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Type SS15. These fine motors are easily reversed, starting and stopplong in less than $5^{0}$ without electrical or mechanlcal braking. Simple be applled to give DC., to winding for a maximum holding torque of $3000 \mathrm{z} /$ In with 35 v at 0.35 amps 120 f . 50 Hz inding. For AC. (synch ronous) operation at Hoiding torque at 50 steps per second- 100 oz/In. Can be wired to glve 100 or 200 steps per revolution witn accuracy of $0.1^{\circ}$ per sted non-cumulative. Torque characteristics can be modified by simple R.C. circuits. Dimenslons: dia. 4" body length 4z", spindle length $2 t^{\prime \prime} x{ }^{* \prime \prime}$ dia. Weight $6 \frac{1}{\frac{1}{6}}$ lbs, BRAND NEW In maker's packing. Offered at less than t maker's price.

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This little unlt gives vertical lift of approxi-
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Bracket incorporates 2 fixing screws. Length of arm $2 \frac{1}{2}$ " 240 V AC. Pult at coll is approximately 1 lb . £1 FREE P. \& P. Special quotes for quantities.

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24 volt DC input for 18 volt sawtooth output. Requires only external capacitor and 100 K ohm potentiometer to control frequency range up to 100 kHz (eg 50 mfd electrolytic gives sweep of approx 1 cm per second). In or out sync capability. Price $\mathbf{2 5} \mathbf{7 5}$ P. \& P. 15p
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Designed for use with VCO FX11 and RAMP FX21. This completes the 3 building blocks required for a basic lowfrequency Spectrum Analyser that covers 100 Hz to 50 kHz . The additional components required are discrete resistors and capacitors, etc. (No inductances or specialized components are needed).

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## Post \＆packing FREE in U．K．

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WE have, from time to time, taken a peep at the pocket calculator market. It has been currently estimated that the world-wide production of chips for electronic calculators for 1974 will be of the order of 28 million units. This exploding market is one of the few fields in which prices are constantly dropping. If the present growth rate continues, it is estimated that there will be an electronic calculator shortage within two years!

There exists a veritable jungle in both price and selection. The prolific arrays of pocket calculators that are available to the consumer that dominate the windows and counters of our local high street.shops are indeed bewildering. There appears to be a greater variety of pocket calculators than transistor radios!
A price war has emerged amongst major manufacturersprices being slashed overnight and indeed putting many retail distributors and 'special offer' organisations on the spot! A recent overnight price reduction by a major manufacturer caused considerable embarrassment to many of his trade and retail outlets. This sort of fiasco is being repeated over and over again. Where will it all end?
One enterprising calculator manufacturer determined to display his 'chips' to members of the public has opened up a 'mobile shop' at a London main line railway station. By all reports, he is doing fantastic business.
What of the 'domestic' pocket calculator? Rumour has it that a basic calculator especially designed for the housewife may be launched. If so, this could be just the thing for calculating and analysing those shopping expeditions to the supermarket. The shopper would be able to check his totals at any time and at the till check-out point. I can foresee many red-faced supermarket managers attempting to explain away the differences that may occur between store and customer calculated totals.
The pocket 'memory' calculator with its inherent potential as a pocket computer, with the ability to recall stored information at the press of a button could be just around the corner!
What of the future? The pocket calculator could become as prolific as the ball-pen-a must for everyone.
However, the pessimists (optimists, if you prefer) are chanting 'Beware, Big Chip is watching you!' (shades of 1984). They could however be forecasting our future.

There is no doubt that the calculator chip has, in many ways, dramatically changed our whole way of life. The question is: are we all in the hands of the Big Chip?

LIONEL E. HOWES-Editor.

> We're off to a good start in the New Year with our three part series on Model Control by Radio and we tell you how to get your licence for this most interesting of hobbies. Do you sometimes wish you had a small audio amplifier around for testing purposes? Our 2 watt IC audio amplifier will fill the bill. The Special Pre-publication Book Offer ought to appeal to many of our readers for all the useful information contained in Radio Servicing Pocket Book, a new 3rd edition. Finally, you won't want to miss the fourth and final part of the PW Buyers' Guide 1974/75. All in the January issue of Practical Wireless.

## From Partridge . . .

Aever increasing number of people are living in space restricted environments. Either through sheer lack of external facilities for the erection of aerials, the inability to receive radio signals inside ferro concrete walls, or the existence of local government legislation preventing the use of outdoor space for aerials, there are ever growing numbers of frustrated readers unable to pursue their hobby of Amateur Radio or Short Wave Listening.

For many years now Partridge Electronics Ltd., of Broadstairs, Kent have specialised in equipment designed to overcome this problem. Five years ago they published a reproduction of a World Record Certificate awarded to American Radio Amateur W6TYP. This was achieved by Mr. Art Child of San Francisco using the Partridge system operated from a hotel room at the foot of San Francisco's famous Nob Hill.

Partridge have now developed a device known as A.G.T.U., an Aerial Tuning Unit which also incorporates an Artificial Earth (or ground). This overcomes the only remaining problem of the high-rise apartment or flat dweller having no access at all to natural earth.

## ON THE COVER

## PW's MINIATURE SCREWDRIVER

Don't despise this very useful workshop aid because it seems to be so small! How many times have you found that your 'small' screwdriver is just too wide or too thick for the grubscrew in a knob or the adjusting slot in a subminiature potentiometer?? The more you use it the more uses you will find for our little present!

## Harrogate Fair

AUDIO '74 or the Northern International High Fidelity Festival at Harrogate was the biggest and best-attended ever. In 1970 there were only 50 exhibitors. 1972 saw 70 firms exhibiting their wares and this year over 90 companies decided to show their faces.

Over the last couple of years, there has been a marked increase in the amount of quadraphonic equipment on show. It is a pity that there seems to be little or no agreement on the kind of system to be favoured for quadraphonic reproduction.

We hope to include a short report on "Audio '74" in a future issue.

## BBC tape deal

ACONTRACT to supply the BBC with more than 100,000 reels of TS Scotch 262 recording tape for stereo broadcasting has been awarded to 3M United Kingdom.

The contract, which is due to run until next June, is in addition to the 70,000 reels supplied to the BBC last year after close liaison between the Corporation's sound engineers and technicians from 3M's magnetic tape facilities at Gorseinon, near Swansea, and Caserta in Italy.

## BEAB approval list

THIS list covers the first category of audio products in the BEAB Approval Scheme which have successfully met the requirements of the British Safety Standard BS.415: 1972.

Decca Radio \& Television with the Decca DS623, ITT Consumer Products Ltd. (ITT KP 820, KP 821, KA 1026, and RGD PA 30, P 83). Pye Limited (Pye 5000 and Invicta 8040). Sony (UK) Limited (Sony HMW-20). Rank Radio International Ltd. (Bush A 1005, A 1016, BS 3013, Dansette A 4005, A 4016, and Murphy MS 3014). Thorn Consumer Electronics Ltd. (HMV 2046, Ferguson 3047, Marconiphone 4047, 4049, Ultra 6046, 6048.

## Computer club

NOW moving into its second year of existence the Amateur Computer Club of Basildon, Essex has now formulised its activities into a constitution and elected officers for the year.

The club now has a firm membership of over 200 with a regular newsletter forming the nucleus of the club.

After two Annual General Meetings in London and committee meetings the start of a club activity schedule has emerged. The first of which was an open afternoon on the 25th May, 1974, at the Galdor Centre, 52 Brighton Road, Surbiton, Surrey.

The people at the Galdor Centre own and run an ICL 1301A computer ( 1960 vintage) which they have installed and made working to provide them and similarly interested persons with computer time at "materials only" cost.

Further activities are being arranged and will be announced in the newsletter which has also provided a unique forum for the airing of ideas and introducing basic principles to the beginner.

Articles in the newsletter have covered transistor working, design and operation of a digital core store, digital computer elements. computer software, software routines, descriptions of various computer systems both working and under design/development, news information items and computer games!

Club members are contributing articles to the newsletter resulting in some cross fertilisation of ideas among the members, which is one of the most important objectives of the club.

New members and ideas are very welcome, membership is $£ 1 \cdot 00$ per year (that includes the near monthly newsletter) and applications should be directed to Mike Lord, 7, Dordells, Basildon, Essex.

## Healhrow computer

CABLE and Wireless Ltd. have installed a new com-puter-based departure control system for airline passengers at London Airport. Japan Air Lines will use the system named "Lopac" which has been jointly developed by $C$ \& $W$ and Scientific Control Systems Ltd.

Apart from speeding passengers' baggage check-in procedure, the system also allows for productivity expansion.

Lopac, incidentally, stands for Load Optimisation and Passenger Acceptance Control.

## PW TOOL KIT OFFER

We apologise to our readers for the delay in dealing with their orders. The overwhelming demand created problems with delivery. If any readers have not received their tool kits, or a suitable alternative, would they kindly contact the Editor.

## Javelin move

JAVELIN Electronics have closed down their City offices and moved to Javelin House, Second Way, Exhibition Grounds, Wembley, Middlesex HA9 OUA. (01-903-6821).
The new building contains the service department, a dealers' advice centre and a customer relations department.

## Sansui 4-channel

THE sponsors of the "QS" 4channel system, Sansui, are making moves to persuade artists in the UK to record material using their system.

The "QS" regular matrix system has been accepted by the American and Japanese Recording Industries Associations and over 20 record manufacturers are producing software in the system.
It has been stated that at least one commercial radio station in the United Kingdom is thinking of using "QS" which has now been adopted by all f.m. stations in Japan.


Having completed the assembly you will want to know the polarity of your car＇s electrical system．If it is negative earth then the set is ready to $g 0$ but if it is a positive earth then you have to change over two of the push－on tag connectors． Not very difficultl Should you decide ever to transfer the radio to a car of opposite polarity the change back can be made more quickly than it takes to tell．

## Installation

RT－VC recommend a check－out of the set with the car battery before final installation in the car．Calibration takes a moment and the aerial trimmer is adjusted using the aerial that is to be fitted to the car．If all is well，and I＇d be surprised if it wasn＇t，installation can now begin．RT－TV＇s instructions on this aspect are，again，as complete as they

## SPECIFICATION

Tuning Range：－Medium Waves 185 to 555 m （ 1620 to 540 kHz ）
Long Waves 1153 to 2000 m （ 260 to 150 kHz ）

Sensitivity：－Better than $15 \mu \mathrm{~V}$ at 1 MHz
Output：－
4 watts to 4 ohm speaker
Controls：－Push－buttons（4 MW 1 EW）， manual tuning control，volumel on－0ff

Dimensions：－$\quad 7^{\prime \prime}$ wide $2^{\prime \prime}$ high $4 \frac{1}{2}{ }^{\prime \prime}$ deep approx．
The supply voltage is nominaliy $\mathbf{t 2}$ volts．The polarity， relative to the case，can be changed over internally simply by reversing twa push－on tags．The circult is protected by an internal fuse and a VDR（valtage dependent resistor）against statlc discharge．

Prices：－Car Radio Kit $\mathbf{1} 7 \cdot 70+55 p$ P／P．Speaker， including baffle and fixing strip £1．65＋23p P／P． Car Aerial，fully retractable and locking $\$ 1 \cdot 37+20 p$ P／P．
Radio and TV Components（Acton）Ltd．， 21 High Street，Acton，London，W3 6NG


The contents of your kit will toon like this, teft. Between the metal casing is the permeabithy lunling unlk and pushbultor assembly. Bottom tight shows the complete PCB which is fully lested before despatch.
If the simple instructions are followed the aimost finlshed sel should look the that in the photograph befow. Only the dist, escutcheon and knobs remaln to be ftteo plus the cover

can be and cover every contingency. There is one point here that might be stressed. If you use the aerial available trom RT-VC the feeder is about ' $^{\prime} 6^{\prime \prime}$ long and the aerial trimmer works perfectly, peaking signais as it should do, when the overall performance is excellent. However, If you need to fit the aerial to the car in such a position that requires the feeder to be extended then this must be done using a special extension lead otherwlse pertormance will definitely be Impaired. Using ordinary coaxial cable just will not work. This point is fully co vered in the instructions.

Apart from the manual tuning over both bands, four of the push-buttons can be set very easily to any desired stations on the MW band, the filth push-button selecting a station on the LW band, usually BBC Radio 2, the band change being automatically effected by the action of the push-button. 14 , for some strange reason, the set does not work at all. or unsatisfactorlly, then the Fautt Finding Guide will come to your aid and the answer found very quickly.

## Interference

Having completed the installation and tested the radio to your satisfaction there is a chance that you will suffer a slight set-back when starting the car, because of inter-
ference to the radio from the various blts of electrical equipment. Generally, unless the car is a real old 'banger', normal suppression capacitors and other devices wlll be fitted to the car already and little trouble will arise. However, this matter is dealt with fully in the notes and if the logical sequence of checking is followed a rapid solution will ba found.

## Conclusions

A very well designed kit with all the bugs ironed out long ago. Being a bit of a fiddler myself I would have liked the oscillator and aerlal trimmer capacitors to be accessible from the outside of the case when the radlo is installed in the car. I compromised by very carefully marking out and drilling two holes in the top cover of the case above the trimmers, sticking a bit of Sellotape over the holes when I had done fiddlling. I wouldn't expect RT-VC to do anything about this point but thought I'd mention it, got to complain about something!

Flnally, I don't know how RT-VC do it at the price but I understand it is due to the purchasing in volume of proven components and direct retail sales. Certainly they are not contributing to the present inflationary movement!

Test gear is often conspicuous by its absence from the amateur's workshop, possibly because such equipment can be expensive to buy but, more likely, because it is not a justifiable outlay considering the relatively few occasions on which it would be used.

The Capacity bridge described here is very cheap to make, will measure capacities from as low as 2 pF and up to about $10 \mu \mathrm{~F}$ and will be found to be quite adequate for general workshop use. Over a period the constructor manages to collect unto himself a quantity of capacitors that have had their markings removed in one way or another. This bridge will enable them to be measured, checked and used again. Incidentally, it is a very wise man who checks the value of every component before using it, regardless of colour code or marking, saving a lot of time and temper.

It is not everyone who has good eyesight and even slight colour blindness can cause confusion with colour coded components, generally with blues, browns and greens, which can lead to wrong values of resistors and capacitors being fitted to PCBs etc. This bridge will eliminate any such problems especially if it is used as a matter of routine.
The dial is simple and easily calibrated and used in conjunction with a four step multiplier switch. The consumption of the bridge is very low and the internal 9 volt battery will last a very long time.

## DESIGN

As you may have guessed, a bridge circuit is used, what else! and was last seen in the Take 20 series


Fig. 1: Thls cifcull IWustrates how the coffector load resistor of an audio oscilimetor is used as part of a capacily measuring britge.
in this magazine. In essence, the collector load resistor of the second transistor of an audio oscillator forms two sides of the bridge, Fig. 1, and, in practice, is a potentiometer. The other two sides of the bridge comprise a capacitor Cs of known value and $C x$, the capacitor under test. If these capacitors have the same value then, for the bridge to balance, R1 will equal R2. A detecting device ' D ' placed across the bridge will indicate a null in the audio tone under these conditions. If Cx is any other value then the bridge is unbalanced and ' $D$ ' will indicate this. Balance can be restored if the ratio of $\mathrm{R} 1 / 2$ is adjusted to have the same ratio as $\mathrm{Cs} / \mathrm{Cx}$.

In the practical circuit, Fig. 2, Cs is in the form of a four position multiplier switch with capacitors of $100 \mathrm{pF}, 1000 \mathrm{pF}, 0.01 \mu \mathrm{~F}$ and $0 \cdot 1 \mu \mathrm{~F}$ all of close tolerance, the switch being marked $\mathrm{xl}, \mathrm{x} 10$, x100

Fig. 2: Complete circuil of the capa- cilly bridge derived from the basle circult of Fig. 1. Other types of transistor suich as BC109, BC149, 8C169 can be used if due note is taken of lead-out cornnections.


In this lastife view of the brifge the capacitors have been moved away from the switch st to show the circult board
and $\times 1000$. The capacitor under test is comected to the two terminals. Transistors Tr 1 and $\mathrm{Tr}^{2}$ form a multivibrator circuit rumming at about 1 kHz but the actual frequency is not of any great importance.

The detector is a simple cyystal earphone of very high impodance, this factor contributing very significantly to the excellent performance of the bridge, the minimal damping imposed by the earphone providing a deep sharp null at balance.

## CONSTRUCTION

The bridge is housed in a heavy plastic box with all the components mounted on an aluminium panel. The oscillator components, with the exception of the potentionneter VR1, are assembled on a small piece of Veroboard as in Fig. 3. The bottom rail of the board is soldered to a tag bolted to the panel, providing adequate support for the board.


Fig. 3: Components comprising the audio oscillator are mounted on Veroboard as shown above.

The test terminals are spring loaded, their soldering tags passing through $3_{8}$ in. holes drilled in the panel. The holes are purposely large to reduce self capacity. An alternative might be to use feedthrough insulators terminated on top of the panel with miniature crocodile clips on stiff leads. Whatever arrangement is used it is essential that a capacitor can be connected to the bridge and removed again very easily.

The potentiometer is a very ordinary linear carbon one with a plastic spindle, which, again, reduces self capacity but one with a metal spindle would probably work just as well. The dial was made from a disc of card held under the potentiometer fixing nut together with a pointer knob of such a size as to allow a single range of calibration figures to be marked on the dial. The dial is marked in the 'preferred' range of values corresponding to the standard markings on capacitors.

