



WIRELESS

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EDITOR

Lionel E. Howes, G3AYA

ASSISTANT EDITOR Eric Dowdeswell, G4AR

ART EDITOR Peter Metalli

PRODUCTION & NEWS EDITOR Colin R. Riches PROJECTS SUB-EDITOR Geoffrey C. Arnold

TECHNICAL ARTIST Alan Martin

BECRETARIAL Susan King 01-634 4292

ADVERTS. MANAGER 01-634 4293 Roy Smith

CLASSIFIED ADVERTS. 01-634 4301 Colin R. Brown

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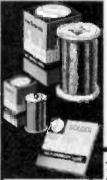
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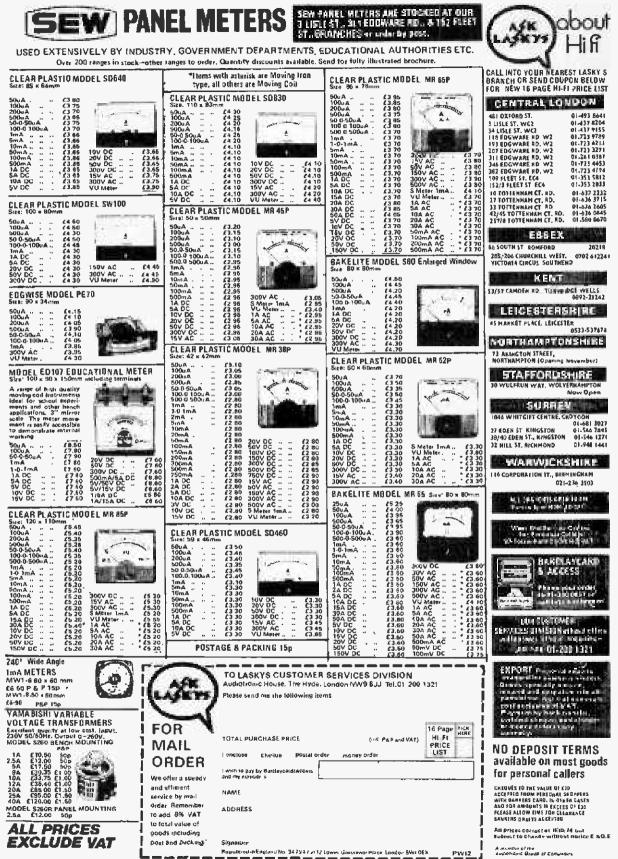






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Car Radio Kit £7.70 + 55p p & p

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Technical specification :

- (1) Output 4 watts B.M.S. output. For 12 volt operation on negative or positive earth.
- (2) Integrated circuit output stage, pre-built three stage IF Module.

NO SOLDERING

REQUIRED!

Controls volume manual tuning and live push buttons for station selection, illuminated tuning scale covering full, medium and long wave hands. Size chassis 7" wide, 2" high and 4%" deep approx

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Input sensitivity 600mV. Aux, input sensitivity 120mV. Power output 2.7 watts per channel. Output impedance 8-15 ohms. Steren headphone socker with automatic speaker cutout. Provision for auxiliary inputs - radio, tapit, etc., and outputs for taping discs. Overall Dimensions, Speakers approx. 151" × 8" × 4". Complete deck and cover in clused position approx. 151" × 12" × 6"

Complete only £19.95 £1.60 p & p. Extras if required. Optional Diamond Styli £1.37. Specially selected Pair of stereo headphones with individual level controls and Padded earpieces to give aptimum performante. £3.85.



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STEREO AMPLIFI just simply screw together. 4 watts per channel into 8 ohms. Inputs: 120mV (for ceramic carbidge). The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion over the audio spectrum.

for use with your stered system. Compatible with Viscount HI system, Unisound module and the Stereo 21. Technical specification Malos input. 248V. Quiout sensitivity 125mV Comparable unit sold eleswhere at E24.00 approx. Yours for only

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System 1. £51.00

40 Watt Amaillier, Viecount III - B102 new 20 watts per channel. System Lincludes

Viscount III amplifier - volume, bass, treble and balance controls, plus switches for mono? stereo on /off function and bass and trebla filters. Plus headphone socket. Specification

20 watts per channel into 8 ohms. Total distortion @ 10W @ 1kHz 0-1%. P.U.1 (for ceramic certridges) 150mV into 3 Meg. P.U.2 (for magnetic cartridges) 4mV @ 1kHz into 47K. equalised within ±1dB R.I.A.A. Radio 150mV into 220K. (Sensitivities given at full power). Tape out facilities : headphone socket, power out 250mW per channel. Tone controls and filter characteristics, Bass: -+ 12dB to -17dB @ 60Hz. Bass filter: 6dB per ostave cut. Tieble control: treble ~ 12d8 to -12d8 or 15kHz Treble filter 12d8 per octave. Signal to noise ratio (all controls at max.) -58dB. Crosstalk better than 35dB on all inputs. Overload characteristics better than 26dB on all inputs. Size approx. 13 1 × 9 × 3 1.

Garrard SP 25 Mk III deck with magnetic cartridge, de June plinth and hinged cover. Two Duo Type II matched speakers - Enclosure size approx. 171"×103"×6" in simulated teak. Drive unit 13" > 6" with parasitic tweater, 10 watts handking.

Complete System £51.00

stem 2. £69.00

amplifier (As System I) Garrard SP 25 Mk III dack (As System II

Two Duo Type III matched speakers - Enclosure size approx. 27" x 13" x 111" Finished in teak veneer. Drive units 13' x 8" bass driver, and two 3" (approx.) tweeters. 20 walls R.M.S., 8 ohms frequency range - 20 Hz to 18,000 Hz.

Complete System £69.00

PRICES : SYSTEM 1

Viscount III R102 Viscount III R102 £24.20 + £1 p 8 p amplifier amolifier 2 Due Type II speakers £14.00 + £2.20 p & p Garrard SP 25 with Mag. cartridge de luxe plinth and hinged cover £21.00 + £1.75 p & p

total: £59.20

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£51 00 - £3.50 p & p PRICES: SYSTEM 2

£24.20 + £1 p & p

2 Dug Type III speakers £39.00 + £4.00 p & p

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Cone, Triple laminated paper with

P.V.C. surround. Mid Range Unit

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The two lightweight cartridge shells have slide-in-holders to facilitate easy inspection of needles and cartridges.



TECHNICAL SPECIFICATION : Pre-amp - Output - 200mV. Auxiliary inputs - 200mV and 750mV into 1 med. Mic input - 6mV into 100K. 240 volt opera Turntables capacity - 7". 10" or 12" records. 240 volt operation. Rumble, wow and flutter - Rumble - Better than -35dB. Wow - Better than 0.2% Flutter - Better than 0.05% (Gaumont kalee meter). Finish - Satin black mainplate with black turntable mat inlaid with brushed aluminium telm. Tonearm and controls in black and brushed aluminium.

Consola size -- Unit Closed -- 17 }** 13 *** 8 ** (approv.) Unit Open -- 35 *** 13 *** 4 ** (approv.) This disco console is ideally marched for the Reliant IV and Disco 50 or any

other quality amplifier. The unit is finished in black PVC with contrasting simulated teak edging diamond spun control knobs with matching control panel.

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45 WATT R.M.S. MONO DISCOTHEDUE AMPLIFIFR Ideal for Disco Work, Oulput Power: 45 watts R.M.S. Frequency Response 3dB points 30Hz and 18KHz. Total Distortion: less than 2% at rated output. Signal to noise ratio: better than 60dB. Bass Control Range: 13dB at 60Hz, Treble Control Range: 12dB at 10KHz. Inputs : 4 inputs at 5mV into 470K, Each pair of inputs controlled by separate volume control. 2 inputs at 200mV into 470K. Size: 194"×101"×8" (approx.) Amplifier £27.50+£1.50 p. & p.



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158 2000 60 0 216 x 15-3 x 10-1 50-25 +
Ref. VA Weight Size cm. Auto Tops P & P No. (watis) Iboz 6 5.8 x 5.1 x 4.5 0.115-210.240 1.3 4 30 13 20 1 5.8 x 5.1 x 4.5 0.115-210.240 1.3 4 30 64 75 2 4 7.4 x 6.7 x 6.1 0.1 15:210.240 2.64 38 4 150 3 8.9 x 7.7 x 7.0 1.15:210.240 3.29 43 66 300 6 9.9 x 9.6 x 6.6 5.29 53 67 500 12 8.1 2.1 x 1.1 2.x 1.0 2.0 2.20-240 3.29 43 63 300 6 9.9 x 7.4 x 6.6 5.20 3.00 3.00 7.3 3.00 4.4 0.0 x 3.9 x 1.3 x 1.3 50 91 93 1500 3.0 4 1.4 0.0 x 13.4 x 14.3 x 1.3 50 91 3.0 x 1.5 50 3.0 x 1.5
TRANSFORMERS
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Ref. Amps. Weight Size cm. Secondary Tabs P & P 124 0.5 2.4 7.0 x 6.7 x 6.1 0.24/30-40-48-60 2.12 38 126 1.0 3.4 9.9 x 7.7 x 7.7 2.97 38 126 1.0 3.4 9.9 x 7.9 x 7.7 2.97 38 125 3.0 8.19 x 7.7 x 7.7 5.0 4.4 9.9 x 7.4 x 7.7 127 2.0 6 4 9.9 x 9.6 x 6.5 - 5.40 45 125 3.0 8.12 2.1 x 9.9 x 10.2 .7 11.6 60 123 4.0 1.3 12 12.1 x 19.8 x 10.2 .9 20.0 67 120 6.0 15.0 1.4 0.9 x 10.2 x .9 20.0 67 .13 35 85 121 8.0 2.5 0 1.7 1.2 1.7 x
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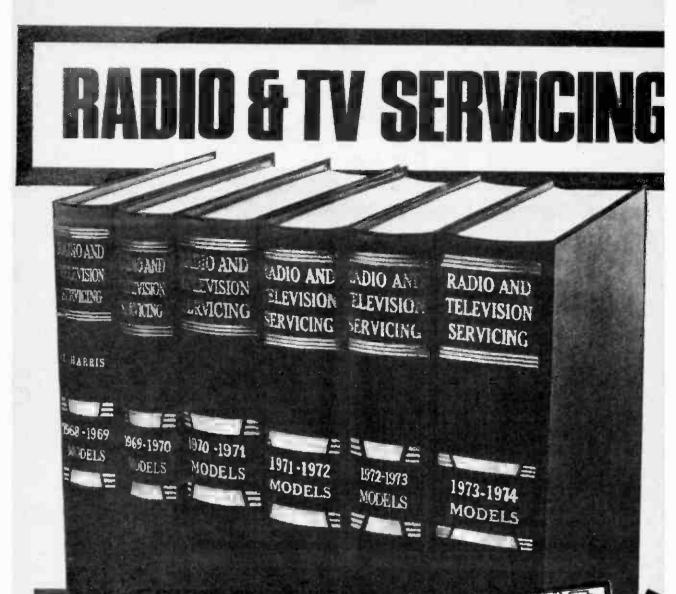
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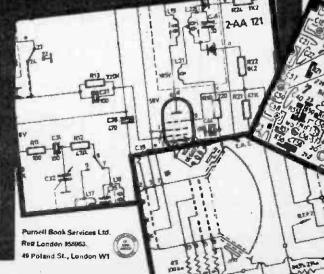
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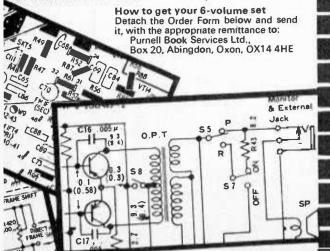
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Parameter	Conditions	Perlormance	
BARMONIC DISTORTION	Po - 3 WATTE !=1KHz	0.25%	
LOAD IMPEDANCE		8 - 16 1	
INPUT IMPEDANCE	1-1KHz	100 k 🗘	
FREQUENCY RESPONSE ± 3dB	Po-2 WATTS	50 Hz - 20 KHz	
BENSITIVITY for RATED O/P	Vs=26V. Rl-8Ω f=1KHz	75mV. RMB	
DIMENSIONS	-	3" × 2#" × 1"	

The abuve table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions

The credit is or the set			and the second day of
Parameter	AL10	ALEO	ALSO
Maximum Supply Voltage	25	30	\$Ú
Power output for 2% T.H.D. $(\mathbf{RL} = \mathbf{S}\Omega \mathbf{i} = 1 \mathbf{K}\mathbf{H}\mathbf{z})$	3 watts RMS Min.	5 waits RMS Min.	10 watis RMS Min.

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B 12. (Une with A L10, A L20, A L30) 68p		T461 (Une with AL10) \$1.38 P ± P 15p
Ph 60. (Ther with A L60) 33-33		T635 (Hae with AL20, AL30)
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£1.10		BMT80 (Use with AL40) \$2.16 P ± P 120p

PA 12, PRE-AMPLIFIER SPECIFICATION

'he PA 12 Pre-amplifier has been designed to match into | Pre tost budget st-red systems. It is compatible with the Bass control-± 12dB at 60Hz Treble controlthat builder stated systems, as is owner amplifiers and it in he subplied from their associated power supplies. Treble control--± 140B at 14KHz *InDut 1. Impedance I Mes. obm Bensitivity 300mV †Input 2. ImDedance 30 K ohme Bensitivity 4mV "here are two stored inputs, one has been designed for use oth "Corande ratiridges while the auxiliary input will alt most foisgnetic cartridges. Full details are given in as specification table. The four controls are, from left to ight: Volume and on/off zwitch, balance, bass and treble. dre 152min × 84mm × \$5mm

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The Blerea DD samplifer is mounted, ready wired and tasted os one-pice classic threawiring 2D cm x 14 cm x 6-6 cm. This compact unit comes of united with onloid switch optimer control, baines, base and tetbie controls, read-former, Power supply and Power amps. Itracticely printed front part and match-ng optical knobs. The 'Btereo 2D has been default of the most turn table bitths ethout interfering atlus the mechanism or detamaticely. Into a separate acknet Dutput power 20 w peak. Input 1 (Cara) Uthor M. Pred. res. 2014;28 kBz. Input 2 (Aux.) 4MV into 2015. Barronle Historiton- Das control ± 1208 at Trehe cout. ± 140B at 14kHz.

TC20 TEAK VENEERED CABINET For Storen 20 (front hoard undrilled) size 104" x 81" x 5", £3-95, plus 50p postage SHP80 STERED HEADPHONES

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- 0 IKHz
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Especially designed to a strict specification. Only the finest components have been used and the latest solid state circuitry incorporated in this powerful little amplifier which should satisfy the most critical A.F. enthusiast.

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13mm

Signal to noise ratio 30dB Overail size 63mm × 105mm ×

TRANSFORMER BMT80 £2.15 p. & p. 28p

STEREO PRE-AMPLIFIER TYPE PA100

GIERCO FRESHMPLIFIER IFFE PAIDS Built to a specification and NOT a price and yet still the preview taile on the market. the PADD store pre-amplifier has been considered from the latest circuit techniques. Built of downee with the ALOD power shallfer system, this guilty made unait incorporates and sees than eight spiller system, this guilty made unait incorporates been than eight spiller system, this guilty made unait incorporates NEW devices for me in the input stars. Three switched store inputs, and runnils and seratch filters are features of the PADO, which side bas a SDEREO/ADOD switch; solume, balance and continuedely variable base and trable Controls.

	SPECIFICATION	
· Charles	Fraquency Response	20日z — 20瓦田z ± 1dB
X-ALE	Harmonic Distortion	better than 0-1%
a second	Inpote: 1. Tape Head	3.25 mV into 50K Ω
	2. Radio, Tuber	75 mV into 50Κ Ω
	3 Magnetic P.IF	3 mV julo 60K Q
	All Input voltages are for an o	ntput of 250mV. Tape and P.U. inputs
ALC: NOT THE OWNER OF	cousteed to RIAA surve with	$10 \pm 10B$ from $20H_2$ to 20B H1.
	Sees Centrol	+ 156B at 20Hz
	Treble Control	+ 15dB at 20 KH3
1. S. 1	Filters: Rombis (High Pass)	100Hz
Contraction of the local division of the loc	Scratch (Low Pase)	SKHI
	Bigual/Noise Ratio	hetter than - 65dB
Constant of the	Input overload	+ 26dB
and the	Supply	+ 35 volts at 20mA
Brank, Services	Dimensiona	292min × 52mm × 35mm
-		ONLY £13-15

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application. I: 550 1:03 PL*3 0.48 3001/PCP80 DAY0 0-81 ETLA3 0-64 FC28 0-77 PL*3 1.06 3001/PCP80 0-54 DY81 0-81 ECLA6 0-63 FC28 0-95 FL43 0-61 3001/PCP80 0-54 DY81 0-41 EF69 0-63 FC28 0-95 FL44 0-87 3001/PCP80 101 DY807 0-41 EF69 0-64 FC28 0-95 FL44 0-87 102 102 102 101 102 101 102 101 102 101 102 101 102 101 102 101 102 101 101 102 101 102 101 102 101 102 101 102 101 102 101 102 101 102 101 102 101 102 102 101 102 102 102 101 102 <t< th=""><th>AA119 0.7 BD132 0.50 Fairchild, Lucas, etc. AA213 0.10 BF167 0.23 Optimity discounts On AA214 0.10 BF167 0.23 Application. Send SAE AC107 0.38 BF177 0.23 Application. Send SAE AC127 0.43 BF180 0.83 for full lists. AC126 0.20 BF181 0.83 AC126 0.20 BF181 0.83 for full lists. AC126 0.20 BF181 0.84 AC126 0.20 BF181 0.84 0.12 Strap044 0.20 AC127 0.23 BF181 0.13 OC16 1.00 ZTX501 0.15 Strap044 0.20 AC137 0.24 BF181 0.30 OC22 0.70 T1741 0.76 Strap044 0.20 AC149 0.40 BF181 0.30 OC23 0.70 T1741 0.</th></t<>	AA119 0.7 BD132 0.50 Fairchild, Lucas, etc. AA213 0.10 BF167 0.23 Optimity discounts On AA214 0.10 BF167 0.23 Application. Send SAE AC107 0.38 BF177 0.23 Application. Send SAE AC127 0.43 BF180 0.83 for full lists. AC126 0.20 BF181 0.83 AC126 0.20 BF181 0.83 for full lists. AC126 0.20 BF181 0.84 AC126 0.20 BF181 0.84 0.12 Strap044 0.20 AC127 0.23 BF181 0.13 OC16 1.00 ZTX501 0.15 Strap044 0.20 AC137 0.24 BF181 0.30 OC22 0.70 T1741 0.76 Strap044 0.20 AC149 0.40 BF181 0.30 OC23 0.70 T1741 0.		
$\begin{array}{ccccc} \text{ECCR0} & 0.48 \\ \text{ECF80} & 0.57 \\ \text{ELL80} & 2.00 \\ \text{ECP82} & 0.58 \\ \text{ECF84} & 0.57 \\ \text{ELL80} & 2.00 \\ \text{ECP82} & 0.58 \\ \text{ECF84} & 0.57 \\ \text{ELL80} & 2.00 \\ \text{ECP82} & 0.58 \\ \text{ECF84} & 0.57 \\ \text{ECF84} & 0.58 \\ \text$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
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DY802 0.43 EL84 0.84 PC2*08 0.60 Diagy 100 16.27 0.84 EARCEO 0.38 RUS6 0.60 PC1A2 0.43 RUA4 0.40 103.45 0.56 0.56 0.56 103.85 0.56 0.56 0.57 0.53 133.85 0.56 0.56 0.57 0.53 133.85 0.56	VAT 8% to be added to all orders including POSTAGE! THIS MONTH'S • OSCILLOSCOPE TUBE TYPE VCR 139A Price £8'00 p & p 25p SPECIAL OFFER		
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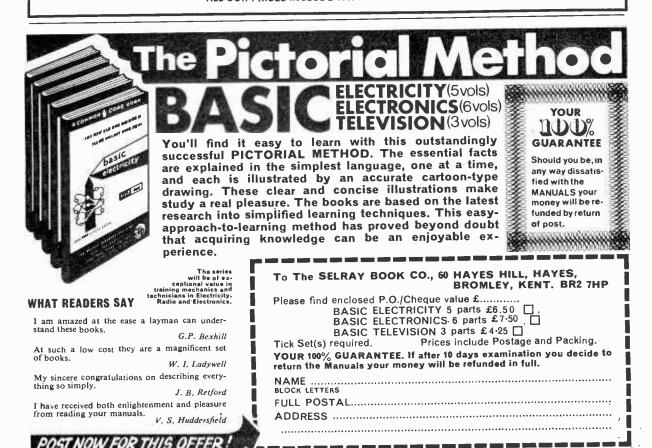
1) 4 sides with handle cutouts, front edges rounded, 1 back with jack socket hole, and 1 baffleboard with speaker cutout

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2 x 12" (illustrated above)	31″x31″x13″x3	£24.50	£17.50	
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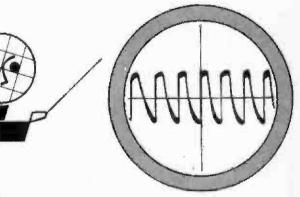
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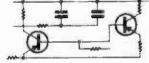
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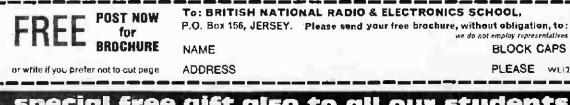
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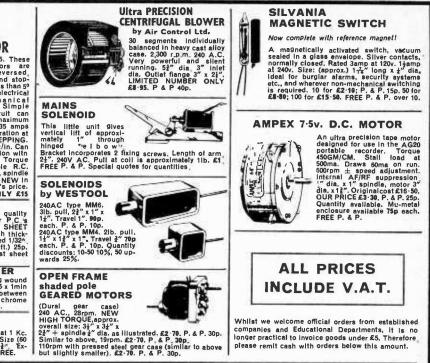
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There exists a veritable jungle in both price and selection. The prolific arrays of pocket calculators that are available to the consumer that dominate the windows and counters of our local high street shops are indeed bewildering. There appears to be a greater variety of pocket calculators than transistor radios!

A price war has emerged amongst major manufacturersprices being slashed overnight and indeed putting many retail distributors and 'special offer' organisations on the spot! A recent overnight price reduction by a major manufacturer caused considerable embarrassment to many of his trade and retail outlets. This sort of fiasco is being repeated over and over again. Where will it all end?

One enterprising calculator manufacturer determined to display his 'chips' to members of the public has opened up a 'mobile shop' at a London main line railway station. By all reports, he is doing *fantastic* business.

What of the 'domestic' pocket calculator? Rumour has it that a basic calculator especially designed for the housewife may be launched. If so, this could be just the thing for calculating and analysing those shopping expeditions to the supermarket. The shopper would be able to check his totals at any time and at the till check-out point. I can foresee many red-faced supermarket managers attempting to explain away the differences that may occur between store and customer calculated totals.

The pocket 'memory' calculator with its inherent potential as a pocket computer, with the ability to recall stored information at the press of a button could be just around the corner!

What of the future? The pocket calculator could become as prolific as the ball-pen—a must for everyone.

However, the pessimists (optimists, if you prefer) are chanting 'Beware, Big Chip is watching you!' (shades of 1984). They could however be forecasting our future.

There is no doubt that the calculator chip has, in many ways, dramatically changed our whole way of life. The question is: are we all in the hands of the Big Chip?

LIONEL E. HOWES-Editor.

