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| WW | 1 | 0.22-3.9 | 9 | 9 | 5 |
| WW | 3 | 1-10K | 7 | 7 | 6 |
| WW | 7 | 1-10K | 9 | 9 | t |

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& \text { pole. } 4 \text { way- } 3 \text { pole, } 4 \text { way- } 2 \text { pole } \\
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| Parameter | Conditions | Pertormance |
| :---: | :---: | :---: |
| HaRMONIC DISTORTION | Po : 3 Watts $1=1 \mathrm{KHz}$ | 0.25\% |
| LOAD impfidance: | -- | $8-16 \Omega$ |
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| hensitivity fur Ratelo ofl | $\mathrm{v}_{\mathrm{s}}=25 \mathrm{~V}, \mathrm{Rl}-8 \Omega \mathrm{i}=1 \mathrm{KHz}$ | 75 nV V. R348 |
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The ahove table relater to the AL.10. AL20 and AL.30
modules. The following table outlines the differences

| Parameter | ALIO | AL20 | AL30 |
| :---: | :---: | :---: | :---: |
| Maxilumin Auplly Voltape | -5 | 30 | 31 |
|  | $\begin{aligned} & \text { 3 watt. } \\ & \text { H. } \$ 1 \times \text { Min. } \end{aligned}$ | $\begin{aligned} & 5 \text { watt } \\ & \text { RS\& } \mathrm{M} \ldots \text {. } \end{aligned}$ | $\begin{aligned} & \text { 10 watt, } \\ & \text { R MA. } 1 \mathrm{lin} \text {. } \end{aligned}$ |

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SPECIFICATION
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Radio, Tulter Radio, Tumer
Magnetic $P$. Magnetic $P$ P. $\quad 35 \mathrm{mV}$ into $50 \mathrm{~K} \Omega$ 1.5 tul unt $50 \mathrm{~K} \Omega$ All input voltages are for all nutput of $250 \mathrm{nd} \mathrm{V}^{\text {. Tape and P. U. }}$ $\begin{array}{ll}\text { ass Contral } & \pm 156 \mathrm{~B} \text { at } 20 \mathrm{~Hz} \\ \text { reble Control } & \pm 104 \mathrm{~B} \text { at } 20 \mathrm{KHz}\end{array}$ T'reble Control Fitters: Rumble (1ligh Pasc) Hignal/Xome Rati liput or
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Unchallenged for two tears, the HY5. our unique multifunctlon preamplifier/tone hybrld, has been brought into line with the advancements In our power hybrids. Like the HY50, the new HY5 has no external components a has been redesigned to run off a split powerline with improvements In signal/noise, overload, capability sa reduced distortlon. The output has bean increased to match the power module (Oob), a film circultry while the device still retains ali the functlons of the earller device. When combined with the soutput facilities expected to be found on Hi-FI amplifiers.
The ampilier with two HY5's two HY50's sharlng a common power supply (PSU50) are linked by a balance control to form a complete stereo system.
INPUTS SPEC.
Magnetic Pick-up $3 m$ V (within 1db RIAA curve)
Magnetic Pick-up
Ceramic Pick-up up to 3 mV
Microphone 10 mV
Tuner 250 mV
Auxillary $3-100 \mathrm{mV}$
Input impedance $47 \mathrm{k} \Omega 1 \mathrm{kHz}$
OUTPUTS
Tape 100 mV .
Main output, Odb (0.775volts)
ACTIVE TONE CONTROLS
Treble $\pm 12 \mathrm{db}$ at 10 kHz
Base $\pm 12 \mathrm{db}$ at 100 Hz 2
OUTPUT NOISE LEVEL (below 10 mV magnetic input) 68db
DISTORTION 0.05\% at 1 kHz
SUPPLY VOLTAGE $\pm 16-25$ volts
SUPPLY CURRENT 15 mA
Price EA 85 mono, $89 \cdot 70$ stereo

## POWER SUPPLY PSU50

The new PSU50 has a low profile look being only $2 t$ inches high and can be used for either mono or stereo systems.
SPEC.
OUTPUT VOLTAGE $\pm 25$ volts
INPUT VOLTAGE $210-240$ volts
SIZE L. $70, \mathrm{D} .90, \mathrm{H} .60 \mathrm{~mm}$
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2 Stage Triode Pentode valve. 3 watte 8 ohm output. Volume on/ofirad tone controls AC mains. Complete and tosted.
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 Bate Benonance 5 to 18,0



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## ELAC 8in. or $10 \times 6$ in.

 HI-FI SPEAKER
Dual cone plasticised roll aurround. Large ceramio magnet. 50-18,000 cpl. Bans resonance 8 sin .10 watts onm tmpedance.

TEAK YENEER HI-FI SPEAKER CABINETS Fluted Wood Fronts MoDEL "A". $20 \times 18 \times 9$ oin.
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IOEI2 WW KIT: 10 of each EI2 value, 22 ohms-IM, total of 570 (CARBON FILM 5\%) 63.65 ner 10 EI 2 IW KIT: 10 of each EI2 value, 22 ohms-IM, a total of 570 (CARBON FILM 5\% $5 \%$, $63 \cdot 65$ ne
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MULLARD POLYESTER CAPACITORS C296 SERIES
$\begin{array}{lll}400 \mathrm{~V}=0.001 \mu \mathrm{~F}, 0.0015 \mu \mathrm{~F}, 0.0022 \mu \mathrm{~F}, 0.0033 \mu \mathrm{~F}, 0.0047 \mu \mathrm{~F}, 2 \frac{1}{2} \mathrm{p} .0 .006 \mathrm{O}_{\mu} \mathrm{F}, \mathrm{C} \cdot 01 \mu \mathrm{~F} \\ 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F} & 0.033 \mu \mathrm{~F}\end{array}$
 $160 \mathrm{~V}=0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F} \quad 0.022 \mu \mathrm{~F}, 14 \mathrm{p}$.
 MINIATURE CERAMIC PLATE CAPACITORS
$50 \mathrm{~V}:(\mathrm{pF}) 22,27,33,39,47,56,68,82,100,120,150,180,220,270,330,390,470$
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$2 \frac{1}{\mathrm{p}}$. each. $0 \cdot 1.30 \mathrm{~V}, 4 \frac{1}{3} \mathrm{p}$. POLYSTYRENE CAPACITORS I60V $5 \%$
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MINIATURE $0 \cdot 25 \mathrm{~W}$ Vertical or horizontal 6p each IK, $2 K 2$, $4 K 7$, IOK, etc. UPLOTMA
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| Miniature Mullard Electrolytics |  |  |  | VEROBOARD 0-110.15 |  |
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| $10 \mu \mathrm{~F}$ | $63 \mathrm{~V} 6 \frac{1}{p}$ | $68{ }_{4} \mathrm{~F}$ |  | $2 \frac{1}{2} \times 5^{\prime \prime}$ | 28p 28p |
| 1. $5 \mu \mathrm{~F}$ | $63 \mathrm{~V} 6{ }^{\text {P }}$ | $68 \mu \mathrm{~F}$ | 63V12p | 21 $\times 3{ }^{\frac{1}{2}}$ | 26p 19p |
| $2 \cdot 2 \mu \mathrm{~F}$ | 63 V 6 ${ }^{\frac{1}{2} \text { P }}$ | $100 / 4 \mathrm{~F}$ | $10 \vee 61 p$ | $3 \pm$ $37 \times 3$ $\times 1$ | 32p 33p |
| $3 \cdot 3 \mu \mathrm{~F}$ | $63 \mathrm{~V} 6 \frac{1}{3}$ | $100 \mu \mathrm{~F}$ | 25V61p | $3 \frac{1}{2}$ | 28p 28p |
| $4.0 \mu \mathrm{~F}$ | 40 V 6 ${ }^{\text {¢ }}$ | $100 \mu \mathrm{~F}$ | $63 \vee 14 p$ | 2\% ${ }^{\frac{1}{2}} \times{ }^{\frac{1}{2}} \times 5^{\prime \prime}$ (Plain) | 7p 7p |
| $4.7 \mu \mathrm{~F}$ | $63 V 6 \frac{1}{2}$ p | $150 \mu \mathrm{~F}$ | 16V6 6 p | $2{ }^{\frac{1}{2} \times 3{ }^{\prime \prime}} \times$ (Plain) | ) $\begin{array}{r}\text { - } 14 p \\ \hline 12 p\end{array}$ |
| $6.8 \mu \mathrm{~F}$ $8.0 \mu \mathrm{~F}$ | $\begin{array}{ll}63 \mathrm{~V} & 6 \frac{1}{2} \mathrm{p} \\ 40 \mathrm{~V} & 6 \frac{1}{3} \mathrm{p}\end{array}$ | $150 \mu \mathrm{~F}$ $220 \mu \mathrm{~F}$ | 63 V 15 p | ${ }^{2} \times \times 3{ }^{\prime \prime}{ }^{\prime \prime}$ (Plain) | ) $\begin{array}{r}-12 p \\ -12 p\end{array}$ |
| $10 \mu \mathrm{~F}$ | 16 V 63p | 220 2 kF | $6.4 V 619$ 10 V ¢ | Insertion tool | 59p $59 p$ |
| $10 \mu \mathrm{~F}$ | $25 V 6 \frac{1}{3} \mathrm{p}$ | $220 \mu \mathrm{~F}$ | 16 V 8p | Track Cutter Pins, Pkt 25 | 44p 44p |
| $10 \mu \mathrm{~F}$ | $63 \mathrm{~V} 6 \frac{1}{2} \mathrm{P}$ | $220 \mu \mathrm{~F}$ | 63V21p | Pins, Pkt 25 | 10p 10p |
| $15 \mu \mathrm{~F}$ 15 | $16 \mathrm{~V} 6 \frac{1}{2} \mathrm{P}$ | $330 \mu \mathrm{~F}$ | 16V 12p |  |  |
|  | 63 V 61 | $330 \mu \mathrm{~F}$ | $63 \vee 25 p$ | TRANSIST | ORS |
| $16 \mu \mathrm{~F}$ | $40 \mathrm{~V} 6 \frac{1}{2} \mathrm{P}$ | 470 hF | $6.4 \vee 9 p$ | AC 127 16\% | BC212L 12p |
| $22 \mu \mathrm{~F}$ | 25V 6ip | $470 \mu \mathrm{~F}$ | $40 \vee 20 p$ | AC128 22p | BC213L 12p |
| $22 \mu \mathrm{~F}$ | $63 \mathrm{~V} 6 \frac{1}{p}$ | 680 HF | 16V15p | BC107 11P B | BC214L 17p |
| 324 F | $10 \mathrm{~V} 6 \frac{1}{3} \mathrm{P}$ | 6800 FF | 40V 25p | BC108 12p | OC44 18p |
| $33 \ldots \mathrm{~F}$ | 16 V 6 ${ }^{\frac{1}{p}}$ | $1000 \mathrm{\mu F}$ | $16 \vee 20 p$ | BC109 13p | OC71 13p |
| 33 HF | $40 \mathrm{~V} 6 \frac{1}{1} \mathrm{p}$ | $1000 \mu \mathrm{~F}$ | 25V25p | BC148 12p | OC81 16p |
| 32 uF | $63 \mathrm{~V} 6 \frac{1}{2} \mathrm{P}$ | $1500{ }^{\prime \prime} \mathrm{F}$ | $6.415 p$ | BC149 12p | OC170 23p |
| 47 If | 10V 61p | $1500 \mu \mathrm{~F}$ | 16V 25p | BC182L 12p | T1543 33p |
| $47_{\mu \prime \prime}$ | $25 \mathrm{~V} 6 \frac{1}{2} \mathrm{p}$ | $2200 \mu \mathrm{~F}$ | $10 \vee 25 p$ | BC183L 12p 2 | 2N2926 11p |
| 7 F | 63 V 8 p | $3300 \mu \mathrm{~F}$ | $6.426 p$ | BCI84L 13p 2 | 2N3702 11p |

POTENTIOMETERS
Carbon Track $5 \mathrm{~K} \Omega$ to $2 \mathrm{M} \Omega$, log or lin. Single, $16 \frac{1}{2}$ p Dual Gang 46p. Log Single with switch 26p
Stider Pots. 10K, $100 \mathrm{~K}, 500 \mathrm{~K}, 30 \mathrm{~mm}, 34 \mathrm{p} .45 \mathrm{~mm}, 47 \mathrm{p} .60 \mathrm{~mm}, 55 \mathrm{p}$. Stider Pors. 10K, $100 \mathrm{~K}, 500 \mathrm{~K}, 30 \mathrm{~mm}, 34 \mathrm{p} .45 \mathrm{~mm}, 47 \mathrm{p} .60 \mathrm{~mm}, 55 \mathrm{p}$.

| DIODES | PLUGS | ELECTROLYTIC CAPACITORS. Tubular \& Large Cans |
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| IN4001 $6 \frac{1}{2}$ P | DIN 2 Pin 12p | ) $1 / 25,2 / 25,4 / 25,4.7 / 10,5 / 25,8 / 25,10 / 10,10 / 50,16 / 25$, |




 IN4006 14p
IN Phono 4
IN

IN \begin{tabular}{ll|l}
IN914 \& $7_{p}$ \& SOCKETS <br>
IN916 \& 7p \&

 

\hline IN916 \& 7pp $_{p}$ \& DIN 2 Pin 10p <br>
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 $2500 / 50,62$ p. $3000 / 50,80$ p. $5000 / 25,66$ p. $5000 / 50,1 / \cdot 10$. HI-VOLT: $4 / 450,14 \mathrm{p} .8 / 350,19 \mathrm{p} .8 / 450,20 \mathrm{p} .16 / 350,22 \mathrm{p}$. $16 / 450,23$ p. 32/350, 33p. 50/250, 20p. 100/500, 88p.





 ZN414 \& 1.32 I Panel Neon, 240 V Red. Amber

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All individually boxed and guaranteed．Full trade discounts to bona fide companies．Price and availability lists on

| application． |  |  |  | $\begin{aligned} & \text { PC88 } \\ & \text { PC88 } \end{aligned}$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| DM70 | 0.63 | EF80 | 0.46 | PC97 |  |
| DY81 | 0.86 | EF83 | 1.08 | PC900 |  |
| DY60／7 | 0.42 | EF5B | 0.48 | PCC84 |  |
| DY802 | 0.46 | EF86 | 0.90 | PCC88 |  |
| EABC80 | 1.00 | EF89 | 0.81 | PCC89 |  |
| EB91 | 0.88 | EF91 | 180 | PCCl89 |  |
| EBC81 | 0.76 | EF02 | 140 | PCF80 |  |
| FBF80 | 0.60 | EFPD | 1.85 | PCF82 |  |
| EBF83 | 0.69 | EFi8s | 0.60 | PCF86 |  |
| EBF89 | 0.68 | EF184 | 0.60 | PCF200 |  |
| EC88 | 0.75 | EH90 | 0.50 | PCF201 |  |
| EC88 | 0.77 | ELS4 | 005 | PCF801 |  |
| ECC81 | 0.45 | ELS6 | 1.05 | PCF802 |  |
| ECCA2 | 0.48 | EL81 | 0.90 | PCF808 |  |
| ECC83 | 045 | EL84 | 0.47 | PCH200 | 0 |
| ECC8 | 055 | ELA8 | 0.85 | PCL82 |  |
| ECCS | 0.59 | EL86 | 0.05 | PCL83 | 0 |
| ECO88 | 0.76 | EL95 | 0.70 | PCL8 |  |
| ECC189 | 0.71 | EL01 | 1.81 | PCL85 |  |
| ECF80 | 0.56 | ELL80 | 1.80 | TCL8 |  |
| ECF82 | 0.78 | EM84 | 1.18 | PCLb0S／8 |  |
| ECF88 | 0.71 | E 487 | 118 |  |  |
| ECH81 | 1.00 | EYOI | 0.88 | PD500 |  |
| ECH83 | 100 | EY88／87 | 0.42 | PFLiz00 |  |
| ECE84 | 0.78 | EY88 | 0.64 | PL36 | 0 |
| ECL80 | 0.88 | E280 | 0.61 | PL81 |  |
| ECL82 | 0.01 | EZ81 | 0.40 | PL81A | 0 |
| ECL83 | 0.68 | GY501 | 0.80 | PL82 | 0 |
| ECL80 | 0.88 | G234 | 0.78 | PL83 | 0 |

NEW VALVES
Individually boxed and guaranteed but of Euro－ pean or other origin at greatly reduced prices． Quotations for any valve not listed．Send SAE for lists．

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AZ1 | 080 | EF＇80 | 0.25 | Plen | 0.60 | UF41 | 0.75 | 6X4 | 0.40 |
| A 231 | 0.55 | EFPb | 0.85 | PC8B | 0.80 | LP89 | 0.40 | 6 E 50 | 0.45 |
| CHL3I | 120 | EF80 | 080 | PC97 | 0.50 | UL41 | 0.85 | 6x6gT | 0.45 |
| CL33 | 1.80 | EFP9 | 0.28 | PC900 | 0.18 | ULS4 | 0.48 | 7B6 | 0.75 |
| CY31 | 0.50 | EF91 | 037 | 1＇ty | 010 | UY41 | 0.48 | 7B7 | 0.70 |
| 1）AF91 | 0.80 | EFY2 | 050 | PC＇88 | 056 | UY85 | 040 | 7 CL | 130 |
| DAFg8 | 0.80 | EF90 | 040 | PC＇89 | 080 | VR100－30 | 0.40 | 7C6 | 0.76 |
| DCezo | 185 | EF98 | 0.75 | PCClsy | 0.80 | VR150－30 | 0.40 | 7H7 | 0.70 |
| DFga | 0.80 | EF゚183 | 080 | PCF＇80 | 040 | OA2 | 0.40 | 7R7 | 0.75 |
| DF＇96 | 0.80 | EF184 | 0.95 | FCFP2 | 0.88 | OB2 | 0.40 | 787 | 2.25 |
| DK91 | 0.46 | EL32 | 0.60 | PCF＇s | 060 | 1R5 | 0.45 | 7 Y 4 | 0.75 |
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| DK96 | 0.60 | EL34 | 080 | PCF802 | 0.80 | 1 T 4 | 0.80 | 12AT7 | 0.40 |
| DL92 | 0.40 | K L3 6 | 050 | PC＋800 | 0.90 | 384 | 0.40 | 12AU6 | 0.45 |
| DL94 | 0.48 | EL37 | 2.50 | PCF800 | 075 | 3 V 4 | 0.70 | 12AU7 | 0.88 |
| DL96 | 0.55 | EL41 | 0.90 | PCFMos | 0.80 | 5 HsOE | 0.80 | 12AX7 | 0.88 |
| DY86／7 | 0.36 | EL42 | 0.90 | PCL． 82 | 085 | 5U4G | 0.40 | 12BA6 | 0.45 |
| DY802 | 0.87 | ELC4 | 0.28 | PCL83 | 0.66 | 0140 | 0.60 | 128E6 | 0.50 |
| EABC80 | 0.88 | FL95 | 0.40 | PCL84 | 0.48 | BY307 | 0.48 | 30 Cl | 0.40 |
| EAF42 | 0.75 | ELLH0 | 1.25 | PCL85 | 080 | 8240 | 0.45 | $30 \mathrm{Cl}{ }^{6}$ | 1.06 |
| En91 | 0.28 | EM80 | 0.45 | 1＇CLBE | 0.45 | 6）30L4 | 0.90 | 30 Cl 7 | 1.10 |
| EBC33 | 1.00 | EM81 | 0.60 | 1＇CL805／85 |  | BAK\％ | 0.40 | 30 Cl 18 | 0.90 |
| EBC41 | 0.75 | EM84 | 0.35 |  | 0.80 | 6．4315 | 1.00 | 30F6 | 1.10 |
| EBC81 | 0.88 | EMes | 1.00 | PD500 | 180 | 6AQS | 0.45 | 30FL1 | 0.80 |
| EHF80 | 0.40 | EYE1 | 0.40 | PEN45 | 0.75 | 8AB7G | 0.86 | 30FL2 | 0.75 |
| EBF83 | 0.40 | EY86 | 0.40 | PL36 | 0.88 | 6AT6 | 0.45 | 30FL14 | 0.90 |
| EBFP日 | 0.82 | EZ40 | 0.78 | PL81 | 0.60 | 6AUE | 0.80 | 30L15 | 1.05 |
| EBL31 | 1.60 | EZ4］ | 0.75 | PL82 | 0.58 | 6 BAO | 0.88 | 30L17 | 0.85 |
| ECCA1 | 0.40 | EZ80 | 0.88 | PL83 | 0.45 | 6BE6 | 0.85 | 30 P 4 MP | 1.80 |
| ECC82 | 0.88 | EZ81 | 0.29 | PL84 | 0.40 | 6BE6 | 0.75 | 30 P 4 MR | 1.80 |
| ECC83 | 0.88 | GY801 | 0.80 | PL500 | 0.80 | 6BJ6 | 0.58 | 30 P 12 | 1.05 |
| ECC84 | 0.80 | GZ30 | 0.45 | PL504 | 0.80 | 6BL7A | 0.55 | 30 Pl 19 | 1.00 |
| ECC8 | 0.40 | GZ32 | 0.80 | PL508 | 0.00 | 6BR7 | 1.00 | 30PL1 | 0.05 |
| HCC88 | 0.40 | GZ34 | 085 | Pla09 | 1.65 | $6 \mathrm{6B87}$ | 1.85 | 30 PL 13 | 1.20 |
| ECH35 | 1．25 | G2， 7 | 125 | PL802 | 0.05 | 6BW6 | 0.00 | 30 PL 14 | $1 \cdot \mathrm{R} 5$ |
| ECH42 | 1.00 | HN309 | 1.50 | PX 4 | 3－50 | ${ }^{613} \mathrm{~W} 7$ | 0.00 | 35 W 4 | 0.50 |
| ECH81 | 0.30 | KT61 | 175 | P $\times 25$ | 8.50 | $6 \mathrm{C4}$ | 0.36 | 35 W 4 | 0.50 |
| ECH83 | 0.45 | KT66 | 2．80 | PY33 | $0 \cdot 68$ | 6 CD 6 F | 180 | 35Z4GT | 0.70 |
| ECL80 | 0.85 | KT81 |  | PY81 | 0.50 | 6 CH | 1.40 | 50CD60 | 1.80 |
| ECL82 | 0.85 |  | 130 | PY82 | 0.85 | 6CW 4 | 1.00 | 807 | 0.80 |
| ECL 83 | 0.70 | KT81 | 1.76 | PY83 | 0.88 | ${ }_{6}^{6 F 23}$ | 1.05 | 813 ITT |  |
| ECL86 | 040 | К T88 | 2.80 | PY88 | 0.40 | $6 \mathrm{~F}^{25}$ | 1.00 | 813 ITT |  |
| FCLL800 | 3.20 | KTW6L | 1.00 | PY500 | 1.05 | 6 F 28 | 0.70 | 813 U日SE |  |
| EF37A | 1.20 | MU14 | 1.00 | PY81＇800 | 0.50 | 6J5M | 0.85 |  | 25.75 |
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|  |  |  |  |  |  |  |
| 79 | 1.0 | 24 | $7.0 \times 6.7 \times$ | -12-15-20-24-3 | 2.11 |  |
|  | 2.0 | 34 | $8.9 \times 7.7 \times 7.7$ |  | 3.18 | 6 |
| 20 | $3 \cdot 0$ | 8 | $9.9 \times 8.3 \times 8.6$ |  |  |  |
| $\begin{aligned} & 21 \\ & 51 \end{aligned}$ | 4.0 5.0 | $\begin{array}{llll}6 & 4 & \\ 6 & 12\end{array}$ | $9.9 \times 9.6 \times 8.5$ | .. .. | 87 | 52 |
| f |  |  |  |  |  |  |
| 88 | 8.0 | 120 | $12.1 \times 11.8 \times$ |  | 0 | 67 |
| 89 | $10 \cdot 0$ | 131214 | $14.0 \times 10.2 \times 11.8$ |  | 11.36 |  |



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$\begin{array}{rr}f & p \\ 2 . & p \\ 3.09 & 30 \\ 4.06 & 36 \\ 5.79 & 52 \\ 7.69 & 52 \\ 1.38 & 67 \\ 2.40 & 97 \\ 8.62 & \end{array}$
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# Project 80 

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Project 80 gives you choice from a range of 9 different modules for combining in a variety of ways to suit your requirements. The Stereo 80 is a versatile pre-amp control unit designed to meet all domestic hi-fi requirements including tape monitoring, high sensitivity magnetic cartridge input, ard of course. individual slide controls on each channel for precise output matching. By separating the F.M. tuner and stereo decoder, useful economies can be effected where stereo radio reception is not needed. Two power amplifiers - Z.40 ( 18 watts RMS continuous into 4 ohms using 35 V ) and Z .60 ( 25 watts RMS continuous into 8 ohms using 50 V ) are available with choice of 3 different power supply units. The PZ. 8 with its virtually indestructible circuitry is particularly recommended. For the final word in system building, the Active Filter Unit puts the finishing touch of quality to what are easily the world's most technically advanced hi-fi modules. Any further units likely to be added to Project 80 range will be compatible with those aiready available.

