

# Write the Specification of your perfect iron and compare it with an Annex 

 low leak rage for delicatePrecis ion fitment

MODEL X25 Soldering Iron 220240 or 100-120 Volts. The leakage current of the NEW $\times 25$ is only a few micro dings and cannot harm the most delicate equipment even when soldered "live". Tested at 1500 v . A.C. This 25 watt ir on with its truly remarkable. heat-capdcity will easily 'out-solder' any conventionally made 40 and 60 watt soldering irons, due to its unique construction advantages.
Fitted long-life iron-coated bit $1 / 8^{\prime \prime}$ 2 other bits available $3 / 32^{\prime \prime}$ and $3 / 16^{\prime \prime}$ Totally enclosed element, ceramic and steel shaft. Bits do not "freeze" and can easily be removed. PRICE E2.05 (rec. retail) P \& P 10p. Suitable for production work and as a genera purpose iron.

MODEL CEN
220 volts or 240 volts. The 15 watt miniature model CCN also has negligible leakage. Test voltage 4000 v . A.C. Totally enclosed element in ceramic shaft. Fitted long. life iron-coated bit $3 / 32^{\prime \prime}$. 4 other bits available $1 / 8^{\prime \prime} .3 / 16^{\prime \prime}$ $1 / 4^{\circ}$ and $3 / 64^{\prime \prime}$ including Heat Shield. PRICE $\mathbf{f 2}-48$ (rec. retail) P \& P $10 p$.


Min C Minature 15 walt soldering iron fitted $3 / 32$ iron coated bit. Many other bits available from $3 / 64^{\prime \prime}$, to $3 / 16^{\prime \prime}$. Voltages 240, 220, 110,50 or 24. PRICE $\boldsymbol{E} .05$ (rec. retail) $P$ \& $P 10 p$.

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MODEL SK. 2 KIT Contains 15 watt miniature iron fitted with $3 / 16^{\prime \prime}$ bit, 2 spare bits $5 / 32^{\prime \prime}$ and $3 / 32^{\prime \prime}$ heat sink, solder, and "How to Solder" booklet. PRICE $£ 3.25$ (rec. retail) P \& P 10 p.


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## Price increase

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IKE many other magazines and paper products "Practical Wireless" has become victim of a world paper shortage resulting in massive increases in the cost of raw materials. In order to maintain the high standard of providing technical information and projects to our readers, we regret that we have been compelled to increase the cover price to 25 p .

## - NEWS \& COMMENT <br> 1048 SAVE MONEY-Leader article and April preview <br> 1049 NEWS ... NEWS ... NEWS ... <br> 1061 TELEVISION-Coming in the March issue <br> 1062 PRODUCTION LINES-Products reviewed by Colin Riches <br> 1071 NEXT MONTH IN PRACTICAL WIRELESS <br> 1081 HOTLINES on recent developments by Ginsberg <br> 1097 ON THE AIR <br> 1097 Broadcast Short Wave-Malcolm Connah <br> 1098 VHF/FM-Simon David <br> 1098 Medium Wave-Charles Molloy <br> 1101 Amateur Bands, Short Wave/VHF-David Gibson G3JDG

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SO the winter's economic crunch has come as most realistic prophets have forecast. We have read, heard, seen and experienced at first hand some of the revivals of the immediate post-war social and economic problems, not forgetting that dreaded winter of 1947. We do not intend here to rub the salt further into the wound but rather to look at ways and means of making our lives just a little more bearable.
Practical Wireless showed foresight in the autumn of 1973 which paid off. The power crises ever looming in our midst, we grabbed at the expected misfortunes in the electricity supply industry by publishing at the right time an emergency lighting unit to operate from a car battery. This proved so popular that we are now short of copies for office use. For those of you who missed it we publish in this issue a slightly different version (suggested by a P.W. reader) that uses a ready-made oscillator coil.
If you have thoughts about visiting the SONEX or other hi-fi exhibitions in the vicinity of London Airport in March, but are seriously wondering where the money to buy is going to come from, because of the Chancellor's mini-budget restrictions, again take a crumb of comfort from P.W. For less than a pound you can have not only the widest variety of do-it-yourself designs over the next three months, but also the freedom to control your own spending over whatever period you choose. You can purchase components and build your own equipment at leisure without worrying about interest charges.
This month's issue sees the start of a new hi-fi project with a difference. We do not recall ever seeing a similar project before in a magazine that incorporates a cassette recorder. We could then be justified in claiming yet another first for the do-it-yourselfer. The result is that you can save on the cost of a system for the home that gives you a.m. and f.m. radio, tape record/playback, the playing of pre-recorded cassettes, and with an added pick-up you can play back stereo discs. This quality system is in stereo and the cassette machine is left to your choice to suit your requirements and, most important, your pocket. If you are seriously interested in quadraphonic sound there is ample room in the unit to include a second pair of amplifiers and an uprated mains transformer.

If you have your own hi-fi set-up already, but you could do with a useful piece of test gear to help you set it up or locate some of those obscure faults, you will be interested in the Trouble Tracer that we published in the last two issues and the Waveform Generator in this issue.

Finally, most of you will already be hooked on our P.W. Datacard system; numbers 7 and 8 in this issue are specially designed for those who require "finger-tip" information on local reception and guidance on aerial installations.
M. A. COLWELL-Editor.


## IMPORTANT MESSAGE TO ALL READERS

Readers of "Practical Wireless" and most other magazines will be aware of the restrictions imposed by the Government and as a result of Trades Union action in various industries. To ensure that you receive your copy of "Practical Wireless" at the earliest possible date, we have to rely on effective communications and delivery through the post and by railway. We also depend on the operation of electrical equipment and printing machinery. Petrol and diesel oil are vital to the needs of our job in quick and effective processing of editorial and advertising material.
We are sure that you will understand the many problems that confront all of us. We therefore request your patience and understanding during any temporary period when publication may be delayed.
We regret that due to the effects of the current industrial situation, the number of pages in this issue has had to be limited. We apologise to advertisers who were unable to insert their full allocation of product announcements and to those unable to appear at all in this issue. Such is the "pulling-power" of Practical Wireless and its advertisements that we recommend booking early for the next available issue.

## Plessey IC book

PLESSEY Semiconductors has produced a comprehensive 235-page Databook giving details of its extensive range of silicon integrated circuits.
Continuous emphasis on the development of processes and circuits by Plessey has been demonstrated by the successful introduction of Bipolar Process III circuits and MNOS electricallyalterable non-volatile memories. The first products from these new processes are detailed in the Databook along with the wide range of both special and standard products currently available.
Copies of the Integrated Circuit Databook are available on application to Plessey Semiconductors Limited, Cheney Manor, Swindon, Wiltshire.

## Sonex rival

HI-FIDELITY ' 74 is a rival exhibition which will run concurrently with Sonex at the Heathrow Hotel. More details next month.

## ISB for broadcast radio?

WORK on the problems of a.m. broadcasting on medium and long waves has been carried out at Siemens laboratories in West Germany. The independent sideband (ISB) system, proposed by the Hamburg Institute of Radio Engineering is being seriously considered to overcome some of the problems of increasing mutual interference.
Siemens engineers are quick to point out that the review of broadcasting frequency allocation, due within the next eighteen months, should recommend ISB to enable expansion up to double the number of programme channels for the same number of transmitters. An added advantage is that ISB offers the equivalent to SSB in terms of interference, bandwidth and fading, and could be implemented locally without the need for international agreement.
The major drawback is that receiver design will have to be altered so that a phase shift network can be employed for the 150 to 4 kHz band to separate the two side-bands by at least 40 dB . ISB receivers would be capable of processing signals in the SSB and DSB modes, with improved reception on DSB by listener selection. Transmitters would probably handle signals with the dynamic range reduced by 30 dB .

## Modules and valves

AT a recent visit to the huge Mullard manufacturing complex at Blackburn recently, we were privileged to see the making of those "liquorice allsorts" coloured capacitors that are now familiar on printed circuit assemblies. Readers will also be pleased to learn that valves. mostly for television, are still being made in millions although the range of types has been rationalised to fit the economic needs of setmakers and servicemen.

We also saw the assembly of Mullard modules: the LP1185 f.m. i.f. strip; LP1186 d.c. voltage controlled tuner for Band II; LP1159 a.m. i.f. strip; LP1162 4 watt amplifier; LP1164/1 r.f./i.f. amplifier for a.m./f.m. radio; LP1402 f.m. tuner with capacitor tuning. Mullard are working on a modular design stereo decoder for release soon.

Our picture here shows the polyester foil type capacitor going through the colour code dip painting process. These are only a few of the vast activities on this 46 acre site employing approximately 4,000 people.

## Torbay A.R.S.

THE Torbay Amateur Radio Society, G3NJA, has produced its first magazine. One of the main features is that of $v . h . f . / u . h . f$ conversions of commercial equipment for the Amateur. This has been written by E. Hayman, G3ABU.

The T.A.R.S. are willing to add any readers' names to their magazine mailing list. Alternatively readers may become Associate Members for the sum of 50 p annual subscription. They would then receive a free copy.

The magazine will be produced on alternate months and further gen may be obtained by sending a s.a.e. to Frederick J. E. Bolton, G3VTQ, Top Flat, 23 Waverley Road, Newton Abbot, Devon.

## Radar pioneer dies

SIR Robert Watson-Watt, C.B., F.R.S. died on 5th December at the age of 81. Sir Robert will be one of those famous names in the U.K. associated with great electronic inventions and in his case radar.

Early in his career he worked on the use of radio to detect thunderstorms. Radio direction finding found fame for him in World War II. Civil applications include airlines and shipping; a fitting tribute being the recently opened computer assisted radar tower and communications system for shipping within a 20 mile range of Liverpool.
'The communications system was installed by Decca Radar rimited.


# A venatile WMAFFRRM Generator 

## J. B.DANCE M.Sc

THE Signetics NE566 integrated circuit function generator can be used to construct a simple unit which will provide a variety of waveforms over a very wide frequency range.

