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TP14 20 OC71 germanium PNP audio pre amp tranTP15 20 OC81, germanium PNP audio output tran TP16 20 Sistor, white glass type. 0 ONP silicon TO-5 TP17 201 watt zen

TP18 20 2N 20 2N3707/8/9/10 ran TP19 100 Diodes, mixture of ded silicon of germanium, gold bonmany types, mark., a useful selection of Mulard OC45 transistors, I.F. amp. PNP TP20 10 Muslardium transistors, I.F. amp. PNP TP23 20 GFY50/1/2, $2 N 696 / 7,2 N 1613$, etc. NPN silicon 10.5 uncoded. COMPLEMENTARY TO PAKKA 24.
TP24 20 BFY64, 2N2904/5, etc., PNP silicon TO-5 TP30 uncoded COMPLEMENTARY to PAK TP23 P30 20 NPN silicon planar transistors, TO-18 TP31 20 PNP silicon planar transistors. TO-18 similar to BC 778 etc. uncoded.
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UT9 40 voitages. silicon planar transistors, of the 2N3707-11 range, low noise amp.
UT10 15 Power transistors, PNP germanium and NPN silicon, mostly TO-3 but some plastic dual in line. TO-5, experimenters pak unmarked, some definitely good but old
FOR FULL RANGES-SEE CATALOGUE
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| BRID. | $50 v^{*}$ | $100 v^{*}$ | $400 \mathrm{v}^{*}$ |
| :--- | :--- | :--- | :--- |
| 1 Amp | $25 \mathrm{p}^{*}$ | $35 \mathrm{p}^{*}$ | $45 \mathrm{p}^{*}$ |
| 2 amp | $35 p^{*}$ | $45 p^{*}$ | $55 p^{*}$ |
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Input impedance: 33Kohms

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79
3
20
21
51
117
88
89

| Ref. | Amps |  |  |  |
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| 226 | 60 | 30 | 17.67 | BR5 |

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103
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| Ref. |  |  | $0 \&$ | 4 |
| ---: | ---: | ---: | ---: | ---: |
| No. | Amps | 4 | $\&$ | 66 |
| 124 | 0.5 | 2.48 | 0.72 | 67 |
| 126 | 1.0 | 3.68 | 0.72 | 84 |
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| 121 | 8.0 | 15.75 | BRS | 5 |
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238
200 Volts
$3-0-3$
$\begin{array}{ll}12 \text { 1A, IA } 0-6,0-6 \\ 100 & 9.0-9\end{array}$ 235330,330 0-9, 0-9
207 500. 500 0-8-9, 0-8-9
$\begin{array}{llll}208 \\ 236 & 200, \\ 200 & 0-15, & 0-15\end{array}$ $\begin{array}{lllll}236 & 200, & 200 & 0-15, & 0-15 \\ 214 & 300, & 300 & 0-20 & 0-20\end{array}$ 221 700(DC) 20-12-0-12-20 $\begin{array}{lll}206 \text { IA, IA } & 0-15-20, & 0.15-20 \\ 203 & 500 . & 500 \\ 0.15-27, & 0-15-27\end{array}$ 204 IA, IA $0-15-27,0-15-27$ $\begin{array}{llll}\$ 112 \quad 500 & 12,15.20 .24,30\end{array}$ pep HIGH VOLTAGE $\begin{aligned} & \text { peb HIGH VOLTAG } \\ & p \text { Mains Isolating }\end{aligned}$


$$
\begin{aligned}
& \text { Ref VA Auto Taps } \\
& \begin{array}{lll}
\text { No } & \text { (Watts) } \\
113 & 20 & 0-115-210-240 \\
64 & 75 & 0-115 \ddot{-200-220-240}
\end{array} \\
& 4 \text { pe } \\
& \begin{array}{l}
.75 \\
.05 \\
.33
\end{array} \\
& \begin{array}{l}
0.51 \\
0.72 \\
0.72
\end{array}
\end{aligned}
$$

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CD4001 CD4002
CD4006 $\begin{array}{ll}\text { CD } \\ \text { CD4007 } & \text { 19pLLM381 } \\ \text { CD4008 } & 18 p L M 702 \mathrm{C}\end{array}$ CD4008
CD4009
CD 4010 CD4010
CD4011
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Frequencies forall

THE Regional Administrative LF/MF Broadcasting Conference (Regions 1 and 3) was held in Geneva last autumn and, among other things, considered the frequency allocations on those bands and it is good to report that the UK seems to have come out of the affray quite well. In Europe and those African and Asian countries bordering on the Mediterranean the use of these broadcasting bands is at present governed by the European Broadcasting Convention and the Copenhagen Plan, negotiated in 1948. Delegations from 103 countries took part in the conference, the UK delegation including representatives of the BBC, the IBA and the Home Office.
-The conference produced an Agreement and Plan which was signed by all but three of the delegations. Other member countries may accede later. The Plan is due to come into effect on 23 November 1978 and is intended to meet requirements for at least the following ten years. Charles Molloy has more to say about the frequency allocations in his Broadcast Bands column.

Let us hope that the radio amateurs will do as well in the World Administrative Radio Conference in 1979. It may seem strange to some that anybody should be worrying about a meeting that will not take place for some three and a half years. But a great deal of work must be done before the UK delegation can depart with a long list of the frequencies and other facilities that have been requested by every user of the radio spectrum in the UK. The radio amateur's case will, of course, be formulated by the Radio Society of Great Britain and every amateur here can be assured that they will do the best job possible in this respect.

Every amateur can help the cause by complying with his licence conditions, in particular by observing what should be normal good behaviour when on the air. There are those around who would be only too happy to snatch some of the amateur's frequencies in order to further their commercial interests. Bad behaviour on the air is playing straight into their hands.

It is a matter for regret that the number of licensed amateurs in the UK who belong to the RSGB is very much less than the ideal $100 \%$. The answer surely must lie in the organisation of the Society. The present set-up should be reviewed and the sooner the better. If the planners of the new National Exhibition Centre saw fit to place the Centre outside London then the RSGB should take up its Headquarters and do likewise!

## IPC MAGAZINES LTD. require two Technical Editors

PRACTICAL WIRELESS magazine invites applications from Radio, Audio and Electronic Engineers, preferably with writing experience to fill the post of Technical Editor. Applicants must have a working knowledge of electronics and communications techniques and a logical approach to circuit analysis to assess technical material for publication.
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## Solar Energy Walch

LASKYS have imported what is believed to be the world's first digital watch, incorporating a wrist-based calculator and powered by solar energy.

It is called the Uranus Time Computer and represents "the State of the Art" in digital integrated circuit technology.

The watch function displays, on command, hours, minutes, day of the month and seconds.

The calculator is four-function, ,$+ \times, \div,-$, machine with an 8digit display, full floating decimal and automatic stand.

The Time Computer contains a solar cell which draws its power from sunlight, daylight or artificial light. The batteries, therefore, never need replacing.

The heart of the Time Computer is a tiny encapsulated "chip" of silicon containing many thousands of transistors and other active electronic devices. (It is available to special order for $£ 295$ including VAT.)

The Uranus Time Computer is on special display at Laskys 481 Oxford Street store.

## Hold very fight please!

THE passengers on the top decks of 30 buses operated by the Scottish Bus Group will be getting music-while-theyride now. A firm called Sounds in Motion Ltd. have installed Pye auto-reversing cassette players to provide the music.

## Alexandra Palace

A$S$ an alternative to the usual Woburn Abbey Rally, the Radio Society of Great Britain is arranging to hold an exhibition at Alexandra Palace, North London, on 30 and 31 July and 1 August, 1976.

The site has very adequate car parking and outdoor facilities. Full catering exists within the building.

## Diary Dafes

March 8-14. Festival International du Son, Paris.
March 9-11. Electro-Optics/Laser International Conference and Exhibition, Metropole Convention Centre, Brighton.
March 9-11. Computermarket 76 Exhibition, Assembly Rooms, Edinburgh.
March 16-18. Computermarket 76 Exhibition, The Forum, Wythenshawe.
March 18-28. 23rd International Exhibition of Electronics, Nuclear Energy and Aerospace Technology, Rome.
March 23-25. CAD 76 Computer Aided Design Conference and Exhibition, Imperial College, London.
March 23-25. Computermarket 76 Exhibition, New Horticultural Hall, London.
March 24-26. Third Conference on Industrial Robot Technology and Sixth International Symposium on Industrial Robots, The University, Nottingham.
April 5-10. International Component Show, Paris.
April 13-15. All-Electronics Show, Grosvenor House, London.
April 26-30. IFSSEC 76--International Fire Security \& Safety Exhibition and Conference, Olympia, London.
April 27 to May 2. Hi-Fidelity 76 Exhibition, Heathrow Hotel, London Airport.
April 28 to May 6. Hanover Fair, Hanover.
May 3-7. IEA 76-International Instruments, Electronics and Automation Exhibition, National Exhibition Centre, Birmingham.
May 3.7. Electrex 76-Electrical Engineering Exhibition, National Exhibition Centre, Birmingham.
May 23-27. International Home Electronics and Domestic Appliance Exhibition (AMDEA/ BREMA), National Exhibition Centre, Birmingham.
May 28-31. Sound and Vision 76 TV and Audio Show, National Exhibition Centre, Birmingham.
June 8-11. Communications 76 Exhibition and Conference, Metropole Convention Centre, Brighton.

June 8-12. Internavex International Audio-visual Aids Exhibition, Olympia, London.
July 5-8. International Conference on Automobile Electronics (IEE), Savoy Place, London.
July 20-22. Conference on Video and Data Recording (IERE), The University, Birmingham.
Aug 24-26. Education and Communication Technology Exhibition, Holland Park School, London.
Sept 13-17. Micro 76 - International Symposium and Exhibition of Microscopes and Ancillary Equipment, Wembley.
Sept 13-19. 21st International Audio Festival and Fair, Olympia, London.
Sept 14-16. Eurocomp-European Computing Congress, Heathrow Hotel, London Airport.
Sept 20-24. IBC 76-International Broadcasing Convention, Grosvenor House, London.
Oct 19-21. Internepcon/UK Electronic Production Conference and Exhibition, Metropole Convention Centre, Brighton.
Gct 26-29. Microforum International Exhibition, Conference Centre, Wembley.
Nov 16-18. International Minicomputer Conference and Exhibition, West Centre Hotel, London.

## Man of Vision

THE University of Strathclyde recently mounted an exihibition, "Man of Vision", as a Jubilee tribute to John Logie Baird, 1888-1946, the inventor of television and a distiguished former student, who fifty years ago showed the world's first pictures by television. "Man of Vision" occupied the University's Collins Exhibition Hall in Rich. mond Street, Glasgow, from December 18, 1975 till January 30, 1976, and for the first time assembled under one roof a comprehensive display of Logie Baird's unique television and other equipment supported by personal, photographic, written and other memorabilia spanning his incredibly active lifetime.

## Bipolar Proms and Roms

INTEL have published a 36 -page booklet which provides technical information on 13 different ROMs and 24 different PROM types they manufacture. All the devices in the booklet are of Schottky bipolar construction and erasable PROMs and not included.

The booklet incorporates a data sheet for each device, and equivalents chart and gives details of PROM programming equipment.

For every Intel ROM there is a pin and performance compatible PROM, which means that no circuit changes have to be made when a project is finalised and information in PROM is committed to mask-programmed ROM.

All Intel PROMs employ polysilicon fuses which coat the surrounding area in a protective oxide layer when they are 'blown'. With polysilicon fuses there is no danger of a fuse 'growing back' as has happened before with conventional metal fuses.

Intel Corporation (UK) Ltd., Broadfield House, 4 Between Towns Road, Cowley, Oxford OX4 3NB.

## International Conference

THE Institute of Physics is organising a Conference to mark the 50th Anniversary of the Discovery of Electron Diffraction. The Conference will be held on 19-22 September 1977 at Imperial College, London. It is the intention of the organisers that all aspects of electron diffraction should be covered with emphasis in specific areas such as crystal struoture determination and surface structure studies. Plenary sessions will be introduced by review lectures from eminent personalities.

There will be an exhibition of equipment held concurrently with the Conference.

For further information please contact: The Meetings Office, The Institute of Physics, 47 Belgrave Square, London SWIX 8QX.


MANY amateur photographers like to play music while presenting a slide show. With the increased popularity of semi-automatic projectors it is fairly simple to synchronise the slide changes to a recorded oommentary or music. The conventional method of synchronisation involves recording tones on one track of the stereo tape machine with the commentary on the other. The commentary is played back in mono while the tones are used to close a relay connected to the slide projector remote control circuit.

## OPERATION

We shall first consider the general requirements for a tape-slide synchroniser before dealing with the details of the electronics. A tone is generated at a nominal frequency of say 18 kHz . This tone is generated continuously and so must be 'gated' to the output whenever the command to change slides is to be recorded. The signal is recorded for the same length of time no matter how brief the push of the slide change button. This necessitates that a form of monostable oscillator be incorporated.

The length of time that the playback relay is closed determines whether the slide projector changes forwards or backwards. Generally, closure for over one second causes the projector to change backwards to the previous slide. Therefore by using a record monostable it is possible to record reversing tones on the tape as well as forward. The detection of the 18 kHz tone from the tape playback (which includes fundamentals, high harmonics and hiss)
is a rather difficult task. A narrow bandwidth sensitive detector is needed. This function is provided by a 567 phase-locked loop IC. An additional feature of the synchroniser unit is that the monostable can be switched into an astable and so be used to change slides independently at preselected intervals for continuous unattended showing.

## CIRCUIT DESCRIPTION

The heart of the unit is ICl, the 567 PLL device. VR1 sets the VCO frequency at about 18 kHz . A square wave at the VCO frequency is available from a fairly low impedance at pin 5. The VCO is running continuously and is very stable. When recording, SI is used as the slide change button to record bursts of the 18 kHz tone on the tape. When VR2 is at minimum resistance, $S 2$, which is mechanically ganged to VR2, is open. The 555, IC2, then operates as a monostable with the output at pin 3 normally low. Closing Sl, earths pin 2 which is normally held to a slightly positive potential by R8. C10 then charges through R11 and D2 while the output at pin 3 goes high, closing the relay. After about 0.5 s , Cl0 will have charged to $2 / 3 \mathrm{Vcc}$ and the output together with pin 7 will go low. ClO discharges through R9 and VR2 (which is at minimum resistance) to wait the next 'change' command.

Keeping Sl closed for longer than the natural monostable period holds the output high until the button is released enabling a long burst of tome to be recorded for reverse slide changes etc. Diodes D4 and D3 prevent pin 3 of the 555 going negative


## components list


when driving the inductive load which can cause 'latch-up'. LED1 is used to show that a slide change signal has been generated or has been received when playing back.

The tone at pin 5 of the 567 is gated to the output by diode D1. The cathode is fixed at about half the supply voltage of the 567 , while the anode is normally at zero volts via R7 and R10. Thus the diode is normally reverse biased and cannot pass any signal. When the 555 switches, the relay on. pin 3 goes to almost the full supply voltage. The anode of D1 is thus pulled positive. C8 is the output
capacitor from the gate. C9 prevents the gabe switching too fast and so avoids the generation of clicks or thuds in the output.

VR3 and R12 form a potential divider for the gated tone, with VR3 setting the tone recording level. R13 and C12 form an integrator to remove some of the harmonics from the square wave and so give a sawtooth. The gated tone is mixed with the audio signal by C13 feeding into the junction of R15/R16 which form a potential divider for the left signal.


Circuit diagram of the complete unit, showing the two IC's. IC1 is a 567 phase-locked-loop device and IC2 is a 555 monolithic timing device. RL1 may be any 12 V 100mA relay with at least one pair of normally-open contacts.



The printed circuil board above is shown full size and accommodates all the components of the circuit. The hole spacings for RL1 are those for the RS Components 'continental' series type 40 relay, although with careful redrilling another suitable relay may be used.

## PLAYBACK DETECTION

Having got the signal on the tape, all that remains is to detect it on playback. The 567 PLL is a fairly sensitive device requiring only 20 mV of tone burst to start the PLL capture process. At small inputs (less than 200 mV ) the PLL bandwidth decreases with decreasing signal input. C5 sets the bandwidth to be $5 \%$ or $6 \%$ with a signal just above the detection threshold. C6 controls the response of the output stage while R1, C1 and C2 form a very simple band-pass filter centred about 18 kHz to reduce the possibility of the 567 detecting low frequency signals. Eiven pure signals below the VCO frequency can be detected if they are large enough, as the input stage is a clipper and so generates harmonics. The output of the 567 goes low for the duration of the tone, once the loop has locked (which takes typically a few $\mu$ S), and so fires the 555 in the same way as closing the 'change' switch S1.

Should a pulse be missed during playback due to dirty heads, S1 still functions and allows the projectionist to catch up with the sound track manually. In the absence of a playback connection, VR2 can be turned clockwise, $S 1$ closed and the 555 will operate as an astable of period set by VR2 over the range of $2 s$ to about 30 s . Thus the unit can be used to give repeated slide changes for demonstration and unattended showing. In the astable mode, C10 charges via R11 and D2 while pin 3 is high. When the voltage at pin 6 reaches $2 / 3$ of the supply voltage then the output, and pin 7 go low. Cl0 now discharges through VR2 and R9 until pin 2 falls below $1 / 3$ of the supply voltage. The output then goes high and the cycle repeats.

The power supply for the unit is very simple. The 555 timing is independent of the supply voltage as is the VCO in the 567. A stabilised supply there-
fore is not required. The supply to the 555 is about 12 V or 13 V while the supply to the 567 has to be limited to no more than 10 V . This is accomplished by R6 with C7 for decoupling.

## CONSTRUCTION

The slide synchroniser is a fairly complex unit and is fairly difficult to build other than by means of a printed panel. The layout is shown full size in Fig. 2. The connections to the relay will of course depend on the actual relay used. The board, with the layout marked in resist, is etched washed, and the resist removed with a solvent or paint stripper. Holes are then drilled with a number 60 drill (except those for VR1 and possibly C14 and RL1 which may need to be larger). The completed PCB in the prototype was mounted on 10 mm stand-offs on a ' U ' shaped chassis 150 mm wide and 205 mm deep. The front and back were bent up by 45 mm to form the front and rear panels.

The rear panel has three phono sockets mounted on it (two for left and right inputs, one for the playback signal input) as well as three holes for the mains lead, lead to the projector and a pair of screened leads terminated in phono plugs to connect to the tape recorder input. These holes are fitted with grommets to protect the cables. The three sockets are connected with screened cable with the shields earthed at the securing screw for the tape replay input socket. The electronics are also earthed at this point with a short lead from the point on the print to which the braiding of the Sl lead is connected. The braidings of the screened output leads are earthed at the terminal adjacent to C13. A mains earth is not used as this could introdurce earth loop problems.
continued on page 1038



THERE are in existence a considerable number of older valve tuners, such as Quad, Leak, Rogers, Armstrong, etc., which are still giving good service. However, stereo decoders for these tuners are no longer available and the writer has frequently been involved with their modification to stereo operation.

Generally the conversions have been "one-offs" with each situation being individually assessed, bearing in mind the availability of suitable decoders. Mullard have now released their LP1400 stereo decoder module, which is physically small and lends itself ideally to modifications of the type referred to, especially as it needs no alignment or other adjustments. The typical input impedance of the LP1400 is around $150 \mathrm{k} \Omega$ which is quite suitable for connection to either a ratio detector or Foster-Seeley discriminator. It must be remembered, however, that any de-emphasis network at the output of the discriminator must be removed.