[^2]Stereo 80 Control Unit Size-260.50.20mm (102.2.z.1ns) Finish - Black with white indicators and transparent sliders Inputs - Magnetic pick up 3 mV RIAA corrected. Ceramic pick up 350 mV Radio 100 mV : Tape 30 mV Signal/noise ratio - 50 db Frequency range - 20 Hz to 15 KHz 1 dB .10 Hz to $25 \mathrm{KHz} \cdot 3 \mathrm{~dB}$ Power requirements -20 to 35 volts Outputs $100 \mathrm{miv} A B$ montoring for tape Controls - Press button tape radio and $P U$ Sliders on each channel for volume bass treble $\quad$ (add C1 19 VAT AT.) f11.95
Project 80 FM Tuner size $-85 \quad 50 \cdot 20 \mathrm{~mm}$ ( $3 \frac{1}{2}, 2$. 2 ins) Tuning range Dual varicap - 87.5 to 108 MHz Detector -1 C balanced orncidence One IC equal to 26 transistors Distortion - $02 \%$ at 1 KHz for $30^{\circ}$, modulatton 4 pole ceramic filter in I.F. section Aerial impedance - $75 \Omega$ or $240300 \Omega$ Sensitivity - 5 microvolts for 30 dB S $/ \mathrm{N}$ ratio Output - 300 mV

Project 80 Stereo Decoder size - 47. 50. 20mm ( 1 音 $\cdot 2$. $\frac{3}{4}$ ins) One 19 transistor I.C. Channel separation greater than 30 dB Power

Active Filter Unit separate controls on each channel size 10850.20 mm ( $4 \frac{1}{\alpha} \quad 2$. 3 ms ) Voltage gain - minus 02 dB Frequency response -40 Hz to 22 KHz controls minimum Distortion - at $1 \mathrm{KHz}-003 \%$ using 30 V supply H F cut off (scratch) -22 KHz to $55 \mathrm{KHz}, 12 \mathrm{~dB}$ /oct slope

Z.40 Power Amplifier size-55 80. 20 mm (2t $\cdot 3 \frac{1}{6}$ (ins) 9 transistors Input sensitivity - 100 mV Output 18 watts RMS continuous into $4 \Omega(35 \mathrm{~V})$ Frequency response $-30 \mathrm{~Hz}-100 \mathrm{KHz}: 3 \mathrm{~dB} \mathrm{~S} / \mathrm{N}$ ratio -64 dB Distortion - at 10 watts into $8 \Omega$ less than $01 \%$ Power requirements -12 to

Z.60 Power Amplifier size-55 $98 \cdot 15 \mathrm{~mm}\left(21 \cdot 3 \frac{3}{4} \cdot \frac{3}{4}\right.$ ins) 12 transistors Input sensitivity - 100-250mV Output - 25 watts RMS continuous into $8 \Omega(50 \mathrm{~V})$ Distortion - Typically $0.03 \%$ Frequency response -15 Hz to more than $200 \mathrm{KHz}+3 \mathrm{~dB} 5 / \mathrm{N}$ ratio - better than 70 dB Buit-in protection


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pROBABLY one of the most interesting features about our activities is that there is always a chance of the unexpected happening. It may be an unusual DX contact, or a circuit design that behaves in a different manner than expected. It could be that someone comes up with a new integrated circuit that can replace a mass of discrete circuitry. The element of surprise always helps to make a magazine interesting; readers are incredibly thirsty for such information because it is born out of curiosity (see last month's leader). Whilst curiosity is the expectation, you may describe surprise as "unexpectation"-if there was such a word.
At the same time, to preserve the value of surprise, one must exercise some degree of secrecy until it is reasonably sensible to release the full details. However, we often find ourselves caught between these two positions when we have to judge how much we can tell you in advance and how much to leave until the last minute.
For this reason, little information was released about Tele-Tennis, much to the disappointment of our competitors and those who have a commercial interest, and little was released about the "PW Super Separates" that are being started in this issue. So far, we can tell you that the "PW Derby" is a high quality amplifier designed specially for us and described by the co-designer of the "Gemini" amplifier. What follows in future articles in this series must remain secret until the time is right to let readers know.
However, we can tell you that these designs are of a very high standard. For those readers who have a good domestic set-up already, we can probably help you to fill the gaps. If you are looking for a second set-up for the bedroom or spare room, then stay tuned to P.W. every month.

The great advantage of the "P.W. Super Separates" is their flexibility; you don't have to spend a lot of money to build a complete integrated unit, that seems to go on endlessly for about a year. Take your choice and we shall try to publish all the required details of each project.
What better to start with than a stereo headphone amplifier, rapidly becoming the accepted way of personal listening, where the 20 or 30 watt amplifier is more expensive and often too much for personal listening. For information on future projects watch our advance notices each month.

Before packing my bags for a fortnight's holiday, there is just one more point. We understand that some readers are having difficulty in obtaining P.W. and that the TeleTennis game has created a rapid demand as soon as it appears. If there are none left on display in your newsagents shop, ask the assistant if they have any more. The chances are that there may be some in the stockroom. Better still, why not place a regular order or take out a subscription and be sure of it.

M. A. COLWELL-Editor.



## BBC and quadraphony

THE BBC has been working for some time on the possible applications of quadraphony to broadcasting. A number of four channel recordings have been made using different production techniques and several transmission systems have been examined. Unfortunately, no system has yet been devised which would enable quadraphonic material to be broadcast from a single v.h.f. transmitter while at the same time providing fully satisfactory reception to listeners using monophonic or stereophonic receivers.
The results obtained with some quadraphonic recordings are impressive, and there is considerable public interest in this development. To enable those who were interested to hear a number of recent BBC quadraphonic recordings, there was an experimental broadcast from 12.05 am to 1 am on the early morning of Saturday, 6 July. Two groups of stereo transmitters were used, Radio 2 carrying the left and right front signals, with Radio 3 carrying the left and right rear signals. To take full advantage of the quadraphonic transmission, listeners required two complete stereophonic receivers, one tuned to Radio 2, feeding the 'front' loudspeakers; a second stereo receiver tuned to Radio 3 connected to the 'rear' speakers.

The special programme included a variety of different musical items as well as some drama and outside broadcast material. The BBC would be grateful for reports from listeners who were able to hear this experimental broadcast.
It must be emphasised that there is no possibility of a regular quadraphonic service on the basis of two separate transmitter networks, but the BBC will continue its investigations into the possibility of a system to provide quadraphonic programmes from a single transmitter, without degrading the results obtained by those with mono or stereo receivers.

## Interface 74

TEXAS Instruments recently held a very interesting seminar called 'Interface $74^{\circ}$.

Several excellent lecturers spoke on new bipolar IC's and their applications and a very interesting talk on new optoelectronic products by Martin Abbott followed.

An ultrasonic remotecon-trolled-colour TV was demonstrated by Clive Hoggar, Product Marketing Manager (Consumer IC's) and this was followed by a talk on power transistors presented by John Thorogood and Bryan Norris, Texas Instruments' Applications Manager.

The "star of the day" was Pauline Hamill, Product Marketing Manager for Small Discrete Products. She gave a most interesting lecture (despite a dodgy radio mike!) on Timtor transistors to over 300 male delegates who sat in awed silence. At the end of her talk, Pauline received a great round of applause. (think what courage you would need fellas, to lecture to over 300 women!) Well done Pauline!

Millis Miller, in a lilting Texan accent told the delegates all about the various applications of optoelectronics and this was followed by a talk describing new MOS products.

The day's lectures finished with a question and answer session chaired by Richard Mann, the "mann" who very ably organised and produced the seminar. Richard is the Market Communications Manager of Texas Ltd.

All the delegates were presented with a very comprehensive Data Pack.

Texas hold these seminars every year and they're jolly good value for moncy, so if you want details of future presentations, contact T. I. Limited at Manton Lane Bedford (0234-67466).

## Preston rally

ON 18th August Preston Amateur Radio Society are holding their mobile rally at Deepdale Primary School, St. Stephen's Rd., Preston.

## Marconi Exhibition at Science Museum

INCLUDED in the Science Museum, London, exhibition commemorating the centenary of Guglielmo Marconi is a case of personalia like this silver table lighter made in the form of a disc discharger used in the Marconi Company's early long range transmitters. A number of these lighters were made for presentation to delegates attending a conference arranged by the Company in 1912.

(Science Muscumi photo)

## Lee Products

L̈EE PRODUCTS (GB) are marketing a range of Aiko home entertainment and ICE products under an agreement with the Japanese manufacturer.

Aiko products are added to the existing Elizabethan, Elpico and Dulci brand names.

The 14 Aiko products range from portable cassette tape recorders to a stereo casette deck operating with the Dolby system and priced at $£ 135$ including VAT.

The announcement of the Aiko range coincides with Lee Products move to their new premises at Dallas House, Aintree Road, Perivale, Middlesex.

## Sinclair price drop

EUROPE's largest manufacturer of pocket calculators, Sinclair, has cut the retail price of its "Cambridge" model to $£ 24 \cdot 95$ plus VAT.
Mr. R. Helmer, Sinclair's marketing manager stated recently that the firm's motive for making the price reduction is to open up a vast new market potential which recent research shows exists around the $£ 20$ mark.

The firm state that they are able to bear the price cut because of the scale already achieved on the production of the Cambridge. More than 200,000 units have been sold since its introduction last August.

Mr. Helmer said that 17,000 of the 25,000 units manufactured every month were required for export.
The Cambridge is still available in kit form at $£ 14 \cdot 95$ plus VAT.

## Our Front Cover

TIIE: Zero 100 SB automatic single player featured on our cover this month was kindly loaned by Garrard Engineering. The Zero 100 was first introduced in 1971 and has established an excellent reputation, especially for its tangential tracking arm. This unique arm, with its pivoted head is claimed to economically reduce tracking error and harmonic distortion to virtually zero.

The Zero 100 SB retains the refinements included in the earlier decks but has the added advantage of belt drive and an automatic record counter to help monitor stylus wear.

Recommended retail price of the unit, fitted with a Shure M93E cartridge is $£ 69 \cdot 72$. Further information may be obtained from Garrard Engineering Lid., Newcastle Streel, Swindon, Wiltshire.

[^3]

ACOMMON procedure used to obtain reception of signals in the 2 m Amateur band is to employ a crystal-controlled converter the output of which is coupled to the aerial input of a standard short wave communications receiver, which is utilised as a tunable IF strip.

Commercial converters are, in the main, quite expensive and in some cases can cost nearly as much as the listener's main receiver. The converter to be described can be built at less than half the cost of its commercial counterpart but, unfortunately, many constructors have a great deal of difficulty, if not in the actual constructional work involved, then in the alignment of the various stages of the converter.

Perhaps the biggest problem in attempting to construct a published design is the duplication of the low inductance coils and persuading them to resonate at the desired frequencies. The problem is made doubly difficult, if not impossible, by the lack of the appropriate test equipment.

On first inspection of the various component catalogues and coil data available no coils are specifically manufactured for frequencies higher than approximately 80 MHz . The types available nearest to our requirements are the Denco Range 7 coils, intended initially for valve usage to cover a frequency range extending up to 78 MHz . Comparatively large parallel capacitance is used to achieve this coverage and simple calculations reveal that, using much smaller values of parallel capacitance, coverage to at least 150 MHz was possible. With this fact in mind the present design was evolved.

## THE CIRCUIT

The circuit of the complete converter is shown in Fig. 1. The RF stage Trl employs an AF139 in the common-base mode with untuned input from the aerial and a double-tuned bandpass arrangement at the output to feed the mixer, top capacitance coupling being provided by means of C4. Extra gain could have been achieved by employing the same transistor in the common-emitter configuration, but this would have required some form of neutralisation so in the
interests of simplicity this was not thought to be desirable. The circuit used has been found, in practice, to provide ample gain and has at no time showed any signs of instability when using such diverse aerials as random lengths of wire and multi-element Yagi arrays.

The crystal oscillator stage $\operatorname{Tr} 3$ employs an AF1 15 as does the common-base frequency multiplier Tr4. The frequency of oscillation is controlled by the quartz crystal X1, Cl0 providing the necessary feedback capacitance to maintain oscillation. The circuit will not oscillate unless the tuned circuit L4/C9 is resonant near to the frequency of the crystal, which in this case is 38.666 MIIz. adjustment of the tuned circuit being achieved by means of the core in L4. The 38.666 MHz output is then link coupled to the tripler stage Tr4, the output of which is tuned to 116 MHz and link coupled via 1.5 to the gate circuit of the 2N3819 EFT mixer Tr?


The amplified RF signal at $145 \pm 1 \mathrm{MHz}$ is then mixed with the oscillator output frequency at 116 MHz . The difference frequency $29 \pm 1 \mathrm{MHz}$ is then extracted from the FET drain circuit and fed via L3, which is tuned to 29 MHz by C7, to the main receiver aerial socket. With the converter oscillator frequency operating below signal frequencies, the direction of tuning on the main receiver will be inaintained. This means that when tuning from 28 MHz up to 30 MHz on the main receiver, the converter is tuning from 144 MHz to 146 MHz .

## CONSTRUCTION

'The converter is housed in a readily available aluminium box with lid measuring $6 \times 4 \times 2 \mathrm{in}$ allowing ample room for the coils and other components. Most of the wiring and small components are accommodated on a $5_{2} \times 31_{2}$ in piece of single sided copper clad board Fig. 2 which has the advantage that components and screens can be soldered directly to it, enabling short earth returns to be made.


## components list

| Resistors |  |  |  |
| :---: | :---: | :---: | :---: |
|  | $1 \mathrm{k} \Omega$ | R6 | 8-2k $\Omega$ |
|  | $12 k \Omega$ | R7 | $39 k \Omega$ |
|  | $3 \cdot 3 \mathrm{k} \Omega$ | R8 | $1 \mathrm{k} \Omega$ |
|  | $1 \mathrm{k} \Omega$ | R9 | $330 \Omega$ |
| R5 | $3 \cdot 3 \mathrm{k} \Omega$ |  | $100 \Omega$ |
| All resistors $\frac{1}{4}$ or $\frac{1}{3} \mathrm{~W} 10 \%$ |  |  |  |
| Capacitors |  |  |  |
|  | 20pF TC | C8 | 1000pF FT |
|  | 1000pF FT | C9 | 25 pF TC |
|  | 5pF TC | C10 | 5pF TC. |
|  | 3 pF TC | C11 | 1000pF FT- |
|  | 5 pF TC | C12 | 10pF TC |
|  | 1000pF FT | C13 | 1000pF FT_ |
|  | 40pF TC |  |  |
|  | Tubular Ceramic | FT F | eedthrough |
| Semiconductors |  |  |  |
| Tr1 AF139Tr2 2N3819 Tr3/4 AF115 |  |  |  |
| Inductors |  |  |  |
| L1/2/5/ Range 7 Red <br> L3/4 Range 5 Blue |  |  |  |
| All Denco miniature dual-purpose (valve type) coils. Cores must be specifically requested for the Range 7 coils. |  |  |  |
| Misceilaneous |  |  |  |
| Aluminium box $6 \times 4 \times 2$ in (Type AB13). Copper-clad boa.d $5 \frac{1}{2} \times 3 \frac{1}{2} \mathrm{in}$. Coaxial sockets (2). Battery plugs/, soctets (2). Crystal $38 \cdot 666 \mathrm{MHz}$ HC6U or HC18U (Ser'ator Crystals, 36 Valleyfield Rd., London, SW16 2HR). |  |  |  |

The copper clad board is mounted on ${ }_{8}$ in spacers, one at each corner, and the five Denco coils are mounted on the aluminium box lid. This means that although ${ }_{1}$ in fixing holes are needed in the lid, ${ }_{1}$ in holes are required in the board so as to clear the main form of the coils. This method of construction, in effect, lowers the coil pins enabling shorter coil connections to be made, which is a distinct advantage at the frequencies involved. The two coaxial sockets and the battery sockets are also mounted on the box lid, holes being suitably provided in the copper board to take their connections.

The copper board should be cut and drilled Fig. 3, making sure that holes have been provided for all

- the coils, the feedthrough capacitors and the aerial, IF output and battery leads plus of course the lioles for the 6BA fixing nuts and bolts. This board can then be used as a template for drilling the box lid. The feedthrough capacitors can now be soldered or bolted into position cutting off just enough of the pins on the non-copper side of the board so that they do not make contact with the underside of the box lid when it is in position.

At this point R10 must be soldered into position between the projecting pins of Cll and $\mathrm{Cl3}$ on the non-copper side of the board. The aerial, IF output and battery sockets can now be fixed in position on the box lid and the copper board mounted on its spacers ready for wiring the remainder of the components.

Short direct wiring must be used and special care taken when soldering to the coil pins. The polystyrene formers used for the coils will melt if subjected to excessive heat and it is perhaps a good idea to use a heat sink on the coil pins, as well as on all the transistor leads, when soldering.


Fig. 2: Layout of components and screens on the copper-clad


The crystal used in the original converter was of the HC6U type and the necessary crystal holder was glued in position on the copper board.
A wire ended crystal of the HC18U type could also be used, no holder then being required.

## ALIGNMENT

Before any 2 m signals can be heard with the converter the crystal oscillator stage $\operatorname{Tr} 3$ must be operating. Adjustment of $L 4$ core will make the oscillator work. This can be checked by connecting a meter in series with one of the battery leads and adjusting L4 for a peak in current, indicating that the
oscillator is functioning correctly The battery supply should be switched on and off several times to ensure that the oscillator works every time. If the oscillator fails to restart at any time, tune L4 very slightly to the high frequency side of the current peak, i.e. anticlockwise about half a turn. Adjustment of L5 core should now produce another similar but smaller increase in current when tuned to 116 MHz .

Operation of the oscillator on any frequency other than $38 \cdot 666 \mathrm{MHz}$ and thus the multiplier on 116 MHz , was found to be impossible with the values of parallel capacitance used. In order to align the amaining tuned circuits the converter should now te coupled to the main receiver by means of a short length of

coaxial cable and the receiver tuned to 29 MHz . A suitable 2 m aerial should be plugged into the converter aerial socket. The IF output coil L3 and the two 145 MHz tuned circuits L 1 and L 2 should be peaked by means of their respective cores for maximum noise from the loudspeaker or headphones. The coils should now be very close to their correct settings and any strong signals on the 2 m band should be heard if the main receiver is tuned from 28 to 30 MHz . The coils can then be finally adjusted on these incoming signals.

As a guide when setting the coil cores the length of brass studding projecting from the top of coils L2, L4 and L5 when correctly aligned was $0 \cdot 4 \mathrm{in}$, LI was $0 \cdot 3 \mathrm{in}$, and L3 was $0 \cdot 2 \mathrm{in}$. When final alignment has been completed the cores can be locked in position with 6BA nuts.

## AERIALS

Although a simple dipole or halo type of aerial will provide satisfactory reception of signals from local or near local stations, the increase in range obtained by using a multi-element Yagi aerial far outweighs its cost and is a very worthwhile acquisition. Dimensions for a simple half-wave dipole suitable for initial tests are given in Fig. 4.