We're off to a good start in the New Year with our three part series on Model Control by Radio and we tell you how to get your licence for this most interesting of hobbies. Do you sometimes wish you had a small audio amplifier around for testing purposes? Our 2 watt IC audio amplifier will fill the bill. The Special Pre-publication Book Offer ought to appeal to many of our readers for all the useful information contained in Radio Servicing Pocket Book, a new 3rd edition. Finally, you won't want to miss the fourth and final part of the PW Buyers' Guide 1974/75. All in the January issue of Practical Wireless.



From Partridge . . .

A ever increasing number of people are living in space restricted environments. Either through sheer lack of external facilities for the erection of aerials, the inability to receive radio signals inside ferro concrete walls, or the existence of local government legislation preventing the use of outdoor space for aerials, there are ever growing numbers of frustrated readers unable to pursue their hobby of Amateur Radio or Short Wave Listening.

For many years now Partridge Electronics Ltd., of Broadstairs, Kent have specialised in equipment designed to overcome this problem. Five years ago they published a reproduction of a World Record Certificate awarded to American Radio Amateur W6TYP. This was achieved by Mr. Art Child of San Francisco using the Partridge system operated from a hotel room at the foot of San Francisco's famous Nob Hill.

Partridge have now developed a device known as A.G.T.U., an Aerial Tuning Unit which also incorporates an Artificial Earth (or ground). This overcomes the only remaining problem of the high-rise apartment or flat dweller having no access at all to natural earth.

ON THE COVER

PW's MINIATURE SCREWDRIVER

Don't despise this very useful workshop aid because it seems to be so small! How many times have you found that your 'small' screwdriver is just too wide or too thick for the grubscrew in a knob or the adjusting slot in a subminiature potentiometer?? The more you use it the more uses you will find for our little present!

Harrogate Fair

A UDIO '74 or the Northern International High Fidelity Festival at Harrogate was the biggest and best-attended ever. In 1970 there were only 50 exhibitors. 1972 saw 70 firms exhibiting their wares and this year over 90 companies decided to show their faces.

Over the last couple of years, there has been a marked increase in the amount of quadraphonic equipment on show. It is a pity that there seems to be little or no agreement on the kind of system to be favoured for quadraphonic reproduction.

We hope to include a short report on "Audio '74" in a future issue.

BBC tape deal

A CONTRACT to supply the BBC with more than 100,000 reels of TS Scotch 262 recording tape for stereo broadcasting has been awarded to 3M United Kingdom.

The contract, which is due to run until next June, is in addition to the 70,000 reels supplied to the BBC last year after close liaison between the Corporation's sound engineers and technicians from 3M's magnetic tape facilities at Gorseinon, near Swansea, and Caserta in Italy.

BEAB approval list

THIS list covers the first category of audio products in the BEAB Approval Scheme which have successfully met the requirements of the British Safety Standard BS.415: 1972.

Decca Radio & Television with the Decca DS623, ITT Consumer Products Ltd. (ITT KP 820, KP 821, KA 1026, and RGD PA 30, P 83). Pye Limited (Pye 5000 and Invicta 8040). Sony (UK) Limited (Sony HMW-20). Rank Radio International Ltd. (Bush A 1005, A 1016, BS 3013, Dansette A 4005, A 4016, and Murphy MS 3014). Thorn Consumer Electronics Ltd. (HMV 2046, Ferguson 3047, Marconiphone 4047, 4049, Ultra 6046, 6048.

Computer club

NOW moving into its second year of existence the Amateur Computer Club of Basildon, Essex has now formulised its activities into a constitution and elected officers for the year.

See.

The club now has a firm membership of over 200 with a regular newsletter forming the nucleus of the club.

After two Annual General Meetings in London and committee meetings the start of a club activity schedule has emerged. The first of which was an open afternoon on the 25th May, 1974, at the Galdor Centre, 52 Brighton Road, Surbiton, Surrey.

The people at the Galdor Centre own and run an ICL 1301A computer (1960 vintage) which they have installed and made working to provide them and similarly interested persons with computer time at "materials only" cost.

Heathrow computer

ABLE and Wireless Ltd. have installed a new computer-based departure control system for airline passengers at London Airport. Japan Air Lines will use the system named "Lopac" which has been jointly developed by C & W and Scientific Control Systems Ltd.

Apart from speeding passengers' baggage check-in procedure, the system also allows for productivity expansion.

Lopac, incidentally, stands for Load Optimisation and Passenger Acceptance Control.

PW TOOL KIT OFFER

We apologise to our readers for the delay in dealing with their orders. The overwhelming demand created problems with delivery. If any readers have not received their tool kits, or a suitable alternative, would they kindly contact the Editor. Further activities are being arranged and will be announced in the newsletter which has also provided a unique forum for the airing of ideas and introducing basic principles to the beginner.

NEWS.

Articles in the newsletter have covered transistor working, design and operation of a digital core store, digital computer elements. computer software, software routines, descriptions of various computer systems both working and under design/development, news information items and computer games!

Club members are contributing articles to the newsletter resulting in some cross fertilisation of ideas among the members, which is one of the most important objectives of the club.

New members and ideas are very welcome, membership is $\pounds 1 \cdot 00$ per year (that includes the near monthly newsletter) and applications should be directed to Mike Lord, 7, Dordells, Basildon, Essex.

Javelin move

JAVELIN Electronics have closed down their City offices and moved to Javelin House, Second Way, Exhibition Grounds, Wembley, Middlesex HA9 OUA. (01-903-6821).

The new building contains the service department, a dealers' advice centre and a customer relations department.

Sansui 4-channel

T HE sponsors of the "QS" 4channel system, Sansui, are making moves to persuade artists in the UK to record material using their system.

The "QS" regular matrix system has been accepted by the American and Japanese Recording Industries Associations and over 20 record manufacturers are producing software in the system.

It has been stated that at least one commercial radio station in the United Kingdom is thinking of using "QS" which has now been adopted by all f.m. stations in Japan.



I MUST confess from the start that I am not entirely unfamiliar with the RT-VC car radio having bought an earlier version, some time ago. I spent a couple of evenings leisurely soldering the bits and pieces to the printed circuit board and putting the thing together, following the instructions most meticulously. On connecting it up to a 12 volt battery in the workshop the radio worked first time and with a tweak of the oscillator capacitor the callbratton was done.

The set soon disappeared into the innards of my daughter's Triumph Herald. I was about to say 'never to be seen or heard of again' but that would be patently untrue since the radio is simple but elegant in appearance and can certainly be heard! Subsequently, the set came out for a further fiddle on the oscillator trimmer to enable London's Capital Radio to be tuned in right at the low frequency end of the medium wave band. A big improvement on the sideband splash that had been tolerated up to then!

This latest Tourist Two car radio kit has taken all the fun out of the home construction of kits and one would be hard pushed to say, with a clear conscience, that 'I made it myself'. Admittedly the earlier version of the PCB had a few components plus the audio IC already soldered in position but I suspect that RT-VC did this so that they could say 'look at our soldering ... now you do the same'. In fact, they insisted that the constructor's soldering was as good as theirs before accepting back any kits for servicing or checking ... and quite rightly so.

Now, alas, the PCB comes completely assembled and the soldering iron remains cold and unwanted! A pair of long nosed pliers and a small screwdriver are all the tools required with this new kit and the remaining assembly work is child's play. In the words of RT-VC 'the kit can be assembled in less than two hours by anyone who has the ability to wire a normal household three pin plug'.

Assembly

The assembly instructions are extremely detailed and i cannot think of any point that would arise that isn't dealt with already. RT-VC's guarantee says 'lf, after receiving your Tourist kit, you feel that its construction is not within your' capabilities we will refund you the full price of the goods, less post and packing, upon the return of all parts supplied on the condition that no constructional work been attempted and all parts are received in the same condition as dispatched'. I hope that the formidable appearance of the assembly instructions, fault-finding guide, Installation instructions and six annotated photographs will not have the opposite effect and trighten off the prospective constructor!

Having completed the assembly you will want to know the polarity of your car's electrical system. If it is negative earth then the set is ready to go but if it is a positive earth then you have to change over two of the push-on tag connectors. Not very difficult! Should you decide ever to transfer the radio to a car of opposite polarity the change back can be made more quickly than it takes to tell.

Installation

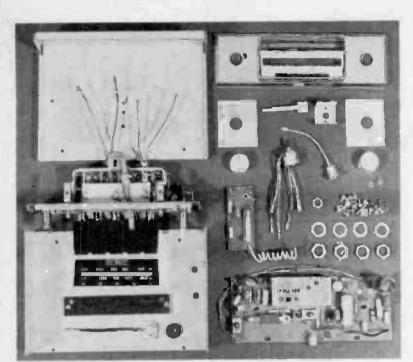
RT-VC recommend a check-out of the set with the car battery before final installation in the car. Calibration takes a moment and the aerial trimmer is adjusted using the aerial that is to be fitted to the car. If all is well, and I'd be surprised if it wasn't, installation can now begin. RT-TV's instructions on this aspect are, again, as complete as they

SPECIFICATION
- Medium Waves 185 to 555m (1620 to 540kHz) Long Waves 1153 to 2000m (260 to 150kHz)
Better than 15µV at 1MHz
4 watts to 4 ohm speaker
Push-buttons (4 MW 1 EW), manual tuning control, volume/ on-off
7" wide 2" high 41" deep approx.

The supply voltage is nominally 12 volts. The polarity, relative to the case, can be changed over internally simply by reversing two push-on tags. The circuit is protected by an internal fuse and a VDR (voltage dependent resistor) against static discharge.

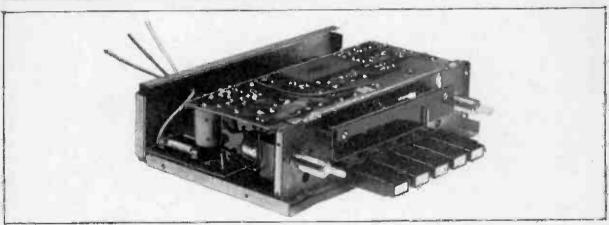
Prices:- Car Radio Kit £7:70 +55p P/P. Speaker, including baffle and fixing strip £1:65 +23p P/P. Car Aerial, fully retractable and locking £1:37 +20p P/P.

Radio and TV Components (Acton) Ltd., 2t High Street, Acton, London, W3 6NG



The contents of your kit will look like this, left. Between the metal casing is the permeability tuning unit and pushbullon assembly. Bottom right shows the complete PCB which is fully tested before despatch.

If the simple instructions are followed the almost finished set should look like that in the photograph below. Only the dial, escutcheon and knobs remain to be fitted plus the cover.



can be and cover every contingency. There is one point here that might be stressed. If you use the aerial available from RT-VC the feeder is about 4' 5" long and the aerial trimmer works perfectly, peaking signals as it should do, when the overall performance is excellent. However, If you need to fit the aerial to the car in such a position that requires the feeder to be extended then this must be done using a special extension lead otherwise performance will definitely be impaired. Using ordinary coaxial cable just will not work. This point is fully covered in the instructions.

Apart from the manual tuning over both bands, four of the push-buttons can be set very easily to any desired stations on the MW band, the fifth push-button selecting a station on the LW band, usually BBC Radio 2, the band change being automatically effected by the action of the push-button. It, for some strange reason, the set does not work at all, or unsatisfactorily, then the Fault Finding Guide will come to your aid and the answer found very quickly.

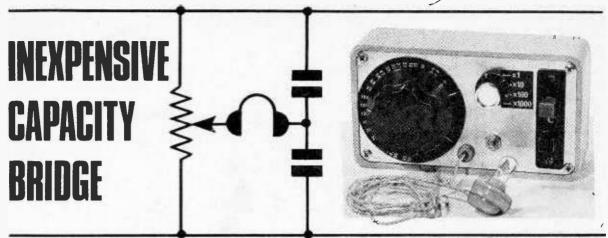
Interference

Having completed the installation and tested the radio to your satisfaction there is a chance that you will suffer a slight set-back when starting the car, because of interference to the radio from the various bits of electricat equipment. Generally, unless the car is a real old 'banger', normal suppression capacitors and other devices will be fitted to the car already and little trouble will arise. However, this matter is dealt with fully in the notes and if the logical sequence of checking is followed a rapid solution will be found.

Conclusions

A very weil designed kit with all the bugs ironed out long ago. Being a bit of a fiddler myself I would have liked the oscillator and aerial trimmer capacitors to be accessible from the outside of the case when the radio is installed in the car. I compromised by very carefully marking out and drilling two holes in the top cover of the case above the trimmers, sticking a bit of Sellotape over the holes when I had done fiddling. I wouldn't expect RT-VC to do anything about this point but I thought I'd mention it, got to complain about something!

Finally, J don't know how RT-VC do it at the price but I understand it is due to the purchasing in volume of proven components and direct retail sales. Certainly they are not contributing to the present inflationary movement!



Test gear is often conspicuous by its absence from the amateur's workshop, possibly because such equipment can be expensive to buy but, more likely, because it is not a justifiable outlay considering the relatively few occasions on which it would be used.

The capacity bridge described here is very cheap to make, will measure capacities from as low as 2pF and up to about 10μ F and will be found to be quite adequate for general workshop use. Over a period the constructor manages to collect unto himself a quantity of capacitors that have had their markings removed in one way or another. This bridge will enable them to be measured, checked and used again. Incidentally, it is a very wise man who checks the value of every component before using it, regardless of colour code or marking, saving a lot of time and temper.

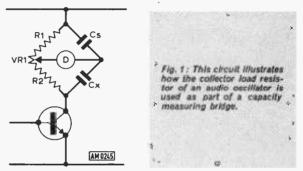
It is not everyone who has good eyesight and even slight colour blindness can cause confusion with colour coded components, generally with blues, browns and greens, which can lead to wrong values of resistors and capacitors being fitted to PCBs etc. This bridge will eliminate any such problems especially if it is used as a matter of routine.

The dial is simple and easily calibrated and used in conjunction with a four step multiplier switch. The consumption of the bridge is very low and the internal 9 volt battery will last a very long time.

DESIGN

As you may have guessed, a bridge circuit is used, what else! and was last seen in the Take 20 series

ERIC DOWDESWELL G4AR



in this magazine. In essence, the collector load resistor of the second transistor of an audio oscillator forms two sides of the bridge, Fig. 1, and, in practice, is a potentiometer. The other two sides of the bridge comprise a capacitor Cs of known value and Cx, the capacitor under test. If these capacitors have the same value then, for the bridge to balance, R1 will equal R2. A detecting device 'D' placed across the bridge will indicate a null in the audio tone under these conditions. If Cx is any other value then the bridge is unbalanced and 'D' will indicate this. Balance can be restored if the ratio of R1/2 is adjusted to have the same ratio as Cs/Cx.

In the practical circuit, Fig. 2, Cs is in the form of a four position multiplier switch with capacitors of 100pF, 1000pF, 0.01μ F and 0.1μ F all of close tolerance, the switch being marked x1, x10, x100

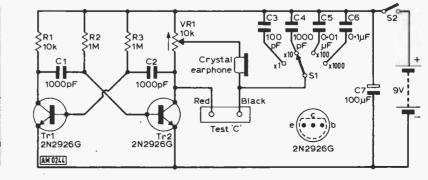
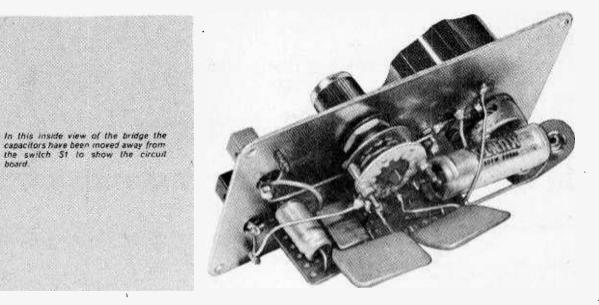


Fig. 2: Complete circuit of the capacity bridge derived from the basic circuit of Fig. 1. Other types of transistor such as BC109, BC149, BC169 can be used if due note is taken of lead-out connections.



and x1000. The capacitor under test is connected to the two terminals. Transistors Tr1 and Tr2 form a multivibrator circuit running at about 1kHz but the actual frequency is not of any great importance.

The detector is a simple crystal earphone of very high impedance, this factor contributing very significantly to the excellent performance of the bridge, the minimal damping imposed by the earphone providing a deep sharp null at balance.

CONSTRUCTION

The bridge is housed in a heavy plastic box with all the components mounted on an aluminium panel. The oscillator components, with the exception of the potentioneter VR1, are assembled on a small piece of Veroboard as in Fig. 3. The bottom rail of the board is soldered to a tag bolted to the panel, providing adequate support for the board.

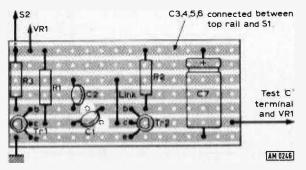


Fig. 3: Components comprising the audio oscillator are mounted on Veroboard as shown above.

The test terminals are spring loaded, their soldering tags passing through ${}^{3}_{8}$ in. holes drilled in the panel. The holes are purposely large to reduce self capacity. An alternative might be to use feedthrough insulators terminated on top of the panel with miniature crocodile clips on stiff leads. Whatever arrangement is used it is essential that a capacitor can be connected to the bridge and removed again very easily.

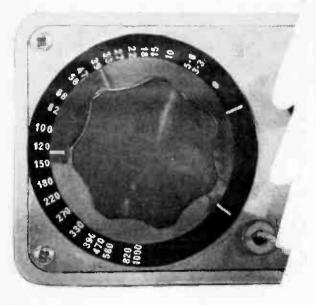
The potentiometer is a very ordinary linear carbon one with a plastic spindle, which, again, reduces self capacity but one with a metal spindle would probably work just as well. The dial was made from a disc of card held under the potentiometer fixing nut together with a pointer knob of such a size as to allow a single range of calibration figures to be marked on the dial. The dial is marked in the 'preferred' range of values corresponding to the standard markings on capacitors.

The crystal earphone is wired directly into the circuit, which again helps to reduce capacity. A combined phone jack and on/off switch was contemplated but a switch and isolated jack could not be found. If any doubt exists as to whether an earpiece is crystal or magnetic it can be checked with an ohmmeter. A magnetic one will show very low resistance whereas a crystal one will show very low resistance whereas a crystal one will show, effectively, an open circuit. Just to make sure that you havn't got an open circuited magnetic earphone put it in the ear and check again with the meter when clicks should be heard even though the meter indicates an open circuit.

The multiplier switch used here is a miniature ceramic one but the more common plastic or paxolin wafer type will suffice. However, if the switch chosen has been used before it must be very thoroughly cleaned before using it in this bridge, for reasons which will be noted later. The standard capacitors C3 to C6 are wired directly between the switch tags and the top 9 volt rail on the circuit board. If a standard size switch is used it will be necessary to move the board down from the position shown in the prototype. It is a good idea anyway, with any project, to shuffle the components around for best positioning before drilling panels etc.

CALIBRATION

After the small amount of wiring is completed and checked, fit the PP3 battery and switch on when the audio tone should be heard in the earphone. The volume, should be adjustable from maximum to zero using the potentiometer. Adjust the position of the knob on the potentiometer spindle so that the ends of its travel are positioned as shown in the photograph of the bridge. Mark these positions on the dial with a sharp pencil. With the multiplier switch on x1 a null should be found near the top of the dial, if the potentiometer has been wired as shown in Fig. 2. This represents the zero position of the bridge without any external test capacitor. Mark this point on the dial.



Close-up of the dial of the bridge. Note that the limits of travel of the potentiometer are also marked.

With a 100pF 1% capacitor connected to the terminals and multiplier on x1 find a new null at about mid position on the dial, then mark it. Turn multiplier to x10 and locate null not far inside the 0 mark. This is marked 10. Note that we have been able to find two points on the dial for one capacitor, using the multiplier. This feature can be used to cross check dial readings.

Change the test capacitor for one of 100pF 1%and mark the null at the bottom end of the dial. Switching to x10 should locate the null at the 100 point, already marked. The remainder of the calbration is done using 1% or 2% capacitors in the preferred range of 120, 150, 180, 220, 270, 330, 390, 470, 560, 680 and 820pF. The x1 multiplier is used to mark the remaining points between 100 and 1000pF and x10 for the points between 10 and 100pF.

TOLERANCES

For a general purpose bridge the cheaper 5% tolerance capacitors are quite adequate for calibration purposes but instead of having to buy the thirteen preferred values it is possible to make do with eight only, the missing values being obtained by paralleling certain capacitors as shown in the Table. There are probably other combinations possible by connecting capacitors in series or even series parallel!

The calibration can be completed with a fine ball point pen or a more fancy dial constructed, as shown in the photograph. As the end points of the potentiometer travel have been marked the dial can be removed for finishing or copying and then replaced without losing calibration.

		BRATION CAP.	
	100	220	470
	120	270*	560*
	150	330*	680*
	180	390*	820
		1000	
ing oth 270	ier valu 120 +	s marked * may be les in paraliel, as f 150 330 150 180 560 220 680 220 4 180	4 180 - 180 150

EXTENDING RANGE

As shown, the maximum capacity indicated on the dial is 1000 x 1000pF or 1μ F but it was later found possible to extend this range to 10μ F enabling small value electrolytic capacitors to be checked, although it should be remarked that there is no polarising voltage applied to the capacitor under test. Nevertheless the bridge has been found very useful for this purpose.

The accuracy of this extension to 10μ F will depend upon the accuracy of a 1μ F capacitor that is required for calibration. Again, a 5% tolerance will do as a 1% capacitor of this value is rather expensive. Connect across the test terminals and locate a null near to the bottom end of the travel, past the 1000 mark. The multiplier should be on x1000. The point can be marked 10nF for simplicity. Only two or three intermediate points are required such as 2200, 4700 and 6800.

IN USE

Normally the null will be very deep and sharp. In my own case, the audio tone actually disappears at the null point and I generally consider my hearing

★ components list

Resist R1		W R2	/3 1MΩ 10% ± or ±W
VRI			ntiometer. See text
Capad	itors		
C1	1000pF 10%	C5	0.01µF 1% SM or
C2	1000pF 10%		Polystyrene
C3	100pF 1% SM	C6	0-1#F 1% Poly-
C4	1000pF 1% SM		styrene
		C7	100µF 16V electrolytic
Calib	ration Capacitors	see	
	laneous		
			none, Battery 9V PP3,
			i, Veroboard 0-15in.
matr	ix, approx. 2} x 1	in. Kno	b and dial. Terminals
(2). (Case and panel 5	x 21 x	1Hn. deep (Stella 99
serie	S. from E. R. Nicl	halls 4b	Lowfield Rd., Stock-

to be better than average. If the null is not deep and seems to be undefined then the capacitor is probably leaky although it may be of the order of a few megohms. The effect can be simulated by connecting a high value resistor across a known good capacitor and testing the combination on the bridge. The lower the resistance the poorer will be the null. In the long run it is better to destroy such leaky capacitors at the time of testing rather than to leave them around to be used in equipment where the leakage might prove highly detrimental to the operation of a circuit.

AUDIO OSCILLATOR

The bridge can also be used as a source of audio tone for testing amplifiers and suchlike, the output being taken from the test terminals and adjustable from zero to maximum output with the potentiometer. The waveform is very rough, of course, coming from a multivibrator but quite adequate for general audio testing. If a Morse key is connected across the on/off switch the unit can be used as a Morse code practice set. A second crystal earpiece can be connected across the test terminals and, if two keys are connected in parallel, two-way simulated signalling will be possible.



presented last month



TELEVISION

IN THE DECEMBER ISSUE

SIGNAL STRENGTH METER

Correct aerial alignment is important if bright, sharp pictures free from blurring due to multipath reception, stably synchronised and with accurate grain-tree colour are to be achieved. This is difficult without a signal strength meter since the receiver's a.g.c. system will hide signal strength variations—quite apart from the physical problems. The TV signal strength meter described is portable and can be used to ensure that any u.h.f. TV aerial is aligned for optimum reception: it is equally useful in local and fringe areas. Features include varicap tuning, three gain ranges and a unique indicator of vision carrier reception by means of a light-emitting diode. Construction is easy since a ready-made surplus i.f. strip is used.

