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VOL. 50 NO. 2 ISSUE 808 JUNE 1974

BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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ESSENTIAL BOOKS FOR RADIO AMATEURS NEW! TELEPRINTER HANDBOOK TEST EQUIPMENT by D. J. Goacher, G3LLZ, and for the radio amateur J. G. Denny, G3NTT by H. L. Gibson, CEng, MIEE, G8CGA This recent RSGB publication covers the theory and practice of radio teleprinter techniques. In addition to full descriptions This book explains in detail the theory behind modern measand maintenance data for all widely used machines, both urement techniques, and describes many items of equipment European and American, the handbook fully covers the design of special interest to the home constructor. Readers are taken and use of ancillary equipment. There is also an extensive through the basics of indicating and electronic instruments reference section covering commercial equipment and and on to techniques of frequency, power and noise measureterminology, and a bibliography. ment, using up-to-the-minute components and methods. The contents include: theory, practice and standards; tele-Other topics include signal sources, attenuators, oscilloprinters; associated machines; power supplies; terminal scopes, swept measurements, aerials and transmission lines. units; auxiliary equipment; frequency shift keying; filters; There is also an extensive section of reference data, test equipment; interconnection and control; operating Detailed instructions are given for the construction of many procedures. items of test gear; including a wide-range fet multimeter, a A "must" for every rtty enthusiast, this volume is also invaluable to all who use, design or service teleprinter transistorized dip oscillator, an oscilloscope for use up to 146MHz, an i.f. sweep generator and digital frequency meter. equipment. Price £2, including p & p 376 pages £5.35 (inc. p & p) These are just two of a complete range of technical publications, log books and maps for the radio amateur. Send a large s.a.e. for the complete list. The RSGB is the national society representing all UK radio amateurs. Membership is open to all interested in the hobby: write to the General Manager and ask for full details. RSGB **RADIO SOCIETY OF GREAT BRITAIN** 35 DOUGHTY STREET, LONDON, WC1N 2AE TEL: 01-837 8688 PRACTICAL

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The original circuit employed Germanium Power Transistors for the negative earth version. **WE NOW SUPPLY SILICON P.N.P. POWER DEVICES AT NO EXTRA COST!** All components available separately. Case size $4\frac{3}{2}$ x $3\frac{3}{2}$ x 2". Complete assembly and wiring manual **25p**, supplied with deluxe kit only, refundable on purchase of kit.

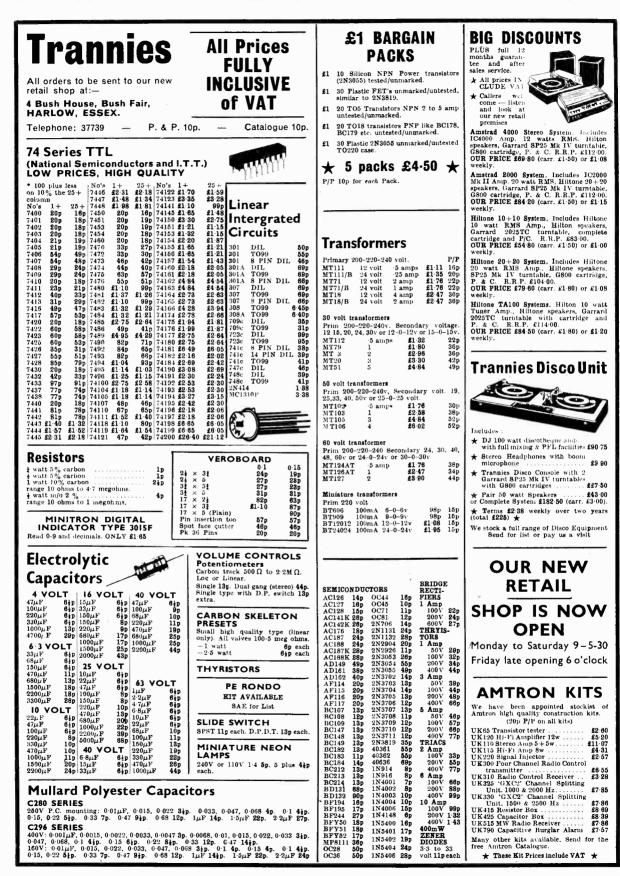
Suitable for 12v systems with Pos. or Neg. earth.

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Technical specification : 1.) Output 2.5 watts R.M.S. into 8 ohms. For 12 volt operation on negative or positive earth.

2.) Integrated circuit output stage, pre built three stage IF Module.

Controls Volume, manual tuning and five push buttons for station selection, illuminated tuning scale covering full medium and long wave bands.

Size Chassis 7 ins. wide, 2 ins. hⁱyh and 4 15 ins. deep approx.



NOTE: The ability to solder on a printed circuitboard is necessary to complete this kit successfully. Circuit diagram and comprehensive instructions 55p.free with kit. **Car Radio Kit**

 $\pounds 6.60 + 55p.$ postage & packing.

Speaker including baffle and fixing strips £1.65 + 23p. postage & packing.

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BSR 3 speed deck, automatic, manual facilities together with ceramic cartridge.

Two speakers with cabinets.

Amplifier module. Ready built with control panel, speaker leads and full, easy to follow assembly instructions. For the technically minded :--

Specifications:

Specifications. Input sensitivity 120mV: Power output 2.7 watts per channel: Output impedance 8–15 ohms. Stereo headphone socket with automatic speaker cutout. Provision for auxiliary inputs – radio, tape, etc., and outputs for taping discs. Overall Oimensions. Speakers approx. 15 $\frac{1}{2}$ × 6". Complete dek and cover in closed position approx. 15 $\frac{1}{2}$ × 12" × 6". Complete only £18.95 Extras if required. Optional Oiamond Styli £1.37 + £1.60 p & p. Specially selected pair of stereo headphones with individual level controls and padded earpoices to give optimum performance, £3.85.

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45 WATT R.M.S. MONO DISCOTHEQUE AMPLIFIER Ideal for Disco Work. Output Power: 45 watts R.M.S. Frequency Response 3dB points 30Hz and 18KHz. Total Distortion: less than 2% at rated output. Signal to noise ratio: better than 60dB. Bass Control Range: 13dB at 60Hz. Treble Control Range: 12dB at 10KHz. Inputs: 4 inputs at 5mV into 470K. Each pair of inputs controlled by separate volume control. 2 inputs at 200mV into 470K. Size: $19\frac{1}{4} < 10\frac{1}{2} < 8ins. approx. Amplifier £27.50 + £1.50 p. & p$

Special Offer: Disco 50 plus two 15" E.M.I. speakers type 14A/780 (as illustrated on opposite page). **Complete £57.00**+**£4.00** p&p.

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£51.00 40 Watt Amplifier.

Viscount III - R102 now 20 watts per channel. System Lincludes,

Viscount III amplifier - volume, bass, treble and balance controls, plus switches for mono/ stereo on/off function and bass and trebie filters. Plus headphone socket. Specification

20 watts per channel into 8 ohms. Total distortion@10W@1kHz0·1%. P.U.1 (for ceramic cartridges) 150mV into 3 Meg. P.U.2 (for magnetic cartridges) 4mV @ 1kHz into 47K equalised within _ 1dB R.I.A.A. Radio 150mV into 220K. (Sensitivities given at full power), Tape out facilities : headphone socket, power out 250mW per channel. Tone controls and filter characteristics. Bass : + 12dB to -17dB @ 60Hz. Bass filter: 6dB per octave cut. Treble control: treble - 12dB to -12dB @ 15kHz. Treble filter: 12dB per octave. Signal to noise ratio: (all controls at max.) -58dB. Crosstalk better than 35dB on all inputs.

Overload characteristics better than 26dB on all inputs. Size approx. 13≩"×9"∧ 3∄ Garrard SP25 deck, with magnetic cartridge,

de luxe plinth and hinged cover. Two Duo Type II matched speakers

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and hinged cover

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2 Duo Type II speakers	£14.00 + £2.20 p & p
Garrard SP25 with	
MAG cartridge de fuxe pligth	

£21.00 + £1.75 p & p.

total £59.20

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PRICES: SYSTEM 2			
Viscount R102 amplifier	£24-20	÷	£1.00 p. & p.
2 Duo Type IIIA speakers	£39-00		£4.00 p. & p.
Garrard SP25 with			
MAG cartridge de luxe plinth	£21.00		£1.75 p. & p.
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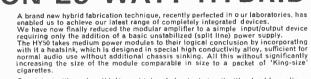
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Consistent with modern thinking a triple rated output circuit with a load fuse allows for peak transient response without distortion but ensures the necessary protection. SPEC

OUTPUT POWER-LOAD IMPEDANCE: INPUT SENSITIVITY: INPUT IMPEDANCE: TOTAL HARMONIC DISTORTION: SIGNAL/NOISE RATIO: FREQUENCY RESPONSE: SUPPLY VOLTAGE: SIZE

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25 watts RMS. 50 watts peak music power 4-16Ω Into8Ω Odb (0.775 volts RMS) 47K Ω Less than 0.1% at 25 watts typically 0.05 better than 75db 10Hz-50KHz ± 1db + 25 volts 105 x 50 x 25 mm Price £5-80 mono, £11-60 stereo

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INPUTS Magnetic Pick-up 3mV (within 1db RIAA curve) Ceramic Pick-up up to 3mV Microphone 10mV Tuner 250mV SPEC Auxiliary 3–100mV Input impedance 47kΩ 1kHz

OUTPUTS Tape 100mV. Main output, Odb (0·775volts)

ACTIVE TONE CONTROLS Treble ± 12db at 10kHz Bass ± 12db at 10kHz OVERLOAD CAPABILITY (equalization stage) 40db on most sensitive input OUTPUT NOISE LEVEL (below 10mV magnetic input) 68db DISTORTION 0:05% at 1kHz SUPPLY VOLTAGE ± 16:25 volts SUPPLY CURRENT 15mA Price £4:45 mono, £9:70 stereo Price inclusive of VAT & P & P



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The new PSU50 has a low profile look being only 21 inches high and can be used for either mono or stereo systems

SPEC OUTPUT VOLTAGE ± 25 volts INPUT VOLTAGE 2t0-240 volts SIZE L. 70, D. 90, H. 60 mm Price £5-23 Price inclusive of VAT & P & P

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0 1, 0 22, 0 47, 1 0 mF/ 35V.	ea. 13p
2·2/16V, 2·2/35V, 4·7/16V, 10/6·3	ea. 13
4 7/35V, 10/16V, 22/6 3V	ea. 16
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10	_	_	_	_	8p	9p	8p	8p
22		-	8p	_	9p	8p	8p	10p
47	8p	_	9p	8p	8p	8p	10p	13p
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8 ohms 2.5mm plug 22p 8 ohms 3.5mm plug 22p	ELEMENTS ECN 240 £1-16 ECCN 240 £1-32	PS 31 Phono Screened 0.14 PS 32 Car Aerial 9.15	CASSETTE CASES Holda 12. 10" x 31" x 5". Lock & Handle.
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B1223. 200 ohms plus on/off switch and 2.5mm and 3.5mm plugs £1.60	ANTEX HEAT SINKS 10p	PLUGS PS 1 D.I.N. 2 Pin (Speaker) 0.11	8-TRACK CARTRIDGE
3-WAY STEREO HEAD-		PS 2 D.I.N. 3 Pin 0.12	
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H1012 £1-87	orders-please add extra for postage,	PS 5 D.I.N. 5 Pin 240° 0.15 PS 6 D.I.N. 6 Pin 0.15	£2-70
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	Pack No. Qty. Description Price	PS 10 Jack 3.5mm Screened 0.12 PS 11 Jack ½" Plastic 0.13	240v. Primary. Secondary voltages available
CAR STEREO SPEAKERS (Angled) \$3.85 per pair.	Cl 250 Resistors mixed values approx. count by weight 0.55	PS 12 Jack ‡" Screened 0.18	from selected tappings 4v, 7v, 8v, 10v, 14v, 15v, 17v, 19v, 21v, 25v, 31v, 33v, 40, 50
	C2 200 Capacitors mixed values approx.	PS 13 Jack Stereo Screened 0.29 PS 14 Phono 0.06	and 20v-0-25v.
BI-PAK	count by weight 0.55 C3 50 Precision Resistors 1%, 2%	PS 15 Car Aerial 0.15 PS 16 Co-Axial 0.10	MT50/1 1 £1.93 30p
CATALOGUE AND LISTS	mixed values 0.55 C4 75 ith W Resistors mixed preferred		MT50/1 1 #2-42 35p MT50/2 2 £3-30 40p
Send S.A.E. and 10p.	values C-55	CABLES CP 1 Single Lapped Screen 0.06	CARTRIDGES
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(Black Vinyl covered) No. Length Width Height Price	Standard Switch Type 0.55	CP 10 Low Loss Co-Axial 0.10	TTC J-2105 Ceramis/Med. Output \$1-64
No. Length Width Height Price BV1 6" × 5½" × 2" 90p BV2 11" × 6" × 3" \$1.20	types mixed values 0.55	CARBON	CARBON FILM RESISTORS
	C13 20 Electrolytics Trans. types 0.55 C14 1 Pack assorted Hardware—	POTENTIOMETERS	The E12 Range of Carbon Film Resistors,
ALUMINIUM BOXES BA1 $5\frac{1}{2}$ " \times $2\frac{1}{2}$ " \times $1\frac{1}{4}$ " $42p$ BA2 4 " \times 4 " \times $1\frac{1}{4}$ " $41p$	Nuts/Bolts, Grommets etc. 0.55	Log and Lin 4.7K, 10K, 22K, 47K, 100K, 220K, 470K,	1/8th watt available in PAKS of 50 pieces, assorted into the following groups:
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C15 4 Mains Slide Switches 0.55 C16 20 Assorted Tag strips & Panels 0.55	1M, 2M VC 1 Single less Switch 0.14	R1 50 Mixed 100 ohms-820 ohms 40p
BA5 4" × 21" × 2" 41p	C17 10 Assorted Control Knobs 0.55	VC 2 Single D.P. Switch 0.26 VC 3 Tandem Less Switch 0.44	R2 50 Mixed 1K ohms-8.2K ohms 40p R3 50 Mixed 10K ohms-82K ohms 40p
BA6 3" × 2" × 1" 34p	C18 4 Rotary Wave Change Switches 0.55 C19 3 Relays 6-24V Operating 0.55	VC 4 1K Lin Less Switch 0.14	R4 50 Mixed 100K ohms-1 Meg. ohms 40p
	C20 4 Sheets Copper Laminate approx. 10" × 7" 0.55	VC 5 100K Log anti-Log 0.44	THESE ARE UNBEATABLE PRICES- LESS THAN 1p EACH INCL. V.A.T.
VISIT OUR COM		HORIZONTAL CARBON	
18 BALDOCK ST., W	ARE Herts (A10)	PRESETS 0.1 watt 0.06 each	BI-PAK SUPERIOR QUALITY
Open MonThurs. 9.15-6 p.m. Sat. 9.15-5.30.	Late Night Shopping until 7 Fri. Tel. 61593		LOW - NOISE CASSETTES C60, 32p C90, 41p C120, 52p
		,,,,,,,	

-the lowest prices

BI-PAK QUALITY COMES TO AUDIO! AL10/AL20/AL30 AUDIO AMPLIFIER MODULES **NOW WE GIVE YOU**



The AL10. AL20 and AL30 units are similar in their appearance and in their general specification. However, careful election of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.8. The versatility of their design makes them relation are in record players, rape recorders, -tereo amplithers and cassette and cartridge tape players in the car and at home.

Parameter	Conditions	Performance
HARMONIC DISTORTION	$P_0 = 3$ WATTS $f = 1$ K Hz	0.25%
LOAD IMPEDANCE		$8 - 16 \Omega$
INPUT IMPEDANCE	f – 1KHz	100 k Ω
FREQUENCY RESPONSE \pm 3dB	Po = 2 WATTS	50 Hz - 25KHa
SENSITIVITY for RATED O/P	$V_S = 25V$. $RI = 8 \Omega$ $f = 1 K H z$	75mV. RMS
DIMENSIONS		$3'' \times 24'' \times 1''$

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter		AL10 AL20		AL30	
Maximum Supply Voltage		25	30	30	
Power output for 2°_{0} T.H.D. (RL = $8\Omega f = 1 \text{ KHz}$)	3 watts RMS Min.		5 watts RMS Min.	10 watts RMS Mm.	
AL 20. 5 watts RMS f	E2 19 E2 59 E3 01	PA 12.	AMPLIFIER (Use with ALI (Use with AL3)	0 & AL20), £4-3;	
FRONT PANELS SP 12 with Knobs	88p	T461 (U T538 (U	se with AL10) se with AL20) (Use with AL30)	21-28 P & P 15; 21-28 P & P 15; 21-93 P & P 15;	

. PA 12. PRE-AMPLIFIER SPECIFI

The PA 12 pre-amplifier has been designed to match into most budget stereo systems. It is compatible with the AL 10, AL 20 and AL 30 audio power amplifiers and it can be supplied from their associated power supplies. There are two stereo inputs, one has been designed for use with "Ceramic cartridges while the auviliary input will sult most †Magnetic cartridges. Full details are given in the specification table. The four controls are, from left to Volume and on/off switch, balance, bass and treble. right: Size 152mm × 84mm × 35m

ICATION
Frequency response- 20Hz - 50KHz (- 3dB)
Bass control-
± 12dB at 60Hz Treble control-
± 14dB at 14KHz *Input 1. Impedance
I Meg. ohm
Sensitivity 300mV †Input 2. fmpedance
30 K ohnis
Sensitivity 4mV

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Electronics Today International Radio Constructor



50w PEAK (25w R.M.S.) **THERMAL PROTECTION!** The NEW AL60 **Hi-Fi Audio Amplifier** FOR ONLY £3.95

- Max Heat Sink temp. 90°c, Frequency Response 20Hz to 100KHz
- 0-1% Distortion
- Distortion better than 1% at 1KHz
- Supply voltage 10-35 volts 100
- Thermal Feedback Latest Design Improvements
- Load 3, 4, 8 or 16 ohms
- Signal to noise ratio 80dB
- Overall size 63mm × 105mm
- 1.3mm

Especially designed to a strict specification. Only the finest components have been used and the latest solid state circuitry incorporated in this powerful little amplifier which should satisfy the most critical A.F enthusiast.

STABILISED POWER MODULE SPM80

AP80 is especially designed to nower 2 of the AL50 APB0 is especially designed to power 2 of the AL50 mplifers, up to 15 wart (r.m.s.) per channel atmul-taneously. This module embodies the latest componenty and circuit techniques incorporating complete short circuit protection. With the addition of the Maina Tran-tormer MT80, the unit will provide outputs of up to 1.5 amps at 35 volts. Size: 63mm × 103mm × 30mm. These units enable you to build Audio 3ystems of the highest quality at a hitherto unobtainable price. Also ideal for many other applications including: — Disco Systems, Public Address Intercom Units, etc. Handbook available 10 **PRICE £3·25**

TRANSFORMER BMT80 £2.15 p. & p. 28p

STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages. Three switched stereo inputs, and rumble and scratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable have and trable controls.

bass and treble controls

SPECIFICATION An input strugger equalised to RIAA curve w Bass Control Treble Control Filters: Runble (High Pass) Serateh (Low Pass) Signal/Noise Ratio Teoret overload Input overload Supply Dimensions

35 volts at 20mA $292 \mathrm{nm}$ × $82 \mathrm{nm}$ 351 ONLY £13.15

SPECIAL COMPLETE KIT COMPRISING 2 AL50's, 1 SPM80, 1 BMT80 & 1 PA100 ONLY £25-30 FREE p. & p.



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NOW that we have a good idea of what effects the 1974 Budget will have, the time is right for a reappraisal of our spending. There are, as always, two sides to the coin-the reader who may also be a constructor and therefore component buyer; the advertiser or component supplier, usually doing his best to satisfy a demand or looking for a new sales line

Where shortage of cash and credit may well seriously affect the sales of commercial equipment, the devotee will look more towards cutting his costs by "doing-it" himself. There are, however, some areas that claim buoyant interest and of late this has been in the "ICE" (in-car entertainment) sector in particular.

IN-CAR ENTERTAINMENT

In this issue of Practical Wireless we are publishing two articles on ICE, one on commercial equipment, the other as a technical appraisal. In this latter one we show you a first class design that has been made and is now touring the country in the designer's car.

Of course this particular design was conceived before anyone really believed that the industrial situation was so serious. Here we have an example where energetic investigations to find readily available components for it may have been frustrated. Alas, there is now, not only a shortage of steel and other materials, but price increases are imminent.

We could not in all honesty, commit readers knowingly to become victims of this situation through a popular published project without warning. In particular there are problems in getting the push button tuner head, and other items used by the author: current output is concentrated on long standing orders with commercial manufacturers.

Even so, these difficulities do not deter us completely from publishing an otherwise excellent design for its own sake. We know that British ingenuity will come to the rescue as it so often does. Many of you will have old car radios that need up-dating. In most cases the tuner head mechanism may still be serviceable. Unfortunately we cannot tell you if yours is suitable; we can only suggest that you look into it thoroughly or ask a knowledgeable friend for advice.

COMPONENT SUPPLIES

Readers will probably have read or heard about other component shortages from some manufacturers, coupled with long delivery times and reorganised or rationalised stock holding. At retail level this is now being felt, although most of our advertisers may still boast large stocks. It all depends really on whether they have what you want at the right price.

We hear a great deal about the "information and communication rift" between suppliers and customers. On the one hand there are those suppliers who do not keep customers fully informed about delays, so aggravating customer relations and creating unnecessary complaints; on the other hand there are those constructors who do not make out their orders in a clear and concise manner, and often pose irrelevant questions or fail to send adequate money to cover VAT and carriage charges.

To solve all these problems to everyone's satisfaction is almost impossible with the limited resources at our disposal. What we can do is to help inform readers through the magazine.

BUYER'S GUIDE

We are planning to launch a special supplementary operation in the autumn aimed to provide readers with details of product lines and trading terms or retail component outlets. To carry any measure of value to both parties we need your help. However, there are limitations and we cannot hope to please evervone.