The crystal earphone is wired directly into the circuit, which again lielps to reduce capacity. A combined phone jack and on/off switch was contemplated but a switch and isolated jack could not be found. If any doubt exists as to whether an earpiece is crystal or magnetic it can be checked with an ohmmeter. A magnetic one will show very low resistance whereas a crystal one will show, effectively, an open circuit. Just to make sure that you havn't got an open circuited magnetic earphone put it in the ear and check again with the meter when clicks should be heard even though the meter indicates an open circuit.

The multiplier switch used here is a miniature ceramic one but the more common plastic or paxolin wafer type will suffice. However, if the switch chosen has been used before it must be very thoroughly cleaned before using it in this bridge, for reasons which will be noted later. The standard capacitors C3 to C6 are wired directly between the switch tags and the top 9 volt rail on the circust board. If a standard size switch is used it will be necessary to move the board down from the position shown in the prototype. It is a good idea anyway, with any project, to shuffe the components around for best positioning before drilling panels etc.

## CALIBRATION

After the small amount of wiring is completed and checked, fit the PP3 battery and switch on when the audio tone should be heard in the earphone. The volume should be adjustable from maximum to zero using the potentiometer. Adjust the position of the knob on the potentiometer spindle so that the ends of its travel are positioned as shown in
the photograph of the bridge. Mark these positions on the dial with a sharp pencil. With the muttiplier switch on xl a null should be found near the top of the dial, if the potentiometer has been wired as shown in Fig. 2. This represents the zero position of the bridge without any external test capacitor Mark this point on the dial.


Cfose-up of the diat of the bridge. Note that the timits of teavel of the potentiometer are afso marked

With a $100 \mathrm{pF} 1 \%$ capacitor connected to the terminals and multiplier on $x 1$ find a new null at about mid position on the dial, then mark it. Turn multiplier to x 10 and locate null not far inside the 0 mark. This is marked 10. Note that we have been able to find two points on the dial for one capacitor, using the multiplier. This feature can be used to cross check dial readings.
Change the test capacitor for one of $100 \mathrm{pF} \quad 1 \%$ and mark the null at the bottom end of the dial. Switching to $x 10$ should locate the nult at the 100 point, already marked. The remainder of the calbration is done using $1 \%$ or $2 \%$ capacitors in the preferred range of $120,150,180,220,270,330,390$, $470,560,680$ and $820 \mathrm{p} F$. The xl multiplier is used to mark the remaining points between 100 and 1000 nF and $\times 10$ for the points between 10 and 100 pF .

## TOLERANCES

For a general purpose bridge the cheaper $5 \%$ tolerance capacitors are quite adequate for calibration purposes but instead of having to buy the thirteen preferred values it is possible to make do with eight only, the missing values being obtained by paralleling certain capacitors as shown in the Table. There are probably other combinations possible by connecting capacitors in series or even series paraltel!

The calibration can be completed with a fine balk point pen or a more fancy dial constructed, as shown in the plotograph. As the end points of the
potentiometer travel have been marked the dial can be removed for finishing or copying and then replaced without losing calibration.

## CALIBRATION CAPAC\&TORS (pF)

| 100 | 220 | 470 |
| :---: | :---: | :---: |
| 120 | $270^{*}$ | $560^{*}$ |
| 150 | $330^{*}$ | $680^{*}$ |
| 180 | $390^{*}$ | 820 |

The capacitors marked * may be obtained by connecting other values in parallel, as follows:-

| 270 | 120 | +150 | 330 | $150+180$ |
| :--- | :--- | :--- | :--- | :--- |
| 390 | 220 | +180 | 560 | 220 |
|  |  | 280 | 220 | $180+150$ |

## EXTENDING RANGE

As shown, the maximum capacity indicated on the dial is $1000 \times 1000 \mathrm{pF}$ or $\mathrm{l}_{\mathrm{p}} \mathrm{F}$ but it was later found possible to extend this range to $10 \mu \mathrm{~F}$ enabling small value eiectrolytic capacitors to be checked, although it should be remarked that there is no polarising voltage applied to the capacitor under test. Nevertheless the bridge has been found very useful for this purpose.

The accuracy of this extension $1010,4 \mathrm{~F}$ will depend upon the accuracy of a $1 \mu \mathrm{~F}$ capacitor that is required for calibration. Again, a $5 \%$ tolerance will do as a $1 \%$ capacitor of this value is rather expensive. Connect across the test terminals and locate a null near to the bottom end of the travel, past the 1000 mark. The multiplier should be on $\times 1000$. The point can be marked 10 nF for simplicity. Only two or three intermediate points are required such as 2200 , 4700 and i 800.

## IN USE

Normally the null will be very deep and sharp. In my own case, the audio tone actually disappears at the null point and I generally consider my hearing

## components list

## Resistors

R1 $10 \mathrm{kS} 10 \%$ or $\frac{1}{2} \mathrm{~W}$ R2/3 $1 \mathrm{MA} 10 \% \ddagger$ or $\frac{1}{4} \mathrm{~W}$ VH1 tok $\Omega$ linear carbon potentiometer. See text

## Capacitors

| C3 | $1000 \mathrm{pF} 10 \%$ |
| :--- | :--- |
| C2 | $1000 \mathrm{pF} 10 \%$ |
| C3 | $100 \mathrm{pF} 1 \% \mathrm{SM}$ |
| C4 | $1000 \mathrm{pF} 1 \% \mathrm{SM}$ |

C5 $0.01 \mu \mathrm{~F} 1 \%$ SM or Polystyrene
C6 $0.1 \mu$ F $1 \%$ Poly. styrene
C7 $100 \mu \mathrm{~F} 16 \mathrm{~V}$ electrolytic
Calibration Capacitors:-see rext and table

## Miscellaneous

Tri/2 2N2926G. Crystal earphone. Battery 9V PP3, battery clips. Onfoff switch, Veroboard 0.15 in . matrix, approx. 2i $\times 1 \mathrm{fin}$. Knob and dial. Yerminals (2). Case and panel $5 \times 2 \mathrm{f} \times 1$ jn. deep (Stella 99 series, from E, R. Nicholls 46 Lowfleld Rd., Stockport, Cheshire.) $\$ 1$, Single pote 4 -way wafer switch.
to be better than average. If the null is not deep and seems to be undefined then the capacitor is probably leaky although it may be of the order of a few megohms. The effect can be simulated by connecting a high value resistor across a known good capacitor and lesting the combination on the bridge. The lower the resistarce the poorer will be the null. In the long run it is better to destroy such leaky capacitors at the time of testing rather than to leave them around to be used in equipment where the leakage might prove highly detrimental to the operation of a circuit

## AUDIO OSCILLATOR

The bridge can also be used as a source of audio tone for testing amplifiers and suchlike, the output being taken from the test terminals and adjustable from zero to maximum output with the potentiometer. The waveform is very rough, of course, coming from a multivibrator but quite adequate for general audio testing. If a Morse key is connected across the on/off switcs the unit can be used as a Morse code practice set. A second ciystal earpiece can be connected across the test terminals and, if two keys are connected in parallel, two-way simulated signalling will be possible.

## PWTECHNICROSS UZZILE No. 7

## presented last month



TEEMETID

## IN THE DECEMBER ISSUE

## SIGNAL STRENGTH METER

Correct aerial alignment is important if bright, sharp plctures free from blurring due to multipath reception, stabiy synchronised and with accurate grain-tree colour are to be achieved. This is difficult without a signal strength meter since the receiver's a.g.c. system will hide signal strength variations-quite apart from the physical problems. The TV signal strength meter described is portable and can be used to ensure that any u.h.f. TV aerial is aligned for oplimum reception: it is equally useful in local and fringe areas. Features include varicap tuning, three gain ranges and a unique Indicator of vision carrier reception by means of a light-emitting diode. Construction is easy since a ready-made surplus i.f. strip is used.

## OECODER FAULT-FINDING

Colour receiver decoders are generatly reliable but when they do give trouble lault-finding can be a headache. In "Practical Decoder Fault Finding" in this issue a number of useful hints and tips based on practical experience are given together with guidance on the logical approach to tracing faults.

## SELF-CONVERGING COLOUR C.R.T.S

The next generation of colour sets-nalready beginning 10 appear on the market-wlll be fitted with self-converging c.f.t. /deflection yoke systems. How these operate, with particular reference to the Mitsubishi SSS tube, will be described.

## SERVICING TELEVISION RECEIVERS

The Baird/Radio Rentals 650,670 and 680 series of TV receivers and their faults will be described by Les Lawry-Johns.

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## ON RECENT DEVELOPMENTS

## MEASUREMENT

IT never ceases to amaze me that measurement in electronics gets more and more sophisticated as every day passes. On reflection this must be so because as the very latest devices are born, some means must be to hand with which to measure, accurately, their performance. At the recent International Microwave Exhibition at Montreux, for example, there were switches shown which could switch at 26 GHz -that's twentysix thousand million times every second! I might add that the man on the stand eagerly told me, ".... and of course we're working on higher frequencies right now'.

While frequency must be measured accurately, what about time? Latest to come to my attention is a time interval counter which is soon to be launched in America. The amazing thing about this one is that it has a resolution of 100 Femtoseconds. If you are not impressed then let me add that a Femtosecond is 0.001 of a picosecond and a picosecond is one millionth of a microsecond which, of course, is one millionth of the common or garden everyday household second. For the technical/boffin types it's $10^{-15}$ seconds. Just think if every Amateur radio station had one of these, it could tell its transmission frequency to a fraction of a cycle even at v.h.f.

## TIMED CALCULATION

Electronic calculators and digital wrist watches always create interest but now I really have heard it all. The ultimate is about to be launched onto the market, something that will satisfy even the most pedantic of tiros. It's a digital wrist watch and calculator combined! The calculator part has a nine digit readout and offers forty functions. When it's not used as a calculator it functions as a digital watch. There are only 20 buttons on the calculator and here the designers have introduced a very crafty dodge.

Although only twenty buttons are employed (because of space considerations) there's a "shift key" which, when activated, gives the twenty buttons other functions thus
giving a 40 button capability. This shift key acts something like the shift key on a typewriter which allows the same keys to be either capital letters or small, lower case letters. The watch/calculator measures about $1.5 \mathrm{in} \times 1.5 \mathrm{in} \times 0.5 \mathrm{in}$. deep. The first models are rumoured to be priced at around $£ 200$ - $£ 250$ but they're not available yet and probably won't be for some time. The buttons, incidentally, are depressed with a small probe, or tip of a ballpoint pen as far as 1 can ascertain. Information is rather scant because this is a state of the art unit and the information is red hot.

## SOLID-STATE C.R.T?

A colleague in Washington reports that the US Army may soon lay its hands on a liquid crystal display which gives an 84 -character output. It also might be used as a liquid crystal cathode ray tube. At present the company doing the development is waiting to get a Government grant with which to continue work. It is also rumoured that the prototype device is coupled up to a miniature warfare computer. If this development is well funded, it could be another avenue of development for the solid state c.r.t. for television receivers.

## SOLID-STATE CAMERA

At the other end of the television signal-the camera, developments are pressing on with solid state sensors which will replace the vidicon camera tubes. This was highlighted at the recent conference on charge coupled devices (c.c.ds) which took place at Edinburgh University. Of great interest was mention (plus photograph) of a miniature entirely solid state television camera which was constructed by Bell Labs at Murray Hill, New Jersey. Another interesting fact about this television camera is that it is battery operated. The size was not mentioned but from objects in the photograph which include a ruler, it is judged to be of the order of $11 \mathrm{~cm} \times 6 \mathrm{~cm}$.

The camera uses a chip sensor which has $256 \times 220$ element array gives excellent results using NTSC scan rates and the author claims
that television image sensors with 525 and 625 line capability are now a viable product. It must be remembered that solid state cameras will not come in over night. At present, users of the "valve" type camera tubes have only to plug in a component and it works whereas these solid state items are still being developed. However, with the world shortage of silver and the search for some other means of photography, it isn't too difficult to see the amateur photographer of the future holding a tiny solid state twin lens reflex which records directly onto tape which can then be played back on the television receiver at home.
These CCD devices are well worth watching. New applications are coming up and are being enthusiastically worked on. To date they are being used in TV applications, infra red cameras, delay lines, telecommunications, memories for computers and are even employed to generate a s.s.b. signal.

## IT'S SIMPLE!

The servicing of televison sets has taken a step nearer to being automated. Grundig colour television receivers are currently manufactured in modular form. A number of modules are used in a plug-in fashion, each unit looking after a specific function within the receiver.
The offending module (in the case of malfunction) is simply unplugged and either repaired immediately or just replaced and then repaired at leisure in the workshop.
Some $75 \%$ of the colour television circuitry is catered for in this way. Now, Grundig has taken care of the other $25 \%$ by adding a simple socket to the receivers. A small diagnostic unit is then simply plugged in. The circuitry is featured on the lid of the diagnostic box, and l.e.ds mounted in this circuit diagram illuminate to pinpoint any fault.
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* IMPORTANT NOTE

This fine receiver is not a mass produced item, but each set is hand built to your order, individually checked and air zested. Please allow for this when ordering-your delivery date will be shown on your order reteiph, sent by return.

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# MAKE YロUR PCB 

## JOHN JACKSON

FOR the amateur, printed rireuit boards hase good and bad points. They are neat. reduce free wiring. make assembly mistakes less likely and can support large items such as transtormers. On the other hand. they take time to make and subsequent modification to them cim be difficult.

Ready-made "universal" printed circuit boards may have no copper where it is required, will have it where it is not needed and mistakes during soldering are easy as different areas look alike. The design and preparation of indiviclual boards is easy and the materials readily available.

## DESIGN

The method used successfully for many projects is as follows. A fairly lasge copy of the circuit is drawn on thin paper. such as that used for typing (thin paper saves time later). All component junctions are ringed, as shown dotted in Fig. 1, to give the basic copper plan. Beneath this is drawn an outline, the size of the intended circuit board and, using components to check spacings, the basic plan is adapted to give a full size layout, Fig. 2.
'Trl.l.1. A mumber can be coosed off rath time a connection is allowed for.

A negative of the plan must now be made. This is easily done by turning the paper over and drawing over the lines that should be visible. This plan is the master diagram, see Fig. 3.

It is possible to forget to reverse the plan, which is not serious with transistor circuits, but it will be tricky reversing a nine-pin valve-holder to match!

## PREPARING THE BOARD

Copper laminate may be backed by tibreglass or SRBP, the latter being cheaper. Areas requiring copper, the "fields", are covered with resist and the unwanted metal is etched away. Resist can be from a purpose-made pen, such as a "Dalo" or use can be made of nail lacquer or paint (thinned enamel or cellulose).

First the board must be cut to size, with a hacksaw having a fine blade, cutting with the copper side up. After filing off any burred edges the copper must be thoroughly cleaned of grease or tarnish, using


Fig. 1: This erccult, used to demonstrate the aroduction of? a printed circwit botard, is of a Gurshot Simulator that appeared in the April 1972 issue of PW in the Take-20 serles.

In the final layout it is advisable to keep input and output points apart and wires leaving the board are better near the edges. Fixing holes must be taken into account and copper should not be too close to these, to prevent shorting to metalwork. To avoid missing a component, a list can be made with each component written once for each wire: R1,1, R2,2,
scouring powder on cotton wool. After rinsing and drying on a soft cloth the copper is ready for the resist and the board must be held only at the edges, as any grease may cause the resist to flake off and prevent areas from etching.

The board is then stuck beneath the master diagram, with a piece of Sellotape to reduce handling,


Fig. 2: The dotted areas of Fig. 1 are transferred to the paper master as shown here, the final layout depending upon the sizes of the components to be used. The copper will be on the other side of the board, which is shown here twice final size.


Fig. 3 When the layout is finalised it must be reversed on to the board as shown here, complete with the holes required, drilled after etching.
and a piece of carbon paper in between, carbon side down against the copper surface. Draw over the master with a pencil which will leave the outlines on the copper. Remove master and carbon paper after which the resist can be painted on the areas of copper which are to be retained. While the resist dries the etching solution can be prepared.

## ETCHING

Ferric chloride is used which can be bought from advertisers in this magazine. One pound will etch many boards. A suitable strength is about one tablespoon per fluid ounce of water. The crystals should be added to the water, not vice versa, and this should be done with care as a lot of heat is generated. The solution may attack skin if splashes are not rinsed off and it will stain cloth and wood, so work over newspaper. The solution must be used in a non-metal dish, a saucer is ideal, and after use it can be stored in an old bottle with a plastic top.

If the prepared board is carefully levered off the paper, the Sellotape can be used as a handle. The board is placed gently on the etching solution copper side down. Surface tension will support it and the insoluble etching product can sink to the bottom, no agitation being necessary. After five minutes or so
lift the board and see that all the copper shows pink. Greasy finger marks show brown and unetched. If all is well, allow the process to continue, taking roughly twenty minutes. When all the unwanted copper has gone the board should be thoroughly rinsed with water and then the resist can be removed. "Dalo" or nail varnish will come off with nail varnish remover (acetone) while paint will require white spirit or stripper. A final wash with soapy water will leave the board ready for drilling.