DECODER FAULT-FINDING

Colour receiver decoders are generally reliable but when they do give trouble fault-finding can be a headache. In "Practical Decoder Fault Finding" in this issue a number of useful hints and tips based on practical experience are given together with guidance on the logical approach to tracing faults.

SELF-CONVERGING COLOUR C.R.T.S

The next generation of colour sets-already beginning to appear on the market---will be fitted with self-converging c.r.t./deflection yoke systems. How these operate, with particular reference to the Mitsubishi SSS tube, will be described.

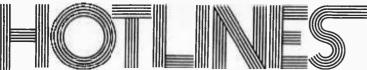
SERVICING TELEVISION RECEIVERS

The Baird/Radio Rentals 660, 670 and 680 series of TV receivers and their faults will be described by Les Lawry-Johns.

PLUS ALL THE REGULAR FEATURES

TO ______(Name of Newsagent) Please reserve(deliver the DECEMBER issue of TELEVISION (25p) and continue every month until further notice. NAME ADDRESS

i



MEASUREMENT

IT never ceases to amaze me that measurement in electronics gets more and more sophisticated as every day passes. On reflection this must be so because as the very latest devices are born, some means must be to hand with which to measure. accurately, their performance. At the recent International Microwave Exhibition at Montreux, for example, there were switches shown which could switch at 26GHz-that's twentysix thousand million times every second! I might add that the man on the stand eagerly told me, "... and of course we're working on higher frequencies right now"

While frequency must be measured accurately, what about time? Latest to come to my attention is a time interval counter which is soon to be launched in America. The amazing thing about this one is that it has a resolution of 100 Femtoseconds, If you are not impressed then let me add that a Femtosecond is 0.001 of a picosecond and a picosecond is one millionth of a microsecond which, of course, is one millionth of the common or garden everyday household second. For the technical/boffin types it's 10-15 seconds. Just think if every Amateur radio station had one of these, it could tell its transmission frequency to a fraction of a cycle even at v.h.f.

TIMED CALCULATION

Electronic calculators and digital wrist watches always create interest but now I really have heard it all. The ultimate is about to be launched onto the market, something that will satisfy even the most pedantic of tiros. It's a digital wrist watch and calculator combined! The calculator part has a nine digit readout and offers forty functions. When it's not used as a calculator it functions as a digital watch. There are only 20 buttons on the calculator and here the designers have introduced a very crafty dodge.

Although only twenty buttons are employed (because of space considerations) there's a "shift key" which, when activated, gives the twenty buttons other functions thus

giving a 40 button capability. This shift key acts something like the shift key on a typewriter which allows the same keys to be either capital letters or small, lower case letters. The watch/calculator measures about 1.5in x 1.5in x 0.5in. deep. The first models are rumoured to be priced at around £200-£250 but they're not available yet and probably won't be for some time. The buttons, incidentally, are depressed with a small probe, or tip of a ballpoint pen as far as I can ascertain. Information is rather scant because this is a state of the art unit and the information is red hot.

SOLID-STATE C.R.T?

A colleague in Washington reports that the US Army may soon lay its hands on a liquid crystal display, which gives an 84-character output. It also might be used as a liquid crystal cathode ray tube. At present the company doing the development is waiting to get a Government grant with which to continue work. It is also rumoured that the prototype device is coupled up to a miniature warfare computer. If this development is well funded, it could be another avenue of development for the solid state c.r.t. for television receivers.

SOLID-STATE CAMERA

At the other end of the television signal-the camera, developments are pressing on with solid state sensors which will replace the vidicon camera tubes. This was highlighted at the recent conference on charge coupled devices (c.c.ds) which took place at Edinburgh University. Of great interest was mention (plus photograph) of a miniature entirely solid state television camera which was constructed by Bell Labs at Murray Hill, New Jersey. Another interesting fact about this television camera is that it is battery operated. The size was not mentioned but from objects in the photograph which include a ruler, it is judged to be of the order of 11cm x 6cm.

The camera uses a chip sensor which has 256 x 220 element array gives excellent results using NTSC scan rates and the author claims

ON RECENT DEVELOPMENTS.

that television image sensors with 525 and 625 line capability are now a viable product. It must be remembered that solid state cameras will not come in over night. At present, users of the "valve" type camera tubes have only to plug in a component and it works whereas these solid state items are still being developed. However, with the world shortage of silver and the search for some other means of photography, it isn't too difficult to see the amateur photographer of the future holding a tiny solid state twin lens reflex which records directly onto tape which can then be played back on the television receiver at home.

These CCD devices are well worth watching. New applications are coming up and are being enthusiastically worked on. To date they are being used in TV applications, infra red cameras, delay lines, telecommunications, memories for computers and are even employed to generate a s.s.b. signal.

IT'S SIMPLE!

The servicing of televison sets has taken a step nearer to being automated. Grundig colour television receivers are currently manufactured in modular form. A number of modules are used in a plug-in fashion, each unit looking after a specific function within the receiver.

The offending module (in the case of malfunction) is simply unplugged and either repaired immediately or just replaced and then repaired at leisure in the workshop.

Some 75% of the colour television circuitry is catered for in this way. Now, Grundig has taken care of the other 25% by adding a simple socket to the receivers. A small diagnostic unit is then simply plugged in. The circuitry is featured on the lid of the diagnostic box, and l.e.ds mounted in this circuit diagram illuminate to pinpoint any fault.





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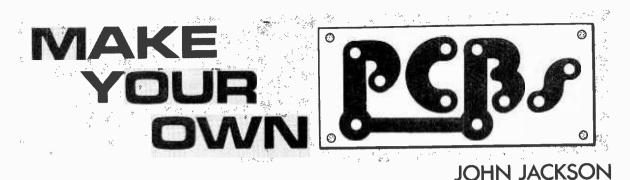


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For the amateur, printed circuit boards have good and bad points. They are neat, reduce free wiring, make assembly mistakes less likely and can support large items such as transformers. On the other hand, they take time to make and subsequent modification to them can be difficult.

Ready-made "universal" printed circuit boards may have no copper where it is required, will have it where it is not needed and mistakes during soldering are easy as different areas look alike. The design and preparation of individual boards is easy and the materials readily available.

DESIGN

The method used successfully for many projects is as follows. A fairly large copy of the circuit is drawn on thin paper, such as that used for typing (thin paper saves time later). All component junctions are ringed, as shown dotted in Fig. 1, to give the basic copper plan. Beneath this is drawn an outline, the size of the intended circuit board and, using components to check spacings, the basic plan is adapted to give a full size layout, Fig. 2. ... Tr1.1.1. A number can be crossed off each time a connection is allowed for.

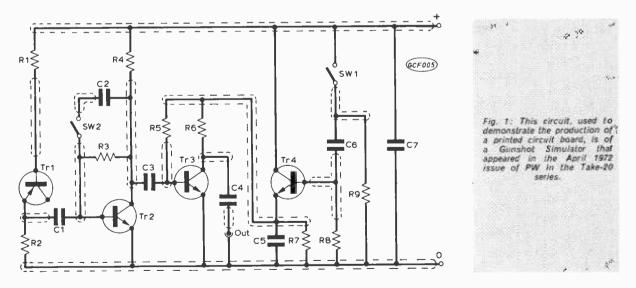
A negative of the plan must now be made. This is easily done by turning the paper over and drawing over the lines that should be visible. This plan is the master diagram, see Fig. 3.

It is possible to forget to reverse the plan, which is not serious with transistor circuits, but it will be tricky reversing a nine-pin valve-holder to match!

PREPARING THE BOARD

Copper laminate may be backed by fibreglass or SRBP, the latter being cheaper. Areas requiring copper, the "fields", are covered with resist and the unwanted metal is etched away. Resist can be from a purpose-made pen, such as a "Dalo" or use can be made of nail lacquer or paint (thinned enamel or cellulose).

First the board must be cut to size, with a hacksaw having a fine blade, cutting with the copper side up. After filing off any burred edges the copper must be thoroughly cleaned of grease or tarnish, using



In the final layout it is advisable to keep input and output points apart and wires leaving the board are better near the edges. Fixing holes must be taken into account and copper should not be too close to these, to prevent shorting to metalwork. To avoid missing a component, a list can be made with each component written once for each wire: R1,1, R2,2, scouring powder on cotton wool. After rinsing and drying on a soft cloth the copper is ready for the resist and the board must be held only at the edges, as any grease may cause the resist to flake off and prevent areas from etching.

The board is then stuck beneath the master diagram, with a piece of Sellotape to reduce handling,

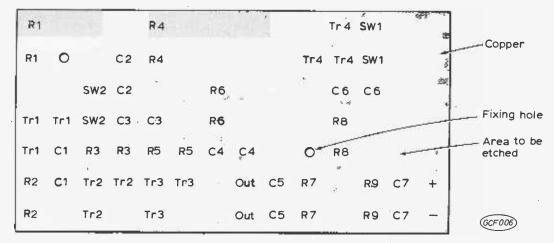


Fig. 2: The dotted areas of Fig. 1 are transferred to the paper master as shown here, the final layout depending upon the sizes of the components to be used. The copper will be on the other side of the board, which is shown here twice final size.

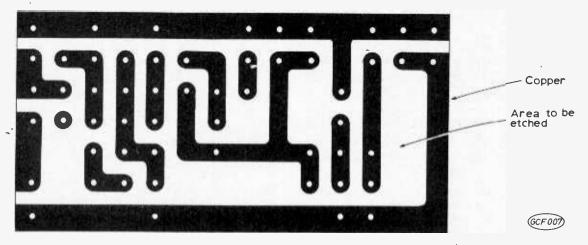


Fig. 3 When the layout is finalised it must be reversed on to the board as shown here, complete with the holes required, drilled after etching.

and a piece of carbon paper in between, carbon side down against the copper surface. Draw over the master with a pencil which will leave the outlines on the copper. Remove master and carbon paper after which the resist can be painted on the areas of copper which are to be retained. While the resist dries the etching solution can be prepared.

ETCHING

Ferric chloride is used which can be bought from advertisers in this magazine. One pound will etch many boards. A suitable strength is about one tablespoon per fluid ounce of water. The crystals should be added to the water, not vice versa, and this should be done with care as a lot of heat is generated. The solution may attack skin if splashes are not rinsed off and it will stain cloth and wood, so work over newspaper. The solution must be used in a non-metal dish, a saucer is ideal, and after use it can be stored in an old bottle with a plastic top.

If the prepared board is carefully levered off the paper, the Sellotape can be used as a handle. The board is placed gently on the etching solution **copper side down**. Surface tension will support it and the insoluble etching product can sink to the bottom, no agitation being necessary. After five minutes or so lift the board and see that all the copper shows pink. Greasy finger marks show brown and unetched. If all is well, allow the process to continue, taking roughly twenty minutes. When all the unwanted copper has gone the board should be thoroughly rinsed with water and then the resist can be removed. "Dalo" or nail varnish will come off with nail varnish remover (acetone) while paint will require white spirit or stripper. A final wash with soapy water will leave the board ready for drilling.

DRILLING AND SOLDERING

Drilling should be done with as fine a drill as possible, for a hand drill this will be about ¹16 in. dia. The slow speed on an electric drill is suitable but only gentle pressure must be used or the board will crack. It will be helpful to mark all the holes with a sharp point (a centre punch will not do) first, then hold the board in front of a piece of wood, in a vice, and drill all the holes. Any burrs can be removed with a larger drill. The board is now ready for use.

The bond holding the copper to the board material is strong but too much applied heat may cause the copper to peel off. As usual, resistors and other passive components should be soldered before semiconductors, though connecting wires should be left until last.

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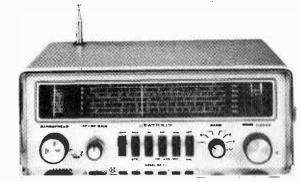
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Pin insertion

689

570 cutter

227

140 VOLT

25 VOLT 40 VOL1 47µF 61p 470µF 100µF 5p 680µF 120µF 100 100 100 220µF 100 2200µF 470µF 132 200µF 680µF 20p 1000µF 22p 63 VOL1 5000µF 68p 2:2µF 4.7µF

68p \$1

57 p 41 41

227

19p 25p 25p 44p

6 ip 10p 11p 12p 22p 22p 24p

Resistors	Veroboard	
* wait 5%, carbon 3.9 ohns to 10 meg 1p * wait 5%, carbon 3.9 ohns to 10 meg 1p * wait 2%, m/o 10 ohns to 1 meg 4p * wait 5%, carbon 5.6 ohns to 10 meg 8p * wait wirewound 1 ohn to 6K8 ohns 10p * wait wirewound """ 10 wait wirewound """	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	Pin insert tool Spot face cutter Pht 50
Volume Controls Potentiometers Carbon track 1k to 2meg Log of Linear Single Dual Gang Stereo Single type with D.P. Switch 32p	Electrolytic Capacitors	Pins
Miniature Presets Carbon Skeleton type All values 100 ohms to 5 meg ohms -1 watt 6p each -25 watt 7p each	4 VOLT 47μF 6ip 220μF 8p 100μF 6ip 320μF 10p 200μF 6ip 470μF 10p 320μF 6ip 1000μF 11p 1000μF 13p 1500μF 30p 4700μF 32p 2200μF 34p	100μF 150μF 220μF 470μF 18
Neons Smm neou indicators Bed or Amber 26p each at 6v, 12v, 28v, 110v or 230 volt.	6-8 VOLT 16 VOLT 33μF 6ip 15μF 6ip 68μF 6ip 33μF 6ip 150μF 6ip 150μF 6ip	1000µF 25
miniature neon lamps 240v or 110v 6p cach	470µF 11p 150µF 3p 680µF 18p 220µF 9p 1500µF 18p 680µF 17p	40 VOLT
Bilver Mica 350v DC, ±1% Values in pFe 3-2 to 220pF, 11p; 250 to 820pF,(15p; 1006 to 1800pF, 17p; 2200pF, 19p; 2700, 3600-F, 24p; 4700, 5000pF, 33p; 6800pF, 44p; 8200, 10,000pF, 55p.	2200µF 189 1000µF 179 3300µF 289 1500µF 259 10 VOLT 22µF 649 25 VOLT	6-8μF 15μF 33μF 67μF 68μF 10
Tantaium Bead Bolid tantaium capacitors Tol ±20%.		100μF 9 220μF 11
All values 20p each. MF/voltage: 1/35, 22/35, 33/35, 47/35, 1/35, 2.2/35, 4-7/35, 10/6.3, 10/16, 10/25, 22/16, 47/6.3, 100/3,	Ceramics Miniature Ceramics 50v D All values 1.8pF of 10,000	
Mullards Polyester Capacitors C250 SERIES 250V P.C. mounting: 0-1µF, 0-015, 0-022 Sip. 0-033, 0-4 0-68 152, 1µF 149, 1-5µF SEP, 2-2µF S7p. C390 SERIES C00V. 4-011 P. 0-011 P. 0-012 A. 0.012 P. 0.012 P.)·22 51p . 0·3

4p. 0.1 4ip. 0.15, 0.22 5ip. 0.33 7p. 0.47 9ip.

usso santas 400° : 0-001μF, 0-0015, 0-0022, 0-0033, 0-0047 8p, 0-0068, 0-01, 0-015, 0-022, 0-033 8 ip, 0-047, 0-068, 0-1 4 ip, 0.15 6 ip, 9.22 8 ip, 0-53 18p, 0-047, 14 ip, 100° : 0-01μF, 0-015, 0-022, 0-033, 0-047, 0-068 8 ip, 0-1 4p, 0-15 4p, 0-14 ip, 0-15, 0-22 8 ip, 0-33 7p, 0-47 9 ip 0-68 12p, 1μF 14 ip, 1-5μF 53p, 2-2μF 54p.

\$1 \$1 \$1 \$1 \$1 \$1 \$1	EI BARGAIN PACKS 10 Silicon ngn power transistors (2N3055), tested/un- marked. 30 Piastic FET's unmarked/untested. Similar to 2N3019. 20 TOS transistors ngn 2 to 54, untested/unmarked. 20 TOS transistors ngn jike BC176, BC179, etc., untested/ unmarked. 30 Flastic 2N3055, unmarked/untested. TO220 case. 30 Elastic 2N3055, unmarked/untested. TO220 case.
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THIS receiver accessory allows the reception of CW (Morse) and SSB (single sideband) signals particularly with receivers whose coverage includes any of the amateur bands. These bands are given below for the guidance of listeners who have not so far paid much attention to them.

160					2·0MHz
80	metres	or	$3 \cdot 5$	to	3.8MHz
40	metres	or	$7 \cdot 0$	to	7·1MHz
20	metres	or	14.0	to	$14 \cdot 35 MHz$
15	metres				21 · 45MHz
10	metres	or	28.0	to	29 · 7MHz

Short wave broadcasts use AM (amplitude modulation) and an envelope detector in the receiver demodulates this but this detector cannot provide the wanted audio output with CW or SSB signals. CW will be heard as an intermittent clicking and SSB as an unintelligible sound varying at syllabic rate. To receive CW a signal from the beat frequency oscillator is combined with the carrier, provided by the CW transmission, the difference in frequency between BFO and CW signals providing an audio output after detection. As a superhet receiver converts all incoming signals to a frequency of, usually, about 470kHz (the intermediate frequency) the BFO is adjustable around this frequency. So if the BFO is set to 469kHz or 471kHz the CW is heard as a 1kHz audio tone.

With SSB the carrier and one sideband are suppressed before transmission. When the BFO is adjusted to occupy the position of the missing carrier the transmission can be resolved and the detector provides intelligible speech.

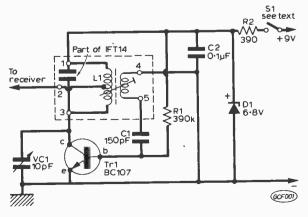


Fig. 1 : Circuit of the simple beat frequency oscillator.



BFO CIRCUIT

This is shown in Fig. 1. The frequency is determined by the coil L1, with fine manual adjustment by the variable capacitor VC1. The coil is suitable for receivers with an intermediate frequency of about 455kHz to 470kHz but the actual frequency need not be known. Windings must be in the phase shown, to secure oscillation.

It is quite a good plan to operate the BFO from its own 9V battery, the zener voltage regulator is not then necessary as satisfactory results can be obtained without it. But if current is taken from the battery running the receiver the current drawn by the receiver will vary considerably, especially at high volume level, so that stable operation of the BFO is impossible. In these circumstances, the zener is required for satisfactory reception.

ASSEMBLY

The components are assembled on a small piece of perforated board, Fig. 2, with wiring underneath. The two points MC are $^{1}_{2}$ in. 6BA bolts, with tags, providing the chassis or negative return.

A piece of aluminium about $3x1^{3}_{4}$ in is bent at right-angles about 1^{3}_{4} in from one end. The pitch capacitor VC1 is fitted to the smaller flange. The other flange is drilled for the two 6BA bolts mentioned, so that the wired board can be locked in place, with leads and joints clear of the metal. Connect the variable capacitor fixed plates to pin 3 on L1, and the moving plates to one MC tag, Fig. 2.

C2 0(1#F 2 D1 Zener diode 6 BV	R1 390kΩ R2 390Ω C1 150pF	VC1 10pF (Jackson C804) Tr1 BC107 L1 Denco IFT14 D1 Zener diode 6-8V
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TESTING THE BFO

components list

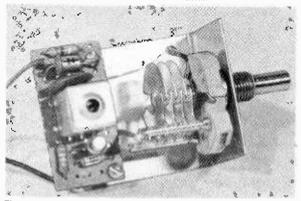
Set VC1 half open. Tune in any AM signal on the receiver. Place an **insulated** lead from pin 2 of L1 near the IF circuitry of the receiver. Connect the BFO to the 9V supply to be used. Rotating the core of L1 with a trimming tool should result in a setting being found where an audio tone arises. Set the core to the central or zero-beat position. If the core is rotated either way from this position an audio tone will be produced, rising in pitch as the core is turned.

Rotating VCl should now give a similar result. That is, a rising audio tone as the capacitor is rotated either way from the central or zero-beat position.

The BFO is not used for AM reception and slight re-setting of the core may be necessary after the unit is fitted in its case, if it is found that VC1 comes at the fully open or fully closed position.

BFO LOCATION

The BFO unit is only about $2^{1}_{4x}1^{3}_{4x}1^{1}_{2in}$ so it may be fitted in almost any receiver, especially homeconstructed types. A reasonably large control knob is best on VC1 and an on-off switch is necessary in the battery positive lead to the unit.



The unit itself is very small indeed so it can be fitted into a convenient corner in any receiver requiring a BFO.

It may be preferred to have the BFO as an external unit, with its own battery, when it can then be used with any receiver. To avoid troublesome handcapacity effects, the unit must be in a metal box. A box about $6x3x2^{1}2in$ with a backplate fixed with self-tapping screws will be suitable. This will also take a 9V battery and switch.

COUPLING TO RECEIVER

A short insulated lead from pin 2 of L1, placed near the receiver or near the receiver IF stages, should normally give suitable coupling which is not too critical. Much looser coupling to the earlier IF

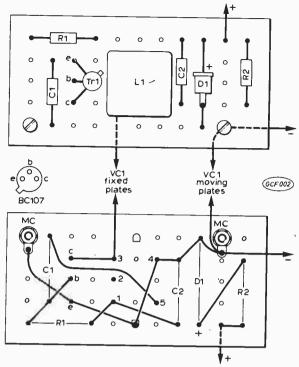


Fig. 2: Layout of components on top of the Veroboard and wiring beneath.

circuits will be required than to those at the diode end of the IF amplifier.

If coupling is too close, receiver sensitivity will fall off considerably when the BFO is switched on. Should coupling be too weak, strong SSB or CW signals will be difficult to resolve, while weak SSB or CW will be resolved easily. However, it should be an easy matter to move the lead from the BFO, or to cut it down, until results are satisfactory.

RECEIVING CW and SSB

Morse signals should be found easily in the amateur and other bands and VCl is simply rotated to produce a suitable audio tone. In some cases rotating VCl one side of the zero position may be found to give better reception than the other side.

To receive SSB, first tune in an amateur SSB signal, probably on 80m, with the BFO off. Switch the BFO on and rotate VC1 slowly until intelligible speech is produced. This requires quite careful adjustment. If the signal cannot be resolved, turn VC1 the other side of the zero position. This alternative position will in any case be necessary on the HF bands, where the upper sideband is usually employed compared to the lower sideband transmitted on the LF bands.

If the receiver is fitted with RF and audio gain controls, the audio gain should be near maximum and the RF control advanced as necessary, for best results on SSB.

VC1 need not be 10pF but larger values give more critical adjustment while smaller values may not give enough range of adjustment. Where the receiver has a fine tuning control this can be used for tuning SSB or CW signals, but if the receiver tuning does not allow very critical adjustment, VC1 can be used for this purpose, after locating the wanted signals.