The prototype unit will be described in detail. However, a number of variations will be discussed so that individual readers can make modifications which may make the unit more useful for their own particular purposes.

The basic waveform generator produces triangular waves and square waves, and it is especially suitable for use in audio amplifier testing. An additional circuit can be used to produce sine waves in addition to the other two waveforms. The circuit can be modified to produce rising or falling waveforms of high linearity instead of the triangular waveforms. In this case short rectangular pulses are available at the output which previously provided square waves.

## THE BASIC CIRCUIT

The circuit of the basic function generator is shown in Fig. 1. The voltage at the slider of VR1 is applied to pin 5 of the NE566V and also pin 6 via C1. The
current passing to this latter pin is determined by the value of the voltage at this pin and by the resistance between it and the positive line. This current is used to charge and discharge the capacitor selected by S1b.

A Beckman 'Helipot' precision ten-turn helical potentiometer is employed for VR1 together with a Beckman turns counting dial; this enables the frequency of oscillation to be set reasonably accurately. The value of R1 has been chosen so that the potential at pin 5 never falls below threequarters of the positive power supply line potential (as recommended by the manufacturers of the integrated circuit).

The frequency of oscillation is proportional to the voltage between the positive power supply line and pin 5; this voltage is in turn proportional to the resistance of VR1 between the positive line and the slider. In the circuit of Fig. 1, the frequency of oscillation is set to $10 \mathrm{~Hz}, 100 \mathrm{~Hz}, 1 \mathrm{kHz}, 10 \mathrm{kHz}, 100 \mathrm{kHz}$


AThe finished waveform generator with its direct reading dial. The necessary components to produce a ramp waveform can be added to the circult board. For converting triangular waveforms to sinewaves a separate unit is required.

Fig. 1: Circuit of generator producing square and triangular waves over a wide range of frequencles.
or 1 MHz (depending on the range) when the slider of VR1 is set at $10 \cdot 0$. At other settings of the dial, the frequency is closely proportional to the dial setting. For example, a dial setting of $5 \cdot 67$ on the 1 kHz range produces an output of 567 Hz .

Many types of capacitor (especially electrolytic types) have very wide tolerances in their capacitance value. It is therefore necessary to calibrate the frequency at one point on each range to obtain accurate frequency readings. In the circuit of Fig. 1 this is accomplished by the adjustment of a different trimmer potentiometer (VR2 to VR7) for each range used. The switch which selects the trimmer, Sla, is ganged with that which selects the range capacitor, S1b.

## FREQUENCY COVERAGE

The frequencies available from the six adjustable ranges employed are shown in Table 1. The upper frequency limit of 1 MHz is determined by the characteristics of the integrated circuit used. In the table it has been assumed that a frequency range of $20: 1$ may be covered using any one capacitor. However, more accurate frequency settings may be obtained by limiting the coverage of each range to $10: 1$, as was done in the prototype.

| RANGE | CAPACITOR | FREQ. COVERAGE |
| :---: | :---: | :---: |
| $\mathbf{1}$ | $10 \mu \mathrm{~F}$ | $0.5 \mathrm{~Hz}-10 \mathrm{~Hz}$ |
| $\mathbf{2}$ | $1 \mu \mathrm{~F}$ | $5 \mathrm{~Hz}-100 \mathrm{~Hz}$ |
| $\mathbf{3}$ | 100 F | $50 \mathrm{~Hz}-1 \mathrm{kHz}$ |
| $\mathbf{4}$ | 10 F | $500 \mathrm{~Hz}-10 \mathrm{kHz}$ |
| $\mathbf{5}$ | 1 nF | $5 \mathrm{kHz}-100 \mathrm{kHz}$ |
| $\mathbf{6}$ | 100 pF | $50 \mathrm{kHz}-1 \mathrm{MHz}$ |
|  |  |  |

TABLE 1. Tolal frequency coverage possible with six capacilors. In practice each range is reduced to a rallo of $10: 1$.
The writer has found that a frequency range of about $30: 1$ is about the limit with any one capacitor. At settings of the frequency dial of less than about 0.3 the output waveforms become distorted, whilst oscillation ceases at settings below about $0 \cdot 25$. It was noted that the square waveform at 1 MHz was somewhat distorted. The lowest frequency range in the prototype was 0.5 to 10 Hz and it is assumed that most readers will not require frequencies below this value. Extra ranges can easily be added if required. However, an additional trimming potentiometer must be included in the Sla circuit for each extra range. A $100 \mu \mathrm{~F}$ capacitor in the Slb circuit can be used to produce a range of 0.05 to 1 Hz , a $1000 \mu \mathrm{~F}$ capacitor a range of 0.005 to 0.1 Hz and a $10000 \mu \mathrm{~F}$ capacitor a range of 0.0005 to 0.01 Hz ( 0.0005 Hz is one cycle in about 33 minutes).

When using very large capacitors, check that their leakage current is not excessive. The lowest possible frequency is probably about one cycle every few hours, but the writer has not tried to obtain frequencies quite as low as this. Some industrial applications may be found for generators of extremely low frequencies.

## CONSTRUCTIONAL NOTES

The basic oscillator circuit of Fig. 1 was constructed in an Eddystone die-cast box of approximate dimensions $4^{3} \times 3^{1}{ }_{2} \times 2^{1}{ }^{1} \mathrm{in}$. (Cat. 6908P). The Helipot VR1 and switch S1 are mounted in the base of the box and the circuit board along one of the


Fig. 2: General layout of components in the die-cast box.
longer sides Fig. 2. No components were mounted on the lid of the box since this procedure enables the lid to be removed without the inconvenience of having wires between it and the main part of the box.

The six miniature Beckman trimmer potentiometers are mounted on the circuit board Fig. 3, their connecting tags being inserted through holes in the board and bent over before the connecting wires are soldered. The integrated circuit socket is also mounted on the circuit board by passing the pins through holes in the board and soldering the connections to them.
C 1 is mounted on the circuit board, but C 2 to C 7 are mounted around the switch S1. No power supply was included in the box, since it is generally more convenient to employ an external 12 V battery. However, a mains power supply could be included if a rather larger box is employed.
If the circuits for the ramp and short pulse generator are required, they must be included in the basic oscillator unit itself. However, if the tri-angle-to-sine wave converter is made, it will probably be more convenient to construct it on a separate circuit board.

## CALIBRATION

The best way of calibrating the frequency settings involves the use of a digital frequency meter which automatically counts the pulses from the oscillator over a timed period. Alternatively a pulse counter may be used with a manually operated stop watch.
Calibration may also be carried out using a good oscilloscope with a calibrated time base. Alternatively the calibration may be set by adjusting the
trimming potentiometers so that the output 'zero beats' with the signal from a calibrated generator. At higher operating frequencies harmonics of the square wave output may be allowed to beat with a radio signal, using a receiver.
If very low frequency ranges are incorporated in the unit, the operating frequencies are best determined by connecting a voltmeter across the square wave output and timing the movements of the meter needle.
It is normally best to calibrate the unit at a point near to the highest frequency on each range. The linearity of the resistance of VR1 with the dial setting is very good (better than $0.25 \%$ ). However, the writer has found that the frequency of oscillation of the NE566V may depart from linearity by up to about $\pm 1 \%$ at the lower frequencies in each range.
If a constructor does not like an instrument in which the oscillation ceases at the very low frequency end of each range, it is possible to set the dial so that it reads from 1.0 to $11 \cdot 0$. In this case a 100 ohm resistor, preferably of $0.5 \%$ tolerance, should be inserted between the upper end of VRI and the positive supply line in Fig. 1 so that the readings are directly related to the frequency of oscillation. Operation in this way is likely to increase the errors in the frequency settings, since the percentage linearity tolerance of a precision helical potentiometer is typically about ten times better than the resistance value tolerance.

## OUTPUTS

The circuit of Fig. 1 provides good square waves and also linear triangular waves, both at 50 ohm output impedance. These outputs are adequate for many applications, since the triangular waves can
often be used instead of sine waves when their harmonic content is not disadvantageous.

Both of these output waveforms are superimposed on steady positive potentials. The latter can be removed by capacitive coupling except at low frequencies where it is difficult to obtain an adequate time constant to preserve the waveform. The average potential of either of the output waveforms can be made equal to earth potential by employing a power supply consisting of suitable positive and negative supply voltages both isolated from earth.

## TRIANGLE-TO-SINE CONVERSION

If a sine wave with a relatively low harmonic content is required, a diode-resistor shaping network may be employed. A fairly complex circuit is required if the shaping must be carried out reasonably accurately. A simpler solution involves the use of the conversion circuit described below.

At a fixed gate voltage, the first part of the drain characteristic of a junction field effect transistor (FET) approximates to half a sine wave. However, further increase of the drain voltage produces little effect on the drain current. The first part of this characteristic can be employed to shape a triangular wave into a reasonably good sine wave. If a triangular wave is applied to this circuit the positive going part of this waveform will produce a drain current of half a sine wave. In order that both the positive and negative parts of the triangular wave shall produce the corresponding parts of a sine wave, the type of circuit shown in Fig. 4 may be employed. This utilises the fact that the drain and source electrodes of an FET are essentially interchangeable.


Fig. 3 : Veroboard pins are used to support the few components on the circuit board. The
 trimmer potentiometers are used to adjust the callbration of the six frequency ranges.


Triangular wave to
sine converter
Fig. 4: Sultable circuit for converting a triangular wave to a sine wave.

## PRACTICAL SINE CONVERTERS

It should be clear that the amplitude of the triangular wave applied to the circuit of Fig. 4 is quite critical if one requires a good sine wave output. If the input to this circuit is too large in amplitude, the output pulses will have fairly flat sections in place of the normal sine wave peaks. If the input amplitude is too small, the output will be approximately the same form of triangular wave as the input.

It must therefore be possible to alter the amplitude of the triangular wave fed to the circuit of Fig. 4. In addition, the output impedance of the source of the triangular waves must be small and there must be no steady voltage superimposed on the triangular waves. An amplifier of variable gain and of low output impedance is therefore employed between the output of the 566 circuit and the input of the triangle-to-sine converter.

