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SEMICONDUCTORS TIP26 TIP36 AAZ12 Z5p BC214 14p IS100 15p TIP36 AC107 35p BC214L 15p IS103 15p TIP37 TIP37	0B 60p 2N2477 1B 65p 2N2646	30p CRS1/05 40p 50p CRS1/10 56p	TRIACS TXL228B 8A 400V 85p SC40D £1·40	★★SPECIAL OFFERS★★
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AC127 25p BC300 30p MJ2801 £1 25 TIP35 AC128 25p BC301 30p MJ2901 £1 95 TIP36	58 £2·71 2N2906 68 £3·50 2N2907	25p CRS1/60 90p 25p CRS3/10 62p	SC45E £2:10 SC50D £2:42	Price 1 -65p, 100 60p ea. 1,000 50p ea. 10,000 40p ea. 8% VAT.
AC176 25p BC302 36p MJE340 56p T1P41 AC187 27p BC303 35p MJE370 75p T1P42 AC188 27p BC303 35p MJE370 75p T1P42	2B 95p 2N3053	25p CRS3/20 62p	SC50E £2·70 DIAC 25p	MINIATURE MAINS TRANSFORMER, Primary 115/240v Sec. 18v/250 Ma at 80p ea.
ACY17 25p BCY32 95p MJE520 65p TIP30	OC 72p 2N3232	£1:35 CRS7/400 £1:00	LINEAR I.C.s LM304 Neg Voltage	+ VAT & postage 33p, 8% VAT.
ACY18 25p BCY33 66p MJ2955 £1:26 1P3 ACY19 25p BCY34 65p MJE3055 75p 11P32 ACY20 25p BCY38 65p MM1613 45p TIP33	2C £1.00 2N3553	£1-40 CRS16/200 90p	Reg. £2 10 LM309K 5V 1A,	MULLARD POT CORE TYPE FX2241 at 66p ea. + 33p p.p. 8% VAT.
ACY21 25p BCY39 95p MM1712 66p TIP34 AD140 66p BCY55 £1-56 MPF102 45p TIP35	4C £1:60 2N3702 5C £3:60 2N3703	12p CRS16/600 £1-60 12p C106B 45p	Voltage Reg. £2·16	24V D.C. SOLENOID by MAGNETIC DEVICES 60p each. 21 long x 1 x 1 in. +
AD142 60p BCY70 20p MPF103 TIP38 AD161 45p BCY71 20p (2N5457) 35p TIP41		12p C106D 70p 12p 40669 90p	LM723C 2:37V. 150m A	8% VAT. 240V. A.C. SOLENOID. Reversible opera-
AF114 25p BD121 75p (2N5458) 35p TIS50		12p TIC44 35p	Voltage Reg. 75p MFC4000 250mW	Non; twin coll. Size approx. 2 x 1 x 1 in.
AF115 25p BD123 85p MPF105 AF116 25p BD124 76p (2N5459) 46p ZTX3 AF117 25p BD131 46p OA47 16p ZTX5	00 15p 2N3709	14p BT10/500A 90p £1.50	Audio 75p TBA800 5 Watt	30 unmarked OC71 transistors £1 00 25 Unmarked 250mW Zener dlodes 4.7V,
AF118 50p BD132 50p OA70 10p ZTX5 AF124 30p BD135 50p OA79 10p ZTX5	01 20p 2N3772 i	£1-60 BRIDGE £1-80 RECTIFIERS	Audio 99p 709C Op Amp	5-1V, 6-2V, 7-5V, 9-1V, 10V, Measured and tested £1-66
AF239 60p BD136 56p OA81 10p ZTX5 BA102 30p BD139 75p OA90 10p ZTX5	2N3794 50 25p 2N3819	38p W02 1A 200V 38p	D.I.L./TO99 45p 741C Op Amp 8/14	Please state voltage required. 50 GE Diode OA47 equivalent. £1-00
BA112 50p BD140 87p OA91 10p N659 BA114 16p BD153 80p OA200 10p N914	8p 2N3823	76p MDA952/2 6A	D.I.L./TO99 35p 747C Dual Op	84F 600V WKG PAPER CAPACITORS, Ideal for Strobe Constructors £1-56 each
BA155 16p BD156 80p OA202 10p IN916 BA156 15p BDY17 £1-50 OA210 35p IN400: BC107 13p BDY18 £1-75 OA211 35p IN400:	1 8p 2N3904	85p 22p 25p	Amp £1 · 20 748C Op Amp D.I.L. 75p	+ 8% VAT + 33p post. Many other values of PAPER CAPACITOR's in stock. Phone for details.
BC108 12p BDY19 £1 90 OC16 90p IN4003 BC109 14p BDY20 £1 26 OC19 85p IN4004	3 9p 2N3906 4 16p 2N4014	25p ZENER DIODES 80p BZY88 Series	ZN414 Radio I.C .	JACKSON AIRSPACED CAPACITORS
BC109c 16p BF152 26p OC22 55p IN4009 BC113 13p BF166 36p OC26 65p IN4009	5 12p 2N4036 6 14p 2N4037	62p 400mW 44p 3:3V-33V 5% 11p	TAD100 Radio I.C. Inc. Filter £1.90	to suit ‡in, spindle: 100pF Two Gang at 55p + 25% VAT 500pF Two Gang at 75p + 25% VAT
BC114 13p BF178 35p OC28 99p IN400 BC115 15p BF180 35p OC35 60p IN4141 BC116 15p BF194 16p OC36 65p 2N696	8 7p 2N4059	14p 1.5W range 25p 14p 10W range 45p 12p	CA3014 £1·55 CA3018 £1·00 CA3028 £1·20	MULLARD TUBULAR CERAMIC UHF TRIMMERS (PROFESSIONAL)
BC117 29p BF195 16p OC42 48p 2N697 BC118 15p BF196 16p OC44 28p 2N698	25p 2N4061	12p L.E.D.	CA3036 £1 · 00 CA3046 95p	Type 092 0-8-2-2p
BC119 30p BF197 16p OC45 25p 2N706 BC143 25p BF200 35p OC70 15p 2N706	12p 2N4126 A 14p 2N4286	18p HP5082 28p	CA3048 £2:35 CA3075 £1:60	991 0·5-1·3p
BC147 12p BF224 18p OC71 12p 2N708 BC148 12p BF244J 18p OC72 20p 2N929	22p 2N4288	25p MA2082R 29p 27p L.D.R.	CA3089E £1 90 CA3090Q £4 85 MC1303L £2 20	QUANTITY DISCOUNTS PLEASE TELE- PHONE
BC149 12p BF245 45p OC75 25p 2N930 BC149c 14p BF259 55p OC76 25p 2N113: BC157 14p BFX29 36p OC77 44p 2N130:	2 25p 2N4290	25p ORP12 60p	MC1310P £2-80 SN76660 EQ	1000pF Feedthrough capacitor 5p ea. Miniature tubular P.C. trimmers 3:5-13pF
BC158 14p BFX34 3ep OC81 25p 2N130 BC159 15p BFX85 3ep OC83 25p 2N130	3 30p 2N4302 4 30p 2N4444 8	45p NE555 Timer 80p ε1·90 TO3 VOLTAGE R	TBA120 65p	6-30pF 19p ea. 4p c/o Varley 700 Ω relay 59p ea.
BC167 14p BFX86 30p OC84 25p 2N130 BC168 14p BFX88 30p OC139 30p 2N130	15 36p 2N4871 16 36p 2N4903 £	£1-30 L005 5V 650mA £036 12V 600mA		Gold Flashed professional TRANSISTOR SOCKETS. To suit small signal TO18.
BČ189 14p BFY10 35p OC170 25p 2N130 BČ169c 15p BFY44 56p OC171 36p 2N130 BČ172 13p BFY50 25p OC200 66p 2N130	8 30p 2N5069 4	90p L037 15V 450mA £1⋅30	£1-60 ea,	etc. 30 for £1-90 + 8% VAT. W. WOUND POTS 1 Ω-100K Ω at 30p each
BC182 12p BFY51 25p OC201 60p 2N161; BC182L 12p BFY52 25p OC202 75p 2N171;	3 30p 2N5192 4	96p £1·20 VEROBOARD £1·10 01 23	0-1 0-15	Colvern or Reliance styles + 25% VAT VERO EDGE CONNECTOR 24 way 1"
BC183 12p BFY53 25p TIP29A 45p 2N189 BC183L 12p BFY90 65p TIP30 55p 2N214	0 60p 2N5195 # 6 15p 2N5245		32p 23p 35p 35p	pitch 36p each + 8% VAT. All the other sizes in stock.
BC184 12p BSV68 70p TIP31A 57p 2N214 BC184L 12p BSW63 65p TIP32A 69p 2N216 BC185 35p BSW68 80p TIP33A £1-00 2N221	7 90p 2N5296	55p 3½ x 5 50p 17 x 2½	35p 35p 48p 41p £1:85 79p	SIEMENS VARLEY RELAY 4P C/O 700 Ω 24V 50p each.
BC185 35p BSW68 86p TIP33A £1.06 2N221 BC186 27p BSX19 15p TIP34A £1.46 2N221 BC212 12p BSX20 15p TIP35A £3.26 2N221	8 25p 2N5458	35p 17 x 3½ 35p 17 x 5	£1:43 £1:12 £1:84 —	PLESSEY RELAY 2 P C/O 6V operation 40p each.
BC212L 14p BSX21 25p TIP36A £3-50 2N222: BC213 12p BY127 26p TIP41A 76p 2N222:	2 20p 2N5485	40p PIN INS. TOOL 55p SP.F. CUTTER 55p 100 PINS SS	72p 72p 52p 52p	MODERN DISC CERAMICS £1 00 a hundred, £8 00 a thousand + 25% VAT.
BC213L 12p BY164 65p TIP42A 85p 2N2300 QTY. DISCOUNTS: 12+ 10%; 25+ 15%; 100+20%		55p 100 PINS SS 65p 100 PINS DS 40p 500 PINS SS	30p 30p 30p 30p £1:55 £1:55	Phone or write for list.
	47 £1-50 SN7481 4	£1-25 500 PINS DS	£1·55 £1·55	CIL SOCKETS, 8 pln 14p, 14 pin 14p, 16 pin 14p, Mica Washers + 2 Bushes (TO3 or
TL (full stocks available) SN7400 18p SN7411 23p SN7430 20p SN745 SN745			op each	TÖ66) 4p.
SN7401 18p SN7412 22p SN7432 42p SN475 SN7402 20p SN7413 48p SN7433 76p SN745	53 20p SN7486	45p U.H.F. V.S.W.R. 75p transmitters £5 eac	probes ex U.H.F.	METAL BOXES
SN7403 20p SN7416 30p SN7437 50p SN746 SN7404 20p SN7417 30p SN7438 50p SN747	60 20p SN7491A 70 30p	All the above are new £1.09 Please add 8% VA	vin original packets.	ALUMINIUM BOXES IDEAL FOR VERO- BOARD WITH BASE & P.K. SCREWS
SN7405 28p SN7420 28p SN7440 28p SN74 SN7406 38p SN7422 38p SN7441 AN75p SN741 SN7407 38p SN7423 38p SN7442 75p SN741	73 40p SN7493	75p POTENTIOMETER	RS	AB7 22 Long 52 Wide 11 High 55p AB8 4" 4" 11 55p
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SN7410 18p SN7428 50p SN7446 £2-00 SN748	80 80p SN7497 #	£2.25 Rotary Switched 2	25p —	AB11 4" 2½" 2" 65p AB12 3" 2" 1" 56p
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MULTICORE CABLE. 20 way 14/0076 + Screen at	70p KOKUSA	AI MECHANICAL FILTER	455 Kc/S, 6 Kc/S	AB15 8" 6". 3" £1·16 AB16 10" 7" 3" £1·32
per yard+postage by weight. MULTICORE CABLE. 25-way, individually screen 14/0076. £1:00 per yard+V.A.T. Postage by weight.		teal for A.M. £5 each INC VA	i. Fostage 33p each,	AB17 10" 4\frac{1}{2}" 3" £1.10 AB18 12" 5" 3" £1.32
3 CORE PVC INSULATED MAINS CABLE, GE	REY 360Ma Se	FORMER 240V A.C. Prima econdary £12+8% VAT+£1		AB19 12" 8" 3" £1.80 ALUMINIUM BOXES WITH SLOPING
ML5650, 3x7/0-2mm, Price 100m-£4-56. 1,000m-£35. 10,00 £336. METAL OXIDE RESISTORS TR4/5/8 in stock.	OMRON	OCTAL RELAY 246V A.C.	. 3P c/o 75p each+	TOP PANEL—IDEAL FOR PRE-AMPS, ETC., USING SLIDER CONTROLS AB20 8" Long 9" Wide 34" High at back £2:26 2" High at front 6" Slope to front
values. 1-off price 3p each. Discount on quantity. 16 TURN TRIMPOTS by Bourns, Mec, Painton, etc.	All SLEEVIN	€G 2000 pleces approx. size ‡	x 2mm. Price £1 · 00	With P.K. Screws AR21 As above but 10" long £2:29
values in stock. 50p each. Discount on quantity.	+33p P&P	P+VAT 8%		AB22 As above but 12" long £2-60

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We have the largest retail selection of components available. Phone or write if you are in difficulties obtaining a particular component.

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PRACTICAL WIRELESS

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BACK NUMBERS

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FOR SPEAKERS AT FANTASTIC REDUCTIONS

ELIZABETHAN

This compact Tuner Amplifier gives you full medium wave and V.H.F. coverage and FM stereo. With inputs for your turntable and tape recorder. It has rotary tuning. Volume, Balance, Bass and Treble controls and push

button selection switches for Plano/tape FM Stereo, FM mono. Medium wave and A.F.C. has built-in stereo beacon and switched headphone socket

Technical Specifications 15 transistors 11 diodes, integrated circuit.

4" x 10" x 151" approx. Finished in selected rosewood veneer with brushed aluminium front panel and matching controls



£29:00

STEREO CASSETTE TAPE DECK

This compact stereo cassette deck is designed to link up with your stereo system. It incorporates features normally found in machines costing far more, these include large illuminated recording level meters, slider level controls, Chromium Dioxide (CrO₂) selector switch. pause control, and autostop, tape/digit counter, Din or Phono connections, twn mic. inputs and outputs for your stereo headphones Technical Specifications – Input level Mic – 65dB into 10K Ω , Line in 20dB into 1MΩ, DIN - 47dB into 100KΩ. Output levels Line out 500Mv 10K Ω , 0IN - 500Mv 10K Ω . Frequency response - Normal 50-10KHz, Chrome 50-14KHz, Signal noise, ratio - better than 40dB



EASY BUILD SPEAKER KIT compact bookshelf speaker system giving a high electro accoustic efficiency for the low powered amplifier

The professional finish can be obtained with the minimum of tools, the infinite baffle type enclosures come ready mitred and professionally finished, simply apply glue fold up around baffle hoard, and fix together with masking tape till glue dries.

The cabinet measures 12"x9"x5" deep approx finished in simulated teak, incorporating a quality 7"x4" elliptical speaker, power handling 4 watts, flux density 30,000 naxwells, impedance 8-15 ohms nominal, voice coil dia 3" magnet size 27" approx.



£6.00 pair inclusive.P & P £1.70

EASY TO BUILD SPEAKER KITS

These superb simulated teak-finished speaker kits have been specially designed by RT-VC for the cost-conscious hi-fi enthusiast who wants top quality speakers but

doesn't want to spend the earth. Built to EMI's exacting specification, these new RT-VC speaker kits (350 type kit) incorporate 13" \times 8" woofer, $3\frac{1}{4}$ " tweeter and matching crossover.

Easily put together with just a few basic tools. Specification (each speaker): Impedance 8 ohms. Power handling 15 watts RMS (30 watts peak). Response 20—20,000 Hz: Size 20" × 11" × 9\frac{1}{2}" approx. Comparable built units (EMI LE3) sold elsewhere for over £45 pair

£22.00 pair complete +£5.20 p & p.

Complete with crossover Components and circuit diagram

diagram







£7.25 +£1.20 p & p.

Complete with crossover Commonents and circuit

System consists of a 13" approx. woofer with a 3" tweeter, crossover components and circuit diagram. Frequency response: 20 Hz to 20 KHz. Power handling 15 watts RMS into 8 ohms. (Peak 30 watts.)

System 1a. £69.00

The new 20 + 20 watt Stereo Amplifier incorporating the latest silicon transistor solid state circuitry, the RT-VC VISCOUNT IV gives you a powerful 20 watts RMS per channel into 8 ohms: Superb teak-finished cabinet, with anodised fascia to harmonise with any decor. Polished trim and knobs.

The VISCOUNT IV has a comprehensive range of controls - volume, bass, treble, balance, mono/stereo, mode selector, and scratch filter

Front panel socket for stereo headphones. And a host of sockets at the rear - for left and right

speakers, tape recorder, auxiliary, tuner, disc and microphone.

SPECIFICATION: 20 watts RMS per channel 40 watts peak. Suitable 8-15 ohms speakers. Total distortion = 10 watts better than 0.2%. Six switched inputs: 1. Magnetic P.U. = 3 millivolts & 47 K ohms (R.I.A.A.): 2. Crystal/ceramic P.U. = 50 millivolts & 50 K ohms (R.I.A.A.): 3. 4, 6. Tape Tuner/Aux. = 140 millivolts & 50 K ohms (RI.A.A.): 3. 4 Six per Source Control of the Contr

50 K onms (that frequency response). CONTROLS. Push button DN/OFF, stereo/mono, scratch filter. 6 position rotary selector. Individual rotary controls for treble, bass, balance and volume. Headphone socket, tape out socket. Aux. mains output. Frequency response: 25 Hz to 25 KHz $_{\rm F}$ full rated output. Signal to noise ratio: better than -50 dB on all inputs. Tone control range: Bass ± 15 dB ≈ 50 Hz; Treble ± 12 dB ≈ 10 KHz. Power requirements: 200-250 x AC mains ≈ 60 walts. Approx. size: $15\frac{1}{8}$ x 3 x 10". MP60 type deck with magnetic cartridge, de luxe plinth and cover.

Two Duo Type If a matched speakers – Enclosure size approx $19\frac{1}{3}$ " \times $10\frac{1}{4}$ " \times $7\frac{1}{4}$ " in simulated teak. Orive unit 13° \times 8° with 3° tweeter, 15 watts handling, 30 watts peak.

Complete System with these speakers £69.00 +£6.50 p & p.

System 2. £85.00

Viscount IV amplifier (As System 1a) MP60 type deck (As System 1a) Two Duo Type III matched speakers Enclosure size approx. $27^{\circ} \times 13^{\circ}$ $11\frac{1}{2}^{\circ}$. Finished in teak simulate Drive units 13" x 8" bass driver, and two 3" (approx.) tweeters. 20 watts RMS, 8 ohms frequency range — 20 Hz to 18,000 Hz.

Complete System with these speakers £85.00 +£7.60 p & p.

PRICES: SYSTEM 1a

Viscount IV R103 £27.50 +£1.90 p & p 2 Dun Tyne tla £30.00 + £6.50 p & p. speakers MP60 type deck with Mag. cartridge de luxe plinth f 22 00 + f 3.30 p & p. and cover Total if purchased

separately: £79.50
Available complete for only: £69 00

+£6.50 p & p.

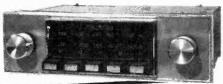
PRICES: SYSTEM 2

Viscount IV R103 amplifier £2 £27.50 +£1.90 p & p 2 Duo Type III £46.00 + £7.50 p & speakers MP60 type deck with Mag. cartridge de luxe plinth f22 00 + f3.30 p& p Total if purchased

+£7.60 p & p. System 1a £1.75 System 2 £3.50



PUSH BUTTON CAR RADIO KIT— THE TOUR



NO SOLDERING REQUIRED

NOW BUILD YOUR OWN PUSH BUTTON CAR RADIO

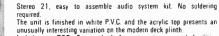
Easy to assemble construction kit comprising fully completed and tested printed circuit board on which no soldering is required. All connections are simple push fit type making for easy assembly. Fine tuning push button mechanism is fully built and tested to mate with printed circuit board.

TECHNICAL SPECIFICATION: (1) Output 4 watts RMS output. For 12 volt operation on negative or positive earth. (2) Integrated circuit output stage, pre-built three stage IF Module.

Controls volume manual tuning and five push buttons for station selection, illuminated tuning scale covering full, medium and long wave bands.

Size chassis 7" wide 2" high £9.50+£1.05 p & p. and 43" deep approx. Speaker including baffle and fixing strip £2.00 +45p p & p. Car Aerial Recommended – fully retractable £1.60 + 40p p & p.

The Tourist I Kit For the experienced constructor. If you can solder on a printed circuit board you can build this model. Same technical specification as Tourist TT. Price £8.20+£1.05 p & p.



unusually interesting variation on the modern deck plinth.
Includes — BSR 3 speed deck, automatic, manual lacilities together with stereo cartridge.

Two speakers with cabinets. Amplifier module. Ready built with control panel, speaker leads and

full, easy to follow assembly instructions.

Specifications — For the technically minded.

Input sensitivity 600mV, Aux. input sensitivity 120mV. Power output 2.7 watts per channel Output impedance 8-15 ohms. Stereo headphone socket with automatic speaker cutout. Provision for auxiliary inputs — radio, tape, etc., and outputs for taping discs. Overall Dimensions. Speakers approx 15\frac{1}{3}\cong \times 8'' \times 4''. Complete deck and cover in closed position approx 15\frac{1}{3}\cdot' \times 12" \times 6''.

Complete only £23.20 +£3.00 p & p.

Extras if required. Optional Diamond Styli £1.60. Specially selected pair of stereo headphones with individual level controls and padded earpieces to give optimum performance £5.80



Reliant Mk IV Mono Amplifier, ideal for the small disco or house parties. Output 20 watts RMS into 8 ohms (suitable for 15 ohms).

Inputs *4 electrically mixed inputs. *3 individual mixing controls. Separate bass and treble controls common to all 4 inputs. Mixer employing F.E.T. (Field Effect Transistors). Solid State circuitry. Attractive styling.

INPUT SENSITIVITIES - Input - 1). Crystal mic. guitar or moving coil mic, 2 and 10mV. (Selector switch for desired sensitivity.) – Inputs – 2), 3), 4). Medium output equipment – ceramic cartridge, tuner, tape recorder, organs, etc. – all 250mV sensitivity. AC Mains, 240V operation. Size approx: 121"×6"×31" £20.00 +£1.35 p & p.

CK HOME CARTRID



Elegant self selector push button player for use with your stereo system. Compatible with Viscount IV system, Unisound module and the Stereo 21. Technical specification Mains input, 240V, Output sensitivity 125mV

Yours for only

£16.20 +£1.70 p & p.

