# PRACTICAL WIRELESS

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### NEWS & COMMENT

1030 FREQUENCIES FOR ALL-Editorial Comment

1031 NEW\$ ... NEWS ... NEWS ...

1038 CQ! CQ! CQ! CQ! CQ!

1054 HOTLINES on recent developments-Ginsberg

1055 NEXT MONTH IN PRACTICAL WIRELESS

1066 PRODUCTION LINES—news about products of interest—
Colin Riches

1069 PUBLISHERS ANNOUNCEMENT

1074 ON THE AIR-Amateur Bands-Eric Dowdeswell, G4AR

1076 1079 Broadcast Bands SW—Derek Bell
Broadcast Bands MW—Charles Molloy

### CONSTRUCTIONAL

1032 AUTOMATIC SLIDE SYNCHRONISER—Alan C. Ainslie

1036 CONVERTING EARLY MONO FM TUNERS TO STEREO—
Keith Cummins

1049 AN INEXPENSIVE WOBBULATOR—T. Bailey

1056 DIRECTION FINDING RECEIVER—F. G. Rayer

### OTHER FEATURES

1041 TRANSIENT DISTORTION IN AUDIO AMPLIFIERS—
A. Foord

1065 GOING BACK—earlier days of wireless—Colin Riches

1068 THE OTHER SIDE HEARD (OIRT/CCIR)—Igor Hajek

1069 TECHNICROSS Solution to Puzzle 12

1071 IC OF THE MONTH—RCA CA3130 CMOS Operational Amplifier

PCB SERVICE FOR READERS—SEE PAGE 1070

**EXTRA WITH THIS ISSUF** 

8-PAGE SUPPLEMENT: FAULT-FINDING GUIDE

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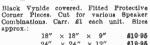
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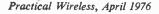
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As featured in 'ETI' Oct. 75 edition

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	ZTX 500	- 16p	H	747 Op-amp				
	MJE 340	- 62p	H	(Dual 741)	-		95p	) S
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EBC81	0.89	EF91	1.35	PCF80	0.63	PY81/800	0.56	30F5/PF8	18
EBF80	0.63	EF92	1.51	PCF82	1.87	PY82	0.70		1.35
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DY86	0.45	EL41	0.90	PCF805	0.90		0 85	12AT7	0.50
DY87	0-45	EL42	1.65	PCF806	0.80	5R4GY	1 20	12AU6	
DY802	0-47	EL84	0.85	PCF808	1.00	5U4G	1 25	12AU7	0-88
EABC80	0-88	EL95	0 60	PCL82	0 45	5U4GB		12AX7	
EAF42	0.70	ELL80	8.00	PCL83	0.70	5 Y 3G T	0.65	12BA6	0.60
EB91	0.80	EM80	0.55	PCL84	0.50	5Z4G	0.95	12BE6	0.60
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AC127	0.25	BF173	0.28						
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AF115	0.85	BFX 29	0-28 0-24	OC42	0.40	IN4005	0.10	2N3615	0.65
AF116	0.35	BFX 88	0.24	OC44	0.20	IN4006	0.13	2N3702	0.11
AF117	0.84	BFY50 BFY51	0.20	OC45	0.20	IN4007	0.12	2N8708	0.18
AF186	0.48	BFY52	0.20	0C11	0.25	1N 4009	0.06	2N3704	0-14
AF239	0.44	BR100	0.40	OC72	0.18	1N4148	0.08	2N 8705	0.15
A8Y27	0.88	BY100	0.27	OC78	0.80	18921	0.07	2N3706	0.11
ABY28	0.25	BY126	0.14	OC77	0.55	IB2033	0.80	2N3707	0.18
BA102	0.25	BY127	0.15	OC81	0.29	182051A	0.20	2N3708	0.07
BA115	0.10	BZX61 M		OC81D	0.28	IB2100A	0-20	2N8709	0.10
BC107	0.14	DAAUI M	0.20	OC812	0-45	183010	0.25	2N8710	0.11
BC108	0.18	BZY88 ac		OC83	0.35	2N696	0-15	2N3711	0-11
BC109	0.12	DAI 100 BC	0.10	OC140	1.14	2N697	0-10	2N3819	0.88
BC113	0.15	CR81-05	0.85	OC170	0.80	2N706	0.10	2N3820	0.50
BC117	0-21	CR81-40	0.50	OC171	0.20	2N706A	0.18	2N3823	0.50
BC143	0.80	CR83-05	0.40	OC200	0.75	2N1131	0-25	2N3903	0-15
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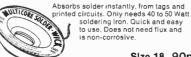
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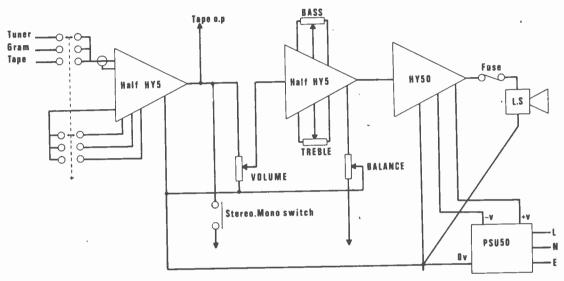
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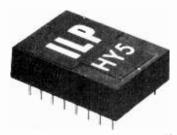
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### SHEER SIMPLICIT



### MONO ELECTRICAL CIRCUIT DIAGRAM WITH INTERCONNECTIONS FOR STEREO SHOWN



The HY5 is a complete mono hybrid preamplifier, ideally suited for both mono and stereo applications. Internally the device consists of two high quality amplifiers—the first contains frequency equalisation and gain correction, while the second caters for tone control and balance.

TECHNICAL SPECIFICATION
Inputs: Magnetic Pick-up 3mV RIAA: Ceramic Pickup 3mV: Microphone 10mV: Tuner 100mV; Auxiliary
3-100mV; Input/Impedance 47kD at 1kHz. Outputs;
Tape 100mV; Main output dob (0·775V RMS). Active
Tone Controls: Treble ± 12db at 100Hz; Bass ± 12db
at 100Hz. Distortion: 0·5% at 1kHz. Signal/Noise
Ratio: 68db. Overload Capability: 40db on most
sensitive input. Supply Voltage: ± 16-25V.

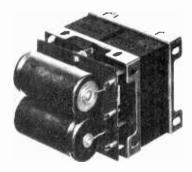
PRICE £4.75 + £1-19 VAT



The HY50 is a complete solld state hybrid Hi-Fi amplifier incorporating its own high conductivity heatslink hermetically sealed in black epoxy resin. Only five connections are provided, input, output, power lines and earth.

TECHNICAL SPECIFICATION
Output Power: 25W RMS Into 80. Load Impedance: 4-160. Input Sensitivity 0db (0:775V RMS). Input Impedance: 47k0. Distortion: Less than 0-1% at 25W typically 0:05%. Signal/Noise Ratio: Better than 75db Frequency Response: 10Hz-50kHz ± 3db. Supply Vcltage: ± 25V. Size: 105 x 50 x 25mm.

PRICE £6.20 + £1.55 VAT



The PSU50 incorporates a specially designed transformer and can be used for either mono or stereo systems.

TECHNICAL SPECIFICATIONS
Output voltage: 50V (25-0-25V). Input Voltage: 210-240V.
Size: L.70. D.90. H.60mm.

PRICE £6.25 + £1.56 VAT

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### High quality audio

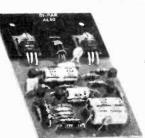


The 450 Tuner provides instant programme selection at the touch of a button ensuring accurate tuning of 4 pre-selected stations, any of which may be altered as often as you choose, by simply changing the settings of the pre-set controls.

Used with your existing audio equipment or with the BI-KITS STEREO 30 or the MK60 Kit etc. Alternatively the PS12 can be used if no suitable supply is available, together with the Transformer T461.

The S450 is supplied fully built, tested and aligned. The unit iseasily in stalled using the simple

Instructions supplied.



25 Watts (RMS)

Max Heat Sink temp. 90C. Frequency response 20Hz. ● Distortion better than 0.1 at 1kHz. ● Supply voltage 15-50v. ● Thermal Feedback. ●Latest Design Improvements. Load-3,4,5, or 160hms. Signal to noise ratio 80db. Overall size 63mm, 13mm.

Especially designed to a strict specification. Only the finest components have been used and the latest solidstate circuitry incorporated in this powerful little amplifier which should satisfy the most critical A.F. enthusiast.

### Stabilised Power Supply Type SPM80

SPM80 is especially designed to power 2 of the AL60 Amplifiers, up to 15 watts (r.m.s.) per channel simultaneously. With the addition of the Mains Transformer BMT80, the unit will provide outputs of up to 1.5A at 35V. Size: 63mm, 105mm, 30mm. Incorporating short circuit protection.

INPUT VOLTAGE OUTPUT VOLTAGE OUTPUT CURRENT OVERLEAD CURRENT DIMENSIONS

33-40V. A.C. 33V. D.C. Nominal 10mA-1 5 amps 17 amps approx.

 $\mathfrak{L}3.00$ 

105mm × 63mm × 30mm TRANSFORMER BMT80 £2:60 + 62p. postage

### D FM TUNER

Fitted with Phase Lock-loop

- **FET Input Stage**
- VARI-CAP diode tuning
- Switched AFC
- Multi turn pre-sets
- LED Stereo Indicator

Typical Specification: Sensitivity 3µ volts Stereo separation 30db Supply required 20-30v at 90 Ma max.

STEREO PRE-AMPLIFIER

A top quality stereo pre-amplifier and tone control unit. The six push-button selector switch provides a choice of inputs together with two really effective filters for high and low frequencies, plus tape output.

Frequency Response + 1dB 20Hz-20KHz. Sensitivity of inputs: 1. Tape input 100mV into 100K ohms 2. Radio Tuner 100mV into 100K ohms 3. Magnetic P. U. 3mV into 50K ohms P. U. input equalization A. P. I.

50K ohms P.U. Input equalises to R1AA curve within 1dB from 20Hz to 20KHz. Supply 20-35V at 20mA. Dimensions—299mm×89mm×

MK60 AUDIO KIT:

Comprising: 2 x AL60's 1 x SPM80, 1 x BTM80, 1 x PA100, 1 front panel and knobs. 1 kit of parts to include onloff switch, neon indicator, stereo headphone sockets plus TEAK 60 AUDIO KIT:

Comprising: Trak veneered cabinet size 15½" x 11½" x 3½", other parts include aluminium chassis, heatsink and front panel bracket plus back panel and appropriate sockets etc. KIT PRICE 25:20 plus 62p postage.

COMPLETE **AUDIO CHASSIS** 



7 + 7 WATTS R.M.S.

7 + 7 WATTS R.M.S.

The Stereo 30 comprises a complete stereo pre-amplifier, power amplifiers and power supply. This, with only the addition of a transformer or overwind will produce a high quality audio unit suitable for use with a wide range of Simple to Instail, capable of producing really first class results, this unit fuse and fuse holder and universal mounting brackets enabling it to be installed in a record plinth, cabinets of your own construction or the cabinet stalled in a record plinth, cabinets of your own construction or the cabinet available. Ideal for the beginner or the advanced constructor who requires Higher and the stalled in a minimum of installation difficulty (can be Installed in 30 mins.).

TRANSFORMER £2.45 plus 62p p & p

TEAK CASE £3.65 plus 62p p & p.

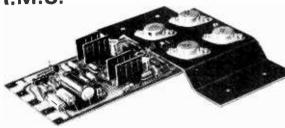
### equipment mono and other modules for Stereo

### IT'S NEW!

'T'S POWERFUL

### IT'S THE AL250

125 watts R.M.S.



### POWER AMPLIFIER

Specially designed for use in-Disco Units, P.A. Systems, high power Hi-Fi, Sound reinforcement systems

The module has a sensitivity of 450mV and a frequency response extending from 25Hz to 20KHz whilst distortion levels are typically below 1%. The use of 4, 115w transistors in the output stage makes the while extremely rugged resulting from incorrect or short-circuit loads is prevented by a four transistor protection circuit.

The unit is intended for use in many applications such as disco units, sound reinforcement systems, background music players, etc.

### SPECIFICATION:

Output Power: 125 watt RMS Continuous

Operating voltage: 50-80 Loads: 4-16 ohms

Frequency response: 25Hz-20kHz Measured at 100 watts

Sensitivity for 100 watts output at 1kHz: 450mV

Input impedance: 33Kohms

50 watts Into 4 ohms: 0.1% 50 watts into 8 ohms: 0.06% S/N ratio: better than 80dBs Damping factor, 8 ohms: 65 Semiconductor complement: 13 transistors 5 diodes Overall size: Heatsink 190mm, length 205mm Height

Total harmonic distortion

ONLY £15.95+8% VAT



Enjoy the quality of a magnetic cartridge with your existing ceramic equipment using the new Bi-Pak M.P.A. 30 which is a high quality pre-amplifier enabling magnetic cartridges to be used where facilities exist for the use of ceramic cartridges only.

Used in conjunction are 4 low noise, high gain silicon transistors. It is provided with a standard DIN input socket for ease of connection. Supplied with full, easy-to-follow instructions.

### POSTAGE & PACKING

Postage & Packing add 25p unless other-wise shown. Add extra for airmail. Min. £1-86

**L10-20-3**0

**AUDIO AMPLIFIER MODULES** 

The AL10, AL20 and AL30 units are similar in their appearance and in their general specification.

However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.S. The versatility of their dealgn makes them ideal for use in record players, tape recorders, atereo amplifiers and cassette and cartridge tape players in the home. Harmonic Distortion Po = 3 watts f = 0.25% Load languages & 150 km. Impedance 8-16ohm

Frequency response ± 3dB Po = 2 welts 50Hz-25KHz Sensitivity for Rated OIP—Vs = 25v. RL = 80ohm f=1KHz 75mV. RMS. Size: 75mm x 63mm x 25mm.

NEW PA12 Stereo Pre-Amplifier completely redesigned for use with AL19 29 39 Amplifier Modules. Features include on/off volume. Balance, Bass and Trebie controls. Complete with tape output.
Frequency Response 29Hz-29KHz (-3dB)
Bass and Trebie range ±12dB Input Impedance 1 meg ohm Input Sensitivity 39emV
Supply requirements 24V. 5mA
Size 152mm x 84mm x 33mm

Power supply for AL10/20/30, S450 etc. Input voltagr 15-20v A.C. Odtput voltage 22-30v D.C. Output Current 800 mA Max. Size 60mm x 43mm x 26mm

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Ref.	VA		p & p					D & D					
No.	(Watts)	£	£	No.	12v	24v	6	£					
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149	60	4.69	0.72	213	1.0	0.5	1 - 86	0.58					
150	100	5 · 33	0 · 85	71	2	1	2.41	0.58					
151	200	8 · 54	1 - 12	18	4	2	2.97	0.72					
152	250	10.32	1 - 4 L	70	6	3	4-43	0.72					
153	350	12 - 47	1:41	108	8	4	5.09	0.85					
154	500	14-33	1.61	72	10	3	5 50	0.85					
155	750	21 - 94	BRS										
156	1000	30 · 57	BR5	116	12	6	5 80	0.97					
157	1500	34-89	BRS	17	16	8	7 · 48	0-97					
158	2000	38 - 92	BRS	115	20	10	10.91	1.61					
159	3000	61 - 48	BRS	187	30	15	14-20	1:41					
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5.0	6.73	0.97	106	4.0	7 98				
6.0	7 - 52	1.12	107	6.0	12:71				
8 0	10.20	1 - 25	118	8-0	13-63				
10.0	10.36	1:41	119	10.0	17.75				
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				93	1500				19-0	)2	BRS
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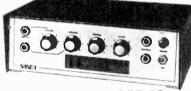
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BC177/8/9	18p	2N2926b
BC182/3/4A	&L10p	2N3053
BC212/3/4A	&L12p	2N3054
BCY70/1/2	16p*	2N3055
BD131 & 13	2 39p*	2N3055
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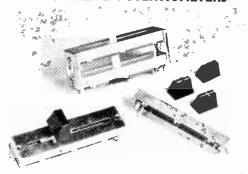
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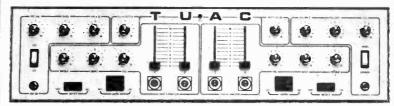
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### Frequencies for all

HE Regional Administrative LF/MF Broadcasting Conference (Regions 1 and 3) was held in Geneva last autumn and, among other things, considered the frequency allocations on those bands and it is good to report that the UK seems to have come out of the affray quite well. In Europe and those African and Asian countries bordering on the Mediterranean the use of these broadcasting bands is at present governed by the European Broadcasting Convention and the Copenhagen Plan, negotiated in 1948. Delegations from 103 countries took part in the conference, the UK delegation including representatives of the BBC, the IBA and the Home Office.

The conference produced an Agreement and Plan which was signed by all but three of the delegations. Other member countries may accede later. The Plan is due to come into effect on 23 November 1978 and is intended to meet requirements for at least the following ten years. Charles Molloy has more to say about the frequency allocations

in his Broadcast Bands column.

Let us hope that the radio amateurs will do as well in the World Administrative Radio Conference in 1979. It may seem strange to some that anybody should be worrying about a meeting that will not take place for some three and a half years. But a great deal of work must be done before the UK delegation can depart with a long list of the frequencies and other facilities that have been requested by every user of the radio spectrum in the UK. The radio amateur's case will, of course, be formulated by the Radio Society of Great Britain and every amateur here can be assured that they will do the best job possible in this respect.

Every amateur can help the cause by complying with his licence conditions, in particular by observing what should be normal good behaviour when on the air. There are those around who would be only too happy to snatch some of the amateur's frequencies in order to further their commercial interests. Bad behaviour on the air is playing straight into

their hands.

It is a matter for regret that the number of licensed amateurs in the UK who belong to the RSGB is very much less than the ideal 100%. The answer surely must lie in the organisation of the Society. The present set-up should be reviewed and the sooner the better. If the planners of the new National Exhibition Centre saw fit to place the Centre outside London then the RSGB should take up its Headquarters and do likewise!

### IPC MAGAZINES LTD. require two Technical Editors

PRACTICAL WIRELESS magazine invites applications from Radio, Audio and Electronic Engineers, preferably with writing experience to fill the post of Technical Editor. Applicants must have a working knowledge of electronics and communications techniques and a logical approach to circuit analysis to assess technical material for publication.

TELEVISION magazine is looking for a person with sound knowledge of receiver techniques, modern constructional methods including colour. This vacancy is ideally suited for Television or Electronic Engineers, preferably with writing experience.

Applicants should write giving full details stating vacancy, salary, career and personal particulars.

The Editor, Practical Wireless—Television IPC Magazines
Fleetway House
Farringdon Street, London
EC4 4AD

### NEWS...

### **Solar Energy Watch**

ASKYS have imported what is believed to be the world's first digital watch, incorporating a wrist-based calculator and powered by solar energy.

It is called the Uranus Time Computer and represents "the State of the Art" in digital integrated circuit technology.

The watch function displays, on command, hours, minutes, day of

the month and seconds.

The calculator is four-function, +,  $\times$ ,  $\div$ , -, machine with an 8-digit display, full floating decimal and automatic stand.

The Time Computer contains a solar cell which draws its power from sunlight, daylight or artificial light. The batteries, therefore, never need replacing.

The heart of the Time Computer is a tiny encapsulated "chip" of silicon containing many thousands of transistors and other active electronic devices. (It is available to special order for £295 including VAT.)

The Uranus Time Computer is on special display at Laskys 481

Oxford Street store.

### Hold very tight please!

THE passengers on the top decks of 30 buses operated by the Scottish Bus Group will be getting music-while-theyride now. A firm called Sounds in Motion Ltd. have installed Pye auto-reversing cassette players to provide the music.

### Alexandra Palace

As an alternative to the usual Woburn Abbey Rally, the Radio Society of Great Britain is arranging to hold an exhibition at Alexandra Palace, North London, on 30 and 31 July and 1 August, 1976.

The site has very adequate car parking and outdoor facilities. Full catering exists within the building.

### NEWS...

### NEWS...

### NEWS...

### **Diary Dates**

March 8-14. Festival International du Son. Paris.

March 9-11. Electro-Optics/Laser International Conference and Exhibition, Metropole Convention Centre, Brighton.

March 9-11. Computermarket 76 Exhibition, Assembly Rooms, Edinburgh.

March 16-18. Computermarket 76 Exhibition, The Forum, Wythen-shawe.

March 18-28. 23rd International Exhibition of Electronics, Nuclear Energy and Aerospace Technology, Rome.

March 23.25. CAD 76—Computer Aided Design Conference and Exhibition, Imperial College, London.

March 23-25. Computermarket 76 Exhibition, New Horticultural Hall, London.

March 24-26. Third Conference on Industrial Robot Technology and Sixth International Symposium on Industrial Robots, The University, Nottingham.

April 5-10. International Component Show, Paris.

April 13-15. All-Electronics Show, Grosvenor House, London.

April 26-30. IFSSEC 76—International Fire Security & Safety Exhibition and Conference, Olympia, London.

April 27 to May 2. Hi-Fidelity 76 Exhibition, Heathrow Hotel, London Airport.

April 28 to May 6. Hanover Fair, Hanover.

May 3-7. IEA 76—International Instruments, Electronics and Automation Exhibition, National Exhibition Centre, Birmingham.

May 3-7. Electrex 76—Electrical Engineering Exhibition, National Exhibition Centre, Birmingham.

May 23-27. International Home Electronics and Domestic Appliance Exhibition (AMDEA/BREMA), National Exhibition Centre, Birmingham.

May 28-31. Sound and Vision 76 TV and Audio Show, National Exhibition Centre, Birmingham.

June 8-11. Communications 76
Exhibition and Conference,
Metropole Convention Centre,
Brighton.

June 8-12. Internavex International Audio-visual Aids Exhibition, Olympia, London.

July 5-8. International Conference on Automobile Electronics (IEE), Savoy Place, London.

July 20-22. Conference on Video and Data Recording (IERE), The University, Birmingham.

Aug 24-26. Education and Communication Technology Exhibition, Holland Park School, London.

Sept 13-17. Micro 76 — International Symposium and Exhibition of Microscopes and Ancillary Equipment, Wembley.

Sept 13-19. 21st International Audio Festival and Fair, Olympia, London.

Sept 14-16. Eurocomp—European Computing Congress, Heathrow Hotel, London Airport.

Sept 20.24. IBC 76—International Broadcasing Convention, Grosvenor House, London.

Oct 19-21. Internepcon/UK Electronic Production Conference and Exhibition, Metropole Convention Centre, Brighton.

Oct 26-29. Microforum International Exhibition, Conference Centre, Wembley.

Nov 16-18. International Minicomputer Conference and Exhibition, West Centre Hotel, London.

### Man of Vision

THE University of Strathclyde recently mounted an exihibition, "Man of Vision", as a Jubilee tribute to John Logie Baird, 1888-1946, the inventor of television and a distiguished former student, who fifty years ago showed the world's first pictures by television. "Man of Vision" occupied the University's Collins Exhibition Hall in Rich-Street, Glasgow, from December 18, 1975 till January 30, 1976, and for the first time assembled under one roof a comprehensive display of Logie Baird's unique television and other equipment supported by personal, photographic, written and other memorabilia spanning his incredibly active lifetime.

### Bipolar Proms and Roms

NTEL have published a 36-page booklet which provides technical information on 13 different ROMs and 24 different PROM types they manufacture. All the devices in the booklet are of Schottky bipolar construction and erasable PROMs and not included.

The booklet incorporates a data sheet for each device, and equivalents chart and gives details of PROM programming equipment.

For every Intel ROM there is a pin and performance compatible PROM, which means that no circuit changes have to be made when a project is finalised and information in PROM is committed to mask-programmed ROM.

All Intel PROMs employ polysilicon fuses which coat the surrounding area in a protective oxide layer when they are 'blown'. With polysilicon fuses there is no danger of a fuse 'growing back' as has happened before with conventional metal fuses.

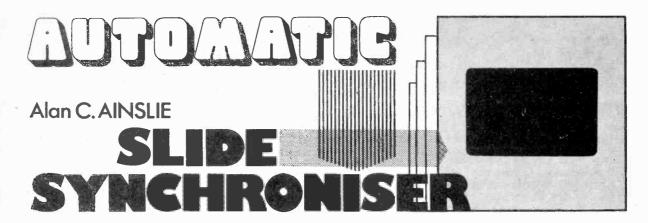
Intel Corporation (UK) Ltd., Broadfield House, 4 Between Towns Road, Cowley, Oxford OX43NB.

### International Conference

THE Institute of Physics is organising a Conference to mark the 50th Anniversary of the Discovery of Electron Diffraction. The Conference will be held on 19-22 September 1977 at Imperial College, London. It is the intention of the organisers that all aspects of electron diffraction should be covered with emphasis in specific areas such as crystal structure determination and surface structure studies. Plenary sessions will be introduced by review lectures from eminent personalities.

There will be an exhibition of equipment held concurrently with the Conference.

For further information please contact: The Meetings Office, The Institute of Physics, 47 Belgrave Square, London SW1X 8QX.



ANY amateur photographers like to play music while presenting a slide show. With the increased popularity of semi-automatic projectors it is fairly simple to synchronise the slide changes to a recorded commentary or music. The conventional method of synchronisation involves recording tones on one track of the stereo tape machine with the commentary on the other. The commentary is played back in mono while the tones are used to close a relay connected to the slide projector remote control circuit.

**OPERATION** 

We shall first consider the general requirements for a tape-slide synchroniser before dealing with the details of the electronics. A tone is generated at a nominal frequency of say 18kHz. This tone is generated continuously and so must be 'gated' to the output whenever the command to change slides is to be recorded. The signal is recorded for the same length of time no matter how brief the push of the slide change button. This necessitates that a form of monostable oscillator be incorporated.

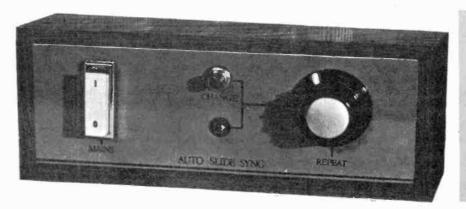
The length of time that the playback relay is closed determines whether the slide projector changes forwards or backwards. Generally, closure for over one second causes the projector to change backwards to the previous slide. Therefore by using a record monostable it is possible to record reversing tones on the tape as well as forward. The detection of the 18kHz tone from the tape playback (which includes fundamentals, high harmonics and hiss)

is a rather difficult task. A narrow bandwidth sensitive detector is needed. This function is provided by a 567 phase-locked loop IC. An additional feature of the synchroniser unit is that the monostable can be switched into an astable and so be used to change slides independently at preselected intervals for continuous unattended showing.

### CIRCUIT DESCRIPTION

The heart of the unit is IC1, the 567 PLL device. VR1 sets the VCO frequency at about 18kHz. A square wave at the VCO frequency is available from a fairly low impedance at pin 5. The VCO is running continuously and is very stable. When recording, S1 is used as the slide change button to record bursts of the 18kHz tone on the tape. When VR2 is at minimum resistance, S2, which is mechanically ganged to VR2, is open. The 555, IC2, then operates as a monostable with the output at pin 3 normally low. Closing S1, earths pin 2 which is normally held to a slightly positive potential by R8. C10 then charges through R11 and D2 while the output at pin 3 goes high, closing the relay. After about 0.5s, C10 will have charged to 2/3Vcc and the output together with pin 7 will go low. C10 discharges through R9 and VR2 (which is at minimum resistance) to wait the next 'change' command.

Keeping S1 closed for longer than the natural monostable period holds the output high until the button is released enabling a long burst of tone to be recorded for reverse slide changes etc. Diodes D4 and D3 prevent pin 3 of the 555 going negative



Photograph showing the front panel of the Slide Synchroniser. The rotary knob marked 'Repeat' is VR2/S2 and the switch marked 'Change' is S1.