We shall be adding to our normal October issue an extra centre pull-out section which will contain information on components, components suppliers and trading terms. Unfortunately this has to be limited in size, so we shall be including further sections in the following three issues. You will be able to collate all these sections to form a valuable "Buyer's Guide" reference book which you will always want to keep handy.

INVITATION

Component suppliers in the retail sector, who sell through shops or by mail order, are invited to submit catalogues or price lists of components only that they always carry in stock or are likely to have in stock regularly by the end of 1974. Trading terms must be included stating minimum order charge (if applicable), carriage and packing terms and quantity discount arrangements (if any). Any non-availability or waiting time in excess of one month for items listed should be indicated. The closing date for sending information to us is 17th June.

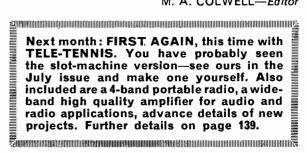
We regret that we cannot entertain telephone queries in respect of this operation. All correspondence should be addressed to "P.W. Electronic Components Buyer's Guide'', Practical Wireless, Fleetway House, Farringdon Street, London EC4A 4AD.

Component suppliers will be pleased to learn that extra space is being made available for inclusion of their own personal announcements in the booklet, offering a permanent record to all readers. Special publicity support is being organised so that the best advantage will be taken to circulate this information among a larger audience.

Full details of the advertisers' announcements facility are available from our Advertisement Manager and bookings for space (no matter how small) should be made by the 1st July for the October issue section and by 1st August for all subsequent sections

In undertaking this exercise we are confident that this Buyer's Guide will be welcomed by all readers. To make sure you do not miss out, we recommend you order your copies of Practical Wireless now.

M. A. COLWELL-Editor



NEWS ...

NEWS ...

The Source of Sound



A feature at this year's Ideal Home Exhibition was a pavilion which showed, in sound and vision, the development of sound recording from early wax discs. Five room-settings were on view, dating from 1920 to the present. Our picture shows the 1930's setting.

Weekend Course

WHAT now looks massive and dominant in our society, only 50 years ago was tentative and experimental.

The beginnings of radio lie deep in the past; indeed one could look back thousands of years to those persons whose curiosity was aroused by small amber beads becoming attracted after polishing. This was investigated by Gilbert in experiments with "electricity" shown to Queen Elizabeth I. There discoveries followed the of Ampere and Volta, Faraday, Maxwell. Hertz and Marconi, which prepared the world for what was to be one of the great revelations of all time-the means of communication by radio broadcasting.

The weekend course will range from the early inventions and inventors of wireless and television to reminiscences of Savoy Hill, while not too technical language will describe Radio and Television studios. The social impact of the growth of broadcasting will be reviewed and its reflection on programming.

The weekend is enlivened with

demonstration and illustration, using working exhibits and archive recordings --- Marconi ---Reith - Nellie Melba, leaning heavily on the tradition of Information - Education - and Entertainment. Antiquities will be on working display, a crystal set of 1920-the pre-broadcasting era and "fireworks" in the form of a replica of Marconi's spark transmitter and receiver. Modern high power equipment will be used for transmission and reception throughout the world, during the weekend, under the callsign GB2HF.

NEWS.

The weekend will begin on Friday 7th June (evening) in an amenable social atmosphere, cultivated in a comfortably furnished guest house and will be led by Mr. Ralph Barrett, C.Eng. MIEE, MIERE.

Further details may be obtained by telephoning 01-203-3381.

SORRY WE ARE LATE! We apologise for the late appearance of Practical Wireless. The delay has been caused by an industrial dispute in the printing industry.

HOW!

THE womenfolk of the Navajo Indian tribe were sitting round the camp fire one balmy, summer evening. One woman, who was sitting on a deer skin, had a son who weighed 140lb. Another woman sitting on a buffalo skin had a son who weighed 160lb. A third woman, who herself weighed a staggering total of 300lb, was sitting on a hippopotamus skin.

What mathematical theorem does this remind you of and why? *Answer at foot of page.

The aforementioned was extracted from the April issue of *The Cornish Link*, the official magazine of the Cornish Radio Amateur Club. Club call is G4CRC.

Subscription to the C.R.A.C. is $\pounds 1.25$ per annum. All enquiries should be addressed to the club p.r.o., Bill Locke G3NKE, "Hill-side," Kehelland, Camborne, Cornwall (Tel. Camborne 2419). Sheila Locke, G3NKE's xyl, is Editor of the Cornish Link.

The C.R.A.C. annual mobile rally will be held on July 21st, 1974 on the campus of the Cornwall Technical College, Pool, Redruth. Prospective exhibitors may obtain further information and stand details from Bill Locke.

Going Back

We have received a letter from Roger Goodman, who wanted some information on the instrument we included in our November 1973 issue (page 667). He says he would like to express his thanks to "Going Back" for the help he received in providing information on his "linesman detector". He received 21 replies and would like to sincerely thank those people who wrote to him, from Adrian Moss, aged 10, to a 71 year-old radio amateur.

*Pythagoras. Because the squaw on the hippopotamus was equal to the sons of the squaws on the other two hides. Hi!

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RICHARD COLLIN

THE first car radio receivers were essentially mains-type valve receivers with a special power supply. The 12 volt DC battery voltage was 'chopped' by a mechanical vibrator into a rough AC which was applied to a special type of power transformer, followed by considerable smoothing circuits. These receivers were very bulky and produced a large amount of noise from the vibrator. So much, in fact, that in many designs the power supply was separate to allow mounting outside the passenger compartment. These receivers were produced for almost 30 years until the transistor arrived on the scene.

Initially, only one transistor was used in the output stage. This led to a significant simplification of the receiver. Valves were still used in the earlier stages, although they were specially designed to operate with a 12 volt 'HT' rail, the receivers being known as 'hybrid' sets. The more expensive 'hybrid' receivers used a transistor driver stage and two power devices in a push-pull transformer output circuit. Up to 5 watts output could be provided into a 3 ohm loudspeaker.

The fully transistorised car receiver did not appear until high-frequency transistors became available at an economic price, when the car receiver underwent a complete change in design and the efficiency increased considerably. The old valve receivers consumed about 40 watts of power (3.5A at 12V) whilst the present generation of receivers require only 12W (1A at 12V). This reduction of heat output allowed more effective screening and helped to reduce size, the average car radio now measuring 7in x 2in x 4in deep, approximately.

CIRCUITRY

Fig. 1 is an example of the circuit of a modern car radio which, in general, is fairly standard, but there are some special considerations. The RF stages must be high gain and the AGC must be fast acting. The oscillator stages must have very low drift and the whole set must operate successfully over a wide temperature range. In addition, the power supply circuits must effectively filter out the spikes and transients and whistles produced by the car electrical system. Allowance also has to be made for connection to either negative or positive chassis cars.

AERIAL INPUT CIRCUITS

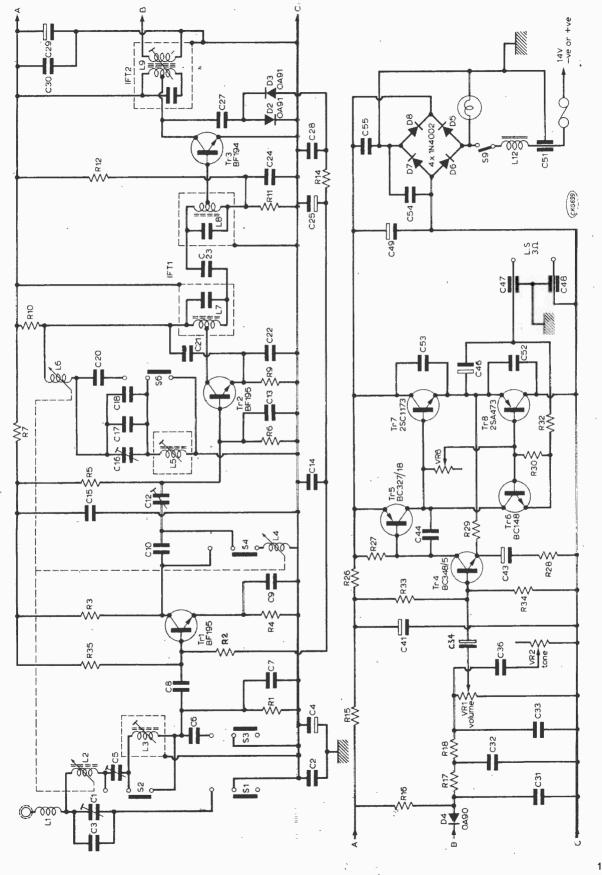
A car radio aerial invariably has a high value of capacitance resulting from the screened feeder that is used to minimise interference pick-up and the input circuits have to accommodate this. A pre-set capacitor (C5, Fig. 1) is provided to balance out the feeder capacitance. This is adjusted once and for all with the receiver finally installed in the car. The normal procedure is to 'trim' for maximum sound output whilst tuned to a weak signal on the high frequency part of the MW band. A similar function is provided by C1 on the LW band.

The tuned circuits (AE, RF and OSC) are provided by a ganged permeability tuner. L2 tunes the aerial circuit and L3 is a loading coil, switched into circuit on LW.

To achieve the high gain necessary in a car receiver a tuned RF stage is used. Transistor Tr1 is a conventional amplifier with AGC applied to the base circuit, via R2/R14, and a tuned circuit, L4, C10/C12 providing coupling to the next stage. L4 is also part of the permeability tuner. This is switched out of circuit on LW. The signal from the RF circuit is fed into the base of Tr2, the mixer oscillator stage.

The oscillator circuit is provided by L6 in conjunction with C16-18 on MW plus C20/L5 on LW. The reason for using C17 and C18 (200pF plus 220pF) instead of just one single capacitor is to provide temperature drift compensation. In the receiver shown C18 is an NTC capacitor with a coefficient of -1500 ppm. This compensates for any drift in the value of L6 and maintains an essentially stable oscillator frequency from -20° C to over 50°C.

The IF output is taken from Tr2 collector via IFT1 primary L7. The primary is capacitively coupled via C23 to the secondary L8 which feeds directly into the base of Tr3 the IF amplifier. The amplified IF is applied to the detector diode D4 via IFT2. AGC is developed by D2, D3 and fed back to the RF stage.



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Fig. 1. Circuit diagram of a typical modern car radio. Its operation is described in the text.

Bias is applied to D4 via R16 to improve signal quality at low output levels.

C31, R17, C32, R18 and C33 provide filtering for the signal. VR1 is the volume control and VR2 provides top-cut tone control in conjunction with C36. Transistors Tr4 to Tr8 form a conventional audio amplifier providing 5W output into a 3Ω load with a fully charged battery (14.4V).

Capacitors C53, C52 and the feed-through types C47, C48 and C51 provide RF filtering of the DC supply. LF smoothing is effected by L12 and C49. An interesting feature is the use of separate diodes D5-D8 which form a bridge rectifier, allowing connection to cars with either negative or positive chassis. An important feature of this design is the method by which the RF earth of the radio is DC isolated from chassis by C2 and C4, but connected to the car chassis by either D6 or D7 depending on the battery polarity.

RECENT TRENDS

The advent of low cost, high performance integrated circuits has recently brought further simplification to car receivers. The audio stages have been replaced by a power IC producing 4 watts output from the detector signal at the volume control. More recently complete AM subsystem IC's have appeared and these allow integration of the RF and IF stages so that it is now possible to produce a car radio with just two integrated circuits.

EXPERIMENTAL	TWO-IC CAR RADIO
Battery Supply:	12-16V, positive or negative chassis.
Power Output:	3·5W/4Ω or 4W/3Ω.
Tuning Range:	MW 185-577 metres. LW 1000-2000 metres.
Temperature Range:	-20°C to 60°C.
Active Devices:	RCA CA3123E RF-IF-OSC-AGC.
	SGS TBA810AS Audio

In the following pages a two-IC 4W car radio built by the author is described, the radio having been in use very successfully for over four months. It must be stressed that anyone wishing to build a similar receiver should ensure that they can obtain the permeability tuner unit before they begin work as these are not readily available to the home constructor.

A full circuit board layout and circuit description is given but the chassis work is left to the individual as it consists of little more than an aluminium surround with top and bottom plates.

CIRCUIT DESCRIPTION

The circuitry is shown in Figs. 2 and 3. The whip aerial is coupled via an RF choke, Ll, into the RF amplifier by a conventional car radio tuned input circuit consisting of L2 and capacitors C3, C4, C5 and R1. C3 is a preset capacitor which is adjusted only after the receiver is finally installed in the car. Its purpose is to balance out the capacitance of the aerial feeder and provide optimum power transfer into the RF stage. On LW, C1 and C2 perform a

★ components list

Resis	tors				
R1	2.2kΩ	R5	150kΩ	R9	100Ω
R2	1 ·2kΩ	R6	1.2kΩ	R10	1Ω
R3	3·3kΩ	R7	100kΩ	VR1	10kΩ log*
R4	330Ω	R8	27Ω		22kΩ log*

* concentric controls, ganged with S5, long bush

Capacitors

C1	390pf ceramic	C21	0·01µF
C2	30/140pf pre-set	C22	0-047µF
C3		C23	180pF ceramic
C4	47pF ceramic	C24	0.047µF
C5	1500pF	C25	0·1µĖ
C6	0.047µF	C26	470µF 6V
C7	470µF.10V	C27	0.0047µF ceramic
C8	0.1µF	C28	1500p É
C9	10µF 16V	C29	0-1µF
C10	47µF 16V	C30	100µF 16V
C11	390pF ceramic	C31	1000µF 25V
C12	180pF	C32	0 1µF
C13	470pF	C33	1000µF 25V
C14	30/140pF pre-set	C34	1000µF 25V
C15	180pF ceramic*	C35	0.1µF
C16	120pF polystyrenet	C36	
C17	0.015µF	C37	1000pF feedthrough
C18	10µF 16V	C38	
C19	56pF ceramic	C39	100µF16V
C20	0.0047µF	C40	0 · 1µF
* temp.	. coeff.—47ppm t		ppm

Inductors

L1 6µH RFC	L3 L6	Toko YXNS 6A139BA Toko YXNS 6A140HM
L4 Tuner, see note		see text
IFT1 Toko YHCS/1 IFT2 Toko YHCS/1 IFT3 Toko YHCS/1	A/ 589	R

Semiconductors

D1	0A90	IC1	CA3123E (RCA)
D2/5	50V 1.5A bridge	IC2	TBA810AS
			(SGS/ATES)

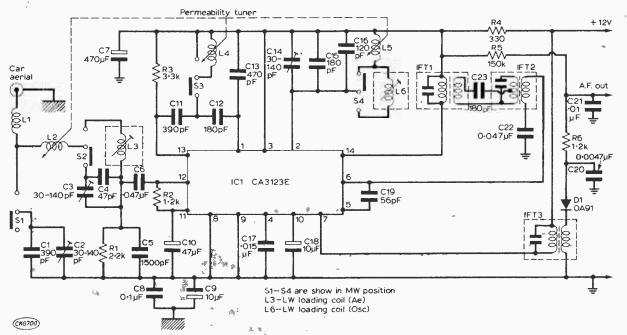
Miscellaneous

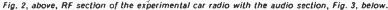
S1 to S4 are ganged. In the prototype a 6 pole changeover was used. For a manually tuned set the switch can be a 'push-on push-off' type. With a pushbutton set this switch is operated by the buttons changing from MW to LW automatically, in which case the return spring and lock must be removed from the switch. S5, on/off switch, is part of VR1/2 assembly. LP1, 14V LES buib and holder. F1, in-line fuseholder and fuse 1.5A.

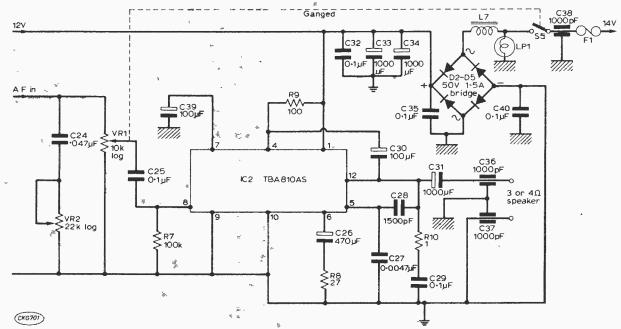
similar function while a loading coil L3 is also switched into circuit.

The RF stage is gain controlled by a frequency counter AGC circuit which allows control of the AGC response by selection of the coupling capacitor, C19. The output of the RF stage is coupled to the mixer stage by a further tuned circuit L4, C11, C12 and C13. On the LW the circuit is untuned and L4 switched out of circuit.

The oscillator stage is tuned by L5 together with Cl4, Cl5 and Cl6. On LW a further loading coil, L6, is switched into circuit. Because of the temperature range experienced within a car, extra care has to be taken in the design of the oscillator circuit. Temperature stability is provided by using three tuning





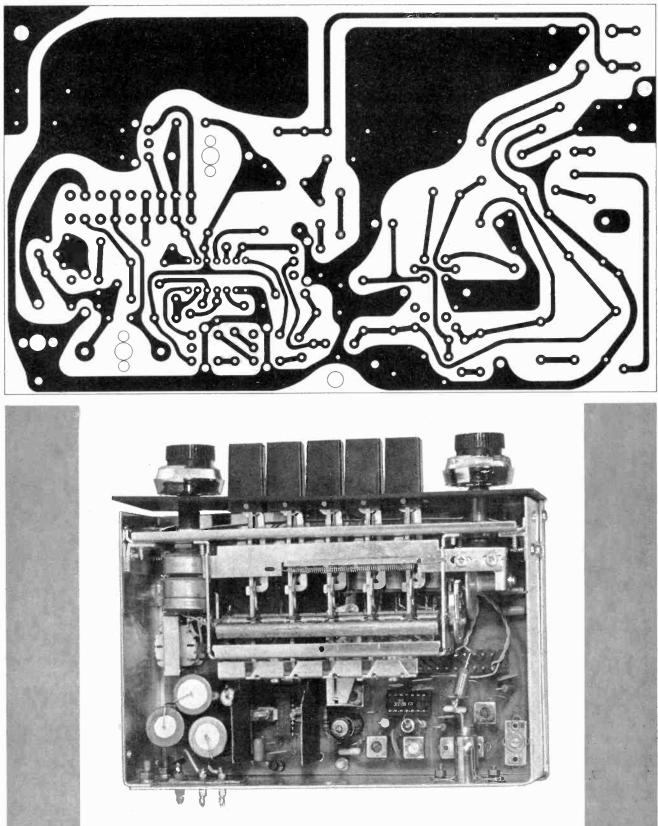


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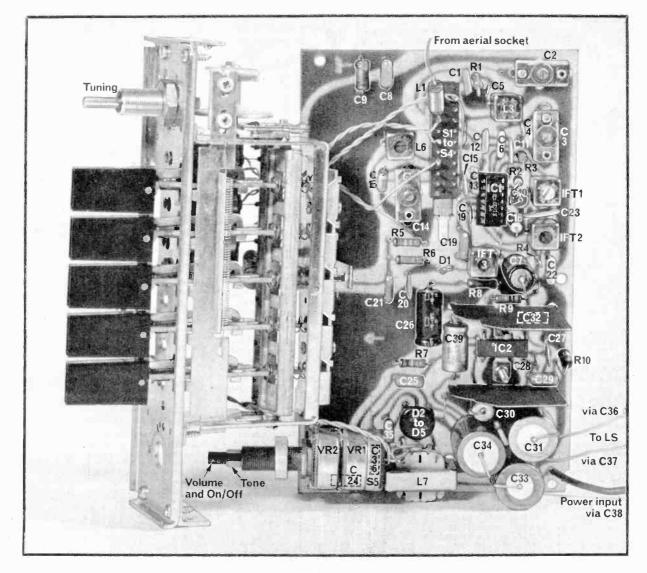
capacitors with specific negative temperature coefficients to compensate for any positive drift in the values of L5 and L6. The three main tuning inductors L2, L4 and L5 are ganged together in a complete permeability tuner which can have push-button facilities and automatic waveband switching.

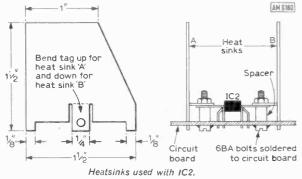
The IF output (470kHz) is taken from the mixer and coupled to the IF amplifier via a double tuned arrangement IFT1 and IFT2. After amplification the signal is fed to the detector diode via IFT3. The detected audio output is developed across the detector load formed by the volume control VR1. Capacitors C20 and C21 provide filtering in conjunction with R6. Top-cut tone control is provided by VR2 and C24. The gain of the audio amplifier is set by C26 and R8 which form a potential divider with the feedback resistor in the IC. Capacitors C27 and C28 determine the top frequency roll-off characteristic. A Zobel network (R10, C29) is effectively connected across the loudspeaker load which thus always appears essentially resistive to the output devices in the IC, protecting them from transients that could occur across inductive loads.

Capacitor C31 is sufficiently large to provide a lower bass limit of -3dB at 40Hz. Capacitors C36, C37 and C38 are ceramic feedthrough types used to further suppress RF interference by decoupling



At the top is shown the full size layout of the PCB. The photograph above shows the PCB and the tuner unit. The photograph at the top of the next page is of the PCB with component locations. The copper areas below are showing through the board.





the loudspeaker lines and the power input. The main smoothing is provided by the 1.5mH choke L7 and C32, C33, C34 and C35. These components greatly attenuate interference produced by charging and ignition circuits. Diodes D2-D5 form a bridge rectifier and provide automatic polarity correction, regardless of which battery pole is connected to the radio case. The earth rail is isolated from the chassis at DC by capacitors C8, C9, which have negligible impedance at RF so that the circuit is effectively earthed to the case.

Basically any three coil ganged permeability coil assembly designed for transistor car radio can be utilized. The type used by the author was an S. Bird type AW160. Probably the easiest way of obtaining a tuner is to order this as a replacement part via a radio dealer or car radio service agent. Either a push-button unit or coil pack only can be used. In the latter case it will be necessary to rig up some form of drive cord and scale pointer.

THE IGNITION CHOKE

Any small choke with an inductance of between 1.5 and 4mH will suffice. The winding should be less than 0.5Ω and able to carry approximately 1A DC. The author wound his own using a miniature transformer core found in the junk box, the winding being 100 turns 18swg enamelled copper wire.

