPDT standard slide | 1974 |  | ¢0.12* |
| Toggle switch SPST $1 \frac{1}{2}$ amp 250 V a,c. | 1975 |  | 80.33* |
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| 1 amp 250 V a.c. | 1976 |  | 50.36* |
| Rotary on-off mains swltch | 1977 |  | E0.42* |
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| A range of rocker | RED | 1980 | 50.22* |
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| Miniature SPST toggle, 2 |  |  |  |
| amp 250 V a.c. | 1958 |  | 50.50 ${ }^{\text {\% }}$ |
| Miniature SPST toggle, 2 | 1959 |  |  |
| Miniature DPDT togale, 2 | 1959 |  | ¢0.55* |
| amp 250 V a.c. | 1960 |  | ¢0.85* |
| Minfature DPDT toggie, |  |  |  |
| centre off, 2 amp 250 V a.c. | 1961 |  | ¢0.85* |
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| Plastic button gives simple on-off action |  |  |
| Rating 10 amp 250 V a.c. | 1969 | c0. 20 |
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| DISPLAYS |  |  |
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| Type | Order No. | Price |
| BDL $7070 \cdot 3 \mathrm{in}$ single | 1510 | E0. 80 |
| EDL7470.6in single | 1511 | E1.50 |
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## 16171

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16175 Pak assorted hardware-
nuts/bolts, gromets, etc. Mains slide switches ass. C16 20 Assorted tag strips and panels 15 Assorted control knobs $\begin{array}{lrl}\text { C18 } & 4 & \text { Rotary wave change switches } \\ \text { C19 } & 2 & \text { Relays 6-24V operating }\end{array}$ Pak, copper
200 sq. in
Assorted fuses $100 \mathrm{~mA}-5 \mathrm{amp}$ Metres PVC sleeving assorted size and colour

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& \text { values } \\
& \text { Presets ass }
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SLIDER PAKS

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| S2 | 6 |
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| 56 |  |

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## BACK NUMBERS

We are very glad to announce the re-establishment of a PW Back Numbers Service for our readers. In future back numbers dated from June 1977 only will be available from our Post Sales Department for 65p, which includes postage and packing. Cheques and Postal Orders should be made payable to IPC Magazines Ltd.
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Perseverance

AWAY from any technicalities this month. Just the story of a PW reader's perseverance. Charlie M. is nearly 78. He was a Marconi marine operator in World War 1 and in his latter years has long cherished the idea of joining the radio amateur fraternity and talking to other folk around the world. He'd done all the swotting but a couple of problems confronted him. His wife is a chronic invalid requiring constant attention, and they live in a remote part of Wales, with but one equally lonely neighbour. How could he leave his wife and go anywhere to take the RAE and the code test?
Following up a couple of suggestions Charlie was able to get the nearest technical college, some 20 miles away, to make the necessary arrangements for him to sit the exam last May. His sole neighbour came round for a few hours and off went Charlie to college, the only candidate! The result? A "distinction" in Part 1 of the paper and a "credit" in Part 2. So far, so good, but taking the code test wasn't quite so simple!
A trip to the nearest testing centre would have meant too long away from home and his wife. He contacted the centre, at Cardiff, and eventually the Marine Radio Surveyor there telephoned Charlie to say that he would call round the next time he was in the area on duty. Eventually he turned up and "they did the necessary test on the kitchen table" A few days later a "pass" certificate arrived. Charlie writes "prompt and willing service like this, in these days of "couldn't care less' is really most heart-warming".

A lovely story, isn't it? A GW4 call ought to be on its way very soon. Another not-so-young amateur has loaned Charlie an AR88 receiver plus a 50 watt transmitter so at long last a dream is about to be fulfilled. Charlie has been reading PW since 1952, "a valuable wireless encyclopaedia that I wouldn't part with for all the tea in China". With the present price of tea, that values PW very highly indeed!

Due to increased production costs, the cover price of your copy of Practical Wireless has been increased to 45 p. The price for new binders has also been increased, as from the 1 st October to $£ 2 \cdot 85$. These price increases have been approved by the Price Commission.

## PLEASE NOTE

We do not operate a Technical Query Service except on matters concerning constructional articles published in PW. We do not supply service sheets or information on commercial radios, TV's or electronic equipment.
All queries must be accompanied by a stamped self-addressed envelope otherwise a reply cannot be guaranteed.

## A Century of Recorded Sound

As previewed in the September issue of PW, the City of London Phonograph and Gramophone Society recently held an exhibition of early reproducers and associated items at the British Institute of Recorded Sound, Exhibition Rd., Kensington, which celebrated one hundred years of recorded sound.
1877 was in fact a year of universal significance for the sound recording industry, seeing the parallel but independent emergence of two versions of a world-shattering device-the sound reproducer, or "talking machine". Charles Cros in France and Thomas Edison in the United States had almost simultaneously arrived at the same answer to an interesting problem, and while Edison's was a practical working model, the Cros version although restricted to a set of detailed plans, was every bit as brilliantly conceived. It was largely lack of funds and his failure to convince a prospective backer which prevented Cros from seeing his machine emerge as a reality.

## Edison v Cros

The exhibition itself naturally displayed an emphasis upon Edison's machines, although Cros was in a sense acknowledged by the inclusion of an Emile Berliner hand-cranked gramophone; it was Berliner who had eventually developed the reality from the plans Cros had deposited at the Academie Francaise in April 1877.

Whatever the arguments about origins, however, a stroll around this display evoked an atmosphere of warm, pre-electric nostalgia. Delicate cylinder phonographs rubbed shoulders with bluff, aristocratic console gramophones in select veneers. Splendid wooden horns balanced at the end of strange foil contraptions with worm gear drives and irresistible cranking handles peered out at an utterly changed world.

Surprisingly, in spite of their great age, most of the machines on view were still playable, in fact, at the height of its popularity, the gramophone was capable of very good reproduction, even though little scientific investigation of basic principles had accom-
panied its development. The HMV "Re-entrant" model (console gramophone of about 1930) proved very pleasant to listen to in spite of a relatively narrow audio range.

Perhaps a good deal of the interest evident at the exhibition may be dismissed as pure sentimentality, for the machines are somewhat crude by modern standards, but they do represent the beginnings of an immense extension of the range of human experience, and as such they will remain vital informational pieces of equipment. They are additionally interesting as a group of acoustic dinosaursthey represent the visible and audible
exhibition was not restricted to the purely acoustic devices, and a selection of early "radio-gramophones" and electrically operated record players was in evidence, including the well-known Decca "Deccalian" with interchangeable heads for 78 or LP. Long-playing records were the "coming thing" in the fifties, and also included in the display was a range of earlier attempts to produce longer playing times, among which was a variable-speed type, designed to exploit the higher speeds at the perimeter of the disc, although this had the disadvantage that a complex device was needed for replay-one which pro-


One of the reproducers in the display-a Thorens phonograph circa 1905.
end of an era, their electrical counterparts proving unequally effective and competitive in the ensuing conflict.
On the other hand, they had, and still retain, real beauty; a combination of satisfying mechanical symmetry and the atavistic flesh-and-blood appeal of real wood, the voices of Melba and Caruso, and above all, an aura of magic and mystery which characterised an age of real discovery.

## Past successes

In terms of the eventual establishment of enterprise in the reproducer field, there was plenty of evidence of the developing "names" in audio devices. Thorens, for example, now heavily committed to quality hi-fi, were represented by an early piece of acoustic precision engineering in the shape of a particularly altractive motor design for a phonograph.

The chronological spani of the
duced a differential slowing towards the centre. Edison's attempts were more practical and saleable-a long player at 78 rpm , which clearly necessitated a remarkably close-cut groove, a good deal closer than a modern LP cut on vinyl.

Another century on may well see an exhibition of 1977's music centres and cassette recorders, languishing in chrome and plastic bowers filled with surround sound, but it is questionable whether they will stimulate the imagination or convey as much of the character of the age as these quaint works of wood, metal and mica. They are important because they stirred up the ripples which led to a gigantic tidal wave in human affairs-the crude boxes which paved the way for the world-wide recording industry, and in so doing, opened up one of the most creative extensions of human commercial and artistic endeavour.

Ted Parratt

## A WIDE RANGE

 VDITMIETERA reliable high-impedance DC and AC voltmeter is an invaluable asset in any enthusiast's workshop. The circuit described is simple to use, exhibits excellent linearity and has a constant input impedance of $11 \mathrm{M} \Omega$ on all ranges. The basic voltmeter is provided with six DC ranges from 1 V to 1000 V full-scale. A variety of probe designs is included in order to facilitate further DC, AC and RF measurements. The unit is portable and operates from the mains or alternatively it may be powered from an external DC supply. An automatic diode switch is included for changing over from internal to external power.

## Circuit Description

A simplified circuit of the DC voltmeter is depicted in Fig. 1. This shows the basic bridge configuration formed by $\operatorname{Tr} 2$; $\operatorname{Tr} 3, R 9$ and R10. A constant voltage is developed across R10, the emitter resistor of Tr3. The input voltage, less approximately 0.6 V which is the base-emitter voltage drop for Tr2, is effectively developed across R9, the emitter resistor of Tr2. The difference between these two voltages produces a


Fig. 1: Simplified circuit of the voltmeter.

## $\star$ specifications



current in the milliammeter, $M$. The calibration of the instrument is set by the variable resistor, VR1.

The voltage to be measured is applied to the potential divider formed by resistors R2 to R7, see Fig. 2. The voltage division ratio is selected by means of the Range Switch, S2. A fixed resistor, R1, is provided in the input lead. To ensure correct calibration this resistor is bypassed by means of S3 when a probe is fitted. The output from the potential divider is fed to the FET transistor, Trl. This transistor is connected as a source follower and provides a very high input resistance and a voltage gain of very slightly less than one.

Transistors $\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ operate as a balanced emitter follower pair. This symmetrical arrangement ensures good linearity and a high degree of temperature stability. The base voltage for $\operatorname{Tr} 3$ is fixed at approximately half the DC supply by means of the potential divider formed by R11 and R12. The circuit may be balanced by means of VR3 which sets the DC potential at the gate of Trl and in turn the potential at the base of $\operatorname{Tr} 2$.
The meter connections are reversed to facilitate positive and negative voltage measurements without the necessity of altering the input lead connections. For AC measurements the instrument is effectively used on the DC negative range and a suitable probe must be employed. The probe is designed to produce a negative DC output using a simple half-wave diode rectifier arrangement. The value of probe resistor, $R$, is chosen so that the instrument is calibrated for RMS AC voltages, see table.

## Construction

The transistors, Tr1, Tr2, Tr3 and associated components are mounted on a $150 \times 115 \mathrm{~mm} 0 \cdot 1$ in matrix board, Fig. 3. Components and connecting leads are located and soldered on this board by means of pressfit terminal pins. Wire links between pins are made using insulated solid wire. The completed board assembly is mounted below the lid of the plastic box and secured by means of the two meter terminals.

Resistors R2 to R6 are wired directly to the contacts of the Range Switch, S2. Resistor R1 is wired across the contacts of the Probe Switch, S3. Care should be taken to keep wiring as short and neat as possible. The mains transformer is secured to the base of the box, Fig. 4, preferably in such a way as to distribute the weight evenly over the base area of the instrument whilst ensuring adequate clearance when the lid and associated components are fitted in place. The external supply sockets are also located in the base of the box, adjacent to the fuseholder. The bridge rectifier and capacitor are fitted to the main circuit board.

## Probes

Various probe designs are given in Fig. 5 together with suitable component values as given in the table. The DC probe of Fig. 5 a is intended for use when DC voltage measurements are to be made in the presence of AC and RF signals. The $1 \mathrm{M} \Omega$ probe resistor provides an extra degree of isolation for the circuit under investigation and minimises reactive loading effects. The construction of this probe is shown in Fig. 6. The

Table of components for probe designs

| Probe | Figure | Component values | Useful voltage range | Useful frequency range |
| :---: | :---: | :---: | :---: | :---: |
| DC - | $5 a$ | R-TMQ $052 \%$ high stability metal oxide | $\begin{aligned} & 0 \text { to } \\ & 1000 \mathrm{~V} \end{aligned}$ | DConily |
| AC <br> low <br> voltage. | 56 | $\mathrm{R}-3 \cdot 3 \mathrm{M} \Omega 2 \%$ high stabllity. $\mathrm{C}-1 \mathrm{a}$ polyester tubular 250 VDC . $\mathrm{D}-\mathrm{OA} 9$ | $\begin{aligned} & 0.5 \text { to } \\ & 30 \mathrm{~V} \end{aligned}$ | 15 Hz to 100 kHz |
| AC medum voltage | 56 | $\mathrm{B}-3.3 \mathrm{MO} 2 \%$ high stability: C-1aF polyester tubular 250VDC D1, D2, D3 OA91 |  | 15 Hz to 100 kHz |
| RF | $5 d$ | $\mathrm{P}-3.3 \mathrm{M} 2 \%$ high stability. C-1nF poly styreme 160VDC. $\mathrm{O}-\mathrm{OA} 91$ | $\begin{gathered} 0.510 \\ 30 \mathrm{~V} \\ \hline \end{gathered}$ | 100 kHz to 100 MHz |

probe circuit is housed in the barrel of a discarded felt-tip pen. The tip contact of the probe makes use of the body of a 3.5 mm jack plug which is inserted in the barrel of the felt-tip pen and held in place by means of epoxy adhesive. Only the tip electrical


Fig. 2: The detailed circuit diagram, including transistor base connections and optional power supply circuit.


Fte 3 : (raove showing infernat layoul and fig. 4 (below) indicating mains invul and transformer detalls:


## $\star$ components

|  |  <br> Re to Rt $\frac{1}{2}$ W metal oxide high stability $2 \%$ R8 to R16. 1 W carbon film high stability $5 \%$ <br> VR1/2 2-2ks horizontal pre-set <br> YR3 : 50 k 0 linear carban <br> BRA - Bridge rectifer looPIV 1 A <br> Note Tr may be replaced by a $2 N 3819$ if R 8 is changed to tokn See lead-out connections on Fig: 2 <br> Switches <br> S1. BP 4 W midget wafer <br> 52. 1P6W. <br> S3 SPST (or DPDT) stide switch <br> Miscellaneous <br> C1. 470 F 25V-Sockets (2) 2mm, red and black Terminals (2), 4 mm red and black Mains transformer, 240 V to $12 V 50 \mathrm{nA}$. Fuse $1 A$ and holder Meter, $1 \mathrm{~mA} F S D_{\text {, }}$ size depending on readout accuracy required. The authorts meter was $117 \times 105 \mathrm{~mm}\left(4 \frac{1}{2} \times 4 \mathrm{~h}\right.$. approx.) Plastic case approx: $225 \times 175 \times 85 \mathrm{~mm}\left(9 \times 7 \times 3 \frac{1}{2} \mathrm{in}\right)$. |
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A view of the thside of the voltmeter to be used in conjunction with Fig. 3 , in which the method of connecting resistors in series to form R2, R3, and RE is clearly shown.

connection of the jack plug is used, the outer connection is ignored.

A short length (approximately 1 m ) of coaxial cable is used to couple the probes to the voltmeter. This should preferably be a substantial RF type cable with a copper braided screen. The braid terminates in a short length of stranded wire fitted with a crocodile clip. This ensures a low-resistance contact with the chassis or common rail of the circuit under investigation. The voltmeter end of the connecting cable is fitted with two 4 mm plugs. The AC and RF probes use a similar construction technique, Fig. 7.