### \* components list

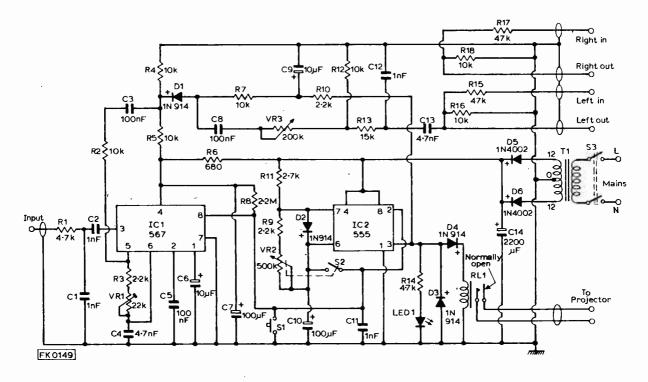
PARTY NAMED IN			41400000				
Resiste	ors			<b>C</b> 7	100 <sub>/4</sub> F	C11	1nF
R1	4 · 7k()	R10	2-2k()	C8	100nF	C12	1nF
R2	10kΩ	R11	2-7ks2	C9	10µF	C13	4-7nF
R3	2·2k()	R12	10kΩ	C10	100nF	C14	2200µF
R4	10kΩ	R13	15kΩ				
R5	10k()	R14	4-7ks2	Sem	iconductors		
R6	6800	R15	47kΩ	IC1	NE567V	D4	1N914
R7	10%Ω	R16	10kΩ	IC2	NES55V	D5	1N4002
R8	2-2M()	R17	47kΩ	D1	1N914	D6	1N4002
R9	2·2kΩ	R18	10kΩ	D2	1N914	LED1	TIL209
' VR1	22kΩ skeleton preset	VR2	500kΩ In ganged with S2	D3	1N914		
VR3	200kΩ panel pres	et		Missol	llaneous		
				The second secon		w contacts	normally open with
All re	esistors # or #W 10	)%		ratin	g to suit projec	tor. T1, 12-	0-12V 100mA mains to-close. S2, on/of
Capaci	itors			gang	ed to VR2. S	3. Double	pole mains on/of
C1	inF	C4	4 · 7nF				, leads, knob and
C2	1nF	Ç5	100nF		to suit.		
C3	100nF	C6	10/2F			*	1, 4

when driving the inductive load which can cause 'latch-up'. LED1 is used to show that a slide change signal has been generated or has been received when playing back.

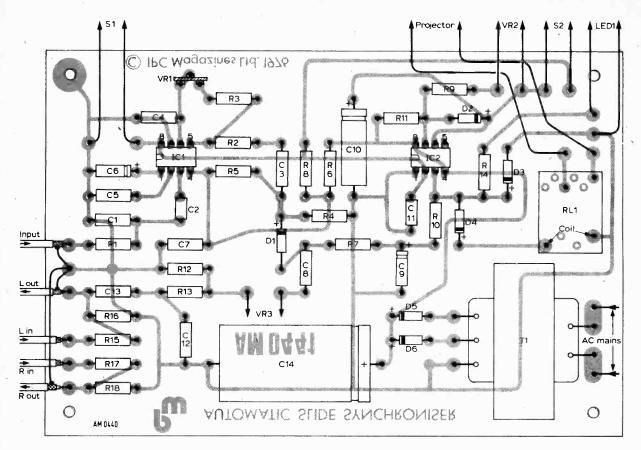
The tone at pin 5 of the 567 is gated to the output by diode D1. The cathode is fixed at about half the supply voltage of the 567, while the anode is normally at zero volts via R7 and R10. Thus the diode is normally reverse biased and cannot pass any signal. When the 555 switches, the relay on pin 3 goes to almost the full supply voltage. The anode of D1 is thus pulled positive. C8 is the output

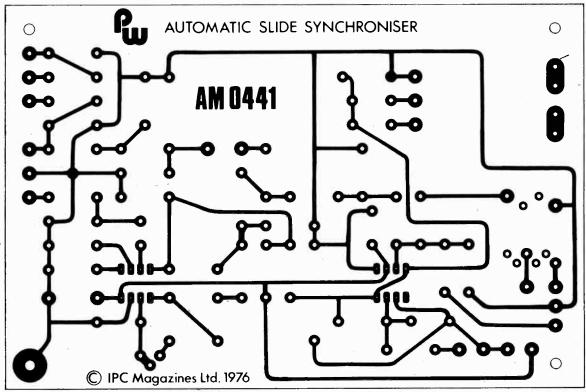
capacitor from the gate. C9 prevents the gate switching too fast and so avoids the generation of clicks or thuds in the output.

VR3 and R12 form a potential divider for the gated tone, with VR3 setting the tone recording level. R13 and C12 form an integrator to remove some of the harmonics from the square wave and so give a sawtooth. The gated tone is mixed with the audio signal by C13 feeding into the junction of R15/R16 which form a potential divider for the left signal.



Circuit diagram of the complete unit, showing the two IC's. IC1 is a 567 phase-locked-loop device and IC2 is a 555 monolithic timing device. RL1 may be any 12V 100mA relay with at least one pair of normally-open contacts.





The printed circuit board above is shown full size and accommodates all the components of the circuit. The hole spacings for RL1 are those for the RS Components 'continental' series type 40 relay, although with careful redrilling another suitable relay may be used.

### PLAYBACK DETECTION

Having got the signal on the tape, all that remains is to detect it on playback. The 567 PLL is a fairly sensitive device requiring only 20mV of tone burst to start the PLL capture process. At small inputs (less than 200mV) the PLL bandwidth decreases with decreasing signal input. C5 sets the bandwidth to be 5% or 6% with a signal just above the detection threshold. C6 controls the response of the output stage while R1, C1 and C2 form a very simple band-pass filter centred about 18kHz to reduce the possibility of the 567 detecting low frequency signals. Even pure signals below the VCO frequency can be detected if they are large enough, as the input stage is a clipper and so generates harmonics. The output of the 567 goes low for the duration of the tone, once the loop has locked (which takes typically a few  $\mu$ S), and so fires the 555 in the same way as closing the 'change' switch S1.

Should a pulse be missed during playback due to dirty heads, S1 still functions and allows the projectionist to catch up with the sound track manually. In the absence of a playback connection, VR2 can be turned clockwise, S1 closed and the 555 will operate as an astable of period set by VR2 over the range of 2s to about 30s. Thus the unit can be used to give repeated slide changes for demonstration and unattended showing. In the astable mode, C10 charges via R11 and D2 while pin 3 is high. When the voltage at pin 6 reaches 2/3 of the supply voltage then the output, and pin 7 go low. C10 now discharges through VR2 and R9 until pin 2 falls below 1/3 of the supply voltage. The output then goes high and the cycle repeats.

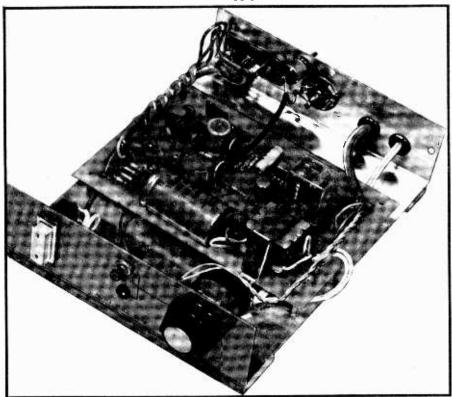
The power supply for the unit is very simple. The 555 timing is independent of the supply voltage as is the VCO in the 567. A stabilised supply there-

fore is not required. The supply to the 555 is about 12V or 13V while the supply to the 567 has to be limited to no more than 10V. This is accomplished by R6 with C7 for decoupling.

### CONSTRUCTION

The slide synchroniser is a fairly complex unit and is fairly difficult to build other than by means of a printed panel. The layout is shown full size in Fig. 2. The connections to the relay will of course depend on the actual relay used. The board, with the layout marked in resist, is etched washed, and the resist removed with a solvent or paint stripper. Holes are then drilled with a number 60 drill (except those for VR1 and possibly C14 and RL1 which may need to be larger). The completed PCB in the prototype was mounted on 10mm stand-offs on a 'U' shaped chassis 150mm wide and 205mm deep. The front and back were bent up by 45mm to form the front and rear panels.

The rear panel has three phono sockets mounted on it (two for left and right inputs, one for the playback signal input) as well as three holes for the mains lead, lead to the projector and a pair of screened leads terminated in phono plugs to connect to the tape recorder input. These holes are fitted with grommets to protect the cables. The three sockets are connected with screened cable with the shields earthed at the securing screw for the tape replay input socket. The electronics are also earthed at this point with a short lead from the point on the print to which the braiding of the S1 lead is connected. The braidings of the screened output leads are earthed at the terminal adjacent to C13. A mains earth is not used as this could introduce earth loop problems. continued on page 1038



General layout view of the chassis, front and rear panels and sockets. The basic chassis is simply a piece of aluminium bent to a 'U' shape.

1035

# converting early MONO FM Tuners STEREO KEITH CUMMINS

THERE are in existence a considerable number of older valve tuners, such as Quad, Leak, Rogers, Armstrong, etc., which are still giving good service. However, stereo decoders for these tuners are no longer available and the writer has frequently been involved with their modification to stereo operation.

Generally the conversions have been "one-offs" with each situation being individually assessed, bearing in mind the availability of suitable decoders. Mullard have now released their LP1400 stereo decoder module, which is physically small and lends itself ideally to modifications of the type referred to, especially as it needs no alignment or other adjustments. The typical input impedance of the LP1400 is around  $150 \mathrm{k}\Omega$  which is quite suitable for connection to either a ratio detector or Foster-Seeley discriminator. It must be remembered, however, that any de-emphasis network at the output of the discriminator must be removed.

### TRANSMISSION THEORY

A very brief discourse on the principles of stereo broadcasting would not be inappropriate at this point. Let us call the two stereo channels A and B. The FM transmitter is modulated in the normal way with a signal consisting of A and B added together (A+B). Non-stereo receivers will produce this signal only, which, being the left- and right-hand channels added, provides normal mono reception. This arrangement ensures system compatibility. The audio bandwidth of this signal extends to 15kHz.

In order to produce the stereo information, the A and B signals are subtracted, and used to modulate a sub-carrier at 38kHz. This double sideband signal therefore consists of (A-B) modulation. If the transmitted signal is monophonic, i.e. A=B, then A-B=O and the 38kHz information vanishes completely, since the subcarrier is suppressed in the absence of "difference signal" modulation.

In order to receive and decode the suppressed subcarrier information, it is necessary to re-insert the missing 38kHz signal at the receiver. To enable this to be done simply, an unmodulated pilot tone at 19kHz is transmitted. As will be seen from Fig.1, this signal slots in between the extremes of the sidebands of the sum and difference signals. The 19kHz signal is doubled in the decoder to provide the missing 38kHz subcarrier, which is then combined with its sidebands. The difference signal can then be demodulated.

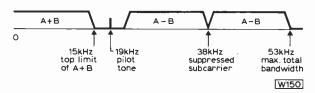


Fig. 1: Frequency spectrum of stereo Multiplex signal. The (A + B) signal provides the normal mono reception.

In order to recover the original A and B signals, a simple algebraic manipulation is carried out. To obtain A, the (A+B) and (A-B) signals are added together: (A+B)+(A-B)=2A. To obtain B, they are subtracted. (A+B)-(A-B)=(A+B)+(B-A)=2B.

Thus, we can recover the original A and B signals (the digit 2 represents a scaling factor). It will be realised that the presence or absence of the 19kHz pilot determines whether the broadcast is stereo or mono. Usually a stereo beacon lamp is provided which lights up when the decoder is presented with a stereo signal. The foregoing description applies to the Zenith-GE multiplex FM stereo broadcast system as used in the UK and Europe.

### SIGNAL STRENGTH

The bandwidth spectrum of the stereo broadcast signal, Fig.1, is considerably wider than that employed for mono. Because of this, any noise present in the system will have a greater interfering effect. The noise in the upper modulation frequency area is much greater than in the lower region and in the process of decoding, this noise is shifted into the audio range and added to the output signal. In order to achieve an equivalent signal-to-noise ratio, about five times the signal is needed on stereo,

compared to mono. Therefore it may be necessary to improve the aerial arrangements if stereo reception is to be entirely satisfactory.

Since the recovered A and B signals contain difference signal (A-B) components in opposite phase, the noise in the two output channels will be predominantly of opposite phase. As a result, we can revert to mono by shorting the A and B outputs together after the decoder, when the stereo noise will cancel. In our application of the LP1400 module, this method works well, so that we can "mono" the

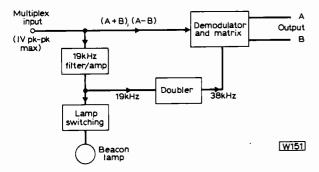


Fig. 2: Block diagram showing the basic circuits of a stereo decoder.

signal at the amplifier control unit or preamplifier without needing to employ the "stereo inhibit" input to the decoder. A block diagram, illustrating the action of the decoder is shown in Fig.2.

### TUNER MODS

Readers will appreciate that "pre-emphasis" of the higher modulating frequencies is applied at the FM transmitter. When de-emphasis is applied at the receiver, the system noise is attenuated in the same proportion. A mono tuner will include a de-emphasis network after the discriminator, and as this would effectively remove the 38kHz difference signal, it is essential that the network be removed when the decoder is fitted. The reader is advised to look for components with  $50\mu s$  time-constant (the de-emphasis figure) e.g.  $47k\Omega$  and 1nF, see Fig.3. When these components have been removed the discriminator

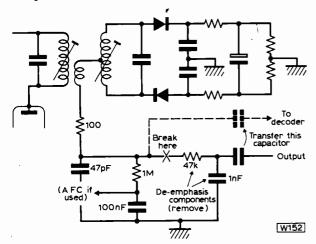


Fig. 3: A typical ratio detector circuit of a valve tuner. Note the removal of the de-emphasis components and the new take-off point.

output can be connected directly to the input of the decoder.

A complete circuit is shown in Fig.4. The low voltage supply is derived from the tuner's HT supply by the use of a resistor R4 and zener stabiliser D1. This simple approach is appropriate where only an HT rail and low voltage heater feed are available. Care should be taken to place the resistor in a position where it can dissipate its heat adequately and feed the circuit from the point where the HT comes into the tuner. Capacitor C3 provides additional filtering of the module power supply.

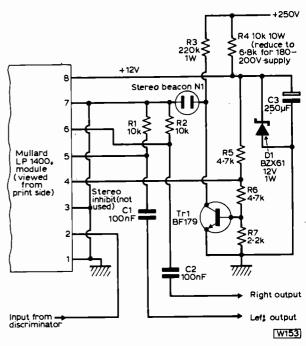


Fig. 4: For correct operation, the Mullard LP1400 module should be connected to a valve tuner, as shown above. The +12V supply to the module is derived from the tuners HT supply via R4, and stabilised by D1 and C3.

### STEREO BEACON

The module is designed to feed a filament lamp as the stereo beacon. Unfortunately no suitable power supply for this is found in the average valve tuner, so a neon indicator is used instead. The filament lamp would normally connect between the supply rail and point 4 on the decoder. Upon reception of stereo, point 4 switches to earth, so turning the lamp on. The neon indicator operates as follows: Transistor Trl is turned on, in the absence of a stereo signal, by the base current feed from +12V via R5 and R6 (point 4 is switched open within the decoder). As a result, Tr1 is bottomed and the whole HT voltage is dropped across R3. When a stereo signal is received, point 4 switches to earth and the absence of a source of base current stops Trl conducting. The collector voltage then rises until the striking voltage of N1 is reached. The neon lamp then lights, indicating stereo reception.

The neon circuit has the advantage that only one transistor is needed and one side is earthed. This makes the mounting easier, in that the cap can be

soldered to a bracket bolted to the chassis. The reader will have his own ideas on where to mount the neon, although a favourite place is at one end of the tuning dial.

The  $10k\Omega$  resistors R1 and R2 are needed to prevent clipping at the output. Note that the decoder module has an overall gain of 6dB under these conditions. If this is too much, R1 and R2 should be replaced by  $10k\Omega$  potentiometers so that the levels can be adjusted as required. Note that C1 and C2 are essential to isolate the DC present at the output of the decoder assuming that the unit is to feed the typically high input impedance of a valve preamplifier.

### **ADJUSTMENTS**

In some cases it may be found that the stereo separation is unsatisfactory resulting from the tuner IF bandwidth being too narrow to accommodate all the sidebands of the difference signal. Careful stagger-tuning of the IF transformers will enable the bandwidth to be increased and so provide adequate stereo effect. The reader is cautioned NOT to attempt adjustments on the decoder board itself, since these will have been correctly carried out during manufacture.

When mounting the decoder in a tuner, make sure that it cannot move and accidently touch the HT supply! This can be an expensive mistake. The positioning should be such that adequate ventilation is provided to prevent overheating. If the unit is to be wired in using the stand-up leads, the print to the edge connector can be cut. This part of the board can then be drilled to accommodate a fixing bracket.

The Mullard LP1400 module can be obtained from Chromosonic Electronics, see ads.



### ISSUES WANTED

..P.W. March to May 1970 (synthesiser article).—J. O'Connor, 23 Rugby Close, Newcastle, Staffs., ST5 3JN.

..two copies of P.W. dealing with the Progressive S.W. Receiver.—T. R. Smith, 7 Purbeck Court, Park Barn, Guildford.

..P.W. for May 1953, January, March, April, August, September 1952, March, November and December 1950 and all copies 1945–1949.—J. Luxton, Bergheim, Battery Hill, Fairlight Cove, Hastings, TN35 4AP.

..issues of P.W. at beginning of 1971 with details of Stereo Tape Recorder.—C. Raymond, 4 St. Augustine's Road, Canterbury, Kent, CT1 1XP.

.. May 1972 P.W. also supplement in same issue on transistors.—E. Barton, Maggieknockater, Craigellachie, Banffshire, AB3 9RA.

..issues of P.W. containing articles on metal detectors.— J. O'Connor, 19 Greenbank Road, Hoole, Chester, CH2 3RW.

..April 1972 issue of P.W. containing circuits of a transistor tester.—R. Murdoch, 5 Banks Road, Mt. Wellington, Auckland 6, New Zealand.

### AUTOMATIC SLIDE SYNCHRONISER-

continued from page 1035

### SETTING UP

With mains applied, a voltage check should show about 13V or 14V on pin 8 of the 555 and about 8V on pin 4 of the 567. With VR2 fully anticlockwise (S2 open), pushing S1 briefly should cause the relay to pull-in and the LED to light for about 0.5s. Keeping S1 depressed should hold in the relay. With the relay held in, the output leads are connected to the input of the tape recorder. With R8 at minimum and the recorder left hand input control turned up, a deflection should be noted on the VU meter. Switching the monitor to 'source' enables one to hear the signal from which the tone burst is derived. With VR1 at maximum the tone should be clearly audible. Decreasing VR1 takes the tone up in frequency. VRI should be set so that the tone is just out of the audible range. S1 is now released to cut off the tone.

The leads that previously carried the tape recorder input signal from the amplifier are now plugged in to the two phono sockets on the back of the synchroniser. The recorder level controls are set to give a normal recording level. Leaving the recorder level controls untouched the audio signal leads are unplugged from the back of the synchroniser. S1 is now pressed and VR3 adjusted to give a reading of slightly less than -20VU on the left hand channel (about 6 or 7% of fsd).

A trial recording is now made of the tone at this level and played back with the left channel tape recorder output connected to the synchroniser tape replay input. Playback of a continuous tone should make the PLL lock-on and the LED light, as well as pulling in the relay. If the playback does not cause the loop to lock, VR3 will have to be reduced in value (assuming that the tape recorder output is turned up full). If this fails then it may well be that the recorder has dirty/magnetised heads or is incorrectly biased.

If all is well and the PLL picks out the replay tone then it is necessary to experiment with VR3 to ensure that there is a reasonable safety margin while on the other hand the recorded signal is not any higher in level than necessary. The tone is recorded at such a low level (-20VU) primarily because the equalisation of the recording amplifier causes the gain to increase with frequency very quickly above 10kHz. Hence the record amplifier is rather susceptible to overload at the frequency used.

When VR2 is turned away from its fully counter clockwise extreme the relay should switch on for 0.5s repeating at intervals of between 2s and about 30s.

### IN USE

The synchroniser is connected between the normal recorder input leads and the tape machine as detailed in the setting-up instructions. With the recorder input level controls set to produce a normal recording level (same position as when synchroniser was set up) every push of the 'change' button records the change tone. If the projector is coupled to the unit it is possible to run through the slide sequence while recording the tones. If a three head tape machine is used it is important that the tape replay input is not connected during recording, as the PLL will lock on to the replayed tones and produce a random series of tone bursts.

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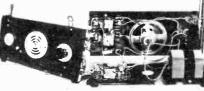
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### in Audio Amplifiers

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The generation of total harmonic and intermodulation distortion in power amplifiers is well known. These types of non-linear distortion may be reduced by negative feedback. However it has been shown that a form of transient distortion can be produced when the open-loop frequency response of the power amplifier is less than the frequency response of the preamplifier. This article discusses why transient distortion is produced, and how it may be eliminated by careful design of the complete amplifier.

### **BANDWIDTH LIMITATIONS**

A complete audio amplifier can be divided into two main sections, pre-amplifier and power amplifier, as in Fig. 1. The preamplifier section may be subdivided for equalisation, tone controls, etc. Any feedback loops in the preamplifier will be over two, or at the most, three transistors.

However, the power amplifier will have a feedback loop enclosing three or more stages. In addition the small signal transistors in the preamplifier will have a much greater gain-bandwidth product than the higher power transistors used in the power amplifier. These factors usually result in the power amplifier determining the frequency response and distortion of the complete amplifier. Typically the power amplifier open-loop frequency, response without feedback, may be as low as lkHz, even though its closed-loop frequency response with feedback, may be over 20kHz.

### **NEGATIVE FEEDBACK**

Before these topics can be discussed in any detail it is essential to understand the basic properties of a feedback amplifier, Fig. 2. The open-loop gain of an amplifier, -A, is the gain with the feedback loop disconnected. The minus sign indicates that the amplifier inverts. The amount of signal fed back is less than unity and B is called the feedback ratio. The closed-loop gain is the overall gain when the feedback path is closed and is given by:—

Closed loop gain = 
$$G = \frac{VO}{V1} = -\frac{A}{1 + AB}$$
 times

For example, if the gain without feedback is 100 times, and the feedback ratio is  $0 \cdot 1$ , then the closed loop gain is:

$$G = -\frac{100}{1 + (100 \times 0.1)} = -\frac{100}{11} = -9.09$$
 times.

This illustrates the very important point that the gain with feedback is approximately 1/B, when the product AB is much greater than unity, i.e.  $G \simeq -1/B$ , if AB>1. In this example the overall gain is REDUCED by a factor of approximately ten times, while the bandwidth is INCREASED by the same factor.

### **NON-LINEAR DISTORTION**

Conventional non-linear distortion arises because of the non-linearities of the input/output transfer characteristics which occur in all physical systems. The distortion produced by a given non-linearity depends on its shape and the nature of the signals. For example, a transfer characteristic such as Fig. 3(a) would cause no distortion of any sinewave having a peak value less than unity, whereas larger sinewaves would be severely distorted. However the transfer characteristic of Fig. 3(b) would severely distort music or small sinewaves, while larger sinewaves would scarcely be distorted at all.

Since musical signals are small most of the time

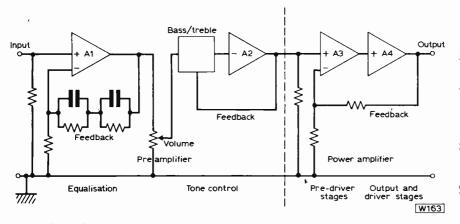
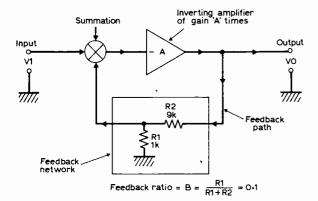


Fig. 1 This block diagram shows the two main sections of a complete amplifier. Three feedback loops, as shown, are typical of a working amplifier.



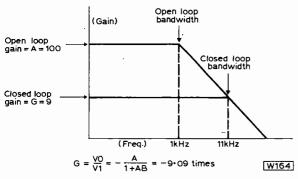


Fig. 2: Properties of an amplifier to which negative feedback is applied

exceeding the RMS value only 15% of the time, a harmonic distortion measurement at full amplifier power has little meaning. Certainly harmonic distortion measurements at lower levels are of much greater importance in detecting cross-over distortion. This can only be satisfactorily detected by using an amplitude of test signal which just spans the cross-over region of +x to -x in Fig.3(b).

### REDUCTION OF NON-LINEAR DISTORTION

For reducing this type of distortion two approaches are usually used. Firstly the non-linearity is reduced by biasing Class B output transistors with a small quiescent current of 30mA or so. Secondly, negative feedback may be applied. A necessary and sufficient condition for low distortion is that the slope of the CLOSED-loop transfer characteristic is constant at all levels below the clipping level.

This condition is satisfied if the OPEN-loop transfer characteristic has a constant slope, or by using sufficient negative feedback to make variations in the open loop characteristic unimportant. This means that the product AB must be much greater than unity. Therefore an open loop characteristic such as Fig. 3(b) would be intolerable, while those of Fig. 3(c) and (d) are acceptable.

The preceeding paragraphs show how non-linear distortion is produced, and may be reduced by negative feedback. Most hi-fi amplifiers are satisfactory in this respect. However, when the open-loop frequency response of the power amplifier is less than the overall response of that portion of the transmission system preceding it, additional problems lead to transient distortion.

### TRANSIENT DISTORTION

Fundamentally, transient distortion arises from the poor overload characteristics of feedback amplifiers. The block diagram for a typical arrangement is shown in Fig. 4. The power amplifier is split into two parts with both a limiting and a time delay section shown diagramatically. The limiting section represents the initial stages of the power amplifier which will limit before the power amplifier's output stages. The time delay section represents the low bandwidth of the power transistors.

When an input signal, having a sufficient amplitude and a higher frequency than the power amplifier open-loop cut-off frequency, is presented to the power amplifier input, overshoots in the internal loop drive voltage may be produced. This effect can best be understood by considering a step input. The overall negative feedback can only come into operation AFTER a time delay determined by the power stages. Therefore internal signals may overshoot momentarily. In a poor amplifier this may be several hundred times greater than the nominal value of this voltage. Consequently overshoots may be clipped in the amplifier driver stages if the overload margin is insufficient. This will produce temporary 100% intermodulation bursts. Since audio signals have their maximum slopes around the zero signal level these distortion bursts usually occur in this region. The audible effects resemble high frequency cross-over distortion and create a 'metallic' sound.

### TYPICAL OVERSHOOT LEVELS

A complete theoretical analysis is complex, and would depend on both the preamplifier and power amplifier characteristics, but some results are given

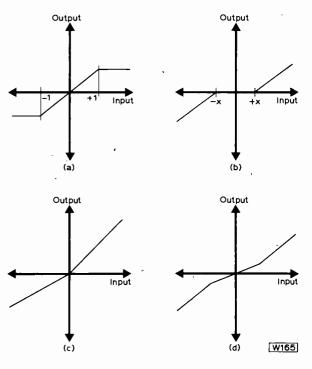
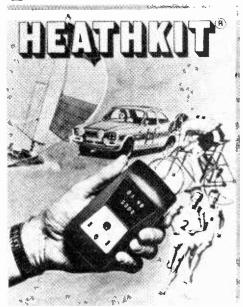


Fig. 3: Transfer characteristic (a) causes clipping, (b) would result in cross-over distortion, (c) is unsymmetrical but acceptable whilst (d) is non-linear but also acceptable.

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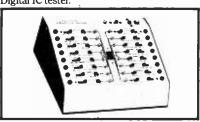
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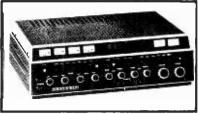
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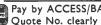
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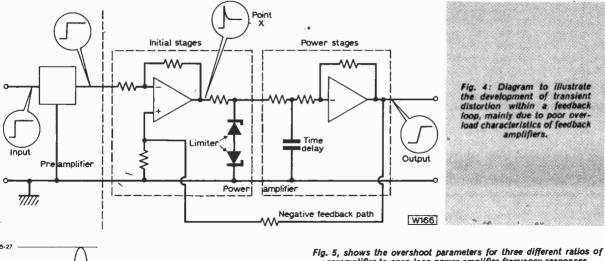
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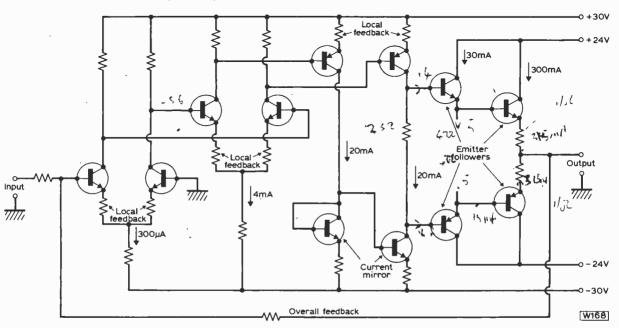
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Overall Frequency Response	Preamp. Frequency Response	Open Loop Power Amp. Freq. Resp.	Closed Loop Power Amp. Freq. Resp.	Peak Output	Overshoot
(a) 22kHz	50kHz	2·5kHz	25kHz	5-27	427%
(b) 19-6kHz	20kHz	10kHz	100kHz	1-58	58%
(c) 19-9kHz	20kHz	20kHz	200kHz	1-00	None

Note:—Peak output is output within the feedback loop, normalised to 1, point X in Fig. 4.



in Fig. 5. For this example the feedback is taken as 20dB and the overall frequency response kept at about 20kHz. In (a) the power amplifier has a closed-loop bandwidth which is half that of the preamplifier, while its open-loop bandwidth is much less. The momentary overshoot within the feedback loop is 427%!