## DRILLING AND SOLDERING

Drilling should be done with as fine a drill as possible, for a hand drill this will be about ${ }^{{ }^{1} 10} 10$. dia. The slow speed on an electric drill is suitable but only gentle pressure must be used or the board will crack. It will be helpful to mark all the holes with a sharp point (a centre punch will not do) first, then hold the board in front of a piece of wood, in a vice, and drill all the holes. Any burrs can be removed with a larger drill. The board is now ready for use.

The bond holding the copper to the board material is strong but too much applied heat may cause the copper to peel off. As usual, resistors and other passive components should be soldered before semiconductors, though connecting wires should be left until last.

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tran |  |  | 14 | BCY 30 | ${ }_{688}^{588}$ |  | 839 |  |  | ${ }^{2} \mathbf{N} 930$ | ${ }_{285}$ |  |  | ins ${ }^{\text {in }} 007$ | ${ }_{4 p}^{88 p}$ | ${ }^{2437}$ | $770$ |  | 88.20 |
| ${ }_{\text {AA }}{ }_{\text {Al107 }}$ |  | ${ }_{\text {BA156 }}$ | ${ }_{180}^{180}$ | ${ }^{\text {BCY }} 31$ <br> BCY70 | 17 | M M E0491 | ${ }_{\text {23, }}^{23}$ | NK T773 | ${ }_{0010}^{80 \%}$ |  | 885 | mistors |  |  | ${ }^{4}$ net | ${ }_{7440}^{7738}$ | 870 | ${ }^{71155}$ | $7^{7}$ |
| ${ }_{\text {Act } 26}$ |  |  | ${ }_{8 p}$ | BCY71 |  | ME0493 | 21p |  | 19 | 2N3132 | ${ }_{808} 8$ | VA10868 | 15p |  |  |  | 1 |  |  |
| ${ }^{\text {ACl }}$ | $18 p$ | bC10 | 140 | BCY72 | , | M 11001 | 16 D | oalo | D | ${ }_{2}{ }^{\text {N1303 }}$ | ${ }_{800}$ | VA10568 |  | 3.37 to | 3\% 18p |  |  | 74160 | ${ }^{8}$ |
|  | 18 p | BC1 | 149 | ${ }^{\text {BDI } 24}$ | 1.80 | ME1002 | 17 p | OA47 |  |  | ${ }^{380}$ | VA1067 | ${ }^{16 p}$ |  |  |  |  |  |  |
| AC141 | 88 | BC10 | 149 | BD131 | 483 | M | 19D | - | D | 2N130 | ${ }^{885}$ | VA1089 | ${ }_{14}$ | Thyrist | tors |  |  |  |  |
| AC141F | 80, | ${ }^{\text {BCII }} 1$ | ${ }^{18}$ | BD182 | 57p |  | 208 | - | 8 | 2N1308 | 478 |  | $14 p$ | 30v |  |  |  | ${ }^{74163}$ |  |
| ${ }_{\text {ACl }}{ }_{\text {A } 22}$ | ${ }^{2}$ | ${ }_{\text {BCl1 }}^{\text {BCI }}$ | ${ }_{19 p}^{19}$ | ${ }_{\substack{\text { BD131 } \\ \text { BD } 131}}$ | ${ }^{121} 18$ | ${ }_{\text {ME2001 }}^{\text {M } 1120}$ | ${ }_{150}^{209}$ | ${ }_{\text {(HG1005 }}$ | 7 | ${ }^{2 N 1807}$ | 439 | VA1077 | ${ }_{14 p}^{15 p}$ |  | 889 | 74 | ${ }_{61}^{10.68}$ | ${ }_{71165}^{74164}$ |  |
|  | \%85 | ${ }_{\text {BCLI }}$ | 885 | ${ }_{\text {BDY }}$ |  | M ${ }^{2} 20$ | 16p | OA200 | p |  | 56 |  |  | ${ }^{2000}$ | 97 | 24 | 81.98 | 71168 |  |
|  |  | ${ }^{\text {BCCI}}$ | P | ${ }^{\text {BFI}}$ |  | M ${ }_{\text {E3001 }}$ | 210 | OA202 | 9 | ${ }_{2}{ }^{\text {N1613 }}$ | 24 | Bridge |  | 3 mmp | 69 | 74 | Op | ${ }^{74174}$ |  |
| ${ }_{\text {ACLIS32k }}$ | ${ }_{\mathbf{M} / \mathrm{P}}^{\text {8, }}$ |  | ${ }_{19 p}^{179}$ | ${ }_{\text {BF177 }}$ |  |  |  |  | 569 | ${ }^{2 \mathrm{~N} 1711}$ | 280 |  |  | 50v | 80, |  | 5p | 711 |  |
| $\mathrm{ACl}^{\text {A } 176 \mathrm{E}}$ | ${ }_{889}$ | ${ }^{\text {BCLI }} 1$ | 19 | ${ }_{\text {BFI78 }}$ | 8 | ${ }_{\text {M }}$ | ${ }_{10 p} 18$ | ${ }_{\text {OC28 }}$ | ${ }_{65 p} 6$ |  | \% | emp |  |  |  |  |  |  |  |
| ${ }^{\text {a clife }}$ | ${ }^{\text {42p }}$ |  | 289 | BF179 | ${ }^{285}$ | ME4002 | ${ }^{178}$ | ${ }_{0} \mathbf{0} 29$ | 690 | 2N2218 | 489 | 200 v | ${ }_{\text {48p }}{ }_{\text {ap }}$ | ${ }_{200 \mathrm{~V}}^{200 \mathrm{~V}}$ | 89p | 74 | 0 |  |  |
| $1{ }^{1} 176$ | ${ }^{218}$ | ${ }^{\text {BC147 }}$ | ${ }^{129}$ | BFI94 | 16p | M E4003 | ${ }^{187}$ | OC36 | 59p |  | ${ }_{888}$ | Or | \% |  |  | ${ }_{7} 77278$ |  |  |  |
| ${ }_{\text {Aciazt }}{ }^{\text {AC178 }}$ | ${ }_{28 p}^{29}$ | ${ }_{\text {B }}$ | 118 | ${ }_{\text {BFIPs }}$ | 180 | ${ }_{\text {M M } 4101}^{\text {M } 4102}$ | ${ }^{178}$ | ${ }^{\text {OC36 }}$ |  | 2N24 | 40p | 2 mmp |  | ${ }^{1000}$ | ${ }_{4}^{468}$ | 仿 | ${ }^{2}$ | 71190 | ${ }^{38} 8.08$ |
|  | 28p | ${ }^{\text {BC }}$ | 170 | ${ }_{\text {BFF } 254}$ | ${ }_{18}$ | ME4103 | 18 p | ${ }^{\circ} \mathrm{CH} 4$ | 80 | ${ }_{2}^{2 \mathrm{~N}^{28}}$ | ${ }_{\text {Sis }}$ | ${ }^{\text {S0V }}$ | ${ }^{489}$ |  | 607 | ${ }^{7474}$ | 93 | ${ }_{71191}$ | 28.80 |
| ${ }_{\text {AClisg }}$ | 238 | ${ }^{\text {BC158 }}$ | 16 | ${ }^{\text {Br }}{ }^{\text {2 } 29}$ | ${ }^{48}$ |  | ${ }^{16 p}$ | OC45 | $20 \%$ | 2N2905 | 200 |  | 870 |  |  |  |  | 741 |  |
| ${ }_{4}$ | ${ }^{29}$ |  | 16 | ${ }_{\text {Bry }}^{\text {Bry }}$ | ${ }^{288}$ | ${ }_{4}^{\text {MEA }}$ | ${ }_{10 p}^{18 p}$ | ${ }^{\text {ochi }}$ | 18 | 2N23053 | ${ }^{288}$ | 50v |  | 2 am | 70, | 74 | 8 | 74 |  |
| ${ }^{\text {A Cry }}$ | 20p | ${ }^{\text {BC1 }} 168$ | 18 | BFX | 255 | M EaO | 17 p | $\mathrm{OCF}^{\text {c }}$ | 18 p | ${ }_{2 \text { 2N30 }}^{2 N}$ | ${ }_{49}^{238}$ | 200 v | ${ }^{11.98}$ | ${ }^{1}$ |  | ${ }^{7481}$ | 17 | 741 |  |
| ${ }_{\text {ACY }}$ | ${ }_{\text {23p }}^{80}$ | ${ }^{\text {BC1 }}$ B9 ${ }^{\text {a }}$ | ${ }^{135}$ |  | ${ }^{275}$ | ME610 | 19 | ${ }^{00785}$ | ${ }_{\text {ckip }}$ | 2N3702 | $18 p$ | ${ }_{10} 0_{\text {cmp }}^{40 \mathrm{v}}$ |  | 10 | ${ }^{80 p}$ | 743 | ${ }_{31}{ }^{1}$ | 71 |  |
| ACY22 | 19p | ${ }_{\text {BC178 }}$ | ${ }^{210}$ | BFY ${ }^{\text {P }}$ | 239 | ME800 | 19 | Ocal | 258 | ${ }^{2} \mathbf{2} 87808$ | 11 p | 50v |  |  | 11:30 | ${ }_{78 \text { dib }}$ | 41. ${ }^{4}$ | ${ }_{7199}$ |  |
| ${ }_{\text {ADI }}$ | ${ }^{67 \%}$ | ${ }_{\text {BC182 }}$ | 24 | ${ }^{\text {BrY } 51}$ | 193 |  | 210 | ocss | 2ap |  | 18 | ${ }^{100 \mathrm{v}}$ | 20. 61 | 74 | 200 | 7486 |  |  |  |
| $\chi_{4} 0143$ | ${ }_{68 p}$ |  |  |  | P | ${ }_{\text {M }}^{\text {ME8003 }}$ | 88p | ${ }_{\substack{\text { OC84 } \\ \text { TIP29 }}}$ | 88p | ${ }_{2} \mathbf{N} 3706$ | ${ }_{11}$ |  |  | 202 | 20\% | ${ }^{7489}$ |  | IC |  |
| AD | ${ }_{880}^{858}$ | ${ }^{\text {BCO}}$ | 18 | ${ }_{\text {BY }}$ | ${ }^{175}$ | Me9 | 118 | ${ }_{\text {TrPa }}$ |  | ${ }_{2}^{2 \times 3707}$ | ${ }^{11}$ | Silic |  | ${ }_{7404} 7403$ | ${ }_{810}^{20}$ | (992 | \% |  |  |
| AD162 | ${ }_{40}$ | ${ }^{\text {BC213 }}$ | 1 | ${ }^{\text {BYY }} 127$ | 17p | ${ }_{\text {M }}$ | 190 | ${ }_{\text {TIP32 }}$ | ${ }_{88}^{78}$ | ${ }^{2} \mathbf{2 N 3 7 0 8}$ | ${ }_{11 p}^{10 p}$ | Rec |  | 740 | ${ }_{410} 18$ | 7894 | 41.04 |  |  |
|  |  | ${ }_{\text {BC }}$ | ${ }_{15}$ | ${ }_{\text {BFZ210 }}^{\text {Br2 }}$ | Pp | ${ }_{\text {M }}$ | 189 | TIP33 | 䂙 | 2N3710 | 111 |  | 7p | ${ }_{7407} 7$ | $4{ }_{40}$ | ${ }^{2} 89$ |  | ${ }_{723} 709 \mathrm{C}$ |  |
| ${ }^{\text {AFF14 }}$ | 20 | ${ }^{\text {b }}$ | 185 |  |  | ME81 | 889 | ${ }_{T 1 \text { TP354 }}$ |  |  | 200 | iN10 | 8 | ${ }_{7}^{7408}$ | ${ }_{\text {288 }} 88$ | 7est | ${ }_{51} 1.14$ | 723 c |  |
| ${ }_{\text {AP }}^{\text {AF }}$ | 800 | ${ }^{\text {BC }}$ | ${ }_{14 p}^{150}$ | ${ }_{\text {C4Y }}$ | 888, | ${ }_{\text {MP8 }}^{\text {M }}$ | ${ }_{\text {40p }}^{40}$ | ${ }_{\text {TP1P884 }}$ |  | - 2 2N3819 | ${ }_{278}^{209}$ | INT0 | ${ }_{\text {10p }}^{00}$ | 74 | ${ }_{\text {cop }}$ | 7100 |  |  |  |
| ${ }_{\text {AFII }}$ | ${ }_{808}$ | ${ }_{\text {BC268 }}$ | ${ }_{18} 18$ | ${ }_{\text {M }}$ | ${ }^{18 p}$ |  |  | ${ }_{\text {TIP4 } 42}$ |  | ${ }^{2 \mathrm{~N}^{2926}}$ | 119 |  | $11 p$ | 741 | ${ }^{86}$ | J 310 |  |  |  |
| AP1 | 29p | BC269 | $14{ }^{\circ}$ | M | 408 | NET | $2 \%$ | ${ }_{\text {TIP }}$ TP2855311 |  | 2N39008 | 178 | ${ }_{\text {PL }}{ }_{\text {PL }}$ | \% | 74 | ${ }_{88}^{40}$ | ${ }_{\text {Jtiob }}$ |  |  | $3{ }^{3}$ |
| ${ }_{\text {AFP128 }}$ | 290 | ${ }_{\text {BC }}$ | ${ }_{\text {18P }}^{185}$ |  | 209 | ${ }_{\text {NKT }}$ | ${ }_{88 p}^{87}$ | TIP3054 | 60 | 2 N 403 | \% |  | 100 | 74 | 9P8 | 74 |  | ${ }_{747} 7$ |  |
| ${ }_{\text {AFP127 }}$ | 20 | ${ }_{\text {BC2 }}$ | ${ }_{\text {ctip }}$ |  | ${ }_{40}$ | NKT281 | ${ }_{\text {ckp }}$ | ${ }_{\text {TIP }}$ | 88 |  | 139 | ${ }_{\text {PL }}$ | 11 | 7417 | $4{ }^{48}$ |  |  | 748 c |  |
| ${ }^{\text {AFP139 }}$ | 88 | ${ }^{\text {BCO}}$ |  | MeS | 18p | NET27 | 21p | ${ }^{7} 763$ | ${ }^{\text {83p }}$ | ${ }_{2 \text { 2N } 4060}$ | ${ }_{139}$ |  | $10^{\circ}$ | 74 | 80p |  |  |  |  |
| ${ }_{\text {AF }}^{4} \mathbf{4 7 9}$ | 789 |  | 48 | M M EO40 | 198 | N ${ }^{\text {NT2 } 24}$ | ${ }_{778}$ | iN338 | ${ }^{11}$ | 2N4061 | $13 p$ | PLA0 | 178 | 74 | ${ }^{60}$ | 2119 |  |  |  |
| A 4 Y28 | 299 | BC | 40, | ME0411 | 28 | NKT404 | 729 | 1N916 | \% | 2N4062 | 12p | INS | 18p |  | ${ }_{48}$ | ${ }_{712}$ |  |  |  |
| ${ }_{\text {A AFY }}$ | 50 | ${ }_{\text {BC302 }}^{\text {BC303 }}$ | ${ }_{40} 38$ | ME0012 | ${ }^{219}$ | NKT | ${ }^{989}$ | IN148 | 5 | ${ }_{\text {ans }}{ }_{\text {2N } 1792}$ | ${ }_{80}^{11 p}$ | INs | 209 | 7 |  |  |  | ${ }_{16}^{14 \mathrm{Pin}}$ | 2p |
| ${ }_{\text {Ar }}$ | 4 |  | 309 | ME0414 | $1{ }^{15}$ | NKT613F | 389 | 1544 | ${ }^{20}$ | 40361 | ${ }_{48} 8$ | inst04 | 23 | 7430 | 809 | 714 | - |  |  |
| ${ }_{\text {BAIIS }}$ | 10 p | ${ }_{\text {BC461 }}$ | 23 | ${ }_{\text {MEP0463 }}$ | ${ }_{\text {23p }}$ | NKT674F | 23p | 2N ${ }^{696}$ |  | 40362 | 48p | IN5405 | 28 | 7432 <br> 743 | csp |  |  |  |  |

Rasistors
watt $5 \%$ carbon 3.9 ohms to 10 meg watt $5 \%$ carbon
Fate $2 \%$ "
watt $5 \%$ carbon 5.6 ohms 10 meg Watt \% carbon 5.6 ohrms to 10 meg 5 wate wirewound 1 ohm to 6K8 ohms wht whrewound

Volume Controls
Potent lometern
Log or Linear
single
Dual Gang Btereo
Bingle \&ype with D.P. Bwitch
1489

Miniature Presets
Gribon gkeleton type
All valued 100 ohms to 5 meg ohme
1 watt 6 p each 25 witt 70 each

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mm neon indicator
Red or Amber
it $6 \mathrm{v}, 12 \mathrm{v}, 28 \mathrm{v}, 110 \mathrm{v}$ or 230 volt. 20 p each
miniature neon lemps
240v or 110
Hve tion 800 v DC. $\pm 1 \%$
Values in pFa 2.2 to 220 pF , 11p; 260 to 820 pF . ( 12 g:
1000 to $1800 \mathrm{pF}, 17 \mathrm{p} ; 2200 \mathrm{pF}, 19 \mathrm{p} ; 2700,3600 \cdot \mathrm{~F}, 8 \mathrm{p} ;$
$4700,5000 \mathrm{pF}, 88 \mathrm{p} ; 6800 \mathrm{pF}, 44 \mathrm{p} ; 8200,10,000 \mathrm{pF}, 55 \mathrm{p}$.
Tantalum Bead
Bolid tentalum capacitore Tol $\pm 20 \%$.
MF/voltage: $-1 / 35, \cdot 22 / 35,-33 / 35,-47 / 35,1 / 35,2 \cdot 2 / 35$ $4 \cdot 7 / 85,10 / 8 \cdot 8,10 / 16,10 / 25,22 / 16,47 / 6 \cdot 3,100 / 3_{*}$