## TRANSMISSION THEORY

A very brief discourse on the principles of stereo broadcasting would not be inappropriate at this point. Let us call the two stereo channels A and B. The FM transmitter is modulated in the normal way with a signal consisting of $A$ and $B$ added together ( $A+B$ ). Non-stereo receivers will produce this signal only, which, being the left- and right-hand channels added, provides normal mono reception. This arrangement ensures system compatibility. The audio bandwidth of this signal extends to 15 kHz .

In order to produce the stereo information, the A and B signals are subtracted, and used to modulate a sub-carrier at 38 kHz . This double sideband signad therefore consists of ( $\mathrm{A}-\mathrm{B}$ ) modulation. If the transmitted signal is monophonic, i.e. $A=B$, then $A-B=0$ and the 38 kHz information vanishes completely, since the subcarrier is suppressed in the absence of "difference signal" modulation.

In order to receive and decode the suppressed subcarrier information, it is necessary to re-insert the missing 38 kHz signal at the receiver. To emable this to be done simply, an unmodulated pilot tone at

19 kHz is transmitted. As will be seen from Fig.l, this signal slots in between the extremes of the sidebands of the sum and difference signals. The 19 kHz signal is doubled in the decoder to provide the missing 38 kHz subcarrier, which is then combined with its sidebands. The difference signal can then be demodulated.


W150

Fig. 1: Frequency spectrum of stereo Multiplex signal. The $(A+B)$ slgnal provides the normal mono reception.

In order to recover the original $A$ and $B$ signals, a simple algebraic manipulation is carried out. To obtain $A$, the $(A+B)$ and ( $A-B$ ) signals are added together: $(A+B)+(A-B)=2 A$. To obtain $B$, they are subtracted. $(A+B)-(A-B)=(A+B)+(B-A)$ $=2 \mathrm{~B}$.

Thus, we can recover the original $A$ and $B$ signals (the digit 2 represents a scaling factor). It will be realised that the presence or absence of the 19 kHz pilot determines whether the broadcast is stereo or mono. Usually a stereo beacon lamp is provided which lights up when the decoder is presented with a stereo signal. The foregoing description applies to the Zenith-GE multiplex FM stereo broadcast system as used in the UK and Europe.

## SIGNAL STRENGTH

The bandwidth spectrum of the stereo broadcast signal, Fig.1, is considerably wider than that employed for mono. Because of this, any noise present in the system will have a greater interfering effect. The noise in the upper modulation frequency area is much greater than in the lower region and in the process of decoding, this noise is shifted into the audio range and added to the output signal. In order to achieve an equivalent' signal-to-noise ratio, about five times the signal is needed on stereo,
compared to mono. Therefore it may be necessary to improve the aerial arrangements if stereo reception is to be entirely satisfactory.

Since the recovered $A$ and $B$ signals contain difference signal ( $A-B$ ) components in opposite phase, the noise in the two output channels will be predominantly of opposite phase. As a result, we can revert to mono by shorting the $A$ and $B$ outputs together after the decoder, when the stereo noise will cancel. In our application of the LP1400 module, this method works well, so that we can "mono" the


Fig. 2: Block diagram showing the basic circuits of a stereo decoder.
signal at the amplifier control unit or preamplifier without needing to employ the "stereo inhibit" input to the decoder. A block diagram, illustrating the action of the decoder is shown in Fig.2.

## TUNER MODS

Readers will appreciate that "pre-emphasis" of the higher modulating frequencies is applied at the FM transmitter. When de-emphasis is applied at the receiver, the system noise is attenuated in the same proportion. A mono tuner will include a de-emphasis network after the discriminator, and as this would effectively remove the 38 kHz difference signal, it is essential that the network be removed when the decoder is fitted. The reader is advised to look for components with $50 \mu$ s time-constant (the de-emphasis figure) e.g. $47 \mathrm{k} \Omega$ and $\operatorname{lnF}$, see Fig.3. When these components have been removed the discriminator


Fig. 3: A typical ratio detector circuit of a valve tuner. Note the removal of the de-emphasls components and the new take-off point.
output can be connected directly to the input of the decoder.

A complete circuit is shown in Fig.4. The low voltage supply is derived from the tuner's HT supply by the use of a resistor R4 and zener stabiliser D1. This simple approach is appropriate where only an HT rail and low voltage heater feed are available. Care should be taken to place the nesistor in a position where it can dissipate its heat adequately and feed the circuit from the point where the HT comes into the tuner. Capacitor C3 provides additional filtering of the module power supply.


Fig. 4 : For correct operatlon, the Mullard LP1400 module should be connected to a valve tuner, as shown above. The +12 V supply to the module is derived from the tuners HT supply via R4, and stabllised by D1 and C3.

## STEREO BEACON

The module is designed to feed a filament lamp as the stereo beacon. Unfortunately no suitable power supply for this is found in the average valve tumer, so a neon indicator is used instead. The filament lamp would normally connect between the supply rail and point 4 on the decoder. Upon reception of stereo, point 4 switches to earth, so turning the lamp on. The neon indicator operates as follows: Transistor $\operatorname{Trl}$ is turned on, in the absence of a stereo signal, by the base current feed from +12 V via R5 and R6 (point 4 is switched open within the decoder). As a result, $\operatorname{Tr} 1$ is bottomed and the whole HT voltage is dropped across R3. When a stereo signal is received, point 4 switches to earth and the absence of a source of base current stops Trl conducting. The collector voltage then rises until the striking voltage of N1 is reached. The neon lamp then lights, indicating stereo reception.

The neon circuit has the advantage that only one transistor is needed and one side is earthed. This makes the mounting easier, in that the cap can be
soldered to a bracket bolted to the chassis. The reader will have his own ideas on where to mount the neon, although a favourite place is at one end of the tuning dial.
The $10 \mathrm{k} \Omega 2$ resistors R1 and R2 are needed to prevent clipping at the output. Note that the decoder module has an overall gain of 6 dB under these conditions. If this is too much, R1 and R2 should be replaced by $10 \mathrm{k} \Omega$ potentiometers so that the levels can be adjusted as required. Note that Cl and C2 are essential to isolate the DC present at the output of the decoder assuming that the unit is to feed the typically high input impedance of a valve preamplifier.

## ADJUSTMENTS

In some cases it may be found that the stereo separation is unsatisfactory resulting from the tuner IF bandwidth being too narrow to accommodate all the sidebands of the difference signal. Careful stagger-tuning of the IF transformers will enable the bandwidth to be increased and so provide adequate stereo effect. The reader is cautioned NOT to attempt adjustments on the decoder board itself, since these will have been correctly carried out during manufacture.

When mounting the decoder in a tuner, make sure that it cannot move and accidently touch the HT supply! This can be an expensive mistake. The positioning should be such that adequate ventilation is provided to prevent overheating. If the unit is to be wired in using the stand-up leads, the print to the edge connector can be cut. This part of the board can then be drilled to accommodate a fixing bracket.
The Mullard LP1400 module can be obtained from Chromosonic Electronics, see ads.

## ISSUES WANTED

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. April 1972 issue of P.W. containing circuits of a transistor tester.-R. Murdoch, 5 Banks Road, Mt. Wellington, Auckland 6, New Zealand.

## AUTOMATIC SLIDE SYNCHRONISER-

continued from page 1035

## SETTING UP

With mains applied, a voltage check should show about 13 V or 14 V on pin 8 of the 555 and about 8 V on pin 4 of the 567 . With VR2 fully anticlockwise (S2 open), pushing S1 briefly should cause the relay to pull-in and the LED to light for about 0.5 s . Keeping S1 depressed should hold in the relay. With the relay held in, the output leads are connected to the input of the tape recorder. With R8 at minimum and the recorder left hand input control turned up, a deflection should be noted on the VU meter. Switching the monitor to 'source' enables one to hear the signal from which the tone burst is derived. With VR1 at maximum the tone should be clearly audible. Decreasing VR1 takes the tone up in frequency. VR1 should be set so that the tone is just out of the audible range. Sl is now released to cut off the tone.
The leads that previously carried the tape recorder input signal from the amplifier are now plugged in to the two phono sockets on the back of the synchroniser. The recorder level controls are set to give a normal recording level. Leaving the recorder level controls untouched the audio signal leads are unplugged from the back of the synchroniser. Sil is now pressed and VR3 adjusted to give a reading of slightly less than -20 VU on the left hand channel (about 6 or $7 \%$ of fsd).

A trial recording is now made of the tone at this level and played back with the left channel tape recorder output connected to the synchroniser tape replay input. Playback of a continuous tone should make the PLL lock-on and the LED light, as well as pulling in the relay. If the playback does not cause the loop to lock, VR3 will have to be reduced in value (assuming that the tape recorder output is turned up full). If this fails then it may well be that the recorder has dirty/magnetised heads or is incorrectly biased.
If all is well and the PLL picks out the replay tone then it is necessary to experiment with VR3 to ensure that there is a reasonable safety margin while on the other hand the recorded signal is not any higher in level than necessary. The tone is recorded at such a low level ( -20 VU ) primarily because the equalisation of the recording amplifier causes the gain to increase with frequency very quickly above 10 kHz . Hence the record amplifier is rather susceptible to overload at the frequency used.
When VR2 is turned away from its fully counter clockwise extreme the relay should switch on for 0.5 s repeating at intervals of between 2 s and about 30s.

## IN USE

The synchroniser is connected between the normal recorder input leads and the tape machine as detailed in the setting-up instructions. With the recorder input level controls set to produce a normal recording level (same position as when synchroniser was set up) every push of the 'change' button records the change tone. If the projector is coupled to the unit it is possible to run through the slide sequence while recording the tones. If a three head tape machine is used it is important that the tape replay input is not connected during recording, as the PLL will lock on to the replayed tones and produce a random series of tone bursts.

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# wiverit oncoro in Audio Amplifiers A. FOORD 

THE generation of total harmonic and intermodulation distortion in power amplifiers is well known. These types of non-linear distortion may be reduced by negative feedback. However it has been shown that a form of transient distortion can be produced when the open-loop frequency response of the power amplifier is less than the frequency response of the preamplifier. This article discusses why transient distortion is produced, and how it may be eliminated by careful design of the complete amplifier.

## BANDWIDTH LIMITATIONS

A complete audio amplifier can be divided into two main sections, pre-amplifier and power amplifier, as in Fig. 1. The preamplifier section may be subdivided for equalisation, tone controls, etc. Any feedback loops in the preamplifier will be over two, or at the most, three transistors.

However, the power amplifier will have a feedback loop enclosing three or more stages. In addition the small signal transistors in the preamplifier will have a much greater gain-bandwidth product than the higher power transistors used in the power amplifier. These factors usually result in the power amplifier determining the frequency response and distortion of the complete amplifier. Typically the power amplifier open-loop frequency ${ }_{3}$ response without feedback, may be as low as 1 kHz , even though its closedloop frequency response with feedback, may be over 20 kHz .

## NEGATIVE FEEDBACK

Before these topics can be discussed in any detail it is essential to understand the basic properties of a feedback amplifier, Fig. 2. The open-loop gain of
an amplifier, $-A$, is the gain with the feedback loop disconnected. The minus sign indicates that the amplifier inverts. The amount of signal fed back is less than unity and $B$ is called the feedback ratio. The closed-loop gain is the overall gain when the feedback path is closed and is given by:-

$$
\text { Closed loop gain }=G=\frac{V O}{V 1}=-\frac{A}{1+A B} \text { times }
$$

For example, if the gain without feedback is 100 times, and the feedback ratio is $0 \cdot 1$, then the closed loop gain is:

$$
G=-\frac{100}{1+(100 \times 0 \cdot 1)}=-\frac{100}{11}=-9 \cdot 09 \text { times. }
$$

This illustrates the very important point that the gain with feedback is approximately $1 / B$, when the product AB is much greater than unity, i.e. $\mathrm{G} \bumpeq$ $-1 / B$, if $A B>1$. In this example the overall gain is REDUCED by a factor of approximately ten times, while the bandwidth is INCREASED by the same factor.

## NON-LINEAR DISTORTION

Conventional non-linear distortion arises because of the non-linearities of the input/output transfer characteristics which occur in all physical systems. The distortion produced by a given non-linearity depends on its shape and the nature of the signals. For example, a transfer characteristic such as Fig. 3(a) would cause no distortion of any sinewave having a peak value less than unity, whereas larger sinewaves would be severely distorted. However the transfer characteristic of Fig. 3(b) would severely distort music or small sinewaves, while larger sinewaves would scarcely be distorted at all.

Since musical signals are small most of the time




$$
\begin{equation*}
G=\frac{V O}{V 1}=-\frac{A}{1+A B}=-9.09 \text { times } \tag{W164}
\end{equation*}
$$

Fig. 2 : Properties of an amplifier to which negative feedback is applled
exceeding the RMS value only $15 \%$ of the time, a harmonic distortion measurement at full amplifier power has little meaning. Certainly harmonic distortion measurements at lower levels are of much greater importance in detecting cross-over distortion. This can only be satisfactorily detected by using an amplitude of test signal which just spans the crossover region of $+x$ to $-x$ in Fig.3(b).

## REDUCTION OF NON-LINEAR DISTORTION

For reducing this type of distortion two approaches are usually used. Firstly the non-linearity is reduced by biasing Class $B$ output transistors with a small quiescent current of 30 mA or so. Secondly, negative feedback may be applied. A necessary and sufficient condition for low distortion is that the slope of the CLOSED-loop transfer characteristic is constant at all levels below the clipping level.
-This condition is satisfied if the OPEN-Ioop transfer characteristic has a constant slope, or by using sufficient negative feedback to make variations in the open loop characteristic unimportant. This means that the product AB must be much greater than unity. Therefore an open loop characteristic such as Fig. 3(b) would be intolerable, while those of Fig. 3 (c) and (d) are acceptable.

The preceeding paragraphs show how non-linear distortion is produced, and may be reduced by negative feedback. Most hi-fi amplifiers are satisfactory in this respect. However, when the open-loop frequency response of the power amplifier is less than the overall response of that portion of the transmission system preceding 'it, additional problems lead to transient distortion.

## TRANSIENT DISTORTION

Fundamentally, transient distortion arises from the poor overload characteristics of feedback amplifiers. The block diagram for a typical arrangement is shown in Fig. 4. The power amplifier is split into two parts with both a limiting and a time delay section shown diagramatically. The limiting section represents the initial stages of the power amplifier which will limit before the power amplifier's output stages. The time delay section represents the low bandwidth of the power transistors.

When an input signal, having a sufficient amplitude and a higher frequency than the power amplifier. open-loop cut-off frequency, is presented to the power amplifier input, overshoots in the internal loop drive voltage may be produced. This effect can best be understood by considering a step input. The overall negative feedback can only come into operation AFTER a time delay determined by the power stages. Therefore internal signals may overshoot momentarily. In a poor amplifier this may be several hundred times greater than the nominal value of this voltage. Consequently overshoots may be clipped in the amplifier driver stages if the overload margin is insufficient. This will produce temporary $100 \%$ intermodulation bursts. Since audio signals have their maximum slopes around the zero signal level these distortion bursts usually occur in this region. The audible effects resemble high frequency cross-over distortion and create a 'metallic' sound.

## TYPICAL OVERSHOOT LEVELS

A complete theoretical analysis is complex, and would depend on both the preamplifier and power amplifier characteristics, but some results are given


Fig. 3: Transfer characteristic (a) causes clipping, (b) would result in cross-over distortion, (c) is unsymmetrical but acceptable whilst (d) is non-linear but also acceptable.

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Fig. 5, shows the overshoot parameters for three different ratios of preamplifler to open loop power amplifier frequency responses.
Fig. 6: bottom, is the outline of a circuit for an amplifier with no transient inter modulation distortion.
(c) W167

|  | Overall Frequency Response | Preamp. <br> Frequency <br> Response | Open Loop <br> Power Amp. <br> Freq. Resp. | Closed Loop <br> Power Amp. <br> Freq. Resp. | Peak Output | Overshoot |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (a) <br> (b) <br> (c) | $\begin{aligned} & 22 \mathrm{kHz} \\ & 19 \cdot 6 \mathrm{kHz} \\ & 19 \cdot 9 \mathrm{kHz} \end{aligned}$ | 50 kHz <br> 20 kHz <br> 20 kHz | 2.5 kHz 10 kHz 20 kHz | 25 kHz 100 kHz 200 kHz | $\begin{aligned} & 5.27 \\ & 1.58 \\ & 1.00 \end{aligned}$ | $427 \%$ <br> 58\% None |

Note:-Peak output is output within the feedback loop, normalised to 1, point $X$ in Fig. 4.

in Fig. 5. For this example the feedback is taken as 20 dB and the overall frequency response kept at about 20 kHz . In (a) the power amplifier has a closedloop bandwidth which is half that of the preamplifier, while its open-loop bandwidth is much less. The momentary overshoot within the feedback loop is $427 \%$ !

In (b) the power amplifier has a closed-loop bandwidth which is greater than the preamplifier, while its open-loop bandwidth is half that of the preamplifier. Here the overshoot within the feedback loop is $58 \%$. In (c) the open-loop bandwidth of the power amplifier is equal to that of the preamplifier, and there is no overshoot. The closed loop bandwidth of the power amplifier is now 200 kHz .

From these results we deduce the general rule that to avoid transient intermodulation distortion the OPEN-LOOP frequency response of the power amplifier should be equal to or greater than the preamplifier frequency response. This requires a good high frequency design with a low value of feedback. When only a moderate value of feedback is used the open loop linearity has to be excellent, because heavy overall feedback is not present to decrease distortion.

When the open-loop frequency response of the power amplifier is higher than the audible frequency range, even moderate overall feedback will give a power amplifier small signal response up to 1 MHz and the limiting of the frequency response to 20 kHz must be accomplished in the preamplifier.

## DESIGN APPROACH

A design criteria for ultimate quality requirements demands that some of the commonly used circuit 'tricks' are not employed. For example, bootstrapping and higher feedback for DC than for AC should not be used. A high DC feedback value can cause clipping effects which force DC level adjustment transients through the feedback loop every time the signal changes. If the feedback is the same for AC and DC a number of capacitors can also be eliminated.

The required high open-loop linearity is obtained by using heavy local feedback in each amplifier stage. This increases the open-loop bandwidth and minimises the amount of overall feedback needed to about 20 dB .

The output transistors should be used as emitter followers to increase their frequency response and improve linearity. They should be driven tfrom emitter followers in order to minimise the effects of non-linearity and to maximise their bandwidth.
A completely symmetrical design should be used, without bypass or bootstrap capacitors, to improve the amplifier clipping and overload characteristics and to increase linearity at high frequencies. All stages should operate in Class A except for the power transistors. These should operate in Class $A B$ with a high quiescent current, typically 300 mA , to totally eliminate cross-over distortion and asymmetrics in the critical low power region.

## CONCLUSIONS

A complete amplifier design along these lines might be similar to Fig. 6. This would have harmonic and intermodulation distortion levels which are comparable with the best designs, but, in addition, would have no transient intermodulation distortion and excellent phase characteristics over the audio band. Dw

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IF YOU build or service radios, particularly superhets, and do not possess a wobbulator then you are working under a severe handicap. A wobbulator is a signal generator whose frequency can be varied by applying an external voltage. In practice, the applied voltage is the timebase output of an oscilloscope, so that as the trace moves horizontally across the screen, the frequency of the signal generator changes. During the flyback period the frequency

## An inexpensiue <br> UOBBULLTOR


returns to its original value.
If the output of the wobbulator is connected to the input of an IF amplifier and the oscilloscope's vertical amplifier input applied to the detector, Fig. 1, the 'scope will display the frequency response curve of the IF amplifier. Adjustments to the IF tuned circuits may then be made and the results seen immediately.