In (b) the power amplifier has a closed-loop bandwidth which is greater than the preamplifier, while its open-loop bandwidth is half that of the preamplifier. Here the overshoot within the feedback loop is 58%. In (c) the open-loop bandwidth of the power amplifier is equal to that of the preamplifier, and there is no overshoot. The closed loop bandwidth of the power amplifier is now 200kHz.

From these results we deduce the general rule that to avoid transient intermodulation distortion the OPEN-LOOP frequency response of the power amplifier should be equal to or greater than the preamplifier frequency response. This requires a good high frequency design with a low value of feedback. When only a moderate value of feedback is used the open loop linearity has to be excellent, because heavy overall feedback is not present to decrease distortion.

When the open-loop frequency response of the power amplifier is higher than the audible frequency range, even moderate overall feedback will give a power amplifier small signal response up to 1MHz and the limiting of the frequency response to 20kHz must be accomplished in the preamplifier.

## **DESIGN APPROACH**

A design criteria for ultimate quality requirements demands that some of the commonly used circuit 'tricks' are **not** employed. For example, bootstrapping and higher feedback for DC than for AC should not be used. A high DC feedback value can cause clipping effects which force DC level adjustment transients through the feedback loop every time the signal changes. If the feedback is the same for AC and DC a number of capacitors can also be eliminated.

The required high open-loop linearity is obtained by using heavy local feedback in each amplifier stage. This increases the open-loop bandwidth and minimises the amount of overall feedback needed to about 20dB.

The output transistors should be used as emitter followers to increase their frequency response and improve linearity. They should be driven from emitter followers in order to minimise the effects of non-linearity and to maximise their bandwidth.

A completely symmetrical design should be used, without bypass or bootstrap capacitors, to improve the amplifier clipping and overload characteristics and to increase linearity at high frequencies. All stages should operate in Class A except for the power transistors. These should operate in Class AB with a high quiescent current, typically 300mA, to totally eliminate cross-over distortion and asymmetrics in the critical low power region.

## CONCLUSIONS

A complete amplifier design along these lines might be similar to Fig. 6. This would have harmonic and intermodulation distortion levels which are comparable with the best designs, but, in addition, would have no transient intermodulation distortion and excellent phase characteristics over the audio band.

R1155B Rx unit aircraft communications & navigational Rx covers 75 to 500Kc, 600 to 1500Kc, 3 to 7.5Mc/s & 7.5 to 18Mc/s, 5 bands in all. Uses 7 valves in Rx & 3 in DF section, also as BFO, AVC or Man control etc. regs ext supplies of 250v HT at 70Ma & 6.3v as O/P for phones. Supplied tested with copy of handbook. £30. SONAR IND UNIT aircraft unit as CRT 5" square dual beam electrostatic with long persistance screen. As approx 40 min & sub min valves etc. int EHT P.U. regs ext HT & LT supplies, unit gives dual beam display with low speed T.B. supplied with copy of circ. £14.50 new or £12.50 S/Hand. DISH AERIALS microwave type 18" dia 43" deep made of dural polished finish new £3.80. AERIAL SYSTEM for use on 100/150mc/s single dipole type with 36ft of 50 ohm coax mast head brk etc. new £5:40. INTER-COM SYSTEM were used by aircraft servicing crew, portable unit will work on 240v AC or 24v DC provides communication for 3 persons, use 3 headsets with throat mikes these are connected to amp unit located in transit case along with P.U. ea headset as vol control & mike swt various ext cables are provided one 100ft & two 24ft cable all stows in transit case. Supplied tested at £18.36 or Untested at £13. V.H.F. AIRCRAFT C/Bx these have two turret swts that select a total of 54 type Hc18 crystals in the range 13.51 to 19.87Mc/s these crystals can be removed or unit can be used as it is with ext power supplies, supplied with circ, full list of crystal freq on request £7. RADIO TELEMETER unit low fre Rx works on 120Kc contains 6 valves, speaker, 2x motors, tape loop, coin box unit works on 200/250v AC all in neat case 14 x 7 x 6" £6.50. FILTER UNITS 10 chan tuned filters cover range 3 to 15Kc approx as 10 tuned circs with LA 2 pot cores okay for remote control £2.50. METER UNIT dual unit at 1 Ma 270' & small 100-0-100Ua meter in same case was used as aircraft range & heading meter 270' scaled 0 to 20 100Ua centre mark only, size case 31 sq. tested £4.50. ROLLER COASTERS ex Ae tuning units coil size 5 x 1¾" 36 tr of 18 swg all RF parts silver plated £3 · 50. **HEADPHONE LEAD & TRANS** made to match high imp O/P to low imp phones 5ft lead with standard jack plug new £1.30. SPEAKER UNITS small horn spk for use on M/Cycle 3 ohm with fix brk & cable spk 5 x 3" new £2.50. METER UNIT X pointer part of R1155 Nav display as 2 115Ua movements, these cross on centre line £2.30. RELAYS 12v DC coil small type 2p c/o with base new 80p. METER PANEL with small 500Ua meter 11 dia scale 0 to 5 & 2 swts £2, CRYSTAL OVEN with 12 type Hc6/u holders these can be removed, oven 24v £1. TAPE DECKS & AMPS BSR type TD2 & 10 two chan £5:50 & £7:50. CALLERS ONLY FOR THESE.

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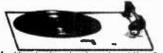
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F YOU build or service radios, particularly superhets, and do not possess a wobbulator then you are working under a severe handicap. A wobbulator is a signal generator whose frequency can be varied by applying an external voltage. In practice, the applied voltage is the timebase output of an oscilloscope, so that as the trace moves horizontally across the screen, the frequency of the signal generator changes. During the flyback period the frequency

An inexpensive

T. BAILEY

returns to its original value.

If the output of the wobbulator is connected to the input of an IF amplifier and the oscilloscope's vertical amplifier input applied to the detector, Fig. 1, the 'scope will display the frequency response curve of the IF amplifier. Adjustments to the IF tuned circuits may then be made and the results seen immediately.

The wobbulator to be described sweeps over a range of at least ±80% of the centre frequency and for selective circuits a "divide by ten" and a continuous control allow  $\pm 0.8\%$  to be achieved. The principle output is a triangular wave which may be attenuated. A square wave output is included which is useful for working on harmonics at higher frequencies. The centre frequency may be varied from about 280kHz to 1.8MHz but this is easily adjusted if necessary. A poor impression may be gained of the linearity when using a very wide sweep range, but up to 40%, far more than is needed for conventional alignment, it is very good. The main use of extremely wide sweeps is for finding spurious responses when linearity is not so important.

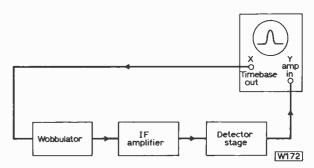


Fig. 1: Block diagram demonstrating the basic use of a Wobbulator.

## THE CIRCUIT

The circuit of the complete wobbulator is given in Fig. 2. Potential constructors will notice the absence of conventional transistor oscillators and coils which always seem to cause trouble. Instead an NE566Y IC

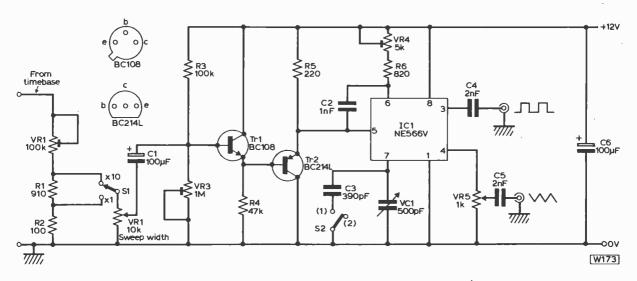


Fig. 2: Circuit diagram of the Wobbulator, showing details of the NE566 IC, and the two outputs giving both square and triangular waveforms. The sweep width control should read VR2.

function generator has been used, which has other advantages as well. A very wide sweep range has been obtained plus very good frequency linearity at moderate deviations.

The circuitry up to C1 is an attenuator VR1/2 for the timebase input voltage which sets the sweep range. Tr1 and Tr2 buffer the voltage control input to the IC with VR3 setting the centre voltage. VR4 provides a frequency adjustment used for setting the ranges whilst C3 and VC1 constitute the main frequency control components.

The wobbulator runs from an external 12V power supply which the author uses for most of his instrumentation, a technique which is recommended to save money! A suitable design for a stabiliser is given in Fig. 3.

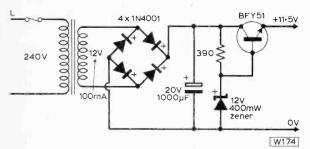
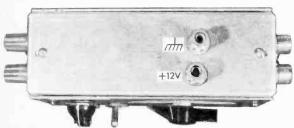


Fig. 3: The above circuit shows a suitable design for a stabilised power supply for use with this Wobbulator.

## CONSTRUCTION

The prototype was built on a small piece of veroboard and housed in a "universal chassis" case. Later a PCB was devised and this is shown in Fig. 4. Con-





External photographs of the unit, showing the positioning of the sockets and switches

## \* components list

Resistors R1 910Ω	R4 47kΩ
R2 100Ω	R5 220Ω
R3 100kΩ	R6 820Ω
All t or tW 10%	02011
VR1 100kΩ preset (PCB)	VR4 5kΩ preset (PCB)
VR2 10kΩ linear pot.	VR5 1kΩ linear pot.
VR3 1MΩ preset (PCB)	
Capacitors	
C1 100µF 25V	C4 2nF ceramic
C2 1nF ceramic	C5 2nF ceramic
C3 390pF SM	C6 100µF 25V
VC1 500pF variable capa	citor
Semiconductors	
Tr1 BC108 Tr2 BC21	4L IC1 NE566V
Miscellaneous	
Casework, 'universal ch	nassis' 6 x 4 x 2in. plu
6 x 4in. plate (Home Radio	o) or box 6 x 4 x 2in. (AB13
Switch S1 cingle note	changeover toggle. S

structors should find little difficulty in adapting the circuit to veroboard and pins. A piece of  $0 \cdot 1$  in matrix is cut down to  $4 \cdot 2 \times 1 \cdot 3$  in thus giving  $41 \times 12$  holes with the copper strips running lengthwise. Cuts are made in the copper strips as appropriate.

The components are then mounted as in Fig. 5. The IC should be soldered last of all but if desired use an

IC holder or use socket pins instead.

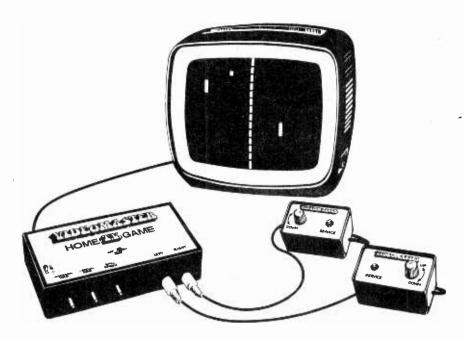
PCB Service Ltd. see ad. page 1070

Mark out and drill the case with the help of the photographs. No dimensions have been given as there is plenty of room and the optimum layout may depend on the components used. The circuit board is bolted to the base with two 6BA nuts and bolts with nuts as spacers. The co-ax sockets also required 6BA fixing. Complete the wiring and check it before switching on.

## SETTING UP

The process of setting up and testing consists largely of adjusting the three preset potentiometers and calibrating the main frequency control. Starting with VR3, this should be adjusted with no sweep input connected so that pin 5 of the IC is 11-5V with a supply of 12V. Next, connect the oscilloscope's timebase output to the input terminal and starting with VR1 at maximum resistance adjust it until the voltage at pin 5 is swept between the supply line of 12V and about 9V. If the oscilloscope is not calibrated vertically and hence cannot be used for this purpose, employ a very slow sweep and a voltmeter.

Lastly, adjust VR4 to achieve the desired frequency ranges (280-465kHz and 400-1800kHz were used in the prototype) and calibrate the main frequency control against a radio or signal generator, with no sweep input. A simple test is to set up the generator with one of the outputs connected to the vertical input of the 'scope, connect the sweep input and set the wobbulator for maximum sweep tuning to its lowest frequency. Adjust the timebase so that a number of cycles are visible. These should vary in period across



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2N2926 all 0-08 2N3053 0-15 2N3054 0-40 2N3055 0-43 2N3702/3/4 0-11 2N3705/6 0-11	4 × 2½ × 1½" 0.49 4 × 2½ × 2" 0.50 3 × 2 × 1" 0.42 6 × 4 × 2" 0.75 7 × 5 × 2½" 0.82 VEROBOARD	7470/72 0.35 7475/76 0.35 7480 0.42 7482 0.73 7483 0.80 7484 0.87 7486 0.87 7486 0.80 7486 0.80 7487 0.80 7486 0.80
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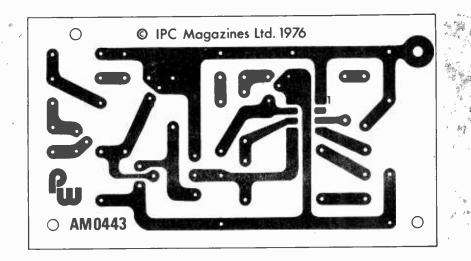
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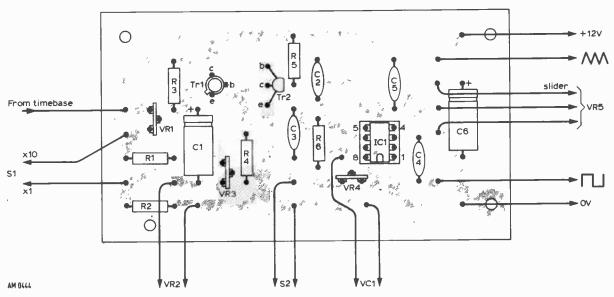


Fig. 4 and Fig. 5: The top drawing shows a foil side view of the pcb, while the lower gives the precise positioning of the various components. Both views are shown full size. Note. A link is required from the rotor of S1 to VR2.

the screen and reducing the sweep width should make the variation less.

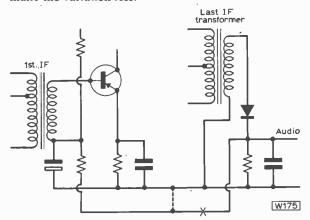


Fig. 6: In order to avoid non-linear displays at maximum sweep, the above AGC neutralising modification is recommended.

The only thing to remember about using the wobbulator is that at near maximum sweeps the display will be decidedly non-linear at the edges. Fig. 1 shows the conventional way of using the wobbulator to align IF amplifiers. When doing this it is advisable to turn off the AGC or otherwise neutralise it. A method of doing this in a conventional IF amplifier is shown in Fig. 6, the circuit being broken at point "X" and the dotted connection being made to earth.

The conventional injection point is the base (grid, in valve receivers) of the mixer which prevents loading the first IF transformer. The 'scope input is connected to the point marked "audio" and the lowest sweep speed used that gives a flicker-free and viewable trace.

Adjustments may also be made to the alignment of RF and oscillator stages but beware of adjusting a tuned circuit to which the wobbulator is connected directly as the loading will be excessive. If, at any time, the output is too great even when fully attenuated, connect a capacitor of a few pF in series with the lead to the receiver.



## ON RECENT DEVELOPMENTS

## AN EXPENSIVE RECEPTIONIST

Hands up if you ever sipped lemonade through a straw. Bet you did when you were little. Now hands up if you earn your living by sucking through a straw. Don't laugh, because that is exactly what one very brave young lady does. Her name is Margaret and she's a receptionist. She's also been paralysed from the neck down since 1956.

It seems impossible and yet, with the aid of electronics, Margaret is leading a very useful life and doing a full-time receptionist's job at a University. So how does it all work. Well, Margaret uses a kind of electronic straw—just like the one you (?) and 1 use to sip that lemonade through, only it's different if you see what I mean. Her straw has two tiny pressure sensors in it. One sensor responds to blowing while the other is trained to respond only to a suck or sip.

A VDU (visual display unit) is a feature and a list of available things, like telephone numbers etc. are thrown up on the cathode ray tube, At the side of the list of actions (or whatever) is a cursor and this travels down the list a line at a time with each puff in the straw. When the desired line is arrived at, Margaret simply sucks/sips and the computer-based system does the rest. A telephone number is dialled and Margaret can then speak to the person at the other end of the line. By selecting other instructions it is possible to select, say, a tape recorder facility for recording messages. Margaret can now handle a multiple-line business telephone system-all by herself.

Oh, yes, I nearly forgot, she types letters, too. The alphabet is simply called up on the VDU and the cursor "puffed" along to select the required letter or numeral. Print out of the letters is a teleprinter-type of keyboard which types out letters and numbers in response to electrical inputs. A voice terminal is the next step for her electronic helpers but this isn't "on-line" as yet. Please note the system is not available for general use and takes the form of an experiment.

## TIRED TYRES

Electronics in motor vehicles has long been a field of development. Transistor ignition is one such area. An interesting development is taking place in Germany, so I hear. This ingenious application allows the driver of a vehicle to know instantly when his tyres start to go down. In other words, his tyre pressure is constantly monitored—even when the vehicle is in motion!

Transmitting and receiving coils are mounted at each wheel suspension. The transmitting coil is fed with a 7kHz signal. On each wheel rim is mounted a small coupling coil which, as each wheel rotates, passes some 10mm from the two coils on the suspension. The small coupling coil on the wheel rim is connected to a tiny pressure sensing switch located in the tyre valve. While the tyre pressure remains above a predetermined minimum level, the small coupling coil will couple the 7kHz signal from the transmitting coil to the receiving coil with each revolution of the wheel. However, if the pressure were to drop below the minimum level, then the pressure-sensing switch at the valve would open and the wheel rim coil would not couple any signal from transmitting coil to receiving coil as they passed. Thus no signal would be passed back to the control unit on the dash board and a warning would immediately be given to the driver. The company is reported to have said that it is ready to go into production with the system if sufficient demand is evident. Doubtless, motorists who are tyred of getting flat tyres will favour what amounts to an airraising innovation.

## TUBES, AGAIN

Just as I thought that the computer memory research front was going to be quiet for a while, so a group of Dutch workers have proved me wrong. They have come up with a new type of memory which is claimed to be cheaper than ferrite-core stores and offering greater density, too. The new memory relies on what is called the Phonon echoes effect. These "echoes" develop when powdered quartz is excited by high-frequency pulses. One important discovery is

that the echoes so recorded and stored can be read out a year later without any problems. A tiny glass tube, 1cm in diameter and 1cm in length is filled with quartz powder and the resultant capsule has a coil plus capacitor combination around it i.e., a tuned circuit. One of these little tubes has been found to store up to 100,000 bits of information. Pulses are applied in pairs and the highest frequency to date has been 80MHz. Workers believe that up to 10GHz is possible as a frequency for these pulses.

## **OW!!**

The ancient art of acupuncture has gained in popularity in recent years. Apparently the idea is to poke needles into the body at certain points and this makes you better. Now you wouldn't think that electronics could have anything to offer here because the actual mechanism i.e., the pin sticking is very simple. But no, you'd better believe it, electronic acupuncture has arrived. Of course it's claimed to be superior to the older techniques. It's more accurate, can be quicker and is more hygienic. First we do away with those needles and use a laser beam instead. The beam is completely sterile which can't be bad. A flexible light fibre probe is used to locate the acupuncture point accurately. Apparently the skin resistance at the exact point is slightly lower than the surrounding skin so the probe measures skin resistance at the point of contact. When the correct point is located, a helium-neon laser is persuaded to emit a one milliwatt blast of power and the beam may be continuous or pulsed. The pulses can be varied, too. Some 10 to 15mm of skin tissue is penetrated by the laser and, claims one report, it doesn't hurt. I would have thought that one would feel a bit of a prick.

It will be very sad to see all those acupuncture needles going to waste as electronics advances. I wonder what the Chinese will do with them all? (No, prizes, no prizes.).

Ginsberg



Practical Wireless, April 1976

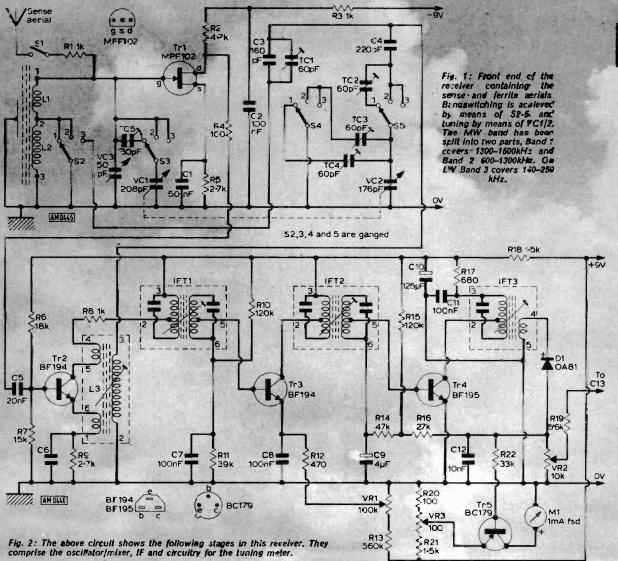
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By USING a rotatable ferrite rod serial, advantage can be taken of its directional properties, either to obtain best reception of a station without needing to turn the receiver itself, or to obtain a directional bearing from a transmitter. The receiver described here is completely screened except for the rotatable aerial, and uses a telescopic serial which can be brought into use if wanted. The latter is for "sense" determination, to remove the

## Directic Find



180° ambiguity which exists with the ferrite rod aerial alone.

The ferrite aerial has two maximum signal strength positions, with the rod at right angles to the direction of the transmitter; and two minimum

positions, with the rod in line with the transmitter. These positions are shown by a panel meter. In many circumstances, as with European or other stations, the approximate direction will be known. In other circumstances the correct direction may not be known.

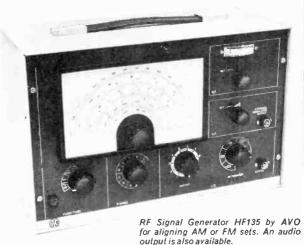
# PRACTICAL WIRELESS FAULT-FINDING GUIDE 8-Page Supplement April 1976

Fault-finding in radio and similar equipment is one of the fastest ways of learning all about electronics. Component suppliers catalogues are an invaluable source of information on the characteristics of components of all kinds and such knowledge is invaluable in locating a fault quickly from the observed symptoms. In this Guide Les Lawry-Johns, a very experienced service engineer, describes the methods of servicing that he has found so successful.

ots of people start off with the intention of making a living out of servicing radio sets. There are several paths to take once the basic theory has been mastered, more or less. One can specialise in, say, car radios and other car entertainment gadgets, cassette players and the like, or perhaps TVs only. Those who work for a company probably stay in the trade but some who set out to be self-employed rarely stay the course. There are several reasons for this, the main one being economic.

It is extremely difficult to get an adequate return for the capital laid out on component stocks and test equipment if one is repairing domestic appliances, mainly because the time involved in properly servicing each item leaves little reward when the job is completed. Therefore a lot of servicing is done on a part-time basis or as a paying 'hobby' with the accent on the hobby aspect rather than on the paying!

We have to assume that the reader has a basic knowledge of electronics and some idea how radios and the like function. The chief requirement after this is patience and a genuine desire to do the job, and to do it properly.



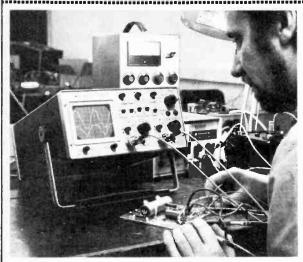
## THE TOOLS

First the tools. A goodly selection of screwdrivers, among the smaller of which must be everybody's friend, the neon screwdriver. This little fellow deserves a chapter on his own, being an indicator, detective, fault tracer, a sure signaller of nearby radiated energy and a life saver. No less, but certainly more.

One must have wire cutters, and side cutters are more useful than top cutters. Pliers and tweezers of various types and sizes, files and spanners are essential and



The Advance 'Alpha' digital multimeter takes up little bench space.



Shown here is the Advance Electronics low-cost dual-trace OS240 oscilloscope.

included in the latter should be the single-ended type with a handle, known as a nut spinner, in at least 6BA and 4BA sizes and with the close metric relatives. A comprehensive set of trimming tools, which can be purchased as a kit; at least two soldering irons, for delicate and heavy work. A reel of 18SWG (1·2mm) resin-cored solder and some means of removing solder, preferably desoldering braid which is copper braiding impregnated with resin flux. It draws the solder away from a heated joint allowing a component to be removed. Alternatively, some form of vacuum pump, possibly combined with a soldering iron.

A small torch which can be held in the mouth, if need be, and a magnifying glass are essential items whatever your age and eyesight! Next, the handmaiden of all electrical work, a decent multi-meter, preferably two. One should be a good quality meter for bench work, the other a smaller, less expensive, knock-about type for general use and back-up for use with the other, as one often wants to make two readings at the same time. Apart from this it often happens that the main meter is out of action for some reason, and at the most inconvenient time. Other instruments such as oscilloscopes, signal generators, bridges and the like can be regarded as highly desirable equipment to be purchased when funds allow.

## MULTIMETERS

The multi-meter should impose as little loading as possible on the circuit being tested otherwise the voltage present will be different when the meter is applied from what it is normally. A voltmeter is operated by current drawn from the circuit being tested and this current must be as small as possible. Most meters are marked on the front with their sensitivity and a figure of 20 000 ohmsper-volt (OPV) should be the minimum requirement. It should also have some form of cut-out or overload protection. The man who hasn't taken a reading with the meter set to the wrong range hasn't yet been born!

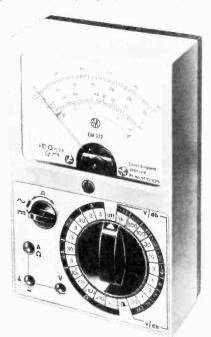
As well as reading voltage, current and resistance the meter can also be used to apply tests to circuits and components since, when switched to the resistance range,

a negative voltage appears at the positive test probe and a positive one at the negative probe. This enables a check of the approximate characteristics of capacitors, transistors, diodes and the like to be made. After voltage readings, this facility is probably one of the most valuable assets of a multi-meter so we will spend a little time on this subject, later on. However, we must continue with our "tools of the trade" requirements.

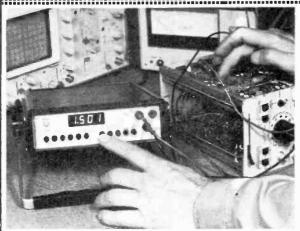
There are a great many aerosols (sprayers, squirters etc.) on the market at the present time, each of which has its own merits. Most engineers would select two, a contact-cleaner lubricant, which does not attack plastics, for cleaning switches, volume controls and the like, and a cooling agent or freezer. The value of these two can hardly be exaggerated. Whilst the former has always been accepted as a must, the choice of the latter has been dictated by experience over the last few years. Large numbers of small components grouped on a board can present a problem when tracing intermittent faults or where any one of a number of transistors in, say, an audio stage can be responsible for upsetting the operation of the others. A judicious squirt of freezer has solved many such baffling problems and a hair drier has its uses too!

## **STARTING**

So here we are, with a few tools of the trade and prepared to do battle. However, it is one thing to identify a faulty component, when all you have to do then is to obtain a replacement, but all too often we can only suspect and it is essential then to make a substitution check. Resistors can usually be tested and passed as fit or thrown out, but capacitors present a different problem. They can leak, partially or completely dry up, become open circuit or



The new AVO Electronic MultImeter EM272 provides 39 ranges in spite of the simplicity of its appearance.



In use here is the Advance DMM7 digital multimeter, a new 3½-digit 5-function instrument.

develop a short sometimes accompanied by heat. Therefore a goodly number of capacitors of various types, capacity and voltage rating must be held in stock.

Voltage rating is important from two aspects. Obviously a capacitor rated at, say, 12V would not be put across a 25V line as the voltage rating marked on the component must not be exceeded, but it is often thought that a capacitor marked, say, 100V can be used in any circuit where the voltage is less than this. Usually this is quite true, but there are exceptions. If the capacitor is electrolytic it requires a certain polarising voltage for it to work efficiently. In some circuits the voltage is very low, say about 4V, and a replacement in such a position should be rated at not much more than 6V or whatever voltage is marked on the defective item.

Diodes are another item which can be checked with a meter, within limits, and a few of the more common types in stock will usually suffice. Bridge rectifiers are commonly used in mains powered equipment and they often give trouble. One is well advised to keep a couple to hand and two types usually suffice, the BY164 for operation up to 40V and the BY176 for higher voltages. Four silicon diodes



A new product from Advance is the J4 signal generator, with sine or square wave outputs.

can be used in place of a bridge and indeed this type of supply will often be found but where a single block bridge is encountered it is often inconvenient to fit four diodes in its place.