## CONVERTER CIRCUIT

The circuit of a practical triangle-to-sine wave converter is shown in Fig. 4. The triangular wave input from the circuit of Fig. 1 is capacitively coupled to the input of a Signetics NE531V high slew rate operational amplifier; it therefore follows that this circuit is unsuitable for use at very low frequencies with the values shown, since the coupling time constant would be inadequate.
The complementary output transistors Tr and Tr 2 provide a low impedance output to the converter circuit of Tr3. The preset potentiometer VR1 is set so that the potential at the emitters of Tr and Tr 2 is zero volts when no input is applied to the circuit.
The voltage gain of the circuit of Fig. 4 from the input to the emitters of $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$ is equal to the resistance of VR2 divided by R1. The amplified triangular wave is applied to the circuit of Tr3, the operation of which has already been discussed. The author found that the sine wave output voltage was of the order of 0.7 V peak to peak and that it has no steady component superimposed on it.

The gain control, VR2, must be set carefully so that the output waveform shows minimum distortion, adjusting the gain whilst examining the output waveform by means of an oscilloscope. If, however, a waveform analyser is available, VR2 may be adjusted for minimum third harmonic distortion.
A satisfactory sine wave was obtained using fixed resistors for R7 and R8. However, one of these resistors may be replaced by a 50 ohm resistor in series with a 100 ohm preset trimmer so that the output may be adjusted for minimum second harmonic distortion (preferably using a waveform analyser). It should then be possible to obtain a sine wave output with very low distortion.

The writer tried replacing the NE531V integrated circuit with a $\mu \mathrm{A} 741 \mathrm{~V}$ which has the same connections. It was found that the NE531V could operate at higher frequencies, but in neither case could satisfactory operation at 1 MHz be obtained.


The secret of the direct frequency read-out lies in the use of the multturn Hellpot potentlometer, right centre.

A simple circuit using two cascaded emitter followers for driving an FET triangle-to-sine converter was published in the February 1973 issue of Wireless World. However, a circuit with voltage gain is required when the triangular wave output from a 566 , operated from a 12 V supply, is to be converted into a sine wave.

## RAMP WAVEFORM GENERATORS

The circuit of Fig. 1 can be easily converted into a generator which produces either a rising or a falling linear ramp waveform. At the end of each ramp the output quickly returns to its initial level and another ramp commences.

In order to produce a rising ramp waveform, the capacitor connected to pin 7 is allowed to charge, but at the end of the charging period it is rapidly discharged. The ramp waveform appears at pin 3 of the 566 in place of the triangular wave. A falling ramp is produced in a similar way; at the end of the discharging period, the capacitor connected to pin 7 is rapidly re-charged.

## RAMP CIRCUITS

Fig. 5 shows the components which must be added to the circuit of Fig. 1 to allow either rising or falling ramps to be produced. When the switch S2 is in position 1, the additional components shown dotted are not used and the circuit therefore provides the normal square and triangular output waveforms. When S 2 is in position 2, a falling ramp waveform is generated, whilst in position 3 a rising ramp is formed. Short negative going pulses are available at pin 4 when S2 is in position 2 and short positive pulses when S2 is in position 3.

Let us now consider in detail the operation of the falling ramp generator when S2 is in position 2.

If the output from pin 4 is in its high voltage state, little current passes through D1 of Fig. 8. The base and emitter of Trl are therefore at about the same potential and this transistor passes little


Fig. 5: Additlonal circuitry, shown dotted, to produce rising or falling ramp waveforms.

## components list

| R1 $3.6 \mathrm{k} \Omega 5 \% \pm \mathrm{W} \quad$ R2 $2.7 \mathrm{k} \Omega 10 \% \div \mathrm{W}$ VR1 $1 \mathrm{k} \Omega 0.25 \%$ linearity (Beckman 'Helipot' Type |  |
| :---: | :---: |
|  |  |
| VR2-7 5 k ת trimmer pots | (Beckman Type 89P) |
| C1 1nF C2 100pF | C3 1 nF |
| All 25 V polystyrene |  |
| C4 10 nF C5 100 nF | C6 $1 \mu \mathrm{~F}$ |
| All 25 V polyester |  |
| C7 $10 \mu \mathrm{~F} 24 \mathrm{~V}$ electrolytic |  |

## Miscellaneous

IC1, NE566V (Low cost alternative is LM566Ambit International). 8 pin DIL socket. S1, 2 pole, 6 way rotary switch. Turns counting dial for Helipot (Beckman Type RB). Die-cast box (Eddystone Type 6908 P ). Piece of plain veroboard. (Note: VR1 with dial and VR2-7 available from Athena SMC Ltd., 140 High Street, Egham, Surrey).
Basic Components for Triangular-Sine Wave Converter

| R1 | $3.9 \mathrm{k} \Omega$ | R2 | $4.7 \mathrm{k} \Omega$ | R3 | $10 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R4 | $10 \mathrm{k} \Omega$ | R5 | $1 \mathrm{M} \Omega$ | R6 | $1 \mathrm{M} \Omega$ |
| All $10 \%$ | $\pm \mathrm{W}$ |  |  |  |  |
| R7 | $100 \Omega$ | R8 | $100 \Omega$ |  |  |

Both $1 \% \frac{1}{2}$ W
VR1 $10 \mathrm{k} \Omega$
C1 $10 \mu \mathrm{~F} 15 \mathrm{~V}$
D1-4 1 N914
Cr 2 C 2100 F 15 V
Tr1 2N697 Tr2 2N2904
NE531V (Low cost alternative is
LM318H-check leadout connections)
Basic Components for Ramp Wave Converter

| R1 | $22 \mathrm{k} \Omega$ | R2 | $10 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: |
| R3 | $4.7 \mathrm{k} \Omega$ | R4 | $22 \mathrm{k} \Omega$ |
| All | 10\% $\frac{1}{2} \mathrm{~W}$ |  |  |
| D1 | 1N914 | D2 | 1N754 |
| Tr1 | 2N3703 | Tr2 | 2N697 |

current. The output from pin 3 therefore falls linearly with time, unaffected by the additional components.
When the output from pin 4 falls to its low voltage state, however, Dl conducts and the base of Trl becomes negative. This PNP transistor therefore conducts and rapidly charges the capacitor selected by Slb. The voltage at pin 3 therefore rises rapidly to its maximum value before a further falling ramp. is generated.

The output from pin 4 consists of short negative going pulses which occur each time the ramp waveform at pin 3 rises to its maximum value. These waveforms are shown in Fig. 6. When the capacitor selected by Sib is small, the negative going pulses at pin 4 were found to be about $0.2 \mu \mathrm{~s}$ in length.


Fig. 6: Waveforms obtainable from the circuit of fig. 5.


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When a large capacitor is in circuit, however, it takes longer to charge from the current passing through Trl. Nevertheless, the time for which the waveform at pin 4 is in its low voltage state is a very small fraction of the total operating time.

The operation of the rising ramp generator, when S2 is in position 3, is rather similar. When the output at pin 4 is in its low voltage state, the zener diode D2 passes little current and $\operatorname{Tr} 2$ remains cut off. During this time the ramp waveform at pin 3 is rising.

When the voltage at pin 4 switches to its upper level, however, the zener diode conducts and $\operatorname{Tr} 2$ receives a positive bias at its base. This NPN transistor therefore conducts and rapidly discharges the capacitor selected by Slb. The potential at pin 3 therefore returns quickly to its lowest level and the ramp commences to rise again.

The output from pin 4 consists of short positive pulses which occur each time the ramp at pin 3 returns to its lowest level.

The rising ramp generator was found to give a poor waveform on the 1 MHz range. However, the rising and falling ramp generators both operated satisfactorily on the other ranges and also at very low frequencies. The writer tried them at frequencies down to about 0.01 Hz and at such frequencies the waveform takes a fraction of a second to return at the end of each ramp.

When either of the ramp generators is employed, the one half of the triangular waveform is eliminated. The frequency of oscillation of the 566 is therefore approximately doubled when $S 2$ is in position 2 or 3. Constructors who intend to use the unit mainly for ramp waveform generation may wish to calibrate the unit so that the ramp frequency can be read directly from the Helipot dial. The dial reading must then be halved to obtain the frequency of the triangular or square wave.

## APPLICATIONS

The fundamental frequencies from the waveform generator can be used to test the functioning of audio amplifiers; they also cover the long wave band and the low frequency end of the medium wave band. In addition, the outputs contain harmonics (mainly odd harmonics) which can be used to test the functioning of radio receivers throughout the medium wave band and also at somewhat higher frequencies.

Both the triangular waves and the ramp waveforms are very suitable for the detection of crossover distortion in audio amplifiers, since these waveforms are essentially linear. If the triangular wave output is fed to the input of an audio amplifier which introduces cross-over distortion in its output stage, the type of waveform shown in Fig. 7a is obtained. The values of the resistors in the audio amplifier which control the quiescent current in the output stage may be altered so as to increase this current slightly; the cross-over distortion should disappear when the quiescent current is sufficient.

It is easier to detect cross-over distortion when using the triangular or ramp waveforms than when the more conventional sine wave is employed. A frequency in the mid-audio region is ideal for this test (perhaps 1 kHz ). The linearity of the waveform on the oscilloscope screen may be measured by placing a straight edge along the tips of the waveform.


Fig. 7a-b-c: Waveforms at the output of an audio amplifier using input signals from the waveform generator.
The square wave output is also very useful for testing audio amplifiers. At fairly high frequencies one may examine the output from an amplifier for ringing of the type shown in Fig. 7b. Ideally there should be no overshoot or ringing. An audio amplifier which can faithfully reproduce a square wave at a frequency of about 10 kHz must have a good frequency response in the high audio frequency region since square waves contain many harmonics and will be reproduced satisfactorily only if the amplifier has a fairly level response at frequencies of up to at least three times the fundamental frequency of the square wave.