## Calibration

Calibration on the DC and AC ranges is carried out by means of VR1 and VR2 respectively. Calibration on the DC ranges may be checked either by the application of an accurately known DC voltage or by reference to another DC voltmeter. If neither is avail-


Fig. 5: Suitable probe designs for the unit.


Fig. 6: The construction of the DC probe, (above) and the circuit of the $A C$ and RF probes (below).

able a new 1.5 V cell may be connected to the instrument and VR1 accurately set for a reading of 1.5 V , after first remembering to set the Probe Switch "off" and zero the meter! Repeat the calibration procedure for the DC negative and AC ranges (but without a probe connected). Calibration can be checked on the AC range if a known source of AC is available. This may conveniently be a low-voltage transformer of known output supplied from the mains. Do not attempt to calibrate the instrument using AC mains voltage directly since this may cause damage to the probe and to the instrument. The AC probes are suitable only for relatively low AC voltages.

## Operation

The voltmeter is switched to the desired Function and the Set Zero control is then adjusted in order to accurately zero the meter. The Range Switch is set to the 1000 V range. The input leads are then connected to the circuit under test and the Range Switch is then progressively advanced to the range which produces an easily measurable indication. Note that, for the sake of simplicity, a separate mains switch is not fitted to the instrument. Thus, when the unit is not required for use, it is advisable to disconnect the instrument from the AC supply by removing the mains plug.

# all band short wave F. RAYER G3OGR COMVEPtER 



The controls are, left to right, RF Tune, Bandswitch, main tuning and BFO Tune. The RF Attenuator/on-off switch is below the RF Tune control at the left.

With a receiver intended particularly for multi-band reception individual coils with parallel and series capacitors are often provided for each range, values being arranged to secure suitable coverage. A bandspreading capacitor suitable for the LF bands is too large in value for the HF bands, so that some ranges need series padders. The number of coils, trimmers and padders for a multi-band receiver of this type becomes large and careful adjustment is needed to track aerial and oscillator tuning.

The converter described here avoids these difficulties, and is in line with the trend to use a high intermediate frequency, to eliminate second channel interference. It is suitable for operation with a receiver tuned to about 5.5 MHz , which will be available with many general coverage receivers, and allows 1.8 to 21 MHz to be covered with a single converter oscillator coil.

Although this article describes a converter intended for use on the amateur bands there is no reason why it should not be aligned for the SW broadcast bands, since most of these bands are adjacent, in terms of frequency, to the amateur bands.


Fig. 1 : Circuit diagram showing the mixer and oscillator sections of the converter, together with the lead-outs for the transistors.

## Circuit Description

Fig. 1 shows the mixer and oscillator stages. The ganged switch Sla /S1b brings into circuit either Ll or L2 for aerial tuning, L1 covering the 15, 20 and 40 m bands, and $L 2$ the 80 and 160 m bands. Each band is peaked by the panel control VCl. This provides five bands with two coils, with no trimming or similar alignment difficulties.

L3 is the oscillator coil, tuned by VC2, with the switch S2a/S2b. This switch has five positions, operating as follows:-

160 m VC2 has C10 and TC1 in parallel, so that the oscillator coverage is $7 \cdot 25$ to $7 \cdot 5 \mathrm{MHz}$. With the $5 \cdot 5 \mathrm{MHz}$ IF, this gives reception over the $1 \cdot 75$ to $2 \cdot 0 \mathrm{MHz}$ range.

80 m C11 and TC2 are in parallel with VC2, giving an oscillator coverage of 9 to 9.5 MHz , or $3 \cdot 5$ to $4 \cdot 0 \mathrm{MHz}$ on reception.
$40 \mathrm{~m} \mathrm{C13}$ and TC3 are across L3, and C12 is in series with VC2. Oscillator coverage is $12 \cdot 5$ to 13 MHz , giving reception of signals in the 7 to $7 \cdot 5 \mathrm{MHz}$ band.

20 m C14, TC4 and VC2 are in parallel, so that L3 tunes $8 \cdot 5$ to 9 MHz and reception is from 14 to $14 \cdot 5 \mathrm{MHz}$.

15 m TC5 is across L3 and C15 is in series with VC2, giving an oscillator range of 15.5 to 16 MHz , for reception over 21 to $21 \cdot 5 \mathrm{MHz}$.
VC2 is operated by a ball drive and is the main tuning, with VC1 peaking signals as mentioned. VC1 is calibrated to avoid tuning to second channel frequencies, which arise at about $11,13,15$ and 18 MHz in the usual way with a $5 \cdot 5 \mathrm{MHz}$ IF. VR1 is an

## components




Fig. 2: The optional If amplifier stage which works at 5.5 MHz . This is a separate unit, and may be fitted if the main receiver is relatively insensitive.
attenuator or aerial input control, enabling the strength of signals to be kept down so that satisfactory CW and SSB reception can be obtained, also preventing the overloading of the receiver with strong AM transmissions. Tr1 is the mixer, with the signal input to gate 1, and the oscillator input to gate 2. $\operatorname{Tr} 2$ is the oscillator stage, operating as described. L4 is tuned to approximately $5 \cdot 5 \mathrm{MHz}$ and is followed by an optional FET $5 \cdot 5 \mathrm{MHz}$ stage. This can be omitted with a reasonably sensitive main receiver, or can be added later. A BFO is included to allow CW and SSB reception with the popular type of receivers which may have no beat frequency oscillator incorporated.

Fig. 2 is the circuit of the $5 \cdot 5 \mathrm{MHz}$ optional stage. Signal input is taken from Trl coupling coil L4 pin 4, to C16. L5-C18 is a further $5 \cdot 5 \mathrm{MHz}$ coil connected in the drain circuit of $\operatorname{Tr} 3$, and coupled to the output socket. This stage is assembled as a separate unit, fitted to the chassis later.

## BFO

The beat frequency oscillator is designed for a centre frequency of 5.5 MHz and uses the circuit in Fig. 3. It is also assembled as a separate unit. Without the BFO, only AM signals can be received, unless a suitable BFO is present in the receiver itself. As AM reception may be required, provision is made to switch off the BFO for this purpose. To do this, the corner of the back moving plate of VC3 is bent so that it contacts the fixed plate when VC3 is fully closed. The stage is then not operative and current is limited to about ImA by R14 and R15. An on-off switch in series with R15 could be used if preferred.


Fig. 3: Another optional unit is the beat frequency oscillator which also operates at about 5.5 MHz . If the main receiver has a BFO then this unit is not required.
www.americanradiohistorv.com



Fig. 5: Details of the assembly mentioned in the photograph. It can be finished completely as shown before mounting on the main chassis.

The positions of components and wiring can be seen from Fig. 4. The chassis returns MC are ${ }^{1}{ }_{2}$ in 6BA bolts, with extra nuts and tags, so that the board can be mounted later with clearance for connections and leads. Insulated leads are provided to go to $\mathrm{S} 2 \mathrm{a} / \mathrm{b}$, VCl , positive, and output socket or IF stage. Leads of Tr1 and Tr2 are shown in Fig. 1. the main tuning dial has been fitted to the panel the remaining panel components can be mounted in the same line.

## Osc/Mixer assembly

VC2 and S2a/b are fitted to a bracket approximately $100 \times 90 \mathrm{~mm}$ ( $4 \mathrm{in} \times 3^{1{ }^{1}}{ }^{2}$ in) as in Fig. 5. The five trimmers are mounted on a strip of paxolin, which is spaced from the bracket by a long bolt, or similar, to clear the switch. Connect C10 to TCl, C11 to TC2, Cl 3 to TC3, and C14 to TC4 before mounting the trimmer strip, including leads to take to the switch tags on that side.
The board is mounted by the bolts described earlier. The switch requires a spindle 2 in long, so that it can project through a ${ }^{1}$ in hole in the panel, when the assembly is bolted in place approximately $1^{1}{ }_{2}$ in behind the panel. Alternatively, a shaft coupler can be added, with a length of rod. The exact distance from bracket to panel is arranged so that the spindle of VC2 engages correctly with the ball drive bush.

Fig. 6 shows the positions of components on the chassis, and connections for L1 and L2. VR1 fits directly below VC1. The aerial lead runs direct to VR1, away from the $5 \cdot 5 \mathrm{MHz}$ circuits to avoid unnecessary $5 \cdot 5 \mathrm{MHz}$ breakthrough. The BFO board fits to the right, as shown.
Part 2 next month will deal with the construction of the BFO and final alignment of the converter plus a few hints on using the converter.


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#### Abstract



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This resonance indicator is not intended to replace more accurate (and more expensive!) apparatus, but rather to provide a rapid method of checking unknown tuned circuits in the range 100 kHz to 28 MHz . With a given inductor in circuit, the values of unknown capacitors may be found within the range of VC1a and $b$ by resonating the inductor at the same frequency, first with and then without the unknown capacitor between terminals N and M . The change in the value of VCla or VClb needed to re-establish resonance is therefore the value of the unknown capacitor.

## Circuit operation

In a series tuned circuit maximum current flows at resonance and in Fig. 1 this current through R1 feeds the emitter of Trl with an increased RF voltage compared with the voltage at other frequencies. The emitter and base of $\operatorname{Tr} 1$, just biased on by R2, VR1, form a detector circuit and the boosted RF thus acts to increase the emitter-base current. The resulting increase in collector current is indicated by the meter so that the resonance of a particular coil with a selected capacitance and frequency is now known.

## Construction

Because a variable capacitor usually has the frame earthed, this has to be fitted at the 'bottom' of the circuit and the operational electronics are therefore at the 'live RF' end, as is the push-button on-off switch. All components apart from R1, S1, S2, VC1 and M1 may be fitted to a piece of Veroboard; VR1 is adjusted to give a small (about 20 per cent) pointer deflection when S1 is closed. R1, a carbon type, is fitted directly from the coaxial RF input socket to terminal 0 to limit excess inductance; the circuit board could be attached across R1 by short stiff wires if one wishes to avoid making additional fixings to the chassis or panel. See Figs. 2 and 3.


Fig. 1: The circuit diagram of the RF Resonance Indicator.

VCl is bolted direct to the case. A metal case is recommended rather than a plastic one. A short pointer on the shaft traverses over a card scale glued to the outside of the box. During construction ensure that the link between terminal N and P is easily removed for ease of calibration.
The single Mallory cell (in its holder) may be glued into place, and should last for several years.


Fig. 2: General wiring inside the aluminium case.

## Calibration

Connect a coil (fifteen turns of plastic or enamel covered wire close-wound and taped securely to a ferrite aerial rod will do) between terminals $\mathbf{P}$ and 0 . Temporarily unsolder the link N-P. Connect a closetolerance 50 or 100 pF silver mica or polystyrene capacitor between terminals N and M , keeping S1 closed. Then vary the tuning of the RF signal generator connected to the $\mathbf{R F}$ input socket while looking for a peak in meter deflection. Without changing the $R F$ generator frequency, remove the external capacitor, connect N-P and vary VCl until the meter reading again peaks.

The scale-card may then be marked with its first 50 or 100 pF calibration point. Close S2, retune VCI for peak reading and calibrate the other scale. Depending upon the particular type of variable capacitor available it is possible that the minimum capacitance of both gangs in parallel is more than 50 pF and that 100 pF will be the first calibration.

Now with VC1 set to the 50 pF calibration point, add the external capacitor and vary the input frequency to obtain a peak meter reading. Remove the external capacitor and increase the value of VC1 to regain the peak meter reading, marking this new calibration point on the scale. In this way calibration points may be located at 50 or 100 pF intervals around the scales.
It will also be possible to confirm the basic frequency formula that if the 15 -turn coil resonates at about 5 to 6 MHz with 50 pF , then at 450 pF , nine
components

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Capacitors: C1 100 nF polycarbonate. VC1, 5001500 pF gang capacitor

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Fig. 3 : Showing the component positions on the Veroboard, and meter and battery interconnections.

times the original capacitance, the resonant frequency becomes one-third of its value at about $1 \cdot 8 \mathrm{MHz}$. This is because resonance is proportional to the squareroot of the ratio of capacitance change.

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 <br> <br> John ThorntonLawrence GW3JGA \& Ken McCoy GW8CMY}

The passing of the Radio Amateurs' Examination, set by the City and Guilds, requires a certain level of theoretical technical knowledge. Whether one considers that this level is too high or too low is beside the point. The course that follows is intended, with the help of certain external aids, to prepare the reader to pass the examination. It will not teach him all about electronics!

## Practical Ohm's Law

Before we move off Ohm's law and resistance, let us see how it can be applied to calculating the resistor values in a practical circuit. We are going to use an audio frequency amplifier as an example and this is shown in Fig. 1a. As we are only concerned with the DC conditions and how they are set up, we can forget about all the AC components, the coupling and de-coupling capacitors, leaving only the DC components as shown in Fig. 1b. Most modern small signal transistors have a beta (DC gain) of 100 or more, this implies a very small base current, sufficiently small


Fig. 1: The application of Ohm's Law to a simple transistor circuit.
that it may be ignored altogether if certain "rule-ofthumb" conditions are observed.
In a small signal audio frequency transistor amplifier stage, the collector current for optimum gain, noise performance, etc., would be about 1 to 2 mA , so for simplicity we will choose $1 \mathrm{~mA}\left(10^{-3} \mathrm{~A}\right)$. Now for the current flowing down the base potential divider, R1 and R2. As a rule-of-thumb guide this should be a tenth of the collector current, so in our circuit it would be $0 \cdot 1 \mathrm{~mA}\left(10^{-4} \mathrm{~A}\right)$. This ensures that this current is large compared with the small bias current of the transistor. The two currents are shown in Fig. 1b.
Now for the voltages in the circuit. First we must know the supply voltage, so for our example we will make this 9 V . The emitter resistor R4 provides stabilisation of the operating conditions for Tr1. A typical voltage drop across this would be 0.5 to 1 V . So again for simplicity we will choose 1V. The collector voltage should sit midway between the emitter voltage +1 V and the supply voltage +9 V , that is at +5 V . This will allow a signal voltage swing on the collector to go positive by 4 V to the supply voltage and negative by 4 V to the emitter voltage. Remember, up the page is more positive and down the page is more negative (away from positive)! Finally, the voltage drop across the emitter-base of a silicon transistor is 0.6 V so if the emitter is at +1 V the base will be at +1.6 V .
Now for the sums to work out the value of the resistors, these are taken in reverse order.