The choice of separate power diodes is large but one cannot go far wrong with a few BY142 (BY127 with a smaller package). Voltage regulator diodes (zeners) appear in all types of equipment and one would be very hard put to try to anticipate what is going to be required if many makes and models of radio are tackled. It is no hardship to order the right components at the right time, if one knows in advance the type of equipment which is to be serviced, but if this is not known the stock list could be endless.

The same can be said about transistors and the position is more complicated as the age of the set to be serviced usually dictates the type of device used. The following is a list of transistors which ought to be kept in stock for the general servicing of audio equipment, radios, car radios etc.

AF115	AC187K	BC131	BC186	
AF117	AC188K	BC132	BC194	
AC127	AD149	BC147	BC195	
AC128	AD161	BC149	BC196	
AC187	AD162	BC157	BFX88	
A C188	BC109	BC159	BFY50	

From this modest list one can often find a suitable replacement for the more difficult-to-obtain types and some which are not marked. The latter present a minor problem but this is about all.

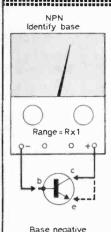
## IDENTIFYING TRANSISTORS

Most transistors have only three leadouts, these being emitter, base and collector. They will belong to one of two basic constructions, NPN (neg-pos-neg) or PNP (pos-neg-pos), so this is the first check to make and it is a very easy one using the ordinary multi-meter. It must be appreciated that when the meter is switched to the 'ohms' range it is battery operated and that the positive (+), or red, probe will be on the negative side of the battery with the negative (—), or black, probe at a positive potential. If the red probe of the meter is applied to the base of a PNP transistor a low reading will be shown when the black probe is touched to the collector or the emitter. On the 'ohms' scale this will look like something between  $10\Omega$  and  $50\Omega$  depending upon the transistor type and the meter.

If only one reading can be obtained note to which leadout the black probe is applied and assume this is the base of an NPN transistor, when the red probe can be applied to the other two to obtain the low reading. If there is no low reading, the red probe should be applied to another leadout on the assumption that the device is a PNP after all, but that you didn't get the base lead in the first place.

Now that the base has been identified and the device established as a PNP or an NPN, it is necessary to identify the collector and the emitter, remembering that we are supposedly dealing with a good transistor and not one with a short or open circuit.

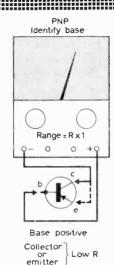
Switch the meter to the high resistance range, and, leaving the base free, connect the probes to the other two.

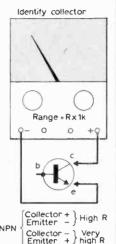


Collector

emitter

Low R





PNP reverse of NPN

W171

Diagrams to show the method of using a multimeter to identify the leadout connections of NPN or PNP transistors. As explained in the text the polarity of the test prods of most meters Is the opposite of that indicated by the colour of the prods. It is best to check this point before using the meter on transistors or electrolytic capacitors.

If the transistor is an NPN and a high resistance is recorded, the negative (black) lead is connected to the collector and the positive (red) lead to the emitter. Reversing the probes should then give a low reading.

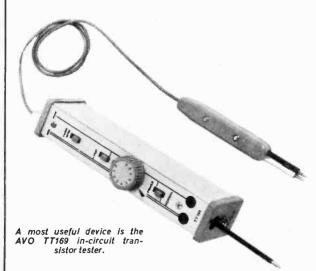
If the transistor is a PNP (we have already established this in the first test, so don't get confused) the readings will be reversed, high reading positive to collector, lower reading negative to collector. A further test can be made on the transistor. Connect as above, negative lead to collector, positive to emitter, if NPN, (reverse for PNP) and note the high reading. Place a finger on the collector and base leads and the reading should drop, showing that the transistor is "turned on". The actual reading will depend upon the current gain of the transistor and the resistance of the skin of the finger. What good is this, you may ask? Well, it does enable you to make a comparison check against a known transistor and so, very roughly, identify the current gain.

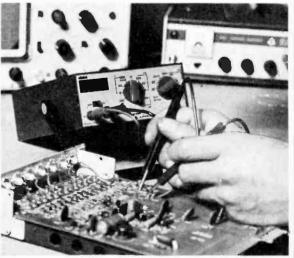
Diodes can be checked in a similar way but of course there are only two connections to make. Positive lead to

cathode (+) gives a low reading, while negative lead to cathode gives a high reading. A little practice with known good transistors and diodes will show the readings which can be expected. These tests can be used on components in circuit provided the associated circuitry is taken into consideration, particularly where transistors are inter-connected, say output transistors with drivers across them, etc.

## COMPONENT CHECKS

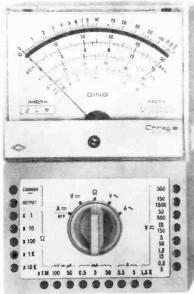
Capacitors can be checked roughly with an ohmmeter switched to the highest resistance range. When the test leads are first applied to a discharged capacitor, the applied voltage will cause the charging current to deflect the meter sharply according to the capacity, the reading going back towards infinity as the capacitor is charged. If the capacitor is leaky, current will continue to flow and a reading





Another useful bench instrument is the Advance 'Alpha' digital multimeter, being used here to make resistance checks on a circuit board.

will be maintained. This is to be expected with high value electrolytics as the meter voltage is insufficient to complete the sealing process. Once again a little practice will show what is to be expected. Very little indication, except leakage, will be shown on capacitors less than say 50nF but the tests are more valuable as the capacity increases. Don't forget, electrolytics require the negative probe to be applied to the positive tag of the electrolytic in order to get the right polarity for the charging voltage.



The Dino is the latest electronic multimeter from Chinaglia,  $200k\Omega$  OPV on DC and  $20k\Omega$  OPV on AC.

Inductors, transformers and the like can be checked for continuity and resistance. The presence of shorted turns can only be assumed if the resistance reading is much lower than that specified.

When a resistor is suspected of being faulty, first look at its appearance. If the colours are clear and bright and the resistor has a fairly low value the chances are that it will be serviceable. If it has a higher value, say over  $100k\Omega$ , it could look right but the value may have increased, particularly if used in a position where it is passing a fair current. Checking depends upon the circuitry, for if it is associated with other resistors or transistors, a direct reading may be of little use and one end may have to be lifted by unsoldering in order to check it out of circuit.

If the colours are not clear or if the resistor presents a well-worn look, replace it, even if it reads right, in order to save probable trouble later. This particularly applies to the low value resistors associated with output transistors usually about  $2\Omega$  or so). If a high value resistor is suspected it can often be checked with the receiver switched on by connecting a voltmeter across it, on a high range. The recorded voltage drop being of less importance than the effect of the resistance of the meter which shunts the suspect resistor and thus, to an extent, takes its place. Care must be exercised when using this dodge in preamplifier stages where the meter resistance can upset the base current of a transistor if the associated resistor values are high.

## SHORT CUTS

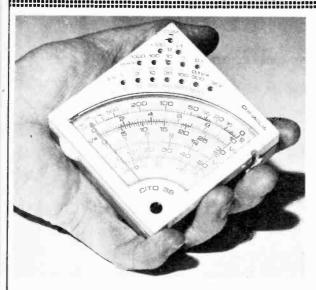
There are no substitutes for routine tests, checking supply and stage voltages in logical sequence, injecting test signals to identify the working and the faulty stages. To do this one must be able to think 'electrically', and while this comes easy to some, it is hard work for others and only comes with time. Following certain guide lines the fault will always reveal itself provided enough time is spent on the problem. However, as one becomes used to the type of equipment being serviced a pattern usually emerges which enables a short cut to be made across the routine tests and thus head straight for the source of the trouble, using eyes and ears and sometimes the sense of smell and of touch. A dry joint (one which has not been properly soldered in the first place) can often be seen, rather than traced, by its discoloured and 'powdery' appearance.

Sound distortion can be caused by many things but after a while the ears will unerringly identify the sound of a rubbing speech coil in a loudspeaker as opposed to a similar noise caused, say, by the output transistors being mismatched. The smell of some types of overloaded or faulty rectifiers immediately proclaims a defective one, whilst touching a hot transistor, apart from being painful, can cool it down and allow it to begin working for a brief period.

Some makes of printed circuit board are more liable to develop hairline cracks than others. Some types of capacitor are far more likely to fail than others. Indeed, we could go so far as to say that where certain types of capacitor are found fitted, we do not bother to check them since they are so very rarely at fault, whilst others are the first suspects and pounced on immediately. Some transistor types are more likely to fail than others. This sort of fault can be repeated over and over again and, whilst it makes life



The Model 8 Mk 5 general purpose multi-range meter is the latest in a very long line of multimeters from AVO. An early version of the meter appears in the background.



Smallest of the Chinaglia range is the Cito multimeter but it still manages to provide 14 ranges on six coloured scales,

a trifle easier for the experienced, the inexperienced person has no option but to employ routine tests and finally arrive at the same conclusion, having spent a considerable amount of time in the process. If in doubt, ask someone who knows and thus profit from their experience.

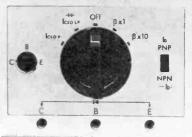
## PRACTICAL ASPECTS

We gave a short list of the items needed to service the simplest of appliances but there are others to consider. A circuit with a layout diagram is an absolute must if the appliance is not well known. Fortunately, in addition to the maker's service information which is the best source of reference, there are volumes of service data in book form available which condense this information, so that it is possible to build up a library of information which is readily to hand and indexed.

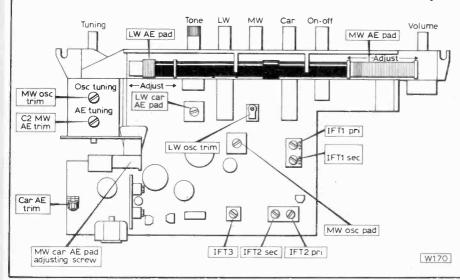
Not all appliances are complete when they are received for repair. For example, a car radio will need a 12V supply and most likely a loudspeaker. This is not too bad since most car radios use a  $3\Omega$  speaker, although more recent imports use  $8\Omega$  in some cases. However, it is often inconvenient to remove sited loudspeakers when a unit audio goes wrong, assuming that the speakers are not at fault, so it is necessary to have suitable speakers for test purposes. These are frequently  $8\Omega$ , but not always, by any means. So be prepared to add series resistors to make up the required loading or keep a goodly selection of loudspeakers!

Before we drop this subject, one further point. There are always power amplifiers requiring repair. If you do

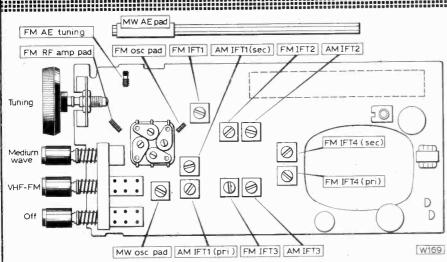




The Chinaglia transistor tester provides a Good-?-Bad indication plus leakage and \$\beta\$, using internal batteries. Test leads can be fitted for checking external circuits or devices,



Service sheets provide information for fault-finding and the alignment of receivers. This particular layout shows the location of the components which may require adjustment when aligning the Marconi 4173 MW and LW receiver.



The Marconi 4184 receiver also incorporates the VHF(FM) range so the number of adjustments needed for a complete allgnment is increased, as shown here.

take on one of these and repair it, have a care for your test loudspeaker. To touch the input socket with the volume control well up is to ask the amplifier to deliver full power into what may be a small loudspeaker, the probable result being a wisp of smoke from the speech coil which, if it survives intact, will never be the same shape again!

## OTHER TEST GEAR

Whilst our multimeter enables us to check voltages, measure current and take resistance readings, plus a few other things, no serious service work can be carried out without the aid of other instruments, the first of which is a signal generator. This enables us to inject signals of known frequency and level and thus to check the alignment and response of the equipment under test.

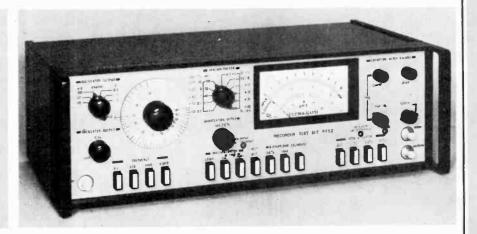
Let us take an average radio set. Considering the medium wave band only, signals from say 600kHz to 1.5MHz have to be selected and amplified. Since there are several stages of amplification, it is clearly not convenient to tune each stage to each frequency separately. What is required is for all signals to be converted to a common frequency which can then be fixed tuned. This is known as

the IF, or intermediate frequency, which for AM reception is usually fixed at about 470kHz. Some imported radios have a lower IF, 455kHz, which is the reason for the annoying whistle sometimes experienced adjacent to stations operating around 908kHz. Therefore the generator will have to cover this band of frequencies plus all RF frequencies likely to be covered by the receiver.

This will enable us to check the tuning of the aerial coils, the oscillator and the IFs. If these coil cores and trimmers are not accurately adjusted the receiver cannot give of its best. The signal generator provides a means of doing this, and much more, since we can now inject signals into various stages of the receiver and thus locate the stage which is not functioning correctly. The wobbulators is a variation of the signal generator, which we will not consider here, but which is essential for many kinds of accurate alignment.

An oscilloscope enables us to "see" into a circuit. The signals are amplified and appear as a trace on a screen so that the effect of each stage can be seen and adjusted, if necessary, to the required amplitude or waveform. It therefore enables us to see where signals are lost or become distorted.

The Ferrograph Test Set RTS2 from Wayne Kerr combines many of the facilities needed for checking the performance of recorders, amplifiers and other audio equipment. Included are an audio oscillator, distortion meter and AF millivoltmeter



## ALIGNMENT

Having mentioned these two valuable aids, let us immediately correct any misconception. In everyday radio repairs they are rarely needed. If the IF alignment has not been disturbed, do not touch it! If it has, it probably needs only a "tweek" to restore normal reception. Note which core or trimmer has been disturbed (wax or seal broken) and bring this, or them, into alignment with the other circuits. If the oscillator and aerial trimmers have been altered, switch to medium waves, set dial to about 1200kHz (250m) and set the oscillator trimmer to bring in Radio 1 (or any other frequency which is known to correspond to a particular station at this end of the dial) reset to around 1500kHz and trim the aerial trimmer. Retune to the lower end of the dial, to say Radio 3 on 647kHz, (this is the low end from a frequency point of view) with the core of the oscillator coil, appreciating the fact that this is going to upset the previous trimmer setting at the HF end which will have to be done again. Do this a couple of times until satisfactory tracking is obtained.

If a ferrite rod aerial is used adjust the medium wave winding on the rod for best reception on about 650kHz finally trimming the aerial trimmer, back on about 1500kHz. Leaving these settings untouched, switch to LW, tuning to 200kHz, or 1500 metres, then adjusting the long wave trimmer to bring in Radio 2, and setting the LW aerial trimmer to peak the signal, or adjusting the LW coil on the ferrite rod.

At this point any disturbance of the IFs can be corrected. If correct tracking cannot be achieved the IFs have probably been more seriously disturbed than was thought and the signal generator can then be brought out of cold store,

Photographs were kindly supplied by the following companies to whom all queries on the instruments illustrated should be addressed. Wayne Kerr, Durban Road, South Bersted, Bognor Regis, Sussex PO22 9RL.

AVO Ltd., Archcliffe Road, Dover, Kent CT17 9EN. Chinaglia Ltd., 19 Mulberry Walk, London SW3 6DZ. Advance Electronics Ltd., through Peter Bush, Bush Steadman and Partners, Saffron Walden, Essex. set to the required IF (as marked on the set, or in the service information) and loosely coupled with a single turn of wire around the ferrite rod. With the set tuned to the low frequency end of the medium wave band, about 600kHz, increase the signal input until the modulating tone can be heard, adjusting the IF coil cores to peak and gradually reducing the signal input from the generator to the minimum, to prevent the AGC coming into action. Repeat the RF tuning procedure.

## SNAGS!

Simple enough, isn't it? So where's the snag? Well, you see, we've only mentioned some of the procedure for AM sets. Two examples of the kind of component layout to be expected are shown, one a long and medium wave design as used in the Marconi 4173. Notice that the tuning adjustment for the low frequency end of the dial is called 'padding' and the high frequency adjustment is called 'trimming'.

The snag arises when there are many coil cans and lots of trimmers! The rule here is not to do anything unless you know the exact purpose of each adjustment. Otherwise you may be disturbing something which was previously correct and this is not the idea at all. Also shown is the layout of another Thorn group model, this time a Marconi 3183. Here we see the IF coil cans clearly marked AM and FM. These will not be marked as such in the actual set and therefore no coil cores should be disturbed unless such a diagram is available. Even then adjustment of the FM coils requires the use at least of an FM signal generator, preferably with 'wobbulator' and oscilloscope, in order to obtain the desired response curves.

The object of all this is to preach the sermon loud and clear. Do not touch what is not fully understood and attend only to that which really requires attention.

THE GENERAL THEME OF THE FAULT-FINDING GUIDE WILL BE CONTINUED IN THE JUNE ISSUE OF PRACTICAL WIRELESS DUE OUT ON 7 MAY.

## PW RADIO SERVICING CHART!

Presented FREE in the MAY issue of PW-Out on 2 nd. April

DOUBLE-SIDED! Use the front of the chart to localise the fault — Turn the chart over for an analysis of the problems!



The sense aerial is then used to provide another signal. With one position of the ferrite rod, signals from both aerials will combine, giving a greater meter deflection than the other position, where ferrite aerial and sense aerials are out of phase. By this means it is possible to find which bearing is correct of the two minimum readings obtained without the sense aerial.

## RF and Tuning

Fig. 1 is the circuit of the aerial, RF and oscillator tuning arrangements. L1 and L2 are MW and LW sections on the ferrite rod, which is assembled on a jack plug. This fits into a socket, through a hole in

the top of the case. S1 allows the sense aerial to be connected. S2/3/4/5 are the four poles of a 3-way switch. Positions 1 and 2 of section S2, short L2, for MW reception. Position 3 introduces C3 and TC1 to load the oscillator coil L3 for LW reception. Sections S3 and S5 introduce series capacitors TC5 and TC2 in position 1, to spread the tuning at the high frequency end of the MW band. S4 connects trimmer TC4 for this band, and trimmer TC3 for the lower frequency bands.

To avoid the need for further aerial trimmers and to allow correct trimming with S1 open or closed, a panel trimmer VC3 is used for aerial circuits. Trl avoids the need for a coupling winding on the ferrite aerial, which would require four connections in all. A 3-way jack plug and socket may thus be used. Point 1 is the inner (tip), point 2 the centre and point 3 the outer sleeve. Trl, together with its associated circuitry is fitted to a tag strip near the jack socket as in Fig. 1.

## IF Circuit

Fig. 2 gives details of the IF circuitry, which comprises the oscillator/mixer Tr2, two IF amplifiers Tr3 and Tr4, and detector D1. External connections to Tr2 go from R4 to C5 with a lead from pin 3 of the oscillator coil, to C3, TC1 and C4, Fig. 1. R8 is under the board, from pin 4 to pin 2.

As strong signals can give more than full-scale on the tuning meter, the 1st IF amplifier Tr3 is arranged to have the manual gain control VR1. This can be adjusted to bring the meter back to a central position, when required, as well as controlling IF gain. Bias from D1 is thus applied for automatic gain control purposes to Tr4, via R14 and R16. The meter is positioned to one side of the tuning scale, while the meter amplifier Tr5, is assembled on a tag strip secured to the dial plate. Trimmer pot VR3 is set so that the meter reading is just beginning to rise, with no signal. Increasing signal strength then causes negative base bias to Tr5 to raise collector current, so that the meter reading rises. Maximum meter reading corresponds to maximum signal strength, when rotating the aerial or VC3. With VR1 set so that this is about half-scale on the meter, the directional null should give almost zero reading on the meter, and is used for bearings, as it is sharper than the maximum.

Audio from the volume control VR2 passes to the AF amplifier.

## **Audio Amplifier**

The AF amplifier comprises pre-amplifier, driver and output stages, Fig. 3, and uses few components and easily obtained transistors. The most suitable



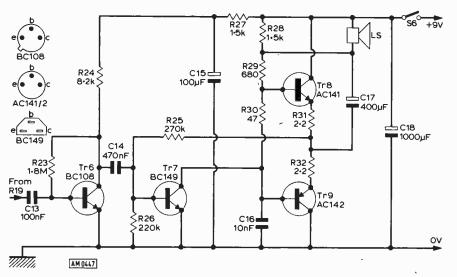


Fig. 3: This shows the circuit for the audio amplifler, which uses for its output a matched pair of AC141/2 transsistors. Speaker impedance should be around 1502.

speaker impedance is about  $15\Omega$ , although the actual value is not too important. However, a speaker of less than about  $10\Omega$  ought not to be used, unless pressed into service by including a series resistor to make up the total, while speakers of over about  $25\Omega$  will result in some saving on battery current, but reduction in output.

## **Chassis and Panel**

Holes are drilled in the front of the chassis as in Fig. 4. For the cabinet listed, allow the panel to project below the chassis about 12 in and mark the hole positions on it. The  $7 \times 2^{1}$ 2 in scale plate is bolted a little back from the panel, which is not fitted until later. Fit the ganged capacitor with 4BA bolts, noting it is essential to use short bolts, or add washers, so that they do not project beyond the thickness of the metal plate. Two small pulleys are pivoted on 4BA bolts, held with lock nuts to the plate. The cord passes twice round the drum, and then round the small wheels, and is held taut by a spring. Drill a hole in the panel for the slow-motion spindle of the capacitor. The pointer is a straight wire soldered to a small piece of tinplate, which is clipped on the cord. Arrange this so that it is fully to the right with VC1/2 closed and the spring to the left.

The case requires two <sup>3</sup>4in diameter holes. One is placed centrally, for the ferrite aerial, and the other near the back right hand corner, for the telescopic

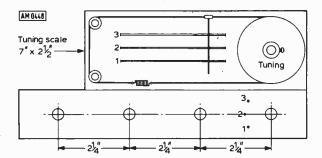


Fig. 4: Details of the scale card, and the spacings required for the variable control positions.

aerial. Using a universal chassis flanged runner,  $8 \times 1$  in, cut sections from each flange 3 in from the ends, so that it can be bent to form the mount shown in Fig. 5. This is bolted to the chassis so that the jack socket comes under the central hole in the case.

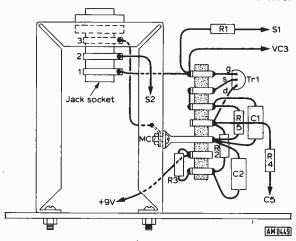


Fig. 5: The mounting for the rotating aerial, and the tag strip that holds the RF stage, is constructed from a Universal chassis flanged runner and bent to fit.

Should a little adjustment of height be required so that the jack socket will clear the top of the case, the legs of this metal part can be spread outwards to lower it. Check that there is sufficient space for the IF board between the mount and scale plate.

The sense aerial must be insulated from the chassis. This was arranged by punching a lin diameter hole, over which a piece of paxolin is fixed with 6BA screws. The bolt on which the aerial screws fits vertically in the paxolin, and a lead runs from it to SI. If necessary, the paxolin can be spaced from the chassis, either above or below, so that the aerial closes flush with the case top. This aerial is run on to its screw after placing the receiver in its case.

The internal speaker is mounted on the left side of the cabinet. A grid of nine  $^34$ in holes was punched over the position to be occupied by the cone. An alternative is to cut a larger hole and cover this with fabric or expanded metal. A  $4 \times 1^{1}2$ in opening is cut in the panel, and is covered by a slightly larger

## \* components list

Resist	ors		
R1	1kΩ	R17	680Ω
R2	4-7kΩ	R18	1 · 5kΩ
R3	1kΩ	R19	5-6kΩ
R4	100Ω	R20	100Ω
R5	2·7kΩ	R21	1 · 5kΩ
R6	18kΩ	R22	33kΩ
R7	15kΩ	R23	1·8MΩ
R8	1kΩ	R24	8·2kΩ
R9	2·7kΩ	R25	270Ω
R10	120kΩ	R26	220kΩ
R11	39kΩ	R27	1-5kΩ
R12	470Ω	R28	
R13	560Ω	R29	680Ω
R14	47kΩ	R30	47Ω
R15	120kΩ	R31	2.2Ω
R16	27kΩ	R32	2.2Ω
All re	esistors 5% 1W	/	
VR1	100kΩ linear p	otentiomet	er
VR2	10kΩ log. pote	entiometer	with switch S6
VR3	100Ω pre-set	potentiome	ter
Capac	itors		

muhuo	11010		
C1	50nF	C10	125µF
C2	100nF	C11	100nF
C3	160pF 2% silver mica	C12	10nF
C4	220pF 2% silver mica	C13	100nF
C5	20nF	C14	470nF
C6	2nF	C15	100µF 10V
C7	100nF	C16	10nF
C8	100nF	C17	470 F 6V
C9	4µF 4V	C18	1000µF 10V
VC1/	2 Jackson 00 208/176pF	slow r	notion gang
VC3	Jackson C804 50pF		
TC1-	TC5 60pF trimmers		

### Semiconductors

Tr1	MPF102	Tr6	BC108
Tr2	BF194	Tr7	BC149
Tr3	BF194	Tr8	AC141
Tr4	BF195	Tr9	AC142
Tr5	BC179	D1	OA81

## Miscellaneous

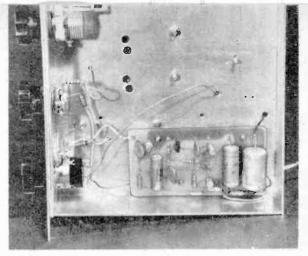
L1/L2, Denco MW/LW 5FR. IFT1, Denco IFT18/465. IFT2, Denco IFT18/465. IFT3, Denco IFT14.L3, Osc. coil Denco TOC1. S1, miniature slide switch. S2-S5 4-pole 3-way rotary switch. Moving coll meter ImA fsd 42 x 42mm. Jackson 54mm dlameter drum. Paxolin tube 150 x 29mn dlameter. 6mm stereo jack socket. 5 control knobs. 550mm telescopic rod aerial. 6mm stereo jack plug. 15 $\Omega$  speaker. 156mm dia. 360 degree protractor. Plastic bowl 156 x 30mm. OSC/IF PCB, 105 x 55mm. AF PCB, 129 x 55mm. Both boards available from the PW Readers PCB Service, page 1070.

### Case

Type W case 10 x 7 x 5½in. Type K chassis 9 x 6½ x 1½in. Type A screen 7 x 2½ x ½in. All HL Smlth & Co. 8 x 1in. flanged Universal chassis runner—Home Radio Ltd.

piece of lein Perspex, held with two screws. A card scale, upon which three lines have been drawn, is fixed with adhesive, so that the three bands can be calibrated later.

A bracket is bent from scrap metal to hold the PP7 battery and is screwed down behind the aerial mount. Do not overlook that holes are required under IFT1 and IFT2, so that the lower cores can be reached. These are simply positioned by marking them through the circuit board before fitting the IFT's.

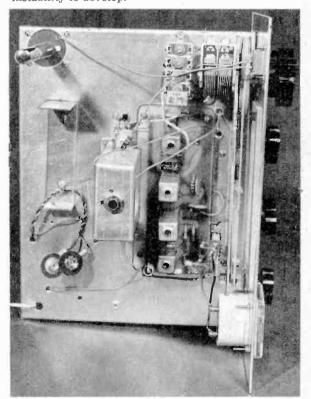


Underside view of chassis, showing the volume control, IF gain and aerial trim controls. The PCB in the lower righthand corner is the Audio board.

## **RF** Stage

The RF circuit is wired as in Fig. 5, which also shows connections to the jack socket. Leads are fitted to run to S1, VC3, C5, battery positive line and S2. The jack plug and socket, S1 and aerial, as well as VC3, contribute to the stray capacitance across L1 and L2 so when wiring, these unavoidable capacitances should be kept as low as possible, otherwise there may be difficulty in reaching the HF end of the range.

With individual samples of Tr1 it is possible that changes to the resistors R2 and R5 could improve gain. Otherwise the values given should be suitable. R4 may be the lowest value which does not allow instability to develop.



General plan view photograph of the receiver, showing layout of the Osc/IF board, tuning capacitor and triamers, and the rotating aerial mounting.

