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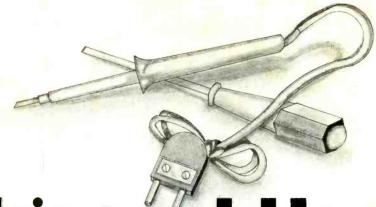
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VOL. 51 NO. 3 ISSUE 821 JULY 1975

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NEWS & COMMENT

196 VAT MUDDLE!—Editor's comment

196 CIRCULATION DETAILS

197 NEWS . . . NEWS . . . NEWS . . .

210 LETTERS—Readers comment

213 HOTLINES on recent developments by Ginsberg

219 NEXT MONTH IN PRACTICAL WIRELESS

230 PRODUCTION LINES by Colin Riches

242 ON THE AIR

242 Amateur Bands-Eric Dowdeswell, G4AR

245 Broadcast Bands-Short Waves-Derek Bell

246 Broadcast Bands-Medium Waves-Charles Molloy

CONSTRUCTIONAL

198 THE P.W. TEXAN II—updating our stereo amplifier— Richard Mann

204 P.W. 'APOLLO' Series—Part 3—Varicap AM/FM Stereo Tuner—W. Poel

220 DIGITAL WAVEFORM GENERATOR—Part 2—John Smith

226 TELE-TENNIS Sound Effects Unit—M. J. Hughes, M.A., C.Eng., MIERE

237 A UHF WAVEMETER-R. Longden

OTHER FEATURES

214 SPECIAL PRODUCT REPORT—Heathkit GR78 General Coverage Receiver

218 TECHNICROSS-No. 9-Solution

225 GOING BACK-Earlier days of Wireless-Colin Riches

229 POINTS ARISING-P.W. 'Easybuild' Organ

233 CALCULATRICKS-R. Stanwicki

246 CQ!CQ!CQ!CQ!CQ!

HEATHKIT COMPETITION — **RESULTS** — **Page 196**

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| No. 142 24V 16 oz 111 0.5 oz 125 a 4-8 x 2-9 x 3-5 0.12V at 0.25A x 2 1 | 1.35 23 1.74 30 2.29 38 |
| 213 1 0 0 0 5 | 7.86 38 |
| 213 1-0 0.5 | 4-12 45 |
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| 116 12 6 6 12 9.9 x 10.2 x 8.6 0.12V at 6A x 2 17 16 8 8 12 12.1 x 9.9 x 10.2 0.12V at 8A x 2 7 | 7.28 60 |
| 70 6 3 3 8 8 9 9 × 8 0 × 7 7 0 12 V at 3 Å × 2 4 7 10 8 8 4 5 8 9 9 × 8 9 × 8 6 0 12 V at 4 Å × 2 4 7 10 5 6 4 9 9 × 9 6 × 8 6 0 12 V at 5 Å × 2 16 12 6 12 6 6 12 9 9 × 10 2 × 8 6 0 12 V at 5 Å × 2 17 16 12 6 8 8 12 12 1 × 9 9 × 10 2 0 12 V at 6 Å × 2 115 20 10 11 8 14 0 × 9 6 × 11 8 0 12 V at 10 Å × 2 115 20 10 11 8 14 0 × 9 6 × 11 8 0 12 V at 10 Å × 2 12 12 12 13 13 14 14 14 14 14 14 14 14 14 14 14 14 14 | 5·52 53 7·28 60 0·39 73 3·59 85 6·83 * |
| | 6.83 * |
| Ref. Amps. Weight Size cm Secondary Tabs | P & P |
| 140. ID 0Z | £ ⊅ |
| 112 0.5 1 4 6.1 x 5.8 x 4.8 0-12-15-20-24-30V 1 79 1.0 2 4 7.0 x 6.7 x 6.1 3 2.0 3 4 8.9 x 7.7 x 7.7 3 20 3.0 4 8 9.9 x 8.3 x 8.6 3 21 4.0 6 4 9.9 x 9.6 x 8.6 5 51 5.0 6 12 12.1 x 8.6 x 10.2 6 51 5.0 6 12 12.1 x 8.6 x 10.2 6 | 1.40 38 1.49 38 1.53 45 5.13 53 5.41 53 7.16 60 |
| 3 2·0 3 4 8·9 × 7·7 × 7·7 20 3·0 4 8 9·9 × 8·3 × 8·6 21 4·0 6 4 9·9 × 9·6 × 8·6 | 1.53 45 |
| 21 40 6 4 9.9 x 9.6 x 8.6 | 5·13 53 5·41 53 |
| | 2:40 38 3:49 38 4:53 45 5:13 53 5:41 53 7:16 60 0:90 67 0:87 73 |
| | 87 73 |
| Ref. Amps. Weight Size cm. Secondary Taps | P & P |
| 102 0:5 12 7:0 x 6:4 x 6:1 0-19-25-33-40-50V 2 | £ p 2-58 30 1-38 38 |
| 102 0.5 1 12 7.0 x 6.4 x 6.1 0.19-25-33-40-50V 2 103 1-0 2 12 8-3 x 7.4 x 7.0 | |
| 104 2-0 5 8 9-9 x 8-9 x 8-6 | 68 45 81 53 60 67 10 67 98 85 |
| 105 3.0 6 12 9.9 x 10.2 x 8.6 , 5 106 4.0 10 0 12.1 x 10.5 x 10.2 , 7 107 6.0 12 0 14.0 x 10.2 x 11.8 , 12 118 8.0 18 0 14.0 x 12.7 x 11.8 , 12 | 10 67 |
| | ·98 85 |
| | |
| Ref. Amps. Weight Size cm. Secondary Tass No. 124 0.5 2 4 7.0 x 6.7 x 6.1 0.24-30-40-48-60 2 126 10.0 3 4 8.9 x 7.7 x 7.7 5 127 2.0 6 4 9.9 x 9.6 x 8.6 5 125 3.0 8 12 12.1 x 9.9 x 10.2 7 123 4.0 13 12 12.1 x 11.8 x 10.2 8 40 5.0 12 00 14.0 x 10.2 x 11.8 9 120 6.0 15 8 14.0 x 12.1 x 11.8 9 120 6.0 15 8 14.0 x 12.1 x 11.8 | P&P |
| No. 16 oz 124 7.0 x 6.7 x 6.1 0.24-30-40-48-60 2 126 1.0 3 4 8.9 x 7.7 x 7.7 x 7.7 x 127 2.2 0 6 4 9.9 x 9.6 x 8.6 5 125 3.0 8 12 12.1 x 9.9 x 10.2 7 7 123 4.0 13 12 12.1 x 11.8 x 10.2 8 12 12.1 x 11.8 x 10.2 8 12 12.1 x 11.8 x 10.2 9 12.1 x 10.2 x 11.8 x 10.2 9 12.1 x 10.2 x 10 | £ p 1-33 38 1-41 38 1-08 45 1-52 60 1-75 67 1-75 73 |
| 126 1-0 3 4 8-9× 7-7× 7-7 1 1 1 1 2 1 2 1 2 1 2 1 2 1 2 1 2 1 2 | 08 45 |
| 123 4-0 13 12 12·1 x 9·9 x 10·2 , , , , , , , , , , , , , , , , , , , | 75 67 |
| 40 5·0 12 00 14·0×10·2×11·8 ,, ,, 9 120 6·0 15 8 14·0×12·1×11·8 ,, ,, 11 | ·75 73 ·30 85 |
| 121 0.0 25 00 14.0 14.7 11.0 | ·30 85 ·00 * |
| No. | £ p 1-33 38 1-41 38 1-41 38 1-60 45 1-75 67 1-75 73 1-30 85 1-30 85 |
| 122 10-0 25 00 17-2 x 12-7 x 14-0 , 17-12 11-12 11-0 11-2 x 12-7 x 14-0 , 17-12 11-12 11-0 11-2 x 12-7 x 14-0 , 17-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-12 11-0 11-0 | 15 P & P |
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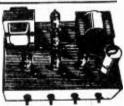
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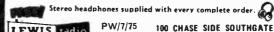
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0·35 BF194/5/6 0·10 BFY50/1/2 0-15 MJE370 0-62 MJE371 0-73 2N2218 0-19 2N2906 0-13 ALI-ROXES MJE371 0-73 2N2218 0-19 2N2906 0-13 2N2926 all 0-09 2N3053 0-15 2N3053 0-15 2N3054 0-42

2N3702/3/4 2N3705/6 0·10 2N 3819 TIP29a TIP30a TIP31a TIP32a

TIP41a TIP42a

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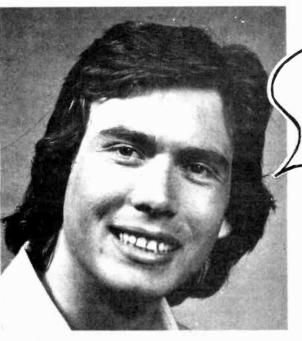
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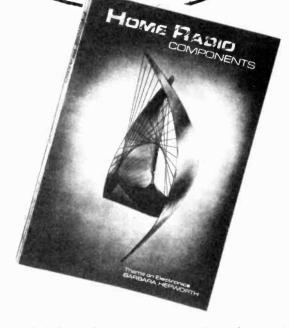
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|--|---|---|---|---|---|--|--|---|---|---|---|--------------|--|---|---|--|--|--|---|--|
| ACY18 022 BC114 0-17 BC300 0-28 0-18 BC125 0-18 BC300 0-20 0-20 0-20 0-20 0-20 0-20 0-20 0 | AC188K | 0.25 | BC109 | 0.9 | BC225 | 0.28 | BF123 | 0.55 | BSY28 | 0.17 | OC200 | 0.28 | 2N711 | 0.33 | 2N2926(R |) 11 | | | 28327 | 0-77 |
| ACY20 022 BC116 0-17 BC302 0-97 BF153 0-50 BSY40 0-31 OC295 0-98 2N726 0-81 DIDDES AND RECTIFIERS ACY20 0-22 BC117 0-20 BC303 0-18 BF155 0-77 BSY95 0-14 OC295 0-99 BC125 0-18 BC440 0-99 BY130 0-18 OA47 0-08 ACY27 0-20 BC119 0-33 BC460 0-40 BF155 0-73 BSY95 0-14 OC295 0-99 BC125 0-18 BC460 0-40 BF155 0-73 BSY95 0-14 OC295 0-99 BC125 0-18 BC460 0-40 BF155 0-73 BSY95 0-14 OC295 0-99 BC125 0-18 BC460 0-40 BF155 0-73 BSY95 0-14 OC295 0-99 BC125 0-18 BC460 0-40 BF155 0-73 BSY95 0-14 OC295 0-99 BC125 0-18 BC460 0-40 BF155 0-73 BSY95 0-14 OC295 0-99 BC125 0-18 BC460 0-40 BF155 0-73 BSY95 0-14 OC295 0-99 BC125 0-18 BC460 0-40 BF155 0-73 BSY95 0-14 OC295 0-99 BC125 0-18 BC460 0-40 BF157 0-61 BN105 22-20 BN105 0-22 BF158 0-91 C111E 0-55 ORF00 0-44 2M918 0-33 AA730 0-10 BY164 0-55 OA79 0-08 ACY30 0-31 BC125 0-13 BCY31 0-28 BF159 0-86 C00 0-33 BF150 0-81 BCY31 0-28 BF159 0-86 C00 0-33 BF150 0-81 BCY31 0-28 BF159 0-86 C00 0-33 BF150 0-81 BCY31 0-28 BF159 0-86 C00 0-83 BF150 0-81 BCY31 0-82 BCY31 0-82 BCY31 0-82 | ACT18 | 0.22 | BC114 | 0.17 | BC301 | 0.30 | BF127 | 0.55 | BSY38 | 0.20 | OC202 | 0.31 | 2N718 | 0.27 | | | | | | |
| ACY21 0.22 BC117 0.22 BC118 0.11 BC440 0.43 BF156 0.73 BSY95A 0.14 0COP1 0.48 2N744 0.22 AA120 0.99 BY130 0.18 0A17 0.08 ACY27 0.20 BC119 0.33 BC460 0.40 BF157 0.61 BN105 £2.20 OHP10 0.48 2N744 0.22 AA120 0.99 BY130 0.18 0A17 0.08 ACY27 0.20 BC119 0.38 BC730 0.27 BF158 0.61 C111E 0.55 ORP60 0.44 2M918 0.33 AA730 0.10 BY164 0.55 OA79 0.08 ACY30 0.31 BC126 0.13 BC730 0.28 BF159 0.86 0.61 C111E 0.55 ORP60 0.44 2M918 0.33 AA730 0.10 BY164 0.55 OA79 0.08 ACY30 0.31 BC126 0.13 BC730 0.24 BF159 0.86 0.61 C111E 0.55 ORP60 0.44 2M918 0.33 AA730 0.10 BY164 0.55 OA79 0.08 ACY30 0.31 BC126 0.13 BC730 0.24 BF159 0.86 0.40 0.33 BF159 0.86 0.40 0.33 BF159 0.86 0.40 0.33 BF159 0.86 0.40 0.33 BF159 0.84 0.40 0.30 0.30 0.30 0.31 BC126 0.13 BC730 0.28 BF159 0.86 0.40 0.33 BF159 0.84 0.40 0.35 BF159 0.35 BF1 | | | BC116 | 0.17 | BC303 | 0.35 | BF153 | 0.50 | BSY40 | 0.31 | OC204 | 0.28 | 2N726 | 0.31 | | DIO | DES AND | RECTIF | | |
| ACV28 0-21 BC119 0-38 BC480 0-40 BF185 0-61 BC193 0-22 BF187 0-61 BC195 0-20 CRP12 0-48 2N914 0-16 AAV30 0-10 BY184 0-55 OA79 0-08 ACV28 0-21 BC195 0-13 BCV30 0-22 BF187 0-61 BC195 0-86 C400 0-23 CRP16 0-44 2N929 0-22 BA100 0-11 BY210 0-39 OA85 0-10 ACV30 0-10 BC195 0-13 BCV32 0-23 BF180 0-86 C400 0-23 CRP16 0-44 2N929 0-22 BA100 0-11 BY210 0-39 OA85 0-10 ACV30 0-10 BC195 0-13 BCV33 0-24 BF180 0-44 C407 0-28 F20 0-55 2N930 0-23 BA100 0-11 BY210 0-39 OA85 0-10 ACV30 0-10 BC195 0-13 BCV34 0-28 BF180 0-44 C407 0-28 F20 0-55 2N930 0-23 BA100 0-11 BY210 0-39 OA85 0-10 ACV30 0-10 BC195 0-13 BCV34 0-28 BF180 0-44 C424 0-28 F20 0-55 2N930 0-23 BA100 0-11 BY210 0-39 OA85 0-10 ACV30 0-10 BC195 0-13 BCV34 0-22 BF185 0-44 C424 0-28 F20 0-55 2N930 0-23 BA100 0-11 BY210 0-39 OA85 0-10 ACV30 0-10 BC195 0-13 BCV34 0-22 BF185 0-44 C424 0-28 BF180 0-10 BC195 0-10 | ACY21 | | | | | | BF155 | 0.77 | B8Y95 | 0.14 | OC309 | 0.44 | 2N743 | 0.22 | | | | | | 0-15 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | ACY27 | 0.20 | BC119 | 0.33 | BC460 | 0.40 | | | | | | | | | AA129 | 0.08 | BY133 | 0.23 | OA70 | 0.08 |
| ACY30 031 BC126 0-20 BCY32 0-38 BF169 0-40 (-4007 0-28 BF20 0-45 2P830 0-22 BA100 0-11 BYZ10 0-39 0A85 0-10 ACY31 0-31 BC134 0-20 BCY33 0-42 BF160 0-44 (-4027 0-28 BF20 0-45 2P830 0-22 BA106 0-24 BYZ10 0-33 0A90 0-07 ACY31 0-23 0-23 BC136 0-17 BCY72 0-18 BF163 0-44 (-4025 0-55 BF36 0-24 BYZ10 0-32 BYZ11 0-33 0A91 0-07 ACY35 0-23 BC136 0-17 BCY72 0-18 BF165 0-44 (-4025 0-55 BF164 0-44 BYZ13 0-24 BA165 0-18 BYZ13 0-28 0A95 0-08 ACY35 0-31 BCY37 0-18 BF165 0-44 (-4025 0-55 BF141 0-19 2N1803 0-18 BA155 0-18 BYZ13 0-44 0A290 0-07 ACY36 0-18 BC137 0-17 BCY72 0-18 BF165 0-44 (-4025 0-25 BF141 0-19 2N1803 0-18 BA155 0-18 BYZ13 0-44 0A290 0-07 ACY36 0-18 BC137 0-17 BCY72 0-18 BF165 0-44 (-4025 0-25 BF141 0-19 2N1803 0-18 BA155 0-18 BYZ13 0-44 0A290 0-07 ACY36 0-19 BC139 0-44 BCZ10 0-22 BF167 0-24 (-4041 0-33 TP29 0-48 BYX1304 0-19 BA155 0-15 BZY18 0-39 BD10 0-08 ACY36 0-19 BC139 0-44 BCZ10 0-28 BF176 0-39 (-4042 0-33 TP29 0-48 BYX1304 0-19 BA155 0-15 BYZ18 0-39 BD10 0-08 ACY36 0-19 BC141 0-33 BCZ11 0-29 BF176 0-39 (-4042 0-33 TP29 0-48 BYX1304 0-19 BX137 0-17 BYX18 0-19 BX137 0-18 BYZ15 0-34 (-4025 0-25 BYX18 0-19 BX137 0-18 BYZ15 0-31 BYX17 0-39 (-4025 0-25 BYX18 0-49 BYX18 0-49 BX18 0-49 BYX18 0-49 BX18 | | | BC125 | 0.13 | BCY31 | | BF158 | 0.61 | CILLE | 0.55 | ORP60 | 0.44 | 2M918 | 0.33 | | | | | | |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | ACY30 | 0.31 | | | BC1 32 | | | | | | | | | | BA100 | 0.11 | BYZ10 | 0.39 | OA85 | 0.10 |
| ACV36 0-23 BC139 0-17 BCV77 0-22 BF164 0-44 C226 0-38 F141 0-19 2N1302 0-16 BA154 0-13 BYZ15 0-28 OAS0 0-08 ACV36 0-18 BC137 0-17 BCV77 0-18 BF164 0-44 C428 0-28 ST141 0-19 2N1303 0-18 BA155 0-18 BYZ15 0-39 OA200 0-07 ACV40 0-19 BC137 0-18 BC137 0-22 BF187 0-24 C442 0-23 T1F29 0-48 2N1304 0-19 BA156 0-15 BZY18 0-39 BD10 0-06 ACV41 0-39 BC140 0-33 BCZ12 0-28 BF176 0-39 C442 0-33 T1F29 0-48 2N1304 0-19 BA156 0-15 BZY18 0-39 BD10 0-06 ACV41 0-39 BC141 0-38 BC142 0-38 BF177 0-39 C445 0-39 T1F31A 0-68 2N1306 0-23 BY10 0-17 C662 BF187 0-39 C445 0-39 T1F31A 0-68 2N1306 0-23 BY10 0-17 C662 BF187 0-39 C450 0-24 BF177 0-24 BF177 0-39 C450 0-24 BF177 0 | | | BC134 | 0.20 | BCY34 | 0-28 | | | C424 | 0.28 | P346A | 0.22 | | | BA126 | 0.24 | BYZ12 | 0.33 | OA91 | 0.07 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | ACY35 | 0.23 | | | | | | | | | | | 2N1132 2N1302 | | BA148 | | BYZ13 | | | |
| ACY41 0-20 BC140 0-33 RCZ11 0-22 BF173 0-24 C442 0-33 ITP30 0-56 2X1305 0-19 BA153 0-16 BY719 0-31 SD19 0-06 ACY44 0-39 BC141 0-38 BCZ12 0-28 BF176 0-39 C444 0-39 TTP31 0-60 ZX1306 0-23 BY100 0-17 C662 1N34 0-08 AD140 0-53 BC143 0-33 BD115 0-68 BF177 0-39 C450 0-24 TTP32 0-73 ZX1307 0-23 BY100 0-17 C662 1N34 0-08 AD140 0-53 BC143 0-33 BD115 0-68 BF177 0-39 C450 0-24 TTP32 0-73 ZX1307 0-23 BY100 0-17 C662 1N34 0-08 AD140 0-53 BC143 0-33 BD115 0-68 BF177 0-39 C450 0-24 TTP32 0-73 ZX1307 0-23 BY100 0-17 C662 1N34 0-08 AD140 0-53 BC143 0-30 BD115 0-68 BF178 0-33 MAT100 0-21 TTP41 0-73 ZX1308 0-28 BY100 0-19 C6651 1N914 0-08 AD140 0-58 BC145 0-50 BD121 0-68 BF170 0-33 MAT101 0-21 TTP41 0-73 ZX1308 0-28 BY114 0-13 (OA70-79) 0-07 IN916 0-08 AD140 0-55 BC148 0-11 BD123 0-72 BF180 0-33 MAT120 0-21 TTP41 0-30 ZX1711 0-22 BY120 0-13 OA5 0-39 IN4148 0-06 AD140 0-55 BC148 0-11 BD124 0-76 BF181 0-33 MAT121 0-22 UT46 0-30 ZX1711 0-22 BY120 0-16 OA5 short 1B021 0-11 BD124 0-76 BB110 0-55 BF181 0-33 BD115 0-55 BF182 0-44 MJE2955 0-55 ZX141 E1.20 ZX189 0-35 BY127 0-17 leais 0-23 IS951 0-07 | | | BC137 | 0.17 | BCY72 | 0.16 | | 0.44 | C428 | 0.22 | BT141 | 0.19 | 2N1303 | 0.16 | BA155 | 0.16 | BYZ17 | 0.39 | OA202 | 0.08 |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | BC140 | 0.33 | BCZ11 | | BF173 | 0.24 | C442 | 0.33 | TIP30 | | 2N1305 | 0.19 | | | BYZ19 | | | 0.06 |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | | | | BF176 BF177 | | | | | | | | | | | .\n.na | | |
| $ \begin{array}{c ccccccccccccccccccccccccccccccccccc$ | AD140 | 0.53 | BC143 | 0.33 | BD116 | 0.88 | BF178 | 0 33 | MAT100 | 0-21 | TIP41A | 0.73 | 2N1308 | 0.26 | BY105 | 0.19 | CG651 | . | 1N914 | 0.06 |
| AD149 0-55 BC148 0-11 BD124 0-76 BF181 0-33 MAT121 0-22 UT46 0-30 2N1711 0-22 BY126 0-16 OA5 short 18021 0-11 AD161 0-39 BC149 0-13 BD131 0-55 BF182 0-44 MJE2955 0-95 ZN414 £1-20 2N1889 0-35 BY127 0-17 leads 0-23 IS951 0-07 | AD143 | 0.42 | | | | | | | | | | | | | | | | | | |
| 17100 and 77100 | | | BC148 | 0.11 | BD124 | 0.76 | BF181 | 0.33 | MAT121 | 0.22 | UT46 | 0.30 | 2N1711 | 0.22 | BY 126 | 0.16 | OA5 shor | t | 18021 | 0.11 |
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| 7403 | 0.15 | 0.14 | 0.13 | 7453 | 0.15 | 0.14 | 0.13 | 74145 | 1.30 | 1 . 25 | 1 20 |
| 7404 | 0.15 | 0.14 | 0.13 | 7454 | 0.15 | 0.14 | 0.13 | 74150 | 1.50 | 1.40 | 1.30 |
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| 7409 | 0.25 | 0.24 | 0 - 23 | 7474 | 0 - 41 | 0.39 | 0.35 | 71156 | 1.20 | 1 . 15 | 1.10 |
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| 7416 | 0.30 | 0.29 | 0.28 | 7482 | 0.90 | 0.85 | 0.80 | 74163 | 1.40 | 1.85 | 1.30 |
| 7417 | 0.30 | 0.29 | 0 . 28 | 7483 | 1.20 | 1.15 | 1.05 | 74164 | 1.80 | 1.75 | 1.70 |
| 7420 | 0.15 | 0.14 | 0.13 | 7484 | 1.00 | 0.97 | 0.95 | 74165 | 1.80 | 1 - 75 | 1.70 |
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| 7423 | 0.40 | 0.39 | 0.38 | 7486 | 0.35 | 0.34 | 0.88 | 74174 | 1.60 | 1.53 | 1.50 |
| 7425 | 0 - 40 | 0.39 | 0.38 | 7489 | 4.00 | 3.75 | 3.50 | 74175 | 1.10 | 1.05 | 1.00 |
| 7426 | 0 . 40 | 0.38 | 0.36 | 7490 | 0.65 | 0.63 | 0.60 | 74176 | 1 . 25 | 1.20 | 1.15 |
| 7427 | 0.40 | 0.38 | 0.36 | 7491 | 1-10 | 1.05 | 1.00 | 74177 | 1.25 | 1.20 | 1.15 |
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| 7432 | 0.40 | 0.38 | 0.36 | 7494 | 0.85 | 0.82 | 0 - 75 | 74192 | 1 . 25 | 1.20 | 1.15 |
| 7433 | 0.42 | 0.40 | 0.38 | 7495 | 0.85 | 0.82 | 0.75 | 74184 | 1.80 | 1.75 | 1.70 |
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| 7438 | 0.35 | 0.32 | 0.30 | 74100 | 1.50 | 1.45 | 1.40 | 74191 | 1.95 | 1.90 | 1 85 |
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UTC04 = 12 × 7403
UTC05 = 12 × 7403
UTC05 = 12 × 7403
UTC05 = 12 × 7407
UTC10 = 12 × 7410
UTC20 = 12 × 7420
UTC30 = 12 × 7430
UTC41 = 5 × 7441
UTC41 = 5 × 7441
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UTC43 = 5 × 7442
UTC43 = 5 × 7442
UTC43 = 5 × 7443 Pak No. Contents 1 UIC99-5 × 7499 UIC91 = 5 × 7491 UIC92-5 × 7492 UIC93-5 × 7493 UIC94-5 × 7494 UIC96-5 × 7496 UIC106-5 × 7496 UIC106-5 × 74196 UIC114-5 × 74191 UIC151-5 × 74191 UIC196-5 × 74191 UIC46 = 5 × 7446 UIC48 = 5 × 7448 UIC50 = 12 × 7450 UIC51 = 12 × 7451 UIC53 = 12 × 7451 UIC53 = 12 × 7454 UIC60 = 12 × 7460 UIC70 = 8 × 7470 UIC72 = 8 × 7472 UIC73 = 8 × 7473 UIC73 = 8 × 7473 0 · 54 0-54 0-54 0-54 0-54 0-54 0-54 $UIC74 = 8 \times 7474$ UIC80 = 5 × 7480 UIC80 = 5 × 7480 UIC81 = 5 × 7481 UIC82 = 5 × 7482 UIC83 = 5 × 7485 UIC86 = 5 × 7486 0.54 0.54 0.54 UICXI = 25 Assorted 74's £1-65