The Toko IFT's are obtainable from Ambit International, 37 High Street, Brentwood, Essex as well as the TBA810AS which costs £1.50 inc. The CA3123E costs £1.98 inc. from Electronic Component Supplies, Thames Avenue, Windsor, Berks.



COLIN RICHES

In-car entertainment or ICE as it is popularly referred to, is a booming business and it does not matter whether you drive an 'old banger' or a gleaming Jensen, music on the move adds pleasure to your leisure.

In this article, I have chosen a selection of ICE units currently available. In some cases, I have quoted manufacturers' recommended prices, but if readers scout around, they will find some very efficient ICE items at quite reasonable discount prices.

Should readers require any additional information, they should write to the manufacturers concerned.

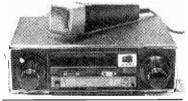
PHILIPS The RN712 plays stereo cassettes. It receives stereo radio programmes and long/medium waves. It records in mono from either radio or microphone and it costs £177.50. One can console oneself over the price however, by working out how much a separate tape recorder, stereo tape player, stereo tuner-amplifier and m.w./l.w. receiver would cost if they were

The RN712 must, without doubt, be classified as one of the most sophisticated in-car units on the market and it has a list of features as intriguing as Aladdin's cave.

Reception of f.m. signals is generally difficult in cars because the multiplex signal is extremely sensitive to interference. Philips have introduced an "I.A.C." circuit to overcome this problem.

The Interference Absorbtion Circuit (I.A.C.) operates on f.m., radio record and mono microphone functions. For the technical, it cuts off the interfering pulses on the audio signal by keeping constant the instantaneous value of this signal from the point just prior to the pulse becoming active until after it has passed on. Operation is limited to 50% of signal time as this cuts distortion which may occur from the absorbtion of too many interference pulses.

This unit will be featured in a Special Product Report in a future issue. Philips Ltd., Century House, Shaftesbury Avenue, London, WC2H 8AS,



AIWA The Aiwa TP-1042 stereo cassette player starts playing when a cassette is inserted and switches off, ejecting the cassette when the tape ends. The amplifier employs all silicon transistors and controls are provided for balance, tone, volume, fast forward wind and fast rewind. Johnsons of Hendon Ltd., Radlett Road, Colney Street, St. Albans, Herts., AL22EA.



EAGLE A very useful item from Eagle International is the FF.21 4-channel car stereo adaptor. It converts and synthesises an existing car stereo system with the addition of two extra loudspeakers. Any 8-track tape player, cassette player or f.m. multiplex receiver can be used with this unit, allowing 4-channel stereo to be enjoyed in the car.

The FF.21 we tested proved to be very effective. After making a few simple connections, the switch on the unit is turned to the '2 ch' position and the two front slider volume controls are set at maximum. The car stereo is then switched on with its controls set as usual. The 'rear speaker' control on the FF.21 is then turned anti-clockwise and the switch set to the '4 ch' position. The rear speaker control is then slowly turned clockwise and the full 4-channel effect is obtained. Eagle International, Precision Centre, Heather Park Drive, Wembley, HA0 1SU.



PYE Model 2253 is an auto-reverse cassette car player. Automatic track switching at the end of the tape is achieved by reversal of the tape running direction. Insertion of a cassette automatically switches on the unit and an illuminated indicator shows the direction of the tape travel. This unit can be fitted to cars of either polarity—a protection diode being fitted to prevent 'blowing up the works'.

When we tested the 2253 with the 'wick turned right up, the current drawn was 1A. Wow and flutter is quoted as less than 0.3% and frequency response as 40Hz to 10kHz, Output power is 3.5W per channel.

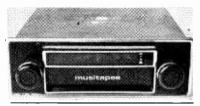
Normal fast wind and rewind facilities are provided and we found a C60 cassette rewound in 64 seconds.

We have had this unit in constant use over the last few months and it has performed without any troubles whatsoever. It is very thoughtfully designed and has excellent tonal quality. Recommended retail price, inclusive of VAT is £44-21. Pye Limited, P.O. Box 49, Cambridge.



MUSITAPES Model 8159 is an 8-track stereo cartridge player with a long and medium wave receiver. The control on the left is for on/off, volume and track change with a separate tone control. The knob on the right controls radio tuning and channel balance.

Output power is quoted as 10W and frequency response 30-10,000Hz. Speaker impedance is 4-8 ohms. Recommended retail price is £58 plus VAT. Musitapes (Wholesale) Limited, 402 Edgware Road, London, W2 1ED.

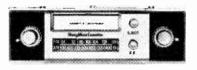


SANYO The FT 8006E is an 8-track stereo cartridge player combined with a m.w./l.w. and f.m. receiver. It has rotary on/off, volume, tone, tuning and balance controls and push-button waveband selection and track change. Output power is 6W per channel and frequency response is quoted as 30-10,000Hz. Operation is on uuoteu as 30–10,000HZ. Operation is on 12V negative earth vehicles only. Recom-mended retail price, including VAT is £64-75. Sanyo Marubeni UK Limited, Bushey Mill Lane, Watford, Herts.



HARRY MOSS Apart from marketing a good range of in-car equipment, this firm also supplies a 12V d.c. unit, operated from the mains and including speakers, that can be used to work car-type 8-track players and radios in the home.

One of their receivers which caught my eye was the 344 stereo cassette player and am./f.m. receiver. Output is 7W per channel and the circuit includes 2 i.c.'s, 28 transistors and 10 diodes. A fast-forward button for tape is provided and there is an indicator light to show when the radio is receiving a stereo programme. Harry Moss (London) Limited, 424 Kingston Road, London, SW20 8LJ.



JAVELIN The Javelin Continental PU612A is a m.w./l.w. receiver and an 8-track stereo tape player. It's a very neat looking unit which performs very well. The controls are easy to operate and an illuminated indicator shows which track the tape is playing at any given time. Output is 5W per channel and the price, excluding VAT is £67. Javelin Electronics Limited, 137-149 Goswell Road, London, EC1V 7EY.



HEATHKIT The CR9502 comes from the famous Heathkit stable and covers long and medium waves. Output power is 4.5W and a special circuit allows the unit to be connected to both positive and negative earth vehicles without re-wiring or changing any components.

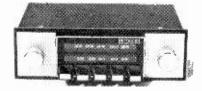
The circuit embodies two integrated circuits and sensitivity is quoted as 8μ V on medium waves and 30μ V on long waves. This kit comes complete with fully comprehensive and lavishly illustrated instruction manual and costs £19-80. We will be including a Second Destin

We will be including a Special Product Report on this receiver kit in a future issue. Heath (Gloucester) Limited, Gloucester, GI 2 6FF.



R & TV COMPONENTS The 'Tourist' comes in kit form at £6.60. It has 2.5W output and an i.c. output stage. It also employs a pre-assembled 3-stage i.f. module. We built up one of these kits from the instructions supplied and found it to work very efficiently. The ability to solder on a printed circuit board however is essential and we would not recommend the absolute beginner to tackle this one.

Radio & TV Components Ltd., 21 High Street, Acton, London, W3 6NG.



SHARP This stereo radio is designated AR/953. It employs a.g.c. and a.f.c. in the circuit and covers f.m. and medium waves. Output power is 5W per channel and recommended retail price £49.95 including VAT. Sharp Electronics (UK) Ltd., 48 Derby St., Manchester, M8 8HN.



PIONEER This Pioneer TP222 is a mini-sized 8-track stereo cartridge player designed to be fitted under the dashboard. The circuit employs 4 i.c.'s and 1 diode. Output is 3.5W per channel and frequency response is said to be 40Hz to 10kHz, wow and flutter less than 0.3% and S/N ratio more than 45dB. Price is £31.46 plus VAT and speakers are extra. Autocar Electrical Equipment Co. Ltd., 1 Chantry Road Industrial Estate, Kempston, Bedford.



HITACHI The WM702 retails at £17 90 (VAT paid) and covers I.w. and m.w. Output is 3W and speaker impedance 8 ohms. The circuit includes 7 transistors and 2 diodes. Supply voltage is 6/12V either positive or negative earth. This radio comes complete with brackets and mounting screws. Hitachi Sales (UK) Ltd., New Century House, Coronation Road, Park Royal, London, NW10 7QN.



BOSCH I have chosen the Blaupunkt ACR 845 from an excellent range of in-car equipment ranging in price from £30 to £300. This unit is an 8-track stereo cartridge player which plays back on 2 (stereo) or 4 (quadraphonic) channels.

Front panel controls include a tape 'head tuner' which compensates for discrepancies in track position between tapes, and slider controls for front and rear volume. The ACR 845 comes complete with fitting kit and four speakers and costs £83 50 including VAT. Bosch Limited, Rhodes Way, Watford, WD2 4LB.



RADIOMOBILE The 308 CSR is a long/ medium wave radio and stereo cassette player. The cassette ejects automatically at the end of play and within 10 seconds if the unit is switched off with cassette in position. Coming complete with two speakers, and fixing kit, recommended price is £67.95 inc. VAT. Radiomobile Ltd., North Circular Road, London, N.W.2.



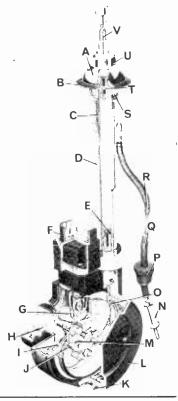
GRUNDIG This is the WK 2503 medium/ long wave receiver in presentation pack which includes fitting kit, speaker and baffle and suppression components. Output is said to be 5/7W, and circuit has tuned r.f. stage and 3-stage a.g.c. A socket is supplied for tape recorder connection. Price is £39-85. Grundig Ltd., Newlands Park, London, S.E.26.



PHILIPS have introduced a range of electric car radio aerials. They are compact, lightweight and corrosion resistant. There are three models: the Standard, Automatic and De-luxe Automatic and the prices, including VAT, are £13 50, £15 50 and £18 respectively.

An important feature of these aerials is the use of a small efficient motor claimed to give superior lift capability with a power consumption of only 600mA. A 12-month guarantee is also included and this covers free aerial replacement.

On the picture, (A) is brass/chromed dome, (B) plastic seal, (C) injected plastic sprung slides ensuring good contact between rods, (F) plug-in relay operates AE from radio on/off switch, (G) limit switch cuts motor at end of rod travel, (H) motor, (I) water-resistant compartment, (J) nylon gears, (K) drain hole, (L) nylon casing, (M) ball bearing clutch, (N) sprung cable, (P) grommet, (Q) correct capacity cable, (R) screening, (S) earthing bar, (T) serrated edge gives good contact with car, (U) mounting nut, (V) stainless steel rods.



MEMOREX The tape used to test some of the cassette machines in this article was the new Memorex MRX2 Oxide. It is claimed to have a distinct 2dB advantage over many competitive brands especially at high fre-quencies. It comes in C30, C45, C60 C90 and C120 sizes.



understanding

PART 1



A. FOORD

THE gain of an amplifier is usually stated as a single number, either as a ratio or in decibels. Although this is adequate for most practical purposes it does imply perfect linearity, or no distortion. In an ideal amplifier, where V is the input, A is the gain, and V_{out} is the output:—

$$V_{out} = AV$$

However, since practical amplifiers are not linear the input/output transfer characteristics will always be curved. The standard form usually assumed for this non-linear function is:—

$$V_{out} = A_1 V + A_2 V^2 + A_3 V^3 + \dots + A_n V^n$$

If we consider only two terms for this expansion and allow V to become the instantaneous voltage of a sinewave, we have:---

$$V_{out} = A_1 V \sin \omega t + A_2 V^2 \sin^2 \omega t$$

The second term may be expanded so that the result becomes:---

$$V_{out} = A_1 V \sin \omega t + \frac{A_2}{2} \times V^2 (1 - \cos 2\omega t)$$

The output from the amplifier now contains an unwanted second harmonic whose amplitude depends

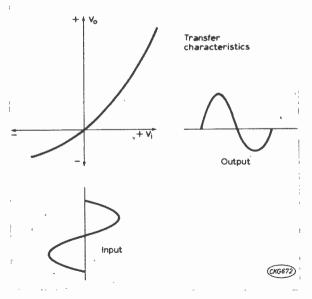


Fig. 1 : The generation of distortion by amplifier non-linearity.

on the square of the input level and the co-efficient A_2 . This means that if the input level is doubled we produce four times the amount of second harmonic distortion which is one reason why distortion increases rapidly with signal level. Similarly the third term in the original series will produce distortion with a strong third harmonic content.

Fig. 1 shows a typical transfer characteristic for an amplifier, with the resulting output signal. If the transfer characteristic for an amplifier is known then the distortion can be calculated by a graphical method. However, this approach is only feasible for a considerably non-linear transfer characteristic and in practice harmonic distortion has to be measured by electronic methods.

This simplified explanation shows what happens when a single frequency is amplified by an amplifier. In a practical system two or more signals are applied simultaneously to any amplifier. If this contains a non-linear element then mixing occurs. This produces not only fundamentals and harmonics of the signals, but also the sum and difference frequencies of the signals themselves and their harmonics. These sum and difference frequency components are called intermodulation products. For audio applications intermodulation measurements are probably more valuable than harmonic distortion measurements, although both are normally quoted.

Effects of Non-linearity

Since audio amplifiers are used for the transmission of music and speech any distortion causes a loss in quality. In music all harmonics up to and including the 6th will "harmonise" with the fundamental, while higher order harmonics may become disagreeable. In general, intermodulation distortion is more noticeable since the products are not harmonically related to the original signals. Although harmonic and intermodulation distortion must in theory be related through the shape of the transfer characteristic, there is no direct and convenient relationship in practice.

Measurement of Non-linearity

Rather than try to measure small deviations in the linearity of the amplifier transfer characteristics it is much simpler, and more sensitive, to measure the effects of non-linearity. Naturally the effects to measure are harmonic distortion using a single signal, and intermodulation distortion using two signals. In spectrum analysis the amplitude of each component is measured individually. This demands elaborate

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TEAK VENEERED SPEAKER CABINETS For & x 5in Speaker sin + Tweeter Sin + Tweeter 13 x 8in + Tweeter 13 x 8in + Tweeter 13 x 8in + Tweeter 12 x 13 x 54 13 x 8in + Tweeter 12 x 13 x 54 13 x 8in + Tweeter 12 x 13 x 54 13 x 8in + Tweeter 12 x 13 x 54 13 x 8in + Tweeter 12 x 13 x 54 13 x 8in + Tweeter 15 x 18 x 84 Sultable for P.A. or DISCO use; takes 12in. speaker unit. Size app (hambook 10p SGS EA1000 3W AMPLIFIER 100 DUE E2-45. Handbook 10p Solidev 15W Class B Solidev 15W Class B Audio Amp thick film IC: £1 · 50. Data 10p. 12 A 800 SW Audio 13 2 Unmarked 250m W Zenerdiode, 47V, 5 14 25 Unmarked 250m W Zenerdiode, 47V, 5 15 0 GE Dide OA47 equivalent. ALL COMPONENTS NEW AND UNUS 21 2 Special OFFERS + * MINIATURE MAINS TRANSFORMER BRI. 240V, SEC. 12V. 100	* SPECIAL	OFFER PRI	CE ★	3 chann Oilwhee	el sound-l	light£
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For 8 x 5in Speaker Sin + Tweeter 19 x 13 x 54 £ 13 x 8in + Tweeter 10 x 13 x 54 £ 13 x 8in + Tweeter 10 x 13 x 54 £ 13 x 8in + Tweeter 12 x 18 x 84 £ 12 n + Tweeter 15 x 18 x 84 £ 12 n + Tweeter 15 x 18 x 84 £ REXINE COVERED SPEAKER CABINETS Suitable for P.A. or DISCO use; takes 12in. speaker unit. Size app 18 x 18 x 81n. £ SPEAKER CLOTH Axallable in Black or Green; approx. width 54in. £1.75 MEADPHONES Type H-202, Features: Mono/stereo switch. Volume controls on a channei. Freq. response: 20-20,000Hz. Impedance: 4-16ohms. £ SGS EA1000 3W AMPLIFIER 100 Electrolytic Condensers MODULE £2-45. 250 Orabon resistors, ±, ±, 1, 2 watt 100 Electrolytic Condensers 250 Cleanic, Polytyrene. Silver Mica, 0 Condensers. Solidav 15W Class B BARGAIN COMPONENTS BARGAIN, Soliter Mica, 0 Condensers. Solidav 15W Class B Bib Assorted Tagstrips Audio Amp thick film 150 GE Diode OA47 equivalent. I.C. £1 50, Data 10p. 10 breact Polycarbonate, apts resulted. 120 Jone, efc. 10 breact Polycarbonate, space resulted. Module £3-75.						
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13 x 8in + Tweeter 10 ± x 17 x 6	8in + Tv	veeter	9	x 131 x	51	
121n + Tweeter 153 × 18 × 84	13 x 8in 13 x 8in		10	x 17 x	6	
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SPEAKER CLOTH Available in Black or Green; approx. width 54in. £1.73 HEADPHONES Type H-202, Features: Mono/stereo switch, Volume controls on a channel. Freq. response: 20-20,000Hz. Impedance: 4-16ohms. £ SGS EA1000 ELECTRONIC COMPONENTS BARGAIN COMPONENT PACKS SW AMPLIFIER Iso Carbon resistors, 1, 1, 1, 2 watt MODULE 22-45. 1500 Electrolytic Condensers Solidev 15W Class B 200 Electrolytic Condensers Solidev 15W Class B 250 Fleintomaters, assorted Audio Amp thick film 525 Speintomaters, assorted I.C. £1-50. Data 10p. 130 Umarked 200mW Zenerdiode, 47V, 5 UA041 5W Amplifier 150 GESourde Tassitors. Module £3-75. 15 OSE Diode OA47 equivalent. ALL COMPONENTS NEW AND UNUS £1 + 25p p.p. per pack, £5 for 5 packs p/f Lact off approxements. 32 Unmarked 200mW Zenerdiode, 47V, 5 Module £3-75. 55 SE Diode OA47 equivalent. ALL COMPONENTS NEW AND UNUS £1 + 25p p.p. per pack, £5 for 5 packs p/f Lact Components New AND UNUS £1 + 25p p.p. per pack, £5 for 5 packs p/f Price 10m-459, 1000-69p ea. 1000-59p ea. 10,000-40p ea. 3 CORE PVC INSULATED MAINS CABLE. GREY ML6650. 3x 7/0-27 Price 10m-459, 1000-60p ea. SORE PVC INSULATE	REXINE CO	VERED S	PEAKER	CABINE	TS	
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SGS E A1000 Pack No. 3W AMPLIFIER 1 500 Carbon resistors, ±, ±, 1, 2 watt MODULE £2-45. 1 500 Carbon resistors, ±, ±, 1, 2 watt Handbook 10p 100 Electrolytic Condensers Solidav 15W Class B 250 Polyester, Polycarbonate, Paper, 10 Condensers. Audio Amp thick film 525 Polentiometers, assorted Audio Amp thick film 525 Polentiometers, assorted Inc. £1-50, Data 10p. 100 Electrolytic Condensers. UA041 5W Amplifier 10 50 Freset Potentiometers. Module £3-75. 15 0 FE Dode OAY equivalent. ALL COMPONENTS NEW AND UNUS £1 + 25p p.p. park, £5 for 5 packs p/f ★ SPECIAL OFFERS ★ * MINIATURE MAINS TRANSFORMER BRI. 240V, SEC. 12V. 100 Manuf: Hinchley Slize: 36 x 45 x 40mm. Price 100-45p ea. 1000-5p ea. 10,000-40p ea. 3 CORE PVC INSULATED MAINS CABLE. GREY ML6550. 3x 7/0-2 Price 100-45p ea. 1000-5p ea. Price 100-45p ea. 1000-5p ea. 247mid, 59V. MYLAR FILM CAPA CITOR. Size 1' x 0·35' x 0·65' for Mount. Price 100-45p ea. 247mid, 59V. MYLAR FILM CAPA CITOR. Size 1' x 0·35' x 0·65' for Mount. Price 100-45p ea. 247 x 1½in. 90p ea.			EL	ECTRON		ONENTS
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13 30 Unmarked OC11 Transistors. 14 25 Unmarked 250mW Zenerdiode, 4-7V.5 Module £3-75. 15 50 GE Diode OA47 equivalent. ALL COMPONENTS NEW AND UNUS £1 + 25 p.p. per pack, £5 for 5 packs p/f ★ SPECIAL OFFERS ★ ★ MINIATURE MAINS TRANSFORMER BRI. 240V, SEC. 12V.100 Maintature MAINS TRANSFORMER BRI. 240V, SEC. 12V.100 Maintature MAINS TRANSFORMER BRI. 240V, SEC. 12V.100 Maintature MAINS TRANSFORMER BRI. 240V, SEC. 12V.100 Maint. Hinchley Size: 36 x 45 x 40mm. Fice 100-4:59. 100-50p ea. 3 CORE PVC INSULATED MAINS CABLE. GREY ML6650. 3 x 7/0-2 Price 100-4:59. 100-50p ea. 1000-50 ea. 1000-4:3p ea. 24 x 1½ x 1½in. Stop ea.	3W AMPLIFII MODULE £2- Handbook 10 Solidev 15W Audio Amp Circuit £3-6	45. p Class B thick film 5.	No. 1 500 Ca 2 100 Ele 3 250 Ce Conde 4 250 Pot 6 250 Hig 7 50 Ass 8 11b As etc.	nsers olyester, F nsers. antiomete gh-stab, 1 orted Tag sorted nu	Polycarbor rs, assorte %, 2%, 5% strips ts, bolts, v	nate, Paper, ed (resistors. washers, spa
13 30 Unmarked OC11 Transistors. 14 25 Unmarked 250mW Zenerdiode, 4-7V.5 Module £3-75. 15 50 GE Diode OA47 equivalent. ALL COMPONENTS NEW AND UNUS £1 + 25 p.p. per pack, £5 for 5 packs p/f ★ SPECIAL OFFERS ★ ★ MINIATURE MAINS TRANSFORMER BRI. 240V, SEC. 12V.100 Maintature MAINS TRANSFORMER BRI. 240V, SEC. 12V.100 Maintature MAINS TRANSFORMER BRI. 240V, SEC. 12V.100 Maintature MAINS TRANSFORMER BRI. 240V, SEC. 12V.100 Maint. Hinchley Size: 36 x 45 x 40mm. Fice 100-4:59. 100-50p ea. 3 CORE PVC INSULATED MAINS CABLE. GREY ML6650. 3 x 7/0-2 Price 100-4:59. 100-50p ea. 1000-50 ea. 1000-4:3p ea. 24 x 1½ x 1½in. Stop ea.	3W AMPLIFII MODULE £2- Handbook 10; Solidev 15W Audio Amp Circuit £3-6 Handbook 15;	45. P Class B thick film 5. p.	No. 1 500 Ca 2 100 Eia 3 250 Ce Conde 4 250 Pc Conde 5 25 Pote 6 250 Hig 7 50 Ass 8 11b As etc. 9 25 Ass	nsers olyester, f nsers. entiomete gh-stab, 1 corted Tag sorted nu corted swi	Polycarbor rs, assorte %, 2%, 5% strips ts, bolts, v itches, rot	nate, Paper, ed (resistors. washers, spa
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6 • 47mfd. 56V. MYLAR FILM CAPACITOR. Size 1 * x 0 • 35 * x 0 • 65 * 1 Mount. Price 100-6 • 5p ea. 1000-5p ea. 10,000 - 4 • 3p ea. 240V. A.C. SOLENOID. Reversible operation; twin coll. Size app 2≵ x 1 ± x 1≵in. 90p ea.	3W AMPLIFII MODULE £2- Handbook 10; Solidev 15W Audio Amp Circuit £3-6 Handbook 15; TBA 800 5V I.C. £1-50. Da UA041 5W Module £3-75 MINIATURE Price 1-65p. 1	45. P Class B thick film 5. V Audio ata 10p. Amplifier ; MAINS 100-60p ea.	No. 1 500 Ca 1 500 Ca 2 100 Ele 3 250 Ce Conde 4 250 P(C 5 25 Pott 5 25 Pott 5 25 Pott 15 30 Pret 13 30 Unr 13 30 Unr 15 50 GE ALL COP 21 5 PECIAI TRANSFC 1000-50P	Naers Neets naers entiometer ph-stab, 1 orted Tag sorted nu sorted sw; etc. set Potent narked 250 5V, 91V, state vol Diode O/ MPONEN p.p.per L OFFER RMER a. 10,000–	Polycarbor rs, assorte %, 2%, 5% strips ts, bolts, \u00ed tches, rot iometers, c71 Trans mW Zeneir 10V. Mea tages requive TS NEW back, £5 (f S \u00ed K BRI. 240V, Manuf.: H SILe: 36 x F.C. 53mrt 40p ea.	hate, Paper, d fesistors. washers, spa rary, lever, n listors. diode, 4-7V, sured and te ulred. AND UNU or 5 packs p SEC. 12V. 10 inchiey 45 x 40mm. D.
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Goodmans Twinaxiom 10, 8 or 15 oh Kef T27 Kef T15 Kef B110 Kef B200 Kef B139	m £7.61 £4.75 £5.75 £6.75 £7.50 £11.75
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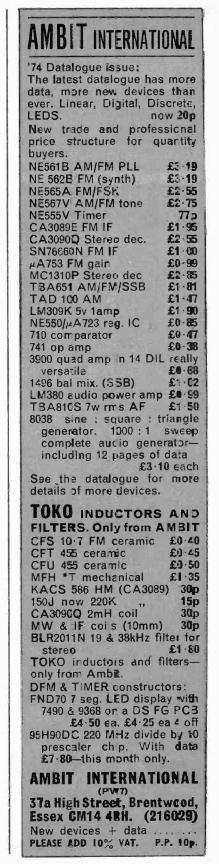
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test equipment but gives detailed information on the distortion mechanisms for design work. The other standard measurement methods give no indication of the relative amplitudes of the various components, and are therefore more suitable for routine testing.