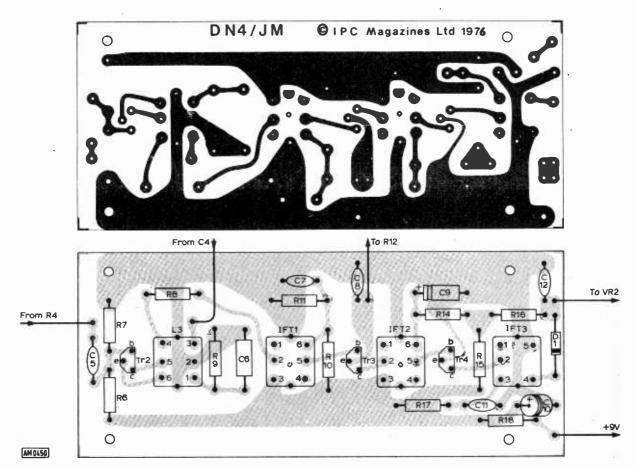


Fig. 6: Foil side and component side views of the Osc|IF board. Both are shown full size. If the board is to be tested outside the receiver, VR2
must be connected

## Osc/IF Board

Fig. 6 shows the PCB carrying the Osc/IF sections of the receiver. The input goes to C5 and the output taken from D1. The oscillator coil and IFTs should fit without any need to use force. If not, the holes for these may be slightly enlarged, taking care not to break the foil. Components are inserted as in Fig. 6, excess length of wire being snipped off after soldering. Provide flying leads for input, output, battery positive (S6), meter amplifier and IF gain control. (If this board is tested before fitting, VR2 must be connected.) Mounting is by means of four \$\frac{1}{2}\$in 6BA bolts, with extra nuts to give spacing from the chassis and locked firmly to provide the necessary chassis return.

Since the gain of individual transistors varies, it might be possible to modify the value of R8, using the lowest value which does not result in uncontrollable oscillation at any frequency. Normally, however, the value given can be fitted.

## **Audio Amplifier**

The AF board is shown in Fig. 7. Colour coded leads can be soldered on for R19, speaker and battery positive. The PCB is mounted under the chassis with three bolts, with the speaker leads made long enough

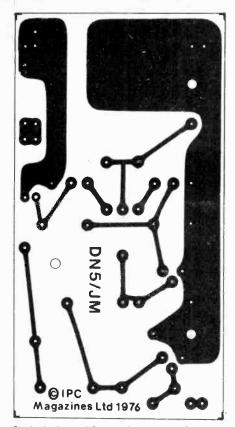
to allow the receiver to come well out of the case. If a jack socket is used here, it must be completely insulated from the chassis or be of the insulated type.

## **Meter Amplifier**

Components for the meter amplifier are wired to the tag strip as in Fig. 8. The meter is a 1mA instrument calibrated in S-points, though the meter is primarily required to show minimum signal positions for the rotating ferrite rod aerial. If after maximum adjustments to VR3 the meter cannot be set so that it is just beginning to rise, with no signal tuned in, then either R20 or R21 may be changed in value, to correct this. Alternatively, R3 can be changed to  $250\Omega$ , provided R20, VR3 and R21 in series total about 1.5 to  $2k\Omega$ . It does not matter how the potential divider is made up, except that adjustment of VR3 becomes more critical if it forms most of the total resistance.

## **Bandswitch**

Connections to the switch are shown in Fig. 9, and can be followed in conjunction with Fig. 1. The rotor tag of VC3 must be wired to the chassis. TC5 is soldered directly across the switch, while the four trimmers TC1 to TC4 are mounted on a strip fixed



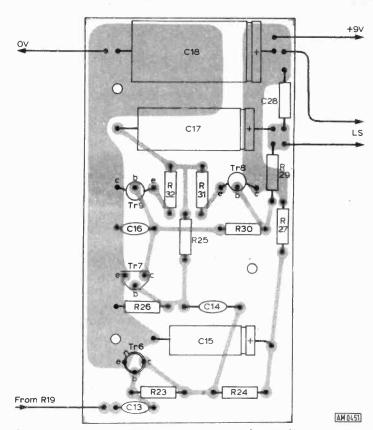


Fig. 7: Audio amplifier board showing the foil side to the left and the component side to the right. Again, both are shown full size. Chassis mounting is by three bolts.

clear of the chassis, by spacers, and behind VC1/2. It is convenient to use these trimmers, from left to right, for the circuit positions in Fig. 1. That is, TC1 LW oscillator trimmer; TC2 Range 1 bandspread coverage; TC3 Range 2 (and LW) oscillator trimmer; and TC4 Range 1 trimmer. This allows a short lead to run from pin 3 of the oscillator coil to TC1 and C4, which is connected from TC1 to TC2. For short leads, use the lower tags of VC1 and VC2, as in Fig. 10.

# VR3 VR3 PD1 and VR2

Fig. 8: Components that make up the meter amplifier are mounted on a tag strip adjacent to the meter itself. VR3 can be any pre-set pot of 100Ω.

## **Rotating Aerial**

A 3-way jack plug is used as a pivot and is assembled as in Fig. 11. A 414 in disc is cut from plywood (this diameter was chosen to suit the diameter of the 0-360° protractor and is a tight push fit on the insulated part of the jack, to which it is cemented. If necessary, a block with a central hole can be glued here to strengthen the assembly. Insulated thin flexible leads are soldered to the plug contacts; these may be green for 1, red for 2, and black for 3. Thread these wires up through the jack moulding and bring them out on top of the disc.

The ferrite rod aerial as received has a few turns for base coupling to L1 and these are removed. L1 and L2 must be in the same phase when connected in series, or LW alignment is impossible. The rod is secured to a small piece of paxolin by thread and

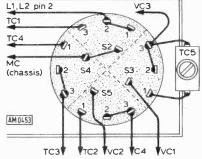


Fig. 9: The band switch comprises four poles and three positions, and the above drawing shows the connections to this switch, and the trimmer TC5.

## The Black Watch kit £14.95!

12 15

\* Practical-easily built by anvone in an evening's straightforward assembly.

\* Complete-right down to strap and batteries.

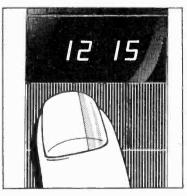
\*Guaranteed. A correctlyassembled watch is guaranteed for a year. It works as soon as you put the batteries in. On a built watch we guarantee an accuracy within a second a day-but building it yourself you may be able to adjust the trimmer to achieve an accuracy within a second a week.

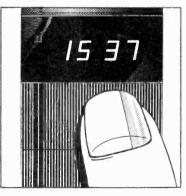
The Black Watch by Sinclair is unique. Controlled by a quartz crystal, and powered by two hearing aid batteries, it uses bright red LEDs to show hours and minutes, and minutes and seconds. And it's styled in the cool prestige Sinclair fashion: no knobs, no buttons, no flash.

The Black Watch kit is unique, too. It's rational - Sinclair have reduced the separate components to just four-and it's simple: anybody who can use a soldering iron can assemble a Black Watch without difficulty. From opening the kit to wearing the watch is a couple of hours' work.

## **Touch and tell**

Press here for hours and minutes... here for minutes and seconds.



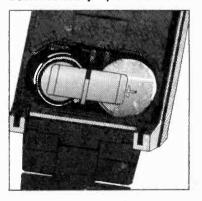


## The specialist features of the Black Watch

Smooth, chunky, matt-black case, with black strap. (Black stainlesssteel bracelet available as extrasee order form.)

Large, bright, red display-easily read at night. Touch-and-see caseno unprofessional buttons.

Batteries easily replaced at home.



Runs on two hearing-aid batteries (supplied), Easily re-set using special button-no expensive jeweller's service.

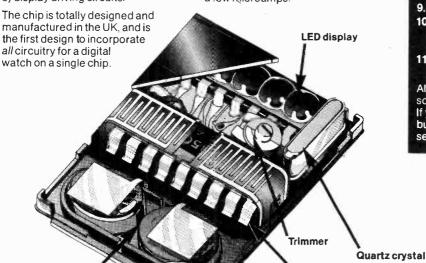
## The Black Watch – using the unique Sinclair-designed state-of-the-art IC.

## The chip...

The heart of the Black Watch is a unique IC designed by Sinclair and custom-built for them using state-of-the-art technology—integrated injection logic.

This chip of silicon measures only 3 mm x 3 mm and contains over 2000 transistors. The circuit includes

- a) reference oscillator
- b) divider chain
- c) decoder circuits
- d) display inhibit circuits
- e) display driving circuits.



### ... and how it works

A crystal-controlled reference is used to drive a chain of 15 binary dividers which reduce the frequency from 32,768 Hz to 1 Hz. This accurate signal is then counted into units of seconds, minutes, and hours, and on request the stored information is processed by the decoders and display drivers to feed the four 7-segment LED displays. When the display is not in operation, special power-saving circuits on the chip reduce current consumption to only a few microamps.

FREEPOST- no stamp required.

## Complete kit £14.95!

### The kit contains

- 1. printed circuit board
- 2. unique Sinclair-designed IC
- 3. encapsulated quartz crystal
- 4. trimmer
- 5. capacitor
- 6. LED display
- 2-part case with window in position
- 8. batteries
- 9. battery-clip
- black strap (black stainlesssteel bracelet optional extrasee order form)
- 11. full instructions for building and use.

All the tools you need are a fine soldering iron and a pair of cutters. If you've any queries or problems in building, ring or write to Sinclair service department for help.

## Take advantage of this no-risks, money-back offer today!

**Batteries** 

The Sinclair Black Watch is fully guaranteed. Return your kit in original condition within 10 days and we'll refund your money without question. All parts are tested and checked before despatch-and correctly-assembled watches are guaranteed for one year. Simply fill in the FREEPOST order form and post it-today! Price in kit form: £14.95 (Inc. black strap, VAT, p & p).

strap, VAT, p&p).

Sinclair Radionics Ltd, London Road, St Ives, Huntingdon, Cambs., PE17 4HJ. Tel: St Ives (0480) 64646.

Reg. no: 699483 England. VAT Reg. no: 213 8170 88.

Total £	St Ives, Huntingdon, Cambs., PE17 4BR.
I	*I enclose cheque for £ made out to Sinclair Radionics Ltd and crossed.
s)	* Please debit my.*Barclaycard/Access/ American Express account number
************	
	Total £s)

2000-transistor silicon integrated circuit

\* Delete as required

PW/4

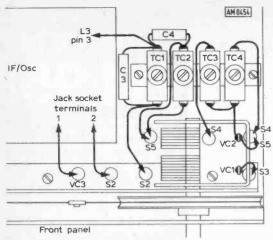
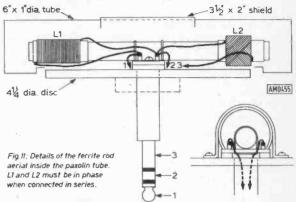


Fig. 10: The trimmers TC1 to TC4 are mounted in the above configuration to enable the leads to be kept as short as possible.

adhesive. This is held with two small screws, with strips to space it slightly from the disc, to clear the plug leads. These are soldered to the appropriate leads from L1 and L2, using pins as anchorage points if required. When the aerial has been tested, it is protected by a  $6 \times 1$  in paxolin tube, cut away just sufficiently on the underside to allow it to be fitted over the rod. A lead from point 3 is brought out from the tube.

The metal shield is bent from aluminium, about  $3^{1}_{2} \times 2$ in, to clamp the paxolin to the wooden disc and it is earthed by a tag under one fixing screw, soldered to lead 3. Its purpose is to improve the minimum null by reducing non-directional pick-up by the connecting wires. Approximate alignment can be made before fitting the paxolin tube. Final small adjustments to the positions of L1 and L2 may be made with an insu-

lated tool, through the open ends of the tube. The ends of the tube may be closed with discs of insulating material. Due to stray pick-up by other wiring, the sharpest directional nulls are obtained only with the receiver in its metal cabinet.



## Alignment

Band coverage is most easily checked if a signal generator is available, but satisfactory alignment is possible without this. The IFTs are pre-aligned by the maker so only small adjustments to these cores should be necessary and should not in any case be made until signals are received. A correctly shaped tool, such as that available from the IFT maker, must be used, otherwise the cores may crack.

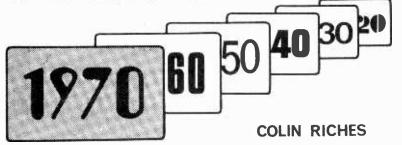
To check the IFTs, tune in any steady, stable signal correctly, with VR1 near maximum gain, but reducing signal strength if needed by rotating the aerial, so that the meter does not go beyond full scale. All the IFT cores can then be adjusted slightly to give the best meter reading. When the IFTs are correctly aligned in this way, they must not be altered or readjusted when aligning the aerial and oscillator



The ferrite aerial is mounted inside a paxolin tube and connected via a stereo jack plug. This permits the aerial to be rotated to find the 'Null' point.

continued on page 1080

## GOING BACK...

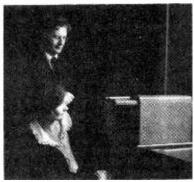


J. L. B.

Y EVERAL readers have expressed interest in the picture of John Logie Baird's "Televisor" shown in the February 1976 Going Back so I thought I would show another couple of pics. of the great man. The small photograph shows J. L. B. with Miss Kingthe first girl ever to be televised. The larger picture shows J. L. B. in 1926 with his original television apparatus. If anyone wants to see this fantastic piece of equipment, pop along to the Science Museum—it's there in a glass case just like the one in our picture.

Some J. L. B. milestones: May 1924—The Baird Television System. "Mr. Baird has achieved some remarkable results which go a long way towards proving that television is practicable." October 1926—"The first TV licence was recently granted to Mr. J. L. Baird's stations. One is situated in St. Martin's Lane and the other at Harrow. At present the London Station is a transmitter and, except for an interval of a fortnight, 'looking-in' has been in progress every night for some weeks on a wavelength of about 200 metres." May 1927—Said J.

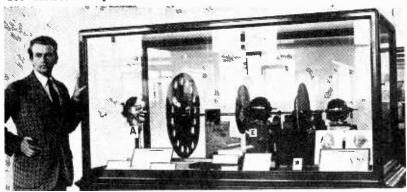
L. Baird, "In ten years time, I prophesy, we shall be able to see on our wireless televisors topical events, such as the finish of the Derby or the finish of the Boat Race."



J.L.B. and his 'first lady'

## Anyone Help?

R. M. HILL, Hillside, Peaslake, Guildford, Surrey is desperately anxious to obtain an old Murphy A92 "Stationmaster" receiver of 1940 vintage. It's an 8-waveband allmains receiver which was claimed to have a very good short-wave performance. If you can help, please contact Mr. Hill direct.



J.L.B. and original apparatus.

## Overseas News

R. KEN McKenzie, one of our New Zealand cousins recently wrote to say that he has been a radio enthusiast since 1924 when he heard, via the telephone, for the first time in his life, a radio broadcast. It was from the South Seas Exhibition on South Island. N.Z. In 1927 he built his first onevalve receiver from a design published in the journal N.Z. Radio. His ultimate project was a three-valve receiver working a "Baby Grand" Philips speaker.

For a long time his nearest transmitter was 2YA Wellington, which ran at 5kW and was over 40 miles away. Later, for a town of a then population of about 12,000 they became very well served by two dealers in radio sets and parts who set up broadcast transmitters. They were N.R. (Ray) Cunningham with 2ZQ and W. D. (Bill) Ausell, with 2ZD.

It's always good to hear from our overseas enthusiasts so keep the letters coming in folks!

## Bintage Radio Society

HEARD from our friend Tudor Rees (of Antique Wireless Newsheet fame) again recently and he says there is a saying "Put two Englishmen upon a desert island and they will form a club". This however certainly isn't based on fact when it comes to a British Vintage Radio Society. There must be literally many thousands of enthusiasts but no sign of a club or society as yet. Things may be looking up though, for a Mr. A. Constable, 18 Ravensbourne Gardens, Ealing, London, W.13 wishes to conduct an initial survey as to the possibility of forming such a group. He would like all those with a genuine interest in a Vintage Radio Club to write to him (I would suggest you enclose a s.a.e.).

## Vintage C@ Column

ROM time to time we publish a special "Vintage CQ Column" for readers who have requests for old books, equipment etc, and those who wish to dispose of such items. If you want to be included in our next column, please address your request to "Vintage CQ", Practical Wireless, Fleetway House, Farringdon St, London EC4A 4AD.

## PRODUCTION LINES colin riches

NEW MIC



A noise cancelling microphone which the manufacturers state has exceptional qualities of discrimination between the voice and random noise is now in production at the Eastleigh, Hampshire works of Selsound Limited.

In their search for the clearest possible transmission of speech, Selsound engineers have demonstrated that the microphone is able to eliminate extraneous noise to an exceedingly high degree. Exhaustive laboratory development resulted in a high level of response within that band of frequencies most important for clarity of speech, a marked diminution on each side of this band and a steep gradiant to the sensitivity/proximity curve.

Selsound microphones are available in the form of a microphone insert, styled "Type 2500", but the company state that they can provide special housings to suit specific requirements and installations.

Full technical details are available from Selsound Ltd., (Dept. P.W.) Victory Close, Industrial Estate, Chandlers Ford, Eastleigh, Hants. Tel: Chandlers Ford 67158.

WIRING PENCIL

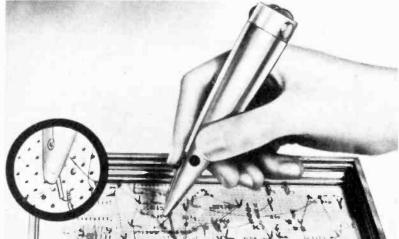
This new wiring pencil, patented by Vector Electronic Co., U.S.A. comprises a lightweight plastic housing, a replaceable spool of wire, and extended metal tip to guide and cut the wire. The wire is said to be a unique solder through nylon-polyurethene insulated tape which, when heat is applied to the wrapped connection points with a fine-tipped soldering iron, the insulation melts away, and produces a soldered joint. The wiring tip of the pencil is angled

to facilitate wrapping and to provide a clear view of operations.

The makers claim that the average time required to make a soldered joint is only seconds—and reckon it's about three times faster than conventional soldering.

The pencil, complete with two 250ft. spools of wire, sells for £6.75 plus postage.

Further information from: J. H. Equipment Limited, (Dept. P.W.) 91 Redbrook Road, Timperley, Trafford, Lancs.



Please mention Practical Wireless when writing to manufacturers and suppliers whose addresses are given in these pages.

-Thank you.

## THE ALL BRITISH CARTRIDGE



Goldring have just brought out a new Cartridge—the G900SE. The key to the G900SE performance is the great mass reduction (moving mass 32g) which immediatley results in extremely low intermodular distortion. (Physical mass has been reduced to 5mg.)

These reductions in mass have been achieved firstly by the introduction of minature magnets to a specification previously believed impossible. Then spurning conventional methods, the coil assembly used in the main body of the cartridge is created using formerless winding techniques through which Goldring have saved valuable space and therefore weight, which in turn reduces the mass which the stylus has to move.

Welded to the magnet is a micro gold plated nickel tie bar, which is there partly as an earth to reduce crucial static discharges that can occur and also to control the movement of the stylus in unwanted modes. The whole assembly is then pivoted via a special Butyl polymer with optimised damping.

Specification:

Frequency range: 10Hz-28kHz.
Frequency response: 20Hz-20kHz
+2dB.

Playing weight: 1 gm.

Playing weight range: 0.75-1.5 gm.

Tip mass: 0.32 mG.

Stylus point radius:  $\cdot 0007'' \times$ 

0002'' (18 $\mu \times 5\mu$ ).

Inductance at 1kHz: 640 mH. Inductance at 10kHz: 630 mH. DC resistance: 720 Ohms.

Channel separation: 25dB NOM.

Output (sensitivity) @ 5 cm/sec:

1kHz. RMS 5mV+ 1·5dB.

Compliance (static): 40 LAT × 10-6cm dyne, 20 VER × 10-6cm

Vertical tracking angle: 24° Net weight: 5 am.

Goldring Limited (Dept. P.W.) 10 Bayford Street, Hackney, London E8 3SE.

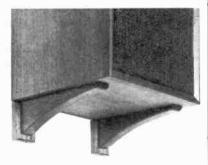
1066

## WHARFEDALE DECK

Rank Hi-Fi have announced the Wharfedale XP cassette deck (with Dolby) at £165 (inc. VAT). Finished in black and walnut, this 4-track stereo deck has an electronically governed DC motor and automatic bias selection. Tape speed: 4.8 cm/ sec (1 $\frac{7}{8}$ ips)  $\pm$  1.5%. Wow and flutter: DIN 45507 0.20% (maximum) (peak weighted). Output levels: DIN socket more than 10K ohm, OVU input,  $580 \,\mathrm{mV} \,\pm\, 1.5\%$ , headphone jack, 2 volts into 50 ohms. Input level: microphone/DIN 2mV, line 30mV. Input impedance (nominal): microphone/ DIN 5.6k $\Omega$ , line 50-500k $\Omega$ . Bias frequency: 79kHz. Frequency response (record/playback): standard tape (Dolby out) 50-10,000Hz  $\pm 3dB$ , 10,000-12,500Hz -3 to -5dB; Cr0<sub>2</sub> tape (Dolby out) 50-12,500  $\pm$ 3dB, 12,500-14,000Hz -3 to -5dB; Dolby in from Dolby out frequency characteristics within ±3dB. Frequency response (playback only): within 3dB of record/playback, response from 50-10,000Hz. Total harmonic distortion (max.): 3.0%. Typical signal/noise ratio: Dolby out 54dB, Dolby in 61dB. Erasure (minimum): 60dB. Channel separation (min. at 1KHz): 32dB.

Rank Audio Visual Ltd., (Dept. P.W.) P.O. Box 70, Great West Road, Brentford, Middx.

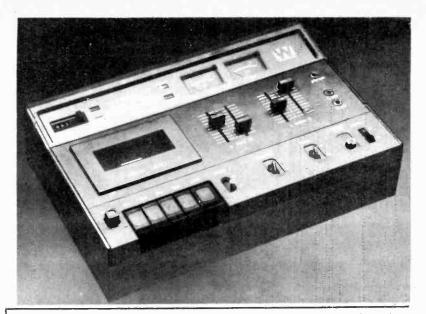
### SPEAKER BRACKETS



The brackets holding this speaker are made of hardwood and are manufactured by Esta Limited, Staffs.

These "Astute" brackets, which are very easy to fit can easily be removed for decorating etc. Rubber pads are incorporated to hold speakers so that no screws need to be driven into the actual speaker cabinets.

They come supplied sanded ready to finish and are complete with screws and plugs. Prices: 14cm £1·71; 19cm £2·16; 26cm £2·70 further gen from Esta Heating Products Limited, (Dept. P.W.) Green Lane, Walsall, Staffordshire.



## PHILIPS MULTI-TESTER

Model SMT-111 has as one of its most important features, a high input impedance of  $0.5 M\Omega V$ . This derives from an integrated circuit amplifier which enables the instrument to be used in many AC applications, up to 25 kHz on the 12 V range, for example. The use of an integrated circuit amplifier also enables a lower-impedance moving coil movement to be incorporated.

The SMT-111 is based on the combined experience of Philips own

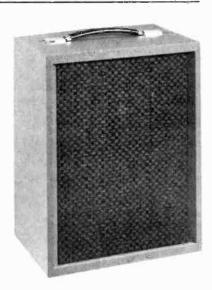
engineers and technicians throughout the world. Its thirty-five measuring ranges, were selected with them in mind and an additional feature has been the inclusion of an AC current range. Both the integrated circuit and movement have been fully protected against peak overload and a checking point for the battery has been incorporated in the range selector switch. The SMT-111 is priced at £30.00. Philips Electrical Limited, (Dept. P.W.), Century House, Shaftesbury Avenue, London WC2H 8AS.

## FOR CINE FANS

The Leeds firm of Farnell-Tandberg Limited recently introduced two new loudspeakers aimed mainly at the home-movie market, for both of them are suitable for use with cine sound projectors. Model FT 108 has a  $4\Omega$  impedance which accurately matches the output of most 8mm sound film projectors. The FT 116 has an impedance of  $8\Omega$  to match the output of the majority of 16mm sound projectors on the market.

The robust cabinets (and you need them to be pretty strong if you are lugging equipment around doing film shows) are finished in grey rexine with matching vynair. Both incorporate a 10in. loudspeaker giving 10W RMS output. The units are supplied with 15 metres of twin-core sheathed cable which terminates in a DIN speaker plug. All of this can be neatly stowed away in the back of the cabinet where there is a compartment with a removable lid.

We tried one of these speakers on an 8mm projector and also tested it with an ordinary cassette tape recorder to play back sound for slide shows. In both cases results were very good. The price of these speakers



is set at £23 25 plus VAT. Further gen on these and other Farnell-Tandberg equipment for sync sound systems may be obtained from Mr. M. R. Cowing, Promotional Services Manager, Farnell-Tandberg Limited, (Dept. P.W.) Farnell House, 81 Kirkstall Road, Leeds, LS3 1HR.



OME time ago, I suggested in the pages of this magazine that it might be worthwhile to explore possibilities of long distance VHF reception on the East European (OIRT) band, 65 to 73MHz. At that time (PW October 1974) I wrote that Sporadic E openings on these lower frequencies could take place more often than those reaching into the 90 to 100MHz region though the statement was rather in nature of an educated guess, being partly based on other people's observations.

## **SEASON 74/75**

During the 1974 and 1975 SpE seasons (mid-May to mid-August) I conducted some experiments of my own and the results have shown that if anything, my prediction had not been optimistic enough. In 1974, long distance propagation of FM radio signals



-a long-skip character

caused by reflection from the ionosphere was observed on 27 occasions; only on 5 of these occasions did the exceptional DX conditions also affect the West European (CCIR) FM band, 87.5 to 104MHz. In 1975, the ratio was 35:6 and there were a few additional days last July when broadcasting stations from Eastern Europe could be received due to enhanced tropospheric propagation.

The duration of these favourable receiving conditions, as well as the times at which they occurred, differed widely. They would last from less than one hour to several hours at any time of the day and on some occasions OIRT stations could be heard from early in the morning till late at night.

Signals were usually of a long-skip character and stations most frequently received were those from the north-western and western parts of the USSR (i.e. Estonia, Latvia, Lithuania, Byelorussia and the Ukraine), eastern Poland, Romania and Hungary, while Bulgarian and Czechoslovakian FM stations appeared less often. The strength was sufficient to make listening in stereo possible, though at times with a considerable level of noise. Indeed, stereo programmes have been received from all the OIRT countries, the only exception being the USSR, where a different system is used for stereo broadcasts (unsuppressed subcarrier at 31·25 kHz), which the common 19kHz pilot tone type of decoder cannot resolve.

## **EQUIPMENT**

My equipment consisted at first of a small 4 metre converter with the oscillator set at 173MHz and an IF at 100MHz, used in connection with an ordinary FM tuner, an aerial preamplifier and a wideband Yagi array. For the 1975 season, however, the converter was replaced with one of the currently available FM tunerheads. Retuned to the 65 to 73MHz band it was built into the tuner as an alternative, switchable front end.

It is this latter arrangement that I can recommend to anyone interested in similar experiments, and results achieved over the past two years certainly do confirm that the lower FM band is ideally suited to VHF DXing. However, it is impossible to give any advice as to the choice of a suitable front end. There are quite a few types available, costing mostly under £10 (e.g. from Ambit International) and the actual selection has to be made with regard to the specifications of the tuner with which it is to be used.

A word of caution seems to be in order as retuning

may prove to be a tricky business as it requires a signal generator or, ideally, a calibrated wobbulator. A simple adjustment of cores and trimmers would probably be not enough. In my case, at least, it was necessary to add approximately two turns to each coil as well as increasing the oscillator feedback capacitor by a few pF.

On the other hand, there should not be any difficulty about finding a suitable aerial as any old 405 line TV aerial will do, in particular those for Channel 5. The OIRT transmitters are both vertically

and horizontally polarized.

## **EXPECTATIONS**

The 65 to 73 MHz band is, under normal conditions, fairly quiet in this country. There is some RT traffic, amplitude modulated, around 71MHz and in most areas of the UK the vision buzz of TV channel B5 can be heard on 66·75MHz. There seem to be less and less amateurs operating on 4 metres (70MHz) these days. This means of course that anything else that may suddenly appear on these frequencies in the summer months is fairly sure to be coming from Eastern Europe via SpE, and do not be surprised if thappens to be English pop, as they play a lot of it over there.



--- advice on a suitable front-end

An exception is the frequency of 67.75MHz on which TV sound can be heard on such occasions originating from Yugoslavia, Spain, Italy and other continental countries. It should also be mentioned that while the OIRT FM band nominally starts at 65MHz, few stations can actually be found below the 66MHz point because there is a small overlap with channel R2 TV sound on 65.75MHz so that frequencies between 65 and 66MHz are used by FM radio only in areas not covered by this TV channel.