The wobbulator to be described sweeps over a range of at least $\pm 80 \%$ of the centre frequency and for selective circuits a "divide by ten" and a continuous control allow $\pm 0.8 \%$ to be achieved. The principle output is a triangular wave which may be attenuated. A square wave output is included which is useful for working on harmonics at higher frequencies. The centre frequency may be varied from about 280 kHz to $1 \cdot 8 \mathrm{MHz}$ but this is easily adjusted if necessary. A poor impression may be gained of the linearity when using a very wide sweep range, but up to $40 \%$, far more than is needed for conventional alignment, it is very good. The main use of extremely wide sweeps is for finding spurious responses when linearity is not so important.


Fig. 1: Block diagram demonstrating the basic use of a Wobbulator.

## THE CIRCUIT

The circuit of the complete wobbulator is given in Fig. 2. Potential constructors will notice the absence of conventional transistor oscillators and coils which always seem to cause trouble. Instead an NE566Y IC


Fig. 2: Circuit diagram of the Wobbulator, showing detalls of the NE566 IC, and the two outputs giving both square and triangular waveforms. The sweep width control should read VR2.
function generator has been used, which has other advantages as well. A very wide sweep range has been obtained plus very good frequency linearity at moderate deviations.

The circuitry up to Cl is an attenuator VR1/2 for the timebase input voltage which sets the sweep range. Tr 1 and Tr 2 buffer the voltage control input to the IC with VR3 setting the centre voltage. VR4 provides a frequency adjustment used for setting the ranges whilst C 3 and VCl constitute the main frequency control components.

The wobbulator runs from an external 12 V power supply which the author uses for most of his instrumentation, a technique which is recommended to save money! A suitable design for a stabiliser is given in Fig. 3.


Fig. 3: The above circuit shows a suitable design for a stabilised power supply for use with this Wobbulator.

## CONSTRUCTION

The prototype was built on a small piece of veroboard and housed in a "universal chassis" case. Later a PCB was devised and this is shown in Fig. 4. Con-


External photographs of the unit, showing the positioning of the sockets and switches

## $\star$ components list

```
Resistors
    R1 910\Omega
    R2 100\Omega
    R3 100k\Omega
    All & or tW 10%
    VR1 100k\Omega preset (PCB)
    VR2 10k\Omega linear pot.
    VR3 1M\Omega preset (PCB)
Capacitors
    C1 100\muF25V C4 2nF ceramic
    C2 1nF ceramic
    C3 390pF SM
    VC1 500pF variable capacitor
Semiconductors
    Tr1 BC108 Tr2 BC214L IC1 NE566V
Miscellaneous
    Casework, 'universal chassis' 6 < 4 < 2in. plus
    6 x 4in. plate (Home Radio) or box }6\times4\times2\textrm{in}.\mathrm{ (AB13).
    Switch S1, single pole changeover toggle. S2,
    single pole on-off toggle. Terminals, insulated (4).
    Coaxial sockets (2). Knobs. PCB from Readers
    PCB Service Ltd. see ad. page 1070
```

structors should find little difficulty in adapting the circuit to veroboard and pins. A piece of $0 \cdot 1$ in matrix is cut down to $4.2 \times 1 \cdot 3$ in thus giving $41 \times 12$ holes with the copper strips running lengthwise. Cuts are made in the copper strips as appropriate.

The components are then mounted as in Fig. 5. The IC should be soldered last of all but if desired use an IC holder or use socket pins instead.

Mark out and drill the case with the help of the photographs. No dimensions have been given as there is plenty of room and the optimum layout may depend on the components used. The circuit board is bolted to the base with two 6BA nuts and bolts with nuts as spacers. The co-ax sockets also required 6BA fixing. Complete the wiring and check it before switching on.

## SETTING UP

The process of setting up and testing consists largely of adjusting the three preset potentiometers and calibrating the main frequency control. Starting with VR3, this should be adjusted with no sweep input connected so that pin 5 of the IC is 11.5 V with a supply of 12 V . Next, connect the oscilloscope's tinebase output to the input terminal and starting with VRl at maximum resistance adjust it until the voltage at pin 5 is swept between the supply line of 12 V and about 9 V . If the oscilloscope is not calibrated vertically and hence cannot be used for this purpose, employ a very slow sweep and a voltmeter.
Lastly, adjust VR4 to achieve the desired frequency ranges $(280-465 \mathrm{kHz}$ and $400-1800 \mathrm{kHz}$ were used in the prototype) and calibrate the main frequency control against a radio or signal generator, with no sweep input. A simple test is to set up the generator with one of the outputs connected to the vertical input of the 'scope, connect the sweep input and set the wobbulator for maximum sweep tuning to its lowest frequency. Adjust the timebase so that a number of cycles are visible. These should vary in period across


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Fig. 4 and Fig. 5: The top drawing shows a foil side view of the pcb, while the lower gives the precise positioning of the various components. Both views are shown full size. Note. A link is required from the rotor of S1 to VR2.
the screen and reducing the sweep width should make the variation less.


Fig. 6: In order to avoid non-Ilnear displays at maximum sweep, the above AGC neutralising modification is recommended.

The only thing to remember about using the wobbulator is that at near maximum sweeps the display will be decidedly non-linear at the edges. Fig. I shows the conventional way of using the wobbulator to align IF amplifiers. When doing this it is advisable to turn off the AGC or otherwise neutralise it. A method of doing this in a conventional IF amplifier is shown in Fig. 6, the circuit being broken at point " $X$ " and the dotted connection being made to earth.

The conventional injection point is the base (grid, in valve receivers) of the mixer which prevents loading the first IF transformer. The 'scope input is connected to the point marked "audio" and the lowest sweep speed used that gives a flicker-free and viewable trace.

Adjustments may also be made to the alignment of RF and oscillator stages but beware of adjusting a tuned circuit to which the wobbulator is connected directly as the loading will be excessive. If, at any time, the output is too great even when fully attenuated, connect a capacitor of a few pF in series with the lead to the receiver.

Hands up if you ever sipped lemonade through a straw. Bet you did when you were little. Now hands up if you earn your living by sucking through a straw. Don't laugh, because that is exactly what one very brave young lady does. Her name is Margaret and she's a receptionist. She's also been paralysed from the neck down since 1956.

It seems impossible and yet, with the aid of electronics, Margaret is leading a very useful life and doing a full-time receptionist's job at a University. So how does it all work. Well, Margaret uses a kind of electronic straw-just like the one you (?) and 1 use to sip that lemonade through, only it's different if you see what I mean. Her straw has two tiny pressure sensors in it. One sensor responds to blowing while the other is trained to respond only to a suck or sip.

A VDU (visual display unit) is a feature and a list of available things, like telephone numbers etc. are thrown up on the cathode ray tube, At the side of the list of actions (or whatever) is a cursor and this travels down the list a line at a time with each puff in the straw. When the desired line is arrived at, Margaret simply sucks/sips and the computer-based system does the rest. A telephone number is dialled and Margaret can then speak to the person at the other end of the line. By selecting other instructions it is possible to select, say, a tape recorder facility for recording messages. Margaret can now handle a multiple-line business telephone system-all by herself.

Oh, yes, I nearly forgot, she types letters, too. The alphabet is simply called up on the VDU and the cursor "puffed" along to select the required letter or numeral. Print out of the letters is a teleprinter-type of keyboard which types out letters and numbers in response to electrical inputs. A voice terminal is the next step for her electronic helpers but this isn't "on-line" as yet. Please note the system is not available for general use and takes the form of an experiment.

## TIRED TYRES

Electronics in motor vehicles has long been a field of development. Transistor ignition is one such area. An interesting development is taking place in Germany, so I hear. This ingenious application allows the driver of a vehicle to know instantly when his tyres start to go down. In other words, his tyre pressure is constantly monitored-even when the vehicle is in motion!

Transmitting and receiving coils are mounted at each wheel suspension. The transmitting coil is fed with a 7 kHz signal. On each wheel rim is mounted a small coupling coil which, as each wheel rotates, passes some 10 mm from the two coils on the suspension. The small coupling coil on the wheel rim is connected to a tiny pressure sensing switch located in the tyre valve. While the tyre pressure remains above a predetermined minimum level, the small coupling coil will couple the 7 kHz signal from the transmitting coil to the receiving coil with each revolution of the wheel. However, if the pressure were to drop below the minimum level, then the pressure-sensing switch at the valve would open and the wheel rim coil would not couple any signal from transmitting coil to receiving coil as they passed. Thus no signal would be passed back to the control unit on the dash board and a warning would immediately be given to the driver. The company is reported to have said that it is ready to go into production with the system if sufficient demand is evident. Doubtless, motorists who are tyred of getting flat tyres will favour what amounts to an airraising innovation.

## TUBES, AGAIN

Just as I thought that the computer memory research front was going to be quiet for a while, so a group of Dutch workers have proved me wrong. They have come up with a new type of memory which is claimed to be cheaper than ferrite-core stores and offering greater density, too. The new memory relies on what is called the Phonon echoes effect. These "echoes" develop when powdered quartz is excited by high-frequency pulses. One important discovery is
that the echoes so recorded and stored can be read out a year later without any problems. A tiny glass tube, 1 cm in diameter and 1 cm in length is filled with quartz powder and the resultant capsule has a coil plus capacitor combination around it i.e., a tuned circuit. One of these little tubes has been found to store up to 100,000 bits of information. Pulses are applied in pairs and the highest frequency to date has been 80 MHz . Workers believe that up to 10 GHz is possible as a frequency for these pulses.

## OW!!

The ancient art of acupuncture has gained in popularity in recent years. Apparently the idea is to poke needles into the body at certain points and this makes you better. Now you wouldn't think that electronics could have anything to offer here because the actual mechanism i.e., the pin sticking is very simple. But no, you'd better believe it, electronic acupuncture has arrived. Of course it's claimed to be superior to the older techniques. It's more accurate, can be quicker and is more hygienic. First we do away with those needles and use a laser beam instead. The beam is completely sterile which can't be bad. A flexible light fibre probe is used to locate the acupuncture point accurately. Apparently the skin resistance at the exact point is slightly lower than the surrounding skin so the probe measures skin resistance at the point of contact. When the correct point is located, a helium-neon laser is persuaded to emit a one milliwatt blast of power and the beam may be continuous or pulsed. The pulses can be varied, too. Some 10 to 15 mm of skin tissue is penetrated by the laser and, claims one report, it doesn't hurt. I would have thought that one would feel a bit of a prick.

It will be very sad to see all those acupuncture needles going to waste as electronics advances. I wonder what the Chinese will do with them all? (No, prizes, no prizes.).
Cimbers


BY USING a rotatable ferrite rod serial, advan: tage can be talen of its direct onal propertiex either to obtain best reception of a station without needing to turn the receirer itsele, or to obtain a directional bearing from a ransmitter. The zeceiver describsd here is completely screered ez cept for the rotatable aerial, and uses a telescopie serial which can be trought into use if wanted. The latter is for "sense" determination, to remove the

Fig. 1: Froint end of the re:elver containing the sense, and ferrite aerials Binciswitching is acolevec b) means of S2-6. anc tuning by means of FC1/2. The MW band has beer spllt into rwo parts, Band: cevers $1500-1500 \mathrm{kHz}$ and Band 2 co0-1300 h/te. On LW Band 3 covers $1=0250$ kHz.
$180^{\circ}$ ambiguity which exists with the ferrite cod aerial alone.

The ferrite aerial has two maximum signal strength positions, with the rod at right angles to the direction of the transmitter; and two minimum
positions, with the rod in line with the transmitter. These positions are shown by a panel meter. In many circumstances, as with European or other stations, the approximate direction will be known. In other circumstances the correct direction may not be.known.

# PRACTICAL WIRELESS  

Fault-finding in radio and similar equipment is one of the fastest ways of learning all about electronics. Component suppliers catalogues are an invaluable source of information on the characteristics of components of all kinds and such knowledge is invaluable in locating a fault quickly from the observed symptoms. In this Guide Les LawryJohns, a very experienced service engineer, describes the methods of servicing that he has found so successful.

Lots of people start off with the intention of making a living out of servicing radio sets. There are several paths to take once the basic theory has been mastered, more or less. One can specialise in, say, car radios and other car entertainment gadgets, cassette players and the like, or perhaps TVs only. Those who work for a company probably stay in the trade but some who set out to be self-employed rarely stay the course. There are several reasons for this, the main one being economic.

It is extremely difficult to get an adequate return for the capital laid out on component stocks and test equipment if one is repairing domestic appliances, mainly because the time involved in properly servicing each item leaves little reward when the job is completed. Therefore a lot of servicing is done on a part-time basis or as a paying 'hobby' with the accent on the hobby aspect rather than on the paying!
We have to assume that the reader has a basic knowledge of electronics and some idea how radios and the like function. The chief requirement after this is patience and a genuine desire to do the job, and to do it properly.


## THE TOOLS

First the tools. A goodly selection of screwdrivers, among the smaller of which must be everybody's friend, the neon screwdriver. This little fellow deserves a chapter on his own, being an indicator, detective, fault tracer, a sure signaller of nearby radiated energy and a life saver. No less, but certainly more.

One must have wire cutters, and side cutters are more useful than top cutters. Pliers and tweezers of various types and sizes, files and spanners are essential and


## FAULT~FINDING GUIDE




Shown here is the Advance Electronics tow-cost dual-trace OS240 oscilloscope.
included in the latter should be the single-ended type with a handle, known as a nut spinner, in at least 6BA and 4BA sizes and with the close metric relatives. A comprehensive set of trimming tools, which can be purchased as a kit; at least two soldering irons, for delicate and heavy work. A reel of 18SWG ( 1.2 mm ) resin-cored solder and some means of removing solder, preferably desoldering braid which is copper braiding impregnated with resin flux. It draws the solder away from a heated joint allowing a component to be removed. Alternatively, some form of vacuum pump, possibly combined with a soldering iron.

A small torch which can be held in the mouth, if need be, and a magnifying glass are essential items whatever your age and eyesight! Next, the handmaiden of all electrical work, a decent multi-meter, preferably two. One should be a good quality meter for bench work, the other a smaller, less expensive, knock-about type for general use and back-up for use with the other, as one often wants to make two readings at the same time. Apart from this it often happens that the main meter is out of action for some reason, and at the most inconvenient time. Other instruments such as oscilloscopes, signal generators; bridges and the like can be regarded as highly desirable equipment to be purchased when funds allow.

## MULTIMETERS

The multi-meter should impose as little loading as possible on the circuit being tested otherwise the voltage present will be different when the meter is applied from what it is normally. A voltmeter is operated by current drawn from the circuit being tested and this current must be as small as possible. Most meters are marked on the front with their sensitivity and a figure of 20000 ohms-per-volt (OPV) should be the minimum requirement. It should also have some form of cut-out or overload protection. The man who hasn't taken a reading with the meter set to the wrong range hasn't yet been born!

As well as reading voltage, current and resistance the meter can also be used to apply tests to circuits and components since, when switched to the resistance range,
a negative voltage appears at the positive test probe and a positive one at the negative probe. This enables a check of the approximate characteristics of capacitors, transistors, diodes and the like to be made. After voltage readings, this facility is probably one of the most valuable assets of a multi-meter so we will spend a little time on this subject, later on. However, we must continue with our 'tools of the trade" requirements.

There are a great many aerosols (sprayers, squirters etc.) on the market at the present time, each of which has its own merits. Most engineers would select two, a contactcleaner lubricant, which does not attack plastics, for cleaning switches, volume controls and the like, and a cooling agent or freezer. The value of these two can hardly be exaggerated. Whilst the former has always been accepted as a must, the choice of the latter has been dictated by experience over the last few years. Large numbers of small components grouped on a board can present a problem when tracing intermittent faults or where any one of a number of transistors in, say, an audio stage can be responsible for upsetting the operation of the others. A judicious squirt of freezer has solved many such baffling problems and a hair drier has its uses too:

## STARTING

So here we are, with a few tools of the trade and prepared to do battle. However, it is one thing to identify a faulty component, when all you have to do then is to obtain a replacement, but all too often we can only suspect and it is essential then to make a substitution check. Resistors can usually be tested and passed as fit or thrown out, but capacitors present a different problem. They can leak, partially or completely dry up, become open circuit or


The new AVO Electronic Multlmeter EM272 provides 39 ranges in spite of the simplicity of its appearance.


In use here is the Advance DMM7 digital multimeter, a new $3 \frac{1}{2}$-digit 5-function instrument.
develop a short sometimes accompanied by heat. Therefore a goodly number of capacitors of various types, capacity and voltage rating must be held in stock.

Voltage rating is important from two aspects. Obviously a capacitor rated at, say, 12 V would not be put ecross a 25 V line as the voltage rating marked on the component must not be exceeded, but it is often thought that a capacitor marked, say, 100 V can be used in any circuit where the voltage is less than this. Usually this is quite true, but there are exceptions. If the capacitor is electrolytic it requires a certain polarising voltage for it to work efficiently. In some circuits the voltage is very low, say about 4 V , and a replacement in such a position should be rated at not much more than 6 V or whatever voltage is marked on the defective item.

Diodes are another item which can be checked with a meter, within limits, and a few of the more common types in stock will usually suffice. Bridge rectifiers are commonly used in mains powered equipment and they often give trouble. One is well advised to keep a couple to hand and two types usually suffice, the BY164 for operation up to 40 V and the BY176 for higher voltages. Four silicon diodes


A new product from Advance is the $\sqrt{4}$ signal generator, with sine or square wave outputs.
can be used in place of a bridge and indeed this type of supply will often be found but where a single block bridge is encountered it is often inconvenient to fit four diodes in its place.

The choice of separate power diodes is large but one cannot go far wrong with a few BY142 (BY127 with a smaller package). Voltage regulator diodes (zeners) appear in all types of equipment and one would be very hard put to try to anticipate what is going to be required if many makes and models of radio are tackled. It is no hardship to order the right components at the right time, if one knows in advance the type of equipment which is to be serviced, but if this is not known the stock list could be endless.

The same can be said about transistors and the position is more complicated as the age of the set to be serviced usually dictates the type of device used. The following is a list of transistors which ought to be kept in stock for the general servicing of audio equipment, radios, car radios etc.

|  |  |  |  |
| :--- | :--- | :--- | :--- |
| AF115 | AC187K | BC131 | BC186 |
| AF117 | AC188K | BC132 | BC194 |
| AC127 | AD149 | BC147 | BC195 |
| AC128 | AD161 | BC149 | BC196 |
| AC187 | AD162 | BC157 | BFX88 |
| AC188 | BC109 | BC159 | BFY50 |

From this modest list one can often find a suitable replacement for the more difficult-to-obtain types and some which are not marked. The latter present a minor problem but this is about all

## IDENTIFYING TRANSISTORS

Most transistors have only three leadouts, these being emitter, base and collector. They will belong to one of two basic constructions, NPN (neg-pos-neg) or PNP (pos-neg-pos), so this is the first check to make and it is a very easy one using the ordinary multi-meter. It must be appreciated that when the meter is switched to the 'ohms' range it is battery operated and that the positive ( + ), or red, probe will be on the negative side of the battery with the negative ( - ), or black, probe at a positive potential. If the red probe of the meter is applied to the base of a PNP transistor a low reading will be shown when the black probe is touched to the collector or the emitter. On the 'ohms' scale this will look like something between $10 \Omega$ and $50 \Omega$ depending upon the transistor type and the meter.
If only one reading can be obtained note to which leadout the black probe is applied and assume this is the base of an NPN transistor, when the red probe can be applied to the other two to obtain the low reading. If there is no low reading, the red probe should be applied to another leadout on the assumption that the device is a PNP after all, but that you didn't get the base lead in the first place.
Now that the base has been identified and the device established as a PNP or an NPN, it is necessary to identify the collector and the emitter, remembering that we are supposedly dealing with a good transistor and not one with a short or open circuit.
Switch the meter to the high resistance range, and, leaving the base free, connect the probes to the other two.