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CACO SA-OR Carriage + 4-16 phms	The second second	STABILISE	<u>د</u>		
SOWY RMS 25-65V	5 . A	PS45	Suitt 2 5A25 or 2 \$A50 (4 ohm)	£4·45	Carcinge
SA100 £12-50 Cerriage * Continuously	10.40	MT45	Transformer for above	£3-50	Carrises 30p
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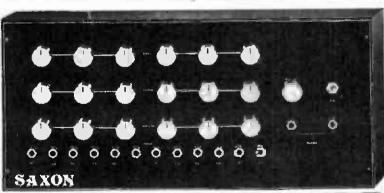
M4HL M6HL £19.50 Carr. £29.50 Carr. Sop Fasturing multiples of our VA30 module, the M4HL and M6HL fulfit the recoursements of all clubs, aroups, etc. where a high quality mixer is required. Each plus volume, trable and bass controls. Input imodances may, if required, be casily changed, The M4HL has four channels, and one output, and the M6HL dis changed (12 inputs) and a master control and two outputs, Either unit may be used free-standing or panel mounted. These mixers will feed all types of amplifier. Recommended for their values for Money.

MULTI-PURPOSE MIXERS

M4HL

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1



SAXON disco-module

saxon sound lite

A





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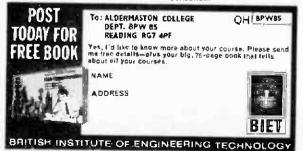
No matter how little you know now, no matter what your background or education, we'll teach you. Step by step, in simple casp-to-understand language, you piek up the secrets of radio and electronics.

radio and electronics. You become a man who makes things, not just another of the millions, who don't understand And you could pave the way to a great new carcer, to add in the thrult and pride you receive when you look at what you have achieved. Within weeks you could hold in your hand your own transitor radio. And aiter the course you can go on to acquire hishDowerd technical qualifications, because our farmous courses go right up to Citly & faulta levels. Send now for SREE

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wireless?

The early days of electronics were based very largely around the topic of radio. Things like computers and calculators are very much an afterthought. AMBIT is instigating a specialist sales and service line, just for AC electricity. From 10Hz to 1000 MHz. With our association with the largest producer of coils and filters in the world, namely TOKO, we think we have got a head start. Add to this our declared commitant to linear monolithic technology, and the result is the most advanced and comprehensive service available to the amateur or industry.

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A^S we go through the Age of Apollo with everything rocketing upwards the prices of dry batteries are no exception. The common PP7 9 volt battery, for example, costs around 33p at the moment and many transistor radios use two of these. Their useful life in a radio is very variable but one factor, above all else, determines how economical they are likely to be in the long run: the sensible use of the volume control.

Just about all transistor radios use output stages designed to operate in what is known as "Class B" conditions, where the current consumption is very low with no signal, rising as the signal input is increased so that low volume levels mean low battery consumption and longer battery life.

At 66p for a pair of PP7s it is immediately obvious that a mains operated power supply unit is going to pay for itself very quickly indeed, after which the cost of the electricity to operate the set is negligible. Taking a month as a typical life span for the batteries the cost of this power supply unit at under £3 could be written off in about four months. For our Senior Citizens and others similarly placed this is no mean saving.

Design

While power units for radios requiring 6 or 9 volts are common enough, units to replace $2 \times PP7$ batteries (18 volts) seem hard to come by. In the author's case, an Ultra 6142 LW, MW and VHF

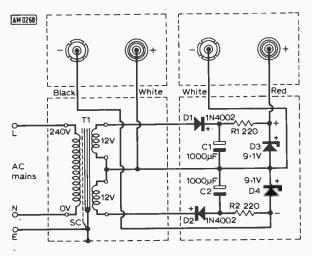


Fig. 1: Circuit of the power unit together with the connections to the terminals of the retained battery tops.

ARTHUR DOW

portable, it seemed logical to make up a power supply unit to fit in the same space as the batteries, so what better than to use the tin cases from a pair of defunct PP7s?

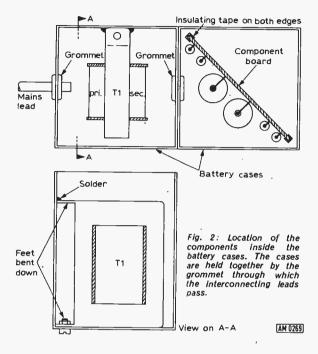
In the final circuit used, Fig. 1, one tin box carries the mains transformer T1, the 12 + 12 volts secondary windings going to the rectifier diodes D1 and D2, smoothing capacitors C1 and C2 and the zener diodes which stabilise the output voltage at $9 \cdot 1$ + 9.1 volts, all contained in the second box. The tops of the boxes carrying the terminals are retained and accept the original battery clips so that no alterations whatsoever need to be made to the radio set itself, a very important consideration. At any time the power unit can be slipped out of the set and normal batteries fitted back in a few seconds. In any other set a check ought to be made to with a voltmeter to ensure that the two batteries are, in fact, in series, requiring 18 volts. Otherwise, as long as the original battery polarities are adhered to, there should be universal use for this type of power unit.

Construction

Initially, two old PP7 type batteries are dealt with as follows: Mark the tops with the + and - signs, as shown on the side of the case, against the respective terminals. Cut across the corners at the top with a pair of sidecutters and ease back the edges until the top can be lifted out complete with battery. Cut the connecting wires or thin metal strips fairly close to the terminals and throw out the battery.

A hole of about $f_{\rm fs}$ in diameter is made in corresponding positions in each case and the two cases held together with a rubber grommet, Fig. 2, noting the polarity markings on the cases. Another hole is made for the mains lead to enter, again via a grommet. The position of this hole will be dictated by the position of the batteries in the set. In the Ultra 6142 a slot was filed at the bottom of one side of the cabinet, adjacent to the battery compartment, from which the mains lead was led out.

Next, all the components, with the exception of the transformer, are soldered on to the small piece of veroboard, Fig. 3, and lead-out wires attached. Some sort of colour coding for the wires is an advantage to avoid wiring errors. The board is fitted across the diagonal of one box and a couple of spots of adhesive will hold it in place. Be particularly careful that the polarity of the four diodes and the smoothing capacitors is carefully observed. The wires from the board are passed through the grommet with the exception of the one white and one red wire which are soldered to the + and terminals on one of the battery tops.



The mains transformer has two mounting feet which must be bent down, Fig. 2, one being fixed to the bottom of the box with a 6BA nut and bolt and the other soldered to the box just below the top. But, before fixing the transformer finally, feed a few inches of the mains lead through the grommet and connect to the primary winding taking the earth lead to the transformer's "screen" connection and to the case. Put a few turns of narrow insulation tape on the end of the mains lead inside the box to prevent the lead being pulled out. This may not be the best arrangement but space is rather limited inside the box. The wires from the board may now be connected to the transformer secondary with a white wire and a black wire going to the terminals on the second battery top, again noting the correct polarity. The transformer may now be dropped into the case and finally fixed into position. Some insulation tape was stuck across the core of the transformer at the top to prevent any possibility of a short circuit of the terminals immediately above. Likewise some tape was put across the top edge of the board in the other box.

Testing

Before replacing the tops in the cases it is a good idea to try out the power unit for correct operation. After checking the wiring again and the polarity of the various components connect a DC voltmeter across the red and black terminals. Select a voltmeter range of, say, 50 volts initially. Switch on the mains, when a reading of about 18 volts should be

★ components list

1/2	
11/6 0	220Ω 5% ‡ watt
21/2	1000µF 25V
01/2	1N4002
3/4	9-1V zener
15.2	(BZY88C9V1)
1	Transformer 240V/12V 12V
	(Douglas MT111CS)
erot	board. Grommets. Battery cases. Mains lead
	01/2 03/4

obtained, with 9 volts between the white wires and either black or red.

If everything appears correct put some insulating tape over the connections to the terminals and put the tops back into the cases finally turning over the edges of the cases to hold the tops in position. If thought necessary, the unit can be checked on the radio itself before fitting the tops back, connecting the battery leads from the set on to the power unit terminals. If there is something wrong it can be attended to now instead of having to open up the cases again. As a further check, the voltage across each of the smoothing capacitors should be about 16 volts.

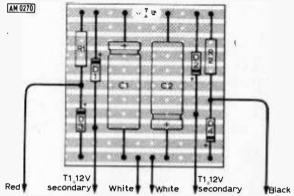


Fig. 3: Layout of components on small piece of Veroboard. Protect vertical edges and top with insulating tape or similar.

Notes

It should be remembered that the on/off switch on the radio set itself still only controls the DC output of the power unit to the set and not the mains input. Although the set consumes very little power from the mains it is still good practice to switch off the mains side when the set is not being used. The set switch can be left on permanently and operation of the set controlled by a switch at the mains outlet point.

The miniature mains transformer specified has a secondary current rating of 250mA which is far in excess of the 20/30mA which will be drawn by the average set. However, since it costs only a matter of a few pence more than the sub-miniature transformers rated at around 30/50mA the additional safety factor was thought to be well worth while. The light loading of the transformer will also assist the output voltage regulation of the unit.

If you're looking for trouble you needn't look any further.



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HE motor car is not an ideal environment for a tape player, or indeed for any electronic apparatus. In particular the problems of power supply regulation and electrical noise are far more acute than those likely to be encountered by a domestic machine.

ENVIRONMENT

The supply voltage, although nominally 12V, is likely to vary considerably under the loading conditions imposed by windscreen wipers and heaters, lights, etc. As a result we must produce a unit capable of working safely up to a possible maximum of around 15.5V, yet also maintaining a satisfactory performance down to 10V. For the amplifiers this is not too difficult-achieving a constant speed for the tape transport is not so straightforward.

Because a negative earth system is more or less universal on modern cars, the unit has been designed for this. Conversion to positive earth working is very simple, however, and will be described later: no change of components is required. Operation on 6V systems is not possible.

The construction of the tape-transport mechanism itself would of course be beyond the resources of the majority of our readers. It is therefore necessary to use a commercial mechanism. The one specified in the components list incorporates facilities for electronic speed control and also auto-stop and cassette ejection at the end of the tape. This feature is very necessary in a car where the machine must "look after itself" if the driver is fully occupied in manoeuvring his vehicle.

Interference from the car's electrical system seems to be worse with the modern alternator and solid-state regulator than it was with their predecessors. Power supply filtering and comprehensive screening are essential if the tape-head output, which is less than 500μ V, is not to be completely submerged in the hash.

Acoustic noise levels in the passenger compartment vary considerably from one car to another. The amplifiers used here provide over 3W rms output into 4Ω loudspeakers from a 12V supply: this should be adequate for pretty well any car.

TAPE AMPLIFIER

The amplifier system can be conveniently divided into three parts, a low-noise preamplifier, an equalisation section and a power amplifier. Silicon transistors are used in all but the power output stages.

A stereo cassette carries four tracks recorded on a tape only ${}^{1}_{8}$ in wide and running at $1{}^{7}_{8}$ in/sec. Hence the very low output level from the tape head. The amplifier input stage must therefore be designed for very low-noise performance. The technique adopted here uses complementary npn and pnp transistors, with the collector current of the first stage providing the base current of the second. The first transistor is thus operating under "starvation" conditions-a factor which greatly assists in the reduction of transistor noise.

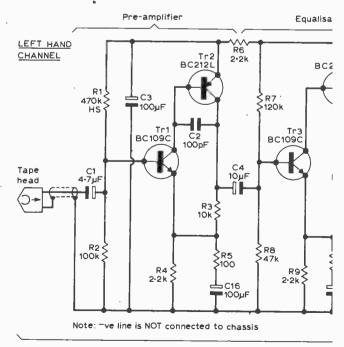


Fig. 1: Circuit of one channel of

PRACTICAL WIRELESS

some may not. It is a chance that the buyer takes.

pliers. If you are experimenting leave the wires long. Only shorten them when you wish to fit them in permanently or in u.h.f. work, where obtain the correct connections for ing iron (15 watts max.) and hold the wire being soldered with wiring the specimen you have obtained. Before you solder into the circuit, make sure that you know or can Do not overheat: use a small solderthe length may be critical.

Some transistors require heatsinks. Take care and observe instructions regarding fitting, insula-

Transistor holders are available for many types and like i.c.s they are worth using in experimental projects, but it is always better to solder in for permanent use. ting washers and position.

TRANSISTOR MOUNTING PADS

further provides a "seat" for the transistor to keep it clear of the to the transistor when handling, and These often-neglected but very cheap little components are recommended to give some measure of protection against accidental knocks component assembly board, so ensuring that the wires are properly protected and insulated.

5

TRIACS

24

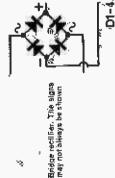
When triggered, triads will pass forward and reverse current; hence their use with a.c. The friggering an isolating 1:1 transformer for the achieve successful firing. Observe the high secondary voltage from the voltage and current is important to the main terminal connections mt1 and mt2 with respect to the gate. Note that the triac does not isolate low trigger voltage. If used with a.c. mains supplies It is wise to employ trigger signal.

PLUGS AND SOCKETS OR CONNECTORS





BRIDGE RECTIFIERS







CHOOSING

COMPONENTS

CAPACITORS

the the Colour coded capacitors can be identified by reference to the Practical Wireless Datacard No. 2 which working voltage and/or tolerance. was provided in the October 1973 capacitance and sometimes Markings usually identify ssue.

Capacitance

catalogue. Directory entry on page 14

petitive prices. Send 10p for

microfarads shown as μ F, mF, mfd.

nanofarads shown as nF, n, k, or kpf=1/1,000µF=1,000pF.

picofarads shown as pF, p, $\mu\mu$ F, mmfd=one millionth of 1μ F= 1/1,000nF.

Ч

ing voltage and shown as a number of volts d.c. (VWDC) or V d.c. or Voltage also known as the work-V a.c.

in applying a lower voltage, but the mum safe recommended voltage minals. There is no different effect stated voltage should not be ex-This value represents the maxithat should be applied to its terceeded.

supplied as substitutes, for example 0.47μ F instead of 0.5μ F or 0.022μ F instead of 0.02µF and so on. There ferred value" components to be is usually no detrimental effect by alternatives, as long as the specified substituting in this way with near It is quite common now for "prevoltage is not exceeded.

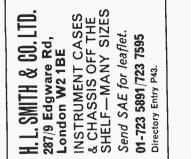
When using capacitors for a.c. mains (200 to 250V) such as for interference suppression, either a 270V (minimum) a.c. type or a 1,000V (minimum) d.c. type should be used.

The insulating material between the metallic foil or plates gives the Dielectric



BUYERS' GUIDE 1974/75

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mult x 1000000) CAPACITANCE CODE (BS 1852) Capacitors can be marked with their nominal value using figures and letters in place of the conventional code. The three multiplier $p = 10^{-13}$ $n = 10^{-6}$ $\mu = 10^{-6}$ mult x 1000) of the capacitance in FARADS. : Becomes (mult x 1) etters in common use are:---: 330p (1 p0 101 Nominal value 330рF 1000рF 4700рF 1⊭F 6-8µF colour ä

2

www.americ

PRACTICAL WIRELESS

now being superseded by plastics. failure symptoms. Paper types are number one suspect of capacitor down after a few years and are of use. Electrolytic capacitors break stable and reliable over long periods although more expensive, are more used, plastic types; for space saving and smoothing, electrolytic types can be tions are ceramic or silver mice text book on the subject). Generally capacitor specific properties (see types; for a.f. and h.f. use one of the the most suitable for r.f. applicaor tantalum types which

COILS

Ready made coils are usually designed for a specific application, hence they seldom carry any characteristic markings other than the makers code number. Unless their properties are known or can be measured accurately, there is little value in unmarked coils, if buying coil formers or bobbins for winding your own coils, check that you order or ask for all parts, especially if a brass or dust iron slug is to be used to adjust the inductance in a funed circuit.

DIODES

Because of the very small size of many - diodes it is not always possible to mark them with the full type number. Some are marked with very small lettering that needs a magnifying glass to read it. One end of the diode body is usually marked with a + sign or a band of distinguishing colour, or maybe black or white; this indicates the cathode terminal. Special types include "Varicap"

or similar variable capacitance diodes. The capacitance effect changes with a change in the applied voltage. This type is now frequently used in radio and television tuners.

> Zener diodes limit the applied voltage to the specified level and are very useful for regulating low voltage d.c. supplies.

FERRITES

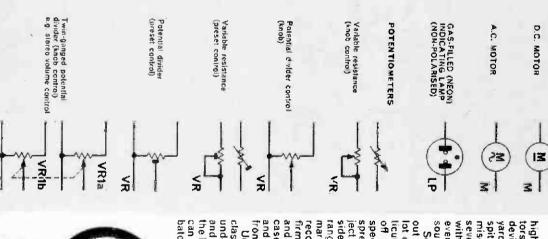
the pot, the bobbin, the clamps and you ask for all the necessary parts pot core assemblies make sure that detailed information consult manu-facturers' literature. When ordering be most effective over a pre-detersitic oscillation) pot cores, rods and beads (used for suppressing paraproperties are quite specific. Ferrite Often the cause of some mis-understanding, "ferrite" is a term tag strips. which usually include two halves or mined frequency range. For more materials and ceramic cores. Their takenly, to some kinds of dust iron now loosely applied, even mistoroids are specifically designed to

HEATSINKS

metals are not always suitable beproperties. cause of inferior heat conductivity are made from copper; alternative must be removed. Other heat sinks Any rough edges on drilled holes insulating washer and nylon fixings carefully achieved with the correct casing must, where required, be paint. Insulation from the transistor that the contact area is free from the electrical connection is required to should be painted matt black, but it and shape. If they are cast or moulded in aluminium alloy they Heatsinks vary enormously in size transistor casing, make sure

INTEGRATED CIRCUITS

In the limited space available it is not possible to give detailed suggestions on all types available; however, here are a few hints to observe.



BUYERS' GUIDE 1974/75

high, so many thousands of transistors (and other semiconductor devices) find their way into a scrap yard or on to the open market. In spite of precautions taken to minimise the number that are released, several do slip through, sometimes with makers' names on them. However, experts can otten identify the source by internal inspection. Sub-standard devices may turn

Sub-standard devices may turn out to be very good bargains; in a lot of cases they can be used, particularly for experimenting with oneoff projects, but It is unwise to specify such devices for widespread adoption in a particular project because of the variations outrange. They usually appear on the market as unmarked, re-marked or recoded types. In the latter case, a firm may have measured a batch and re-classified them, in which case you should identify the coding and obtain the correct specification from the supplier.

Unmarked devices cannot be Unmarked devices cannot be classified unless they are measured under normal operating conditions and with a proper instrument. For the low prices often asked, the buyer the low prices often asked, the buyer can expect to have a very mixed batch; some may be usable and



Directory entry on page 40

www.americanradiohistory.com

PRACTICAL WIRELESS

cumstances it is wise to measure tained at low cost and in these cirthe triggering voltage and current olerance. Thyristors can be obrequired to fire it. Also the "release" voltage should be measured

TRANSFORMERS

Well made transformers are often have flying leads connected to usually wound on cheeked bobbins. Cheap versions have no cheeks and the windings.

through the windings, otherwise quent overheating could occur. This Satisfy yourself that the physical size is large enough to handle the current expected to be passed saturation of the core and subseapplies particularly to mains transformers and valve output transformers.

2 Mains transformers with a screen between the primary and secondary reduce problems from mains borne interference and high frequency ransference. This screen must be windings are recommended. earthed with the laminations.

TRANSISTORS

Many problems arising from the purchase of transistors are due to misunderstandings about their characteristics.

characteristics, particularly on the Published data often give the range of gain for a particular type Transistors are made first, then measured and classified according to test measurements made on them. The result is a wide spread of gain (hre) and leakage current (lco).

type number have characteristics outside the quoted figures, then they are either classified into annumber. If transistors made for that other appropriate type number or rejected. The reject rate is fairly

















R









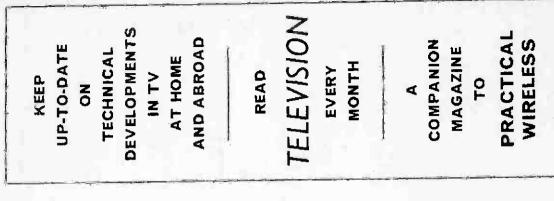
application. For example, you may buy a 7400 quad gate i.c. This device To be reasonably certain of get-ting a good specimen look for the ion so you are entitled to ask for a dard or "out-of-spec." items do a fault may be present on one of the unctional It could be used if the ault does not interfere with your manufacturer's official trade mark able. However, it does happen that oin connections. If it is otherwise as well as type number. Some specimens may not carry all this informa-'ull specification. Some sub-stanappear and in many cases are uswas designed to contain four gates, but if one gate is faulty you may still be able to use the other three.

assumed first grade i.c. may have an intermittent or faulty internal connection. If the device has been properly used in the circuit then the It can sometimes occur that an buyer could expect the supplier to replace it, unless it was declared as aulty at the time of purchase.

proving that the fault could have wise to use i.c. holders for this not expect the supplier to replace a aulty i.c. if it has not been operated However, a problem arises im-mediately if the device has been been there before it was soldered in or overheated soldering. It is always reason and to make removal of the .c. from the board easier. You canas recommended by the manufacsoldered and there is no way of or may have resulted from clumsy Urer.

Unmarked i.c.s or unidentifiable Even with test equipment it is almost impossible to ascertain the the supplier can offer some clue to the originally intended function. .c.s are seldom worth having unless properties of such devices. Whatever i.c.s you buy always ask for a data sheet or obtain a copy

BUYERS' GUIDE 1974/75



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giving the expected specification. tors. This is most valuable for pin connection identification as well as from the manufacturers or distribu-

correct position; i.c.s can be costly and difficult to replace. have the correct device in in, until you are satisfied that you A golden rule is never to solder very the

PRINTED CIRCUIT BOARDS P.C.B.s are mainly of two kinds:

Small soldering irons (15 watt maxi-mum) should be used; larger irons ally where it is in narrow strips lead to the copper cracking, especibending or flexing of any board can being more rigid and stable. Slight sive but is superior to s.r.b.p. board glass fibre board and s.r.b.p. Glass fibre board is more expen-

a fine toothed hacksaw. Glass fibre rapidly than s.r.b.p. tends to blunt the blade more A washing-up scouring pad or powder can be used with care. etching and again before soldering. When cutting the board always use must be thoroughly cleaned before tected and not tinned so the copper can melt the copper away. Most unetched board is unpro-

plane" and, a "ground-plane". The copper on clear of the copper on the "ground ponents should be mounted just etched or peeled away from holes side, the copper can be carefully one side is etched to suit the circui to avoid short-circuits. All com-Double-sided board is sometimes on the other (ground-plane) side to avoid short circuits.

some are able to supply etched boards for specific purposes and arrange Some Kits are available for etching p.c.b.s yourself. Read and follow the leave the bottle of solution open. instructions carefully and do not component suppliers to supply ready-etched a

> boards to individual design require ments.

sary. knite or adding link wires as necesbe done by either peeling away copper carefully with a sharp penconnection. Any modifications to to ensure a satisfactory soldered allowed where holes are required boards. Adequate copper must be constructors can etch their own printed circuit patterns for their the board after etching can easily projects where applicable so that Magazines usually publish the

POTENTIOMETERS

monly used for volume controls. bon tracks and can be obtained for vertical or horizontal mounting on exceeded trol, this rating should never be in particular with d.c. voltage conpotentiometers determines the curwirewound; logarithmic or linear rent that can be safely handled, and The maximum power rating of all types have open unprotected cartrack resistance. Skeleton prese ties to quote are: carbon track or resistance value, the other properous styles: Apart from the overall Potentiometers are made in vari-

RESISTORS

groups. The following information should be provided when ordering: tion will show many different A look at the directory classifica-

(b) Resistance in ohms, kilohms $(\Omega \times 1,000)$ or megohms $(\Omega \times 1,000)$ (a) Construction material e.g. carbon tilm, etc.

The tolerance, e.g. 1%, 2% etc. <u></u>

<u>ê</u>0 The power rating, e.g. 1, 1 wat etc.