For the British DXer the most difficult problem may well turn out to be the identification of individual stations and countries of origin. Being able to recognize the main languages of the area is of some importance and listening to the foreign broadcasts of the BBC, which are always introduced in English,

could be quite helpful in this respect. After a time, one gets attuned to the **sound** of a language and it is then possible to identify it without actually understanding it. Once this point is reached, it should be much easier to catch the odd word which makes closer identification possible. News broadcasts and weather reports are particularly revealing as the emphasis tends to be on local events and temperatures

## PW TECHNICROSS PUZZLE Solution to No. 12 presented last month



## Mail Order Protection Scheme

The Publishers of Practical Wireless are members of the Periodical Publishers Association which has given an undertaking to the Director General of Fair Trading to refund monies sent by readers in response to mail order advertisements, placed by mail order traders, who fail to supply goods or refund monies owing to liquidation or bankruptcy. This arrangement does not apply to any failure to supply goods advertised in a catalogue or in a direct mail solicitation.

In the unhappy event of the failure of a mail order trader readers are advised to lodge a claim with Practical Wireless within three months of the date of the appearance of the advertisement, providing proof of payment. Claims lodged after this period will be considered at the Publisher's discretion. Since all refunds are made by the magazine voluntarily and at its own expense, this undertaking enables you to respond to our mail order advertisers with the fullest confidence.

For the purpose of this scheme, mail order advertising is

'Direct response advertisements, display or postal bargains where cash had to be sent in advance of goods being delivered'. Classified and catalogue mail order advertising are excluded.

## **EDITORIAL ANNOUNCEMENT**

## WIRELESS Denominer for denomination

Our new PCB service is well under way and we are now able to add PCBs for two popular projects published prior to December 1975. All boards, except SRBP, are epoxy glassfibre, drilled and roller-tinned.

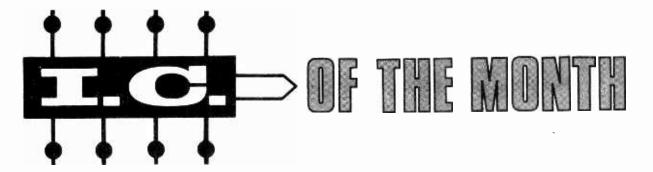
## To:- READERS PCB SERVICES LTD, PO BOX 11, WORKSOP, NOTTS

Please supply PCB/s as indicated by tick/s in box/es

PCB SERVICES and not to the Editorial offices.

Issue	Project	Ref	Price	
Mar 75	Electronic Organ (set of two)	AMO315 AMO318		
Sep 75	Electronic Clock (set of three)	AMO387 AMO389 AMO392	2·40 + 15	
Dec 75	Radio-Pickup Link	DN0792	0.98 + 12	
Dec 75	Random Number Selector	DN0793A	0.98 + 12	
Dec 75	Sound-To-Light Display	DN0798	1.15 + 12	
Dec 75	12V PA System	DN2/JM	0.98 + 12	
	Disco System, Amplifier	•		
	(2 required) eac	ch AM0421	3.40 + 18	
Dec 75	Disco System, Light Modulator	A M0423	2.70 + 18	
Jan 76	Music Box SRE	P DN1/JM,	2.25 + 18	
	glassfib	re DN1/JM	2·25 + 18	
Jan 76	Emergency Light Unit	AM0419	3 ⋅ 50 + 18	
Mar 76	CMOS Crystal Calibrator	AM0438	1.19 + 12	
Apr 76	DF Receiver (set of two)	DN4/JM ) DN5/JM )		
Apr 76	Wobbulator	AMO443	1.08 + 12	
Post and packing is for one board. For each additional board add 4p to the 10p or 18p rate as applicable. Prices include VAT.  Remittances with overseas orders must be sufficient to cover despatch by sea or air mail as required.				
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Number 57

RCA CA3130 CMOS OPERATIONAL AMPLIFIER

THE relatively new CA3130 operational amplifiers manufactured by RCA employ the well-known CMOS (Complementary Metal Oxide Silicon) techniques in which the complementary FET's are fabricated on the same silicon chip as conventional bipolar transistors. This enables important advantages to be obtained in circuits employing this device.

#### HIGH INPUT IMPEDANCE

One of the most noticeable features of the CA3130 is the very high typical input impedance of  $1\cdot 5 \times 10^{12}$  ohms ( $1^1_2$  million megohms). In practice this means that either of the inputs of a CA3130 device can be

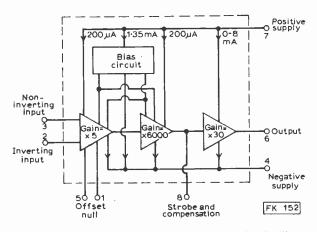


Fig. 1: Internal block diagram of the CA3130, showing the three amplifiers connected in cascade.

connected into almost any circuit without affecting the operation of that circuit by taking an appreciable load current from it. The input current required by a typical CA3130 device is only about 5pA (5 millionths of a microamp) which again shows that this device imposes an extremely small load on the circuit feeding its input. The input current increases by a factor of about two for each 10°C rise in temperature, but even at 80°C it rises only to about 100pA.

Another advantage is obtained by the use of CMOS circuitry in the internal output stage of the device. The CA3130 output voltage can swing to within a few mV of the potential of either supply line if the load impedance is relatively high.

The gain-bandwidth product of this very economi-

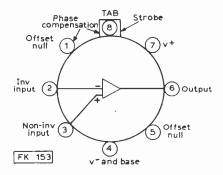


Fig. 2: The CA3130 is encapsulated in a TO-5 type can, and is supplied via eight leads as shown above. The view is from above.

cal device is 15MHz, being a very high value for an amplifier with such a high input impedance. In addition, the slew rate of the CA3130 is about  $30V/\mu s$  with no capacitance in the output circuit; this may be compared with the value of about  $0.5V/\mu s$  quoted for the well-known 741 device. The CA3130 can therefore deliver a higher output voltage than the 741 at a given frequency when this is determined by the slew rate.

#### INTERNAL CIRCUIT

The internal circuit of the CA3130 comprises three amplifier stages in cascade together with a biasing circuit for the first two stages, as shown in Fig. 1. The input amplifier stage employs CMOS devices to provide a very high input impedance, but the voltage gain of this stage is only about five times. The gate electrodes of CMOS devices are susceptible to damage when an electrostatic charge accumulates in

the high input impedance circuit, since such charges can puncture the insulating layer of silicon oxide between the gate and the channel. Four zener diodes are integrated on the silicon chip to protect the device from damage by static charges in most circumstances

The second amplifier stage employs a bipolar transistor in a circuit which provides a voltage gain of about 6000 times. The third stage of the CA3130 operates in Class A with a typical voltage gain of thirty times varying with the load impedance of the circuit.

#### CONNECTIONS

The CA3130 is available only in a metal can type package with eight leads, Fig. 2, like a TO-5 type of transistor encapsulation but with eight leads instead of three. The CA3130 has the normal inverting and non-inverting inputs of an operational amplifier. The quiescent output voltage can be adjusted to a value half way between the power supply lines if a potentiometer is connected between pins 1 and 5 with its rotor connected to pin 4 (the negative supply).

The output stage can be rendered inoperative by connecting pin 8 (input to this stage) to the negative line at pin 4. The output potential at pin 6 then rises virtually to the positive supply line voltage of pin 7. Electrical strobing pulses may be applied to pin 8 so that the device only operates at the desired times.

#### TYPES AVAILABLE

The most economical device of the series is the CA3130, suitable for most applications. However, specially selected devices are available for more critical purposes. The CA3130A has a lower maximum input current than the CA3130 and lower input offset voltage and current. The input circuit specifications of the CA3130B have even tighter tolerances. All of the devices operate satisfactorily over the very wide temperature range of -55°C to +125°C.

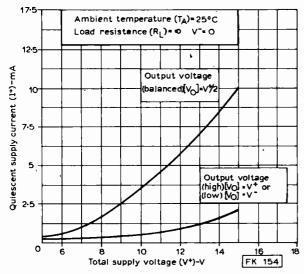


Fig. 3: Graph of the CA3130, showing increase in supply current with supply voltage. These curves occur when the device is not supplying output current.

A letter 'T' or an 'S' may be added. For example, RCA produce types CA3130T, CA3130AS, CA3130BT, etc. The 'T' signifies that the device has straight leads, whilst the 'S' types have their leads bent so that their ends are in an 8 pin dual-in-line configuration.

#### **POWER SUPPLY**

The CA3130 will operate from supply voltages of 3V to 16V or from balanced positive and negative supplies of  $\pm 2.5V$  to  $\pm 8V$ . The current required is very low, especially if the load impedance is high and the power supply voltage is low, an advantage obtained with most CMOS devices. Typical power supply currents when the output current is zero are shown in Fig. 3. The supply current is particularly low when the output voltage from the device is equal to either of the supply line potentials, but is higher when the output voltage is half way between the supply line potentials. If a single supply of 5V is

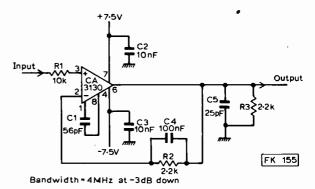


Fig. 4: To achieve a high degree of accuracy between the input and output voltages, the device is connected with a balanced power supply.

employed, the power supply current is only about  $300\mu A$  when the load impedance connected to pin 6 is infinity and when the potential at this pin is 5V; if the output potential falls to 2·5V, the supply current rises to about  $500\mu A$  for the same load impedance. The CA3130 series is therefore very useful with equipment which must be operated from small batteries.

#### TYPICAL CIRCUITS

One of the most useful applications of the CA3130 is as an impedance transformer. The non-inverting input of the device is connected to a signal source which may have a very high impedance and which can therefore supply only a very small current. The output circuit of the CA3130 can either supply or accept an output current of up to about 20mA, this being of the order of four thousand million times the input current required by the device. Thus the CA3130 can be used to drive a stage which requires appreciable current; in other words it can 'transform' a high impedance at its input to a relatively low impedance in its output circuit.

A typical impedance transformer circuit is shown in Fig. 4. In this case the device is used as a 'voltage follower' where the output voltage 'follows' the input voltage. One can achieve an accuracy of 0.01% between the input and output voltages in this type of circuit.

The capacitor C1 in Fig. 4 provides frequency compensation. Negative feedback from the output to the inverting input is provided by R2 in parallel with C4. The circuit shown employs balanced power supplies with a supply voltage near to the maximum so as to obtain maximum output voltage swing. Supplies of ±2.5V may be used for minimum current consumption.

Another voltage follower circuit is shown in Fig. 5 in which a single power supply is employed. The potentiometer VR1 enables the quiescent voltage at the output to be adjusted to a required value. In both Figs. 4 and 5 capacitors are incorporated in the power supply lines to assist stability at high frequencies.

Voltage followers of this type are useful when the potential of the high impedance input is to be measured, since it is transformed to the low output impedance which can be measured with a conventional meter.

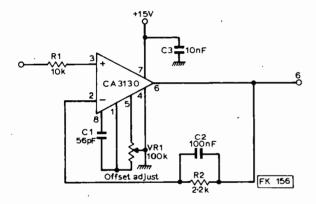


Fig. 5: The circuit above is similar to that shown in Fig. 4, but in this case is supplied by a single power supply. The potentiometer VR1 is used for setting the quiescent voltage at the output.

#### **OSCILLATOR**

A simple square-wave generator circuit is shown in Fig. 6. The resistors R1 and R2 bias the non-inverting input of the CA3130 to a mean voltage equal to half the supply voltage. The timing capacitor is selected by the range switch, S1. The time for which the output voltage is in its 'high' state can be adjusted by VR1 and the time for which it is in its 'low' state by VR2. When the largest capacitor, C1, is selected by S1, each part of the pulse can have a period in the range 4ms to 1s (according to the setting of VR1 and VR2). This period varies by factors of ten with the setting of S1 until one obtains 4µs to 1ms with the capacitor C4.

When the voltage at the inverting input is low, the output voltage will be high and the capacitor selected by S1 will charge through VR1, R4 and D1. As the voltage across this capacitor increases, the potential at pin 2 rises above that at pin 3 and the voltage at the output falls to a low value very suddenly. The same timing capacitor now discharges through D2, R5 and VR2 until the pin 2 voltage falls below that at pin 3, when the output switches

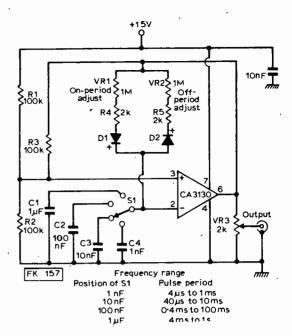


Fig. 6: In this circuit, the CA3130 is used as the heart of a square wave generator equipped with independent adjustment for both periods of the waveform.

back to its former high voltage state. The potential at pin 3 varies with the CA3130 output potential owing to the current flowing through R3.

The use of the CA3130 in this type of circuit has certain advantages. The high input impedance enables relatively high values of timing resistor (VR1 and VR2) to be used and therefore one can obtain very low frequencies with a moderate capacitor value. The timing capacitors used in this circuit should not be electrolytics as they pass an appreciable leakage current which would produce a large voltage drop across VR1 and VR2. The potentiometer VR3 is an attenuator in the output circuit. The supply voltage shown enables square waves of about 15V amplitude to be obtained, but smaller supply voltages down to about 5V may be employed for smaller output amplitudes.

#### HANDLING CMOS DEVICES

Although the gate electrodes of the CA3130 are protected with internal zener diodes, it is recommended that reasonable precautions should be taken when using them. Whilst the manufacturer's recommendations are often ignored without the device being damaged, it is certainly wise to observe them. Soldering iron tips used for soldering CMOS devices should be earthed. The devices should not be soldered into the circuit whilst power is applied or even removed from a socket, since transient voltages can be developed which can cause damage. No signals should be applied to the inputs unless the power supply is connected and the input current should be limited to lmA.

The CA3130 is available from Chromasonic Electronics, 56 Fortis Green Road, London, N10 3HN, at 84p (including VAT) plus 20p packing and postage.



# AWATEUR BANDS

#### by Eric Dowdeswell G4AR

N oft-repeated complaint from those who would wish to listen to the bands in some sort of reasonable quiet concerns the radiation from the line timebases of colour TV sets. Paul Turner (Bishops Stortford) asks for advice since he now finds DX-chasing almost impossible because of the QRM from a set just across the road. All I can suggest is that the equipment is checked for complete screening, that the aerial is placed as far away as possible from the source of the ORM and that some experiments be made on the earthing of the equipment. I think that I have mentioned before that the removal of the mains earth from the equipment can often effect a cure but this can mean an electrical hazard so due care must be taken. Experimentally, a separate earth in the garden can be tried.

Strangely enough the ordinary TV viewer is completely unaware of the trouble he is causing because his own radio is off! But just try walking around the house with a portable radio and see how widespread is the QRM! Particularly near the TV set's coax! If one of us radiated a signal on another frequency at the same field strength of the average colour TV set we would soon be in trouble! Of course, in some civilised countries the set has to be screened but I wonder how long it will be before we get around to taking some practical measures to combat yet another form of pollution.

A mild reprimand from **Tom Brady** G8GAZ for saying that Alan Rae had held the callsign GM8GRO before becoming GM4ENN. G8GRO is a pal of Tom's so apologies all round. Callsigns are very personal, often conveying much more than actual forenames to the distant listener. Incidentally, the junior op at the GAZ QTH is G8HEB. Dad said it, not me!

Pete Allen (Taunton) decided to take my advice and put up a 132ft wire. The improvement in his log shows that it was all worthwhile. Now he has fun switching between the long wire and his G5RV. Mike Green A8088 (Northwich) has been reorganising his equipment to the detriment of his log. He now has a new 2m beam consisting of an 8+8 slot fed at 20ft. His log shows four stations on 2m heard via the aurora of Jan. 10th. Martin Kessel A9016

(Stoke-on-Trent) has now abandoned his one-valver plus five-valve superhet in favour of an AR88D. He is still wearing a groove in the carpet awaiting his RAE results and if successful will be on with a Liner 2 and a five element beam on 2m at 35ft. A Microwaves Modules converter has been added to the AR88 on the receiver side. Notwithstanding the 2m bias Martin is getting his code up to the speed required for the Morse test.

Robin Bayley (Kingswood School, Nr Wolverhampton) has started off his DX-ing career with an ex-RAF 1475 set and a long wire, 30ft up. A converter for 2m is under construction. Welcome OM and I am sure that you will soon get into the swing of short wave radio. Overseas now to New Zealand and Mark Corrigan of Wanganui whose Heathkit SW717 pulled in some good Europeans for him using either a 20m dipole or 75ft long wire. Seems this column is responsible for Mark becoming a regular correspondent with another Mark, Mark Hill, another contributor of ours. Dennis Anderson is now using the receiver section of a 62 set and wonders if anyone has made up a mains unit to power this rig. He'd appreciate any help at 33 Manor Crescent, Brookwood, Pirbright, Surrey. Mike (Slough) finds the 80m band wide open all night with the Far East and Africa coming in from dusk to midnight and the North and South Americans continuing on until mid-morning. However, he has not neglected the other bands, I'm glad to report. Steve Cottis A8961 (Harrogate) also found plenty on 80m including ZL3NR/C which looks like Chatham Island, a good catch for anyone. Steve likewise roamed around the other bands from 15 to 40m.

Paul Barker BRS34898 (Sunderland) reports some W's on 80m, frequently missing from other people's logs, perhaps because they do not realise that they are to be found only above 3.8MHz! Paul's SSTV station-of-the-month was CT1JI, commended for his excellent picture quality. Graham Sewell (Greenford) stuck to 20m and the VK and ZL gang as garnered on his Codar CR70A and 20ft of wire. Don't know how far he would get with a decent aerial! Peter Walton A9002 pulls me up for saying he has a 359x, should be 358x of course. I must have been thinking about signal reports! Peter now has a half wave aerial up aimed at South America. Alan Doherty (Portrush) now sports an inverted vee aerial on 80m but as he says, "it's a bit close to the dirt".

Stephen Terry BRS35669 (Banbury) has a Microwave Modules converter feeding into his FR50B on 2m driven by a 6 over 6 element beam at 20ft



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which, considering he is at 425ft asl, sounds like a good set-up! Lastly, Ray Woodward (Colne) is also a first-timer to the page and seems to have been doing well with his Codar CR70A and he awaits the associated ATU. He is one of the brave few that get up at 4a.m. to get in on the DX!

#### Log extracts

P. Turner:— 10m from 2m via Oscar 7 OE3JBC DB8OP DC6HY PA0GBL I2SRR

P. Allen:— 80m FP8DH KP4AM VP9HM 20m CR9AJ VK4PX VK6LK

M. Green:— 20m KZ5AS VK1JC 2m Auroral DC9DZA GI8HY GM8FFX

M. Kessel:— 80m ZC4PK 40m EA8CR 20m EA9FE FY0BHI VK5MS VP2EEG YB0ACG 15m SV0WZ VK6HE YN7MHN ZS6DQ

M. Corrigan:— 80m OA4ASN VK0DA VR1AT ZK2AE 3D2AN 20m C21DC CX7DC KJ6BZ KS6SFA VR1Z YN1AZ WA6LRG/KB6

M. Bennett:— 80m A4XFW HK1CHL JY1 KZ5HP VS5DB 9M2PV 20m FB8ZG Amsterdam Is. HR6SWA Swan Is. KC4AAA VK9XI Christmas Is. VU7ANI Andaman Is. YJ8DS 15m A6XP FY0BMI YB0ACG

S. Cottis:— 80m CR9AK CT2BU PJ3BB VS5JH ZL3NR/C 40m EA6DA VK9AAN VP8AA 20m CX5DT TG9GI VQ9DF 15m EA8ND KZ5AL ZD7FT 9H4K

P. Barker:—80m EA8JP 20m SSTV CT1JI F3RT I1RHB K1WPS OE1SBA YU2CB 20m A2CGD EA9FC C9MAF VP2LBR 9L1BH

G. Sewell: 20m VK1BH VK6HS ZL1KN

P. Walton:— 20m KH6BB ZB2A 5L7F 8P6FX 9J2LL

A. Doherty:— 80m A4XFW EL7F FG7AO HI8RRD JY3ZH KZ5HP VP2LC VR1AA VR4DX VR8A ZL3NR/C 40m YN1AWS 20m PZ9AJ VP8HA 9N1MM 2m via Oscar 7 DC6PZ F1BFH 18CVS ON5PX

S. Terry: - 2m EI9Q HB9AEN/P HB9AKG

R. Woodward:— 80m CR4BS 15m AC2PV M1D 9G1LZ

All SSB except those in bold which are CW.



# SHORT WAVE BROADCASTS by Derek Bell

TRANGE are the items that are used for aerials!

Neil Braeman from Southwater sleeps on his!

He has hooked his bedframe to a Pye radio of uncertain vintage by way of a thirty foot length of wire. I would imagine that in the event of an

electric storm in close proximity the results could be rather alarming!

Andrew Gay of Wernham Farm, Marlborough, Wiltshire asks if anyone can oblige by letting him have their redundant copy of the Radio Nederland antenna amplifier leaflet. He has written twice with no reply forthcoming and is willing to refund any expenses incurred. Andrew is a jazz fan and has high praise for the SBC Sunday afternoon show on 11870 at 1530. It is packed with inside information for jazz enthusiasts and, comments Andrew, often has a quality that is good enough for recording.

A representative of the clan Mcleod, namely John Mcleod of Inverness, sends some interesting notes on the stations that he picks up that are, shall we say, not for our ears. These are the services for other target areas, that pass over the UK. John thinks that living in the highlands of Scotland he has more advantage in DXing than those of us who live rather more south. In this I rather agree with him, considering the DX that the Scandinavians pull in. It is on the cards however that other DXers will be able to tune to these stations and a selection follows:

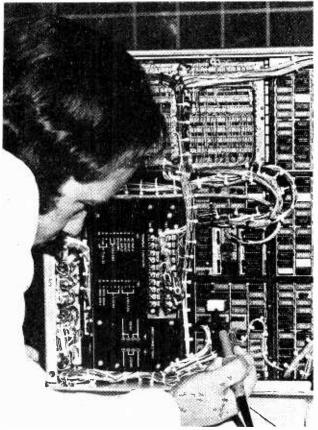
RAI Rome, to N. America 6010 at 0100 SBC Bern, to Africa 9590 at 0530 ORF Austria, to E. Asia 15105 at 0830 Deutsche Welle, to N. America 6010 at 0530

John goes on to tell us that ORF Austria has informed him that "in future QSL cards will only be issued by ORF if they are specifically requested". This policy statement also says that they are looking for more critical comment on their programmes than hitherto. This is a station sticking its neck out with a vengeance! While on the subject of ORF, Richard Fuchs of Windsor points out the difference between Radio Austria and Austrian Radio. If this is a little confusing to you, Richard says that the Radio Austria station is a commercial firm and Austrian Radio is the one often referred to as "ORF" and is the station that transmits the Austrian Short Wave Panorama DX show on 6115 and 9770 at 0915 on Sundays, from Moosbrun.

Having sorted out your Austrian stations Niels Montanana recommends that the booklet issued by ORF is well worth having. To get this the DXer sends a reception report in to PO Box 700, A-1136 Vienna, Austria.

These are days of belt tightening and general pulling in of horns. Not least in the area of our hobby and one such person affected is **H. E. Forder** of Leeds. H.E.'s problem is that he would like to buy a rig that will pull in the short wave bands but not one that is expensive. Asks Mr. Forder, "are the sets under £50 as good as the advertisers claim?" This is a question that I cannot really answer but I will say that many good sets can be obtained for under £50 that are mains operated and can be improved by the addition of extra aerial wire or an aerial tuner unit in a matter of minutes, with little technical knowledge.

Over the water we go now for a couple of letters from readers who's DXing is a little different from ours. Lindsey Crawford Cull of Salisbury, Rhodesia forwards the address of the recently featured National Public Radio the Public Affairs segment of the AFRTS network. This system comprises 142 member stations and can be contacted at 2025 M. Street N.W., Washington DC, 20036 USA. Vincent Carabott of Malta GC whose name I have managed



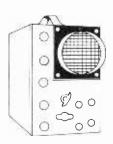
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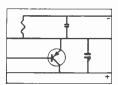
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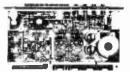


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1A3	-65	6BE6	-41	6L1	2.84	12K5	1.17	35D5	-90	DK40	-82
1A5GT	-59	6BH6	-75	6L6GC	-68	12K7G7	r -50	35L6G1	88	DK92	1.15
1A7GT	-60	6BJ6	-64	6L7	-59	12K8	-85	35W4	-60	DK96	.70
1B3GT	-59	6BK7A	-85	6L18	-64	12Q7G7	60	35Z3	-88	DL96	-64
1H5GT	-80	6BQ7A	-64	6L19	2.00	128C7	-50	35 Z4GT	.88	DM70	-80
1L4	- 25	6BR7	1.20	6LD20	-88	128G7	-55	35 Z5G T	- 90	DM71	1.76
1N5GT	-76	6BR8	1.25	6N7GT	-70	128H7	-50	42	1.00	DY87/6	
1R5	-50	6B87	1.64	6Q7G	-50	128J7	-60	43	1.00	DY802	-47
184	-89	6BW6	1.00	6Q7GT	-60	128Q7	.76	50B5	1.00	E80CC	2.57
1U4	-70	6BW7	-65	6Q7(M)	-64	128R7	.75	50C5	.70	E80F	2.20
105	-88	6BZ6	-57	6R7G	-70	14H7	-64	50CD60	1	E88CC	1.20
2D21	-60	6C4	-47	68A7	-55	1487	1.10		1.46	E92CC	.70
2GK5	-75	6C5G	-59	68C7G1	-50	19AQ5	-65	50EH5	-88	E180F	1.17
2X2	-70	6C6	-47	68G7	-52	19G6	7.00	50L6G1	1.00	E182CC	38-00
3A4	-60	6C9	2.00	68H7	-55	20DI	-80	85A2	.75	E1148	-62
3D6	-47	6CB6A	-47	68J7	-64	20F2	-88	85A3	.75	EA50	-40
3Q4	-85	6CD6G	1.60	68K7G	Г -52	20L1	1.29	90AG	2.98	EA76	1 40
3Q5GT	.70	6CG8A	-88	68Q7	-50	20PI	1.00	90C1	-88	EABC8	
384	-47	6CL6	-76	6V6G	-80	20P3	-94	90CG	2.81	EAC91	-65
3V4	-82	6CL8A	-94	6V6GT	-58	20P4	1.17	150B2	1.00	EAF42	-88
4CB6	-75	6CM7	-88	6X4	-47	20P5	1.50	2158G	-59	EAF80	1 .80
5CG8	.75	6CU5	-88	6X5GT	-50	25 A6G	.70	807	1.17	EB34	-85
5R4GY	-94	6CW4	1.17	7B6	-88	25L6G	-70	5702	1.20	EB91	-28
5U4G	-50	6D3	-75	7B7	-82	25 Y 5 G	-60	5763	1.76	EBC41	-88
5V4G	-59	6DE7	-88	7H7	-88	25Z4G	-50	6057	1.00	EBC81	-45
5Y3GT	-55	6DT6A	-88	7R7	2.00	25Z5	-75	6060	1.00	EBF80	
5Z3	-88	6EW6	-88	7¥4	-80	25Z6G	-80	6067	1.00	EBF83	-50
5Z4G	-55	6E5	1.17	724	-80	28D7	2.00	7193	-62	EBF89	
5Z4GT	-55	6F1	-80	9D7	.70	30 A 5	-76	9002	-59	EBL21	
6/30L2	-80	6F6G	-60	10C2	-76	30C15	-80	9006	-50	EC86	-90
6ABC	1.46	6F13	-90	10DE7	88	30C17	-85	ACPEN		EC88	-90
6AC7	-60	6F14	-88	10F1	88	30C18	85	AC2/PE	IN/	EC92	-55
6AG5	-35	6F15	-76	10F9	-76	30F5	-75	DD	1 00	ECC33	2.00
6AH6	-80	6F18	-64	10F18	-80	30FL1	1.10	AC6PE	N -60	ECC35	8.00
6AJ\$	-76	6F23	80	10LD11		30FL2	1.10	AC/TH	Ł	ECC40	1.20
6AK5	-47	6F24		10P13	-88	30FL13			1.00		-40
6AK6	.70	6F25	1.17	10114	2.84	30FL14		AL60	1.17		-88
6AM8A	-70	6F28	.78	12A6	75	30L15	-82	ATP4	-50	ECC83	-39
6AN8	-82	6F32	.70	12AC6	.90	30L17	76	AZI	-50	ECC84	-40
6AQ5	-58	6G6G	-60	12AD6	-90	30P4M1		AZ31		ECC85	-47
6AR5	-80	6GH8A	-88	12AE6	-90		1.05	AZ41	-50	ECC86	1.00
6A87	1.17	6G K5	-76	12AT6	-47	30P12	-80	BL63	2.34	ECC88	- 55
6AT6	-53	6G U 7	-88	12AU6	-58	30P19/		CL33	1.85	ECC189	
6AU6	-40	6H6GT	-29	12AV6	-59	30P4	-88	CY1C	1.00	ECC807	
6AV6	-98	6J5GT	-53	12BA6	-58	30PL1	1.00	CY31	-70	ECF80	-50
6AW8A		6J6		12BE6	-59	30PL13		DAF91	40	ECF82	-80
6AX4	.88	6J7G	-85	12BH7	-59	30PL14		DAF96	-60	ECF86	-88
6B8G	-85	6JU8A	-88	12BY7	-85	30PL15	-80	DC90	-70	ECF80	r S-68