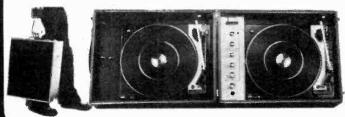
.D YOUR OWN STEREO AMPLIFIER*



For the man who wants to design his own stereo - here's your chance to start, with Unisound - pre-amp, power amplifier and control panel. No soldering - just simply screw together. 4 watts per channel into 8 ohms. Inputs: 120mV (for ceramic cartridge). The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion over the audio spectrum, 240V, AC only,

Also available with 2 speakers (7°x4°) £10 \pm £1.75 p & p. f E8.95 \pm £1.05 p & p. Also available with the 'Compact' (see opposite page) easy build speaker kit £13.50 + £2 p & p

BLE DISCO CONSI



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BN7416	0.86	8N7470	0 86	8N74119	1.68			1.4.1	
BN7413	0.86	BN7460	0.18	BN74118	0.90			100	
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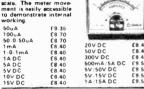
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50uA	£4.20		1
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200 u A	£4.10	1	
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1mA	€4.05		1000
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200u A	£4 60	The same at the same	
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50 - 0 - 50 u A	£4.65	A.	- 1
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1mA	€4.50		188 20
5mA	€4.50		2.0
10mA	€4.60	-	-
50mA	€4.50	10V DC	£4 50
100mA	£4 50	ZOV DC	£4.50
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Size: 42 x 42mr		JULE WIN JOF	
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100uA	£3.40	1 Leaning	. T
200-4A	£3.30	* STEEL	30
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50-0-50uA	£3.40	0 44	a 1
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500uA	£4 15	* 5555 A	2000
50-0-50uA	£4.25	1 2 2	× .
100-0-100uA	€4.20	\ ~-	- 1
500-0-500uA	€4.10	Decuring	
1mA	£4 10	11111111	
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MODEL AF. 105 VOM 50,000 opv. Mirror scale. Meter protection. 0/-3/3/12/60/120/ 300/600/1200V DC. 0/6/30/120/ 300/600/1200V DC 0/30uA/6/

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Ranges: 0,3/1.5/6/
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100 V		60 0.70		78 0 78	0.83 0.83	1-01 1-01
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			1 Eart	h		
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250	152	13.81	0.98	10.31	1.18	
350	153	18.54	0.98	12.50	1.28	
500	154	18-38	0.98	14.31	1.44	
750	155	28-72	1.25	22-12	O.A.	
1000	156	37-44	1 25	30.57	O.A.	
1500	157	44-37	1.25	34-98	O.A.	
2000	158	52.45	2.95	38-91	O.A.	
3000	159	77.18	2.95	61-51	O. A.	
12 8	24	Volts	Prim 2	00-240V		

Amps Ref Price

	12V	24V	No.	4	4
	0.3	0.15	242	1.66	0.34
	0.5	0.25	111	1.60	0.46
	1	0.8	213	1.90	0.61
1	2	1	71	2.47	0.61
	4	2	18	3.07	0.62
	6	3	70	4.50	0.72
	8	4	108	5-11	0.85
	10	5	72	5-68	0.85
i	12	6	116	5.80	0.85
	16	8	17	7.26	0.97
	20	10	115	10.96	1.18
	30	15	187	14 06	1.36
	40	20	232	15.63	O.A.
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Prim.	200-240V. Ref.	Sec.	12, 15, 20, Price	24, 80V. Post
	No.		£	4
0.5	112		2.04	0.61
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5	51		6.75	0.95
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ı	Sec. 1	Bec. 2	Sec. 1	Sec. 2	No.		4
ı	3-0-3	_	200	_	238	1.56	0.34
1	06	0-6	500	500	234	1.56	0.34
1	0-6	0-6	1000	1000	212	2.12	0.46
ı	9-0-9	_	100	_	13	1.60	0.34
ı	0-9	0-9	330	330	235	1.62	0.34
1	0-8-9	0-8-9	\$00	500	207	1.69	0.46
d	0-8-9	0-8-9	1000	1000	208	2.79	0.46
ı	15-0-15		40		240	1.55	0.34
ı	015	015	200	200	236	1.56	0.34
ı	20-0-20	_	30	_	241	1.55	0.34
ı	0-20	0-20	150	150	237	1.56	0.34
1	0-15-20	0-15-20	500	800	205	2.88	0.58
Į	0-20	0-20	300	300	214	2.03	0.61
1	0-20	_		NO SCREEN	1116	3.45	0.97
	20-12-0-12-20	1000	700 (ID/0		221	2.50	0.61
	0-15-20	0 - 15 - 20	1000	1000	206	2.85	0.72
	0-15-27	0-15-27	500	500	203	3.16	0.58
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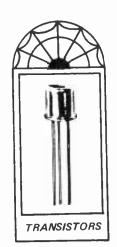
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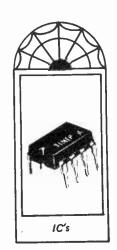
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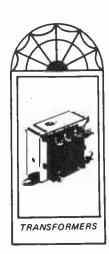
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AC179 0.29	OC22 0-47	BC108 0	08 2N3	054 0-47	BF273	0.86
AC180 0-20 AC180K 0-30	OC23 0-49 OC24 0-57		008 2N3		BF274 BFW20	0.86
AC181 0-20	OC24 0.57 OC25 0.89	BD137 0	.41 2N3	319 0·15 391 A 0·17	BFX29	0·61 0·28
AC181K 0-80	OC26 0-80		-51 2N3	392 0.15	BFX84	0.22
AC187 0-22	OC28 0.51	BD139 0	-56 2N3	393 0-15	BFX.85	0.81
AC187K 0.28	OC29 0.51	BD140 0	-61 2N3	394 0-15	BFX86	0.22
AC188 0-22 AC188K 0-23	OC35 0-48 OC36 0-51	BD155 0 BD175 0	81 2N3		BFX87	0.25
ACY17 0.26	OC41 0.20	BD176 0	-61 2N3		BFX88 BFY50	0·22 0·20
ACY18 0.20	OC42 0.25	BD177 0	67 2N3	104 0.29	BFY51	0.20
ACY19 0.20	2N918 0-81		67 2N3		BFY52	0.20
ACY20 0.20	2N929 0.21	BD179 0	·71 2N3	114 0-16	2G309	0.87
ACY21 0.20	2N930 0.21	BD180 0	·71 2N3		20339	0.20
ACY22 0.17 ACY27 0.19	2N1131 0.20 2N1132 0.22	BD185 0	67 2N3	116 0.29	2G339A	0.17
ACY27 0-19 ACY28 0-19	2N1132 0.22 2N1302 0.15	BD186 0 BD187 0	·67 2N3	17 0-29 25 0-77*	2G344 2G345	0·19 0·17
ACY29 0.86	2N1303 0.15		71 2N3		2G371	0.17
ACY 30 0-29	2N1304 0·18	BD189 0	·77 2N36	15 0.76	2G371B	0.12
ACY31 0.29	2N1305 0-18	BD190 0	·77 2N36	16 0.76	2G373	0.18
ACY34 0.21	2N1306 0.21	BD195 0	·87 2N36	346 0-09	2G374	0.18
BC173 0.15 BC174 0.15	2N1307 0.21 2N1308 0.24	BD196 0 BD197 0	-87 2N37	02 0.18	2G377 2G378	0.81
BC175 0-22	2N1309 0-24		92 2N37		2G378 2G381	0·17 0·17
BC177 0-19	2N1613 0-20	BD199 0	98 2N37		2G382	0.17
BC178 0-19	2N1711 0.20	BD200 0	98 2N37	06 0.12	2G401	0.81
BC179 0-19	2N1889 0-82	BD205 0	81 2N37	07 0-18	2G414	0.81
BC180 0.25	2N1890 0.46	BD206 0	81 2N37	08 0.08	2G417	0.26
BC181 0-25 BC182 0-15	2N1893 0.38 2N2147 0.78		98 2N37		2N388	0.86
BC182L 0.15	2N2148 0.58	BDY20 \$1	98 2N37 02 2N37	10 0.09 11 0.09	2N388A 2N404	0·56 0·20
BC183 0·15	2N2192 0-86		25 2N38	19 0.29	2N404A	0.29
BC183L 0.15	2N2193 0-86	BF117 0-	46 2N38		2N524	0.48
BC184 0-20	2N2194 0.86	BF118 0	71 2N38		2N527	0.50
BC184L 0.20 BC186 0.29	2N2217 0.22 2N2218 0.20	BF119 0-	71 2N38		2N598	0.48
BC187 0.29	2N2218 0.20 2N2219 0.20	BF121 0- BF123 0-	46 2N39 51 2N39	03 0.29 04 0.81	2N 599 2N 696	0·46 0·18
BC207 0·11	2N2220 0.28		46 2N39	05 0.29	2N697	0.14
BC208 0·11	2N2221 0-20	BF127 0	51 2N39		2N698	0.25
BC209 0·18	2N2222 0.20	BF152 0-	56 2N40	58 0.12	2N699	0.86
BC212L 0.18 BC213L 0.18	2N2368 0-18 2N2369 0-15	BF153 0-	46 2N40		2N706	0.08
BC214L 0.17	2N2369 0-15 2N2369A 0-15	BF154 0- BF155 0-	46 2N40 71 BC11		2N706A 2N708	0·09 0·12
BC225 0-26	2N2411 0.25	BF156 0-	49 BC11		2N711	0.81
BC226 0-86	2N2412 0.25	BF157 0-	56 BC11	5 0.16	2N717	0.86
BC301 0.28	2N2646 0.48	BF158 0	56 BC11	6 0-16	2N718	0.25
BC302 0-25 BC303 0-81	2N2711 0.21		61 BC11	7 0-19	2N718A	0.51
BC303 0.81 BC304 0.87	2N2712 0-21 2N2714 0-21	BF160 0- BF162 0-	41 BC11 41 BC11	8 0·10 9 0·81	2N726 2N727	0·29 0·29
BC440 0.81	2N2904 0·18	BF163 0-	41 BC12		2N743	0.20
BC460 0.87	2N2904A 0.21		41 BC12	5 0.18	2N744	0.20
BCY30 0.25	2N2905 0.21	BF165 0-	41 BC12	6 0.19	2N914	0.15
BCY31 0.27 BCY32 0.81	2N2905 A 0.21 2N2906 0.16	OC44 0-	16 BC13 18 BC13		2N4061	0.12
BCY32 0-81 BCY33 0-22	2N2906 0-16 2N2906A 0-19	OC45 0- OC70 0-	18 BC13 10 BC13	4 0·19 5 0·12	2N4062 2N4284	0·12 0·18
BCY34 0-26	2N2907 0.20	OC71 0-	10 BC13		2N4284 2N4285	0.18
BCY70 0.15	2N2907A 0.22		15 BC13	7 0.16	2N4286	0.18
BCY71 0-20	2N2923 0·15		15 BC13	9 0.41	2N4287	0.18
BCY72 0-15 BCZ10 0-20	2N2924 0-15 2N2925 0-15	OC75 0:	16 BC14	0 0.81	2N4288	0.18
BCZ10 0.20 BCZ11 0.26	ACY35 0-21	OC76 0:	16 BC14 26 BC14	1 0.81 2 0.81	2N4289 2N4290	0·18 0·18
BCZ12 0.26	ACY36 0.29	OC81 0	16 BC14	3 0.81	2N4290 2N4291	0.18
BD115 0.68	ACY 40 0-18	OC81D 0	16 BC14	5 0-46	2N4292	0.18
BD116 0-81	ACY41 0-19	OC82 0:	16 BC14	7 ' 0.10	2N4293	0.18
BD121 0-61 BD123 0-67	ACY44 0.86 AD130 0.89	OC82D 0	16 BC14		2N5172	0.12
BD123 0.67 BD124 0.70	AD130 0-89 AD140 0-49	OC83 0: OC139 0:	20 BC14		2N5194	0.56
BD131 0.51	AD142 0-49	OC140 0:			2N5294 2N5296	0-56 0-56
BD132 0-61	AD143 0-89	OC169 0-	26 BC15	2 0.18	2N5457	0.82
BD133 0-67	AD149 0.51	OC170 0-1	26 BC15		2N5458	0.88
BD135 0-41	AD161 0.86	OC171 0:	26 BC15	4 0.81	2N5459	0.41
BFY53 0·18 B8X19 0·16	AD162 0-86	OC200 0-1	26 BC15	7 0.19	2N6122	0.69
B8X19 0-16 B8X20 0-16	ADI61 &	OC201 0-1 OC202 0-1			28301 28302A	0.51
BSY25 0.16	AD162(MP) 0-69	OC202 0-1			28302A 28302	0·48 0·48
BSY26 0.16	ADT140 0.51	OC204 0:	26 BC16	0.51	28303	0.56
BSY27 0-16	AF114 0:25	OC205 0-1	86 BC16	7 0-12	28304	0.71
B8Y28 0-16 B8Y29 0-16	AF115 0.25	OC309 0-4	11 BC16	8 0-12	28305	0.80
BSY38 0.19	AF116 0.25	OCP71 0-44 ORP12 0-44	BC16 BC17		28306 28307	0.80
BSY39 0-19	AF117 0-25	ORP60 0.41			28321	0.75
					_	

SEMICONDUCTORS

1								_ `	450		•
*		74	SER	IES	T.T.I	L. I.	C's	1	TITE	111	A
BI-PAK	STIL	L LO	WEST	IN PRI	CE. FUI	L SP	ECIFIC	ATION G	HARA	TERT	N D ATT
				PAMOL	B MANI	TEACT	URER	A.	0 1116111	, , , , , ,	, Au
Type	Ou	antitie	,	Type		antities		Type	٥	antities	
1 - 22	1 -	25	100 +	1 ppc	1	25	100+	1 ype	1 44		
7400	0.14	0.18	0.12	7448	£1.02	0.99	0.97	74122	0.65	25 0.68	100+
7401	0.14	0.18	0.12	7450	0.14	0.18	0.12	74123	0.69		0.60
7402	0.14	0.13	0.12	7451	0.14	0.18	0.12	74141	0.79	0.68 0.76	0.65
7403	0.14	0.18	0.12	7453	0.14	0.18	0.12	74145			0.78
7404	0.14	0.18	0.12	7454	0.14	0.18	0.12	74140	21.20	£1-16 £1-80	
7405	0.14	0.18	0.12	7460	0.14	0.18	0.12	74151	\$1.02	0.97	£1.20 0.98
7406	0.86	0.21	0.28	7470	0.80	0.27	0.25	74153	0.98	0.88	0.83
7407	0.86	0.81	0.29	7472	0.80	0.27	0.25	74154		£1.48	£1.48
7408	0.28	0.22	0.21	7473	0.88	0.86	0.32	74155	81.11	\$1.06	\$1.02
7409	0.28	0.22	0.21	7474	0.88	0.86	0.82	74156		£1.06	\$1.02
7410	0.14	0.18	0.12	7475	0.56	0.54	0.58	74157	0.98	0.88	0.83
7411	0.28	0.22	0.21	7476	0.41	0.40	0.89	74160		£1.25	£1.20
7412	0.26	0.25	0.24	7480	0.56	0.54	0.51	74161	81.90	\$1.25	\$1.50
7413	0.80	0.29	0.28	7481	1.02	0.97	0.98	74162	#1.90	\$1.25	#1·20
7416	0.28	0.27	0.26	7482	0.88	0.79	0.74	74163		£1.25	£1.20
7417	0.28	0.27	0.26	7483	#1-11		0.97	74164		\$1.62	\$1.55
7420	0.14	0.18	0.12	7484	0.98	0.90	0.88	74165	41.47		\$1.55
7422	0.28	0.27	0.26	7485	£1.48	\$1.44		74166	#1.49	£1-44	£1.89
7423	0.87	0.86	0.86	7486	0.82	0.81	0.80	74174		\$1.44	\$1.39
7425	0.87	0.86	0.85	7489	\$8.70			74175	\$1.02	0.97	0.88
7426	0.87	0.85	0.88	7490	0.60	0.58	0.56	74176	81.10 81.10	81 11	\$1.06
1427	0.87	0.85	0.88	7491	£1.02	0.97	0.98	74177	41.16	\$1 11 \$1 11	£1-06
7428	0.42	0.89	0.87	7492	0.69	0.66	0.59	74180	41.16	\$1.11	£1 06
7430	0.14	0.18	0.12	7498	0.69	0.66	0.59	74181	48-66	£8-56	\$8-47
7432	0.87	0.85	0.88	7494	0.79	0.76	0.69	74182	41.14	\$1.11	81.08
7433	0.89	0.87	0.85	7495	0.79	0.76	0.69	74184	81-87	\$1.62	41.66
7487	0.88	0.80	0.28	7496	0.89	0.86	0.80	74190	41-81	£1.78	\$1.71
7438	0.82	0.80	0.28	74100	#1-89	£1.84	£1.30	74191	£1 81	£1.76	81.71
7440	0.14	0.18	0.12	74104	0.56	0.54	0.51	74192	£1·81	\$1.76	81.71
7441	0.69	0.66	0.59	74105	0.56	0.54	0.51	74193		"1·78	\$1.71
7442	0.69	0.66	0.59	74107	0.41	0.89	0.87	74194		£1·16	#1·11
7443	\$1.11	£1.06	£1.02	74110	0.56	0.51	0.46	74195	£1.02	0.97	0.98
7444	\$1.11		\$1.02	74111	0.88	0.81	0.78	74196		\$1.06	£1 02
	£1·48		£1·39	74118	0.98	0.88	0.88	74197			\$1.02
7446	£1·11	£1.06	£1·02	74119	£1.89		£1-20	74190	42-55	42.50	
7447	£1.02	0.99		74121	0.46	0.44	0.41	74199	£2-31	#2-21	42-11
Devices n	asy be	mixed	to quali	fy for a	uantity p	rice. (7	TL 74	series only) data i	avails	able for
the above	series	of I.C'	s in boo	klet forn	. PRICE	35p.			,	ma	

1 25 100+ 1 25]	RIES	30 SE	D.T.L.		*	*
BP930 014 018 012 BP944 015 014 018 BI BP932 015 014 013 BP945 0.28 0.26 0.23 BI BP935 015 014 013 BP946 014 013 012 BI BP935 015 014 013 BP946 0.28 0.26 0.23 BI BP935 015 014 013 BP946 0.28 0.26 0.23 BI	pe Quantities	Type	Quantities	Type		Qu	Type
BP932 0-15 0-14 0-13 BP945 0-28 0-26 0-23 B BP933 0-15 0-14 0-13 BP946 0-14 0-13 0-12 B BP935 0-15 0-14 0-13 BP948 0-28 0-28 0-28 0-28 BB	1 25 100+	100+	1 25		5 100+	25	1
BP932 0.15 0.14 0.18 BP945 0.28 0.26 0.23 B BP933 0.15 0.14 0.18 BP946 0.14 0.18 0.12 B BP935 0.15 0.14 0.18 BP946 0.28 0.28 0.28 B		0.18 BP96	0.15 0.14	BP944	18 0.12	4 0.18	BP930 0-14
BP933 0.15 0.14 0.18 BP946 0.14 0.18 0.12 B BP935 0.15 0.14 0.18 BP948 0.28 0.26 0.28 B				BP945	14 0.18	5 0-14	BP932 0.15
BP935 0-15 0-14 0-18 BP948 0-28 0-26 0-23 B						5 0.14	BP933 0.15
							BP935 0:15
BP936 0-15 0-14 0-13 BP951 0-65 0-60 0-56 B1				BP951			BP936 0.15

6 Am 10 Am	TO66 TO48	0 51 0·77	0 61 0 92	0·77
*	D.I.L. SOC	KET	s	1
mant4	14 = 4 = 4 = 4	1	25	100+
T8016	14 pin type 16 pin type	081	0.28	0.25
	24 pin type 8 pin type (low cost)	0.69	0.64	0.60
BP814	14 pin type (low cost) 16 pin type (low cost)	0-15 0-16	0·18 0·14	0-11

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LINEAR I.C's

Type	Qua	ntities		Type	Que	antities		Type	Qu	antities	
	1	25	100 +		1	25	100+		1	25	100 +
72702	0.46	0.44	0.42	8L701C	0.46	0.42	0.87	uA723C	0.45	0.48	0.40
72709	0.28	0.21	0.19	8L702C	0.48	0.42	0.87	76003	£1·39	\$1.84	£1-80
72709P	0.19	0.18	0.17	TAA263	0.74	0.65	0.56	76023	\$1.89		\$1.80
72710	0.88	0.81	0.28	TAA293	0.98	0.88	0.88	76660	0.88	0.86	0.88
72741	0.28	0.27	0.26	TAA350	A.			LM380	0.88	0.90	0-88
72741C	0.26	0.25	0.24		#1.71	£1-67	£1.57	NE555	0.45	0.48	0.40
72741P	0.28	0.27	0.26	uA703C	0.26	0.24	0.22	NESS6	0.88	0.86	0.88
72747	0.79	0.74	0.61	uA709C	0.19	0.18	0.17	TBA800	\$1.89	£1.84	£1.80
72748P	0.85	0.88	0.81	uA711C	0.88	0.81	0.28	ZN414	\$1.11	-	27.00
8L201C	0.46	0.42	0.87	uA712C	0.88	0.81	0.28				

SILICON RECTIFIERS

	300mA	750mA	1 Amp	1.	5Amp	3Amp	10Amp	30Amp
PIV	(DO 7)	(80 16)	Plastic	(80	16)	(80 10)	(80 10)	
50	0.05	0.08	IN4001	0.05	0.07	0.14	0.19*	0.56*
100	0.08	0.07	1N4002	0.06	0.09	0.16	0.21*	0.69*
200	0.06	0.08	1N4003	0.07	0.12	0.20	0.23+	0.98*
400	0.07	0.14	1N4004	0.08	0.14	0.28	0.85*	£1.25.
600	0.08	0.16	1N4005	0.09	0.16	0.88	0.42*	\$1.76+
800	0.11	0.18	1N4006	0.10	0.18	0.85	0.51*	81-94*
1000	0.13	0.28	1N4007	0.11	0.28	0.44	0.60*	£2·81*
1200		0.82			0.28	0.54	0.69*	£2-88 *

PO BOX 6 WARE HERTS

SUPER UNTESTED PAKS

Pak	Ħо.	Description &c		Price
U 1	120			0-60
U 2				0.60
U 3		Germanium gold bonded sub-min. like OA5, OA47		0-60
U 4		Germanium transistors like OC81, AC128		0.60
U 5		200m A sub-min, silicon diodes		0.60
T 6		Sil. Planar trans. NPN like BSY95A, 2N706		0-60
TU 7		8il. rect. TOP-HAT 750mA VLTG. RANGE up to 100		0.60
TU 8		Sil. planar diodes DO-7 glass 250mA like OA200/202		0.60
υ 9		Mixed voitages, 1 Watt Zener Diodes		0.60
U10	20	BAY50 charge storage dlodes DO-7 glass		0.60
U11	20	PNP Sil, planar trans. TO-5 like 2N1132, 2N2904		0.60
U13		PNP-NPN Sil. transistors OC200 & 28104		0.60
U14		Mixed silicon and germanium diodes		0.60
U15	20	NPN Sil. planar trans. TO-5 like 2N696, 2N697		0.60
U16		3Amp sil. rectifiers stud type up to 1000 PIV		0.60
U17	30	Germanium PNP AF transistors TO-5 like ACY 17-22		0.60
U18		6 Amp sil. rectifiers BYZ13 type up to 600 PIV		0.60
U19		Silicon NPN transistors like BC 108		0.60
T20		1.5 Amp sil. rectifiers top hat up to 1000 PIV	٠.	0-60
U21		AF. Germ. alloy transistors 2G300 series & OC71	٠.	0.60
U23		MADT's like MHz series PNP transistors	٠.	0.60
U24		Germ. 1 Amp rectifiers GJM series up to 300 PIV	٠.	0.60
U25		300 MHz NPN silicon transistors 2N708, BSY27	٠.	0.60
U26		Fast switching silicon diodes like IN914 Micro-Min	٠.	0.60
Ψ29		1 Amp SCR's TO-5 can. up to 600 PIV CRS1/25-600		£1-20*
U82		Zener diodes 400 mW DO-7 case 3-33 volts mixed	٠.	0-60
U33		Plastic case 1 Amp sil. rectifiers IN4000 series	٠.	0-60
U34		Silicon PNP alloy trans. TO-5 BCY26 28302/4	٠.	0.60
US		Silicon planar transistors PNP TO-18 2N2906	• •	0.60
US		Silicon planar NPN transistors TO-5 BFY50/51/52	٠.	0.60
US7	7 80	Silicon alloy transistors SO-2 PNP OC200, S2322	٠.	0.60
U38		Fast switching silicon trans. NPN 400 MHz 2N3011	• •	0.60
USS		RF. Ger. PNP transistors 2N1303/5 TO-5	٠.	0.60
U40		Dual transistors 6 lead TO-5 2N2060	٠.	0.60
U48		Silicon trans. plastic TO-18 A.F. BC113/114	• •	0-60 0-60
U44		Silicon trans. plastic TO-5 BC115	٠.	£1.20*
U44		7 3A SCR, TO66 up to 600 PIV		
U44		O Unijunction transistors similar to TIS4S	٠.	\$1.20°
U47	7 10	10220112 Pillotto		41.20
U48	5 1) NPN Sil. power transistors like 2N3055		£1.20
U49	9 12	s mentioned above are given as a guide, to the type of		
the	pak te Mo	The devices themselves are normally unmarked.	-	12
270			_	

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VOLTAGE REGULATORS

TO.3 Plastic Encapsulation uA.7805/L129 5V (Equiv. to MVR5V) \$1-25p uA.7812/L130 12V (Equiv. to MVR12V) #1-25p uA.7815/L131 15V (Equiv. to MVR15V) \$1.25p uA.7818 18V (Equiv. to MVR18V) \$1.25p

THYRISTORS

		- 1						_		
PIV	0-6A	0-8A	1A	3.A.	5A	5 A	7.A.	10A	16A	30A
	TO18	TO92	TO5	TO66	TO66	TO64	TO48	TO48	TO48	TO48
10	0.18	0.15	_	_	_		_	_		_
20	0.15	0.18	_		_	-	_		_	_
30	0.19	0.22	_	_	_					
50	0.22	0.28	0 20	0.25	0-36	0.36	0.48	0.51	0.54	\$1-18
100	0.25	0.80	0.25	0.25	0.48	0.48	0.51	0.57	0.58	\$1.48
150	0.81	0.88		_						
200	0.88	0.44	0.25	0.80	0.50	0.50	0.57	0.62	0.62	\$1-68
400	_		0.80	0.89	0.55	0.57	0.68	0.71	0.77	21.79
600	_	_	0.89	0.48	0-69	0.69	0.78	0.99	0.90	
800	_		0.58	0.65	0.81	0.81	0.92	£1-22	#1-89	\$4.07

DIODES

Tupe	Price	Type	Price	Type	Price	Type	Price
AA119	0.08	BY101	0.18	BYZ16	0.41	OA85	0.09
AA120	0.08	BY105	0.18	BYZ17	0-86	OA90	0.07
AA129	0.08	BY114	0-12	BYZ18	0.36	OA91	0.07
AAY30	0.09	BY124	0.18	BYZ19	0.28	OA95	0.07
AAZ13	0.10	BY126	0.15	CG62		OA200	0.07
BA100	0.10	BY127	0.16	(OA91E	a) 0.08	OA202	0-07
BA116	0.21	BY128	0.16	CG651 (ŎA70-	BD10	0-08
BA126	0.22	BY130	0.17	OA79)	0.07	BD19	0-06
BA148	0.15	BY133	0.81	OA5 Sho	ort	1N34	0-07
BA154	0.12	BY164	0.51	Leads	0.21	1N34A	0.07
BA155	0.15	BYX38	300-48	OA10	0.14	1N914	0.08
BA156	0.14	BYZ10	0.86	OA47	0.07	1N916	0-06
BA173	0.15	BYZ11	0-81	OA70	0.07	1N4148	0.08
BB104	0.15	BYZ12	0.81	OA79	0.07	18021	0.10
BY100	0.16	BYZ13	0.26	0.481	0.07	18951	0.70

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Pak l		Quality Tested Paks	Price
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Q 9	7	OC 81 type transistors	0.60
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Q12		AF 116 type transistors	0.60
Q13		AF 117 type transistors	0.60
Q14	3	OC 171 H.F. type transistors	0.60
Q15	7	2N2926 Sil. Epoxy transistors mixed	
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Q17		NPN 2 × ST.141. & 3 × ST.140	0.60
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Q19	3	MADT'82 × MAT 101 & 1 × MAT 121	0.60
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Q31		Silicon switch translators 2N708 NPN	0.60
Q32		PNP Sil. trans. 2 × 2N1131, 1 × 2N1132	0.60
Q33		Silicon NPN transistors 2N1711	0.60
Q34	7	81. NPN trans. 2N2369, 500MHz	
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Q35	3	Bilicon PNP TO-5 2×2N2904 & 1×	
		2N2095	0.60
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040			0.6
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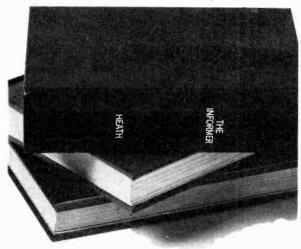
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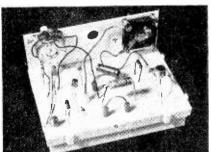
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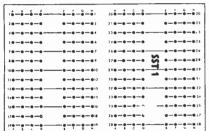
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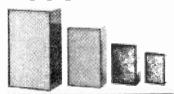
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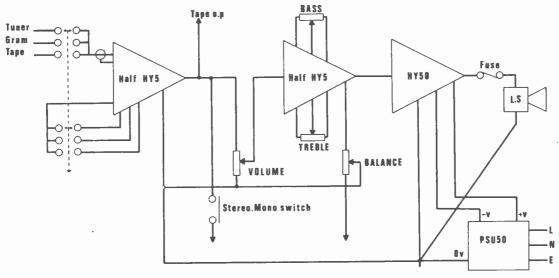
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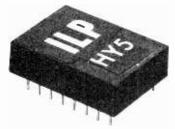
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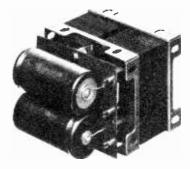
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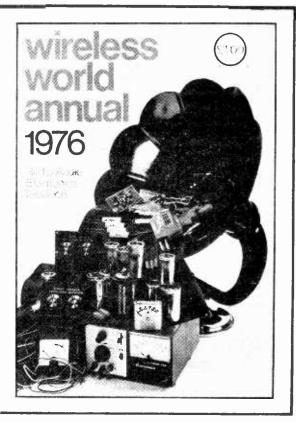
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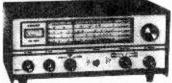
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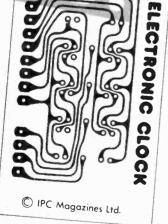
As a result of continued requests from readers we are happy to announce the start of a printed circuit board service for projects published in Practical Wireless. A list of PCBs now available, plus ordering coupon, will be found below. The list will be extended as new PCBs are made available. Generally the boards will be of epoxy glassfibre, drilled and roller-tinned. For the time being PCBs for projects published in PW before December 1975 are not available through this new service

To:- READERS PCB SERVICES, PO BOX 11, WORKSOP, NOTTS

Please supply PCB/s as indicated by tick/s in box/es

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Dec 75	Disco System, Amplifier	, ,						
	(2 required) SRBP each	AM0421	3⋅40 + 18 □					
	glassfibre each	AM0421	4.10 + 18					
Dec 75	Disco System, Light Modulator	A M0423	2.70 + 18					
Jan 76	Music Box SRBP	DN1/JM	2.25 + 18					
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NEWS...