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SPECIFICATION 170-410
Frequency coverage 170-410kHz, 525-1250kHz, 1:25-3-0MHz, 3-7-50MHz, 7:5-18MHz, 18-30MHz (Dual conversion)
Bandspread 3-5-4MHz, 7-7-53Hz, 14-14-6MHz, 12-21-5MHz (Dual conversion), 26-30MHz (Dual conversion)
Modes AM, USB, LSB, CW
Selectivity 2 position wide/narrow
Antenna 50-10ΩΩ
Sensitivity 14V for 10dB SIN (SSBICW)
AF Output More than 1-5W Into 8Ω. Internal speaker fitted
Power supply 100/117/1220/240V ac 50/60Hz, External 12V dc. Internal 12V batteries, Automatic changeover to Internal supply in the event of mains failure
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Options 500kHz marker QR6MK, FM broadcast tuner
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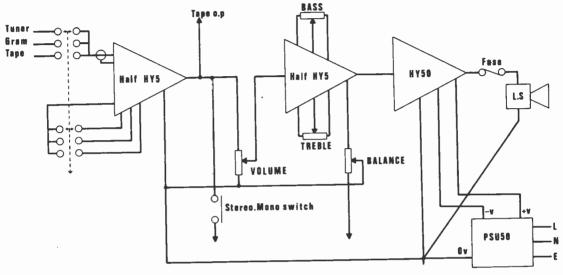
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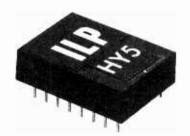
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Ratio: 88db. Overload Capability: 40db on most
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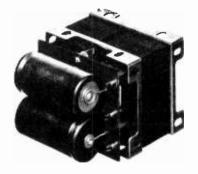
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power lines and earth.
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Impedance: 47k0. Distortion: Less than 0:1% at 25W
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Voltage: ± 25V. Size: 105 x 50 x 25mm.

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| 1.5µF 63V | 7p | 100µF 63V | 17p | 3 × 3 * " | | 33p | |
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| 6 8µF 63V | 7p | 220μF 10V 220μF 16V | 7p | 21 232 | (Plain) | | |
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| 22µF 63V | 7p | 680µF 40V | 28p | ACI27 | 21p BC | 2212L I | IЗp |
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| 33µF 16V | 7p | 1000µF 25V | 28p | BC107 | 12p BC | 214L I | 18p |
| 33µF 40V | 7p | 1500µF6 4V | 17p | BC108 | | C44 I | 9p |
| 47µF 10V | 7p | 1500µF 16V | 28p | BC109 | 13p O | Ç7! I | 3p |
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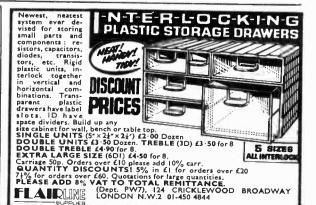
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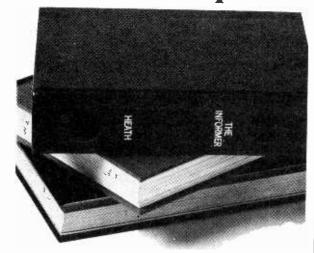
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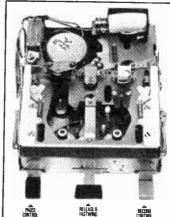
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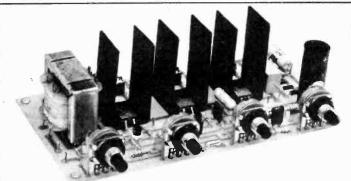


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20 WATT SPEAKER SYSTEM

System consists of a $13^{\prime\prime}\times8^{\prime\prime}$ (approx.) eliptical woofer unit with a $8^{\prime\prime}\times5^{\prime\prime}$ (approx.) mid-range unit incorporating parasitic tweeter and crossover components and circuit diagram

Technical Specification: Bass Unit: Flux density — 100 K, speech coil — 1½". Cone. Triple laminated paper with P.V.C. surround. Mid-Range Unit: Flux density — 33 K, speech coil - 1" with parasitic tweeter. Power handling: 20 watts RMS, impedance 8 nhms frequency response -Our Price £8.70

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Components and circuit diagram

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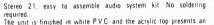
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Elegant self selector push button player for use with your stereo system. Compatible with Viscount IV system, Unisound module and the Stereo 21 Technical specification Mains input. 240V, Output sensitivity 125mV. Comparable unit sold elsewhere at £24.00 approx. Yours for only

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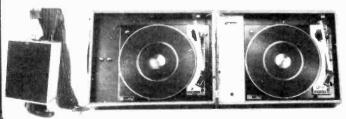


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VAT MUDDLE!

HE ominous expansion of VAT to 25% has indeed brought forth justifiable protests from many quarters of the electronic components industry.

Customs and Excise Notice 742 states that the 25% rate of VAT is applicable not only to assembled radio receivers, amplifiers, TV's etc. but applies also to all component parts, accessories and service in respect thereof. Notice 742 states that the 25% VAT rate applies to all resistors, capacitors, coils, transistors, etc. if they are of a kind suitable for use as parts of goods for the aforementioned items, even when these goods are supplied for the manufacture or service of other equipment not taxed at 25%.

There is considerable uncertainty within the trade and industry over the new VAT schedule. The industry is quite justifiably up in arms over this punitive rate of tax.

The pursuit of our hobby, and the pursuit of many others, could be severely restricted by the extra cost of components. Research, development and experimentation will be throttled and the widespread implications of this should be obvious to anyone.

LIONEL E. HOWES—Editor

WIRELESS

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Practical Wireless—the favourite magazine of the radio and electronics constructor—extensively read by the trade and many others concerned with modern electronics

108,698

ABC*JULY-DECEMBER 1974

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NEWS...

Heathkit Competition Result

N our March issue we invited readers to assess advantages of building one's own electronic equipment over buying ready-made outfits.

Having considered all entries, the judges decided that the best received was that submitted by Mr. Robert Gregory, of Mansfield, Notts, who had listed the featured advantages in the following order: 1st—C; 2nd—A; 3rd—J; 4th—E; 5th—L; 6th—B; 7th—K; 8th—D.

Mr. Gergory wins a £100 voucher to spend on equipment from Heathkit.

The four next best entries were from:—Mr. H. Boland, Armagh; Mr. J. McKeown, Wigtown; Mr. P. Garside, Kings Lynn; Mr. I. Marsden, Nottingham. Each wins a £50 Heathkit voucher.

To complete the prize-list there were a further eight £25 Heathkit vouchers, and these went to Mr. R. Armstrong, Farnborough; Mr. M. Clay, Sevenoaks; Mr. B. Cambray, Croydon; Mr. Pidun, Braintree; Mr. P. Royle, Bristol; Mr. E. Rumble, Haywards Heath; Mr. S. V. Bentall, Buntingford; Mr. P. G. Hazelwood, Brierley Hill.

Advertisers Note

RECENTLY Practical Wireless has been able to offer a unique service to its advertisers. On request, advertisers have been given advance information concerning components for P.W. projects.

Advertisers should contact Dennis Brough on 01-634 4116 or Christine Dunn on 01-634 4293.

Essex Repeater Group

THE above group have submitted their application to the Home Office for a 70cm repeater to be sited on Danbury. To assist fund raising a Grand Bring & Buy and Junk Sale will be held at St. John's Hall, Vicarage Road, Chelmsford, on Saturday, June 28th from 11 a.m. to 6 p.m. The Group will be arranging 'talk in' on 433.200 UHF S20/S22 and 4 metres. For further information contact G3VKO. G3WCO or G3MVV.

NEWS...

NEWS...

NEWS...

Sinclair wins Queen's award



Sinclair Radionics has won a Queen's Award to Industry, 1975, in recognition of its outstanding export achievement and for technological innovation in scientific electronic calculators.

During a three-year period ending in April 1974 the company, which is Europe's largest manufacturer of electronic calculators increased its exports tenfold to £2,232,040 p.a. or 56 per cent of turnover.

Award for technological innovation has been made for the development of the low cost, Sinclair 'Scientific' pocket calculator.

Picture shows Clive Sinclair, aged 35, founder and Managing Director of Sinclair Radionics of St. Ives, Cambs.

More awards

THE X-Ray Systems Division of EMI Limited and the Telecommunications Division of EMI Sound & Vision Equipment Limited have both won the 1975 Queen's Award to Industry for export achievement.

EMI contract

THE original £1·25 million contract won by EMI Sound & Vision Equipment Limited to supply the complete antenna system for the CN Tower in Toronto, the world's tallest self-supporting structure, has been boosted by £60,000. This latest contract covers the provision of additional antennas for Ch. 70.

Three Q concept

THE ability to provide quality products in quantity, quickly has always been the strength behind the Mullard company. At the International London Electronic Components Show at Olympia this 'Three Q' concept was adopted as an overall theme aptly illustrating the company's attitude towards trading in the challenging years ahead.

Eleven major displays on a stand of 300 square metres highlighted what is believed to be the broadest range of components ever shown. In addition to the 'Three Q' components available now to meet equipment production needs, the displays included over a hundred new products for tomorrow's designs, many of them on show for the first time.

A team of Mullard engineers was on hand to discuss all aspects of the displays and a data-bar provided visitors with the latest information on every product in the Mullard range.

Following their participation at the London Electronic Components Show, Mullard took their displays to Edinburgh, Manchester and Bristol. At each centre the displays were backed by a series of lectures from Mullard experts.

Books received

Slide-Tape and Dual Projection By R. Beaumont-Craggs

Covers all aspects of music and 'chat' with slides. Topics covered include essential equipment, taking pictures, preparing the sound track, dual projection, special effects, audio visual in education and the all-important presentation of the show. It would prove invaluable to tape-recording enthusiasts, photographers, photographic and amateur cine clubs, teachers, sales and publicity personnel etc.

Price £3
Focal Press Limited 31 Fitzroy
Square, London, WIP 6BH

Plessey Semiconductors Integrated Circuit Data Book

No author

Contains full information on the continually-growing range of standard products manufactured by the Plessey Company.

No price quoted Plessey Semiconductors, Cheney Manor, Swindon, Wilts, SN2 2QW

Tape Recording from A to Z By Doug Crawford

Simple language explanation of how tape recording works—a simple step-by-step account of using reel-to-reel machines; what to look for when buying one etc.

Price £1.85

Kaye and Ward Limited, 21 New Street, London, EC2M 4NT

Questions and Answers on HiFi

By Clement Brown

Q and A in very simple language on most things you need to know about HiFi. All sources are covered — discs, tapes, radio. Guidance on costs is given, specifications, planning requirements, etc. etc.

Price: 75p Butterworth & Company, 88 Kingsway, London, WC2B 6AB

BBC Handbook 1975

No author

Almost everything you need to know or want to know about the BBC.

No price quoted
British Broadcasting Corporation,
35 Marylebone High Street,
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RICHARD MANN*

LTHOUGH this article is headed The Texan II it would probably be more accurate to describe it as the Texan III/II! Since the first design appeared in these pages about three years ago I am told that approximately 45,000 kits have been sold. (Next time, I'm going to make sure that I have a slice of the action!) With all those Texans knocking around it was inevitable that there should be quite a bit of correspondence on the subject. These notes, therefore, are intended to deal with some of the points which have come up most often and aimed at the man who already has a working Texan and who wants to upgrade it slightly. In the not-toodistant future I hope that PW will be able to publish a new design which is currently gestating, but new designs are not much comfort if you have already spent your money.

The three points which have arisen most consistently have been:—

- 1 Susceptibility to RF interference.
- 2 How to increase the power output.
- 3 How to install a Tape Monitor facility.

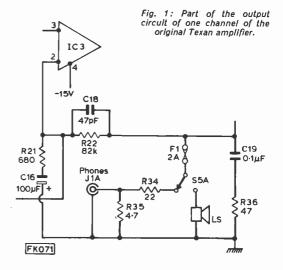
There have been other comments, of course. Some of them are repeatable, but not really within the scope of the Texan concept. The idea of the Texan was to produce a value-for-money design without a lot of frills but which would be very reproducible and would sound really good under normal domestic conditions.

SUSCEPTIBILITY TO RFI

I think this fault was the one real shortcoming of the original design. Unfortunately it is not a very easy thing to test for under laboratory conditions. It's not until 45,000 fridges have clicked on and off a few times that you know you really have a problem on your hands! The weakness was partly due to the rather skimpy screening of the Texan metalwork and partly to the over-simplification of the design so that there were no filtering components in it from input to output.

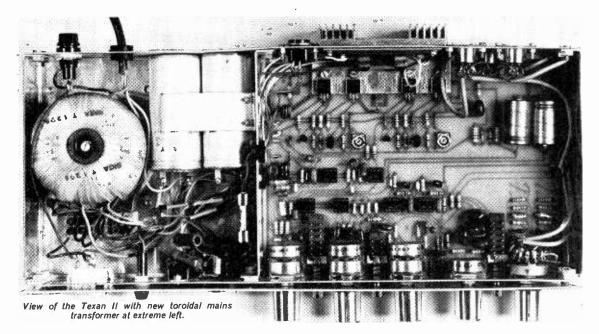
Basically, anything which is wired into the amplifier is capable of introducing interference, the mains lead, the pick-up leads and the loudspeaker leads.

I mention the loudspeaker leads last because it appears that these have been the major cause of the trouble. They are usually long for a start, and in the output circuit, which is shown in Fig. 1, it will be noted that there is virtually a short-circuit to RF from the output, through C18 and on to the inverting input of IC3. Now although they are miraculous things, operational amplifiers are not normally noted for the fastness of their slew-rates. Slew-rate being the maximum volts per second that they can deliver. They might give out 100mV at 1MHz or 10V at 10kHz but there is no way they will give 10V at 1MHz! Consequently a fast signal appearing spuriously at an input terminal will tend to be greatly amplified in the early high-gain stages of the op-amp but the later stages will be unable to follow it with the result that there will be distortion and demodulation of the signal and rude noises at the output.



Two simple high-pass filters have been added, R39/C24 in Fig. 2a and R40/C26 in Fig. 2b. These have a cut-off frequency of 2·2MHz so they do not have any audible effect on the amplifier response. However they filter out most of the spurious RF before it can do any harm. A further capacitor, C25,

^{*} Texas Instruments Limited



is added directly across the input terminals of IC3 in order to provide a shunt for any residual noise which appears differentially at this point. This capacitor causes a slight drop in the high-frequency open-loop gain of the op-amp which consequently causes a slight increase in the high-frequency distortion of the Texan but the audible difference is quite undetectable.

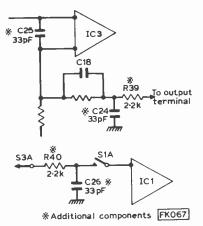


Fig. 2: Circuits of the two high-pass filters added to each channel.

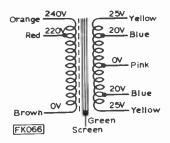
These extra components are very easy to add. Resistor R40, and its complementary resistor in the other channel, R140, are wired in directly between switch S3 and points H and I on the PCB which is shown in Fig. 3. These resistors replace the short wire connections originally there. The PCB can then be drilled to take the remaining filter components. This can be done quite accurately with a sharp drill held in a pin-chuck and twisted in the fingers. If it is a Texan kit with a removable base it is easy to hold the board against a light and drill through from the top. The exact positioning of the holes is not critical but it is obviously important to avoid any damage to existing components. Take care also that

the track is not drilled through as the solder joint, when made, may fail to close the gap in the track. It is better to drill just alongside the track and bend the component wire across.

INCREASING OUTPUT POWER

There are two approaches to increasing output power: one is to increase the peak power obtainable under transient conditions; the other is to increase the continuous output power from both channels simultaneously. The first is a function of the power rail voltage while the second is a function of the power supply regulation. Both of these factors, in turn, are primarily a function of the mains transformer used. The transformer used in the original design was chosen for its combination of economy and good performance. It would not, however, give the regulation obtainable from a rather more expensive toroidal transformer, such as that used here in the Texan II. This has been designed to fit in the same space but it has a 75VA rating and has some extra taps. The primary has a tap for 220V input as well as 240V and the secondary is wound to give 25-20-0-20-25V.

The Texan I was capable of delivering 20W+20W into 8 ohms with an intermittent sine wave input but would give only 16W+16W with continuous



Colour coding of the toroidal transformer. A small terminal block is desirable to take extra secondary leads. The block can be seen below the transformer in the photograph above.

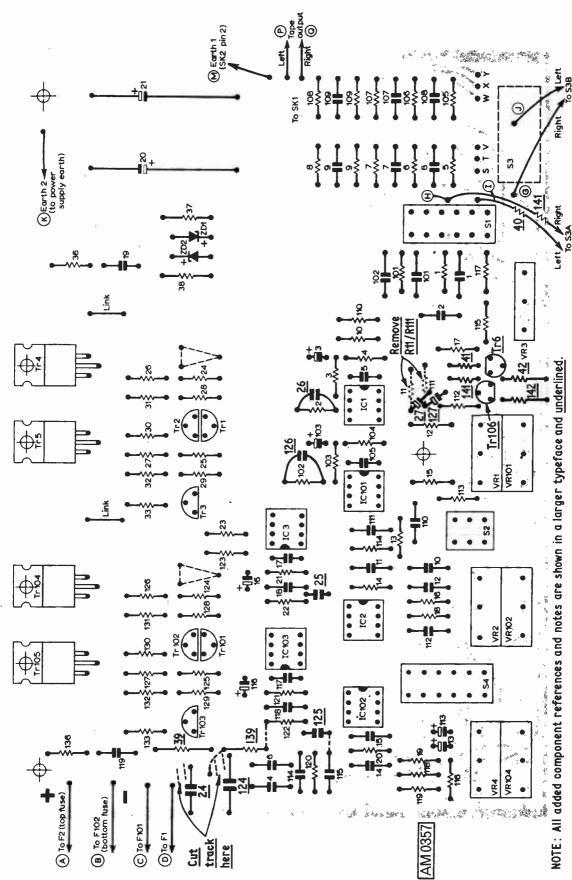


Fig. 3 : Original Texan PCB with RFI suppression components added. Tape monitor modifications, centre bottom, are shown from foll side in Fig. 11.

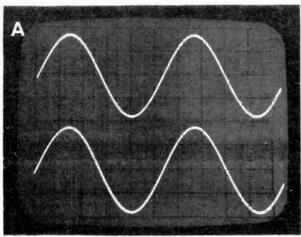


Fig. 4: Sinewage output with amplifier running at 2 x 20W into 8Ω speakers and using 20V taps on transformer.

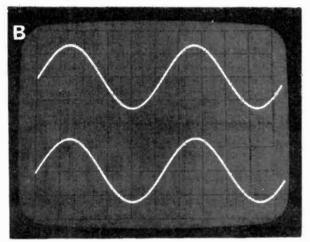


Fig. 5: Output of 22W per channel into 4Ω speakers. Again, 20V taps on transformer.

inputs. Simply by replacing the original transformer with a toroidal version, the amplifier will comfortably deliver 20W continuously into 8 ohm loads or 22W+22W into 4 ohm loads. No other circuit changes are necessary except that the two 2A fuses in the supply lines should be increased to 3A rating. The oscillograms in Figs. 4 and 5 show that there is no clipping under these maximum output conditions.

If it is wished to increase the output power substantially then the 25V secondary taps can be used. It then becomes necessary to change the output transistors, Tr4 and Tr5, since the breakdown voltage, $V_{\rm CEG}$, for the TIP41A and TIP42A is only 60V. The DC rail voltage under quiescent conditions is now ± 37 V. It is therefore quite possible that the breakdown voltage of the transistors will be exceeded and although there is a chance that they will stand it, it is far wiser to be on the safe side and replace them with TIP41B and TIP42B respectively. These have a breakdown voltage of 80V. It is not necessary to change any other components.

Oscillogram, Fig. 6, shows the clean output of the amplifier, with the higher voltage rails, delivering a continuous sine wave power of 28W+28W in 8 ohm loads. Probably of more significance is the oscillogram shown in Fig. 7 which shows a con-

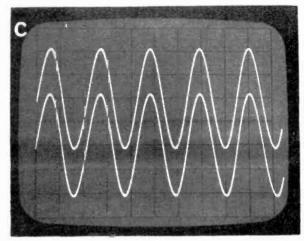


Fig. 6: This time the 25V transformer taps are used, giving 2 x 28W into 8Ω speakers.