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	ECH21	9.94	EY81 -50	PCF86 -50	Q8150/15	VP41 -88	ACY21 4	25	BY127	-23
i	ECH35		EY83 .70	PCF200 1-00	1.90	VR105 59			BY210	-88
-1			EY84 -92	PCF201 1 05	QV06/20	VU111 -80			BYZ11	-88
- 1	ECH42	- 80								
	ECH81	-40	EY86/7 ·40	PCF801 -65	8 - 50	VU120 1-17			BYZ12	.83
ŀ	ECH83	.52	EY88 -60	PCF802 -50	R19 -75	VU120A			BYZ13	-88
	ECH84	-50	EY91 -50	PCF806 -60	TH233 1.00	1.17	AD161 -		FSY11A	-29
	ECL80	-50	EZ40 -55	PCH200	TP2620 1-00	VU133 -80	AD162 ·	59 I	F8Y41A	-29
ı	ECL82	-45	EZ41 -55	1.00	UABC80 -47	W107 -75	AF114 4	38	OA9	-16
ı	ECL83	-82	EZ80 -35	PCL82 -45		W729 1:17			OA10	-55
: 1	ECL84	-70	E281 -85	PCL83 -50	UAF42 .75	X66 1.46			OA47	.13
,			GY501 -82	PCL84 -50	UBC41 -60	Z759 5.85			OA70	.20
6	ECL85	.70		PCL86 -55	UBC81 -60	Transistors			OA73	.20
1	ECL86	-47	GZ32 ·59		UBF80 -47				OA79	-12
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)	EF40	-88	GZ34 ·80	PEN45 1.00	UBL21 2-84	1N4744 ·18		28	0A81	
ιl	EF41	-82	GZ37 1.20	PEN45DD	UC92 ·60	2N404 28		12	OA85	-12
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il	EF73	1.76	-80	PEN46 -60	UCC85 -58	2N1756 -64			OA91	-18
	EF80	-80	HL23DD	PEN453DD	UCF80 -90	2N2147 1·10			OA95	-12
,	EF83	1.45	-80	8.00		2N2297 ·29	BA129 ·1		OC44	-13
,	EF85	-40	HL41DD	PENDD	UCH21 2-34	2N2369 ·18			OC45	-14
	EF86	-50	1.00	4020 1:00	UCH42 ·88	2N3053 -42	BA153 -2		OC46	-20
1	EF89	-85	HL42DD	PFL200 -82	UCH81 -47	2N3121 8-22	BC107 ·1	16	OC70	-16
!	EF91	-50	1.00	PL33 50	UCL82 ·45	2N3703 -25			OC71	-14
!	EF92	-60	HN309 1.76	PL36 ·70	UCL83 -64	2N3709 -26			OC72	-14
1	EF97	-94	HVR2 1:00	PL81 58	UF41 -82	AA119 -20			OC74	-29
וי	EF98	-95	HVR2A		UF42 -82	AA120 -20	BC115 ·		OC75	14
3				PL81A -60	UF80 -41	AA129 -20			OC76	.20
)	EF183	.40	1.17	PL82 ·48	UF85 -58	AAZ13 28			OC77	-25
)	EF184	-40	KT41 1.17	PL83 .50	UF89 -47				OC78	-20
i	EF804	1.75	KT66 2.98	PL84 50	UL41 .75				OC78D	-20
1	EH90	-44	KT81 2-10	PL504/500	UL84 ·49				OC81	.14
ı	EL32	-60	KT88 5.75	0.82						-14
ì	EL34	1.00	KTW61 1.76	PL505 1.65	UM80 -60	AC127 -28			OC81D	
١ ،	EL35	8.00	KTW621.76	PL508 1.10	UY41 ·50	AC128 ·26			OC82	-14
i	EL37	8.00	KTW63 1-17	PL509 1:65	UY85 .50	AC132 -26			OC82D	-14
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П	EL83	.70	P61 -60	PY81 -40	U19 4.00	AC157 ·88			OC123	-29
H	EL84	-86	PABC80 -45	PY82 -40	U25 ·70	AC165 -38			OC169	-89
	EL86	-80	PC86 ·70	PY83 45	U26 · · 65	AC166 -88	BF181 -		OC172	-46
1	EL95	.70	PC88 -70	PY88 47	U33 1.75	AC168 -49			OC200	-59
:	EL360	1.80	PC95 -70	PY500A	US5 1.75	AC176 -71	BFY50 .		OC201	-59
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۱!	EM80	-53	PC900 80		U81 -80	ACY17 -38	BFY52 -S	26	OC203	-89
: 1	EM81	-76	PCC84 -40		U191 -50	ACY18 -26	BY100 -2	8	OC204	-89
!	EM83	-64	PCC85 -50	PY801 45	U251 -94	ACY19 -25			OC205	-55
1	EM84	47	PCC88 -65	PZ30 .50		ACY20 .23			OC206	1.17
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ıſ				Q875/20	U404 -75	LP15 (AC113	AC154. AC	157.	AA120)	-689
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to decipher this time, reports that the Deutsche Welle African service is coming in very strongly in that part of the world. On his Philips 361A Vincent reports this service at 1340 on 17500 and alongside this go Radio Pakistan on 5955 at 2140 and SBC on 6309 at 2120.

One of the main snags with radios is the nagging thought that the set may not be properly calibrated and may be pulling in a frequency other than that shown on the dial. This is particularly so when one builds a set or when that faint station that has never been heard before whispers in and is just the one to fill that gap in your QSL album. Our old friend G. E. W. Hewlett, whom many will remember from columns past, writes of a station that is not only a calibration aid but also a test of that copper wire cobweb in the loft. While tuning around a few weeks ago George decided to try for WWV in order to check his calibration. The service in question is located at Fort Collins, Colorado USA and transmits on 2.5, 5, 10, 15, 20 and 25MHz. The distinctive signal is a time signal and a male voice announcement every minute. Much to George's surprise he also heard a female voice which is the other time and frequency checking station WWVH at Kauai, Hawaii. WWVH transmits on the same frequencies but is most unlikely to be heard here very frequently.

George goes on to tell us that Radio Australia has opened a 250kW transmitter at Carnarvon to cover the gap in its Asian service. The test transmissions are, at the moment, as follows:

9540 Indonesian 0800 to 1030 9560 Mandarin 1030 to 1300 9560 Cantonese 1300 to 1430

The 9560 channel is best heard around 1300 but in summer, when the short route gets better and an extra transmitter has been put into service, these signals should be worth listening for.

For those who like the African stations John Dipre using a VEF204 comes up with a few goodies:

4850 Radio Mauritania at 2038 4904 Radio Chad at 2035

4904 Radio Chad at 2035 4915 Radio Ghana at 2300

4940 Abidjan at 2250

5047 Radio Togo at 2257

To these we can add the loggings of Charles Winpenny who reports ETLF Ethiopia at 2020 on 11755 to give you a good handful of the infrequently reported services. Charles also asks if anyone knows what has happened to the Voice of Turkey English service on 9515 at 2200, which seems to have been dropped in favour of a Turkish language service.

Finally, we welcome two newcomers, Julian Blake of London and, lo and behold, our first lady correspondent Diane Kinnear from Cullicudden, Rossshire. Both ask the same question. "Please recommend a book to start us off and fill the gaps." The one I would plump for is "A Guide to Amateur Radio" by Pat Hawker G3VA from the Radio Society of Great Britain, 35 Doughty St., London WC1, price £1.14 inc. Don't be put off by the title, however, since our SWL DXing owes a lot to the licensed

amateur. As well as explaining many of the terms that they use, the book explains many of the matters that the two branches of our hobby have in common. This winds up the session for this month so I will say 73s to you and yours.

# MEDIUM WAVE DX by CHARLES MOLLOY

TEVE WHITT (G8KDL) reports from London NW4 with a good bag of North American medium wave DX. With his Chapman S6BS communications receiver, MW loop and FET pre-amplifier he logged WINS in New York City on 1010kHz at 0130 which he describes as "a phenomenal signal, I actually considered ringing into their phone-in programme". Other North Americans logged by Steve include CJOX Grand Bank in Newfoundland on 610kHz; WOR in New York City on 710kHz; WABC in NYC on 770kHz; CHNS in Halifax, Novia Scotia on 960kHz; KDKA in Pittsburg on 1020kHz and WNEW in NYC on 1130kHz.

North American medium wave stations are allocated identifying call letters which are used frequently by announcers, which makes identification easy for the DXer. These stations can be logged in the UK throughout the year whenever the path across the North Atlantic is in darkness. Even in midsummer, reception is possible for about an hour before sunrise. During March and April start listening around 0130GMT. Reception can be very good at this time of year since interference from Europe is much less than during the earlier winter months owing to the approach of daybreak from the east.

An interesting letter comes from New Zealand reader Ash Nallawalla of Dunedin. Ash is president of the Otago branch of the New Zealand Radio DX League and is a keen medium wave DXer. With his Sanyo receiver, 40in delta shaped loop and an FET booster he logged Malta on 1570kHz and Munich, West Germany on 1602kHz. Reception in New Zealand of European broadcasts at the HF end of the medium waves has been reported before. In 1971, the well known New Zealand DXer Arthur Cushen in a letter to the writer, mentioned his reception of Langenburg on 1586kHz and Munich on 1602kHz at 2000GMT. The path at that time of day would be on the western route across South America, propagation being by five-hop F layer rather than by the E layer, which is responsible for most of the DX heard on the medium waves. New Zealand and Australia are not heard on the medium waves in the UK probably because there are so few high power transmiters in these countries and the high level of interference at our end of the path. Reception of 40D, the 50kW outlet at Emerald in Queensland has been reported on more than one occasion from Finland on 1550kHz, a frequency that is almost buried in QRM in this country during the evening.

Tuning-in a signal on a radio receiver is usually quite a straightforward business. The tuning control is adjusted to give maximum reading on the S meter, or if there isn't a tuning indicator, then the control is "rocked" until the receiver is spot-on the carrier frequency. This procedure works well in the absence of interference when adequate bandwidth is avail-

able (selectivity control at "wide") to include both sidebands of the transmitted signal. When trying to pick-out a weak DX signal in a crowded MW band, high selectivity is desirable to try to reduce adjacent channel interference. High selectivity leads to sideband cutting and loss of HF response at audio frequencies. Speech becomes muffled and difficult to follow. Intelligibility can be improved if the receiver it detuned slightly. Its IF passband now covers all one sideband instead of part of both, speech clipping is reduced while selectivity is maintained and cleaner and easier to understand speech will be the result. If the interference is coming from only one side of the DX then detune away from it. The strength of the unwanted transmission will be reduced while the level of the DX will be unchanged.

The second session of the International Telecommunications Union Conference on the future of medium and longwave broadcasting in Regions 1 and 3, which includes Europe, was held in Geneva last autumn. As expected, the 9kHz channel spacing in Europe is to continue though many channels on the medium waves will have their frequency increased by 1kHz so that they are multiples of 9kHz. Heterodyne interference will be reduced if each channel is harmonically related to the channel spacing. The UK is allowed two additional transmitters on the longwaves, both of which will be located in Scotland. One will be on 200kHz (1500m), the existing longwave channel and the other will be on 227kHz (1321m). They will come into use after the start of the new plan in November 1978.

The retention of the 9kHz spacing will continue to favour the DXer who is interested in reception of Region 2 (North and South America) where the spacing is 10kHz but the 1kHz change in Europe will bring its problems. Reception of KOMO in Seattle and WCFL in Chicago both on 1000kHz will become more difficult as the nearest European will now be on 999kHz. Whether there will be any compensating gains, remains to be seen.

Latin American medium wave stations, especially those situated along the east coast of South America, come in well in the UK. The long sea path across the North and South Atlantic favours propagation from Argentina and Brazil enabling some of the higher powered broadcasters in Buenos Aires and Rio de Janeiro to be heard at surprising strength at times. D. R. Mayhew (Littlehampton) has been chasing DX from this area between the hours of midnight and 0300 using a Philips receiver and a 20in loop with RF amplifier. He says "the Brazilians are very exciting and well worth waiting for" and he mentions hearing two broadcasts from Buenos Aires; Radio Belgrano on 950kHz and Radio el Mundo on 1070kHz and no fewer than five from Rio de Janeiro; Radio Mundial on 860kHz, Radio Jornal do Brazil on 940kHz, Radio Nacional on 980kHz, Radio Globo on 1180kHz and Radio Eldorado on 1220kHz plus Radio Record in Sao Paul on 1000kHz.

Portuguese is spoken in Brazil, a language that sounds a bit different from Spanish which is used in Argentina and the remainder of Latin America. The majority of Brazilian stations are commercial, owned often by newspapers. Musical programmes include the rhythms of the samba and bossa nova which beat out from trumpets, guitars and marimbas to entertain the distant DXer!

#### D. F. RECEIVER—continued from page 1064

circuits. Band coverage is determined by the settings of TC1, TC2, TC3, TC4 and the position of the oscillator coil core.

Aerial alignment is determined by TC5, VC3 and the positions of L1 and L2 on the rod. Correct alignment of the aerial tuning is shown by maximum meter reading. If VC3 enables a signal to be peaked up, and is not fully open or fully closed, alignment may be regarded as correct at that frequency. However, the settings of TC5, L1 and L2 must be approximately correct or the trimming compensation afforded by VC3 may be insufficient at some frequencies.

Band 1. With each band the low frequency end is reached with VC1/2 closed and the high frequency end with VC1/2 open. For this band, TC4 sets the HF limit and TC2 the LF limit. TC5 is set so that VC3 can be peaked as described and may need re-adjustment after dealing with Band 2.

Band 2. TC3 sets the HF band limit. With a signal tuned in near the HF end of the band, adjust VC3 for best volume or meter reading. Tune in a signal near the LF band end and move L1 on the rod for best signal level, leaving VC3 untouched. Check that VC3 can peak signals throughout the band.

Band 3. Oscillator coverage is independently adjusted by TC1 and L2 which is adjusted at the LF end of the band. A 60pF trimmer may be wired from pin 2 to pin 3, for LW trimming, but is not essential.

On all bands a small adjustment to the oscillator coil core setting will cause a substantial shift in frequency. So if this is made on any one band, the other two bands have to be checked again, as described. The actual coverage which is obtained can be modified quite substantially. It is not necessary that any particular bands are obtained by these adjustments, as other settings will result in no loss of efficiency, provided VC3 allows signals to be peaked up. The ranges actually provided were: Band 1: 1300-1500kHz; Band 2: 600-1300kHz; Band 3: 160-250kHz.

#### In use

To locate the position of the receiver, bearings have to be taken from at least two transmitters whose positions are known. If these are plotted on a map or chart, the receiver will lie roughly at the intersection of the lines. A third bearing can be expected to give more accuracy and should confirm the first result. To locate the position of a transmitter, directional bearings on its signal have to be taken from two known positions. When these are plotted, their intersection shows the transmitter location.

Low frequency and ground wave signals will generally give quite accurate bearings. Ground wave signals are those which have not been reflected by ionised layers above the earth. Their useful range depends on power, frequency and other factors and may extend to fifty miles or more. Sky-waves, on the other hand, are those reflected down and they provide greatly increased range, especially for higher frequency signals after dark but they may give confused bearings. In coastal areas wavefront bending may cause a deviation of 10-15° while nearby metal objects or structures may also modify the apparent direction of a signal. For ordinary reception purposes, it is only necessary to rotate the aerial for best reception, or minimum interference.

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12V 100 MA
14V 75 MA
14V 75 MA
C 5MM 28V 40 MA
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- check tape switch for encoded monitoring in three-head machines

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		BFX30 30p	CRS1-60 65p	2N1131 15p
AC141 18p				2N1132 16p
AC141K 28p	BC212L 11p*	BFX84 23p		
AC142 18p	BC213 12p*	BFX85 25p	CRS3-10 45p	2N1304 20p
AC142K 28p	BC213L 12p*	BFX88 20p	CRS3-20 50p	2N1305 20p
AC176 16p	BC214 14p*	BFY50 20p	CRS3-40 60p	2N1711 18p
		BFY51 18p	CRS3-60 85p	2N2102 44p
AC176K 25p	BC214L 14p*	Dr 131 10p	MJ480 80p	2N2369 14p
AC187 18p	BC237 16p*	BFY52 19p		
AC187K 25p	BC238 16p*	BFY64 35p	MJ481 £1:05	2N2369A 14p
AC188 18p	B C300 34p	BFY90 65p	MJ490 90p	2N2484 16p
AC188K 25p	BC301 32p	BR100 20p	MJ491 £1-15	2N2646 50p
	BC323 60p	BRY39 40p	MJE340 40p°	2N2905 18p
AD140 50p	BC323 00P		MJE371 60p	2N2905A 22p
AD142 50p	BC327 18p°	BSX19 16p		
AD143 46p	BC328 16p°	BSX20 18p	MJE520 45p	2N2926R 10p*
AD149 45p	BC337 17p*	BSX21 20p	MJE521 55p	2N2926O 9p*
AD161 35p	BC338 17p*	BSY95A 12p	OA5 50p*	2N2926Y 9p*
AD162 35p	BCY70 12p	BT106 £1 00	OA90 8p	2N2926G 10p*
		BT107 £1 .60	OA91 8p	2N3053 15p
AL102 95p				2N3054 40p
AL103 93p	BCY72 12p	BT108 £1 69	OC41 15p	
AF114 20p	BD115 55p	BT109 £1 00	OC42 15p	2N3055 50p
AF115 20p	BD131 36p	BT116 £1 00	OC44 12p	2N3440 56p
AF116 20p	BD132 40p	BV105 £1-88*	OC45 10p	2N3442 £1 · 20
AF117 20p	BD135 36p	BV105/	OC70 10p	2N3570 80p
		02 £1 90*	OC71 10p	2N3702 10p*
AF118 50p	BD136 39p	02 21.80	OC72 22p	2N3703 10p*
AF139 33p	BD137 40p	BV126 £1 60°		
AF239 37p	BD138 48p	BY206 15p*	OC84 14p	2N3704 10p*
BC107 14p	BD139 8p	BY207 26p*	SC40A 73p	2N3705 10p*
BC107B 16p	BD181 86p	BYX36-300	SC40B 81p	2N3706 10p*
BC108 13p	BD182 92p	12p*	SC40D 98p	2N3707 10p*
		BYX36-600	SC40F 65p	2N3714 £1 · 05
BC109 14p				2N3715 £1-15
BC109C 16p	BD184 £1 20	15p*	SC41 A 65p	
BC117 19p*	BD230 90p	BYX36-900	SC41B 70p	2N3716 £1 ·25
BC125 18p*	BD231 90p	18p*	SC41D 85pr	2N3771 £1 · 60
BC126 20p°	BD 232 00p	BYX36-1200	SC41F 60p	2N3772 £1 ·60
BC141 28p	BD233 90p	210*	ST2 20p	2N3773 £2-10
		BYX38-	TIP29A 44p°	2N3819 28p*
BC142 23p	BD237 06p		TIPZSA 44P	2143018 46-8
BC143 23p	BD238 90p	300 <b>50</b> p	TIP30A 52p*	2N3904 16p*
BC144 30p	BD239 00p	BYX38-	TIP31A 54p	2N3906 16p*
BC147 9p°	BDY20 80p	600 55p	TIP32A 64p	2N4124 14p
BC148 9p*	BDY38 60p	BYX38-	TIP34 £1.05	2N4290 12p
BC140 BP	BDY60 60p	900 60p	TIP41A 68p	2N4348 £1 · 20
BC149 9p°		BYX38-	TIP42A 72p	2N4870 35p*
BC152 25p°	BDY61 65p	D 1 A 30-	11F42A /2D	
BC153 18p*	BDY62 55p	1200 65p	IN2069 14p	
BC157 9p°	BF178 28p	BZX61 series	IN2070 16p*	2N4919 70p*
BC158 9p°	BF179 30p	zeners 20p	IN4001 4p*	2N4920 50p*
BC159 9p°	BF194 10p*	BZX83 or	fN4002 5p*	2N4922 58p*
BC160 32p	BF195 10p*	BZY88 series	N4003 6p*	2N4923 64p*
	BF196 12p*	zeners 11p°	IN4004 7p*	2N5060 20p*
			N4005 8p*	2N5061 25p°
BC168B 9p°	BF197 12p*	C106A 40p	IN4005 8p*	2110001 25P

MIMIOSIA	E-3 /3. WIN	30 10 20 201	
DIGIT	AL DIS	PLAYS &	LED's
		D1 247	4 35

DE707	99p	DL75		1 - 75	GREEN C	LEAR	15p
THYR	STORS	·8A (TO92)	1A (TO5)	3A (C106 type)	6A (TO220)	8A (TO220)	10 A (TO220)

#### 50 100 200 400 600 TAB) TO-220 PKGE, ISOLATED

#### (a) (b) (a) (b 4A (a) (b) 0:60 0:60 0:64 0:64 0:77 0:78 0:96 0:99 6 5A (a) (b) 0.70 0.70 0.75 0.75 0.80 0.83 0.87 1.01 8·5A (a) (b) 0·78 0·78 0·87 0·87 0·97 1·01 1·21 1·26

14	TTL	mix	ed prices								
	1-24	25-99	100+		1-24	25-99	100+		1-24	25-99	100+
7400	14p	12p	18p	7445		71 p	57p	7492	57p	46p	36p
7401	14p	12p	10p	7447	81 p	75p	65p	7493	45p	48p	32p
7402	14p	12p	10p	7448	75p	62p	58 p	7495	67p	55p	45p
7403	15p	12 p	10p	7447	A 95p	83p	67p		£1 -88	\$9p	72p
7404	16p	13p	11p	7470	38p	25p	28p	74107	35p	28p	22p
7408	16p	13p	11p	7472	25p	21 p	17p	74121	34p	28 p	23p
7409	16p	13p	11 p	7473	30p	25 p	28 p	74122	47p	39p	31 p
7410	16p	13p	11p	7474	32p	26p	21 p	74141	78p	63p	53p
7413	29p	24p	20p	7475	47p	39p	31 p	74145		58 p	48p
7417	27 p	22 p	20p	7476	32 p	26p	21 p			£1-48	86p
7420	16p	13p	11p	7482	75p	62p	50 p	74174	£1.00	83p	67p
7427	27p	22 P	18p	7485	£1 · 30	£1 · 09	87p	74180	£1 · 06	88p	71 p
7430	16p	13p	11 p	7486	32p	26p	21 p	74181	£3.20	£2:50	£1 · 90
7432	27p	22 <del>j</del> p	18p		£2.92	£2-80	£2·10	74102	£1 · 35	64-14	90p
7437	27p	22 p	18p								90 p
7441	75p	62p	50p	7490		40 p	32p		£1 · 35		
7442	65p	55p	43p	7491	65p	55p	45p	74196	£1 · 64	£1:34	99p

LINEAR IC'	8			
301 A 8 pin DIL 307 309 K 380 14 pin DIL 381 14 pin DIL Matching charge COMPLETE LIST		3900 14 pin DiL 709 8/14 pin DIL 741 8/14 pin DIL 748 8 pin DiL 555 8 pin DiL pair. P & P 20p—Ov	70° 35° 28° 36° 45 /erseas	585 14 pin DIL £2:00° 566 8 pin DIL £1:50° 567 8 pin DIL £2:00° CA3046 14 pin DIL 50° 80p. SEND SAE FOR

HIGHAM MEAD, CHESHAM, BUCKS. Tel. (02405) 75154 VAT-Please add 8% except items marked \* which are 25%

#### **MULLARD AUDIO AMPLIFIERS**



MULLARD AUDIO AMPLIFIERS

All in module form, each ready built complete with heat sinks and connection tags, data supplied.

Model 1153 500mW power output \$1.10 + 40p post & VAT.

Model 1172 1W. power output \$1.35 + 45p post & VAT.

Model EP9000 4 watt power output \$2.40 + watt

power output \$2.40 + 50p post & VAT.
EP 9001 twin channel or stereo pre amp. 49-50

#### LIGHT SWITCH



Attomatically switches on lights at dusk and off at dawn. Can also be used where light and dark is a convenient way to stop and start an operation. Requires only a pair of wires to the normal switch-plate size. VAT and Postage 50p.

#### MAINS TRANSISTOR PACK

Designed to operate transistor sets and amplifiers. Adjustable output 6v., 9v., 12 volts for up to 500ma (class B worklag). Takes the place of any of the following batteries: PPI, PP3, PP4, PP6, PP7, PP9 and others. Kit comprises: main transformer rectifier, smoothing and load resistor condensers and instructions. Real snip at only \$21.50 VAT & Postage 60p.

#### SOUND TO LIGHT UNIT

Add colour or white light to your amplifier. Will operate 1, 2 or 3 lamps (maximum 450w). Unit in Box all ready to work. 27.95 plus 95p VAT and





#### MAINS MOTOR

Precision made—as used in record decks and tapes recordrecord decks and tapes recorders—ideal also for extractor fans, blower, heaters, etc. New and perfect. Snip at 95p + VAT & Postage 35p.

1" stackmotor \$1.50 + VAT & postage 35p. 11" stackmotor 22 + VAT & Postage 40p.

#### 6 DIGIT COUNTER

Made by famous American Company, operated by 24V D.C. or mains through resistor, 19/18" x 1" x 2j" deep. 80p Post & VAT



#### MINIATURE WAFER SWITCHES



2 pole, 2 way—4 pole, 2 way—2 pole, 3 way—4 pole, 3 way—2 pole, 4 way—2 pole 6 way—1 pole, 12 way. All at 30p + 15p poet & VAT each.

#### MULTI-SPEED MOTOR

Six speeds are available 500, 850 and 1,100 r.p.m. and 8,000, 12,000 and 15,500 r.p.m. Shaft is 1 in. diameter and approximately 1 in. long, 230/240v. Its speed may further controlled with the us may our Thyristor controller. Very powerful and useful motor s approx. 2 in. dia. x 5 in. lor Price \$1.40 + 45p post & VAT. ng.



#### **BATTERY CHARGER**

Famous Atlas in metal case with meter, output leads terminated by crocodile clips. For 6 or 12V charging simply by changing plug on front panel. Ready built new and still \$2.95 plus £1 Post & VAT.



AMMETERS

Ideal for chargers etc. 2" sq. full vision 0.8 amp 95p, 1;" round 0.2 amp 55p, 0.4 amp 78p. Post & VAT 25p each.

#### RELAY BARGAIN

Type 600 relay, 2 changeover one open and one closed contact. Twin 500 ohm colla make this suitable or closing off DC 6v, DC 12v, DC 24v or AC mains using resistor and rectifier, 40p each. Resistor or rectifier 20p extra, Post & VAT 20p.

#### ONLY £1.50 FOR SEVEN **ELECTRIC MOTORS**

powerful batt, motors as used in racing cars & power models. Output & types vary for use in hundreds of different projects — Tools, toys, projects models. toys projects — Tools, toys, models, etc. All brand new reversible & for 1\(\frac{1}{2}\)-1222 battle Wiring diagram, inc.



#### **AUDIO AMPLIFIER**

Part of the famous Reditune background music system, secondhand, but believed in good order. However, no gnarantee: we are salling for gnarantee. system, secondhand, but believed in good order. However, no guarantee; we are selling for spares value only. These are 6 valve amplifiers, the output valves are 2 x EL 84 in push/pull, complete with mains transformer, rectifier and ample smoothing equipment. The mains transformer alone, today would cost at least \$4.8 kize is \$9\forall x \tilde{5}\tilde{1}\tilde{x} \tilde{4}\tilde{x}''. Price only \$2.00 + postage and VAT £1.50.



#### TWIN OUTPUT POWER PACKS

These have two separately R.C. smooth outputs so can operate two battery radios on a sterec amp without cross modulation (they will of course operate one radio-tape-cassette-calculator in fact any battery appliance and will save their cost in a few months). Specs.: Full wave rectification, double insulated mains transformer—total enclosed in bard P.V.C. case—three core mains lead or 24v. Price \$3.95, post and VAT included.