Veroboard

| -1 | . 15 | Pla insertion |  |  |
| :---: | :---: | :---: | :---: | :---: |
| $2{ }^{21} \times 3188$ | 88 | tool | 88 | 88p |
| $21 \times 5 \quad 81 p$ | 818 |  |  | - |
| $37 \times 818$ | 318 | Spot face |  |  |
| $34 \times 5$ 17 $\times 85$ | 359 | cutter | 57\% | 57p |
| $17 \times 24$ | 749 |  | 87 | 67 p |
| $17 \times 34$ $17 \times 58188$ | . 11.18 | Pkt 50 |  |  |
| $17 \times 5$ Plain | 81.10 | Pina | 2\% | 22 |

## Electrolytic

Capacitors


 \begin{tabular}{ll|ll|ll|ll}
$100 \mu \mathrm{~F}$ \& 6 P \& $380 \mu \mathrm{~F}$ \& 10 P \& $100 \mu \mathrm{~F}$ \& 8 p \& $68 \mu \mu \mathrm{~F}$ \& 26 p <br>
$200 \mu \mathrm{~F}$ \& 6 p \& $470 \mu \mathrm{~F}$ \& 10 p \& $150 \mu \mathrm{~F}$ \& 8 p \& $1000 \mu \mathrm{~F}$ \& 25

 

$200 \mu \mathrm{~F}$ \& 1 P \& $1000 \mu \mathrm{~F}$ \& 11 p \& $100 \mu \mathrm{~F}$ \& $220 \mu \mathrm{~F}$ \& 10 p \& $2200 \mu \mathrm{~F}$ <br>
\hline $200 \mu \mathrm{~F}$

 

$1000 \mu \mathrm{~F}$ \& 18 p \& $1500 \mu \mathrm{~F}$ \& 80 <br>
$4700 \mu \mathrm{~F}$ \& 20 P \& $2200 \mu \mathrm{~F}$ \& 84
\end{tabular} 8.8 VOLT 16 VOLT



 \begin{tabular}{ll|l}
$150 \mu \mathrm{~F}$ \& 61 p \& $150 \mu \mathrm{~F}$ <br>
1051

 

$470 \mu \mathrm{~F}$ \& 11 p \& $150 \mu \mathrm{~F}$ <br>
$680 \mu \mathrm{~F}$ \& 18 F \& $200 \mu \mathrm{~F}$

 

$1500 \mu \mathrm{~F}$ \& 18 p \& $220 \mu \mathrm{~F}$ <br>
\hline $200 \mu \mathrm{~F}$

 $1500 \mu \mathrm{~F} 18 \mathrm{p} \quad 680 \mu \mathrm{~F} \quad 17$ 

$2200 \mu \mathrm{~F}$ \& 18 p \& $1000 \mu \mathrm{~F}$ \& 17 p <br>
$3800 \mu \mathrm{~F}$ \& \&

 

$3300 \mu \mathrm{~F}$ \& 269 \& $1500 \mu \mathrm{~F}$ <br>
$2000 \mu \mathrm{~F}$ \& 28 p

 

10 <br>
$22 \mu \mathrm{FOLT}$ \& $2000 \mu \mathrm{~F}$ \& 88 <br>
25 VOLT
\end{tabular}



Ceramics
Mindature Ceramics 50 v DC
All values 1.8 pF ot $10,000 \mathrm{pF}$ 8p each

## Mullards Polyester Capacitors

Ceso singits
250V P.C. mounting: $0.1 \mu \mathrm{~F}, 0.015,0.022$ 8tp. $0.038,0.047,0.068$ 4p. 0.144 . $0.15,0.2254 \mathrm{p} .0 .337 \mathrm{p} .0 .4704 \mathrm{p}$. 0.68 1. $1 \mu$




## £I BARGAIN PACKS

10 shilicon npn power transtatorn (2N3055), tested/un. marked.
30 Piastic FET's unmarked/untested. Bimilar to $2 N 3$ alo. 20 TOS transigtors npn 2 to $\$ \mathrm{~A}$, untented/unmarked. 20 TO18 translators pnp like BC178, BC179, etc., untented/ 30 Plastic
130 Plastic 2N305S, unmarked/unteated. TO220 ease.
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* Pair robust 50 watt speakers.
* Stereo headphones and microphone Complece System $£ 189.95$ Carriage $\mathbf{E 4 . 0 0}$.
* NO DEPOSIT terms available $\subset 10.63$ monthly over two years.

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THIS receiver accessory allows the reception of CW (Morse) and SSB (single sideband) signals particularly with receivers whose coverage includes any of the amateur bands. These bands are given below for the guidance of listeners who have not-so far paid much attention to them.

| 160 | metres | or | $1 \cdot 8$ | to $2 \cdot 0 \mathrm{MHz}$ |
| ---: | :--- | :--- | :--- | :--- |
| 80 | metres | or | $3 \cdot 5$ | to |
| $3 \cdot 8 \mathrm{MHz}$ |  |  |  |  |
| 40 | metres | or | $7 \cdot 0$ | to $7 \cdot 1 \mathrm{MHz}$ |
| 20 | metres | or $14 \cdot 0$ | to $14 \cdot 35 \mathrm{MHz}$ |  |
| 15 | metres | or $21 \cdot 0$ | to $21 \cdot 45 \mathrm{MHz}$ |  |
| 10 | metres | or $28 \cdot 0$ | to $29 \cdot 7 \mathrm{MHz}$ |  |

Short wave broadcasts use AM (amplitude modulation) and an envelope detector in the receiver demodulates this but this detector cannot provide the wanted audio output with CW or SSB signals. CW will be heard as an intermittent clicking and SSB as an unintelligible sound varying at syllabic rate. To receive CW a signal from the beat frequency oscillator is combined with the carrier, provided by the CW transmission, the difference in frequency between BFO and CW signals providing an audio output after detection. As a superhet receiver converts all incoming signals to a frequency of, usually, about 470 kHz (the intermediate frequency) the BFO is adjustable around this frequency. So if the 13 FO is set to 469 kHz or 471 kHz the CW is heard as a 1 kHz audio tone.

With SSB the carrier and one sideband are suppressed before transmission. When the BFO is adjusted to occupy the position of the missing carrier the transmission can be resolved and the detector provides intelligible speech.


- Fig. 1 : Circuit of the simple beat frequency oscillator.



## BFO CIRCUIT

This is shown in Fig. 1. The frequency is determined by the coil L1, with fine manual adjustment by the variable capacitor VCI. The coil is suitable for receivers with an intermediate frequency of about 455 kHz to 470 kHz but the actual frequency need not be known. Windings must be in the phase shown, to secure oscillation.

It is quite a good plan to operate the BFO from its own 9 V battery, the zener voltage regulator is not then necessary as satisfactory results can be obtained without it. But if current is taken from the battery running the receiver the current drawn by the receiver will vary considerably, especially at high volume level, so that stable operation of the BFO is impossible. In these circumstances, the zener is required for satisfactory reception.

## ASSEMBLY

The components are assembled on a small piece of perforated board, Fig. 2, with wiring underneath. The two points MC are ${ }^{1}{ }_{2}$ in. 6BA bolts, with tags, providing the chassis or negative return.
A piece of aluminium about $3 \times 1^{3}{ }_{4}$ in is bent at right-angles about $1^{3_{4}}{ }^{\text {in }}$ from one end. The pitch capacitor VC1 is fitted to the smaller flange. The other flange is drilled for the two 6BA bolts mentioned, so that the wired board can be locked in place, with leads and joints clear of the metal. Connect the variable capacitor fixed plates to pin 3 on L1, and the moving plates to one MC tag, Fig. 2.
$\star$ components list


## TESTING THE BFO

Set VCl half open. Tune in any AM signal on the receiver. Place an insulated lead from pin 2 of Ll near the IF circuitry of the receiver. Connect the BFO to the 9 V supply to be used. Rotating the core of Ll with a trimming tool should result in a setting being found where an audio tone arises. Set the core to the central or zero-beat position. If the core is rotated either way from this position an audio tone will be produced, rising in pitch as the core is turned.

Rotating VCl should now give a similar result. That is, a rising audio tone as the capacitor is rotated either way from the central or zero-beat position.

The BFO is not used for AM reception and slight re-setting of the core may be necessary after the unit is fitted in its case, if it is found that VCl comes at the fully open or fully closed position.

## BFO LOCATION

The BFO unit is only about $2^{1}{ }_{4} \times 1^{3}{ }_{4} \times 1^{1}{ }_{2}$ in so it may be fitted in almost any receiver, especially homeconstructed types. A reasonably large control knob is best on VCl and an on-off switch is necessary in the battery positive lead to the unit.


The unit itself is very small indeed so it can be fitted into a convenient corner in any receiver requiring a BFO.

It may be preferred to have the BFO as an external unit, with its own battery, when it can then be used with any receiver. To avoid troublesome handcapacity effects, the unit must be in a metal box. A box about $6 \times 3 \times 2{ }^{1}{ }_{2}$ in with a backplate fixed with self-tapping screws will be suitable. This will also take a 9 V battery and switch.

## COUPLING TO RECEIVER

A short insulated lead from pin 2 of L1, placed near the receiver or near the receiver IF stages, should normally give suitable coupling which is not too critical. Much looser coupling to the earlier IF


Fig. 2: Layout of components on top of the Veroboard and wiring beneath.
circuits will be required than to those at the diode end of the IF amplifier.

If coupling is too close, receiver sensitivity will fall off considerably when the BFO is switched on. Should coupling be too weak, strong SSB or CW signals will be difficult to resolve, while weak SSB or CW will be resolved easily. However, it should be an easy matter to move the lead. from the BFO, or to cut it down, until results are satisfactory.

## RECEIVING CW and SSB

Morse signals should be found easily in the amateur and other bands and VCl is simply rotated to produce a suitable audio tone. In some cases rotating VCl one side of the zero position may be found to give better reception than the other side.

To receive SSB, first tune in an amateur SSB signal, probably on 80 m , with the BFO off. Switch the BFO on and rotate VCl slowly until intelligible speech is produced. This requires quite careful adjustment. If the signal cannot be resolved, turn VCl the other side of the zero position. This alternative position will in any case be necessary on the HF bands, where the upper sideband is usually employed compared to the lower sideband transmitted on the LF bands.

If the receiver is fitted with RF and audio gain controls, the audio gain should be near maximum and the RF control advanced as necessary, for best results on SSB.

VCl need not be 10 pF but larger values give more critical adjustment while smaller values may not give enough range of adjustment. Where the receiver has a fine tuning control this can be used for tuning SSB or CW signals, but if the receiver tuning does not allow very critical adjustment, VCl can be used for this purpose, after locating the wanted signals.

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common PP7 9 volt battery, for example, costs around 33 p at the moment and many transistor radios use two of these. Their useful life in a radio is very variable but one factor, above all else, determines how economical they are likely to be in the long run: the sensible use of the volume control.

Just about all transistor radios use output stages designed to operate in what is known as "Class B" conditions, where the current consumption is very low with no signal, rising as the signal input is increased so that low volume levels mean low battery consumption and longer battery life.

At 66p for a pair of PP7s it is immediately obvious that a mains operated power supply unit is going to pay for itself very quickly indeed, after which the cost of the electricity to operate the set is negligible. Taking a month as a typical life span for the batteries the cost of this power supply unit at under £3 could be written off in about four months. For our Senior Citizens and others similarly placed this is no mean saving.

## Design

While power units for radios requiring 6 or 9 volts are common enough, units to replace $2 \times$ PP7 batteries ( 18 volts) seem hard to come by. In the author's case, an Ultra 6142 LW, MW and VHF


Fig. 1 : Circuit of the power unit together with the connections to the terminals of the retained battery tops.
portable, it seemed logical to make up a power supply unit to fit in the same space as the batteries, so what better than to use the tin cases from a pair of defunct PP7s?

In the final circuit used, Fig. 1, one tin box carries the mains transformer T1, the $12+12$ volts secondary windings going to the rectifier diodes D1 and D2, smoothing capacitors C 1 and C 2 and the zener diodes which stabilise the output voltage at $9 \cdot 1+$ $9 \cdot 1$ volts, all contained in the second box. The tops of the boxes carrying the terminals are retained and accept the original battery clips so that no alterations whatsoever need to be made to the radio set itself, a very important consideration. At any time the power unit can be slipped out of the set and normal batteries fitted back in a few seconds. In any other set a check ought to be made to with a voltmeter to ensure that the two batteries are, in fact, in series, requiring 18 volts. Otherwise, as long as the original battery polarities are adhered to, there should be universal use for this type of power unit.

## Construction

Initially, two old PP7 type batteries are dealt with as follows: Mark the tops with the + and - signs, as shown on the side of the case, against the respective terminals. Cut across the corners at the top with a pair of sidecutters and ease back the edges until the top can be lifted out complete with battery. Cut the connecting wires or thin metal strips fairly close to the terminals and throw out the battery.

A hole of about $\frac{s}{16}$ in diameter is made in corresponding positions in each case and the two cases held together with a rubber grommet, Fig. 2, noting the polarity markings on the cases. Another hole is made for the mains lead to enter, again via a grommet. The position of this hole will be dictated by the position of the batteries in the set. In the Ultra 6142 a slot was filed at the bottom of one side of the cabinet, adjacent to the battery compartment, from which the mains lead was led out.

Next, all the components, with the exception of the transformer, are soldered on to the small piece of veroboard, Fig. 3, and lead-out wires attached. Some sort of colour coding for the wires is an advantage to avoid wiring errors. The board is
fitted across the diagonal of one box and a couple of spots of adhesive will hold it in place. Be particularly careful that the polarity of the four diodes and the smoothing capacitors is carefully observed. The wires from the board are passed through the grommet with the exception of the one white and one red wire which are soldered to the + and terminals on one of the battery tops.


Fig. 2: Location of the components inside the battery cases. The cases are held together by the grommet through which the interconnecting leads pass.

View on $A-A$

The mains transformer has two mounting feet which must be bent down, Fig. 2, one being fixed to the bottom of the box with a 6BA nut and bolt and the other soldered to the box just below the top. But, before fixing the transformer finally, feed a few inches of the mains lead through the grommet and connect to the primary winding taking the earth lead to the transformer's "screen" connection and to the case. Put a few turns of narrow insulation tape on the end of the mains lead inside the box to prevent the lead being pulled out. This may not be the best arrangement but space is rather limited inside the box. The wires from the board may now be connected to the transformer secondary with a white wire and a black wire going to the terminals on the second battery top, again noting the correct polarity. The transformer may now be dropped into the case and finally fixed into position. Some insulation tape was stuck across the core of the transformer at the top to prevent any possibility of a short circuit of the terminals immediately above. Likewise some tape was put across the top edge of the board in the other box.

## Testing

Before replacing the tops in the cases it is a good idea to try out the power unit for correct operation. After checking the wiring again and the polarity of the various components connect a DC' voltmeter across the red and black terminals. Select a voltmeter range of, say, 50 volts initially. Switch on the mains, when a reading of about 18 volts should be

## * components list


obtained, with 9 volts between the white wires and either black or red.

If everything appears correct put some insulating tape over the connections to the terminals and put the tops back into the cases finally turning over the edges of the cases to hold the tops in position. If thought necessary, the unit can be checked on the radio itself before fitting the tops back, connecting the battery leads from the set on to the power unit terminals. If there is something wrong it can be attended to now instead of having to open up the cases again. As a further check, the voltage across each of the smoothing capacitors should be about 16 volts.


Fig. 3 : Layout of components on small piece of Veroboard. Protect vertical edges and top with insulating tape or similar.

## Notes

It should be remembered that the on/off switch on the radio set itself still only controls the DC output of the power unit to the set and not the mains input. Although the set consumes very little power from the mains it is still good practice to switch off the mains side when the set is not being used. The set switch can be left on permanently and operation of the set controlled by a switch at the mains outlet point.

The miniature mains transformer specified has a secondary current rating of 250 mA which is far in excess of the $20 / 30 \mathrm{~mA}$ which will be drawn by the average set. However, since it costs only a matter of a few pence more than the sub-miniature transformers rated at around $30 / 50 \mathrm{~mA}$ the additional safety factor was thought to be well worth while. The light loading of the transformer will also assist the output voltage regulation of the unit.

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| W715A | 220，F | $35 Y$ | 10p |
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THE motor car is not an ideal environment for a tape player, or indeed for any electronic apparatus. In particular the problems of power supply regulation and electrical noise are far more acute than those likely to be encountered by a domestic machine.

## ENVIRONMENT

The supply voltage, although nominally 12 V , is likely to vary considerably under the loading conditions imposed by windscreen wipers and heaters, lights, etc. As a result we must produce a unit capable of working safely up to a possible maximum of around $15 \cdot 5 \mathrm{~V}$, yet also maintaining a satisfactory performance down to 10 V . For the amplifiers this is not too difficult-achieving a constant speed for the tape transport is not so straightforward.

Because a negative earth system is more or less universal on modern cars, the unit has been designed for this. Conversion to positive earth working is very simple, however, and will be described later: no change of components is required. Operation on 6 V systems is not possible.