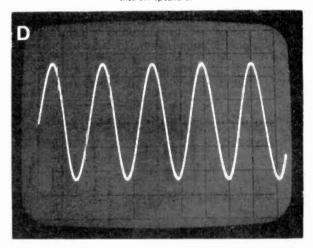


Fig. 7: Output from one channel providing 40W into an 8Ω speaker using 25V taps on mains transformer.

tinuous sine wave power of 40W being delivered to an 8 ohm load. The amplifier will, in fact, give an instantaneous power of about 100W on transient inputs. The effect of this, for normal music listening, is that peaks sound extremely clean. My record of Beethoven's Ninth suddenly seemed much better, and all the time I have been blaming it on the recording company!

In order to maintain these higher powers it now becomes highly advisable to add an extra heat sink. For this I have used a short length of Redpoint M-type Powersink. Unfortunately this is just too wide to fit in between the sockets on the back of the Texan without some modification. One fin section has therefore been sawn off each side of heatsink reducing its size to $3^1_4 \times 1^3_4$ in. It can then be drilled and tapped to take the 6BA screws which hold the original heat sink assembly together.

Alternatively it might prove easier to use separate countersunk screws to hold the transistor mounting plate and the heatsink independently on to the back panel of the amplifier. In this case all the screw heads will be "blind" being sandwiched between the parts of the assembly. The screws should therefore be inserted and held in place with a touch of Durofix until they can be tightened up with the nuts, Fig. 8. Although this is rather tricky it does avoid a slight

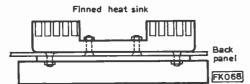


Fig. 8: Suggested method of fixing new heatsink.

"bodge" which is needed to work the screws between the fins of the Redpoint Powersink. Whichever method is used a smear of heat sink compound should be placed on the adjoining surfaces.

TAPE MONITOR

The tape monitor facility is very simple to add from a circuit point of view but it requires rather more care to add mechanically. The function of the tape monitor is to provide a means of breaking the amplifier between the equalization stage and the tone control stage so that a tape recorder with separate record and replay functions can be inserted to "fill the gap". This allows a recording to be made off a disc, for example, using the correct equalization in the first stage. The remainder of the amplifier can then be used to amplify the tape recorder output so that a direct comparison can be made between input and recorded signals.

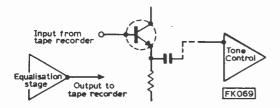


Fig. 9: Emitter-follower buffer stages must be introduced for the tape monitor facility.

The tone control stage in the Texan must be driven from a low impedance source so it is necessary to buffer the tape monitor inputs with a pair of emitter-followers as shown in Fig. 9. This modification can be incorporated by wiring the extra transistors across the back of the Auxiliary Input socket and putting a small switch on the back panel. A neater alternative is to make use of the Mono/Stereo switch. Although it is normal to have this facility on a stereo amplifier I have found that it is very seldom used in practice. Since the switch unit S2 is a 2-pole changeover type it is ideal for its new role.

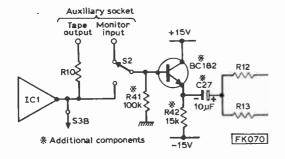
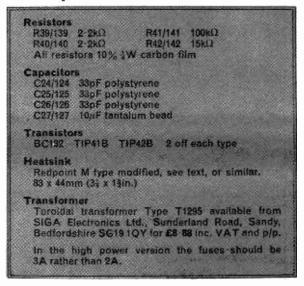


Fig. 10: Circuit of one of the buffer stages.

★ components list



The actual circuit modifications are shown in Fig. 10. Resistor R111 is no longer necessary and can be removed from the PCB, making room for the new components. The circuit track connecting to S2 is removed. The easiest way to do this is to cut the track with a sharp razor blade at the ends of the unwanted section and then heat the track with a fine soldering iron so that it can be peeled off with a pair of tweezers. The board should then be drilled very carefully as shown in Fig. 11 and the extra components wired in position. It is, unfortunately, necessary to use a few wire links in order to complete the modification but they fit in quite neatly as shown.

The input connection to the Monitor switch can be made using the existing length of twin screened

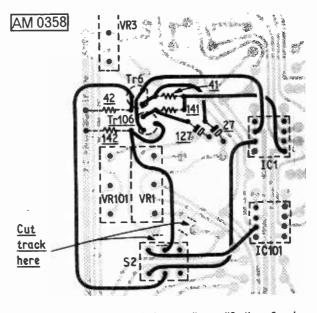
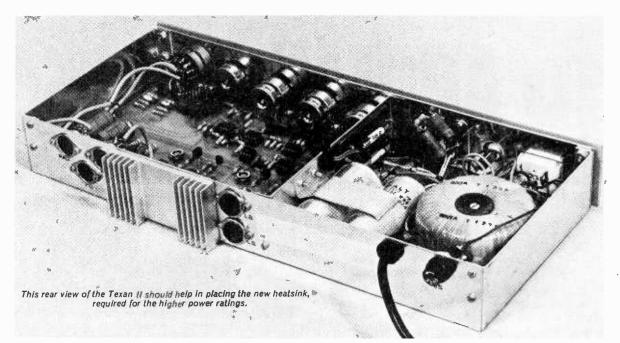


Fig. 11: Area of PCB affected by tape monitor modifications. See also Fig. 3.



cable which normally runs between the AUXILIARY DIN-socket and the AUX. position of S3. In the photograph this wire is shown running underneath the PCB, however it can just as easily be run over the top with the connections being made to the upper leads on S2. The unused contacts on S3 can be left open or, more usefully, can be shorted across to the RADIO contacts so that two different sensitivities could be selected for one source by switching from RADIO to AUX. at the front panel.

Another rather fortuitous point is that the "0" of "MONO" on the front panel can be removed with a little delicate surgery leaving an appropriate

"MON" for "monitor".

Adding this tape monitor modification gives an extra advantage in that it AC couples the equalisation stage to the tone control stage. On reflection I think I was rather over-anxious to reduce the number of capacitors in the Texan to an absolute minimum. The result of DC coupling between these two stages is that the DC gain of the tone control stage becomes dependent on the setting of the bass control. Thus, if there is a small offset voltage at the output of IC1 this will be amplified by the following stage. If the bass control is then moved rapidly there can be a rather disconcerting plop in the loudspeakers. If your Texan suffers from this it is well worth while to insert a 10 µF capacitor between R11 and the junction of R12 and R13 even if you do not wish to add the tape monitor facility itself.

IN CONCLUSION

I hope that the modifications suggested above will provide the answers to the majority of constructors' problems. They are not very dramatic but, as I said earlier, to do much more would be to change the concept of the Texan's value-for-money design. In spite of the odd bits of "knocking copy" that have since appeared I still think it was quite a good concept. It is clear that the changes can be made

singly or collectively according to how much time and money the constructor wants to spend.

To those people who have blown up several sets of output transistors, there is little I can offer but my sympathy. If the specified devices are used it is extremely unlikely that they will have been faulty themselves. However, they are connected across a beefy power supply with no form of current limiting in series with them. Any circuit fault which causes both transistors to turn on at the same time, even momentarily, will almost certainly cause them to blow. It is therefore vital to ensure that the greatest care is taken when soldering the output stage components. There is always a reason why things go wrong no matter how sure the unlucky constructor may be that "it just happened." Furthermore, one disaster may well cause a degradation of another component, so if you have an accident make sure you remove and check all the devices before throwing away another good set of power transistors. All the transistors can be checked adequately with an Avo and ICs can be checked by swopping around. If IC3 or IC10 is removed, protect the output devices by breaking the set-up link in the emitter of Tr4 or Tr104 respectively. Finally, if you do not have a fine soldering iron or do not know how to use it, buy one and practice. I have seen some of the plumbing jobs that have been perpetrated! You don't know whether to laugh or cry!

Editorial Note—The author has also supplied some technical information on disc equalisation. Interested readers can obtain a copy of this by forwarding a self-addressed stamped envelope to PW marking the outside of the covering envelope "Texan II." No other correspondence should be enclosed.

Reprints of the original series of articles on the Texan can still be obtained from PW for 40p inc. p/p. Make out cheques/postal orders to IPC Magazines Ltd. and mark covering envelope "Texan Reprint."

UAPOLLO /efic/ VARICAP AM/FM STEREO TUNER

W. POEL*

IN THIS, the third part of the Apollo series, we will look at the way varicap diodes can be used in an AM/FM system to give simple frequency control using a single long-throw slider potentiometer.

The complete tuner offers a specification compatible with most hi-fi systems, yet it is built from a series of AM/FM modules which are simply interconnected on a base board. This method of construction does away with the uncertainties of various pieces of wire trailing around the chassis and allows the constructor to use ready-built modules for sections such as the FM IF strip which otherwise may be considered beyond one's resources to test and align.

THE COMPLETE SYSTEM

The theme of the Apollo series is the "all-electric wireless" so do not be surprised to find that varicaps abound in all the signal frequency tuned circuits. The tuning is accomplished by means of the long

slider pot and the cursor gives direct scale readout. Fig. 3.1 shows a block diagram of the complete unit.

For the front end of the FM section the new Toko EC3302 varicap tunerhead was chosen since it offers a low-cost combination of performance and varicap tuning together with an a.f.c. system that is directly compatible with the output of the IF detector.

The importance of compatibility should not be overlooked since methods of a.f.c. vary considerably and the system used in the LP1186 for example does not suit a quadrature detection system such as that used by the KB4402 IF IC.

The input stage to the tunerhead is an FET with facilities for either 300 or 75 ohm aerials. The mixer stage then feeds the IF signal at 10.7MHz into the IF amplifier block with the local oscillator functioning at the signal frequency plus 10.7MHz in accordance with usual superhet techniques.

The IF amplifier (Fig. 3.2) is worthy of note since it employs two linear phase filters rather than the popular ceramic filters, giving good selectivity at 10.7MHz.

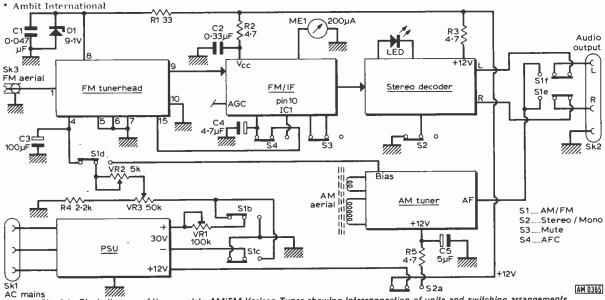


Fig. 3.1: Block diagram of the complete AMIFM Varicap Tuner showing Interconnection of units and switching arrangements.

C8 330pF

C9 0.47µF 35V tantalum

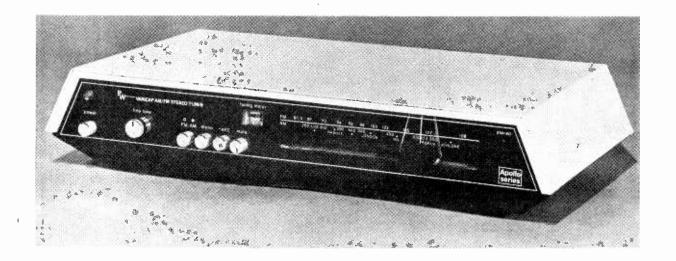
FM TUNERHEAD Inductors Toko EC3302U (Ambit) T1 Toko 6A6371 Toko 6A6372 Toko YHCS11100AC2 Toko CFU050D IFT1 CF1 FM IF MODULE Resistors Ferrite rod aerial (see text) R1 330Ω R9 10kΩ 18kΩ 470Ω R10 Semiconductors R3 2.2kΩ R11 33kΩ 1N4148 R4 56Ω R12 4.7kΩ IC1 LM1820N (or CA3123E, μΑ720, NE546) R5 2·2kΩ R6 120kΩ R7 330Ω R13 2·7kΩ R14 4·7kΩ R15 4.7kΩ R8 470Ω POWER SUPPLY All 1W ±5% carbon VR1 470kΩ skeleton preset Resistors R1 R2 100Ω 1W 4.7Ω 1W Capacitors VR1 100kΩ skeleton preset C1 0.01µF C2 0.01µF 0.01µF VR2 5kΩ linear carbon C8 0.01/4F 50kΩ linear 150mm slider (Rivlin WS150) C9 C3 0.022µF 0-01/4F C4 0·01μF C5 0·022μF C10 0.01µF Capacitors C11 0.01#F C1, C2 C3, C5 C4 100μF 25V (2 off) 1000μF 25V 470μF 40V C6 0-22/1F Inductors 0.1µF (4 off) F1, F2 Toko BBR3125N Linear phase filter (2 off) C6-C8 Toko TKACS 34342/3 double tuned detector Semiconductors 1N4148 (2 off) 1N4001 (4 off) 9·1V 400mW Zener D1, D2 D3-D6 Semiconductors Tr1 BF274 D7 IC1 CA3089E or TDA1200 IC1 78L12 IC2 MC7818CP STEREO DECODER MODULE Miscellaneous Resistors Mains primary, 0-20V 0-20V 6VA secondary R1 18kΩ R4 3.9kΩ R2 $1k\Omega$ R5 R3 $3\cdot 9k\Omega$ All $\pm W \pm 5\%$ carbon VR1 $5k\Omega$ skeleton preset Mains neon indicator R5 390Ω MISCELLANEOUS Resistors R1 33 Ω R2, R3 4.7 Ω Capacitors C1 470pF 0.25µF R4 2.2ks C2 0.25µF C8 2/4F 16V C3 0·5μF C4 0·05μF C9 10μF 25V C10 10μF 25V Capacitors C1 0.047μF C5 0.02/4F C11 0-047/F C6 0.02µF 0-33µF Filter F1 Toko BLR3107N pilot tone filter C3 100µF 10V 4-7/1F 16V 5µF 16V Integrated Circuit and LED IC1 KB4400 (or MC1310P, CA1310E, SN76115N) D1 TIL209 or similar Switches, etc S1-S4 4-way pushbutton unit (6 pole c/o + 2 pole c/o + 2 pole c/o + 2 pole c/o, non-inter-AM TUNER MODULE locking) Resistors Mains on/off pushbutton 200µA f.s.d. edgewise meter R1 4712 100kΩ ME1 R2 330Ω 33kΩ Case approximately 400 x 220 x 75mm (16 x 81 x 3in) R3 100kΩ 200%Ω R4 100kΩ Escutcheon 1kΩ R8 Printed circuit boards, coaxial cable, twin screened All 1W ±5% R9 2.2kΩ cable Sk1 Sk2 Mains input socket 5 pin 180° DIN Capacitors C1 1500pF C10 0.047µF Sk3 Coaxial socket C2 10µF 25V C11 10µF 16V C3 10µF 25V C4 1500pF C12 0·1μF C13 0·1μF D1 7-5V Zener Complete kits including case and escutcheon are available from T.T.S. Ltd., 7 West Road, Westcliff-on-Sea, Essex. Kits for FM/IF, stereo decoder and AM modules are available from Ambit International. C5 10µF 16V C14 0.47µF 35V tantalum C15 4700pF C16 4700pF C6 0·1μF C7 56pF

Order numbers are 91200, 91310 and 9720 respec-

tively.

4µF C17

TC1, TC2 5 to 25pF miniature trimmer (2 off)



Linear phase filters have certain advantages over the ceramic types and they may be summarised as follows:

Lower intermodulation distortion;

Being LC the temperature stability is better;

The out-of-band attenuation is superior. This means that whereas some of the signal from the local oscillator may leak through ceramic filters from the front end it will be very much more severely attenuated in this eight-stage filter.

Experience has shown that the susceptibility of the IF amplifier device to local oscillator leakage is unpredictable: some chips may not be affected at all whilst others suffer severe muting as a result of instability induced by this leakage signal.

TRANSISTOR STAGE

The transistor gain stage compensates for the loss caused by the two filters and then feeds the IC with a suitably tailored 10.7MHz signal for amplification, limiting, detection and muting.

Much has already been said about the CA3089E, but the other versions (e.g., Kyodo's KB4402, SGS's TDA1200 and Hitachi's HA1137W) all seem to perform similarly except for the muting function. Although there is a preset on the board to set the threshold of muting, the muting variability of different devices leads to problems in predicting the exact effect that any sample will provide.

Most devices tried to date have offered a quite acceptable level of muting and some are quite fault-less.

The meter drive facility is fed to the panel meter to provide a guide to fine tuning. Although a facility exists for centre-zero tuning meters it is not necessary unless one is after a tuner that resembles a Concorde flight deck rather than a means of reproducing euphonic sounds.

QUADRATURE DETECTOR

The quadrature detector of the IC is quite simple but can pose problems in alignment where the double

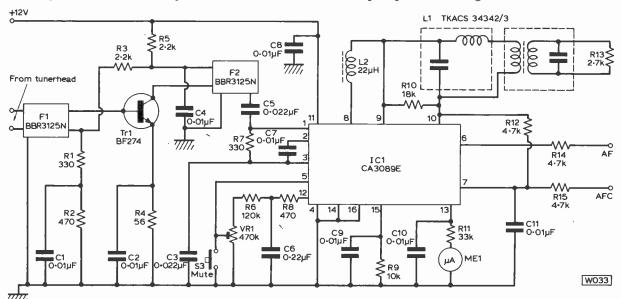


Fig. 3.2: Circuit diagram on the FM/IF section of the tuner. This unit takes its input from the tunerhead.



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And it promised the first-ever professional electronics service for amateurs.

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| x 45mm High | x × 82mm | High × | | |
| 40mm Deep. | 43mm Dee | | | |
| Movement 1.1 | | | | |
| Ohn | | Ohms | | |
| 0-50 micro A. 125 | | | | |
| 0-100 micro A. 58 | 30 0-100 micr | o A. 730 | | |
| 0-500 micro A . 17 | | o A. 200 | | |
| 0-1 mA 17 | 70 0-1 mA | 200 | | |
| 0-5 mA 17 | 70 0~5 mA | 200 | | |
| 0-10 mA | | | | |
| 0-50 mA 0 | ·5 0-50 mA | 0.5 | | |
| 0-100 mA 0 | 5 0-100 mA | 0.5 | | |
| 0-500 mA 0 | 5 0-500 mA | 0.5 | | |
| 0-1 AMP 0 | ·5 0-1 AMP | 0.5 | | |
| 0-2 AMP 0 | 5 0-2 AMP | 0.5 | | |
| 0-25 Volt 15 | K 0-25 Volt | 15K | | |
| 0-50 Volt 50 | K 0-50 Volt | 50 K | | |
| 0-300 Volt 300 | | | | |
| "g" Meter 17 | 70 "g" Meter | 200 | | |
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| SAFETY | ISOL | ATING | ì |
|--------|------|-------|---|
| | | | |

| VA | Ref | Price | Price | Price | |
|---------|-----|-------|---------|-------|------|
| (watts) | No. | Cased | Plugs | Open | Post |
| | | £ | 2 Pin + | £ | £ |
| | | | 1 Earth | | |
| 60 | 149 | 8.35 | 0.88 | 4.87 | 0.5 |
| 100 | 150 | 9.15 | 0.88 | 4-90 | 0.6 |
| 200 | 151 | 11.45 | 0.88 | 8-14 | 0.8 |
| 250 | 152 | 12.90 | 0.88 | 9-80 | 0.8 |
| 350 | 153 | 15.50 | 0-88 | 11.88 | 0.9 |
| 500 | 154 | 17.25 | 0.88 | 18-62 | 1.13 |
| 750 | 155 | 27:10 | 1.10 | 20-59 | O.A |
| 1000 | 156 | 35-40 | 1.10 | 29-15 | O.A |
| 1500 | 157 | 42.00 | 1.10 | 33-37 | O. A |
| 2000 | 158 | 49.75 | 2.64 | 37-10 | O.A |
| 3000 | 159 | 78:15 | 2.64 | 58-55 | O. A |

| 12 | & 24 Yo | its Prim | . 200-240V. | |
|-----|---------|----------|-------------|------|
| A | mps | Ref. | Price | Post |
| 12V | 24V | No. | | 4 |
| 0.3 | 0.15 | 242 | 1.58 | 0.34 |
| 0.5 | 0.25 | 111 | 1.38 | 0.34 |
| 1 | 0.5 | 213 | 1.74 | 0.47 |
| 2 | 1 | 71 | 2.30 | 0.47 |
| 4 | 2 | 18 | 2:96 | 0.56 |
| 6 | 3 | 70 | 4.18 | 0.56 |
| - 8 | 4 | 108 | 4.56 | 0.64 |
| 10 | 5 | 72 | 5-20 | 0.72 |
| 12 | 6 | 116 | 5-51 | 0.72 |
| 16 | 8 | 17 | 7.00 | 0.80 |
| 20 | 10 | 115 | 10-42 | 0.88 |
| 30 | 15 | 187 | 13-25 | 1.01 |
| 40 | 20 | 232 | 14.85 | O.A. |
| 60 | 30 | 226 | 16-83 | O.A. |

| | 30 Y | olts | | |
|---|--------|-----------|--------------|-------------|
| 1 | Prim. | 200-240V. | Sec. 12, 15, | 20, 24, 20V |
| į | Ampe | Ref. | Price | Post |
| | ľ | No. | 4 | |
| | 0.6 | 112 | 1.90 | 0.47 |
| | 1 | 79 | 2.40 | 0.56 |
| | 2 | 3 | 8-50 | 0.56 |
| | 2 3 | 20 | 4-50 | 0.64 |
| | 4 | 21 | 5-15 | 0.72 |
| | 5 | 51 | 6:40 | 0.72 |
| | 6 | 117 | 7.16 | 0.88 |
| | 8 | 88 | 9-55 | 0.95 |
| | 10 | 90 | 0.67 | 0.95 |

AUTO TRANSFORMERS

| | | Price | Price | Price | |
|--------|---------|------------|-----------|-------|-------|
| VA | Ref. | Cased | Plugs | Open | Post. |
| Watte | No. | B | 2 & 3 pin | £ | |
| Tapped | at 115, | 220, 240 1 | Volts | | |
| 20 | 113 | 3.85 | 0.20 | 1.71 | 0.47 |
| Tapped | at 115, | 200, 220, | 240 Volts | | |
| 150 | 4 | 6.38 | 0.20 | 4.13 | 0.56 |
| 200 | 65 | 7-04 | 0.20 | 4.95 | 0.64 |
| 300 | 66 | 8.00 | 0.20 | 5-81 | 0.72 |
| 500 | 67 | 10.99 | 0.20 | 8-85 | 0.88 |
| 750 | 83 | 13.82 | 0.85 | 10.80 | 0.95 |
| 1000 | 84 | 17-27 | 0-85 | 13-68 | 1.13 |
| 1500 | 93 | 21.87 | 0-85 | 18.81 | 0·A |
| 2000 | 95 | 33-11 | 1.60 | 24-25 | 0·A |
| 3000 | 73 | 47-94 | 2.10 | 35.10 | 0·A |
| | | | | | |

| 50 Volts Prim. 200-240V. Sec. 19, 25, 33, 40, 50V. | | | 60 Volts Prim. 230-240♥. Sec. 24, 30, 40, 48. 60V. | | | | |
|--|------------|--------------|---|-----|-------------------|----------------------|----------------------|
| | | | | | | | Amps |
| 0.5 | 102 103 | 2·58 3·48 | 0·47 0·56 | 0.5 | 124 126 | 2·30 3·41 | 0.56 0.56 |
| 2 | 104 | 5.03 | 0.64 | 3 | 127 125 123 | 5·09 7·58 8·75 | 0·72 0·80 0·95 |
| 3 4 | 105 106 | 5-81 7-58 | 0·72 0·88 | 5 | 40 120 | 9 75 11 20 | 0.95 1.01 |

0.95

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| MINIATIDE | AND | EOUIPMENT |
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| MINIAIUNE | AND | EUUIFFIERI |

12:30

18-20

107

118

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| Prim. 240V with screen. | | | | | | |
|-------------------------|---------|----------|----------|------|-------|------|
| Volts | | Milliamp | | Ret. | Price | Post |
| Bec. 1 | Sec. 2 | Sec. 1 | Sec. 2 | No. | | |
| 3-0-3 | | 200 | - | 238 | 1.50 | 0.25 |
| 0-6 | 0-6 | 500 | 500 | 234 | 1.38 | 0.25 |
| 0-6 | 0-6 | 1000 | 1000 | 212 | 1.90 | 0.47 |
| 9-0-9 | _ | 100 | _ | 13 | 1.40 | 0.25 |
| 0-9 | 0-9 | 330 | 330 | 235 | 1.50 | 0.25 |
| 0-8-9 | 0-8-9 | 500 | 500 | 207 | 1.93 | 0.34 |
| 0-8-9 | 0-8-9 | 1000 | 1000 | 208 | 2-75 | 0.47 |
| 15-0-15 | | 40 | | 240 | 1.35 | 0.25 |
| 0-15 | 0-15 | 200 | 200 | 236 | 1 38 | 0.25 |
| 20-0-20 | _ | 30 | _ | 241 | 1.35 | 0.25 |
| 0-20 | 0-20 | 150 | 150 | 237 | 1.88 | 0.25 |
| 0-15-20 | 0-15-20 | 500 | 500 | 205 | 2.78 | 0.56 |
| 0-20 | 0-20 | 300 | 300 | 214 | 1.98 | 0.47 |
| 0-20 | without | 3500 N | O SCREEN | 1116 | 8.30 | 0.84 |
| 20-12-0-12-20 | | 700 (D/C | · - | 221 | 2-20 | 0.47 |
| 0-15-20 | 0-15-20 | 1000 | 1000 | 206 | 3.50 | 0.56 |
| 0-15-27 | 0-15-27 | 500 | 500 | 203 | 8.00 | 0.56 |
| 0-15-27 | 0-15-27 | 1000 | 1000 | 204 | 3.85 | 0.56 |

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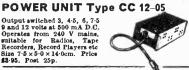
| One Amp | Two Amp | Four Amp | Six Amp |
|----------------------------------|----------------------------------|----------------------------------|----------------------------------|
| 50 P.I.V. 20p | 50 P.I.V. 35p | 100 P.I.V. 55p | 50 P.I.V. 65p |
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1·19 O.A. O.A.