If an audio amplifier has only a moderately good high frequency response, the corners of the output waveform will be rounded off at 10 kHz , as shown in Fig. 7c. An approximate value for the frequency response of the amplifier may be obtained by estimating the time taken for the output waveform from the amplifier to rise from $10 \%$ to $90 \%$ of its final value. The maximum frequency at which the response is reasonably constant is of the order of $1 /(3 \times$ the rise time). if the rise time of a square wave is very short, one sees only the lines at the top and bottom of the oscilloscope display, the rising and falling parts of the waveform being so short that they are barely visible.

One can also use the square wave output from the 566 unit to examine the low frequency response of audio amplifiers. As one reduces the frequency of the square wave, the upper and lower parts of the output waveform do not remain horizontal, but develop a definite slope. At very low frequencies, a differentiated waveform will be obtained. The input of the oscilloscope marked 'DC' should be used for these low frequency tests, since the ' AC ' input is connected to a series capacitor inside the oscilloscope which may distort the waveform.

In the audio amplifier tests discussed above, it has been assumed that the amplifier under test has a volume control at its input which can be adjusted to provide the required signal output level. At high levels it will be necessary to include a series canacitor in the input circuit to block the steady voltage at the 566 outputs. In this case care should be taken to ensure that the coupling time constant is adequate for the lowest frequency to be employed.

# DRY BATTERY CHARGER <br> <br> R.A.Butterworth 

 <br> <br> R.A.Butterworth}

MOST of us either make or buy a mains supply unit to operate our battery tape recorders, receivers etc., when used at home to save the cost of dry batteries. However batteries are still needed around the home and unfortunately they seem to cost more each time. One could of course use rechargeable cells but they are cxpensive and need a rather special charging unit which is also expensive.

If we could get a few more hours out of our dry battery we could cut our costs considerably, even one more 'run' would be equivalent to cutting the cost by a half. With the charging units described here two, three or more 'lives' can be given to a set of batteries, perhaps not quite as long a period of operation as the first but certainly for periods long enough to make the building of a charger show an economical return for the effort involved.

The idea of reforming dry cells is by no means new. Investigation of the possibilities were made as long ago as the early 1950's with encouraging results. With modern methods of manufacture and materials, the life of the primary cell can be considerably extended if a few basic rules are born in mind. These are:

1 The battery must be charged before its voltage (on load) drops from 1.5 V to below 1 V .
2 It must be put on charge as soon as possible after being removed from service and put into service as soon as possible after re-charge.
3 It is not economical to charge a single unit, a 1.5 V 'pen light' HP7 for example. Therefore it is better to have one set of batteries in service and another on charge.
4 The charging rate should be adjusted to distribute the charge, in other words avoid heating up the cell by charging at too high a current.
5 If there is the slightest suspicion of battery leakage throw them away or you will have a horrible mess to clear up.
The cylindrical types like the U2, U1l and HP7, respond much better than the layer batteries, such as the PP3. The use/charge cycle is less than half that of the cylindrical types. The table gives details for popular zinc-carbon types which have responded successfully to several use/charge cycles with the equipment shown.

## Battery holders

Standard battery holders can be used to hold the cells whilst charging in blocks of 2,4 , or 6 . From experience it would appear that, after setting at the current showh, if after the first couple of hours there

is no drop in the charging current, then discard the battery as the electrolyte has probably dried out. If the batteries get appreciably warm or show signs of leaking throw them out. Different sets of batteries have given a different number of cycles. This, the author believes, is due to 'freshness' of the unit cells when first purchased; in other words how long they had been on the shelf in store.

## DRY BATTERY CHARGING

| Battery | Use | No. of <br> Cells | Charging <br> Current <br> mA <br> Min. | Max. <br> hours. <br> of <br> charging | No. of <br> cycles |  |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: |
| U2 | Torches, <br> Hand lamps <br> Radios | 4 <br> 6 | 150 | 300 | 5 | 3 |
| Umall <br> U11 <br> Torches, <br> Radios | 1 or2 <br> Cassette <br> Tape <br> Recorders | 4 | 100 | 150 | 4 | 4 |

In the circuits shown in Figs. 1 and 2 it will be noted that very little smoothing of the d.c. output has been incorporated. This is deliberate; investigation has shown that it is advantageous to have a little a.c. present. This "dirty d.c." appears to shake up the electrolyte and therefore assists in the reforming.


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 MENT CASE－A MODELS Model 120 all aluminturn two payrconstruction．Top atid sldes．blur construction．ToD athd sides．blur base：white．Others
hree part construction．
Top，hase．bldes and detachabl
rear panel，blue harnmer．Detach able aluminium front panel finsishel th ahite Dimensions la inchen

| Model | W | 11 | D | Price |
| :---: | :---: | :---: | :---: | :---: |
| 120 | 8 | 21 | 6 | 21.85 |
| $\because 20$ | 8 | 6 | 31 | 29．65 |
| 221 | 8 | 6 | 6 | 18.80 |
| 320 | 12 | 8 | 12 | 25.00 |
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Chassis for model $3: 0 \quad 21.75$ extra LARGE
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| TRANSISTORS，DIODES \＆IC＇s． |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| ACl27 | 25p | BF194 | 15p | 0.490 | 7 p |
| ． Cl 128 | 20 p | BFY51 | 13p | O．A91 | 6p |
| dClis | 17p | MPF102 | 36 p | $1 \times 914$ | 40 |
| AD149 | 47p | $\mathrm{OCH}_{4}$ | 20p | 1 N 4148 | 4 |
| AD161／2 | 68p | $0 \mathrm{C71}$ | 20p | 1：4001 | 6 p |
| BC107 | 10p | T1843 | $28 p$ | 1N 4002 | 61p |
| BCl08 | 10p | 2N1711 | 24p | 1N4003 | 70 |
| BC109 | 10p | 2N2219 | 259 | 1N4004 | 7 p |
| BCl47 | 10p | 2N2646 | 45p | 1N4005 | 8p |
| 13C148 | 10p | 2N2905 | 33D | 1） 14006 | 810 |
| BCl49 | 12D | 2N2907 | 250 | 1N4007 | 90 |
| BC168 | 13p | 2N29260 | 10 p | W005 | 30 D |
| BCl 69 C | 12p | 2N2926 ${ }^{\text {P }}$ | $10 p$ | W04 | 33 p |
| BC182L | 10p | 2S2926G | 10 p | 741C 8．pin |  |
| BC204 | 14 p | 2 N 3053 | 18p | D．1．L． | 88 p |
| BC209C | 140 | 2N3055 | 49p | 741 C 14－pin |  |
| BD131 | 45p | 2N3819 | 24p | D．1．L． | 45p |
| SD132 | 543 | AA119 | 70 | D．I．L．Sock |  |
| BD131／2 | 21.20 | BY127 | 16D | 8 －pio | ${ }^{20 p}$ |
| BD135 | 360 | BY164 | 40p | 14－pin | 15 | See our catalogue

I．C．＇s hridges etc．

## PLUGS AND SOCKETS



## din pldgs


 $\begin{array}{llll}\left(180^{\circ} 0^{\circ}\right. & 5 & \text { pin } & \text { pin } \\ \left(240^{\circ}\right) . & 6 & \text { pin } & 10 p\end{array}$ $8 p$
pin
B
$7 p$


## MAIMS

 chassis ${ }^{3}$ pin $\begin{gathered}\text { plig } \\ \text { with } \\ \text { Hine socket }\end{gathered}$ padr81
2190
3
DIN Sockets
$\qquad$ ${ }_{3}$ pin， 4 pin． $\mathrm{A}\left(180^{\circ}\right), \mathrm{B}$ pin B
$\left(240^{\circ}\right) . \mathrm{B}^{2}$ ${ }_{\left(240^{\circ}\right) .6^{\circ}} \mathrm{pin}^{7}$

## POTENTIOMETERS

Rotary miniature carbon track $\mathbf{t}^{\prime \prime}$ apindle
Slingle gang Lin or Log


PP3， 6 etc．battery clip dual min．
PP1， 9 etc．hattery clip separate per pair 8 p ． Pair crocodile ellips 1 red， 1 black Insulated sleeve．
Solder Multicore 22 swg 10 metrea $\quad 20$ p Silicone grease in apecial dispenser 20 ml ．43p Red neon 240 V panel mounting 25p Lacing Cord Strong rason cored PYC 25 m ．
Panel tuse bolders 20 mm 20p； $1 \mathbf{z}^{\prime \prime} \quad 30 \mathrm{p}$
Transformers
LT700 min．output transformer Pri． $1.2 \mathrm{k} \Omega$ 8 cc ． $\mathrm{s} \Omega 200 \mathrm{~mW}$
Suh－min．Mains Tranalormer
6.0 .6 V 100 mA
$12 \cdot 0-12 \mathrm{~V} 80 \mathrm{~mA}$
Size：Both approx． $30 \times 27 \times 25 m \mathrm{~m}$ ．
Min．Maina Transfornuer（Size： $48 \times 31 \times$ $38 \mathrm{~mm}) 0.12 \mathrm{~V} 250 \mathrm{~mA}, 0-12 \mathrm{~V} 250 \mathrm{~mA}$ A 61.35 Maina tranaformer 31T3AT
Prl．200－220－240V．Sec．12．15－20．24－30V 2A
Maina Transormer MTemat

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Dual gang （Stereo）without ${ }_{5 k}$ witch 2 M Lis above 38 g ．

Slogle gang with DP switch


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Wirewound $10 \% 1$ Wi $z^{\prime \prime}$ spindle 10， $60,100 \mathrm{R} 84 \mathrm{p} ; 250,500,1 \mathrm{k}$ ， 5 k 33p；10k，87p；25k 40p；50k 44p．

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KNOBS


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## Charger units

Fig. 1 shows a simple unit which can be easily put together and used to try out the idea. A good quality bell transformer, BY100 diode, m.e.s. lamps, lamp holder and a $220 \Omega 1 W$ resistor and you are in business. The writer found this unit successful but it lacked flexibility. If the bell transformer shown in Fig. 1 has various outputs then the number of cells to be charged can be varied and by changing the lamp the charging current can be varied within limits.