> by the resistor in conjunction with mum current that can be handled tolerance are important factors to the application. The power rating quoted is an indication of the maxiwhere low thermal noise and close are more expensive and are used adequate for the application. the applied voltage, and should be Some of the high stability types

SWITCHES

nut. The wafer specifies the switchtainable in kit form and it is essentia ing mode, which is described later to ask for every part down to the last Common abbreviations used for Wafer switch assemblies are ob-

switches are: SP = single pole (one switch).

DP = double pole (two switches

3-pole = three switches operated operated simultaneously)

ST = single throw simultaneously, etc. ٩ on-ofi

DT = double throw or change runction.

4-pole, 3-way over function. tour switches each simultaneously, lets and operated having three out-

CO = changeover. usually on a wafer

MB = make before break. **BM** = break before make. MB

Centre-off applies where a toggle

or lever switch has two outlets and central neutral position.

THYRISTORS & TRIACS

Side triggering level which may be outways if they are not up to manutacbut in others they may be unreliable. The most common defect is the specimens may appear to function, some applications such low cost turers' published specification. In Thyristors can behave in various the manufacturer's quotec

ting the nominal value of the resistor has a single letter added to it rep-resenting the tolerance figure:---Examples :---TOLERANCE. The marking indicaresistor, thus:--which replaces the decimal point when indicating the value of the 6.2 7.5 9.1 and their decades. 1.0 1.2 1.5 1.8 2.2 2.7 3.3 3.9 4.7 5.6 6.8 8.2 together with their decades such as 47 470 4700 47000 etc. and tolerance using figures and of marking resistors with their value Increasing use is being made of the British Standards (BS 1852) method 1-1 1-3 1-6 2-0 2-4 3-0 3-6 4-3 5-1 the E24 Series by adding the following The E12 Series can be expanded to single letter:---The multiplier is represented by a letters only instead of a colour code. intermediate values:--as the E12 Series:--mon range of twelve values is known PREFERRED VALUES. The com-1K8G 120KJ 6R8M 2M2F signifies 2.2MO 1% 5-60 150 **RESISTANCE CODE (BS 1852)** R = x1 K = x1000 M = x1000000 18MΩ 47kΩ 1-2MΩ CAPACITORS (pF) **RESISTORS** (a) MARKING OF 330R 47K 18**M** 15R = = : ? (,, = x1) (multiplier = x1000) (multiplier = x1000) (mult = x1000000) AND 1-8kΩ 2% 120kΩ 5% (mult = x1000000)(multiplier = x1) 6-80 20% 150 10%



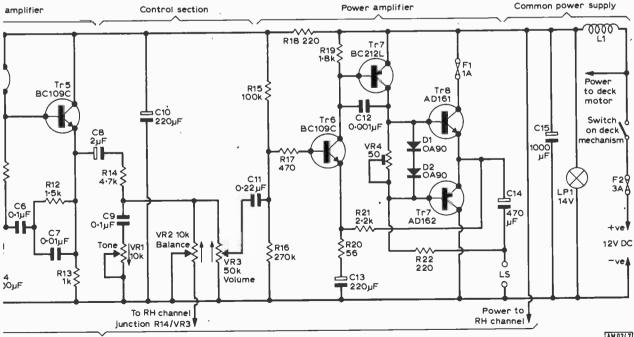
Transistor gain will vary from sample to sample and will also change with the supply voltage. To overcome these problems, negative feedback is used to stabilise the gain of the preamplifier.

The preamplifier has now raised the signal from the tape to a more reasonable level, but it still has a "Velocity characteristic"-that is, for every doubling of the recorded frequency the output level also doubles. This is because the tape head output level is proportional to the rate of change of magnetic flux due to the tape moving past the head. For a constant recorded amplitude, an increase in pitch of one octave (doubling of frequency) will cause the flux to change at twice the rate, and hence the output doubles also. It continues to double with each octave rise until tape head losses become significant at the higher frequencies.

At the time of recording, the higher frequencies are pre-emphasised or boosted relative to the low and middle frequencies. This means that the signalto-noise ratio of the tape is improved, since tape noise is predominantly at high frequencies.

From the foregoing it is obvious why we need to have an equalisation amplifier. This has a characteristic which is the inverse or "dual" of the overall tape curve. The output of this section has a flat frequency response over the audio range.

At this point the signal is suitable for feeding into the power amplifier, which uses a conventional complementary-symmetry circuit. The output voltage can swing between the two supply rails, less the residual voltage drop across each output transistor, say about 12-2=10V. The rms equivalent of this peak-to-peak voltage is approximately 3.6V which will produce about 3.25W using a 4Ω loudspeaker.



Right hand channel is identical

amplifier board, plus common power supply. NOTE.-The AD162 should be Tr 9.

AM 0247

★ components list

-		AMP	LIFIERS		
Resisto R1		Ba			
R1 R2	470kΩ	R9	2.2kΩ	R17	470\$2
	100kΩ	R10	10kΩ	R18	22011
R3	10kΩ	R11	47Ω	R19	1·8kΩ
R4	2 2kΩ	R12	1 -5kΩ	R20	5612
R5	100Ω	R13	1kΩ	R21	2 2kΩ
R6	2 2kΩ	R14	4 · 7kΩ	R22	22011
R7	120kΩ	R15	100kΩ		
R8	47kΩ	R16	270k\$1		
R1 IS	±₩ High	Stability	. R22 is 11	N 5% Re	emainder
are 👘	N 5% carl	oon.			à l
	ometers				
VR1 VR2	10412 100	(gange	t with othe	r channe	el)
VR2 VR3	10kΩ lin.				
VR3 VR4	50K12 100	(gange	d with othe	r channe	∋i)
VR4	50Ω hori	zontal p	reset		
0					
Capacit			-		
C1 4 C2 1	-7µF 6V T 00pF Cer.		C9 0·1/4	F Cer.	
	100µF Cer.		C10 220µ	F 16V	
	0//F 10V		C11 0-22 C12 0-00	41 10V 1	ant.
	00 / F 6V			IµF Cer.	
	1.1µF Poly			F 10V	
Č7 0	01 _N F Pol		C14 470µ C15 1000/		
	#F 10V		C15 1000/	wF 16V	
		n hand	Cer - Dis	r 6V	
Doly	- Tantaiui Dolyosto		ainder elect	sc ceran	nc
, vij -	- r viyeste	- Renie	amoer elec	aviyac	
Semico	nductors				
	13, Tr5, Tr	6	Tr8 AD16	1.)	hod
			Tr9 AD16		uệđ
Tr2. T	r4. Tr7 BC	912F	D1, D2 OA		
NOTE	-The abo	Vecom	onents are	for AnA	channel
only	All excent	C15 ar	d VR2 are	a dualic	ated for
the se	cond chan	nel	11 VILL 201	e dupace	
		incr.			
Miscella	upeous				
		or chok	e; LP1 14)	/ lamn:	
E1 1A	fuse wit	h chase	sis-mountii	na hold	er (two
	required	<u>}:</u>		.9 11414	
F2 3A	tuse with		holder:		
Casset	te mecha	nism,	enco FF	R. Stere	o with
D.C. n	notor;				
Verobe	oard 6 - 75 x	2.5in.0	1in pitch:	DIN con	nectors
for lou	Idspeaker	outputs	; 412 louds	speakers	metal
case; /	mounting	kits for "	Tr8, Tr9; ki	nobs, etc	C.
					1
	MOTOF	CONT	ROL BOA	ARD	

Resistors

R51 2·2kΩ		15Ω		100kΩ	
R52 6-8kΩ	R57	820Ω	R62	2 · 7kΩ	
R53 8-2k(2		5600		680Ω	
R54 1·5kΩ	R59	680Ω	R64	120Ω	
R55 3-911	R60	4-7kS2			
R55, R56 are ½W, VR51 1kΩ miniati	rema ure pr	tinder 🖁 W eset.	± 5%	5	

Capacitors

C51, C52 22µF 25V Electrolytic

Semiconductors D51—D53 BA100 Tr51, Tr54 BC109 Tr52 AD162 Tr53 AC128

Miscellaneous

Mounting kit for Tr52; pcb.

The use of class B output with output transformers could, with correct design, yield 10 watts per channel if needed. However, we have to consider the size, weight and economics of the machine, as well as the problems of obtaining specialised components. The complementary output stage produces as much power as is likely to be needed for practical purposes, and all components are easily obtainable.

PREAMPLIFIER

The circuit of the complete unit is shown in Fig. 1. It will be seen that the signal from the tape head is coupled to the base of transistor Tr1 via capacitor C1. The biasing of Tr1 base is set by R1 and R2. Resistor should be R1, a low-noise, high-stability type, but R2, the lower leg of the bias divider is effectively by-passed by the low impedance of the head so far as audio is concerned, and is a normal carbon type.

The collector of Tr1 connects directly to the base of the complementary pnp transistor, Tr2. The base current of Tr2 and the collector current of Tr1 are therefore the same.

We can now consider the DC stabilising action of the circuit. If the current in Tr1 increases, so does the base current of Tr2. This change is amplified by Tr2 so that its collector current increases. Thus, more current flows through R3, which in turn connects to R4. The voltage drop across R4 is almost entirely due to the current flow via R3, rather than current in Tr1 which is operating under "starvation" conditions. An increase in the collector current of Tr2 therefore causes the emitter of Tr1 to move positively towards the supply rail. This is equivalent to a negative shift of its base bias and the collector current of Tr1 is so reduced. The change is amplified by Tr2 and this heavy DC feedback action stabilises the working point of the complete preamplifier.

We do not need such heavy AC feedback—in fact appreciable AC gain is required. By decoupling R4 completely, a very high gain could be obtained, but it would be unpredictable and unstable. By introducing R5, the gain of the stage is set at about 100 by the ratio R3:R5 and is almost independent of voltage, temperature and transistor variations. The output from the preamplifier is therefore about 50mV. The supply to the preamp is decoupled by R6 and C3, and the output is coupled to the equalisation amplifier via capacitor C4.

EQUALISATION

The biasing method and stabilisation technique is the same as that employed in the preamplifier. However, an extra emitter-follower output stage is added which feeds both the Tone and Volume controls and the equalisation network comprising R11, C6, R12 and C7. The basic amplifier without equalisation would provide a gain determined by the ratio R10: R11, in this case, 200.

It is essential that the feedback network, which operates into the low impedance R11, should be fed from a low impedance source. If this were not the case, the response correction would be hopelessly inaccurate, as the network loads the source.

It will now be seen why Tr5, the emitter-follower stage, is included. It is DC coupled to Tr4 and provides a low impedance output. Basic correction for the velocity characteristic of the tape is provided by R12 and C6; C7 provides extra feedback to compensate for the tape pre-emphasis.

The equalised signal, which has now been amplified to around the 250mV level, is conveyed via C8 to R14 which is included to increase the impedance "seen" by the tone and balance networks. Resistor R14 forms the upper leg of a divider network, whose lower leg is formed by the Balance control VR2. This control operates differentially upon the two stereo channels, so that increased attenuation of one simultaneously results in an increase of output from the other. The tone control network consists of C9 and VR1. This is a simple "top cut" network which is adequate for use in the car.

Finally we come to the Volume control, VR3, which taps off the required output to drive the power amplifier.

POWER AMPLIFIER

The power amplifier consists of four transistors, Tr6, Tr7, Tr8 and Tr9. The latter two are complementary output transistors mounted on the backplate of the machine, which serves as a heat sink.

The action of the driver stage is similar to that of the previous amplifier. Transistor Tr6 has its base level set by R15 and R16. In this case, the level set is approximately half-way between the 12V rail and earth. Capacitor C12 is included to prevent RF instability, as is R17. The collector of Tr7 feeds the base of Tr8 directly, and the base of Tr9 via D1 and D2 and VR4, before reaching the collector load resistor R22.

Potentiometer VR4 sets the forward bias applied to the output transistors. In order to compensate for changes in temperature, diodes D1 and D2 are shunted across VR4. As the output transistors are germanium types, germanium diodes are used. When

the temperature increases (a condition which would cause increased conduction in Tr8 and Tr9) the impedance of the diodes falls, so decreasing the forward bias and stabilising the working conditions.

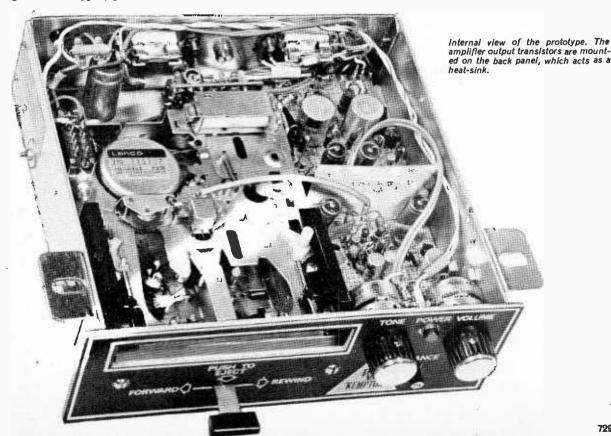
The emitters of Tr8 and Tr9 are connected via R21 to the emitter of Tr6, giving overall stabilisation of the DC working point of the amplifier. The emitter of Tr6 is decoupled by C13, and R20 is included to provide AC feedback in the ratio R21:R20, so stabilising the gain at around 40. If we consider a level of 200mV coming in from the volume control, this means we are just inside the overload point of the amplifier. The audio signal is coupled to the speaker via C14.

The loudspeaker also completes the DC return for R22. The audio output signal is in phase with that at the collector of Tr7 and hence there is positive feedback. This raises the input impedance of the output stage and enables the small transistor Tr7 to drive the output pair fully. This technique is known as "boot-strapping."

The output pair operate in class B. Forward bias is needed to prevent cross-over distortion, and VR4 is set up to provide a 10mA quiescent current measured at the fuse-holder. The fuse is connected in series with the collector of Tr8, to protect the output stage from conditions of gross overload.

The incoming supply from the vehicle is filtered by L1 and decoupled by C15. Power to the deck motor and panel light are also fed from this part of the circuit. The on-off switch is included as part of the tape deck mechanism.

The second part of the article describes the motor control circuitry and construction of the circuit boards.



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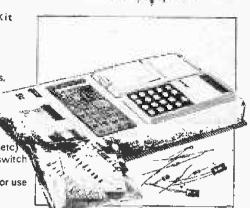
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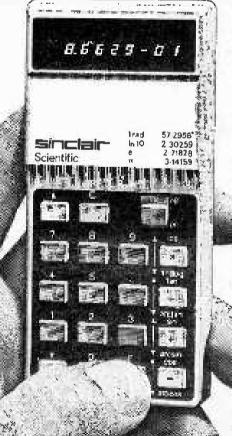
Components for Scientific Kit

- (illustrated)
- 1. Coil
- 2. LSI chip
- 3. Interface chips
- 4. Case mouldings, with buttons, windows and light-up display in position
- 5 Printed circuit board
- 6 Keyboard panel
- 7 Electronic components pack (diodes, resistors, capacitors, etc)
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- 9, Battery clips and on/off switch 10. Soft wallet
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- rd keyboard. ed for complex calculations.
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A series of simple transistor projects, using not more than twenty components.

NCE again we turn to that very useful integrated circuit, the SN7400, for a low-cost novel application, acting as the sensing circuitry for a photo detector. There are innumerable applications for this type of circuit. This particular one will operate in a multitude of roles without change to circuit layout or component values and possible uses range from burglar alarms to process control and object counters.

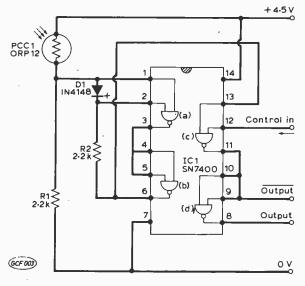


Fig. 1: Circuit of the photo trigger using an SN7409.

Photo detector

The photo detector itself is a photo-conductive cell, PCC1, which forms part of a potential divider circuit with R1. When the cell is illuminated the potential at the junction of these two components rises to some positive level, the actual level depending on the degree of illumination and on the value of R1. As long as this potential exceeds +3V, with the power supply of 4.5V the circuit will work satisfactorily. To achieve this level it is necessary to use a reasonable level of light such as the focussed beam of a small torch. In the absence of illumination PCC1 becomes a very high resistance and the potential referred to falls towards zero.

The potential is applied to the input of a trigger circuit comprising ICI (a) and (b). Positive feedback is achieved by R2 in conjunction with D1. Even though the controlling potential may rise slowly the regenerative feedback action causes the output of gate (b) to change rapidly and the change occurs as the input voltage moves around the +2.5V level. There is a certain amout of hysteresis built in and this is set by the value of R2.

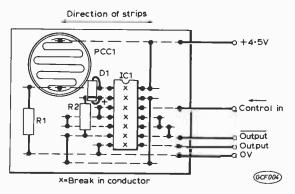


Fig. 2: Simple layout of the circuit using Veroboard.

The sense of the signal at the output of gate (b), pin 6 of the integrated circuit, is such that it rises to +5V when the cell is illuminated and falls to zero volts when the cell is obscured. We could have left the circuit at that stage and have said that the output was at pin 6; however we can make use of the other two gates within the integrated circuit to make the device more versatile.

Control operation

Firstly we introduce a control operation by means of gate (c). The control signal should come from a source impedance of $2k\Omega$ or less and should be a DC level of either OV or +4.5V. A control signal of OV will hold the output of gate (c) at +4.5Virrespective of what the photo detector might be sensing. We call the output signal at pin 11 the OUTPUT (NOT 'output') and use the final gate in the package (d) to invert this, thus, for the conditions stated, when the control signal is at OV the final output at pin 8 will be OV irrespective of the illuminating conditions. If the control signal is switched to +4.5V the output at pin 8 will be +4.5V when the cell is illuminated and OV when it is obscured. The OUTPUT signal at pin 11 will be the opposite of this.

Audio square wave

If desired, the control signal could be an audio frequency square wave. When the cell is in darkness the output at pin 8 will be zero volts but when illuminated the audio frequency will appear at the output. Should the control facility not be required pin 12 can be permanently wired to the positive supply rail. An advantage of having the complementary pair of outputs is that one can select the "bias" of the system; this is particularly useful if the output signals are to drive relays which may be required to be biassed either "ON" or "OFF".



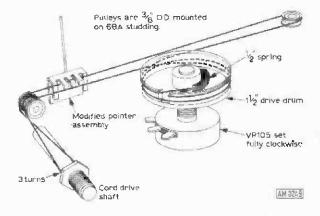
CONTROL PANEL

Front panel 9 ½ x 4 ½ x 16 swg aluminium

Dial backplate cut from $5\frac{3}{2} \times 1 \times 1$ aluminium angle

The layout of the prototype control panel is shown in the photographs. Since all functions are DC controlled the layout is not critical and can be altered to suit your own requirements. Also, as mentioned earlier, any features which you do not require may be omitted.

The manual tuning drive was constructed on a framework built mainly of aluminium angle, as shown in Fig. 8a. Details of the drive-cord arrangements are given in Fig. 8b.



A .

Fig. 8b: Drive cord stringing arrangements. The pointer assembly is modified by trimming the ends of the carriage to clear the pulley mountings and also inverting the pointer on the carriage.

A remby mounting bracket $3_4^* \times 3_4^*$ a luminium angle bolted to front panel

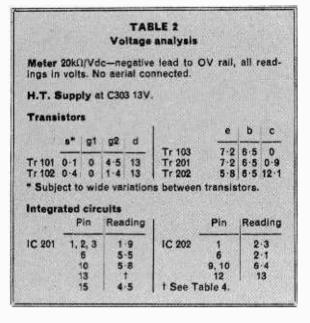
VR105 mounting bracket 2[°]x 1¹/₂[°]x 10swg aluminium

Fulley mounting bracket $5\frac{3}{4} \times \frac{5}{6} \times \frac{5}{8}$ aluminium angle (cut-out to clear drive cord)

Double bracket formed from 1"x 1" aluminium angle (space to suit cord drive shaft)

AM 0248

Fig. 8a: Construction of the prototype tuning and dial drive.



INITIAL TESTING AND SETTING UP

Before any RF adjustments are made it is wise to check the DC conditions at each stage in turn. A construction error or a faulty component is likely to produce an incorrect voltage in an associated part of the circuit. Table 2 shows the voltages to be expected at important points in the circuit when measured with a 20,000 ohms per volt meter, on the range most appropriate to the voltage to be measured.

Switch on and check the voltages appearing in the front end and oscillator stages. If they are correct connect the meter, on its $2 \cdot 5V$ or 3V range, to the positive end of VR104 which should be adjusted until a reading of $2 \cdot 0V$ is obtained with VR105 at minimum and S101 switched to Manual.

Now solder in R205 to apply power to the IF section and check the voltages against Table 2. Follow the same procedure with the demodulator and stereo decoder integrated circuits to complete the initial testing. The voltage appearing at pin 15 of IC201 indicates the strength of the signal at its input. A high reading here could indicate that a programme is being received or that there is some instability in the IF section. If rocking the tuning control does not reduce this voltage to the correct level, check that all the IC201 decoupling capacitors and the link joining the top and bottom earth planes are in place.

ALIGNMENT

When all the DC tests have been completed satisfactorily you are ready to move on to the final stage of construction, aligning the receiver. Connect two lengths of screened wire to the Left and Right audio output pads ready for attachment to the output socket. Remove the temporary earth wire and mount the receiver in the die-cast box. The earth connection is now made via the mounting stud in the power supply section of the pcb.

Connect a short length of wire from the centre pin of the aerial socket to L101, as shown in Fig. 7, and solder the audio output leads to the 5-pin DIN socket (Fig. 9). If your audio amplifier is earthed via its mains plug, avoid hum loops by breaking the earth connection between the tuner and the amplifier (which is made by the screen of the audio connecting lead) at a convenient point.

RF/IF ALIGNMENT

The method of alignment adopted depends on the facilities available to the constructor. Two methods are therefore proposed; the first requires the use of a VHF signal generator but the second needs only another, aligned, FM tuner.

FIRST METHOD

Short out the oscillator coil, L106, with a crocodile clip and connect the signal generator to the 'hot' end of L104. The output level of the generator should be set to about 1mV and the frequency set to the nominal centre frequency of the particular ceramic filter used. The filters are graded into batches of varying centre frequency, each frequency being identified by different colours. Table 3 lists the frequencies and their corresponding colours.

If a signal strength meter is not included a high impedence multimeter should be connected to pin 13 of IC201. By varying the frequency of the generator slightly about the nominal value it should be possible to detect a deflection on the signal strength meter or the multimeter. Once this has been found the core of the mixer load coil, L105, should be adjusted until maximum deflection is obtained. This circuit has a low Q so the peak is very broad.

Leaving the generator frequency unchanged remove the dustcore of L202. The tuning meter should now show only a slight deviation from the null position. Screwing in the core will make the tuning meter give a large deflection to the right, pass through the null position and deflect to the left before returning to the null.

This demonstrates the S-shaped curve of the detector, the correct position for the core being that which resulted in the null between the two large deflections. Slight variation of the generator frequency on either side of the null should now produce deflections of the tuning meter to the left and right.

To align the front end, first remove the clip from the oscillator coil and set the tuning voltage to the low end of its range. Sweep the generator frequency slowly over the range 80-100MHz when a deflection should be observed on the tuning meter or multimeter. Once this has been located, set the generator to 88MHz and separate or push together the turns on the oscillator coil to produce a maximum deflection again. Then transfer the signal generator to the tuner input and maximise the deflection by adjusting L101, 102, 104. As the signal strength reading increases, the output of the signal generator should be backed off to avoid overloading or oscillator pulling.