The construction of the tape-transport mechanism itself would of course be beyond the resources of the majority of our readers. It is therefore necessary to use a commercial mechanism. The one specified in the components list incorporates facilities for electronic speed control and also auto-stop and cassette ejection at the end of the tape. This feature is very necessary in a car where the machine must "look after itself" if the driver is fully occupied in manoeuvring his vehicle.

Interference from the car's electrical system seems to be worse with the modern alternator and solid-state regulator than it was with their predecessors. Power supply filtering and comprehensive screening are essential if the tape-head output, which is less than $500 \mu \mathrm{~V}$, is not to be completely submerged in the hash.

Acoustic noise levels in the passenger compartment vary considerably from one car to another. The amplifiers used here provide over $3 W$ rms output into $4 \Omega$ loudspeakers from a 12 V supply: this should be adequate for pretty well any car.

## TAPE AMPLIFIER

The amplifier system can be conveniently divided into three parts, a low-noise preamplifier, an equalisation section and a power amplifier. Silicon transistors are used in all but the power output stages.

A stereo cassette carries four tracks recorded on a tape only $1_{8 i n}$ wide and running at $1^{7_{8}} \mathrm{in} / \mathrm{sec}$. Hence the very low output level from the tape head. The amplifier input stage must therefore be designed for very low-noise performance. The technique adopted here uses complementary npn and pnp transistors, with the collector current of the first stage providing the base current of the second. The first transistor is thus operating under "starvation" con-ditions-a factor which greatly assists in the reduction of transistor noise.


[^2]BUYERS＇GUIDE 1974／75



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## 530010

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Heatsinks vary enormously in size

## HEATSINKS

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voltage to the specified level and
are very useful for regulating low
voltage d.c. supplies.
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MB $=$ make before break．
BM $=$ break bbefore make．
Centreof applies where a toggle
or lever switch has two outlets and
a central neutral position． simultaneously，
usually on a wafer．
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four switches each
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Transistor gain will vary from sample to sample and will also change with the supply voltage. To overcome these problems, negative feedback is used to stabilise the gain of the preamplifier.

The preamplifier has now raised the signal from the tape to a more reasonable level, but it still has a "Velocity characteristic"-that is, for every doubling of the recorded frequency the output level also doubles. This is because the tape head output level is proportional to the rate of change of magnetic flux due to the tape moving past the head. For a constant recorded amplitude, an increase in pitch of one octave (doubling of frequency) will cause the flux to change at twice the rate, and hence the output doubles also. It continues to double with each octave rise until tape head losses become significant at the higher frequencies.

At the time of recording, the higher frequencies are pre-emphasised or boosted relative to the low and middle frequencies. This means that the signal-to-noise ratio of the tape is improved, since tape noise is predominantly at high frequencies.

From the foregoing it is obvious why we need to have an equalisation amplifier. This has a characteristic which is the inverse or "dual" of the overall tape curve. The output of this section has a flat frequency response over the audio range.

At this point the signal is suitable for feeding into the power amplifier, which uses a conventional com-plementary-symmetry circuit. The output voltage can swing between the two supply rails, less the residual voltage drop across each output transistor, say about $12-2=10 \mathrm{~V}$. The rms equivalent of this peak-to-peak voltage is approximately 3.6 V which will produce about $3 \cdot 25 \mathrm{~W}$ using a $4 \Omega$ loudspeaker.


Right hand channel is identical
4M0247

- ampllfer board, plus common power supply. NOTE.-The AD162 should be Tr 9.


## components list

| Resistors AMPLIFIERS |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |
| R1 | $470 \mathrm{k} \Omega$ | R9 | $2.2 \mathrm{k} \Omega$ | R17 | 47082 |
| R2 | 100kS | R10 | $10 \mathrm{k} \Omega$ | R18 | 22082 |
| R3 | 10 kS | R11 | 478. | R19 | 1.8k』 |
| R4 | 2-2kS | R12 | 1.5k $\Omega$ | R20 | 5612 |
| R5 | $100 \Omega$ | R13 | 1 kS 2 | R21 | $2 \cdot 2 \mathrm{k} \Omega$ |
| R6 | 2.2ks | R14 | $4.7 \mathrm{k} \Omega$ | R22 | 22051 |
| R7 | $120 \mathrm{k} \Omega$ | R15 | $100 \mathrm{k} \Omega$ |  |  |
| R8 | 47k』 | R16 | 270 ks 3 |  |  | are $\frac{1}{2} W 5 \%$ carbon.

## Potentiometers

VR1 $10 \mathrm{ks} 2 \log$ (ganged with other channel)
VR2 $10 k \Omega \mathrm{lin}$.
VR3 50 ks 2 log (ganged with other channel)
VR4 50SI horizontal preset
Capacitors

| C1 | 4.74F6V Tant. | C9 | $0 \cdot 14 \mathrm{FC}$ |
| :---: | :---: | :---: | :---: |
| C2 | 100pF Cer. | C10 | $220 \mu \mathrm{~F} 16 \mathrm{~V}$ |
| C3 | $100 \mu \mathrm{~F} 16 \mathrm{~V}$ | C11 | $0 \cdot 22 \mu \mathrm{~F} 10 \mathrm{~V}$ Ta |
| C4 | $10, \mathrm{~F} 10 \mathrm{~V}$ | C12 | $0 \cdot 001 \mu \mathrm{~F}$ Cer. |
| C5 | $100 \mu \mathrm{~F}$ 6V | C13 | $220,5 \mathrm{~F} 10 \mathrm{~V}$ |
| C 6 | $0 \cdot 1 \mu \mathrm{~F}$ Poty | C14 | ${ }_{470 \mu \mathrm{~F}}^{16 \mathrm{~V}}$ |
| C7 | $0.01,4 \mathrm{FPoly}$. | C15 | $1000 \mu \mathrm{~F} 16 \mathrm{~V}$ |
| ce | $2, \mathrm{~F} 10 \mathrm{~V}$ | ${ }^{\text {C16 }}$ | 100/f 6 VV |

Tant - Tantalum bead Cer - Disc ceramic
Poly - Polyester Remainder electrolytic
Semiconductors
Tr1, Tr3, Tr5, Tr6 Tr8 AB161 matched BC10gc Ti9 AD162 pair
Tr2, Tr4, Tr7 BC212L D1, D2 OA 90
NOTE-The above components are for one channel only. All except C15 and VR2 are duplicated for the second channel

## Miscellaneous

L1 2A suppressor choke; LP1 14V lamp;
F1 1A fuse with chassis-mounting holder ftwo required?;
F2 3A tuse with in-line holder;
Cassette mechanism, Lenco FFR, Stereo with D.C. motor;

Veroboard $6.75 \times 2.5$ in, 0.1 in pitch: DIN connectors for loudspeaker outputs; 4!! loudspeakers; metal case; mounting kits for Tr8, Tr9; knobs, etc.

## MOTOR CONTROL BOARD

Resistors


Capacitors
C51, C52 22 2 F 25 V Electroly̆tic
Semiconductors
D51-D53 BA 100
Tr51, Tr54 BC109 Tr52 AD162 Tr53 AC128
Miscellaneous
Mounting kit for Tr52; peb:

The use of class B output with output transformers could, with correct design, yield 10 watts per channe! if needed. However, we have to consider the size, weight and economics of the machine, as well as the problems of obtaining specialised components. The complementary output stage prodices as much poner as is likely to be needed for practical purposes, and all components are easily obtainable.

## PREAMPLIFIER

The circuit of the complete unit is shown in Fig. 1. It will be seen that the signal from the tape head is coupled to the base of transistor TrI via capacitor Cl . The biasing of Trl base is set by R1 and R2. Resistor should be KI, a low-nuise, high-stability type, but R2, the lower leg of the bias divider is effectively by-passed by the low impertance of the head so far as audio is concerned, and is a normal carbun type.

The collector of Tr 1 connects directly to the base of the complementary pnp transistor, Tr2. The base curient of Tr 2 and the collector current of Trl are therefore the same.
We can nuw consider the IC stabilising action of the circuit. If the current in Trl increases. so does the base current of ' r 2. This change is amplified by Tr2 so that its collector curient increases. Thus, more current flows through R3, which in turn connects to R4. The voltage drop across R4 is almost entirely due to the current flow via R3, rather than current in Tr l which is operating under "starvation"" conditions. An increase in the collector current of Tr 2 therefore causes the emitter of Tr 1 to move positively towards the supply rail. This is equivalent to a negative shift of its base bias and the collector current of $\operatorname{Trl}$ is sar reduced. The change is amplified by Tr 2 and this heavy DC feedbick action stabilises the working point of the conplete preamplifier.
We do not need such licavy AC feedback-in fact appreciable AC gain is reguired. By decoupling R4 completely, a very high gain could be obtained, but it would be unpredictable and unst:ible. By introducing R5, the gain of the stage is set at about 100 by the ratio RJ:R5 and is almost independent of voltage, temperature and transistor variations. The output from the preamplifier is therefore about 50 mV . The supply to the preamp is decoupled by R 6 and $\mathrm{C3}$, and the output is coupled to the equalisation amplifier via capacitor C 4 .

## EQUALISATION

The biasing method and stabilisation technique is the same as that employed in the preamplifier. However, an extra emitter-follower output stage is added which feeds botlo the Tone and Volnme controls and the equalisation network comprising 1111, CG, R12 and C7. The basic amplifier without equalisation would provide a gain determined by the ratio R10: R11. in this case, 200.
It is essential that the feedback network, which operates into the low impedance R1l, should be fcd from a low impedance source. If this were not the case, the response correction would be hopelessly inaccurate, as the network loads the source.

It will now be seen why Tr5, the emitter follower stage, is included. It is DC coupled to Tr4 and provides a low impedance output. Basic correction for the velocity charracteristic of the tape is provided by R 12 and C6; C7 provides extra feedback to compen. sate for the tape pre emphasis.

The equalised signal, which has now been amplified to around the 250 mV level, is conveyed via C8 to R14 which is included to increase the impedance "seen" by the tone and balance networks. Resistor R14 forms the upper leg of a divider network, whose lower leg is formed by the Balance control VR2. This control operates differentially upon the two stereo channels, so that increased attenuation of one simultaneously results in an increase of output from the other. The tone control network consists of C9 and VR1. This is a simple "top cut" network which is adequate for use in the car.

Finally we come to the Volume control, VR3, which taps off the required output to drive the power amplifier.

## POWER AMPLIFIER

The power amplifier consists of four transistors, $\operatorname{Tr} 6, \operatorname{Tr} 7, \operatorname{Tr} 8$ and $\operatorname{Tr} 9$. The latter two are complementary output transistors mounted on the backplate of the machine, which serves as a heat sink.

The action of the driver stage is similar to that of the previous amplifier. Transistor $\operatorname{Tr} 6$ has its base level set by R15 and R16. In this case, the level set is approximately half-way between the 12 V rail and earth. Capacitor C 12 is included to prevent RF instability, as is R17. The collector of Tr7 feeds the base of $\operatorname{Tr} 8$ directly, and the base of $\operatorname{Tr} 9$ via D1 and D2 and VR4, before reaching the collector load resistor R22.
Potentiometer VR4 sets the forward bias applied to the output transistors. In order to compensate for changes in temperature, diodes D1 and D2 are shunted across VR4. As the output transistors are germanium types, germanium diodes are used. When
the temperature increases (a condition which would cause increased conduction in $\operatorname{Tr} 8$ and $\operatorname{Tr} 9$ ) the impedance of the diodes falls, so decreasing the forward bias and stabilising the working conditions.

The emitters of Tr8 and Tr9 are connected via R21 to the emitter of Tr6, giving overall stabilisation of the DC working point of the amplifier. The emitter of Tr6 is decoupled by C13, and R20 is included to provide AC feedback in the ratio R21: R20, so stabilising the gain at around 40 . If we consider a level of 200 mV coming in from the volume control, this means we are just inside the overload point of the amplifier. The audio signal is coupled to the speaker via C14.

The loudspeaker also completes the DC return for R22. The audio output signal is in phase with that at the collector of $\operatorname{Tr} 7$ and hence there is positive feedback. This raises the input impedance of the output stage and enables the small transistor Tr 7 to drive the output pair fully. This technique is known as "boot-strapping."

The output pair operate in class B. Forward bias is needed to prevent cross-over distortion, and VR4 is set up to provide a 10 mA quiescent current measured at the fuse-holder. The fuse is connected in series with the collector of Tr8, to protect the output stage from conditions of gross overload.
The incoming supply from the vehicle is filtered by L1 and decoupled by C15. Power to the deck motor and panel light are also fed from this part of the circuit. The on-off switch is included as part of the tape deck mechanism.

The second part of the article describes the motor control circuitry and construction of the circuit boards.


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3. Interfacechips
4. Case mouldings, with bultons.
windows and light-up display in posithon
5 Printed arcutt board
6 Keyboard panel
7 Electronic components pack (diodes. resistors, capacitors.
5. Baltery assembly and on/ofl switch

9 Solt carying wallet
10. Comprehensive instructions for use

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Fig. 1: Circuit of the photo trigger using an SN7400.

## Photo detector

The photo detector itself is a photo-conductive cell, PCC1, which forms part of a potential divider circuit with R1. When the cell is illuminated the potential at the junction of these two components rises to some positive level, the actual level depending on the degree of illumination and on the value of R1. As long as this potential exceeds +3 V , with the power supply of 4.5 V the circuit will work satisfactorily. To achieve this level it is necessary to use a reasonable level of light such as the focussed beam of a small torch. In the absence of illumination PCC1 becomes a very high resistance and the potential referred to falls towards zero.
The potential is applied to the input of a trigger circuit comprising ICI (a) and (b). Positive feedback is achieved by R2 in conjunction with D1. Even though the controlling potential may rise slowly the regenerative feedback action causes the output of gate (b) to change rapidly and the change occurs as the input voltage moves around the +2.5 V level. There is a certain amout of hysteresis built in and this is set by the value of $\mathbf{R} 2$.


Fig. 2 : Simple layout of the circuit using Veroboard.
The sense of the signal at the output of gate (b), pin 6 of the integrated circuit, is such that it rises to +5 V when the cell is illuminated and falls to zero volts when the cell is obscured. We could have left the circuit at that stage and have said that the output was at pin 6; however we can make use of the other two gates within the integrated circuit to make the device more versatile.

## Control operation

Firstly we introduce a control operation by means of gate (c). The control signal should come from a source impedance of $2 \mathrm{k} \Omega$ or less and should be a DC level of either OV or +4.5 V . A control signal of OV will hold the output of gate (c) at +4.5 V irrespective of what the photo detector might be sensing. We call the output signal at pin 11 the OUTPUT (NOT 'output') and use the final gate in the package (d) to invert this, thus, for the conditions stated, when the control signal is at OV the final output at pin 8 will be OV irrespective of the illuminating conditions. If the control signal is switched to $+4 \cdot 5 \mathrm{~V}$ the output at pin 8 will be +4.5 V when the cell is illuminated and OV when it is obscured. The OUTPUT signal at pin 11 will be the opposite of this.

## Audio square wave

If desired, the control signal could be an audio frequency square wave. When the cell is in darkness the output at pin 8 will be zero volts but when illuminated the audio frequency will appear at the output. Should the control facility not be required pin 12 can be permanently wired to the positive supply rail. An advantage of having the complementary pair of outputs is that one can select the "bias" of the system; this is particularly useful if the output signals are to drive relays which may be required to be biassed either "ON" or "OFF".

## Pw

## CONTROL PANEL

The layolt of the prototype control pancl is shown in the photograplis. Since all functions are DC controlled the layout is not critical and can be altered to suit your own requirements. Also, as mentioned earlier, any features which you do not require may be omitted.

The manual tuning drive was constructed on a framework built mainly of aluminium angle, as shown in Fig. Ba. Details of the drive-cord arrangements are given in Fig. 8b.


4
Fig. 8b: Drive cord stringing arrangements. The pointer assemoly is modfied by ttimming the ends of the cartiage to ciear the pultey mountings and also inverting the pointer on the carriage.

Fig. Ba: Construction of the protos type tuning and dial drive.

## TABLE 2 <br> Voltage analysis

Meter 20kO/Vdc-negative lead to OV rail, all readings in volts. No aerial connected.
H.T., Supply at C303 13V.

Transistors

|  | $8{ }^{*}$ | 91 | g2 | $d$ |  | e | $b$ | c |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | Tr 103 | 72 | 6.5 | 0 |
| Tr 101 | 0.1 | 0 | 4-5 | 13 | Tr 201 | 7-2 | $6 \cdot 5$ |  |
| Tr 102 | 0.4 | 0 | 1.4 | 13 | Tr 202 | $5 \cdot 8$ |  | $12 \cdot 1$ |
| * Subject to wide variations between transistors. |  |  |  |  |  |  |  |  |

Integrated circuits


## INITIAL TESTING AND SETTING UP

Before any RF adjustments are made it is wise to check the DC conditions at each stage in turn. A construction error or a faulty component is likely to produce an incorrect voltage in an associated part of the circuit. Table 2 shows the voltages to be expected at important points in the circuit when measured with a 20,000 ohms per volt meter, on the range most appropriate to the voltage to be measured.

Switch on and check the voltages appearing in the front end and oscillator stages. If they are correct connect the meter, on its $2 \cdot 5 \mathrm{~V}$ or 3 V range, to the positive end of VR104 which should be adjusted until a reading of 2.0 V is obtained with VR105 at minimum and S101 switched to Manual.