Fig. 2 is a more elaborate unit and in the author's case serves two purposes; A dry battery charger and mains unit for various equipment used in the shack. Should additional smoothing be required then it is a simple matter to add this. It is advisable to install the meter permanently so that the charging current can be monitored. A d.p.d.t. switch with a suitable shunt series resistor would enable both voltage and the current to be monitored. Diode D6 provides for reversal protection and prevents the battery discharging through the $470 \Omega$ resistor.

Zinc-carbon batteries are very amenable to recharging.


Fig. 2: A more elaborate design.

## * components list (Fig. 2)

| R1 | $10 \Omega \frac{1}{2} \mathrm{~W}$ |
| :--- | :--- |
| R2 | $470 \Omega 1 \mathrm{~W}$ |
| VR1 | $500 \Omega 3 \mathrm{~W}$ linear wirewound |
| C1 | $500 \mu \mathrm{~F} 20 \mathrm{~V}$ |
| C2 | $2 \mu \mathrm{~F} 20 \mathrm{~V}$ |
| Tr1 | OC36, OC28 or similar rating |
| T1 | Mains transformer 12.5V 1A secondary |
| D1-D4 | 1N4001 diodes |
| D5 | 1N4001 diode |
| D6 | 1N914 diode (see text) |
| M1 | Meter 300mA f.s.d. |
| S1 | Double-pole on/off toggle switch |
| LP1 | 3.5 V or $6.5 \mathrm{~V} 0.1 / 0 \cdot 2 \mathrm{~A}$ (Fig.1) |

NEXT MONTH
An Automatic Battery Charger for 12 volt car batteries.

## TEEEUSTII

## IN THE MARCH ISSUE

## ASSEMBLING A MODULAR COLOUR SET

There are various ways of going about building a colour receiver. One approach is to make use where possible of manufacturers' surplus units. David Robinson describes the set he built on this basis and how the various problems of interfacing different units not originally intended for use together were overcome.

## LOG-PERIODIC SET-TOP AERIAL

A simple log-periodic set-top aerial can be made using printed circuit board. Full constructional details will be provided.

## TV SET SAFETY

With the introduction of the BEAB television receiver testing system and BS415:1972 there has been a tightening up in safety requirements. It is essential that anyone handling TV sets should be aware of what is involved. A detailed account starts next month.

## FAULT FINDING

John Law looks at the power supply and line timebase circuits used in BRC 18 in . dualstandard portable models. These make excellent second sets.

## PHASEIN COLOUR TV

The phase of the chrominance signal indicates the colour being transmitted: phase is thus the key to colour television. A special article next month describes the basic technique and PAL signal processing, paying particular attention to practical points that are not always made clear.

## PLUS ALL THEREGULAR FEATURES

Details of the March issue are subject to the current national situation at the fime of going to press.


# production LINES coliniciches 

 coliniciches}

## JOSTY KITS

Our Advertisement Manager has asked me to point out that Swanley Electronics will not be supplying "Josty" kits as per their December advertisement.

## HEATHKIT CATALOGUE

The latest catalogue from Heath (Gloucester) Limited contains details of the company's kits and some new models featured for the first time include the GR-990 12in. Black and White Television kit for either 12 V or mains operation; the GD-39 Home Intrusion Alarm, disguised as an unobtrusive book - an ultrasonic burglar alarm/surveillance system; the CR-1008 a.m. Radio and the CM-1045 Small Engine Tune - up Meter.
Also included are the 10-104 Solid State 15 MHz Oscilloscope; IB-1103 180 MHz Frequency Counter; the GC-1005 Electronic Digital Clock which incorporates a 'snooze' alarm; the CR9502 Push-Button a.m. Car Radio and the IC-2108 Desk Top Electronic Calculator.
Readers may obtain their free catalogue by writing to Heath (Gloucester) Limited, Bristol Road, Gloucester, GL2 6EE.


## SCREW DRIVING BOON



Thunder Screw Anchors Ltd. announce an addition to their range of screwdrivers by the introduction of tour screwholding screwdrivers. Two are suitable for slotted head screws and two for recessed head screws, their dimensions being $8 \frac{1}{2} \mathrm{in}$. and 94 in . overall length, $3 / 16 \mathrm{in}$. and tin. blade diameter respectively. The screw is firmly held at the tip of the screwdriver by sliding the springloaded shank over the head of the screw, (see picture) leaving one hand free to hold the article to be fixed. It is possible to fix screws or bolts in the most difficult of places, where to hold a screw in the hand might normally be impossible.

Prices, excluding V.A.T. are 20372 and 20376 69p each, 20374 and 20378 $79 p$ each.

We understand that due to the shortage in the foreign plastics industry, supplies of these screwdrivers may be subjected to extended delay. However, this firm does have some further useful and novel tools that would be of interest to readers. Supplies are through retail outlets. Thunder Screw Anchors Lid., Victoria Way, Burgess Hill, Sussex, RH15 9NF.

## MICROELECTRONICS

We apologise to Microelectronics for being unable to include their advertisement in the Feb. issue. If readers refer to this month's issue, page 1028, they will see that the company markets the Minicomp 100 Random Number Selector. When the button
on the front panel is pressed, numbers are displayed at high speed on a Nixietube read-out before a random number is displayed-in effect a miniature "ERNIE".

The circuit includes 6 TTL logic i.c.'s and three transistors and the manufacturers say that typical applications include number selection for dice, roulette, bingo etc. Price of the Minicomp 100 kit is $£ 42 \cdot 50$. A fully assembled version is available at £45•00.-Microelectronics, 51 Mexfield Road, London, SW15 2RG. (Tel. 01-870 2368).

## ONE-HAND DESOLDERER

When desoldering, have you ever wished you had three hands? Well, here is something that will brighten your day!

Only one hand is required to operate the Picard soldering/ desoldering iron. The whole body of the tool forms a suction tube which is pressed down towards the job during heating and released to produce suction.
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The bit is made of alloy steel and molten solder is sucked through it by the release of the spring-loaded body. The faster the release, the stronger the suction. The solder collecting chamber is easy to clean out while the bit is still warm.

A soldering stand is supplied with every tool and the price of the complete unit is $£ 6 \cdot 49$. Henry Picard \& Frere Limited, 357/359 Kennington Lane, London, S.E.11.


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$899200 \begin{aligned} & \text { Mixed Capacitors. } \\ & \text { Approx. quantly, }\end{aligned}$ Approx. quantlty,
counted by welght $55 p$
$P \& P_{15}$
H4 $250 \begin{aligned} & \text { Mixed Resistors. } \\ & \begin{array}{l}\text { Approx, quantly } \\ \text { counted byweight }\end{array}\end{aligned} \quad$ P \& P 15p
H35 100 Mixed Diodes, Germ, Gold bonded, etc. Marked and Unmarked. 55p Short lead Transistors,

55p
H39 6 Integrated Circuits. 4 Gates BMC 962, 2 Flip
Floos BMC 945
H41 $2 \begin{aligned} & \text { Sil Power Iransistors } \\ & \text { comp pair BD } 13 t / 132\end{aligned}$ 55p

## D Unmarked Untested Paks

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$0 A 202$
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55p
H20 $20 \begin{aligned} & \text { By126f7 Type Slicon } \\ & \text { Rectifier }\end{aligned}$ Rectifiertis. Amp platic.
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## A Cross Hatch

 Generator $£ 3.85$ paidA complete kit of parts Including Printed Circuit Board. A tour position switch gives Integrated Circuit design lor easy construction and reliablity. A project in the Sept. '72 edition
of Television.
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## 1

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H63 4 2N305s type NPN Sil. power transistors. Below spec. devices 5 p
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H66 440362 Type PNP Sil. transistors 55 p
H67 $10 \begin{gathered}3819 \mathrm{~N} \text { Channel FETz } \\ \text { plastic case type }\end{gathered} \quad 55 \mathrm{p}$

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LM380 Audio I.C. as featured in Practical Wireless Dec. Issue, complete with application data E1-10p.

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CRYSTAL calibrators have always found wide application with radio amateurs and short wave listeners. They fill a need for low cost frequency measurement and now that the price of transistors and integrated circuits is at an all time low, may be constructed relatively cheaply, depending upon the source of components. The crystal, if purchased new. should cost no more than $£ 1 \cdot 50$ -£2-00.

The object was to design a unit which would provide $1 \mathrm{MHz}, 100 \mathrm{kHz}, 10 \mathrm{kHz}$ markers at good strength to at least 30 MHz or higher. The calibrator to be described will, when used with the average receiver, provide strong frequency markers to above 30 MHz and will give markers as high as 144 MHz at reduced level.

## OPERATION

The crystal oscillator runs at 1 MHz and is based on the Colpitts circuit. In the design, good stability results in respect of both temperature variation and variation of supply rail voltage. In order to maintain this performance silver mica capacitors are specified for C2 and C3. The crystal in the prototype required about 40 pF in series and this is made up by Cl plis TCl. If necessary, Cl can be altered to suit different crystals.

The output from the crystal oscillator is taken from the collector of Trl. The waveform is roughly a sine wave and in order to drive the dividers must
be squared. $\operatorname{Tr} 2$ acts as a buffer amplifier and is biased into saturation on positive half cycles. This gives a square wave output of five volts peak to peak, which is used to drive the dividers.

The SN7490N (IC1-1C2) are TTL logic binary dividers and contain two gates and four bistables. They are used in this circuit to divide the 1 MHz square wave by a factor of ten, giving in the first case 100 kHz and in the second 10 kHz . The output is a square wave of five volts (approx.).

The three outputs, one from each divider and the 1 MHz waveform from $\operatorname{Tr} 2$ buffer are selected by Sl and are used to drive lC 3 and Tr 3 . These stages form the harmonic generator.