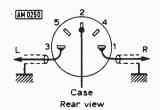
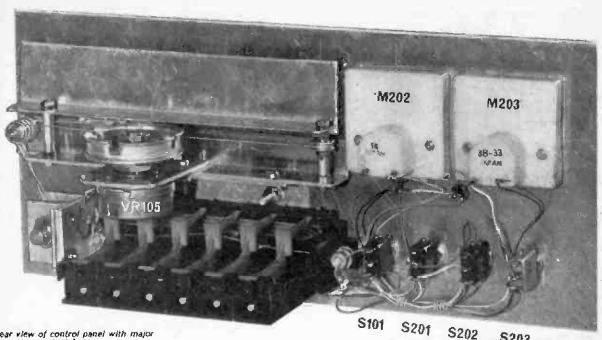


Fig. 9: Audio output connections to match DIN Standard amplifier Input socket.



Rear view of control panel with major companents identified.

Next change the tuning voltage to maximum, increase the generator frequency to 105MHz and restore its output to ImV. Vary the generator frequency about 105MHz until a signal strength meter deflection is obtained and bring this to a peak at this frequency by adjustment of VR101-103. The alignment at the bottom end of the scale does not have to be altered as the two adjustments do not interact when done in the manner described.

SECOND METHOD

This method may be used by those who do not have access to an RF signal generator. A second FM tuner, which must have an IF of 10.7MHz and a tuning meter, is used both as a signal generator and as a monitor to check the frequency of the local oscillator of the tuner which is being aligned. Connect a loop of wire to the aerial input of the second tuner and place it in the proximity of the oscillator of the first. Set VR105 to its low-voltage end and adjust L106 until the local oscillator appears as a carrier at 98.7MHz on the scale of the second tuner.

Now reverse the situation with the wire loop feeding the first tuner and the second tuner set to 88MHz. Adjust the tuning control of the first tuner until the tuning meter (or a multimeter connected as in the previous section) gives a deflection, indicating that the local oscillator of the second tuner is being received. L105 is now adjusted to maximise the response and L202 is adjusted as described in the previous section.

It now remains to align the RF circuits. Disconnect the wire loop and connect a good FM aerial. The sensitivity of the tuner is such that some stations will be received even if the RF stages are not correctly aligned. Set VRI01-103 to maximum voltage and tune in a signal near the bottom of the band (the local Radio 2 transmitter will usually be the most suitable). Now adjust L101, 102, 104 to produce maximum response on the signal strength meter. Adjust the presets VR101-103 with a signal towards the top of the band, a local radio station for example.

S203

DECODER ADJUSTMENTS

The alignment of the stereo decoder is very simple and requires no special equipment. With the receiver tuned to a stereo transmission the core of L203 is screwed in until the stereo indicator illuminates. The lamp will now remain illuminated over a range of several turns of the core and the correct setting is at the middle of this range.

The precision of this setting may be increased by use of the BBC test tone transmissions on Radio 3 each evening after the end of normal broadcasting. These transmissions include a tone in one channel only. With the tuner connected to an amplifier and speakers, the speaker of the channel with the tone should be disconnected and the setting of L203 varied to give minimum signal in the other channel.

USING THE TUNER

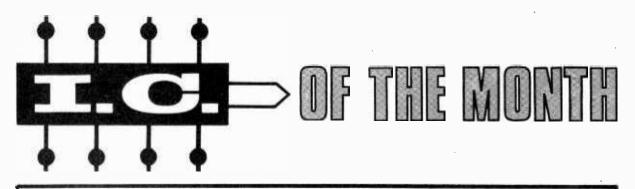
We would like to conclude this series of articles with a description of the tuner in use so that constructors can check the operation of their receivers and get the best use out of them.

The operation of the tuning meter is straightforward. The centre-zero meter should give a slight deflection to the left (low frequency) with no signal present. As the receiver is tuned through a transmission from the low frequency side the meter will deflect strongly to the left, pass through zero and then deflect to the right. The correct tuning point is at the central zero. For maximum accuracy, tuning should be carried out with the AFC off.

If the centre-zero tuning meter is omitted from the tuner the signal strength meter may be used as a tuning indicator by simply tuning for the maximum deflection. This method is, however, not as accurate. Table 4 shows the voltage at pin 13 of

--- continued on page 742

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Number 49

SGS TBA 790 AUDIO POWER AMPLIFIER

THE TBA 790 is an audio power amplifier integrated circuit available in various forms which have absolute maximum voltage ratings of 12, 15 and 18V and respectively providing maximum output powers of 1.2, 2.2 and 3.45W into an 8 ohm loudspeaker.

The TBA 790KSD

In this article we will discuss the TBA 790KSD device which has an 18V, 3 45W rating, having the type of encapsulation shown in Fig. 1. The bracket is permanently attached to the back of the device, acting as a small heat sink. The bracket contains two holes, tapped 6BA, by which it can be fastened to a larger additional heat sink. For most applications at normal room temperatures the additional heat sink is not required. However, the constructor will often find it convenient to bolt the device to a sheet of metal and this will help to cool it.

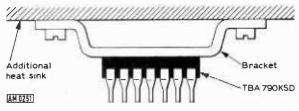


Fig. 1. The integral bracket of the IC provides the normal heat sink for the TBA 790 series.

The pins of this IC are in the quad-in-line configuration, the connections being shown in Fig. 2. Constructors are advised to solder directly to these pins, partly because sockets for quad-in-line devices are not easily obtainable and partly because the use of a socket renders spurious feedback more likely.

Circuit

A simple circuit for the use of the TBA 790 is shown in Fig. 3. The input impedance of the device itself is very high, typically 50 M Ω , and the circuit input impedance is therefore normally determined by R1. The high input impedance enables the circuit to be used with ceramic record player cartridges.

As the value of R2 is reduced, the amount of negative feedback decreases and the gain rises, being equal to 8000/R2. Thus if R2 is 100 ohms, the voltage gain is 80 or 38dB. R2 should not be less than about 39 ohms where the voltage gain is 200

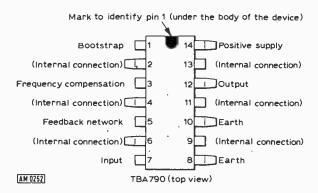


Fig. 2: Pin connections for the TBA 790. The heat sink is omitted for clarity.

or 46dB, since instability is likely at very high gain. The value of R2 should not, generally, be greater than about 200 ohms.

Frequency compensation

The components C2 and C3 provide frequency compensation. Ideally their values should be chosen according to the graph of Fig. 4, although these values are by no means critical. One should therefore estimate the gain required and then ascertain the value of R2 in Fig. 3. The value of C3 can then be read from the left hand side of Fig. 4 and the value of C2 from the right hand side of Fig. 4.

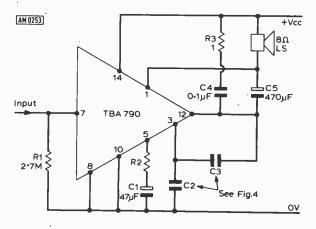


Fig. 3 : Bas ic circuit of the TBA 790 as an audio amplifier.

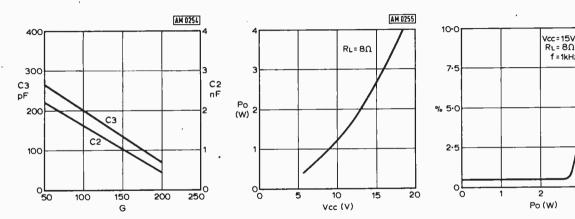
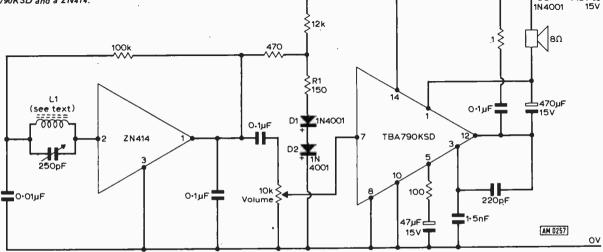


Fig. 4: above, graph for selecting values of C2 and C3 in Fig. 3. Fig. 5: centre, output power related to supply voltage. Fig. 6: right, distortion level at various output levels.

Fig. 7: below, is a practical circuit of a radio receiver using the TBA 790KSD and a ZN414.



Power supply

The maximum output power which can be obtained from the TBA 790KSD at various supply voltages is shown in Fig. 5 where an 8 ohm loudspeaker is employed. In general it is wise to regard the maximum power supply voltage as about 16V to allow a small margin of safety.

It can be seen that an output of just under 2W can be obtained when the device is used in a 12V , car radio, although more than 2W should be obtainable when the battery is being charged.

The quiescent current is only about 10mA at 15V or 7mA at 10V, but it will rise to around 1 to 3A when 3W is being delivered to an 8 ohm speaker. The efficiency (output power/input power) is typically 65 per cent at the 2.7W level.

The circuit shown has a frequency response which is 3dB down at about 70Hz and at about 12kHz. The use of a capacitor of larger value for C5 of Fig. 3 will extend the bass response, whilst the high frequency response can be altered by changing the value of C2 or C3.

The components R3 and C4 of Fig. 3 compensate for the speaker inductance.

The total harmonic distortion is plotted as a percentage against the output power in Fig. 6 for a 15V supply and an 8 ohm speaker. It can be seen that the total harmonic distortion is fairly constant

at a fraction of a per-cent until the power exceeds about 2.6W. It then rises rapidly with the onset of clipping to about 10 per cent at 3.4W.

Typical use

The writer has used the TBA 790SKD as the output stage of a very simple radio receiver employing the well known Ferranti 'ZN414. The circuit is shown in Fig. 7. The voltage gain of the audio amplifier has been set at about 80 which has been found to provide good volume. The two diodes D1 and D2 are forward-biased silicon diodes which stabilise the ZN414 supply voltage. If these diodes are replaced by a resistor, the receiver will not function satisfactorily over a range of supply The gain of the ZN414 circuit can be voltages. adjusted by altering R1, reducing it in value or removing it altogether if the ZN414 stage oscillates.

The diode D3 in the supply lead is included to prevent the destruction of the TBA 790 if the power supply is accidentally connected with the wrong polarity. It may be omitted if desired.

The coil L1 consisted of about 80 turns of 28 SWG enamelled copper wire close wound on a 4in. long ferrite rod. A long-wave coil of around 220 turns of much finer wire could be placed at the other end of the rod and switched into circuit to replace L1 if long wave reception is required.

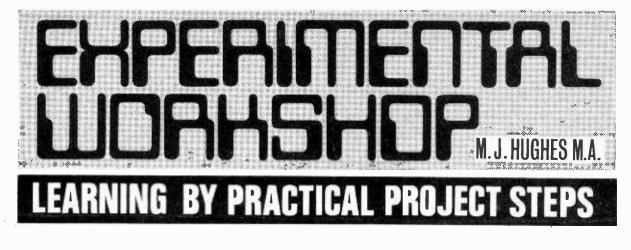
AM 0256

f=1kHz

3

+12V to

D3



PART 13—PHASE SHIFT CIRCUITS

THERE is more to a top cut filter than an attenuation factor, as described last month. Apart from the potential divider effect of the resistor and total circuit impedance on the input voltage, the circuit introduces what is called Phase delay. This means that when a sine wave signal is applied to the input we will see an attenuated sinewave at the output but the peaks and troughs of the wave will not occur at the same instances of time. To confuse the issue, the time discrepancy between input and output depends on the frequency of the signal we apply. This is not an easy feature to demonstrate without an oscilloscope but we hope the following experiment, coupled with a bit of thought, might clarify the situation a little.

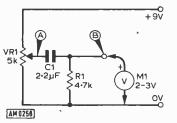


Fig. 90 : Experiment to show phase shift in a top cut filter.

In Fig. 90 we shall simulate an AC input signal by moving the wiper of VR1. Because we are limited to slow movements (low frequencies) we shall have to use a suitable high value capacitor for C1 so that useful signals can be measured on the meter M1. This meter must be sensitive, 20,000 ohms per volt, and switched to a low DC voltage range, about 2 or 3 volts. The voltage at "A" will be set by the potentiometer and can be anything in the range of 0 to +9V. We can, with a bit of manual dexterity, make this voltage follow a near sinusoidal pattern; to do this, start with the wiper at minimum voltage and rotate it, slowly at first, reaching a maximum speed of rotation at the half way point, then start to slow down gently until you reach the top end of its track. You should aim to slow down progressively, so that you don't suddenly stop when you reach the top. Having reached the top, peak positive voltage, immediately start turning the knob the other way, slowly at first, speeding up to the halfway point and

then slowing down as you reach the bottom end, again without an abrupt stop. This needs a bit of practice but it is not as difficult as it might at first appear. If you manage to do this satisfactorily the voltage at the wiper should approximate to a sine wave and if repeated over and over again should produce a waveform something like that shown in Fig. 91.

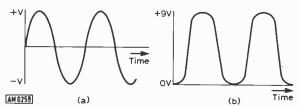


Fig. 91 : (a) Ideal sine wave oscillating about zero volts. (b) Approximate waveform from Fig. 90, oscillating between zero and +9V.

The thing to do now is to monitor the voltage at point "B" on the circuit as you go through the "sine wave" cycle. Initially make the cycle stretch over about two seconds and watch the meter closely. During the slow portion of the rising waveform the meter will read virtually nothing but as you speed up at the halfway point the meter voltage will rise. As you pass the halfway point and slow up towards maximum you should see that the meter voltage

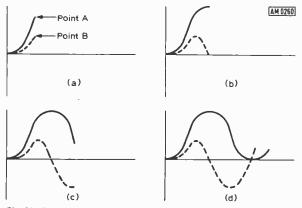


Fig. 92: Progressive construction of waveform obtained in Fig. 91 (b).

starts to fall back to zero and reaches zero just as you reach maximum voltage. The voltage you see on the meter should be proportional to the **rate** at which the input signal was changing. If you had an oscilloscope the output voltage would trace out the line shown in the progressives of Fig. 92.

When you turn the potentiometer in the opposite direction, describing the negative half of the input sine wave, the meter will try and read backwards so reverse its leads and you will find that a similar effect is produced in a negative direction. If you repeat this cycle many times you can imagine that the voltage at point B has the same sinusoidal shape as that at A but it is reduced in amplitude (attenuation by top cut filter action) and it reaches a positive peak as the input voltage is going through the centre part, the fast moving part, of its positive going swing. The voltage at B is zero when A is peak positive, maximum negative when A is moving in a negative direction and zero again when A is at its peak negative, zero volts, level. The final trace in Fig. 92 clearly shows that the voltages at B are out of step with those at A by a quarter of a wavelength.

Because a complete wavelength of a sinewave is a cyclic event we sometimes say it corresponds to a 360° cycle hence we can say a quarter of a wavelength is 90°. Using this nomenclature we can say there is a 90° phase shift between the input and output signals for this circuit, at the low frequencies we are considering.

If you had a signal generator instead of a potentiometer as an input signal and a double-beam oscilloscope monitoring the voltages at A and B you would see this more clearly. You would also see that if the frequency of the input signal were increased the amplitude of the output would increase but the phase shift would also start to reduce. As the input signal frequency becomes very high the phase difference approaches zero and the output becomes an almost exact replica of the input, both in phase and amplitude.

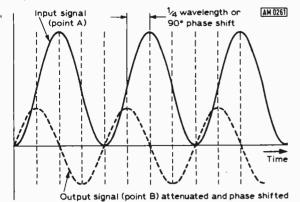


Fig. 93 : Curves showing 90 phase shift of LF signal through top cut filter.

We can thus say for a top cut filter:---

1. At very low frequencies we get 90° phase shift and heavy attenuation, Fig. 93.

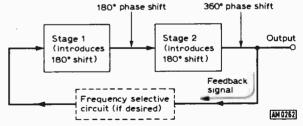
2. At very high frequencies we get no phase shift and little attenuation.

3. At intermediate frequencies we get a graded scale of phase shift (between 0° and 90°) and graded attenuation, depending on the frequency we choose, and, of course, on the values of the components in the filter.

This phase shift effect can be put to good service in certain types of oscillators. To obtain oscillation all we need is an amplifier with frequency selective positive feedback. This means that we have to take the output of the amplifier and at a certain frequency feed it back to the input with a phase relationship that enhances the output.

We have seen several examples of the opposite effect in amplifier stages, previously described in this series. Negative feedback was achieved by feeding the signal from the collector of a transistor back to its base. A single transistor stage, in grounded emitter configuration, has 180° phase shift between its input and output, when the input moves positive the output moves negative and vice versa. To get positive feedback we must arrange to feed back a signal that is in phase (i.e. having zero or 360° or any multiple of 360° phase shift).

One simple way of doing this is to use two transistor stages, one cascaded into the next. The output of the second stage will be 360° out of phase with the input to the first and this is equivalent to there being no overall phase shift. If we feed the output signal back to the input the circuit will oscillate at a frequency set by any frequency dependent components, capacitors or inductors, that form part of the loop, from input to output and back to the input again. If there are no such frequency sensitive devices and the amplifier is DC coupled then the oscillator becomes locked in one or two possible states (it tries to oscillate at zero frequency!!). This circuit is, in effect a bistable which has been described in a previous part.



This block diagram shows concept o an oscillator, producing zero phase shift, gain and frequency selective feedback.

For regenerative feedback to occur, a pre-requisite for oscillation, it is necessary for the gain of the amplifier to equal or exceed any signal losses in the feedback path. Positive feedback alone is not sufficient. We can turn the two transistor stage into a free running oscillator as shown in Fig. 94. The capacitors determine the frequency and, if looked at from a different view point, this circuit is very similar to a free running (astable) multivibrator. Changing the value of the capacitor in the feedback loop changes the frequency of oscillation; you can try this and, with the values given, the frequencies should be in the mid-audio range. Layout shown in Fig. 95.

If we accept that we can get 90° phase shift from a simple RC filter it might seem that two such filters cascaded into one another Fig. 96(a) would give us 180° phase shift. This would be true of signals of zero frequency but, apart from zero frequency being a rather impracticable concept when dealing with oscillators, the attenuation would be infinite and no measurable signal would be seen at the output. If, however, we extend the logic a little and consider three such filters connected together (Fig. 96(b)) there will be a specific frequency that undergoes 60°

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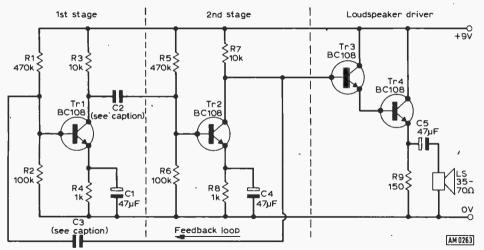
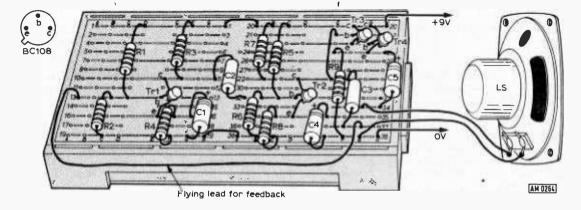


Fig. 94: Two stage amplifier converted to an oscillator, frequency being determined mainly by C2 and C3.



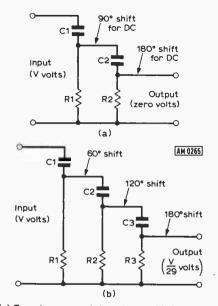


Fig. 96: (a) Two stages cascaded as shown will give theoretical 180° phase shift at zero frequency. (b) With three stages each stage will give 60° shift at a certain frequency giving 180° shift overall.

Fig. 95 : Layout for Fig. 94. Try values of 1000pF to 0.47 μF for C2 and C3 in any combination.

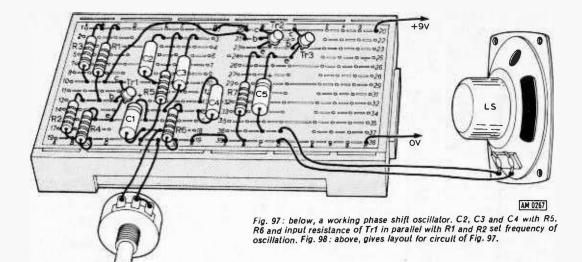
phase shift through each of the three stages. Three lots of 60° shift give 180° shift overall but this time we are no longer dealing with zero frequency; it will be a finite frequency and although there will be considerable attenuation it will certainly not be infinite and we can guarantee at least some measurable signal at the output for this particular frequency.

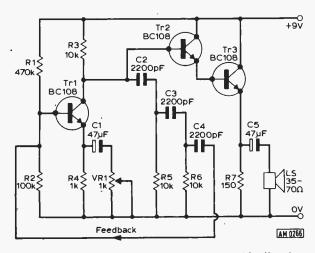
It can be shown that if each of the resistors in the three stage filter have values R (in ohms) and the capacitors are of equal value C (in farads) the frequency that is subjected to 180° phase shift is given by:—

$$f = \frac{1}{2\pi CR \sqrt{6}}$$

Because of the inter-relationships of impedance, reactance and frequency the attenuation for this circuit at this particular frequency is always a factor of 29.

We can now conceive using this network to replace the second transistor in our experimental circuit, to give 180° phase shift instead of the second transistor and simultaneously determine the frequency at which this phase shift occurs. By using this network in the feedback path of a single transistor stage we should be able to get regenerative feedback at a predetermined frequency provided that the voltage gain of





the single transistor stage exceeds 29. Ideally the gain of the amplifier should be greater than, but as near to 29 as possible, otherwise clipping will occur and providing the gain is just right the oscillator will produce a very pure sinusoidal output waveform. VR1 introduces a controllable amount of negative feedback and thus sets the gain of the amplifier, Fig. 97. Start with this set to maximum resistance and no oscillations will be heard in the loudspeaker; as it is reduced in value a pure note will be heard and reducing its value to zero will provide zero negative feedback, maximum gain, and some distortion might be heard in the loudspeaker as clipping starts to occur. The latter effect will depend on the transistor latent gain. Layout is given in Fig. 98.

This is a very useful and simply made oscillator for audio and sub-audio frequencies and is sometimes used for generating low frequency vibrato signals in electronic organs as it has a comparatively pure signal content. The only problems are that the gain of the amplifier needs setting carefully for optimum performance and that it is rather difficult to change its frequency of operation with a variable control. Small changes in frequency can be provided by varying the value of one or two of the resistors in the feedback loop by small amounts. The best way of setting the frequency to a predetermined value is to leave the resistors fixed and substitute different sets of capacitors in the feedback circuit.

Phase shift has many other useful applications in electronics and it can be obtained in other ways. Under some circumstances it can be detrimental and is sometimes encountered unexpectedly in audio amplifiers giving rise to undesirable.spurious oscillations.

Next month: Some more applications of positive feedback.

P.W. SANDOWN—continued from page 735

IC201 measured for various signal strengths for a typical tuner. This information may be used to calibrate the signal strength meter if required, although quite wide variations can be expected between tuners.

With the muting or squelch switched off there is considerable inter-station noise and the usual distorted output as the signal enters the edge of the tuner passband. With the squelch in operation the background should be silent until a noise-free signal is received. It should normally be left on unless a weak signal is being received.

TABLE 3 Filter centre frequencies		TABLE 4 Signal strength meter indication	
		Voltage at Pin 13,	Approx. signal level
Colour code	Centre frequency (MHz)	IC201 (v)	at aerial socket
1	(minta)	0.15-0.3	0
Orange	10-625	0.4	1µV
Yellow	10.665	1.3	10,4V
Green	10.700	2.0	100µV
Blue	10.735	3.0	1mV
Violet	10.775	4.6	10mV

The stereo defeat facility automatically inhibits the decoder when the signal falls below the level required for noise-free stereo. Alternatively the tuner can be held in the mono or the stereo mode independent of the signal level by moving the mode switch R203 to the appropriate position.