## FAULT~FINDING GUIDE




Base negative
Collector $\left.\begin{array}{l}\text { Collector } \\ \text { or } \\ \text { emitter }\end{array}\right\}$ Low R emitter

If the transistor is an NPN and a high resistance is recorded, the negative (black) lead is connected to the collector and the positive (red) lead to the emitter. Reversing the probes should then give a low reading.

If the transistor is a PNP (we have already establighed this in the first test, so don't get confused) the readings will be reversed, high reading positive to collector, lower reading negative to collector. A further test can be made on the transistor. Connect as above, negative lead to collector, positive to emitter, if NPN, (reverse for PNP) and note the high reading. Place a finger on the collector and base leads and the reading should drop, showing that the transistor is "turned on". The actual reading will depend upon the current gain of the transistor and the resistance of the skin of the finger. What good is this, you may ask? Well, it does enable you to make a comparison check against a known transistor and so, very roughly, identify the current gain.

Diodes can be checked in a similar way but of course there are only two connections to make. Positive lead to

cathode ( + ) gives a low reading, while negative lead to cathode gives a high reading. A little practice with known good thansistors and diodes will show the readings which can be expected. These tests can be used on components in circuit provided the associated circuitry is taken into consideration, particularly where transistors are inter-connected, say output transistors with drivers across them, etc.

## COMPONENT CHECKS

Capacitors can be checked roughly with an ohmmeter switched to the highest resistance range. When the test leads are first applied to a discharged capacitor, the applied voltage will cause the charging current to deflect the meter sharply according to the capacity, the reading going back towards infinity as the capacitor is charged. If the capacitor is leaky, current will continue to flow and a reading


Another useful bench instrument is the Ad'rance 'Alpha' digital multimeter, being used here to make resistance checks on a circult board.
will be maintained. This is to be expected with high value electrolytics as the meter voltage is insufficient to complete the sealing process. Once again a little practice will show what is to be expected. Very little indication, except leakage, will be shown on capacitors less than say 50 nF but the tests are more valuable as the capacity increases. Don't forget, electrolytics require the negative probe to be applied to the positive tag of the electrolytic in order to get the right polarity for the charging voltage.


The Dino is the latest electronic multimeter from Chinaglia, $200 \mathrm{k} \Omega$ OPV on DC and 20k $\Omega$ OPV on AC.

Inductors, transformers and the like can be checked for continuity and resistance. The presence of shorted turns can only be assumed if the resistance reading is much lower than that specified.

When a resistor is suspected of being faulty, first look at its appearance. If the colours are clear and bright and the resistor has a fairly low value the chances are that it will be serviceable. If it has a higher value, say over $100 \mathrm{k} \Omega$, it could look right but the value may have increased, particularly if used in a position where it is passing a fair current. Checking depends upon the circuitry, for if it is associated with other resistors or transistors, a direct reading may be of little use and one end may have to be lifted by unsoldering in order to check it out of circuit.

If the colours are not clear or if the resistor presents a well-worn look, replace it, even if it reads right, in order to save probable trouble later. This particularly applies to the low value resistors associated with output transistors usually about $2 \Omega$ or so). If a high value resistor is suspected it can often be checked with the receiver switched on by connecting a voltmeter across it, on a high range. The recorded voltage drop being of less importance than the effect of the resistance of the meter which shunts the suspect resistor and thus, to an extent, takes its place. Care must be exercised when using this dodge in preamplifier stages where the meter resistance can upset the base current of a transistor if the associated resistor values are high.

## SHORT CUTS

There are no subsțitutes for routine tests, checking supply and stage voltages in logical sequence, injecting test signals to identify the working and the faulty stages. To do this one must be able to think 'electrically', and while this comes easy to some, it is hard work for others and only comes with time. Following certain guide lines the fault will always reveal itself provided enough time is spent on the problem. However, as one becomes used to the type of equipment being serviced a pattern usually emerges which enables a short cut to be made across the routine tests and thus head straight for the source of the trouble, using eyes and ears and sometimes the sense of smell and of touch. A dry joint (one which has not been properly soldered in the first place) can often be seen, rather than traced, by its discoloured and 'powdery' appearance.
Sound distortion can be caused by many things but after a while the ears will unerringly identify the sound of a rubbing speech coil in a loudspeaker as opposed to a similar noise caused, say, by the output transistors being mismatched. The smell of some types of overloaded or faulty rectifiers immediately proclaims a defective one, whilst touching a hot transistor, apart from being painful, can cool it down and allow it to begin working for a brief period.

Some makes of printed circuit board are more liable to develop hairline cracks than others. Some types of capacitor are far more likely to fail than others. Indeed, we could go so far as to say that where certain types of capacitor are found fitted, we do not bother to check them since they are so very rarely at fault, whilst others are the first suspects and pounced on immediately. Some transistor types are more likely to fail than others. This sort of fault can be repeated over and over again and, whilst it makes life


The Model 8 Mk 5 general purpose multi-range meter is the latest in a very long llne of multimeters from AVO. An early version of the meter appears in the background.

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Smallest of the Chinaglia range is the Cito multimeter but it still manages to provide 14 ranges on six coloured scales.
a trifle easier for the experienced, the inexperienced person has no option but to employ routine tests and finally arrive at the same conclusion, having spent a considerable amount of time in the process. If in doubt, ask someone who knows and thus profit from their experience.

## PRACTICAL ASPECTS

We gave a short list of the items needed to service the simplest of appliances but there are others to consider. A circuit with a layout diagram is an absolute must if the appliance is not well known. Fortunately, in addition to the maker's service information which is the best source of reference, there are volumes of service data in book form available which condense this information, so that it is possible to build up a library of information which is readily to hand and indexed.

Not all appliances are complete when they are received for repair. For example, a car radio will need a 12 V supply and most likely a loudspeaker. This is not too bad since most car radios use a $3 \Omega$ speaker, although more recent imports use $8 \Omega$ in some cases. However, it is often inconvenient to remove sited loudspeakers when a unit audio goes wrong, assuming that the speakers are not at fault, so it is necessary to have suitable speakers for test purposes. These are frequently $8 \Omega$, but not always, by any means. So be prepared to add series resistors to make up the required loading or keep a goodly selection of loudspeakers!

Before we drop this subject, one further point. There are always power amplifiers requiring repair. If you do


The Chinaglia transistor tester provides a Good-?-Bad indicalion plus leakage and $\mathcal{B}$, using internal batteries. Test leads can be fitted for checking external circuits or devices.


Service sheets provide information for fault-finding and the alignment of receivers. This particular layout shows the location of the components which may require adjustment when aligning the Marconi 4173 MW and LW receiver.

# FAULT~FINDING GUIDE 



The Marconi 4184 receiver also incorporates the VHF(FM) range so the number of adjustments needed for a complete allgnment is increased, as shown here.
take on one of these and repair it, have a care for your test loudspeaker. To touch the input socket with the volume control well up is to ask the amplifier to deliver full power into what may be a small loudspeaker, the probable result being a wisp of smoke from the speech coil which, if it survives intact, will never be the same shape again!

## OTHER TEST GEAR

Whilst our multimeter enables us to check voltages, measure current and take resistance readings, plus a few other things, no serious service work can be carried out without the aid of other instruments, the first of which is a signal generator. This enables us to inject signals of known frequency and level and thus to check the alignment and response of the equipment under test.

Let us take an average radio set. Considering the medium wave band only, signals from say 600 kHz to 1.5 MHz have to be selected and amplified. Since there are several stages of amplification, it is clearly not convenient to tune each stage to each frequency separately. What is required is for all signals to be converted to a common frequency which can then be fixed tuned. This is known as
the IF, or intermediate frequency, which for AM reception is usually fixed at about 470 kHz . Some imported radios have a lower IF, 455 kHz , which is the reason for the annoying whistle sometimes experienced adjacent to stations operating around 908 kHz . Therefore the generator will have to cover this band of frequencies plus all RF frequencies likely to be covered by the receiver.
This will enable us to check the tuning of the aerial coils, the oscillator and the IFs. If these coil cores and trimmers are not accurately adjusted the receiver cannot give of its best. The signal generator provides a means of doing this, and much more, since we can now inject signals into various stages of the receiver and thus locate the stage which is not functioning correctly. The wobbulators is a variation of the signal generator, which we will not consider here, but which is essential for many kinds of accurate alignment.
An oscilloscope enables us to "see" into a circuit. The signals are amplified and appear as a trace on a screen so that the effect of each stage can be seen and adjusted, if necessary, to the required amplitude or waveform. It therefore enables us to see where signals are lost or become distorted.

The Ferrograph Test Set RTS2 from Wayne Kerr combines many of the facilities needed for checking the performance of recorders, amplifiers and other audio equipment. Included are an audio oscillator, distortion meter and AF millivoltmeter


## FAULT~FINDING GUIDE



## ALIGNMENT

Having mentioned these two valuable aids, let us immediately correct any misconception. In everyday radio repairs they are rarely needed. If the IF alignment has not been disturbed, do not touch it! If it has, it probably needs only a "tweek" to restore normal reception. Note which core or trimmer has been disturbed (wax or seal broken) and bring this, or them, into alignment with the other circuits. If the oscillator and aerial trimmers have been altered, switch to medium waves, set dial to about 1200 kHz ( 250 m ) and set the oscillator trimmer to bring in Radio 1 (or any other frequency which is known to correspond to a particular station at this end of the dial) reset to around 1500 kHz and trim the aerial trimmer. Retune to the lower end of the dial, to say Radio 3 on 647 kHz , (this is the low end from a frequency point of view) with the core of the oscillator coil, appreciating the fact that this is going to upset the previous trimmer setting at the HF end which will have to be done again. Do this a couple of times until satisfactory tracking is obtained.
If a ferrite rod aerial is used adjust the medium wave winding on the rod for best reception on about 650 kHz finally trimming the aerial trimmer, back on about 1500 kHz . Leaving these settings untouched, switch to LW, tuning to 200 kHz , or 1500 metres, then adjusting the long wave trimmer to bring in Radio 2, and setting the LW aerial trimmer to peak the signal, or adjusting the LW coil on the ferrite rod.

At this point any disturbance of the IFs can be corrected. If correct tracking cannot be achieved the IFs have probably been more seriously disturbed than was thought and the signal generator can then be brought out of cold store,

Photographs were kindly supplied by the following companies to whom all queries on the instruments illustrated should be addressed. Wayne Kerr, Durban Road, South Bersted, Bognor Regis, Sussex PO22 9RL.
AVO Ltd., Archcliffe Road, Dover, Keni CT17 9EN.
Chinaglia Lid., 19 Mulberry Walk, London SW3 6DZ.
Advance Electronics Ltd., through Peter Bush, Bush Steadman and Pariners, Saffron Walden, Essex.
set to the required IF (as marked on the set, or in the service information) and loosely coupled with a single turn of wire around the ferrite rod. With the set tuned to the low frequency end of the medium wave band, about 600 kHz , increase the signal input until the modulating tone can be heard, adjusting the IF coil cores to peak and gradually reducing the signal input from the generator to the minimum, to prevent the AGC coming into action. Repeat the RF tuning procedure.

## SNAGS!

Simple enough, isn't it? So where's the snag? Well, you see, we've only mentioned some of the procedure for AM sets. Two examples of the kind of component layout to be expected are shown, one a long and medium wave design as used in the Marconi 4173. Notice that the tuning adjustment for the low frequency end of the dial is called 'padding' and the high frequency adjustment is called 'trimming'.
The snag arises when there are many coil cans and lots of trimmers! The rule here is not to do anything unless you know the exact purpose of each adjustment. Otherwise you may be disturbing something which was previously correct and this is not the idea at all. Also shown is the layout of another Thorn group model, this time a Marconi 3183. Here we see the IF coil cans clearly marked AM and•M. These wilf not be marked as such in the actual set and therefore no coil cores should be disturbed unless such a diagram is available. Even then adjustment of the FM coils requires the use at least of an FM signal generator, preferably with 'wobbulator' and oscilloscope, in order to obtain the desired response curves.
The object of all this is to preach the sermon loud and clear. Do not touch what is not fully understood and attend only to that which really requires attention.

THE GENERAL THEME OF THE FAULT-FINDING GUIDE WILL BE CONTINUED IN THE JUNE ISSUE OF PRACTICAL WIRELESS DUE OUT ON 7 MAY.


The sense aerial is then used to provide another signal. With one position of the ferrite ron, signals from both aerials will combine, giving a greater meter deflection than the other position, where ferrite aerial and sense aerials are out of phase. By this means it is possible to find which bearing is correct of the two minimum readings obtained without the sense aerial.

## BIF and Tuning

Fig. 1 is the circuit of the aerial, RF and oscillator tuning arrangements. L1 and L2 are MW and LW sections on the ferrite rod, which is assembled on a jack plug. This fits into a socket, through a hole in
the top of the case. S1 allows the sense aerial to be connected. S2/3/4/5 are the four poles of a 3-way switch. Positions 1 and 2 of section S2, short L2, for MW reception. Position 3 introduces C 3 and TCl to load the oscillator coil L3 for LW reception. Sections S3 and S5 introduce series capacitors TC5 and TC2 in position 1, to spread the tuning at the high frequency end of the MW band. S4 connects trimmer TC4 for this band, and trimmer TC3 for the lawer frequency bands.

To avoid the need for further aerial trimmers and to allow correct trimming with Sl open or closed, a panel trimmer VC3 is used for aerial circuits. Trl avoids the need for a coupling winding on the ferrite aerial, which would require four connections in all. A 3-way jack plug and socket may thus be used. Point 1 is the inner (tip), point 2 the centre and point 3 the outer sleeve. Trl, together with its associated circuitry is fitted to a tag strip near the jack socket as in Fig. 1.

## IF Circuit

Fig. 2 gives details of the IF circuitry, which comprises the oscillator/mixer $\operatorname{Tr} 2$, two IF amplifiers $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$, and detector D1. External connections to $\operatorname{Tr} 2$ go from R4 to C5 with a lead from pin 3 of the oscillator coil, to C3, TCl and C4, Fig. 1. R8 is under the board, from pin 4 to pin 2.

As strong signals can give more than full-scale on the tuning meter, the lst IF amplifier Tr3 is arranged to have the manual gain control VR1. This can be adjusted to bring the meter back to a central position, when required, as well as controlling IF gain. Bias from Dl is thus applied for automatic gain control purposes to Tr4, via R14 and R16. The meter is positioned to one side of the tuning scale, while the meter amplifier Tr5, is assembled on a tag strip secured to the dial plate. Trimmer pot VR3 is set so that the meter reading is just beginning to rise, with no signal. Increasing signal strength then causes negative base bias to Tr5 to raise collector current, so that the meter reading rises. Maximum meter reading corresponds to maximum signal strength, when rotating the aerial or VC3. With VR1 set so that this is about half-scale on the meter, the directional null should give almost zero reading on the meter, and is used for bearings, as it is sharper than the maximum.

Audio from the volume control VR2 passes to the AF amplifier.

## Audio Amplifier

The AF amplifier comprises pre-amplifier, driver and output stages, Fig. 3, and uses few components and easily obtained transistors. The most suitable


Fig. 8: This shows the circuit for the audio ampllfier, which uses for its output a matched patir of AC141/2 transistors. Speaker impedance should be around 150 .
speaker impedance is about $15 \Omega$, although the actual value is not too important. However, a speaker of less than about $10 \Omega$ ought not to be used, unless pressed into service by including a series resistor to make up the total, while speakers of over about $25 \Omega$ will result in some saving on battery current, but reduction in output.

## Chassis and Panel

Holes are drilled in the front of the chassis as in Fig. 4. For the cabinet listed, allow the panel to project below the chassis about ${ }_{2}$ in and mark the hole positions on it. The $7 \times 2^{1}{ }_{2}$ in scale plate is bolted a little back from the panel, which is not fitted until later. Fit the ganged capacitor with 4BA bolts, noting it is essential to use short bolts, or add washers, so that they do not project beyond the thickness of the metal plate. Two small pulleys are pivoted on 4BA bolts, held with lock nuts to the plate. The cord passes twice round the drum, and then round the small wheels, and is held taut by a spring. Drill a hole in the panel for the slow-motion spindle of the capacitor. The pointer is a straight wire soldered to a small piece of tinplate, which is clipped on the cord. Arrange this so that it is fully to the right with VCI/2 closed and the spring to the left.

The case requires two $3_{4}$ in diameter holes. One is placed centrally, for the ferrite aerial, and the other near the back right hand corner, for the telescopic


Fig. 4: Details of the scale card, and the spacings required for the varlable control positions.
aerial. Using a universal chassis flanged runner, $8 \times$ lin, cut sections from each flange 3 in from the ends, so that it can be bent to form the mount shown in Fig. 5. This is bolted to the chassis so that the jack socket comes under the central hole in the case.


Fig. 5: The mounting for the rolaling aerial, and the tag strip that holds the RF stage, is constructed from a Universal chassis flanged runner and bent to fit.
Should a little adjustment of height be required so that the jack socket will clear the top of the case, the legs of this metal part can be spread outwards to lower it. Check that there is sufficient space for the IF board between the mount and scale plate.

The sense aerial must be insulated from the chassis. This was arranged by punching a lin diameter hole, over which a piece of paxolin is fixed with 6BA screws. The bolt on which the aerial screws fits vertically in the paxolin, and a lead runs from it to S1. If necessary, the paxolin can be spaced from the chassis, either above or below, so that the aerial closes flush with the case top. This aerial is run on to its screw after placing the receiver in its case.

The internal speaker is mounted on the left side of the cabinet. A grid of nine ${ }_{4}{ }_{4}$ in holes was punched over the position to be occupied by the cone. An alternative is to cut a larger hole and cover this with fabric or expanded metal. A $4 \times 1^{1}{ }_{2}$ in opening is cut in the panel, and is covered by a slightly larger

* components list


VC1/2 Jackson 00 208/176pF slow motion gang VC3 Jackson C804 50pF
TC1-TC5 60 pF trimmers
Semiconductors

| Tr1 | MPF102 | Tr6 | BC108 |
| :--- | :--- | :--- | :--- |
| Tr2 | BF194 | Tr7 | BC149 |
| Tr3 | BF194 | Tr8 | AC141 |
| Tr4 | BF195 | Tr9 | AC142 |
| Tr5 | BC179 | D1 | OA81 |

Miscellaneous
L1/L2, Denco MW/LW 5FR. IFT1, Denco IFT18/465. IFT2, Denco IFT18/465. IFT3, Denco IFT14.L3, Osc. coil Denco TOC1. S1, miniature slide switch. S2-S5 4 -pole 3 -way rotary swltch. Moving coil meter 1 mA fsd $42 \times 42 \mathrm{~mm}$. Jackson 54 mm dlameter drum. Paxolin tube $150 \times 29 \mathrm{~mm}$ diameter. 6 mm stereo jack socket. 5 control knobs. 550 mm telescopic rod aerial. 6 mm stereo jack plug. $15 \Omega$ speaker. 156 mm dia. 360 degree protractor. Plastic bowl $156 \times 30 \mathrm{~mm}$. OSC IF PCB, $105 \times 55 \mathrm{~mm}$. AF PCB, $129 \times 55 \mathrm{~mm}$. Both boards available from the PW Readers PCB Service, page 1070.