. . . some practical experience is desirablel
$\mathrm{R} 4=\frac{\mathrm{V}}{\mathrm{I}}=\frac{1 \mathrm{~V}}{10^{-3} \mathrm{~A}}=10^{3} \Omega=1 \mathrm{k} \Omega$
$R 3=\frac{V}{I}=\frac{4 V}{10^{-3} \mathrm{~A}}=4 \times 10^{3} \Omega=4 \mathrm{k} \Omega$
$R 2=\frac{V}{I}=\frac{1.6 \mathrm{~V}}{10^{-4} \mathrm{~A}}=1.6 \times 10^{4} \Omega=16 \mathrm{k} \Omega$
$R 1=\frac{V}{I}=\frac{9-1 \cdot 6 \mathrm{~V}}{10^{-4} \mathrm{~A}}=\frac{7 \cdot 4 \mathrm{~V}}{10^{-4} \mathrm{~A}}=7.4 \times 10^{4} \Omega=74 \mathrm{k} \Omega$
In a practical circuit the value of each resistor would have to be chosen from the list of "preferred" values. There are 12 "preferred" values in each decade of the $10 \%$ tolerance range of resistors and 24 "preferred" values in the $5 \%$ range.
$10 \%$ (E12) range:-
$1 \cdot 0,1 \cdot 2,1 \cdot 5,1 \cdot 8,2 \cdot 2,2 \cdot 7,3 \cdot 3,3 \cdot 9,4 \cdot 7,5 \cdot 6,6 \cdot 8,8 \cdot 2$.
$5 \%$ ( E 24 ) range. All the above values plus:-
$1 \cdot 1,1 \cdot 3,1 \cdot 6,2 \cdot 0,2 \cdot 4,3 \cdot 0,3 \cdot 6,4 \cdot 3,5 \cdot 1,6 \cdot 2,7 \cdot 5,9 \cdot 1$.
To complete our exercise let us now specify the preferred values for our circuit.

|  | R 1 | R 2 | R 3 | R 4 |
| :--- | :---: | :---: | :---: | :---: |
| Calculated value | $74 \mathrm{k} \Omega$ | $16 \mathrm{k} \Omega$ | $4 \mathrm{k} \Omega$ | $1 \mathrm{k} \Omega$ |
| $5 \%$ range (E24) | $75 \mathrm{k} \Omega$ | $16 \mathrm{k} \Omega$ | $3 \cdot 9 \mathrm{k} \Omega$ | $1 \mathrm{k} \Omega$ |
| $10 \%$ range (E12) | $68 \mathrm{k} \Omega$ | $15 \mathrm{k} \Omega$ | $3 \cdot 9 \mathrm{k} \Omega$ | $1 \mathrm{k} \Omega$ |

## Magnetism

We are not proposing to spend any time on permanent magnets except to say that a permanent magnet has a "north seeking" pole and a "south seeking" pole and that imaginary lines of magnetic field or force run from the north to the south pole of the magnet. If two magnets are brought close together then the poles attract one another if they are dissimilar, N-S or S-N, and repel one another if they are similar, N-N, S-S. (See Radio Amateurs' Examination Manual, page 9 ).

If you are a family man, perhaps you could borrow your son's copy of the Ladybird Book, "Magnets, Bulbs and Batteries"! Seriously though, it's an excellent little book and illustrates pictorially the effects we are going to discuss.

## Magnetic Effect of an Electric Current

In the following section we shall look at the magnetic effects produced by currents flowing in conductors. When illustrating these effects in diagrams it is essential to know the direction in which

Fig. 2


Current flowing"Into" page


Current flowing "Out" of page
the current is flowing and the way this is done is shown in Fig. 2. A cross on the conductor relates to the flight of the arrow and indicates that the current is flowing away from the observer and a dot on the conductor represents the point of the arrow and indicates that the current is flowing towards the observer.

Now, let's get down to business and look at a conductor in cross section as shown in Fig. 3. The conductor is surrounded by button compasses, no current is flowing and the compasses are taking up a position in line with the earth's magnetic field. When current flows through the conductor away from you, as shown in Fig. 4a, a magnetic field is produced and the compasses align themselves with the lines of this field, in a clockwise direction. When the current flows in the reverse direction, towards you, as shown in Fig. 4b, you can see that the direction of the magnetic field is also reversed. Remember, reversal of the current produces a reversal of the field.


Dotted lines indicate direction of earth's magnetic field


The Solenoid
If a conductor is formed into a single turn coil, a cross-section view would appear as shown in Fig. 5. You will now notice that the magnetic fields produced in the centre of the coil are in the same direction and are, therefore, more concentrated. The solenoid is a coil comprising a number of turns, as shown in section in Fig. 6. Here you can see the overall effect of the lines of magnetic field around each conductor, combining to produce a concentrated field in the centre of the solenoid, with an overall magnetic field similar to that produced by a permanent bar magnet

with its "north seeking" pole and "south seeking" pole. The magnetic polarity of the solenoid can be deduced by observing the direction of the current flow when viewing the coil at one end, as shown in Fig. 7. The arrows on the letters indicate the direction of the current and make a useful memory aid.


Now, suppose we place a conductor in a magnetic field, with no current flowing, as shown in Fig. 8a, there is no disturbance to the field. When a current flows through the conductor, its resultant magnetic field reacts with the existing field, as shown in Fig. 8b. You will see that on one side of the conductor the lines of magnetic field are in the same direction as those produced by the current and tend to reinforce the field on that side whilst on the other the fields tend to cancel out. This causes a force to be exerted on the conductor resulting in its moving in the direction indicated. A reversal of current produces a reversal in the direction of movement, as shown in Fig. 8c.


Fig. 8: Physical effect of current flowing in a conductor situated in a magnetic field.


Fig. 9: Effect on a conductor when it is moving in a magnetic field.
Finally, let us look at the converse of this effect where the conductor is moving at right angles to a magnetic field, as shown in Fig. 9. Here a flow of current is INDUCED in the conductor and its direction depends on the direction of the motion. The memory aid for this, which is Fleming's Left Hand Rule, is illustrated in Fig. 10.

## The Left Hand Ruie

If the thumb, forefinger and second finger of the Left hand are placed at right angles to one another,
(i) The Forefinger indicates Field direction.
(ii) The ThuMb indicates Motion direction.
(iii) The SeCond finger indicates Current direction.

So that, if we know any two of the three directions, the third can be found.

To summarize what we have seen in this section,
(i) If we pass current through a conductor a magnetic field is set up around it.
(ii) The direction of the field depends on the direction of the current flow.
(iii) If the conductor is in a magnetic field and a current is made to flow in it, the conductor will move, the direction of motion being dependent on the direction of current flow.
(iv) If a conductor is moved in a magnetic field, then a current will be induced in the conductor, the direction of which is dependent on the direction of motion.


Fig. 10: Illustration of Fleming's Left Hand Rule. The importance of memorising this rule cannot be stressed too strongly.

You may begin to wonder what on earth all this has to do with amateur radio, so we will explain that the relationship between the direction of the current flowing in the conductors and the resulting magnetic field, together with the rate at which a conductor is moved in a magnetic field, are all basic ideas related to the generation of Alternating Current (AC).

## Electromagnetic Induction

In the previous section you will have noticed the term INDUCED current, or a current produced by electromagnetic induction. This effect can best be demonstrated by means of the interaction of a bar magnet and a solenoid, Fig. 11. If the bar magnet is moved into the solenoid a deflection will be noticed in the meter connected between the ends of the windings. When the bar magnet is removed a deflection will be noticed again, but this time in the opposite


Fig. 11: A practical experiment which will show that a current is generated when a bar magnet is inserted into or removed from a solenoid. Remember :-No movement, no current!
direction. Whilst the magnet is stationary, no deflection will be observed. As an aside, you will also notice the fact (and by no means an insignificant one) that the faster you move the magnet, the greater the meter deflection.

As we have said before, some practical experience is very desirable, so why not wind yourself a solenoid, 50 to 100 turns of insulated wire on a toilet roll tube, connect it to a milliammeter, push in a magnet and see what happens!

The meter deflections indicate the presence of a potential difference between the ends of the solenoid conductors; giving rise to INDUCED current. If we think about this for a minute we will remember that, while current is flowing in the solenoid, that current will produce a magnetic field. Now, the direction of that field will be such as to oppose the motion of the magnet which induces it. Thus, if the north pole of the magnet is pushed inside the solenoid the current flow induced will produce an apparent north pole at that end of the solenoid, thus tending to oppose the magnet's motion. As the magnet is withdrawn the induced current will produce an apparent south pole at that end of the solenoid, again opposing the extraction of the magnet, since a north pole will attract a south pole.


The German physicist Lenz formalised this in his Law in 1834. Basically it means that the direction of the induced potential difference tends to set up a current opposing the motion or change of magnetic field producing that potential difference. Now the magnetic field which is used to induce currents in a solenoid need not come from a permanent magnet. It could come from another solenoid placed in close proximity to the first. In this we have the bones of the TRANSFORMER, but, before we look at that subject, the question of the nature of ALTERNATING CURRENT (AC) arises. Again, the previous sections will be of assistance since AC is best understood when reference is made to the facts relating to conductors moving in a magnetic field.

## To be continued next month

Readers are asked to note that the publications mentioned already in this series as recommended reading have recently been increased in price. They are "A Guide to Amateur Radio" and "The Radio Amateurs" Examination Manual" which now cost $£ 1 \cdot 38$ and 86 p respectively. They are obtainable from the Radio Society of Great Britain, 35 Doughty Street, London WCI. The prices are inclusive of postage.


Fig. 1 shows the melody keying, percussion, sustain and tone forming circuits in their entirety. ICs 7, 8 and 9 are the priority encoders described in Part 1. They receive the 37 tones from the generators on pins 16 to 27 in the case of ICS 7 and 8, and 15 to 27 for IC9. There are 13 inputs to the latter to allow for bottom C. Single lines to each keyboard contact can be seen clearly. When one of these lines is pulled to ground through the respective switch, the note associated with that key is latched and fed out at pin 9 . The links between the ICs give priority to the highest note played.

## Melody Circuits

The high level signals generated at the outputs of the priority encoders are fed to potential divider (R11 and R12) which reduces them to a level less than Vbe for Tr3 which is connected as an emitter follower. If there is no bias at the base of this transistor the audio signal will not appear at the emitter; the rate of application and removal of bias at this point controls the envelope of the output signalthence the duration of sustain. If S1 and S2 are closed the priority output from IC9 (pin 31) is routed through the three cascaded gates of IC11b, c and d, and eventually appears, at reduced level, across VR5. A proportion of this is fed through D2 to the base of Tr3 providing the bias necessary to allow the audio signal to appear at its emitter. C6 creates a slight time constant, in conjunction with the setting of VR5, to introduce attack in the envelope.
When the selected key is released the priority signal falls immediately to zero but D2 becomes reverse biased allowing a charge to remain on C6. This charge keeps Tr3 (which can be considered to be an analogue gate) open and the audio continues to appear at its emitter. Over a short period the DC charge on C6 leaks away through Tr3 as base current and the bias is slowly lost. As this happens the audio signal at the emitter dies away. Because the signal is a square wave to start with there is no distortion in this operation. The period of charge leakage sets the sustain duration and this can be controlled by adjustment of VR6 which sets the base current for
the transistor. This latter control is brought out to the front panel.

S2 introduces a low-leakage tantalum capacitor into the path of the keying strobe. This differentiates the control signal for Tr3; this opens the analogue gate momentarily allowing a short burst of audio through, The sustain setting controls the rate at which this percussive burst dies away. The burst of audio occurs on the depression of the key and will not sound again until the key is released and pressed again.

ICIO is the repeat percussion oscillator, frequency controlled by VR4 (again a front panel control). When S1 is open the low-frequency pulses of this oscillator are fed through IC11a and pass through the following gate when a key is depressed. Instead of getting a steady DC level at pin 10 of ICIId, the keying signal is now chopped by the repeat signal. This creates note repetition. Using this in conjunction with the sustain control produces effects such as banjo or xylophone sounds. Note that C 7 should be a tantalum capacitor.

The RC circuitry following $\operatorname{Tr} 3$ creates the voicing. Normally S3, 4 and 5 are closed which shorts the signals to ground. Opening one or more of these switches introduces a particular tone colour. The signals of these three options are mixed by R21, 23 and 26 before being fed to the front panel "Melody Volume" control and thence to the melody buffer amplifier with gain set by VR8. This signal is then fed to the power amplifier or phono output stage.
Use Soldercon sockets for ICs 7 to 9 but do not insert the integrated circuits. Complete the assembly of the rest of this section by reference to Fig. 2. To facilitate testing, solder temporary links across the pairs of pins which will eventually go to S1 and S2. At the same time, temporarily wire in VR4, VR6 and VR7. Set the potentiometers and presets as follows to start with: VR4 Midway, VR5 To bottom (ground) end, VR6 To bottom end, VR7 Midway, VR8 Midway.
Insert the tone generator ICs. With a couple of lengths of wire fitted with clips, select one of the tone lines (see last month's circuit) and hook it tem-

porarily to the end of R11 which goes to the priority encoders. This will provide a test signal. The other wire should have one end clipped to pins 5 and 6 of IC11 (the end of R16 going to this point will do). The other end of this wire simulates keying by touching it to the +12 V rail (at the positive end of C 8 ).

Connect the power supply as described last month plus a loudspeaker. When you apply power you should hear nothing. Next hook the keying wire to +12 V and you should still hear nothing. Gently adjust the wiper of VR5 away from the bottom end of its track to produce a tone in the loudspeaker. Adjust VR5 until the tone just reaches a stable level (ie does not get louder with increase of the setting). If, at this stage the volume is uncomfortably loud or is distorting, reduce the value of VR8. Remove the keying wire
from the 12 V source and the tone should stop immediately. Slowly advance VR6 and tap the keying wire on and off the 12 V point. The sustain effect should get greater as VR6 is increased in value. If you get an unpleasant click at each contact with the keying point, you have probably advanced VR5 too muchthis setting is fairly critical.

Remove the link across the pins for S2 and try the keying test. You should get the single burst of sound when the keying contact is made. Finally remove the link across the pins for S1. This time, when you key, you should hear repeated percussive bursts of soundrate adjustable by VR4.

Turn off the power and remove all temporarily connected potentiometers and also remove IC12 or it will be impossible to test following stages.


## Drum and Rhythm Section

Fig. 3 shows the drum and cymbal voicing circuits. Tr 7 is used as a white noise generator and feeds the cymbals and snare drum stages. Cymbal pulses from the rhythm generator IC are used to gate white noise through Tr8. The envelope of the gate is set by C25 with R63 and R56. The noise is filtered at top and bottom by C26 and C27 respectively. VR15 is used to balance the cymbal level with that for the other instruments.

The snare drum circuit is a little more complex. A sharp burst of white noise is generated at the collector of $\operatorname{Tr} 9$ when the trigger is received from the rhythm generator. This is fed to IC17 which is connected as a low-frequency phase-shift oscillator. VR16 is set so that the circuit is just NOT oscillating. When the white noise burst arrives it triggers a decaying oscillation in this stage and mixes with the frequency so produced. Some care is needed in setting VR16 for optimum results but the sound is quite realistic. The bass drum sound is produced by using
the rhythm pulse to trigger a similar phase shift oscillator which is tuned to a lower frequency. VR19 controls the oscillation point.

Assembly details are shown in Fig. 4. Do not insert the rhythm generator chip (IC14) at this stage. Note that this is an 18 -pin package. When everything apart from IC14 has been correctly inserted, temporarily connect VR17 to its pins and set the controls as follows: VR15 Minimum resistance, VR16 Minimum resistance, VR17 Midway, VR18 Midway, VR19 Minimum resistance.

Connect the power supply. Slowly increase the value of VR19 until oscillation just starts then turn it back slightly so that it just stops again. With a flying lead, momentarily touch +12 V to the top end of R79. You should hear a "thump" similar to that from a bass drum. Adjust VR19 for the correct amount of decay. Use VR18 to preset the level.