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DEPT PW6, SIMMONDS ROAD, WINCHEAP, CANTERBURY, KENT. Tel: (0227) 52436

INVERTORS for use. Price list sent on receipt of stamped addressed envelope. P.W. AUTOMATIC EMERGENCY SUPPLY 250v—50Hz—150 want invertor with built in battery chargin; in event of power failure switches over automatically from battery charging to invertor operation. Cct. as appeared in Dec, 73.P.W. Complete kit of parts (excluding meter) £22:59 + £1:10 p & p. COMPLETE FLUORESCENT LIGHT INVERTOR KIT 8 watt—12v—Fluorescent light, suitable for tents, caravans, houses, boats and secondary lighting for, factories, hotels etc. 12"—8 watt £2:90 + 25p p & p. 21"—13 watt. £3:30 + 30p p & p. & p. & 21"—13 watt. £3:30 + 30p p & p. & p. & 21"—15 watte. 25 both high volume & amail order capacity available for Mains, R.F., & i.F. Transformers. Before you buy elsewhere let us quote you and see what you save. you save. V.A.T. at 8% Included.

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£8'50 each Stereo pair £16'50 INCLUSIVE OF VAT AND POSTAGE

web europa

P.O. Box 9, Ruthin Clwyd

tuned detector coil option is chosen. It operates by simply mixing the original FM signal and an out-of-phase portion so that the original AM results. A single tuned coil can be aligned by a meter but a double tuned coil can only be set up accurately with aid of a wobbulator to observe the characteristics of the "S" curve while the adjustment is carried out.

A single tuned detector will give 0.5% total harmonic distortion though in practice this is usually only 0.3% with standard broadcast levels. The double tuned circuit gives 0.1% THD when accurately set up. In practice this figure can again be improved to around 0.08% which is rather better than most FM tuners costing over £100 claim in their specification.

Layout is everything with the CA3089E IF amplifier. Deviate from the suggested circuit at your peril since instability can easily be introduced, not easily traced and cured only by revising the track layout until it ceases.

until it couses.

STEREO DECODER

From the detector the audio passes through the mute gate to the stereo decoder (Fig. 3.3). The Kyodo KB4400 (equivalent to the MC1310P) performs the task of decoding a multiplex signal and producing the two discrete channels for power amplification.

Since the various switching signals tend to produce a series of unpleasant waveforms together with the pilot tone at 19kHz and the 38kHz regenerated signal, trouble is removed at source with the Toko pilot tone filter on the module. The block contains two

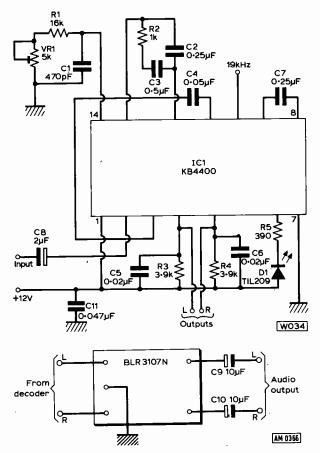


Fig. 3.3: Circuit diagram of the stereo decoder and pilot tone filter.

notches: one at 19kHz and one at 38kHz, plus a lowpass filter with a roll-off commencing at 15kHz which is the upper limit of the multiplex bandwidth. When correctly matched only 1dB will be lost at 15kHz which is not likely to spoil listening enjoyment. If allowed through unattenuated the pilot tone and the residual hash could cause amplifier problems of intermodulation and high frequency instability.

Facilities are provided to switch out the muting and to manually defeat the operation of the stereo decoder. On weak stereo signals intermittent operation of the stereo decoder will cause annoyance if left in the automatic mode.

On switching to AM the same power supply is used for the tuning voltage but it is switched to positive earth system to account for the different orientation of the AM tuning diode block.

The 12V supply is fed to the AM module. Operation of this particular unit has been extensively covered on Part 1 of this series. The quality of the AM section is truly excellent providing a very tolerable partner to the FM section. The purity of the oscillator waveform is good and this results in little interstation noise when tuning the medium wave.

POWER SUPPLY

Two windings are required for the secondary of the transformer to accommodate the different earth requirements for the AM tuning voltage from the rest of the equipment. Rectification is carried out in conventional fashion but the stabilisation and smoothing make use of one of the popular 78 series three terminal regulator ICs. Fig. 3.4 shows the power supply circuit diagram.

The Marconi International Marine Co. Ltd., of Chelmsford, has asked us to point out that there is no connection between the Apollo SSB/General Purposes marine communication receiver manufactured by that company and any receiver described by us in our current Apollo series of articles.

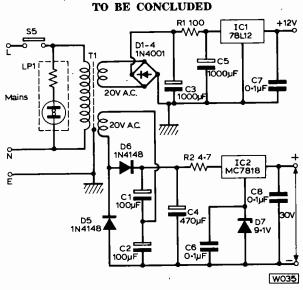


Fig. 3.4: Circuit diagram of the power supply section of the AM|FM Varicap Tuner.



Equally tempered or **Just natural**

In reply to P. G. Quatermain (Letters, P.W. May 1975) may I offer one reason why purists might wince at the idea of an organ tuned to the equally tempered scale?

As Mr. Quatermain points out, notes tuned to the equally tempered scale will sound at a slightly different frequency to those of the Natural or Just scale and he correctly observes that within an octave, these tiny errors will not be noticed. However, the Just scale represents the ratios of frequencies which sound most pleasing to the human ear, so the slight errors which arise through equal temperment are in fact small dissonances; if there were circumstances under which these errors could add, a discordant note might result.

Alan Douglas suggests (Electronic Music Production, Pitman 1973, p 31) that when dealing with pure sine waves, results become dubious after adding waves corresponding to a fundamental and its sixth harmonic. If we are adding complex waves, each with its own harmonic series, the chances of discord are more likely. In the case of the "Easybuild" organ with its limited footages and stop-circuits tending to suppress high harmonics, this problem is likely to be negligible, but when considering a large electronic or pipeorgan, the possibility of discord is very real. Thus intervals are "stretched" away from equal temperament to tune out dissonances the rule being to reconcile purity of the octaves with a concordant

sound. It is in these circumstances that the skill of an experienced organ tuner really counts.

The fact that notes generated by frequency-division cannot be "stretched" has precluded its use in large electronic organs designed for classical or church use. Examination of these instruments reveal that they usually use individually tuned oscillators, for example the Miller Organ, or alternatively pipe organ sounds are somehow recorded, stored and retrieved electronically. The latter system has been brought to a high degree of perfection in the Allen Computer Organ which uses LSI devices to store digitally encoded pipe organ tones.

Nonetheless, now that CMOS frequency dividers and generators are available, construction of a small organ is at last a practical reality even for the beginner in electronics, and Mike Hughes deserves thanks for his clear and thoughtful instructions on the subject.--Thomas Weil (Crovdon).

Ouchⁿ!

The letter from Mr. Rix in the May issue has given me the final prod to write a letter. I have wanted to write for quite some time on the subject of the misuse of certain of the symbols used for the metric system multipliers, namely 'k' and 'm'. As we should all know there is no upper case K used at all, only the lower case k meaning $\times 1,000$. With the M both upper and lower case are in use with the upper case M meaning $\times 1,000,000$, and the lower case m meaning ×1/1,000, respective names are mega and milli.

In a single page advertisement appearing in P.W. one regular advertiser used upper case K no less than 21 times in lieu of lower

In addition we were offered the following interesting items: Grid Dip Meter—to 280 millihertz A.C. millivoltmeter-to 1.2 millihertz

R.F. Generator-to 500 millihertz Portable Radio, MW/LW-600 output megawatt (Rather whacks Mr. Rix!)

L.F. Generator-to 1 millihertz VHF timer—120-160 millihertz P.S.U. 6-9V--300 megamps.

In the current issue, however,

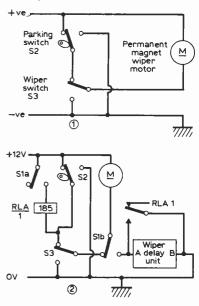
things have improved somewhat. as we have K in place of k only eight times.

Turning now to Mr. Quartermain's letter (also of the May issue) there are two numerical misprints in the third paragraph. Line five should surely read the ratio is 1:1.0594 while line seven should read $1.0594^{12}=2$.—James Livie (Heston).

Car wiper delay modification

With reference to the car wiper delay unit as featured in the May issue of Practical Wireless, I wish to point out that during the last few years permanent wiper motors have been fitted to many cars. These motors are wired up as shown in Fig. 1.

As there were no details in the article concerning fitting the delay unit to this type of motor, I decided to devise a method of my own. The only extra components needed were a miniature relay (12V 1850hm coil) with two pairs of changeover contacts, wired in parallel, and a DPDT switch in place of the one specified, Fig. 2. I find this arrangement works very well and I hope that it will be helpful to other readers.-Colin Robertson (King's Langley, Herts).



All switches and relay contacts shown in the "off" position.

Fig. 1: above, shows the circuit of a perma-

nent magnet car wiper motor, while Fig. 2 shows the connections necessary for the May PW wiper control to be used with this type of motor.

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ON RECENT DEVELOPMENTS

ORGAN CHIP

M USIC lovers and electronic organ tyros can rejoice at the latest offering from Italian-based SGS-Ates, manufacturer of integrated circuits. One of its latest prodigies bears the innocent title of M251. It is claimed to be the first IC ever to integrate bass lines, chords and arpeggios.

You have to actually hear this tiny chip working to appreciate just what it will do. It plays the correct bass notes, the right chord and the right arpeggio accompaniment (if you want it) all in one go, automatically—and it changes key, too.

Having heard this wonder chip, I feel quite sure that organ players of the future will just whisper the tune into a loudspeaker and the organ will reply, "If you can 'um it mate, I'll play it".

D.I.L. SWITCHES

At the Paris Components Show earlier this year many people were exhibiting dual - in - line switches. These seem to be coming on to the market now and could be of use to the amateur constructor who specialises in miniature and sub-miniature projects.

Eight tiny single pole changeover switches can be accommodated in a single 16-pin DIL package with minute switch actuators brought out on top of the case and operated with a rocker action, or at the sides and operated using a slide action. How about a fixed inductance ferrite rod midget radio where you could just switch in (or out) various values of capacitance to tune the stations in?

CHOOSING 'Cs'

Ah, says you, getting exact values of capacitance isn't quite that simple. I can buy a 100pF capacitor, but what if I want an odd value to tune in some station exactly?

Well, you could try using a Vee Cal TrimChip capacitor. It's an adjustable capacitor but its fixed—if you see what I mean? These tiny chip capacitors have a series of minute adjustment points on their sides. By connecting these points in a variety of

configurations, it is possible to vary the capacitive value of the fixed capacitor. The amount by which you can vary the capacitance of individual units ranges from 1pF to 20pF per increment. The components are manufactured to a nominal value. As an example, a capacitor with a base value of 100pF and with ten incremental adjustments can be set to any value between 100pF and 152pF. It can be done by rubbing the sides with a soft lead pencil—readers are left to draw their own conclusions!

Typical size of a Vee Cal TrimChip is 0·18in. long by 0·005in. wide. Experimental kits are available which consist of a selection of TrimChips, a metallic epoxy (for setting the final capacitance instead of using pencil), dispenser and a book of instructions.

GETTING TOUCHY

Another interesting new approach (in practical terms, the idea's been there for some time) was talk by one manufacturer/supplier to market touch-sensitive keyboards for things like electronic calculators. The keyboards are not, as I understand it, capacitive and they do need a very slight "push", however, the force is so small that they could be fairly described as touch sensitive.

The touch causes the plastic film itself to move less than four thousandths of an inch and this is sufficient to cause a switching effect since the plastic film back is metallised. The open circuit resistance is around the $10M\Omega$ mark and claims have been made that the contact resistance is only $0\cdot 1\Omega$. A touching story.

ELECTRONIC PATTERNS

When was the last time you bought yourself a decent dress? (So, why shouldn't lady electronics/radio enthusiasts read Ginsberg?). Think of the processes involved in making a double-knit pattern. Sketches through to finished product. A long business.

Not anymore, though. An Israeli company has brought out a machine which seems to do it all in no time. The designer sits comfortably at the console with a colour display. Here, the sketch can be "sketched" and

colour varied and/or altered until they suit. The input of the whole system relies for its nourishment on an input of nice fresh sketches. It promptly converts these into a digital code. Needless to say there's a computer hidden in the system somewhere which assures that everything happens in the right order.

The system takes only one hour to change a sketch into colour separations and that used to take 150-200 hours before. (The system can also be used to do wallpaper patterns).

KNITTING LIBRARY

How does it automate things still further? Well, the output, in the case of a double-knit pattern, is simply fed to the knitting machines. A "library" of 999 colours is held in the system which gives quite a choice. Ah well—Ginsberg's going to miss his old spinning wheel.

MINI HENRYS

Earlier, we looked at some variable chip capacitors. I see that some miniature variable inductors are now on the US market. There's 37 standard values in the range which goes from 0.001 μ H up to 1,000 μ H—but they're variable, too! A minute threaded core allows a 20% variation from nominal value. But there's still more to come—the size. Each unit measures an almost unbelievable 0·15in. x 0·2in. with a height of 0·16in. It looks as though tweezers and a magnifying glass will become a standard part of the constructor's tool box.

NEW OP AMP

I was interested to hear of the new CA3130 op amp which manufacturers RCA put out. It is an interesting beasty because it combines MOS/FET, bipolar and COS/MOS. The input resistance is $1.5 \times 10^{12}\Omega$ or $1.5 \text{T}\Omega$, and the signal voltage gain is 110dB.



SPECIAL PRODUCT REPORT

GENERAL COVERAGE RECEIVER

HEATHKIT GR-78

THE GR78 is basically a portable receiver for the short wave listener and radio amateur although the medium and part of our long wave band are included. The LW band is particularly useful now that the BBC has taken it into its head to broadcast many sports commentaries on this band only!

One of many interesting features of the set is the provision in the kit of two bandspread scales, one for the amateur bands and the other for the short wave broadcast bands, the constructor using the one of his choice. Since most SWL's eventually turn to the amateur bands in the course of time so the scale could be changed accordingly.

If the idea of a portable receiver conjures up thoughts of piles of dead expensive batteries, forget it! The GR78 has an internal nickel-cadmium battery which is automatically charged from the mains when the set is plugged in but switched OFF, or from an external 12 to 15V DC supply if that is all that is available. The internal battery can be expected to maintain a full charge even if it is used for as much as eight hours daily at average listening levels. No need to worry about overcharging either, since the set can be left plugged into the mains but switched off for as long as a month without the trickle charge facility damaging the battery. A spring-loaded switch on the dial lights helps to reduce the load on the battery.

CIRCUIT DETAILS

The internal telescopic aerial, or external aerial, feeds into a 40673 mosfet RF amplifier stage which has its own gain control. Another 40673 is used in the first mixer which derives its injection voltage from an MPF105 Hartley oscillator operating on signal frequency plus 455kHz on Bands A, B, C and D and minus the IF on Band E. On Band F it operates at 4034kHz higher than the signal frequency when it feeds into a second mixer stage, again using a 40673. The 2N3694 conversion oscillator is crystal controlled on 3579kHz also feeding into the second mixer stage, the output of which is again 455kHz, the IF on the lower frequency bands.

The double IF of 455 and 4034kHz on Band F is designed to reduce the interference from images which can be very troublesome on the higher frequencies when a single IF of 455kHz is used. The change from single to double conversion is achieved automatically with the band switching.

The output of the second mixer IF stage is fed to four 455kHz ceramic filters, eliminating any need for IF alignment. Two 2N3694 IF amplifier stages feed into a 40673 product detector for SSB and CW, another 2N3694 being used in the BFO. On AM a simple diode detector circuit is employed. A portion of the IF signal is fed to an AGC amplifier stage providing two control voltages, for the RF amplifier and the first IF amplifier.

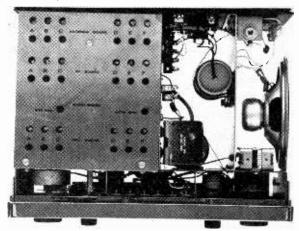
The audio from the PD can be fed direct to the 2N3393 audio pre-amplifier or via a simple automatic noise limiter stage. Another stage of audio precedes the 2N2430/31 complementary pair output stage, feeding either the internal speaker or headphones. The relative signal strength meter is part of the first IF amplifier circuit and is operated by the AGC line voltage.

Instant calibration checks are obtainable from a 500kHz crystal calibrator using a 2N3393, the output being fed into the aerial input circuits.

CONSTRUCTION

Construction is considerably simplified by the use of six boards; one main board for the power supply and certain auxiliary components, a receiver board for the IF stages, etc. and four switch boards for the aerial, RF, mixer and oscillator stages. The only point of criticism is that holes on the switch boards had to be slightly enlarged to take some of the switch tags but this did not take very long to perform.

Installation of the boards and chassis construction proceeds logically with even the smallest nut and bolt being specified as it is used. There is a line sketch of every item used, down to washers, and this is very helpful, even to the experienced constructor, when faced with a shapeless two-lead blob that turns out to be a $300\mu H$ inductor! Where possible components are marked with their part number.



The plate covering the RF and oscillator boards is clearly marked for easy alignment. The capacitor-like object to the left of the speaker is the nickel-cadmium battery.

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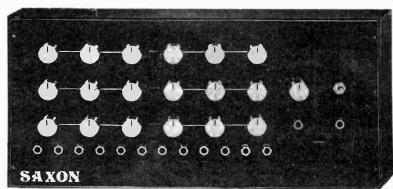
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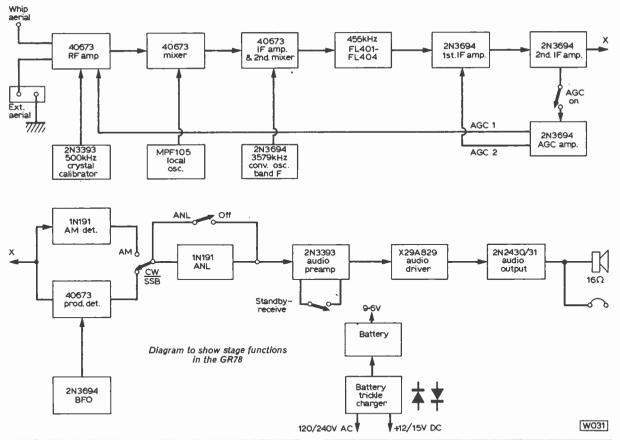
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| Frequency Cover | Band A: Band B: Band C: Band D: Band E: | 200kHz | 1300kHz 3 0MHz 7 5MHz 18 0MHz |
|---------------------------------------|---|----------------------|--|
| Strate-Allie Albita Model Attended to | M | CONTRACTOR OF STREET | SSB |
| Low | High | Low | High |
| End | End | End | End |
| Band A: 10µv | 3,44 | Bpv | 2µv |
| Band B: 3 | Aug 1 | 2 | 0.7 |
| Band C: 3 | 0.6 | 1.5 | 0.4 |
| Band D: 2 | 0.3 | 2 3 | 0.2 |
| Band E: 3 | 0-2 | 3 | 0.2 |
| Band F: 2 * Signal level for 10 | 0·3)dB signal- | plus-noise | |
| Image Rejection | | 65dB or r | |
| | | 60dB or r | |
| \$100 man (1) | | 48dB or r | |
| | | 35dB or r | |
| | Band E: | 25dB or r | nore |
| | Band F: | 35dB or r | nore |
| IF's | Band A t | o E: 455kH | 1z |
| | Band F: 4 | 55kHz and | 4034kHz |
| | - Control of the | | |

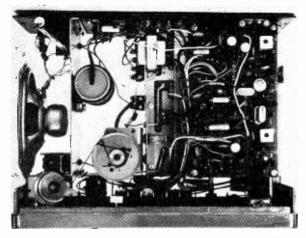
| Audio Output | 300 milliwatts |
|-------------------|--|
| Crystal Calibrato | or 500kHz |
| Meter | Indicates relative signal strength |
| Panel Controls | Bandspread AM-CW/SSB AF Gain-Off AVC-MVC RF Gain ANL-OFF Panel light Bandswitch RCV-STBY Main Tuning CAL |
| Rear Panel | Muting External aerial 12 VDC Receptacle 120/240 VAC Receptacle Phone Jack |
| Battery Drain | 65mA at 50mW audio output 48mA at no audio output |
| Weight | 4·5kg (10ibs) |
| Overall Size | 292mm wide, 160mm high, 230mm deep (11½" x 6½" x 9") |

Transistor identification proved a little difficult with some devices where the marking was completely missing but a few moments with the drawings soon cleared up the identification.

In check lists the colour code is given for each resistor as well as the actual value. The length of every wire that is used is given, cut from the wire provided. Where necessary the length of leads to be left on components is given and even the lead shape where appropriate!

Everything goes together very well, which perhaps is not surprising when one considers the enormous amount of work that has obviously gone into the preparation of the manual. Nevertheless, it is very satisfying when the pile of bits and pieces has dwindled to almost nothing!

The potential builder of this receiver kit needs two things, time, and the ability to wield a small soldering iron successfully. As is usual with Heathkit the accompanying manual gives every step of the construction with many detailed illustrations, some of which are seemingly much too detailed for the step involved. However for the newcomer to kit construction they are invaluable.



In this top view the main circuit board is on the right, main tuning gang just left of centre-bottom linked to the bandspread dial at extreme left.