The choice of output frequency of the converter was purely a personal one and 28 to 30 MHz used because an Amatcur-bands-only receiver was in


Fig. 3: Too left, gives all the drilling information required to prepare the board for wiring. The screens are soldered directly to the main board as are many of the component earth returns. The photograph emphasises the simplicity of the design. This view is of the RF tuned circuits and the IF output coul L3 at extreme left.
use. It is realised that not all general coverage receivers provide adequate performance at such high frequencies, often lacking in sensitivity, image frequency rejection and bandspreading facilities. In such cases a lower tunable IF is desirable, the most popular seeming to be 4 to 6 MHz . For this lower IF the crystal must be changed to $46 \cdot 666 \mathrm{MHz}, \mathrm{C} 9$ to 18 pF , C.12 to $6 \cdot 8 \mathrm{pF}$. C7 to 35 pF and LJ to a Range 3 Blue coil.


Fig. 4. This simple dipole will do for initial tests of the converter but a beam aerial will greatly improve results.
Although the converter is fully screened, if the lower IF is used trouble may be experienced with signals breaking through at the tunable IF frequencies, especially if the main receiver is not fully screened. The shortest practicable length of coupling coax should be used in these cases and if this is unsuccessful the metal case of the converter should be bonded to the main receiver case by a short metal strap.



## IN THE AUGUST ISSUE

## COMPONENT DISTRIBUTION SURVEY

Along with the rapid growth of the electronics industry in recent years there has arisen a very complex component distribution system. In fact there are so many manulacturers and suppliers operating with many different trading policies that it can be difficult and time consuming to find out what is the best course to adopt in seeking supplies, whether for one-off construction, servicing requirements or equipment manufacture. "Television's" survey next month examines this field with the aim of niving readers a clear picture of the current situation, and lists the trading policies and stock lines of a number of suppliers who are likely to be useful to readers.

## SERVICING TELEVISION RECEIVERS

The next chassis to be covered by Les LawryJohns is the BRC/TCE 1590/1591 solid-state mainsbattery portable chassis.

## LINE OUTPUT STAGE PROTECTION CIRCUIT

When the line generator falls to oscillate the line output pentode is left without bias and draws a very heavy current. This can damage not only the line output valve but the boost diode and line output transformer as well. It is tempting to speculate on how many line output valves and other components have been unnecessarily destroyed in this way over the years. Keith Cummins decided to see whether there was a simple solution to the problem and found that for a matter of pence an effective protection circuit could be built.

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## LM381N DUAL LOW NOISE AMPLIFIER

THE National Semiconductor LM381N device contains two similar low noise preamplifiers in a single integrated circuit. It has a wide range of uses in entertainment cquipment, such as amplifying the signals from stereo tape recorder heads or cartridges. It is an idcal device for amplifying low level signals in low noise applications. The amplifiers are completely independent and each provides a gain, without feedback, of about 112 dB ; a voltage gain of 160,000 .
The device provides a channel separation of 60 dB whilst the internal power supply decoupling and regulator circuits provide 120 dB rejection of signals on the power supply line, such as mains hum. Although many attempts have been made to use suitable operational amplifiers for low noise audio applications, the availability of the new LM381N designed specifically for these applications makes it possible to obtain lower noise levels, better rejection of signals on the power supply lines, wider bandwidth, with fewer external components.

A specially selected ultra-low noise version of the LM381N is available under the coding LM381AN. It is used in critical applications requiring the lowest possible noise levels, such as hydrophone amplifiers, studio sound equipment, scientific instrumentation etc. The LM381AN is naturally somewhat more expensive than the more commonly used LM381N.

The LM38.1N operates from a single power supply in the range 9 V to 40 V . The typical supply current is 10 mA . The device contains internal circuits which protect it from damage if the output is accidentally shorted limiting the output current to about 12 mA . The maximum output voltage swing which can be


Fig. 1 : The internal input circult of the LM381N.
obtained from the LM381N is only 2 V less than the power supply voltage used. The total harmonic distortion is typically $0 \cdot 1 \%$.

## Input

The basic circuit of the input stage of one of the amplifiers in the device is shown in Fig. 1. In the circuits and text the pin numbers of the second amplifier will be shown in brackets. The optimum noise performance is obtained with 'single ended operation'. In this case $\operatorname{Tr} 2$ is biased OFF and feedback is taken to the common emitter of pin 3 (pin 12). Noise figures with single ended operation are typically ldB with $50 \mathrm{k} \Omega$ input impedance, $1 \cdot 3 \mathrm{~dB}$ with $10 \mathrm{k} \Omega$ and 1.6 dB with $5 \mathrm{k} \Omega$ input over the frequency bandwidth 10 Hz to 10 kHz .

When the extra noise contributed by Tr 2 can be tolerated, the feedback may be taken to the inverting input of pin 2 (pin 13). The impedance at the base of $\operatorname{Tr} 2$ is about one hundred times higher than that at the emitter; smaller capacitors and larger resistors can therefore be employed when the feedback in tone and equalization circuits is returned to the base. However, in this 'differential' configuration the noise is increased by a factor of $\sqrt{ } 2$. The input impedance is of the order of $100 \mathrm{k} \Omega$ whilst the output impedance is $150 \Omega$.

## Bandwidth

The amplifiers each contain an internal frequency compensating capacitor which results in a gainbandwidth product of about 15 MHz . This is the frequency at which the gain falls to unity. This compensation is adequate to preserve stability at a

Fig. 2: The connections of the LM381N. The connections to the two internal amplifiers are distinguished by the numbers in brackets.
closed loop gain of 10. A suitable external capacitor may be placed in parallel with the internal capacitor connecting between pins 5 and 6 (pins 10 and hll), Fig. 2. This reduces the amplifier bandwidth and thus removes most of the high frequency noise.

## Applications

Tape Playback Preamplifier using the LM381N is shown in Fig. 3. Tape playback amplifiers must contain frequency compensation circuits so that the overall record-replay operation shall produce a level frequency response. The capacitor Cl provides an amount of negative feedback which increases with rising frequency. The gain therefore decreases with rising frequency, the circuit being designed to have a response complying with the NAB standard for a tape speed of $3^{3}$ i.p.s.


Fig. 3: A typical tape playback preamplifier.
The circuit will convert an output of $800 \mu \mathrm{~V}$ from a playback head into a 0.5 V RMS signal at the preamplifier output at a frequency of 1 kHz , a voltage gain of 56 dB . This circuit requires about five seconds before it can be used after the power has been supplied since C2 takes time to charge through R1.


Fig. 4: A fast turn-on tape playback amplifier.

The circuit of Fig. 4, is slightly more complex than Fig. 3 but it has the advantage that it can be used immediately the power is applied. It has been designed to have a similar performance to that of the Fig: 3 circuit. The 120 dB rejection of signals on the power supply line has been preserved in this circuit.
Tape Record Preamplifier used to feed tape recording heads must also be tailored to produce the correct response. Consider the case where a microphone producing a peak output signal of 10 mV is required to drive a tape recording head which requires $30 \mu \mathrm{~A}$ of audio drive current. This requirement can be met by the circuit of Fig. 5. A single ended input circuit is used for optimum noise performance.


Fig. 5: A preamplifier for driving a lape recording head.
The values of the inductance L1 and of the capacitor C 1 should be chosen to suit the particular recording head used. The feedback network R1 to R4, C2 and C3 provides the required frequency response.

Magnetic Pick-ups provide outputs which are typically in the range 3.5 mV to 8 mV at a velocity of $5 \mathrm{~cm} /$ second; high quality recordings use velocities of this order. The output is proportional to the velocity.


Fig. 6: A preamplifier for use with a magnetic cartridge in a record

A typical preamplifier for use with a magnetic pick-up is shown in Fig. 6. It provides the required response which falls with increasing frequency and has been designed for use with a cartridge of $0.5 \mathrm{mV} /$ $\mathrm{cm} / \mathrm{sec}$ sensitivity. The circuit will drive a power amplifier which reaches the overload level when a signal of 5 V RMS is applied to its input. The resistor Rll provides the load to a standard cartridge with the normal RIAA characteristics.


Fig. 7: A tone control circuit suitable for use between the output of the Fig. 6 circuit and the input of a power amplifier.

Tone controls. In many circuits two preamplifiers are employed, one before and one after the tone control circuits, in order to compensate for the insertion loss in the tone control network. However, when the LM381N is used as a preamplifier, only a single preamplifier stage is required owing to the high gain and high maximum output voltage provided by this device. A simple tone control circuit with bass and treble boost and cut facilities is shown in Fig. 7 which can, for example, be placed directly between the output of the record player amplifier of Fig. 6 and a power amplifier.


Fig. 8: The characteristics of the tone control circuit of Fig. 7.


Fig. 9: An audio mixer circuit. Further inputs can be added, if required as indicated by the components shown in dotted lines.

The characteristics of the tone control circuits of Fig. 7 are shown in Fig. 8. It can be seen that a maximum boost or cut of about 20 dB is available on both treble and bass.

Audio Mixer is the final example of the versatility of the LM381N, Fig. 9 designed for use with $600 \Omega$ dynamic microphone providing output level of 10 mV . The circuit provides an output signal of 5 V and can be used over a dynamic range of 80 dB . A number of input signals (A to E) can be selected or combined with any other input signal.

The LM381N and AN are available from Athena Semiconductor Ltd., 140 High St., Egham, Surrey.
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THE quality of the signals dispatched from the BBC studios for broadcast over the VHF frequency-modulation network is of a very high standard indeed. Development of domestic tuners and amplifiers over recent years has been such as to enable justice to be done to the high standard of received signals. Hi-fi radio enthusiasts will readily confirm the excellent results that can be obtained, yet sometimes with a note of reservation. It is often found that broadcasts originating in an area remote from the regional transmitter are of a lower standard than those coming from the local studio. So listeners in the South cannot expect as good results from a live broadcast at the Edinburgh Festival as from London's Festival Hall.


Fig. 1 : (a) Typical audio analogue signal with instantaneous sampling intervals shown. (b) Quantisation, where each sample is assigned a digital value according to the number of units (bits). Arrows indicate samples where level is between two bits. (c) First three samples represented by train of pulses.

The reason for this is the links that are used to convey the signals from the studio or concert hall to the various transmitters. Owing to the limited range of VHF transmitters these must be sited within the locality they serve, hence the inescapable need for long studio links, often of several hundred miles. Many things can happen to a signal on a journey of that length, the higher frequencies can be lost, there can be phase differences due to varying transit times of different frequencies, any non-linearity will produce harmonic and intermodulation distortion, and of course noise can be picked up from numerous sources, thus imposing a restriction on the dynamic range which can be allowed. Furthermore reactive elements can give rise to 'ringing', the spurious oscillation produced by transients in the signal.

## NEW LINKS

All this will be a thing of the past as the new pulse-code-modulation (PCM) links are installed between studios and transmitters all over the country. The South East is already so equipped and the links are being extended Westward and Northward, so that within two or three years the same standard of quality will be transmitted irrespective of the area of origin. By means of PCM, signals can be sent over great distances without any loss of information and with zero noise and distortion. This like the per-petual-motion machine may seem to be a sciencefiction dream, but it really does work. Like a lot of 'new' ideas, it is not new at all, having been invented in 1938, but the complex circuitry required, had to wait until IC's were developed before it could become a practical proposition.

In order to understand how it works we must first consider the nature of the normal audio signal such as the output of a microphone. It takes the form of a constantly varying voltage which in fact is comparable or analogous to the varying pressures of the sound-wave producing it. For this reason it is termed an analogue signal, and, because it consists of a wide range of frequencies and amplitude levels, it needs equipment capable of handling such ranges without modification of the signal in order to process it. Therein lie the difficulties.



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## QUANTISATION

If we take a typical audio signal, and sample the level at regular intervals we will get the result as shown in Fig. 1. Each sample represents the instantaneous level of the audio signal at the moment of sampling, and this level can be expressed by a certain number of electrical pulses. The individual samples are known as words, and the pulses making up each sample as bits. The conversion of the analogue signal into pulses is termed quantisation because it is quantitively expressed as a certain number of bits. As the signal is now a series of digits or numbers it is described as digital. This information can be later decoded and used to construct a wave identical to the original.

The quality of the result depends on two main factors. First, the number of samples or words that are taken in a given time. Any alteration of the waveshape that occurred between two successive samples would be lost. Such an event would occur if the sampling rate was lower than the highest frequency contained in the signal. In practice it has been found that the sampling rate must be at least twice as high as the highest frequency to be sent. BBC FM broadcasts transmit frequencies up to 15 kHz , and so the sampling rate is a little higher than twice this at 32 kHz .

The other factor is the number of bits contained in each sample. If the amplitude of the original wave is to be accurately represented, the maximum number of levels definable must be large. Should the analogue wave amplitude fall between two specified levels, it will be assigned the value of the lower one and be reproduced at that level in the decoding process. Thus the wave shape will not be identical to that of the original and harmonic distortion will be added. This type of distortion arising during quantisation is the only type of distortion than can arise. Once the signal is encoded no further distortion can appear in the transmission. Thus it is always a known quantity and does not depènd on outside variables.

## BBC PCM

The BBC system uses a large number of sampling levels, actually 8191 different amplitudes, and so quantisation distortion is kept to a very low level. It is in fact 1 part in 8191, maximum, which is $0.0122 \%$, far better than the domestic equipment used to reproduce it.
As described here though, the system has one major snag. With a sampling frequency of 32 kHz , and each sample can contain up to 8000 bits, the resulting frequency will be 262 MHz ! This is completely unrealistic, and no link would have the bandwidth to accommodate anything like such a frequency, especially for a single audio channel.

Many readers who have followed thus far, will, by now, have cast their eyes down the following paragraphs with some apprehension and perhaps disgust. Practical men are often allergic to maths, and so the tendency may be to finish about here and turn over to the constructional features. However, don't be put off by what may appear to be a formidable array of figures. It's much easier than it looks, and actually it is very interesting to see the rather ingenious way by which the bandwidth problem has been solved. On the other hand, mathematical types, will probably have solved it already.

## BINARY CODE

The solution lies in the use of the binary code by which large numbers can be represented by a small number of digits of only two factors, 0 and 1. To start with, most readers will know that when a number is multiplied by itself (squared), it is said to be raised to the second power and written $\mathrm{n}^{2}$; when so multiplied twice ( $\mathrm{n}^{3}$ ) it is raised to the third power, and so on The table lists 13 values, the twelve powers of 2 , and also 1 . When all these are added the result is 8191 and it is a fact that any number between 1 and 8191 can be obtained by taking one or more of these numbers and adding them. None need be used more than once.

To illustrate the point consider a couple of examples. The number 3417 can be obtained by adding: $-2^{11}=2048 ; 2^{10}=1024 ; 2^{*}=256 ; 2^{\text {in }}=64 ; 2^{4}=16$; $2^{3}=8$ and 1 . Agreed? Well, that wasn't too bad, so we will try another one, this time let's choose a nice round number, 5000. This is made up of : $2^{12}=4096$ : $2^{y}=512 ; 2^{8}=256 ; 2^{7}=128$ and $2^{3}=8$.

In these examples we only listed the values actually used and ignored the others. However, to enable us to get the sequence right we must list all 13 even if it means assigning a zero value to the unused ones by multiplying by 0 .

Going back to our first example then, the sequence is: $2^{12} \times 0 ; 2^{11} \times 1 ; 2^{10} \times 1 ; 2^{9} \times 0 ; 2^{\times} \times 1 ; 2^{7} \times 0 ; 2^{6} \times 1$ : $2^{5} \times 0 ; 2^{4} \times 1 ; 2^{3} \times 1 ; 2^{2} \times 0 ; 2^{2} \times 0 ; 1 \times 1$.

The second example gives us: $2^{12} \times 1 ; 2^{11} \times 0 ; 2^{10} \times 0$; $2^{9} \times 1 ; 2^{\mathrm{n}} \times 1 ; 2^{\mathrm{i}} \times 1 ; 2^{\mathrm{i}} \times 0 ; 2^{5} \times 0 ; 2^{4} \times 0 ; 2^{3} \times 1 ; 2^{2} \times 0$ : $2^{1} \times 0 ; 1 \times 0$.

Then, if both sending and receiving equipment 'understand' that they refer to a consecutive series of powers of 2, each sample of up to 8191 amplitude levels can be accurately represented by thirteen digits of either 0 or 1 . In our examples the series would be $3417=0110101011001$ and $5000=1001110001000$. In the transmission, 1 is represented by a pulse and the 0 by a space.

BINARY TABLE

| 1 | 1 | 1 |
| :---: | :---: | :---: |
| 2 | 21 | 2 |
| 3 | $2{ }^{2}$ | 4 |
| 4 | $2^{3}$ | 8 |
| 5 | 24 | 16 |
| 6 | 25 | 32 |
| 7 | 26 | 64 |
| 8 | 27 | 128 |
| 9 | 28 | 256 |
| 10 | 29 | 512 |
| 11 | 210 | 1024 |
| 12 | 211 | 2048 |
| 13 | 212 | 4096 |

This table shows the 13 binary bits, 1 and the 12 powers of 2. Any number between 1 and 8191 can be obtained by adding specifled bits. Use or omission of a bit is indicated by 1 or 0 expressed electrically by pulse or space.

Thus there is a dramatic saving in bandwidth; now the frequency will be 13 binary bits $\times 32000$ (the sampling frequency) or just over 400 kHz . It may be thought that this is still rather high for an audio link that handles just the same programme as a 15 kHz analogue link. This, of course, is true, but if we consider the advantages the extra bandwidth is well worth it.

Take noise, for example. Radio amateurs know from experience that when conditions are poor and noise levels high. that the morse code is far more


Fig. 2: Quantisation distortion. Wave-form of Fig. 1 distoried because number of bits (12) is insufficient to accurately represent amplitude levels as indicated by arrows in Fig. 1.
intelligible than speech. Morse is, of course, a digital signal being composed of a series of pulses and spaces similar to our PCM. A feature of both is that the pulses are all of the same amplitude, irrespective of whether the modulated audio signal in the case of PCM, is of high or low level. Low audio signals cannot then get lost in a high noise-level, so this in turn enables a higher dynamic range (ratio of high to lowlevel signals) to be sent. As the receiving equipment responds only to the pulses, noise originating in the link has no effect at all, so it is, in fact, noiseless. Only if the noise approached the level of the pulses would it have an effect but this would be extremely unlikely

## PULSE SHAPE

Pulse-shape is of minor importance as long as the receiver recognises it as a pulse and counts it; harmonic distortion therefore will likewise not affect the signal and there can be no loss of information contained within the modulation, so the audio frequency response cannot be modified. Hence there is zero distortion over the link. It can be seen then that high bandwidth requirement is more than compensated for by the virtually ideal transmission characteristics.

The BBC links combine 13 PCM channels into one having an overall bandwidth of $5 \cdot 5 \mathrm{MHz}$, the same as for a single television channel, which enables the links and associated equipment to be standardised with that of the television service. The 13 channels can be used for separate mono programmes or six stereo with one spare.

## NOISE

Although the signal becomes unaffected by noise once it is encoded, noise in the analogue or encoder circuits will be encoded along with the audio signal. The noise is stated to be -69 dB weighted, which is of
a very low order, much less than could be picked up on a long analogue studio link. The possibility of error in the signal has been provided for. Each sample, as we have seen, consists of thirteen pulses or spaces. If, due to an error in the encoder or elsewhere, there is a discrepancy, the decoder will recog. nise the error and hold the value at the last errorfree sample until the next such one arrives.

## RESULTS

For high-quality results the sampling rate and bit quantity used by the BBC is necessary, but good results are possible with more modest parameters. Some private telephone systems which carry speech only use an 8 kHz sampling rate to give a 4 kHz upper frequency response and 7 binary bits. An interesting feature of some of these systems is the polarity reversal of alternate pulses. Thus two pulses form a complete cycle and thus halve the bandwidth re. quirement.

A demonstration at the Sonex 1973 exhibition gave a direct comparison, with recorded piano music, of results obtained with different bit quantities. When using 12 bits, results were indistinguishable from the 13. At 11, results were still very good but there was a barely perceptible trace of distortion, while at 10 it was more easily detected. From 9 down it became progressively worse. The quantisation distortion has a rather unusual sound which can best be described as a 'crumbling' effect. It should be noted that each binary digit reduction corresponds to a halving of the actual sampling levels, and a doubling of the distortion.

It should be emphasised too, that PCM applies only between studios and transmitters, the broadcast signal being in the normal analogue form irrespective of the type of link used. Digital broadcasting is possible but existing receivers would be rendered obsolete unless both forms existed together, since compatibility is always a major consideration when contemplating any change in a broadcasting system. Furthermore, with the present congestion of the radio bands, the extra bandwidth, although technically easy to achieve. would be impractical.

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# TAKE 2® DAVID ANDREWS 

## No. 62 <br> VARIABLE RATIO COUNTER

## A series of simple transistor projects, using not more than twenty components.

THIS circuit gives a fast 9 V positive-going pulse for a preset number of operations of the push button PB1. The principal of operation is the diode pump circuit. When the button is pressed Cl discharges into C2 througli DI; as soon as the discharge is complete Dl prevents any back flow of the charge out of C2 and provided D1 and Trl and Tr2 all have low leakage characteristics this charge will remain on C 2 as a voltage.

Repeated pressing of PB1 will build up the potential on C2 until it exceeds the level set at the base of Trl which is preset by VRl. When this happens $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$ go rapidly into conduction, aided by regenerative feedback, and C2 is discharged giving rise to a negative going signal at the collector of $\operatorname{Tr} 2$. This is fed to the PNP transistor ( $\operatorname{Tr} 3$ ) and generates a 9 V spike with a reasonably low source impedance.


Circuit of the variable ratio electronic counter.
With the values shown the circuit should divide satisfactory up to frequencies of about 1 kHz . To interface the input with an electronic drive source PBl and R1 should be discharged and Cl should be taken straight to a point that can give DC voltage swings from 0 V to +9 V at low impedance, e.g. the emitter of an emitter follower that is normally held at 0 V . The output of the circuit can easily be used to drive a pulse stretching circuit which could trip a low speed counter or a relay.