Now test the snare-drum circuit. Apply +12 V pulses to the top end of R64 and adjust VR16 for best results. Try to achieve a reasonable balance with the bass drum. A $100 \mathrm{k} \Omega$ component for VR16 would make for easier adjustment. After building several models it was found that the best setting is very close to the bottom end if the original $500 \mathrm{k} \Omega$ potentiometer is used.

Finally, test the cymbals by applying +12 V to the end of R63 going towards the rhythm generator and adjust VR15 until the sound is realistic. As with the snare drum circuit, adjustment may be easier with VR15 as a $100 \mathrm{k} \Omega$ component.
The quality of the cymbals is to some extent controlled by Tr8. There is a large variation in gain for this device and a very high gain might saturate the device with the trigger pulse. This can be detected by a kind of "hesitation" at the beginning of the cymbal sound. It is remedied by reducing the value of R 58 from $10 \mathrm{k} \Omega$ to $4 \cdot 7 \mathrm{k} \Omega$.

## Accompaniment Circuits

The Accompaniment circuits are shown in Fig. 5 and the assembly details of this stage in Fig. 6. IC14 is the rhythm generator the speed of which is controlled by VR11. Rhythms are selected by the switches S 8 to S13 singly or in any combination. The switches couple the rhythm select inputs with the "Any Key Down" signal produced by the chord generator. This ensures a synchronised start of rhythm at the instant an accompaniment key is depressed.
The chord waveform is different from the simple square


Fig. 5: The last part of the circuit to be described is for the Accompaniment.

## components




Fig. 6: Assembly details for the circuit shown in Fig. 5.
wave produced in the melody circuits in that it is more akin to a staircase which constantly changes its shape (depending on the harmonic relationships between the three or four elements it comprises). The simple emitter follower type of envelope shaper would introduce asymmetric distortion. Tr5 in conjunction with R42 acts as a voltage controlled attenuator. The mixed chord signal is applied to its collector via C15 and taken from this same point via C19 for further processing. If $\operatorname{Tr} 5$ is "turned on" the signal is shunted to the positive rail and its amplitude falls to nearly zero. The transistor is biassed so that this is the usual condition. When it is turned off-by means of the snare-drum pulse-the signal momentarily rises at the collector and then dies away as
the charge on C20 is shunted to ground through VR12. This gives a percussive attack and a reasonable sustain; the latter being preset by VR12. If S14b is in the "Vamp OFF" position a steady DC level is maintained on C20 and this holds Tr5 permanently off. In this condition any signals from the chord generator are unaffected by the envelope shaper.

The envelope shaper for the alternating bass is similar to the emitter follower circuit used for the melody rail except that it produces a slightly larger signal (to allow for losses in the heavier filtering which is applied to it). A zener diode (D3) is used to back off the transistor's Veb so that larger signals can be applied without them appearing at the emitter prematurely.

## Last Assembly

Complete the assembly of this stage by reference to Fig. 6. Insert Soldercon sockets for ICl3 and IC9 but do not insert these ICs yet. Wire in temporary links between the pole pins of S14a and $b$ to the DC level (at the pin adjacent to R45)-this disables the Vamp and will make initial testing easier. Temporarily short out R35 to inhibit chords. Refer to Fig. 4 which shows the position of IC14 and connect a temporary link between the pin labelled "S13" and "Common". This selects the waltz rhythm. Wire VR11 and VR13 to their respective pins. Set all controls as follows: VR9 to minimum resistance, VR10 to "ground" end of track, VR11 midway, VR12 to maximum resistance, VR13 midway, VR14 midway.

Connect the power supply and loudspeaker but before turning on insert ICs 13 and 14. Take great care not to damage the pins. Double check the orientation of these two ICs (they are expensive!).

You can now apply power and should, initially, hear nothing from the loudspeaker. Depress the key marked for the chord of C or, alternatively, use a piece of wire with clips to bridge the contacts in the position of this switch. Slowly move the wiper of VR10 away from ground to produce the bass note. It will be alternating and its speed should be adjustable with VR11. There should be no percussion or sustain at this stage. Set VR10 so that there is no further increase in volume as it is adjusted. If necessary adjust VR14 for correct level.

## Final Steps

Switch off the power and remove the link between the pole of S14a and the DC level pin. Now insert a link between the pole and its adjacent pin (which carries the bass drum pulses).

Re-apply power to hear the alternating bass with percussion and sustain. Adjust VR10 to remove undesirable clicks and then set VR9 for sustain period. Try different chord selections by pressing other keys and you should find that the pairs of bass notes change accordingly.

Removing the shorting link across R35 should produce static chords-depending on the key you are depressing. Try the 7 th and Minor select keys in conjunction with the selected chord.

Switch off the power and re-connect the pole pin for S14b to its immediately adjacent neighbour (carrying the snare-drum pulses). Re-apply power and you should now hear rhythmic chords interspersed with the alternating bass. Adjust VR12 for the best duration of chord sustain.

Insert IC9 and then refer to Fig. 2 in Part 2 and insert ICs 7 and 8-at the same time checking all the top side wiring links.

Board assembly is now complete and all the stages have been tested and initially adjusted. Remove all temporary leads. Remember to replace IC12 and IC19.

Next month-the final stages-assembly into the cabinet.

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| Nov 76 | Burglar Alarm | A019 | $0 \cdot 50+12$ | $\square$ |
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|  | Polyphon, tune disc blank, (SRBP) | ) A008* | $0 \cdot 90+15$ | $\square$ |
| Feb 77 | Transistor Checker | A026 | $1 \cdot 18+12$ | $\square$ |
| Mar 77 | FM Stereo Touch Tuner | D023/4/5 | $7 \cdot 50+20$ | $\square$ |
| Apr 77 | Tug 'o' War (set) A | A029/030 | $2 \cdot 88+12$ | $\square$ |
| Apr 77 | Gas/Smoke Sensor Alarm | A028 | $0 \cdot 65+12$ | $\square$ |
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| May 77 | Seekit Metal Locator | A031 | $3 \cdot 38+12$ | $\square$ |
| June 77 | Reverberation Amplifier | A032 | $2 \cdot 38+12$ | $\square$ |
| June 77 | Versatile AF Generator | A033 | $2 \cdot 38+12$ | $\square$ |
| June 77 | Tele-Games | D029 | $3 \cdot 22+18$ | $\square$ |
| July 77 | 20W IC Amplifier | A034 | $1 \cdot 38+12$ | $\square$ |
| July 77 | Radio 2 Tuner | A035 | $1 \cdot 68+12$ | $\square$ |
| July 77 | Digital Clock Timer | A036 | $3 \cdot 28+12$ | $\square$ |
| Aug 77 | Shoot (Telegames) | D035 | $1 \cdot 55+15$ | $\square$ |
| Aug 77 | Atomic Time Receiver | D036 | $2 \cdot 65+15$ | $\square$ |
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| Sept 77 | Electronic Car Voltage Regulator | D037 | $1 \cdot 25+12$ | $\square$ |
| Oct 77 | Audio Level Indicator | D039 | 0.98+12 | $\square$ |
| Oct 77 | Sine-Square Wave Generator | D040 | $2 \cdot 35+15$ | $\square$ |

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## CAR GOURTESY LIGHT

## TOBY BAILEY \& BOB WHITAKER

Courtesy lights in cars can be very annoying. You get into your car at night, sit down, shut the door and the light goes out; leaving you fumbling in the dark trying to insert the ignition key! Most, if not all, of these problems can be solved by an appropriate circuit which keeps the light on for a few seconds after the door is closed-besides, this provides us with an interesting design exercise!

## Specification

Assuming that the car has a negative earth power supply, the circuit in the car before modification will consist of a 12 V supply driving the light bulb, with a switch, operated by the door, in the positive line. We want our circuit to supply current to the light for about fifteen seconds after the switch is opened. This arrangement is shown in Fig. 1.

## Design

Well then, how are we going to set about doing this? The only way that springs readily to mind (ours at any rate) is to charge up a capacitor when the switch is on and to let it discharge when the switch is turned off. After all, most timing circuits are based on this principle! Unless we are going to become involved with relays and the like we will need a series pass transistor in parallel with the switch to turn on the light after the switch is turned off. The arrangement will be something like that in Fig. 2.


Fig. 1: Above, the normal car courtesy light plus our circuit gives a worthwhile advantage. Fig. 2: below, is the germ of the idea. Don't worry about the incomplete transistor! All will be revealed later.


R1 is the resistor through which we charge up capacitor Cl. We haven't drawn an emitter on the pass transistor yet, this is because we've not decided whether it's going to be PNP or NPN! Anyway, there's a slight problem with the circuit as it stands. We want


Fig. 3: The diode D1 turns out to be the critical component in this month's circuit.

Trl to turn on when the voltage at point ' $A$ ' reaches a sufficiently high value: we then want Cl to discharge slowly when S1 is turned off. However, C1 will charge up just as effectively through $\operatorname{Tr} 1$ as through the switch, so there's no way that we can discharge Cl when S1 is turned off again. Hence, with the present arrangement, the light will never turn off. Somehow we have to isolate the effects of the switch and the transistor for the purpose of charging up Cl .

A small amount of thought produced the following simple modification: we insert a diode between the switch and the light, so that the transistor is in parallel with both. We then take the charging resistor from the switch side, Fig. 3. Now when the switch is closed Cl will still charge up and we can use the voltage at the sense point to hold Tr 1 on. The difference now is that when S1 is off and Trl is on, D1 will be reverse biased and hence no current can pass through R1. This allows us to discharge Cl, in some manner yet to be specified!

Having solved that problem, how are we going to fit those two 'dangling wires' in Fig. 2 together? It's fairly obvious that we're going to need another transistor and that we want it to turn off when the voltage at the sense point becomes low enough. We can then


Fig. 4: A second transistor and a working circuit at last.

## * components

R1 $100 \mathrm{k} \Omega$ R2 $6 \cdot 8 \mathrm{k} \Omega$ both $\frac{1}{4}$ or $\frac{1}{3} \mathrm{~W}$ carbon
C1 $\quad 2.5 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic $\quad \mathrm{C} 2 \quad 0.68 \mu \mathrm{~F}$
Tr1 OC35 Tr2 2N3702 Tr3 2N3704 D1 1N4001
The lamp and the switch $\$ 1$ are part of the car wiring
use this transistor to control Trl. If we use an NPN transistor here then Trl will have to be PNP to make them fit together sensibly, as in Fig. 4.

You can see that two additional resistors have appeared as well as $\operatorname{Tr} 2$. We've included R3 to limit the base current in Tr1-it should stop anything nasty happening! If we don't include R2 then Cl will be discharged very rapidly. This is because Tr2 will saturate and then pass a large current through the forward biased diode of its base-emitter junction. With R2 in the circuit the emitter of Tr 2 will just float up to about 0.5 V below the capacitor voltage: the current drawn from the capacitor is just the current through the emitter resistor divided by the gain of the transistor. On further consideration, what on earth do we need R3 for? The current that flows in the base of Tr1 is just Tr2's collector current; since R2 will limit this anyway we don't need R3 as well. Also, R3 would be a bit of an embarrassment if it caused $\operatorname{Tr} 2$ to saturate so, on second thoughts, let's dispense with it.


Fig. 5: The test circuit for the idea, using an LED instead of the car's lamp bulb. Note the use of a 6 V supply here.

At this stage it's probably a good idea to play with the circuit on S-Dec to make sure that it works. Fig. 5 shows the circuit we assembled; the 6 V supply and the LED were used merely because they were nearest to hand. This arrangement gives a good idea of the feasibility of the circuit so far developed.
$10 \mathrm{k} \Omega$ seems a reasonable sort of value for R 2 , although we could have used any of a wide range of values equally well. It should keep the current drawn from Cl small and prevent excess base current in Trl. The choice of $39 k \Omega$ for R1 is also fairly arbi-trary-it charges C1 quite quickly. Rx limits the current in the LED to around 10 mA . With these values the circuit works with a delay of about five seconds: so far so good. However, the light turns off rather slowly, taking a couple of seconds after the light starts dimming before it is completely extinguished. The problem is that at the turn-off point the current being drawn from Cl is very small and so everything happens very slowly. We could try sticking a resistor across C1 to increase the current drawn at turn-off but then we'd need a much larger capacitor, since it would discharge very quickly to start with. We must be able to do better than this!

Surely the way to get fast switching is to use positive feedback, i.e. regenerative switching. The only way to produce positive feedback here is somehow to connect the point marked ' $X$ ' in Fig. 5 to the base of Tr2. We don't want to use a resistor since this will mess up our biasing and the whole business then becomes very confused. What happens if we use a capacitor to provide the feedback? It certainly should speed up the switching in the critical region: as soon as the light starts to turn off the voltage at point ' X ' will start to drop and since the voltage drop across a capacitor can't change instantaneously, the voltage at the base of $\operatorname{Tr} 2$ will also be forced down. For our first try the use of a $0.68 \mu \mathrm{~F}$ capacitor produced rather a strange result-the LED flashed a few times as it turned off. Perhaps something like that was to be expected; after all we have very nearly constructed an oscillator! With further trials we found that a $0 \cdot 1 \mu \mathrm{~F}$ capacitor had little effect, that $0.47 \mu \mathrm{~F}$ produced a vast improvement in switching speed without any untoward effects and that larger values (about $2 \mu \mathrm{~F}$ electrolytic) also speed up switching with no hint of oscillation. Having reached this stage it's now time to design the complete circuit for a proper light bulb; we can find the optimum value of 'speed-up' capacitor by trial and error.

A quick attack on the car produced the information that the interior light is rated at 12V 6W. From this it doesn't require much mental strain to work out that we will need to supply about 0.5 A to keep the bulb alight. Of the selection of power transistors that we possess an OC35 seems to be the most suitable-


Fig. 7: The final circuit can be bullt up on a piece of striphoard as shown here. In the author's unit the board was stuck in the bottom of an aluminlum die-cast box with flexible leads coming out for the switch, supply and lamp.

## ron <br> PRODUCTIONLINES

## Protection racket

Not a lot to look at is it? but then a burglar alarm should be fairly unobtrusive in order that it can perform its task to the best of its ability. This latest one from ADE (Security) Co. is called the Maxi-guard Mk 4, and is designed around ultrasonics with an operational range of between 6 ft and 30 ft . When the device is properly set up it transmits a frequency of 40 kHz , and provided there is no movement within the room the same frequency is returned to the units built-in re-

ceiver. However, if there is something in the room that moves, the frequency of the returned signal is altered (Doppler effect), activating the alarm.

The Maxi-guard operates from a 12 V DC source and draws approximately 100 mA . Measuring $181 \times 126 \times 64 \mathrm{~mm}$, it can be obtained from the manufacturers for $£ 35 \cdot 00$ plus $12 \frac{1}{2} \%$ VAT.

ADE (Security) Co., 217 Warbreck Moor, Aintree, Liverpool. Tel: 051-525 3440.

## Quartz controlled

A rather smart looking digital clock has recently been announced by those wizards of miniaturisation-Sinclair Radionics. Finished in matt black, the Microquartz GT is primarily designed for use in the car, although it's equally effective fixed on a desk, bedside table or workbench. Fixing is by means of adhesive pads.