## HARMONIC GENERATOR

From a pulse rising at an infinite rate an infinite frequency spectrum could be derived, and if the pulse were to be repetitive at some frequency, say 1 MHz , then the spectrum would be related to the repetition rate of the pulse. However after the rise the pulse amplitude must decay again in time for next transition. If the decay is fast and at half the pulse repetition time then obviously a square wave would result. This could be shown to contain, in a pure case only, odd harmonics of the basic repetition rate. Now if the decay point were to be shifted from the half repetition rate time, then the even harmonic content would become apparent. Therefore in generating both odd and even harmonics of a fre-

fig. 1: Circuit of the callbrator


Fig. 2: Veroboard layout for the i.c. crystal harmonic calibrator

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## PHONOSONICS

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quency or rate, the main functions governing them are the rise or transition time of the pulse and its duration with respect to repetition rate.
It can now be seen that the principal requirement for a harmonic generator is that it must generate a pulse with a rapid transition or rise time which is as narrow as possible with respect to the repitition rate.
A number of methods exist whereby a fast pulse may be generated, these include tunnel diodes, reverse recovery effect of diodes, fast switching transistors etc.
For ease and cheapness the method used here is a standard SN74121N monostable (IC3) which drives Tr 3 the emitter follower into saturation. The SN74121N has provision for external timing components, but none are used here. This gives a pulse width of $30-40 \mathrm{nS}$. The output rise time (transition time) is quoted as 10 nS , but this is speeded up considerably by Tr3, which is a high speed switching device. Tr3 also provides a low output impedance.
The $75 \Omega$ resistor R 7 is worth mentioning. The output impedance of the emitter follower ( $\operatorname{Tr} 3$ ) is not governed directly by R6. It is in fact much lower than this and for matching purposes may be taken as zero. If it is desired to pass the signal along a coaxial line or to use an attenuator then R7 should be chosen to match the impedance of the cable in use, in the range of $50-300 \Omega$. However, many people will simply want to connect receivers or to squirt the output into a few feet of wire in which case make R750ת.

## POWER SUPPLIES

The limiting factors here are the integrated circuits. The voltage required is five volts $\pm 10 \%$. The design of the oscillator assures stability to within a few Hz for a $\pm 20 \%$ change in supply potential. This should not however present too great a problem as many constructors now run some form of equipment from which a five volt supply could be borrowed to operate the calibrator.
Fig. 3 shows the circuit of a simple stabiliser for use with this calibrator.


Fig. 3: Simple stabillser

## CONSTRUCTION

Building the calibrator should not present any problems, all components may be assembled on perforated board of suitable matrix. However in order to realise the best h.f. performance the leads around 1C3 Tr3 should be kept as short as possible and the output socket wired direct to Tr3 emitter. In particular, ensure that the output lead from pin 6 of 1C3 is short and direct to $\operatorname{Tr} 3$ base.

The crystal, if of a miniature type, may be fastened to the board and secured with a loop of wire. Solid
vibration free wiring in the crystal oscillator circuit will avoid microphony. If S1 cannot be wired direct to the board, all leads to it should be kept short. When completed and tested the board may be fitted in a small metal case or die-cast box.

## components list



Capacitors:

| C1 | 30 pF silver mica |
| :--- | :--- |
| C2 | 330 pF silver mica $2 \%$ |
| C3 | 330 pF silver mica 2\% |
| C4 | 5000 pF polystyrene |
| C5 | $0 \cdot 1 \mu \mathrm{~F}$ ceramic |
| C6 | $0 \cdot 1 \mu \mathrm{~F}$ ceramic |
| TC1 | $3-30 \mathrm{pF}$ Philips trimmer |

Semiconductors:

| Tr1 | BC108 |  |
| :--- | :--- | :--- |
| Tr2 | BC108 |  |
| Tr3 | BSX20 |  |
|  | Texas Instruments |  |


| Integrated Circuits |  |  |
| :--- | :--- | :--- |
| IC1 | SN7490N |  |
| IC2 | SN7490N |  |
| IC3 | SN74121N |  |

## Miscellaneous

S1 1 pole 3 way Crystal 1Mhz HC6U or similar

## TESTING

Connect a suitable five volt supply to the calibrator and couple the output to a receiver (b.f.o. on) tuned to 1 MHz . If all is in order a marker will be heard. Tune the receiver throughout its range and check that markers are present. Switch S1 to 100 kHz and check that there are 100 kHz markers present. Switch to 10 kHz and carefully check that 10 kHz markers are present.

If no markers are present on any range first check the oscillator circuitry. If markers appear only at 1 MHz intervals check the dividers for a fault.
The simplest way of controlling the injection of markers to a receiver is to vary the coupling. Obviously the markers are less strong around 30 MHz and the coupling may have to be increased. Direct coupling without the use of an attenuator is likely to overload the receiver and may introduce spurious responses. A little experiment will reveal the best method of operation.

Once the unit has been checked the frequency may be accurately set against WWV or MSF on either $2 \cdot 5,5 \cdot 0$ of 10 MHz . The calibrator should be rechecked from time to time against the standard frequency services to maintain its accuracy. TC1 may be adjusted as necessary to maintain this accuracy.

We regret that the December 1973 issue of Practical Wireless is now out of print

# PORTABLE FIUORISCENTLAMPUNIT A FURTHER DESIGN <br> PAUL COOPER 

A12volt d.c. portable flourescent lamp unit is a very useful piece of equipment to ownespecially in these days of power cuts! This article describes an alternative to the unit described in the December 1973 issue of Practical Wireless. There is the bonus that it is easier to build the circuit on a standard piece of veroboard than to produce a special printed circuit board and, by using a ready made transformer, reduces the cost.

## TRANSFORMER

A transformer specifically for ' 12 volt inverters to run flourescent tubes from car batteries is available from G. F. Milward* for only 50p + post packing \& VAT. It saves the time taken to wind the transformer, which is something which might put off the inexperienced amateur from building the project.

The revised circuit diagram is shown opposite.
The circuit is basically the same as in the original article except for the extra tertiary winding on the transformer which is connected in parallel with capacitor C3. The unit will work without this winding connected but in the circuit shown it tunes the transformer thus producing a better output.

It is most important that terminals $1,2,3 \& 4$ of the transformer are connected to the right points on the circuit diagram (as shown by the dots) since if, say, 3 and 4 are reversed the circuit will not oscillate. To cure this, should it occur, connections 3 and 4 should be interchanged and the circuit should then oscillate. (For the complete setting-up procedure see the original article.)

## LAYOUT

The Veroboard layout is shown opposite for 0.1 inch matrix veroboard. The board size is the same as for the original printed circuit board so no problems should occur in mounting this board in the completed unit. Note that the fixing hole in this circuit board is in a different place to that of the original board, so a different hole will have to be drilled in the unit case.

The transformer is fixed to the circuit board by two links of insulated copper wire as shown in the circuit board layout diagram.

Resistor R1 should be mounted about ${ }_{4}{ }_{4}$ in clear of the circuit board and clear from Cl as it gets hot! Since drilling of the holes for the legs of potentiometer VRI cuts the circuit board tracks completely, care must be taken to ensure contact when soldering the legs in.

Exact values of R1 and VR1 are not very critical. Values were chosen because of availability.

As my unit was built primarily as an emergency light for use in power cuts, the case has been designed to stand on a table with the tube vertical, and it is made of wood.

- G. F. Milward, 369 Alum Rock Rd, Birmingham, B8 3DR.



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SAVE on your tools. Get Khis exclusive TOOLKIT OFFER at reduced price when you buy the April issue of Practical Wireless. The kit contains soldering iron kit, wire cutters, wiring pliers with wire stripper blades, small screwdriver with neon tester, large screwdriver for cabinet and chassis work. All these tools are of high quality and of well established manufacture. They are available to Practical Wireless readers at a special low price. Use the coupon in the April issue.


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## GUIDE TO MULTI-RANGE TESTMETERS: IMPEDANCE MATCHING

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THE
(1) 5-BAND RECEIVER

This unusual receiver is designed to give five ranges from 160 kHz to 27 MHz , using simple plug-in coils to cover broadcast and amateur transmissions. Only eight transistors are used, and, with a telescopic aerial the "Slimline" becomes a versatile a.m, receiver to take almost anywhere.



THIS constructional feature describes a stereomultiplex AM/FM tuner-amplifier providing 10 watts RMS output per channel into $8 \Omega$ loads with facilities for incorporating a cassette tape recorder. The integrated unit provides very good results which, although not to true high fidelity standards, will give satisfying listening for a moderate outlay.

Facilities on the prototype included full Band II FM coverage together with one preset AM station and an input for a ceramic cartridge. Additional circuitry and printed boards are shown in this article so that inputs for magnetic cartridge and tape heads can be accommodated, together with record/playback connections for a cassette or reel-to-reel tape recorder. Additional tuning capacitors may also be fitted along with a selector switch to provide more extensive AM coverage. The AM section uses an internal ferrite aerial, but an external aerial may be added if required. The stereo decoder incorporates automatic mono/stereo switching and stereo beacon lamp drive.

The complete unit is built up on five main circuit boards. The power supply is built directly onto the chassis which is constructed from aluminium angle and strip. The following unit numbers will be used as a prefix to identify components which are mounted off the circuit boards:-

> 1 Pre-amplifiers
> 2 Power amplifiers
> 3 Tuner and IF
> 4 Stereo decoder
> 5 Power unit and input/output sockets.

The front panel is fashioned from 3 mm Perspex, using Letraset marking and gives a very professional finish to the unit.

The complete circuit uses 3 integrated circuits, 19 transistors and 7 semiconductor diodes. The FM tuner head is a Mullard module, simplifying construction and greatly reducing alignment problems.