## Case

Type W case $10 \times 7 \times 5 \frac{1}{2} \mathrm{in}$. Type $K$ chassis $9 \times 6 \frac{8}{8} \times$ $1 \frac{1}{3} \mathrm{in}$. Type A screen $7 \times 2 \frac{1}{2} \times \frac{1}{2} \mathrm{in}$. All HL Smith \& Co. $8 \times 1$ in. flanged Universal chassis runner-Home Radio Ltd.
piece of ${ }^{1}{ }_{16}$ in Perspex, held with two screws. A card scale, upon which three lines have been drawn, is fixed with adhesive, so that the three bands can be calibrated later.

A bracket is bent from scrap metal to hold the PP7 battery and is screwed down behind the aerial mount. Do not overlook that holes are required under IFT1. and IFT2, so that the lower cores can be reached. These are simply positioned by marking them through the circuit board before fitting the IFT's.


Underside view of chassls, showing the volume control, If gain and aerlal trim controls. The PCB in the bower righthand corner is the Audio board.

## RF Stage

The RF circuit is wired as in Fig. 5, which also shows connections to the jack socket. Leads are fitted to run to $\mathrm{S} 1, \mathrm{VC} 3, \mathrm{C} 5$, battery positive line and S 2 . The jack plug and socket, Sl and aerial, as well as VCJ , contribute to the stray capacitance across L 1 and L2 so when wiring, these unavoidable capacitances should be kept as low as possible, otherwise there may be difficulty in reaching the HF end of the range.

With individual samples of $\operatorname{Tr} 1$ it is possible that changes to the resistors R2 and R5 could improve gain. Otherwise the values given should be suitable. R4 may be the lowest value which does not allow instability to develop.


General plan view photograph of the neceiver, showing layout of the Osc/IF board, tuning capacilor and trimmers, and the rotating aeria/ mounting.


Fig. 6 : Foil side and component side views of the Osc/IF board. Both are shown full size. If the board is to be tested outside the receiver, VR2 must be connected

## Osc/IE Board

Fig. 6 shows the PCB carrying the Osc/IF sections of the receiver. The input goes to $C 5$ and the output taken from D1. The oscillator coil and IFTs should fit without any need to use force. If not, the holes for these may be slightly enlarged, taking care not to break the foil. Components are inserted as in Fig. 6, excess length of wire being snipped off after soldering. Provide flying leads for input, output, battery positive (S6), meter amplifier and IF gain control. (If this board is tested before fitting, VR2 must be connected.) Mounting is by means of four ${ }^{1}{ }_{2}$ in 6BA bolts, with extra nuts to give spacing from the chassis and locked firmly to provide the necessary chassis return.

Since the gain of individual transistors varies, it might be possible to modify the value of R 8 , using the lowest value which does not result in uncontrollable oscillation at any frequency. Normally, however, the value given can be fitted.

## Audio Rmplifier

The AF board is shown in Fig. 7. Colour coded leads can be soldered on for R19, speaker and battery positive. The PCB is mounted under the chassis with three bolts, with the speaker leads made long enough
to allow the receiver to come well out of the case. If a jack socket is used here, it must be completely insulated from the chassis or be of the insulated type.

## Meter Amplifier

Components for the meter amplifier are wired to the tag strip as in Fig. 8. The meter is a 1 mA instrument calibrated in S-points, though the meter is primarily required to show minimum signal positions for the rotating ferrite rod aerial. If after maximum adjustments to VR3 the meter cannot be set so that it is just beginning to rise, with no signal tuned in, then either R20 or R21 may be changed in value, to correct this. Alternatively, R3 can be changed to $250 \Omega$, provided R20, VR3 and R21 in series total about 1.5 to $2 \mathrm{k} \Omega$. It does not matter how the potential divider is made up, except that adjustment of VR3 becomes more critical if it forms most of the total resistance.

## Bandswifch

Connections to the switch are shown in Fig. 9, and can be followed in conjunction with Fig. 1. The rotor tag of VC3 must be wired to the chassis. TC5 is soldered directly across the switch, while the four trimmers TCl to TC4 are mounted on a strip fixed


Fig. 7: Audio amplifier board showing the foil side to the left and the component side to the right. Again, both are shown full size. Chassis mounting is by three bolts.
clear of the chassis, by spacers, and behind VC1/2. It is convenient to use these trimmers, from left to right, for the circuit positions in Fig. 1. That is, TCl LW oscillator trimmer; TC2 Range 1 bandspread coverage; 'ГC3 Range 2 (and LW) oscillator trimmer; and TC4 Range 1 trimmer, This allows a short lead to run from pin 3 of the oscillator coil to TCl and C4, which is connected from TC1 to TC2. For short leads, use the lower tags of VCl and VC 2 , as in Fig. 10.

## AM0652



Fig. 8: Components that make up the meter amplifier are mounted on a tag strip adjacent to the meter itself. VR3 can be any pre-set pot of $100 \Omega$.

## Rotating Rerial

A 3-way jack plug is used as a pivot and is assembled as in Fig. 11. A $4^{1}{ }_{4}$ in disc is cut from plywood (this diameter was chosen to suit the diameter of the $0-360^{\circ}$ protractor and is a tight push fit on the insulated part of the jack, to which it is cemented. If necessary, a block with a central hole can be glued here to strengthen the assembly. Insulated thin flexible leads are soldered to the plug contacts; these may be green for 1 , red for 2 , and black for 3. Thread these wires up through the jack moulding and bring them out on top of the disc.

The ferrite rod aerial as received has a few turns for base coupling to L1 and these are removed. L1 and L2 must be in the same phase when connected in series, or LW alignment is impossible. The rod is secured to a small piece of paxolin by thread and


Fig. 9: The band switch comprises four poles and three positions, and the above drawing shows the connections to this switch, and the frimmer TC5.

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The chip is totally designed and manufactured in the UK, and is the first design to incorporate all circuitry for a digital


The Sinclair Black Watch is fully guaranteed. Return your kit in original condition within 10 days and we'll refund your money without question. All parts are tested and checked before despatch-and correctlyassembled watches are guaranteed for one year. Simply fill in the FREEPOST order form and post it-today!
Price in kit form: $\mathbf{\Sigma 1 4 . 9 5 \text { (inc. black }}$ strap, VAT, $p$ \& $p$ ).
Price in bullt form: $£ 24.95$ (inc. black strap, VAT, p\&p).


[^0]Reg. no: 699483 England. VAT Reg. no: 213817088.
... and how it works
A crystal-controlled reference is used to drive a chain of 15 binary dividers which reduce the frequency from $32,768 \mathrm{~Hz}$ to 1 Hz . This accurate signal is then counted into units of seconds, minutes, and hours, and on request the stored information is processed by the decoders and display drivers to feed the four 7 -segment LED displays. When the display is not in operation, special power-saving circuits on the chip reduce current consumption to only a few microamps.

## Complete kit S14.95:

The kit contains

1. printed circuit board
2. unique Sinclair-designed IC
3. encapsulated quartz crystal
4. trimmer
5. capacitor
6. LED display
7. 2-part case with window in position
8. batteries
9. battery-clip
10. black strap (black stainlesssteel bracelet optional extrasee order form)
11. full instructionis for building and use.

All the tools you need are a fine soldering iron and a pair of cutters. If you've any queries or problems in building, ring or write to Sinclair service department for help.


Fig. 10: The trimmers TC1 to TC4 are mounted in the above configuration to enable the leads to be kept as short as possible.
adhesive. This is held with two small screws, with strips to space it slightly from the disc, to clear the plug leads. These are soldered to the appropriate leads from L1 and L2, using pins as anchorage points if required. When the aerial has been tested, it is protected by a $6 \times$ lin paxolin tube, cut away just sufficiently on the underside to allow it to be fitted over the rod. A lead from point 3 is brought out from the tube.

The metal shield is bent from aluminium, about $31_{2} \times 2 \mathrm{in}$, to clamp the paxolin to the wooden disc and it is earthed by a tag under one fixing screw, soldered to lead 3. Its purpose is to improve the minimum null by reducing non-directional pick-up by the connecting wires. Approximate alignment can be made before fitting the paxolin tube. Final small adjustments to the positions of L1 and L2 may be made with an insu-
lated tool, through the open ends of the tube. The ends of the tube may be closed with discs of insulating material. Due to stray pick-up by other wiring, the sharpest directional nulls are obtained only with the receiver in its metal cabinet.


## Alignment

Band coverage is most easily checked if a signal generator is available, but satisfactory alignment is possible without this. The IFTs are pre-aligned by the maker so only small adjustments to these cores should be necessary and should not in any case be made until signals are received. A correctly shaped tool, such as that available from the IFT maker, must be used, otherwise the cores may crack.

To check the IFTs, tune in any steady, stable signal correctly, with VR1 near maximum gain, but reducing signal strength if needed by rotating the aerial, so that the meter does not go beyond full scale. All the IFT cores can then be adjusted slightly to give the best meter reading. When the IFTs are correctly aligned in this way, they must not be altered or readjusted when aligning the aerial and oscillator


The ferrite aerial is mounted inside a paxolln tube and connected via a stereo jack plug. This permits the aerial to be rotated to find the 'Null" point.


## 3．I．和．

SEVERAL readers have expressed interest in the picture of John Logie Baird＇s＂Televisor＂shown in the February 1976 Going Back so I thought I would show another couple of pics．of the great man．The small photograph shows J．L．B．with Miss King－ the first girl ever to be televised． The larger picture shows J．L．B． in 1926 with his original tele－ vision apparatus．If anyone wants to see this fantastic piece of equipment，pop along to the Science Museum－it＇s there in a glass case just like the one in our picture．
Some J．L．B．milestones：May 1924－The Baird Television System．＂Mr．Baird has achieved some remarkable results which go a long way towards proving that television is practicable．＂October 1926－＂The first TV licence was recently granted to Mr．J．L． Baird＇s stations．One is situated in St．Martin＇s Lane and the other at Harrow．At present the London Station is a transmitter and， except for an interval of a fort－ night，＇looking－in＇has been in progress every night for some weeks on a wavelength of about 200 metres．＂May 1927－Said J．

L．Baird，＂In ten years time，I prophesy，we shall be able to see on our wireless televisors topical events，such as the finish of the Derby or the finish of the Boat Race．＂


J．L．B．and his＇first lady＇

## Antone 賏elp？

MR．M．HILL，Hillside，Peas－ lake，Guildford，Surrey is desperately anxious to obtain an old Murphy A92 ＂Stationmaster＂receiver of 1940 vintage．It＇s an 8 －waveband all－ mains receiver which was claimed to have a very good short－wave performance．If you can help，please contact Mr．Hill direct．


J．L．B．and original apparatus．

## Morcseas 理pms

MR．KEN McKenzie，one of our New Zealand cousins recently wrote to say that he has been a radio enthusiast since 1924 when he heard，via the telephone，for the first time in his life，a radio broadcast．It was from the South Seas Exhibition on South Island， N．Z．In 1927 he built his first one－ valve receiver from a design published in the journal N．Z． Radio．His ultimate project was a three－valve receiver working a Philips＂Baby Grand＂cone speaker．

For a long time his nearest transmitter was 2YA Wellington， which ran at 5 kW and was over 40 miles away．Later，for a town of a then population of about 12,000 they became very well served by two dealers in radio sets and parts who set up broad－ cast transmitters．They were N．R． （Ray）Cunningham with 2ZQ and W．D．（Bill）Ausell，with 2ZD．

It＇s always good to hear from our overseas enthusiasts so keep the letters coming in folks！

## Fintage kidio sorietp

IHEARD from our friend Tudor Rees（of Antique Wire－ less Newsheet fame）again recently and he says there is a saying＂Put two Englishmen upon a desert island and they will form a club＂．This however certainly isn＇t based on fact when it comes to a British Vintage Radio Society．There must be literally many thousands of enthusiasts but no sign of a club or society as yet．Things may be looking up though，for a Mr． A．Constable， 18 Ravensbourne Gardens，Ealing，London，W． 13 wishes to conduct an initial survey as to the possibility of forming such a group．He would like all those with a genuine interest in a Vintage Radio Club to write to him（I would suggest you enclose a s．a．e．）．

## Fintage $\mathbb{C O} \mathbb{C}$ Column

FROM time to time we pub－ lish a special＂Vintage CQ Column＂for readers who have requests for old books， equipment etc，and those who wish to dispose of such items．If you want to be included in our next column，please address your request to＂Vintage CQ＂，Practi－ cal Wireless，Fleetway House， Farringdon St，London EC4A 4AD．

# PRODUCITON LINES 

## NEW MIC



A noise cancelling microphone which the manufacturers state has exceptional qualities of discrimination between the voice and random noise is now in production at the Eastleigh, Hampshire works of Selsound Limited.

In their search for the clearest possible transmission of speech, Selsound engineers have demon-
strated that the microphone is able to eliminate extraneous noise to an exceedingly high degree. Exhaustive laboratory development resulted in a high level of response within that band of frequencies most important for clarity of speech, a marked diminution on each side of this band and a steep gradiant to the sensitivity/ proximity curve.

Selsound microphones are available in the form of a microphone insert, styled "Type 2500 ", but the company state that they can provide special housings to suit specific requirements and installations.

Full technical details are available from Selsound Ltd., (Dept. P.W.) Victory Close, Industrial Estate, Chandlers Ford, Eastleigh, Hants. Tel: Chardlers Ford 67158.

## WIRING PENCIL

This new wiring pencil, patented by Vector Electronic Co., U.S.A. comprises a lightweight plastic housing, a replaceable spool of wire, and extended metal tip to guide and cut the wire. The wire is said to be a unique solder through nylon-polyurethene insulated tape which, when heat is applied to the wrapped connection points with a fine-tipped soldering iron, the insulation melts away, and produces a soldered joint. The wiring tip of the pencil is angled
to facilitate wrapping and to provide a clear view of operations.

The makers claim that the average time required to make a soldered joint is only seconds-and reckon it's about three times faster than conventional soldering.

The pencil, complete with two 250 ft . spools of wire, sells for $£ 6 \cdot 75$ plus postage.

Further information from: J. H. Equipment Limited, (Dept. P.W.) 91 Redbrook Road, Timperley, Trafford, Lancs.


Pleasemention Practical Wireless when writing to manufacturers and suppliers whose addresses are given in these pages.
-Thank you.

THE ALL BRITISH CARTRIDGE


Goldring have just brought out a new Cartridge-the G900SE. The key to the G900SE performance is the great mass reduction (moving mass 32 g ) which immediatley results in extremely low intermodular distortion. (Physical mass has been reduced to 5 mg .)
These reductions in mass have been achieved firstly by the introduction of minature magnets to a specification previpusly believed impossible. Then spurning conventional methods, the coil assembly used in the main body of the cartridge is created using formerless winding techniques through which Goldring have saved valuable space and therefore weight, which in turn reduces the mass which the stylus has to move.

Welded to the magnet is a micro gold plated nickel tie bar, which is there partly as an earth to reduce crucial static discharges that can occur and also to control the movement of the stylus in unwanted modes. The whole assembly is then pivoted via a special Butyl polymer with optimised damping.
Specification:
Frequency range: $10 \mathrm{~Hz}-28 \mathrm{kHz}$.
Frequency response: $20 \mathrm{~Hz}-20 \mathrm{kHz}$
$\pm 2 \mathrm{~dB}$.
Playing weight: 1 gm .
Playing weight range: $0 \cdot 75-1.5 \mathrm{gm}$.
Tip mass : 0.32 mG .
Stylus point radius: $\cdot 0007^{\prime \prime} \times$ $0002^{\prime \prime}(18 \mu \times 5 \mu)$.
Inductance at 1kHz: 640 mH .
Inductance at $10 \mathrm{kHz}: 630 \mathrm{mH}$.
DC resistance: 720 Ohms.
Channel separation: 25 dB NOM.
Output (sensitivity) @ $5 \mathrm{~cm} / \mathrm{sec}$ : 1 kHz . RMS $5 \mathrm{mV} \pm 1.5 \mathrm{~dB}$.
Compliance (static): 40 LAT $\times$ $10^{-6} \mathrm{~cm}$ dyne, 20 VER $\times 10^{-6} \mathrm{~cm}$ dyne.
Vertical tracking angle: $24^{\circ}$ Net weight: 5 gm .
Goldring Limited (Dept. P.W.) 10 Bayford Street, Hackney, London E8 3SE.

## WHARFEDALE DECK

Rank Hi-Fi have announced the Wharfedale XP cassette deck (with Dolby) at $£ 165$ (inc. VAT). Finished in black and walnut, this 4-track stereo deck has an electronically governed DC motor and automatic bias selection. Tape speed: $4.8 \mathrm{~cm} /$ $\sec \left(1 \frac{1}{8} i p s\right) \pm 1 \cdot 5 \%$. Wow and flutter: DIN 45507 0.20\% (maximum) (peak weighted). Output levels: DIN socket more than 10 K ohm, OVU input, $580 \mathrm{mV} \pm 1.5 \%$, headphone jack, 2 volts into 50 ohms. Input level: microphone/DIN 2 mV , line 30 mV . Input impedance (nominal): microphone/ DIN $5.6 \mathrm{k} \Omega$, line $50-500 \mathrm{k} \Omega$. Bias frequency: 79 kHz . Frequency response (record/playback): standard tape (Dolby out) $50-10,000 \mathrm{~Hz} \pm 3 \mathrm{~dB}$, $10,000-12,500 \mathrm{~Hz}-3$ to $-5 \mathrm{~dB} ; \mathrm{CrO}_{2}$ tape (Dolby out) $50-12,500 \pm 3 \mathrm{~dB}$, $12,500-14,000 \mathrm{~Hz}-3$ to -5 dB ; Dolby in from Dolby out frequency characteristics within $\pm 3 \mathrm{~dB}$. Frequency response (playback only): within 3 dB of record/playback, response from $50-10,000 \mathrm{~Hz}$. Total harmonic distortion (max.): $3 \cdot 0 \%$. Typical signal/noise ratio: Dolby out 54 dB , Dolby in 61 dB . Erasure (minimum): 60 dB . Channel separation (min. at 1 KHz ): 32dB.

Rank Audio Visual Ltd., (Dept. P.W.) P.O. Box 70, Great West Road, Brentford, Middx.

## SPEAKER BRACKETS



The brackets holding this speaker are made of hardwood and are manufactured by Esta Limited, Staffs.
These "Astute" brackets, which are very easy to fit can easily be removed for decorating etc. Rubber pads are incorporated to hold speakers so that no screws need to be driven into the actual speaker cabinets.
They come supplied sanded ready to finish and are complete with screws and plugs. Prices: 14 cm £1.71; 19cm £2.16; 26 cm £2.70 further gen from Esta Heating Products Limited, (Dept. P.W.) Green Lane, Walsall, Staffordshire.


## PHILIPS MULTI-TESTER

Model SMT-111 has as one of its most important features, a high input impedance of $0.5 \mathrm{M} \Omega \mathrm{V}$. This derives from an integrated circuit amplifier which enables the instrument to be used in many AC applications, up to 25 kHz on the 12 V range, for example. The use of an integrated circuit amplifier also enables a lowerimpedance moving coil movement to be incorporated.

The SMT-111 is based on the combined experience of Philips own
engineers and technicians throughout the world. Its thirty-five measuring ranges were selected with them in mind and an additional feature has been the inclusion of an AC current range. Both the integrated circuit and movement have been fully protected against peak overload and a checking point for the battery has been incorporated in the range selector switch. The SMT-111 is priced at $£ 30 \cdot 00$. Philips Electrical Limited, (Dept. P.W.), Century House, Shaftesbury Avenue, London WC2H 8AS.