All time settings are adjusted by the

## So simple

Unless you happen to possess a photographic memory, the constructor using TTL IC's almost always has to refer to data books for correct pin configuration. A simple, yet highly effec-
tive idea from Concept Electronics, is IC-size self-adhesive printed labels showing pin-outs for the 61 most popular 14 and 16 pin ICs. Aptly named Stickies, they are attached to the top of ICs and can be used for constructing and fault finding in prototypes, designing PCB layouts, fault finding on production circuits, and are invaluable as a teaching aid.
Available in sets of 450 , they are packed in a re-usable plastic folder complete with comprehensive instructions. Also included in the pack is a list of equivalents which extends the range of Stickies to cover 86 ICs. Priced at $£ 2.80$ for the pack, further details can be obtained from:-

Concept Electronics, 8 Bayham Road, Sevenoaks, Kent. Tel: 0293514110.

touch of a button, and as the unit is quartz controlled; it is claimed to operate for up to two years on two pen light batteries. The black anodised alloy case measures $90 \times 45 \times 16 \mathrm{~mm}$ and weighs in at $30 z$.

Available from the normal retail shops, the price is $£ 12.95$. If trouble is encountered in getting one, then apply direct to Sinclair Radionics, London Road, St. Ives, Huntingdon, Cambs. Tel: 048064646.

## 5-way controller

Plug it in, connect an external transducer and 240 V AC and what've you got? Well you've got a temperature controller; a light controller; a variable time delay; a liquid level sensor or a touch switch. To perform any of these control functions it is only necessary to connect a transducer between terminals 5 and 6 (thermistor for temperature control, capacitor for timing control, light dependent resistor for lighting control etc.) and a resistor of similar resistance to the transducer between terminals 6 and 8 . Also as this


5 in 1 module operates from the mains it generates its own internal isolated supply of +10 V DC at terminal 5 . Called the Universal Control Module, it contains its own internal comparator and the level required is obtained by adjusting the knob at the top of the module. The internal single pole/ change over contact is rated at 240 V $5 A$ AC or 30V 5A DC.
For one-off the price is $£ 14.95$ plus VAT, and for an extra $£ 4 \cdot 80$ a kit containing resistors, capacitors, a light sensitive resistor, thermistor etc. can be obtained.

Tangent Electronics, 136 Whitehall Road, Norwich, Norfolk. Tel: 060328015.

## Master meter

A new arrival from Alcon Instruments is a $20 \mathrm{k} \Omega / \mathrm{V}$ multimeter with claimed accuracy figures of $1.5 \%$ on DC and $2 \%$ for AC. Called the Master 20 it is available in two versions-standard


## Legal "Scrumping"?

Mention the words Microprocessor system to the average enthusiast and he'll draw in his breath and mention things like the cost of petrol going up, and food isn't getting any cheaper and that he'd like to indulge but just can't afford it. If that person is you-then read on because Bywood Electronics have launched a system, which at $£ 55$ is claimed to be more price competitive than any other system available. With the rather unusual and mnemonic name "Scrumpi" it has nothing to do with apples, but is designed for the engineer or student who wishes to obtain
experience of using and designing with microprocessors.
All parts are supplied in the Scrumpi kit, which incidentally is based on the National Semiconductor SC/MP eightbit microprocessor. The switches are soldered to the PCB by their terminals while the circuit needs a power supply of +5 V and -7 V and these can be derived from a single 12 V supply with a five volt Zener diode. Comprehensive instructions and operating data are provided with Scrumpi along with details for the SC/MP microprocessor. Bywood Electronics, 68 Ebberns Road, Hemel Hempstead, Herts. Tel: 0442 62757
and USI. The latter model derives its name because it incorporates a Universal Signal Injector capable of supplying a 1 kHz -modulated 500 kHz 20 V output, rich in harmonics and detectable up to 500 MHz .

Both models feature a DC range capable of measuring from 100 mV to 1 kV and currents from $50 \mu \mathrm{~A}$ to 3 A ; an AC range which measures from 10 V to 1 kV and currents from 1 mA to 3 A and resistance ranges from 200 ohms to 20 M ohms.

Optional extras include a 30 kV probe which extends the DC voltage range for servicing TV's, 'scopes etc.

The Master 20 measures $170 \times 140 \times$ 62 mm and is supplied with leads, prods and instructions. For the standard model the price is $£ 37.15$ and for the USI model $£ 41 \cdot 90$. The 30 kV probe is $£ 16.95$.

Alcon Instruments Ltd., 19 Mulberry Walk, London SW3. Tel: 01-352 1897.


Quite a number of monolithic timer devices are now on the market, the " 555 " being one of the best-known types. Although the economical 555 can provide a very wide range of delay times from about $5 \mu \mathrm{~s} u p$ to some minutes, it is not suitable for a long delay time of the order of an hour or a week. The problem of using an analogue timer to obtain very long delays is that the product of the timing resistor value and of the timing capacitor value must be very large. However, one cannot employ a large value electrolytic capacitor if one requires an accurate delay time, since this type of capacitor has a large tolerance in its value and the value can change with time. In addition, the leakage current of such capacitors makes it impossible to employ a large value of timing resistor.

## The ZN1034E

A recent device from Ferranti employs an analogue timer, but the same chip also incorporates a 12 -stage frequency divider. Thus the basic oscillator must pass through 4095 cycles before the timing period is terminated. One can therefore employ moderate values of the timing components and multiply the oscillator period by a large factor.
It is not usually necessary to employ an electrolytic capacitor to control the timing of the ZN1034E oscillator. Successive timing periods can therefore be repeated very accurately, to within about 0.01 per cent. Similarly the change of the timed period with temperature can be as low as 0.01 per cent per ${ }^{\circ} \mathrm{C}$ if the temperature coefficients of the timing resistor and capacitor are very low.


Fig. 1: Connections for the ZN1034E timer IC together with the internal circuit shown in block form.

The ZN1034E device is supplied in a 14 -pin dual-inline package with the connections shown in Fig. 1, but electrically similar devices are available in an 8 -pin dual-in-line and in a 10 -lead circular metal can under the type numbers ZN 1034 P and ZN 1034 T respectively.

## Power supply

If a 5 V regulated supply (as used with TTL circuits) is available, pin 4 should be connected to the +5 V line and pin 7 to the 0 V line. $\mathrm{A} 0 \cdot 1 \mu \mathrm{~F}$ capacitor should be connected directly between these pins to provide high frequency decoupling. Alternatively a supply of 6 V up to 450 V can be used in the type of circuit shown in Fig. 2. The positive line is connected through a dropping resistor $R_{D}$ to pins 4 and 5 . The internal regulator connected to pin 5 ensures that the correct voltage of +5 V is applied to pin 4.


Fig. 2: The ZN1034E with its input and timing circuits and power supply connections.
The value of $R_{D}$ in $k \Omega$ is given by the equation:-

$$
\mathrm{R}_{\mathrm{D}}=\frac{\left(\mathrm{V}^{+}-5\right)}{(\mathrm{I}+7)}
$$

where I is the load current in mA. Additional decoupling may be required if the supply voltage should exceed 50 V . The current consumption of the ZN1034E is about 5 mA plus any current taken from either of the outputs.

## Timing

The timing resistor ( $\mathrm{R}_{\mathrm{r}}$ in Fig. 2) should have a value of between $5 \mathrm{k} \Omega$ and $5 \mathrm{M} \Omega$, but for optimum linearity and performance, the value should be between $50 \mathrm{k} \Omega$ and $1 \mathrm{M} \Omega$. The product of the values of
$\mathrm{R}_{\mathrm{T}}$ and $\mathrm{C}_{\boldsymbol{r}}$ sets the period of the internal oscillator. If the value of $\mathrm{C}_{\mathrm{r}}$ exceeds 68 nF , the delay period is 2700 multiplied by $\mathrm{R}_{\mathrm{r}} \mathrm{C}_{\mathrm{T}}$ if pins 11 and 12 are joined so as to bring the internal calibrating resistor of $100 \mathrm{k} \Omega$ into circuit. Typical values of $\mathrm{R}_{\mathrm{T}}$ and $\mathrm{C}_{\mathrm{T}}$ and the time delays which can be obtained by multiplying $\mathrm{R}_{\mathbb{T}} \mathrm{C}_{T}$ by a large factor are shown in Table 1.
The value of $\mathrm{C}_{T}$ should exceed $0.01 \mu \mathrm{~F}$ for optimum performance; although smaller values may be employed when the timed period must be short, the period is then not linearly related to $\mathrm{R}_{\mathrm{T}} \mathrm{C}_{\mathrm{T}}$. The minimum recommended value of $C_{T}$ is $3 \cdot 3 \mathrm{nF}$. For very long delays, electrolytic capacitors are convenient, but they do not provide such accurate timing.

| TIMING COMPONENTS |  | $\mathrm{R}_{\mathrm{T}} \mathrm{C}_{\mathrm{T}}$ | TIMED PERIOD  <br> 2736RTC P500R <br> (Pins 11 (300 <br> and 12 from pin <br> joined) 12 to earth) |  |
| :---: | :---: | :---: | :---: | :---: |
| $\underset{(\mu \mathrm{F})}{\mathrm{C}_{\mathrm{T}}}$ | $\begin{aligned} & \mathrm{R}_{\mathrm{T}} \\ & (\Omega) \end{aligned}$ |  |  |  |
| 0.01 | 39k | 0.39 ms | 1 sec | 2.91 sec |
| 0.1 | 220k | 22 ms | 1 min | 2.74 min |
| 1 | 100k | 100 ms | 5 min | 12.5 min |
| 1 | 1-2M | $1 \cdot 2 \mathrm{sec}$ | 54 min | 2.5 hours |
| 10 | 1.2M | 12 sec | 10 hours | 27 hours |
| 10 | 3.3M | 33 sec | 1 day | 2.7 days |
| 100 | 2.2M | 220 sec | 1 week | 2.7 weeks |

Table 1: Giving various values of $R$ and $C$ that can be used with the timing circuit of the ZN1034E.

An internal calibration resistor of $100 \mathrm{k} \Omega$ in value is connected in circuit when pins 11 and 12 are joined; the delay time is then equal to about $2736 \mathrm{R}_{\mathrm{T}} \mathrm{C}_{\mathrm{T}}$. If, however, an external calibrating resistor of $300 \mathrm{k} \Omega$ is connected between pin 12 and earth (pin 7), the timed period is $7500 \mathrm{R}_{\mathrm{r}} \mathrm{C}_{\mathrm{r}}$. The multiplying factor can also be fixed at 2500 by the use of a $50 \mathrm{k} \Omega$ resistor between pin 12 and ground or at 4100 with a $150 \mathrm{k} \Omega$ resistor.

## Measuring the period

The basic oscillator period can be measured by connecting a probe to pin 13 , but the probe impedance should not be less than $10 \mathrm{R}_{\mathrm{T}}$ or it will cause a considerable change in the period of oscillation. For short
times the output from this pin should be viewed on an oscilloscope, but for long times a stop watch is convenient. The total delay time is 4095 times the period of the oscillator. The measurement of the period of the basic oscillator is much quicker than the measurement of the whole of a long timed period at the output of the frequency divider circuit, but the measurement of the total timed period at the output will normally provide a more accurate value of this period.


Fig. 3: Two types of output circuit suitable for the timer.

## Starting up

The timing in a ZN1034E circuit may be started by joining pin 1 to earth by closing the switch S1 in Fig. 2 for a moment. The timing process is then unaffected by any further operation of S1. Alternatively, if pin $l$ is earthed, timing will begin immediately the power is first applied to the circuit.

## Output circuit

Two complementary outputs are provided from the ZN1034E. The output at pin 2 is normally at a low voltage, but rises to $+3 \cdot 6 \mathrm{~V}$ at the end of the complete timed period. On the other hand, pin 3 is normally at a 'high' voltage, but this voltage falls from about $+3 \cdot 0 \mathrm{~V}$ to a 'low' value at the end of the


Fig. 4 St Were the timer is used in an alarm circuit which can provide delays from : to 11 minutes. The transistor type should be shown as $27 \times 450$.


timed period, Either output can deliver or accept up to 25 mA .

A typical output circuit for the operation of a relay is shown in Fig. 3(a). At the end of the timed period, the output from pin 2 rises in voltage and this causes the ZTX302 NPN transistor to conduct. A current therefore flows from $\mathrm{V}^{+}$through the relay coil and the relay closes. The $\mathrm{V}^{+}$supply in Fig. 3(a) is chosen to suit the relay used. The diode D1 suppresses transient voltages developed in the relay coil and hence protects the ZTX302 transistor.

If the resistor R of Fig. 3(a) is connected to pin 3 of the ZN 1034 E instead of pin 2, the relay will be closed during the timed interval and will open at the end of the interval. The resistor $R$ of Fig. 3(a) must limit the current flowing from the ZN1034E output to a value no greater than 25 mA . A value of a few hundred ohms is suitable with a minimum value of about $150 \Omega$. Fig. 3(b) shows how the output from a ZN1034E can be used to control a triac device which itself switches the power to a load on or off. As before, $R$ must limit the ZN1034E output current to 25 mA .

## Minute timer

In Fig. 4 the product $R_{T} C_{T}$ can be varied from 0.02 to 0.22 second by increasing VR1 from 0 to $1 \mathrm{M} \Omega$. When multiplied by the 2700 factor, times of 1 to 11 minutes can be obtained. Timing starts when S1 is closed and power is applied to the circuit. The alarm sounds at the end of the timed period and continues to sound until Sl is opened. A suitable alarm is obtainable from Doram Electronics Ltd.

## Repetitive timer

The circuit of Fig. 5 shows how a second ZN1034E can be started at the end of the timed period of the first device. At the end of the period timed by the second device, the timing process is started again in the first device. Thus this timer circuit continues to operate with each device working in turn. The output from pin 3 of either device provides the signal through R2 or R3 which begins the timing in the other device. Thus one has an oscillator with a period which can exceed a week!

A wide selection of other circuits is included in the ZN1034E data sheet including (i) a battery charger
which can accurately charge nickel-cadmium cells for a known period at a known current (ii) a metronome (iii) a timer for periods of 1 minute to 1 hour (iv) a 0 to 1 hour industrial timer with suppression against noise pulses (v) a delayed windscreen wiper motor control for vehicles (vi) the use of two ZN1034E devices in cascade to obtain a very large pulse division factor and hence delays of up to a year with an accuracy of 6 minutes after calibration. Other applications include the use of the device on farms for watering, etc, at the required times.

## HHOLY note:

## ATOMIC TME RECEIVER

## August 1977

The author has kindly supplied further information on the coil assembly T1. An alternative to the one specified can be obtained from Hawnt Electronies Ltd, 112 Pritchett Street, Birmingham B6 4EN This is the 10 mm Vinkor LA2936 comprising parts: LA1421 pair of cores, LA1383 ad juster, DT2169 coil former DT2341 ring, DT2342 clip (4 off) and DT2344 tas board. The windings required are, Primary 110 turns of 40 SWG enamelled copper wire Secondaries: two of 20 turns each centre tapped. There are suitable holes in the PCB for this alternative assembly.

> PLEASE MENTION PRACTICAL WIRELESS WHEN REPLYING TO ADVERTISEMENTS



## by Eric Dowdeswell G4AR

Not too many reports this month, with just about everyone away on holiday I suppose. With the appalling weather we are having in the south I thought that a lot of you would have been tied to your sets instead of looking after the leeks! Weather or not, it seems that quite a few of you have been doing the rounds of the rallies and other "do's".