PRODUCTION LINES colin riches

EKCO ZU540

Sound Project ZU540 from Ekco is a tuner-amplifier/turntable/Dolby cassette tape recorder unit.

The Dolby noise reduction system operates on both record and playback. The v.h.f. varicap tuner employs 4 push-button pre-selectors plus free tuning and a built-in stereo decoder with beacon indicator.

The transcription-type 2-speed record player uses a Philips GP400 magneto-dynamic cartridge with a 15 micron diamond stylus.

There is a facility for using chrome dioxide tapes on the recorder and there is an automatic level control with a manual override.

An electronic tape-end auto stop allows for automatic 'pop-up' disengagement of the cassette keys.

Output power is quoted as 20W per channel into 4Ω .

I have tried out this unit and found it to give excellent quality reproduction through the DX181 speakers which come with the system.

I cannot give full details of the impressive specification in the limited space I have here but please write to Pye Limited, P.O. Box 49, Cambridge if you would like further details.

BANISH THE IRON!

Banish the soldering iron—that's what Radio and TV Components have done with their latest car radio kit.

All the electrical connections are made through colour-coded press-on tags and R and TV Ltd. claim that a complete novice can build it in under two hours.

The "Tourist TT" has five pushbuttons which can be tuned to any pre-selected station. Four operate on m.w. and one on l.w.

This new radio kit developed from the firm's very successful and efficient "Tourist" radio, utilises an i.c. and a p.c. board allied to tested sub-assemblies. Constructing the kit is simply a matter of fixing the various component assemblies to the chassis using the screws provided.

The kit features permeability tuning and long-wave coils to ensure good sensitivity and selectivity on both bands. The r.f. sensitivity at 1MHz is said to be better than 15μ V and power output into a 3Ω speaker is claimed to be better than 4W.

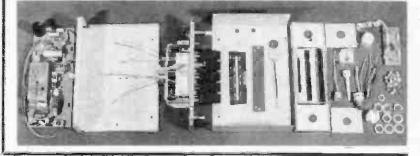
Both the tuner and the i.f. module are pre-aligned and the kit is suitable for 12V positive or negative operation.

The klt comes complete with stepby-step assembly instructions and instructions for installing the radio into the car Itself.

This excellent kit is available by post or direct from Radio and TV Components Ltd., 21 High Street, Acton, London, W.3. The price is £7 plus VAT. Postage and packing cost 55p.

Extras available are a speaker with baffle and fitting strips, at £1-65 (post and packing 23p) and a retractable, matched locking aerial for £1-37 (20p postage and packing).

We are publishing a Special Product Report on the "Tourist TT" car radio on page 704 of this issue of Practical Wireless.





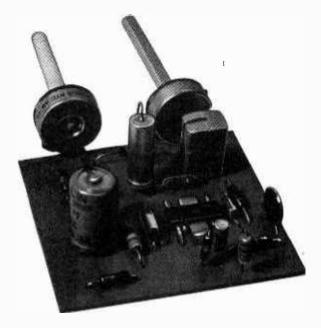
COMDEL SPEECH PROCESSOR

The Comdel CSP 11 is a communication aid designed for any system using a microphone for voice transmission. Its prime feature is the achievement of peak limiting without distortion which is the very undesirable by-product of conventional speech clippers. Therefore the average or 'talk power' gain obtained is more effective.

Features of the CSP 11 are: instantaneous limiting action; no appreciable distortion; talk power gain greater than 10dB; optimum frequency response for voice; installs in microphone lead; all silicon solid-state circuitry. The unit costs £55 (including VAT and postage and is available from Interface International, 29 Market Street, Crewkerne, Somerset.







IN the medium power range there is now a wide variety of i.c. audio amplifiers available, with power outputs ranging from 1 to 6 watts r.m.s. As with the majority of semiconductor devices, the prices of these have dropped in recent years and most now represent very good value for money.

This article describes an amplifier based on such an i.c., the Motorola MFC9020, which gives a maximum output power of 2W r.m.s. into a 15Ω load. A peak power of about 4W is available. In the configuration used here the device has a typical distortion level of approximately 0.5% at full output at 1kHz, with an input sensitivity of 250mV r.m.s.

The prototype was made for use as a tape recorder monitor amplifier, but as the input impedance is high it is also suitable for use in simple record playing equipment in conjunction with a crystal or ceramic cartridge. With the addition of a suitable preamplifier it would of course be suitable for many other applications.

The unit has built-in volume and simple tone controls. A circuit of a simple mains power unit for the amplifier is provided. A diagram of the internal circuit of the MFC9020 is shown in Fig. 1. Basically this is divided into two sections. The first four transistors form a differential amplifier while the other five form a fairly conventional complementary class B output stage.

Operation of the differential amplifier is quite simple. For high gain and input impedance this uses two darlington pairs. The first is used in the emitter follower mode, and the output of this stage is developed across the emitter resistor. The second darlington pair operates as a grounded base amplifier to the signals appearing across the emitter resistor. No voltage amplification is provided by the emitter follower stage which provides the circuit with a high input impedance and has a low enough output impedance to drive the grounded base stage. The grounded base stage does provide a degree of voltage amplification.

Neither an emitter follower, nor a grounded base stage provides any phase change to the signal, and so the input to pin 7 is in phase with the output at pin 5. There is a second input to the circuit at pin 8. For an input at pin 8 the second darlington pair will operate as a common emitter amplifier, with the amplified and inverted output appearing at pin 5. Thus pin 7 is a non-inverting input and pin 8 is an inverting input.

OUTPUT STAGE

This is quite conventional, the only unusual feature being that two transistors are used in the upper section, and three in the lower, rather than the more usual two in each section. The two silicon diodes connected across the two inputs to the two sections of the output stage operate as low voltage zeners, and provide a suitable bias for the output transistors to reduce cross-over distortion to an unnoticeable level. The diodes also provide temperature stabilisation of the output stage.

Under normal operating conditions the output stage is biased to give about half the supply potential at the output (pin 3). The two upper transistors operate as another darlington pair in the emitter follower mode, providing current amplification to positive-going half cycles. The lower three transistors consist of another darlington pair, this time in the common emitter configuration, driven by a pnp common emitter amplifier. There is 100% negative feedback between pin 3 and the emitter of

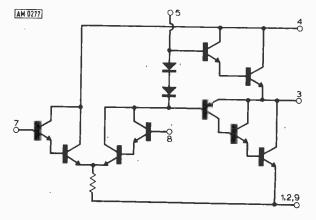
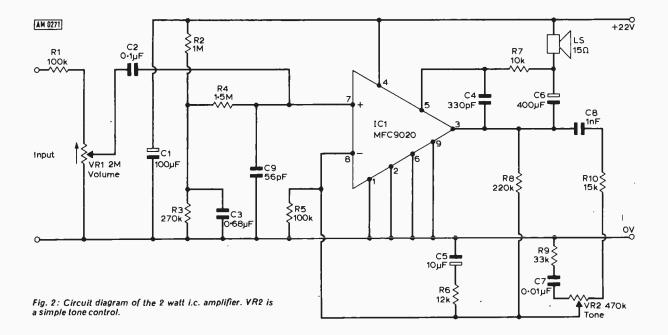


Fig. 1 : Internal circuit of the MFC9020.



the first of these three transistors, and this forms what is termed a compound amplifier. Like an emitter follower, a compound amplifier provides no voltage gain, but has a high current gain. It also has the input and output signals in phase. These three transistors amplify negative-going half cycles. Due to the high current amplification of the output stage, the output at pin 3 is at a very low impedance. and can directly drive the loudspeaker via a d.c. blocking capacitor.

AMPLIFIER CIRCUIT

A circuit diagram of a practical amplifier using the MFC9020 is shown in Fig. 2. The input is taken via R1 to the volume control, VR1. C2 couples the signal from here to the non-inverting input of the i.c. This input is biased via R4 from a potential divider across the supply, R2-R3. C1 and C3 are decoupling capacitors.

The inverting input is biased from the output of the i.c. by the potential divider, R5-R8. This introduces negative feedback and helps to give a stable biasing arrangement, though it seriously reduces the sensitivity of the circuit. C5 and R6 are therefore used to decouple some of the a.c. feedback and so provide increased sensitivity.

A simple treble boost and cut tone control is provided in the feedback network. This consists of VR2, C7, C8, R9, and R10. With the slider of VR2 towards the right, R10 and C8 are in effect shunting R8. The impedance of R10-C8 is frequency dependent, and reduces as frequency increases. The negative feedback in the circuit will therefore increase with frequency, causing the response of the amplifier to drop at high frequencies. With VR2 in this position the circuit is given top cut.

With the slider of VR2 at the other end of the track, C8 and R10 are in effect cut out of circuit due to the high value of VR2. However, R9 and C7 are now shunted across R6 and C5. Again, the impedance of these will be frequency dependent, but as they are connected across the other section of the potential

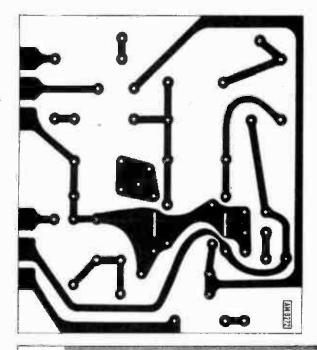
divider, the feedback will be increased as frequency increases. This gives treble boost. R9 and R10 are required to limit the effect of VR2 to a certain extent, in the interest of good stability.

Capacitors C4 and C9 are required for good stability. C6 couples the output to the loudspeaker. R7, which is the load resistor for the differential amplifier, is connected to the positive supply via the L.S. so as to give bootstrapping to the circuit.

The input impedance of the amplifier varies with the setting of VR1, but is about $2 \cdot 1M\Omega$ at minimum sensitivity, reducing to about $700k\Omega$ at maximum sensitivity.

★ components list

AMI	PLIFIER
Resistors, 1 watt, 5%-	
R1 100kΩ	R6 12kΩ
R2 1MΩ	R7 10kΩ
R3 270kΩ	R8 220kΩ
R4 1-5 MΩ	R9 33k12
D4 ** 100LC	R10 15kΩ
VR1> 2 MΩ log.	VR2 470kΩ lin.
Capacitors	
C1 100#F 25y	C5 10µF. 10V
C2 0-1µF	C6 400µF. 25V
C3 0 68aF	C7 0-01#F
C4 330pF polyester	CB 0-001µF potyester
	C9 56pF polyester
nents): Materials for g	available from SCS Compo- p.c.b., 150 loudspeaker, rated nore; Wire, solder, etc.,
R11 390Ω, ±W, ± 10% 25V Tr1 MJE340 D	R SUPPLY . C9 1000µF 50V C10 500µF 11-D2 1N4001 D3 22V, 1W ansformer 20-0-20V 250 mA



CONSTRUCTION

A printed circuit board measuring $3I_4 \times 3in$, is used and this carries all the components except the loudspeaker. Fig. 3 shows the pattern of the copper side of the p.c.b., and also the drilling points. Fig. 4 shows the component layout on the board.

The integrated circuit requires two ${}^{1}_{4}$ in. long slots in the p.c.b. into which its heat tabs fit. These are cut using a coping saw or a fret saw. Although potentiometers with pins which fit into p.c.b. mounting holes are manufactured, these would not seem to be widely available to the amateur, and this p.c.b. has therefore been designed to accept ordinary potentiometers with tag connections. The tags are taken under the edge of the p.c.b.. and soldered to the copper backing.

POWER SUPPLY

The amplifier requires a supply of approximately 20-22V. As the i.c. has a maximum supply voltage rating of 24 volts, it would be difficult to find a suitable unregulated power supply circuit considering that the amplifier has a class B output stage. This is because the supply should not rise to more than 24V under quiescent conditions, with a current con-

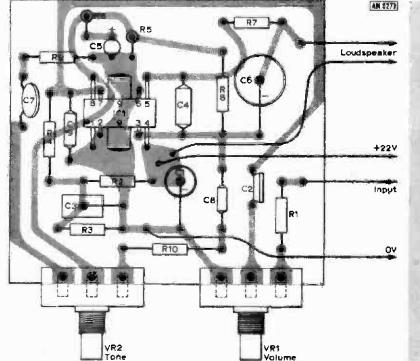


Fig. 3: above, shows the PCB layout actual size. Note that this is turned through 90° compared with Fig. 4.

Fig. 4: left, shows the layout of components on the PCB. The tags of VRt and VR2 are soldered to the underside of the board.

Fig. 5: below, is a circuit of a suitable stabilised mains power supply unit for the amplifier,

Tr1 MJE340 Sta D1 +22V 1N4002 24000000 R11 20 390 AC ŕ٩ C10 mains 1000µF 500µF D3 22V ov 1N4002 E AN 0274

sumption of perhaps only 10mA, and yet maintain about 21 volts under full load conditions with the current consumption peaking as high as 500mA.

It is more practical to use a simple stabilised circuit as shown in Fig. 5. This is a fairly standard configuration, using a zener diode stabilisation circuit feeding an emitter follower. This uses few components, and can easily be constructed on a small tagstrip or connector block. The MJE340 can be mounted on a strip of aluminium which will act as a heat sink and can be bent to form a suitable mounting bracket for the component.



Storp of the P.S.U.

THILE reading through one of my favourite vintage radio reference books, the BBC Year Book of 1930, I noticed a page devoted to telling listeners about power supplies for their receivers. It certainly was intended as a serious article then but these days one cannot help but smile when one reads about a BBC warning on making a direct connection between a receiver and the mains supply. So, below are a few pointers which listeners should have taken note of in the days 10 years or so before World War II.

"No receiver can give really good quality reproduction if the power supply to it is inadequate. Since broadcast receivers first came into use by the general public there has been a tendency to gradually increase the power supply to the last stage of amplification. Electric light supply mains provide a constant and convenient source of power for wireless re-

COLIN RICHES

ceivers, but in no circumstances should the mains be connected direct to the receiver without the use of an intermediary mainsunit.

A year ago, the BBC drafted a pamphlet which describes the many ways in which electric light supplies can be utilised for wireless receivers. The publication of this pamphlet has been delayed owing to the fact that a number of bodies, such as the Institution Electrical Engineers, the of Engineering Standards British Association and the Radio Manufacturers' Association, are all interested in its contents and the BBC naturally is anxious to conform with their views and wishes. It will however be published as soon as possible.

The BBC wishes to take this opportunity to warn listeners most seriously against the direct connection of their receivers to supply mains, and also strongly recommends that no listener who is unaquainted with handling power and electric light circuits should attempt the home construction of a mains-unit. It is a far more difficult matter to build a safe and satisfactory mains-unit than it is to build a valve receiver. Owing to the danger to life if a number of improperly designed and constructed mainsunits come into use by the listening public, the Institution of Electrical Engineers, in collaboration with the other bodies concerned, has drawn up a set of regulations which governs the use of electric power supplies to wireless receivers. One set of regulations, by the I.E.E. has already been published but new and more detailed regulations are now under consideration. These new regulations, if agreed, will be written in formal technical language and it is thought that many listeners will not be able to follow them conveniently. It is therefore probable that in its mains-unit pamphlet, the BBC will print an explanation written in more simple terms.

In conclusion, listeners are reminded that they are likely to have some difficulty in the future electricity supply conwith tractors, fire insurance authori-ties and other similar bodies, if they are using a mains-driven receiver which does not conform with the agreed regulations."

I suppose it is a matter of familiarity breeding contempt since electronic enthusiasts have successfully assembling been mains operated equipment and power supply units for a very long time now without any seriouslosses among their numbers from electric shock!



These interesting photographs show some "mint" items of vintage radio equipment kindly provided by Mr. Ken H. Rann of Lancing, Sussex.

It's rather unusual to locate brand new components but new items in their original boxes are interesting items indeed!







by Eric Dowdeswell G4AR

THIS month I am glad to be able to give a plug for the West of Scotland Amateur Radio Society. Publicity and QSL Manager Graham Bleakley reports a thriving membership of 80 and space for many more and promises a warm welcome for SWL's, young or old. In the past the club has concentrated more on the interests of the licenced amateur so it is very good to hear that the SWL is actually being welcomed! It is an unfortunate fact that many clubs catering for the licenced chap tend to spurn the SWL who goes along once, gets the cold shoulder and then decides to drop the idea of pursuing the hobby. The fact that the SWL of today is the licenced amateur of tomorrow seems to escape notice. The SWL is also only too pleased to be a general dogsbody around the club, taking on tasks that no-one else wants to do, especially on Field Day events. SWL's in the Glasgow area are invited along to 81 Virginia Street, Glasgow every Friday evening at 8pm to sample the Morse classes, junk sales, films, library and lectures etc. More details from Secretary K. Drinkwater at that address.

Steve Blake (Aylesbury) joined the flock with a report of 40m doings including a nice collection of ZL's on SSB. Hope Steve will favour me with some details of his gear in his next log. Michael Crimes (Exeter) has forsaken VHF now that he can really hear the DX on his shiny new Yaesu FR50B coupled to 132ft of wire via an ATU. Like several other reporters he is a little disgusted with the antics of the Italian boys especially when a rare call pops up.

Michael Green A8088 (Northwich, Cheshire) refutes any suggestion that the 4m band only comes alive in contests and submits a long list of G's heard in one evening on his home-made converter plus CR100 and 4-element beam at only 12ft. Regular John Porter (Baslow, Derbys) is glad to have left the classroom for an OND course at Chesterfield Tech. His Trio 9R59DS was not allowed to get cold, evidenced by the list of DX from 15 to 160m. Andrew Darragh (Wetherby, Yorks) sends his first log and promises more. Last reported in 1968 it seems, getting married in the interim, now 'back on the rails' and I should jolly well think so! A Geloso converter puts signals into an AR88 from a 12AVQ trapped vertical and nine radials per band!!! He must be located in the centre of the racecourse up there!

Alan Rae (Glasgow) found a few nice calls on 20m thoughtfully omitting the lists of W's that are not of much interest to anyone. Tim Charles (Colchester) in again with six pages of notes and calls gives the impression that he never goes to sleep! His long wires suffered in the gales but one would never think so! Interesting catch was F9LC on 7MHz with two watts of SSB and over S9 at that. I'm a bit put out to hear Alan had to look up ST2 in the prefix list since yours truly was ST2AR for 15 years! Incidentally, I've just had the very great pleasure of meeting ST2AS in London. I'm glad to say that I started him off as a SWL some years ago when he was a medical student and now he is Dr. Ibrahim, opthalmic surgeon and the only active ST2 for some years past.

Bernard Hughes (Worcester) also stuck at 20m SSB which seems a pity with a lovely FR500SDX! The other bands are quite lively too, OM! Bernard keeps a record of the number of countries heard on each band and wonders if anyone is interested in seeing a totals table in this column from time to time? Paul Barker (Sunderland) is another of the sleepless brigade! Three pages of rare ones from 15 to 80m including several on SSTV but nothing exceptional this month, he says!

Max France (Warrington, Lancs) now has an RA1 but still prefers his old R107 for sorting out the DX on 80m. Back to school means less burning of the midnight oil however, so it looks as if 20m will be favourite for some time now, with a picture rail aerial. Ought to be good for SSTV!

Log extracts

Max France:—80m PQ0NS PZ0CJ VS6DO ZL2CB 5Z4LW 6Y5BM 20m VP8NS XV5AB XW8GV.

Paul Barker:—15m CX2AAO (1700) 20m JW5DQ KH6IAG KL7MF KX6LP VS6FB ZD3U ZK1DJ 4W1GM 20m SSTV CT1TX 16RME K1LEM LU4CN.

Bernard Hughes:—20m HK0BKX KM6DZ TR8VE YK1KAS 4W1GM.

Tim Charles:—80m ZL3NC ZJ4AU 40m CE5BMN YA2KL ZL1AUL ZL2ALR ZL3PW 20m HK4SAJ HK0BKX JY5UMC KC6BL TG5YD XZ1AB 2m DC3GEC DC4JHA.

Alan Rae:---20m CR3AX HK3CKW K3C1/OE K7RSC.

John Porter:—15m EA8JP PY8RW 20m CT3AT EA9FB FY7AU KV4AD TG9VN TR8SS ZB2CH 8R1CB TI2AJF.

Steve Blake:—40m EA9AI HC0HM KZ5PW M1C SV1DO TU2DO VK7GK XE3U ZL3AR ZL4GN ZL4KS 8P6AG.

Michael Crimes:—20m CR4BS DU1XK ET3USE HZ1AB ST2AY VP1MT VP2DH 4W1GM. Andrew Duragh:—15m CX2XC VQ9MC VU2DK ZP5NT 7P8AQ 20m AC3PT CR3ON DU2EF FC2CD HR2JAG JY9GR KC4AAC KG4AM ST2AY TA2QR VK9XX VP8HA VS5MC ZD7SD 8R1CB.

CW stations in bold, remainder SSB. Please note that logs should be in alphabetical order for every band.



MEDIUM WAVE BROADCASTS

by Charles Molloy

R OY PATRICK reports again from Derby. With his Trio 9R59DS communications receiver he has logged Dakar, Senegal on 764kHz; Amman, Jordan on 800kHz; Rio de Janerio, Brasil on 980kHz; Cluj, Romania on 1151kHz; Tripoli, Libya on 1250kHz; Conakry, Republic of Guinea on 1403kHz. Roy sends a mobile report of reception in North Wales. The receiver is a National RF 1400 portable connected to a car aerial and his daytime reception includes BBC Radio Merseyside on 1484kHz; BBC Radio Cumberside 1457kHz; Piccadilly Radio in Manchester on 1151kHz; Manx Radio, Isle of Man on 1295kHz (good signal) and 1594kHz (weak). After dark Tunis was heard on 962kHz and the Voice of Tangiers at 2000hrs in Arabic on 1232kHz.

M. J. Clarke (Warley) is a self confessed local radio enthusiast. Using a Philips RL210 portable receiver he has pulled-in BBC Local Radio outlets at Blackburn on 845kHz; Stoke on 1052kHz; Derby on 1115kHz and Birmingham on 1475kHz together with IBA Capital Radio on 557kHz and Birmingham on 1151kHz.

Timothy James (Southampton) has been tuning around the medium waves with his Fidelity RAD16. He reports hearing Capital Radio (London) on 557kHz; Radio Solent on 998kHz; Radio Medway on 1034kHz; Radio Sweden on 1178kHz and Radio

SHORT WAVE BROADCASTS

by Derek Bell

H ELLO there! my name is Derek Bell and our editor has invited me to take over Malcolm Connah's Short Wave News column for a spell. May I say that I hope all readers will give me the same help and friendship that they gave Malcolm. All columnists must rely on the help of their readers, especially in this sort of column, since it could be said that the readers write the column with their contributions. I hope also that in your letters you will pop in a line or two telling me what you would like to see included in this feature.

Having said all that I will declare the meeting open with the first log. This is from another first timer, namely **David Lovatt** of Cheadle, Staffs, and he reports the following:—

5980 SBC in English at 2130

5990 Prague in English at 2131

- 6010 Budapest at 2136
- 6800 Pekin S/on at 2030
- 7200 Deutsche Welle at 2031

15350 Peace and Progress at 0920

Brighton on 1484kHz.

Peter Kirkbride (Kenilworth, Warwickshire) still enjoys "scanning the medium waves" with his 20 year old Bush valve receiver. He mentions reception of AFN Frankfurt on 872kHz and Munich on 1106kHz; Radio Sweden on 1178kHz; Radio Tirana, Albania on 1394kHz. Peter asks if it is possible to pick up North America using this receiver. Provided that a good outdoor aerial is used it should be possible to hear a few of the stronger trans-atlantic signals when conditions are good for reception of this area. Try after 2330hrs GMT for CJON St John's, Newfoundland on 930kHz; CBA in Moncton, New Brunswick on 1070kHz and WNEW in New York City on 1130kHz.