## FOR CINE FANS

The Leeds firm of Farnell-Tandberg Limited recently introduced two new loudspeakers aimed mainly at the home-movie market, for both of them are suitable for use with cine sound projectors. Model FT 108 has a $4 \Omega$ impedance which accurately matches the output of most 8 mm sound film projectors. The FT 116 has an impedance of $8 \Omega$ to match the output of the majority of 16 mm sound projectors on the market.
The robust cabinets (and you need them to be pretty strong if you are lugging equipment around doing film shows) are finished in grey rexine with matching vynair. Both incorporate a 10 in . loudspeaker giving 10W RMS output. The units are supplied with 15 metres of twin-core sheathed cable which terminates in a DIN speaker plug. All of this can be neatly stowed away in the back of the cabinet where there is a compartment with a removable lid.

We tried one of these speakers on an 8 mm projector and also tested it with an ordinary cassette tape recorder to play back sound for slide shows. In both cases results were verygood. The price of these speakers

is set at $£ 23 \cdot 25$ plus VAT. Further gen on these and other FarnellTandberg equipment for sync sound systems may be obtained from Mr . M. R. Cowing, Promotional Services Manager, Farnell-Tandberg Limited, (Dept. P.W.) Farnell House, 81 Kirkstall Road, Leeds, LS3 1HR.


SOME time ago, I suggested in the pages of this magazine that it might be worthwhile to explore possibilities of long distance VHF reception on the East European (OIRT) band, 65 to 73 MHz . At that time (PW October 1974) I wrote that Sporadic E openings on these lower frequencies could take place more often than those reaching into the 90 to 100 MHz region though the statement was rather in nature of an educated guess, being partly based on other people's observations.

## SEASON 74/75

During the 1974 and 1975 SpE seasons (mid-May to mid-August) I conducted some experiments of my own and the results have shown that if anything, my prediction had not been optimistic enough. In 1974, long distance propagation of FM radio signals


一a long-skip character
caused by reflection from the ionosphere was observed on 27 occasions; only on 5 of these occasions did the exceptional DX conditions also affect the West European (CCIR) FM band, $87 \cdot 5$ to 104 MHz . In 1975, the ratio was $35: 6$ and there were a few additional days last July when broadcasting stations from Eastern Europe could be received due to enhanced tropospheric propagation.

The duration of these favourable receiving conditions, as well as the times at which they occured, differed widely. They would last from less than one hour to several hours at any time of the day and on some occasions OIRT stations could be heard from early in the morning till late at night.

Signals were usually of a long-skip character and stations most frequently received were those from the north-western and western parts of the USSR (i.e. Estonia, Latvia, Lithuania, Byelorussia and the Ukraine), eastern Poland, Romania and Hungary, while Bulgarian and Czechoslovakian FM stations appeared less often. The strength was sufficient to make listening in stereo possible, though at times with a considerable level of noise. Indeed, sterea programmes have been received from all the OIRT countries, the only exception being the USSR, where a different system is used for stereo broadcasts (unsuppressed subcarrier at $31 \cdot 25 \mathrm{kHz}$ ), which the common 19 kHz pilot tone type of decoder cannot resolve.

## EQUIPMENT

My equipment consisted at first of a small 4 metre converter with the oscillator set at 173 MHz and an IF at 100 MHz , used in connection with an ordinary FM tuner, an aerial preamplifier and a wideband Yagi array. For the 1975 season, however, the converter was replaced with one of the currently available FM tunerheads. Retuned to the 65 to 73 MHz band it was built into the tuner as an alternative, switchable front end.

It is this latter arrangement that I can recommend to anyone interested in similar experiments, and results achieved over the past two years certainly do confirm that the lower FM band is ideally suited to VHF DXing. However, it is impossible to give any advice as to the choice of a suitable front end. There are quite a few types available, costing mostly under £10 (e.g. from Ambit International) and the actual selection has to be made with regard to the specifications of the tuner with which it is to be used.

A word of caution seems to be in order as retuning
may prove to be a tricky business as it requires a signal generator or, ideally, a calibrated wobbulator. A simple adjustment of cores and trimmers would probably be not enough. In my case, at least, it was necessary to add approximately two turns to each coil as well as increasing the oscillator feedback capacitor by a few pF.

On the other hand, there should not be any difficulty about finding a suitable aerial as any old 405 line TV aerial will do, in particular those for Channel 5 . The OIRT transmitters are both vertically and horizontally polarized.

## EXPECTATIONS

The 65 to 73 MHz band is, under normal conditions, fairly quiet in this country. There is some RT traffic, amplitude modulated, around 71 MHz and in most areas of the UK the vision buzz of TV channel B5 can be heard on 66.75 MHz . There seem to be less and less amateurs operating on 4 metres ( 70 MHz ) these days. This means of course that anything else that may suddenly appear on these frequencies in the summer months is fairly sure to be coming from Eastern Europe via SpE, and do not be surprised if it happens to be English pop, as they play a lot of it over there.


An exception is the frequency of 67.75 MHz on which TV sound can be heard on such occasions originating from Yugoslavia, Spain, Italy and other continental countries. It should also be mentioned that while the OIRT FM band nominally starts at 65 MHz , few stations can actually be found below the 66 MHz point because there is a small overlap with channel R2 TV sound on $65 \cdot 75 \mathrm{MHz}$ so that frequencies between 65 and 66 MHz are used by FM radio only in areas not oovered by this TV channel.
For the British DXer the most difficult problem may well turn out to be the identification of individual stations and countries of origin. Being able to recognize the main languages of the area is of some importance and listening to the foreign broadcasts of the BBC, which are always introduced in English,
could be quite helpful in this respect. After a time, one gets attuned to the sound of a language and it is then possible to identify it without actually understanding it. Once this point is reached, it should be much easier to catch the odd word which makes closer identification possible. News broadcasts and weather reports are particularly revealing as the emphasis tends to be on local events and temperatures

## PW TECHNICROSS PUZZLE

 Solution to No. 12 presented last month
## Mail Order Protection Scheme

[^1]


Number 57 RCA CA3130 CMOS OPERATIONAL AMPLIFIER

THE relatively new CA3130 operational amplifiers manufactured by RCA employ the well-known CMOS (Complementary Metal Oxide Silicon) techniques in which the complementary FET's are fabricated on the same silicon chip as conventional bipolar transistors. This enables important advantages to be obtained in circuits employing this device.

## HIGH INPUT IMPEDANCE

One of the most noticeable features of the CA3130 is the very high typical input impedance of $1.5 \times 10^{12}$ ohms ( $1_{2}$ million megohms). In practice this means that either of the inputs of a CA 3130 device can be


Fig. 1: Internal block diagram of the CA3130, showing the three amplifiers connected in cascade.
connected into almost any circuit without affecting the operation of that circuit by taking an appreciable load current from it. The input current required by a typical CA3130 device is only about 5pA ( 5 mil lionths of a microamp) which again shows that this device imposes an extremely small load on the circuit feeding its input. The input current increases by a factor of about two for each $10^{\circ} \mathrm{C}$ rise in temperature, but even at $80^{\circ} \mathrm{C}$ it rises only to about 100 pA .

Another advantage is obtained by the use of CMOS circuitry in the internal output stage of the device. The CA3130 output voltage can swing to within a few mV of the potential of either supply line if the load impedance is relatively high.

The gain-bandwidth product of this very economi-


Flg. 2: The CA3130 is encapsulated in a TO-5 type can, and is supplied via eight leads as shown above. The view is from above.
cal device is 15 MHz , being a very high value for an amplifier with such a high input impedance. In addition, the slew rate of the CA3130 is about $30 \mathrm{~V} / \mu \mathrm{S}$ with no capacitance in the output circuit; this may be compared with the value of about $0.5 \mathrm{~V} / \mathrm{us}$ quoted for the well-known 741 device. The CA3130 can therefore deliver a higher output voltage than the 741 at a given frequency when this is determined by the slew rate.

## INTERNAL CIRCUIT

The internal circuit of the CA3130 comprises three amplifier stages in cascade together with a biasing circuit for the first two stages, as shown in Fig. 1. The input amplifier stage employs CMOS devices to provide a very high input impedance, but the voltage gain of this stage is only about five times. The gate electrodes of CMOS devices are susceptible to damage when an electrostatic charge accumulates in
the high input impedance circuit, since such charges can puncture the insulating layer of silicon oxide between the gate and the channel. Four zener diodes are integrated on the silicon chip to protect the device from damage by static charges in most circumstances.

The second amplifier stage employs a bipolar transistor in a circuit which provides a voltage gain of about 6000 times. The third stage of the CA3130 operates in Class A with a typical voltage gain of thirty times varying with the load impedance of the circuit.

## CONNECTIONS

The CA3130 is available only in a metal can type package with eight leads, Fig. 2, like a T0-5 type of transistor encapsulation but with eight leads instead of three. The CA3130 has the normal inverting and non-inverting inputs of an operational amplifier. The quiescent output voltage can be adjusted to a value half way between the power supply lines if a potentiometer is connected between pins 1 and 5 with its rotor connected to pin 4 (the negative supply).

The output stage can be rendered inoperative by connecting pin 8 (input to this stage) to the negative line at pin 4 . The output potential at pin 6 then rises virtually to the positive supply line voltage of pin 7. Electrical strobing pulses may be applied to pin 8 so that the device only operates at the desired times.

## TYPES AVAILABLE

The most economical device of the series is the CA3130, suitable for most applications. However, specially selected devices are available for more critical purposes. The CA3130A has a lower maximum input current than the CA3130 and lower input offset voltage and current. The input circuit specifications of the CA3130B have even tighter tolerances. All of the devices operate satisfactorily over the very wide temperature range of $-55^{\circ} \mathrm{C}$ to $+125^{\circ} \mathrm{C}$.


Fig. 3: Graph of the CA3130, showing increase in'supply current with supply voltage. These curves occur when the device is not supplying output current.

A letter 'T' or an ' S ' may be added. For example, RCA produce types CA3130T, CA3130AS, CA3130BT, etc. The ' $T$ ' signifies that the device has straight leads, whilst the ' $S$ ' types have their leads bent so that their ends are in an 8 pin dual-in-line configuration.

## POWER SUPPLY

The CA3130 will operate from supply voltages of 3 V to 16 V or from balanced positive and negative supplies of $\pm 2.5 \mathrm{~V}$ to $\pm 8 \mathrm{~V}$. The current required is very low, especially if the load impedance is high and the power supply voltage is low, an advantage obtained with most CMOS devices. Typical power supply currents when the output current is zero are shown in Fig. 3. The supply current is particularly low when the output voltage from the device is equal to either of the supply line potentials, but is higher when the output voltage is half way between the supply line potentials. If a single supply of 5 V is


Bandwidth $=4 \mathrm{MHz}$ at -3 dB down
Fig. 4: To achieve a high degree of accuracy between the input and output voltages, the device is connected with a balanced power supply.
employed, the power supply current is only about $300 \mu \mathrm{~A}$ when the load impedance connected to pin 6 is infinity and when the potential at this pin is 5 V ; if the output potential falls to $2 \cdot 5 \mathrm{~V}$, the supply current rises to about $500 \mu \mathrm{~A}$ for the same load impedance. The CA3130 series is therefore very useful with equipment which must be operated from small batteries.

## TYPICAL CIRCUITS

One of the most useful applications of the CA3130 is as an impedance transformer. The non-inverting input of the device is connected to a signal source which may have a very high impedance and which can therefore supply only a very small current. The output circuit of the CA3130 can either supply or accept an output current of up to about 20 mA , this being of the order of four thousand million times the input current required by the device. Thus the CA3130 can be used to drive a stage which requires appreciable current; in other words it can 'transform' a high impedance at its input to a relatively low impedance in its output circuit.
A typical impedance transformer circuit is shown in Fig. 4. In this case the device is used as a 'voltage follower' where the output voltage 'follows' the input
voltage. One can achieve an accuracy of $0.01 \%$ between the input and output voltages in this type of circuit.

The capacitor C1 in Fig. 4 provides frequency compensation. Negative feedback from the output to the inverting input is provided by R2 in parallel with C4. The circuit shown employs balanced power supplies with a supply voltage near to the maximum so as to obtain maximum output voltage swing. Supplies of $\pm 2.5 \mathrm{~V}$ may be used for minimum current consumption.

Another voltage follower circuit is shown in Fig. 5 in which a single power supply is employed. The potentiometer VR1 enables the quiescent voltage at the output to be adjusted to a required value. In both Figs. 4 and 5 capacitors are incorporated in the power supply lines to assist stability at high frequen, cies.

Voltage followers of this type are useful when the potential of the high impedance input is to be measured, since it is transformed to the low output impedance which can be measured with a conventional meter.


Flg. 5: The circuit above is similar to that shown in Fig. 4, but in this case is supplied by a single power supply. The potentiometer VR1 is used for setting the quiescent voltage at the output.

## OSCILLATOR

A simple square-wave generator circuit is shown in Fig. 6. The resistors R1 and R2 bias the noninverting input of the CA3130 to a mean voltage equal to half the supply voltage. The timing capacitor is selected by the range switch, S1. The time for which the output voltage is in its 'high' state can be adjusted by VR1 and the time for which it is in its 'low' state by VR2. When the largest capacitor, Cl , is selected by S 1 , each part of the pulse can have a period in the range 4 ms to 1 s (according to the setting of VR1 and VR2). This period varies by factors of ten with the setting of S1 until one obtains $4 \mu \mathrm{~s}$ to 1 ms with the capacitor C 4 .

When the voltage at the inverting input is low, the output voltage will be high and the capacitor selected by S1 will charge through VR1, R4 and D1. As the voltage across this capacitor increases, the potential at pin 2 rises above that at pin 3 and the voltage at the output falls to a low value very suddenly. The same timing capacitor now discharges through D2, R5 and VR2 until the pin 2 voltage falls below that at pin 3, when the output switches


Fig. 6 : In this circuil, the CA3130 is used as the heart of a square wave generator equipped with independent adjustment for both periods of the waveform.
back to its former high voltage state. The potential at pin 3 varies with the CA3130 output potential owing to the current flowing through R3.

The use of the CA3130 in this type of circuit has certain advantages. The high input impedance enables relatively high values of timing resistor (VR1 and VR2) to be used and therefore one can obtain very low frequencies with a moderate capacitor value. The timing capacitors used in this circuit should not be electrolytics as they pass an appreciable leakage current which would produce a large voltage drop across VR1 and VR2. The potentiometer VR3 is an attenuator in the output circuit. The supply voltage shown enables square waves of about 15 V amplitude to be obtained, but smaller supply voltages down to about 5 V may be employed for smaller output amplitudes.

## HANDLING CMOS DEVICES

Although the gate electrodes of the CA3130 are protected with internal zener diodes, it is recommended that reasonable precautions should be taken when using them. Whilst the manufacturer's recommendations are often ignored without the device being damaged, it is certainly wise to observe them. Soldering iron tips used for soldering CMOS devices should be earthed. The devices should not be soldered into' the circuit whilst power is applied or even removed from a socket, since transient voltages can be developed which can cause damage. No signals should be applied to the inputs unless the power supply is connected and the input current should be limited to 1 mA .
The CA3130 is available from Chromasonic Electronics, 56 Fortis Green Road, London, N10 3HN, at 84 p (including VAT) plus 20 p packing and postage.


by Eric Dowdeswell G4AR

AN oft-repeated complaint from those who would wish to listen to the bands in some sort of reasonable quiet concerns the radiation from the line timebases of colour TV sets. Paul Turner (Bishops Stortford) asks for advice since he now finds DX-chasing almost impossible because of the QRM from a set just across the road. All I can suggest is that the equipment is checked for complete screening, that the aerial is placed as far away as possible from the source of the QRM and that some experiments be made on the earthing of the equipment. I think that I have mentioned before that the removal of the mains earth from the equipment can often effect a cure but this can mean an electrical hazard so due care must be taken. Ex. perimentally, a separate earth in the garden can be tried.

Strangely enough the ordinary TV viewer is completely unaware of the trouble he is causing because his own radio is off! But just try walking around the house with a portable radio and see how widespread is the QRM! Particularly near the TV set's coax! If one of us radiated a signal on another frequency at the same field strength of the average colour TV set we would soon be in trouble! Of course, in some civilised countries the set has to be screened but I wonder how long it will be before we get around to taking some practical measures to combat yet another form of pollution.

A mild reprimand from Tom Brady G8GAZ for saying that Alan Rae had held the callsign GM8GRO before becoming GM4ENN. G8GRO is a pal of Tom's so apologies all round. Callsigns are very personal, often conveying much more than actual forenames to the distant listener. Incidentally, the junior op at the GAZ QTH is G8HEB. Dad said it, not me!

Pete Allen (Taunton) decided to take my advice and put up a 132 ft wire. The improvement in his log shows that it was all worthwhile. Now he has fun switching between the long wire and his G5RV. Mike Green A8088 (Northwich) has been reorganising his equipment to the detriment of his log. He now has a new 2 m beam consisting of an $8+8$ slot fed at 20ft. His $\log$ shows four stations on 2 m heard via the aurora of Jan. 10th. Martin Kessel A9016
(Stoke-on-Trent) has now abandoned his one-valver plus five-valve superhet in favour of an AR88D. He is still wearing a groove in the carpet awaiting his RAE results and if successful will be on with a Liner 2 and a five element beam on 2 m at 35 ft . A Microwaves Modules converter has been added to the AR88 on the receiver side. Notwithstanding the 2 m bias Martin is getting his code up to the speed required for the Morse test.

Robin Bayley (Kingswood School, Nr Wolverhampton) has started off his DX-ing career with an ex-RAF 1475 set and a long wire, 30 ft up. A converter for 2 m is under construction. Welcome OM and I am sure that you will soon get into the swing of short wave radio. Overseas now to New Zealand and Mark Corrigan of Wanganui whose Heathkit SW717 pulled in some good Europeans for him using either a 20 m dipole or 75 ft long wire. Seems this column is responsible for Mark becoming a regular correspondent with another Mark, Mark Hill, another contributor of ours. Dennis Anderson is now using the receiver section of a 62 set and wonders if anyone has made up a mains unit to power this rig. He'd appreciate any help at 33 Manor Crescent, Pirbright, Brookwood, Surrey. Mike Bennett (Slough) finds the 80 m band wide open all night with the Far East and Africa coming in from dusk to midnight and the North and South Americans continuing on until mid-morning. However, he has not neglected the other bands, I'm glad to report. Steve Cottis A8961 (Harrogate) also found plenty on 80 m including ZL3NR/C which looks like Chatham Island, a good catch for anyone. Steve likewise roamed around the other bands from 15 to 40 m .

Paul Barker BRS34898 (Sunderland) reports some W's on 80 m , frequently missing from other people's logs, perhaps because they do not realise that they are to be found only above $3 \cdot 8 \mathrm{MHz}$ ! Paul's SSTV station-of-the-month was CT1JI, commended for his excellent picture quality. Graham Sewell (Greenford) stuck to 20 m and the VK and ZL gang as garnered on his Codar CR70A and 20ft of wire. Don't know how far he would get with a decent aerial! Peter Walton A9002 pulls me up for saying he has a 359 x , should be 358 x of course. I must have been thinking about signal reports! Peter now has a half wave aerial up aimed at South America. Alan Dobherty (Portrush) now sports an inverted vee aerial on 80 m but as he says, "it's a bit close to the dirt".