Tom Learmonth of Cwmbran, Gwent, tells me in his first letter to the column that he has now passed his RAE. Congratulations Tom, but I have to remark that it is usually the other way round! Letters first, pass the RAE, and not another word! Tom is not too keen to get the code test over and done with although I have advised him otherwise. He is anxious to get hold of a secondhand transceiver for the 2 m band, possibly for mobile work, so any offers to Tom at 10 Glade Close, Coed Eva, Cwmbran, Gwent. Incidentally, Tom studied entirely on his own for the RAE and now his Dad is thinking of having a go!

From Hastings, Brian Harrison has stuck to the job in hand and covered 10,15 and 20 m on SSB while Robin Bayley A9203, up in Kemberton, Shropshire, patiently awaits his RAE course to begin so that he can take the exam next May. In the meantime he is using his EC10 and Marconi R1475 to good advantage from 15 to 80 m .

John Tye G4BYV writes from Dereham, Norfolk, concerning the lads who work continental stations via repeaters and then ask for a QSL! Frequently they have only worked over a couple of miles! John spreads his time over a wide range of bands from 2 m down to 23 cm where he has worked 107 different stations in 9 countries! $A$ very creditable achievement that really means something, and all with home-made equipment.

From Trowbridge, Wiltshire, comes a complaint from David Birch, aged 13, who is fed up with QRM from TV sets, pointing out that according to the TV licence the "apparatus" is not supposed to interfere with other "wireless telegraphy" equipment. You are quite right Dave, but just try to get someone to do something about it! I read recently that there is a possibility of legislation in the US on this matter but I hate to think how long it will take to get it into law and then to implement it. Pity it wasn't done at the beginning, but there, it costs money! Only hope is to try screened twin feeders properly matched and to keep the set and the aerial as far from. the source of QRM as possible.
J. Hodgson of Morpeth, Northumberland, comments on some strange calls heard in the " 10 m " band but I fear that these are rubbish from the adjacent 11 m band! Unfortunately, with the improving conditions on the
higher frequencies, we shall be able to hear more and more of the overseas Citizens Band stuff.

The organisers of the Worked All Britain Award have now introduced the WAB Counties Award which is also available to listeners. It is issued in two classes, depending upon the number of counties worked/heard. QSLs are not required. A record book to facilitate the "book-keeping" is really a must for this sort of award. Full details from Alec Brennend G4AVA, 76 Deneley Avenue, Todmorden, Lancs. Incidentally, as an added incentive to have a go, all profits from WAB activities go to the Radio Amateur [nvalid and Bedfast Club.

Club News. The newly formed Brighton and District Radio Society is well under way and forthcoming events include a talk on Computers by G3XJG on October 12 and on the 26th G3OEM will discourse on Aeronautical Radio matters. Info from the Hon. Sec. Nigel Hewitt G8JFT, 74 Carlyle Street, Brighton.
The Cheltenham ARS and the local RSGB group have investigated the possibility of forming a single club and the likely date for the first combined meeting is November 3 . Let's hope the move will be beneficial to all concerned. Further info from Derek Lively G3KII, 26 Priors Road, Cheltenham.
The very active Wessex AR Group has its AGM on October 7 and on the 21st they will be reviewing the results of their efforts in the VHF NFD. Several members were successful in the last RAE. It is expected that at least a dozen will start the new course at the Bournemouth College. Further info on the Club from Geoff Cole G4EMN, 6 St. Anthony's Road, Bournemouth. Meetings in the Club Room at the Dolphin Hotel, Holdenhurst Road, Bournemouth. 7.30 p.m.

Several readers have queried the new prefix P28 now being heard on the bands. This is the Republic of Djibouti previously using FL8 as a French colony. The series starts with J28AA so it's a bit difficult to tie up old calls in use with the new ones.
From Adlington, Lancs, comes a letter from Paul Farnworth who is listening and working for the RAE, "then I will leave school and try to get a job". Paul is 15 so let us hope that his plans work out. John Overton writes from Glasgow with some nice log entries on CW. He is very frustrated at not being able to answer back but perhaps it will not be for much longer as he is taking the RAE in December. His BC348 only goes to 18 MHz so he's thinking of making another set for the 10 and 15 m bands. Once again I must point out that a converter is the proper answer. Why not use all the other facilities you have in the 348, John? No point in duplicating them, and you are not likely to get hold of a better dial movement!

Radial, the journal of the RAIBC, reports a healthy growth in the Club membership and activities and a few volunteers are needed for jobs such as Equipment Secretary, Shows and Rallies Manager, Tapes Manager and a Transport Manager. It is not generally appreciated just how much work is involved in the transporting of gear to and from the invalid and bedfast members of the Club, apart from the odd servicing and maintenance chore.

Anyone interested in helping a most deserving cause can contact Harry Boutle G2CLP at 14 Queen's Drive, Bedford MK41 9BQ.
A report from Alan Doherty BRS34968 in Portrush, Co. Antrim, just made the dateline. A rare call these days logged by Alan was Libya in the form of K5CO/5A. Not much activity there since the Forces moved out. Alan says not to be fooled by those CY calls, just read VE instead! Two other nice ones that one can go for many years without hearing were VR4DX and VR6TC, Tom Christian on Pitcairn.

## Log extracts

J. Hodgson:- 20m FG7XL JW7BK J29AI OJ0MA YB2SV 5W1AU 15m HK3AMV HR6SWA
J. Tye:- (G4BYV) worked on $23 \mathrm{~cm}(1296 \mathrm{MHz})$ DF8QK DK3UC PA0FWS PA0VTW PA0EZ ON6AT SM6ESG
R. Bayley:- 80 m A2GCO CT2AP KP4EJA VE4BC 40 m HK0COP JA4AKU 15m VE7DIY 7P8BC
B. Harrison:- 20 m F0CH/FC 15m HM2JV JA1PPC 10m 7X2DG
A. Doherty:- 80 m FG7AN ZS5LB 20 m K5CO/5A TU2GA-VR4DX VR6TC W6OKJ/KS6 ZD7SD 3D2AN, 5WIAU 15m WA4RQK/VQ9 ZD8RR 5N2AAX
J. Overton:-20m A9XBC C31A SV1GR TG9DF VP2AA VP1WS

All calls are SSB except those in italic which are CW.


## SHORT WAVE BROADCASTS

 by Charles Molloy G8BUSSolar activity is on the increase according to the Swiss Shortwave "Merry-go-round" which regularly broadcasts the latest sunspot number and gives predictions, which are obtained from the Zurich Observatory. Forecasts of the number of sunspots for the coming months show a gradual rise from 27 in October to 33 in January 1978 and this upward trend is reflected in reports of DX on the higher frequencies. The writer has been listening recently on Sunday mornings at 0840 to the DX programme from Radio Australia on the new frequency of 21570 kHz in the 13 m band. Although beamed to Asia this transmission comes in better in the UK at this time than the frequencies in the 25 m and 31 m bands that are beamed to the UK.
Harold Emblem who DXes in Mirfield, in Yorkshire, reports hearing the afternoon transmission of "Sweden Calling DXers" on a new frequency of 21690 kHz . HCJB in Quito Ecuador is also on a new 16 m channel of 17755 kHz , Radio Australia is on 15140 and 15410 in the 19 m band and Radio South Africa is on 17780 . Harold asks what sort of information should go into reports to this column. The exact frequency (if known) plus the date and time of reception will help readers to search for the station and some information of the gear used and the aerial will help those who intend purchasing or building a receiver or are thinking of putting up an aerial.
An interesting report comes from Derek Taylor of Preston in Lancashire who uses a Realistic DX160 receiver, a calibrator and a 30 ft . loft aerial when operating on the shortwaves. He reports hearing the International Service of Radio Nacional de Venezuela in English at 2200 on 15400 and he received a confirmation letter from them after one month. Radio Korea (Seoul) was heard in English at 1330 on 11860 kHz and the Voice of Nigeria outlet at Benin on 4932 in the 60 m band was logged at 2100.

A newsletter has been received from the Bristol Path-
finder DX-Group. This club has about 20 members, mostly in the Bristol area, but DXers from anywhere in the UK are welcome. Enquiries should go to Lawrence Bennett, 7 Maple Avenue, Fishponds, Bristol BS16 4HJ. D. M. Tinker is a keen DXer who would like to know if there is a DX club in the Rotherham or Sheffield areas. Reply please to 20 Croft Road, Brinsworth, Rotherham, S Yorks S60 5AP.

Roger Fitzpatrick of Roscrea, Co. Tipperary and his friend Sean Keevey recovered a couple of old Pye 5 -valve receivers from their respective lofts and were surprised, after blowing away the dust, to pull-in between them the following DX:-The Voice of Vietnam on 10040 kHz at 1807, Nigeria on 15220 at 1615, Radio Australia on 9570 at 0800. "Have you any information on Radio Rodina?" asks Roger. Radiostantsia Rodina (Radio Station Homeland according to the World Radio Handbook translation) is not a radio station but a radio programme. It is in Russian and is carried by the external service of Radio Moscow and is intended for Russians living abroad.

Michael Walker (BRS 38836) has been listening to Radio Baghdad and he would like to know the address of this station. Write to:-Iraqi Broadcasting and TV Establishment, Salihiya, Baghdad, Iraq. Frank Hannam sent in a $\log$ from Colne in Lancashire. Using a Fidelity Rad 21 and a 35 ft inverted-L aerial he heard the Voice of Turkey on 9515 kHz at 2210 (there is a DX programme nightly at 2230), Radio Australia on 21570 at 0815 and Radio South Africa on 21535 at 1400. Frank has just been given a big box of valves and he is looking for details of a valve receiver to build.

Can you suggest a good aerial for indoor use, asks Ian Radford (Derby) who reports hearing Radio Australia on 9570 at 0800 and RSA on 21535 at 1700 with his Eddystone EC10 and whip aerial. You seem to be doing very well at the moment, Ian! Why not try the TV aerial? Unplug it from the TV and connect the co-ax lead to the ECl0. If results are good then you can get hold of a 2-way outlet with switch from a TV dealer and switch the aerial to either the TV or the EC10 as required. Do not join all three, the TV the ECIO and the aerial together, they may not get on with one another!
"Just received a QSL card from Radio South Africa (on 21535) so it looks like the high bands are coming back" writes W. G. Holmes-Jones from Abergavenny, in Gwent. He uses a R209 and a home-brew 16-transistor receiver for the broadcast bands together with the choice of a Joystick, 84 ft loft aerial or 45 ft longwire plus an ATU and a tunable notch filter. The highlights of a very comprehensive log are Radio 4VEH Haiti on 9779 at 1130, Radio Finland 15260 at 1300 in English, Radio Australia 9570 each day at 0700 but it gets lost before scheduled sign-off at 0900 (try 21570), Radio Iran 17730 at 1930 in English, The Voice of Greece 9760 at 2200, Radio Mozambique on 6115 at 1800. Radio South Africa was heard on 15220 at 1345 with its weekly Wednesday DX programme.
"I have acquired an ex-RAF R1155 receiver which I know you are familiar with" says Alan Spencer who lives at Ryhall, in Lincolnshire. When connected to a 45 ft long wire it produced ELWA Monrovia, Liberia, on 4770 at 2230 and Radio Nacional Espejo, Ecuador, on 4680 at 0355. Two resistors have now burnt out and Alan is unable to get hold of a circuit or manual. A. J. Brooks, 5 Farrant House, Winstanley Road, London SW11 2EJ can supply diagrams and manuals for most ex-WD and some other communications receivers. An SAE will bring a list. The paper decoupling capacitors in the R1155 are liable to leakage and it is worth doing what the writer did with his and replace the lot with modern $0 \cdot 1 \mu \mathrm{~F} 350 \mathrm{VW}$ capacitors. If a decoupler does short circuit then a burnt out resistor may follow. An old dodge for testing decouplers is to connect the positive lead of a voltmeter to the HT line, disconnect the wire from the live side of the decoupler and tap-on the negative probe from the voltmeter in place of the wire just removed. A good capacitor will give a kick on the meter as it charges and the needle will then go back to zero. A leaky capacitor may give a kick and the needle will return slowly to some intermediate reading

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caused by the current leaking through it. A steady reading on the meter equal to the HT volts indicates that the capacitor is short-circuit and will have to be replaced. Be careful to have the meter switched to the appropriate voltage range (to measure the HT volts) or it will have to be replaced as well!

A large mailbag this month has meant that some letters are being held over to next month. My apologies to those concerned.


## MEDIUM WAVE DX

by Charles Molloy G8BUS

"Readers will think I am mad, from your remarks about me in the July issue" writes Harold Brodribb from St Leonards-on-Sea, who has taken up the challenge of DXing with vintage radio receivers. "I am getting good results with pre-war sets provided they are maintained well and used on this high site with an outdoor aerial and ATU." Harold mentions that his CR100 has many advantages over vintage equipment. He has changed the RF valves for quieter types (the writer used 6BA6) and fitted an $S$ meter and a stabilised voltage supply for the oscillator. He has adapted the BFO valve to perform a dual function as BFO and product detector. The writer used the CR100, also known as the B28, for MW DXing for a number of years. Even unmodified it is a very good receiver though it too, could now almost be classified as vintage. A large number of CR100s came on the surplus market after the last war and they can still be obtained privately for quite a modest sum. They have an internal power pack and can be run direct from 240 V mains. They are not too bulky, rather heavy, like most ex-WD equipment. An external speaker is required though there is space to fit one inside the metal cabinet.

A useful report of Spanish DX comes from Declan O'Dea who lives in Ballinasloe, Co. Galway. With a 10transistor domestic portable he logged La Voz de Madrid on $1097 \mathrm{kHz}, \mathrm{R}$. Espana Madrid on 917 , Radio Madrid on 800, R. Zaragoza 872, R. Valencia 1259, R. Sevilla 809, R. San Sebastian 1025, R. Centro Madrid 1385, R. Popular de Jerez 1385, R. Reloj Barcelona 1124 and La Voz de Gerona on 1385. From North America WINS on 1010 was logged at 0300 and there was an unidentified VOA transmission on 1295 which would be from the 600 kW BBC transmitter at Crowborough in the UK. Declan would like to contact other PW readers in his area. The address is c/o Bank of Ireland, Society Street, Ballinasloe, Co. Galway.

John Little writes from Sunninghill, Berks, to say he was interested in the reference in the July issue to DXing the Middle East. He has just spent two years in Iran where DXing Europe prior to going to work at 0430 was great fun! With local stations not yet on the air, being $3^{1} 2_{2}$ hours ahead of London, the BBC frequently came through on $200 \mathrm{kHz}, 647 \mathrm{kHz}$ and 908 kHz both on the builtin rod aerial and on an outside inverted L. A further illustration that it is interference (QRM) rather than distance that limits the range of DX on the medium waves.

A Realistic DX160 receiver, a MW loop and a 250 ft long wire from the house to a 25 ft pole at the bottom of the garden is used by Martin Liezers who lives in Newport, in Gwent. DX heard with this set-up between midnight and 0300 included La Voix de la Revolution, Conakry, Guinea, very strong on 1403 kHz ; CJON St John's, Newfoundland on 930; WNEW New York City on 1130 and an unidentified with the call KB Radio on 1520. The latter is WKBW in Buffalo NY and the complete call will be used in the formal identifications on the hour and the half-hour. Many
stations try to form slogans out of their call signs and some of these will mislead the newcomer. KLOK is "Clock Radio," WIOD is the "Wonderful Island of Dreams" (Miami), KYAK is in Alaska, and there used to be a KOLD in the same territory at one time! Some call signs may help the DXer. WNEW is in New York, WBAL is in Baltimore, WBOS in Boston, WCBS is owned by the Colombia Broadcasting System, WNBC by the National Broadcasting Company and WINS was the International News Service. There are no prizes for guessing what can be heard from WPOP and WFUN!