## components list

| R1 | $10 \mathrm{k} \Omega \pm$ W | R4 | $1 \mathrm{k} \Omega$ | ${ }_{4}^{1} \mathrm{~W}$ |
| :---: | :---: | :---: | :---: | :---: |
| R2 | $2 \cdot 2 \mathrm{k} \Omega+\mathrm{W}$ | R5 | 10kS | $\frac{1}{4} \mathrm{~W}$ |
| R3 | 4kS ${ }_{4} \mathrm{~W}$ W |  |  |  |
| VR1 | $5 \mathrm{k} \Omega$ linear pot. |  |  |  |
| C1 | $0 \cdot 15 \mu \mathrm{~F}$ |  | $0 \cdot 22 \mu$ |  |
|  | $2 \cdot 2 \mu \mathrm{~F}$ low leakage | polyc | rbon |  |
| D1/D | D2 1N914 |  |  |  |
| Tr1 | BCY71 (general | pos | pnp | silicon) |
| Tr2 | BC108 | Tr3 | BCY |  |
| PB1 | Normally open |  |  |  |



Circuit arranged on Veroboard, VR1 and pushbutton being mounted externally.

The divide ratio is given by the number of times PB1 has to be pressed before C2 is discharged by the transistors and with the values given in this circuit is adjustable, by means of VRI, between about 3 and 20 . If the repetition rate of button pressing is low there is bound to be some charge lost from C2 due to its own and transistor leakage. However, the prototype worked quite reliably at a rate of approximately one press per second. It is, however, anticipated that this circuit would interface with an electronic source of signal operating at a low audio frequency and this problem is then not likely to arise.

## P.W. ELECTRONIC COMPONENTS BUYERS' GUIDE

Special supplement in the October issue giving details of components commonly available, foliowed by additional sections in succeeding issues. More details on page 116 of the June issue.


#### Abstract

WIRELESS TELEGRAPHY ACT Readers and advertisers are reminded of the requirements laid down by the Wireless Telegraphy Act. It is an offence in the U.K. to install or operate wireless telegraphy apparatus except under the provisions of the Act and, except in the case of broadcast soundonly receivers, a licence must be obtained. Included within the provisions of the Act are any apparatus transmitting deliberate signals for any purpose such as "walkie-talkies", radio-controlled models or servos and some types of metal detectors. Apparatus radiating interference signals are subject to controls which also come under the administration of the same Ministry. If you require full information, please write to Waterloo, Bridge House, Waterloo Rd., SE1 8UA.


[^6]
# LenhanIng by practictl proueg steps 

## PART 10-LOUDSPEAKER DRIVERS

IN ANY audio system there comes a time when it is necessary to use electronic signals to drive a loudspeaker. This part of the series will describe several alternative ways this can be done but we shall limit ourselves to considering only low powers in the experimental projects mentioned. The reason for this is solely to keep construction simple and to ensure that only low cost components need be used. Having said that let us hasten to add that the principles to be described are also applicable to the highest of power amplifiers, however, there are usually special protection circuits in these cases which tend to complicate the issue-and in many instances the protection circuitry can be more complex than the amplifier itself.

In one or two previous projects we have driven loudspeakers without saying too much about the method we have adopted; now is the time to fill the omission.

In an amplifier we have to provide several logical stages of amplification some of which we have already covered; basically these can be summarised as, (a) an input pre-amplifier which helps compensate for the impedance of the signal source, (b) a stage which will tailor the frequency response or provide a degree of tone control and (c) a stage that increases the level of signal voltage; this latter stage often brings the signal level up to the maximum needed for the application but usually the output impedance of such a stage is fairly high and certainly cannot be used to pass sufficient current through the low impedance of a loudspeaker speech coil-which can be anything in the range of from 3 to 70 ohms. The prime objective of a power stage is to take the output from the voltage amplifier and match this to the low impedance of the loudspeaker's coil; at the same time a degree of voltage amplification might also be applied.

The loudness of a loudspeaker is proportional to the amount of electrical power one can dissipate within the speech. coil of the loudspeaker. If one knows the impedance of the loudspeaker the power can be quite simply calculated in terms of either the voltages developed across the speech coil or the current flowing through it. These, of course, are a.c. quantities because we are dealing with signals as opposed to bias currents-in some instances (as
we shall see) we have to take account of the latter. If we assume that all the current flowing through the coil is a.c. and comprises signal current the power dissipation can be stated as

$$
\mathrm{I}^{2} \times \mathrm{Z} \text { or } \frac{\mathrm{V}^{2}}{\mathrm{Z}}
$$

where $I$ is the current through the coil and $V$ is the voltage developed across it (these can be peak or r.m.s. values depending on whether we are dealing with r.m.s. or peak power). Z is the loudspeaker's impedance. It is simpler to take the second equation for most purposes and we can see from it that for a given signal voltage we get most power dissipation for the smallest loudspeaker impedance; however we must ensure that the voltage source is not "current limiting" i.e. it must come from a very low source impedance.

For maximum power coupling the source impedance should equal the loudspeaker's impedance. Assuming ideal impedance matching ;if we have a signal amplified to 1 V r.m.s and apply this to a $35 \Omega$ loudspeaker the output power will be

$$
\frac{1 \times 1}{35}
$$

which is just under 30 mW ; reducing the speaker impedance to $3 \Omega$ would, theoretically, give about 300 mW of power but the current requirement would be up by a factor of about ten.

It would be better to double the voltage of the signal to get higher power, because there is a square law relationship between the two, and one does not have to provide a very low source impedance-this is always difficult and provides other problems with power supplies etc. For highest powers it is obviously desirable to have as high a signal voltage as possible together with a low impedance output. To obtain 50 W into a $15 \Omega$ loudspeaker would require signal voltages in the order of 27.5 V r.m.s. To obtain this high signal level it is necessary to have power rail voltages in excess of 50 V . It is thus impossible to get really high powers unless one is prepared to operate with reasonably high voltages as well as low loudspeaker impedances.

Throughout this series we have operated, in the main, with a 9 V supply rail and a $35 \Omega$ loudspeaker. Assuming we made preamplifiers with ideal mid rail
biasing the peak signal voltages we could obtain would be $4 \cdot 5 \mathrm{~V}$ which corresponds to about $3 \cdot 2 \mathrm{~V}$ r.m.s. Given these parameters the maximum powers we could produce would not exceed 300 mW r.m.s.

Summing up, we need to get as high a current with as high a voltage as possible across the speech coil and the experiments that follow show various attempts at getting to this end by different methods -each method has its pros and cons which we shall discuss.

Fig. 71 shows an obvious way of driving a loudspeaker and is an extension of the grounded emitter. amplifier-covered in previous parts. Strictly speaking we should consider the loudspeaker as having an impedance a.c. signal but in practice this is very close to its d.c. resistance; inductance is low and hence inductive reactance at low frequencies is fairly small. If one considers LSl of Fig. 71 as being a $35 \Omega$ resistor we can select a value for R1 which will give us a mid rail bias at the collector of Tr 1 .


Fig. 71 : For the collector potential to be mid rail Ic $\Omega 65 \mathrm{~mA}$ and hence R1 must be about 5k $\Omega$. Quiescent power dissipation in Tr1 is about 150 mW . Input impedance is low.

Before doing this we have to consider the maximum current rating of the transistor with reference to the maximum current that might flow through LS1 when the transistor is fully conducting. Imagine that the supply voltage was our usual 9 V and that Trl was fully conducting; the potential at the collector would be a fraction of a volt (the saturation voltage) and the current flowing would be nearly

$$
\frac{9}{35}=\text { approx } 250 \mathrm{~mA}
$$

This is more than twice the current rating for the transistor hence if a.c. input signals were of sufficient amplitude we might drive the transistor into saturation and burn it out at the same time. By reducing the supply rail to $4 \cdot 5 \mathrm{~V}$ we would only just be exceeding lc(max) for the BC108 even if we applied this maximum input signal. Due to saturation voltages and forward drops in the preceding circuits it would be unlikely that the collector current would exceed the maximum rating of 100 mA . We have thus deduced that with this particular transistor the maximum supply voltage in this application is 4.5 V for safety. R 1 is calculated in the same way as in a previous part to give a mid rail collector voltage so that signals can give peak positive and negative going excursions of $2 \cdot 25 \mathrm{~V}$.

Wire up the circuit of Fig. 71 and measure the quiescent voltages but also take special note of the quiescent current being drawn in the absence of input signal. It is comparatively high and causes power to be dissipated in the transistor and the
speech coil of the loudspeaker to no useful effect. This is a feature of this type of amplifier which comes into the general class of Type A circuits. The maximum r.m.s. power output for a $2 \cdot 25 \mathrm{~V}$ peak signal would be approximately 70 mW and this compares with nearly 150 mW of static dissipation caused by the quiescent current. Not very efficient!

In theory the maximum efficiency of a Class $A$ amplifier is 50 per cent and this is its main drawback; it means that transistors get unduly hot, a lot of current is drawn from the supply under quiescent conditions and, in the case of portable equipment, one would suffer from rapid battery exhaustion. Some Hi-Fi purists will claim—probably correctlythat the class A circuit will provide the best fidelity of signal reproduction because the transistor is operating as a "more or less" linear amplifier, i.e. the current through the loudspeaker is directly proportional to the signal current and there is no way that distortion can creep in. This, of course, is not strictly true-particularly in a simple circuit such as this one because, for a start, $\mathrm{h}_{\mathrm{FE}}$ for a transistor varies with collector current and thus the true linearity (assumed) is not realisable in practice without considerably more complexity. Nevertheless this is a very simple way of providing an audio low power output in simple applications-in particular those that will be subjected to intermittent use.

An example is shown in Fig. 72 where the output from a simple oscillator is used to drive a loudspeaker as a morse practice oscillator. When constructing this unit observe that LS1 must be $35 \Omega$ and the supply should not exceed $4 \cdot 5 \mathrm{~V}$.


Fig. 72: Using the simple class A power stage in a morse practice oscillator circuit. As the signal voltage is high C3 could be omitted and R5 is then connected directly between Tr2's collector and Tr3's base.

Because we have signals as high as 4.5 V at the collector of Tr 2 it is not necessary to have C 3 in circuit because the signal will be driving $\operatorname{Tr} 3$ from one extreme of conduction to the other and the sophistication of mid rail biasing is not necessary hence the circuit can be simplified by taking R5 from the collector of $\operatorname{Tr} 2$ direct to the base of $\operatorname{Tr} 3$.

To obtain a higher output power we need to increase the supply voltage and reduce the loudspeaker's impedance. If this is done we have to use a transistor with a higher current and power dissipation rating; at the same time we illustrate, in Fig. 74, how we can use the simple expedient of making the power stage from an emitter follower (the input signal is so high that we do not need any form of voltage amplification). To provide sufficient


Fig. 73. Layout for Fig. 72


Fig. 74 : Using a power transistor and an emitter follower driver enables us to use a lower resistance load (giving more power) and at the same time we can increase the supply vollage for more power.
signal base current into Tr 4 without loading the output of the multivibrator we have inserted $\operatorname{Tr} 3$ making, in effect, a super alpha pair. This type of output is ideal if we are not worried about mid rail biasing in the output stage.

The base of $\operatorname{Tr} 3$ could have been connected directly to the collector of a conventional grounded emitter amplifier and the mid rail voltage would automatically have been reflected in the quiescent potential at $\operatorname{Tr} 4$ 's emitter-if one allows for base/ emitter forward drops. The only problem with that would be that there is a high standing quiescent current flowing through the speech coil of the loudspeaker giving rise to heating and also the cone would be displaced preferentially in one direction.

To be continued


Fig. 75 : Layout for Fig 74

## ON RECENT DEVELOPMENTS

## NO TICK GIVEN HERE

CMOS circuits intended to form a two-chip digital watch system have recently gone into quantity production at intel. A total average power consumption of only $15 \mu \mathrm{~W}$ means that the watch will operate for more than a year from one mercury cell.
The oscillator/divider chip is. intended for use with a 32 kHz crystal and is capable. of an accuracy of better than 1 minute per year. The other chip contains the decoder/ driver circuitry and is offered in two versions. One of these provides the facility of being able to switch the display to show minutes and seconds. The hours display is then blanked. To help you time intervals of a few seconds, both versions of the output chip cause the colon separating the hours and minutes to flash at 1 Hz .

## GROWING

Developments in liquid crystal displays continue apace. A French company has recently exhibited a 5000-point matrix display giving a text of 96 characters and, even more intriguing, a simple animated picture display twelve inches square.

At the IEA exhibition in London, an Austrian firm was showing a seven-segment display some 6 inches high.

## MORE SCOPE OR LESS ?

Whilst television CRTs have got a lot shorter over the years, those used in oscilloscopes have stayed much the same length, mainly as a result of the good deflection linearity required. Now Philips have developed a new type of CRT which has a diverging lens in the form of a domed mesh between the deflection plates and the screen. The tube length for a given size of display is considerably reduced as a result.

## ELECTRIFYING

News from the USSR that scientists at the Latvian Academy of Sciences have discovered a method of rotating non-metallic objects by passing them through an intense electric field. This effect, similar to that of a magnetic field upon ferromagnetic materials, has been demonstrated using wood, mica and plastics components. Suggested practical applications include alignment of parts on a conveyor belt or in other assembly systems.

## SOMETHING'S MOVING

Small enough to be held in the palm of the hand, Mullard's new X-band ( 3 cm .) Doppler transmitterreceiver modules may well find application in future vehicle collision alarms.

Greatly enhanced signal-to-noise ratio has been achieved by using separate cavities for the transmitter oscillator and receiver detector, both coupled to a single integral antenna.
When used in an intruder detection system, the module can pick out a man moving at a range of 50 feet. Just the thing to protect your priceless art treasures!

## SUNPOWER

In the United States, a Senate investigation has been set up to consider Federal support for a programme of solar energy development. Giving evidence to the investigating committee, RCA Research director Paul H. Rappaport forecast that economical solar energy systems could be in widespread use in the U.S. within five years.

A planned extension to the RCA Building in New York will use solar energy to help run its heating and air-conditioning system.

## FACE TO FACE

A spin-off resulting from the recently introduced local government changes is a new video-telephone system developed by Rediffusion Industrial Services.

The idea was that members of the public wanting to make an enquiry or complaint should not have to travel long distances to one of the new regional government offices in order to see an officer specialising in a particular field. Instead they would go to their local office where an automatically operated console would give them "across-the-desk' contact with the regional office via video-phone. Also included is a document scanner large enough to show household goods or package foods which may be the subject of complaint.

Already, one large company has expressed interest in the system as a means of providing conference facilities for its senior managers.
It would appear that the system has great potential for saving time and fuel by reducing the need for travel.

## MULTIPLEX

More news from British Rail on improved communications, this time aboard Inter-City expresses.

Equipment being fitted will provide three channels-guard to passenger, guard to driver and an audio message playback system which is controlled by distance travelled along the track. All this information is distributed through the train on only two wires, which are also used to control the train lighting.

Rather special measures have been taken to protect the audio equipment from spikes on the train wiring. These spikes can reach 7 kV !
Nams



RIGHT CHANNEL


MANY hi-fi enthusiasts tend to dismiss headphones out of hand, probably through memories of the strangulated reproduction of the Services surplus 'cans'. In contrast, modern stereo headphones are capable of giving a startlingly clear and well defined stereo image, with a quality of reproduction exceeding that of the best loudspeakers. By isolating the listener from his environment they give a sense of detachment, enabling one to devote one's entire attention to the music. For the same reason they are excellent for studying languages or for those whose musical tastes differ from those of their family.

Headphones are ideal for those just starting to acquire a hi-fi system as they minimize the expenditure required. Later, when it is desired to expand the system, it is only necessary to add a pair of amplifier modules, a power supply and a pair of


Fig. 3: Response curves of the amplifier for record or radio.



Fig. 2: Circuit of the power supply section of the 'Derby'.


Fig. 4: The effects of the tone controls are shown in these curves.

[17006]
Fig. 5: Curves relating distortion with output voltage and load impedance.
loudspeakers as the headphones amplifier serve as a preamplifier. The circuit described here gives a standard of perfomance equal to a good hi-fi amplifier and it can be used with any make of headphones provided the impedance is greater than 8 ohms. The circuit is designed to give an output level of at least 1 volt into any impedance and this will be sufficient to generate a sound pressure level of 90 dB or more with most types of stereo headphones.

## CIRCUIT

The circuit diagram of the amplifier is shown in Figs. 1 \& 2. The input stage comprising $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$ is conventional and provides a 5 mV input with RIAA equalisation for magnetic cartridges and a 100 mV input with a flat frequency response for radio etc. Other inputs can be added by the constructor if desired. The response curves of the radio and disc inputs are shown in Fig. 3.
The output stage, comprising $\operatorname{Tr} 3-\operatorname{Tr} 7$, follows the same general lines as a normal hi-fi power amplifier but has been designed for a very much lower power level. The tone control is of the Baxendall type and is incorporated into the feedback loop of the amplifier. The response curves of the tone control are shown in Fig. 4. The output stage thus serves as both a power amplifier and a tone control stage.

The balance control operates by varying the feedback and hence the gain of the output stage and for this reason it cannot reduce the signal level to zero. It does however provide a variation of $\pm 9 \mathrm{~dB}$ between channels. This is entirely adequate for use with headphones as the headphones themselves are usually well matched. The variation of distortion with output level is shown in Fig. 5.

## CONSTRUCTION

The prototype was constructed in a $71_{4} \times 4{ }^{1} 2 \times 2 \mathrm{in}$. diecast box which was decorated with a coat of silver paint and a pair of wooden ends, to give a domestically acceptable appearance. However, any suitable case can be used, provided that the same layout is adhered to. A duplicate of the prototype has been constructed in a record player plinth on a small aluminium chassis. Drilling details for the diecast

## components list

## Resistors

| R1 | R101 100k $\Omega$ | R11 R111 4.7k $\Omega$ | R21 |
| :---: | :---: | :---: | :---: |
| R2 | R102 4-7k』 | R12 R112 15k $\Omega$ | R22 R122 100ks |
| R3 | R103 3308 | R13 R113 10k | R23 R123 4.7ks |
| R4 | R104 100k $\Omega$ | R14 R114 470k $\Omega$ | R24 R124 1ks |
| R5 | R105 470ks | R15 R115 2-2k $\Omega$ | R25 R125 10k $\Omega$ |
| R8 | R106 $330 \Omega$ | R16 R116 15k | R26 R126 $1 \mathrm{k} \Omega$ |
| R7 | R107 47k $\Omega$ | R17 R117 15k $\Omega$ | R27 R127 $10 \Omega$ |
| R8 | R108 10k $\Omega$ | R18 R118 39k $\Omega$ | R28 R128 $10 \Omega$ |
| R9 | R109 $220 \mathrm{k} \Omega$ | R19 680 | R29 R129) Fig |
| R1 | R110 470 | R20 R120 15k | R30 R130 ${ }^{10}$ |

All $\frac{1}{3}$ W or $\frac{1}{2}$ W 5\% carbon film LH channel numbers have 100 prefix

VR1 VR101 $10 \mathrm{k} \Omega \log$ dual gang with DPST switch VR2 VR102 $100 \mathrm{k} \Omega$ linear dual gang
VR3 VR103 $100 \mathrm{k} \Omega$ linear dual gang
VR4 $\quad 2 \cdot 2 \mathrm{k} \Omega$ skeleton preset pot
If a fully variable balance control is desired VR4 should be made a $2 \cdot 2$ or $2 \cdot 5 \mathrm{k} \Omega$ pot (linear law) and mounted on the front panel

## Capacitors

C1 C101 $1 \mu \mathrm{~F} 35 \mathrm{~V}$ TB C12 C112 0.022 $\mu \mathrm{F} 160 \mathrm{~V}$ P C2 C102 4.7 $\mu$ F 35V TB C13 C113 1000pF 125V Poly
C3 C103 47 $\mu$ F 25V Elec C14 C114 1000pF 125V Poly
C4 C104 33pF 125 V Poly C15 C115 $47 \mu \mathrm{~F} 10 \mathrm{~V}$ Elec
C5 C105 $10 \mu \mathrm{~F} 25 \mathrm{~V}$ Elec C16 C116 22pF 125 V Poly
C6 C106 $1 \mu \mathrm{~F} 35 \mathrm{~V}$ TB C17 C1176.8 $\mu \mathrm{F} 40 \mathrm{~V}$ Elec
C7 C107 470pF125V Poly C18 C118 $0 \cdot 1 \mu$ F 250 V P
C8 C108 6800pF 160 V P C19 C119 $680 \mu \mathrm{~F} 16 \mathrm{~V}$ Elec C9 C109 $0.022 \mu \mathrm{~F} 160 \mathrm{~V}$ P C20 $2200 \mu \mathrm{~F} 25 \mathrm{~V}$ Elec
C10 $\quad 470 \mu \mathrm{~F} 25 \mathrm{~V}$ Elec C21 $\quad 0.01 \mu \mathrm{~F} 750 \mathrm{~V}$ D
C11/111 $11 \mu \mathrm{~F} 35 \mathrm{~V}$ TB
TB-Tantalum bead Elec-Electrolytic
Poly-Polystyrene P-Polyester D-Disc ceramic

## Semiconductors



## Miscellaneous

S1, 4 pole 3 way rotary switch. S2, Single pole toggle switch. LP1, Miniature neon indicator lamp. SK1/2, 5 pin DIN sockets (2). SK3, Stereo jack socket. T1, Mains transformer $12 \mathrm{~V}+12 \mathrm{~V} 6 \mathrm{VA}$ (RS Components Ref. Min. Tr. 12V). Knobs (4). Diecast box Eddystone 6827P.

Davian Electronics, PO Box 38, Oldham, Lancs, OL2 6XJ can supply PCB at £1.85, kit of semiconductors at $£ 3 \cdot 10$ or both for $£ 4 \cdot 75$, ail inclusive of VAT and P/P.

| OUTPUT | $\left.\begin{array}{l}1 \cdot 3 V \text { into } 8 \text { ohms } \\ 4 V \text { into } 50 \text { ohms } \\ 6 \mathrm{~V} \text { into } 500 \mathrm{ohms}\end{array}\right\}$This is sufficient to generate a sound <br> pressure level of over 90 dB with most <br> headphones |
| :---: | :---: |
| DISTORTION | $0.14 \%$ with 8 ohm load $0.02 \%$ with $50,500 \mathrm{ohm}$ load $\} 1 \mathrm{~V}$ output at 1 kHz |
| TONE CONTROLS | $\begin{aligned} & \text { Bass } \pm 12 \mathrm{~dB} \text { at } 50 \mathrm{~Hz} \\ & \text { Treble } \pm 12 \mathrm{~dB} \text { at } 15 \mathrm{kHz} \end{aligned}$ |
| DYNAMIC RANGE (Input) | 25 dB referred to 1 V output |
| SIGNAL/NOISE RATIO |  |
| BALANCE CONTROL | $\pm 9 \mathrm{~dB}$ variation between channels |
| FREQUENCY RESPONSE | Disc within 1 dB of RIAA curve 20 Hz to 20 kHz Radio -3 dB at 20 Hz and 22 kHz |



Fig 6 above, gives drilling information for the diecast box while in fig. 7 below, the printed circuit board is shown actual size.