NEWS...

Sinclair digital watch

THE watch is controlled by a quartz crystal and on command displays either hours and minutes or minutes and seconds, depending on the switch that is operated. The display is internally timed for one second or will stay on as long as the switch is closed. The two operating switches are located on the watch front beneath the LED display. There is a third switch on the rear which permits setting of the watch and holding of the time to which it has been set. Closing the read hours and minutes switch and then depressing the set switch will clock hours round at the rate of one per second and similarly depressing the minutes and seconds switch followed by the set switch will clock minutes round at one per second. Seconds are automatically reset to zero. Depressing the set switch only will stop the watch and hold the set time.

Sinclair guarantee an accuracy of better than one second per day and typically several times better than that will be obtained. The accuracy is fundamentally determined by the quartz crystal and the precision to which this is trimmed. The watch is powered by two small mercury cells and will give a life of typically one year dependent on the frequency with which the display is used.

The electronic circuitry to control the watch is all contained on a single integrated circuit which Sinclair Radionics have designed using injection logic technology. The chip requires only a quartz crystal, a trimmer capacitor, an LED display and batteries to complete the electrical line-up.

Three years ago, having spent a considerable time reviewing and analysing various technologies appropriate to electronic watches, Sinclair realised that the process which was gradually emerging from the research laboratories of Philips and IBM had both electrical parameters and cost potentials well-suited to a watch. The process is now known as I²L and is capable of very low power consumption, having a speed power product of less than 1pJ, combined with an ability to supply



high peak currents without using excessively large output devices. The process is intrinsically capable of low voltage operation without needing tight parameter control.

A study carried out by the company showed that without recourse to fine geometries a chip area saving of 1.5:1 could be achieved compared with ion implanted CMOS devices and at

the same time both segment and digit drive components could be incorporated on the chip. With one exception presently available CMOS chips require separate bipolar digit drivers. The process careful development required with an able semiconductor company, but it had a good start as it was based on a well-established bipolar process with a considerable amount of knowledge already to hand. The development lay in optimising a different range of parameters.

Close analysis of chip size, slice processing cost and yield showed that the balance should weigh considerably in favour of the bipolar technology and therefore a major design programme was undertaken.

The whole design was carried out by Sinclair engineers to the extent of producing an actual circuit layout, which was diffused and refined in conjunction with ITT in England. During all stages of both circuit and process development, close contact was maintained between the two companies to ensure that circuit parameters married up to process requirements and vice versa.

Part Exchange Scheme

ENRY'S-LINDAIR hi-fi and audio retail group is operating a new Part Exchange Department.

The firm states that customers who bring their old equipment into any Henry's-Lindair store will be given a reasonable 'trade-in' allowance which they may then use against the purchase of new equipment from that particular store. The trade-in equipment will then be passed to the Service Department, if necessary, where it will be tested and overhauled. It will then be sold through one of the group's newly established Bargain Centres in Edgeware Road and Tottenham Court Road, London, with a three month guarantee.

MORE NEWS...ON
PAGE 758

Arrow Stock Sheet

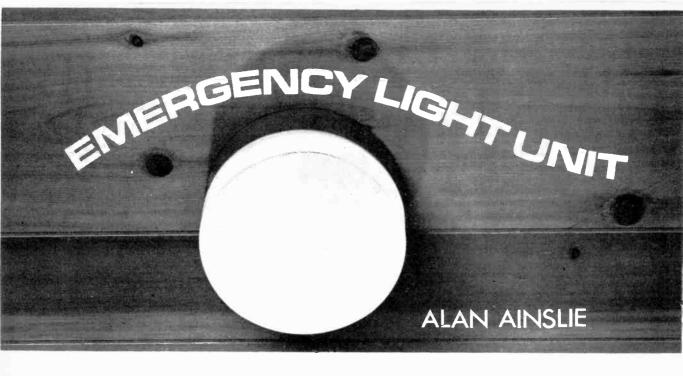
ARROW Electronics Ltd., recently sent us a copy of their latest stock sheet and price list. Included in it are their special low price specialities of COS-MOS logic devices and items ranging from a metal detector. and S-Dec products to optoelectronic devices and jack plugs. A very useful list of available components and prices to have by the workbench.

If you would like a free copy of the Arrow list, send a stamped, self-addressed envelope to Arrow Electronics Ltd., Mail Order Dept., P. W., 7 Coptfold Road, Brentwood, Essex, CM14 4BW.

Aerialite

AERIALITE Aerials have transferred their sales, production and technical departments from Congleton in Cheshire, to Whitegate, Broadway, Chadderton, Oldham, Lancs, OL9 9QC. Telephone: 061-652 1111.

743



ITH another season of possible power failures approaching interest must again be centred on ways of lighting the home when the mains fail. This article describes an Emergency Light Unit which will automatically illuminate a central position in a home during a power cut. The light output is sufficient to illuminate a hall or landing and stairs to prevent accidents in the dark. By using an inexpensive moulded commercial case the unit can be made to look very presentable, becoming a permanent part of the decor.

This unit is the type of 'luminaire' known as "nonsustained" as it lights up only under mains failure conditions. It belongs to the general class of '3-hour luminaires' although the rechargeable cells used allow a discharge period of over 4 hours. The 3-hour rating applies to a cycle period of 24 hours, i.e. one mains failure or less per day.

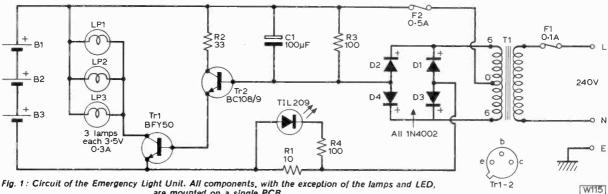
Circuit

A 6-0-6V transformer, Fig. 1, is permanently connected across the mains to provide both a charging current for the cells and a 'mains-on' reference voltage, which ceases when a mains failure occurs. Diodes D1 and D3 are connected as a full wave rectifier to charge the cells through the current limiting resistor, R1. The unit uses three nickel cadmium cells B1/3 giving a total terminal voltage of 3.75V to power three 3.5V 0.3A bulbs in parallel.

The specification for this class of Emergency Light Unit requires that it should be capable of operating on a 24 hour charge/discharge cycle. The lamps fitted to the unit consume almost 1A and for the specified 3-hour discharge period this represents 75% of the capacity of the 4Ah cells. In a 24 hour cycle therefore, a charging period of 21 hours is available to replace 75% of the cell capacity or 3Ah.

The value of R1 has been chosen to give approximately 250mA charging current recommended by the cell manufacturers as not giving rise to damage through overcharging, and which, in fact, replenishes the cells, after a 3 hour discharge at 1A, in 17 or 18 hours, safely exceeding the requirements of the specification.

A proposal to the British Standards Institute recommends that it shall be mandatory to have a warning should the cells fail to charge. This is to take the form of a long-life red indicator lamp monitoring the actual charging current, rather than the presence of a mains input to the 'luminaire.' In this design an LED is used with its limiting resistor



are mounted on a single PCB.

to sense the voltage drop across R1, which is about 2.5V when the cells are charging normally. Should a cell become open circuit or a fault develop in the charger circuit then the voltage drop across R1 will fall to zero and the LED will go out, as proposed in the above recommendation. In practice the LED must be arranged so as to be visible at all times, easily arranged by placing the LED behind, but close to, the diffuser giving a patch of red light during normal charging.

The 'mains-on' reference voltage is produced by D2 and D4 which give -6V from the transformer relative to the positive side of the battery when the mains is applied. The reference voltage is smoothed by C1, to prevent 100Hz triggering of the lamp, and fed to Tr2 base which biases this transistor off by making its base more negative than its emitter. However, when the mains fail C1 discharges into R3 and Tr2 is no longer cut off. Base current through R3 turns on the transistor which in turn turns on Tr1 by effectively connecting R2 between its base and the positive supply.

Transistor Tr1 is supplied with such heavy base current through R2 and Tr2 that it saturates and behaves as a simple diode of low voltage drop in series with the cells and the bulbs. In practice a saturation voltage of 650mV is typical, corresponding to a power dissipation in Tr1 of only 600mW. With Tr1 saturated the bulbs receive about 3.3V and pass a little under 1A if three 0.3A bulbs are used. Higher current bulbs should **not** be used in an effort to increase the light output as Tr1 will fail to saturate and will overheat. It is possible to use a lower current load $(3\times0.15A)$ bulbs, for instance which will lengthen the maximum discharge time for the unit.

The Emergency Light Unit is equipped with two fuses, one of 0·1A on the primary side of the mains transformer and one of 0·5A on the secondary, designed to offer protection against a fire hazard in the event of any components failing. Only the specified types should be used otherwise the unit may be dangerous under fault conditions.

Construction

There are two possible ways of constructing the Emergency Light Unit; either as a self-contained lamp or as a 'control box' driving a separate decorative lamp. In the latter case the PCB is constructed as will be described and housed in a suitable cabinet, with any metalwork connected to mains earth. The LED to indicate cell charging should be mounted on the front of the control box and a small socket provided for connection to the bulb(s), which can be concealed in an ornamental oil lamp or something similar.

Self-contained 'luminaires' are most popular commercially and this unit was primarily designed to be both self-contained and attractive in appearance. A rather pleasing case for the unit is available in a choice of colours from British Home Stores as an interior light fitting. It is a simple matter to remove the reflector and lampholder fitted in the bottom of the case, as well as all metal attachments, to leave an empty shell into which the PCB and lampholder board can be fitted.

To ensure long term reliability a PCB, Fig. 2, has been designed to accommodate all the electronics. The board is octagonal as it has to fit in the bottom of the round case. It is convenient to mount the transformer first. The specified one is for PCB mounting.

* components list

Resistors

R1 10 Ω 2W, R2 33 Ω , R3 100 Ω , R4 100 Ω (R2/3/4 are $\frac{1}{2}$ W 5 or 10%)

Semiconductors

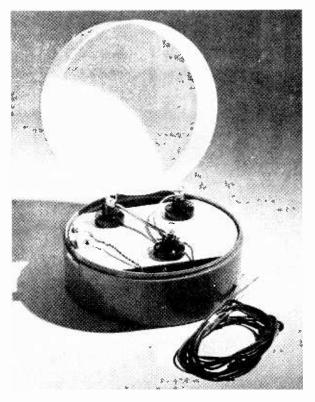
Tr1 BFY50 Tr2 BC108 or 109 D1/4 1N4002 LED TIL209

Miscellaneous

C1, 100µF 10V. T1, 240V primary, 6-0-6V 250mA secondary (B.B. Electronics, 1 Windsor Walk, South Anston, Nr. Sheffield, Yorks. Type EL3/6A £1:86 + 25p P/P). B1/3, Ever Ready NCC400 Style HB, or similar, 3 off. F1, 100mA 20mm fuse. F2, 500mA 20mm fuse. Fuse holders, for PCB, 2 off. Lamps, 3:5V 0:3A with holders, 3 off. Case, British Home Stores type 1914. TO5 heatsink for Tr1.

Alternatives can be used but mounting holes will have to be drilled in the board and the transformer connected with flexible leads.

All the other components, except the cells, can then be mounted as in the PCB layout drawing Fig. 3. The fuse holders are easier to mount if they are clipped on to a fuse before insertion into the board. Tr1 is fitted with a TO5 finned heatsink to keep it cool during discharge. Solder tags are inserted for the six external connections to the board. The cells are inserted last because, as received, they are partially charged and could damage partially completed



The completed 'luminaire'. The PCB is mounted in the bottom of the case, the lamp board resting on a rim Inside the case. Both boards should be a tight fit in the case.

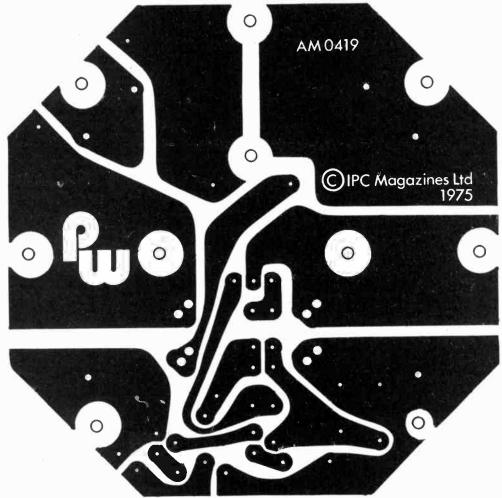


Fig. 2: Full-size layout of the PCB. Fig. 3: next page, shows the component layout. The cell retaining straps have been removed in this view.

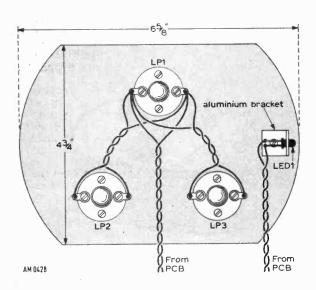


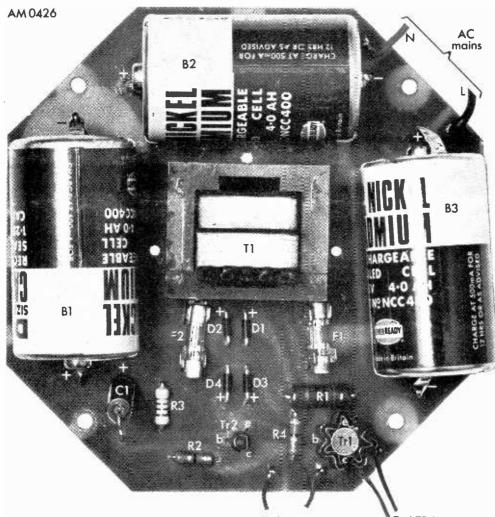
Fig. 4: The lamp board also carries the LED which should be bright enough to be visible through the translucent part of the case when the cells are charging normally. Diameter of the board will depend upon the actual case used by the constructor.

circuitry. Short lengths of tinned copper wire are used to connect the cells to the board and give some support. Small straps are then made from sheet tinplate, one for each cell held down on either side using the 6BA holes in the PCB. Alternatively, simple straps can be formed from thick copper wire passed through the holes, twisted and soldered under the board.

Three bulbs are used in the prototype and the three MES lampholders are mounted on a piece of perspex, fixed to the top of the bottom half of the case, and painted white to act as a reflector. The perspex is a tight push fit in the case and needs no mounting screws. A small bracket is made from aluminium to hold the LED against the translucent dome. All three lampholders are wired in parallel with a short length of flex left for connection to the PCB. Similarly a length of flex is soldered to the LED, Fig. 4.

(N.B. On no account should wood be used to make the lampholder board or any other part of the luminaire as this would present a fire hazard.)

The PCB is placed in the bottom of the case and a felt pen used to mark the position of the four mounting bolts. The base is then drilled to accept 4BA bolts which are held captive with nuts. This is necessary because the PCB has to be removed prior to installation to reveal the holes for the wall screws.



When the board has been mounted, the wires to the lampholder panel are soldered to the tags and the panel fixed in place.

After thoroughly checking all connections the mains can be connected to the input of the unit. The LED should glow indicating that the cells are being charged. A voltmeter across R1 should indicate a voltage drop of about 2.5V showing that the charging current is of the right order. After a period of ten minutes or so the cells should be sufficiently charged to run the lamps for a couple of minutes when the mains is switched off.

Installation

The unit can be mounted in any position as the cells are held by their straps. Should the unit be mounted on a ceiling it is important to check that the lampholder panel is a tight fit.

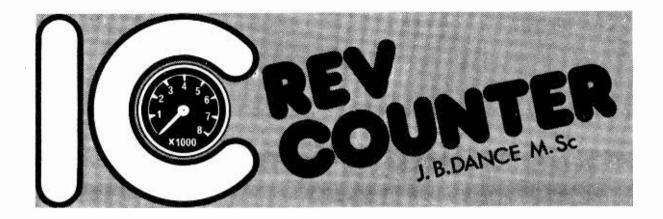
There are three mounting holes for woodscrews, in the bottom of the case, together with a central hole for the mains cable. With the PCB removed the bottom of the case is screwed to the wall or ceiling with a short length of mains cable left floating. The PCB is replaced and the mains input soldered in. Alternatively a short fly-lead with a terminal block can be used to save soldering at the installation

To lamps To LED1

stage. The lampholder board is pushed into position and the three bulbs tightened. At this stage, if the cells are charged, the bulbs will light because there is no mains input. With mains on the bulbs should extinguish and the LED will come on. Snapping the dome on completes the installation.

In use the Emergency Light Unit requires no maintenance other than a regular check, by switching the mains off, to ensure that it is operating correctly. The cells have an operating life of several years and providing that no extremes of temperature are encountered the need for replacement would be unlikely. Should the unit be used outside or where the temperature could drop below 10°C then the cell manufacturers recommend that precautions be taken to prevent damaging the cells by over-voltage during charging. Protection can be provided by connecting a 4·7V 2W zener diode across the cells, the cathode to the positive end of C1 and the anode to the emitter of Tr1.

Finally, a warning about the nickel cadmium cells used in this project. This type of sintered plate cell has an internal resistance of only a few milliohms which means that dangerously high currents will flow if a cell is accidentally short-circuited. They should therefore be treated with respect and kept in their packing until needed.



In this article it will be shown how an integrated circuit especially designed for use in the automobile field can be employed as the heart of a simple engine 'rev counter'. These are much used in sports cars for rally driving to enable maximum performance to be obtained. They show the driver the optimum moment at which to change gear in order to obtain the best possible performance without the risk of damaging the engine by 'over-reving'. Rev counters can also be most instructive to the learner driver, whilst some car owners feel that they confer a prestige value on their vehicle.

The SAK115

The integrated circuit used in this project is the SAK115 which is manufactured by ITT Semi-conductors. The device is encapsulated in a plastic dual-in-line case which has a metal tab on each side of the device and eight connecting pins.

The device has been designed for vehicles having negative earth since almost all modern cars are of this type. However, it will be shown that the same device can also be used with an extra transistor in a slightly more complex circuit for vehicles which have positive earth systems.

Negative earth

The use of the SAK115 in the simpler negative earth circuit of Fig. 1 will be considered first. Each time the contact breaker points on the car open, a voltage pulse is developed across them. Each pulse occurs at the same time as a spark in the engine. The number of pulses per minute (ppm) is thus proportional (but not equal) to the engine revolution rate. The pulses can therefore be used to drive the rev counter provided that each pulse causes a constant amount of charge to flow through the meter.

The input to the circuit of Fig. 1 is fed by the fairly high voltage pulses from the contact breaker which are then fed to the potential divider R1 and R2. Consequently, only about one-tenth of the original pulse amplitude is fed to pin 1 of the IC. The SAK115 is monostable and of the flip-flop type. Each pulse fed to pin 1 switches the circuit, so that the output voltage at pin 6 changes for a short time, during which

time a current flows through the meter M1. At the end of the timed period the circuit automatically returns to its former stable state. The circuit remains in the latter state until the next pulse arrives.

The duration of the current pulse to the meter is determined by the product of C1, R3 and VR1. If the value of VR1 is increased, the length of the current pulse increases and so does the deflection of the meter. The trimmer VR1 can thus be employed to calibrate the circuit so that the correct readings are provided by the instrument. If the meter is to indicate the correct rpm under all conditions, the current which passes through the meter during any pulse must always have the same value. It must not, for example, vary with the battery supply voltage or the readings of the meter would depend on the charge/discharge battery current and on the state of charge of the battery.

In order to keep the amplitude of the current pulses through the meter fairly constant, a zener diode is incorporated to provide a relatively constant voltage supply to the IC. As the car battery voltage

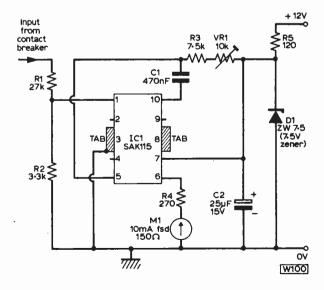


Fig. 1: Basic circuit of the rev counter utilising the SAK115 integrated circuit. The above circuit is only sultable for vehicles having a negative earth system.

changes, the voltage across the zener diode D1 remains virtually constant and the whole of the change of voltage appears across R5. The capacitor C2 smooths the supply to the IC and removes any

stray pulses.

The duration and amplitude of each current pulse is fixed by the circuit component values, so each pulse from the contact breaker causes the same amount of charge to flow through the meter. The meter deflection is therefore proportional to the rate of revolution of the engine. Although the current through the meter actually consists of individual short pulses (each of a few thousandths of a second in duration), the mechanical inertia of the meter smooths out these pulses to give a virtually steady reading.

Noise pulses

The electrical system of a vehicle is notoriously noisy, consisting of transient changes in voltages at various points in the circuit, which would normally trigger a conventional monostable circuit and cause a high reading to be obtained. However, the SAK115 has been specifically designed for use in such noisy environments and cannot be triggered by pulses which have an amplitude of less than about 8V at

The potential divider resistors R1 and R2 reduce any spurious input pulses still further and the circuit is therefore insensitive to pulses of less than about 80V at the contact breaker itself. In negative earth cars, a positive pulse considerably greater than this value is developed at the contact which is not earthed, each time the current ceases to flow through the ignition coil when the contacts open. It is the inductance of the coil which is responsible for the generation of these pulses.

The SAK115, being specifically designed for negative earth vehicles, is insensitive to negative-going pulses. This again greatly reduces the likelihood of incorrect readings being obtained due to triggering of the circuit by spurious pulses. Any negative pulses

* components list

Resistors R1 27kΩ R5 120Ω R2 3 · 3kΩ R6 270Ω R3 7 · 5kΩ VR1 10k Ω vert preset. 270Ω (see text) miniature All resistors 10% 1W Capacitors C1 470nF 25V C2 25/F 15V

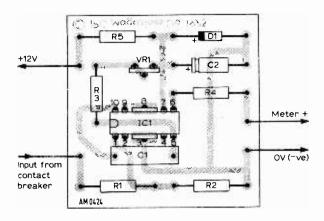
Semiconductors

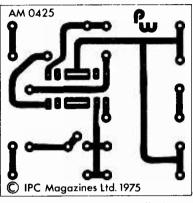
SAK115—Available from Phoenix Electronics (Portsmouth) Ltd., 139-141 Havant Rd., Drayton, Portsmouth, Hants. PO6 2AA. Priced £1.14 each plus 48p VAT and p&p. D1 , ZW7.5 zener diode

Tr1 2N2904 or similar pnp transistor

Miscellaneous

M1, 0-10mA fsd moving coil meter. 50 x 50mm piece of veroboard, or pcb. T1, mains transformer with secondary 80 to 200V RMS. Br1, bridge rectifier or 4 rectifier diodes.





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18 ·

The suggested printed circuit board and component layout are shown actual size, and for negative earth systems only. It is also suggested that the board be suitably drilled, and mounted directly on the back of the meter.

which reach pin 1 are shorted to earth by a diode inside the IC connected between pins 1 and 3.

A further advantage of the use of a purpose built IC is that the internal push-pull output stage of the device is specially designed to drive a moving-coil meter. It provides adequate drive even when the meter coil has a relatively high inductance and when the revolution rate is high.