Martin raises a couple of interesting points in his letter. He mentions "a lot of crackles which disappear at dawn" and he asks what precautions can be taken to protect the house if his long wire is struck by lightning! Static, QRN, atmospherics, are the names given to the noise heard by Martin and each crackle is caused by a lightning discharge. Since the static disappears at sunrise it must, like DX, have been propagated for quite some distance. During the summer, thunderstorms in the tropics create a considerable amount of static which travels as far as the UK after dark and, although not loud enough to interfere with local reception, it can be troublesome to the DXer. A loop will reduce static provided that the DX and the static are not coming from the same direction. Summer static is usually from the south of the UK but it can come from other directions as well.

The advice about lightning protection usually offered in radio books is that the aerial should terminate at the point of entry to the building, on the moving contact of a knife switch. The upper contact goes to the receiver and the lower to a good, short, outside earth.

Summertime ends on October 23 this year in the UK and the return to GMT will mark the start of the winter season for North American DX. It will then be possible to listen to Canada and the USA before midnight and on nights when conditions are good some DX should be heard as early as 2300 . The nearest, most consistent and earliest station to appear is CJON, located in St John's Newfoundland, which transmits with a power of 25 kW on 930 kHz . It can be found just on the low frequency side of AFN Berlin on 935. DXers who have never heard North America on the medium waves should try for CJON. Another regular is WINS in New York City on 1010 kHz which is reasonably clear of QRM once the Dutch station on 1007 leaves the air, usually around 2300 .

All North American medium wave stations use call signs which are mentioned over the air frequently. The prefix $C$ is used on Canada and either a $W$ or a $K$ in the United States. All stations are on channels which are multiples of 10 kHz . The best DX is often heard after midnight but quite a number of stations appear earlier whenever conditions are good. Tune slowly, as all these broadcasters suffer from slow fading and are easily missed. If unsuccessful, try again a few days later. If conditions are poor one night they will probably pick up again before long.

by Ron Ham BRS15744
Several contributors have expressed their pleasure at our journal's new format and the start of a series about taking the RAE. Nigel Golds BRS36910 West Chiltington, Sussex, leads his report with "I am pleased that there is a series which will help me with my studies for the RAE". Like many others, Nigel is a keen listener on 10 m and has heard the DLs, OKs, Fs, and Gs as well as the German beacon, DLOIGI, during the periodic short skip openings in August.

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collection, I met Vic Elliott BRS37850 Midhurst, Sussex, who emphasised his delight about the RAE series and explained, that as an ex-RN morse instructor, he is now brushing up his basics for the next exam and plans to become active on the HF bands. Later, I called on Gordon Goodyer BRS37345 Petworth, Sussex, a PW reader for many years, who said that he likes the new format but the increase in size upsets his very tidy bookshelves! Gordon spends a lot of time listening on 10 m with his CR100 and dipole and on 2 m with his home-brew frontends, indulging in his special interest of making and testing VHF ground plane aerials.
A period of solar activity began on July 23 rd and ended on August 5th during which time our extra-terrestrial observers monitored the event. John Smith, Cranleigh, Surrey, recorded two definite peaks in the solar noise output at 142 MHz , the first started on the 23 rd , reached it's peak on the 28th, and returned to normal on August 2 when it rose again to a climax on the 5 th and down again by the 10th. In both cases the maximum was about four times the normal level. While the noise was fluctuating, both John and I recorded a host of individual solar bursts, each lasting between one and five minutes, throughout the event. Cliff Ranft, Chilworth, Surrey, found evidence of ionospheric disturbance on July 29th and 30th and he recorded a moderate SCNA (Sudden Cosmic Noise, Absorption) between 1410 and 1510 on August 5th.
Although cloudy skies prevented systematic use of the optical instruments, John Smith did manage to see a sunspot group on July 26th, and Cmdr. Henry Hatfield, Sevenoaks, using his spectrohelioscope, observed a variety of sunspots between August 1st and 4th, in addition to several small filaments and plages. On August 1st and 2nd Henry saw a bright prominence on the sun's east limb and his records show that each time he sees one of these events we all record some form of radio noise at metre waves. Henry counted five sunspots, plus two plages on the 9 th. I received bursts of radio noise at 136 MHz on the 10th and on the 13th John Smith noted that the solar noise level was up, and Cliff Ranft again found evidence of an ionospheric disturbance.

According to my observations the cause of the disturbed conditions on the 4 th was due to a mixture of tropo, due to the falling pressure noted by both Ciaran and myself, and sporadic-E which manifested itself for most of the morning. At 0913 I received a 599 signal from the 70 cm beacon at Sutton Coldfield GB3SUT, a strong picture from Lichfield on Ch. 8 and good signals from ten continental broadcast stations in Band II. At the same time, the influence of sporadic-E ranged from 40 to 73 MHz , bringing a host of continental signals into the UK in Band I plus 14 east-European broadcast stations between 66 and 73 MHz .
Although the tropo-lift was waning I received 59 signals from F1ENH and G8FAS in Somerset, via the London repeater, GB3LO. Sporadic-E occurred again on the 5th and was most intense at 0910 when I received very strong signals from 46 east-European stations between 66 and 73 MHz in addition to sync. pulses on R1, $49 \cdot 75 \mathrm{MHz}$ and a crop of continental stations in Band I.

The falling barometer indicated another tropo opening on August 10 and 11th. At 2300 on the 10th Alan heard a GM station just above the noise on 2 m and at 2355 he worked G8JJR near Doncaster on SSB and while he, at the east end of Sussex, listened to a mobile north of Darlington, via the Cambridge repeater, GB3PI. Your scribe, located at the west end of the county, listened to the Bristol Channel repeater GB3BC and it's "Bing. Bong" code, which must be familiar to our GW readers under normal conditions. I am told that the original aerial at the Brighton 70 cm repeater $\mathrm{GB} 3 \mathrm{BR} 433 \cdot 15 \mathrm{MHz}$ has been changed for an improved colinear. G8LGQ who lives to the east of the repeater, with 400 ft of chalk in the way, is getting a much better signal than before. Further reports to me or to G8HVV, QTHR.

I received a reasonable signal from GB3SUT from 0050 on the 10th to midday on the 11th, and at 0740 on the 11th I heard the Emley Moor beacon GB3EM $432 \cdot 910 \mathrm{MHz}$
at 559. Slight tropo-lifts produced signals from GB3SUT on 70 cm during the early mornings of the 13 th and 16 th ; more reports about 70 cm activity would be welcome.
Interest in our microwave reports is growing and a most welcome letter from Sam Jewell G4DDK, Stone, Staffs, who says there is some dozen stations active on 10 GHz from Birmingham in the south to Manchester in the north and that there is some activity most weeks between various stations in that area. A typical path recently covered was Mow Cop on the Staffordshire-Cheshire border to Winter Hill in Greater Manchester, a line-of-sight distance of 59 km . On this occasion G4DDK, G8ANZ and G8BHH were at Mow Cop and G8AXE with G8AFC on Winter Hill.
The type of equipment being used in the Midlands is typical of modern wideband FM gear for 3 cm ; a 12 mW Gunn diode transmitter to a 16 in dish and a separate tunable Gunn diode/Sim-2 mixer as receiver with a 106 MHz IF, resolved on an FM broadcast receiver. I know just how good this equipment has to be because I spent part of Sunday, August 21st on the Trundle, a hilltop some $675^{\prime}$ ASL, just north of Chichester, Sussex, with Colin Boys G8BCO, Peter Kerry G8ARO and David Bookham G8JNL to see their respective 10 GHz stations as they prepared to take part in the RSGB's 10 GHz Cumulative contest.

The extreme neatness of each station was impressive. The aerials and the electronics are compact, mounted on sturdy tripods with provision for precise adjustments in both altitude and azimuth. At one time, Colin removed his 18 in dish and demonstrated that he could just receive the $10 \cdot 1 \mathrm{GHz}$ beacon GB3IOW St. Catherines, Isle of Wight, on open waveguide proving that he had the full 30 dB gain of the dish in hand on that signal. It did not surprise me when I learnt that Colin's microwave gear won him the award at the construction contest organised by the Famborough and District Radio Society. Peter was using a 12 in dish, giving him 24 dB gain on his receiver and a 14 dB horn on his transmitter. At 1300 a 599 signal from GB3IOW was booming from his receiver and he demonstrated just how critical the direction is; in fact he lost the signal by moving his aerial just $1^{1}{ }_{2}$ in! David's receiver consists of a balanced mixer (pair of 1 N 23 s ) into a 40673 mosfet preamp at 100 MHz (IF) and then to Mullard modules. His transmitter is a 160 mW Gunn diode and his aerial an 18in dish. David also received the beacon signal and a strong signal from G3KSU/P at St Catherines. Each station had two-way contacts with G8BDJ/P Chanctonbury Ring, Sussex and G3IZD/P Lynch Down, Sussex. The climax of their day came at 1800 when G8BCO/P had a 55 contact with GU3JHM/P on Alderney and G8ARO/P had a 59 contact with the Alderney station. Peter told me later that several other UK stations had made it to the Channel Islands on 3 cm that afternoon.

The Microwave round table meeting held on August 7th in Winchester was very successful and well-attended in view of the short notice, which goes to show that once again the amateurs are prepared to experiment and pioneer those difficult signal paths. To help them, the 3 cm beacon at Alderney GB3ALD is now active and its signals have already been received on the Trundle, a distance of 167 km . I understand that several of the microwave boys are planning to get going on 24 GHz and I will certainly look forward to receiving their reports for this column.

> Reports on the vartous bands are welcome and should be sent direct, by the 15 th of the month, to:
> AMATEURBANDS EIC Dowdeswell G4AR Silver Firs, Leatherhead Road; Ashtead; Surrey KT21 2TW. Logs by bands, etch in alphabetical order.
> MEDIUM and SW BANDS Charles Molloy G8BUS; 132 Segars Lane, Southport, PR8 3UG, Reports for both bands must be kept separates
> VHF BANDS Ron Ham BRS15744, Faraday, Greyfriars, Storington, Sussex RH20 4HE


Fig. 6: The final circuit with all the snags ironed out, giving a sharp turn-off to the light, which now remains on for about 15 seconds after the car door is closed.
this is a 30W type so we shouldn't blow it if we use it as the series element. Its gain is given as 25 to 75 at 1 A , so let's take a minimum of 20 , which means that the base current will need to be $500 / 20=25 \mathrm{~mA}$. If we try to supply all this current from one transistor then the current drawn from Cl will be too high; the easiest way out seems to be to reduce the base current that needs to be supplied, by making the pass element a Darlington pair. The circuit will then look like Fig. 6.

The 2N3702 and 2N3704 transistors have been kept since we were using them in our experiments before. Previously the timing period was a bit short but this should go up with increased supply voltage-we can always make C1 bigger if the delay is still too small. R1 has been doubled in value since the supply voltage has been doubled, although this isn't really necessary. D1 can be any diode capable of taking 0.5 A with a maximum reverse voltage of about 20 V -a 1 N 4001
should be fine. Silicon types must be preferable here, since we don't want any problems with leakage currents through D1, keeping Cl charged. What value do we need for R2? Well we want 25 mA of base current for the OC35 and a catalogue tells us that we can rely on a gain of at least 50 from the 2N3702: this means that the 2 N 3704 has to supply $500 \mu \mathrm{~A}$, at least until the voltage across C.1 is down to 3 V or so. A $6 \cdot 8 \mathrm{k} \Omega$ resistor should be OK here; it gives a safe limit to the maximum current that $\operatorname{Tr} 3$ can supply.
It would be good practice normally to put a resistor from the emitter of $\operatorname{Tr} 2$ up to the +12 V line. This stops the Darlington pair doing funny things at low currents. However, we're not involved with low currents here so we'll not bother with this resistor.

It is not entirely obvious what effect changing the load will have on the optimum value for $C 2$, so we'll try $0.47 \mu \mathrm{~F}$ again and see what happens. We can do this final experimenting when we've built the rest of the circuit on a piece of Blob Board. With the circuit wired up we find that the courtesy light, temporarily excised from the car, stays alight for about Gifteen seconds and then turns off. As for C2, the turn-off seems fast and very stable: yet again $0 \cdot 1 \mu \mathbf{F}$ appears to be not quite enough but $0.47 \mu \mathrm{~F}, 0.68 \mu \mathrm{~F}$ and several larger values that we tried all speed up the switching, with none of that embarrassing flickering that we had before, so let's settle for $0.68 \mu \mathrm{~F}$ as the final value for C2. A practical layout is shown in Fig. 7.

The output levels and the output impedances of things like cassette recorders don't always match the associated amplifiers so next month's design is for a simple matching circuit.

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## AMPLIFIER PANEL



6 photo sockets and d.p. changeover slide switch all


## THIS MONTH'S SNIP.

## BREAKDOWN PARCEL-

four unused made for computer units containing most useful components, and these components unlike those from most computer panels, have wire ends of easily usable length. The transistors for instance have leads over $1^{\prime \prime}$ long, the diodes have approx. $\frac{1}{2}$ leads. List of the major components is as follows: 17 assorted transistors, 38 assorted diodes, 60 assorted resistors and condensers, 4 gold plated plugs in units which can serve as multipin plugs or as hook up boards for experimental or quickly changed circuits (note we can supply the socket boards which were made to receive these units). The price of this four units parcel is $£ 1$ including VAT and post (considerably less than value of the transistor or
diodes alone). Don't miss this splendid offer.
diodes alone). Don't miss this splendid offer.
MAINS TRANSFORMER BARGAINS
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18 t amp
1 amp
18 v 1 amp
$6 \cdot 3 \mathrm{v} 2 \mathrm{amp}$
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erator: requires only a oltmeter connected to its exminals. Voltage is Higher or lower speeds give proportional volts,
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10 amps-second switch 10
contact opens a few mecond contact opens a few minutes
after 1 st contact. 95 p.