Causes of Non-linearity

There are many causes of non-linearity, and include:----

- 1 The inherent curvature of the amplifier transfer characteristics.
- 2 Mismatch between halves of push-pull stages, which causes an excessive even harmonic distortion for class A and AB stages.
- 3 Cross-over distortion in class B push-pull stages, which may produce an increase in percentage distortion as the signal amplitude is reduced.

Spectrum Analysis

In spectrum analysis the amplitude of each individual frequency component of a waveform is measured separately, and these components can be summed to calculate a total harmonic distortion factor if required. This instrument is called a spectrum (or wave) analyser or a frequency selective voltmeter. It can be designed on two different principles, but is essentially a narrow band filter which can be tuned over any part of the audio band. It can be used to measure harmonic distortion as shown in Fig. 2.

The bandwidth of the filter is very narrow, perhaps 3Hz, so that it is possible to measure the amplitude of any selected harmonic without measuring an unwanted harmonic or the fundamental. If for example the fundamental were 1V and the amplifier output had a 2nd harmonic content of 0.01%, then the analyser has to measure a 0.1 mV signal at 2kHz without reading the 1V fundamental. This 80dB dynamic range illustrates the complexity, and hence cost, of this technique.

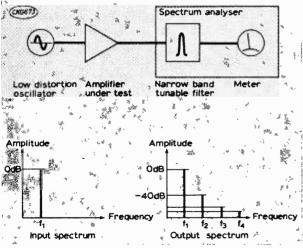


Fig. 2: Harmonic distortion measurement by spectrum analysis.

A low distortion input signal is applied to the amplifier under test, and the spectrum analyser is used to measure the amplitudes of the fundamental and each harmonic in turn. This measurement can be made either in absolute terms, or as shown in the figure, in relative terms. If a single figure is required for total harmonic distortion the terms can be summed on an RMS basis. Then total harmonic distortion D% is given by;—

$$\mathsf{D} = \frac{\sqrt{\mathsf{V}_2^2 + \mathsf{V}_3^2 + \mathsf{V}_4^2}}{\mathsf{V}_1} \times 100\%$$

For example, if:

$$V_1 = |V|$$
 (Fundamental)
 $V_2 = 0 \cdot 1mV$ (2nd Harmonic)
 $V_3 = 0 \cdot 3mV$ (3rd Harmonic)
 $V_4 = 0 \cdot 1mV$ (4th Harmonic)

Then:--

$$D = \frac{\sqrt{0.12 + 0.32 + 0.12}}{1000} \times 100\% = 0.033\%$$

A similar arrangement can be used to measure intermodulation products, as shown in Fig. 3. To simulate actual operating conditions the two frequencies and their relative levels can be varied, producing an infinite variety of test conditions! In instrumentations applications these values would be chosen to represent particular test requirements, but for audio applications two standard methods may be used.

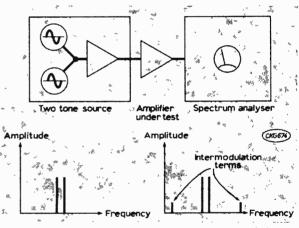


Fig. 3: Intermodulation measurement by spectrum analysis.

One advantage of two frequency intermodulation distortion measurements is that the test signals need not have a low HARMONIC distortion content if suitable frequencies are used. For example if signals of $1 \cdot 1 \text{kHz}$ and 900Hz are used, then possible intermodulation terms are:—

The harmonic distortion terms inherent in the two sources will be

2A	2·2kHz	and	2B	1.8kHz
3A	3·3kHz		3B	2·7kHz
4 A	4∙4kHz		4B	3.6kHz
et	TC .			etc

These harmonic distortion terms are well separated from the intermodulation terms, allowing them to be distinguished on the spectrum analyser.

Distortion Factor Meter

If a plot of total harmonic distortion against frequency is required for several different amplifier power levels then it is laborious to use a spectrum analyser and calculate the results. The distortion factor meter is designed to make such measurements quickly and simply, but cannot indicate the individual distortion components. The basic block diagram is shown in Fig. 4.

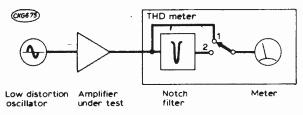


Fig. 4: Total harmonic distortion measurement.

The fundamental is eliminated by a narrow band rejection filter and the total harmonic content of the residue measured. The narrow band filter may be a bridged or parallel T or a Wein bridge and can be tuned over the audio band. When the switch is in position 1 the fundamental plus distortion is measured, while in position 2 the distortion only is measured. Then the THD is given by:

THD =
$$\frac{\sqrt{V_{2^2} + V_{3^2} + V_{4^2} + \dots}}{\sqrt{V_{1^2} + V_{2^2} + V_{3^2} + V_{4^2} + \dots}} \times 100\%$$

In normal audio equipment the distortion is low (less than 1%) and this expression approximates to the previous equation:

$$\Gamma HD = \frac{\sqrt{V_{2^2} + V_{3^2} + V_{4^2} + \dots}}{V_1} \times 100\%$$

This assumes that the final detector and meter measures a true RMS value. In practice such meters are expensive, and either an average or pseudo-RMS reading meter may be used. A pseudo-RMS reading meter uses diodes or other non-linear elements to give a reading which is approximately correct for waveforms with a high harmonic content such as a squarewave or noise. When an average reading meter is used the difference between this and the correct RMS reading is less than 1 part in 100 even for distortions of up to 14% and may be ignored. However true RMS reading meters are important for some other applications.

CCIF Intermodulation Measurement

As previously discussed the main advantage of the two frequency methods of intermodulation measurement is that a very low distortion source may not be required. There are methods to CCIF (Comite Consultatif International Telephonique) and SMPTE (Society of Motion Picture and Television Engineers) standards. The two methods may give widely differing results and it is revealing to use them both in performance measurements. For the CCIF measurement the test signal consists of two sinewaves of equal amplitude but close together in frequency. The basic block diagram is shown in Fig. 5.

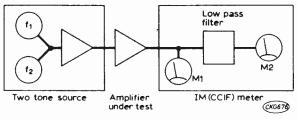


Fig. 5: Intermodulation distortion measurement (CCIF standards).

Two frequencies (perhaps $1 \cdot 1 \text{kHz}$ and 900Hz) are summed and applied to the amplifier under test. The low pass filter removes all the odd order intermodulation products, $(2f_1-f_2)$, $(3f_1-2f_2)$, etc, and the sum components, (f_1+f_2) , $(2f_1+f_2)$, etc. The even order intermodulation products, (f_1-f_2) , $2(f_1-f_2)$, $3(f_1-f_2)$, etc, are indicated on a peak reading meter M2. This is compared with the peak reading on M1 for the input signal and the IM distortion calculated:—

$$1M(CC1F) = \frac{M2}{M1} \times 100^{\circ}{}_{o}$$

Although this technique only indicates an intermodulation distortion figure obtained by measuring certain even order components it is still useful for routine testing.

SMPTE Intermodulation Measurement

In the SMPTE method two tones widely separated in frequency are used, with the amplitude of the low frequency f_1 being four times that of the high frequency f_2 . Typical frequencies would be lkHz and 10kHz. When this two tone signal is amplified by a non-linear system the intermodulation will produce sidebands symmetrically spaced about f_2 . For example, $(f_2 \pm f_1)$, $(f_2 \pm 2f_1)$, etc. The basic block diagram is shown in Fig. 6.

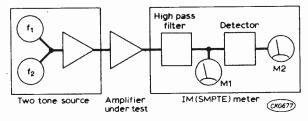


Fig. 6: Intermodulation distortion measurement (SMPTE standards).

In the measurement the low frequency tone f_1 is removed by a high pass filter, leaving an amplitude modulated waveform at a carrier frequency of f_2 which is detected and indicated on M2. The intermodulation distortion is given by the conventional expression for modulation depth.

IM (SMPTE) =
$$\frac{\text{sidebands level}}{\text{carrier level}} = \frac{M2}{M1} \times 100\%$$

Practical Information

When measurements are made on an amplifier using the techniques discussed it is found that there is no simple rule for comparing the different results, and each technique has its own advantages and disadvantages. Most published amplifier specifications



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SPEAKER BARGAINS £ EMI 13" x 8" 3, 8 or 15 ohm 2:05	ELAC 8" 8 ohm Duaicone 2 10 ELAC 8 ohm Duaicone 10 watt 3 35				
With Co-Axial Tweeter 2:20 Twin Tweeter 3:55 Type 350 8 or 15 ohm,	ELAC 8" 8 ohm Duaicone 2.10 ELAC 8 ohm Duaicone 10 watt 3.35 FANE 7" x 4" 3 or 8 ohm 1.00 8" Duaicone 8 ohm 2.40 CELESTION 8" 15 ohm 1.55				
20 watt 8 •00 6 <u>4</u> ″ 8 ohm, 10 watt 2·70 8″ 8 ohm, 10 watt 3·75 12″ 8 ohm, 20 watt 5·59	ADASTRA 10" 8 or 15 ohm, 10 watt 3 05 BAKER GROUP 25 12" 8 or				
8 8 0 hm, 10 watt 3 75 12" 8 0 hm, 20 watt 5 50 8" x 5" C/Mag. 5 watt 1 20 8" x 5" Dualcone	15 ohm, 25 watt				
GOODMANS 61 8 ohm	5″ 8 ohm, 5 watt C/Mag •85 2½″ 8 ohm or 64 ohm •50				
Dualcone 1.60 TWEETER & CROSSOVER EMI 3½ 3 or 8 ohm C/Mag 1.00	P. & P 10 Dome Tweeter 8 ohm, 30 watt 4-85				
Cone Tweeter 8 or 15 ohm, 10 watt 2.40	Crossovers CN23 (3 ohm), CN28 (8 ohm), CN216 (16				
Cone Tweeter 8 ohm, 3 watt 1 40 Horn Tweeter 8 ohm, 20 watt 5 85 KIT FORM CABINETS TEAK V	ohm)				
12 x 12 x 6 with 8" 8" x 5" or 64" and 34" cut out 2.45	18 x 11 x 9 with 13" x 8" cutout for EMI 350 4-25				
17 x 10 x 9 with 8" or 13" x 8" cutout	P. & P. ea. 35				
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switch crystal 1.55 DM160 Dynamic uni-dir, ball metal 3.95	Cassette Stick Mike with R. Control on/off switch (2·5 & 3·5mm J/Ply) 1·35				
UD130 50K/600 ohm, uni-dir ball me al	P. & P. →15				
SOLDERING IRONS ANTEX CN240 15 watt 1.60 SK 1 Kit (15 watt Iron	X25 25 watt (low leakage) 1.60				
CARTRIDGES ACOS GP91/2SC or GP91/3SC	P. & P. 10 19-TI Stereo crystal				
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give the total harmonic distortion curves for various power levels, but intermodulation methods are valuable for very low distortion levels (less than 0.25%). In general for intermodulation measurements the peak to peak input voltage should be the same as for simple harmonic distortion measurements, and all the frequencies involved should be within the pass band of the amplifier under the test.

Naturally the test signals should be combined in a way which does not introduce any intermodulation, the virtual earth summing amplifier is ideal, and the measuring instrumentation itself should be above reproach from a distortion and noise viewpoint.

Basic Causes and Cures

In a class B push-pull amplifier one output transistor conducts for one half of the cycle, and the other transistor conducts for the other half of the cycle. This gives an improved efficiency over a class A amplifier and is extensively used in audio power stages. However, due to the 0.6V base to emitter potential required for each transistor there is a region of input voltage around 0V where the output voltage is very small.

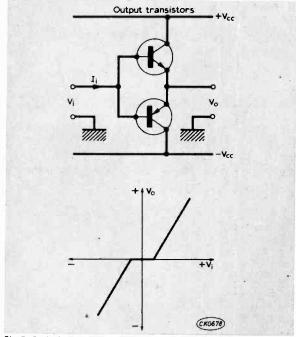


Fig. 7 : Distortion production in complementary class B emitter follower power amplifier output stage.

As shown in Fig. 7 this produces considerable crossover distortion and a reduction of gain in this region. The main problem in audio power amplifier design is the reduction of crossover distortion without degrading the thermal stability of the output stage, and many articles have been written on this aspect. The simplest remedy is to enclose the class B output stage within a negative feedback loop to reduce this distortion, as shown in Fig. 8.

The loop gain "forces" the input voltage of the output stage so that this non-linear transition is as rapid as possible. This arrangement has several disadvantages. Firstly, the amount of feedback needed is considerable and, secondly, the distortion has a high harmonic content so that the frequency

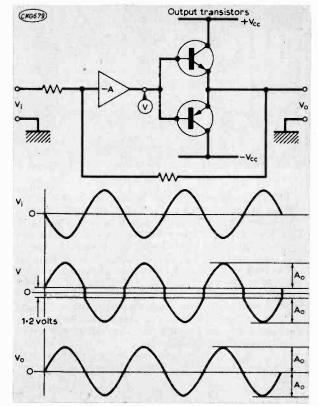


Fig. 8 : Reduction of distortion of output stage by overall negative feedback.

response around the loop has to be maintained far outside the audio band. If an amplifier had 2% distortion without feedback, and its gain were reduced by 26dB, we would now expect the distortion to be reduced to 0.1%.

For a conservatively designed system this would be correct in practice, and at low levels. However at high signal levels the slope of the input/output gain characteristics will change. It can be shown that although the 2nd harmonic distortion may be reduced, the 3rd and higher order distortions may be INCREASED by the feedback around the loop. The net result might be that the amplifier might actually need 35dB of feedback to reduce the THD to 0.1%. Clearly, it is important to reduce the distortion to an absolute minimum BEFORE applying overall feedback.

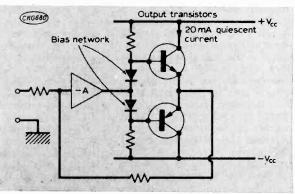


Fig. 9 : Distortion reduction in class B output stage by means of a small quiescent current.

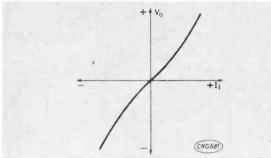
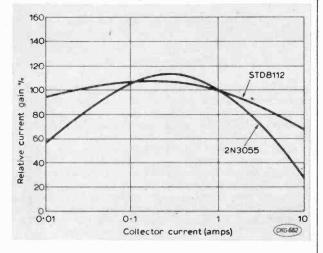


Fig. 10: A plot of output voltage against input current for the output stage of Fig. 7.

The basic circuit of Fig. 8 can be improved by biasing the transistors so that each conducts slightly even when there is no input signal, as shown in Fig. 9. This is very effective in reducing crossover distortion but may introduce the danger of thermal runaway. One treatment has the driver stage directly coupled to the load at low signal levels, but allows the output stage to conduct only at high signal levels. This gives a high efficiency but needs a special driver transformer. Another proposal adds a non-linear resistance network in the base circuit of complementary output transistors to compensate for the non-linear input impedance at low signal levels.





However since a transistor is essentially a current operated device, the output voltage of Fig. 7 more closely reproduces the input CURRENT, as shown in Fig. 10. There is still a residual non-linearity near the crossover due to the decrease in β at low current levels in the output transistors, and also non-linearity over the whole transfer characteristics due to changes over the whole region. The popular 2N3055 type is poor in this respect, with the triple diffused planar power transistor giving an improved performance at a price. This is illustrated in Fig. 11.

Since the input impedance of the output transistors becomes high when the input voltage is near zero, the current drive must be supplied from a high impedance source. At each zero crossing the transistor drive can more readily step the necessary 1.2V. If suitable precautions are observed then thermal stability is not impaired.

To be continued

TELEUISION

IN THE JUNE ISSUE

THE VLP SYSTEM

The Philips video long play disc system at present under development offers a reasonable cost home colour video playback system. The discs themselves are similar to conventional gramophone LP records and can be mass-pressed in the same way. The whole system has many ingenious features, from the way in which the full PAL signal plus sound is impressed on the disc as a modulated pattern of pits and scanned for playback by a laser to the signal encoding and automatic control techniques used.

PYE COLOUR RECEIVER FAULTS

Paul Soanes describes various fault conditions commonly experienced in the Pye group's 691, 693 and 697 single-standard colour chassis.

IC IF PREAMPLIFIER

Lack of gain in an i.f. strip can be overcome by adding a preamplifier between the tuner unit and the i.f. strip. The problem can occur when a different type of tuner unit is being used or a set is being assembled from various surplus units The preamplifier to be described uses a μ A703C i.c. and was designed for use in a colour receiver.

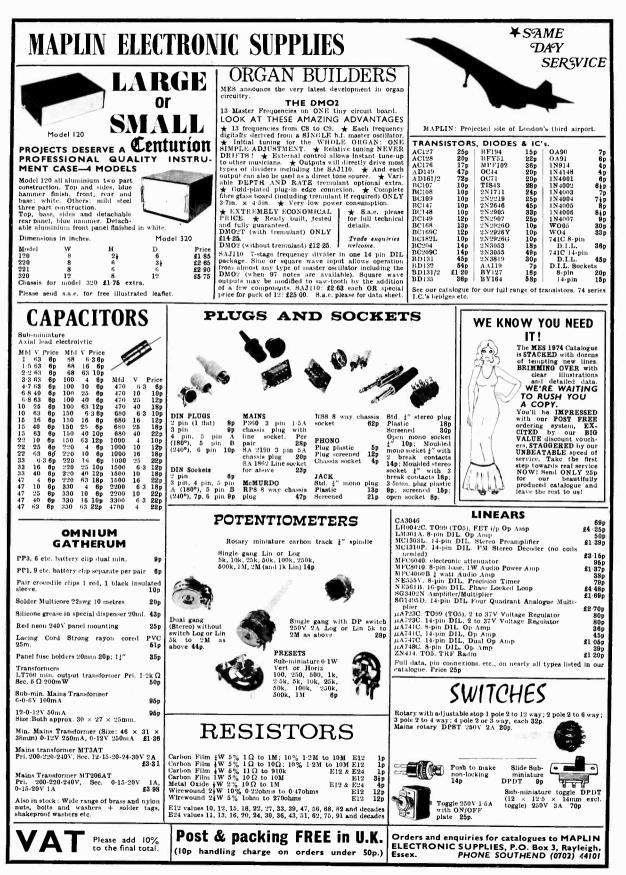
SERVICING TV RECEIVERS

The next chassis to be dealt with by Les Lawry-Johns is the Philips 300 series single-standard monochrome chassis.