#### TANGENTIAL HEATER UNIT



This heater unit is most efficient, and quiet running. Is as fitted in Hoover and blower heaters costing £15 and more. Comprises motor, impelier. 2kW element and lkW element allowing switching 2kW element and IkW element allowing switching 1, 2 and 3kW and with thermal safety cut-out. Can be fitted into any metal line case or cabinet. Only needs control switch. \$582 plus VAT & post 21, 2kW Model as above except 2kW \$4.25 plus VAT & post 25, Don't miss this. Control Switch 44p. P. & P. 40p.

#### ISA ELECTRICAL PROGRAMMER



Learn in your sleep: Have radio playing and kettle boiling as you awake—switch on lights to ward off intruders—have a warm house to come home to. All these and many other things you can do if you invest in an electrical programmer. Clock by famous maker with 15 amp. on/off switch. Switch-on time can be set anywhere to stay on up to 6 hours. Indeory jogger. A heautiful unit. Price 22-95, VAT & Postage

endent 60 minute memory jogger. A beautiful un 0p, or with glass front, chrome bezel, £1.50 extra.

#### THIS MONTH'S SNIP

YOUR TIME is the most precious thing you have. Do you waste it waiting for the soldering iron to heat up? You can be soldering in a few seconds with the E.T.P. Soldering Gun which we offer at a specially keen price. It is in fact this month's snip. A well made lightweight unit with flash lamp to illuminate the work. Has 100 watt double insulated mains Transformer and the work of the property of is built into a shockproof Thermo-plastic case. Suitable for 240 volt, 5@c.p.a. This comes complete with 5 spare tips and is offered at a special snip price \$2.75 plus tips and is offere 85p Post & VAT.



#### CENTRIFUGAL FAN

Mains operated, turbo blower type. Pressed steel housing contains motor and impeller. Motor is 1/10th h.p. giving considerable air flow but virtually no noise Approx. dimensions 10½" x 4½" 28°50 plus Post & VAT.

#### THERMOSTAT WITH THERMOMETER



Made by Honeyweil for normal air temperatures 40-80 F (5-25 C). This is a precision instrument with a 40-80 F (5-25 C). This is a precision instrument with a differential which can be adjusted to better than 1-5 F. A mercury switch breaks on temp. rise. Elegantly styled and encased in an invery plastic case with clear plastic windows, thermometer above and switch setting scale below—size approx. 36 "X 32" X 1-4" deep—can be mounted on conduit box or directly on wall. Price 22-25 plus 90F post & VAT.

#### SHORTWAVE CRYSTAL SET

Although this uses no battery it gives really amazing results. You will receive an amazing assortment of stations over the 19, 25, 31, 29 metre bands-Kit contains chassis front panel and all the parts, £1.50—crystal earphone 55p, VAT & Postage 75p.

#### SWITCH TRIGGER MATS

So thin is undetectable under carpet but will switch on with alightest pressure. For burglar alarms, shop doors, etc. 24in x 18in £1-93. Post & VAT 80p.
13in x 10in £1-56. Post & VAT 65p.

#### SMITHS CENTRAL HEATING CONTROLLER



Push button gives 10 variations as follows:-(1) continuous hot water and continuous central heating (2) continuous hot water but central heating off at night (3) continuous hot water but central heating off an inght (3) continuous hot water but central heating off an only for 2 periods during the day (4) hot water and central heating off to be water all day but central heating only for 2 periods during the day (6) hot water and central heating only for 2 periods during the day (6) hot water and central heating on heating off (7) hot water continuous (8) hot water day time only (9) hot water twice daily (10) everything off. A handsonie looking unit with 24 hour movement and the switches and other parts necessary to select the desired programme of heating. Supplied complete with wiring diagram. Originally sold, we believe, at over \$15—we offer these, while stocks last, at \$6.95 each, VAT & Postage \$65p each.

TERMS: Where order is under 25 please add 30p surcharge to offset packing expenses. Send SAE for monthly list.

### J. BULL (ELECTRICAL) LTD.

(Dept. PW), 103 TAMWORTH RD. GROYDON GRO IXX

THIS MONTH'S SPECIAL OFFER is a very versatile transformer which can be used for many purposes. Rated at 250 watas it is very well built with frames to pright the continuating and is varnish to expect the pright for 230/240 volts to expect that for pright for 230/240 volts to expect that four secondaries each 10 very high current wholings. Just a few of the circuits it can power are: 10-0-10 at up to 12 amps; 10-0-20 at up to 6 amps; single 10 v at 25 amps; single 20 v at 12 in up; single 30 v at 9 amps; single 40 v at 6-5 amps. The transformer can be used for power circuits (charging, etc.) or for amplifiers, there being an earth screen between primary and secondaries. A transformer like this to-day would cost at least £15 from the makers; however, we are making a special offer at \$3.50 + tal. THIS MONTH'S SPECIAL OFFER is a very

amplifiers, there being an earth screen between primary and secondaries. A transformer like this to-day would cost at least £15 from the makers; however, we are making a special offer at \$5.60 + 28p, post £1 + 8p each. Grab some while you can, out stock may not least long. Mains isolation kit. Apart from the fact that it is lilegal for you not to provide adequate protection for any staff or persons working for or with you, your own personal comfort will be greater when you work isolated from the mains. Also, you are not likely to damage equipment if your soldering from becomes earthy, as often beginned to the provide and the staff of the provide and the staff of the provide and the staff of the staff of the staff of the soldering transformers are staff or the staff of the soldering transformers are staff or the staff of the soldering transformers are staff or the staff of the soldering transformers are staff or the staff of the soldering transformers are staff or the staff of the soldering transformers are staff or the staff of the soldering transformers are staff or the staff of the staff of the soldering transformers are staff or the staff of 
and below alphabetically and numerically so cach can be easily ideutified. Contacts are capable of making positive connection with a strip or wire as each contact is spring loaded and has a gold "pip". Ideal if you want to make yourself a computer or for circuit bread-boarding fresistors, etc. plug straight in) or for working out printed circuits, even for teaching electronics and novelties such as puzzles, combination locks, etc. Taken from unused computer panels, price only \$2 + 16p each which works out to only 1p per contact, probably less than the value of the gold pip. Gold plated strips for permanent contacts into slot of above panels, 15 for \$1 + 8p. Vennor 1 rev per hour motor with spindle threaded and nutted ready to easily attach discs or drums. Bakelite encased motor beautifully made and nutsel for this, for instance a disc or drum attached could operate microswitches for display or mood lighting, etc.

Digital Display Unit, Digivisor'. This is a precision

could operate microwattenes for display or moot lighting, etc. Digital Display Unit, Digivisor'. This is a precision Instrument which consists basically of 12v lamp focused by a lens system through a numbered scale, the number appears on a ground glass front acreen. The number is selected by applying a different voltage to the coil which rotates the scale e.g. 1 volt applied shows figure 1 on scale—by using shunts or multipliers however any voltage or current could be made to indicate any voltage or current could be made to indicate any voltage or retree to ell is positioned on the screen then an alarm could be triggered. Similarly this could be used for voltage or current regulation. Overall size of the unit is  $24'' \times 14'' \times 44''$ .

Overall size of the unit is  $24'' \times 14'' \times 44''$ . Price  $34.60 \times 36$ .
Pulse transformer with circuit for sound to light unit. It is a sery simple circuit and all parts are realily obtainable from us or you may already have them in your junk box. Price of the transformer with circuit 75p, post and VAT paid. ORF 18 light cell. This device has been going for some years now but it has not been bettered and new applications keep being found for it. We have good stocks, price 65p + 5p. Throat mikes. These are an ex WD item as used by air crew on their intercom, but being electromagnetic they also serve as pick-ups on musical instruments, talking to passengers on motor bike and no doubt many other uses. Price 60p a pair +15p.

+ 15p.

One chip radio, Ferranti ZN 414 IC radio is still in stock, current price £1.49 + 38p. We can also still supply the £1 Q kits to go with them, most popular one kit No. 4, comprises a permiability tuner for medium wave, and the resistors and condensers which when added to the ZN 414 complete the radio for medium wave band.

lete the radio for medium wave band, of this HQ kit No. 4 is 68p + 17p, post Price of this HQ kit No. 4 is 689 + 17p, post 20p + 5p. 12\text{} watt speaker bargain, 8" round mid-range, made for high priced hi-fi outfit, a really super speaker, 23 + 75p, post 60p + 15p. Bicroswitch, Honeywell ref. no. YZ RW 84-N88. This has fairly long lever and is changeover 15 amp

This has fairly long lever and is changeover 13 amp 250v rating. Price 30p + 21p each. Two circuit microswitch, tamous American Llcon, maker's ref. 16-40411, size approx. 1" long \( \) " wide \( \) " thick \( \) " thick \( \) Two electrically separate circuits, one makes, the other breaks, when nylon push rod is depressed. Circuit rating we estimate at 5 amps 250v. A real bargain at 15p each \( + 1p \)— subject to normal quantity discounts. Reed relay in solenoid. Resistance 1-5K, this will operate from voltages of 10 v upwards on a current of 12mA upwards. The flow of the control current closes the reed switch but if you bias this with a small magnet or an opposing current, then the flow of the control current could be made to open the reed switch. Price 75p \( + \frac{5}{9} \),

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Practical Wireless, April 1976

(DEPT. PW4), SIMMONDS ROAD, WINCHEAP CANTERBURY, KENT Tel: (0227) 52436

# TRANSFORMERS 18%

#### CASED TRANSFORMERS

HANS-FURMER Housed in smart resin coated steel cases with 3 core power cable and outlet socket, fused primary winding. Isolation types are fitted with 3-pin outlet sockets and are available with 110 volt or 240 volt output (please state). Auto types are fitted with 2-pin flat style sockets up to 500VA. 3-pin sockets from 750 to 3000VA. See Auto Isolation Sections for prices. Plugs extra.



SAFETY ISOLATING	See catalogue for full rang
Prim. 120/240V, Sec. 120/240V.	Centre Tap with screen.

250	152	13-81	0.98	10.31	1.18
200	151	12.29	0.98	8-61	0.97
60	149	9-03	0.98	4.70	0.72
(Watts)	NO.	£	£	£	£
V.A.	REF	CASED 2	Pin + Earth	OPEN	POST
		PRICE	PLUGS	PRICE	
			PRICE		

#### **AUTO TRANSFORMERS**

VA (Watts) 1500	REF. NO. 93	PRIČE CASED £ 23:26	PLUG8 2 & 3 pin £ 0.95	PRICE OPEN £ 19 22	POST £ O/A		
TALLET A THE PARTY OF THE PARTY							

#### MINIATURE & EQUIPMENT

40 0 4						
0-9	0-9	330	330	235	1.62	0.34
9-0-9	_	100	-	13	1-60	0.34
0-6	0-6	1000	1000	212	2.12	0.46
0-6	0-6	500	500	234	1.56	0.34
3-0-3	_	200	_	238	1.56	0.34
Sec. 1	Sec. 2	Sec. 1	Sec. 2	NO.	£	£
	LT8		IAMP8	REF.	PRICE	POST
	240 V W			see catar	ogue for i	un range

#### 12 & 24 VOLTS

TRANSISTORS

Primary 200-240 Vol	ts. See	catalogue	for full range
AMPS	REF.	PRICE	POST
12V 24V	NO.	£	£
2 1	71	2-47	0.61
4 2	18	3.07	0.62
6 3	70	4.50	0.72
8 4	108	5.11	0.85
		-	

#### 30 VOLTS

50 VOLTS

60 VOLTS Primary 200/240V

0.5

	200/240 12, 15 y	V , 20, 24, 3	0V
	REF.	PRICE	POST
AMP8	NO.	£	£
0.5	112	2.04	0.61
L	79	2.57	0.66
3	3	3.91	0.72
3	20	4.80	0.85
4	21	5.58	0.85
5	51	6.75	0.95
6	117	7.52	0.97
8	~ 4	9-93	1.18
10	89	10.27	1.18

Primary 200/240V Secondary 19, 25, 33, 40, 50V

PRICE POST

PRICE POST

0.76 0.85

0.85 1.08 1.18 1.44 1.86

0.72

1·18 1·18

3·58 5·30

6-10

7.97 12.93 13.75 17.79

2·51 3·75 5·36 7·91

9-20

12·10 15·74 20·10

18-87

REF. NO. 102

103 104

105

Secondary 24, 30, 48, 60 V REF.

NO

120

121 122

	V) 47 77	PRICE	D000	50P.I.V.	0.25	100P.I.V.	0.5
_	REF.	PRICE	POST	100P.I.V.	0.25	200P.I.V.	0.5
8	NO.	£	£	200P.I.V.	0.28	400P.I.V.	0.8
	112	2.04	0.61	600P.I.V.	0.30	600P.I.V.	0.7
	79	2.57	0.66	0001.1.7.	0.90	000F.I.V.	0.7
	3	3.91	0.72	Two Amp	Price	Six Amp	Price
	20	4.80	0.85				
				50P.I.V.	0.35	50P.I.V.	0.6
	21	5.58	0.85	100P.I.V.	0.40	100P.I.V.	0.70
	51	6.75	0.95	200P.I.V.	0.45	200P.I.V.	0.8
	117	7.52	0.97	400P.I.V.	0.50	400P.I.V.	0.9
	HA.	9-93	1.18	4001.1.7.	0.30	400F.I.V.	0.91
				Add 25%	VAT on	all prices	
	89	10.27	1.18	Aug 20 /0	AVI OR	an prices.	

#### **BRIDGE RECTIFIERS**

one Amp	rrice	rouramp	Price	
50P.I.V.	0.25	100P.I.V.	0.55	
100P.I.V.	0.25	200P.I.V.	0.59	
200P.I.V.	0.28	400P.I.V.	0.65	
300P.I.V.	0.30	600P.I.V.	0.75	
Two Amp	Price	Six Amp	Price	
50P.I.V.	0.35	50P.I.V.	0.65	
100P.I.V.	0.40	100P.I.V.	0.70	
.V.1.4002	0.45	200P.I.V.	0.80	
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0-100 mA 0-500 mA 0-1 Amp	0·5 0·5 0·5	0-100 mA 0-500 mA 0-1 Amp	0·5 0·5 0·5		
0-2 Amp 0-25 Volt	0·5 15K	0-2 Amp 0-25 Volt	0-5 15 K 50 K		
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Vu meters are complete with detectors. Modern wide view. Price 2" £3:20 Post 10p. Price 4" £4:00 Post 10p. VAT 25%. Lamps 95p per set. Plus 8% VAT.

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ч	AF114	24	BC108	10	BC153° 1	18	BC208A* 11	BC309B*	16	BD138*	47	ı
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u	AF186	50	BC119	28		16	BC238A* 15	BC557	9	BF159*	26	ı
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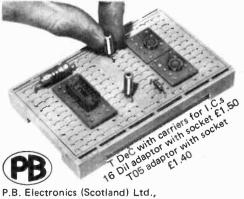


\*\*Components: 4-Octave keyboard C-C £15-50, 5-Octave keyboard C-C and F-F £20-00. Top octave tone generator, complete with external tuning capacitor, GU500, £12-95. Top octave tone generator and divider unit complete with external tuning capacitor, GD500 £50-00. Construction Manual for Portable Organ, using discrete components £2-25. Catalogue 60p.

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Organ Centre: 12, Brett Rd., Hackney, London E8 1JP. 01-986 8455 Component Shops: 8, Putney Bridge Rd., London SW18 1H U, 01-870 4949. 401/42a, Dalston Lane, Hackney, London E8 2AZ, 01-249 5624. All prices are exclusive of VAT.





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FOR SPEAKERS AT FANTASTIC

This compact Tuner Amplifier gives you tull medium wave and V.H.F. coverage and FM stereo. With inputs for your turntable and tape recorder, It has rotary tuning, Volume, Balance, Bass and Treble controls and push

button selection switches for Phono/tape FM Stereo, FM mono. Medium wave and A.F.C. has built-in steren heacon and switched headphone socket. **Technical Specifications** 15 transistors, 11

diodes; integrated circuit.



Power output 8 watts. Size of tuner amplifier: 4" x 10" x 151" approx. Finished in selected rosewood

£29.00 + p & p £1.50 veneer with brushed aluminium front panel and matching controls

As above but with a BSR C123 Turntable in matching teak veneered plinth and a pair of £39.00 + p & p 'Compact' easy to build speakers (see opp. panel)



MP 60 Type (illustrated)	£16.00
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C141 (not illustrated)	£12.00
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Auto, with Stereo Crystal Cartridge	p & p £1 ·50
All plinths finished in matching	Teak vencer.

EASY BUILD SPEAKER KIT 🎤 A compact bookshelf speaker system giving a high electro accoustic efficiency for the low powered amplifier

The professional finish can be obtained with the minimum of tools, the infinite baffle type enclosures come ready mitred and professionally finished, simply apply glue, fold up around baffle board, and fix together with masking tape till glue dries.

The cabinet measures 12"x9"x5" deep approx finished in simulated teak, incorporating a quality 7"x4" elliptical speaker, power handling 4 watts, flux density 30,000 maxwells, impedance 8-15 ohms nominal, voice coil dia 3" magnet size 2%" approx.



pair inclusive.P & P £1.70

#### **EASY TO BUILD SPEAKER KITS**

These superb simulated teak-finished speaker kits have been specially designed by RT-VC for the cost-conscious hi-fi enthusiast who wants top quality speakers but

doesn't want to spend the earth. Built to EMI's exacting specification, these new RT-VC speaker kits (350 type kit) incurporate 13"  $\times$  8" woofer,  $3\frac{1}{4}$ " tweeter and matching crossover.

Easily put together with just a few basic tools.

Specification (each speaker): Impedance 8 ohms. Power handling 15 watts RMS (30 watts peak). Response 20–20,000 Hz. Size 20" × 11" × 9½" approx. Comparable built units (EMI LE3) sold elsewhere for over £45 pair

£22.00 pair complete +£5.20 p & p.

Complete with crossover Components and circuit diagram





### **SPEAKERS**

15" 25 watts **£19.00** 

12" 20 watts £14.00



#### EMI 350 KIT £7.25 +£1.20 0 & 0.

Complete with crossover Components and circuit diagram

System consists of a 13" × approx. woofer with a 3" tweeter, crossover components and circuit diagram. Frequency response: 20 Hz to 20 KHz. Power handling 15 watts RMS into 8 ohms. (Peak 30 watts.)

#### System IA £69.00 VISCOUNT IV STEREO SYSTEM

new 20+20 watt Stereo Amplifier incorporating the latest silicon transistor solid state circuitry, the RT-VC VISCOUNT IV gives you a powerful 20 watts RMS per channel into 8 ohms. Superb teak-finished cabinet, with anodised fascia to harmonise with any decor. Polished trim and knobs.

The VISCOUNT IV has a comprehensive range of controls - volume, bass, treble, balance, mono/stereo, mode selector, and scratch filter.

Front panel socket for stereo headphones. And a host of sockets at the rear — for left and right

Speakers, tage recorder, auxiliary, tuner, disc and microphone.

SPECIFICATION: 20 watts RMS per channel 40 watts peak. Suitable 8-15 ohms speakers. Total distortion # 10 watts better than 0.2%. Six switched inputs. 1. Magnetic P.U. – 3 millivolts # 47 K ohms (R.I.A.A.). 2. Crystal/ceramic P.U. – 50 millivolts # 50 K ohms (R.I.A.A.). 3, 4, 6. Tape Tuner, Aux. — 140 millivolts # 50 K ohms (flat frequency response). 5. Microphone — 3 millivolts # 50 K ohms (flat frequency response).
CONTROLS: Push button ON/OFF, stereo/mono, scratch filter, 6 position rotary selector. Individual

rotary controls for freble, bass, balance and volume. Headphone socket, tape out socket. Aux mains output. Frequency response: 25 Hz to 25 KHz e full rated output. Signal to noise ratio: better than -50 dB on all inputs. Tone control range: Bass ± 15 dB = 50 Hz. Treble ± 12 dB = 10 KHz. Power requirements: 200-250V A C. mains # 60 watts. Approx. size: 15\frac{1}{2}" \times 3" \times 10".

MP60 type deck with magnetic cartridge, de luxe plinth and cover. Two Duo Type Ha matched speakers — Enclosure size approx.  $19\frac{1}{4}^{\circ} \times 10\frac{1}{4}^{\circ} \times 7\frac{1}{4}^{\circ}$  in simulated teak. Drive unit 13"  $\times$  8" with 3" tweeter 15 watts handling, 30 watts peak. Complete System with these speakers **£69.00**  $\pm$  £6.50 p.8 p.

System 2. £85.00

Viscount IV amplifier (As System 1a) MP60 type deck (As System 1a) Two Duo Type III matched speakers

Enclosure size approx. 27" × 13" 113". Finished in teak simulate Drive units 13" × 8" bass driver, and two 3" (approx.) tweeters. 20 walts RMS, 8 ohms frequency range — 20 Hz to 18.000 Hz.

Complete System with these peakers £85.00 +£7.60 p & p PRICES: SYSTEM to Viscount IV Rt03

£27.50 + £1.90 p & p amolitier 2 Duo Type lia speakers £30.00 + £6.50 p & p.

MP60 type deck with Mag. cartridge de luxe plinth £22.00 + £3 30 p& p and cover Total if purchased separately: £79.50

Available complete for only: £69 00 +£6.50 p & p.

PRICES: SYSTEM 2

Viscount IV R103 amplifier £27.50 + £1.90 p & p 2 Duo Type III speakers £46.00 + £7.50 p &

MP60 type deck with Mag. cartridge de luxe plinth and cover f22 00 - f3 30 o 8 o Total if purchased

separately: £95.50



#### PUSH BUTTON CAR RADIO KIT— NOW BUILD YOUR OWN £9.50 +£1.05 p. & p. THE TOURIST TT\*



NO SOLDERING REQUIRED

Easy to assemble construction kit comprising fully completed and tested printed circuit board on which no soldering is required. All connections are simple push fit type making for easy assembly. Fine tuning push button mechanism is fully built and tested to mate with printed circuit board.

TECHNICAL SPECIFICATION: (1) Output 4 watts RMS output. For 12 volt operation on negative or positive earth. (2) Integrated circuit output stage, pre-built three stage IF Module. Controls volume manual tuning and five push buttons for station selection, illuminated tuning scale covering full, medium and long wave bands.

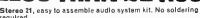
Size chassis 7" wide 2" high and 43" deep approx.

Speaker including baffle and fixing strip £2.00 +45p p & p. Car Aerial Recommended — fully retractable £1.60+40p p & p.

The Tourist I Kit For the experienced constructor. If you can solder on a printed circuit board you can build this model. Same technical specification as Tourist TT Price £8.20+£1.05 p & p.

The Tourist | Kit. same specification as Tourist TT complete with speakers, fixing + p & n kit and fully re-£10.50 £1.50 tractable aerial

# **ALITY SOUND FOR**



required.
The unit is finished in teak veneer and the acrylic top presents an unusually interesting variation on the modern deck plinth.

deck plinth. includes—BSR 3 speed deck, automatic, manual facilities together with stereo cartridge.
Two speakers with cabinets.
Amplifier module. Ready built with control panel, speaker leads and full, easy to follow assembly instructions.
Specifications—For the technically minded:

Input sensitivity 600mV. Aux. input sensitivity 120mV. Power output 2.7 watts per channel. Output Impedance 8-15 ohms. Stereo headphone socket with automatic speaker cutout. Provision for auxiliary inputs—radio, tepe, etc., and outputs for laping discs.

Overall Dimensions. Speakers approx 12"×9"×5" Complete deck and cover in closed position approx. 15½"×12"×

#### Complete only £23.20 +£3.00 p & p.

Extras if required, Optional Diamond Styli £1.60.
Specially selected pair of stereo headphones with individual level controls and padded earpieces to give optimum performance £5.80.

# DISCO AMPLIF



Reliant Mk IV Mono Amplifier, ideal for the small disco or house parties. Output 20 watts RMS into

8 ohms (suitable for 15 ohms).

Inputs \*4 electrically mixed inputs. \*3 individual mixing controls. \*Separate bass and treble controls. common to all 4 inputs. \*Mixer employing F.E.T. (Field Effect Transistors). \*Solid State circuitry. Attractive styling

INPUT SENSITIVITIES — Input — 1). Crystal mic. guitar or moving coil mic, 2 and 10mV. (Selector switch for desired sensitivity.) — Inputs -2), 3), 4). Medium output equipment — ceramic cartridge, tuner, tape recorder, organs, etc. — all 250mV sensitivity. AC Mains, 240V operation. Size approx: 121"×6"×31" £20.00 +£1.35 p & p.

#### **8 TRACK HOME CARTRIDGE PLAYER**



Elegant self selector push button player use with your stereo system. Compatible with Viscount IV system, Unisound module and the Stereo 21 Technical specification Mains input, 24NV Output sensitivity 125mV

#### $\Xi H$

As above but complete with build yourself Unisound Amplifier Kit (see opposite panel) + 2 'Compact' to build £25.00 speaker kits (see + p & p £2.00 opposite page)

### UR OWN STEREO AMP



For the man who wants to design his own stereo - here's your chance to start, with Unisound - pre-amp, power amplifier and control panel. No soldering - just simply screw together. 4 watts per channel into 8 ohms. Inputs: 120mV (for ceramic cartridge). The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion over the audio spectrum. 240V. AC only.

Also available with 2 speakers (7"x4") £10 + £1.75 p & p. £8.95 + £1.05 p & p. Also available with the 'Compact' (see opposite page) easy build speaker kit £13.50+ £2 p & ho

INCORPORATES: Pre-Amp with full mixing facilities, including switched input

#### RTABLE DISCO CONSOLE\*



All prices include VAT at current rates

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#### for mic with volume control, switched input for auxiliary with volume control, bass and treble controls, volume control and blend control for turntables. Two B.S.R. MP80 type single play professional series decks, fitted with crystal certridges. TECHNICAL SPECIFICATION:

Pre-amp — Output — 200mV. Auxiliary inputs — 200mV and 750mV into 1 meg. Mic input — 6mV into 100K. 240 volt operation. Turntables capacity — 7". 10" or 12" records. Rumble, wow and flutter Rumble. Reter. than — 356R. Wow. Rumble Better than -35dB, Wow Better than 0.2%. Flutter Better than D.06% (Gaumont kalee meter)

Finish — Satin black mainplate with black turntable mat inlaid with brushed aluminium trim. Tonearm and controls in black and brushed aluminium

#### Console size

Unit Closed - 17 7 × 13 7 × 8 7 (app.) Unit Open  $-35\frac{1}{4}$ "× $13\frac{1}{4}$ "× $4\frac{1}{4}$ " (app.) This disco console is ideally matched for the Reliant IV and Disco 50 or any other quality amplifier. The unit is fir ished in black PVC with

contrasting simulated teak edging, diamond spun control knobs with matching control panel

Yours for only £49.00 +£6.50 p & p.



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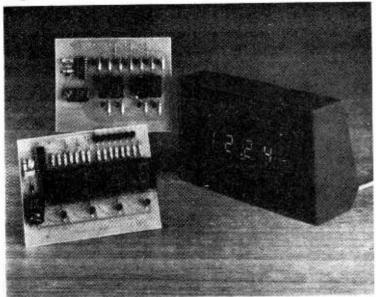
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AY-5-1224A 4 digit basic clock £3-50 MK 50253 4/6 digit alarm/snooze £5-50

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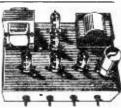
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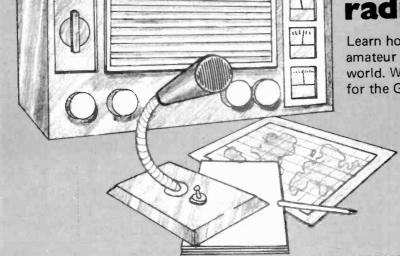
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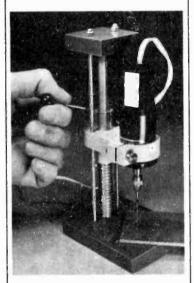
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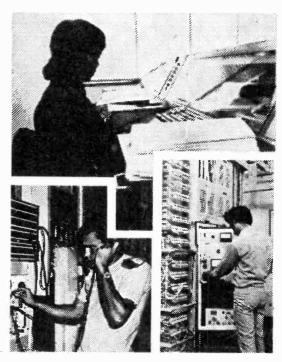
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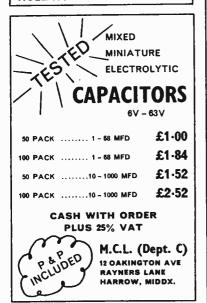
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TIP31A 8 8
TIP31B 70
TIP31B 70
TIP31C 84
TIP32A 88
TIP32B 80
TIP32B 80
TIP32C 94
TIP32C 95
TIP33C 95
TIP33C 130
TIP34A 115
TIP34B 167
TIP34B 167
TIP34B 167
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TIP34B 167
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2N4444

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6A500V 150p

3A400V 100p

10A500V 165p

MCR101

15

85 55

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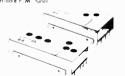
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