Stephen Terry BRS35669 (Banbury) has a Microwave Modules converter feeding into his FR50B on 2 m driven by a 6 over 6 element beam at 20 ft

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which, considering he is at 425 ft asl, sounds like a good set-up! Lastly, Ray Woodward (Colne) is also a first-timer to the page and seems to have been doing well with his Codar CR70A and he awaits the associated ATU. He is one of the brave few that get up at 4a.m. to get in on the DX!

## Log extracts

P. Turner:- 10 m from 2 m via Oscar 7 OE3JBC DB8QP DC6HY PA0GBL I2SRR
P. Allen:- 80m FP8DH KP4AM VP9HM 20 m CR9AJ VK4PX VK6LK
M. Green:- 20 m KZ5AS VK1JC 2m Auroral DC9DZA GI8HY GM8FFX
M. Kessel:- 80 m ZC4PK 40 m EA8CR 20 m EA9FE FY0BHI VK5MS VP2EEG YB0ACG 15 m SV0WZ VK6HE YN7MHN ZS6DQ
M. Corrigan:- 80 m OA4ASN VK0DA VR1AT ZK2AE 3D2AN 20m C2IDC CX7DC KJ6BZ KS6SFA VR1Z YNIAZ WA6LRG/KB6
M. Bennett:- 80m A4XFW HK1CHL JYI KZ5HP VS5DB 9M2PV 20m FB8ZG Amsterdam Is. HR6SWA Swan Is. KC4AAA VK9XI Christmas Is. VU7ANI Andaman Is. YJ8DS 15m A6XP FY0BMI YB0ACG
S. Cottis:- 80m CR9AK CT2BU PJ3BB VS5JH ZL3NR/C 40 m EA6DA VK9AAN VP8AA 20 m CX5DT TG9GI VQ9DF 15 m EA8ND KZ5AL ZD7FT 9H4K
P. Barker:- 80 m EA8JP 20 m SSTV CT1JI F3RT I1RHB KIWPS OE1SBA YU2CB 20m A2CGD EA9FC C9MAF VP2LBR 9L1BH
G. Sewell:-20m VK1BH VK6HS ZL1KN
P. Walton:- 20 m KH6BB ZB2A 5L7F 8P6FX 9J2LL
A. Doherty:- 80m A4XFW EL7F FG7AO HI8RRD JY3ZH KZ5HP VP2LC VR1AA VR4DX VR8A ZL3NR/C 40 m YNIAWS 20 m PZ9AJ VP8HA 9N1MM 2 m via Oscar 7 DC6PZ F1BFH I8CVS ON5PX
S. Terry:-2m EI9Q HB9AEN/P HB9AKG
R. Woodward:- 80 m CR4BS 15 m AC2PV MID 9GlLZ

All SSB except those in bold which are CW.


## SHORT WAVE BROADCASTS by Derek Bell

STRANGE are the items that are used for aerials! Neil Braeman from Southwater sleeps on his! He has hooked his bedframe to a Pye radio of uncertain vintage by way of a thirty foot length of wire. I would imagine that in the event of an
electric storm in close proximity the results could be rather alarming!

Andrew Gay of Wernham Farm, Marlborough, Wiltshire asks if anyone can oblige by letting him have their redundant copy of the Radio Nederland antenna amplifier leaflet. He has written twice with no reply forthcoming and is willing to refund any expenses incurred. Andrew is a jazz fan and has high praise for the SBC Sunday afternoon show on 11870 at 1530. It is packed with inside information for jazz enthusiasts and, comments Andrew, often has a quality that is good enough for recording.

A representative of the clan Mcleod, namely John Mcleod of Inverness, sends some interesting notes on the stations that he picks up that are, shall we say, not for our ears. These are the services for other target areas, that pass over the UK. John thinks that living in the highlands of Scotland he has more advantage in DXing than those of us who live rather more south. In this I rather agree with him, considering the DX that the Scandinavians pull in. It is on the cards however that other DXers will be able to tune to these stations and a selection follows:

> RAI Rome, to N. America 6010 at 0100
> SBC Bern, to Africa 9590 at 0530
> ORF Austria, to E. Asia 15105 at 0830
> Deutsche Welle, to N. America 6010 at 0530

John goes on to tell us that ORF Austria has informed him that "in future QSL cards will only be issued by ORF if they are specifically requested". This policy statement also says that they are looking for more critical comment on their programmes than hitherto. This is a station sticking its neck out with a vengeance! While on the subject of ORF, Richard Fuchs of Windsor points out the difference between Radio Austria and Austrian Radio. If this is a little confusing to you, Richard says that the Radio Austria station is a commercial firm and Austrian Radio is the one often referred to as "ORF" and is the station that transmits the Austrian Short Wave Panorama DX show on 6115 and 9770 at 0915 on Sundays, from Moosbrun.

Having sorted out your Austrian stations Niels Montanana recommends that the booklet issued by ORF is well worth having. To get this the DXer sends a reception report in to PO Box 700, A-1136 Vienna, Austria.

These are days of belt tightening and general pulling in of horns. Not least in the area of our hobby and one such person affected is H. E. Forder of Leeds. H.E.'s problem is that he would like to buy a rig that will pull in the short wave bands but not one that is expensive. Asks Mr. Forder, "are the sets under $£ 50$ as good as the advertisers claim?" This is a question that I cannot really answer but I will say that many good sets can be obtained for under $£ 50$ that are mains operated and can be improved by the addition of extra aerial wire or an aerial tuner unit in a matter of minutes, with little technical knowledge.

Over the water we go now for a couple of letters from readers who's DXing is a little different from ours. Lindsey Crawford Cull of Salisbury, Rhodesia forwards the address of the recently featured National Public Radio the Public Affairs segment of the AFRTS network. This system comprises 142 member stations and can be contacted at 2025 M . Street N.W., Washington DC, 20036 USA. Vincent Carabott of Malta GC whose name I have managed


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to decipher this time, reports that the Deutsche Welle African service is coming in very strongly in that part of the world. On his Philips 361A Vincent reports this service at 1340 on 17500 and alongside this go Radio Pakistan on 5955 at 2140 and SBC on 6309 at 2120.
One of the main snags with radios is the nagging thought that the set may not be properly calibrated and may be pulling in a frequency other than that shown on the dial. This is particularly so when one builds a set or when that faint station that has never been heard before whispers in and is just the one to fill that gap in your QSL album. Our old friend G. E. W. Hewlett, whom many will remember from columns past, writes of a station that is not only a calibration aid but also a test of that copper wire cobweb in the loft. While tuning around a few weeks ago George decided to try for WWV in order to check his calibration. The service in question is located at Fort Collins, Colorado USA and transmits on $2 \cdot 5,5,10,15,20$ and 25 MHz . The distinctive signal is a time signal and a male voice announcement every minute. Much to George's surprise he also heard a female voice which is the other time and frequency checking station WWVH at Kauai, Hawaii. WWVH transmits on the same frequencies but is most unlikely to be heard here very frequently.

George goes on to tell us that Radio Australia has opened a 250 kW transmitter at Carnarvon to cover the gap in its Asian service. The test transmissions are, at the moment, as follows:

9540 Indonesian 0800 to 1030
9560 Mandarin 1030 to 1300
9560 Cantonese 1300 to 1430
The 9560 channel is best heard around 1300 but in summer, when the short route gets better and an extra transmitter has been put into service, these signals should be worth listening for.

For those who like the African stations John Dipre using a VEF204 comes up with a few goodies:

4850 Radio Mauritania at 2038
4904 Radio Chad at 2035
4915 Radio Ghana at 2300
4940 Abidjan at 2250
5047 Radio Togo at 2257
To these we can add the loggings of Charles Winpenny who reports ETLF Ethiopia at 2020 on 11755 to give you a good handful of the infrequently reported services. Charles also asks if anyone knows what has happened to the Voice of Turkey English service on 9515 at 2200, which seems to have been dropped in favour of a Turkish language service.
Finally, we welcome two newcomers, Julian Blake of London and, lo and behold, our first lady correspondent Diane Kinnear from Cullicudden, Rossshire. Both ask the same question. "Please recommend a book to start us off and fill the gaps." The one I would plump for is "A Guide to Amateur Radio" by Pat Hawker G3VA from the Radio Society of Great Britain, 35 Doughty St., London WCl, price $₫ \in 1 \cdot 14$ inc. Don't be put off by the title, however, since our SWL DXing owes a lot to the licensed
amateur. As well as explaining many of the terms that they use, the book explains many of the matters that the two branches of our hobby have in common. This winds up the session for this month so I will say 73 s to you and yours.

## MEDIUM WAVE DX by CHARLES MOLLOY

STEVE WHITT (G8KDL) reports from London NW4 with a good bag of North American medium wave DX. With his Chapman S6BS communications receiver, MW loop and FET pre-amplifier he logged WINS in New York City on 1010 kHz at 0130 which he describes as "a phenomenal signal, I actually considered ringing into their phone-in programme". Other North Americans logged by Steve include CJOX Grand Bank in Newfoundland on 610 kHz ; WOR in New York City on 710 kHz ; WABC in NYC on 770 kHz ; CHNS in Halifax, Novia Scotia on 960 kHz ; KDKA in Pittsburg on 1020 kHz and WNEW in NYC on 1130 kHz .

North American medium wave stations are allocated identifying call letters which are used frequently by announcers, which makes identification easy for the DXer. These stations can be logged in the UK throughout the year whenever the path across the North Atlantic is in darkness. Even in midsummer, reception is possible for about an hour before sunrise. During March and April start listening around 0130 GMT . Reception can be very good at this time of year since interference from Europe is much less than during the earlier winter months owing to the approach of daybreak from the east.

An interesting letter comes from New Zealand reader Ash Nallawalla of Dunedin. Ash is president of the Otago branch of the New Zealand Radio DX League and is a keen medium wave DXer. With his Sanyo receiver, 40in delta shaped loop and an FET booster he logged Malta on 1570 kHz and Munich, West Germany on 1602 kHz . Reception in New Zealand of European broadcasts at the HF end of the medium waves has been reported before. In 1971, the well known New Zealand DXer Arthur Cushen in a letter to the writer, mentioned his reception of Langenburg on 1586 kHz and Munich on 1602 kHz at 2000GMT. The path at that time of day would be on the western route across South America, propagation being by five-hop $F$ layer rather than by the E layer, which is responsible for most of the DX heard on the medium waves. New Zealand and Australia are not heard on the medium waves in the UK probably because there are so few high power transmiters in these countries and the high level of interference at our end of the path. Reception of 4 QD, the 50 kW outlet at Emerald in Queensland has been reported on more than one occasion from Finland on 1550 kHz , a frequency that is almost buried in QRM in this country during the evening.

Tuning-in a signal on a radio receiver is usually quite a straightforward business. The tuning control is adjusted to give maximum reading on the $S$ meter, or if there isn't a tuning indicator, then the control is "rocked" until the receiver is spot-on the carrier frequency. This procedure works well in the absence of interference when adequate bandwidth is avail-
able (selectivity control at "wide") to include both sidebands of the transmitted signal. When trying to pick-out a weak DX signal in a crowded MW band, high selectivity is desirable to try to reduce adjacent channel interference. High selectivity leads to sideband cutting and loss of HF response at audio frequencies. Speech becomes muffled and difficult to follow. Intelligibility can be improved if the receiver it detuned slightly. Its IF passband now covers all one sideband instead of part of both, speech clipping is reduced while selectivity is maintained and cleaner and easier to understand speech will be the result. If the interference is coming from only one side of the DX then detune away from it. The strength of the unwanted transmission will be reduced while the level of the DX will be unchanged.

The second session of the International Telecommunications Union Conference on the future of medium and longwave broadcasting in Regions 1 and 3, which includes Europe, was held in Geneva last autumn. As expected, the 9 kHz channel spacing in Europe is to continue though many channels on the medium waves will have their frequency increased by 1 kHz so that they are multiples of 9 kHz . Heterodyne interference will be reduced if each channel is harmonically related to the channel spacing. The UK is allowed two additional transmitters on the longwaves, both of which will be located in Scotland. One will be on 200 kHz ( 1500 m ), the existing longwave channel and the other will be on 227 kHz ( 1321 m ). They will come into use after the start of the new plan in November 1978.

The retention of the 9 kHz spacing will continue to favour the DXer who is interested in reception of Region 2 (North and South America) where the spacing is 10 kHz but the 1 kHz change in Europe will bring its problems. Reception of KOMO in Seattle and WCFL in Chicago both on 1000 kHz will become more difficult as the nearest European will now be on 999 kHz . Whether there will be any compensating gains, remains to be seen.

Latin American medium wave stations, especially those situated along the east coast of South America, come in well in the UK. The long sea path across the North and South Atlantic favours propagation from Argentina and Brazil enabling some of the higher powered broadcasters in Buenos Aires and Rio de Janeiro to be heard at surprising strength at times. D. R. Mayhew (Littlehampton) has been chasing DX from this area between the hours of midnight and 0300 using a Philips receiver and a 20 in loop with RF amplifier. He says "the Brazilians are very exciting and well worth waiting for" and he mentions hearing two broadcasts from Buenos Aires; Radio Belgrano on 950 kHz and Radio el Mundo on 1070 kHz and no fewer than five from Rio de Janeiro; Radio Mundial on 860 kHz , Radio Jornal do Brazil on 940 kHz , Radio Nacional on 980 kHz , Radio Globo on 1180 kHz and Radio Eldorado on 1220 kHz plus Radio Record in Sao Paul on 1000 kHz .

Portuguese is spoken in Brazil, a language that sounds a bit different from Spanish which is used in Argentina and the remainder of Latin America. The majority of Brazilian stations are commercial, owned often by newspapers. Musical programmes include the rhythms of the samba and bossa nova which beat out from trumpets, guitars and marimbas to entertain the distant DXer!

## D. F. RECEIVER-continued from page 1064

circuits. Band coverage is determined by the settings of TC1, TC2, TC3, TC4 and the position of the oscillator coil cure.

Aerial alignment is determined by TC5, VC3 and the positions of L1 and L2 on the rod. Correct alignment of the aerial tuning is shown by maximum meter reading. If VC3 enables a signal to be peaked up, and is not fully open or fully closed, alignment may be regarded as correct at that frequency. However, the settings of TC5, L1 and L2 must be approximately correct or the trimming compensation afforded by VC3 may be insufficient at some frequencies.

Band 1. With each band the low frequency end is reached with $\mathrm{VCl} / 2$ closed and the high frequency end with VCl/2 open. For this band, TC4 sets the HF limit and TC2 the LF limit. TC5 is set so that VC3 can be peaked as described and may need re-adjustment after dealing with Band 2.

Band 2. TC3 sets the HF band limit. With a signal tuned in near the $\mathrm{HF}^{\prime}$ end of the band, adjust VC3 for best volume or meter reading. Tune in a signal near the LF band end and move Ll on the rod for best signal level, leaving VC3 untouched. Check that VC3 can peak signals throughout the band.

Band 3. Oscillator coverage is independently adjusted by TCl and L 2 which is adjusted at the LF end of the band. A 60 pF trimmer may be wired from pin 2 to pin 3, for LW trimming, but is not essential.

On all bands a small adjustment to the oscillator coil core setting will cause a substantial shift in frequency. So if this is made on any one band, the other two bands have to be checked again, as described. The actual coverage which is obtained can be modified quite substantially. It is not necessary that any particular bands are obtained by these adjustments, as other settings will result in no loss of efficiency, provided VC3 allows signals to be peaked uo. The ranges actually provided were: Band 1: $1300-1500 \mathrm{kHz}$; Band 2: $600-1300 \mathrm{kHz}$; Band 3: $160-$ 250 kHz .

## In use

To locate the position of the receiver, bearings have to be taken from at least two transmitters whose positions are known. If these are plotted on a map or chart, the receiver will lie roughly at the intersection of the lines. A third bearing can be expected to give more accuracy and should confirm the first result. To locate the position of a transmitter, directional bearings on its signal have to be taken from two known positions. When these are plotted, their intersection shows the transmitter location.

Low frequency and ground wave signals will generally give quite accurate bearings. Ground wave signals are those which have not been reflected by ionised layers above the earth. Their useful range depends on power, frequency and other factors and may extend to fifty miles or more. Sky-waves, on the other hand, are those reflected down and they provide greatly increased range, especially for higher frequency signals after dark but they may give confused bearings. In coastal areas wavefront bending may cause a deviation of $10-15^{\circ}$ while nearby metal objeots or structures may also modify the apparent direction of a signai. For ordinary reception purposes, it is only necessary to rotate the aerial for best reception, or minimum interference.

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|  | 4MM | 4 L 250 MA |  |  | ${ }^{5-6}$ 60 MA |
|  |  | 5 V 60 MA | E | 4 MM | 6 V 200 MA |
|  |  | 12 V 40 MA |  |  | 6.3200 MA |
|  |  | 12 V 100 MA |  |  | 14 V 40 MA |
|  |  | 14 V 75 MA | F | 4 MM | 2.7 V 60 MA |
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Deaigned to operate transistor sets and ampliflers. Adjustable output 6v., $9 \mathrm{v} ., 12$ volts for up to 500 mA (class B working). Takes the place of any
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 Add colour or white light operate 1,2 or 3 lamps(maximum $450 \%$ ). Unit in Box all ready to work e7.95 plus 96p VAT and postage.


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Preciaion made-as used in record decks and taper record-ers-Ideal also for extractor fans, blower, heaters, etc. New
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Made by famous American Company, operated by 24 V D.C. or
 20p each.

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 2 pole, 2 way- 4 pole, 2 way-
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pole, 4 way- 3 pole, 4 way- 2 pole
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Six apeeds are available 500,850
and $1,100 \mathrm{r} . \mathrm{p} . \mathrm{m}$. and $8,000,12,000$ and 1,100 r.p.m. and $8,000,12,000$
and 15,500
r.p.11. ghaft is and 15,500 r.p.15 Shaft is
diameter and arorimately
long. $230 / 240 \mathrm{v}$. Its epeed ina urther controlled epeed may be our Thyristor controller use of powerful and useful motor sizy approx. 2 in . dia. $x 5$ in. long.

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Type 600 relay, 2 changeover one open and one closed contact. Twin 500 ohm coils make this suitable or closing off DC $6 \mathrm{v}, \mathrm{DC} 12 \mathrm{v}, \mathrm{DC} 24 \mathrm{v}$ or AC mains using realstor and rectlfier. 40 p each.
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Part of the famous Reditune background music systern, secondhand, but believed in good order. value only these are 6 valve ampllfiers, the output value only. $x$ EI 84 in puibjpull complete with mains transiormer, rectifter and ample smoothing equipment. The nains tranaformer alone, today wovid cost at least 84 . Size is $\left.9 f^{\prime \prime} \times 5 f^{\prime \prime} \times 4\right\}^{\prime \prime}$. Price only $28.00+$ postage and VAT 1.50 .

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These have two aeparately R.C. amooth outputs so can operate two battery radios on a starec amp without cross modulation (they will of course operate one radio-tape-cassette-calculator in fact any battery appliance and will save their coat in a few montha). Apecs. : Full wave rectification, double inaulated terminal output. When ordering please state output voltage $4 f v, 6 v, 7 f v, 9 v$, 12 v or 24 v . Price $\mathbf{2 3}$-95, post and VAT Included.

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This heater unit is most effrcient, and quiet running. Is as fitfed in Honver and blower heaters costing $\& 15$ and more. Comprises motor, impelier. 1,2 and $3 k W$ and with thermal safety cut-out. Can be fitted into any metal line case or cabtnet. Only needs control switch. 45.82 plus VAT \& pust $21,2 \mathrm{~kW}$ Model os above except $2 \mathrm{~kW} 24 \cdot 25$ plus VAT post 75 p . Don't miss this. Control
Switch 44 p . P. 8 P. 40 p .