PLUS ALL THE REGULAR FEATURES

Details of the June issue are subject to the current national situation at time of going to press.

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WITH the onslaught of local radio stations, BBC and IBA, to the medium wave band some form of frequency separation may be required in some areas. The writer decided to make something more compatible with the living room than the now famous PW frame aerial. Consequently it was decided to try a ferrite rod aerial as a possible solution. Of course, if the radio is a transistor one then it will almost certainly have an internal ferrite rod aerial so the set can be rotated to eliminate unwanted stations.

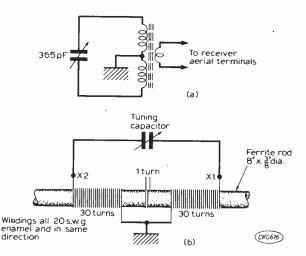


Fig. 1(a): Prototype circuit for medium waves only. (b) shows construction of circuit using a ferrite rod.

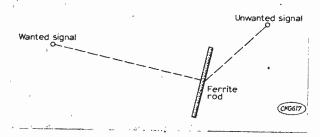


Fig. 2: The ferrite rod aerial has a broad maximum pick-up at right angles to its axis and a very sharp minimum off each end.

Results proved exciting and the circuit shown in Fig. 1a was effective in separating stations having only a small front-to-back angle, Fig. 2. It occurred to the writer to add another winding to the rod to cover the long wave band, Fig. 3. Going a step further another coil was added for the short wave bands, Fig. 4, according to the table. When fixing this coil on the rod tune to the highest frequency and slide the coil along the rod for maximum signal.

At this point thoughts turned to the possibility of switching the coils and producing an aerial tuning unit (ATU). The tuning capacitor can be changed for a two-gang capacitor and connected as in Fig. 5, using an external aerial.

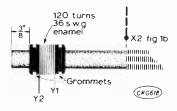


Fig. 3 : Construction of the long wave coil on one end of the ferrite rod.

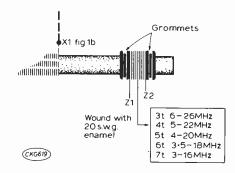


Fig. 4: The short wave coil at the other end of the rod, the number of turns depending upon the tuning range required.

Construction

Construction is simple, as shown in Fig. 1b and Figs. 3/4, the rod being mounted in a plastic or wooden case. The case must not be of metal, which would screen the rod aerial. First make the single turn link at the centre of the rod, holding it down with polystyrene cement or plastic insulating tape.

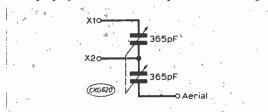


Fig. 5: When an external aerial is used the single tuning capacitor is replaced by a two-gang unit.

Next wind on the two 30-turn coils either side of the link and join their inner ends together and take them to earth. The outer end of each coil can be held with cement or under a grommet chosen to be a good fit on the rod. Do not be tempted to use more than one turn for the link. It may increase the signal transfer but will reduce selectivity. Add the short wave and long wave coils if these are required, Fig. 6.

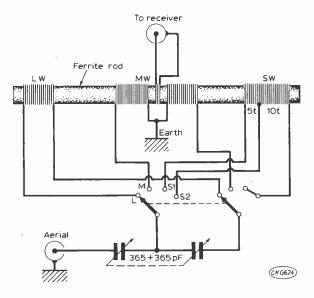
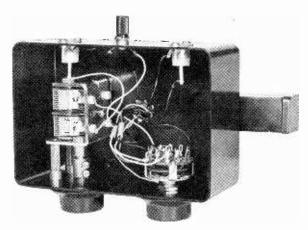


Fig. 6: The complete circuit as finally adopted. Complete short wave coverage is obtained with one tapped coil and range switch.

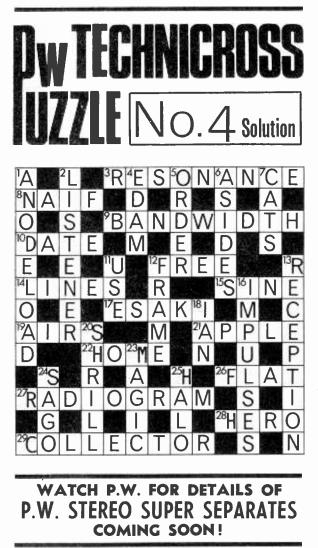
In use

If the receiver has an S-meter peak the wanted signal and then rotate the rod to eliminate the unwanted signal at the same time keeping the circuit tuned using the unit's tuning capacitor. A point will be found where the wanted signal level is acceptable, consistent with minimum unwanted signal. If the receiver has a manual RF gain control keep the gain as low as possible to prevent the signal operating the automatic gain control which would tend to negate any adjustments made.



The tuning unit is contained in a **plastic** box, the ferrite rod being mounted in the square **plastic** tube which swivels on top of the box.

It was found necessary to use a reduction drive on the tuning capacitor as the point at which an unwanted signal could be eliminated was quite critical.



If Wimbledon is washed out! Have a go with...

Have you seen those slotmachine games where you play tennis on a television screen? Now you can make your own! TELE-TENNIS is designed to be plugged into the aerial socket of a 625-line television set. Switch on and the game commences. The "court" outline is shown; you can move the two "bats" by simple controls; press the button and the "ball" is served.

Fascinating fun for all the family. Raise funds at garden parties, fetes, rallies or clubs. Part 1 in the July issue.



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The above details are subject to the national industrial situation at the time of going to press.

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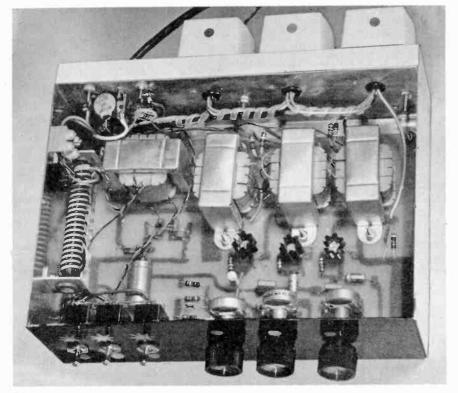
SOUND TO LIGHT CONVEN Peter Richards

O-DAY, many young electronics enthusiasts are involved with discos of one sort or another. For most of these some sort of light show is required. The unit described here will flash, in time with the music, three independent lamps, (or sets of lamps) up to 250 watts per channel. One lamp responds to bass, one to middle, and the other to treble. Also provided is a facility to turn any of the lamps on full, or off completely. The channels are identified as follows-Red for bass, Green for middle and Blue for treble.

AF CIRCUITRY

The audio input is applied to the filter network which divides it into treble, middle and bass. The signal levels in the three channels are controlled by VR1, VR2 and VR3 respectively. A master control is not required as the filter network, being entirely passive, cannot be overloaded. Each filter is based on simple tone control networks which favour the appropriate frequency range. The separation of treble, middle and bass is not complete, but is sufficient for this application.

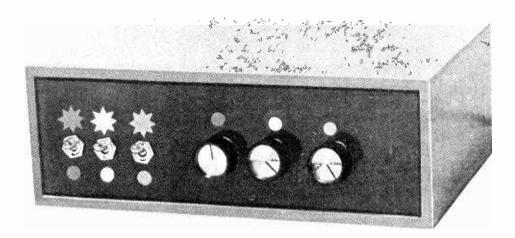
The following description applies to the Blue channel, the others are similar. The separated signal is passed through capacitor C8 to the base of Trl. This transistor is biased by R4 and normally draws about 100mA, so a small heatsink is required. The 6.3V winding of T2 forms the collector load, whilst the 240V winding goes to the SCR. Note this carefully. The change in collector current induces a large voltage across the mains winding and this is used to trigger the SCR.



This view shows the com-ponent layout. The SCRs shown here are in TO66 packages and are not widely available. A stud-mounted version is specified in the components list.

for the disco

TER



The power supply for the transistors comes from T1 via a standard rectifier arrangement. and gives about 18V DC on load.

SCR OPERATION

Without wishing to go too deeply into the theory of silicon controlled rectifiers (SCRs), some explanation of their operation may be helpful here. Normally an SCR will block current from both directions. However, when triggered by a positive voltage on the gate it conducts like a diode until the current through it is reduced to zero. With 50Hz AC mains the current reaches zero one hundred times every second, so there is no problem in turning the SCR off.

To trigger the SCR a current above a certain level has to flow through the gate and also, in this circuit, through R5, D5 and T2. If R5 is too small, the leakage through the SCR from the cathode will trigger the device and the lamp will glow. The value of R5 is therefore chosen so that this just fails to happen. This value depends entirely on the individual SCR and was found to lie between $47k\Omega$ and $180k\Omega$ for one batch tested, averaging about $150k\Omega$.

In most cases use of a preferred value resistor will be satisfactory. Occasionally it may be necessary to use the next higher value and connect a second resistor of $1M\Omega$ in parallel to achieve the desired effect. If R5 is too large, the Blue channel will be insensitive.

When an audio signal appears at the secondary of T2 it will be superimposed on the mains frequency voltage applied to the gate of SCR1. At some stage the two voltages will add and the resultant increase in gate current will trigger the SCR. Having fired, it will remain in conduction until the end of that mains half-cycle. The abruptness of the switching is smoothed out by the thermal delay of the lamp filament and so the overall effect is flashing in time with the music.

MAINS WIRING

The mains input is via a three core lead as a good earth is essential both for safety and for interference suppression reasons. The output is via three 13A sockets. The earth of these must be connected to the mains input earth.

When any of the switches is in the Bypass position

full power is applied to the lamp in question. With all three switches in the Bypass position the transformer T1 is switched off, thus removing the power supply from the transistors. If double pole switches are used, the poles should be connected in parallel.

To avoid shorts, hum loops, etc., the input circuit is not earthed except via R1 and C2, the static drain and spike suppression components. When connected to an amplifier the earth follows through from the amplifier.

INTERFERENCE SUPPRESSION

In the switching circuit used here the SCRs are firing at random points during the AC mains cycle. The resulting voltage transients can cause considerable interference to nearby radio and TV reception

★ components list

-										
	Resist	ors								
1		4·7MΩ		5.6ks			R11			
		10Ω 2W		22kΩ				22kΩ		
		47kΩ		See				See		
li		22kΩ		3 · 9k				W 10		
1	R5	See text	R10					n exc		
11	VR1	$100k\Omega \log$	VR2	10kΩ	10	9	VR3	100k	10	3
	_									
	Capacitors									
		1000µF	25V		8		= 25V			
	C2	47pF		C	9		μF			
	C3	0∙047µF	250 V A	C C	10	0.0)47μ ⊢			
	C4	0∙047µF	250VA	C C	11	-4μΙ	- 25 V			
	C5	0·1µF	250V A	C C	12	0.0)47µ⊦			
	C6			C	:13	10 ₁	F 25،	V		
	C7	0∙047µF				-				
	Semiconductors									
11	Tr1—Tr3 BFY52									
	D1D4 1N4002									
	D5-D7 OA81									
	SCR1—SCR3 CRS 3/40AF									
	BELOOG	llaneous								
1	MISCE	maneous		T 4 0	403			Rat	h +v	100
1	T1 2	240V: 12V	1A, 12	-14 2	4U \	1:0	V 2P	1_C2	SD/	00
	from	RSC (H	II-FI C	entre	5) 4 a v	⊾เ0 ∔.⊔	., J Antoi	nke f	or Tr	1-3
	250\	/ 3A; SK1-	5K3; L	1 266	iex	ų n	Jaisi	11671		,- U
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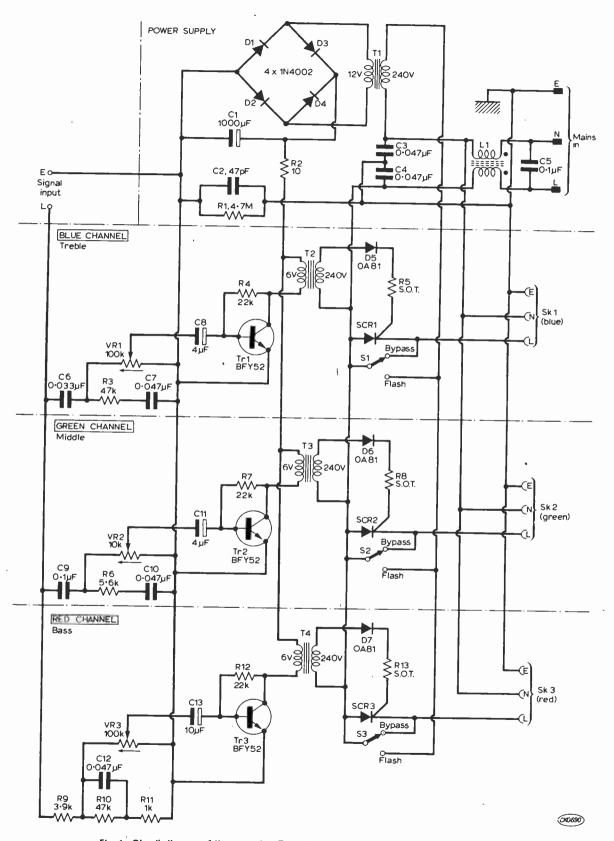


Fig. 1: Circuit diagram of the converter. The mains input should be via a suitably fused plug.

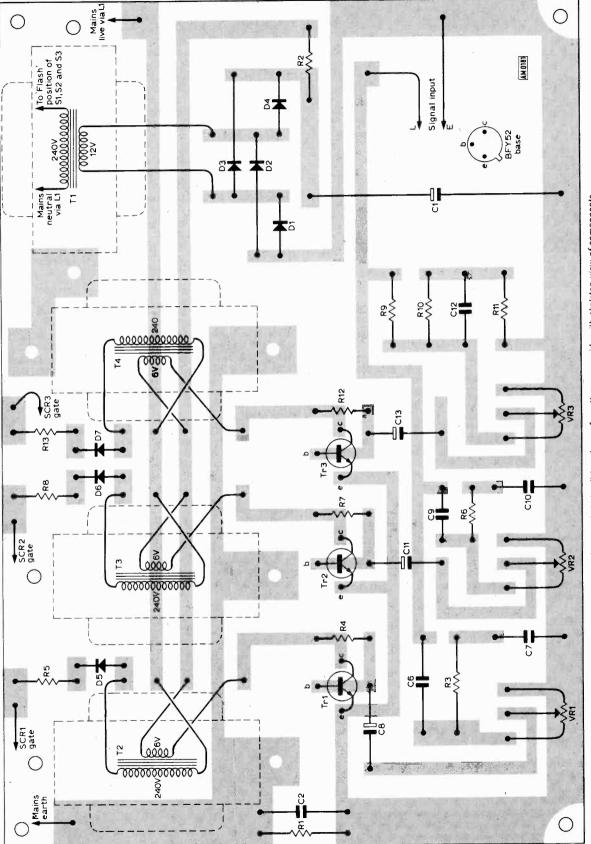
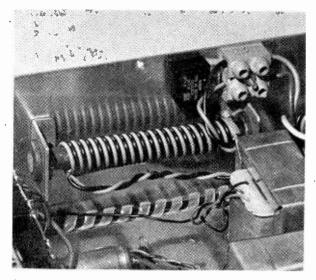


Fig. 2: Full size layout of the printed circuit board seen from the copper side with skeleton view of components.



Choke L1 is mounted on the left-hand end of the box using grommets and aluminium-angle feet.

and even to audio amplifiers. It is therefore essential to incorporate some form of suppression, which in this unit comprises C3, C4, C5 and L1, a bifilar-wound ferrite cored choke. Winding data for L1 is given later in the article.

As load currents are increased it becomes more and more difficult to obtain adequate suppression whilst keeping the filter circuits simple and inexpensive. The limit of 250W per channel is set for this reason.

The length of leads between the unit and the lamps also has quite an effect on the interference problem. These leads should be kept as short as possible—preferably not much over a couple of yards.

CONSTRUCTION

In the interests of reliability the unit was built on a printed circuit board housed in a $10 \times 7 \times 3$ in. aluminium box. The PCB should be mounted on spacers giving adequate clearance between the metal box and the printed tracks carrying mains potential.

The SCRs and switches are mounted on the box, the potentiometers are mounted on the circuit board. The three 13A sockets are fixed to a length of plywood which is bolted to the back of the box and provides a safety cover over the SCR anode studs. The ply must be recessed to clear the studs, otherwise leakage may occur via the wood with consequent risk of shock.

All four transformers are small enough to bolt direct to the PCB, though this should preferably be of fibre-glass to take their weight safely.

Exact drilling details are not given for the PCB because the layout may have to be changed slightly to allow for variation in component size, especially Cl. However, plenty of room is available on the board.

The SCRs are mounted using insulating kits and silicone grease. The anode leads are soldered to a busbar joining solder tags which are placed on the bolts holding the SCRs.

The mains wiring must be done very carefully, using wire of adequate gauge. The mains filter choke L1 is wound on a ${}^{3}_{8}$ in. diameter ferrite rod 4in. long. Each winding is 20 turns of 14/0.0076in. or 16/0.2mm pvc insulated wire, requiring a length of about 36in. including flying leads. The two windings are put on together so that the turns of one are between the turns of the other. Capacitor C4 must be mounted as close as possible to the SCR anodes.

When construction is complete the values for R5, R8 and R13 can be determined by test. It is suggested that Veropins are fitted to the circuit board in these positions, and the resistors soldered across them. In this way it is easier to experiment with different values.

Presets are unsuitable for R5, R8 and R13. Because of the voltages involved, small sparks from slider to track cause pitting. It is in order to use a preset initially to determine R5 etc., but it should be replaced by a fixed resistor afterwards.

Any channel may be omitted if desired. No other modifications are needed if this is done. Just omit the appropriate parts.

Finally a sleeve of ${}^{1}_{4}$ in. ply was made to go round the box and fixed to it by four self-tapping screws, which also secure the four rubber feet.

OPERATION

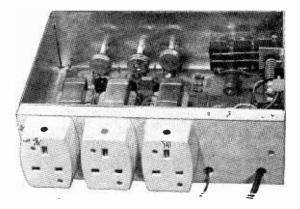
Turn all three controls to minimum, and all three switches to Bypass. Connect to amplifier and mains. Plug in 3 lamps, each should come on as it is plugged in. Set each switch to Flash, the appropriate lamp should then go out. With all three switches in the Flash position, play a record and advance each control until the corresponding lamp just flashes. Overloading spoils the effect.

The input to the unit comes from across one of the speakers. For good operation 2VAC or more is needed, but negligible power is taken. This represents slightly over 1W and should present no problem in any disco. Adjustments to volume, tone, etc. on the amplifier will probably mean that the controls for the lights need readjusting.

A domestic sound system operating at normal listening levels will probably not provide adequate drive for this unit.

The lights should be wired to a standard 13 amp plug, fitted with a 3 amp fuse, in the conventional way. All metal parts must be earthed.

Any lamps may be used but banks consisting of many low wattage bulbs, as opposed to 250 watt spotlights, flash better. The effect is improved by colours.



Input and output connections are at the rear. The live SCR studs are protected by the socket mounting block.



No. 60 LIGHT CONTROLLED OSCILLATOR

A series of simple transistor projects, using not more than twenty components.

THIS is a very simple project that employs a voltage controlled oscillator. Admittedly not a very sophisticated oscillator nor any guarantee of a well definable law relating voltage to frequency but the principle is so simple that it may prove an interesting sound source to electronic music experimenters. This application uses the output voltage from a photo-resistive cell/resistor combination (PCCI and VRI) to control the frequency of the signal.

Circuit

Tr1 and Tr2 are the active members of a fairly conventional free-running multivibrator; C2 and C3 form the timing element for one half of the cycle but the usual timing resistor from the base of Tr2 has been replaced by a resistor and Tr3, Fig. 1. Tr3 acts as an emitter follower and sets the potential at the top end of R2. It is this potential that governs the rate at which the voltage at the base of Tr2 rises, controlling the time of the other half of the multivibrator's cycle. The higher the potential at the top end of R2 the higher the frequency of the oscillator. This potential MUST, however, be greater than 600mV otherwise no oscillation will occur. This potential is controlled via the base of Tr3; any input voltage in the range of 1.2V to 4.5V on the base of this transistor will effect frequency control.

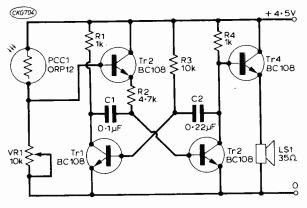


Fig. 1: Circuit of light controlled oscillator.

The lower portion of this range gives an exponential relationship between voltage and frequency but the law tends to linearise at the top end. In this application the control voltage is taken from the junction of PCCl and VR1; the potentiometer being used to set the input to respond to any range of ambient lighting. Any shadow falling on the cell will reduce the frequency. This could be caused by persons passing the detector or, with care, the hands could be used to control the shading and thus produce a "Theremin" type of music.

Alternative Inputs

There is no reason why other sources of input voltage should not be used provided that they fall in the correct range and comes from a source impedance not greater than $100k\Omega$. Note that only one half of the multivibrator's waveform is controlled hence it is not possible to maintain unity mark/space ratio. This could be effected, together with a wider range of frequency sweep, if the Tr3/R2 combination was repeated on the other side of the astable. The same voltage source could be used to drive both halves or, alternatively, two independent noninteracting voltage sources could be used for different effects.

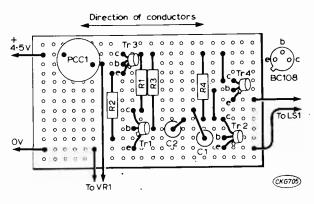


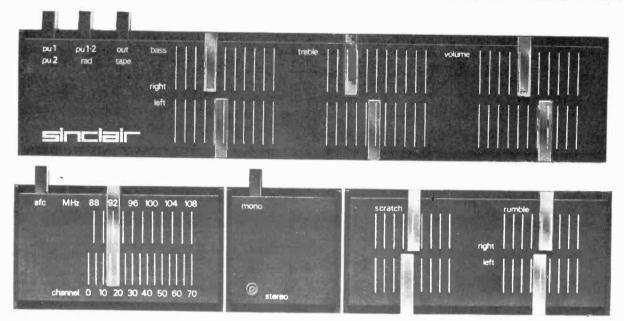
Fig. 2: Author's layout of circuit shown in Fig. 1.