The meter

The meter should be calibrated over the range required. For a small car, 6,000 rpm is about the maximum one should ever use, but in some sportscars a value up to about 8,000 rpm is permissible. One therefore requires a meter scaled from zero up to about seven or eight for a typical small car, or possibly up to ten for a sports car. This allows an adequate margin at the top end of the scale. Unfortunately meters calibrated from zero up to about eight are not normally available.

The simplest solution is to employ a 10mA fsd meter, where each milliamp of the scale can be made to correspond to 1000 rpm. The uppermost part of the scale will not then be used. Constructors who are good at artwork will be able to make a scale marked 0-8,000 rpm from transfers (such as 'Letraset'). The top part of the scale could then be marked with a red band to show that the engine should not be taken to such a high rpm.

The current which flows through the meter under any conditions is inversely proportional to the sum of R4 and the meter resistance. The circuits shown are suitable for use with meters which have an fsd of about 10mA and a resistance of about 150Ω . If the meter resistance is much less than 150Ω , the value of R4 should be increased to make up the difference. Similarly, if a more sensitive meter is used, the total resistance of the meter circuit must be increased to reduce the current which flows under any specified pulse rate. The total resistance of the meter circuit of Fig. 1 is about 420Ω . If a meter with an fsd of 2mA is used, one-fifth of the current is required to obtain a given deflection, and therefore the total resistance in the meter circuit should be about $1.6\text{k}\Omega$.

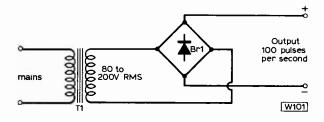


Fig. 2: The circuit shown here provides a simple method for obtaining an output of 6,000 pulses per minute. This is for the calibration of the circuits shown in Figs. 1 & 3.

Calibration

One can, of course, calibrate the circuit by driving the car at a known speed in a specified gear and getting a colleague to adjust VR1 so that the meter indicates the correct rpm for the speed and gear concerned, calculated from the vehicle manufacturer's data. This procedure is somewhat tedious and requires a constant speed to be kept up for at least a minute or so; in addition, it relies on the accuracy of the speedometer. It is more accurate however to make at least a preliminary bench adjustment of VR1 by feeding pulses at a known frequency into the circuit. The 50Hz mains supply is the obvious source, since it is easy to obtain 3,000 or 6,000 ppm by half-wave or full-wave rectification of the supply.

Most small cars are four cylinder, four stroke types, whose camshaft rotates at half the engine revolution rate, giving four sparks per revolution of this shaft. Thus the contact breaker provides two pulses to the rev-counter circuit per revolution of the engine. If 6,000 ppm are fed to the circuit, the trimmer VR1 must be adjusted so that the meter indicates 3,000 rpm.

The very simple circuit of Fig. 2 can be employed as a source of 6,000 ppm.

An AC output from the transformer of not less than about 80V is fed to the bridge rectifier circuit shown. This circuit inverts each alternative half cycle of the 50Hz mains voltage and thus produces 100Hz output of 6,000 ppm. The output from Fig. 2 must be connected with the correct polarity to the input of Fig. 1 or no meter reading will be obtained. The negative output line from Fig. 2 is connected to the

OV line of Fig. 1, whilst the positive output is connected to the upper end of R1 of Fig. 1.

Although it is possible to feed the mains directly to the bridge rectifier of Fig. 2, this can be very dangerous in the hands of the inexperienced experimenter. It is far safer to use a transformer.

If a transformer with a secondary winding providing 80 to 200V RMS output is not available, a transformer providing a somewhat lower voltage may be used for the calibration, but R1 of Fig. 1 must be reduced during the calibration only, so that an adequate pulse reaches the IC.

6/8 cylinder vehicles

In the case of a six cylinder, four stroke vehicle, the cam shaft again rotates at half engine speed, but there will be six pulses per rotation of the cam shaft instead of four. The contacts therefore provide three pulses per engine revolution. Thus when the bridge circuit of Fig. 2 is used to provide 6,000 ppm VR1 should be adjusted so that the meter indicates 2,000 rpm.

In the case of an eight cylinder, four stroke vehicle, each engine revolution produces four pulses from the contact breaker. When the circuit of Fig. 2 is used, VR1 should be adjusted so that the meter shows 1,500 rpm. In the case of six and eight cylinder vehicles, it may be necessary to increase R4 somewhat in order to achieve correct readings. A value of 390Ω for six cylinder cars and 560Ω for eight cylinder cars should be suitable, but these values are not critical and it is only necessary to ensure that VR1 can be adjusted to give the correct reading.

Once the circuit has been calibrated using the mains frequency it can be fitted into the vehicle and should require no further attention. However, recalibration will be necessary if a meter of different internal resistance is employed or the zener diode is changed.

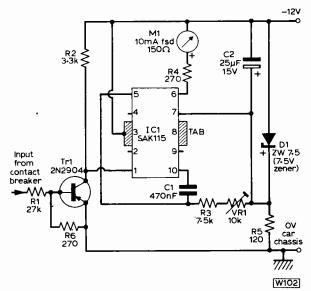


Fig. 3: The above circuit is similar in design to that shown in Fig. 1, but is only suitable for vehicles having a positive earth. The purpose of the transistor is to amplify and reverse the polarity of the pulses.

continued on page 765.



I can just imagine the old chap bawling at Rudolph "Here's another nice mess you've landed us in!" And there's Rudolph smirking all over his face, fondly imagining he's another Biggles. They've certainly a lot of ground to cover to deliver all those toys, not to mention all those gorgeous Home Radio Components Catalogues!

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Y OU may have noticed in the sparkling advertisements for sparkling amplification gear that when it comes to output wattage there is usually more sparkle than watts-per-pound sterling. For some time RT-VC have specialized in offering concrete value-for-money in their range of products. From my expereince of the range one can find very useful equipment performance without the fancy treatment that characterises goods offered by the 'Big Boys'. This does not mean that looks are placed second; indeed the result a happy compromise of both appearance and performance. For those of us on a restricted budget it is surely good that such firms can still hold their head above water. Quite obviously there is a strong market for watts without frills.

FIRST LOOK

I have just been living with the new Viscount IV stereo amplifier and find the unit most suitable for inclusion within a stereo system where that difficult combination of power and price seem to get out of balance.

The quoted specifications are given below and were borne out in practice. Laboratory data does not always check out with practical realisation (theory into practice and all that) thus more time was spent in the subjective appraisal of this unit. However, under lab conditions I am glad to report that the unit was able to provide 20W RMS of trueblue power from each channel at 1kHz! With both channels driven simultaneously nigh-on 16W was throbbing into each load resistor.

Frankly, I do not know of any other equipment available that is completely built, ready for connection to the mains, looks good and offering this solid output power at the price. The Viscount IV is compact and features a slimline appearance within its real teak veneered case. No plastic 'simulation'!

FACILITIES

The front panel incorporates the bright aluminium and matt black of more costly units. No less than six varieties of input signal can be selected by the switch seen at the left side of the fascia. Next along are two rotary wide-range tone controls affording adjustment of the bass and treble ends of the audio spectrum. Between these is a pushbutton activating the low-pass filter so attenuating HF scratch from carelessly kept records.

A stereo-mono pushbutton offers useful flexibility and some devious minds may even care to indulge in a little monomixing or perhaps have different sounds in different rooms.

The volume control is conventional in that both channels are affected equally while the balance control enables either channel to be reduced to zero level without disturbing its partner.

Two remaining features at the front are the on-off pushbutton with flush mounted indicator lamp and a ½in. diameter stereo headphone socket. Clear labelling is a feature of both front and rear, right down to the pinning of the DIN input sockets. Certainly this avoids the confusion in referring to drawings where the artist has forgotten to mention whether the diagram refers to a plug or a socket!

Four such sockets are provided on the rear panel to allow signals from magnetic cartridge, crystal cartridge, microphone, tuner, tape machine and one other auxiliary source to be coupled in to the audio system. The tape facility has in-out pinning to permit the single cord connection that eases the lot of the tape enthusiast. Outputs to speakers sees use of DIN sockets again for convenience. Also of sure convenience is the provision of two mains outlets in the US twin flatpin configuration that has been common on much imported audio apparatus. These outputs are activated with the amplifier itself. Unit protection is by a single 'slo-blo' fuse accessible from outside the case.

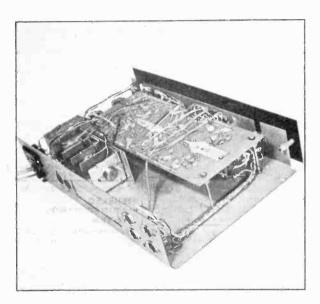
Well, that's the unit. Simple, yet incorporating many features not found on amplifiers costing more. Back in the lab for a second I'm glad to report that no sign of crossover distortion was evident at any output level. Traces seen on the scope screen were always clean, right up to the unit's clipping point where evidence of the latter was observed to be symmetrical.

SPECIFICATION 20 + 20W RMS into 8Ω **Power Output** Speakers : 8 to 15Ω Better than 0.2% @ 10W **Total Distortion** 1. Mag PU 3mV @ 47kΩ Six Switched Inputs 2. Crystal/Ceramic PU 50mV @ 50kΩ 3. Tape 140mV @ 50kΩ 4. Tuner as 3. 5. Microphone 3mV @ 50kΩ 6. Auxilary as 3. 25Hz to 25kHz @ full rated Frequency Response output Better than - 50dB at all Signal/Noise Ratio inputs Bass ± 15dB @ 50Hz **Tone Control** Treble + 12dB @ 10kHz 200/250VAC 60W Supply 15}" wide, 3" high, 10" deep Dimensions (388 x 77 x 254mm)

CONCLUSIONS

Wired up to the normal components of my audio system the amplifier certainly gave a good account of itself. Amazingly so in view of the price, especially compared to the price of my normal amplifier! I tried many types of signal source and all were processed by the Viscount IV in a very satisfactory manner. Using a pair of inelegant and not very expensive loudspeakers I found that the wide range of tone control available from the unit was able to replace what was obviously lacking in the speakers. Coupled with a significantly more expensive pair of speakers the range of control available from those controls marked 'bass' and 'treble' was very marked. Some 'disco-bass' sounds were recreated right in my living room! With more natural settings of these controls and in conjunction with a broad range of listening material, extending from rock to the classics, I was able to enjoy a pleasingly smooth performance. Distortion, especially that ugly crossover type, was indiscernible.

The range of output powers employed in the listening tests extended from the 'normal' background levels used when guests are present right up to fruity power levels I sometimes like to indulge in when alone (I think my neighbours have either become used to me or fled the district).



Plenty of room inside, with the output transistors well clear of the rest of the circuitry.

I found myself constantly referring back to the price of the amplifier the more it seemed to please me in sheer performance. The only peculiarity that bothered me, and I must say that J did become used to it, was the unorthodox positions of the knob datum lines. These appear to have a middle position at five o'clock and while unnatural at first it could even be a fresh novelty in these days of style-oneupmanship by the manufacturers. In all then a very versatile amplifier with power enough for most domestic installations. I would recommend it highly where funds are particularly tight, where kit-building is 'out', and where upgrading of an existing installation is called for without breaking the bank. Altogether extremely good value for money.

The RT-VC Viscount IV Stereo Amplifier retails at £27.50 including VAT and is available separately or as part of a complete Hi-Fi system. Many permutations are available for the Hi-Fi enthusiast with an eye on cost and good performance. For further information on the complete RT-VC Viscount IV Stereo System, please refer to their advertisement in this issue. RT-VC 21C High Street, Acton, London, W3, and 323 Edgware Road, London,

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TELEVISION

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UHF PREAMPLIFIER

The addition of a preamplifier can significantly improve the noise performance in low-signal areas or enable extra distant TV transmissions to be received. The design to be presented this month is simple and very stable. It is based on the BF272 transistor.

SOLID-STATE MONO CHASSIS FAULTS

There have been only two large-screen UK produced solid-state monochrome TV chassis, the Philips 320 and RBM A816. John Coombes describes faults experienced with these.

TRANSISTOR LINE TIMEBASES

In Part 2 of his series E. J. Hoare describes the exacting requirements for correct line output transistor operation and how these are met in practical designs, and provides a clear account of the complexities of line output transformer tuning.

N1500 VCR SERVICING GUIDE

Regular maintenance is essential if the performance of a videocassette recorder is to be kept up to scratch. What this involves in mainly careful lubrication and cleaning. Michael Gladwell sets out what is required with the Philips Model N1500.

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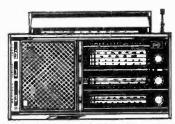
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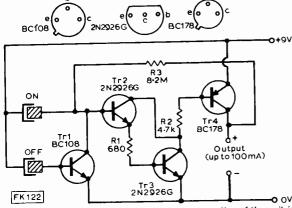
N an increasing number of applications ordinary mechanical switches are being superseded by touch activated switches. These are operated by body resistance between two electrodes, rather than by mechanical pressure or movement. Apart from the obvious novelty value, these have the practical advantage of having no moving parts to wear out. giving them the reliability of the main electronic part that they are switching.

This article describes a simple touch switch which provides the ON/OFF switching of any small piece of battery-powered equipment which has a current consumption of between a few micro-amps and 100mA, such as portable receivers, signal generators

and other test equipment.

The Circuit

The device uses only four transistors, three resistors, and when initially connected to the supply is in the off state; no current flowing except for leakage currents. As the transistors are all silicon types, the total leakage current is only a fraction of $1\mu A$ and for all practical purposes can be considered as zero. This is an important feature as



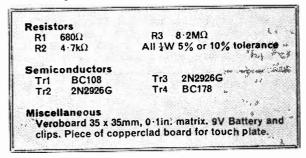
Circuit diagram of touch switch. Current consumption of the unit is 1-3mA when in the ON state, and less than 1µA when in the OFF state.

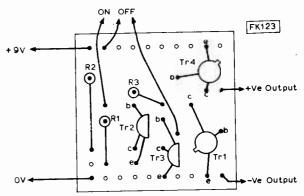
otherwise the unit would be drawing power even when the main equipment was turned off.

When the ON plate is touched a small bias current flows from the positive supply into the base of Tr2. This is wired as the first transistor of a Darlington pair, Tr3 being the second transistor. This bias current will begin to turn on Tr2 and Tr3 and cause a base current to be supplied to Tr4 via Tr3 and R2.

As Tr4 turns on, the voltage at its oscillator will

* components list





The circuit is constructed on 0-1in matrix Veroboard, with flying leads to the touch plates.

begin to rise, and this will cause further base current to flow into Tr2. This is supplied from Tr4 collector via R3. This extra base current will cause Tr2, Tr3 and Tr4 to conduct more heavily, which in turn causes an even greater current flow through R3. This regenerative action results in Tr4 being switched quickly to saturation. The equipment connected in its collector circuit will thus be turned on, and as the circuit is self latching, it will remain on, even when the operator's finger is removed from the touch plate.

When the OFF plate is touched, Tr1 receives a base current from the positive supply, turning it on. In doing so, it shunts the base current of Tr2 to earth, and so turns Tr2, Tr3 and Tr4 off. The circuit is thus returned to its original condition. R1 and R2 are current limiting resistors included to prevent Tr3 and Tr4 from passing an excessive current. The current consumption of the unit when it is in the ON state is about 1 500A, and it is a secondary function of R1 and R2 to limit this current to an

economic level.

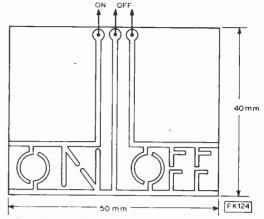
Construction

Construction of the unit is very straightforward being built on a piece of $0 \cdot lin$ Veroboard. The touch plate can be made to conventional designs from PCB or Veroboard, or the novel printed circuit design employed by the author can be copied.

This is perhaps a little less sensitive than conventional designs, but it still provides adequate

sensitivity when used with this circuit.

For practical use on a piece of equipment an aperture should be cut in the front panel of the equipment, or any other convenient point, then the touch plate glued or bolted in place behind the cutout. In use it should be found that the touch plates only need to be touched momentarily to initiate the switching action. The only exception to this will be if the controlled equipment has a fairly high value decoupling capacitor connected across the supply lines (such as in a transistor radio). In this case it will be necessary to touch the OFF plate fractionally longer than normal, so that the



Although any shape can be used for the touch plates the above design was used by the author.

decoupling capacitor has a chance to discharge. Otherwise the unit may turn on again as the finger of the operator is removed from the plate.

NEWS...

NEWS...

NEWS...

Greenweld Meter Catalogue

REENWELD Electronics tell us that they have now compiled a catalogue detailing the various types of multimeter that they have in stock.

If anyone would like a free copy, together with price list, they can get one by sending a 9in x 4in stamped addressed envelope to: Peter Green, Greenweld Electronics, 51 Shirley Park Road, Southampton.

Sound & Vision '76

S OUND & Vision '76 will be the title of next year's TV and audio show to be held at the National Exhibition Centre, Birmingham (May 28th to 31st).

The show follows on from HEDA—the first International Home Electronics and Domestic Appliances Exhibition—a five day trade show sponsored by the Association of Manufacturers of Domestic Electrical Appliances (AMDEA) and the British Radio Equipment Manufacturers' Association (BREMA) which opens on May 23rd.

With the exception of the first day of the public show, when the doors will open at noon, the TV and audio show will be open from 10 a.m. to 10 p.m. daily including the Spring Bank Holiday Monday.

GB2RS News Broadcasts

THE R.S.G.B. has operated these broadcasts on 80m and 2m for many years now and the service for Region 1 has been improved by the addition of two more news readers.

They would appreciate any information on the coverage obtained and the number of readers listening on each of the two bands. It would also interest the R.S.G.B. to know how many non-members are listeners to these broadcasts. Also, if you have any suggestions for material to be included in these weekly bulletins, the R.S.G.B would be pleased to hear from you.

VHF-UHF Manual (3rd edition)

THIS completely revised and enlarged edition is also available from the R.S.G.B All the existing chapters have been up-dated and expanded. In addition, chapters on Space Communication and Microwaves have been included for the first time.

The volume, which has an increased page size and a lot more pages, is case-bound to overcome the binding problems that existed with earlier editions. Price had not been decided at the time of our going to press.

Woollies own

T'S the Wonder of Good Old Woollies — that's what the adverts tell us—and the latest wonder may well be Winfieldbrand audio equipment.

Woolworths are setting up audio centres in 170 of their larger stores. Initially, the departments will concentrate on branded goods (HMV, Ultra, Ferguson, Pye, Philips, Fidelity, etc.) with prices ranging from £40 to £400, but if these items go down well with the public, the Winfield brand may soon be available.

Each department is headed by a manager who has been given training organised by various manufacturers and Woolworths will set up their own network of manufacturer - approved service agents.

1976 Amateur Radio Callbook

HE new edition of the R.S.G.B. Callbook is available from the Radio Society of Great Britain, 35 Doughty Street, London, WC1N 2AE.

The price of £1.47, although

The price of £1.47, although higher than for the 1975 edition includes the cost of postage and packing.

MORE NEWS ON PAGE 743

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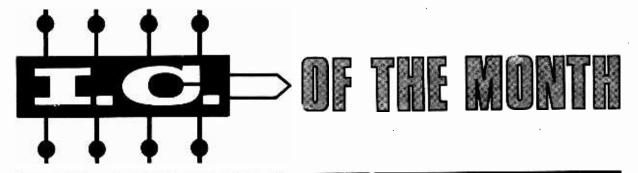
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Number 55

SGS-ATES AUDIO POWER AMPLIFIERS

NUMBER of medium power IC audio amplifiers are produced by SGS-ATES Ltd. in quad-in-line packages. Here we consider the TBA810 and TCA830 which incorporate thermal shut-down circuits and the TCA940 which has output short-circuit protection in addition to the thermal shut-down circuit.

If any of these devices become so hot (about 130°C) that a further rise in temperature might damage them, the drive currents to the bases of the output transistors are automatically diverted. The current in the output stages is thus greatly reduced so that the internal power dissipation remains small until the device becomes cool. It is therefore most unlikely that the experimenter will accidentally destroy any of these devices provided that the maximum permissible power supply voltage is not exceeded. Thermal runaway cannot occur.

TYPES

The TBA810S can provide 7W into a 4Ω loudspeaker when fed from a 16V line or 6W into 4Ω from a 14V supply. Thus it is very suitable for use in car radio receivers. This device is encapsulated in the 'Findip' package which has two cooling fins fitted to the sides of the device. The TBA810AS is electrically identical with the TBA810S but has two short hori-

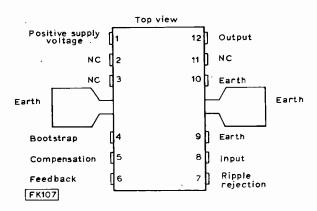


Fig. 1: Connections of all the devices discussed.

zontal cooling tabs with a hole for attaching a heatsink to each tab.

The TCA830S has the Findip encapsulation of the TBA810S but provides up to 4.2W into a 4Ω speaker when fed from a 14V supply line or 3.7W into 8Ω from a 16V supply.

The TCA940 is supplied in the same package as the TBA810AS and it can provide up to 10W into a 4Ω speaker when a 20V supply is used or 6.5W into 8Ω with the same supply voltage. The TCA940E has the same internal circuit as the TCA940, but the package of the TBA810S is used. It is wise to limit the maximum continuous power delivered by this device to about 7W into a 4Ω speaker or it will get very warm. However, it can supply up to 10W for a moment. The protective circuits will prevent it from overheating to the point of damage. The pin connections of all the devices are identical, shown in Fig. 1.

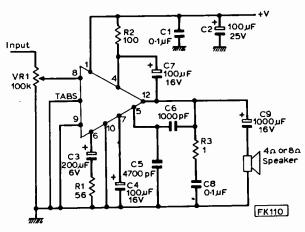


Fig. 2: A typical circuit.

TYPICAL CIRCUIT

A typical circuit for any of the devices under discussion is shown in Fig. 2. Volume control VR1 may be replaced by a $100k\Omega$ resistor.

Capacitor C1 should be soldered close to pin 1 of the device to prevent the possibility of high frequency oscillations, but C2 may be in the power unit. Feedback for the bootstrap circuit at pin 4 is provided by C7 and R2, whilst C9 prevents a steady current from flowing through the loudspeaker speech coil. If the value of C9 is reduced, the bass response will be affected, since this capaictor sets the low frequency cut off.

GAIN

The gain of Fig. 2 is equal to the ratio of the value of an internal $4k\Omega$ feedback resistor divided by the value of R1, and is between 34 and 40dB. This corresponds to a voltage gain of between 50 and 100 times.

If the value of R1 is reduced, the fraction of the voltage fed back through the internal $4k\Omega$ resistor

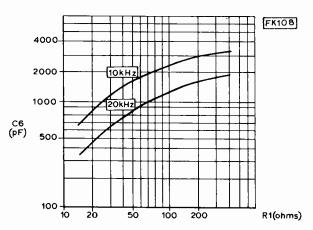


Fig. 3: The values of C6 for various values of R1 for the upper cut-off frequencies of 10kHz and 20kHz.

to pin 6 will be reduced and the gain will be increased. For example, if R1 is 15Ω , the voltage gain will be about 270, whilst if R1 is 150Ω the gain will be about 27. It is recommended that R1 should have a value between these limits, although R1 can have a value of up to 220Ω with a 12V supply before saturation occurs in the input stage.

The variation of gain in these devices arises from the tolerance of the internal feedback resistor ($\pm 30\%$) and from the tolerance in the value of R1. This variation can be reduced by connecting a resistor of less than $4k\Omega$ and 5% tolerance from the lower end of C9 in Fig. 2 to the upper end of R1. Capacitors C5 and C6 control the frequency

Capacitors C5 and C6 control the frequency response but the values required are also affected by the value of the gain controlling resistor R1, so Fig. 3 shows the value of C6 required with various values of R1 for upper cut-off frequencies (3dB down) of 10kHz and 20kHz. A value of C5 about five times that of C6 produces optimum stability. The values shown in Fig. 2 provide an upper cut off frequency of about 17kHz.

In the case of the TCA830S, C5 may be omitted and the value of C6 can be 390pF. This gives a response to 10kHz with a 56Ω resistor for R1, but the value of C6 should be selected in proportion to the value of R1.

The components R3 and C8 form a 'Boucherot cell' or 'Zobel' network. These components, in parallel with the speaker inductance and capacitance, present a load to the output of the amplifier

which approximates to a pure resistance (without any inductive or capacitive components) at all frequencies. This greatly reduces any tendency to instability at high frequencies.

SUPPLY VOLTAGE

The absolute maximum supply voltage to the TCA940 is 24V. However, it is wise to regard 20V as the maximum voltage to leave a reasonable margin of safety. The TBA810 devices and the TCA830S have the lower absolute maximum voltage rating of 20V so the maximum working voltage should be regarded as being about 16V. The TBA810 devices can deliver more current than the TCA830S.

The minimum recommended supply voltage for the TBA810 and the TCA830S is 4V, but the power output at this voltage is only a fraction of a watt. The minimum recommended operating voltage for the TCA940 is 6V, at which the device will deliver about 1W into a 4Ω speaker or $^{1}_{2}$ W into 8Ω .

DISTORTION

The maximum output power levels quoted are for 10% total harmonic distortion. In actual practice such a peak distortion level is reached only occasionally. The typical distortion is about 0.3% for power levels of up to 2W (TCA830S), up to 3W (TBA810 devices) and up to 5W (TCA940 devices).

However, the distortion rises very rapidly indeed with the onset of waveform clipping, as shown in Fig. 4 for the TCA940 with an 18V supply. The capacitor C4 of Fig. 2 attenuates any hum on the power supply line by about 45dB, but the attenuation falls to about 40dB if R1 is reduced to 20Ω .