A frequent worry of the do-it-yourselfer is the subsequent electrical alignment required and the fear that a workshop full of test equipment will be necessary before the fruits of all the labour can be tasted. But no worries need be entertained here. A short list of tests to be carried out with a simple multimeter coupled with a fault-finding chart obviate any serious faults before switching on.

All the coils in the RF and oscillator stages are pre-aligned enabling stations on known frequencies to be quickly located on each band and cross-checked with the integral 500kHz crystal oscillator, in conjunction with the set's relative signal strength meter. If one has access to a signal generator however then advantage can be taken of the full instructions given, enabling the receiver to be aligned to give of its best on all bands.

Having reassured the potential builder of the GR78 kit that he need have no worries about alignment it should be said that he must be prepared to sit down for quite a few evenings, wading through the manual ticking off each step as it is done. Spaces are even provided for the ticks! The biggest mistake is to jump or anticipate any steps and strangely enough, this is more likely to happen with the experienced constructor who thinks he can beat Heathkit to the finish!

Naturally, some previous experience of the construction of electronic equipment is desirable and the GR78 kit is probably best suited to the hobbyist who has had a go at a few simple projects already, and now feels that he is ready for a serious project.

One or two tips as you open the box! Try to find a workspace where the set and tools can be left out as construction progresses and where the many bits and pieces and components can be sorted out and located within easy reach. Do follow all instructions and check all parts as and when directed, especially at the start, before any attempt is made to begin construction, however great the temptation may be! Tidy up after each session and cover over the set and workspace. In this way even short periods of half an hour can be put to good use, the steps completed to date being clearly shown in the manual.

ALIGNMENT

The set was working after the initial series of simple circuit checks had been carried out and the set had been plugged into the mains and left, with the on-off switch at OFF, for 24 hours while the battery was charged. For peace of mind the set was disconnected from the mains while tests and alignment were carried out, and plugged into the mains again between times.

Alignment is conventional, trimmer capacitors at the HF end of each band and coils at the LF end, but as mentioned before, the coils are prealigned and should need little adjustment. As Radio 2 is on 200kHz it was necessary to cheat a bit on Band A (200 to 400kHz) and alter the oscillator coil to bring 200kHz just inside the end of the scale to ensure that it was possible to tune in Radio 2 properly.

Band B covers part of our MW band, the balance being found on Band C and there are plenty of stations here for calibration purposes. Needless to say, the internal 500kHz calibration oscillator is invaluable during alignment especially on the SW bands. Further adjustments include the BFO, calibration oscillator and 5.5MHz trap circuit.

The kit K/GR78 now costs £125 which includes the new rate of VAT at 25%, from Heath (Gloucester) Ltd., Gloucester, GL2 6EE.

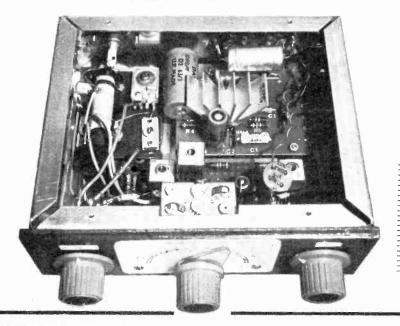
Dw Technicross Uzzle No. 9

presented last month

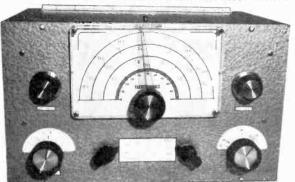




This easily built receiver provides switch selected stations or manual tuning. Three transistors plus a cheap audio module rated at 5 watts out. Suitable for positive or negative earth vehicles. Economical consumption allows optional operation from dry batteries.



Dual ConversionReceiver



A reliable design for the 20, 40, 80 and 160m bands, CW/SSB/AM. Conversion at 5.5MHz and 465kHz reduces second channel interference especially at the higher frequencies.

plus

'IC of the Month' looks at the versatile

TDA 2020 audio IC

ON SALE IN JULY



HE function generator is constructed in a RS instrument case type 4. This case has a very slim front panel, dimensions 432 x 88mm (17 x 3.5in). Whilst this particular case is not essential (any other type would be suitable), it does lend itself to the construction of an instrument having a very modern appearance. This, together with the in-line layout of the switches and the LED indicators make a very functional instrument.

The instrument is constructed in three parts: the front panel; the centre circuit board; and the rear power supply. The front panel accommodates the switches and most of the switched components. The circuit board in the centre contains the 8038 IC, the transistors, and most of the remaining components. The rear panel is utilised for the power supplies, ± 15 volts. An inside view of the general construction was shown last month.

DRILLING

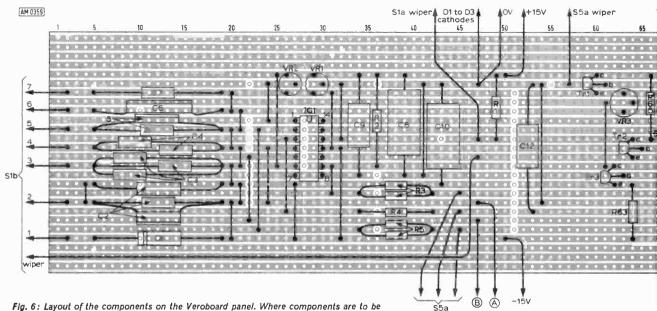
First drill the front and rear panels to take all the necessary components. The front panel is marked with Letraset legends to suit the knobs chosen, then sprayed with a varnish protective.

Fit the four stand-off mountings and screw in the

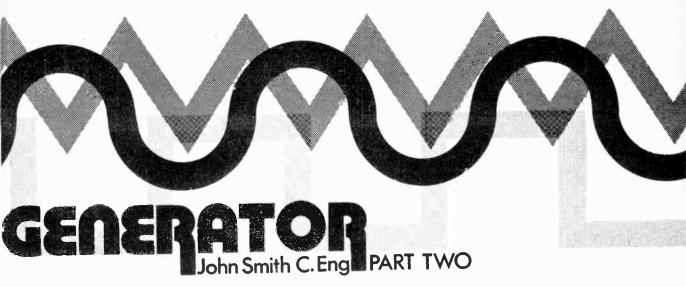
4BA studding which holds the circuit board.

Some switches may necessitate mounting the circuit board further back. Next, fit all the switches and indicators to the front panel then the circuit board must be drilled with 4BA clearance holes to fit the studding and temporarily fitted.

CAUTION The circuit board is long and thin and cannot be used without adequate support. Therefore it is necessary to fit a metal frame around the board. or two metal strips as fitted to the prototype instrument illustrated in Fig. 6. Any convenient metal bars



trimmed it is advisable to use Veropins for mounting. Note that the number of components for a trimmed value may vary from that shown. Note also that there are some variations between the board shown here and that shown in the photographs.



may be used here, with the whole assembly bolted to the 4BA studding. Finally the power supply components are mounted on the rear panel as shown in Fig. 7.

The whole unit is then assembled in the case to ensure that there is adequate clearance for all components. The three parts, front panel, circuit board and rear panel are removed from the case for wiring.

WIRING

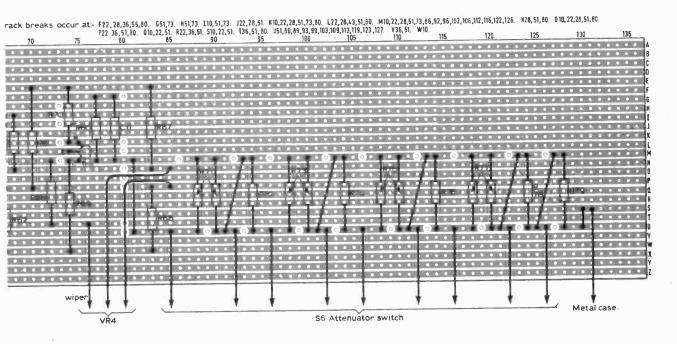
The power supply is wired first as shown in the circuit diagram published in Part 1. Connect the unit to the mains supply and (after checking) switch on. The supply should give ± 15 volts. If it does not it will be due either to faulty wiring or to component failure. However, it is essential to check out the power supply before proceeding further, as any

trouble in this area can damage the very expensive 8038 IC.

It is desirable to check the supply on a load of about 50 mA. This can be accomplished by monitoring the output voltage with a voltmeter and then connecting a resistor of about 330 ohms across the supply to see that the voltage does not change appreciably. It is also worth checking the ripple.

The output voltage need not be precisely 15 volts; the instrument will function quite well on 15 ± 1 volt, but it must be stable and have a low ripple voltage.

The front panel is wired next, fitting all the resistors around switches S3, S4, and S6. Fig. 8 shows the positioning of the switches on the front panel. The components on S2 have to be selected, so R6 and R15 only are temporarily wired into circuit. Of course, readers building option 2 will proceed with the wiring of S2 using the design values.



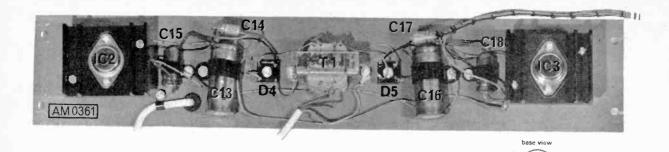


Fig. 7: Layout of the components on the rear panel. The wiring should be completed by referring to the circuit diagram of Fig. 5 in Part 1. Note the polarity of the regulator ICs and the resistor in series with the lead which is hidden behind the heatslink.

CIRCUIT BOARD

The circuit board is wired last. Cut the tracks and fit the components as shown in Fig. 6, with the exception of the components marked "trim" on the circuit diagram. Cl to C7 are not fitted until later, R3 to R5 and R68 are fitted temporarily with the design values. The whole instrument is now wired together with enough spare wire for the component board to lay flat, so that the selected components may be wired to S2 and the capacitors Cl to C7 may be fitted to the component board.

With all the "trim" components it is advantageous to fit a wiring pin onto the circuit board to facilitate removal and rewiring. Carry out a complete and final check of the wiring and the unit is ready to switch on, BUT DO NOT do so until the following instructions have been carried out.

TESTING AND COMPONENT SELECTION

Before starting the test and selection procedures it is necessary to know the function of the selected components. Firstly, frequency is controlled primarily by capacitors Cl to C7, so a high degree of accuracy and stability is necessary here. Resistors R6 to R23 not only control frequency, or period, but also control waveform symmetry. This means that these components must be selected with considerable care, using an oscilloscope to check symmetry.

VR1 and VR2 control the purity of the sine wave signal and must be carefully adjusted at a low frequency. Resistors R3 to R5 control the output voltage of the signal and are adjusted with the aid of an oscilloscope. VR3 and R68 are concerned with the offset control and are also adjusted with the aid of an oscilloscope.

CAPACITOR SELECTION

Before switching on the instrument VR1 and VR2 must be set to the centre of their range. Then fit either C5 3,000pF or C6 300pF; the value chosen will depend upon the accuracy of the oscilloscope used to calibrate the instrument. Range 5 (3,000pF) gives 100μ S to 900μ S. Range 6 gives 10μ S to 90μ S so pick the one most suited to the oscilloscope used and fit that capacitor—1% silver mica or Suflex is recommended.

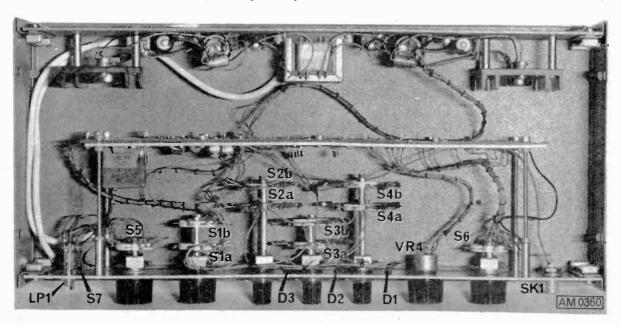


Fig. 8: Layout of the switches and the LEDs on the front panel. Wiring should again be completed by reference to the circuit diagrams in Part 1.

Switch on the instrument, with the range switch set to range 5 or range 6 depending upon which capacitor has been fitted, and set S3 and S4 to zero. Set the DC shift control to the centre of its range, LED B or C should be on. Check that when the range switch is turned from the left (range 7) to the right the LED's go through the sequence (ABCABCA), LED A being the extreme left hand one.

Next, turn the attenuator switch S6 to maximum output and examine the waveform on the coaxial socket. This waveform should be sine, triangle or square as selected by the function switch, ten volts approximately peak amplitude and roughly swinging about zero.

Check that each function gives an output, that the offset control works and the attenuator functions. If any of these facilities do not work there are wiring or component errors or faults which must be corrected before proceeding further.

TRIGGER PULSE

Some oscilloscopes need a trigger pulse to function properly, such a pulse may be obtained from the junction of R2 and R3. This pulse is about 24 volts in amplitude but may be attenuated ($\div 10$ for example), with the aid of a $10k\Omega$ and $1k\Omega$ resistor divider. Some users may consider a trigger output as a useful permanent feature of the function generator, although the prototype shown does not incorporate this feature. Having attended to the trigger pulse, adjusted the oscilloscope and repaired any faults, the calibration procedure may begin.

CALIBRATION

In addition to the oscilloscope a frequency meter is necessary for the highest possible accuracy. If this degree of accuracy is not sought after the instrument may be adjusted to correspond to the oscilloscope time base calibration.

First switch to the triangular waveform and see if the output is asymmetrical as is shown in Fig. 9a. Here the up stroke is shorter than the down stroke. This wave form is made symmetrical by selecting R6 and R15. Shunt each one in turn with a $100 \mathrm{k}\Omega$ resistor to determine which affects the up and the down stroke.

Symmetry is very important because this form of distortion affects both the sine wave purity and the duty cycle of the square wave, see waveforms b and c Fig. 9. Having adjusted R6 and R15 to give a perfectly symmetrical waveform with an upstroke/downstroke time of 50µSec (100µSec period), the frequency must now be corrected.

FREQUENCY CALIBRATION

Before discussing the frequency calibration a few words about procedure: R6 and R15 are selected by fitting series or shunt resistors to correct their value. It is relatively easy to find out what adjustment is needed if one makes use of the other two decade switches S3 and S4. S3 introduces resistance increases of $1k\Omega$ whilst S4 introduces resistance increases of 100Ω . By making use of these two switches the increase or decrease in value can be estimated.

Now switch to sine output and measure the frequency. This should be 10kHz ($100\mu Sec$ period) or 100kHz if range 6 is being used. The use of range 5 will be assumed from now on, so readers who have

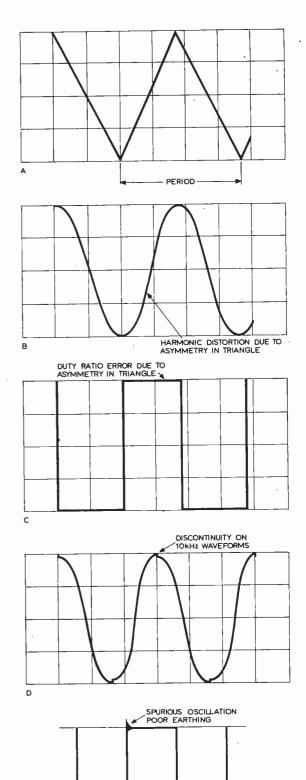


Fig. 9 (a) Asymmetry in the triangular waveform is indicated by a difference in the up and down strokes as shown here (b) Asymmetry in the triangular wave results in a slight flattenning of the sine wave form (c) The mark-space ratio of the square wave will also be asymmetrical (d) If the square and triangular outputs are not earthed discontinuities in the sine wave result (e) poor earthing causes ringing on the square wave.

chosen range 6 must divide period by ten and multiply frequency by 10 whenever they are mentioned. However, it is important to carry out all the calibration on one range if at all possible.

If the frequency meter reads high adjust S3 and S4 until the correct reading is obtained. This shows the value of series resistor needed to correct the frequency. Warning, if more than one step of S3 is necessary (e.g. three steps) fitting $3k\Omega$ in series with both R6 and R15 whilst correcting frequency will also distort symmetry.

In this case it is better to fit values proportional to those already in circuit and re-check to find the final value needed. If on the other hand the frequency were too low R6 and R15 have to be shunted. In this case use S3 and S4 to lower frequency by a corresponding amount to arrive at an estimate of the shunt percentages needed.

All this is rather a long-winded procedure especially as each resistor R6 to R23 must be adjusted, but once the correct procedure is understood it becomes easier with practice. It will take at least a weekend to complete an accurate calibration of this instrument.

SYMMETRY AND PERIOD

Next fit temporarily R7 and R16 ($10k\Omega$). Use the same procedure as before to adjust for symmetry and a period of 200μ Sec. Switch to sine output and adjust frequency to 5kHz. Work through each component on switch 2 in sequence; R8 and R17 gives 300μ Sec (3.3kHz), R9, R18 400μ Sec (2.5kHz), R10, R19 500μ Sec (2.0kHz), R11, R20, 600μ Sec (1.66kHz) R12, R21 700μ Sec (1.43kHz), R13, R22 800μ Sec (1.25kHz) and R14, R23 900μ Sec (1.1kHz).

People who have paid the extra for the 8038BC will find that they have a big advantage during calibration due to the higher accuracy of this unit. For those with suitable instrumentation it is well worth spending time on this calibration procedure because the 8038 is a very stable IC. Temperature stability is 50ppm/°C and as the power supplies are also stabilised the instrument will retain its accuracy. Unfortunately if the 8038 needs replacing at any time the instrument will need recalibration.

RANGE SWITCH

Next the range switch is calibrated. Switch to range 6 and adjust the period switches to 10µSec. Switch to sine output and connect the frequency meter. Fit C6 (300pF), switch on, and check frequency. C6 must be adjusted to give 100kHz. Switch to range 5 and adjust C5 (3,000pF) to give 10kHz (this range has of course already been adjusted). Now proceed with each range: Range 4, C4, 30,000pF adjust frequency to 1kHz; Range 3, C3, 0.3μ F, 100Hz; Range 2, C2, $3 \cdot 0 \mu F$, 10Hz; and Range 1, C1, 30μF, 1Hz. It may be difficult to find a suitable capacitor for range 1; a 15 volt tantalum is recommended although many electrolytics will perform quite well. Finally fit C7. The 8038 will only oscillate up to 1MHz on the square wave output, the other waveforms being of very poor quality. Fit any value between 5pF and 30pF which is capable of giving a useful range of signals.

ADJUSTING SINE PURITY

If the sine wave output is examined on Range 6 it will be seen that it has a high frequency discontinuity, see Fig. 9. This is caused by breakthrough

from the pulse and triangular waveforms. It can be improved by making use of a three pole switch (S5) arranged to short R4 to earth when switched to sine output. It may also be improved by running the sine lead from R5 to S5 separately, or screened from the other function leads.

Discontinuities are made worse by poor earthing. To investigate the earthing, switch to square wave and examine the edges of the waveform. If the edge of the square wave shows oscillations as indicated in Fig. 9e try earthing various parts of the front panel to the Veroboard. Take care to ensure that it is not the oscilloscope giving rise to spurious oscillations on this test.

In practice these oscillations and discontinuities are at a very high frequency and may be ignored providing one is aware of their presence. The final adjustment of sine purity is carried out by switching to Range 5, period $500\mu Secs$ (which is a frequency of 2kHz) and adjusting VR1 and VR2 to give the purest sine wave possible.

This may be carried out using an oscilloscope or it may be adjusted by comparing the waveform with another sine wave. Those able to measure harmonic distortion can adjust for minimum second and third harmonic. Those able to hear distortion may be able to pass the signal through an amplifier and adjust by ear.

ADJUSTING OUTPUT VOLTAGE

Adjust the output voltage to give a ten volt swing on each waveform. This is carried out by checking the output with an oscilloscope and adjusting R3 for the correct square wave amplitude, R4 for the triangular wave amplitude and R5 for the sine wave amplitude. The design values should give a voltage quite close to the swing required.

ADJUSTING OFFSET

Switch to the triangular waveform and set the offset potentiometer VR4 to its centre position (calibrated zero). Examine the waveform on the oscilloscope and adjust VR3 so that the excursion is ± 5 volts. If, due to power supply and component tolerances, VR3 is unable to centralise the waveform, select another value for R68 to give a reasonable degree of control on VR3. Increasing R68 will push the waveform down in a negative direction and decreasing it will push the waveform in a positive direction.

This completes the adjustment and calibration of the instrument which is now ready for use. Fit the instrument into its case and run through all the controls to familiarise yourself with their functions. Examine the DC shift control and attenuator carefully.

These are designed so that the signal can be shifted to all positive, symmetrical about earth, or all negative. This is equally true of all settings of the attenuator. Thus at maximum output the DC shift is ± 5 volts, but if the signal is attenuated to 100 mV the DC shift is ± 50 mV.

In next month's article we shall discuss how to simplify the instrument and mention some of the uses to which it may be put.

GOING BAC

Memories

LESLIE SPENDLA R. from Hampshire tells us that after 50 years it still thrills him to know that he was an on-the-spot witness of the early lead taken by Britain in the field of wireless, with the formation of the British Broadcasting Company and the opening of its first transmitter on medium waves at Savoy Hill in November 1922. A few months after this date, a local advertisement stated that a public demonstration of wireless reception by the Marconi Co. was to be given at the Station Road Garage, Winslow, seven miles from his home in Buckingham.

Mr. Spendla was a schoolboy at the time and he went there with some friends to listen.

To introduce wireless reception and Marconi sets to the public, the company organised tours of the country districts-often setting up their equipment in garages-these eventually becoming their first trade outlets. These garages had only just progressed from the practice of dispensing petrol (Pratts Motor Spirit) from 2-gallon cans.

Two tall white masts in the adjoining field carried an aerial similar to those seen in pictures of an ocean liner-its parallel wires being separated by spreaders at each end.

The open garage doors revealed the sloping desk type receiver, with its row of glowing bright emitters, feeding two large upright horn speakers, with whistles, crackles and mush, as the engineers tuned up in preparation for the opening of the evening programme from the London transmitter some 50 miles away.

Then, over the ether, came the magic voice-"Hello! Hello! This is 2LO calling." This thrilled the crowd as much as if it had come all the way from the moon. In the next few years, Mr. Spendla says he was absorbed by

COLIN RICHES

wireless, moving on to one-, two-

and three-valve sets.

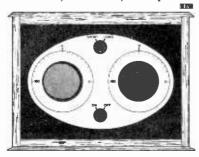
After burning much midnight oil, the success of a DX session on the medium wave in those days was measured by the ability to receive such items as the nightingale from Milan, cuckoo call from Ljubljana, the musical box notes from Budapest (Buda-Pest as it was then), the trumpet call from Krakow, the rapid metronome from Vienna or the slow one from Munich.

Over are the days when people used to have to cycle to a garage in the next town to hear the wonders of that array of Marconi equipment and know-how, heralding the birth of a new science. These 50 years of progress enable the schoolboy of today to carry around in his pocket the means to receive "London" and many other broadcasts at will-Tempus

Attic searcher

R. M. J. DARBY of 266 Canley Road, Coventry, Warwickshire, happened to be searching the loft of an old house when he discovered a receiver like that shown in our

The set has two aerial input terminals, one earth, two speaker



terminals and wires for a 2V l.t. battery, h.t. battery with two positive tappings, and a grid bias battery.

The valves are an Osram H2 triode detector coupled to a P220 Osram output triode through a Cossor transformer. Two dials are marked from 0° to 180° and one is marked 'A' for tuning. The other is designated 'B' for reaction. There is no volume control-just a short/long wave switch and an on/off switch.

The receiver's wooden case has a hinged top lid, and the speaker with its associated transformer is in its own wooden case.

The set works quite well when connected to suitable power supplies-radio 2 and 3 being received at good strength.