A suitable layout of the unit on veroboard is shown in Fig. 2. VR1 could be mounted at the left end of the board provided the copper rails were broken to prevent short circuits. Finally, the board could be fitted in a box with a suitable aperture for the light to reach the photo cell, together with the battery.

★ components list

· · · · · · · · · · · · · · · · · · ·		-	124.
R1 $1k\Omega \pm W$	PCC1	ORP12	· • • • • •
R2 4.7kΩ	Tr1	BC108	- (<u>)</u>
- R3 10kΩ	Tr2 .	BC108	4 ×.
R4 1kΩ	Tr3	BC108	* <u>`</u> ``````
C1 0-1µF	Tr4	BC108	4 14 S
C2 0.22µF	LS1	35 ohm	(min) 🧹
VR1 10kΩ pot.	ę	ີ ຊີ ຕ ໂ 	. in the second
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Sinclair Project 80 exciting

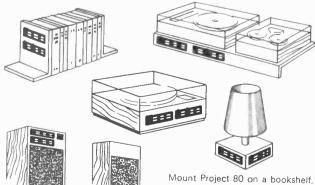


only $\frac{3}{4}$ " deep x 2" high

Living with hi-fi takes on new meaning with Sinclair Project 80. The electronics of these revolutionary new modules are all contained within elegantly designed matching cases no more than three-quarters of an inch deep. They are designed for mounting on any appropriate flat surface by means of 6BA bolts extending from the rear of each module and which pass through suitably drilled holes. Connections are taken away out of sight in a similar manner. The possibilities opened up by Project 80 are endless – superb hi-fi systems can be installed in ways hitherto only dreamed about and never before made practical. No more cutting out and shaping to put modules in position. A few holes drilled with the aid of templates supplied and the job is done. Now you need never again be faced with problems of keeping the hi-fi from clashing with carefully thought-out furnishing schemes. (That will surely please wives!) Slider controls have been introduced in place of knobs and all modules in the range incorporate new up-dated circuitry with emphasis on performance standards and built-in protection against overload and shorting. The aim was to re-think modular construction completely – to make it infinitely more versatile, even simpler and more reliable – the result – Project 80 – another triumph for Sinclair, and the most exciting construction modules ever.

the slimmest, most elegant hi-fi modules ever made

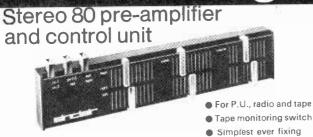
System	The Units to use	Units cost
Simple battery record player	Z.40	£5 45 + 54p V.A.T.
Mains powered record player	Z.40, PZ.5	£10·43 +£1.04 V.A.T
30W. RMS continuous sine wave stereo amp.	2 × Z.40s, Stereo 80; PZ.6	£30 83 +£3.08 V.A.T.
50W (8 Ω) RMS continuous sine wave de luxe stereo amp	2 × Z.60s, Stereo 80; PZ.8	£33·83 +£3.38 V.A.T.
Indoor P.A.	Z.60, PZ.8	£14 93 +£1 49 V.A.T



Mount Project 80 on a bookshelf, a loudspeaker, a lampshade base a false wall with two Q.16 loudspeakers...almost anywhere.

Project 80 FM tuner, decoder, and A.F.U. may be added as required

new thinking in modular hi-fi Z.40 & Z.60 power amplifiers



Each channel has its own separate tone and volume controls operated by sliders, enabling ideal environmental matching to be obtained. A virtual earth input stage forms part of the up-dated circuitry that ensures the finest possible quality from all signal sources. Generous overload margins are allowed on all inputs. Clear instructions with template are supplied.

TECHNICAL SPECIFICATIONS

 $\begin{array}{l} Size-260 > 50 \times 20 mm \left(10\frac{1}{4} < 2 \times \frac{3}{4} ins\right) \\ Finish-Black with white indicators and transparent sliders \end{array}$ Inputs - Magnetic pick-up 3mV RIAA corrected; Ceramic pick-up 300mV Radio 300mV: Tape 30mV

radio 300 mV: rape 30 mV Signal/noise ratio = 60 db Frequency range = 20 Hz to 15 KHz \pm 1dB. 10 Hz to 25 KHz \pm 3dB Power requirements = 20 to 35 volts Outputs = 100 mV + AB monitoring for tape Controls = Press button for tape radio and PU. Sliders for volume, bass (+12dB to = 14dB at 100 Hz) treble (+11dB to = 12dB at10 KHz)

R.R.P. £11.95 +£1.19 VA.T. Project 80 FM tuner and stereo decoder





Twin dual varicap tuning: 4 pole ceramic filter: switchable A.F.C.

 On the decoder, solid state stereo indicating beacon

Making the Project 80 F M, tuner and decoder available separately gives a wider choice of systems and saves money where stereo reception may not be required. The tuner is a triumph of electronic design and assures excellent performance. The decoder gives a 40dB channel separation with 150mV output per channel. Both, units may be used with other than Project 80 systems.

TECHNICAL SPECIFICATIONS OF TUNER $\begin{array}{l} \text{Size} = 85 \times 50 \times 20 \text{mm} \left(3\frac{1}{2} \times 2 \times \frac{3}{4} \text{ins} \right) \\ \text{Tuning range} = 87 \cdot 5 \ \text{to} \ 108 \ \text{MHz} \\ \text{Detector} = 1.C, \ \text{balanced coincidence for good A.M. rejection} \end{array}$ One I.C. equal to 26 transistors Distortion - 0.2% at 1 KHz for 30% modulation 4 pole ceramic filter in I.F. section Aerial impedance - 75 Ω or 240-300 Ω Sensitivity - 4 microvolts for 30dB quieting R.R.P. £11.95 +£1.19 V.A.T. Output – 300 mV for 30% modulation Power requirements – 23 to 33 volts DECODER R.R.P. £7.45 +0.74

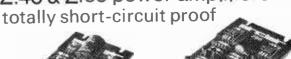
Size $-47 \times 50 \times 20$ mm $(1_{\overline{6}} \times 2 \times \frac{3}{4}$ ins) One=19 transistor I.C.

Guarantee

If, within 3 months of purchasing any product direct from us, you are dissatisfied with it, your money will be refunded on production of receipt of payment. Many Sinclair appointed stockists also offer this guarantee. Should any defect arise in normal use, we will service it without charge.



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Intended for use in Project 80 installations, these modules readily adapt to an even wider range of applications. Both incorporate built-in protection against short circuiting and risk of damage from mis-use is greatly reduced.

7.40 TECHNICAL SPECIFICATIONS Size = 55 × 80 × 20mm (24 × 34 × 3 ins) 9 transistors Input sensitivity = 100mV Output – 15 watts RMS continuous into 8 Ω (35v) Frequency response - 10Hz - 100KHz ± 1dB Signal/noise ratio - 64dB Distortion - at 10 watts into 8 Ω less than 0.1% Power requirements - 12 to 35 volts

Z.60 TECHNICAL SPECIFICATIONS Size $-55 \times 98 \times 15$ mm (24 $\times 3\frac{3}{4} \times \frac{3}{4}$ ms) 12 transistors Input sensitivity $-100 \cdot 25$ mV Output – 25 watts RMS continuous into 8 Ω (45V). Distortion - typically 0.03% Frequency response - 10Hz to more than 200KHz + 1dB Signal/noise ratio – better than 70dB Built-in protection against transient overload and short circuiting Load impedance - 4 Ω min, max. safe on open circuit Z.40 R.R P. £5.45 + 0.54 V A.T , Z.60 R R P. £6.95 - 0.69 PV A.T.

Project 80 active filter unit

Makes a highly desirable part of any worthwhile system where inputs may be from record, radio or tape. As with Stereo 80. separate controls applied to each channel make it easier to obtain ideal stereo balance.

TECHNICAL SPECIFICATIONS Size $-108 \times 50 \times 20$ mm $(4\frac{1}{4} \times 2 \times \frac{3}{4}$ ins)

Voltage gain - minus 0.2dB Frequency response – 36Hz to 22KHz controls minimum Distortion – at 1 KHz – 0:03% using 30V supply HF cut off (scratch) - 22KHz to 5.5KHz, 12dB/oct. slope L.F. cut off (rumble) - 28dB at 20Hz, 9dB/oct slope



R.R.P. £6.95 +0.69

Power supply units **PZ.8**

Stabilised Re-entrant current limit ing makes damage from overload or even direct shorting impossible. Normal working voltage (adjust-able) 45V.

R.R.P. £7.98 + 0.79p V.A.T. Without mains transformer PZ.5 30V unstabilised R.R.P. £4·98 + 0·49p V.A.T.

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For scratch and rumble control Transistorised active circuitry





NE often wishes to have a fairly simple grounded emitter amplifier stage that gives reasonably well defined gain and at the same time will work with transistors having a fairly wide spread of $h_{\rm FE}$. The feedback bias method of controlling the working point of the output is one technique but the quiescent output voltage (typically mid-rail) is still dependent on the $h_{\rm FE}$ of the device in question. It was shown last month, that we can define the gain of a stage very accurately by using two transistors and associated negative feedback, but sometimes this is too sophisticated a circuit for simple applications.

A very commonly used method of biasing is to use the *potential divide* method; this has the advantage of being less dependent on h_{FE} and at the same time allows us to tailor the signal gain of the stage by using negative feedback. It is not as predictable a circuit as the two transistor version we saw previously but nevertheless is frequently used by designers.

Biasing

The basic potential divide biasing method is shown in Fig. 59. R1 and R2 between them set the bias but R4 is also a very important component because it helps stabilise the quiescent output voltage. Let's see how this is done. To arrive at component values we must first decide what we need as a quiescent output and what current we want to flow in the collector circuit of the transistor (Trl). As a rule of thumb one should aim for a collector current that is at least ten times higher than the current that needs to be drawn from this circuit to power another stage. At the moment we have not given ourselves any specification in that direction so it need not bother us too much. If we specify a mid-rail output of $4 \cdot 5V$ and a collector current of about $0 \cdot 1mA$ the

of 4.5V and a collector current of about 0.1mA the value of R3 has to be $\frac{4.5}{0.1}$ k Ω . In practice we have

made it $39k\Omega$ so the voltage at A (provided we do everything else right) will be slightly higher than mid-rail but this is no hardship!

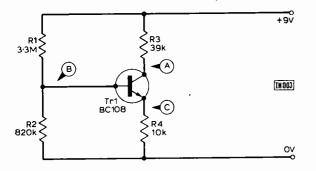
We must now turn our attention to how we generate the necessary base current to control 0.1mA of collector current; this is where R1, R2 and R4 come in. Base current is that which flows between points B and C. This is going to be part of the current flowing down R1 and will go through the base emitter junction to add to any collector current already flowing through R4. We now rely very much on the fact that we can predict, fairly accurately, that there will always be a potential difference of 600mV between points B and C (this is the forward voltage drop across a silicon pn junction); also we hope that the transistor we use will have a fairly high h_{FE} so that when the base current adds to the collector current through R4 it will make insignificant contribution to voltage changes at point C. Provided h_{FE} is 200 or more the increase in current through R4 caused by this will be less than 0.5%.

In practice we usually try to select a value for R4 that will give us a quiescent potential at C of about 1V. Assuming our original quiescent collector current is all that flows through it (i.e. ignoring base current) its value works out at $\frac{1}{0 \cdot 1} k\Omega$ to $10k\Omega$. We can now say that the potential at B will be 600mV more positive than the 1V at C (i.e. $\pm 1.6V$). It is now a simple matter to calculate the values for R1 and R2 provided that we set ourselves the criterion that the total current flowing down the chain of R1 with R2 should be four or five times our

desired base current. If we say 5 times $I_{\rm b}$ flows down R1 then only 4 times $I_{\rm b}$ will flow down R2 (because one unit of $I_{\rm b}$ is extracted at point B to feed the transistor's base emitter circuit). If we assume $h_{\rm FE}$ to be approximately 200 we can expect a base current requirement of $\frac{I_C}{h_{\rm FE}} = \frac{0.1}{200} = 0.0005 \text{mA}$ (don't worry about whether the $h_{\rm FE}$ is exactly this in practice for the moment).

Having assumed this we can now work out the theoretical values for R1 and R2. We know that the potential at B is $\pm 1.6V$ hence if five times I_b flows through R1 the resistor should have a value of $\frac{9-1.6}{5\times0.0005}$ k Ω = approx. 3,000k Ω (or to a near aproxi-

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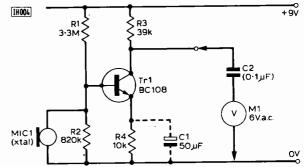
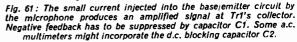


Fig. 59 : The values of the bias resistors, R1 and R2, are usually chosen to set point A at a mid-rail voltage.



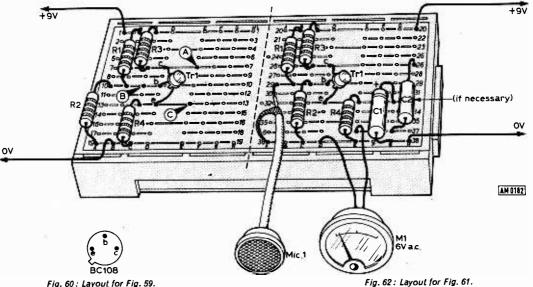


Fig. 60 : Layout for Fig. 59.

mation $3.3M\Omega$). The voltage drop across R2 is 1.6Vand it has four times I_b flowing through it so its value $\frac{1}{4 \times 0.0005}$ k $\Omega = 800$ k Ω (we have works out as rounded it up to $820k\Omega$ to match the rounding up of R1).

Make up this circuit and using a $20,000\Omega$ per volt meter, measure the potentials at A, B and C and see how near we are to our predicted requirements.

Within reasonable limits the quiescent output level is controlled by the potential at C and the forward voltage drop across the base emitter junction.

The transistor works, to some extent, like an emitter follower; i.e. provided there is sufficient h_{FE} in the first place (and we have sufficient total current flowing through R1 and R2) the transistor will draw the necessary amount of base current to keep the potential at C 600mV more negative than that at B. If we ensure we have several times the predicted base current flowing through the potential divide resistors then small variations in actual base current drawn will not significantly affect the potential at B. It would, obviously, be better to reduce the values of R1 and R2 to ensure that the standing current was very much higher than I_b but this is undesirable for some applications. For example if we wish to use a crystal microphone or cartridge as a source of signal for amplification these two resistors act as if they were both connected in parallel

across the source and thus reduce the input impedance of the amplifier with the predictable drop in low frequency response from a high impedance capacitative source.

Why not use a crystal microphone (in the same manner as last month) and measure the a.c. voltage changes at the collector of Tr1-use the circuit and layout for Fig. 61.

At first leave out the capacitor C1 and try the "hum and whistle" test. You will probably see very little signal. The reason for this is that not much of the extra current, supplied by the microphone, is being used to modulate the collector current. The reason is that as soon as you try to inject more current into the base, the potential at the emitter rises to combat it (negative feedback). This negates the effect of the extra base current—in so doing it shows that we have a nice stable biasing system! However this is not particularly desirable when it comes to amplifying a signal so we have to do something about it. As our applied signal is a.c. by nature it will flow through a capacitor so we connect a high value capacitor between the emitter of Tr1 and ground. Any a.c. signal applied to the base will cause maximum a.c. base current to flow and this produces maximum modulation of the quiescent collector current.

Connect C1 into the circuit and try your test again; you should now get a much larger response at the

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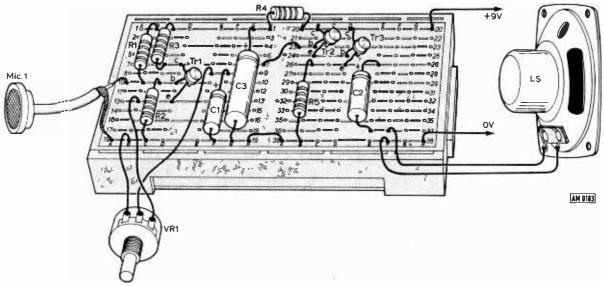


Fig. 64: Layout for Fig. 63.

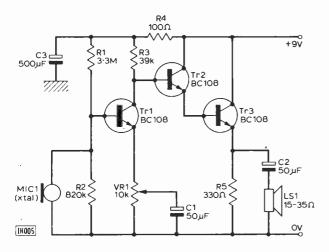


Fig. 63: A simple microphone amplifier (for use as an intercom or baby alarm) using a potential divider biased stage. Volume is controlled by VR1.

collector. We still have negative feedback to d.c. (thus stabilising the bias) but, provided C1 is of high enough a value, we have removed all negative feedback to a.c. We call C1 an emitter by-pass or decoupling capacitor. We obviously get more amplification by including C1 but at the expense of frequency response.

Because we are drawing maximum current from the a.c. source we can say that the input impedance of our amplifier is much less when we reduce the negative feedback; this means that although the amplification at high frequencies increases dramatically it is severely reduced at low frequencies. Usually one has to compromise with the amount of emitter decoupling as shown in Fig. 63. This circuit allows you to apply more or less of the, effect of C1 by adjustment of VR1. With the extra power stage you can experiment and hear the difference between high gain and poor frequency response or low gain with better response. Some circuits use the technique of adjustable feedback to control volume, in which case you trade volume for quality.

(TO BE CONTINUED)

ARE YOU ORDERING COMPONENTS P

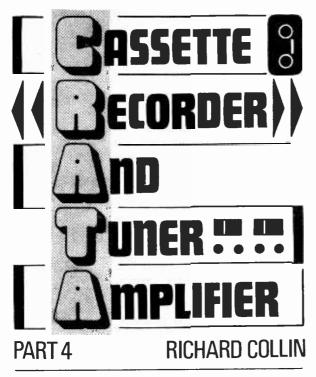
During the past few months the components supply situation has undergone significant changes, creating long delivery times and price alterations. Catalogues now available may not carry current prices and availability. We strongly recommend readers to ascertain these points, including V.A.T. and carriage charges before placing orders to avoid disappointment and embarrassing situations arising.

See also the Leader article on page 116.

CQ! CQ! CP! CP!

EXCHANGE

...R209 In perfect working order, exchange for other communication receiver (eg AR88, HRO, CR70A, etc), or sell.—P. J. Kay, 85 Northway, Maghull, Liverpool.



ASSEMBLY AND WIRING

Having constructed the chassis and power supply and made up the five main boards, final assembly can commence. The boards are mounted on to the chassis skeleton frame in the positions shown in the photographs. It is important when bolting the boards into place to make sure that they are totally isolated from the metalwork-transistor mounting bushes make neat insulators for this application. The power amplifier board should be mounted before the heatsink clearance holes in the rear panel are drilled. These holes can then be accurately marked out. It is important that the transistor leads are not strained when the heat sink plate is bolted to the rear panel. A smear of silicone grease should be applied between the plate and the panel to ensure good thermal contact.

Once all boards, switches, potentiometers and sockets are mounted, wiring may commence. Be sure to follow the wiring diagrams exactly. Take particular notice of the screened lead connections. The



screen is not often connected at both ends as this would cause earth loops. This applies especially to the wiring to the input sockets. To ensure that earth loops are not created by the connection of external apparatus (e.g. gramophone deck or tape recorder) most screens are not connected at the sockets.

Each of the +34V and OV leads from the PCB's should be taken direct to the tags of 5C3. The negative tag is then earthed to an adjacent chassismounted solder tag. This is important so that the power supply and signal earth paths are clearly defined. For the same reason, all screened cables must have an overall insulating sheath.

Failure to follow the wiring routes shown could result in serious hum and instability problems. Any stereo system has critical earth return paths, because any length of wire has a finite resistance. It is possible to generate voltages across this resistance which will be added to the intended input signals. The phase and magnitude of these unwanted voltages can be such that oscillations occur which may be at very high frequencies and therefore inaudible. They can however cause distortion and also lead to failure of transistors. In addition high hum levels can be generated.

INITIAL TESTS

Having completed all construction and wiring, a further very thorough check of all connections, electrolytic capacitor polarities and component positioning should be made.