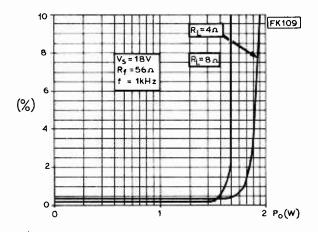
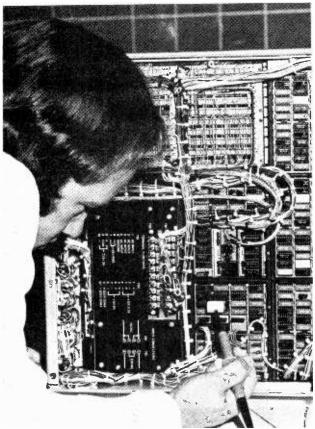


Fig. 4: Distortion plotted against output power for a typical TCA940 device for an 18V supply.

SIMPLER CIRCUIT

An alternative circuit which is somewhat simpler than that of Fig. 2 is shown in Fig. 5. Neither side of the speaker can be connected to the negative (earth) line, but the capacitor C6 of Fig. 5 replaces both C7 and C9 of Fig. 2.

The remainder of Fig. 5 is similar to Fig. 2, except continued on page 765



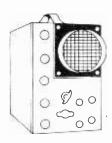
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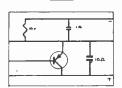
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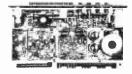


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IC OF THE MONTH—continued from page 762

that the hum attenuating capacitor on pin 7 has been omitted, since Fig. 5 is often used in portable receivers. If desired, tone control circuits can be incorporated in the input circuit of an amplifier or in an external feedback loop.

MOUNTING

The Findip package of the TBA810S type may be mounted on a printed circuit board, the cooling tabs each being soldered to copper foil of about 20 to 30mm square depending on the maximum power output required. Mounting of the TBA810AS package should present few problems since the device can be soldered into a printed circuit board with small metal heat sinks bolted to each of the tabs of the device.

AVAILABILITY

The devices are available from Chromasonic Electronics, 56 Fortis Green Road, Muswell Hill, London N10 3HN and from The Radio Shop, 16 Cherry Lane, Bristol BS1 3NG. The prices are in the region of £1 to £2.

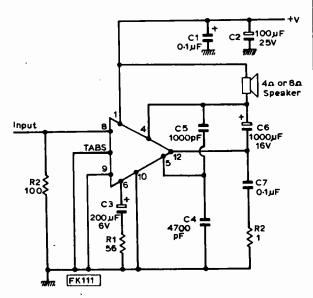


Fig. 5: A simple circuit in which neither side of the foudspeaker can be earthed.

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I.C. REV COUNTER—continued from page 750

Positive earth cars

The circuit of Fig. 3 may be employed with vehicles having positive earth, where the input pulses from the contact breaker have a negative polarity. They are fed into the potential divider consisting of R1 and R6. Where only about one hundredth of the initial pulse amplitude is fed to the base of Tr1. It has been found experimentally that, with the values of R1 and R6 shown in this circuit, the input pulse amplitude required to just trigger this circuit is about the same as that required to trigger the circuit of Fig. 1.

Smaller pulses are obtained from the junction of the potential divider resistors in Fig. 3 than in Fig. 1, but the transistor amplifies the pulses. The amplification provided by various transistors differs somewhat, but is in no way critical. The amplified pulses appear across the resistors R2 and are positive going, since the transistor circuit changes the pulse polarity. These pulses are used to drive the IC connected in the same type of circuit as in Fig. 1.

Positive earth calibration

The positive earth circuit of Fig. 3 may be calibrated in exactly the same way as the circuit of Fig. 1, but requires negative pulses to trigger it. The negative output line from Fig. 2 is therefore connected to R1 in Fig. 3, whilst the positive line from Fig. 2 may be connected to either of the power supply lines in Fig. 3. No meter reading will be obtained if these connections are made the wrong way around.

Power supply

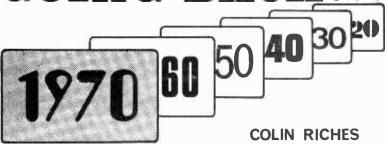
The power supply to the IC should be obtained in the following way so that no current will be drawn when the car's ignition is switched off. In addition, protection is then provided by the car's ignition fuse. The negative power supply line in Fig. 1 or the positive supply line in Fig. 3 should be connected to a good chassis earth on the vehicle, such as the one on the control box. The other power supply line should be connected to the output from the fuse controlled by the ignition switch. Constructors will probably find it most convenient to clamp the meter to the steering column by means of a bracket and a suitable clip. The circuit board itself can be placed in any convenient place, for example, behind the meter.

IC information

The following information is included for those readers who wish to have more information on the SAK115 itself. The power supply (that is, the zener voltage in Figs. 1 and 3) must not exceed 9V or the device may be damaged. It is therefore recommended that the actual supply should lie between 7.5V and 8V at pin 7. The power supply current required is about 12 to 22mA.

The input frequency from the contact breaker should not exceed 10kHz, but this is well above that obtainable from any vehicle. It is also recommended that the resistance between pins 7 and 10 should be between 5k and $20k\Omega$.

GOING BACK.



HIS month we do not go back quite so far in time with a piece of equipment kindly loaned to us by Mr. T. C. McCulley, 31 Cleveland Road, New Malden, Surrey. As far as we know, it is of about 1947 vintage and was an American development made under licence in this country.

Basically the machine is a very sophisticated version of the disc record used by BBC correspondents in the last war to make recordings at the front line so that the people back home could hear the real sounds of war.

Our machine is called a "Recordon" and was to be used on a.c. only 200/250V or 100/130V. To make a recording, one had to turn the volume controlpower supply switch clockwise and turn the 'record' switch to the 'on' position. The recording disc was then placed on the turntable lining it up with positioning pins so that it would not slip round. A grooved disc or 'scroll' was then placed on the recording disc and the tonearm placed against the knob in the centre of the



Top view showing disc in position.

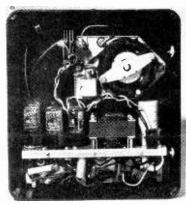
scroll. All that remained was then to speak into the microphone.

To hear the recording, the 'play' switch was operated and the tonearm placed against the knob in the centre of the scroll. The volume was adjusted to suit and if the playback became muffled, one could rotate the tuner knob to restore clarity.

This machine was used as some form of office dictating device and it had amongst its features, a button for the erasing of dictation errors, a footswitch control and a push-button 'executive' type microphone.



The accessories that go with Mr. McCulley's recorder.



Rear view showing valves and motor.

An inscription on the case tells us that the suppliers were Thermionic Products Ltd., of London, S.E.11 and the machine was manufactured under agreement with the Brush Development Co., the Brush Crystal Co., Magnetone Inc. and Thermionic Products Ltd. Patent Nos. 454595 and 599751 applied.

If anyone has further information on the Recordon, please would they contact Mr. McCulley direct.

Vintage vision

OUND is closely allied to vision and this brings us to an interesting note to make for your diaries if you are keen on vintage sound projectors and audio equipment. It's the first ever British Film Collectors' Convention and it will be held on Saturday 24th January 1976 at the Holborn Central Library Theatre, High Holborn, London, WC2.

There will be an exhibition of vintage cine equipment, some of which will actually be working, plus displays of photographs of the old times. There will also be continuous shows of the latest package films released on Super 8mm and some interesting sound projectors in use.

Anyone interested in attending, please send a stamped, addressed envelope to Paul Van Someren, 145 New Kings Road, London, SW6 4SL.

Bintage Rews-sheet

If anyone would like a free copy of the Antique Wireless Newssheet, send a stamped, self-addressed envelope to Tudor Rees (Vintage Services), 64 Broad St., Staple Hill, Bristol, BS16 5NL.

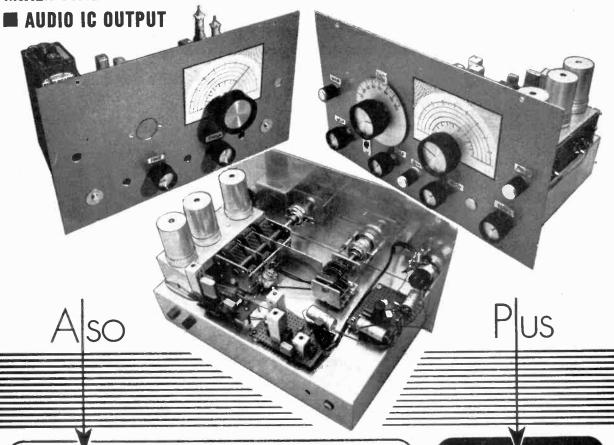
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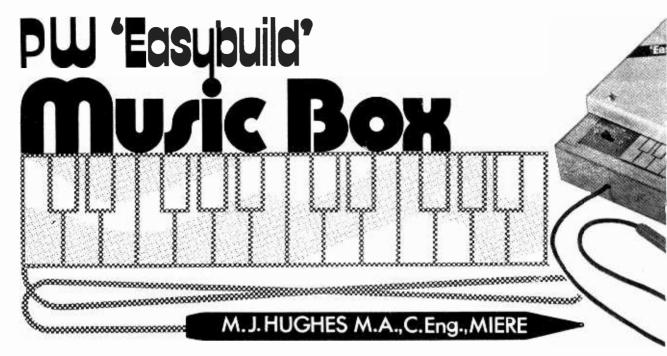
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THIS is a comparatively simple project which most beginners could easily undertake. It is a monophonic organ (i.e. only one note can be played at a time) in which the note is selected by touching a key-shaped electrical contact on the printed circuit board with a probe. In that respect it does not differ greatly from other designs already published but a few features have been added which make the project novel in some respects. It was a temptation to add a number of other refinements but it was felt that one of the big attractions of this project would be its absolute simplicity.

PERFORMANCE

A 25 note keyboard spanning two octaves (from C to C) is used and each note is individually tuned with its own preset potentiometer. A master preset allows the pitch of the organ to be shifted over several octaves without altering any other component values. The individual notes will need a slight amount of retuning after this operation because the

voltage control effect of the master preset is not linear. In practice this is no hardship, because once having made the instrument and decided whether to have bass, tenor, alto or soprano pitch simply adjust the presets and leave them.

The advantage of being able to set the pitch of the organ is useful if the project were to be used in school because there need be no variance from one organ to another and later an "Ensemble" of several of the organs could be used to form the basis of a band, similar to a recorder group.

A switch allows vibrato to be selected and a preset control determines the depth of the vibrato. There is no tone control nor volume control; they could be fitted but were left out, with a very good motive. Because a printed circuit board is used there is virtually no free wiring, which sometimes causes problems for beginners and certainly, in this case, would detract from the neat mechanical assembly. The only free wires are those to the battery and probe.

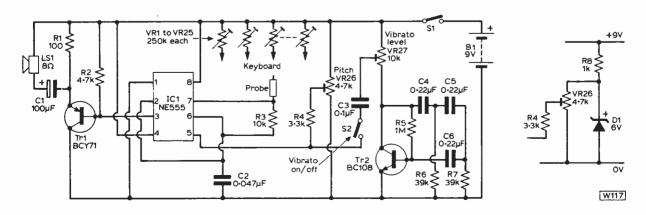
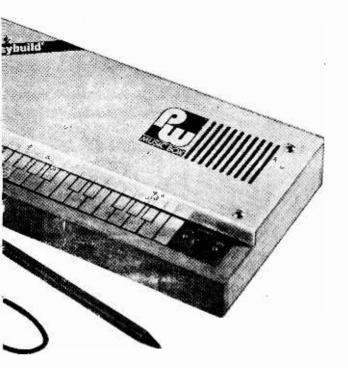


Fig. 1: Full circuit of the Music Box with, inset right, optional circuit for improved stability of the tuning voltage.



CIRCUIT

The circuit is shown in Fig. 1 and the heart of it is an NE555 IC timer operating in astable mode, The frequency of oscillation is set by the value of C2 together with R3 and the selected preset potentiometer from VR1 to VR25. It is the probe, connected to the top end of R3 which is used to select the potentiometer and, hence, the note. The output of IC1 is a square wave which has an amplitude of several volts and it is only necessary to take this from pin 3 and provide a degree of current amplification with the emitter follower Tr1 before it is used to drive a small loudspeaker.

A PNP emitter-follower stage is used so that when no note is being played Tr1 is not conducting, reducing battery consumption. By using an NE555 one can make use of its voltage control capability. A DC voltage at pin 5 will shift the frequency of operation altering the pitch of the instrument over a wide range without changing C2 or any of the other potentiometers. The control voltage is produced by VR26. As the battery voltage falls this control voltage will change slightly affecting the tuning of the instrument but in the majority of cases where the instrument is used as a toy this is not likely to present problems.

If very stable tuning is required this control voltage can be obtained using a zener diode and an extra resistor as shown in the inset to Fig. 1. This modification would require a slight change to the PCB but it is felt that few would want to do this, keeping to the simpler version.

A low frequency signal on top of the DC control voltage will frequency modulate the signal from IC1 which provides perfect vibrato. Tr2 and its associated components form a simple phase shift oscillator which produces a pure 6Hz sinewave output. A controllable portion of this is selected by VR27 and fed via C3 and the vibrato switch to the voltage control input of the main oscillator. Adjustment of VR27 sets the depth of vibrato. It is important that a branded

★ components list

$\begin{array}{cccccccccccccccccccccccccccccccccccc$
VR1-25 \cdot 250kΩ (25 off) vertical sub=miniature preset pots. VR26 \cdot 4·7kΩ ditto VR27 \cdot 10kΩ ditto
Capacitors C1 100μF 12V C3 0-1μF C5 0-22μF C2 0-047μF C4 0-22μF C6 0-22μF All polyester except C1. Semiconductors Tr1 BCY71 Tr2 BC108
IC1 NE555 D1 6V 400mW zener Miscellaneous Miniature slide switch, on-off, 2 off. Speaker,
8 to 35Ω, not more than 2½ in. overall diameter. PCB (see page 742). PP3 battery and press-stud connector. Cabinet, probe and material for cover.
A solid mahogany cabinet with plywood base can be obtained from Birch & Ridley, Watson Road, Worksop, Notts. for £3.50 plus 40p p/p. An aluminium top plate with circular speaker hole can be obtained from H. L. Smith Ltd., 287 Edgward Road, London W2 for 33p plus 17p p/p.

BC108 is used for Tr2 as some general purpose NPN transistors will not have sufficient gain to get the vibrato circuit oscillating. For the same reason use good quality polyester capacitors for C4, C5 and C6 and avoid ceramic types.

The circuit will work with just about any speaker having an impedance of 8Ω or greater but the crucial factor is its diameter so that it will fit on the printed circuit board. An 8Ω speaker will give the largest output but a 35Ω one still gives quite an appreciable output.

CONSTRUCTION

For assembly of the printed circuit board refer to Fig. 2/3. Start by inserting and soldering in all the preset potentiometers. This is a bit monotonous but it gives plenty of practice at soldering before coming to the semiconductors! Next glue the loudspeaker into position with a fast-setting epoxy resin, and avoid getting the resin on the cone of the speaker. Before going on to the rest of the components fix the two slide switches S1 and S2 into position. These switches and the loudspeaker should be mounted on the plain side of the board.

Go on to solder in all the fixed resistors and then the capacitors. The only polarised component so far is C1 so make sure this is inserted the right way round, the positive end of the capacitor should go into the hole nearer to the loudspeaker connection. Insert and solder the two transistors into their correct position and the leads the right way round. The emitter is the wire nearest the spigot on the can, the collector is the wire diametrically opposite the emitter and the base lead is midway between the two but offset to one side. Finally insert the integrated circuit making sure that its orientation mark is in the position shown on the layout drawing.

The only wiring left goes to the battery switch, the loudspeaker and the vibrato switch. A single wire goes to the probe.

TESTING

Before testing, set all the potentiometers to the middle of their range. Connect the battery, switch on and try touching the end of the flying lead on any of the keys, when a strong note should come from the loud-speaker but the tuning will be meaningless at this point. While touching a single key check the vibrato by switching it on and altering the depth by adjustment of VR27. Check, also that adjustment of VR26 will change the note you are holding.

Now decide how you wish to pitch the instrument. Holding the probe lead on the central "C" of the keyboard, adjust VR26 until the note heard corresponds to the middle "C" of the two octave span required. (A piano is a great help here). From there on it is only necessary to touch each note in turn and adjust the corresponding potentiometer until the instrument is accurately tuned over the entire two octaves in question. It is much easier to tune if the vibrato is switched off.

FINISHING OFF

Make the wooden cabinet and the bent aluminium lid as shown in the drawings. If it is not possible to use aluminium then make the lid out of thin plywood or plastic. In fact some readers might prefer to make the whole box from plastic. The printed circuit board should just be a snug fit inside the case.

Place the printed circuit board inside the box and put some temporary packing under the front edge to keep the board level. Mark the holes for mounting the board to the underside of the lid, one in each corner. Make sure that the holes are clear of the printed wiring.

Use long 4BA screws with nuts to bolt the PCB to the underside of the lid and make sure that it stands off sufficiently to leave a small gap between the bottom edge of the front drop and the keys, otherwise a short circuit might occur.

Before completing assembly glue a card strap inside the front edge of the box to hold the battery. Position the battery and thread the probe lead through the hole in the front. A knot in this lead will take the

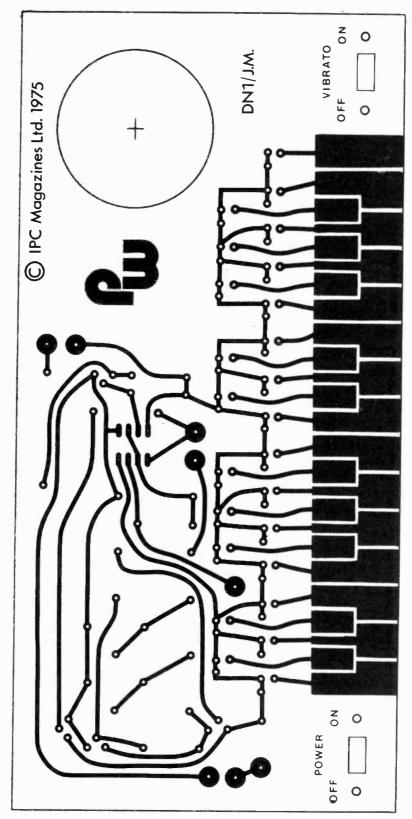
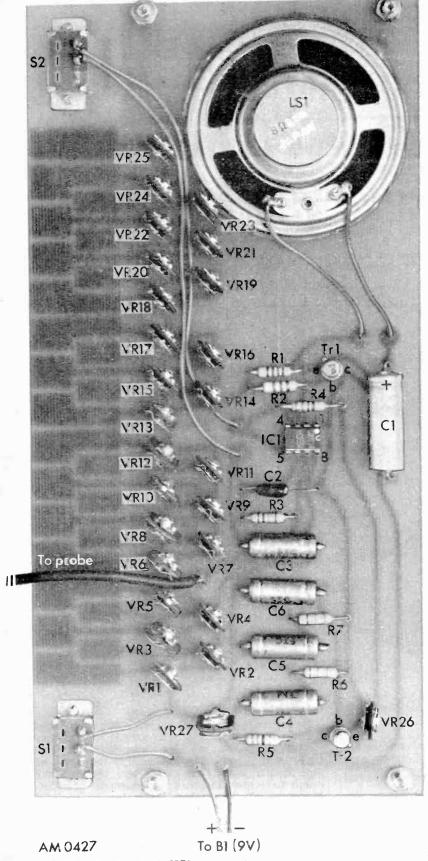


Fig. 2: above, shows the PCB for the Music Box, drawn actual size. Fig. 3: next page, is a guide to the layout of the components on the PCB. The voltage stabilising circuit shown in Fig. 1 is not included on this board. The two switches and the speaker are glued to the plain side of the PCB.



Middle 0 ∞ 9

Fig. 4: 'Keyboard' layout with the 'keys' numbered to enable tunes to be played using the notation shown on the next page.

strain and prevent pulling of the lead from its solder pad. Make a final check on the tuning and then screw the PCB into position in the box.

To make the probe use the body of a felt-tipped pen having first removed the tip and the internals. The flying lead should be threaded through the body, if necessary drill out the back end and through the tip. Strip off a bit of insulation and fold the wire back on itself and apply a smooth blob of solder.

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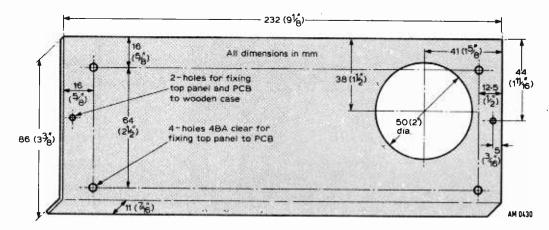
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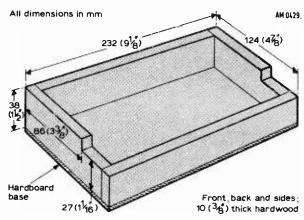
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'JINGLE BELLS'

13 13 — 13 13 13 — 13 16 9 11 13 — 14 14 14 — 14 14 13 13 13 13 13 11 13 11 16 — 13 13 13 — 13 13 13 — 13 16 9 11 13 — 14 14 14 — 14 14 — 13 13 — 13 13 16 14 13 11 9.

To assist the non-musical the notes of some well-known tunes are numbered as shown here to correspond with the 'keyboard' of Fig. 4.





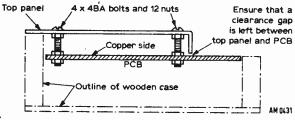


Fig. 5: Dimensions of the top cover of the Music Box. The speaker aperture can be backed with a small plece of cloth or the cutout can be made ornamental as in the author's model.

Fig 6: left, shows the simple case for the Music Box. Fig 7: below left, illustrates the way in which the PCB is fitted to the top cover. It is very important to see that the gap shown is adequate to prevent the top cover shorting the 'keys'.

Finally, carefully glue the wire and the tip into place with epoxy resin.

An overlay, Fig. 4, can be cut out and stuck on the lid to match up with the keys. This is for the benefit of those who cannot read music but would like to practice playing music such as the selection of seasonal tunes shown.

MAKING MUSIC

Having built and tested the Music Box the natural desire will be to play a tune on it! For the non-musical constructor we have reproduced the 'key-board' with numbers, together with the notes of four popular ditties given as numbers, thus enabling a tune to be played without any knowledge of music. The dash indicates a short pause.

To carry the idea further and to make the playing of a tune even easier by this method, the 'keys' can be marked with the numbers by means of small sticky labels or even with a felt-tipped pen.

Eric Dowdeswell Asst. Editor

T has occurred to us that considering something around 110,000 copies of PW are sold every month, the number of articles received from readers for publication is remarkably small! Apart from articles commissioned from established authors, and those written by our own staff, we rely upon material received from readers.

We believe that PW pays authors reasonably well for their efforts so we came to the conclusion that among the many constructors there are plenty who think that they are not capable of putting their practical experience into words and diagrams. We believe they are wrong, so let us see what is wanted by us from you and how we can help you to help us

to help you to a little folly. Phew!

One of the most important aids for the electronics constructor, whether he works on the kitchen table or in a well-equipped workshop, should be a notebook in which he can record circuits used, values of components, lead-out connections of IC's and transistors, circuit changes and modifications and a host of other information that will prove in-

valuable when it comes to writing an article.

Don't be afraid of large circuit diagrams. In my own case, my favourite field in design and construction is receivers and transceivers yet I have never drawn a complete circuit diagram of one in my life! Of each separate stage, yes, with precise details of any home-made components, such as coils, as they were actually made. It is our Technical Illustrator who will put it all together, if necessary. So, if your circuit is at all complicated split it into separate logical stages, taking care to identify various inputs, outputs and power supply lines. Use ruled or graph paper to assist in the preparation of a drawing.

The drawings should be clear, naturally, but masterpieces of artwork are not wanted and will not be used as such, anyway. Accuracy is the watchword and if you make any last minute modifications to the actual model then do not forget to alter the diagrams where relevant and the copy, if affected. This is where the notebook really comes in useful.

Put all diagrams, graphs, tables and suchlike on separate sheets of paper and mark them with figure numbers to agree with the text. Under no circumstances must such material be

included in the main copy.

We like to have your manuscript with wide margins at the top, bottom and both sides and typed double spaced. Even if your copy is perfect we still have to mark it with instructions for the compositors. Of course, the copy can be handwritten but it must be clear and easy to read or the Editor will not be very impressed! I should perhaps point out that all articles received are first seen by the Editor and then passed round the technical staff for their comments before being accepted or rejected by the Editor. It doesn't take very long to do this, so don't worry!

As for general style of writing, look at any articles in PW and follow that. A short introduction, the general thinking leading to the final design, brief description of how the circuit works plus general notes on construction and alignment where called for. As for symbols in the text, again look

at PW.

When typing try to keep to about 48 characters a line and then it is an easy matter to assess the total number of words, which should be shown on a cover sheet to the manuscript.

One item often omitted by an author is a components list and the source and price of any parts which may be difficult to obtain or not generally available. If you have been a constructor for a while you will have accumulated a lot of spare components so, in a project intended for publication, make sure that you quote the correct specification for say, a resistor, for the particular circuit and not the value and wattage that you happened to use from your junk box! Don't quote

several different values of bypass capacitor, just because they were available, where a common value would be much more helpful to the reader.

Check that the components list agrees with the circuit diagram for values and don't forget the items that do not show on circuit diagrams or physical layouts, such as battery clips, transistor holders if used, knobs, dials etc.

Photographs of a treasured project are a rather sensitive point with some authors! Unless good photography happens to be another achievement of the author the results are generally grim if the shots are made at home. Out-of-focus blobs on rumpled patterned tablecloths leave a lot to be desired! Initially they do give us an idea of what the thing looks like but if the article is accepted we will probably ask you to send the prototype to us for photographing in our own studios. DO NOT SEND IT UNTIL ASKED!