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## IT'S FREE

Our monthly Advance Advertising Bargains List gives details of bargains arriving or just arrived-often bargains which sell out before ing advertisement can appear-le's an interesting list and it's free-just send S.A.E. Below are a few of the Bargains still available from previous lines.
Rigonda "'Party Time" Stereo Record Players. A further batch has just arrived, but we have a lot of further batch has just arrived, but we have a lot of
out-standing orders and so we urge you, if you want one, to call in or post your order right away. As with the first batch all are "returns under guarantee" or "service room rejects", but we guarantee them to be repairable, and will exchange any not so. Price is repairabe, and will exchange any not so. Price is
only $£ 5.95+75 \mathrm{p}$. Carriage $£ 2.00+25 \mathrm{p}$, this is of course less than the price of a turntable, so they are a very popular item, hence the urgency for ordering quickly.
Spares for Party Times. Circuit diagrams 50p, Cartridges $£ 2.25$ Record mats 85p, Mains trans formers $£ 3 \cdot 00$, Amplifiers $£ 2 \cdot 50$, Gram motors £3-00.
Ask about any other spares you require and when Party Time speakers, $£ 9.50$ a pair. All prices include post and V.A.T.
This Months Special Offer. All our stocks of 7.029 cable with earth wire have now been sold, but we still have some of metres, also as an price, namely $\mathbf{5 8} \cdot 50+72 \mathrm{p}$ for 100 metres, also as an extra inducement to buy, during August and September, with every coil we will give
free; 100 metres of single $1 \cdot 5 \mathrm{~mm}$ which you can use as the earth wire. If not collecting, please add $£ 3 \cdot 00$ carriage.
250 watt Mains Transformer-40 vecondary, made up of four 10 v sections, all the ends of which are brought out to the tag panel, so they can be separated if required-also the 10 v coils are all a very heavy of these coils can be logded un to the all 250 any one his wattage can be spread to the full 250 watts, or We can recommend spread over two or more coils. be can recommend his transformer for heavy duty battery charging-high power amplifier-plastic sealing-soll heating-light welding and dozens of
other jobs. Price, still only $£ 4 \cdot 50+36 \mathrm{p}$. Post $£ 1-50$ +12 p .
Flex Bargain. 3 core of $14 / 0 \cdot 006$, modern coloured cores. White circular p.v.c. outer. A standard flex for appliances using up to 6 amps, or for extensions, leads etc. Special purchase enables us to offer this at £8. 50 for 100 mm coils $(+68 \mathrm{p})$. Post $£ 1 \cdot 50+12 \mathrm{p}$.
Save Yourself A Fortune. Build your own rechargeable batteries; using our ex-Home Office nickel cadmium cells-these cells are German made, ref NCB 22 M , which we understand are $\frac{1}{2}$ amp hour rating. Normally these cells retail at about $\mathbf{1 1} 00$ each, but a special purchase enables us to offer them at only 30p each, or four for £1-08. Post $30 \mathrm{p}+3 \mathrm{p}$.
Free Gift: all who purchase 12 cells, will receive, free of charge, a mains operated ni-cad charger unit. DONT miss this offer
Self Repairing Fuses-not exactly; but our magnetic circuit breakers do the same job and are a boon for the test bench, saving valuable time. In the event of a short, they trip almost instantly, before the fuse can blow. They are rated at 1.5 amps (enough for the average repair bench). Simply wire it in parallel with your bench switch-you would then use the circuit
breaker to switch bench supply on, but keep your breaker to switch bench supply on, but keep your
normal switch for loads over 1.5 amps-a real normal switch for loa
bargain @ $£ 1 \cdot 00+8 \mathrm{p}$.
9v-0-9v Mains Transformer. ' $C$ "' core construction, $\frac{1}{2}$ amp continuous rating. Very compact, but there is still room to add a few extra turns for an extra
winding, or to change the voltage to, say, 20 v . In fact, the transformer uses a separate bobbin for the secondary-its not varnished so if you want a special voltage transformer quickly, then this could be the answer. Price $£ 1 \cdot 50+12 \mathrm{p}$. Post $20 \mathrm{p}+2 \mathrm{p}$.
$6 \cdot 5 \mathrm{v}-0.6 \cdot 5 \mathrm{v}$ Mains Transformer. Continental make, but has standard $230 / 40 \mathrm{v} 50 \mathrm{~Hz}$ primary and is uprigh mounting, and is rated at $0 \cdot 75 \mathrm{~A}$. Price $£ 1 \cdot 75+14 \mathrm{p}$. Post $20 \mathrm{p}+2 \mathrm{p}$
$\mathbf{1 5}$ Core Flex Cables: Coloured coded cores, rated at 3 amp, with circular p.v.c. outer-suitable for module inter-connections etc. 10 meter coil $£ 1 \cdot 00+$ 8 p .
Rotary Switch. Heavy duty-made for switching d.c., these will make and break really high a.c. currents. cover engraved $\mathbf{0}$ or more amp-we have t) pe (A) engraved "on", "high", "off", "low". Six wires can be brought to the switch and would be joined as follows: 1 to 5 and 6 to 2 and in the other position, 1 to 3 and 2 to 4. Prices: (A) $£ 1 \cdot 00+8 \mathrm{p}$. (B) $£ 1 \cdot 50+12 \mathrm{p}$.
Motor with Fan Blades, mains operated, nicely made motor with long bearing for quiet operation and good quality set of fan blades, made by Smiths (air moving division). It is a simple matter to make a stand out of
14 gauge (clothes line) wire, you then have a simple 14 gauge (clothes line) wire, you then have a simple
hut efficient desk fan. Or if you fit this behind a hut efficient desk fan. Or if you fit this behind a heating element, in a box, you have a fan heater.
Price of motor and fan, $22 \cdot 50+32 \mathrm{p}$. Post $50 \mathrm{p}+6 \mathrm{p}$.


Doram's new catalogue is one of the great events of the electronic year, 64 pages of new ideas in construction kits, capacitors, resistors, semiconductors, wires and cables, transformers, plugs and sockets, hardware, indicators, switches, radio equipment, tools and test equipment, audio equipment, books. All top quality and terrific value because you can depend on Doram.

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## Sirac Mk1 valve Amplifier <br> Circuit Diagrams Outline Drawings Exploded Views...


all you need to know for constructing Chris Rogers' outstanding new valve amplifier. Then compare the musicality for yourself with a transistor-type unit!

## Controversial Comparison

An evaluation of the new crop of moving-coil phono cartridges and their complementary voltage step-up devices. Among those tested are the Fidelity Research FR 3, Entré I, Sony XL55, Ultimo 10A, and Nakamichi 1000, and 7 others.

## Win some Aiwa Super-fi

Another big competition, with the new Autumn range of Aiwa equipment to be won.

## Listening with Beyer

A special review of the Beyer infra-red headphone system.

## Amplifiers Examined

This series for the more technically-minded looks this month at the 'Pulse Width Modulation' philosophy. We also test Cambridge's P80 amplifier - and the new Meridien loudspeaker/power amplifier and pre-amplifier.

## Hifleno

November issue
On sale Friday, October 14

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ELECTRONIC CAPACITORS: Axial lead type (Values are in $\mu \mathrm{FF}$ )
63V: $0.47,1-0,1-5,2-2,25,3-3 ; 4.7,6 \cdot 8,8,10,15,22,9 \mathrm{p} ; 47,32,50,12 \mathrm{p} ; 63,100,27 \mathrm{p}$;
$50 \mathrm{Y}: 1.0,7 \mathrm{p} ; 50,100,220,25 \mathrm{p} ; 470,50 \mathrm{p} ; 1000,62 \mathrm{p} ; 2200,68 \mathrm{p} ; 40 \mathrm{~V}: 22,33 \mu \mathrm{~F}, 9 \mathrm{p} ; 100$,
 $80,100,160,3 \mathrm{p} ; 220,250 ; 13 \mathrm{p} ; 470,640,25 \mathrm{p} ; 1000,27 \mathrm{p} ; 1500,30 \mathrm{p} ; 2200,34 \mathrm{p} ; 3300,52 \mathrm{p} ;$
$4700,54 \mathrm{p} ; 16 \mathrm{~V}: 1040,47,68,7 \mathrm{p} ; 100,125,8 \mathrm{p} ; 470,16 \mathrm{p} ; 1000,1500,20 \mathrm{p} ; 2200,34 \mathrm{p} ;$

 | TANTALUM SEAD CAPACITORS | POTENTIOMETERS (AB of EGEN) |
| :--- | :--- | :--- | :--- | $35 \mathrm{~V}: 0.1 \mu \mathrm{~F}, 0 \cdot 22,0 \cdot 33,0 \cdot 47,0.68,1 \cdot 0$,

$2 \cdot 2 \mu \mathrm{~F}, 3 \cdot 3,4 \cdot 7,6 \cdot 25 \mathrm{~V}: 1-5,10,20 \mathrm{~V}:$
$1 \cdot 5 \mu \mathrm{~F} \quad 13 \mathrm{p}$ each. $10 \mathrm{~V}: 22 \mu \mathrm{~F}, 33$, $6 \mathrm{~V}: 22 \mu \mathrm{~F}, 47,68,3 \mathrm{~V}: 100 \mu \mathrm{~F}$ 20p e
100V:0.001, $0.002,0.005,0.01 \mu \mathrm{~F}$
$0.015,0.02,0.03,0.04,0.05,0.056 \mu \mathrm{~F}$
0 p $\frac{0.1 \mu \mathrm{~F}, 0.15,0.27 \mathrm{p} \text {. }}{\text { CERAMIC CAPACITORS } 50 \mathrm{~V}} \mathbf{0 . 4 7 \mu \mathrm { F }} 10 \mathrm{P}$

| Range: 0.5 pF to 10 nF |
| :--- |
| 15nF, $22 n \mathrm{nF}, 33 \mathrm{nF}, 47 \mathrm{nF}, 4 \mathrm{p}, 100 \mathrm{nF}$ |

POLYSTYRENE CAPACITORS:



TRANS FORMERS * (Mains Prim. 220-240V)

| 6-0-6V 100 | ${ }^{90} \mathrm{p}$ | $\begin{array}{ll}20-0-20 & 2 A \\ 6-0-6 \mathrm{~V} & 1-5 \mathrm{~A} \\ & 320 \mathrm{p}+ \\ \\ \text { 34, }\end{array}$ |  | Easibuild Organ. General Coverage |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9-0-9V 75 m | 95p |  |  |  |  |  |
| 12-0-12V 100 mA | 92 p | 0-18 0-18V 1.5A |  |  |  | ke Sensor Alarm, |
| 15-0-15V 100mA | 185p |  |  |  |  | S. |
| 0-12 0-12V 150mA | 140p | $9-0-9 \mathrm{~V} 2 \mathrm{~A} 270$ |  | Digita |  | dio 2 Tuner, TV |
| 0-6 0-6V 280 mA | 150p | 12-0-12V 2A 320 |  | Games and Kit for RIfle attachment. |  |  |
| 12-0-12V 0.5A |  | 30-25-20-0-20- |  |  |  |  |
| 0-12 0-12 0-5A 24 | 40p+ | 25-30 2A |  | 'JUBILEE Elactronic Organ, GP SW |  |  |
| 15-0-15V 0.5A 22 | 20p+ | LT44 |  | Wave Generator, Wide Range Volt- |  |  |
| $20-0-20 \mathrm{~V} 8 \mathrm{VA} 22$ | 20 p | 0-6 |  | meter RF Resonance Indicator. |  |  |
| 24-0-24V 0.5A 28 | 80 p |  |  | Send SAE plus 5p per list. |  |  |
| 0-12V 1 A |  | 0-15 0-15V 6VA |  | NEL METERS* |  | FSD <br> $50 \mu \mathrm{~A}-0-50 \mu \mathrm{~A}$ <br> $100 \mu \mathrm{~A}-0-100 \mu \mathrm{~A}$ <br> $500 \mu \mathrm{~A}-0-500 \mu \mathrm{~A}$ <br> £4-25 each |
| 30-24-20-45-12-0 $1 A$ |  |  |  | $60 \times 46 \times$ | 35mm |  |
| - | 360p |  |  |  | mA |  |
| 30-24-20-15-12-0 |  |  |  | 0-100ر | $0-500 \mathrm{~mA}$ |  |
| 2A multi tap 4 | 45 p | LT700 Min. O |  | 0-500 0 A | 0-1 Amp |  |
| 16-0-15V 1A 24 | 25 | 1.2K, Sec. 3.28 |  |  | C |  |
| 18-0-18V1A 27 | 75p+ | MOT Min. O/P |  | 0-1mA | $0-300 \mathrm{~V}$ DC | $108 \times 82 \times 38 \mathrm{~mm}$ |
| $30-0-30 \mathrm{~V} 1 \mathrm{~A} \quad 29$ | 95p+ | 1-2K, Sec. 8 , |  |  |  | $0-50 \mu \mathrm{~A}$ |
| (Please add 48p | p\&p | harge to all pri |  | 0-50mA "VU" |  | $0-100 \mu \mathrm{~A}$ |
| marked + , above | our | mal |  |  |  |  |
| RF CHOKES PC mounting |  | FORMERS 6 mm .10 mm |  | DERING |  |  |
| $1 \mu \mathrm{H}, 4.7,10.22$ |  | 20p each |  |  | 340p | atio |
| $33 \mu \mathrm{H} 47{ }^{\prime} 100{ }^{\prime 2}$ |  |  |  |  | 365p | above Meters 79p |
| $470 \mu \mathrm{H} 7501 \mathrm{mH}$ |  | Quick Blow |  | 25W | 340 p |  |
| $1.5 \mathrm{mH} 2.55 \& 10$ |  |  |  | Stand | 140p | DUAL "VU" |
| 35p each |  | 1 Anti-Surge 8p |  | dless Iron | 1400p | METER |
| $\mathrm{mH}=100 \mathrm{mH}$ |  | ders Enclosed 22p |  | 40p po | tage on |  |
| 90 p each |  | nt |  | f the ab | ve | ¢5 |



WATEOAD EIECTRONICS

## (Continued from opposite side)

 <br> \section*{DIODES <br> \section*{DIODES <br> AA119 *BRIDGE} *BRIDGE}SPEAKERS 8
8
2
2.5
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2

AEY11
BA100
BA102
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BY100
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BY128
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OA9
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OA91

| OA 95 |
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| OA 20 |

OA20
iN914
IN916
iN40

IN4006/7*
in448 iN44

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LEDS + Clip TLL209 Red $13 p$ 7 Segment Displ TiL211 Grn 23 p 2-LT-01, Futabe

3A/400V* 20p $3 \mathrm{~A} / 600 \mathrm{~V}^{*} 27 \mathrm{p}$ $3 \mathrm{~A} / 1000 \mathrm{~V}$ *30p
 SCR's*



## 




 | TIL117 | 164p |
| :--- | :--- | :--- |
| VOLTAGE | REGL | $\begin{array}{ll}\text { 723 DIL } & \text { REGULA } \\ \text { TBA625B } & \text { 95p } \\ \text { TO3 Can } \\ \text { Type }\end{array}$

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|  | Plastic <br> body <br> spp <br> 10 <br> 15 pp <br> 15p <br> 8p | $\begin{gathered} \text { Open } \\ \text { metal } \\ 8 p \\ 8 p \\ 13 p \\ 15 p \\ \hline \end{gathered}$ | Moulded with contacts 20p |
| Din | Piugs | Sockets | In line |
| 2PIN Loudspeaker 3,4 \& 15 piñ Audio | 13p | 8p | 20p |
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$1 \cdot 5 \mathrm{~mA}$-6A
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\% D.C.,
$1.5 \%$ A.C.

U4313
20,000 o.p.v. $0.6 \mathrm{~mA}-1.5 \mathrm{~A} \quad 0.5 \mathrm{~mA}-2.5 \mathrm{~A}$ $75 \mathrm{mV}-600 \mathrm{~V} \quad 75 \mathrm{mV}-1000 \mathrm{~V}$ $15 \mathrm{~V}-600 \mathrm{~V}$ 1K-1M $0.5 \mu \mathrm{~F}$ $1.5 \%$ D.C., $2 \cdot 5 \%$ A.C.
$50 \mu \mathrm{~A}-2 \cdot 5 \mathrm{~A}$
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