Now solder in R205 to apply power to the IF section and check the voltages against Table 2. Follow the same procedure with the demodulator and stereo decoder integrated circuits to complete the initial testing. The voltage appearing at pin 15 of IC201 indicates the strength of the signal at its input. A ' high reading here could indicate that a programme is being received or that there is some instability in the IF section. If rocking the tuning control does not reduce this voltage to the correct level, check that all the IC201 decoupling capacitors and the link joining the top and bottom earth planes are in place.

## ALIGNMENT

When all the DC tests have been completed satisfactorily you are ready to move on to the final stage of construction, aligning the receiver. Connect two lengths of screened wire to the Left and Right audio output pads ready for attachment to the output socket. Remove the temporary earth wire and mount the receiver in the die-cast box. The earth connection is now made via the mounting stud in the power supply section of the pcb.

Connect a short length of wire from the centre pin of the aerial socket to L101, as shown in Fig. 7, and
solder the audio output leads to the 5 -pin DIN socket (Fig. 9). If your audio amplifier is earthed via its mains plug, avoid hum loops by breaking the earth connection between the tuner and the amplifier (which is made by the screen of the audio connecting lead) at a convenient point.

## RF/IF ALIGNMENT

The method of alignment adopted depends on the facilities available to the constructor. Two methods are therefore proposed; the first requires the use of a VHF signal generator but the second needs only another, aligned, FM tuner.

## FIRST METHOD

Short out the oscillator coil, L106, with a crocodile clip and connect the signal generator to the 'hot' end of L104. The output level of the generator should be set to about 1 mV and the frequency set to the nominal centre frequency of the particular ceramic filter used. The filters are graded into batches of varying centre frequency, each frequency being identified by different colours. Table 3 lists the frequencies and their corresponding colours.

If a signal strength meter is not included a high impedence multimeter should be connected to pin 13 of IC201. By varying the frequency of the generator slightly about the nominal value it should be possible to detect a deflection on the signal strength meter or the multimeter. Once this has been found the core of the mixer load coil, L105, should be adjusted until maximum deflection is obtained. This circuit has a low Q so the peak is very broad.

Leaving the generator frequency unchanged remove the dustcore of L202. The tuning meter should now show only a slight deviation from the null position. Screwing in the core will make the tuning meter give a large deflection to the right, pass through the null position and deflect to the left before returning to the null.

This demonstrates the S -shaped curve of the detector, the correct position for the core being that which resulted in the null between the two large deflections. Slight variation of the generator frequency on either side of the null should now produce deflections of the tuning meter to the left and right.

To align the front end, first remove the clip from the oscillator coil and set the tuning voltage to the low end of its range. Sweep the generator frequency slowly over the range $80-100 \mathrm{MHz}$ when a deflection should be observed on the tuning meter or multimeter. Once this has been located, set the generator to 88 MHz and separate or push together the turns on the oscillator coil to produce a maximum deflection again. Then transfer the signal generator to the tuner input and maximise the deflection by adjusting L101, 102, 104. As the signal strength reading increases, the output of the signal generator should be backed off to avoid overloading or oscillator pulling.


Fig. 9: Audlo output connectlons to match DIN Standard ampliffer input socket.


Next change the tuning voltage to maximum, increase the generator frequency to 105 MHz and restore its output to 1 mV . Vary the generator frequency about 105 MHz until a signal strength meter deflec. tion is obtained and bring this to a peak at this frequency by adjustment of VR101-103. The alignment at the bottom end of the scale does not have to be altered as the two adjustments do not interact when done in the manner described.

## SECOND METHOD

This method may be used by those who do not have access to an RF signal generator. A second FM tuner, which must have an IF of $10 \cdot 7 \mathrm{MHz}$ and a tuning meter, is used both as a signal generator and as a monitor to check the frequency of the local oscillator of the tuner which is being aligned. Connect a loop of wire to the aerial input of the second tuner and place it in the proximity of the oscillator of the first. Set VR105 to its low-voltage end and adjust L106 until the local oscillator appears as a carrier at $98 \cdot 7 \mathrm{MHz}$ on the scale of the second tuner.

Now reverse the situation with the wire loop feeding the first tuner and the second tuner set to 88 MHz . Adjust the tuning control of the first tuner until the tuning meter (or a multimeter connected as in the previous section) gives a deflection, indicating that the local oscillator of the second tuner is being received. L105 is now adjusted to maximise the response and L202 is adjusted as described in the previous section.

It now remains to align the RF circuits. Disconnect the wire loop and connect a good FM aerial. The sensitivity of the tuner is such that some stations will be received even if the RF stages are not correctly aligned. Set VRI01-103 to maximum voltage and tune in a signal near the bottom of the band (the local Radio 2 transmitter will usually be the most suitable). Now adjust L101, 102, 104 to produce maximum response on the signal strength meter.

Adjust the presets VR101-103 with a signal towards the top of the band, a local radio station for example.

## DECODER ADJUSTMENTS

The alignment of the stereo decoder is very simple and requires no special equipment. With the receiver tuned to a stereo transmission the core of L 203 is screwed in until the stereo indicator illuminates. The lamp will now remain illuminated over a range of several turns of the core and the correct setting is at the middle of this range.

The precision of this setting may be increased by use of the BBC test tone transmissions on Radio 3 each evening after the end of normal broadcasting. These transmissions include a tone in one channel only. With the tuner connected to an amplifier and speakers, the speaker of the channel with the tone should be disconnected and the setting of $£ 203$ varied to give minimum signal in the other channel.

## USING THE TUNER

We would like to conclude this series of articles with a description of the tuner in use so that constructors can check the operation of their receivers and get the best use out of them.

The operation of the tuning meter is straightforward. The centrezero meter should give a slight deflection to the left (low frequency) with no signal present. As the receiver is tuned through a transmission from the low frequency side the meter will deflect strongly to the left, pass through zero and then deflect to the right. The correct tuning point is at the central zero. For maximum accuracy, tuning should be carried out with the AFC off.

If the centre-zero tuning meter is omitted from the tuner the signal strength meter may be used as a tuning indicator by simply tuning for the maximum deflection. This method is, however, not as accurate. Table 4 shows the voltage at pin 13 of


## Number 49

THE TBA 790 is an audio power amplifier integrated circuit available in various forms which have absolute maximum voltage ratings of 12 , 15 and 18 V and respectively providing maximum output powers of $1 \cdot 2,2 \cdot 2$ and $3 \cdot 45 \mathrm{~W}$ into an 8 ohm loudspeaker.

## The TBA 790KSD

In this article we will discuss the TBA 790 KSD device which has an $18 \mathrm{~V}, 3 \cdot 45 \mathrm{~W}$ rating, having the type of encapsulation shown in Fig. 1. The bracket is permanently attached to the back of the device, acting as a small heat sink. The bracket contains two holes, tapped 6BA, by which it can be fastened to a larger additional heat sink. For most applications at normal room temperatures the additional heat sink is not required. However, the constructor will often find it convenient to bolt the device to a shect of metal and this will help to cool it.


Fig. 1. The integral bracket of the IC provides the normal heat sink for the TBA 790 series.

The pins of this IC are in the quad-in-line configuration, the connections being shown in Fig. 2. Constructors are advised to solder directly to these pins, partly because sockets for quad-in-line devices are not easily obtainable and partly because the use of a socket renders spurious feedback more likely.

## Circuit

A simple circuit for the use of the TBA 790 is shown in Fig. 3. The input impedance of the device itself is very high, typically $50 \mathrm{M} \Omega$, and the circuit input impedance is therefore normally determined by R1. The high input impedance enables the circuit to be used with ceramic record player cartridges.

As the value of $R 2$ is reduced, the amount of negative feedback decreases and the gain rises, being equal to $8000 / \mathrm{R} 2$. Thus if R2 is 100 ohms, the voltage gain is 80 or 38 dB . R2 should not be less than about 39 ohms where the voltage gain is 200


Fig. 2 : Pin connections for the TBA 790. The heat sink is omitted for clarily.
or 46 dB , since instability is likely at very high gain. The value of R2 should not, generally, be greater than about 200 ohms.

## Frequency compensation

The components $C 2$ and $C 3$ provide frequency compensation. Ideally their values should be chosen according to the graph of Fig. 4, although these values are by no means critical. One should therefore estimate the gain required and then ascertain the value of R2 in Fig. 3. The value of C3 can then be read from the left hand side of Fig. 4 and the value of C 2 from the right hand side of Fig. 4.


Fig. 3: Bas ic circuil of the TBA 790 as an audio a mplifier.




Fig. 4: above, graph for selecting values of C2 and C3 in Fig. 3. Fig. 5 : centre, outout power related to supply vollage. Fig. 6: right, distortion level at various outpul levels.


## Power supply

The maximum output power which call be obtained from the TBA 790 KSD at various supply voltages is shown in Fig. 5 where an 8 ohm loudspeaker is employed. In general it is wise to regard the maximum power supply voltage as about 16 V to allow a small margin of safety.

It can be seen that an output of just under 2 W can be obtained when the device is used in a 12 V car radio, although more than 2 W should be obtainable when the battery is being charged.

The quiescent curtent is only about 10 mA at 15 V or 7 ma at 10 V , but it will rise to around 1 to 3 A when $3 W$ is being delivered to an 8 ohm speaker. The efficiency (output power/input power) is typically 65 per cent at the $2 \cdot 7 \mathrm{~W}$ level.

The circuit shown has a frequency response which is 3 dB down at about 70 Hz and at about 12 kHz . The use of a capacitor of larger value for $C 5$ of Fig. 3 will extend the bass response, whilst the high frequency response can be altered by changing the: value of C 2 or C 3 .
-The components R3 and C4 of Fig. 3 componsate for the speaker inductance.

The total harmonic distortion is plotted as a percentage against the output power in Fig. 6 for a 15 V supply and an 8 ohm speaker. It can be seen that the total harmonic distortion is fairly constant
 about $2 \cdot 6 \mathrm{~W}$. It then rises rapidly with the ouset of clipping to about 10 per cent at $3 \cdot 4 \mathrm{~W}$.

## Typical use

The writer has used the $T B A \quad 790 S K 1)$ as the output stage of a very simple radio receiver employing the well known Ferranti 'ZN414. The circuit is shown in Fig. 7. The voltage gain of the audio amplifier has been set at about 80 which has been found to provide good volume. The two diodes D1 and D2 are forward-biased silicon diodes which stabilise the ZN414 supply voltage. If these diodes are replaced by a resistor, the receiver will not function satisfactorily over a range of supply voltages. The gain of the ZN414 circuit can be adjusted by altering $R 1$, reducing it in value or removing it altogether if the ZN414 stage oscillates.

The diode D3 in the supply lead is included to prevent the destruction of the TBA 790 if the power supply is accidentally connected with the wrong polarity. It may be omitted if desired.

The coil L.l consisted of about 80 turns of 28 SWG enamelled copper wire close wound on a 4 in . long ferrite rod. A long-wave coil of around 220 turns of much finer wire could be placed at the other end of the rod and switched into circuit to replace Ll if long wave reception is required.


# LERRNING BY PRAGTICAL PROJEET STEPS 

## PART 13-PHASE SHIFT CIRCUITS

THERE is more to a top cut filter than an attenuation factor, as described last month. Apart from the potential divider effect of the resistor and total circuit impedance on the input voltage, the circuit introduces what is called Phase delay. This means that when a sine wave signal is applied to the input we will see an attenuated sinewave at the output but the peaks and troughs of the wave will not occur at the same instances of time. To confuse the issue, the time discrepancy between input and output depends on the frequency of the signal we apply. This is not an easy feature to demonstrate without an oscilloscope but we hope the following experiment, coupled with a bit of thought, might clarify the situation a little.


Fig. 90: Experiment to show phase shift in a top cut filter.
In Fig. 90 we shall simulate an AC input signal by moving the wiper of VR1. Because we are limited to slow movements (low frequencies) we shall have to use a suitable high value capacitor for Cl so that useful signals can be measured on the meter M1. This meter must be sensitive, 20,000 ohms per volt, and switched to a low DC voltage range, about 2 or 3 volts. The voltage at " $A$ " will be set by the potentiometer and can be anything in the range of 0 to +9 V . We can, with a bit of manual dexterity, make this voltage follow a near sinusoidal pattern; to do this, start with the wiper at minimum voltage and rotate it, slowly at first, reaching a maximum speed of rotation at the half way point, then start to slow down gently until you reach the top end of its track. You should aim to slow down progressively, so that you don't suddenly stop when you reach the top. Having reached the top, peak positive voltage, immediately start turning the knob the other way, slowly at first, speeding up to the halfway point and
then slowing down as you reach the bottom end, again without an abrupt stop. This needs a bit of practice but it is not as difficult as it might at first appear. If you manage to do this satisfactorily the voltage at the wiper should approximate to a sine wave and if repeated over and over again should produce a waveform something like that shown in Fig. 91.


Fig. 91 : (a) /dea/ sine wave oscillating about zero volis. (b) Approximate waveform from fig. 90, oscillating between zero and +9 V .

The thing to do now is to monitor the voltage at point " $B$ " on the circuit as you go through the "sine wave" cycle. Initially make the cycle stretch over about two seconds and watch the meter closely. During the slow portion of the rising waveform the meter will read virtually nothing but as you speed up at the halfway point the meter voltage will rise. As you pass the halfway point and slow up towards maximum you should see that the meter voltage


Fig. 92 : Progressive construction of waveform obtained in Fig. 91 (b).
starts to fall back to zero and reaches zero just as you reach maximum voltage. The voltage you see on the meter should be proportional to the rate at which the input signal was changing. If you had an oscilloscope the output voltage would trace out the line shown in the progressives of Fig. 92.

When you turn the potentiometer in the opposite direction, describing the negative half of the input sine wave, the meter will try and read backwards so reverse its leads and you will find that a similar effect is produced in a negative direction. If you repeat this cycle many times you can imagine that the voltage at point $B$ has the same sinusoidal shape as that at $\mathbf{A}$ but it is reduced in amplitude (attenuation by top cut filter action) and it reaches a positive peak as the input voltage is going through the centre part, the fast moving part, of its positive going swing. The voltage at $B$ is zero when $A$ is peak positive, maximum negative when $A$ is moving in a negative direction and zero again when $A$ is at its peak negative, zero volts, level. The final trace in Fig. 92 clearly shows that the voltages at $B$ are out of step with those at A by a quarter of a wavelength.

Because a complete wavelength of a sinewave is a cyclic event we sometimes say it corresponds to a $360^{\circ}$ cycle hence we can say a quarter of a wavelength is $90^{\circ}$. Using this nomenclature we can say there is a $90^{\circ}$ phase shift between the input and output signals for this circuit, at the low frequencies we are considering.

If you had a signal generator instead of a potentiometer as an input signal and a double-beam oscilloscope monitoring the voltages at A and B you would see this more clearly. You would also see that if the frequency of the input signal were increased the amplitude of the output would increase but the phase shift would also start to reduce. As the input signal frequency becomes very high the phase difference approaches zero and the output becomes an almost exact replica of the input, both in phase and amplitude.


Fig. 93 : Curves showing 90 phase shift of LF signal through to cut filter.

We can thus say for a top cut filter:-

1. At very low frequencies we get $90^{\circ}$ phase shift and heavy attenuation, Fig. 93.
2. At very high frequencies we get no phase shift and little attenuation.
3. At intermediate frequencies we get a graded scale of phase shift (between $0^{\circ}$ and $90^{\circ}$ ) and graded attenuation, depending on the frequency we choose, and, of course, on the values of the components in the filter.

This phase shift effect can be put to good service in certain types of oscillators. To obtain oscillation all we need is an amplifier with frequency selective positive feedback. This means that we have to take the output of the amplifier and at a certain frequency feed it back to the input with a phase relationship that enhances the output.

We have seen several examples of the opposite effect in amplifier stages, previously described in this series. Negative feedback was achieved by feeding the signal from the collector of a transistor back to its base. A single transistor stage, in grounded emitter configuration, has $180^{\circ}$ phase shift between its input and output, when the input moves positive the output moves negative and vice versa. To get positive feedback we must arrange to feed back a signal that is in phase (i.e. having zero or $360^{\circ}$ or any multiple of $360^{\circ}$ phase shift).

One simple way of doing this is to use two transistor stages, one cascaded into the next. The output of the second stage will be $360^{\circ}$ out of phase with the input to the first and this is equivalent to there being no overall phase shift. If we feed the output signal back to the input the circuit will oscillate at a frequency set by any frequency dependent components, capacitors or inductors, that form part of the loop, from input to output and back to the input again. If there are no such frequency sensitive devices and the amplifier is DC coupled then the oscillator becomes locked in one or two possible states (it tries to oscillate at zero frequency!!). This circuit is, in effect a bistable which has been described in a previous part.


This block diagram shows concept o an oscillator, producing zero phase shift, gain and frequency selective feedback.

For regenerative feedback to occur, a pre-requisite for oscillation, it is necessary for the gain of the amplifier to equal or exceed any signal losses in the feedback path. Positive feedback alone is not sufficient. We can turn the two transistor stage into a free running oscillator as shown in Fig. 94. The capacitors determine the frequency and, if looked at from a different view point, this circuit is very similar to a free running (astable) multivibrator. Changing the value of the capacitor in the feedback loop changes the frequency of oscillation; you can try this and, with the values given, the frequencies should be in the mid-audio range. Layout shown in Fig. 95.