## PART 1




## RICHARD COLLIN

## Performance Specification

## AMPLIFIER

Power output: 10 watts RMS per channel into $8 \Omega$
Frequency response: 20 Hz to $30 \mathrm{kHz} \pm 3 \mathrm{~dB}$ at full power
50 Hz to $20 \mathrm{kHz} \pm 1 \mathrm{~dB}$ (power amplifier)
Channel separation: 54 dB at 1 kHz and 10 watts
Noise: -60 dB at 10 watts (ceramic cartridge input)
Total harmonic distortion: $<0.2 \%$ at 1 kHz and 10 watts
Tone controls: Bass $\pm 16 \mathrm{~dB}$ at 50 Hz
Treble $\pm 14 \mathrm{~dB}$ at 15 kHz

## F.M. TUNER

Frequency range: 88 to 104 MHz
Channel separation: 40dB

## PRE-AMPLIFIER (UNIT 1)

The inputs from the various programme sources, attenuated and matched as necessary by R1-R5, are selected by Sla (Slc for the Right channel). Transistors Tr l and Tr 2 are connected as a highgain pair and amplify the input signals to a level sufficient to drive the tone control circuit. The bias resistor R7 for the first stage may need to be selected for optimum operation. This will be dealt with in a later part of the article. Its final value should lie between 120 and $270 \mathrm{k} \Omega$.


## components list



Non-electrolytic capacitors should be polyester or polystyrene

## Semiconductors

Tr1 BC149 Tr2 BC148 Tr3 BC149
NOTE-With the exception of the four dual-ganged potentiometers, two sets of the above components are required for the two channels.

## Miscellaneous

S1 6 pole, 6 way, 3 wafer rotary switch
S2 DPST miniature toggle switch
Pre-amplifier printed circuit board
Equaliser printed circuit board

## POWER AMPLIFIERS

Resistors

| R1 $91 \mathrm{k} \Omega$ | R6 10k $\Omega$ | R11 $0.47 \Omega 2.5 \mathrm{~W}$ w/w |
| :---: | :---: | :---: |
| R2 100k $\Omega$ | R7 $47 \Omega$ | R12 $0.47 \Omega 2.5 \mathrm{~W} \mathrm{w} / \mathrm{w}$ |
| R3 $22 \Omega$ | R8 $100 \Omega 2 \cdot 5 \mathrm{~W}$ w/w | R13 $10 \Omega$ |
| R4 $470 \Omega$ | $\mathrm{R} 9100 \Omega 2 \cdot 5 \mathrm{~W} \mathrm{w} / \mathrm{w}$ | All $\downarrow \mathrm{W}$ 5\% Ca |
| R5 470, 2 | R10 $10 \Omega$ | film unless |

VR1 $50 \mathrm{k} \Omega$
VR2 $100 \Omega$ miniature presets (horizontal mounting)

## Capacitors

C1 $25 \mu \mathrm{~F} 25 \mathrm{~V} \quad \mathrm{~V} 40.01 \mu \mathrm{~F} 100 \mathrm{~V}$ C $7200 \mu \mathrm{~F} 30 \mathrm{~V}$
C2 $47 \mu \mathrm{~F} 40 \mathrm{~V}$ C5 $0.22 \mu \mathrm{~F} 100 \mathrm{~V}$ C8 $1,500 \mu \mathrm{~F} 25 \mathrm{~V}$
C3 $1,000 \mu \mathrm{~F} 25 \mathrm{~V}$ C6 $0.001 \mu \mathrm{~F} 750 \mathrm{~V}$ C9 $0.047 \mu \mathrm{~F} 100 \mathrm{~V}$
Semiconductors

| Tr1 | BC158 | Tr4 | 2N6288 (RCA) |
| :--- | :--- | :--- | :--- |
| Tr2 | BC148 | Tr5 | 2N6111 (RCA) |

Tr3 2N6288 (RCA)
Tr3, 4 and 5 are supplied with the necessary mounting hardware
NOTE-Two sets of the above components are required for the two channels.

## Miscellaneous

Printed circuit board. Heat sinks and brackets (see Figs. 8 and 9)
NOTE-RCA Semiconductors for this project are available from E.C.S. (Windsor) Ltd., Thames Avenue, Windsor, Berks.
Total requirements are: 2 N6111 at 50p
5 2N6288 at 54p
1 CA 3089 E at $£ 1 \cdot 96$
1 CA 3090 Q at $£ 4 \cdot 23$
Add 40p post and packing per order and 10\% VAT

Feedback around $\mathrm{Tr} 1 / \mathrm{Tr} 2$ provides high stability and is also used to set the gain and, for the magnetic pick-up and tape-head inputs, the frequency response. The appropriate feedback path is selected by Slb (Sld for the Right channel). The value of Rll, which with C 5 provides equalisation for the tapehead input, must be chosen according to the tape speed to be used.

A constructor not requiring the full complement of input facilities may of course omit the unwanted circuitry and connectors.

An output is taken via R16 for connection to a tape recorder, allowing recording of a programme being played through the amplifier (subject to the provisions of the Copyright Act, 1956). The signal at this point is equalised but is unaffected by the Volume and Tone controls. Because of the high value of R16, the two channels can be paralleled at the input of a mono recorder with only slight worsening of stereo crosstalk within the amplifier.

The tone controls are in the familiar Baxandall configuration, providing both lift and cut at bass and treble frequencies. Transistor $\operatorname{Tr} 3$ is the active


Prototype boards for the pre-amplifier (above) and power amplifier (below)

element of this stage and also makes up for the losses incurred by the frequency selective circuits. A bass cut or rumble filter may be provided by removing the short circuit from across 6.17

Ensure correct polarity of the electrolytic capacitors when assembling the circuit boards. In the R7 position fit $220 \mathrm{k} \Omega$ resistors, leaving the wires long as the value may need to be changed later. Once


4M 016


Fig. 3: Actual size layout for the pre-amplifier printed circult board


Fig. 4: Actual size layout of equaliser printed circuit board and location of components
4

Fig. 5: Circuit of the power amplifier. One channel only shown. The other channel is identical

complete, these boards may be placed in a safe place until the chassis and power unit are completed. A number of components included in the pre-amplifier circuit diagram are not mounted on the boards. These are dealt with in a subsequent part of the article.

## POWER AMPLIFIER (UNIT 2)

The familiar complementary-symmetry configuration is used and designed around silicon transistors. Good low frequency response and stability is ensured by the use of DC coupling throughout the amplifier. The output pair, RCA plastic packaged 'Versawatt' devices, deliver 10 watts RMS into an $8 \Omega$ load. A similar device $\operatorname{Tr} 3$ operates as a class ' $A$ ' driver.

The small forward bias required to minimise crossover distortion is provided by a small signal transistor Tr 2 connected between the bases of the output pair. The first stage Tr 1 provides amplification of the input signal and in addition acts as a DC comparator, enabling the output stage to be set up for symmetrical clipping under overload conditions. The DC potential at the output mid-point is connected to the emitter of Trl via R4. The base potential of Tr 1 is determined by the potential divider R1, R2, VR1 and R6. The high loop gain of the circuit keeps the small difference between Vb and Ve constant, so that the output mid-point voltage is defined by the base potential of Tr regardless of component tolerances. Negative feedback is provided by R4, C3 and R3.

Fig. 7: Actual size layout for the power amplifier printed circuit board $\nabla$

## 4 AM 0151



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## A complete kit!

The kit comes to you packaged in a heavy-duty polystyrene container. It contains all you need to assemble your Sinclair Cambridge.
Assembly time is about 3 hours.
Contents:

1. Coil.
2. Large-scale integrated circuit.
3. Interface chip.
4. Thick-film resistor pack.
5. Case mouldings, with buttons, window and light-up display in position.
6. Printed circuit board.
7. Keyboard panel.
8. Electronic components pack (diodes, resistors, capacitors, transistor).
9. Battery clips and on/off switch.
10. Soft wallet.

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Price fuily built : £29.95 + £3.00 VAT. (Total : £32.95)



Fig. 8 :
Design and assembly of driver transistor heatsink
A Zobel network C9/R13 is connected across the output terminals. The purpose of this network is to ensure that the loudspeaker load always appears essentially resistive to the output transistors. This means that the output stage is protected against inductive transients which could exceed the breakdown voltage of the transistors.


Fig. 9: Design and assembly of output transistor heatsink

## PART 2 next month will describe the Tuner/IF and FM Decoder units



## ACROSS

Employs a coupling of ferrous esters (4)
A shaker in the transformation scene (8)
A stick-up in the rockery (4)
Radio engineers meet with such resistance? (8)
Come back to fix a little drink (3)
The Spanish miss her in the end (4)
Already fixed on the wavelength? (3-3)
A key piece of mechanism (4)
As familiar as Liz (4)
Bell's slowest ringing tone (4)
Basso loudspeakers amplify this single? (4)
How to dispense with an earth! (6)
You talk nonsense about defeat (4)
Dipole once connected with him! (3)
If about to bewail a valve component! (8)
Not so hot in acoustic editing (4)
Salty type's crystallization at the mike! (8)
Collections of old wirelesses (4)
DOWN
Land in court with such maintenance? (7)
Glass in pieces from these transmissions? (7) Jim pleased about the little rascal (3)
The longest-ever tape? (6)
They're well up about antennae (5)
A composed musical performance (7)
Such a charge about a cathode? (5)
The more hearty kind of con-man (7)
Birds do such load-shedding? (5)
Do riots break such coils? (7)
Told Sue about being so noisy! (7)
More l'd swap for a position in golf (6)
Classification of a crystal-set? (5)
Nickel-coating is zero-rated? (3)

## ON RECENT DEVELOPMENTS

## WATCH IT!

,AM looking at a Swiss electronics journal. There's a circuit which uses two ICs, a readout chip, and a one-transistor oscillator. Connected together they form an electronic clock complete with digital readout. The only circuitry which needs "building"is the single transistor oscillator and this comprises five resistors, five capacitors, a crystal and one of the ICs mentioned. For the record, the two chips are the SCL5437F (oscillator) and SCL5424F which drives the liquid crystal readout direct.

## UNIVERSITIES HELP

One of the major criticisms levelled at universities is that their experiments are all too often of academic value only. While this may be true in some instances, it certainly is not true in the case of the University of Utah in the U.S. This establishment has a section devoted to making blind people see again. Although in the experimental stages, blind people have been able to see- light patterns which have been simulated by an external "eye" and fed into their brains by small electrodes.