Once everything has been checked out, the loudspeakers should be connected, the Volume control set at minimum, the Bass, Balance and Treble set mid-way. Before connecting the mains supply, the

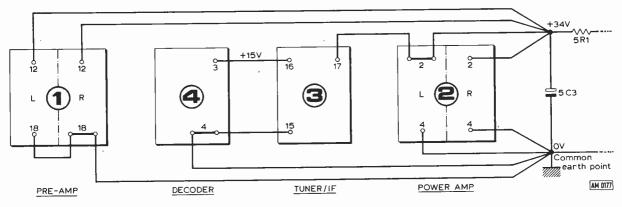
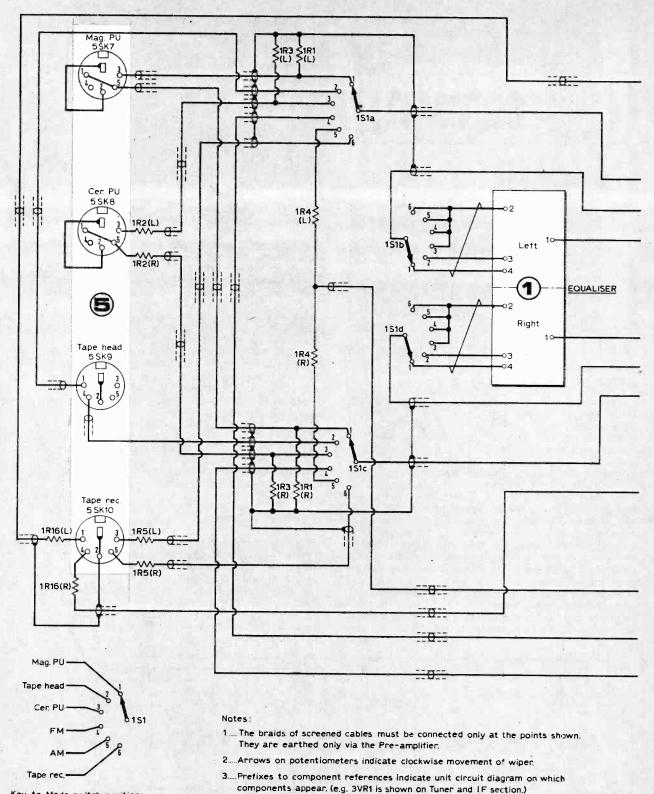
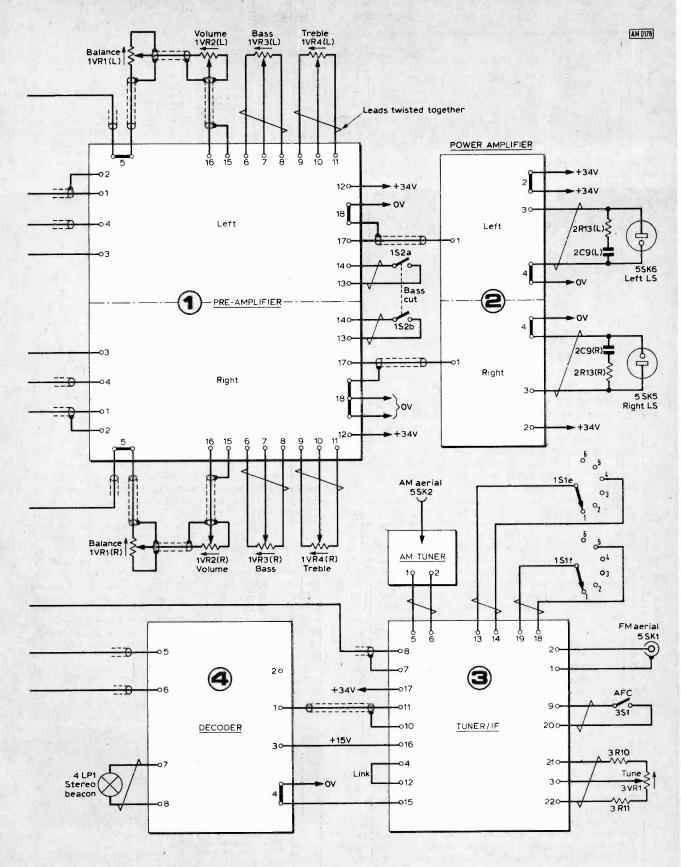


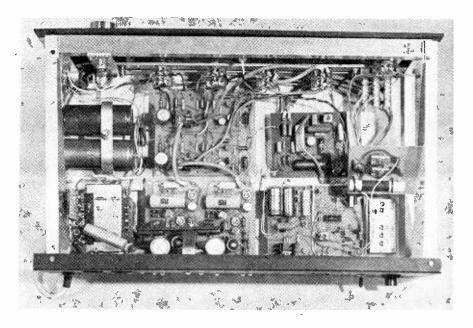
Fig. 20: Wiring diagram of power distribution to PCBs.



Key to Mode switch positions

Fig. 21 : Overall wiring diagram, excluding power and earthing (see Fig. 20). Screened wire must be used where shown. The Balance, Volume, Bass and Treble potentiometers for the Right and Left channels are each ganged.





Top view of CRATA showing unit positions with Power Supply at the left. The Pre-Amplifier and Decoder are at the top, Power Amplifier and Tuner/IF at the bottom. The Equaliser board, which is not shown in this photograph, should be mounted near the input selector switch.

two preset resistors on each power amplifier should be set as follows:

VR1—midway VR2—fully anti-clockwise

Connect the mains supply and switch on—a faint hiss thould then be audible in each speaker. Measure the HT supply across the smoothing capacitor 5C3. This should be approximately 34V. If the voltage is much lower, then switch off and recheck all wiring and boards for short circuits—check also the power transistors which could have been damaged during lead forming or soldering.

If the voltage is correct, connect a meter (preferably a valve-voltmeter) to the emitter of Tr4 on the left power amplifier. Adjust VR1 (left) so that this voltage is half the HT voltage i.e. 17V. Next the bias for the output stage should be set. This is best carried out using an oscilloscope and sinewave generator. Connect the 'scope' across the left hand speaker socket and feed a 1kHz sine wave into the input of the left power amplifier. Feed in only sufficient signal to produce a low output volume. The output waveform is certain to exhibit crossover distortion (see Fig. 22). Adjust VR2 (left) until the distortion just disappears. If an oscilloscope and signal generator are not available, the bias may be set with a milliammeter. Disconnect one end of R12 and connect the meter (100mA fsd) in series with this resistor. Adjust VR2 (left) so that the current flowing is 10mA. Reconnect R12 and then repeat the entire setting up procedure on the right hand power amplifier.

Next, using a high impedance voltmeter, check the operation of Tr1/2 in the preamplifiers. Measure the voltage on Tr2 collector—it should be about 5V. If the voltage is much different, change the value of R7 until the voltage is correct. Reducing R7 will increase the voltage and vice versa. Check both channels.

To test the preamplifiers and socket wiring, select the Magnetic P.U., Ceramic P.U., Tape head and Tape recorder replay positions in turn, feeding the associated sockets with their respective input signals. Having ensured that each input is working, select whichever is the most convenient to use and make a more thorough check on the amplifier performance. Check that the Tone controls behave as expected, check the Bass Cut switch (if fitted) and also the action of the Balance control. If a signal generator and oscilloscope are available the operation may, of course, be checked in greater detail.

TUNER ALIGNMENT

Once satisfied that the audio stages are functioning correctly, select AM Radio. Check that +15V is present at the emitter of 3Tr2. If a selector switch is fitted select the first position. Adjust the appropriate trimming capacitor associated with the ferrite aerial until the desired station is received. Orientate the board for maximum volume, with the complete receiver in the plane in which it will be operating when finally installed. Lock the board into position. Then adjust the trimmer capacitor associated with L2 on the aerial board for maximum volume. Readjust the two trimmers until no further improvement can be obtained. With the multi-station version repeat the procedure for each selector switch position, being careful not to disturb those trimmers already adjusted.

Next select FM Radio. Without a signal, a high background noise is to be expected. Connect an aerial (FM dipole), switch off the AFC and rotate the Tuning control until a station is located. (If using preselected tuning. select any push button

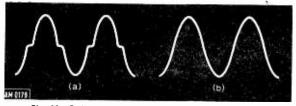


Fig. 22: Output waveform of sine wave (a) With crossover distortion. (b) With VR2 adjusted for correct bias on output transistors.

and adjust the appropriate preset resistor, having first set the fine tune potentiometer to mid-way). As soon as a signal is located, adjust the core of 3L4 (the FM IF coil) for maximum volume, using an insulated trimming tool. Then select several other stations and recheck the IF coil setting.

DECODER ADJUSTMENT

Tune to a station broadcasting in stereo. Adjust the decoder oscillator coil L1, again using a proper tool, until the Stereo indicator lamp lights—as it does so the decoder should automatically switch into the stereo mode, making the previous monaural sound image appear to spread out. Continue turning the core until the lamp goes out again and the decoder switches back to mono. The correct tuning point is mid-way between the point where the lamp lights and the point where it goes out again.

Now turn the Tuning until off tune. The lamp should extinguish and the audio become louder and severely distorted. Switch on the AFC—the station should instantly come on tune again and the lamp relight. Switch off the AFC and tune back through the correct point until a distorted signal is again received. Switching on the AFC should again bring the receiver on tune. Finally check that the Stereo lamp does not come on when tuned to a station broadcasting in mono.

To prevent the decoder being triggered by noise or by the 23kHz tone on Radio 4, capacitor 3C20 was added across the audio output of the FM tuner. Too high a capacitance at this point will degrade stereo separation with some samples of the decoder IC. The value fitted should therefore be the minimum consistent with correct operation, i.e. lamp On for stereo and Off for mono broadcasts.

Having completed the alignment, it only remains to check the Tape recorder output. This may be accomplished with an oscilloscope, or a tape recorder set to 'record'. This should respond to the programme being received. The Volume and Tone controls on the equipment will not affect the tape record output.

The equipment is now fully aligned and fully operational. It only remains to mount CRATA into its case.

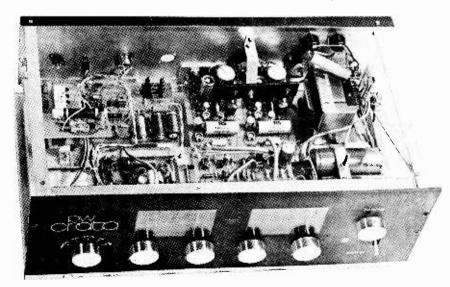
★ Voltage analysis

Meter $10k\Omega/Vdc$ —negative lead to OV rail, all readings in volts

H.T. Supply at 5C3 34V Power Amplifier (each channel)					r	
Pre Amplifier				e	b	с
(each channel)						
eb	c	Tr1 BC		17	16	*
		Tr2 BC	148	17	17.5	
Tr1 BC149 * *	2	Tr3 2N		0	*	17
Tr2 BC148 * 2	4	Tr4 2N		17	18	34
Tr3 BC149 0 *	5	Tr5 2N	5111	17	17	0
Tuner & IF						
(a) AM Radio selected	1 1			e I	bΙ	с
			_			
		Tr1 BC	113	0	0.6 0	·75
IC1 ZN414 1 1	-5	Tr2 2N	6288 ⁻	5	16	34
(b) FM Radio selected						
IC2 Pin	123	456789	010111	2:13	3 14 1	5 16
				_ _	-	
CA3089E Reading	222	005555	5 5 12	0 2	05	0
NOTE-The reading	on p	in 7 (Al	FC out	put) va	ries
with tuning.	•					
	,					
Decoder FM Radio broadcast		lected-		to	1	reo
IC1 Pin	1234	156789	10 11 1	2 13	3 14 1	5 16
			- -			
CA3090Q Reading	2200	0 6 1 1 10) 10 15	0 0	315	515
	e	b c				
Tr1 BC158	15 1	4 · 5 15				
* Indicates very low re meter.	eadin	ig due to	circui	lo	ading	j by
				4	<u>`</u>	·

FAULT FINDING

To help with any problems encountered during testing, or with any future service requirements, all transistor and IC terminal voltages are given in the table.



The Power Amplifier heatsink arrangements are visible here. The small pcb on the mains transformer tagboard carries the rectifier assembly.



PART 4 **TECHNIQUES** ALAN AINSLIE

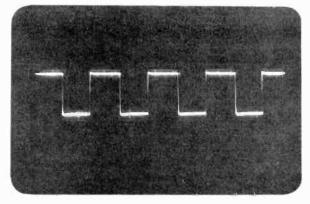
If the switching waveform is not a pure square wave it will tend to blur the trace on the CHOP mode, but on ALT switching takes place during flyback and is of no consequence, unless it is very bad. Beam blanking is often employed to render switching transients unseen and to produce a clearer trace.

When using a dual trace plug-in there are difficulties with timebase triggering, but these will be dealt with later.

Often the dual trace unit has a polarity reversal switch for each beam to reverse the direction of deflection. Also the ALT/CHOP switch besides having positions for CHI only and CH2 only has a sum position. The deflection in this position is the sum of the signals, or if one channel is inverted, the difference. Hence the dual trace unit can be used as a differential amplifier. However, results are not generally as good as a proper differential plug-in.

The differential plug-in usually has two inputs, one being inverted. A mode switch enables the operator to add the two signals and so anything common to both inputs at the same level is rejected. The degree of rejection is termed the "common mode rejection". Elaborate facilities are provided to optimise the CMR at all attenuator settings and frequencies.

Differential amplifiers are used to investigate balanced signals, investigate phase changes and in the analysis of distortion, as well as for precise balancing methods. The average amateur laboratory can usually manage with a dual trace unit and a bit of common sense.

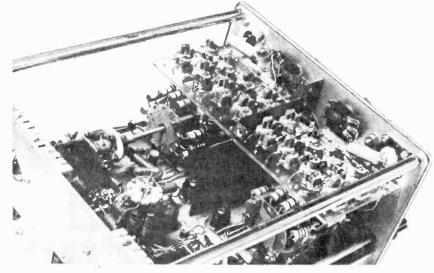


A 180kHz beam switching waveform, The overshoot and lack of blanking during the switching transients cause the overall trace to lack definition.

PROBES

As mentioned earlier the input impedance of a typical scope is perhaps $1M\Omega$ in parallel with 25pF. When a screened input lead is connected the capacitance would be well over 100pF. At 100pF and 500MHz this is an impedance of a little less than 32 ohms!

Probes have been developed to reduce this capacity to as little as 1 or 2pF. The simplest types are the passive attenuator probes, Fig. 9 shows the arrangement. The resistors Rp and Ry are the divider, for a 10:1 probe with Ry (the input resistance) of $1M\Omega$



The inside of a double beam plug-in. The altenuator switches and the associated trimmer capacitors can be clearly seen. Because of the high input impedances screening between the channels is necessary and can be seen between the two attenuators.

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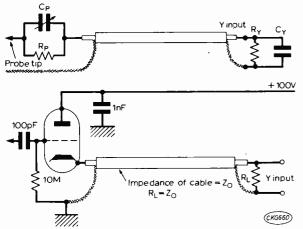


Fig. 9. Two simple probe circuits.

then Rp would be $9M\Omega$. Cp and Cy (input capacity) plus the cable capacity form the capacitive divider. Cp is adjusted on a lkHz square wave to give a good response. Then:—

$Rp \times Cp = Ry \times Cy + Cable Capacity$

The capacity seen at the probe tip is therefore much less than the capacitance at the scope input and even with several feet of coax a 10:1 probe gives a capacitance of only about 12pF. Higher ratios are available giving even less capacity and are invaluable for serious work.

A passive probe has to be matched to the scope by adjustment of Cp the series trimmer, which is adjusted to give a good display on a 1kHz square wave as shown in Fig. 10. The effect of slight maladjustment may be thought to be negligible, but Fig. 10 also shows the display of a brief pulse. It can be seen that in order to keep the amplitude calibration accurate at all frequencies the probe must be carefully adjusted.

The second approach, also shown in Fig. 9, is to take the input cathode follower right up to the circuit under test. The capacitance is reduced to only a few pF and there is only a small attenuation (output= $0.85 \times input$; sometimes reduced to 0.5 for ease of

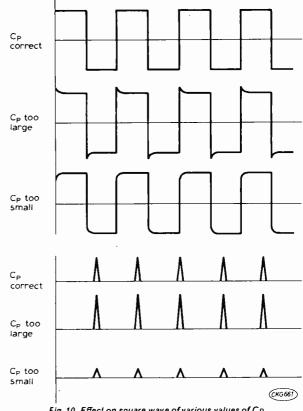
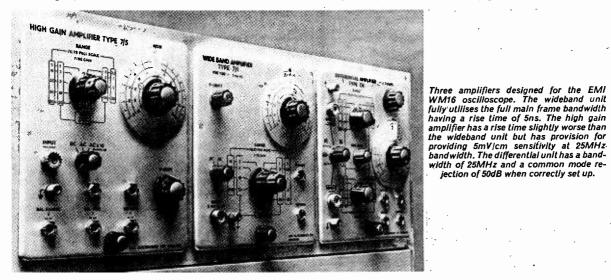


Fig. 10. Effect on square wave of various values of Cp.

calculations). However the input signal range is limited and attenuators have to be added to the front of the probe. One other major snag is that power has to be fed to the probe along the signal cable. The resistor RL is to terminate the cable and prevent reflections.

The cathode follower probe is most useful but tends to be expensive and easily damaged by overvoltage at the input. These two facts alone mean that most amateurs stick to passive probes which virtually never wear out, cannot be blown up, unless you try very hard, and are reasonably priced.





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CALIBRATION

The calibration of the Y deflection system does not usually present a very great problem, the main difficulty being in the adoption of a standard against which the scope is to be set. Usually this standard will be the lab voltmeter if it is known to be correct within a per cent or so and is reliable.

Valve scopes should be run for an hour or more, then the power supply voltages checked and adjusted. After a further hour or so the calibration can be started. In order for non-linearity not to affect the results, signals are applied to give about 75% max. deflection. For example, with the attenuator set to the 5V/cm position (Y shift range 25V) a DC signal of 20V would be used.

The first step is to set the input levels to the main frame amplifier. First a meter is connected between the two balanced inputs and the Y shift adjusted to give zero voltage between them. The drive amplifier balance control (centreing) is then adjusted to centre the trace (timebase free running) on the central graticule line. Then the voltage difference (produced by Y shift control) to deflect, say, 2cm is noted. The gain preset (main frame) is adjusted to bring the sensitivity to the value quoted in the manual (usually 0.1 to 0.5V for 1cm deflection).

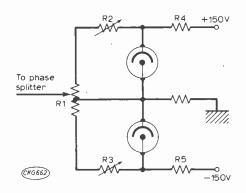


Fig. 11. Circuit for calibrating Y deflection system.

The attention can now be turned to the plug-ins. The first step here is to calibrate the Y shift if necessary. The calibrated shift is set to 0V and the trace centred by the Y shift. A DC input is applied and the calibrated shift adjusted to again centre the trace. The reading on the dial is noted and compared with the applied voltage. Fig. 11 shows the general arrangement of the calibrated shift. The mechanical centre (0V) of the calibrated shift R1 is set so that the resistance between slider and centre tap is zero when the scale indicates 0V. R2 is used to calibrate the positive half of the rotation.

When the calibration shift has been set the fine gain control (if fitted) is turned to maximum and the preset gain (usually the phase splitter cathode resistor) is adjusted for the required volts/cm from a DC input producing three-quarters of full deflection. The calibration can be checked by noting the rotation of the calibrated shift for a certain deflection both in a positive and negative direction. It should be noted that the calibrated shift once set is accurate regardless of the settings of the preset gains or the main frame gain.

To be continued

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2D21 40 6C6 40 6SH7 44 20P3 80 5702 80 EBF80 89	EL81 .60 PABC80 .38 PY83 .35 U251 .80 ACY28 .20 BFY50 .25 OC77 .80
2GK5 .55 6C9 1.25 6SJ7 55 20P4 1.00 6057 1.00 EBF83 .48	BLOI .00 TABOOT.00 TTO .00 UD140 40 DRW1 01 0070 15
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8A4 50 6CG8A 75 68Q7GT 45 25A6G 38 6067 1.00 BBL21 2.00 3D6 40 6CH6 60 6V6G 17 25L6G 60 7475 1.00 BC86 70	BL85 .44 PC95 .75 PY500A .85 U404 .49 AD161 .50 BY100 .20 OC81 .12
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	EL91 40 PC900 45 PY801 35 U4020 55 AF106 55 BY114 20 OC82 19
	EL360 1.80 PCC84 40 PZ30 48 VP23 75 AF114 28 BY126 17 OC82D 12
384 35 6CM7 75 6X5GT 40 2525 80 DD 96 ECC33 1.50 4CB6 55 6CU5 75 7B6 75 25Z6G 70 AC6PEN 88 ECC35 95	ELL80 80 PCC85 44 00V03/10 VP41 75 AF115 17 BY127 20 0C83 28
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5A8G 1.25 6F18 .55 10F9 .65 30FL13 .55 CY31 .45 ECC804 .80	E163 .04 FCF802 .00 0 DC41 .05 212147 .94 D tate 04 04 47 13 0 0007
6AC7 .49 6F23 .80 10F18 .55 30FL14 .70 DAF91 .30 ECC8071-00	10104 .10 101000 .00 00001 .40 202201 .00
6AG5 .27 6F24 .85 10LD11 .70 30L15 .75 DAF96 .44 ECF80 .84	
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SHORT WAVE DX by MALCOLM CONNAH

WITH such a large number of reports this time I think I should start straight away with the contribution from Ian L. Wadman of Didcot in Berkshire. Ian has a new Trio 9R-59DS and a 70 foot end-foot antenna. Some concentration on 60 metres produced the following excellent results:

4770 ELWA, Liberia in English at 0615.

- 4832 Radio Capital, Costa Rica, Spanish at 0405.
- 4860 R. Maracaibo, Venezuela, Spanish at 0420.
- 4882 R. Commercial, Dominican Rep., music at 0530.
- 4900 R. Juventud, Venezuela, Spanish at 0355.
- 4940 R. Yarucuy, Venezuela, Spanish at 0345.
- 4970 R. Rumbos, Caracas in Spanish at 0455.
- 5030 R. Continente, Venezuela, S/off at 0500.
- 5035 Bangui, Cent. Afr. Rep. with music at 0545.
- 5050 R. Tirana, Home Service at 0340.

The **Rev. W. John Mckae** of Birkenhead has built the 3 Band SW receiver described in the December issue. This combined with a 45 foot indoor aerial and ATU produced the following:

- 5995 VOA, noted in English at 2130.
- 6045 Hilversum, Holland, English at 1045.
- 6065 Radio Sweden in English at 1600.
- 6120 Vatican Radio noted in English at 2100.
- 7260 Monte Carlo, S/off in English at 0845.
- 7310 Radio Vilnius, Lithuania S/off at 2300.
- 7345 R. Prague noted in English at 2200.
- 11815 WYFR noted in English at 2240.
- 15185 R. Finland in English at 1830.
- 21520 Radio Switzerland noted in English at 2125.
- Linford Fevrier sends in our first report from the West Indies; St. Lucia to be precise; using a Pye valve domestic receiver and 100 foot long wire to hear:
- 6010 R. Sweden in English at 2114.
- 6090 R. Luxembourg in English at 0210.
- 9570 Swiss B.S. in English at 0905.
- 9635 R. Nacional de Colombia, Spanish at 1539.
- 11775 WINB, Red Lion, USA in English at 2130.
- 11855 Broadcasting Service of Saudi Arabia at 1855.
- 11880 Voice of Turkey in English at 2213.
- 11895 R. Senegal in French at 2225.
- 11935 R. Portugal in English at 0208.
- 15190 La Voix de la Revolution Congolaise at 2010.

Matthew Phillips of Halstead in Essex is only 12 years of age but this Domestic receiver is 37 years old; using a metal bed frame as an aerial the combination produced the following log:

- 5995 R. Australia in English at 0900.
- 6180 BBC, Cyprus relay at 1730.
- 7210 Red Cross Radio in English at 1730.
- 7245 Austrian Radio noted at 1030.
- 9005 R. Tehran, Iran at 2000.
- 9520 ORTF, Paris noted at 1415.
- 9525 AIR, Delhi in English at 2230.
- 9570 R. Australia noted at 1500.
- 9670 Adventist World Radio at 0930.
- 11710 Radio Kiev, USSR noted at 1930.
- 11730 R. Tashkent, USSR noted at 1400.
- 11765 R. Australia in English at 0645.
- 11770 BBC, Ascension Island relay at 1700.
- 11815 NHK, Japan in English at 0800.
- 11850 R. Norway in English at 0815.
- 11900 RSA, South Africa noted at 1900.
- 11970 Radio Tunis in English at 0900.
- 17825 RSA, South Africa noted at 1600.