If any readers could tell Mr. Darby more about this set, could they please contact him direct.

Avo 1923

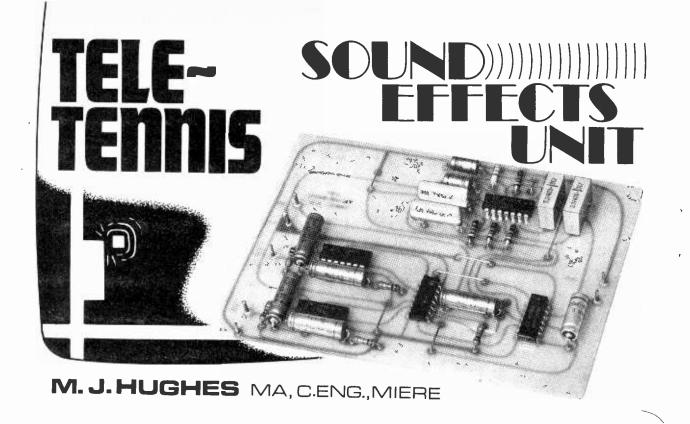


THE year 1973 marked the Golden Jubilee of Avo Limited, the makers of the well-known Avometer.

In 1923 the Automatic Coil Winder and Electrical Equipment Company (as Avo was then known) was formed to manufacture a range of coil-winding machines. Soon afterwards they introduced the first test meter in the world with multi-range facilities. Its picture is shown above.

On the right track

LL Austrian trains in 1926 were equipped with wireless. A fee of 50 groschen (312d. then) was made for a journey of any length.



Increase your enjoyment of the game!

N the original articles describing the construction of our Tele-Tennis game (July to November 1974—reprints of which are still available) reference was made to sound effects, but did not show any circuitry which would provide this function. Since the article first appeared, PW has had numerous requests from readers for a sound effects unit which could be a simple attachment to the unit already constructed.

This article describes a simple, and comparatively cheap, sound effects unit which can be wired into the original game without any wiring modifications being made to the constructed unit. All that is required is access to three signal points and the 0V and +5V rails of the Tele-Tennis game. The whole of the attachment is housed on a single PCB which, with care, could be bolted within the existing case. But, as a loudspeaker is required, most readers might prefer to construct a separate enclosure and take off the five lines from the Tele-Tennis game via a multi-pin plug and socket. This can be positioned in the space provided for the "Video" output of the original game.

SUB-CARRIER

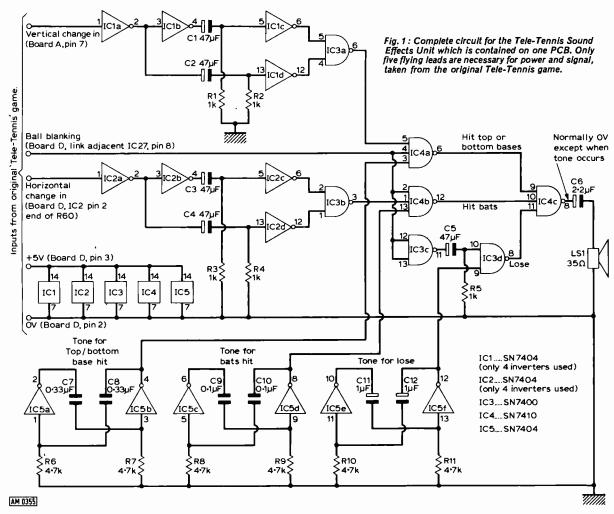
Originally a 6MHz sub-carrier suitably frequency modulated and fed to the modulator of the original game was envisaged. This meant that the sound effects would come from the audio channels of the television receiver to which the game was connected. In principle this is quite easy to do, but in practice

there are quite a few problems in maintaining the sub-carrier stability, and there was complexity enough in handling the video signals through the modulator without having sub-carriers to contend with. Consequently it was decided to go for the simple expedient of a separate loudspeaker. In actual fact there is no difference in the overall cost and there should be no problems in getting this system to work.

CIRCUIT

The complete circuit is shown in Fig. 1. Three sounds are generated by the free-running multivibrators made from the six inverters of IC5. These tones are continuous at the oscillators, but are gated by the logic to give three different pitches of "bleep" when the ball hits the top or bottom bases, bats, or left and right bases. The frequencies of these bleeps can be set by the values of C7 to C12, and in the prototype a rebound off top or bottom base produces a medium pitch, a successful return off the bats produces a high pitch, and contact of the ball with the left and right bases (which constitutes a "Lose") gives a rather rude low frequency "burp"!

The logic is fairly simple to follow if the production of each audio signal is described in turn. First of all, the rebound from top or bottom bases. As those who have already constructed the original game will know, the ball is in motion around the screen all the time, but is only in play when it is brightened up by the Ball Blanking logic. Consequently the only sounds wanted occur while the Ball



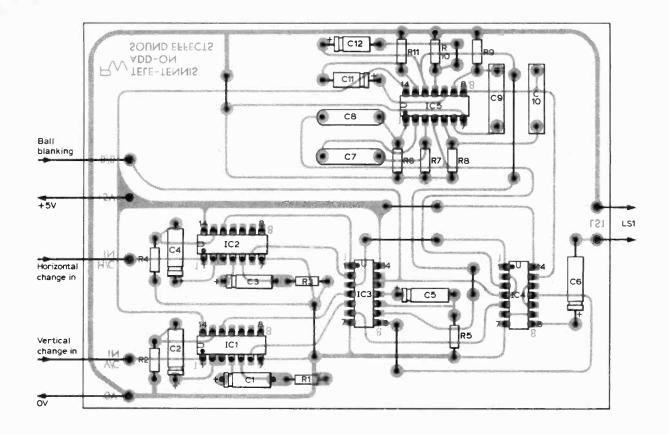
★ components list

| esisto | | | SILVE THE SECTION OF |
|---------|--------------|----------|---|
| RIV 6 | 1812 | R7 | 4-7k() |
| R2 | ſkΩ | R8 | 4·7kΩ |
| R3 | tkΩ | R9 | 4·7kΩ |
| R4 | 1kf2 | R10 | 4 7kD |
| R5 | 1kΩ | R11 | 4-7kΩ |
| R6 | 4·7kΩ | * | W 10% |
| apacit | ors | | |
| Ct | 47µF (6V) | C7 | 0-33µF) |
| C2 | 47µF (6V) | C8 | 0.83 F poly- |
| C3 | 47µF (6V) | C9 | 0.1µF (ester |
| C4 | 47µF (6V) | C10 | 0-1µF |
| C5 | 47 HF (6V) | C11 | 1.0µF (6V) |
| CF | 2-2aF (8V) | C12 | 1.0/LF (6V) |
| tegrat | ted circuits | | 635 |
| JC1 | SN7404 | 1C4 | SN7410 |
| IC2 | SN7404 | IC5 | SN7404 |
| IC3 | SN7400 | | |
| liscell | anegus | | |
| | | Five. 14 | lead DIL socket |
| | | | ay panel mounti |
| | | | th of E-way cab |
| | | | lass PCB, availab |
| | | | oine Road, Twicke |

Blanking signal is at Logic Level "l" (i.e. when the ball appears on the screen). When the ball hits top or bottom base the signal, which in the original game was designated "Vertical Change", alternates from a logical "l" to a "0" and vice versa. This signal is therefore ideal to initiate a bleep for a rebound from the top or bottom bases, and can be produced at pin 7 on Board A.

DIFFERENTIATION

ICla acts as a logic buffer to prevent loading on the original circuitry, so an inverted form of Vertical Change is fed to C2 which differentiates it. Therefore, on the negative going edge of Vertical Change, a positive going pulse (having a width set by the value of C2 and R1) is fed to ICld. The duration of this pulse is a few hundred milliseconds, long enough to give a useful bleep when used to gate the tone oscillator. A pulse like this must be produced for both the positive and negative edges of Vertical Change so that a bleep is produced by a change in either direction. Therefore the signal from ICla is inverted by IClb and is used to carry out the same differentiation operation. IClc and ICld together with IC3a, give an OR function so



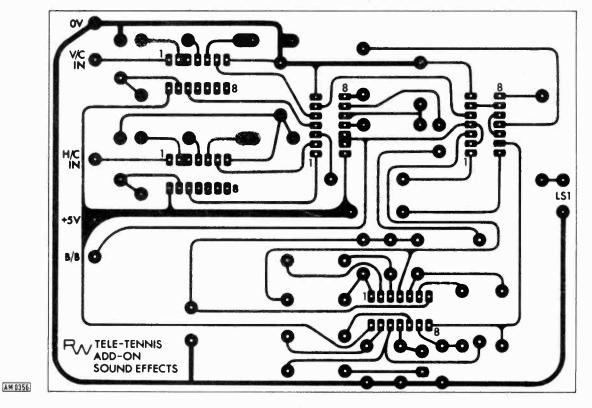


Fig. 2: Top diagram of the PCB gives details of the component layout and flying lead configuration, while the lower drawing shows the foll side only. Both are reproduced full size.

that the output from IC3a will be a positive pulse whenever the ball hits top or bottom base.

This signal is fed to IC4a together with Ball Blanking and the tone from IC5a and IC5b. Provided the ball is bright (i.e. Ball Blanking is "1") the pulse from IC3a will allow the tone to appear at the output of IC4a for the duration of the pulse caused by the contact. This signal is fed to IC4c where it is effectively ORED with the two other signals and fed to the loudspeaker.

A 'GLITCH'

The signal for contact with the bats is produced in exactly the same way except that the Horizontal Change signal is used to initiate it. This signal occurs at pin 2 of IC27 and can be conveniently picked up from the end of R60 going to this pin on board D. A Horizontal Change signal is produced by contact of the ball with either bats or the left and right bases. However, as soon as contact is made with one of the bases, the ball is blanked in a few nanoseconds, and hence the pulse so produced (usually called a "Glitch") is not resolvable as a bleep. The composite stretched pulse, produced by contact of the ball with either bat is fed from IC3b to IC4b, together with Ball Blanking and the tone from IC5c and IC5d. As already mentioned, this signal (the bat hit bleep) is ORED by IC4c before feeding the loudspeaker.

The easiest tone to generate is the rude tone for a lose. It should always occur when the ball is blanked, i.e. on the falling edge of Ball Blanking. Hence Ball Blanking, which is obtained from pin 8 of IC27 on board D, is fed to IC3c which acts as a buffer and an inverter. To gain access to Ball Blanking there is a convenient connection going from pin 8 of IC27 to which a lead can be soldered. The falling edge of Ball Blanking produces a positive-going pulse at the differentiator (C5 and R5) which is used to gate the low frequency from IC5e and IC5f. Some people might like to make the rude tone have a longer duration, in which case the value of C5 can be increased to about $100\mu F$.

It is advisable to use a loudspeaker having an impedance not less than 35Ω , but the prototype has worked on several ranging from 15 to 70Ω without damage to IC4c. Apart from taking note of this point there are not many critical values in the circuit, although the constructor should stick to the recommended resistor values and be within the quite wide tolerances in capacitance values. The prototype board was mounted with spacers, on the bottom of a metal case made to match the original game, with the loudspeaker bolted to the underside of the lid.

CONCLUSION

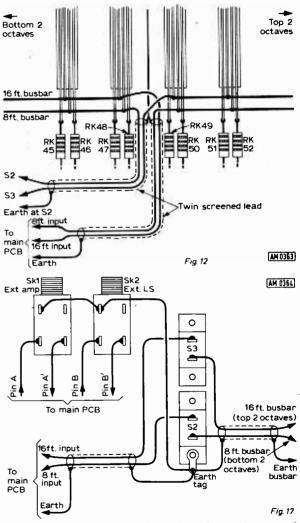
The output volume is not great but is ample for a living room. The unit was demonstrated to visitors at the International Audio Fair in Olympia last year and amongst the cacophony of sounds there, it could be heard over quite a long distance.

Without doubt the addition of this comparatively small extra, livens up the Tele-Tennis game enormously, and those people who have already made the original unit are recommended to try it.

Points arising . . .

PW EASYBUILD ORGAN

It has come to our notice that the 8ft and 16ft pitch switches were reverse connected. Therefore Figs. 12 (May issue) and 17 (June issue) were incorrectly drawn. The corrected drawings are reproduced, in part, below, with the relevant figure numbers.

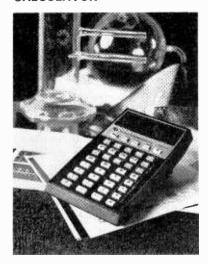


There has been a number of readers who wanted the base connections of the BCY71's used in the Master osc., Vibrato and Tune circuits. Below is shown the lead configuration of this type viewed from the underside.



PRODUCTION LINES colin riches

TEXAS INSTRUMENTS CALCULATOR



A new version of the popular Datamath TI-2500 portable electronic calculator has been announced by Texas Instruments. Model TI-2500 (II) has a percent key and automatic constant in addition to the four basic functions.

Featuring an eight-digit LED display, the TI-2500 (II) weighs less than nine ounces and fits neatly in a pocket, briefcase or purse. With the percent key, problems such as taxes, discounts, and percentage calculations are easily solved.

The automatic constant allows multiplication or division of a series of numbers by one number and addition or subtraction of a constant number to or from a series of numbers.

Operation is either from two "AA" size alkaline batteries or from two nickel-cadmium batteries. Included with the calculator is an AC adapter/charger for use with nickel-cadmium batteries.

The TI-2500(II) electronic calculator is warranted for a period of one year from the original purchase date under normal use and service against defective materials and workmanship. Price is about £30.

Texas Instruments Limited, Manton Lane, Bedford, MK41 7PA

TELE-TENNIS REPRINTS

These are still available from:

Chief Cashier (P.W. Tele-Tennis) IPC Magazines, Tower House, Southampton St., WC2E 9QX. Price is 75p + 7p postage.

12V DRILL

Electroplan Limited, the Royston based distributors of electronic instruments, tools and accessories have introduced a new versatile drill to their range of laboratory bench aids.

Manufactured by EXPO, the 12V operated drill is supplied complete with a full range of accessories which include twist drills, cutting, milling, reaming and grinding tools. Although small, the drill has a high torque with a typical load current between 500mA and 1 Amp.

The chuck rotates at approx. 9000 r.p.m. and has three collets that accommodates the range of accessories

The new handy drill will saw, grind, de-burr, brush and polish with the efficiency of drills that are more expensive and larger in size and yet, is sufficiently small to reach places where a conventional drill could not be used. Price is £19·17 plus VAT. Available same day despatch by post. Electroplan Limited, P.O. Box 19, Orchard Road, Royston SG8 5HH, Herts. Tel: Royston (0763) 41171

TAKING THE MICKEY?

When I first saw the picture of this new Decimo calculator, I wondered if it was a take-on but I've found it's quite genuine and not such a mickeytaking idea as it at first seems!

Known as the Mickey Math, it is a basic four-function, one-chip calculator with green read-out, powered by four pen-cells and with facilities for an external 6V power supply. It's not pocket-sized (unless you're a poacher) as it's 7½in. square, but it's robust and ideal for being stuffed into a school satchel without being damaged.

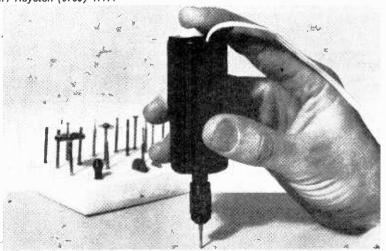
Basically, the Mickey Math is a bit of a gimmick but it's a calculator that should appeal to children and perhaps initiate them into the use of a



calculator—something which will be very useful to them in these days of scientific advancement (rich Dads take note).

At £17.50 plus VAT it's not cheap for what it does but it'll raise a laugh even if people do think you are a bit Goofy using it!

Further gen from Douglas Dorsett, Managing Director, Decimo Limited, Park House, 2/16 Chobham Street, Luton, Beds.



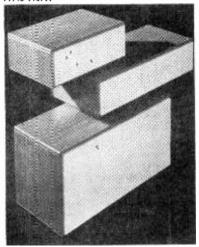
WIRE STRIPPER



The Scotchlok TH 213 tool is a pliers type stripper which operates without adjustment on wires from 0.75 to 6 mm² conductor area $(\frac{1}{32}$ to $\frac{1}{4}$ in²). Quick and easy to use, the tool cuts into the insulation and strips it from the core in one simple action, without risk of damage to solid or stranded conductors. The TH 213 has a spring loaded return action so that it is always ready for immediate use, and has an auxiliary side wire cutter. The 213 wire stripper is 183 mm (71in) long and weighs less than 180 g (approximately 6oz). Further gen from: 3M United Kingdom Limited, 3M House, Wigmore Street, London W1A1ET.

NEW CASES

West Hyde Developments have announced some useful little cases with a woodgrain finish. They come in 13 sizes and prices range from £4·64 (Mod.2-A) to £14·63 (Mod 2L), excluding p.p. and VAT. Further information from West Hyde Developments Limited, Ryefield Crescent, Northwood Hills, Northwood, Middx. HA6 1NN.



BSR DECK

BSR Limited have introduced a new series of belt drive transcription engineered turntables. First in the series is the BDS80. The belt gives almost silent power transmission between the constant speed high-torque motor and the 4lb machined, diecast turntable thereby reducing 'rumble' to an insignificant level.

The BDS80 has a low-mass aluminium tone-arm with a calibrated stylus pressure control. There is provision for full counter-balance adjustment and bias compensation. A viscous cueing device ensures a

feather-like touchdown of the stylus on a record and the head-shell incorporates a slide-in carrier.

A 'click' suppressor and a muting switch are fitted to eliminate the possibility of unwanted noise through the amplifier while the 'set-down' and 'switch-off' are in operation.

The BDS80 comes complete with an ADC K7E cartridge. Mounted in a plinth with cover, the suggested retail price is £41.00. In chassis form, the price is £25.20. BSR Limited, Monarch Works, Cradley Heath, Warley, Worcs., B64 5QH.



NEW LIFE FOR WHARFEDALE

Rank Radio International Limited are offering their dealers a new XP range of speakers carrying the well-known names of Denton, Linton and Glendale. All will have greater power handling and better performance than their predecessors.

These new speakers were introduced to the Company's dealers at it's Hi-Fi Dealer Conference at the Skyline Hotel, Heathrow on 6th April.

The previous Denton 2 (launched in 1967) and Linton 2 (launched in 1965) have each narrowly approached the half million mark in production and have been successfully sold throughout the world. Succeeding these will be the Denton 2XP and Linton 3XP.

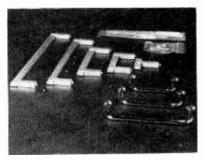
All the three new loudspeakers have been given a new appearance. They can be used with or without their grille cloth which is held in place with simple snap fastenings.

Further information and prices from:—Rank Radio International, PO Box 596, Power Road, Chiswick, London W4 5PW. Tel: 01 994 6491.

VERO HANDLES

Vero (the board makers) are marketing a range of handles which help to give a professional look to items of home-constructed equipment, etc.

In addition to the range of chrome "D" handles, an aluminium panel handle with an attractive anodised finish can now be supplied. Handles are available in various sizes suitable for panels from 1½ in to 10½ in in height. Vero Electronics Ltd., Industrial Estate, Chandler's Ford, Eastleigh, Hants.



- MK2

Sparkrite Mk. 2 is a high performance, high quality capacitive discharge, electronic ignition system in the property of the property of the problems of the contact breaker. There is no mislike because contact breaker bounce is eliminated electronically by a pulse suppression circuit which prevents the unit firing if the points bounce open at high IAP Microsoft of the property of

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continual peak performance.

NOTE—FLEL CONSUMPTION:
The fitting of a Sparkrite Mk. 2 should reduce fuel consumption atthough the amount of the reduction will vary. A fair estimate of the savings which could be expected based on reports by our customers and upon any 4-cylinder vehicle. 10% improvement any 4-cylinder vehicle. 15% improvement any 8-cylinder vehicle. 20% improvement it is worth remembering that while fuel saving is important there are many other advantages to be galred from fitting a Sparkrite ignificancy are

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COLCULOTRICKS

R.STAWICKI

ith ever growing numbers of electronic calculators in use the craze of 'calculatricks' just had to come sconer or later! Imagine the scene—there you are, with a calculator in your hand, thinking of a calculation which will put the electronic wizard to a real tough test, at the same time knowing that the answer will come out instantaneously and correct, up to the last decimal point or will it?

For instance, your calculator will tell you the name of our local barmaid! Try it, as I did. Her phone number 31471, and clearly defined 40, 26, 36 vital statistics were the only data available. Therefore enter 31471+40+26+36 and the result:—

60908

might not mean much to you at first glance but if you turn the calculator upside down the full impact of its hitherto undiscovered potential strikes you and drives you to further tests, and so calculatricks gains another addict.

Want to know what my job is like now? That's easy to work out. I started 12 years ago at a salary of £1,289, but this is now worth only about half. Therefore enter 1289, divide by 2=644·5 and multiply by 12 to find out what my job is like at present. The answer, right enough, is 7734, upside down.

0000

If you use your car travelling 35.5 miles around for a day for 20 working days every month, what should you check?

000

Do you want to find out what could be in my girl-friend's pockets? No names, no telephone exchange given but all data absolutely genuine! We have four known facts on her vital statistics:— B=35, W=24, H=36 and phone number P=4692. Using the formula:

 $(B \times W \times H) + (P \times Workdays/week) + number of known facts).$

Therefore: $(35 \times 24 \times 36) + (4692 \times 5) + 4 =$

60000

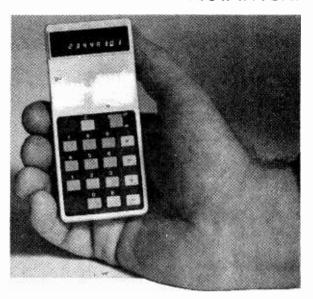
is the answer to your question.

And a topical one? 14215 investors each buy shares worth £469 to buy 5 tankers. So who owns the tankers?

So start by entering 14215469×5, turn it upsidedown and hey presto! You have the answer!

00000000

There must be countless other calculatricks still to be discovered so try it yourself. All you need



is an electronic calculator with an eight-digit capacity and seven-segment type of display.

You have paid 81p for two drinks. Where? simply divide £0.81 by 2 to find out the answer which is

0909

This one is more complicated and shows the planned maintenance points of my car, calculated as follows:

| Engine number | 19249 |
|--|-----------|
| Number of shifts worked | 3 |
| Max. number of days in month | 31 |
| Max. number of months between | service 6 |
| Number of work days per week | 5 |
| Therefore $19249 \times 3 \times 31 \times 6 \times 5 =$ | |

6800000

which indicates the points needing attention.

Sharing the car with your wife? If you drive to work 9 miles and she drives a further $25 \cdot 5$ miles with return journeys that's twice each day for 5 days a week = 10 journeys. The formula is simply $(9 + 25 \cdot 5) \times 10$ and the answer 345 will tell you who should pay for the petrol.

899

Finally a true calculator addict will not count the people at a party. He will count the legs and divide by two. Much more fun that way and always a chance to prove your calculator wrong if Long John Silver comes along. . . . !