Mike Larvin (Redcar, Cleveland) has a Pye 1403D and an ITT Weekend Automatic Radio. Both are portable receivers and although neither has a socket for an external aerial for the medium waveband and external aerial 25m long and 20ft high is pressed into use by means of the following ingenious device. "I use a 6 inch ferrite slab wound with 75 turns of 20-30 SWG wire one end of which is connected to a good earth and the other to the aerial". The slab is brought near the receiver until peak signals occur, coupling being by induction between the slab and the receiver's internal aerial. Mike's log includes WKBW Buffalo NY on 1520kHz at 0230hrs GMT; BBC Relay Stations in Cyprus on 638kMz and 1322kHz; AFN stations in Germany on 872kHz (Frankfurt), 935kHz (Berlin), 1106kHz (Munich), 1142kHz Stutt-gart); Budapest, Hungary on 1340kHz at 2245hrs; Norte, Portugal on 755kHz and 1061kHz. A total of 23 BBC local outlets were heard as well as London Broadcasting on 719pHz and Metropolitan Radio (Newcastle) on 1151kHz with Radio Clyde and Piccadilly Radio in the background.

Clive Barwood (Grimsby) is another local radio enthusiast. He uses an Ekco Mariner 6 valve domestic receiver connected to an outdoor aerial 75 ft long and 25ft high. He reports hearing Capital Radio 557kHz; IBA Birmingham 1151kHz; Metro Radio also on 1151kHz; Manx Radio 1294kHz and BBC Radios at Stoke 1502kHz; Cleveland 1546kHz and Leicester 1594kHz.

This is a shortened version of a superb log from our thirteen year old correspondent who is equipped with an Ultra domestic valved receiver and a 60 ft aerial suspended 20 feet above terra firma.

Christopher Hall of Birmingham has the other sort of aerial, a 4-ft telescopic one, bolted to his Bush VTR178 Multiband. Using this line-up he reports an impressive list of catches the cream of which is as follows:—

6185 R. Norway in English at 1200

9770 R. Australia at 1600

11955 B.B.C. Malaysia relay in English at 1500

I was interested in your comments at the end of your letter Christopher. As far as DX clubs go one must rely on the adverts they place in various magazines so "yer pays yer money and takes yer choice" in other words! Your request for the latest information on equipment for the BC stations however brings forth the information that Uganda is pressing ahead with a new SW transmitter setup that will bring the voice of Uganda blaring out loud and clear. Recently a member of Radio Nederlands staff went on record as saying that they are to increase the power of their transmitters, another victim I fear of the "power game".

From the biggest to the smallest now, **Paul Heath** says his equipment "is somewhat joked about". This Heath kit (sorry about that!) is a home-built HAC one valver plugged in to various "out board motors" namely an ATU and feeding out through a transistor amplifier. Well Paul, let them laugh!, you pulled in a fine list, as is shown below:—

9005 Voice of Iran at 2020

9625 R. Jerusalem at 2000 (This is R. Israel, Paul) 9655 R. Damascus at 0830

9670 A.W.R. Portugal at 0945

You remark Paul, that you have received QSLs from only a couple of stations but that "there are more to come". Well OM, this is purely a matter of being patient. Radio Tirana, for instance, has been known to take 125 days to deliver, while Polish Radio Warsaw has taken only seventeen. Your logging of Damascus on 9655 was fortunate since Damascus is a notorious "wanderer" having been heard as far off frequency as 9630.

My final letter for this month is written by **Robert** Hill who hails from Hough, near Crewe, and he reports that he heard:—

9005 R. Tehran in English at 2015

9480 R. Tirana in English at 1830

9550 R. Finland in English at 1605.

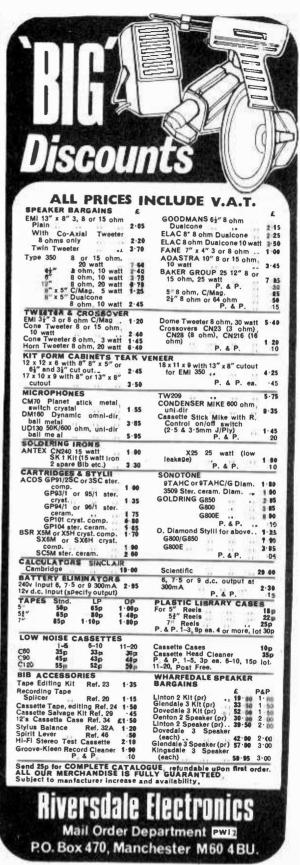
11775 R. Bucharest in English at 1300

Having Crewe as a QTH seems to me to pose some unusual problems, I imagine it is possible that with all the QRM around from electric railways DXing is rather difficult. I would be interested to find out if I am right.

Well folks, that winds up my first venture into the pages of Practical Wireless. I hope that having read it you will feel that you want to write in with your logs (see address box) so I look forward to hearing from you, best 73s to you and yours.

BROADCAST BANDS Short Wave and VHF/FM reports by the 15th of the month to Derek Bell c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD. Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG. AMATEUR BANDS Logs covering any amateur band/s in band/ alphabetical order by the middle of the month to Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey, KT21 2TW. A reprint of the P.W. Tele-Tennis series is being prepared and will be available shortly,

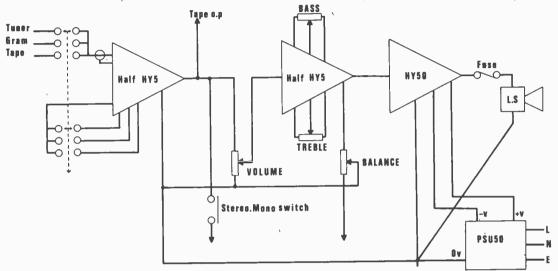
Further details in the January 1975 issue of



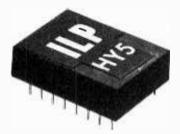
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82/500V 25/25V 50/50V	50p 10p 10p	8+8/450V 8+16/450V 16+16/450V	22p 25p 40p	82+82/450V 100+50+50/350 82+82+82/850	
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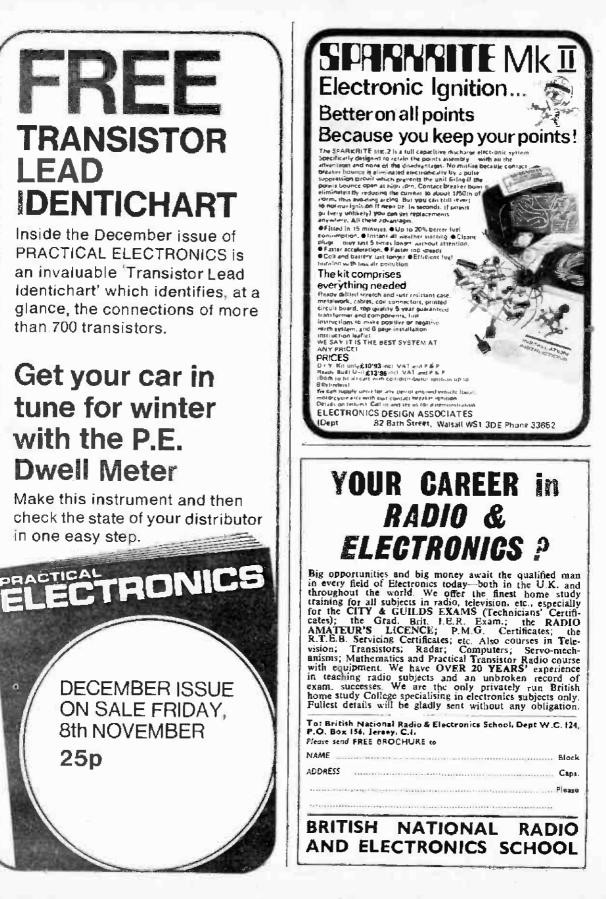
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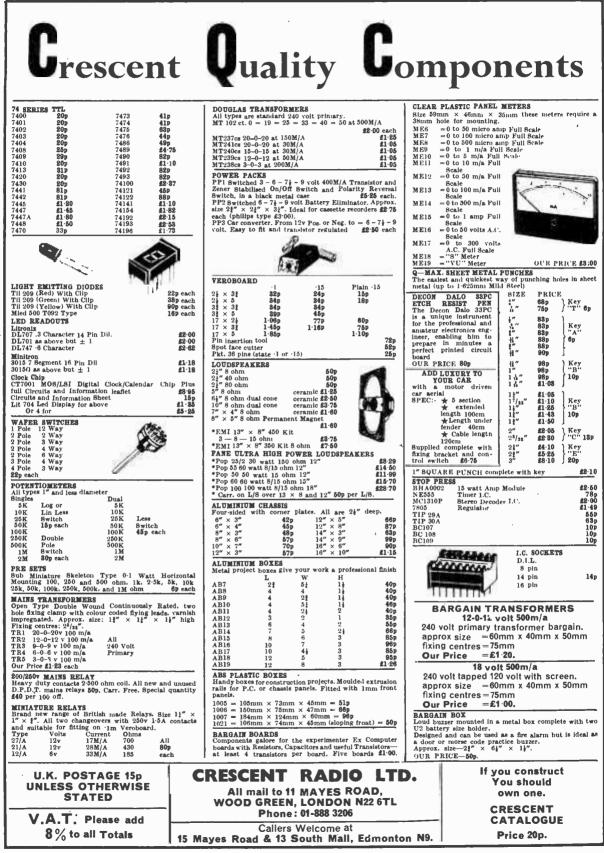
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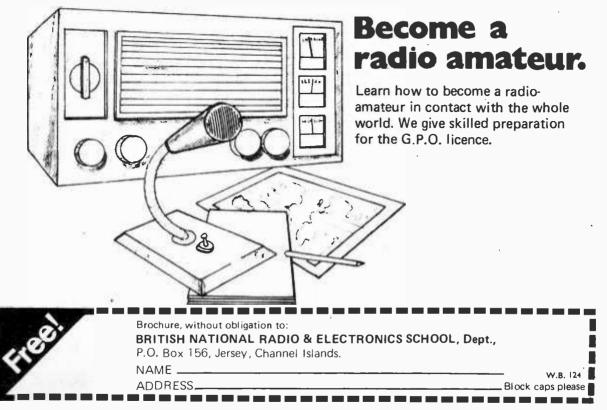








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	with Switch, 6 metres Cable and Plug 600 ohms/50kΩ	£12-00 SN75	2 Way Crossover	Network Imp 8 ohms	FF11 Stereo F	requency Controller and Pre-
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EXPERIMENTER PRINTED CIRCUIT KIT BUILD 66 INTERESTING PROJECTS CONTENTS: (1) 2 Copper Laminade Boards 4; m. v 2µm (2) 1 Board for Matchbox Radio, 3; 1 Board for Wristwatch Radio, etc. (4) Resist. (5) Resist Solvent. (6) Elchant. (7) Cleanser, Degresser. (8) 16-page Socielt Frinted Circuits for Amateurs. (9) 2 Ministure Radio Dials BW/ MW/LW. Also free with each kit. (10) Resential Design Data Circuits, Chassis Plans, etc. for 60 TRANSIBTORIBED PROJECTS. Circuits Lo suit exeryone's requirements. Price 21, post paki.



RECORD PLAYSACK MEADS (TRUVOX) Individual projects of these are: 2 track record playback heads 500 each. 4 track record playback heads 500 each. Erase beads are also available separately: 2 track 530, 4 track 550. MV metal mounting shields 500 each. 2 track 530, already fixed on heavy mounting plate with ahleki \$1.32.



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powerful battery motors as used in racing cars and power models. Output and types vary to make them suitable for hundreds of different wolexts-tools, toys, models, etc. All brand new, verstible and for 1 is to 120. Bate., writing dis-trams included. Post and VAT 309. **FREE** Details of how to make miniature power station. mak grams is

BSR TAPE DECK TWIN CHANNEL

TWIN CHANNEL Mounted on a wooden plinth with amplifier. Not new, but unused. Originally intended for schools teaching aystem. The tage deck is perfectly stan-dard and has the usual record, playback and fast rewind controls. Limited quanity--only \$8:50 plus 61 post and insurance.

BATTERY SWITCH

Famous Atlas in metal case with meter, output leads terminated by crocodle clips. For 6 or 12v charging simply by about by crocodile clips. For 8 of 12v charging simply by changing plug on front panel. Ready built, new and still in makers original packing. Two models: 14 amp \$109 and 34 amp \$25.06. Please add 40p postage for one and 75p postage for two.

TIME SWITCH Smith's mains driven clock with



Smith's mains driven clock with 15 amp switch, also notes showing how you can wake up with music playing, kettle boiling or come home to a warm house, warn off burglars, keep pets warm, halve your beating bills, etc. \$1.95.

- inst

RELAY BARGAIN Type 600 relay, 2 changeover one open and one closed contact. Twin 500 ohm colls make this suitable for closing of DC 6v. DC 12v, DC 24v or AC mains using resistor and rectifier. 359 each. Resistor and rectifier 209 estra.

BATTERY ELIMINATORS Kit of parts comprising mains transformer, recti-fer and necessary smoothing components with instructions, showing how to make up for 6v. 9v or 19v types

Radio from mains	£1-20
Cassette from mains	£1-50
Cassette or radio from car (Mabilized)	£2·10

AMPLIFIER PANELS

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Very nice looking, polished black presephan with fixing holes, 6 phono sockets and changeover slide over slide switch and is printed as sketch. Price is 30p.





CENTRIFUGAL BLOWER Miniature mains driven blower centrifugal type blower unit by Woods. Powerful but specially built for quick specially built low noise bearings. Overall size $4\frac{1}{2} \times 4\frac{1}{2}$ $\times 4^{\circ}$. When mounted by fiange, aris is blown into the equipment but to suck air out, mount it from centre using clamp. Ideal for cooling electrical equipment or fitting into a cooker hood, film drying eabinet or for removing flux snoke when soldering, etc. etc. A real bargain at 22-05.

TANGENTIAL MEATER UNIT This heater unit is the very latest type, most efficient, and quiet running. Is as fitted in Hoover and blower heaters. Comprises motor, innuclier. 2kW. element allowing writching 1, 2kW. and with thermal safety cut-out. Can be fitted into any metal line case or cabinet. Only needs control switch, 22-75. Don't miss this. Control Switch, 449. P. & P. 409.

for this:--1 Unitex Amptifier Ref. EP 9000 \$1:60 1 Unitex Pre-Amp Ref. EP 9000 \$1:60 1 Unitex Power Unit Ref. EP.9001 \$1:80 1 Unitex Power Unit Ref. EP.9002 \$2:80 1 Onitor panel kit with soma luminium faced knobe \$2:80. Or the complete outfit-fil:80 powt paid. Pair of 15 ohm speakers made by E.M.I. are also available if required, \$3:80 the pair. No extra postage if ordered with the above, otherwise add 25p.



SMORTWAVE CRYSTAL SET Although this uses no battery is gives really amaxing results. You will receive an amaxing assoriment of stations over the 19.25.31.39 metre bands—Kit contains chassis front panel and all the parts. \$1.25—crystal ear-phone 339.

THIS MONTHS SNIPS

AM/FM TUNER Unit made by the American GEC company. N transistor, all-wired ready to work. Complete with tuner condenser, needs only scale and pointer. Tunes AM range 540 to 1620 KHz, FM range 88 to 108 MHz Switches for on-off and APC. Output for MXP or direct. Special snip price \$5 plus 30p post. Three or more post free.

7 WATT STEREO AMPLIFER Again by the American GEC company. This has exceptionally good tone quality. Is complete with pre-amp and treble base, volume and balance controls. Also has nusins smoothing circuit and rectifiers so requires only nusins transformer. Output for 15 ohm speakers. Inputs for tuner pick-up, mike. etc. Special snip price \$8 plus 30p post. Three or more post free.

DIGITAL DISPLAY UNIT 'DIGIVISOR' A precision instrument consisting basically of a 12 volt lamp focused by a lens system to shine through a nunbered scale onto a ground giass front screen, the number being selected by applying a different voltage of the coll. Overall size approx. $2\frac{1}{4}^{\prime\prime} \times 1\frac{1}{4}^{\prime\prime} \times 4\frac{1}{4}^{\prime\prime}$. Price 23:50.

TAPE DECK In metal case with carrying bandle, heavy fly wheel and capetan drive. Tape speed 31. Maius operated on metal platform with tape head and guide, Not new but guaranteed perfect. Price 51.95 pius fi post and insurance.



HORSTMANN 24-HOUR TIME SWITCH With 6 position programmer. When fitted to hot w systems this could programme as follows:-Programme Hot Water Central Heating



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ti Twice Daily Off 2 All Day Off 2 All Day Off 3 Twice Daily Off 3 Twice Daily Twice Daily 4 All Day All Day 5 Continuously 5 Continuously 5 South State State

WANT A CHEAP OSCILLOSCOPE We offer this month a laboratory type instrument made by (J.E.C. for their communications laboratory. In a steel case with carrying handle. It is mains operated and has its own internal time base and plenty of room to add another base if you with. Probable cost of this instrument is in excess of 2100. We offer this tested and in working order. \$17:50 plus \$2 carriske for first 200 miles then \$1 for each 100 miles atter.

OIL PUMP Driven by Redmond Motor of approx. 1/20th horse power, pump originally intended for oil fired boilers stc. with normal inlet and outlet pipes and unions. \$2-15 plus 30p post and insurance.

TINY BATTERY MOTOR Works off 1_0 or Sy requires no on off switch as it will not draw current until it is spinning. Approx. $\frac{1}{2}^{n}$ long $\times \frac{1}{2}^{n}$ diameter. Ideal for hand held fan. propeijor driven model etc. 209 each, 10 for \$1.80.

LUMINOUS ROCKER SWITCH ON/OFF Luminous Rocker switch on/off. Panel mounting, snaps into a 1" hole. Rated at 10A 250-. 159 scato rol 10 for \$12.56.

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Add 8% V.A.T. Send postage where quoted-other items, post free if order for these items is £6.00. otherwise add 30p.

AUTOMATIC EMERGENCY

Forwer cut days will soon be upon us. Our simple kit makes any light a fail-safe light. Kit containing relay and rectifiers and data, only 65p each. 10 or more 60p each. Suitable case 60p extra.

PORTABLE CABINET OFFER A nicely made portable cobinet, soft padded black finish intended for portable stereo system. Dimensions hear icat out for Garnard SP 25. This was obviously a very costly cabinet SF 25. Inits was obviously as very costly cabinet originally made for a de-inter record player. Offered at f195 plus f1 carriage free it bought with the (tarrar) or INM



record decks.

LIGHT DIMMER KIT Por dimming up to 250w without heat sink or 750w with heat sink. This comprises, quadrac, variable control potentiometer, condenser, real-tors, tag strip for mounting and data. Prior £1500

MACLAREN THERMOSTAT Make and break 20A a.c. with the sensor probe coupled by a 2 feet capillary covering range of 10-100°C-complete with large engraved control knob. Price 88p.





TREASURE TRACER Complete Kit (except wooden battens) to make the metal detector as the circuit in Practical Wireless August issue. \$430 plus 20p poet and ionwance urance

MAINS MOTOR Precision made—as used in record decks and tape recor-ders—ideal also for extractor fans, blower, heaters. etc. New and perfect. Snip at 65p. Portage 20p for first one then 10p for each one ordered. 1° stackmotor 94p. 1 i ″ stackmotor 941-10. used in

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NEED A SPECIAL SWITCH Double Leaf Conlact. Very slight pressure closes to contact. Sp each 10 for 609, Plastic pushrod suitable for operating. 6p each. 10 for 549. 3 2

AMPLIFIER IN CASE WITH

AMPLIFIER IM CASE WITH SPEAKER Marketed by British Relay under the name Luxitor. This is in a very neat looking cabinet and is ideal around the home or in the workahop for trouble shooting or for testing out a quick lash up. Size approx. 91" x 64" x 34" dep. Input is via a matching transformer and volume control and amplifier may be powered by an internal 9v battery or an external 110v source. Rpeaker is an B-A eliptical 6" x 34" 10.000 Fauss. The amplifier proper is a Newmarket model ref. P.C.4. Price \$3.755 each. 10 for \$31.50. Post and insurance 20p.



 Image: Construction of the state o

HEADPHONE STEREO AMP. With volume. balance and tone control. Output approx. 2 wati into 22 ohm speaker but will operate with reduced output into 16 ohm or 6 ohm headphones. Power supply 14 v AC (We can supply suitable transformer—509). The amplifier has all controls mounted and is ready to ally into a simple box. Price \$2.99 plus 50p post and insurance.

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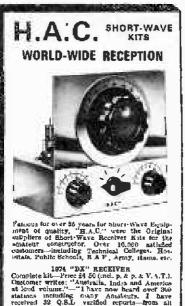
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33.04 F at 6V or 10V 47-	0. Wat SV or SV - 100.0. E at SV
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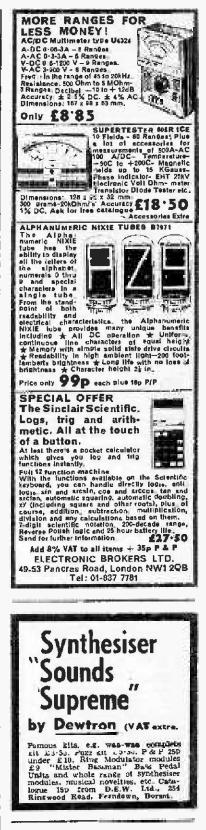
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E1830C EPRO 449 PCTR0 409 CTR0 8 E718 E7183 459 PCTR2 409 8C1/600 E4360 409 E7164 359 PCTR4 409 8C1/600 E4360 409 E7164 359 PCTR4 409 8C1/80 E4381 259 E143 259 PCTR4 409 PTT21 550 E831 259 E143 259 PCTR40 759 PTT21 559 ERC3481 401 81.30 409 PCTR40 559 U25 259 E80C34 F59 E143 153 407 PCTR40 559 U25 259 E80C34 F59 E143 1530 PCTR40 559 E80C34 F59 E143 1530	AF 116 BCT 72 OA 47 OC 62 AF 117 BF 116 OA 70 OC 62 AF 118 BF 167 OA 71 OC 63 AF 124 BF 167 OA 71 OC 63 AF 124 BF 167 OA 71 OC 63 AF 124 BF 165 OA 72 OC 14 AF 125 BFT 51 OA 79 OC 14 AF 126 BFT 52 OA 200 OC 17 AF 127 BFT 50 OA 200 OC 17 UTP85 459 123 409 V.A.T.	DBI 2N 1307 40230 2N 1309 40231 309 40231 2N 2062 6660 20 <td>274 809 2014 81.10 \$12.00 9D40 404 254.60 750 D013-2 1122 58.00 354.67 750 D013-2 128.45 59 352.67 700 M137-35 128.45 59 352.67 700 M137-35 128.47 459 50C3 600 525.04 128.47 459 50C3 600 VC81.20A 128.477 359 521.06 11 22.620A 128.477 359 25 53.04 24.60 128.478 459 25 52.5 250.68 128.478 459 25 52.5 25.00</td>	274 809 2014 81.10 \$12.00 9D40 404 254.60 750 D013-2 1122 58.00 354.67 750 D013-2 128.45 59 352.67 700 M137-35 128.45 59 352.67 700 M137-35 128.47 459 50C3 600 525.04 128.47 459 50C3 600 VC81.20A 128.477 359 521.06 11 22.620A 128.477 359 25 53.04 24.60 128.478 459 25 52.5 250.68 128.478 459 25 52.5 25.00
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