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Learn in your aleep: Have radio playing and kettle boiling as you awake-switch on ighta to ward oft
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E.T.P. Bolderlag Gun which we offer at a speclally E.T.P. Soldering Gun which we oner at a specially
keen price. It is in fact this month' snip. A well made lightweight unit with flash lamp to iluminate the work.
Has 100 watt double insulated mains Transformer and Has 100 watt double insulated mains Transtormer and
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Mains operated, turbo hlower type. Pressed ateel housing contalna motor and impeller. Motor is l/10th h.p. giving considerable sir flow but virtually no noise Approx.
dimensions $10 t^{\prime \prime} \times 4 t^{\prime \prime}$ e9.50 plus Post \&AT. dimensions $10 t^{\prime \prime} \times 4 t^{\prime \prime}: 8.50$ plus Post \& VAT.

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Made by Honeyweil for normal air temperatures $40-80 \mathrm{~F}$ (5-25 C). This bs a precision instrument with a differential which can be adjusted to better than
$1-5 \mathrm{~F}$. A mercury switch breaks on tejnp. rise. Flegantly 1-5 F. A mercury switch breaks on teinp. rise. Flegantly
styled and encased In an ivory piastic case with clear plastic windows, thermometer above and swltch plastic windows, thermometer above and switch
setting acale below.-size spprox. $3 \cdot 8^{\prime \prime} \times 3.2^{\prime \prime} \times 1 \cdot 4^{\prime \prime}$
deep-can be mounted on conduit box or directly on deep-can be mounted on conduit box or directly on
wril. Prlce 82.25 plus 50 p Post \& VAT.

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Although this uses no battery it glves really amazing results. You will recelve an amazing assortmient of stations over the $19,25,31,29$ metre bands-Kit contains chassia front panel and all the parta, $41-50-\mathrm{crystal}$ ear
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Bo thin is undetectable under carpet but will awitch on with slightest pressure. For burglar alarms, sbop doors, etc. $24 \operatorname{in} \times 18 \operatorname{in} 31 \cdot 99$. Post \& VAT 80p.
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Push button gives 10 varintions as follows:-(1) con. (2) contin water and continuous central heating night (3) continuows hot but central heating on at only for 2 periods during the day (4) hot water and central heating both on but day time only (5) hot water all day but central heating oniy for 2 perioda
during the day ( 8 ) hot water and central heating on during the day ( 6 ) hot water and central heatlag on
day time only- then for summer time use with central for 2 periods durlng the day time only-then for summer time use with central heating of (7) hot water continuous (8) hot water day time only (9) hot water t.wice dally (10) everything off, A handsonie looking unit with 24 hour movement heating. Supplied complete with wiring diagram. Originally sold, we believe, at over $415-w e$ offer theae, while stocks last, at 86.95 esch, VAT \& Postage 65p each.

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THIS MONTH'S BPECLAL OFFER is a very versatile transformer which can be used for many purposes. Rated at 250 watts it is very well huilt with frames for upright mounting and is varnith
impregnated. Ita primary is for $230 / 240$ volts impregnated. Ita primary is for $230 / 240$
50 cycles, It $h$ volts
four aecondaries each 10 v very 50 cycles, it has four accondaries each 10 v very
high current $w$ Indings. Just a few of the clrcuits high current windings. Jast a few of the circuirs
it can power are: $10.0-10 \mathrm{v}$ at up to 12 amps; 20.0 .20 v at up to 6 amps ; single 10 v at 26 amps ; $20 \cdot 0 \cdot 20 \mathrm{v}$ at up
single 20 v at $12 \dagger$ amps; single 30 v at 9 amps; single 20 v at $12 \neq a \mathrm{mpa}$; Qingle
single 40 v at $\mathrm{s}-5 \mathrm{mmps}$. The transformer can be used for power circuits (charging, etc.) or for Rmpiffiers, there being an earth bereen between primary and aecondaries. A transiormer like this to-day would coat at least \&15 from the makera; however, we are making a special ofter at $88.80+$
28 p , post $\mathrm{el}+8 \mathrm{p}$ each. (rab some while you 28 p, post $£ 1+8 \mathrm{P}$ each. (rab
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you work trolated from the maing. Alao, you are not likely to damage equipment if your soldering iron becomes earthy, as often happens. Isolation transformers are normaily very costly, in tact we see that the average wholesaler is charging 215 plus for a 250 w model. We can offer 250 watts of inolation at only $87+56 p$. Carriage $82+16 \mathrm{p}$. Telephone handsetis, ex GPO, but in good order, kitchen and your cellar, attle or shed down the kotchen and your cellar, attic or shed down the wire and two of these handsets. Price $50 p+40$ post $25 \mathrm{p}+2 \mathrm{p}$. Twin wire $44+32 \mathrm{p}$ per 100 metres. post 60p +5 p .
Splt motor with Carter gear box, probably one of the best sptt motors mate. Originally intended to he used in very high priced cookers; however this can he pat to plenty of other uses, for Jnstance your garden brrbecue or to drive a colour disc for a dance or flisplay or to drive a tumber for stone polishing; in fact, there ig no end to it January and February $2 \boldsymbol{2}-50+20 p$, poat $30 p+2 p$
 this has 200 contacts each croas referenced above and helow alphabetically and numerlcally so each can be casily ideutifled. Contacts are capable of making positive connection with a strip or wire as each contact is spring loaded and has a gold "pip". Theal if you want to make yourseif a computer or for clrcuit bread-boarding (resiators etc. plag atraight in) or for working out priated such as puzzles, comblnation locks, etc. Taken from unused computer panels, price only es + 16p each which works out to only 1p per contact probably less than the value of the gold pip Poot 15p
Gold plated stripa for permanent contacts into Slot of ahove panets, 15 for $\mathrm{sl}+8 \mathrm{p}$.
Vennor 1 rev per hour motor with spindle threaded and nutted ready to easily attach dises or druma Bakelite encased motor beautifully made and Anished. $22+16 \mathrm{p}$, post $20 \mathrm{p}+2 \mathrm{p}$. Very many uses for this, for instance a dise or drum atached Iighting, etc. $\quad$ Digital Display Unit, -Digivisor'. This is a prectaton Instrument which consists basically of 12 v lam focused by a lens system through a narnbered scale, the number appears on a ground glass fron screen. The number is selected by applying scale eq 1 volt spplied ahows figure 1 on ecale by using shunts or multipliers however any voltage or current could be made to indicate an number, or if a photo cell is positioned on the screen then an alarm could be triggered. Similarly this could be used for voltage or current regulation Overall size of the unit is $2 t^{\prime \prime} \times 1 t^{\prime \prime} \times 4 t^{\prime \prime}$
Price $44.50+36 \mathrm{p}$
Palse transformer with chrcuit for gound to light unit. It is a very simple circuit and all parts are
readily obtainable from us or you may already readlly obtainable from us or you may already
have them in your junk box. Price of the trang former with circult 75p, post and VAT paid. ORP 18 light coll. Thls device has been going for some years now but it has not been bettered and new appllicatlons keep belng found
have good atocks, price $65 \mathrm{p}+5 \mathrm{p}$. Throst miken. These are an ex WD item as need by air crew on their intercom, but being electro-
magnetic they alao aerve as pick-ups on muelcal instruments talking to passengers on motor bite and no doubt many other uses. Price 60p a palr $+15 p$. One chip radio. Ferrantl ZN 414 IC radio
in stock, current price $\$ 1.49+38 \mathrm{p}$. We can also still supply the Hi $Q$ kits to go with them, mos popular one kf No. E, compriaes a permiabilit tuner for medjum wave, and the reslstors and condensers which when addediun wave band Price of this HQ kit No. 4 is 68p +17 p , posi Price of th
$20 \mathrm{p}+5 \mathrm{p}$.
12t watt ipeakor bargain, $8^{\prime \prime}$ round mid-range, made for hlgh priced hi-fi outfit, a really super
 This has fairly long lever and is changeover 15 amp 250 v rating. Price $80 \mathrm{p}+2 \mathrm{p}$ each.
Two circuit micromwitoh, famous American Llcon, maker"s ret. $16-40411$, aize approx. $1^{\prime \prime}$ long $\times$
$f^{\prime \prime}$ wide $\times i^{\prime \prime}$ thick. Two electrically geparate circuits, one makes, the other breaks, when nylon push rod la depressed. Circult rating we estimate at 5 amps 250v. A real bargain at $15 p$ each $+1 \mathrm{p}-$ subject to normal quantity dlecounts.
Reed relay in molenoid. Realstance 1.5 K . this will operate from rodtager of 10 v upwards on a current
of 12 mA upwards. The fow of the control of 12 mA upwards. The flow of the control current closes the reed switch but amall magnet or an oppoaing current then the flow of the control current could be made to open the reed switch. Prlce 75p +6 p .

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SAFETYISOLATING See catalogue fur full radge． Prim．120／240V．Sec．120／240V．Centre Tap with screen．

$$
\begin{gathered}
\text { VA } \\
\text { (Watts) } \\
\text { REF }
\end{gathered}
$$

|  |  | PRICE | PLUGS | PRICE |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| VA | REF | CASED 2 | Pin + Earth | OPEN | POST |
| （Watts） | NO． | $£$ | $£$ | $£$ | $\&$ |
| 60 | 149 | 9.03 | 0.98 | 4.70 | 0.72 |
| 200 | 151 | 12.29 | 0.98 | 8.61 | 0.97 |
| 250 | 152 | 13.81 | 0.98 | 10.31 | 1.18 |

## AUTO TRANSFORMERS

See catalogue for full range．PRICE

| VA | REF． | PRASED | PLUGS | PRICE |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| （Watte） | NO． | $\pm$ | 2 pin | OPFN | POST |
| 1500 | 93 | 23.28 | 0.95 | 10.29 | $\pm$ |

## MINIATURE \＆EQUIPMENT

$$
\begin{aligned}
& \begin{array}{c}
\text { Prinary } 240 \mathrm{~V} \text { with screen. See catalogue for full range } \\
\text { VOLTS MILIIAMPS REF. PRICE POST }
\end{array} \\
& \text { Bec. } 1 \text { gec. } 9 \text { MiLIIAMPs RE }
\end{aligned}
$$

| 8ec． 1 | 8ec．${ }^{\text {－}}$ | Sec． 1 | sec．＇－ | NO． | 4 | ） |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3－0－3 |  | 200 |  | 238 | $1 \cdot 56$ | 034 |
| 0－6 | 0－6 | 500 | 500 | 234 | 1－56 | $0 \cdot 34$ |
| 0.6 | $0 \cdot 6$ | 1000 | 1000 | 212 | $2 \cdot 12$ | $0 \cdot 46$ |
| 9－0－9 |  | 100 | － | 13 | 1.80 | 0.34 |
| 0.9 | $0 \cdot 9$ | 330 | 330 | 235 | 1－62 | 0.34 |

## 12 \＆ 24 VOLTS <br> Primary 200－240 Volts



| See catalogue for full range |  |  |
| :---: | :---: | :---: |
| REF． | PIICE | PO8T |
| NO． | $\&$ | 2 |
| 71 | 2.47 | 0.61 |
| 18 | 8.07 | 0.62 |
| 70 | 4.50 | 0.72 |
| 108 | 5.11 | 0.85 |

30 VOLTS
Sicondiry $12,15,20,24,30 \mathrm{~V}$

| IMPS | $\begin{aligned} & \text { REF. } \\ & \text { NO. } \end{aligned}$ | $\underset{£}{\text { PRICE }}$ | PosT |
| :---: | :---: | :---: | :---: |
| 0.5 | 112 | 2.04 | $0 \cdot 61$ |
| I | 79 | 2－57 | 0.66 |
| $\cdots$ | 3 | 3.91 | 0.72 |
| 3 | 20 | 4.80 | 0.85 |
| 4 | 21 | 5－58 | 0.85 |
| 5 | 51 | 8.75 | 0.95 |
| 6 | 117 | $7 \cdot 52$ | 0.97 |
| 8 | a | 9.93 | $1 \cdot 18$ |
| 10 | 89 | 10.27 | 1－18 |

## 50 VOLTS

Pecondary 19， $05,33,40,50 \mathrm{v}$

| Secondary $19,25,33,40,50 V$ |  |  |  |
| :---: | :---: | :---: | :---: |
|  | REF． | PRICE | POST |
| AMPS | NO． | $£$ | 1 |
| 0.5 | 102 | 2.71 | 0.61 |
| 1 | 103 | 3.58 | 0.76 |
| 2 | 104 | 5.30 | 0.85 |
| 3 | 105 | 6.10 | 0.85 |
| 4 | 106 | 7.97 | 1.08 |
| 6 | 107 | 12.93 | 1.18 |
| 8 | 118 | 18.76 | 1.44 |
| 10 | 119 | 17.79 | 1.86 |

60 VOLTS

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AMPg

AMPs
0.5


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| :---: | :---: | :---: | :---: | :---: | :---: |
| INTEGRATED CIRCUITS LINEAR |  |  |  |  | ED |
|  |  |  |
|  |  | 103A A Amber |
| 709（8［ifin bil） | 40p |  |  |  | ぶi，iv2 tiv． |  |  | 27p |
|  |  |  |  |  |  |  |  | Ow |
| ES5． | 60p | $15 \mathrm{~J}, 18 \mathrm{y}, 30 \mathrm{y}$ ． | 1A |  | TILy09 Rma |

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X Components：4－Octave kerboard C．C E15．50，5－Octave keyboard nal tuning capacitor，GU500，tome generator，complete with exter divider unit complete with external tuning capacitor，GD500 650.00 ． Construction Manual for Portable Organ，using discrete components ELVINS ELECTRONIC MUSICAL INSTRUMENTS
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 MPGO type deck with magnetic cartridge. de luxe plinth and cover.
Two Duo Type lla matched speakers - tnclosure size approx. $19 \frac{1}{2}^{*} \times 10 \frac{1}{4}^{\prime \prime} \times 7 \frac{1}{4}^{*}$ in simulated teak Drive unit $13^{\prime \prime} \times 8^{\prime \prime}$ with $3^{\prime \prime}$ iweeter. 15 watts handling. 30 watis peak.
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System 2. $\mathbf{£ 8 5 . 0 0}$
Viscount IV amplifier (As System la\} MP60 rype dech (As System 1a)
Two Duo Type III matched speakers

- Enclosure size approx $27 \times 13^{\prime \prime}$ $\times 11 \frac{1^{\circ}}{2}$. Finished in teak simulate. Drive units $13^{\prime \prime} \times 8$ bass driver, and two 3 " (approx) Iweeters. 20 walts RMS. 8 ohms trequency range 20 Hz to 18.000 Hz .
Complete System with these
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PRICES: SYSTEM Ia Viscount iv R103
amplifier $£ 27.50+£ 190 \mathrm{psp}$. 2 Duo Type lia speakers $£ 30.00+£ 6.50 \rho \& p$. MP60 Iype deck with Mag. cartridge de fuxe plinth and cover $£ 22.00, £ 3 \mathbf{3 0} \mathrm{p} \% \mathrm{p}$ Total if purchased
separately: $£ 79.50$
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+ $\mathbf{f 6} .50 \mathrm{p}$ \& p

PRICES: SYSTEM 2
Viscount IV R 103
amplite: $\quad \mathbf{~} 27.50+\mathbf{f 1 . 9 0}$ p $p$.
2 Duo Type III
speakers $£ 46.00+£ 7.50 \mathrm{D} 8$
MP60 type deck wath Mag cartridge
de luxe plinth
Total if purchased
ratal if purchased
f95.50

EMI 350 KIT $\mathbf{f} 7.25+£ 1.20 \rho \& \rho$. Complete with crossover Components and circuit diagram

System consists of a $13^{\prime \prime} \times 8^{\circ \prime}$ approx. woofer with a $3^{\prime \prime}$ iweeter, crossover comporents and circuit diagram. Frequency response: 20 Hz to 20 KHz . Power handling 15 watts RMS into 8 ohms. (Peak 30 watts.)


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IWCOAPORATES: Pre-Amp with full mixing facilizies, including switched inpu tor mic with volume control, switched input lor auxiliary with volume control, bass and treble controls, volume contsol and blend contriol for turntables. Two B.S.R. MP60 type single play professional saries decks, fitted with crystal cartridges.

## TECHNICAL SPECIFICATION: Coneole size-

 Auxiliary inputs - 200 mV and Unit Open $\left.-351^{\prime \prime} \times 13 z^{\prime \prime} \times 4\right\}^{\prime \prime}$ (app.) 750 mV into 1 meg. Mic input -6 mV This disco console is ideally matched into 100K. 240 volt pperation. for the Reliant IV end Oisco 50 of any Turntables capacity - $7^{\prime \prime}$. $10^{\prime \prime}$ or other quality amplifier
$12^{\prime \prime}$ records. Rumble, wow and flurter Rumble Batter than -35 dB . Wow Better than $0.2 \%$. Flutter Better than $0.05 \%$ (Gsumont kalee meter)
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## Greenbank Electronics



The illustration shows the two P.C.B. module kits already asembled, one has 8 mm high digits, the other has 16 mm high digits. Also shown is an example of a complated clock.
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DL-750E $16 \mathrm{~mm}\left(0.6^{\prime \prime}\right)$ \& $1 \cdot 50$.
CMOS WITH DISCOUNTS! (Any mix: disc. $10 \% 25+, 25 \% 100+$ )

|  |  |  |  |  | $0 \cdot 80$ | 4066/14066 | 0.55 | 4096/ | $0 \cdot 8$ | 14515/4515 | 2.55 | 145431 | 1-50 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4000/14000 | $0 \cdot 15$ | 4023/14023 | - 0.60 | $4044 / 14044$ | 0.75 | 40671 - | $2 \cdot 5$ | 40971 - | $2 \cdot 95$ | $14516 / 4516$ | 1.10 | \|4549] | 2. |
| $4001 / 4001$ | -.15 | $4025 / 14025$ | 0.15 | 4045/ - | $1 \cdot 15$ | 4068/14068 | 0.15 | 40991 - | 1. 50 | $14517 /$ - | $5 \cdot 40$ | 14552 | 3. |
| $4006 / 14006$ | 0.95 | 4026 - | 1.40 | 4046/14046 | $1 \cdot 10$ | 4069/14069 | 0.15 |  |  | $14518 / 4518$ | 1.00 | $14553 /$ | 3-50 |
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| 4009/14009 | N/S | 40291- | $0 \cdot 90$ | 4049/14049 | $0 \cdot 45$ | 4072/14072 | 0.15 | 7003 ${ }^{\text {\% }}$ - | 4.25 | 14524/ $=$ | N/S | \|4557| - | $3 \cdot 20$ |
| 4010/14010 | N/S | 4030/14507 | 0.45 | 4050/14050 | 0.45 | 4073/14073 | 0.15 | 7083) |  | \|4526| | 1-50 | \|4558) - | 0.90 |
| $4011 / 14011$ | 0.15 | $4031 /$ - | 1.80 | $4051 / 14051$ | 0.75 | 4075/14075 | -1.25 |  |  | 14527/4527 | 1.20 | 14559 / | $2 \cdot 2$ |
| 4012/14012 | 0.15 | 4032/14032 | - $\cdot .5$ | 4052/14052 | $0 \cdot 75$ | 4076/14076 | - 0.15 |  |  | 14528/4098 | 0.85 | 14560 / | 1.55 |
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