If you think you can manage to wield the camera successfully we want clear black and white half-plate pictures but the size is not so important. Identify pictures by writing on the back with a very soft pencil, never a biro pen, or preferably by writing on a small label and sticking that on the back of

the picture.

Now that you are getting close to the stage of sending the lot to us, there are a couple of points more. When the copy is right, number the pages consecutively. Read it through as if you were a reader seeing it for the first time, referring to your circuit diagrams etc. which will crosscheck your figure numbering. Small alterations may be made by hand in the text but if extensive should be typed on a separate sheet of paper with instructions to insert where indicated.

It will be a nuisance I know, but before you part with all your bumph do get it photocopied, diagrams and all. We may need to refer to you on some point or other which is pretty pointless if you haven't got a copy of your article!

When we get your masterpiece we will acknowledge its receipt at once followed by a letter later on to advise acceptance or otherwise. Payment is usually on publication of the article but the Editor may, in certain circumstances, decide to pay on acceptance but this would be exceptional. Obviously a project should appeal to our readers and it does not have to go to six pages or several parts, a couple of pages can be just as interesting and equally welcome.

We do not expect our authors to invent new circuits but if you know that your design is based upon a circuit already published then we would expect you to acknowledge the fact in the text, as is frequently done. Our editorial staff read an awful lot of technical magazines in the course of a month and a couple of us have pretty long memories (and a lot of years!) so don't bother to submit a direct 'pinch' from another magazine. If we don't spot it, our eagle-eyed readers

will!

SUMMARY

Diagrams, circuits, graphs and the like must be on pages separate from the copy and numbered to correspond with the copy.

The copy should be typed with double line spacing and with ample margins at the top, bottom and sides of the pages and on one side only of each sheet. Try to type to about 48 characters a line.

Photographs should be clear and in black and white, preferably half plate size. Identify each photograph on the back, see text.

Look at any copy of PW for guidance as to symbols and style to be used.

WHY NOT CONTACT THE EDITOR NOW WITH BRIEF DETAILS OF THAT PROJECT YOU WOULD LIKE TO WRITE ABOUT?

Now...the most exciting Sinclair kit ever

The Black Watch kit

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★ practical – easily built by anyone in an evening's straightforward assembly.

*complete - right down to strap and batteries.

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works as soon as you put the
batteries in. On a built watch
we guarantee an accuracy
within a second a day-but
building it yourself you may be
able to adjust the trimmer to
achieve an accuracy within a
second a week.

The Black Watch by Sinclair is unique.

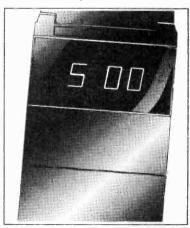
Controlled by a quartz crystal...
powered by two hearing aid
batteries... using bright red LEDs to
show hours and minutes and
minutes and seconds...it's also
styled in the cool prestige Sinclair
fashion: no knobs, no buttons,
no flash.

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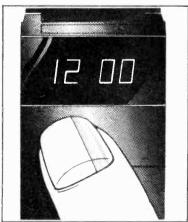
The special features of The Black Watch

Smooth, chunky, matt-black case, with black strap. (Black stainless-steel bracelet available as extrasee order form.)

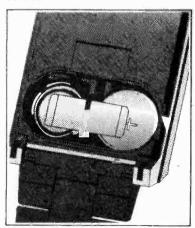


Large, bright, red display - easily read at night.

Touch-and-see case – no unprofessional buttons.



Runs on two hearing-aid batteries (supplied). Change your batteries yourself – no expensive jeweller's service.



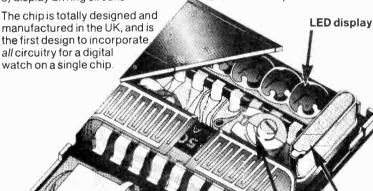
The Black Watch—using the unique Sinclair-designed state-of-the-art IC.

The chip...

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This chip of silicon measures only 3 mm x 3 mm and contains over 2000 transistors. The circuit includes

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- b) divider chain
- c) decoder circuits
- d) display inhibit circuits
- e) display driving circuits.



...and how it works

A crystal-controlled reference is used to drive a chain of 15 binary dividers which reduce the frequency from 32,768 Hz to 1 Hz. This accurate signal is then counted into units of seconds, minutes, and hours, and on request the stored information is processed by the decoders and display drivers to feed the four 7-segment LED displays. When the display is not in operation, special power-saving circuits on the chip reduce current consumption to only a few microamps.

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Quartz crystal

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GENERAL SERVICING

An occasional series by LES LAWRY-JOHNS chatting this time on—

1 - UNIT AUDIO EQUIPMENT

THE units referred to in this article are mainly those of the cheaper variety costing, say, under £100. Such a unit could have an auto-changer of the cheaper BSR type with a simple amplifier system using a single audio chip for each channel or perhaps an audio pair, a driver and a preamplifier for each channel. Several examples of such units have been produced by various firms, some with radio, some without, and they all tend to follow a similar pattern of a basic design with limited output and few frills.

Auto-changers

We shall start by taking a quick look at the autochanger which does tend to give one or two troubles which occur so often that they can be predicted, within reason. The most common trouble which we have experienced of late is due to lack of lubrication on the centre post, the friction sometimes becoming so great that it is difficult to spin the turntable by hand. Normally things do not get to this stage as the user is concerned by the slow and varying speed of the turntable and either does something about it or gets something done.

A variation on the same theme is noisy rotation, causing the pick-up arm to vibrate. The answer is to remove the centre trim and circlip, ease off the turntable and oil the centre post. Check for any roughness and do the same with the turntable centre bearing. Whilst doing this it is worthwhile checking the motor and idler. Whilst the bottom bearing of the motor rarely needs attention, although it does happen, the top bearing loses its lubrication, understandably enough, much earlier. So a few drops in the top bearing do not come amiss. The screeching of a dry bearing is not an uncommon noise to issue from the average type of motor.

Another cause of speed variation is lack of friction between the motor spindle and the rubber of the idler wheel. The rubber tends to become shiny and requires roughening with a piece of fine sandpaper or the like. Make sure that no oil gets on this rubber and that it spins easily on its post. It is often thought that wear on this rubber idler will cause the speed to vary, due to its smaller diameter. This is not so. The size of the idler wheel has no influence on the speed of the turntable at all, unless of course it has an irregularity on its surface when it will produce a bumping effect. The speed is controlled by the motor and its drive spindle and the size of the turntable driven surface.

Having got that off our chest we should now have a smoothly running motor, an evenly spinning idler driving a turntable which is freely rotating about the centre pillar. Belt driven and direct drive turntables need not concern us here as they are found only in more expensive assemblies.

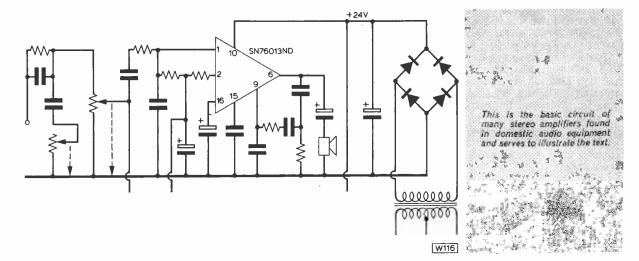
The Amplifier

Before considering any specific faults we should first consider external factors which can cause them. The most common fault is failure of the output transistors or ICs (chips). Such failure can be caused by the use of unsuitable loudspeakers or a fault in the cable to them, including the possibility of the leads in the plug touching. It pays to check the plug and lead, plus any joins in it, and the loudspeaker itself. If the amplifier output is specified for 8Ω working, ensure that the loudspeaker is an 8Ω one and that no other loudspeaker has been wired across it.

A good number of loudspeakers clearly marked 8Ω have been found to be 3Ω , and usually of unknown origin, and this has meant that the equipment to which they have been fitted has been overrun, dissipating excessive current and thereby excess heat. This has meant the early demise of the ICs



-with suspicion of the driver-



or output transistors operated beyond their rated power. Quite often the loudspeakers are fixed in a position, together with their wiring, which makes removal inconvenient so that when the amplifier fails it is only this which is taken for repair. With new components fitted and tested upon correct speakers, the equipment is once more coupled up and the overruning is repeated.

A permutation of this state of affairs is often that one speaker is incorrect, one correct. One channel fails due to overrunning and the owner changes over the speaker plugs to "check the speakers". This means that the wrong speaker is now connected to the good channel and the correct speaker to the failed one. The equipment can be operated like this for some time on the basis that "some sound is better than none" with the resultant destruction of the good channel.

Another consideration here; if one channel fails and the supply is not regulated, the remaining channel will operate at a higher supply voltage and thus



-leave no whiskers which can rotate-

may fail due to this factor. The only moral which can be drawn is that if one channel fails, for whatever reason, the equipment should not be used until the fault(s) is rectified and the system checked.

Before leaving the subject of loudspeakers let us make one or two points, probably elementary to most, quite clear. If loudspeakers are to be added to an existing system and there is no provision for this on the amplifier, add them in series (cut one wire and insert the speaker), never loop off in parallel. Parallel working decreases the impedance and thus increases the load on the amplifier. Series working increases the impedance and decreases the load; not so much power but the amplifier will last longer! If an amplifier is designed to work into 8Ω , use an 80 load, or more, but not less. If leads have to be joined, make sure they cannot touch accidentally, If plugs are to be soldered, bring the insulation right up to the tags and leave no whiskers which can rotate and touch if the leads are twisted. These simple precautions can avoid annoying and costly repairs. If space permits, put a short length of insulating sleeving over the insulation of the wire and slide it over the joint when it has been soldered.

Servicing Amplifiers

The rather simple stereo amplifier which is likely to be fitted in our unit under discussion, will have a pair of audio chips or two pairs of output transistors with driver(s) and a preamplifier. An example of one channel a unit, with the bare necessities, is shown in the circuit.

Undoubtedly the most common fault in these units is the failure of one or both of the ICs, usually SN76013ND or SN76013N. The main difference is that the ND lies flat on the panel with two pieces of metal soldered to the print earth as a heat sink. The N series differs by having these pieces of metal bent up to form a larger finned heat sink.

If one is lucky, and things have not gone too far, the unit can be connected to the speakers and switched on to produce sound from one speaker and nothing (or a hum) from the other. If there is no sound at all from one channel this chip will be quite cold and a voltage check will show a reading on pin 10 only. If there is a hum from one side the chip will be overheating and again is easily identified.

Replacement of a defective chip is not at all difficult provided one has an efficient means of removing the solder to leave the chip loose in the holes so that it can be lifted out and the new one popped in, soldered on all active pins, and any flux removed from between the joints. Removing the solder in the first place is the major part of the battle. A soldering bit which fits over all pins at once and sucks up the solder in one go is a luxury which not everyone has available. Most are content to use a simple vacuum pump or perhaps the more efficient desoldering braid. On occasions this is all that is required but, more often than not, things are not that simple.



-many engineers are climbing Mount Everest-

For example, both channels may be inoperative but only one chip need be at fault (check voltages for this one) because one chip can turn the other off. Again, one channel may be working when tested and the other is defective. When the latter is replaced the unit may work fine for a time and then one channel fails, quickly followed by the other. Investigation may show that the new chip has failed but the other is now functioning just to add to the confusion. The answer is that one has been intermittent causing the voltage to rise, in turn causing the otherwise good one to short internally. The answer is to replace both chips when there is the slightest hint of "one channel went first, and then the other". Such hanky panky can also cause trouble elsewhere. For example, a shorted chip (or output pair of transistors) can cause a heavy flow of current sufficient to cause the bridge rectifier to short out before the fuse fails. Hence one can be faced with a blown fuse, apparently caused by a defective rectifier. Replacement of these parts should be followed by a careful check on the supply line to ascertain whether there is still a contributory short.

It is alarming just how much time, money and patience can be expended on a seemingly simple job if one is not aware of the pitfalls that await the unwary or unwarned.

This is one of the reasons why audio unit repairs are not exactly sought after by workshops, often engaged in the usually more straightforward servicing of TV receivers. The fact that these latter devices are being served up with ever-increasing numbers of chips probably explains why many engineers are leaving the trade and taking up the less arduous pursuit of climbing Mount Everest or deep-sea diving. Those remaining hope that replacement panels will save them in the field whilst the faulty panel can be put on a test rig under test for diagnosis by someone else during the day or by himself in the wee small hours!

In all cases the rule is to know what the voltages should be at various points or at least be able to compare a working stage with a non-working one, and to take these voltages without damaging the item under test. An ordinary voltmeter test prod is a pretty clumsy affair and can easily slip between adjacent pins of a chip. Either sharpen the probe or bind a needle to it. If there is doubt, check all relevant components. A leaky capacitor or a faulty resistor is often found after a chip has been needlessly replaced.

AC or DC Coupling

Whilst most up-to-date inexpensive amplifiers use chips, some modern and all older ones use a balanced pair in the output stage of each channel with their drivers and pre-amplifiers. The very early amplifiers used transformer coupling from the driver to the output pair and this made fault diagnosis very easy as the output stage was, from a supply point of view, bias, etc., independent of the earlier stages. Thus if one transistor's voltages were high it was a comparatively easy matter to cold test each transistor and associated resistors to ascertain where the short or open circuit was occurring.

It hasn't been that easy for some considerable time now, as transformers are a thing of the past; stages are DC coupled and thus interdependent. A fault in an early stage can easily switch off all succeeding stages so that wildly wrong voltages in the output stage need not denote a fault here, or in the driver stage(s). The rule is therefore to regard the amplifier as a whole and start from the beginning, say from where the preamplifier is isolated from the preceding stage by a capacitor. The snag, once again, is that the pre-amplifier may depend for its bias on the output stage, then where are you?

Quite often the job is less tedious than it could be by virtue of the fact that certain types of transistor are more prone to fail than others. For example, if we know that AC128 transistors are used, these are tested first, together with the associated emitter resistors. This has saved time, again and again. The method of cold testing transistors with an ohmmeter has been described on many occasions and will not be repeated here. Quite apart from this, if the emitter resistors appear scorched or otherwise distressed, these usually being about $2 \cdot 2\Omega$, it is a pretty safe bet that the output pair need replacement together with suspicion of the driver.

If in doubt it is far better to replace all suspects in one go rather than try to pinpoint one particular transistor. Low and medium power audio transistors are cheap and easy to replace (as a rule, but there are always exceptions) but it is not always easy to gain access. So once the panel or unit is out for repair, do what is necessary plus anything else remotely suspect before reassembling.



-the answer is to replace both chips-

Noise

We have so far considered the causes of inoperative stages, but, all too often, the fault is the annoying one of excessive background noise. Usually the suspect items are capacitors or transistors, the latter being the main culprits, with electrolytic capacitors following close behind. Sometimes the responsible component is heat conscious and can be identified by a judicious squirt of cooling solution (Freezit) but more often the trouble is due to an internal defect which no amount of freezing or disturbing will alter. Operation of the volume control will immediately identify the rough position in the circuit (before or after the control, always assuming the control itself is not responsible) and this is a starting point

Bearing in mind the fact that the whole circuit is probably DC coupled and that shorting the base to emitter of an early stage would probably shut down the whole circuit and thus do very little to identify the actual culprit, a fairly high value capacitor can be used (depending upon the circuit values) to short out the signal and eventually the noise when the faulty stage is reached.

Distortion

Distortion is usually due to transistors working under improper conditions, sometimes caused by leaky capacitors, sometimes by faulty transistors, very occasionally by incorrect value resistors. The action taken depends very much upon the experience of the repairer. Very often a short-cut can be taken if the type of capacitors fitted are those which are well-known to be likely to break down. If, for example, some small electrolytic capacitors are fitted which are coloured black with silver writing denoting their value, etc., it is prudent to check the voltages of the associated stages and if these are suspect, remove the capacitor and test again. If the voltages are now right, and a meter check reveals heavy leakage through the capacitor, the short cut is well justified. Quite often the output transistors are unmatched or one is defective, this showing in a voltage check followed by a cold resistance test. If the voltages are wrong but the cold test appears about right, check the driver stages where a high reading may be found both ways, base to emitter or base to collector, or perhaps a low reading in the reverse (when it should be high, taking into consideration the circuit values) direction.

Dry Joints, and the like

It is often the case that incorrect working is not due to component failure at all and it is always worthwhile spending a little time gently rocking various components to ensure that they are properly soldered to the panel. It is surprising how long a piece of equipment will function with a component not being soldered at all in the first place! It doesn't usually show up until, as a rule, the equipment is disturbed. Since this is usually due to a fault developing in another section, the repairer is faced with two faults instead of one although he probably only realises this when the more obvious fault has been located and cleared. This is irritating, to put it as mildly as possible.

A variation of this is a crack in a copper track which may not show up until the panel is flexed. This again is a great time waster and a combination of signal injection, voltage reading and continuity testing may be required to locate the break if it cannot be seen.

Checking the Cartridge

One of the more common faults is that the output of one channel is normal but the output of the other is low or absent. It is prudent to check the cartridge on the pick-up head before taking any other action. This is done quite easily by disconnecting the leads from the cartridge, with the amplifier on and the balance control at centre, when hum, equal from each channel, should be obtained, picked up by the active lead to each channel, usually the red for one channel and white for the other, the black and green leads being earthed and common. If the red clip provides a reasonable hum when touched as does the green for the other channel, the amplifier is likely to be in order and the cartridge at fault. A replacement cartridge is probably the only attention required. If there is hum from one side but not the other, follow the leads underneath to the tag strip and repeat the hum test. If equal hum is obained, the continuity of the relevant lead to the pick-up head should be checked. If no hum is received on one side follow through to the amplifier and check the input to this with the lead connected and with it off; to check for the rather unlikely possibility of a short in the cable, from inner to screening.

Having said this we hasten to add that if phono plugs are used for the connection to the amplifier or to the tag strip the possibility of such a short becomes a probability and will be found where the screening is soldered to the plug body, the heat used having melted the insulation between the inner and the outer. If this is so, cut back the cable and make the connection with a longer pigtail on the screen. It may not look so nice but a short is less likely.

TO BE CONTINUED

PRODUCTION LINES colin riches

THE LOCKABINET

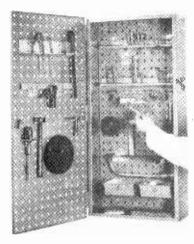
As tools of all types become increasingly expensive Lockpanel Ltd. have introduced a "Lockabinet".

The photograph illustrates the all British-made cabinet which is ruggedly constructed from 1·25mm (18G) metal panels. The cabinet has overall dimensions of 1000 mm (39") x 460 mm (18½") x 200 mm (8"). The back panel and door are perforated with a regular pattern of square holes into which can be hooked a wide range of tool holding accessories suitable for storing virtually any type of hand tool, engineers or electrician's tools.

The Lockabinet is wall mounted, with access to the fixing brackets from inside the cabinet. Thus, when locked it offers security for its contents whilst providing an orderly and visually effective storage method—each tool being easily located when required.

Finished in anti-chip epoxy stove enamel of light green colour the Lockabinet is provided with a chromium plated integral lock.

All the accessories can be purchased separately from the cabinet



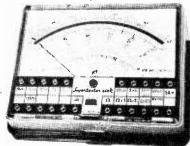
but the firm offers a complete kit which includes a cabinet plus a selection of the most generally useful accessories at £37.48. The price includes packing, carriage and VAT.

Lockpanel would be pleased to send full details of the Lockabinet to any readers on application. The Lockpanel Company Limited, Marjorie Street, Leicester, LE4 5GZ.

THE SUPERTESTER

The Supertester 680R is an 80-range test meter with a 20,000 ohm/V sensitivity.

Technical data—Volts A.C. 11 ranges: 2-10-50-250-1000-2500 Volts and 4-20-100-500 and 2000 Volts. Volts D.C. 13 ranges: 100mV-2V-10-50-200-500-1000 Volts 200mV-4V-20-100-400 and 2000 Volts. Amp. D.C.12 ranges: 50 μA-500 μA-5 mA-50 mA-500mA-5 Amp and 100 μA-1 mA-



10mA-100mA-1 Amp and 10 Amp. Amp. A.C. 10 ranges: 250 µA-2 5mA-25mA-250mA-2·5A and 500/LA-5mA-50m A-500m A-5A. Ohms 6 ranges: x1-x10-x100-x1000-x10,000 and Low Ohms. Detector Reactance 1 range: from 0 to 10 Megohms. Frequency Output 2 ranges: from 0 to 500 and from 0 to 5000Hz. Voltage Output 9 ranges: 10-50-250-1000-2500V and 20-100-500-2000 Volts. Decibels 10 ranges from -24 to +70dB. Capacity 6 ranges: from 0 to 50,000 and from 0 to 500,000pF using the mains and from 0 to 20, from 0 to 200, from 0 to 2,000 and from 0 to 20,000 microfarad using the incorporated 3 Volts battery. Bold figures indicate A V x 2. Price complete with case and probes is around £18.50. Further information on the 680R and other instruments from: Electronic Brokers Ltd., 49-53 Pancras Road, London,

KNOBS, ETC.

A broad range of collet knobs and accessories is now available from Roxburgh Electronics Ltd.

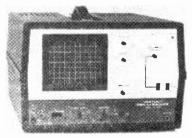
Designed for ease of handling and simplicity of assembly, they are produced to fit shaft diameters of 3mm., 4mm. or 6mm., and 1 in. or 1 in. The diameters of the knobs, at 10, 11, 15, 21 and 29mm., are such that they will fit into the cap recess of the next largest size, enabling double knobs to be formed.

The knobs and nut covers are available in winged and plain styles, with or without line, in matt finished black, red or grey nylon; the caps and pointers, which are also of matt finished nylon, are additionally available in green, blue or yellow. The captioned dials, which can be supplied with a variety of standard legends and symbols, are of polycarbonate. Roxburgh Electronics Ltd., 22 Winchelsea Road, Rye, Sussex. Telephone: Rye 3777.

DC-5MHz, 100mV SCOPE

The new Heathkit 10-4560 'scope's sweep speed is continuously adjustable from 20 ms/cm to 200 ns/cm. Maximum vertical sensitivity is 100mV with a front panel switch for X1, X10 and X100 attenuation, AC or DC. Vertical input impedance is 1 megohm for low circuit loading. Up to 400 VDC can be applied directly without circuit damage, making it a great 'scope for students' use. For phase and frequency measurements, an external horizontal input can be applied directly through the front panel input jack. It has 250mV sensitivity with DC to 100kHz bandwidth. Display stability is excellent because the low voltage supplies for the amplifiers and sweep circuit are zener regulated. The primary circuit of the power transformer is fused for protection from over-load.

Kit K/IO-4560 costs £69.90 including VAT and delivery within the United Kingdom. Full details available upon request from: Heath (Gloucester) Ltd., Bristol Road, Gloucester GL2 6EE or The London Heathkit Centre, 233 Tottenham Court Road, London W1P 9AE.



AERIAL TUNER UNIT

The Codar RQ-80 A.T.U. has been designed to match the random lengths of single wire often employed as aerials on short wave receivers, and to provide an efficient coupling to the receiver input with appreciable increase in signal level. It is particularly effective where short or indoor aerials have to be used because of space limitations.

The RQ-80 employs an air spaced Hi-Q low-loss "Codarcoil" inductor in a tuned input/output PI-network with a very wide range of matching obtainable with 10 switch positions of inductance taps. An additional switch position transfers the aerial direct to the receiver.

The nominal range covered is 1.5-30MHz continuous, the L.F. end limit being dependent on the type and length of aerial in use, and can be lower than quoted.

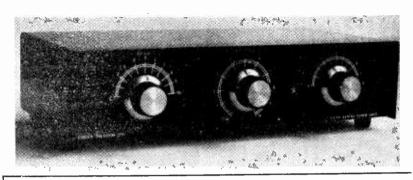
It is fully screened in a metal cabinet 23cm x 12cm x 5cm (9" x $4\frac{3}{4}$ " x 2") and finished in charcoal grey and black with white legends. Co-ax output socket to receiver is provided. 12 months guarantee. Price is £12 50 posted. Codar, Valcon Works, Burrell Buildings, Churchill Industrial Estate, Lancing, Sussex, BN15 8TZ. Tel. Lancing 61901.

VEROBOXES

Vero Electronics Limited announce the introduction of a new range of Plastic Veroboxes® which have been designed to house the smaller type of instrument or control unit.

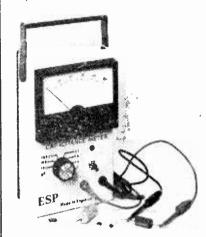
The boxes are constructed of two mouldings in light grey high impact A.B.S. and contain built-in guide slots for vertical mounting of P.C. boards or metal plates. The base panel is also fitted with threaded inserts for the attachment of a horizontal P.C. board or chassis. The boxes include, anodized aluminium front and rear panels for the mounting of switches, knobs, meters or plugs and sockets. These panels are held in position by the mouldings so that no panel fixing screws are required. The two mouldings themselves are screwed together by four screws which enter through the base moulding and are hidden from view by the plastic feet used with the boxes.

The illustration shows the various sizes of Verobox® which are available together with examples of the fixing of P.C. boards. A new full colour brochure is now available describing these latest additions to the Vero range of small enclosures. Vero Electronics Limited, Industrial Estate, Chandlers Ford, Eastleigh, Hants.



CAPACITANCE METER

Electronic Services & Products Limited, have introduced a new linear capacitance meter to meet a requirement for fast accurate



measurement of a wide range of capacitors.

The instrument incorporates integrated circuits with a reliable linear scale meter producing accuracies usually reserved for manually balanced instruments.

Measurements as low as 1pF and up to $10\mu F$ are easily obtained by the simple selection of the appropriate range and NO balancing is required at any stage of the operation. The correct value is simply read direct from the meter.