Fig. 8: Layout of compwnents on the PCB and details of the associated wiring. The photograph shows the location of the components mounted on the box.



Fig. 9: Detailed information on the connections to the input sockets and various controls.
box are given in Fig. 6, and after drilling the box should be painted as desired. If wooden ends are required the ends of the box should be left unpainted.

Most of the small components are mounted on a single fibreglass printed circuit board, Fig. 7, measuring $5 \times 3 \mathrm{in}$. There is not a great deal of room to spare and miniature components should be used throughout. The first step is to assemble all the components on the board as shown in Fig. 8, and then to solder all wires for the external connections. Twin screened wire should be used at the input and between the volume control and R15/R115, but ordinary thin connecting wire is satisfactory elsewhere. All leads should be as short and direct as possible.

Mount the stereo/mono switch S2, the pilot lamp and the output jack socket SK3 on the front panel of the case and then mount the mains transformer inside. The assembled printed circuit board can now be fixed in place on ${ }^{1} 4 \mathrm{in}$. spacers and wired up to S 2 and SK3. Then mount the three potentiometers and the selector switch and wire up as shown in Fig. 9. Finally mount the two DIN input sockets and C20 and complete the wiring. The two rectifier diodes D3 and D4 are wired directly between the transformer and the positive tag of C20. It may be necessary to cut short the negative tag of C20, or bend it down, to avoid shorting against the transformer. After assembly the wooden ends can be fixed in place with contact adhesive.

The specified selector switch has three 'ways', so an extra input can be added if desired. All that is necessary is to provide an extra DIN input socket and wire it as for the Radio input. If a sensitivity differing from 100 mV is required $\mathrm{R1}$ and R 2 can be altered appropriately.

## HEADPHONES

Headphones specifications tend to be rather confusing, as they are often specified as "suitable for $4 / 16 \mathrm{ohm}$ amplifiers" when the impedance of the phones themselves is usually much higher than 4 ohms. Most commercial hi-fi amplifiers feed the phones output through a high value series resistor,


Fig. 10: Altenuator circuit for use when 'Derby' is employed to drive power amplifiers. Take values of resistors from table below.

| AMPLIFIER | R29 | R30 |
| :---: | :---: | :---: |
| SENSITIVITY | R129 | R130 |
| 50 mV | $1 \mathrm{k} \Omega$ | $47 \Omega$ |
| 10 mV | $1 \mathrm{k} \Omega$ | $100 \Omega$ |
| 200 mV | $1 \mathrm{k} \Omega$ | $220 \Omega$ |
| 500 mV | $1 \mathrm{k} \Omega$ | $1 \mathrm{k} \Omega$ |
| 1 V | 0 | $1 \mathrm{k} \Omega$ |

to reduce the signal level to an acceptable level. This unit feeds the headphones direct and has a very low output impedance, giving good electrical damping. If the reader is in any doubt about the correct impedance of his headphones the best course it to measure the DC resistance with an ohmmeter. The impedance is not likely to be less than this figure.

## USE AS A PREAMPLIFIER

As stated earlier, this circuit will make a very satisfactory preamplifier. The output of $1 V$ is rather too high for most power amplifier modules, so it will be necessary to interpose an attenuator between the unit and the power amplifier. Suitable values for various amplifier sensitivities are given in Fig. 10. If the attenuator resistors are connected via a switched jack socket then the amplifiers will be automatically muted when the headphones are plugged in.


## Physical Features

Apart from the modulator itself, layout of the game is not critical; nevertheless constructors are strongly advised to use printed circuit boards due to the large number of integrated circuits. Mechanical construction of the prototype was kept as simple as possible. In many respects the single plane layout adopted proved to be ideal, allowing easy access to all the preset controls. Another advantage of the planar construction is that you can build the unit in stages without having to keep it inside its case-this is useful for carrying out tests and checking each board as you go along.

Six circuit boards are used, each secured to a sub-frame made of lengths of aluminium bar or extrusion; when completed this subframe is lowered inside a case. The only extra connections then required are to the front panel controls and the output points. The case was made from bent aluminium sheet carefully glued at the corners with an epoxy resin. The sloping front panel is hinged.

## M.J. HUGHES MA

The six boards are designated $A$ to $F$ and these are laid out on the sub frame as shown in Fig. 7. The mains transformer is bolted on to an aluminium plate shaped to screw under the longer struts of the subframe. When making the subframe ensure that you allow sufficient clearance between the aluminium struts so that there can be no chance of short circuits between them and the pcb tracks. (About ${ }_{3}$ in. clearance is allowed between the longer edges of each board and the copper to prevent such short circuits.)

Apart from Board $F$ each printed circuit has overall dimensions of $3^{3}{ }_{4} \mathrm{in}$. $\times 5^{1}{ }_{2}$ in. Board $F$ has a length of 3in. but it has the mains transformer alongside it. The overall length of your subframe should take into account the dimensions of the transformer used if different to that in the prototype. By making this subframe first you can get the system partly functioning at each stage. Make sure that there is at least one inch clearance between the underside of the circuit boards and the lowest points on the subframe. This is to prevent the modulator screening box,


Fig. 7 : Layout of printed circuit boards and mains transformer on the subframe. In the prototype
this was made from aluminium bar but any material of similar size may be used.
which is live, touching the bottom of the Tele Tennis final enclosure.

This month we shall describe the operation and construction of boards $E$ and $F$. If these are built first it is then possible to monitor the signals from other boards on your own television set-this obviates the need for an oscilloscope (although if you have one it would be most useful for setting up purposes!).

## Power Supplies

Three power rails are needed; a stabilised +5 V for the logic circuits, +12 V (nominal) for the Ball control ramp generators and +12 V (nominal) for the modulator. We have separated the latter two 12 V supplies with heavy decoupling to prevent hum on the RF carrier and to prevent the ball control ramps altering the supply level to the modulator. Apart from this heavy smoothing and decoupling it is not necessary to stabilise the 12 V rails.

The circuit for the power supply board is shown in Fig. 8. The stable 5 V rail is provided by a TO-3 encapsulated voltage regulator 7805 . Other similar devices could be used but some are prone to high frequency oscillation which could present problems. A. $1000 \mu \mathrm{~F}$ capacitor on board A provides LF decoupling, while $0 \cdot 1$ 's at various points on other boards reduce the chances of noise spiking from the TTL. The smoothing capacitors for the two 12 V rails are located on boards $D$ and $E$ respectively.

Layout is pretty straightforward but it is essential to heat-sink the voltage regulator with a piece of shaped aluminium sandwiched between the IC and the board. This heatsink can be live and there is thus no

## PCB functions

Board

## Function

A Time bases, Sync mixer, Ball generator, Ball vertical change control
B Left and Right Base generators, Bat width generators, Bat output
C Top and Bottom Base generators, Bat height and position generators
D Ball control ramp generators, Ball control logic, Service and Ball Boy control, Ball blanking
E Video mixer, Video blanking, Sync/Video mixer, UHF Modulator
F Power supply


Fig. 8: Power supply circuit diagram. Smoothing capacitors for the +15 V rails are mounted on Boards $D$ and $E$.


Fig. 9: Actual size layout of Board $F$ and location of componenis.


Fig. 10: Circuit diagram of the UHF modulator. Component relerences within the shaded area are those used by the kit suppliers and should not be confused with references in the rest of the project.
need for insulating mountings. Mount board $F$ and the transformer on to the subframe and check that the correct voltages are present. Do not worry if the 12 V rails are reading high (probably around 15 V ) because they are off load.

## Modulator

The next step is to assemble the modulator. The circuit is shown in Fig. 10 and we are indebted to Crotton Electronics for permission to publish it here. Provided the kit's instructions are carefully followed in every detail there are no major problems to be expected. Remember, though, to take care with the ceramic feedthrough capacitors and ensure that the strip inductors Lil and Litz are precisely cut and positioned. Mark and drill or cut holes in the uniform copper area of the Mixer/Modulator board so that the modulator will rest flush against the square copper land. Bolt the modulator case firmly into position under the board by means of the potentiometer bush, so that the control spindle and input and output connections all protrude through the plain side of the board.

Using a large soldering iron you should, eventually, run a fillet of solder between the tinned modulator case and the copper land to give extra mounting support. Before doing this, however, it is as well to test the modulator. Connect temporary leads between the +12 V and 0 V pins of the modulator
board and the corresponding points on board $F$ and fit the $2000 \mu \mathrm{~F}$ smoothing capacitor (C39) on board E. Set the tuning trimmer of the modulator and the modulation potentiometer to mid positions and connect the output socket of the modulator to the aerial socket of a 625 line standard television set via a short length of coaxial cable. Switch on the power and there should immediately be some indication on the television screen that something has happenedmaybe the screen will brighten up or blacken off.

Check that the supply voltage is now about +12 V and try adjusting the tuning of the television set. In the absence of any modulating signal there will be no picture as such, but it should be quite obvious that there is a carrier present as you tune through the range. By turning up the modulation control (turning anticlockwise) and touching the input pin with a finger you might be able to display a faint hum bar. At this stage it is sufficient to know that there is a carrier. You can now progress with the rest of board E.

## Video mixer

The circuit for the mixer stages is shown in Fig. 11. Diodes D17 and D23 in conjunction with R61 form a diode OR gate which assembles all the waveforms that define portions of the final picture. We call this stage the Video Mixer. The combined output of this stage is fed to the blanking circuit where the mixed


Fig. 11 : Circuit diagram of Board E. including Video Mixer, Blanking and Sync/Video Mixer.


Interior view of the prototype Tele-Tennis unit. The composite video outpul socket is not connected up.
sync (from board A) is ANDED with it by IC30a. This has the function of ensuring that no video signal is present during periods when we shall be adding the field and line sync pulses.

The next stage is to combine synchronisation pulses with blanked video. R62, R63 and R64 form an additive mixer for the two signal sources, whilst D24 clamps the tops of the sync pulses to ground. Therefore, whenever a sync pulse occurs this is added to the video in a negative going direction. The ratios of the resistors in this stage are important to ensure the correct proportions of video and sync.

Two outputs are provided from this point. The composite video signal can be taken straight to a monitor if required, however we expect that most constructors would not possess such an instrument, and in that case C37 and R65 can be omitted. The alternative is to feed the composite signal to the modulator input via C38. Make sure that you connect this capacitor with the correct polarity because the case of the modulator is connected to the positive rail.

Throughout this project we recommend that you use dual-in-line sockets for all the integrated circuits. Apart from allowing you to replace suspect devices you will protect the guarantee given by most reputable suppliers. Do NOT connect any of the power lines to the subframe as chassis grounds. There is only one connection to chassis and this is made on final assembly into the case.

## components list

| BOARD 'E' |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Resistors-all $\frac{1}{\text { a }}$ or $\frac{1}{4} \mathrm{~W}$ |  |  |  |  |  |
| R61 | $330 \Omega$ | R62 | 4700 | R6E | 33012 |
| R64 | 3308 | R65 | 33012 |  |  |
| Capacitors-all 25 V electrobtics |  |  |  |  |  |
| C36 | $47 \mu \mathrm{~F}$ | C37 | $100 \mu \mathrm{~F}$ | C38 | $47 \mu \mathrm{~F}$ |
| C39 | $2000 \mu \mathrm{~F}$ |  |  |  |  |
| Semicenductors D17-[24 1N914 IC30 S137400 |  |  |  |  |  |

## Miscellaneous

PCB; DIL14 IC sacket; 14 wiring pins; Modulator kit from Crofton Electronics, 15/17 Cambridge Road, Kingston-upon-Thames, Surrey K.T1 3NG, price $£ 7 \cdot 30$ including p.p. and VAT.

## Resistors

$$
\begin{array}{llll}
\text { R66 } & 12 \Omega & 5 W & \text { F67 63S } 1 \mathrm{~W} \\
\text { R63 } & 220 \Omega & \frac{1}{2} W &
\end{array}
$$

## Capacitor

C40 $3000 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolyt:-

## Semicanductors

D25-L28 1N4001 IC31-7.305 regulator

## Miscellaneous

T1 Pri: 240V, Sec: 12-15V $\frac{7}{3} A$; PCE; 6 wiring pins; material for heat-sink, transformer maunt and subframe.


Fig. 12: Aclual size layout of Board $E$ and location of components.



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## Mreilercope

## PART 6

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## POWER SUPPLIES

It is not intended in this section to go into all aspects of power supply theory as it is very involved and all manner of supplies are used in oscilloscopes. However we can take a general look at power supplies and some of the problems encountered.

## VALVE HEATERS

Valve heaters are usually wired in parallel, in groups of perhaps 5 or 6A maximum. Because of considerations of heater-cathode voltages some of the heater lines may be at certain potentials, e.g. 0 V , +100 V or -150 V etc. Perhaps the most obvious case of this is in the case of the CRT heater which must be at -1 or -2 kV . The bright up bistable is usually at EHT potential as would be the EHT series regulator if fitted. All these heaters would be run from one transformer winding and strapped to the negative EHT supply.

We shall shortly look at RF EHT generators which provide an output that is usually doubled or tripled to provide the 10 or 12 kV needed on a high voltage tube. If the tripler uses valves then the heaters are usually run from a winding on the EHT transformer. A failure of the EHT generator will therefore cause these valves not to light.
In order to prevent hum and drift the input valves to the Y amplifier are sometimes fed from a stabilised HT line in series. One open circuit heater will therefore cause the whole lot to go out. One further difficulty is that heater cathode shorts can put a few valves out without affecting the others, giving rise to very misleading faults. However this practice of series valves is limited to only a few valves in very complex oscilloscopes and is not uswally found in fairly simple ones.

Also supplied from a heater line is the graticule illumination, if fitted. This usually consists of a pair of small $6.3 \mathrm{~V}, 0 \cdot 1 \mathrm{~A}$ bulbs in parallel, fed from a 6.3 V line by a 100 ohm pot. This enables the illumination to be changed to suit the display intensity.

## HT SUPPLIES

The HT requirements of a small AC coupled scope may be quite modest and if no accurate calibration is intended the power supply can follow normal radio practice, i.e, a full wave rectifier and simple smoothing. Both metal and valve rectifiers are used but care should be taken when replacing a valve with a couple of BY127's, as is often done for economy in the event
of a failure having occurred. In general it is very bad practice as the HT comes on straight away and decoupling capacitors can short circuit through overvoltage and electrolytics can blow up making a mess when they do so and that can be dangerous so always replace a valve with a valve, or provide a thermal switch to put the HT on after 30 scconds or so.

This is the method incorporated in several large oscilloscopes where valve rectifiers would waste too much power. A small thromal switch puts $6 \cdot 3 \mathrm{~V}$ on to a relay after 30 scrouds or so. The relay flips over and connects the HT windings to their rectifiers as well as providing a "holding" current for the relay and taking the supply off the terminal switch which cools down. If there is a small power break the relay loses its holding current and the HT cannot be reconnected until the thermal switch has heated up again. This protection can be extended to switch off the HT in the event of a plug-in unit being removed and another inserted, HT taking another 30 seconds to come on.


Fig. 1. Circuit requirements for a series slabilised HT hine.
If some valve heaters are run from the HT line then there is also a delay while these warm up. In general this type of scope takes about 5 minutes to switch on and sort itself out, but the advantage of circuit protection is well worth the operating delay.

In most oscilloscopes some or all of the HT lines are stabilised. Because the HT load is predictable (except under fault conditions) the series stabiliser can be arranged to stabilise with little loss of power.

Fig. 1 shows the general arrangement of this type of stabiliser. $R_{3}$ can be made such that the power dissipation in the stabiliser valve is kept to a reasonble level, whilst maintaining adequate stabilisation. The comparator, usually a long-tailed pair, senses the difference in potential between the points $A$ and $B$ and drives the series element so as to correct the difference. The ratio R1/R2 sets the output voltage and R1 is usually made preset so that the HT rail can be accurately set to its prescribed value.


Fig. 2. Method of obtaining EHT for a small CRT using a standard mains transformer.

The circuit also has a hum reducing action in that no hum exists at point $A$ (set by VR1) and so the comparator "makes sure" that no hum exists at point B. Hum can be injected into the comparator as well to give virtually perfect DC (ripple less than 25 mV ) with a ripple input of several volts. The series element is usually a power pentode or triode. If the current demand is large several valves may be placed in parallel to meet the current requirements.

If more than one $H T$ line is required to be stabilised it is usual to make a very good job of stabilising one of the lightly loaded lines and to use this to stabilise all higher voltage lines. A typical oscilloscope would usually have HT rails at -150 , $+150,+400 \mathrm{~V}$ to cover the requirements of the Y amplifier and timebase.


Fig. 3. Development of the voltage multiplier to produce $2 k V$.

EHT can be derived from one winding of the mains transformer at full voltage (say 1.5 kV ) and rectified and smoothed. If the oscilloscope is calibrated then the EHT must be regulated and a small series pentode is generally used for this purpose. The provision of a 1.5 kV winding on a mains transformer is difficult and expensive (also lethal if you happen to get hold of it!) and so many scopes use voltage multiplication from a low voltage winding, followed by a series regulator if necessary.

Fig. 2 shows how 700 V can be obtained from the 350-0-350 mains transformer of a small oscilloscope and Fig. 3 shows how the idea is extended to give 2 kV from 500 V . The Solartron D1400 used this principle to produce nearly $1 \cdot 5 \mathrm{kV}$ from a 140 V transformer winding.

These methods of deriving HT from a mains transformer are satisfactory up to a few kV but when 8 or 10 kV is needed RF supplies are usually employed. These have the advantage that the supply can be self stabilising, can supply all the EHT supplies, operates at a high frequency and so does not need bulky smoothing capacitors and is fairly harmless in the event of accidents. Fig. 4 shows a block diagram of a typical form of this type of generator. The oscillator is self-oscillating by virtue of positive feedback from the transformer (a small winding feeding the output valve grid). The comparator provides an error signal to maintain the potential at point $A$ as it should be, obviating any changes in the cathode supply. The PDA supply tends also to be stabilised but not so well, but is in any case not so important.


Fig. 4. Block diagram of RF generator producing 8 to 10 kV .
The oscillator is tuned by a capacitor across the anode transformer winding and normally runs at 25 to 30 kHz . The transformer is usually a ferrite toroid for high efficiency with the windings on polythene bobbins. As we have already mentioned, there are also windings for the voltage multiplier valve heaters if fitted. The whole EHT unit is usually isolated in a small compartment and the supply leads decoupled to prevent RF appearing everywhere. It is advisable to keep dust and damp out of this compartment and vulnerable points are usually given a coat of shellac during manufacture. Any damp might cause tracking which can cause a surprising amount of damage. In damp environments it is perhaps useful to place a small bag of silica gel in the compartment to keep the area as dry as possible.

When setting the EHT voltage with the "SET EHT PRESET" it is as well not to go over the voltage prescribed as this overruns the output valves, overruns the multiplier heaters and puts a strain on the insulation and the CR'T. Any repairs in the EHT unit must

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be done with neat. round soldered joints to prevent corona discharge which produces ozone which destroys the insulators. It is also important to replace all screcning and earth braidings. Spark gaps are often provided, especially in equipment with transistors, to break down wheu excess voltages occur, preventing damage to other parts of the circuit and they should be kept free of dirt otherwise they will flash over for no apparent reason.

The EHT generator is usually supplied from the highest available voltage rail in the oscilloscone and the supply line is very well decoupled. The current taken is usually only about 50 or 60 mA and so represents a light load on the line.

Taking into account the overall power requirements of a complete oscilloscope the mains transformer is physically rather large (weight perhaps 10 or 151b) and tends to produce a large magnetic field. In order to guard against this field and external magnetic fields the CRT is enclosed in a Mumetal shield which acts as magnetic screen. The excellent screening properties of Mumetal make it possible to mount the transformer fairly near to the tube without ill effects. When removing a CRT it is important not to bend the Mumetal as it loses its properties if bent and replacement shields are expensive. The Mumetal is also carthed to prevent external electric fields penetrating the tube and causing deflection.

The internal layout of the oscilloscope is to a greal extent governed by thermal considerations. For example the $X$ and $Y$ oulput stages and the power supply regulator valves are situated so that they can lose their heat easily. Small signal stages can be tucked away in any odd corners without coming to much harm. Power valves are always operated vertically for maximum reliability as the grids may sag when used horizontally. This should be borne in mind if the scope is run on its side for long periods during calibration etc.

Signal leads also play a part in dictating the layout in that signal-carrying leads are kept as short as possible to reduce capacitance and stray pick-up. When undertaking any modifications on oscilloscopes it is important to bear the above facts in mind as re. gards positioning of any extra stages or wiring.

## GENERAL MAINTENANCE

Apart from recalibration. say every 6 months, or if obviously needed, an oscilloscope needs additional care and attention. The heat generaled causes dirt and dust to stick and if a fan is fitted this makes matters worse. When used in a dusty environment it is as well to keep the oscilloscope covered with a plastic sheet to keep out unnccessary dust. However when the scope is in use there is litile that can he done because to obstruct the dust is to obstruct the


The EHT section of an oscllloscope. the rectifier valves heaters being fed from individual windings on the transformer.