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|--------|------|--------|------|----------------|--------------|----------------|--------------|----------|------|
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| DM70 | 0.61 | ECL83 | 0.66 | PC86 | 0.95 | PL84 | 0.68 | 30C15/ | |
| DY51 | 0.80 | ECL86 | 0.64 | PC88 | 0.95 | PL500 | 0.90 | PCF800 | 1.01 |
| DY86/7 | 0.41 | EF80 | 0.42 | PC97 | 0.42 | PL504 | 0.90 | 30C17 | 1.01 |
| DY802 | 0.48 | EF83 | 0.98 | PC900 | 0.57 | PL508 | 1.24 | 30C18/ | |
| EABC80 | 1.03 | EF85 | 0.42 | PCC84 | 0.54 | PL509 | 1.56 | PCF805 | 1.00 |
| EB91 | 0.64 | EF86 | 1.16 | PCC85 | 0 80 | PL802 | 1.40 | 30F5/PF8 | 118 |
| EBC81 | 0.79 | EF89 | 1.14 | PCC88 | 0.86 | PY33 | 0.65 | 00.0,110 | 1.03 |
| EBF80 | 0.58 | EF91 | 1.00 | PCC89 | 0-64 | PY81/800 | 0.49 | 30 FL1/ | |
| EBF83 | 0.59 | EF92 | 1.37 | PCC189 | 0-80 | PY82 | 0.57 | PCE800 | 1.00 |
| EBF89 | 0.53 | EF95 | 1.47 | PCF80 | 0.54 | PY88 | 0.58 | 30FL2 | 0.80 |
| EC86 | 0.73 | EF183 | 0.63 | PCF82 | 1.22 | PY500A | 1 02 | 30FL12 | 1.18 |
| EC88 | 0.76 | EF184 | 0.63 | PCF86 | 0.64 | PY800 | 0 49 | 30FL14 | 1.00 |
| EC90 | 0.86 | EH90 | 0.85 | PCF200 | 1.00 | PY801 | 0.49 | 30L1/PCC | |
| EC97 | 0.60 | EL34 | 0.92 | PCF201 | 1.00 | U26 | 0.88 | 30LI/FO | 0.54 |
| ECC81 | 0.47 | EL36 | 1.01 | PCF801 | 0.64 | U191 | 0.88 | 30L15/ | 0.94 |
| ECC82 | 0.44 | EL81 | 0.85 | PCF802 | 0.70 | U193 | 0.54 | PCC805 | 1.03 |
| ECC83 | 0.47 | | | PCF806 | 0.84 | UABC80 | | 30L17 | 0.89 |
| ECC84 | 9.58 | EL84 | 0.47 | PCH200 | 1.15 | UBC81 UBF89 | 0.71 0.58 | 30P4MR | 1.27 |
| ECC85 | 0.71 | EL85 | 0.85 | PCL82 PCL83 | 0.56 0.64 | UCC85 | 0.59 | 30P4MR | 1.27 |
| ECC88 | 0.84 | EL86 | 0.92 | PCL83 | 0.61 | UCH81 | 1.12 | PC801 | 1.01 |
| ECC189 | 0.68 | EL91 | 0.00 | PCL85 | 0.64 | UCL82 | 0.72 | 30P19/ | 1 01 |
| ECF80 | 0.60 | EL95 | 0.72 | PCL86 | 0.64 | UCL83 | 0.72 | PC802 | 0.89 |
| ECF82 | 0.86 | ELL80 | 2.50 | PCL805/8 | | UF89 | 0.80 | 30PL1/ | |
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| ECH81 | 1.16 | EY86/7 | 0.40 | PD500 | 1.86 | UY85 | 0.54 | 30PL13/ | |
| ECH83 | 0.94 | | | PFL200 | 0.83 | 6/30L2/ | | PCL800 | 1.15 |
| ECH84 | 1.00 | EY88 | 0.72 | PL36 | 0.90 | ECC804 | 0.98 | 30PL14/ | |
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| CCCC | 3/4 | 4 · 7 - 1 0 M | 1 - 5 | 1 . 2 | 0-97 nett |
| Č | 1 | 4 · 7 - 10M | 3 - 2 | 2.5 | 1 92 nett |
| ● MO | 1/2 | 10-1 M | 4 | 3 - 3 | 2·3 nett |
| ww | 1 | 0 · 22 - 0 · 47 \O | 16 | 14 | 11 nett |
| ww | 1 | 0.56-3.9 € | 12 | 10 | ■ nett |
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A UHF WAVEMETER

R. LONGDEN

WAVEMETER is an essential item of equipment required to check the order of multiplication obtained in the various tuned circuits of a transmitter. For example, consider a 144MHz transmitter using an 8MHz oscillator. The oscillator is usually followed by a stage tuned to the third harmonic, to obtain 24MHz. This is followed by a 3x harmonic amplifier, then a doubler, giving 24x3x2, or 144MHz. Wrong tuning could give 2x4 or 4x2 in the early stages, providing 64MHz, doubled to 128MHz. Tuning the PA to this would cause out-of-band operation.

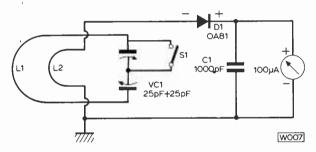
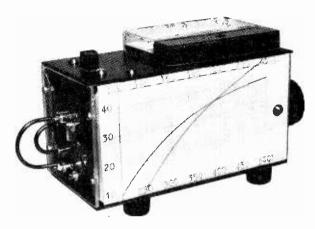


Fig. 1: Simple circuit of the two-range UHF wavemeter.

A calibrated wavemeter will ensure that the output is at 144MHz. It can also be used to check for possible harmonic output on 288MHz, 432MHz, or other related frequencies. A wavemeter is not intended to show the exact frequency, but to indicate that the correct harmonic or band is in use. If a large graph is prepared to show wavemeter dial readings and frequency, good accuracy is obtainable, but a much smaller graph is quite adequate for harmonic and similar checks.

For frequencies above about 300MHz, a very low minimum tuning capacitance is necessary and it becomes difficult to use ordinary plug-in coils,

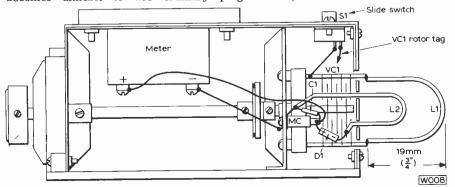


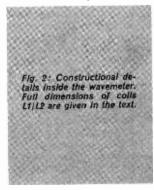
fixed loop L1, but switch S1 allows two ranges to the holder and leads. The circuit in Fig. 1 has a because of the stray capacitance and inductance of be obtained.

For the higher range of approximately 220 to 500MHz, the two sections of the butterfly capacitor VC1 are in series, giving a maximum capacitance of about 12.5pF and a very low minimum. With S1 closed one section of 25pF is in use, and the range is approximately 120-240MHz. VC1 is operated by a small reduction drive. The diode is coupled by the loop L2 to avoid loading L1 and rectification by diode D1 provides current for the $100\mu A$ meter. Resonance is indicated by the maximum meter reading.

CONSTRUCTION

The layout is shown in Fig. 2. The sides of the case are 4×2 in flanged universal chassis members. A further 4×2 in member is cut into two. One part





of this provides the end, on which the ball drive is mounted. The other part is used to mount VC1. The end flanges of the sides are cut off at the ball drive end. The top of the box is paxolin, $4^{1}_{16} \times 2$ in, and cut to take the meter and S1.

Assembly is most easily carried out by fitting together the top, one side, and parts to take VC1 and the drive. A length of \$^1_4\$ in rod fits between the drive and insulated flexible coupling. The shaft of VC1 occupies a clearance hole, and VC1 is fixed by two short 6BA bolts into the "dead" bushes provided. As VC1 spindle is slightly smaller, a piece of tinplate is cut and bent round it to bring it up to about \$^1_4\$ in diameter. Wiring can then be done as in Fig. 2, except for L1 and L2. C1, D1 and the meter lead are anchored at an insulated tag.

* components list

C1 1000pF disc ceramic. D1 OA81.
VC1 25 + 25pF botterfly type (Jackson C713).
M1 Moter, 100µA. Universal coupling.
Drive. (Eagle 1∮in. dia.) Rod ∮in. dia.
Universal chassis members 4 x 2in. (3) (Home Radio).
S1, miniature slide switch.

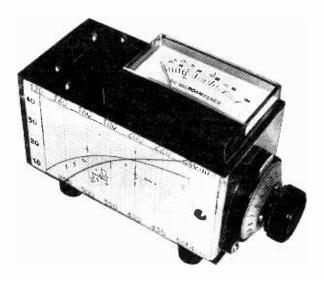
The case end was \$^1_{16}\$in thick Perspex, so that drilling positions can be seen. Clearance holes are drilled for the four studs of VC1. Two holes are also drilled for the ends of L2. About one-half the width is cut off the end flanges of the metal sides members, and these and the end are drilled for four 8BA bolts. L1 is 16swg or other stout wire and is 22mm (\$^7_{6}\$in) across and 19mm (\$^3_{4}\$in) long (Fig. 2). It is soldered to the projecting studs of VC1, near the position for L2. L2 is of similar wire, 13mm (\$^1_{2}\$in) across and projecting about 13mm (\$^1_{2}\$in), with ends long enough to reach the MC tag and D1. When L2 is soldered on, the case bottom can be fixed with self-tapping screws. The dial reads zero with VC1 closed.

USE OF WAVEMETER

The wavemeter loop or coil is positioned so that it can pick up RF energy from the oscillator, amplifier or other coil of the equipment, and the wavemeter is tuned to resonance, as shown by maximum meter indication. The frequency is then found from the wavemeter scale.

Best accuracy is secured when coupling is loose, so that only a small meter indication is obtained. So, as the wavemeter tuning position is found, it is moved away from the RF coil where energy is present. With very low power circuits, close coupling is needed to begin with, inductors or windings in line. Coupling is reduced by moving the wavemeter away, or turning it to place its coil at an angle. Where a few watts of RF may be present, a full-scale reading may be obtained at some inches spacing, so care is needed when first testing any circuit, to avoid possible damage to the meter.

Exactly similar methods are used to couple the wavemeter to a circuit for calibration purposes, except that in this case the frequency will be known already.



CALIBRATION

One or more of several methods can be used. As the final calibration is an important aspect, three methods are described. In each case it is wise to plot a graph showing dial readings against frequency, because this gives intermediate readings, and helps avoid any error as a displaced calibration point is suspect.

As the wavemeter is a passive device, it is always necessary to provide an oscillator or other source of RF energy, even if this is not itself the origin of calibration.

Lecher Line. This can be excited by an oscillator whose frequency is not known, and the frequency found by measurement with a ruler, to calibrate the wavemeter. With care it is usually considered that accuracy can be better than 1%..Fig. 3 shows essential features of the line. It can be made on a board about 130×25mm (5×1in) and 1.85m (6ft) long (actual dimensions are not important). X-X can be a strong tag-strip anchoring the wires about 25mm (1in) to 40mm (1¹2in) apart. An insulated loop about 13mm (12in) in diameter with ends some 50mm (2in) long is soldered on here. The wires can be 20SWG tinnedcopper, 25mm (1in) or more clear of the board. Points Y-Y can be long screws with nuts, so that the wires can be drawn taut. The wires must be parallel. but fixing details at X-X and Y-Y do not influence calibration.

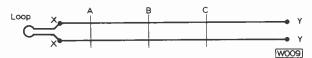


Fig. 3: Arrangement of Lecher line as a means of calibrating wavemeter.

Energy is coupled to the line by positioning the loop near the oscillator inductor. A metal straightedge, at right-angles to the wires, is then slid along in contact with the wires, from X-X. At some point such as A, resonance causes the line to draw power. This is marked. The straight-edge is moved on, until this is repeated, as at B. The distance A to B is then measured. If measured in cm, 15,000/cm=MHz. E.g., 30cm=500MHz, or 60cm=250MHz, and so on.



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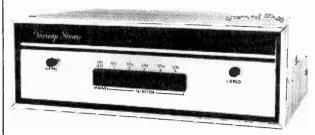
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With low power, resonance with the oscillator is most easily shown by including a meter to show anode or collector current. With the frequency determined, tune the wavemeter to it as described, and mark the graph. The oscillator frequency is then changed, and the procedure repeated for a new point.

Fig. 4 is an oscillator found suitable for up to 500MHz. L1 is three-quarters of a turn 8mm (516in) in diameter soldered directly across TC2. TC1 is a miniature tubular pre-set and though this needs to be near minimum capacitance, oscillation was not obtained without it. The whole is assembled in any convenient form, but with very short leads for RF circuits.

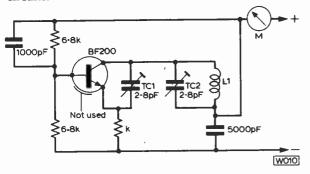
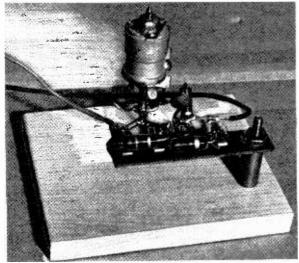


Fig. 4: Circuit of low power oscillator, used as a source of energy at UHF.

Best indication was obtained using a 1mA meter, with the supply voltage reduced for nearly a full-scale reading. Shorting or holding TC2 should cause a drop in current. If not, the circuit is not oscillating.

The line loop is coupled to LI so that a dip can be seen on the meter for two positions of the shorting bar. The line is then removed, and the wavemeter is loosely coupled and tuned to produce the same dip, and its chart marked with the frequency determined by the line.



Layout of Fig. 4 on a simple tag strip. A 9V supply should be adequate.

Use of GDO. If a calibrated grid dip oscillator can be used, the wavemeter can be easily calibrated within the range available on the GDO. Keep GDO and wavemeter separated so that only a small wavemeter reading is obtained on resonance.

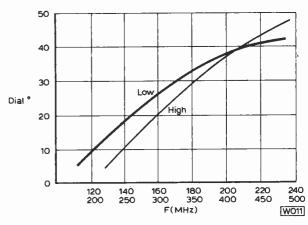
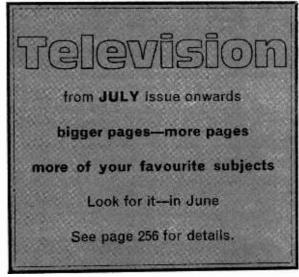


Fig. 5: Typical calibration curves for the two ranges on the wavemeter

Transmitter Harmonics. A 2m transmitter will provide a 144MHz calibration mark. With some circuits, second and other harmonics of this or other frequencies may be found. With a transmitter such as the 10 watt one for 2m (PW, October 1973) where RF is generated at 72MHz and followed by three circuits tuned to 144MHz, it may prove impossible to find any harmonic or spurious frequencies, in normal operation, with the wavemeter. Some calibration marks can be obtained by temporarily changing the doubler anode coil for operation on a higher harmonic. HT is reduced so that doubler current cannot exceed some 30-40mA at 200V or so. The PA is removed or similarly kept within its anode dissipation rating, and can be operated as a doubler for this purpose.

Fig. 5 is a guide on what to expect when calibrating the circuit in Fig. 1. A larger graph on graph paper is recommended. Calibration was done using a tunable oscillator, Lecher line, and harmonics.





AMATEUR BANDS

by Eric Dowdeswell G4AR

S this copy is being bashed out there will be many hundreds of likely candidates around the country doing their utmost to put on to paper their answers to a few technical questions which, they hope, will result in a 'pass' slip for the Radio Amateurs Examination coming through the post in a couple of months' time. One of the best articles I have ever seen on the subject appeared in Radio Communication for April, entitled "Taking the Radio Amateurs' Examination", by R. G. Marden G3MWF.

Strangely enough, it wasn't technical but it did show how to approach the examination on strictly commonsense lines thus giving a candidate an edge over those who arrive at the examination centre hot and bothered, without pens or pencils and without the faintest idea of how they are going to tackle the questions. I have invigilated at many of these exams and I can tell you it has broken my heart to see the way that some candidates have gone about their task. I would say that the vast majority had sufficient knowledge to pass but many made a complete hash of the written work, entirely through lack of preparation.

Frankly, the amount of technical knowledge required is pretty small and the papers are so similar every time that it doesn't take a genius to assess just what is wanted and to concentrate on learning the essentials. Like any other examination, find out what the questioner wants to know and give it to him, without any frills. And the most important piece of advice, as underlined by Mr. Marden: regardless of having finished the paper or not spend at least ten minutes at the end reading your answers and making corrections, and there will be some, I assure you, and these could make all the difference between a pass and a fail.

Obviously many of you enjoyed copying lots of nice new prefixes in the CQ WPX Contest, some of which were pretty easy to fix but others like XX for CR(6) were not so obvious. Steve Blake (Aylesbury) logged some, such as CVOZ, CQ7AZ and PW4. Steve is improving his 2m rig by changing his ground-plane for two five-element quads at around 40ft. Mark Corrigan (New Zealand) sent a brief first log but the only ones of possible interest were G8PO and G3WMZ on 80m SSB. Mark has a Heathkit SW717 and ATU with 100ft wire and dipole for

20m. Paul Heath of Wolverhampton did well with his 1155 set to get VQ9M on 80m SSB and the address for QSL's is Box 191 Mahé, Seychelles. Paul also mentioned OA4S/P/4X of the UN contingent on the Golan Heights, which must be a DX'ers dream QTH judging by the TV coverage we have seen of those parts! Mike Green (Northwich, Cheshire) has not been very active but managed to spend some time in the WPX contest when he captured PJ9UA, VP5B, 3B6DW, among many others on 15m which confirms my long-held theory that it's lack of activity rather than bad conditions that turns people against this band and 10m.

Ian Moore (Leeds) turned in a very brief log for 20m that included YN1WB, a prefix not heard all that often. Paul Barker (Sunderland) reports little doing on the SSTV frequencies apart from usual Italians and a few other Europeans. He notes 5L9A, yet another recent prefix, in place of the perfectly respectable EL series! Excuse this time, 10th anni-

versary of the President!

Stephen Budd A8713 (Worthing) was kind enough to send me a copy of the Geoff Watts DX News Sheet which is the place to get all the gen on these new calls as they come up. The cost is modest and it is posted out every Tuesday. Can't be more up to date than that! Details from Geoff at 62 Belmont Road, Norwich NR7 0PU. On his FRDX400 Stephen has found Asia open from 14 to 1600 and the Pacific from 07 to 0800. Tim Charles (Colchester) thought chess players might be interested in the net on 3798kHz around 1700 every evening. He says G3ZYY claims to have worked ZL3RB on Top Band again, 449 both ways. Tim is one of our few stalwarts who actually enjoys listening to the CW ends of the bands. More should try it as it can be very rewarding.

M. J. Connolly A8796 (Yeovil) stuck to 20m SSB trying out an ATU he has now completed. Paul Heath, again, had to think quick when he lost a vital guy wire from his mast but saved the day by using one if his dipoles in lieu! John Porter (Baslow, Derbys) used his FR50B and two multiband dipoles to drag in stations on 80, 20 and 15m and was pleased to copy VE8RCS of the Polar Amateur Radio Club in the North West Territories, this at 1040 in the morning!

Log extracts

S. Blake:—20m CV0Z VP5B ZY5YZ 15m CQ6LF FH8CY PW4KL ZZ8JO.

M. Green:—80m YB0ABV 40m CR4BC HC2BV HZ1AB 9Y4VU 20m FK8CA PJ9EE YS1JWD ZF1MA 3C1AGD (Expedition to Equat. Guinea by SM0ATD) 15m CW3BH PW4FL 3B6DW.

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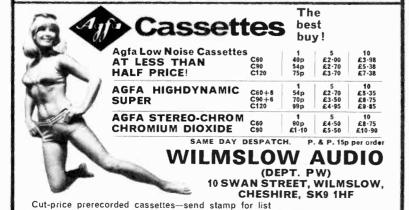
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M, Connolly:—20m A6XR HR3JJR OA42/P/4X VP2AA YS1GMV 3D6AW 6Y5DA 9M2CX.

P. Heath:—80m EA6CE KZ5BC PJ3HM VQ9M ZL4KF 20m VE8DC VP5B OA4S/P/4X.

J. Porter:—80m FC2CD HZ1AB ZB2A 20m PZ3EVK VE8RCS 8P6CC 15m LU9CV ZD7FT ZP5NP.

All stations are SSB except those in bold which are CW.



SHORT WAVE BROADCASTS by Derek Bell

HOPPED over to the other side of the fence recently and went to the North Midlands mobile radio rally at Drayton Manor Park. There I chanced upon three youngsters bent on forming a DX club in the Birmingham area. So in response to their plea for help I would ask anyone interested to write to **Tony Fenton**, 124 Wolverhampton Road, Oldbury, Warley, West Midlands B68 0LW and help them get it off the ground.

Another cry for help comes from **Dave Evered** of Cardiff, he is another of these lucky people who has managed to pick up a communications receiver for a few pence. He would like anyone who can supply any literature or gen on an Eddystone S640 to write to him at 13 Daviot Street, Roath, Cardiff. Dave also wants to know the best frequency for the BBC World Service here in the UK. This is on the Medium Waves in Charles Molloy land, on 1088kHz, radiated from Crowborough. SINPO, by the way Dave, stands for Strength, Interference, Noise, Propagation and Overall Readability. These are ways of measuring a strongest, 0 weakest, and most stations like to have SINPO ratings on QSL requests.

Tony Rowland from Glorious Devon writes with a beef, and that is because he has waited since November for his 1975 World Radio and TV Handbook. Tony, I am afraid that I had to wait almost as long, and in the end the book came by post from Denmark. Can anyone help Tony identify "Radio Carlos" heard on 5050 at 2245, the programme content was news, documentary items and music, so let us know folks if any of you can pinpoint this station. An answer now to a recent "crie de coeur" comes from Lawrence Bennett of Bristol. He provides the info that the station RTV Dominicana has an outlet on 9505 and that Radio Messiah comes from Radio Luxembourg transmitters on 6090. Lawrence sends quite a list of Latin American "goodies," heard on an Astrad 17, among them the following:

11700 Radio Clarin Dominica at 2255 11925 Radio Bandierentes at 2200 11805 Radio Globo Brazil at 2230

15135 Radio Record Brazil at 2135.

Andrew Cope of Southport also fills us in on RTV Dominicana and he says it is a 50 kilowatter using the callsign HISD and is best heard around 0215 to 0230. Andrew recommends very highly his ex-army A510 this being fed by an ATU. It also has a unique earthing system in that Andrew has installed in the ground three large dog meat tins and from these a spider's web of 18SWG copper wire, this is all connected to the set by another length of copper wire!

More unusual happenings are reported by Robert Hill of Crewe. These come from the sunny Algarve in Portugal where Robert has been on holiday. It seems that while listening to the Portuguese domestic radio which, Robert says, is controlled by the military, the transmitter signed off with, of all things, the march "A life on the ocean wave"! Has any one else a funny story to tell us? From Kettering, QTH of Peter Bowyer comes the question "how can I fit a bandspread capacitor." Well, Peter, I cannot of course speak on your Murphy A168 simply because I do not know the set but the basic theory is that you fix a variable capacitor to the chassis in such a position that the capacitor spindle protrudes through the set "box," then connect it to the chassis of the existing tuner and to the fixed vanes of the oscillator tuning capacitor, Vague, I know, but there it is, there is never a way of doing anything that is common to every set except perhaps fitting a valve or making a soldered joint.

Jonathon Marks of Norwich has an item for all those fans of Radio Canada. He writes to say that RCI have changed their OSL policy and now cease to put date time and frequency details on the card, and, as Jonathon says, have made it like the BBC acknowledgement card. I am sure we wish a "get well soon" to our old mate James Walker of Milton Keynes. He has been in hospital for a month and has taken the trouble to drop a few lines to the column. James passes on the tip that Radio Bucharest has in its DX show on Thursdays at 1300 on 15250, 11940 and 9690 a short item for radio amateurs. Robert Gibson of Wadhurst asks if it is worth while fitting a preselector. This gadget is an RF amplifier, tunable over the SW bands, and has the job of boosting the signal that comes from the aerial and feeding it into the set. Unfortunately it also boosts the noise as well. However despite my saying this they are undoubtedly a very useful tool especially to anyone who is in an area of weak radio signals.