Power is provided by two 9 volt (PP3) batteries whose condition is continuously monitored by a Light Emmitting Diode. Should the batteries fall below the voltage required for accurate measurement then the LED will not light. Price £35.00. Electronic Services & Products Ltd., Braunston, Daventry, Northants. NN11 7HH. Tel. Rugby 890672.

SINCLAIR'S DIGITAL WATCH

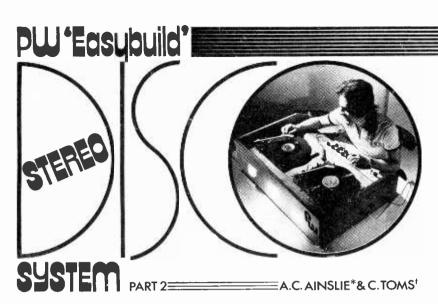
Sinclair recently announced their new digital watch (see News . . .) The electronic circuitry which controls the watch is all contained on a Sinclair-designed IC measuring 117 x 123 thou.—developed using injection logic technology—I²L.

Sinclair believes that this original watch chip design, containing over 2.000 active devices is the sole

production watch chip, using injection logic, available in the world today. The chip requires only a quartz crystal, trimmer capacitor, a LED display and mercury cells to complete the watch circuit.

The three-function watch employs a 32·768kHz flexural bar crystal as the frequency control element for the oscillator and this is trimmed in production to a precise frequency.





Continued from last month

Heavy feedback around the power amplifiers has produced a design very tolerant of supply voltage fluctuations. This has saved the expense of a stabilised power supply and allows a reserve of power in the smoothing capacitors to give a transient music power output exceeding 100W.

Current consumption for one channel at full power is in the order of 2A. Ample safety margins are therefore provided by specifying a 6-6A bridge rectifier to power a stereo console. Smoothing is provided by two separate 1000 pF capacitors since a single 2000 pF capacitor to handle the necessary ripple current and high voltage is not generally available.

THE LIGHT MODULATOR

As there is sufficient audio signal voltage available from powerful amplifiers, a passive selective network is used for channel separation. The crossover frequencies are 3kHz and 7kHz giving better results than the more usual low frequency crossover networks. Fig. 5 shows the circuit diagram.

The level of each channel is controlled by VR16 (HF) VR15 (MID) and VR14 (LF). Overall display brightness is controlled by VR13 with R53 as a limiting resistor. Trigger transformers T2, T3 and T4 drive the gates of the thyristors and isolate the input circuitry from the mains. To reduce any mains borne interference, a capacitive suppression filter is provided (C33-39).

CONSTRUCTION

Ease of assembly and repeatability of results are ensured by assembling all the electronics on printed circuit boards with the exception of the mixer which is so simple that a p.c.b. is not needed.

Each sub-assembly is completed and preferably bench tested before being mounted into the console. The power supply is assembled in the console as it acts as a structural support and would need to be built before the other units could be tested.

STEREO/MONO OPTIONS

A mono disco console comprises a single pre-amp/power amp board, mono mixer and a power supply. Mono cartridges would be used in the turntables or stereo cartridges wired for mono (both channels paralleled).

LIGHT MODULATOR (OPTIONAL)

Resistors

R52 * 39 Ω 5W wirewound VR13 250 Ω 1W wirewound

VR14 100Ω

VR15 1000 >horiz. skeleton presets

VR16 100Ω

Capacitors

C30 0-47/rF 100V working

C31, C32 8 F bipolar (B. B. Atkin) (2 off)

C33-C39 0 1/rF 1000VDC (7 off)

Inductors

L1 1mH Type WK05/3K L2 0-5mH Type WK1/B3K }(B. B. Atkin)

T2-T4 High frequency pulse transformer (ITT) (3 off) (B, B, Atkin)

Thyristors

SCR1-SCR3 BTY79-400R (for 1kW per channel) or BT106 for console lights only (3 off)

Bulbs

LP2-LP4 100W spot bulbs (B. B. Atkin) (3 off)

Miscellaneous

Brass/ceramic bulb holders (3 off) (B. B. Atkin) S4-S6 S.P.S.T. miniature toggle switches (3 off) S7 S.P.S.T. illuminated rocker switch F3 2A 20mm fuse and page! mounting holder

F3 2A 20mm fuse and panel mounting holder Terminal pins (10 off), printed circuit board (1 off)

^{*}Consultant †W.K.F. Electronics

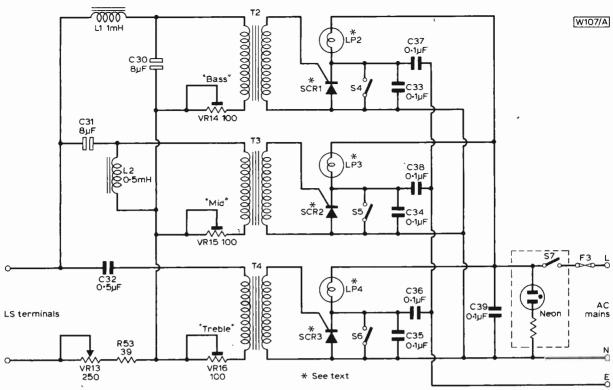


Fig. 5: Circuit diagram of the Light Modulator for use with the Disco system. The thyristors may be either BT106 for console lights only or BTY79-400R for up to 1000W of external lighting.

A stereo console would have a pair of pre-amp/power amp boards (one for each channel), as well as a stereo mixer using tandem controls and incorporating a balance control. A single power supply of adequate current rating is used, this being the same as for the mono version.

To allow for future conversion to stereo, a mono system could be built using a single pre-amp/power amp board but with a stereo mixer. To convert to stereo all that would be involved would be the construction of a second amplifier board and the removal of the cross-channel shorting link on the pick-up cartridges.

AMPLIFIER BOARDS

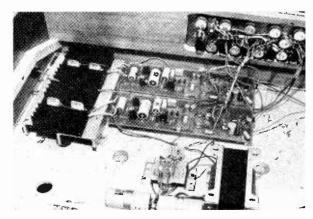
The p.c.b. design and component layout are shown in Figs. 6 and 7. Component mounting is quite straightforward and should follow normal practice. Attention should be paid particularly to capacitor and transistor polarities. Some of the transistor numbers are rather similar and particular care has to be taken not to confuse them. Close tolerance resistors have been specified to ensure consistent performance and all capacitor voltages have been chosen to allow a wide safety margin. C23 must be a low leakage component of adequate voltage rating. Polyester or tantalum capacitors are satisfactory but an electrolytic should not be used as the leakage currents upset the amplifier balance.

Small terminal pins (Veropins) are soldered to the board to take external connections.

All three driver transistors in the power amplifier dissipate quite high powers and need heatsinks. Simple black anodised clip-ons are perfectly satisfactory giving a thermal resistance of 50°C/W in free air.

The output transistors Tr15 and Tr16 are TO3-cased devices which require an insulating mounting kit on account of their "live" cases. A 150mm (6in) length of black anodised extruded heatsink which gives a thermal resistance of little more than 1°C/W and is adequate for both output transistors.

Silicone grease or special heatsink compound should be lightly smeared over the insulating washers prior to mounting the transistors. Shakeproof washers should be used on the mounting nuts and a solder tag placed under one nut of each transistor as the collector connection. A simple ohmmeter check should be made to ensure that none of the transistor connections is shorting to the heatsink. Two bundles of three colour coded wires connect the output transistors to the p.c.b. terminal pins.



Layout of the amplifier boards, power transistors on heatsinks and power supply components on the wooden cabinet described in detail next month.

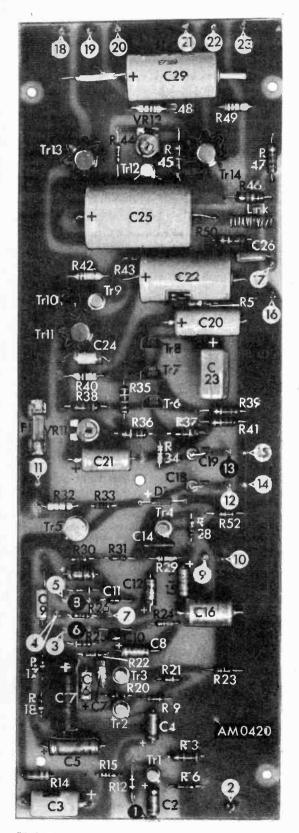




Fig. 6 and 7: Layout of the components on the amplifier board p.c.b. and printed circuit design (not to scale). The link to the right of C25 is colled to aid high frequency stability (about ten turas).



Front view of the completed Disco Unit

POWER SUPPLY

The power supply transformer is mounted centrally on the bottom of the console. In this way it offers some support to the centre of the deck board which rests directly on top. If the recommended transformer is not used additional packing may be required to bring the overall height to 123mm. A transformer of low leakage flux should be used to reduce the possibility of hum pickup.

The bridge rectifier is mounted on a small heatsink which, together with a clip for the smoothing capacitor is screwed directly on to the wooden baseboard (see photo).

A terminal block is fixed to the bottom of the console to supply mains from the on/off switch to the transformer. When the decks are installed they will also draw their mains from this terminal block.

SETTING UP THE POWER AMPLIFIER

Before power is applied to the board, VR12 (quiescent current preset) must be set fully clockwise and VR11 (common mode voltage) set to midway to avoid damaging the pre-amplifier on switch on. No connections need be made to the pre-amp and the power amp input (negative end of C19) is temporarily shorted to carth.

With 80V applied to the power amplifier, VR12 is adjusted to bring the positive end of C25 to exactly 40V.

Should an oscilloscope and signal generator be available. VR11 can be adjusted for symmetrical clipping of a 1kHz sine wave applied to the power amplifier input. There is no need to have a load connected for this adjustment which is just as well as few loudspeakers would safely handle a 100W plus sine wave.

In the event of no equipment being available. VR11 should be replaced with a two per cent $60k\Omega$ resistor which would give near to optimum performance.

Adjustment of the quiescent current preset VR12 is made with amplifier at operating temperature preferably installed in the plinth. Before VR12 is moved from its fully clockwise position, the amplifier is used to deliver a medium power (20 or 30W) into a load for a quarter of an hour or so to give sufficient time for the temperature to stabilise. With the input short circuit removed, the power ampli-

fier will accept the output signal from most radio tuners or tape recorders and will drive a loud-speaker or dummy load (four 15Ω 10W resistors in parallel). The input signal is connected between earth and the negative end of C19, a suitable amplitude being 100mV or so.

When the temperature has stabilised the supply should be switched off, the input short circuit replaced and the supply fuse on the p.c.b. removed. The collector connection to Tr15 (pin 18 on the p.c.b.) is then removed and a 50mA meter placed in series. The load is removed from the output as the surge of current charging the output capacitor would damage the meter.

Having checked that the meter connections are secure the fuse is replaced and power applied. Vkl2 is adjusted carefully for a reading of 8 to 10mA. this quiescent current being sufficient to virtually eliminate crossover effects.

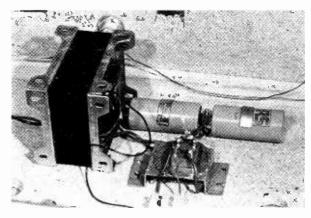
It is necessary to carry out this adjustment fairly rapidly so that the transistors do not cool down significantly from their operating temperature. When the complete Disco system has been assembled in the console, it is as well to reset the quiescent current after an evening's use. Readers without the equipment necessary for this setting-up procedure should turn the preset 20° from the fully clockwise position. This will result in a low but adequate standing current.

Under no circumstances should power be applied to the amplifier without the milliammeter or Tr15 collector connected otherwise most of the transistors will be destroyed.

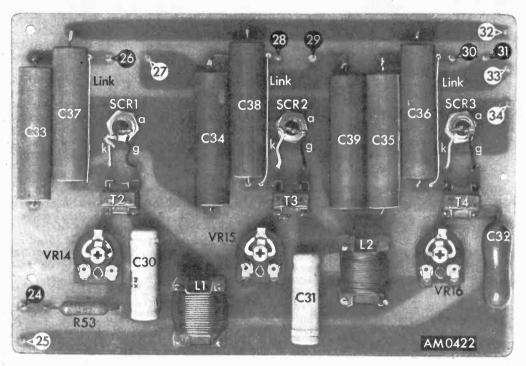
LIGHT MODULATOR CONSTRUCTION

The three-channel light modulator is assembled completely on a single p.c.b. (see Figs. 8 and 9).

Three amp stud-mounting thyristors are specified which are capable of driving up to about 300W of lighting for each channel. The devices need to be considerably over-rated because of the low resistance of filament lamps when cold, i.e. on switch-on. The 3A devices are simply cooled by an excess of copper on the p.c.b. but additional heatsinks would be advisable should higher current devices be employed to drive larger light columns. Such heatsinks could take the form of a simple aluminium "U"



View of the power supply components which are mounted on the base board. The power supply can be built temporarily in order to test the amplifier boards.



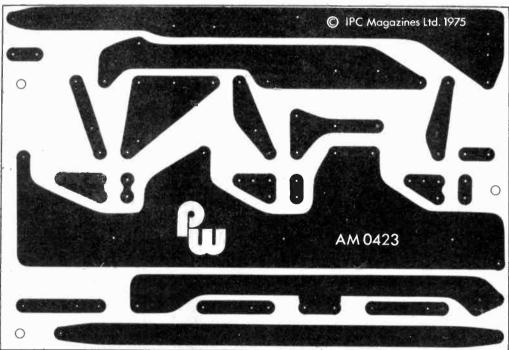


Fig. 8 and 9: Construction of the Light Modulator board showing layout of components and printed circuit layout.

sandwiched between the device and the board of two or three inches area or a commercial stud package cooler could be used.

The trigger transformers must be of good quality as the safety of the whole Disco system depends on the interwinding insulation of these components. The amplifier side of the electronics and the turntable metalwork should be properly earthed through the three-core mains lead to ensure operator safety

even in the event of a breakdown of these transformers.

VR13 adjusts the overall sensitivity of the modulator and is set to produce a satisfactory display after installation.

In Part 3 cabinet construction and interwiring of the complete unit will be described.



by Eric Dowdeswell G4AR

REMINDER of the winter comes with the No. 1 edition of the 160m DX Bulletin from "Stew" Perry W1BB for the 75/76 season. If you once listened to Top Band in the daytime and found nothing, you could not be blamed if you wrote-off the band for good! However, you would be very pleasantly surprised if you tried again after dark! Last season was the best yet for Stew, working 62 countries and all the signs are that he will do even better this season. Prefixes already active include VK, KH6, ZL, JA, VS6, PY and many others, with promise of activity from KC4, VR1, VP2 and HB0.

Once again W1BB has organised Transatlantic Tests especially for Europeans who have not so far been able to work a W station, and vice versa. Dates are December 21, January 11 and February 8 from 0500 to 0730 GMT. Even if you are only listening it is still a thrill to realise that your local G station with his 10W is probably making it across the "pond" for the first time! Remember, the W/VE's can be found between 1800 and 1807kHz and the Europeans around the so-called "DX window" 1825 to 1830kHz. Considering the chaos on some other bands this gentleman's agreement works very well indeed. Any European calling W's on their own frequency soon gets told the facts of life!

W. C. Johnson, 72 Estcourt Street, Newbridge Road, Hull is a newcomer to the short wave bands and after refurbishing an old CR45 with new valves etc has been pleasantly surprised at its performance. However he would be very glad to get hold of a manual for this set and naturally will be only too pleased to reimburse anyone who can help.

Dennis Anderson (London SE11) kindly relieved my ignorance of his Realistic DX150 receiver by sending in the handbook, duly statted for reference. Made in Japan and handled by the Radio Shack Co. in the States it is general coverage with bandspread and resembles a solid-state 9R59DS! But I imagine its performance is rather better especially at the higher frequencies. For £30 Dennis certainly got a bargain!

Tim Charles (Colchester) finds that 15 and 20m are beginning to die down for the winter but he is compensated by the ZL's on 80m nowadays. He says 'not to be worried' if you hear ZL4ZLV, permitted

to use the amateur bands but normally the commercial station at the works of ZL4AV, producing marine radio equipment. Home one morning after visiting his dentist Tim found YJ8CS on 20m for a new one, in the New Hebrides. Martin Kessel A9016 (Stoke-on-Trent) reports getting cards from KS6ET and KS6FF, proof of the efficiency of his HMV 5-valver or at least his handling of it! Neil Whiteside A8859 (Hitchin) got his Microwaves Module working on 2m with a longwire as a start but found things much better with a proper yagi for the band.

Seems my note on the Pioneer Radio Club in Edinburgh, in the September issue, produced a few new faces. Co-founder Bob Henderson GM4DTJ reports that they now have a room of their very own, a basic requirement of any successful club, and a programme of equipment construction is already under way, with the club transmitter active on the HF bands and on 2m. Paul Barker BRS34898 (Sunderland) was very happy to 'see' 9K2DO, on his SSTV setup on 20m. Paul discovered that XJ6UM was really VE6UM in a different hat! Won't be long before we are allowed to pick our own prefixes in celebration of a birthday or something equally daft!

Stephen Budd A8713 (Worthing) seems to have been on the 'A' prefix hunt copying A2CJP, A4XGC, A6XB and A9XBB from Botswana, Oman, United Arab Emirates and Bahrein respectively. Those envious of the KS6's mentioned previously might like to know, via Stephen, that several KS6's hang around 14284kHz on SSB. Andrew Swiffin A8603 (Cheadle) may have to mortgage his receiver, he says, to be able to pay the postage for his reports to this column! He too, found the two KS6's, around 0845 GMT.

Back to Tim Charles again, reporting some of the repeaters he has been hearing on 2m, including OZ3REI on channel R5. According to Tim, a North Essex Raynet (RSGB's emergency network) group exercise was being repeated all over Denmark by an unidentified repeater on R8 recently! Being an anti-repeater man myself I think the day is not far off when the amateur community will be sorry that it ever went in for repeaters. The behaviour of many operators on these frequencies has to be heard to be believed!

Mike Green A8088 (Northwich) found seven LU's, six PY's and three ZP's on 10m which can't be bad on a band often accused of being dead.

Although this is being compiled in October for the January issue which will be out on 5 December it is appropriate to wish you all a VERY HAPPY CHRISTMAS and to hope that Father Christmas will bring along all that nice new gear that we have all been waiting for!



NOTE:— Please ensure logs are posted in time to reach me by 25th of each month.

Log extracts

M. Kessel:— 80m EA6BG VU2GDG 20m DU6EG KL7BJW M1D VK5WD VK9KK ZL1AH

J. Hinton:— 20m FC9UK YS1AE 8P6CC 15m HZ1KE 707RM 9G1LZ 9J2BO

M. Bennett:— 80m 4W1AF 9K6OG 20m HB0AIC HL9UF KG6JES ZS1AMB (Queen Maud Land ITU Zone 67) 15m CM6AI FL8AC VK9XX 9N1MM 10m DU3ON HK3LT ZP5JN 7Q7RM

D. Anderson:— 20m KL7HFQ PZ1DR 15m 9J2BO PY1AZ

P. Barker:— 20m EA9EX JY9JM ZL4PD 20m SSTV EA3AUM I2PET OH5RM OK2OI 9K2DO 15m ZS1E 9L1JM (QSL W4BAA)

T. Charles:— 160m OE5NT OH2BO OH3VV 80m JY3ZH W6CXQ ZL1JX ZL4ZLV 5V7WT 40m HV3SJ WAOKXJ/OY 20m YJ8CS ZL1BN ZL1TY 15m JE3NB KZ5EK LU7EY ZS6BR 9H1EN 2m DM3WCB OZ3REI (repeater, FM)

A. Swiffin:— 80m CX9BT 20m KS6ET KS6FF YB0PG 15m TU2FH 5L2FM

S. Budd:— 20m AP2KS A2CJP A4XGC A6XB A9XBB C5AN WA6LRG/KB6 KJ6CF KM6EB KS6DV KS6ET KS6FF P29CW VP8NP VS5DB XP1AA (Greenland) 3B9DA (Rodriguez Is) 4S7BR-5T5CJ 5V7WT 7P8AC (Lesotho)

M. Green:— 40m TR8SS 20m C5AN H18REL YN8GTG 15m CX3VR VU2DK 5L7F 9J2AB HP7XJS (DXpedition) 10m LU4DSZ PY4KL ZP5RS 2m via Oscar 7 from 10m VP9GE

All SSB except those in bold which are CW.



SHORT WAVE BROADCASTS by Derek Bell

R. R. CORBETT of Kettering recently picked up a copy of PW during his teabreak at work, and upon reading this column became converted to DXing, and, pausing only to finish his sandwiches, dashed out to trade his portable for one with short wave coverage. "I am amazed at the possible obtained."

with short wave coverage. "I am amazed at the results obtained" says Mr. Corbett, and I am flattered at the results of this column, says I! Our friend then asks several questions on how to get the best from his new purchase which I will do my

best to answer.

The first one is that, setting aside ex-service sets, there are not many sets under £50 that have complete short wave coverage. The Codar CR70A is within your price range and adding on the PR40

pre-selector will improve reception. Otherwise you will have to have the medium wave plus the SW coverage. I must say that I have heard of some strange shacks but under the stairs is a new one on me! I would think that this situation is prone to all the interference that comes from domestic appliances.

The second question posed was the one that puzzles a lot of DXers. If, in the SINPO code, 5 is the strongest then how does one estimate the propagation? The simple answer is that for a 5 rating one looks for perfect propagation, free from all fading, in fact, of local radio quality. In propagation measurement all sorts of factors must be taken into consideration, notably, fading, audio quality and the noise that accompanies the signal. There is an alternative system that uses only the letters SIO, Strength Interference and Overall readability, lumping noise and propagation under the one heading.

From Long Eaton, Notts, H. A. Mead writes about a map that Radio Prague has sent him showing the ITU zones. He comments that the zone numbers on the map are different from those on the map in the Radio Amateurs Handbook. I would suspect that the ITU number were drawn up by the International Telecommunications Union for the use and benefit of the broadcasters while amateurs have a zoning system of their own making. (And in use many years before the ITU one was thought of. Again, change for changes sake. Eric G4AR.)

An information-packed letter arrived chez Bell recently from **John McLeod** of Inverness. Firstly, he tells us that Radio Kiev has announced a new English service on 7390, 6045, 6020 at 1930 to 2000 Mondays, Thursdays and Saturdays. Further on the DX scene a fault in one of Radio Sweden's aerials has resulted in the closedown of some of the services from the Horby and Karlsborg transmitters. John then goes on to nominate RBI as producing the most boring QSL card! It has a decibel table overprinted RBI in red. There are also a few harsh words from John on the way some secretaries address cards to him using "England" or, in one case, "Scotland, England, GB!"

Station address lists seem to be popular for the avid QSLer so here are a few that have been requested:—

Radio Kuwait, PO Box 397, Kuwait. Radio Cairo, PO Box 795, Cairo, Egypt. Radio Finland, PO Box 528, Helsinki, Finland.

A rarely reported station comes from Robert Hill at school in Colwyn Bay, Wales This is Radio Athens on 7250 at 1915. The set in use is an Invicta 8027 with an internal aerial and on the high ground of that part of the country pulled in the skywaves from the following:—

9755 AWR Malta relay, 2030 Saturdays only, in English.

11940 Radio Kuwait, at 1730.

11642 Radio Israel, at 2050, sign off time.

Robert then asks for details of the Malta relay since he logged not only AWR but IBRA at 2100 to 2115. The transmitters in question are run by Deutche Welle and leased to other broadcasters. They comprise one 600kW for MW and three 250kW on the short waves. They also own the transmitter in Portugal used by AWR.

Recently this column featured a vintage SW receiver, so C. H. Wood, of Sunbury-on-Thames, comes along with a 1936 Murphy A36, this set is certainly pre-April 1937 since that is the month it was



reviewed in (dare we mention it?) Wireless World! The set has had little done to it except for a new valve and transformer and a couple of switches, C.H. mentions that he has had to paint some of the insulation to protect it and some of the stations printed on the dial have long since vanished!

Congratulations are in order for the American folk music show "Grand old 'opry" heard on the AFRTS air waves. The show is fifty years old this year and was the subject of a "happy birthday" piece on BBC recently. Another BBC curiosity is a recently issued record in praise of radio, by an outfit calling themselves "The Medium Wave Band", friends of Charles Molloy?

Finally, an official statement from Radio Canada has reached me regarding the sad demise of the RCI Short Wave Club. The reason for this is said to be "the need for stringent budgetry controls". It is stated that they need listeners cooperation in giving their views on programme content rather than just OSLing, and in this area what they describe as an "unsatisfactory result" came out of their recent QSL policy. Therefore they have decided that no more QSLs will be issued until Spring 1976. When the new schedules are issued for the 1976 short wave season then listeners on the mailing list will get a QSL. If the collector wishes to make it an "official" QSL he must return it to RCI having filled in the details in order that it may be stamped. The new card will have an Olympic Games motif and it seems that RCI are set fair to continue this policy since they say that a card will be sent automatically each year.

Well, that seems to wind things up for this month so I will wish you and yours a Very Happy Christmas and, although we are coming up to the sunspot minimum, the best of DX for 1976.

MEDIUM WAVE DX by CHARLES MOLLOY

EDIUM wave transmitters in Europe operate on channels which, over the greater part of the band, are spaced 9kHz apart. In other parts of the world, channels are multiples of 10kHz and occasionally 5kHz and the two systems coincide at intervals of 90kHz, for example 620, 710 and 800. DXing on those frequencies can be difficult for the listener in Europe. Fortunately there are other parts of the band where the DX channels are 4kHz away from the nearest European broadcast and the DXer who hunts in these areas is often well rewarded.