## COOLING

Large oscilloscopes usually have a fan at the back to keep the scope cool and the field from the fan motor is such that a piece of Mumetal is offen needed around the motor. This should always be replaced when servicing of the motor is completed. The danger of an excessive rise in internal temperature is so great in some scopes that a thermal cut-out is incorporated to switch off the HT', but leave the fan running if the temperature should become too high. Clogged air filters can cause this to hippen and it should not be ignored because all manner of awkward faults can be brought on by excessive temperatures.
airflow necessary to matitain a safe working 1 cm perature.
The author used to think that a scope could not be cleaned and pampered too much but is now a bit wiser! When cleaning out dust with a small brusli connections become distodged and dust gets into switches and controls. So it is best to keep the number of "spring cleans" to ats few as are really necessary and to allow a bit of time for fault finding afterwards. But do not be put off-the resull of a clean scope is a more reliable scope that is much easier to work on when it does break down.

For general chassis cleaning a brush round with a $l^{\prime \prime}$ paint brush is usually aldeguate unless the dirt is greasy when the chassis may be rubbed down with a
rag soaked in acetone or carbon tetrachloride. it is important not to disturb any preset pots or trimmers, especially in the distributed amplifier and attenuator and in the timebasc. The EHT generator whether RF or from the mains should be kept clean as the dust builds up quickly in this area and also can do the most damage. Oil from leaking EHT capacitors also aggravates the situation but a cloth soaked in acetone. will probably clear up the mess.

## CONTROLS

Controls quite naturally come in for a lot of hard wear and pots and switches tend to become erratic. A gentle squirt of "SERVISOL" aerosol will sort out most problems. It is important not to spray too much as it can make rather a mess. Beware of the cheaper brands, they dissolve plastic switch parts in a flash, leaving a gooey mess in place of the switch! When potentiometers become noisy or erratic in operation a gentle squirt of "SERVISOL" on the track will probably effect a lasting cure. Some spurious effects can be traced to the spindle bearing and a gentle squirt here may well help, but it is important not to get the fluid on to the front panel as it can make rather a mess and dissolve some types of lettering.

Input sockets (especially the UHF83) sometimes need tightening to ensure reliable contact but it is necessary to be careful not to cause too great a deformation especially with the BNC sockets which are quite fragilc. Oscilloscopes equipped with plug-in units often need a Jittle lubrication on their runners and it is advisable to keep the rear connector clean otherwise erratic operation will result. One point often overlooked is that power valves (regulator, $\mathbf{X}$ and $Y$ outputs and EHT generator) when they are greasy suffer a much higher running temperature due to lack of cooling. It is a good idea to keep all valves clean and polished and to give the base a tiny squirt of "SERVISOL" before replacing the valve. Several oscilloscopes place the EHT generator valves in screening cans (to prevent radiation) and if these fill up with dust, as often happens, the valve tends to run scorching hot with the possibility of early failure.

## SERVICING

With regard to the electronics there is little that can be done in the way of maintenance on a regular basis, it being necessary to wait for faults to occur before they can be rectified. Fortunately the majority of oscilloscopes are constructed to be as reliable as possible for the price and consequently the fault rate is low. Most faults can be found with a multimeter and a signal source applicd to the scope. When found the faults usually turn out to be due to faulty valves, faulty rectifiers, open circuit or "high" resistors or short circuited capacitors. When making replacements it is important to keep to a high standard of workmanship and to use good quality components of adequate rating.

## COMPONENT REPLACEMENT

A word is perhaps of use here concerning the AC qualities of resistors. The reactances of resistors becomes important at high frequencies in critical cir-
cuits, such as the Y amplifier and timebase. The standard carbon rod type of resistor, usually $10 \%$ tolerance at best, is perbaps one of the best types with regard to its AC performance. Its inductance is zero and the capacitance is usually less than 1 pF . Metal film resistors are also as good in this respect and are available in a wide range of ratings and with tolerances as close as $0.5 \%$ if necessary. Other types of carbon resistor although of high reliability may have quite significant inductance and also fairly high self-capacitance. Wirewound resistors are absolutely useless in such applications and should only be used where they are well decoupled and their reactance of no consequence.

In general it is best to replace any components by identical types, which can be ordered from the scope manufacturer if necessary. Replacement component tolerances should be better or the same as the item they replace. Servicing of oscilloscopes, particularly by their owner, rarely creates any problems as the circuits are well defined in their operation and the layout in the majority of cases is intended to aid servicing.

## To be continued

## TELE-TENNIS

-continued from page 338
The reason for making an issue over grounding is that the Crofton modulator has inverted supply rails, i.e. its case is at +12 V , whereas we shall ultimately be making our system ground OV. Do not under any circumstances let the case of the modulator come into contact with other metal work or you will put a dead short across the power supply. It is best to cover all exposed metal work of the modulator's case with a couple of layers of PVC tape.

When Board $E$ is complete it can be screwed to the subframe alongside the power supply board and the supply leads wired in. Apply power and check that a carrier is present by watching the television screen. If you have a signal generator (you can make a simple one from a standard multivibrator circuit) giving outputs of up to 5 V you can inject a $15 \cdot 625 \mathrm{kHz}$ signal into the mixed sync input. Turn up the brightness of the television set and you shouldif the set is in tune-sec a dark band running down the left hand side of the screen. Adjust the tuning for maximum signal-it is easier to adjust the set rather than the modulator-and then see the effect of varying the modulation level. Alternatively injecting a 50 Hz square wave into the same point should produce a dark horizontal band running across the screen. The signal generator will need fine adjustment to obtain precise field or line lock. A square wave having a frequency between 50 Hz and a few hundred kilohertz connected to the inputs of diodes D17 to D23 should cause a random array of white dots to appear on the face of the television set. Further tests must wait until we have produced a correctly generated set of field and line sync pulses. This we shall do next month when we describe the circuitry and construction of boards A and B.

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18 ： 18 wat
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BDI Kit
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2025TC
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$13 i n \times 8 i n$ Bass unit
15 wate 8 ohm
Gin $\times 5$ in 5 watt $3, A$ or 15 hm
$\sin \times \sin 10$ watt Dualcone 8 ohm
$6 \frac{1}{2} 10$ watt 8 ohm
8 in 10 watt 8 ohm
480． 50
880.50
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c106．95
612.95 69.00 611.00

12 in 20 watt 8 ohm
Fane $\sin 4$ ohm
E2 25 NT5 E
Fane in $\times 4$ in 3 or 8 ohm $\& 120$ N75－E） 2
Celestion 8 in 15 ohm
Elac Bin 8 ohm Dualcone
Elac 10 in 日 ohm Dualcone
Goodman 6 tin 8 ohm
Dualcone
Baker Group 25 12in 8 or
15 ohm
Adastra＇Top 20＇ 12 in
25 watt 8 or 15 ohm Adastra＇Hi－Ten＇ 10 in
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14 in $\times 12 i^{\prime \prime} \times 9 i n$
（ $8 \times 5,8^{\prime \prime}, 5 \frac{1}{\frac{1}{2}}$ \＆ $\left.8 \frac{1^{\prime \prime}}{4^{\prime}}\right)$
$18 \operatorname{in} \times 1 \operatorname{lin} \times 9$ in
$\left(8^{\prime \prime} \times 2^{\prime \prime}\right.$ or $13 \times 8$ ）
22 in $\times 14$ in $\times 9$ in

## 

TWEETERS \＆CROSS
EMI 3⿺𠃊⿳亠丷厂 8 ohm
Cone Tweeter 10 watt
8 or 15 ohm（K2006）
Cone Tweeter 3 watt
80 hm （K2003）
Horn Tweeter 8 ohm （K2007）
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2－way Crossovers（CN23 CN28，CN216）
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CARTRIDGES
Acos ${ }_{\text {GPI／25C or } 35 C}$ GP93／1
GP94／I
GP96／1
GPIOI
GPIOA
BSR
5C6M
$5 \times 6 \mathrm{M}$
$5 \times 6 \mathrm{H}$
$\times 5 \mathrm{M}$
$\times 5 \mathrm{H}$
Sonotone
9 TAHC（Diamond）
9TAHC／G（Diamond）
Double Diamond Stylii
for above
Goldring
G850 Cartridge
G800
G800E
Audio Teenica AT55
Empire 999 REX
STYLII for
G850／G800／G800H
CC90／7
G800E
CS91／E
AT66
N44－5
N44－7

C3． 75
N75／6
MICROPHONES
UDI 30 50K／600 ohm
uni－dir．ball metal
UDI47
Condenser Mic． 600 ohm uni－dir
Cassette Stick Mic．with R／Conerol
Mic－Mixers Mono／stereo
AKAI ADMI 4
HEADPHONES
Rotel
RH430
RH 630
RH 700
Akai ASE 11
Akai A5E20
Koss
KRO71I
K6
K6LC
K 0727 B
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HVI
PRO4AA
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| A |  |  |  |
| :---: | :---: | :---: | :---: |
|  | Stnd． | L／P | D／P |
| 5＂ | 55p | 69p | 90p |
| 53＂ | 69p | 88p | $1 \cdot 25 p$ |
| 7＂ | 88p | 1－20p | $1.60 p$ |
| High frequency |  |  |  |
| 5 ＇ | － | 1．40p | 1．55p |
| 7＂ |  | $1.90 p$ | $2.95 p$ |

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IF you are a conscientious constructor, you would not be I able to get very far without getting frustrated by the need for a multi-range meter. It is almost as essential as a speedometer to a motorist. Without one, how can you locate fault conditions, or check component values.

Practical Wireless recently published an article on this subject, illustrating examples of well known types. When looking around to buy a multimeter what should you look for? Well this will depend to some extent on the usage expected of it. There are meters renowned for robustness and the ability to withstand fairly rough handling. There are those that have a high sensitivity, or an extended voltage range, or built-in capacitance meter. Good ones are not cheap to buy, but this does not mean that cheap ones are not worth having.
.There has been a recent introduction of some Italian instruments into the U.K. which are certainly worth looking

## MANUFACTURER'S SPECIFICATION

Sensitivity
Accuracy
Bandwidth
Dimensions
Weight
Power requirements
A.C. \& D.C. $40 \mathrm{k} \Omega / \mathrm{V}$
D.C. $\pm 2.5 \%$ Ohms $\pm 2 \%$

20 Hz to 10 kHz
$156 \times 100 \times 40 \mathrm{~mm}$
650 grammes
Internal, $2 \times 1.5 \mathrm{~V}$ HP7 or similar) $1 \times 22.5$ (B 122 or similar) for resistance. External, $220-240 \mathrm{~V} 50 \mathrm{~Hz}$ for capacitance and frequency only.

## RANGES

| Volts |  |
| :---: | :---: |
| D.C. | A.C. |
| $0-420 \mathrm{mV}$ | $0-3 \mathrm{~V}$ |
| 0-1.2V | 0-12V |
| 0.3 .0 V | $0-30 \mathrm{~V}$ |
| 0-12V | $0-120 \mathrm{~V}$ |
| $0-30 \mathrm{~V}$ | $0-300 \mathrm{~V}$ |
| $0-120 \mathrm{~V}$ | 0-1,200V |
| $0-300 \mathrm{~V}$ |  |
| $0.1,200 \mathrm{~V}$ |  |


| Current |  |
| :--- | :---: |
| D.C. | A.C. |
| $0-30 \mu \mathrm{~A}$ | $0-3 \cdot 0 \mathrm{~mA}$ |
| $0-300 \mu \mathrm{~A}$ | $0-30 \mathrm{~mA}$ |
| $0-3 \mathrm{~mA}$ | $0-0.3 \mathrm{~A}$ |
| $0-30 \mathrm{~mA}$ | $0-3.0 \mathrm{~A}$ |
| $0-0.3 \mathrm{~A}$ |  |
| $0-3.0 \mathrm{~A}$ |  |
|  |  |

## GOING BACK... <br>  <br> COLIN RICHES

THIRTY-FIVE years ago this year the Zenith TransOceanic was born.
Over the years new knowledge and improved technology have gone into successive improved versions. The latest-the TransOceanic Royal D-7000Y - is equipped to tune to 11 wave bands. (1) a.m., $540-166 \mathrm{MHz}$, (2) f.m., $\quad 88-108 \mathrm{MHz}$, (3) l.w., $150-$ 400 kHz , (4) s.w., $1 \cdot 6-3 \cdot 5 \mathrm{MHz}$, (5) $3 \cdot 5-90 \mathrm{MHz}$, (6) $9 \cdot 4-10 \cdot 1 \mathrm{MHz}$, (7) $11 \cdot 4-12 \cdot 33 \mathrm{MHz}$, (8) $14 \cdot 6-15 \cdot 8 \mathrm{MHz}$, (9) $17 \cdot 1-18 \cdot 5 \mathrm{MHz}, \quad(10) \quad 20 \cdot 6-$ $22 \cdot 4 \mathrm{MHz}$ and (11) $161-164 \mathrm{MHz}$.

It is designed and treated to operate in extreme climatic conditions, and incorporates r.f. gain control, b.f.o., vernier tuning and battery level meter, illuminated dial and chart panel, telescopic aerial and personal earphone. Navigational benefits include a time zone indicator, logging scale and azimuth compass. A swivel base platform can be supplied to aid directional tuning. It operates on 9 standard U2 type batteries but also has a built-in a.c. power
supply for either 115 V or 230 V a.c.

The Trans Oceanic theory was developed into practice in 1939, when Commander E.F. McDonald (Zenith's late founder-president), having asked the company's engineering department to produce a shortwave battery operated radio, found that he could sit in his Canadian fishing lodge and pick up both the weather forecast from Ohio and broadcasts from London.

After a combination broadcast and shortwave receiver with broad bandspread for easier tuning had been produced, McDonald took one to Northern Canada and sent another to Commander Donald B. McMillan in the Arctic. McMillan tested it on Baffin Island, and then further north on Ellesmere and Greenland. Finding it fully satisfactory, he radioed McDonald to express his approval.

When some further 20 experimental models had been tested and subsequent modifications


Experimental S.W. transmission with singing Eskimos (1925). Zenith's founder-president Commander McDonald is standing on the right.


An early "mobile" Trans-Oceanic
adapted, the set went into production several months before the Zenith factory was converted for the war effort in 1941. At that stage 100,000 Trans-Oceanic radios were on the order books, and though many of these were never completed, several thousand had been by the time the US entered the war. Members of the allied forces were frequently comforted throughout the duration of the war by broadcasts from their native countries, the radio set often being their only link with home.

About his Trans-Oceanic radio, a British army officer wrote,


First multioand recemer made in 1941
"During the whole war, it was either with me or close behind with my luggage. Besides being under enemy fire, it has stood in the open in blistering heat and sandstorms, likewise in monsoon rain and snow. I have watched it dropped into cargo holds by coolies and have sympathised with it after suffering a kick by a donkey. In, spite of such treatment, there has been no occasion during its ten years life that the set has failed to work."

Since introduction in 1941, a number of major improvements have taken place. Announced to yachtsmen in 1951, as a "king-size

[^7]SPECIAL PRODUCT REPORT-continued from page 348
appropriate range multiplication factors. The $30 \mu \mathrm{~A}$ range enables low leakage currents to be detected, whilst the 3 amp range is useful for average thyristor d.c. load measurement.
The voltage ranges are divided into two scales- 0 to 12 and 0 to 30 with appropriate multipliers. The advantage of using two scales is to maintain average meter indications between a half and full scale deflection, usually recommended for most measurements on load, without having to interpolate at the low end of the scale. The $1,200 \mathrm{~V}$ ranges will cope with most applications except e.h.t. for cathode ray tubes; the optional extra probe will extend this range to 30 kV d.c., sufficient for most oscilloscope or television c.r.t.s., for an additional $£ 7 \cdot 27$ plus VAT.

The resistance ranges are from 0 to $2 \mathrm{k} \Omega$ (useful readings) on a $20 \mathrm{k} \Omega$ scale, up to 0 to $20 \mathrm{M} \Omega$ (useful readings) on a $200 \mathrm{M} \Omega$ scale. This will cater for a very wide range of measurements from 1 ohm to $20 \mathrm{M} \Omega$ d.c. but does not, as is usual, mean that "cold insulation" tests on capacitors or wiring will necessarily give reliable results.
Two 1.5 V batteries have to be fitted to give the low resistance ranges and one 22.5 V battery for the high resistance ranges.
Decibel measurements are based on the standard $0 \mathrm{~dB}=$ ImW in 600 ohms, or 0.775 V a.c., using the a.c. voltage circuit for measurements ranging from -10 to +63 dB .

Using an interpolation scale in the instructions an indication of frequency is possible based on the use of the capacitance circuit and, in the case of the X100 range, it depends on an external accurate $4,700 \mathrm{pF}$ capacitor being applied. Both the frequency and capacitance ranges require this instrument to be connected to an accurate 50 Hz mains supply of 220 to 240 V for which a lead is provided. The meter uses a resistance measurement circuit to determine reactance, and hence interprets the result as a direct capacitance reading up to a maximum $0.5 \mu \mathrm{~F}$. For most purposes the $10,000 \mu \mathrm{~F}$ "ballistic capacitance" range is likely to be the maximum required, and this is achieved by interpolation of the d.c. AV scale using the chart given in the instructions.

The optional extra U.S.I. (Universal Signal Injector) is virtually a square wave signal generator using two transistors and mounted inside a "pen" type tube with a 1.5 V battery. It provides a 1 kHz "pulse" waveform from a blocking oscillator suitable for signal tracing and fault finding procedures in a wide range of radio, audio and TV equipment. The probe is claimed to withstand, on test, 500 V d.c. and provide. 20 V peak-to-peak output.

In the event of repairs being needed, the manufacturers have appointed Coates-Clarke (Services) Ltd., of 110a St. Margarets Road, Hanwell, London W.7. to carry out this service.
*Chinaglia (UK) Ltd., 19 Mulberry Walk, London SW3 6DZ

## GOING BACK

-continued from page 349
aspirin for the headaches of amateur sailors" and "the world's newest aid to navigation," the new Trans-Oceanic had had added to it two new continuous tuning bands that covered the entire 38 to 150 metre band, ( 2 to 8 MHz ).

In 1954 another new version of the Trans-Oceanic was introduced and included a ferrite rod aerial which, in conjunction with new circuits, was said to "treble the range" for standard broadcast reception. Other additions included a horizontal slide-rule type tuning dial. Push-button band selection and a reel-away take-up on the power control. Inside the set's cover were located a series of flip charts, a world-wide time map and listings for all major short-wave stations.

McDonald's next challenge to his company engineers was to develop a transistorised TransOceanic portable radio that would "equal or better the performance" of the valved version. Compactness was his stipulation to the engineers. Whether for yachts or expeditions, it was paramount that weight and bulk size was kept to a minimum but without the sacrifice of performance. There was not to be room for a teaspoon of sugar, or the engineers "would get it back." After three years of research and development Zenith announced "the world's first all-transistor band-spread short wave portable radio" in 1957.


The 1974 version of the Trans-Oceanic. Recommended retail price is $£ 247 \cdot 50$ inc. VAT.

Components and circuitry were built into a case measuring $10{ }_{4} \times$ $12^{1}{ }_{2} \times 4^{7}{ }_{8}$ in representing a major achievement in miniaturisation and space efficiency. It included a new rotary band switch and associated circuits for electrical band-spread tuning which occupied a fraction of the space required in valved short wave sets. The band selector switch rotated a "rolling pin" dial scale so that only one tuning band was visible at a time.
"The ultimate in personal radios" was announced in 1962this was a 9-band Trans-Oceanic, the Royal 3000. This transistorised receiver combined super. lative performance and virtually
"drift-free" tuning of the f.m. broadcast band with new sensitivity on short wave, long wave and standard broadcast bands. It was similar to the previous model but less the 13 metre band and plus the f.m. broadcast band ( 88 to 108 MHz ).

August 1964 saw the one millionth Trans-Oceanic portable radio roll off the Zenith production line.

In 1968 the Trans-Oceanic was again altered quite significantly with the addition of the wave bands. The Royal 7000, as the new model was called, featured 11 bands and incorporated a v.h.f. fixed crystal U.S. "weather" band at $162 \cdot 55 \mathrm{MHz}$. The set was tuned to the weather position to hear up-to-the-minute weather reports. The second band addition was short wave (a division of the earlier $2-9 \mathrm{MHz}$ spread), making a total of seven short wave bands, long wave, f.m. a.m. and weather band. Other improvements in the Royal 7000 included a b.f.o. and manual r.f. gain controls.

In 1971, the Royal 7000 was further refined with replaceable crystals for the weather band, enabling the listener to receive weather stations assigned to frequencies other than the common $162 \cdot 55 \mathrm{MHz}$ (U.S.), in 1972 the Royal D-7000Y was improved again with the addition of the adjustable weather band and minor cabinet changes. The 1974 version is shown in our picture.

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H3s $100 \begin{gathered}\text { Mixed Diodes, Germ, } \\ \text { Gold bonded. etc. } \\ \text { Marked and Unarked. }\end{gathered} \quad$ 55p
H3: $30 \begin{aligned} & \text { Short lead Transistors, } \\ & \text { NPN Silicon Planar types }\end{aligned} 55 \mathrm{p}$
H39 $6 \begin{aligned} & \text { integrated Circults. } \\ & 4 \text { Gates } \\ & \text { BMC } \\ & \text { a }\end{aligned}$ FGates BMC 962, 2 Flip Flops BMC 945
H41 2 Sill Power transistors
H63 $4{ }^{2 N 3055}$ type NPN Sil. power transistors. Below
NBA $4 \begin{aligned} & \text { 38ec. N Channel FETs } \\ & \text { 2N3B19 in plastic case }\end{aligned}$
Untested Paks

| $\mathrm{Br}_{1}$ | 50 | Germanium Transistors PNP, AF and RF | 55p |
| :---: | :---: | :---: | :---: |
| вы | 150 | Germanium Diodes Min. glass type | 55p |
| ${ }^{38}$ | 200 | Transistors, manufacturers reiects, AF, RF, SII. and Germ. | $55 p$ |
| 834 | 100 | Sllicon Diodes DO-7 glass equiv. to OA200, $\mathbf{O A} 202$ | 55p |
| в 6 | 100 | Sil. Diodes sub. min. IN914 and IN916 types IN914 and IN916 types | 55p |
| H34 | 15 | Power Transistors, PNP. Germ. NPN Silicon TO-3 Can. | 55p |
| H67 | 10 | 3819N Channel FETs plastic case type | 5 p |

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$\begin{array}{lll}0-50 \mathrm{HA} & 0.5 & 0-10 \mathrm{~mA} \\ 0-50 \mathrm{~mA}\end{array}$
$\begin{array}{lll}0.505 & 0-106 \mathrm{~mA} \\ \text { a-500 111A } & 0.5 & 0-500 \mathrm{~mA}\end{array}$


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| 1 | 103 | 3.08 |
| 2 | 104 | 4.29 |
| 3 | 105 | 6.77 |
| 4 | 106 | 7.48 |
| 4 | 107 | 11.00 |
| 8 | 118 | 1418 |
| 10 | 119 | 17.60 |

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| $0_{0} 015-20$ | 0．13－20 | 10 mon | 1000） | 206 | 8.80 | 038 |
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| 0.5 | 124 | $2 \cdot 10$ | $0 \cdot 38$ |
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12 \＆ 24 Volts Prim．200－240v

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## SHORT WAVE DX by MALCOLM CONNAH

A'Radio Australia Listeners' Club Group' has been formed by George Hewlett of 22 Park Hill Road, Torquay, Devon and Miriam Bryant of 2 Broad Street, St. Columb, Cornwall. The club is not only for members of the official Listeners' Club but for anyone interested in listening to Radio Australia.