Robin Hookham of Stretford, Manchester certainly managed to hook'em when he used his Codar Multiband-6 and 40 foot end-fed antenna to record:

- 4970 R. Rumbos in Spanish at 2345.
- 4980 Ecos del Torbes in Spanish at 0026.
- 5920 R. Kiev, Ukraine noted at 1950.
- 5940 R. Vilnius with Mailbag show at 0047.
- 6130 R. Norway with id. in English at 1900.
- 9545 R. Ghana, 'Africa Worldwide' at 2125.
- 9670 IBRA Radio with religious pgr. at 2015.
- 11720 R. Nacional de Brazil, English at 2312.
- 11805 R. Globo in Portuguese at 2008.
- 11860 R. Canada Int., SW Club at 2148.
- 11880 Voice of Turkey in English at 2203.
- 15130 WYFR with news at 1905.
- 15300 HCJB, Quito, Ecuador 'DX Partyline' at 1944.
- 15410 UN Radio noted at 1921.

Please remember to correct all times to GMT when sending in reports and also remember the new address.

MEDIUM WAVE DX by CHARLES MOLLOY

AROLD Emblem (Mirfield Yorkshire) has been listening to the Middle East on the medium waves with his Eddystone 730 communications receiver and MW loop antenna. He reports hearing Riyadh, Saudi Arabia on 587kHz; Cairo on 710kHz; Baghdad 760kHz; Tartar, Syria 782kHz; Quazvin, Iran 841kHz; Damman, Saudi Arabia 885kHz; Izmir, Turkey 926kHz; Diyabakir, Turkey 1061kHz; Sharjah, United Arab Emirates 1535kHz. Harold also reports

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hearing CSB81 at Santa Maria, Azores on 1570kHz at 2336hrs GMT. Stations in the Middle and Near East can be logged during the evening and after 2300hrs GMT, the time when a number of Europeans sign-off for the night. A sensitive and selective receiver together with a medium wave loop antenna is essential for this type of DXing though a few of the stronger outlets can be heard with simpler equipment. Try for Kuwait on 539kHz; Batra, Egypt on 620kHz; El Beida, Libya on 1124kHz; Tripoli, Libya on 1250kHz and Kuwait on 1345kHz.

Brendon Rooney (Glencar, Co. Sligo in Eire) has sent in an excellent log of North American reception. Using a Trio 9R59DS, a Heathkit GR78 transistor communications receiver and a medium wave loop with balanced differential amplifier, he reports hearing CBN St John's in Newfoundland on 640kHz; WOR New York City on 710kHz; WABC also in NYC on 770kHz; WCCO Minneapolis on 830kHz; WHDH Boston on 850kHz; CJON St John's on 930kHz; CBM Montreal 940kHz; CHNS Halifax, Nova Scotia on 960kHz; CBA Moncton, New Brunswick 1070kHz; WBAL Baltimore on 1090kHz; WNEW New York City on 1130kHz; WOWO Fort Wayne, Indiana 1090kHz. Although these stations were heard between 2300hrs and 0200hrs during December it is possible to hear North America on the medium waves in the UK at any time of year provided there is a path of darkness between transmitter and receiver. In June stations can be logged during the hour before sunrise. North Americans broadcast on 'channels' which

VHF/FM DXING

by SIMON DAVID

AST month I reported on the strange events in January. My Correspondent E. W. Earnshaw is now on his way around the world as a seagoing Radio Officer. The reported Turkish station, Radio Ankara news, has been verified by an official at the Turkish Embassy who heard the tape recording made in Newcastle. Other recordings made were of f.m. broadcasts from Russian and Polish origin followed by a Spanish station. I hope this will not deter others reporting more modest DXing achievements.

Openings of a less dramatic nature in February enabled **Roy Patrick** of Derby to pick up Hessischer Rundfunk, Frankfurt on 99MHz. He received a very quick QSL card from them.

George E. Sykes is only 50 feet above sea level at Bolton-le-Sands, Lancashire but has a clear view all round. On his AR2000, with an Aerialite 264 and Stolle rotator 15 feet above his garage, he has received local radio stations from Blackburn, Merseyside, Carlisle and Sheffield. He wonders if going upstairs means better results! An unidentified station was picked up on 102MHz, but best reception comes from local mobiles. Kirk O'Shotts, Blaenplwyf and Divis have also been picked up.

Colin Chatfield of Camborne, Cornwall has a home made 5-element Yagi feeding a P.W. design preamp and Heathkit FM4-TU tuner. He has received Radio Eirean in English and Gaelic, Radio 4 from Wenvoe and Haverfordwest, BBC radio from North Hessary Tor and ORTF from Brest $97 \cdot 7MHz$.

Finally, anyone in the home counties who heard a foreign station, probably East European, between 97.7 and 98MHz (above LBC) on 23rd March, please

are multiples of 10kHz and they are easy to identify as they use their callsigns frequently (prefix C for Canada and W or K for the US.) followed by the name of the city or town where the studios are located.

Julian Allan (Hadleigh, Suffolk) has been trying the medium waves with his Audiosonic transistor portable with internal ferrite rod aerial. He reports hearing London Broadcasting on 719kHz (417m); American Forces Network (AFN) Frankfurt on 872kHz (344m); BBC Radio Medway 1034kHz (290m); AFN Munich 1106kHz (271m); Radio Sweden 1178kHz (254.5m) in English at 2245hrs GMT; Radio Tirana, Albania 1394kHz (215.2m); Trans World Radio, Monte Carlo 1466kHz (204.6m), On the long waves Julian has heard Mainflingen, West Germany on 151kHz (1986m); Allouis, France 164kHz (1829m); Luxembourg 236kHz (1271m). Others to look for on the long waves are the Voice of America, Munich 171kHz (1734m); Azilal, Morocco 209kHz (1435m) in Arabic; Tipaza, Algeria 251kHz (1195m) normally in French but in English at 1900hrs GMT; Lahti, Finland 254kHz (1181m).

Brian Murray (Edinburgh) has been busy again with his Astrad transistor portable coupled to an old 405-line TV aerial. His log includes CSB2 Lisbon, Portugal on 1034kHz at 0020hrs; Radio Portugal 1061kHz in English at 2300hrs; Radio Denmark also on 1061kHz at 2300hrs; BBC Radio Derby on 1115kHz at 2240hrs and BBC Radio Manchester 1457kHz at 1800hrs, all times being in GMT.

let me know. Reception on my receiver was not good enough to identify it.

Please state the date, frequency and country of origin in all reports; also your receiver and aerial type would be useful.

Station information

Among the latest information to hand are the following: Perth, BBC Radios 1/2,3 and Radio Scotland are now on $89 \cdot 0$, $91 \cdot 2$, $93 \cdot 4$ MHz respectively; Campbeltown BBC services are similarly changed to $88 \cdot 6$, $90 \cdot 8$, $93 \cdot 0$ MHz respectively. Listeners with preset push-button receivers will need to alter the tuning of the appropriate channels in these areas.

The IBA station BRMB Radio started broadcasting official programmes on $94 \cdot 8$ MHz from Lichfield. VHF transmissions are said to be better here than the alternative medium wave transmissions. The aerial is directional, mounted on the 1,000ft television mast, and beamed towards Birmingham centre. Polarisation is circular to help car radio and portable radio reception.

Piccadilly Radio (IBA) went on the air on 2nd April in the Manchester Area. The transmitter situated at Saddleworth broadcasts on 97 0MHz using a circular polarised directional aerial. The next to follow will be Swansea Sound from Kilvey Hill on 95 1MHz using an omni-directional circular polarised aerial.

Full details of IBA independent radio broadcasts on v.h.f. and medium wave can be obtained by sending a stamped addressed envelope to the Engineering Information Service, Independent Broadcasting Authority, 70 Brompton Road, London SW3 1EY, or Crawley Court, Winchester, Hampshire SO21 2QA.

BBC local radio information can be obtained from Engineering Information Dept., BBC Broadcasting House, London W1A 1AA.



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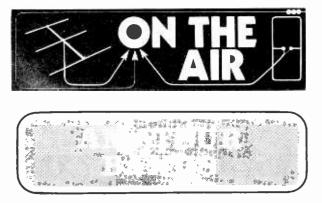
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by Eric Dowdeswell G4AR

F IRST, the bad news! Dave Gibson G3JDG, your conductor around the amateur bands for so long, reports that for personal reasons he is no longer able to produce the monthly page. Dave's reports under the heading of 'The Amateur Bands' began in October 1964 and the following month became part of the feature 'On the Short Waves'.

We owe a lot to Dave for keeping us up-to-date on amateur affairs over the years. His humorous, free-and-easy style of writing will be missed. Good luck in the future Dave and thanks a lot, keep in touch.

And now, more bad news! This page is being taken over by yours truly who will endeavour to give you at least as good a service as did JDG. How well I shall succeed remains to be seen. A lot depends upon the number and quality of the reports received so start them rolling to my QTH given below.

Reporting

A few pointers which will help all round:- letters short, reports accurate and to the point and preferably on a separate sheet of paper and above all, legible! Call signs, in particular, should be in clear block letters but I hope I have enough experience to be able to spot the odd boo-boo. I don't want to hear about those routine QSO's heard on 20m made by fellows using 400W of SSB and a multielement beam. But do tell me all about that unusual callsign, that newly activated country or exotic expedition plus the DX that is really DX when related to the band/ power/distance involved.

Reports of QRP work may prove of interest as they may encourage others to try a little less power and more ingenuity and operating know-how to achieve the results they do with high power.

Break for a commercial! As ST2AR in Khartoum, Sudan from 1953 to 67 I worked nearly 300 countries, using homemade equipment and mostly wire aerials, but not one of these QSO's held the same thrill for me as did the QSO I had a couple of years ago with W1BB on Top Band with a genuine 10W input. In recent times G3XAP has worked all continents with 9W input on this band and now threatens to repeat the performance with 5W, which leaves me gasping! He does have the slippery slope of the sunspot cycle to slide down so others ought to try and emulate him while the going is good. The glow of self-satisfaction attending success has to felt to be appreciated!

GB Operations

With the proliferation of GB prefixes for use at just about any event that a club secretary cares to dream up their novelty value has decreased to zero. However, there are a couple of calls around that rise about this modern day mediocrity. In the centenary year of the birth of Marconi, GB2MT was operated from Bayswater, London from April 25 to 28 on 15, 20 and 80m SSB. The QTH was the house in which Marconi and his mother lived in 1896/7.

Another event associated with the centenary and taking place over the weekend of June 7/9 is a House Party at Stratford-Upon-Avon where guests will face a programme of films, talks and demonstrations to illustrate the progress of radio communications. GB2HF will be on the air to demonstrate how it is done. QSL's and reports to Ralph Barrett G2FQS (QTHR) or the Bureau, for both stations.

By the time this appears in print you may have heard GB2MT already on April 7 when it was located at the top of the GPO building in St. Martins-le-Grand in London from where Marconi made the first official demonstration of wireless in this country to a second station on the Embankment just half a mile away. QSL as above.

Deadlines

The deadline for your reports each month is a rather flexible feast since the date, from month to month, when the magazine "goes to bed" can vary by as much as seven days. Aim at the middle of the month but remember that every effort will be made to squeeze in material received after this time. Incidentally, I often wonder if the brief listing of future events is really of any interest. I have a sneaking feeling that anyone with sufficient enthusiasm will have already acquainted himself with the full details from other sources.

Starting off with a nil balance of readers' reports and an aversion to nicking anything from the other scribes the reports on the band conditions must wait until next month. Suffice to say that the sunspot number is dropping more or less as predicted so take the hint and keep an eye on the lower frequency bands for your reports. Cheers for now.

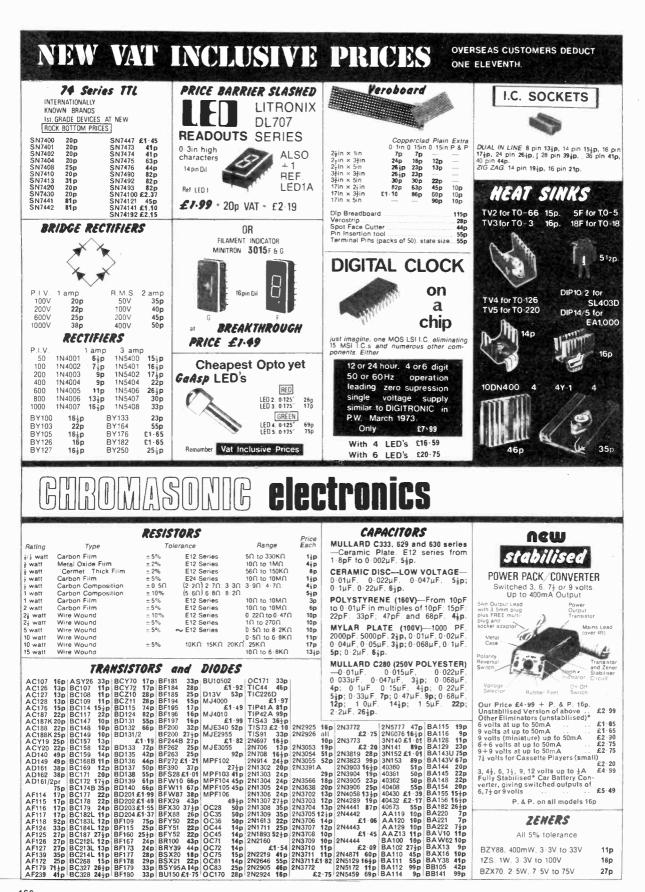
BROADCAST BANDS

Short Wave Reports by 15th of the month to Malcolm Connah, 27 Lismore Road, Highworth, Swindon, Wiltshire, SN6 7HU.

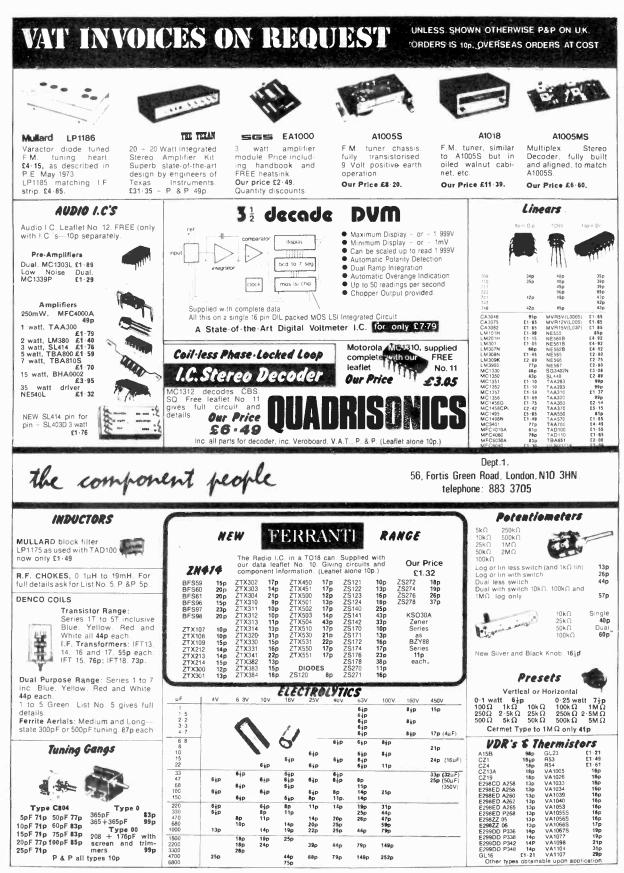
Medium Wave Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG. VHF/FM Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

AMATEUR BANDS

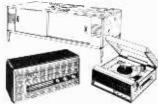
Logs covering any amateur band/s in band/alphabetical order by the middle of the month to Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey, KT21 2TW.



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The items below are from the March Sup-plement to our 1974 Catalogue. You can receive this Catalogue and the next 12 supplements by sending 66p₊



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Relay, Clare Eliot, Sealed and wire ended, 675 ohn with two pairs change over contacts. Price #1-A5

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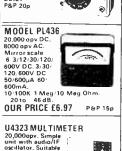
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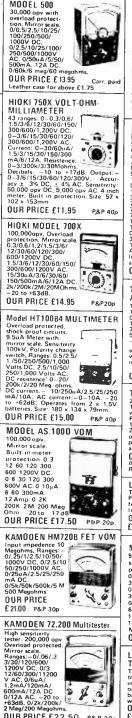


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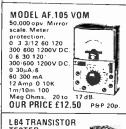




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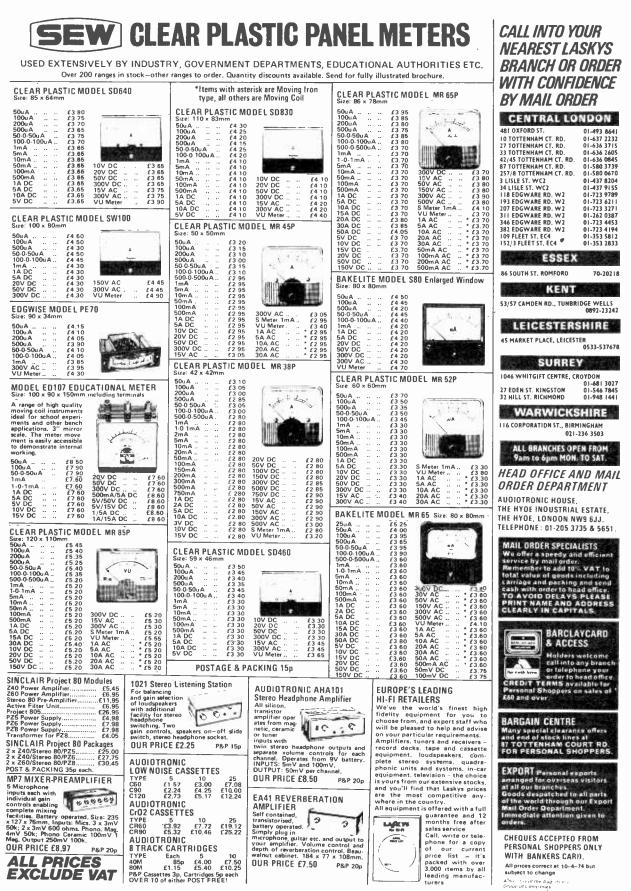


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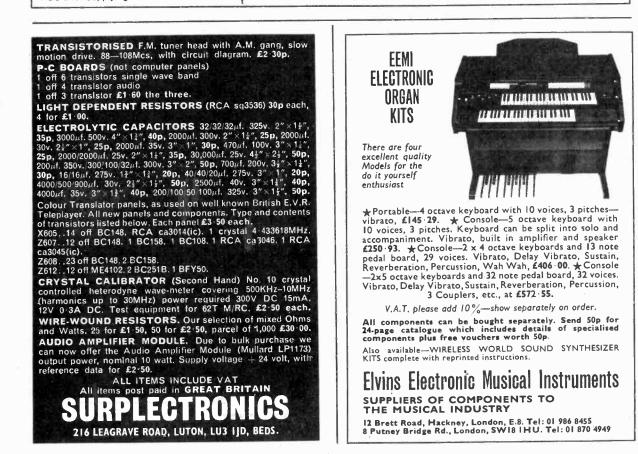
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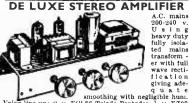
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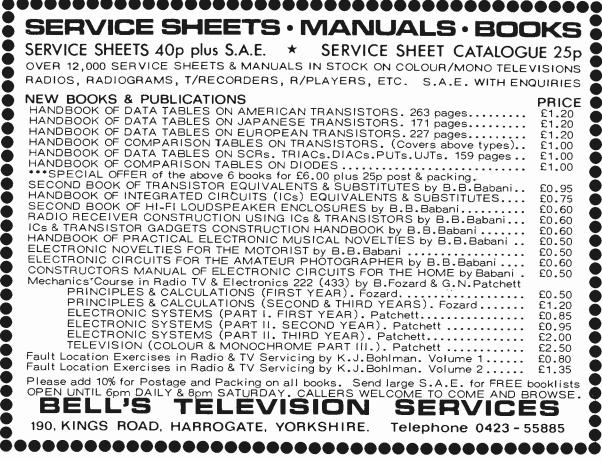
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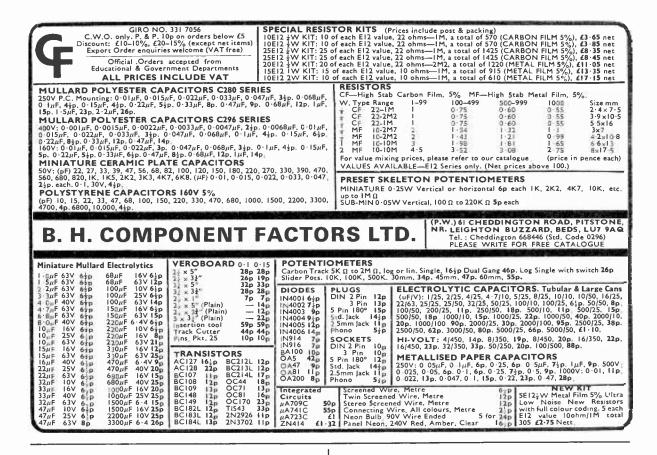
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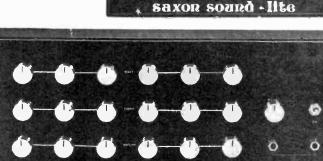
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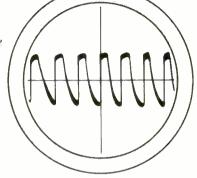
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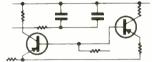


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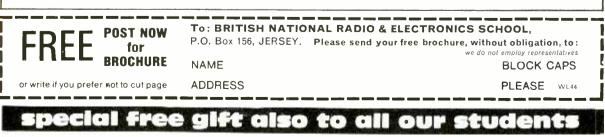


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