During the evening search for Baghdad on 760kHz; Isfahan in Iran on 1100kHz; Kabul in Afghanistan on 1280kHz; Kuwait on 1345kHz; Ahwaz, Iran on 1390kHz; Dubai, United Arab Emirates on 1480kHz and Sharjah on 1575kHz. After midnight listen for Surinam on 725kHz; Georgetown, Guyana on 760kHz; CJON St John's, Newfoundland on 930kHz; Hofei, China on 940kHz; Hyderbad, Pakistan on 1010kHz; St John's Antigua on 1100kHz; Radio Globo, Rio de Janeiro on 1180kHz and Radio Tupi, also in Rio, on 1280kHz. All of these stations have been logged

recently in the UK by DXers using communications type receivers and a MW loop or longwire aerial.

Alfred Johnson, of Barnet, has been active on the band between 0200 and 0300 GMT. The highlights of his North American log include the following from the USA; WOR in New York City on 710kHz; WABC also in NYC on 770kHz; WGY in Schenectady, NY on 810kHz; WHAS Louisville, Kentucky on 840kHz; WCFL Chicago on 1000kHz; KDKA Pittsburg on 1020kHz and WHN in NYC on 1050kHz.

Harold Emblem writes again from Mirfield in Yorkshire to report a good bag of North American outlets using his Eddystone 730 and MW loop. Canadians heard include four from Newfoundland; CBNA in St Anthony on 600kHz; CBN in St John's on 640kHz; CKVO in Clareville on 710kHz and CJON St John's on 930kHz plus a couple from Nova Scotia; CHER in Sydney on 960kHz and CKEC in New Glasgow on 1320kHz.

DX from the USA includes WINS in NYC on 1010kHz; WTIC Hartford on 1080kHz; WNEW in NYC on 1130kHz; WLOB Portland, Maine on 1310kHz and WOKO in Albany, NY on 1460kHz. Harold reports reception of Nouakchott in the African republic of Mauritania on 1349kHz at 2230 GMT, the time when the French stations on this channel usually sign off. A very good catch. Another to look for is Enugu in Nigeria on 1320kHz which can be heard with news in English at 2300 before signing-off for the night five minutes later.

Radio St Pierre which transmits with a power of 4kW on 1375kHz is the sole broadcasting station in the French islands of St Pierre and Miquelon which are located a few miles off the south coast of Newfoundland. Radio St Pierre is often heard in the UK during the winter. Listen after Lille on 1367kHz has closed down for the night, usually at 2300. Radio St Pierre is on the air until 0100, its local time is three hours behind GMT and the station will answer a correct reception report with a verification letter. Write to Radio St Pierre, BP7, St Pierre et Miquelon if you want to add this North American "country" to your list of countries verified.

BROADCAST BANDS

Short Wave reports by the 15th of the month to Derek Bell c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.

AMATEUR BANDS

Logs covering any amateur band/s in band/ alphabetical order by the 25th of the month to Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey, KT21 2TW.

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HOTLINES

ON RECENT DEVELOPMENTS

HOT POT

It seems that component technology never stands still, and while the semiconductor manufacturers often hit the headlines with new devices, there are times when the more mundane components come to the forefront. Take the humble potentiometer as an example. Basically it might be thought of as a length of resistive material along which a small metallic wiper is moved. Thus by moving the finger along the material, the resistance between wiper and one end can be varied.

Two differing approaches have come to light and the first obvious difference is that there is no finger nor any wiper and thus no actual frictional contact of any sort!

The first approach employs two small ferrite cylinders with wire wound round them to form inductors. A permanent magnet also features and is used to vary the saturation of the ferrite as it is rotated. Of course, left to their own devices, the inductances across the ferrites are constant. But by passing a magnet over them a strange effect occurs; the inductance of the other decreases. A signal between the two ferrite cylinders thus provides an output which is proportional to the angular position of the magnet. Note that there is no actual physical contact between the elements. It is claimed that these potentiometers, which are no larger than conventional pots, can survive and operate happily at temperatures of 200°C which would seem to indicate applications in engine control and the like.

The second approach to potentiometer design is quite ingenious and delves into the realms of semiconductor resistors. The resultant devices are called field plate potentiometers and operate as follows.

Certain materials exhibit a marked change in resistance under the influence of a magnetic field. This is called the magneto-resistive phenomenon. The effect has been known for many decades but new advances in semiconductor materials have led to new crystaline structures, considerably increasing the range over which the resistance can be varied.

The technique employed is to embed minute needles of a conducting substance in a semicon-

ductor material. In the absence of a magnetic field the current passing through the structure passes through these regions via the shortest possible route. By applying a magnetic field, the current paths between the tiny needles become deflected causing the current to travel further and thus there is an increase in resistance due to this longer path effect.

TEMPERATURE

Perhaps one of the most popular and recurring circuit ideas in electronics construction journals is some form of temperature measurement and/or control. A common approach is to use an op amp (operational amplifier) since the two inputs offer a means of comparing one thing with another. The voltage on one input can be held constant and the variation in voltage applied to the other input (usually caused to vary by the sensor) gives a difference which shows up at the output.

Temperature tyros will be pleased to hear that a semiconductor manufacturer has brought out a chip (measuring 50 x 50mil) which has temperature sensor, zener diode stabilized voltage reference, and op amp all included. Designed for use in the range -25°C to 85°C it comes in an uncalibrated form to within $\pm 10^{\circ}\text{C}$. However, the user can calibrate it to within $\pm 0.5^{\circ}\text{C}$ with the simple addition of an external potentiometer. Price is not easy to guess but in the US the quoted cost for quantities of 100 to 999 are just a dollar each.

NEW DDM

Each time a new instrument is launched onto the market, it seems to have better and better specifications. A DMM (digital multimeter) marketed recently offered a capability of measuring resistance up to $2G\Omega$ (that's two million million Ohms). Not satisfied with this, the manufacturers built in the ability to resolve currents down to 100pA (picoampsa million millionth of an Amp) and dc voltages down to 100µV. It can also measure AC voltages up to 700MHz. Price in the US is under \$1,700 and it's the product of a Dutch company. My £3.50p Lisle Street special will never seem the same again.

FOOD FOR THOUGHT

If you want food for thought, how about the new induction heating for cookers. Not to be confused with microwave ovens, the approach is to employ fast turnoff thyristors operating at some 30kHz. The idea is to cause eddy currents in the base of a cooking utensil. This is done by a coil just beneath the cooker surface. Estimated to halve electricity useage, the system doesn't work until a utensil is placed above it since, with nothing there, there will be nothing in which to induce the eddy currents.

FAST-RECOVERY DIODE

A new fast-recovery diode (BD277) from RCA Solid State-Europe is available in a low-cost TO-220 Versawatt plastic package, giving excellent heat-sink capability and making the device particularly suitable for use in the deflection systems for 110° large-screen television tubes. Two of the diodes, used in conjunction with two thyristors, form the complete deflection circuitry, controlling the horizontal yoke current during the beam trace interval and acting as the commutating switch to initiate trace/retrace switching and controlling yoke current during retrace.

The diode is designed for operation from supply voltages between 150 and 270V (nominal), and can handle a maximum reverse voltage of 800V and an average current between 2A and 7A, depending on the heat sinking of the device. The diode can handle surges of more than 100A, and a low, 'soft' (low in harmonics) recovery characteristic.

Other applications in television sets include clamp and booster diodes, diode modulators and switching power supplies, and the diode can also be used in hammer drivers, invertors and convertors for induction heating systems, electronic ignition circuits, or speed controls for domestic appliances such as washing machines. Ban those washday blues with a BD277!

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ISSUES FOR DISPOSAL

..P.W. for April, May, August 1970 and June 1971.—D. Horrill, Mark House, Lindale, Grange-on-Sands, Cumbria. ..Television for Jan. 1972 to October 1974 excluding August 1972 to December 1972 inclusive.—B. C. Jackson, 28 High Street, Frodsham, Cheshire, WA6 7HE.

...P.W. 1970 to 1974.—M. Pedersen, 19 Belgrave Street, Brighton, BN2 2NS.

CORRESPONDENTS WANTED

...someone of my own age (14) who is interested in Amateur radio in general and electronics.—Andrew Sharpe, Hazel Dene, High Horse Close, Rowlands Gill, Tyne and Wear, NE39 1AW.

... anyone who has built the Galleon VHF kit advertised in P.W. I have found this kit extremely satisfying.—F. Ward, 2 Brookdown Terrace, Saltash, Cornwall, PL12 6HU.

... I am 17 and would like to correspond with readers, especially hams about my own age. Very interested in satellites.—G. Selvakumaran, 16 Jalan Batu Pahat (opp. Ban Ho Lee Shell), Kluang, Johore, West Malaysia.

BOOKS WANTED

.. I want to collect older Mullard Data Book publications.— John B. Millin Jnr., 39 Dalgleish Avenue, Cumnock, Ayrshire, KA18 1QG.

..a copy of Practical Television Circuits. 1968 edition by Street.—S. H. Biggs, Bell Cottage, Bonfire Lane, Horsted Keynes, Sussex, RH17 7AJ.

EQUIPMENT WANTED

..active filter unit and stereo FM tuner for Sinclair Project 60.—M. Stanley, 9 Ormiston Gardens, Knock, Belfast, BT5 6JD.

..microphone transformer, ratio 100-1 or 150-1.—W. L. Brunson, 28 Meadfoot Road, Moreton, Merseyside.

..Telefunken radio valve type 199 for a c1938 TRF set made by Dr. Georg Seibt A.G. model VE 301 DYN. Also any gen on this equipment.—Sgt. J. Irvire REME, 1 Cheshire Regiment, Weeton, Lancs.

. Cossor valves 63 SPT and 61BT for 1035 oscilloscope.— Ian Ropper, 29 Wakefield Avenue, Edinburgh, EH7 6TN.

..receiver wanted for a 13-year old SWL.—P. Jeffries, 29 Walworth Grove, Acklam, Middlesborough, Teeside, TS5 8NN.

..the type of transistor used in Two Tone Door Bell (P.W. May 1973).—A. Fanzeres, P.O. Box 2483-ZC-00, Rio, Brazil.

..Sinclair Project 60 FM tuner.—C. Parkins, P.O. Box 10, Stanmore, Middlesex.

...an R107 receiver in working order.—J. King, 2 Delacherois Avenue, Lisburn, Co. Antrim, N. Ireland.

..power leads and headphones belonging to R209 receiver.—I. Simpson, 107 Derryhale Road, Portadown, Craigavon, Co. Armagh, N. Ireland, BT62 3SR.

..loan of CL33 valve required for old Bush receiver to see if any other faults present apart from this missing valve.— K. G. Bailey, 29 Anstruther Road, Norfolk Park, Edgbaston, Birmingham, B15 3NN.

a balanced armature speaker unit.—J. Claxton, 6 Lloyd Park House, Forest Road, Walthamstow, London, E.17.

INFORMATION WANTED

..design for bias oscillator working at approximately 100kHz. Erase head must not be used and supply voltage must be around 6-12V.—R. Hill, 30 Queens Road, Bradford, West Yorks., BD8 7BT.

..manuals, circuit diagrams or any info. on Cossor 1052 D.B. scope, also C. F. Lord, FM3-3 frequency meter and Jason EM-10 valve voltmeter.—M. Roebuck, 16 Elizabeth Street, Newsome, Huddersfield, West Yorkshire.

..Schaub Lorenz Weekend T50L circuit diagram wanted. Will stat and return.—R. F. Nicholls, 11 Rue Dufrexou, 44 St. Nazaire. France.

..good condition DX Data Chart (P.W. March '73 issue). Also issue of P.W. containing A.T.U.—R. Rooney, Rolestown, Kilsallaghan, Co. Dublin, Ireland.

..instruction manual/handbooks for the Trio JR310 and Trio 9R59DS communications receivers.—K. Arasu, School House, Brighton College, Brighton, BN2 2AL, Sussex.

..details, circuit, manual, etc. for STC B46 receiver, oscillator tuned, roller coaster coil, manufactured 1948 (STC No. 406).—T. D. Jackson, 60 Industrial Street, Todmorden, Lancs., OL14 5BT.

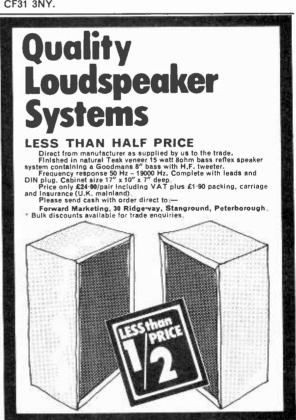
..instruction handbook and/or circuit diagram for a ex-WD scope 'Indicator CTR type 103'. Ref. 10Q/16208, part of 'Monitor type 101' and its associated power pack.—P. V. Hill, 25 Southern Crescent, Bramhill, Stockport, Cheshire, SK7 3AQ.

..borrow or buy circuit for Philips car radio N4G40T serial L21600. Version only has two windings on L6. Collector T2 goes to L4 via 350 ohms.—J. Palmer, 70 Westbury Road, Northwood, Middlesex, HA6 3BY.

..Schaub Lorenz T50L. Information on how to receive BBC MW with external aerials. Circuit and alignment details also required.—R. Nicholls, 85 Avenue de Plaisance, 44 St. Nazaire, France.

..manual or circuit diagram for the TR1143 serial 11041 ex-WD Transceiver.—B. Bridges, 22 Bell Avenue, Harrow Crescent, Romford, Essex.

..circuit diagram for Ferranti 194 mains receiver.—J. Carver, 112 Merthyr Mawr Road, Bridgend, Glamorgan, CF31 3NY.



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Dual cone plasticised roll sur-round. Large ceramic magnet. 50-16,000 cps. Bass resonance. 55 cps. 8 ohm impedance. 8in. 10 watts £4.35

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All purpose transistorised.
Ideal for Gronps, Disco and P.A.
4 inputs speech and music. 2 way
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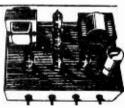
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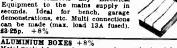
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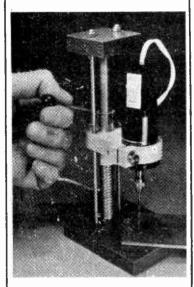
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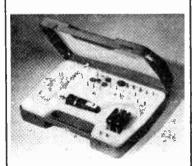
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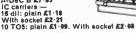
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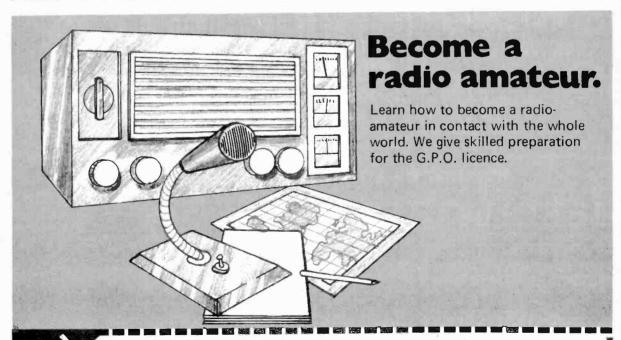
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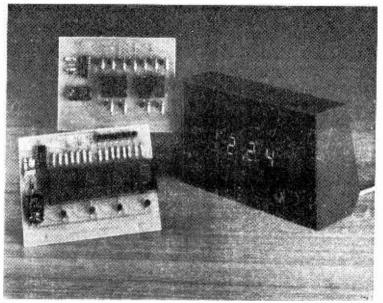
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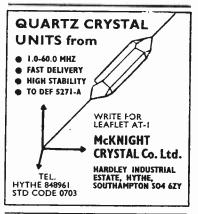
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| 2-5mm
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Standard Ster | | 8p
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13p
15p | with
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contacts
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22p | MINIATURE
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3-5mm plug | 30p | | | | |

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| TOGGLE: SPST 20p
DPDT 24p
BUB-MIN TOGGLE
SP changeover 45p | Push on/Push off, spring loaded 44p
Miniature Non Locking
Push to Make 15p
Push to Break 25p | Low profile
8 pln 12;
14 pin 13; |
| SPST on/off 40p
DPDT 6 Tag 64p
DPDT Centre off 80p
SLIDE: | ROCKER (white): 10A 250V
SP changeover centre off 25p
ROCKER: (black) on/off10A 250V 20p
ROCKER: illuminated (white)
lights when on, 3A 240V 45p | HEAT SINKS
TO5/5F 8
TO18/18F 8
TO66/TV2 15 |
| 1A DP 250V 10p
1A DP 250V C/O 12p
1A DP 250V 9p | ROTARY: 1p/2w, 2p/6w, 2p/2w, 2p/4w, | TO3/TV3 15;
Insulation Kit- 6p
(Mica & 2 washers |

| 1 | TM DP 2504 SP (SP/SW SP/SW, 4P/S | cw, 4p/3w Znp (Mica & 2 washers |
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| ı | 9-0-9 (miniature) 100mA 86p | LES BULBS 6v and 12v 7g |
| đ | 12-0-12 (miniature) 100mA 90p | MES HOLDERS Chrome cover, Red or |
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| | 30-24-20-15-12-0 2A * 340p | MES BULBS 3:5V 6V 12V 7 |
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| • | 15-0-15 1 A * £2 · 46 | Round top Red sealed with Resistor 21; |
| • | 6-3V-1-6A/240V 60mA* £2-34 | Neon with leads |
| | LT44 Mini, Driv, Pri 20K Sec 1K 54p | |
| | LT700 Mini, Output, Pri 1 · 2K Sec 5 Ω 54p | KNOBS * (fits 1" shaft, with grub screw |
| 0 | | except K2 (push fit) & K8 (for sliders). |
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| , | 0-1 0-15 0-15 | K2 Slim silvered aluminium 18g |
| 2 | (copper clad) (plain) | K3 Black 1±" with chrome rim 15s |
| , | 24x31" 32p 24p 15p | |
| p | 2½x5" 35p 35p 18p
3½x3½" 35p 35p — | K4 Black serrated, Metal top with |
| n | 3½x3½" 35p 35p —
3½x5" 40p 41p 20p | line Indicator 33m diam. 29p |
| 0 | 2+x17" 185p 78p 60p | K5 Black fluted metal top and skirt |
| | 31x17" 145p 115p 75p | calibrated 0–10, 37mm dla. 22p |
| | 44x17" 1850 - 1100 | K6 PK2 as K5 with pointer on skirt 22p |

| | i Pro undrock Dollie sliaben, ken' b | HUW. |
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| 88p | LES BULBS 6v and 12v | 7 p |
| 96 p | MES HOLDERS Chrome cover, Re- | |
| * 285p | Amber, Jewelled top | 50p |
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| £2 · 46 | Round top Red sealed with Resistor | |
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| | Meon with reads | - ab |
| | | |
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| | except K2 (push fit) & K8 (for slide | |
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| (plain) | K2 Slim silvered aluminium | 18p |
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| 29p | line indicator 33m diam. | 29 p |
| 60p | K5 Black fluted metal top and skirt | |
| 75p | calibrated 0-10, 37mm dla. | 22p |
| 110p | K6 PK2 as K5 with pointer on skirt | 22p |
| 22p | K7 Black, knurled, tapered, Metal | top |
| 52p | top & skirt, Calib, 0-10, 30mm | 22p |
| 72p | K8 Black or silvered for silder pot | 7p.# |
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| | 140 | 7484 | 95p | •709 | | 8/14 pin DIL | 36p | 723 | 11 | amp + | Ve — | Ve | A C128 | 11p | MJE3055 | 65p | 2N3442 | 140p |
| | 14p | 7485 | 120p | •710 | | . 14 pin DIL | 30p
50p | 14 pin E | | 5v 7805 | 140p 790 | | | 18p | *MPSA06 | 30p | *2N3702/3 | 11p |
| | 16p | 7486 | 30p | 19741 | | 8/14 pin DiL | 25p | D-4- Ch | | 12v 7812 | 140p 7912 | | AC176 | 11p | MPSA12 | | 2N3704/8 | 11p |
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Vol. Re | | 15v 7815
18v 7818 | 140p 7915 | | | 12p | *MPSU06 | | *2N3706 | 10p |
| | 16p | 7490 | 40p | *748 | Ext. Comp. | 8 pln DIL | 36p | 10p eac | | 18v 7818
24v 7824 | 140p 7918
140p 7924 | | AC188
AD149 | 11p
43p | *MPSU56
OC28 | | °2N3707 | 11p |
| | 38p | 7491 | 75p | 776 | Prog. Op | Amp. TO5 | 140p | - | | | 140D /924 | 200p | AD161/2 | 36p | OC35 | 61p | *2N3708/9 | |
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2N3866 | 220p |
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20p | 7493
7494 | 40p
75p | *LM3900 | Quad Op. | Amp 14 DIL | 70 p | OCP70 | 30p \$ | Seven Se | gment Di | plays | AF116/7 | 16p | *OC44/5 | 16p | *2N3903/4 | 70p |
| | 14 _D | 7495 | 65p | *MC1458
NE536T | FET Op. A | mp. 8 pin DII | | OCP71 | | 015F 0-3 | in DIL | 120p | AF139 | 33p | *OC71 | 16p | *2N3905/6 | |
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40364 | 40p |
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85p | *CA3089E
*CA3090 | | tem 16 pln DI | 200p | 1 A 100 V | | 40p BT1
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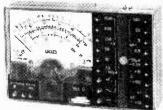
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| 7402 | 14p* | 12p * | 10p * |
| 7403 | 15p* | 125p* | 10p * |
| 7404 | 16p* | 13p * | 11p * |
| 7408 | lóp* | 13p* | [1p * |
| 7409 | 16p* | 13p* | ∏p ° |
| 7410 | 16p* | 13p* | 11p * |
| 7413 | 29p° | 24p* | 20p 1 |
| 7417 | 27p° | 22.p* | 20p * |
| 7420 | 16p* | 13p* | llp * |
| 7427 | 27p° | 22 2p* | 18p ° |
| 7430 | 16p* | 13p * | 11p * |
| 7432 | 27p* | 22 p* | 18p * |
| 7437 | 27p* | 22 2p* | 18p * |
| 7441 | 75p* | 62p* | 50p ° |
| 7442 | 65p* | 55p* | 43p * |
| 7445 | 85p* | 71p* | 57p ° |
| 7447 | 81p* | 75p* | 65p ° |
| 7448 | 75p* | 62p* | 50p * |
| 7447A | 95p° | 83p* | 67p ° |
| 7470 | 30p* | 25p* | 20p ^ |
| 7472 | 25p* | 21p* | 17p * |
| 7473 | 30p* | 25p* | 20p 1 |
| 7474 | 32p* | 26p* | 21p ° |
| 7475 | 47p* | 39p* | 31p- * |
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| 7404 | 16p* | 13p * | llp | |
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| 7437 | 27p° | 22 2p* | 18p | * |
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| 7475 | 47p* | 39p* | 31p | * |
| 7476 | 32p* | 26p* | 21p | * |
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| 7486 | 32p* | 26p* | 21p | |
| 7489 | £2.92 * | £2.80 ° | £2.10 | |
| 7490 | 49p* | 40p* | 32p | * |
| 7491 | 65p* | 55p* | 45p | * |
| 7492 | 57p* | 46p* | 36p | |
| 7493 | 45p* | 40p* | 3 2p | * |
| 7495 | 67p* | 55p* | 45p | * |
| 74100 | £1.08 * | 89p* | 72p | * |
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| 74174 | £1.00 ° | 83p* | 67p | |
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| / 41/0 | L1.04 | U1.04 | 7.7p | |
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|---|-------------------------|---------------------------|-------------------------------|-------------------------|
| 555 (14 pin dip) | 555 (8 pin dip)V 55p * | AV-1-0212 £6.93 | I M2111 £1.12 | SN76001N (TAA611) £1.82 |
| 555 (14 pin dip) E 2 2 A7-5-1224 E3.95 A7-5-350 E6.59 A7-530 E6. | | | | SN76003N £3.30 |
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| 733 (RF/IF Ampl) 68p / 475-3307 £ 6.55 | | AY-3-3300 10.37 | | |
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| MC1312 | | AY-5-4007 £7.94 ° | MC1310P £2,10 | 314/003 514 |
| 27.10 (Fig. 9) 45p | | | | |
| To (Tid - pin - aip) | | BHA0002 £3.01 | MC1314P £4.34 | |
| 210 | | 51.10 | | |
| Table Tabl | | | | |
| TAN | | | MC1339P £1.60 | |
| 720 (10-99) \$1.09 \$2.09 \$1.04 \$2.43 \$41 (4 pin dip) \$50 \$40 \$40 \$40 \$40 \$40 \$40 \$40 \$40 \$40 \$4 | | | | |
| 7.32 (4 pin dip 7.32 (4 pin di | 720 (A. M. Rodia) £! 76 | | MC1351 92p | |
| TAM Spin of property Tamps Tam | | CA3075 £1.64 | | 17.07.00.1.00.1 |
| 7.41 (TD-99) 4.56 (C.A.308) 2.1.86 (C.A. | | | | |
| 741 (I d pin dip) | | | | |
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| 7.48 (10 - 99) 469 469 479 | | | | 1704030 |
| 748 (14 oin dip) | | | | |
| 748 (I 4 pin dip) 4 Pp | | | MC1458CPI 89p | |
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| Table Tabl | | | MC1495L £4.48 | |
| Execution 100 mA | | CA3600E £1.44 | | 101150. (- ==) |
| Regulation 100 mA | | | | |
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| Temporary Temp | BI 100 A | | | |
| 78.15 (70-2) 6 b c c c c c c c c c c c c c c c c c c | | | | |
| Table Tabl | | | | TBA560CQ £5.29 |
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| Regulators 100mA 781.02 AWC TBA625A 90p TBA625C \$1.03 *** TBA625C \$1.04 ** TBA625C \$1.04 *** T | | | | |
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| 781 KC (TO-3) £ 2 0 9 * CABOOC £ 7, 24 * CABOCC £ 1, 26 * CABOCC £ 7, 24 * CABOCC £ 1, 26 * CABOCC £ 7, 24 * CABOCC £ 1, 26 * CABOCC £ 1, 26 * CABOCC £ 7, 24 * CABOCC £ 1, 26 * | | 1 M200Y F2 34 * | | |
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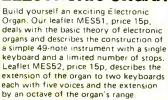
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