Although the club will mainly serve the South West of England the founders are prepared to answer any queries about the reception of Radio Australia. They would appreciate a stamped addressed envelope with any query requiring an answer.

## Readers' Logs

The first two logs this month come from the husband and wife team of Douglas and Rita Malpus from Cumberland. Douglas uses a 5 valve domestic receiver and a 25 foot end-fed antenna, which is often used at an alternative address in Scotland. Rita uses a Ferguson-Caravelle Transportable with a 120 feet long-wire and ATU. The results achieved were as follows.

## Douglas Malpus

6205 R. North Sea International at 1900.
9670 IBRA Radio noted at 2100.
11775 R. Nacional D'Espana at 1715.
15185 R. Finland noted at 1820.
15295 ORTF, Paris, France at 1110.
15305 SBC, Berne, Switzerland at 1100 .
15415 R. Kuwait noted at 1850.
15440 WYFR, USA noted at 2230.
17770 Radio Sweden at 1400.
17885 HCJB, Quito, Ecuador at 2130.
Rita M. Malpus
9525 AIR, General Overseas Service at 2020.
9535 SBC, Berne, Switzerland at 2200.
9650 Deutsche Welle, Cologne at 2145.
9690 R. Bucharest, Rumania at 1315.
9833 R. Budapest, Hungary noted at 2230.
9750 R. Vilnius, Lithuania at 2230.
11810 V. of Turkey, Ankara noted at 2230.
15185 R. Finland noted at 2030.
Christopher L. Hodgson of Sunderland used his

Codar MultiBand 6 with a 50 foot end-fed, 9 metre inverted vee and an ATU to hear:
9455 Radio Pyongyang noted at 2015.
9540 Radio Australia, S/on at 1800.
9695 Trans World Radio, Monte Carlo at 0820.
11720 R. Nacional, Brazilia at 2315.
11905 UN Radio, Greenville at 2205.
15084 R. Tehran, Iran in Farsi at 1030.
15310 BBC, Far East Relay (Malaysia) at 1530.
15410 UN Radio, Greenville at 1625.
15570 Radio Pakistan, S/on at 1530.
17820 Radio Canada Int. in Czech. at 1715.
17885 BBC, Cyprus relay at 1155.
21685 Radio Kuwait, S/off in Arabic at 1505.
William F. Kitching of Telford in Shropshire has a Grundig Satellit 2000 receiver and using only the telescopic aerial he heard the following:
3980 VOA, Munich noted at 2100.
3985 SBC, Berne, Switzerland at 0700.
6015 ORTF, Paris, France noted at 0515.
11730 Radio Nederland, Bonaire relay at 0630.
15012 Voice of Vietnam at 1800.
15195 R. Afghanistan noted at 1130.
17855 NHK, Radio Japan at 0900.
21535 RSA, South Africa noted at 1500.
21655 R. Norway (Sundays) at 1400.
21740 VOA, Greenville at 1700.
25790 RSA, South Africa noted at 1330.
Albert E. Ord of South Shields again used his Trio 9R59DS with a Joystick antenna and Hamgear preselector the log for this month including:
3905 AIR, India in English at 2330.
4955 R. Nacional, Colombia in Spanish at 0530.
5990 HCJB, Quito, Ecuador in English at 0645.
9410 R. Pyongyang in English at 2140.
9570 R. Australia noted at 0800.
9620 S.O.D.R.E., Uruguay in Spanish at 2200.
11775 R. Bucharest in English at 0430.
11780 R. New Zealand heard at 0730.
11825 V. of Free China, Taiwan, English at 1930.
15415 R. Kuwait, Pop Music at 1945.
17755 HCJB, Quito, Ecuador in English at 1900.
21540 R. Ghana heard in English at 1500.
Trevor Bland of Lea, near Gainsborough in Lincolnshire, used his Telton TF-182 to log the following:
5960 R. Canada Int. in English at 1030.
6030 AFRTS, Washington in English at 0130.
6040 VOA, Washington in English at 1935.
7280 R. Moscow in English at 2025.
9022 R. Tehran, Iran in English at 2005.
9585 R. Finland in English at 2030.
9625 R. Canada Int. in English at 2400.
11815 TWR, Bonaire relay in English at 0100.
15385 R. Nacional, Brazil in English at 2015.
15430 AFRTS, Washington in English at 1730.
17880 HCJB, Quito, Ecuador in English at 2015.


MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

NTICHOLAS Taylor who lives at Sunbury-onThames does his medium wave DXing with an Ultra 4175 receiver and a medium wave loop antenna. Local radio stations logged include IBA London on 719 kHz ; BBC Radio Blackburn on 854 kHz ; Solent on 998 kHz ; Medway on 1034 kHz ; Leeds on 1106 kHz ; Derby on 1115 kHz ; London on 1457 kHz ; Brighton on 1484 kHz ; Nottingham on 1520 kHz ; Bristol on 1546 kHz . Nicholas has been hunting-out the stations on the American Forces Network in West Germany and he reports hearing AFN Frankfurt on 872 kHz ; Berlin on 935 kHz ; Munich on 1106 kHz ; Stuttgart on 1142 kHz ; Heidelberg on 1304 kHz ; Augsburg on 1394 kHz and low power relays on 611 kHz and 1502 kHz . Karlsruhe on 1034 kHz is another outlet to look for. The Armed Forces Radio and Television Service (AFRTS) operates in many countries other than Germany. Stations heard occasionally in the UK are Keflavik, Iceland on 1484 kHz ; Lajes, Azores on 1500 kHz ; Kenitra, Morocco also on 1484 kHz and Athens, Greece on 1594 kHz .

Kevin Peel (Hornchurch, Essex) has been busy with his Astrad receiver and 100 ft outdoor aerial. He reports hearing BBC Radio Derby on 1115kHz; AFN Munich on 1106 kHz ; AFN Stuttgart 1142 kHz and the 1000 kW station at Cluj in Romania on 1151 kHz . During the summer months Cluj along with Lugof on 755 kHz carry a multi-lingual programme for
tourists at 2230 hrs GMT with programmes of Romanian music and announcements in English, French and German. Both stations will verify a correct reception report with a QSL card.

Brendon McNamee reports again from Portrush in N. Ireland. With his Sharp BZ-23 receiver and whip antenna he has logged BBC Radio Derby 1115 kHz at 2338hrs; Manx Radio, Isle of Man on 1295 kHz at 1655hrs; Radio Sweden 1178 kHz with its international service at 0020 hrs .

Our regular reporter Brian Murray (Edinburgh) has been concentrating on the local radio networks. With his Astrad VEF 204 receiver connected to an externally mounted TV aerial he has heard IBA Birmingham on 1151 kHz with close down at 0105 hrs ; IBA Manchester also on 1151 kHz testing at 0130 hrs ; BBC local radio stations at Carlisle on 755 kHz at 1415 hrs ; Blackburn on 854 kHz at 1410 hrs ; Sheffield on 1034 kHz at 0100 hrs ; Medway 1034 kHz at 2245 hrs ; Leeds 1106 kHz at 2350 hrs ; Derby 1115 kHz at 2240 hrs ; Bristol 1546 kHz at 2258 hrs and Leicester 1594 kHz at 2255 hrs . Brian also reports hearing two stations from the Iberian peninsula. From Spain, Radio Centro, Madrid on 1385 kHz at 0155 hrs and from Portugal CSB2, Radio Club Portugues in Lisbon on 1034 kHz at 0020 hrs . Externally mounted TV aerials often give good results as a medium wave antenna. Try connecting both the inner and the outer of the co-axial down lead to the aerial socket of the MW receiver. The outer (shield) will make a good vertical aerial in localities free from electrical interference.

Radio Algeria can be heard on 251 kHz (1195m) on the long waves in English between 1900 hrs and 1930 hrs GMT every evening. The signal, which comes from a 750 kW transmitter at Tipaza, is heard well in the UK. The station asks for reception reports which should be sent to Radio Algeria, 21 Boulevard des Martyrs, Algiers, Algeria.

## VHF/FM DXING

## by SIMON DAVID

IF we could forecast, with a useful degree of accuracy, likely openings for f.m. DXing then one could assume that we would be able to tune in together and all obtain near perfect results. It is easy to assume this, but the facts are different. What one DXer may pick up at one instant may be very different from the fortunes of another 100 miles or more away. It is sometimes forgotten that some British local radio stations may be as far away as some of the continentals, for example, North France and North England are approximately the same distance from Bristol or Oxford.

Here is a useful idea that could be helpful to f.m. DXers. For 50 p you can buy the new large British Rail timetable. Now why should this be of any value to DXing? Well, included with it are two large double-sided maps--one of Gt. Britain and the other of Europe as far east as the Black Sea. These are clearly marked with the main towns and railways and make a very clear f.m. DXers map. (These maps are worth the 50 p alone in my opinion.) If you cannot get one then any other flat map of Europe will do. ("Global" maps tend to distort distance lines.)

Now use a large pair of compasses, or the cotton-and-pencil technique, to draw concentric circles about the centre point representing your home town. These circles can be drawn to the scale of the map to represent distances of $25,50,75,100$ etc. miles from
your home. Next go over the map thoroughly and pick out all the known f.m. transmitting stations and draw a box around the place name to help it to stand out. When you have received any of these stations on your f.m. radio receiver, you can fill in the box with a light coloured pencil.

If your aerial is installed in a fixed position, determine as accurately as possible the compass point or transmitter towards which it is directed. Draw a straight line on the map through your home town representing this aerial direction and continue that line as far as possible across the map. You now have a quick reference chart to locate any station that comes in within a reasonable distance of that aerial line. If you want a reference for marking f.m. transmitters on the map you can either do it the hard way by going through all the radio station details in the World Radio and TV Handbook or use the f.m. station list that I mentioned last month.

My thanks to all readers who have written to me including Bob Bonsall of Buxton, F. Walshe of Southport who has picked up the Isle of Man, R.T.E., Lille and several northern local stations using a Stolle rotator. Geoffrey Tyrell writes from Aylesbury who (I am delighted to learn) has come back to P.W. after four years in the wilderness. He makes some observations about stations that he can pick up with only a single dipole arrangement and a Hacker Hunter portable radio. These include BRMB, LBC, Capital, BBC Radio London, Medway, Birmingham, Oxford and Stoke.

The new Oryx 50 is temperature controlled. Ilght. small. easy io hande. rapid heating and high pontrol within $\pm 2^{\circ} \mathrm{C}$ and adjusted in seconds whilst punnino to any velue between $200^{\circ} \mathrm{C}$ and $400^{\circ} \mathrm{C}$ Long life tron coated tip as standerd (11 sizes avallable)
Oryx De-Soldering Irons-small model SA3A instantly removes solder from printed circuits. Etc nozzie Larger instrument SR2 glves more suck. less recoll as only piston moves

De.Soldering Tools SR 3 A 15.06
SR2 $£ 6.65$ SR2 56.65
Oryx 50 1ron
1 at $£ 6.60$
Prices Correct May 197


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| $2{ }^{2} \times$ B | 87 p | 288 |
| $31 \times 32$ | 27p | 28D |
| $3!\times 5$ | 810 | 810 |
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| $17 \times 32$ | 81.10 | 87 p |
| $17 \times 5$ (Plain) |  | 80 p |
| Pln insertion too | 67p | 578 |
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Electrolytic

## Capacitors

## 4

 2 YOLT $47 \mu$100
240
330
3300
4700

6

## $33 \mu$ $68 \mu$ 150

150
470
680


| $2200 \mu \mathrm{~F}$ | 18 p | $100 \mu \mathrm{~F}$ |
| :--- | :--- | :--- |
| $3300 \mu \mathrm{~F}$ | 86 p | $150 \mu \mathrm{~F}$ |

10 V

10
10
$22 \mu \mathrm{~F}$
$47 \mu \mathrm{~F}$

| $47 \mu \mathrm{~F}$ | $8+\mathrm{p}$ | $670 \mu \mathrm{~F}$ | 18 |
| :--- | :--- | :--- | :--- |
| $100 \mu \mathrm{~F}$ | 80 |  |  |
| $100 \mu \mathrm{~F}$ | 61 p | $1000 \mu \mathrm{~F}$ | $\mathbf{8 2}$ |


| $100 \mu \mathrm{~F}$ | 61 p |
| :--- | :--- |
| $220 \mu \mathrm{~F}$ | $1000 \mu \mathrm{~F}$ |
| $2200 \mu \mathrm{~F}$ | 82 |
| 102 |  |


| $330 \mu \mathrm{~F}$ | 10 p | $5000 \mu \mathrm{~F}$ | 68 |
| :---: | ---: | :---: | :---: |
| $470 \mu \mathrm{~F}$ | 10 p | 40 VOLT |  |

$470 \mu \mathrm{~F} \quad 10 \mathrm{p} \quad 40 \mathrm{VOLT} \left\lvert\, \begin{aligned} & 1020 \mu \mathrm{~F} \\ & 1000 \mu \mathrm{~F}\end{aligned}\right.$

| $1000 \mu \mathrm{~F}$ | 11 p | $6.8 \mu \mathrm{~F}$ | $6 \nmid \mathrm{p}$ | $330 \mu \mathrm{~F}$ |
| :--- | :--- | :--- | :--- | :--- |
| $1500 \mu \mathrm{~F}$ | 20 p | $15 \mu \mathrm{~F}$ | 68 p | $270 \mu \mathrm{~F}$ |
| 28 | 28 |  |  |  |

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## DAVIAN ELECTRONICS

PO BOX 38 OLDHAM, LANC8, OLE BXJ


## by Eric Dowdeswell G4AR

HURRAH! First past the post to drop a report into my lap was Stanley Sharred (Birmingham) who is no newcomer to this page. To refresh your memories he has a CR100 with a horizontal centre-fed aerial, feeding an aerial tuning unit I am glad to note! An ATU will produce more extra ' S ' points on the meter than anything else! The 60ft legs of Stan's aerial are in a Vee configuration so the aerial becomes quite a useful beam at the higher frequencies. His Morse is obviously pretty good so it's high time he went off to get his RAE, providing he doesn't neglect his reports of course!

Dave Patrick (Carlisle) at 15 is a regular reader of PW and honoured this page with his first-ever report. His set-up of an R1475 plus two 150 ft wires 25 ft up should pull in most signals. Try combining the aerials Dave, with an ATU, as does Stanley, above. Switch in one or the other or both. If they can be arranged more or less at right angles good all-round coverage can be obtained. I suppose many readers of this page wouldn't mind being able to get just one 150 footer hanging on the aerial socket!

John Porter (Baslow, Derbys.) wrote an extremely short note with his list of goodies, but very welcome, nevertheless. All I can say about John is that he uses the 9R59DS and 33 ft of aerial which is obviously a good combination in the right hands. Incidentally, I am sending out some log sheets which I have run off to those who kindly report in to this feature, hoping that they will jot down for me any worthwhile DX that they hear, at the time they hear it. I know only too well what a bore it is to copy out logs especially some time after the event when interest has waned. A sheet of carbon paper slipped in the log is also a good way of saving time if a copy is wanted. As I point out on the log sheets, it is the rare country or prefix or QRP stations that I would like to know about.
It seems that BV2A on Taiwan (Formosa of old) now has the OK from the authorities to operate and is active on 14218 SSB and 14025 CW. QSL's
have been forthcoming from BV land in the past but this ought to make it very much easier now. You might like to get excited over OJOMA who is expected on from Market Reef with SSB on 14 and 21 MHz . The number of these DX-peditions that do eventually get on the air seems to be quite small compared to the number of rumours that one hears and I long ago learnt to wait until the pileup hits the headphones before letting the blood pressure rise at the thought of a 'new one' for the log!
I expect to hear from some of you on the Royal Signals Amateur Radio Society expedition to the British Honduras spot of English Cay, active midJune as VPIB probably. QSL's to the Society's headquarters station G4RS.

Don't despair of conditions on the HF bands-the information-crammed 160 m DX Bulletin of Stew Perry W1BB reckons that things have not been so good last season on our 'DC' band possibly due to too many sunspots around! They would indeed come in useful on the higher frequencies. In spite of all this, however, Stew still lists many prefixes worked on 160 m that would grace any $20 \mathrm{~m} \log$. How about 4S7, VP2, VP8, ZP9, PJ8, ZP1 etc? 'Worked All Continents' is always an exciting achievement, even on the HF bands, but W5RTQ almost did it in one evening on 160 m ! Only missed out on Africa.

## Log Extracts

S. Sharred:-160m GC5BGV GD4BEG G13YFY GM6CH OE5ANL OHISJ VE2DN VP2EEL W1HGT (599) WB8APH 80m 7X2AH 9K2DC HC8GI HI8EJH OA4OS ZL2BCG ZL4KF 40m 3D6AW G4AKQ/7Q7 JY3ZH MIC OH2BGM/OH0 Tl2SW VK2WC VP9AO ZP5AR ZS6ME 20m CR4BS WA2ZDF/CPI KL7BJW KM6DZ OA3XI PJ2CW PJ9JR VE6RP VK7PR VK80M VP2AB VP2MW VP2VBH VP8LP VR1AC ZL4AD 4S7PB 5X5NK 6Y5ED 8P6EX 15m CR7EK FM7WG HK3CTJ JH3GET KG4FX SV0MEE (Crete) TJIEZ TU2DV.
D. Patrick:-80m CR4BS EP2VJ OY1M 9H4L 40m CR6CD JW8IL 20 m CP1DN CR4BS PJ9DI 9Y4MA.
J. Porter:-15m 9GlAR 9W1BX 20m CP1QCC CP3BY EL5C HK3BET JA0CRL PJ9EE T12CF ZB2CJ CR4LA
S. Sharred again:-160m KZ5AA VE1MX VP2LPJ (St. Lucia) 80m CP1EU EP2VJ (0200) HZ1AB (0200) KV4FZ (2300) VP8NP (0030) ZS6DW (0330) 40 m JY3ZH (Amman 0400) KV4FZ (0130) LU8AHW (2330) TR8DG (2130) 20m HM1AQ (1330) KH6BB (1000) KS6UA (1600) FL8BH (1900) PJ9EE (2130) TA2SC (1530) VE8RCS (0900) YB1AY (1730) ZL1AXT (1030) 5U7HA (1730) 15m A51PN (1230) CX8BZ (2030) EL2KS (1230) FG0BAR (1800-QSL to F6CXL) KZ5CZN (2130) VP2SQ (1800-St. Vincent) VP2VBU (1300-Tortola)

CW stations in bold, remainder SSB.

## BROADCAST BANDS <br> Short Wave Reports by 15th of the month to Malcolm Connah, 27 Lismore Road, Highworth, Swindon, Wiltshire, SN6 7HU. <br> Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3 JG. <br> VHF/FM Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

## AMATEURBANDS <br> Logs covering any amateur band/s in band/alphabetical order by the middle of the wonth to Eric Dowdeswell G4AR, SIlver Firs, Leatherhead Road, Ashtead, Surrey, KT21 2TW.

The Pye Book of Audio Published by Pye Limited, Cambridge. Produced by Daily Mirror Books, 79 Camden Road, NW1 9NT 124 pages, $12 \times 8$ fin. Price 95p.

WHEN I first heard about the Pye Book of Audio, I thought "Oh no, another advertising gimmick," but how wrong I was.
This book is a profusely illustrated guide to audio in general and is aimed at the beginner and possibly first-time buyer rather than the man with all the gear already installed in his Hi-Fi den.

The contents are divided into thirteen chapters and there is a foreword written by Benny Green the musician. Chapter 1, The Original Sound, by Tom Stephenson describes what goes on at the recording studio and explains how a record is made.

Chapter 2, written by John Borwick delves into the whys and wherefores of pickups, and illustrates how sound is reproduced from tape or record.

Clement Brown, in Chapter 3 writes on pickups and motors and John Gilbert in Chapter 4 expounds on tuners and amplifiers. Chapter 5 is written by Michael Mayer of the BBC's Engineering Information Department. It's entitled The Broadcast Signal and the title really speaks for itself. Chapter 6, by Pat Hawker is called Commercial Radio and includes a useful question and answer section.
Chapter 8 is on tape recorders for the home and car. Chapter 9 on purchase and care of records and tapes and Chapter 10 describes the ins and outs of 4-channel sound. Chapter 11 helps the reader decide which system to use and how to get value-for-money and Chapter 12 explains how your audio unit is manufactured.

The final chapter helps you decide where to place your audio set-up in your home, and the end of the book contains a useful little glossary of audio terms.

There's only one strange thing in this work that I spotted and that is where a beautiful colour picture of a vintage Thorens phonograph is shown. There is a disc on the turntable but the caption tells us that the machine had a cabinet with facilities for storing the playing cylinders-strange!

Well, Messrs Pye, you are to be congratulated on producing a very well written, well illustrated book which I know will be of great interest and help to many people who are thinking about or are just entering the world of audio.

With the price of 95 p, this book just cannot go wrong and I thoroughly recommend it. Excellent value--Colin Riches

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G150/2 Thyratrons ex-equip 33p. $6 \times 4$. $4 \Omega$ Now Speakers fi 10pr (20p). Hewlett-Packard 100 MHz counter/ timer 524D \& 6 + carr.