If we accept that we can get $90^{\circ}$ phase shift from a simple RC filter it might seem that two such filters cascaded into one another Fig. 96(a) would give us $180^{\circ}$ phase shift. This would be true of signals of zero frequency but, apart from zero frequency being a rather impracticable concept when dealing with oscillators, the attenuation would be infinite and no measurable signal would be seen at the output. If, however, we extend the logic a little and consider three such filters connected together (Fig. 96(b)) there will be a specific frequency that undergoes $60^{\circ}$


Fig. 94: Two stage amplifier converted to an oscillator, frequency being delermined mainly by C2 ant C3


Fig. 95: Layout for Fig. 94. Try values of 1000pF to 0.47uF for C2 and C3 in any combination.


Fig. 96: (a) Two stages cascaded as shown will give theoretical $180^{\prime}$ phase shift at zero frequency. (b) With three stages each stage will give $60^{\circ}$ shlft at a certain frequency giving $180^{\circ}$ shift overall.
phase shift through each of the three stages. Three lots of $60^{\circ}$ shift give $180^{\circ}$ shift overall but this time we are no longer dealing with zero frequency; it will be a finite frequency and although there will be considerable attenuation it will cortainly not be infinite and we can guarantee at least some measurable signal at the output for this particular frequenc..

It can be shown that if each of the resistors in the three stage filter have values $R$ (in ohms) and the capacitors are of equal value $C$ (in farads) the frequency that is subjected to $180^{\circ}$ phase shift is given by:-

$$
\mathrm{F}=\frac{1}{2.7 C R \mathrm{~V}^{\prime} 6}
$$

Because of the inter-relationships of impedance, reactance and frequency the attenuation for this circuit at this particular frequency is always a factor of 29.

We can now conceive using this network to replace the sccond transistor in our experimental circuit, to give $180^{\circ}$ phase shift instead of the second transistor and simultancously determine the frequency at which this phase shift occurs. By using this network in the feedbach path of a single transistor stage we should be able to get regenerative feedback at a predetermined frequency provided that the voltage gain of


the single transistor stage exceeds 29 . Ideally the gain of the amplifier should be greater than, but as near to 29 as possible, otherwise clipping will occur and providing the gain is just right the oscillator will produce a very pure sinusoidal output waveform. VR1 introduces a controllable amount of negative feedback and thus sets the gain of the amplifier, Fig. 97. Start with this set to maximum resistance and no oscillations will be heard in the loudspeaker; as it is reduced in value a pure note will be heard and reducing its value to zero will provide zero negative feedback, maximum gain, and some distortion might be heard in the loudspeaker as clipping starts to occur. The latter effect will depend on the transistor latent gain. Layout is given in Fig. 98.

This is a very useful and simply made oscillator for audio and sub-audio frequencies and is sometimes used for generating low frequency vibrato signals in electronic organs as it has a comparatively pure signal content. The only problems are that the gain of the amplifier needs setting carefully for optimum performance and that it is rather difficult to change its frequency of operation with a variable control. Small changes in frequency can be provided by varying the value of one or two of the resistors in the feedback loop by small amounts. The best way of setting the frequency to a predetermined value is
to leave the resistors fixed and substitute different sets of capacitors in the feedback circuit.

Phase shift has many other useful applications in electronics and it can be obtained in other ways. Under some circumstances it can be detrimental and is sometimes encountered unexpectedly in audio amplifiers giving rise to undesirable.spurious oscillations.

## Next month: Some more applications of positive feedback.

## P.W. SANDOW N-continued from page 735

IC201 measured for various signal strengths for a typical tuner. This information may be used to calibrate the signal strength meter if required, although quite wide variations can be expected between tuners.
With the muting or squelch switched off there is considerable inter-station noise and the usual distorted output as the signal enters the edge of the tuner passband. With the squelch in operation the background should be silent until a noise-free signal is received. It should normally be left on unless a weak signal is being received.

TABLE 3
Filter centre frequencies

| Colour <br> code | Centre <br> frequancy <br> $(\mathrm{MHz})$ |
| :---: | :---: |
| Orange | 10.625 |
| Yellow | 10.665 |
| Green | 10.700 |
| Blue | 10.735 |
| Violet | 10.775 |

TABLE 4
Signal strength meter indication

| Voltage at <br> Pin 13, | Approx. <br> IC201 |
| :---: | :---: |
| (v) | at al lerial <br> socket |
| $0 \cdot 15-0 \cdot 3$ | 0 |
| 0.4 | $1 \mu \mathrm{~V}$ |
| 1.3 | $10 \mu \mathrm{~V}$ |
| $2 \cdot 0$ | $100 \mu \mathrm{~V}$ |
| 3.0 | 1 mV |
| $4 \cdot 6$ | 10 mV |

The stereo defeat facility automatically inhibits the decoder when the signal falls below the level required for noise-free stereo. Alternatively the tuner can be held in the mono or the stereo mode independent of the signal level by moving the mode switch R203 to the appropriate position.

# PRODUCTION LINES colin riches 

## EKCO ZU540

Sound Project ZU540 from Ekco is a tuner-amplifier/turniable/Dolby cassette tape recorder unit.
The Dolby noise reduction system operates on both record and playback. The v.h.f. varicap tuner employs 4 push-button pre-selectors plus free tuning and a built-in stereo decoder with beacon indicator.
The transcription-type 2-speed record player uses a Phllips GP400 magneto-dynamic cartridge with a 15 micron diamond stylus.
There is a facility for using chrome dioxide tapes on the recorder and there is an automatic level control with a manual override.
An electronic tape.end auto stop allows for automatic 'pop-up' disengagement of the cassette keys.
Output power is quoted as 20 W per channei into $4 \Omega$.
1 have tried out this unit and found it to give exceltent quality reproduction through the DX181 speakers which come with the system.

I cannot give full details of the impressive speclfication in the limited space I have here but please write to Pye Limited, P.O. Box 49, Cambridge if you would like further details.

## BANISH THE IRON!

Banish the soldering iron-that's what Radio and TV Components have done with their latest car radio kit.

All the electrical connections are made through colour-coded press-on tags and R and TV Ltd. claim that a complete novice can build it in under two hours.

The "Tourist TT" has five pushbuttons which can be tuned to any pre-selected station. Four operate on m.w. and one on l.w.

This new radio kit developed from the firm's very successful and efficient "Tourist" radio, utilises an i.c. and a p.c. board allied to tested sub-assemblies, Constructing the kit is simply a matter of fixing the
various component assemblies to the chassis using the screws pro. vided.

The kit features permeability tuning and long-wave coils to ensure good sensitivity and selectivity on both bands. The r.f. sensitivity at 1 MHz is said to be better than $15 \mu \vee$ and power output into a $3 \Omega$ speaker is claimed to be better than 4 W .

Both the tuner and the i.f. module are pre-aligned and the kit is suitable for 12 V positive or negative operation.

The kit comes complete with stepby+step assembly instructions and instructions for installing the radio into the car ltself.

This excellent kit is available by past or direct from Radio and TV Components Ltd., 21 High Street, Acton, London, W.3. The price is $£ 7$ plus VAT. Postage and packing cost 55p.

Extras available are a speaker with baffle and fitting strips, at £1 65 (post and packing 23p) and a retractable, matched locking aerial for §1•37 (20p postage and packing).

We are publishing a Special Product Report on the "Tourist TT" car radio on page 704 of this issue of Practical Wireless.


## COMDEL SPEECH PROCESSOR

The Comdel CSP 11 is a communication aid designed for any system using a microphone for voice transmission. Its prime feature is the achievement of peak limiting without distortion whlch is the very undesirable by-product of conventional speech clippers. Therefore the average or 'talk power' gairr obtained is more effective.

Features of the CSP 11 are: instantaneous limiting action; no appreciable distortion; talk power gain greater than 10 dB ; optimum frequency response for voice; installs in microphone lead; all silicon solid-state circuitry. The unit cosis £55 (including VAT and postage and is available from interface international, 29 Market Street, Crewkerne, Somerset.



IN the medium power range there is now a wide variety of i.c. audio amplifiers available, with power outputs ranging from 1 to 6 watts r.m.s. As with the majority of semiconductor devices, the prices of these have dropped in recent years and most now represent very good value for money.

This article describes an amplifier based on such an i.c., the Motorola MFC9020, which gives a maximum output power of 2 W r.m.s. into a $15 \Omega$ load. A peak power of about 4 W is available. In the configuration used here the device has a typical distortion level of approximately $0.5 \%$ at full output at 1 kHz , with an input sensitivity of 250 mV r.m.s.

The prototype was made for use as a tape recorder monitor amplifier, but as the input impedance is high it is also suitable for use in simple record playing equipment in conjunction with a crystal or ceramic cartridge. With the addition of a suitable preamplifier it would of course be suitable for many other applications.

The unit has built-in volume and simple tone controls. A circuit of a simple mains power unit for the amplifier is provided.

A diagram of the internal circuit of the MFC9020 is shown in Fig. 1. Basically this is divided into two sections. The first four transistors form a differential amplifier while the other five form a fairly conventional complementary class $B$ output stage.

Operation of the differential amplifier is quite simple. For high gain and input impedance this uses two darlington pairs. The first is used in the emitter follower mode, and the output of this stage is developed across the emitter resistor. The second darlington pair operates as a grounded base amplifier to the signals appearing across the emitter resistor. No voltage amplification is provided by the emitter follower stage which provides the circuit with a high input impedance and has a low enough output impedance to drive the grounded base stage. The grounded base stage does provide a degree of voltage amplification.

Neither an emitter follower, nor a grounded base stage provides any phase change to the signal, and so the input to pin 7 is in phase with the output at pin 5. There is a second input to the circuit at pin 8. For an input at pin 8 the second darlington pair will operate as a common emitter amplifier, with the amplified and inverted output appearing at pin 5. Thus pin 7 is a non-inverting input and pin 8 is an inverting input.

## OUTPUT STAGE

This is quite conventional, the only unusual feature being that two transistors are used in the upper section, and three in the lower, rather than the more usual two in each section. The two silicon diodes connected across the two inputs to the two sections of the output stage operate as low voltage zeners, and provide a suitable bias for the output transistors to reduce cross-over distortion to an unnoticeable level. The diodes also provide temperature stabilisation of the output stage.

Under normal operating conditions the output stage is biased to give about half the supply potential at the output (pin 3). The two upper transistors operate as another darlington pair in the emitter follower mode, providing current amplification to positive-going half cycles. The lower three transistors consist of another darlington pair, this time in the common emitter configuration, driven by a pnp common emitter amplifier. There is $100 \%$ negative feedback between pin 3 and the emitter of


- Fig. 1 : Internal clrcult of the MFC9020.

the first of these three transistors, and this forms what is termed a compound amplifier. Like an emitter follower, a compound amplifier provides no voltage gain, but has a high current gain. It also has the input and output signals in phase. These three transistors amplify negative-going half cycles. Due to the high current amplification of the output stage, the output at pin 3 is at a very low impedance. and can directly drive the loudspeaker via a d.c. blocking capacitor.


## AMPLIFIER CIRCUIT

A circuit diagram of a practical amplifier using the MFC9020 is shown in Fig. 2. The input is taken via R1 to the volume control, VR1. C2 couples the signal from here to the non-inverting input of the i.c. This input is biased via R4 from a potential divider across the supply, R2-R3. C1 and C3 are decoupling capacitors.
The inverting input is biased from the output of the i.c. by the potential divider, R5-R8. This introduces negative feedback and helps to give a stable biasing arrangement, though it seriously reduces the sensitivity of the circuit. C5 and R6 are therefore used to decouple some of the a.c. feedback and so provide increased sensitivity.

A simple treble boost and cut tone control is provided in the feedback network. This consists of VR2, C7, C8, R9, and R10. With the slider of VR2 towards the right, R10 and C8 are in effect shunting R8. The impedance of R10-C8 is frequency dependent, and reduces as frequency increases. The negative feedback in the circuit will therefore increase with frequency, causing the response of the amplifier to drop at high frequencies. With VR2 in this position the circuit is given top cut.

With the slider of VR2 at the other end of the track, C8 and R10 are in effect cut out of circuit due to the high value of VR2. However, R9 and C7 are now shunted across R6 and C5. Again, the impedance of these will be frequency dependent, but as they are connected across the other section of the potential
divider, the feedback will be increased as frequency increases. This gives treble boost. R9 and R10 are required to limit the effect of VR2 to a certain extent, in the interest of good stability.

Capacitors C4 and C9 are required for good stability. C6 couples the output to the loudspeaker. R7, which is the load resistor for the differential amplifier, is connected to the positive supply via the L.S. so as to give bootstrapping to the circuit.

The input impedance of the amplifier varies with the setting of VR1, but is about $2 \cdot 1 \mathrm{M} \Omega$ at minimum sensitivity, reducing to about $700 \mathrm{k} \Omega$ at maximum sensitivity.

## components list




## CONSTRUCTION

A printed circuit board measuring $31_{4} \times 3$ in. is used and this carries all the components except the loudspeaker. Fig. 3 shows the pattern of the copper side of the p.c.b., and also the drilling points. Fig. 4 shows the component layout on the board.

The integrated circuit requires two ${ }^{1}$ in. long slots in the p.c.b. into which its heat tabs fit. These are cut using a coping saw or a fret saw. Although potentiometers with pins which fit into p.c.b. mounting holes are manufactured, these would not seem to be widely available to the amateur, and this p.c.b. has therefore been designed to accept ordinary potentiometers with tag connections. The tags are taken under the edge of the p.c.b.. and soldered to the copper backing.

## POWER SUPPLY

The amplifier requires a supply of approximately $20-22 \mathrm{~V}$. As the i.c. has a maximum supply voltage rating of 24 wolts, it would be difficult to find a suit. able unregulated power supply circuit considering that the amplifier has a class B output stage. This is because the supply should not rise to more than 24 V under quiescent conditions: with a current con-


Fig. 3: above, shows the PCB layou? actual shee. Note that this is turned through $90^{\circ}$ compared with Fle. 4.

Fig. 4: left, shows the layoul of componenis on the PCB. The tags of VRt and VRI dre soldered to the underside of the board.

Fig. 5: below, is a checuit of a sujtable stablifsed mains power supply unit for the amplifier.

sumption of perhaps only 10 mA , and yet maintain about 21 volts under full load conditions with the current consumption peaking as high as 500 mA .

It is more practical to use a simple stabilised circuit as shown in Fig. 5. This is a fairly standard configuration, using a zener diode stabilisation circuit feeding an emitter follower. This uses few components, and can easily be constructed on a small tagstrip or connector block. The MJÉ340 can be mounted on a strip of aluminium which will act as a heat sink and can be bent to form a suitable mounting bracket for the component.


## Biory of the 伃. 6.

WHILE reading through one of my favourite vintage radio reference buoks, the BBC Year Book of 1930, I noticed a page devoted to telling listeners about power supplies for their receivers. It centainly was intended as a serious article then but these days one cannot help but smile when one reads about a BBC warning on making a direct connection between a receiver and the mains supply. So, below are a few pointers which listeners should have taken note of in the days 10 years or so before World War II.
"No receiver can give really good quality reproduction if the power supply to it is inadequate. Since broadcast receivers first came into use by the general public there has been a tendency to gradually increase the power supply to the last stage of amplification. Electric light supply mains provide a constant and convenient source of power for wireless re-
ceivers, but in no circumstances should the mains be connected direct to the receiver without the use of an intermediary mainsunit.

A year ago, the BBC drafted a parmphlet which describes the many ways in which electric light supplies can be utilised for wireless receivers. The publication of this pamphlet has been delayed owing to the fact that a number of bodies, such as the Institution of Electrical Engineers, the British Engineering Standards Association and the Radio Manufacturers' Association, are all interested in its contents and the BBC naturally is anxious to conform with their views and wishes. It will however be published as soon as possible.

The BBC wishes to take this opportunity to warn listeners most seriously against the direct connection of their receivers to supply mains, and also strongly recommends that no listener who is unaquainted with handling power and electric light circuits
should attempt the home construction of a mains-unit. It is a far more difficult matter to build a safe and satisfactory mains-unit than it is to build a valve receiver. Owing to the danger to life if a number of improperly designed and constructed mainsunits come into use by the listening public, the Institution of Electrical Engineers, in collaboration with the other bodies concerned, has drawn up a set of regulations which governs the use of electric power supplies to wireless receivers. One set of regulations, by the I.E.E. has already been published but new and more detailed regulations are now under consideration. These new regulations, if agreed, will be written in formal technical language and it is thought that many listeners will not be able to follow them conveniently. It is therefore probable that in its mains-unit pamphlet, the BBC will print an explanation Written in more simple terms.

In conclusion, listeners are reminded that they are likely to have some difficulty in the future with electricity supply contractors, fire insurance authorities and other similar bodies, if they are using a mains-driven receiver which does not conform with the agreed regulations."

I suppose it is a matter of familiarity breeding contempt since electronic enthusiasts have been successfully assembling mains operated equipment and power supply units for a very long time now without any serious losses among their numbers from electric shock!

These interesting photngraphs
show some "mint" items of
 vintage radio equipment kindly provided by Mr. Ken H. Rann of Lancing, Sussex.
It's rather unusual to locate brand new components but new items in their original boxes are interesting items indeed!