I recently cast an eye over the latest copy of



"Communication" the journal of the newly formed Twickenham DX Club. The editor, namely Dave Kenny of 37a Popes Grove, Twickenham gave me permission to quote the fact that one of their members reported Radio Omdurman in the Sudan at 1655 on 11835. This is a 120 kilowatter and is very rarely reported. The service is for Sudanese people abroad and is only on for one hour a day from 1800 to 1900 except Saturday, when it changes to 1900 to 2000, so no wonder it is a rarity.

That, I am afraid, draws the meeting to a close, a very heavy post bag this month for the space allowed so apologies if you were left out and 73s to you and yours.

MEDIUM WAVE DX

by CHARLES MOLLOY

TOKE-ON-TRENT listener Christopher Owens uses a Bush BP12 receiver when DXing on the medium waves. His transatlantic successes are WNBC in New York City on 660kHz at 0115, CJON St John's Newfoundland on 930kHz at 0145, WBZ in Boston on 1030kHz at 0150, CBA Moncton New Brunswick on 1030kHz at 0205. Other catches are Radio Algiers on 251kHz on the long waves (this station has a daily programme in English at 1900 GMT), Dakar in Senegal, West Africa on 764kHz carrying an international programme at 0130, Agadir in Morocco on 935kHz at 0030 and the Voice of Tangiers on 1232kHz at 0040.

An excellent log of Latin American DX heard between 0200 and 0300 GMT comes from Alfred Johnson of London. Among the more notable are HJND Radio Nacional, Bogota in Colombia on 570kHz, HJHJ Radio Libertad, Barranquilla Colombia on 600kHz, YVLH Radio Giradot, Maracay in Venezuela on 650kHz, YVLL Radio Rumbos, Caracas in Venezuela 670kHz, HJCX Radio Sutatenza, Cali on 700kHz, YVKY Radio Capital, Caracas 710kHz, HJDK La Voz de Antioquia, Medellin 750kHz, YVQQ Radio Puerto La Cruz 760kHz, PJB Trans World Radio Bonaire, Netherlands Antilles 800kHz, HJCY Radio Sutatenza Bogota 810kHz, HJKC Emissora Nuevo Mundo, Bogota 850kHz, PRA3 Radio Mundial, Rio de Janeiro Brasil on 860kHz, Radio Jornal do Brasil on 940kHz, HJHN Radio Sutatenza, Magangue 960kHz, YVTB Exitos 980 in Maracaibo 980kHz, Radio Margarita, La Asuncion 1020kHz, PRE3 Radio Globo in Rio de Janeiro on 1180kHz, YVMN Radio Coro 1210kHz and ZYD74 Radio Tupi, Rio de Janeiro on 1280kHz. Latin Americans are usually at their best here in the UK in summer. Listen during the hour before sunrise for Brazilian stations which peak up at this time, such as Radio Jornal on 940kHz, Radio Nacional 980kHz and Radio Globo 1180kHz all in Rio de Janeiro and Radio Record 1000kHz, Radio Tupi 1040kHz and Radio Nacional 1100kHz in Sao Paulo.

Steve Whitt, who is a recent convert to the medium waves, reports again from London. His shack is equipped with an 8 valve Chapman 6BS

communications receiver with the Practical Wireless Audio Processor Unit and his 40ft L shaped aerial strung between three chimneys at 30ft above ground level is connected to the receiver via the PW Aerial Tuning Unit. DX reported includes Sud Radio Andorra on 818kHz, CJON St John's on 930kHz and CBA Moncton on 1070kHz. Steve is building the Practical Wireless medium wave loop aerial including the FET balanced preamplifier.

Dr H. S. Brodribb (St Leonards-on-Sea) asks for information about the ITU LF/MF Conference which was held in Geneva last October. The recommendations made would maintain the 9kHz channel spacing in the European Area but would start at 531kHz instead of 539kHz as at present. This 9kHz spacing is useful to the medium wave DXer since stations in other parts of the world are spaced on multiples of 10kHz and consequently there are parts of the band where DX can be found between European stations. Listen at sunset for Rivadh in Saudi Arabia on 587kHz, Baghdad on 760kHz, Teheran on 1326kHz, Gorgan Iran on 1426kHz, Kuwait 1345kHz, Kirkuk in Iraq on 1360kHz, Ahwaz in Iran on 1390kHz and Dubai in the Persian Gulf on 1480kHz.

An unusual broadcaster can be found on 1095kHz during the evening. This is Radio Bayrak located in the Turkish held part of Cyprus. Heard by the writer at 2030 GMT with Turkish music, on a Marconi Mercury communications receiver and a 90ft outdoor aerial.

BROADCAST BANDS

Short Wave Reports by the 15th of the month to Derek Bell, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD. Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.

AMATEUR BANDS

Logs covering any amateur band/s in band/ alphabetical order by the middle of the month to Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey, KT21

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... numerous issue of P.W. from 1959 to 1973.—R. A. Miller, 7 Woodrow Court, Melbourne Road, London, N.17.
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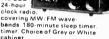
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| 5128: 85 X 64 | HIDATI | | | | | |
|---------------|--------|-------|--------------|---|------|-------|
| 50uA | | £4.21 | | | | |
| 100u A | | £4.16 | - | | _ | _ |
| 200u A | | £4.10 | 1 | | dan. | 1 |
| 500u A | | €4.05 | and the same | | - | · 1 |
| 50-0-50u A | | £4.16 | | A | | |
| 100-0-100u A | | €4.10 | 1000 | | | - 1 |
| 1mA | | €4.05 | | - | | |
| 5mA | | €4.05 | | | | |
| 10mA | | £4.05 | 100 | | | |
| 50mA | | £4.05 | 10V DC | | | €4.05 |
| 100mA | | £4.05 | 20V DC | | | £4.05 |
| 500mA | | £4.05 | 50V DC | | | €4.05 |
| 1A DC | | £4.05 | 300V DC | | | £4.05 |
| 5A DC | | £4.06 | 1EV AC | | | €4.16 |
| 10A DC | | £4.05 | 300V AC | | | €4.16 |
| 5V DC | :- | £4.05 | VJ Meter | | | €5.00 |

CLEAR PLASTIC MODEL SW100

| 50uA 100uA 500uA 50-0-50uA | £5.08 £4.97 £4.75 £4.97 | A |
|-------------------------------------|----------------------------------|---------------------------------|
| 100-0-100uA 1mA | £4.91 £4.75 | NAME OF TAXABLE |
| 1A DC 5A DC | £4.75 £4.76 | 160V AC £4.91 |
| 20V DC 50V DC 300V DC | £4.75 £4.75 £4.75 | 300V AC £4.91 VU Meter £6.25 |
| | _ | |

EDGWISE MODEL PE70 Size: 90 x 34mm

| 50uA | | €4.59 |
|------------|-----|-------|
| 100uA | | €4.54 |
| 200uA | | €4.48 |
| 500u A | •• | £4.32 |
| 50-0-50uA | | €4.53 |
| 100-0-100u | Α., | £4.48 |
| 1mA | | £4.27 |
| 300V AC | | £4.37 |
| VU Meter | | £5.50 |
| | | |



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A range of high quality moving coil instruments ideal for school experi-ments and other bench applications. 3" mirror scale. The meter move-ment is easily accessible to demonstrate internal working.



| 50uA ., ., ., | €9.40 | 1000 | |
|---------------|----------------|------------------|-------|
| 100uA | €8.75 | | _ |
| 50-0-50uA | €8.75 | 2014 D.O | |
| 1mA | £8.42 | 20V DC 50V DC | £8.42 |
| 1-0-1mA | £8.42 | 300V DC | €8.42 |
| 1A DC | £8.42 | 500mA/5A DC | €9.50 |
| 5A DC | £8.42 £8.42 | 5V/50V DC | €9.50 |
| 5V DC | £8.42 | 5V/15V DC | €9.50 |
| 15V DC | £8.42 | 1/5A DC | £9.50 |
| 194 PC | 10.92 | | |

CLEAR PLASTIC MODEL MR 85P Size: 120 x 110mm 50uA £6.05

| 100uA | | ** | €5.99 |
|----------|------|-------|-------|
| 200u A | | | €5.94 |
| 500uA | | | €5.83 |
| 50-0-50u | Α | | €5.99 |
| 100-0-10 | Ou/ | A | €5.94 |
| 500-0-50 | Ou A | Α | €5.78 |
| 1mA | | | €5.78 |
| 1-0-1mA | | | €5.78 |
| 5mA | ••• | | |
| | ** | • • • | £5.78 |
| 10m A | ** | ** | £5.78 |
| 50mA | | | €5.78 |
| 100mA | | | €6.78 |
| 500mA | | | €5.78 |
| 1A DC | | | £5.78 |
| 5A DC | | | £5.78 |
| 15A DC | ** | •• | |
| | •• | ** | £5.78 |
| 30A DC | | | £5.99 |
| 10V DC | ** | | £6.78 |
| 20V DC | | | €5.78 |
| 50V DC | | | €5.78 |
| 150V DC | | | €5.78 |
| | | | |



| 8 | THE REAL PROPERTY. | | - | and the |
|---|--------------------|-----|----|---------|
| 8 | | | | _ |
| 8 | | | | |
| 8 | 300A DC | | | £5.8 |
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| 8 | S Meter 1 | mA. | | £5.71 |
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| 8 | 5A AC | | | £5.71 |
| В | 10A AC | | | €6.71 |
| Ř | 20iA AC | | | €5.74 |
| R | 30A AC | | ٠. | €5.74 |
| | | | | |

*Items with asterisk are Moving Iron type, all others are Moving Coil

CLEAR PLASTIC MODEL SD830

| Size: 110 x l | 33mr | n | | | |
|---------------|------|-------|----------|--------------------|-------|
| 50uA | | £475 | - | | |
| 100uA | | £4.70 | | 1.11 | - |
| 200u A | | £4 64 | Nation . | to be seemed about | |
| 500uA | | €4 59 | | | - |
| 50-0-50u A | | €4 70 | | A | |
| 100-0-100u A | ١ | £4 64 | 15.11 | - | - 1 |
| 1mA | | £4 54 | | | |
| 5mA | | £4.54 | | | - |
| 10mA | | €4.54 | | | |
| 50mA | | £4 54 | 10V DC | | €4.54 |
| 100mA | | £4.54 | 20V DC | | £4.54 |
| 500mA | | £4 54 | 50V DC | | £4.54 |
| 1A DC | | £4.54 | 300V DC | | €4.54 |
| 5A DC | | £4 54 | 15V AC | | £4.64 |
| 10A DC | | £4 54 | 300V AC | | €4.64 |
| 5V DC | | £4 54 | VU Meter | | €5.63 |
| | | | | | |

CLEAR PLASTIC MODEL MR 45P

| 2156: 20 : | K 54 | Jmn | 3 | |
|------------|------|-----|-------|-------------|
| 50uA | ٠. | | £4 56 | |
| 100u A | | | £3.51 | (mm |
| 200u A | | | £3.46 | 6/3 |
| 500u A | | | £3 35 | 1.3650 |
| 50-0-50u | | | £3.61 | 140 |
| 100-0-10 | 0u / | ۱ | £3 46 | 1000 |
| 500-0-50 | Ou A | ۱ | £3 29 | 100 |
| 1mA | | | £3 29 | Direction 1 |
| 5mA | | | €3.29 | 10111111 |
| 10mA | | | €3.29 | 1011111 |
| 50mA | | | £3.29 | CHILIP |
| 100mA | | | £3 29 | - |
| 500m A | | | £3.29 | 300V AC . |
| 1A DC | | | £3.29 | S Meter 1m |
| 5A DC | | | £3.29 | VU Meter. |
| 10V DC | | | £3.29 | 1A AC . |
| 20V DC | | | 63.20 | EA AC |



CLEAR PLASTIC MODEL MR 38P

| 50uA | | . £3,46 | | |
|----------|------|---------|-------------|------|
| 100uA | | €3.40 | 7.3 | -00 |
| 200u A | | £3.35 | 100000 | - |
| 500u A | | | See mm | 50.5 |
| 50-0-50u | Α . | | 100 | |
| 100-0-10 | Ou A | €3.35 | | |
| 500-0-60 | OuA | €3.08 | | |
| 1mA | | | | _ |
| 1-0-1mA | | | 0.010 | |
| 2mA | | | 0.000 | |
| 5mA | | | ELIH SA | |
| 10mA | | | 4 | |
| 20mA | | | | |
| 50mA | | | 201.00 | _ |
| 100mA | | | 20V DC | £ |
| 150mA | | | 50V DC | £: |
| 200mA | | | 100V DC | £ |
| 300mA | | | 150V DC | £ |
| 500mA | | | 300V DC | £ |
| | | | 500V DC | €: |
| 750mA | | | 750V DC | £ |
| 1A DC | | £3.08 | 15V AC | £3 |
| 2A DC | | £3.08 | 50V AC | £3 |
| 5A DC | | £3.08 | 150V AC | £3 |
| 10A DC | | £3.08 | 300V AC | £3 |
| 3A DC | | £3.08 | 500V AC | €3 |
| 10V DC | | €3.08 | S Meter 1mA | €3 |
| 15V DC | | £3.08 | VU Meter | €4 |
| | | | | |

| | ** | €3.08 | 11012 | |
|----|----|-----------|-------------|-------|
| | | £3.08 | CLITTE | |
| ۱ | | €3.08 | | |
| ۱ | | £3.38 | | |
| ١ | | £3.98 | 20V DC | £3.08 |
| Α | | €3.98 | 50V DC | €3.08 |
| A | | £3.08 | 100V DC | €3.08 |
| A | | £3.08 | 150V DC | €3.13 |
| A | | £3.08 | 300V DC | €3.13 |
| A | | €3.88 | 500V DC | €3.19 |
| Α | | £3.08 | 750V DC | €3.19 |
| 0 | | £3.08 | 15V AC | £3.19 |
| С | | £3.08 | 50V AC | €3.19 |
| C | | £3.08 | 150V AC | €3.19 |
| OC | | £3.08 | 300V AC | £3.19 |
| С | | €3.08 | 500V AC | £3.35 |
| ЭC | | €3.08 | S Meter 1mA | €3.56 |
| ЭС | | £3.08 | VU Meter | £4.13 |
| | | | | |

CLEAR PLASTIC MODEL SD460

| PR6: 02 x 40W | HTTH | | |
|---------------|-------|--|---------------|
| 50uA, | £3.89 | | |
| 100uA | £3.83 | - | |
| 200u A | £3.78 | Y | |
| 500uA | £3.73 | The same of the sa | manufacture . |
| 50-0-50u A | £3.83 | 1 1 | ~ |
| 100-0-100uA | | a landon 2 a | |
| 1mA | £3 67 | A | |
| 5mA | £3.87 | IN COLUMN 2 | |
| 10m A | £3.67 | 100000 | |
| 50mA | £3.87 | 10V DC | £3.6 |
| 100mA | £3.87 | 201/ D.C | 62.4 |
| E00 A | £3.67 | EMI/ DG | |
| 1A DC | £3.87 | | |
| | | 300V DC | . £3.6 |
| 5A DC | €3.57 | 15V AC | . £3.8 |
| 10A DC | €3.87 | 300V AC | €3.8 |
| 5V DC | | 1/11 84-1 | |
| JT DC | €3.57 | VU Meter | . £4.6 |
| | | | |

CLEAR PLASTIC MODEL MR 65P

| 50uA | €4.37 | 6 10 |
|-------------|-------|-----------------------|
| 100u A | £4.27 | |
| 200u A | £4.21 | Age of the face |
| 500u A | €4.18 | 1 0 A 100 |
| 50-0-50u A | €4.27 | 2.4 |
| 100-0-100uA | €4.21 | and the second second |
| 500-0-500uA | €4.10 | DISCOURAGE WATER |
| 1mA | €4.10 | |
| 1.0.1-4 | £4.10 | HI HOUSE STREET |
| E-A | £4.10 | 12111111 |
| 10- 4 | £4.10 | 300V DU 641 |
| EOm A | £4.10 | |
| 100-A | €4.10 | |
| 600m A | €4.10 | |
| 1A DC | £4.10 | |
| EA DC | £4.10 | |
| 104 DC | £4.10 | 500V AC £4.3 |
| 15A DC | £4.10 | S Meter 1mA £4.8 |
| | | VU Meter £4.5 |
| 20A DC | €4.21 | 1A AC £4.1 |
| 30A DC | £4.27 | 5A AC £4.1 |
| 50A DC | €4.48 | 10A AC * £4.10 |
| 5V DC | £4.10 | 20A AC * £4.1 |
| 10V DC | £4.10 | 30A AC * £4.16 |
| 15V DC | £4.10 | 50mA AC * £4.10 |
| 20V DC | £4.10 | 100mA AC * £4.10 |
| 50V DC | £4.10 | 200mA AC * £4.16 |
| 150V DC | £4.10 | 500mA AC * £4,10 |
| DAMELIER | | |

BAKELITE MODEL S80 Enlarged Window

| SIZE: OU X BUITIM | | |
|-------------------|-------|--|
| 50u A | €4.97 | |
| 100uA ., ., | €4.91 | |
| 500uA | £4.64 | |
| 50-0-50u A | €4.91 | 10.7 |
| 100-0-100uA | €4.86 | Control of the Contro |
| 1mA | £4.84 | 100 |
| 1A DC ., ., | £4.64 | |
| 5A DC | £4.64 | |
| 20V DC | £4.64 | |
| 50V DC | £4.64 | Marie Laborated A. |
| 300V DC | £4.64 | The Control of the Lot |
| 300V AC | £4.75 | 100 |
| VU Meter | £6.00 | |
| 24 2 2 2 24 2 2 | | the state of the s |

CLEAR PLASTIC MODEL MR 52P

| 50u A | £4.10 | |
|--------------|-------|-----------------------------------|
| 100uA | £3.89 | Committee of the committee of the |
| 500u A | £3.73 | 257 # 175 # 175 B |
| 50-0-50uA | €3.89 | 20 mm 10 mg/s |
| 100-0-100u A | £3.73 | HA W |
| 1mA | €3.67 | |
| 5mA | £3.67 | |
| 10mA | £3.67 | THE PARTY NAMED IN |
| EOm A | £3.67 | 11110 Feet |
| 100- A | £3.67 | |
| E00 A | E3.67 | (MILITAL DE LA COLLEGA |
| 1A DC | | 440 |
| EA DO | €3.67 | S Meter 1mA £4 |
| | £3.67 | |
| 10V DC | £3.67 | VU Meter £4. |
| 20V DC | €3.67 | 1A AC * £3. |
| 50V DC | £3.67 | 5A AC * £3. |
| 300V DC | €3.67 | 10A AC * £3. |
| 15V AC | €3.87 | 20A AC * £3. |
| 300V AC | €3.87 | 30A AC * £3. |
| | | |

| €3.67 | | | |
|-------|--------------|----|-------|
| | 0.10-1-1-0 | | |
| €3.67 | S Meter 1m A | ١ | £4.28 |
| €3.67 | VU Meter | ** | €4.88 |
| €3.67 | 1A AC | • | £3.67 |
| £3.67 | 5A AC | * | £3.67 |
| £3.67 | 10A AC | • | £3.67 |
| €3.87 | 20A AC ., | • | €3.67 |
| €3.87 | 30A AC | • | €3.67 |
| | | | |

BAKELITE MODEL MR 65 Size: 80 x 80m

| 25uA | £5.83 | ARREST ATTENDED |
|-------------|---------|-------------------|
| 0uA | £4.43 | |
| 00u A | £4.37 | |
| 00uA | £4.06 | |
| 0-0-50uA | £4.38 | nA \ |
| 00-0-100uA | £4.32 | |
| 00-0-500u A | £4.00 | |
| mA | . £4.00 | |
| -0-1mA | £4.00 | |
| mA | . £4.00 | |
| Om A | £4.00 | The second second |
| 0mA | £4.00 | 308V DC |
| nn-A | €4.00 | 30V AC * £4.2 |
| OOm A | €4.00 | 50V AC * £4.0 |
| A DC | . €4.00 | 150V AC * £4.0 |
| A DC | £4.00 | 300V AC * £4.6 |
| A DC | £4.00 | BOOV AC . CA |

| 500-0-500u | Α | £4.00 | | Name and Address of the Owner, where |
|------------|----|-------|----------|--------------------------------------|
| 1mA | | £4.00 | | |
| 1-0-1mA | | £4.00 | | |
| 5mA | | £4.00 | | 110 |
| 10mA | | £4.00 | 1000 | |
| 50mA | | €4.00 | 300V DC | |
| 100mA | | €4.00 | 30V AC | * £4.21 |
| 500mA | | €4.00 | 50V AC | ° £4.00 |
| 1A DC | | €4.00 | 150V AC | ° £4.00 |
| 2A DC | | £4.00 | 300V AC | ° £4.00 |
| 5A DC | | £4.00 | 500V AC | ° £4.00 |
| 10A DC | | £4.00 | VU Meter | 64.00 |
| 15A DC | | £4.00 | 24 40 | 0 00 00 |
| 30A DC | | €4.00 | 54 45 | |
| EOA DO | | £4.21 | 104 40 | |
| EV DC | | | | ° £4:00 |
| 10V DC | •• | £4.00 | 20A AC | ° £4.00 |
| | | £4.00 | 30A AC | ° £4.00 |
| 15V DC | | €4.00 | 50A AC | ° £4.00 |
| 20V DC | | €4.00 | 500mA AC | • £4.00 |
| 50V DC | | £4.00 | 50mV DC | £4.00 |
| 150V DC | | €4.00 | 100mV DC | £4.16 |
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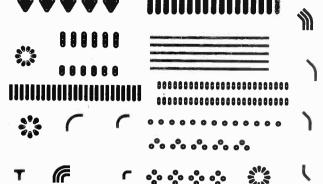
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The bargains in this column are just some of the items which appeared in the April supplement of our catalogue. You can receive this catalogue and the next 12 supplements by sending \$1.

Pre-recorded tapes, Those of you who had our selection of ten tapes last month may wish to order selection 50 which is 50 more reel to reel pre-recorded tapes, new in perspex type storage box, different titles, classical and light music Our assortment £25 the lot post paid.

50v amplifier transformer made by Parmeko so obviously very well-made, 2 amp, upright mounting with shrouds, a transformer that will enhance the performance of any amplifier. Offered at only \$4.50 + 75p post—less than current cost.

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following ranges: 0-10 amps 0-20 amps 0-30 amps 0-40 amps 0-50 amps 0-100 amps 0-200 amps.

50 amp luses, cartridge type, mounted in plug-in fuse carrier with panel mounting fuse holder. Price 50p each. 100 amp ditto, price 85p each. Post 25p each.

100 amp 50 volt silicon rectifier on heat sink for panel mounting, 23.50.

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Edge mounting moving coil meter, size $3''\times 2''$ scaled DB made for the GPO, unused still in original maker's cartons. £2.50 each.

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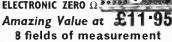
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| 220 | 16 | | sinale | end p/c | fitting |
| 330 | 16 | 12 | | | - |
| 1000 | 16 | 20 | | | |
| 10 | 25 | 7 | | | |
| 22 | 25 | 7 | | | |
| 47 | 25 | 7 | | | |
| 100 | 25 | 7 | | | |
| 150 | 25 | 9 | | | |
| 200 | 25 | 11 | | | |
| 1250 | 25 | 24 : | single | end car |) |
| 5000 | 25 | 55 | | end can | |
| 1000+1000 | 30 | | single | end car | 1 |
| 2500 | 30 | 40 | single | end car | 1 |
| 6 - 8 | 40 | 7 | | | |
| 16 | 40 | 7 | | | |
| 100 | 40 | 9 | | | |
| 1000 | 50 | | single | end car | 1 |
| 1 | 63 | 7 | | | |
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| Oddments to c | | | | | |
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