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## PUSH BUTTON CAR RADIOKIT The Tourist II



## NOW BUILD YOUR.OWN PUSH BUTTON CAR RADIO

Easy to assemble construction kit comprising fully completed and tested printed circuit board on which no soldering is required. All connections are simple push fit type making for easy assembly.
Fine tuning push button mechanism is fully built and tested to mate with printed circuit board.
Technical specification:
(1) Output 4 watts R.M.S. output. For 12 volt operation on negative or positive earth.
(2) Integrated circuit output stage, pre-built three stage IF Module.

Controls volume manual tuning and five push buttons for station selection, illuminated tuning scale covering full, medium and long wave bands.
Size chassis 7" wide, $2^{\prime \prime}$ high and $4 \frac{5}{16}$ " deep approx
Car Radio Kit $£ 7.70+55 p$ post. \& pack. Speaker including baffle and fixing strip
f1. $65+23$ p postage \& packing
Car Aerial Recommended - fully retractable and locking £1. 35 post paid


QUALITY SOUND** FOR LESSTHAN 19.00
Stereo 21 easy to assemble audio system kit, - no soldering required. Includes:-
BSR 3 speed deck, automatic, manual facilities together with ceramic cartridge.
Two speakers with cabinets.
Amplifier module. Ready built with control panel, speaker leads and full, easy to follow as sembly instructions.

For the technitally minded:Specifications:
Input sensitivity 600 mV :Aux. input sensitivity 120 mV : Power output 2.7 watts per channel: Output impedance $8-15$ ohms. Stereo headphone socket with automatic speaker cutout. Provision for auxiliary inputs - radio, tape, etc., and outputs for taping discs. Overall Dimensions. Speakers approx. $15 \frac{1^{\prime \prime}}{}{ }^{\prime \prime} \times 8^{\prime \prime} \times 4^{\prime \prime}$. Complete deck and cover in closed position approx. $15 \frac{1}{2}^{\prime \prime} \times 12^{\prime \prime} \times 6^{\prime \prime}$. Complete oniy $\mathbf{f} 18.95$ Extras if required. Optional Diamond Styli f1.37
Specially selected pair of stereo headphones with individual level controls and padded earpiece's to give optimum performance, $\mathbf{~} \mathbf{3 . 8 5}$.

## 5, DISC0 AMPLIFIER

Reliant Mk IV Mono Amplifier, ideal for the
small disco or house parties.
Outputs 20 watts R.M.S. into 8 ohms (suitable for 15 ohms).
Inputs * 4 Electrically Mixed Inputs *3 Individual Mixing controls. *Separate bass and treble controts common to all 4 inputs

* Mixer employing F.E.T. \{Field Effect Transistors). *Solid State Circuitry. *Attractive Styling. INPUT SENSITIVITIES
-Input-1.) Crystal mic. guitar or moving coil mic, 2. and 10 mV . (selector switch for desired sensitivity.-Inputs-2), 3), 4, Medium output equipment-ceramic cartridge, tuner, tape recorder, organs etc. all 250 mV sensitivity.
AC Mains 240V. operation.
Size approx. $12 \frac{1}{2}$ ins $\times 6$ ins $\times 3 \frac{1}{2}$ ins
$\mathbf{f 1 5 . 0 0}+\mathbf{6 0 p}$. post \& pack


## DISCO 50



45 WATT R.M.S. MONO DISCOTHEQUE AMPLIFIER Ideal for Disco Work. Output Power: 45 watts R.M.S. Frequency Response 3 dB points 30 Hz and 18 KHz . Total Distortion: less than $2 \%$ at rated output. Signal to noise ratio: better than 60 dB . Bass Control Range: 13 dB at 60 Hz . Treble Control Range: 12 dB at 10 KHz . Inputs: 4 inputs at 5 mV into 470 K . Each pair of inputs controlled by separate volume control. 2 inputs at 200 mV into 470K. Size: $19 \frac{1}{4} \times 10 \frac{1}{2} \times 8$ ins. approx. Amplifier $\mathbf{f} 27.50+\mathbf{f 1} .50 \mathrm{p}$. \& p
Special Offer: Disco 50 plus two 15" E.M.I. speakers type 14A/780


# COMPLETE ${ }^{* *}$ STEREO SYSTEM 

## 651-00

40 Watt Amplifier.
Viscount III-R102 now 20 watts per channe System I includes.
Viscount III amplifier - volume, bass, treble and balance controls, plus switches for mono/ stereo on/off function and bass and treble filters. Plus headphone socket. Specification
20 watts per channel into 8 ohms. Total distortion@10W@1kHz 0.1\%.P.U.1 (for ceramic cartridges) 150 mV into 3 Meg. P.U. 2 (for magnetic cartridges) 4mV@1kHzinto 47K. equalised within $\pm$ IdB R.I.A.A. Radio 150 mV into 220K. (Sensitivities given at full power). Tape out facilities: headphone socket, power out 250 mW per channel. Tone controls and filter characteristics. Bass: + 12dB to-17d8@ 60 Hz . Bass filter: 6 d 8 per octave cut. Treble control: treble +12 d 8 to $-12 \mathrm{~dB} @ 15 \mathrm{kHz}$. Treble filter: 12 dB per octave. Signa/ to noise ratio: (all controls at max.) - 58 dB .
Crosstalk better than 35 dB on all inputs. Overload characteristics better than 26 dB on all inputs. Size approx. $13 \frac{3_{4}^{3 "} \times 9 " × 3 \frac{3}{4}}{}$ Garrard SP25 deck, with magnetic cartridge. de luxe plinth and hinged cover.
Two Duo Type II matched speakers Enclosure size approx. $17 \frac{1}{2}$ " $\times 10 \frac{3}{4}{ }^{\prime \prime} \times 6^{\prime \prime}$ / 1 п simulated teak. Drive unit $13^{\prime \prime} \times 8^{\prime \prime}$ with parasitic weeter 10 watts handling

Complete System $£ 51.00$

### 669.00

System II
Viscount III amplifier (As System I)
Garrard SP. 25 (As System I)
Two Duo Type IIIA matched speakersEnclosure size approx. $31^{\prime \prime} \times 13^{\prime \prime} \times 11 \frac{1_{2}^{\prime \prime}}{}$. Finished in teak veneer. Drive units approx. $13 \frac{1}{2}{ }^{\prime \prime} \times 8 \frac{1}{4}$ " with $3 \frac{1}{4}{ }^{\prime \prime} \mathrm{HF}$ speaker. Max. power 20 watts. 8 ohms. Freq. range 20 Hz to 20 kHz .

## Complete System £69.00

PRICES: SYSTEM 1
Viscount III R 102 amplifier $\quad £ 24 \cdot 20+\mathbf{f} 1 p \& p$ 2 Duo Type il speakers $\quad £ 14 \cdot 00+\mathbf{f 2} \cdot 20 p \& p$ Garrard SP25 with
MAG. cartridge de luxe plinth and hinged cover ${ }^{\text {- }}$
$\mathrm{f} 21.00+\mathrm{f} 1.75 \mathrm{p}$ 千p
total $£ 59.20$
Available complete for only $\mathbf{£ 5 1 . 0 0 + £ 3 . 5 0 p . ~ \& p}$
PRICES: SYSTEM 2
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THE ULTIMATE COMPLETE SPEAKER SYSTEM EMI LE 315

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A professional standard five way speaker system with enclosure giving top quality performance
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Drive Units
Hand built - $15^{\text {" diameter bass with } 3^{\prime \prime}}$ voice coil, - two $5^{\prime \prime}$ diameter Mid Range units, - two $3 \frac{1}{4}{ }^{\text {n }}$ HF. units, plus matchung crossover panel with two variable potentiometers for mid and high frequency adjustment
Power Handing
Continuous rating 35 W rms., Peak power rating 70 W
Frequency Response
$20 \mathrm{~Hz} 20,000 \mathrm{~Hz}$. Jmp. 8 oh ms
Our price $£ 45 \cdot \mathbf{0 0}+\mathfrak{f 3} \mathbf{5 0} \mathbf{p}$. \& p.


15" 14A/780 BASS UNIT Bass unit on a rigid diecast chassis Superior cone material handles up to 50 watts RMS, and is treated 10 give a smooth frequency response. Resonance 30 Hz . flux density 360,000 Maxwells. Impedance at 1 kHz is 8 ohms. $3^{\prime \prime}$ voice coil.
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| 10.5 GHz |
| 11.5 GHz |
| 9.35 GHz |
| 8.35 GHz |
| 0.35 GHz |
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D
10 Volis: $0.5 / 2 \mathrm{~A} .5$
$10 / 50 / 250 / 1000 \mathrm{~V}$ AC. $30 / 1 / 20 / 50 / 2000 \mathrm{~V}$
501 $500 / 10000$ DC.


MODEL AF. 105 VOM
$60,000 \mathrm{opv}, \mathrm{M}$
scele. Merer scsic. Meter
protection. 0/3/3/12/80/120/ $300 / 600 / 1200 \mathrm{~V}$ DC $0 / 8 / 30 / 120 /$
$300 / 600 / 1200$ $30 / 30 \mu \mathrm{~A} / \mathrm{B} /$
$60 / 300 \mathrm{~mA}$ $60 / 300 \mathrm{~mA} /$
$12 \mathrm{Amp} .0 / 10 \mathrm{~K}$ $12 \mathrm{Amp} .0 / 10 \mathrm{~K}$
$1 \mathrm{~m} / 10 \mathrm{~m} / 100$
Meg Ohms. 20 to 17 dB . OUR PRICE £12.50 P\&P 30p. LB4 TRANSISTOR TESTER Tests PNP or NPN indication. Opperates on two 1.5 V battories. Complete
with instructions currant $10 / 100 \mathrm{LA} / 10 /$
$10 / 100 / 500 \mathrm{~mA} / 2.5 / 10 \mathrm{~A}$ 10/100/500mA/2.5/10A. Resistence: ik/iok/100k/10 Meg/100 Mog ohms.
Oecibels: -10 to +49 dB . Plastic case with carrying handle. Siza: $190 \times 172$
$\times 99 \mathrm{~mm}$. $\times 99 \mathrm{~mm}$.
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370WTR MUL TIMETER

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$0 / 2.5 / 10 / 50 / 250 /$
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$0 / 501 \mathrm{~A} / 1 / 10 / 100$ mA/1/10A DC.

$0 / 100 \mathrm{~mA} / 1 / 10 \mathrm{~A}$ AC. $0 / 5 \mathrm{k} / 50 \mathrm{k} / 500$ $5 \mathrm{Meg} / 50 \mathrm{Mep}$ | OUR PRICE £19.95 P\&P 30p |
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| KAMODEN 72200 Multitester |

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Ranges: $-0 / .06 /-3$
$3 / 30 / 120 / 600 /$ 1200 V DC. 0/3 $12 / 60 / 300 / 11200$
VAC. $0 / 6 \mathrm{~A} /{ }^{2} /$ $V A C .0 / 6 u A /$
$1.2 \mathrm{~mA} / 120 \mathrm{~mA}$ $1.2 \mathrm{~mA} / 120 \mathrm{~mA}$
$600 \mathrm{~mA} / 12 \mathrm{~A}$
0 OC
$0 / 124 \mathrm{AC}-20$ $0 / 12 \mathrm{AAC},-20$ to
$+6 \mathrm{MdB} .0 / 2 \mathrm{k} / 200 \mathrm{k} /$
 2 Meg/200 Megotrins. OUR PRICE E22.50 P\&P 30p

## U4317 MULTIMETER

instrument for fiel
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and laboratory work
Knite
86 med
86 mm . mir por scater
Ranges: $100 \mathrm{mV} / \mathrm{l}$
Rangas: 100mV/
$0.5 / 2.5 / 10 / 25 / 50 / 100 / 250 / 500 / 1000 / 1$ VDC. $0.5 / 2.5 / 10 / 25 / 50 / 100 / 250 /$ $500 / 1000 \mathrm{~V}$ AC. Current: 500AA/0.5/

$1 / 5 / 10 / 50 / 250 \mathrm{~mA} / 5 \mathrm{~A}$. | $1 / 5 / 10 / 50 / 250 \mathrm{~mA} / 1 / 5 A$ |
| :--- |
| $0.5 / 1 / 5 / 10 / 50 / 250 \mathrm{~mA} / 1 / 5 A A C$ |
| $0.25 /$ | istance: $0.5 / 10 / 100 / 200$ ohms $/ 1 / 3 /$

$30 / 300 \mathrm{k}$ ohms. Decibela: -5 in +10 s . Battery ophms. Decibels: $-510+10 \mathrm{~dB}$
operated. Size: $210 \times 115 \mathrm{x}$ 90 mm . Supplied in carrving case com OUR PRICE f
MDDEL U4311 Sub-standard

## Multi-range Volt-Ammeter

 Sensitivity 330Onms ${ }^{3}$ IVolt AC
and DC. And DC. $0.5 \%$ DC. 1\% AC. Scaidength:
165 mm.
$0 / 300 / 750 \mathrm{u}$ A/ $1.5 / 3 / 7.5 / 15 /$
$30 / 75 / 150 / 300$ $750 \mathrm{~mA} / 1.5 / 3 /$ 7.5A DC. $0 / 3 /$ $7.5 / 15 / 30 / 75 /$
$150 / 300 / 750$ $150 / 300 / 750 \mathrm{~mA}$
$1.5 / 3 / 7.5 \mathrm{~A} \mathrm{AC}$
0/75/150/300/750mv/1.5/3/7.5/15/ $30 / 75 / 150 / 300 / 750 \mathrm{~V}$ DC. $0 / 750 \mathrm{mV} /$ 1.5/3 $/ 7.5 / 15 / 30 / 75 / 150 / 300 / 750 \mathrm{~V}$ AC. Automatic cut out devica. Supp-
lied complete with test lemeds, manusl and test certificatos.
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with instructio
$\mathbf{~} 14.50$ PRP 20p Transistor Tester 27 ranoes. 16,700apv. Ranges: 0.3/1.5/6/ $30 / 60 / 150 / 300 / 900 \mathrm{~V}$ DC. $1.5 / 7.5 / 30 / 150 /$ Current: $0.06 / 0.6$ $6 / 60 / 600 \mathrm{~mA}$ DC $0.3 / 3 / 30 / 3 \mathrm{DOMC}$. AC Resistancs: $0.08 /$
$0.6 / 2 / 6 / 20 / 60 / 200$ O.6/2/6/20/60/200k ohms/2 Mohms. with probers, leads und steat carmin case. size: $1115 \times 215 \times 90 \mathrm{~mm}$.
OUR PRICE S100TR MULTIMETER PaP 30p TRANSISTOR TESTER 100,000opv. Mir protection. $0 / 0.12 t$
$0.6 / 3 / 1230 / 120 /$ $0.6 / 3 / 12 / 30 / 120 /$
600 V DC. $0 / 6 / 30$ 600V DC. 0/6/30
$120 / 600 \mathrm{~V}$. $0 / 12 / 600 \mathrm{~A} / 12 /$
$30 \mathrm{mmA} / 6 / 12 \mathrm{~A}$ $300 \mathrm{ma} / 6 / 12 A$ D
$0 / 10 \mathrm{k} / 1 \mathrm{Meg}$ $0 / 10 \mathrm{k} / 1 \mathrm{Mog}$
100 Meg -20 to +50 dB .
$0.01-0.2 \mathrm{MFD}$

ransistor tester measures Alpha, Beta
and ICO. Complete with imiructions and ICO. Complete with imatructions,
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Megohms, 500 V .
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VRMS VRMS/mm: $0.1-25$;
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width: 500 kHz Sonsitivity ay 100 kHz
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$1-3000 u s{ }^{2}$. Frep running 20-200 $\mathrm{kHz}_{\mathrm{z}}$ in nine ranges. Calibrazor pipe.
$220 \times 360 \times 430 \mathrm{~mm}$. $115-230 \mathrm{VAC}$ OUR PRICE E39.00 Cerr. peid
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embeivent respe and
mocuracy at low cout. Resistence
cenges: 0.1 ohm-11.1 megohm $\pm 1 \%$ Inductence: 5 ranges: 1 microhanry 111
henries $\pm 2 \%$ Capacity: 8 ranges henriez $110 \mathrm{mfd} \pm 2 \%$ Turn 月otio:
10pt-110 Bridge Voltage er $1,000 \mathrm{cps}$. Opera. ted from 9 -volt battary. 100 micro. $6^{6 \prime} \times 2^{\circ}$ OUR PRICE $£ 25.00$ Pa $P 30 \mathrm{p}$

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GENERATOR GENERATOR MHz on of bencle. Dincetly ofility
for entibertion 220 output, $X$ tal sock forend now with inetructione. $5 \mathrm{me} 140 \mathrm{~mm} \times 215 \mathrm{~mm} \times 170 \mathrm{~mm}$. OUR PRICE EI7.50 PEPEOP.

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| A rampe of high quality moving coil instrumants ioven or school experi moplication. $3^{\prime \prime}$ mirror ment. The mater move ment is amily secensible to demonstrato internel |  |  |  |
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| 1 mA | f7.60 |  |  |
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| BVOC ... | 17.60 <br> 8.80 | 5V/50V |  |
| OVOC | 17.60 |  |  |
| $\checkmark$ OC |  | 1/5A 154 DC |  |
| CLEAR PLASTIC MDDEL MR 85P Size: $120 \times 110 \mathrm{~mm}$ |  |  |  |
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| 100.0 .100$500-500$ |  |  |  |
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| S00mA .. .. ${ }_{\text {ct }}$ |  |  |  |
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|  |  |  |  |
| DC .. | 58.20 | 30A AC | - 56.20 |



## CLEAR PLAST SI2e: $42 \times 42 \mathrm{~mm}$



CLEAR PLASTIC MODEL MR 65P
Size: $86 \times 78 \mathrm{~mm}$


BAKELITE MODEL S8O Enlarged Window
Size. $80 \times 80 \mathrm{~mm}$


| CLEAR PLASTIC MODEL MR 52P |
| :--- |
| SIze. $60 \times 60 \mathrm{~mm}$ |


| 50 A A | 6370 |  |  |
| :---: | :---: | :---: | :---: |
| 100uA | 6350 63 |  |  |
| 50.0-50 u A | $f 350$ |  |  |
| $100.0 \cdot 100 \mathrm{u}$ A | f345 |  |  |
| 1 ma | $\begin{array}{r}1330 \\ \text { c3 } \\ \hline\end{array}$ |  |  |
|  | [330 |  |  |
| 50 ma | 1330 |  |  |
| 100 mA | 6330 |  |  |
| 500 mA | 1330 |  |  |
| 1A ${ }^{\text {S OC }}$ | 6330 63 | S Mater 1 mA . |  |
| 10 V OC | f330 | $\checkmark$ M Mater | 6380 |
| 20V DC | 6330 63 | ${ }_{1}^{1 / 4 A C}$ | 6330 6330 |
| 3000 DC | ¢330 | 10a AC | - 13.30 |
| 15 V AC 300 VAC | 6340 6340 | 20A AC 30 AC | : $\begin{array}{r}6330 \\ 83\end{array}$ |

## BAKELITE MODEL MR 65 Size. $80 \times 80 \mathrm{~mm}$

 25 L50 A
10 A
500 u
50 u

## 1500 A 50.0 .50 A 50 <br> 50.0 .500 A 100.0 .100 u

100.0 .1000 A
500.500 A


| 1.0 .1 m |
| :--- |
| 5 mA |
| 10 mA |

$\begin{array}{ll}\text { 5A DC } & \\ 10 A D C \\ 15 A D C & . \\ 30 A D C & .\end{array}$
 $\begin{array}{ll}27 \text { IOTTENHAM CT. RD. } & 01.6363715 \\ 33 \text { TOTTENKAM CT. RD. } & 01.6362605\end{array}$ 42/45 TOTTENKAM CT. RO. 01.6360045 $\begin{array}{ll}87 \text { TOTTENHAM CT. RD. } & 01-5803739 \\ 257 / 8 \text { TOTTENHAM CT. RD. } & 01-5800670\end{array}$ 3 LISLE STENAM CT. RD. 34 LISLEST. WCZ 118 EDGWARERD. W2 01-4379155 193 EDGWARE RD. W2 01-7239789 207 EDGWARE RD. W2 $\quad 01-7236211$ 311 EDGWARERD. W2 $01-2620387$ $\begin{array}{ll}346 \text { EOGWARERD. W2 } & 01.7234453 \\ 382 \text { EDGWARE RD. W2 } & 01-7234194\end{array}$ 382 EDGWARE RD. W2 01-7234194 $\begin{array}{ll}152 / 3 \text { FLEETST. EC4 } & 01-3532833\end{array}$



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## MULTIMETER TYPE U4323

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        Sensitivity: 20,000s2/V.
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7 D.C. Voltage ranges $0 \cdot 5-1000 \mathrm{~V}$ 6 A.C. Voltage ranges $2 \cdot 5-1000 \mathrm{~V}$ 5 D.C. Current ranges $0 \cdot 05-500 \mathrm{~mA}$ 4 Resistance ranges $1 \mathrm{k} \Omega-1 \mathrm{~m} \Omega$
Built-in oscillator providing AF output of 1 kHz and I.F. output of 465 kHz with an amplitude of 1 volt minimum.
Dimensions: $140 \times 87 \times \mathbf{4 0} \mathrm{mm}$. Welght 0.5 kg
PRICE complete with leads and plastic storage case £7•70. Packing \& postage £0.50

## AC/DC MULTIMETER TYPE U4313



Mirror scale 86 mm long.
Dimensions: $115 \times 215 \times 90 \mathrm{~mm}$, Weight 3-3lb. PRICE, complete with test leads, service manual and steel carrying case $£ 12 \cdot 50$. Packing \& carriage $£ 0 \cdot 50$.

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[^7]:    -continued on page 350

[^8]:    

[^9]:    SERVICE SHEETS for Televisions, Radios, Transistors. Record Players, Tape Recorders, etc., from 5p with free Fault-Finding Guide. Over 10,000 models available. S.A.E. enquiries. Catalogue 20 p and S.A.E. Hamilton Catalogue 20 p and S.A.E. Leomards. Sussex. Telephone Hastings 429066 .

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