## by Eric Dowdeswell G4AR

THis month I am glad to be able to give a plug for the West of Scotland Amateur Radio Society. Publicity and QSL Manager Graham Bleakley reports a thriving membership of 80 and space for many more and promises a warm welcome for SWL's, young or old. In the past the club has concentrated more on the interests of the licenced amateur so it is very good to hear that the SWL is actually being welcomed! It is an unfortunate fact that many clubs catering for the licenced chap tend to spurn the SWL who goes along once, gets the cold shoulder and then decides to drop the idea of pursuing the hobby. The fact that the SWL of today is the licenced amateur of tomorrow seems to escape notice. The SWL is also only too pleased to be a general dogsbody arotend the club, taking on tasks that no-one else wants to do, especially on Field Day events. SWL's in the Glasgow area are invited along to 81 Virginia Street, Glasgow every Friday evening at 8 pm to sample the Morse classes, junk sales, films, library and lectures etc. More details from Secretary K. Drinkwater at that address.

Steve Blake (Aylesbury) joined the flock with a report of 40 m doings including a nice collection of ZL's on SSB. Hope Steve will favour me with some details of his gear in bis next log. Michael Crimes (Exeter) has forsaken VHF now that he can really hear the DX on his shiny new Yaesu FR50B coupled to 132 ft of wire via an ATU. Like several other reporters he is a little disgusted with the antics of the Italian boys especially when a rare call pops up.
Michael Green A8088 (Northwich, Cheshire) refutes any suggestion that the 4 m band only comes alive in contests and submits a long list of G's heard in one evening on his home made converter plus CR100 and 4 -element beam at only 12 ft . Regular John Porter (Baslow, Derbys) is glad to have left the classroom for an OND course at Chesterfield Tech. His Trio 9R59DS was not allowed to get cold, evidenced by the list of DX from 15 to 160 m . Andrew Darragh (Wetherby, Yorks) sends his first $\log$ and promises more. Last reported in 1968 it seems, getting married in the interim, now 'back on the rails' and I should jolly well think so! A Geloso converter puts signals into an AR88 from a 12AVQ trapped vertical and nine radials per band!!! He must be located in the centre of the racecourse up there!

Alan Rae (Glasgow) found a few nice calls on 20 m thoughtfully omitting the lists of W's that are not of much interest to anyone. Tim Charles (Colchester) in again with six pages of notes and calls gives the impression that he never goes to sleep! His long wires suffered in the gales but one would never think so! Interesting catch was F9LC on 7 MHz with two watts of SSB and over S 9 at that. I'm a bit put out to hear Alan had to look up ST2 in the prefix list since yours truly was ST2AR for 15 years! Incidentally, I've just had the very great pleasure of meeting ST2AS in London. I'm glad to say that I started him off as a SWL some years ago when he was a medical student and now he is Dr. Ibrahim, opthalmic surgeon and the only active ST2 for some years past.
Bernard Hughes (Worcester) also stuck at 20 m SSB which seems a pity with a lovely FR500SDX! The other bands are quite lively too, OM! Bernard keeps a record of the number of countries heard on each band and wonders if anyone is interested in seeing a totals table in this column from time to time? Paul Barker (Sunderland) is another of the sleepless brigade! Three pages of rare ones from 15 to 80 m including several on SSTV but nothing exceptional this month, he says!
Max France (Warrington, Lancs) now has an RAl but still prefers his old R107 for sorting out the DX on 80 m . Back to school means less burning of the midnight oil however, so it looks as if 20 m will be favourite for some time now, with a picture rail aerial. Ought to be good for SSTV!

## Log extracts

Max France:-80m PQONS PZOCJ VSGDO ZL2CB 5ZALW $6 \mathrm{Y} 5 B \mathrm{M} 20 \mathrm{~m}$ VP8NS XV5AB XWagV.

Paul Barker:-15m CX2AAO (1700) 20m JW5DQ KH6IAG KL7MF KX6LP VS6FB ZD3U ZKiDJ 4W1GM 20 m SSTV CTITX 16RME KILEM LU4CN.

Bernard Hughes:- 20 m HK0BKX KM6DZ TR8VE YK1KAS 4WIGM.

Tim Charles:-80m ZL3NC ZJ4AU 40 m CE5BMN YazKl ZLIAUL ZLZALR ZL3PW 20m HK4SAJ HKOBKX JY5UMC KC6BL TG5YD XZ1AB $\mathbf{z m}$ DCZGEC DCAJHA.
Alan Rae:-20m CR3AX HK3CKW K3CI/OE K7RSC.
John Porter:-15m EABJP PY8RW 20m CT3AT EA9FB FY7AU KV4AD TG9VN TR8SS ZB2CH 8R1CB TI2AJF.

Steve Blake: -40 m EA9AI HCOHM KZ5PW M1C SVIDO TU2DO VK7GK XE3U ZL3AR ZL4GN ZL4KS 8PGAG.

Michael Crimes:-20m CR4BS DUlXK ET3USE HZ1AB ST2AY VP1MT VP2DH 4WIGM.

Andrew Duragh:-15m CX2XC VQ9MC VU2DK ZP5NT 7P8AQ 20m AC3PT CR3ON DUU2EF FC2CD HR2JAG JY9GR KC4AAC KG4AM ST2AY TA2QR VK9XX VP8HA VS5MC ZD7SD 8R1CB.

CW stations in bold, remainder SSB. Please note that logs should be in alphabetical order for every band.


## MEDIUM WAVE BROADCASTS

by Charles Molloy

ROY PATRICK reports again from Derby. With his Trio 9R59DS communications receiver he has logged Dakar, Senegal on 764 kHz ; Amman, Jordan on 800 kHz ; Rio de Janerio, Brasil on 980 kHz ; Cluj, Romania on 1151 kHz ; Tripoli, Libya on 1250 kHz ; Conakry, Republic of Guinea on 1403 kHz . Roy sends a mobile report of reception in North Wales. The receiver is a National RF 1400 portable connected to a car aerial and his daytime reception includes BBC Radio Merseyside on 1484 kHz ; BBC Radio Cumberside 1457 kHz ; Piccadilly Radio in Manchester on 1151 kHz ; Manx Radio, Isle of Man on 1295 kHz (good signal) and 1594 kHz (weak). After dark Tunis was heard on 962 kHz and the Voice of Tangiers at 2000 hrs in Arabic on 1232 kHz .
M. J. Clarke (Warley) is a self confessed local radio enthusiast. Using a Philips RL210 portable receiver he has pulled-in BBC Local Radio outlets at Blackburn on 845 kHz ; Stoke on 1052 kHz ; Derby on 1115 kHz and Birmingham on 1475 kHz together with IBA Capital Radio on 557 kHz and Birmingham on 1151 kHz .

Timothy James (Southampton) has been tuning around the medium waves with his Fidelity RAD16. He reports hearing Capital Radio (London) on 557 kHz ; Radio Solent on 998 kHz ; Radio Medway on 1034 kHz ; Radio Sweden on 1178 kHz and Radio

Brighton on 1484 kHz .
Peter Kirkbride (Kenilworth, Warwickshire) still enjoys "scanning the medium waves" with his 20 year old Bush valve receiver. He mentions reception of AFN Frankfurt on 872 kHz and Munich on 1106 kHz ; Radio Sweden on 1178 kHz ; Radio Tirana, Albania on 1394 kHz . Peter asks if it is possible to pick up North America using this receiver. Provided that a good outdoor aerial is used it should be possible to hear a few of the stronger trans-atlantic signals when conditions are good for reception of this area. Try after 2330hrs GMT for CJON St John's, Newfoundland on 930 kHz ; CBA in Moncton, New Brunswick on 1070 kHz and WNEW in New York City on 1130 kHz .

Mike Larvin (Redcar, Cleveland) has a Pye 1403D and an ITT Weekend Automatic Radio. Both are portable receivers and although neither has a socket for an external aerial for the medium waveband and external aerial 25 m long and 20ft high is pressed into use by means of the following ingenious device. "I use a 6 inch ferrite slab wound with 75 turns of 20-30 SWG wire one end of which is connected to a good earth and the other to the aerial". The slab is brought near the receiver until peak signals occur, coupling being by induction between the slab and the receiver's internal aerial. Mike's log includes WKBW Buffalo NY on 1520 kHz at 0230hrs GMT; BBC Relay Stations in Cyprus on 638 kMz and 1322 kHz ; AFN stations in Germany on 872 kHz (Frankfurt), 935 kHz (Berlin), 1106 kHz (Munich), 1142 kHz Stuttgart); Budapest, Hungary on 1340 kHz at 2245 hrs ; Norte, Portugal on 755 kHz and 1061 kHz . A total of 23 BBC local outlets were heard as well as London Broadcasting on 719 pHz and Metropolitan Radio (Newcastle) on 1151 kHz with Radio Clyde and Piccadilly Radio in the background.

Clive Barwood (Grimsby) is another local radio enthusiast. He uses an Ekco Mariner 6 valve domestic receiver connected to an outdoor aerial 75 ft long and 25 ft high. He reports hearing Capital Radio 557 kHz ; IBA Birmingham 1151 kHz ; Metro Radio also on 1151 kHz ; Manx Radio 1294 kHz and BBC Radios at Stoke 1502 kHz ; Cleveland 1546 kHz and Leicester 1594 kHz .

## SHORT WAVE BROADCASTS

 by Derek Be/lHELLO there! my name is Derek Bell and our editor has invited me to take over Malcolm Connah's Short Wave News column for a spell. May I say that I hope all readers will give me the same help and friendship that they gave Malcolm. All columnists must rely on the help of their readers, especially in this sort of column, since it could be said that the readers write the column with their contributions. I hope also that in your letters you will pop in a line or two telling me what you would like to see included in this feature.
Having said all that I will declare the meeting open with the first log. This is from another first timer, namely David Lovatt of Cheadle, Staffs, and he reports the following:-
5980 SBC in English at 2130
5990 Prague in English at 2131
6010 Budapest at 2136
6800 Pekin S/on at 2030
7200 Deutsche Welle at 2031
15350 Peace and Progress at 0920

This is a shortened version of a superb log from our thirteen year old correspondent who is equipped with an Ultra domestic valved receiver and a 60 ft aerial suspended 20 feet above terra firma.

Christopher Hall of Birmingham has the other sort of aerial, a $4-\mathrm{ft}$ telescopic one, bolted to his Bush VTR178 Multiband. Using this line-up he reports an impressive list of catches the cream of which is as follows:-
6185 R. Norway in English at 1200
9770 R. Australia at 1600
11955 B.B.C. Malaysia relay in English at 1500
I was interested in your comments at the end of your letter Christopher. As far as DX clubs go one must rely on the adverts they place in various magazines so "yer pays yer money and takes yer choice" in other words! Your request for the latest information on equipment for the BC stations however brings forth the information that Uganda is pressing ahead with a new SW transmitter setup that will bring the voice of Uganda blaring out loud and clear. Recently a member of Radio Nederlands staff went on record as saying that they are to increase the
power of their transmitters, another victim I fear of the "power game".

From the biggest to the smallest now, Paul Heath says his equipment "is somewhat joked about". This Heath kit (sorry about that!) is a home-built HAC one valver plugged in to various "out board motors" namely an ATU and feeding out through a transistor amplifier. Well Paul, let them laugh!, you pulled in a fine list, as is shown below:-
9005 Voice of Iran at 2020
9625 R. Jerusalem at 2000 (This is R. Israel, Paul)
9655 R. Damascus at 0830
9670 A.W.R. Portugal at 0945
You remark Paul, that you have received QSLs from only a couple of stations but that "there are more to come". Well OM, this is purely a matter of being patient. Radio Tirana, for instance, has been known to take 125 days to deliver, while Polish Radio Warsaw has taken only seventeen. Your logging of Damascus on 9655 was fortunate since Damascus is a notorious "wanderer" having been heard as far off frequency as 9630 .

My final letter for this month is written by Robert Hill who hails from Hough, near Crewe, and he reports that he heard:-
9005 R. Tehran in English at 2015
9480 R. Tirana in English at 1830
9550 R. Finland in English at 1605.
11775 R. Bucharest in English at 1300
Having Crewe as a QTH seems to me to pose some unusual problems, I imagine it is possible that with all the QRM around from electric railways DXing is rather difficult. I would be interested to find out if I am right.

Well folks, that winds up my first venture into the pages of Practical Wireless. I hope that having read it you will feel that you want to write in with your logs (see address box) so I look forward to hearing from you, best 73 s to you and yours.

## BROADCAST BANDS

Short Wave and VHF/FM reports by the 15th of the month to Derek Bell c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.
Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.

## AMATEUR BANDS

Logs covering any amateur band/s in band/ alphabetical order by the middle of the month to Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey, KT21 2TW.

A reprint of the P.W. Tele-Tennis series is being prepared and will be available shortly. Further details in the January 1975 issue of Practical Wireless.


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\hline 50 & 15 & 1＊T & 11.05 & & 0.47 \\
\hline 40 & 20 & 234 & 118 & & 1.00 \\
\hline 50 & 30 & 224 & 15.36 & & 110 \\
\hline \multicolumn{6}{|l|}{30 Volts} \\
\hline \multicolumn{6}{|l|}{} \\
\hline Asugi & & Ret． & Frice & & Post \\
\hline Oid & & 112 & 1.78 & & 0.24 \\
\hline 1 & & 7 & Es 1 & & \(0 \cdot 98\) \\
\hline 4 & & ， & －\({ }^{\text {ct }}\) & & \(0 \cdot 88\) \\
\hline 2 & & 20 & 410 & & \(0 \cdot 42\) \\
\hline 4 & & 1 & 4．68 & & 0.62 \\
\hline \(s\) & & 81 & －10 & & 052 \\
\hline \({ }^{4}\) & & 117 & \(0 \cdot 60\) & & 0.812 \\
\hline 1 & & Hi & 6.80 & & 0 Of \\
\hline 10 & & 88 & B．\({ }^{7}\) & & 0 O\％ \\
\hline
\end{tabular}
\begin{tabular}{|c|c|c|c|}
\hline \multicolumn{4}{|l|}{50 Yolts} \\
\hline \multicolumn{4}{|l|}{Prim， \(100-\mathrm{LeDF}\) ， 600．18，85，34，40，60\％．} \\
\hline Ampa & \begin{tabular}{l}
Hei． \\
Mo．
\end{tabular} & Prle＊ & Propt \\
\hline 00 & 102 & 838 & 0.50 \\
\hline 1 & 103 & \％ 09 & 0.35 \\
\hline 1 & 104 & 4－57 & 0.42 \\
\hline 1 & 101 & 120 & 08.2 \\
\hline 4 & 108 & 689 & 0.82 \\
\hline 1 & 107 & 11－17 & 0.85 \\
\hline 8 & 118 & 14－10 & 0.97 \\
\hline 10 & 118 & 14－47 & 097 \\
\hline
\end{tabular}

60 Vofts
Prim．290－240才，
Gec． \(84.30,40,45,107\)
\begin{tabular}{|c|c|c|c|}
\hline Ampe & \begin{tabular}{l}
Hef． \\
No．
\end{tabular} & Frice & Pont \\
\hline 0.0 & 124 & 808 & \(0 \cdot 3 \mathrm{l}\) \\
\hline 1 & 128 & E＇8E & 038 \\
\hline 1 & 137 & 481 & 041 \\
\hline 1 & 128 & E＇84 & \(0 \cdot 6\) \\
\hline d & 122 & 794 & 0 ¢ \({ }^{\text {\％}}\) \\
\hline 5 & \({ }^{6}\) & \(4 \cdot 18\) & O57 \\
\hline 1 & 120 & 16．15 & － 82 \\
\hline \({ }^{6}\) & 121 & 18．39 & 100 \\
\hline 10 & 122 & 12．25 & 100 \\
\hline 12 & 189 & 18.90 & 1.10 \\
\hline
\end{tabular}
mintature and equipment


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 ateel cased moite conted tu sougb regin with power lead， tomend 13 s Vole american tgpo nocket up to BOOVA， abore 500 VA cable ritry．
\begin{tabular}{|c|c|c|c|c|c|}
\hline VA & Ref． & Frire Cingers & Price Plukt & lrice Open & Yort \\
\hline Wiatt． & Na． & 2 & 9 \＆ 3 ph， & ＊ & － \\
\hline \multicolumn{6}{|l|}{Tapped a 115.220 .240 Voltos} \\
\hline 20 & 115 & 2－80 & 0.15 & 135 & 030 \\
\hline \multicolumn{6}{|l|}{Tapput at I16． 200.2800 .240 Vollo} \\
\hline 100 & 4 & （5－8） & 0.18 & t－98 & 0 39 \\
\hline 200 & 5＇5 & 6.40 & 0 If & \(4 \cdot 50\) & 0.40 \\
\hline 3011 & H\％ & 727 & 0.15 & 8．28 & 002 \\
\hline B0l & 87 & 989 & 0.15 & \(5 \cdot 8\) & 0．67 \\
\hline 750 & 68 & 12．509 & 075 & 8.78 & 0－82 \\
\hline 1000 & 64 & 13.70 & 075 & 18.40 & 0－82 \\
\hline 35 Ch & 93 & 2088 & 0－75 & 18.58 & \(1 \cdot 50\) \\
\hline 2000 & 85 & 30.10 & 1.44 & 92.05 &  \\
\hline 3000 & 73 & 43－58 & 1.10 & 8200 & 1.90 \\
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olaln \\
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