The light images or patterns are called phosphenes and are stimulated (in these experiments) by the generation (and careful control) of pulses, in other words, the vision has been created by purely electronic means. The width of the pulse and its duration determined the intensity or "shades" of the image which the totally (otherwise) blind person can "see". Researchers see no reason why some form of imaging device (like a solid state t.v. camera) should be used and the impulses fed into the brain-after suitable processing, of course. This latter idea is well within the realms of readily available electronics which one can obtain today.

Embedded image sensors could even be controlled by the eye muscles themselves. Already,
computer-generated images have been drawn quite accurately by a totally blind person. The image was viewed on a c.r.t. so that a fair comparison could be made.
If you know of a blind person, it would be unkindly premature to mention these experiments with too great an enthusiasm because it may well take many years to perfect it into a practical device.

## A TOOTHGRAPH?

Still in the realms of medicinewell, almost, is the latest use of lasers. Now, the dental profession have taken an interest. By using a small laser it is possible to take holographic photographs of a person's teeth. One interesting thing to emerge from this useage is not that it will offer an invaluable aid in dental practice (although this is very true) but its use for security purposes. Apparently no two peoples teeth are the same so instead of fingerprints one could have toothgraphs or teggypix.
Criminals of the future will do well to heed the old addagewhen in doubt, keep your mouth shut. In any case the idea should give Scotland Yard something to get its teeth into.

## LARGE-SCREEN COLOUR

Perhaps one of the most interesting battles currently being fought is the one for television screens/tubes/systems. All sorts of ideas are currently under examination including a flat screen solid state beasty. News has arrived about another contender. This one is called a Video-Beam projector and houses optics inside the colour tubes. It shows promise for large screen colour television and claims the advantages of doing away with colour dots, lattices and shadow masks.
Each electron beam (one for each of the three colours) is fired at a "target" which has the relevant colour phosphor. This beam is reflected back inside the tube to a concave mirror which in turn reflects the image out of the tube onto the screen. Extremely good results are reported, however,
there is a snag-the projection distance is fixed at eight feet and is unalterable. The company working on the device do not see this as a problem and claim that once the colour tube "projector" has been adjusted at the manufacturing facility, it requires no adjustment or fiddling by the user.
No mention is made of the power requirements but one presumes that they are considerably lower than the $25-30 \mathrm{kV}$ needed for the earlier black-and-white projection systems where many people expressed concern about radiation from such a set up.

## MULTI- CHIPS

A new IC chip, the 2240 , is claimed by its makers to do just about anything. It is currently hailed as a programmable timer, binary counter, music synthesiser, A/D converter, ultra-long delay generator, digital sample and hold circuit, frequency synthesiser, pulse counter, binary pattern. generator, precision oscillator... etc., all in one innocent looking sixteen-pin dual in-line package. I have contacted the company with a view to obtaining further information which I will pass on as and when it arrives. It may be possible to include some circuitry of the more practical applications for the home constructor.

## BIG CHIPS!

Remember the days when semiconductor devices were fragile and sensitive to fluctuations in power. Contrast that with the latest beast from International Rectifier. This is a silicon controlled rectifier which handles 2,500 Amps r.m.s. at'up to 1,200 volts. A $2,000 \mathrm{~V}$ version is already planned. The wafer for this device is almost $2 \frac{1}{2}$ inches in diameter. This is probably the largest chip which has ever been employed in any semiconductor device.
Gimbers

#  OTBME MOMTM 

THE LM377N is an IC, manufactured by the National Semiconductor Company, which contains two separate two-watt amplifiers in a single device. The connections are shown in Fig.1. A 14 pin dual-in-line encapsulation is employed which can be fitted into a socket or soldered into a printed circuit board. A similar device, the LM377N-10, has metal tab connections which may be soldered to a printed circuit board. Pins 3, 4 and 5 and also 10, 11 and 12 of Fig. 1 are replaced by metal tabs on each side of the device. These are very convenient for soldering to a heat sink.


Fig. 1. PIn connectlons to the 14 p/n DIL LM377N.
The LM377 devices are intended mainly for use in stereo equipment where the output power required does not exceed 2W. However, they can also be used in a bridge circuit where the two amplifiers in the device are used in push-pull to provide a monaural output of up to $4 W$.

## Advantages

The following features make the LM377N especially attractive to the amateur constructor as well as to the professional circuit designer:-
(i) The output stages are automatically centred at the correct bias so that the output voltage can swing an equal amount in either direction resulting in maximum power output at a given distortion level. (Some power amplifiers circuits require a preset potentiometer so that the bias can be adjusted manually.)
(ii) The LM377N contains internal circuits which protect it from overheating. If the silicon chip becomes too hot, the device switches itself off until it becomes cooler.
(iii) Protective circuits prevent the device from being damaged by excessive current. Such currents are likely to flow if either of the outputs is accidentally shorted to earth.
(iv) The input impedance is relatively high, $3 \mathrm{M} \Omega$, and this increases the versatility of the device.
(v) Any hum on the power supply line is reduced by 80 dB . The separation between the two channels is typically 70 dB .

## Circuits

In all circuits the inputs of both amplifiers should be biased by the voltage from pin 1 . The bias current is typically $0.5 \mu \mathrm{~A}$ to each amplifier.

In addition, feedback from each output should be applied to the feedback input of the same amplifier. The amount of feedback controls the gain.


Graphs relating supply vollage to output power for the LM377N.


Fig. 2. Circuit of a practical stereo amplifier suitable for a record player. A volume control will be required on the input circuit.

fig. 3. This mono circuit utilises both ampliflers to provide 4W oulput.

Similarty, the gain of the lower amplifier is $R 6 / R 4=50$. The typical gain of an amplifier without any feedback is 30,000 ( 90 dB ).

The mean output potential is equal to approximately half the supply voltage. An electrolytic capacitor (C6 and C7) must therefore be placed between the outputs of the device and each speaker so that direct current cannot flow. If the value of the capacitors is reduced, an inferior bass response will be obtained.

## Power supply

The L.M377N can be fed from a supply line having any value between 10 V and 22 V . The absolute maximum supply voltage is 26 V , but one should always allow a safety margin to avoid the risk of damage to the device.

A current of about 15 mA is taken from a 20 V supply when no signal is applied to either input, but the current rises towards 1 A when full output power is being delivered to the speakers.

The maximum output power which can be obtained from each channel depends on the supply voltage used and also by the speaker impedance. A typical LM377N provides 2.5 W per channel when fed from a 20 V supply into $8 \Omega$ speakers. whilst all devices should provide a minimum of 2 W per channel under these conditions.

The LM377N can dissipate up to about 2.5 W continuously without a heat sink. but if the centre pins

A typical circuit for the use of the LM377N as the two power anplifiers of a stereo system is shown in Fig. 2.

Bias from pin 1 is decoupled by ( 3 and applied to the inputs at pin 6 and 9 via Rl and R2. The input signals are capacitively coupled through Cl and C'2 respectively in order to prevent the bias from being affected by the impedance of any previous stage. The input impedance of the $1, M 377 \mathrm{~N}$ is relatively high and therefore the coupling capacioms can be faitly small in value.

In the upper amplifier of Fig. 2, the feedback is taken from the output at pin 2 through R5 to pin 7. The voltage gain is equal to R5/R3 which is 50 times or 34 dB . The gain may be increased by reducing R3 but the distortion will increase.
of the device are soldered to $2 \cdot 5$ sq. in of copper on a printed circuit board, the maximum dissipation is increased to about $4 \cdot 2 \mathrm{~W}$. Some form of heat sink seems required when an $8 \Omega$ speaker is employed, unless the power supply voltage does not exceed about 14 V . In practice, however, the device is seldom operated at maximum power level for more than a moment (unless one likes to listen to sine waves!). Normally one is not likely to require a heat sink when using supply voltages of up to 18 V provided that the speaker impedance is not less than $8 \Omega$.

## Mono Amplifier

A single LM377N device can be used in a single channel system to provide an output power of 4 W . Fig. 3. continued on page 1086

## PRESELECTOR for

 10-30MHzMANY receivers are susceptible to second channel interference when working on the higher frequencies. This means that if the receiver employs an intermediate frequency of 470 kHz , the oscillator is working at a frequency 470 kHz higher than that of the wanted transmission and signals which are 470 kHz higher than this, or 940 kHz higher in frequency than the wanted transmission, can beat with the receiver oscillator frequency, to produce a signal which passes through the 470 kHz amplifier, interfering with the wanted signal. On the lower frequencies, there is usually sufficient selectivity ahead of the mixer to avoid difficulty from this cause. But on higher frequencies, the receiver is unable to totally eliminate the offending signals which cause interference and whistles.

Even a well-designed receiver with one RF stage may not provide second channel rejection better than 15 dB at 30 MHz . If a signal strength scale of 6 dB per S -point were used, as is quite usual, this would mean that if a wanted signal read S9, an unwanted signal of equal strength 940 kHz higher in frequency would read $66+$, which is a severe level of interference.

Such interference can be greatly reduced by raising the receiver intermediate frequency, or by increasing the second channel rejection ahead of the mixer. Changing the IF is probably impossible, but the unit here will enormously increase the second channel rejection.

The maximum benefit will be found with receivers which have no tuned RF stage, or only one RF stage, and employ a $455-470 \mathrm{kHz}$ intermediate

## F. G. RAYER G30GR



Completed preselector in its $6 \times 4 \times 4$ in cablnet.
frequency. With such receivers, 19 m broadcasts may greatly mar reception of 20 m amateur signals, for example. The unit can also be employed with other receivers including those with a $1 \cdot 6 \mathrm{MHz}$ or other IF.

## CIRCUIT

This is shown in Fig. 1. As second channel interference is not usually troublesome at signal frequencies lower than about 10 MHz , the unit covers approximately 10 MHz to 30 MHz in a single band, thus avoiding any need for band switching. L2 and


Fig. 1. Circuit of preselector using a single integrated circuit, Input, output and battery connections are at the rear. When placed between aerial and receiver useful galn will result as well as a reduction in second channel interference.

L3 are tuned with the ganged capacitor VCl/VC2 providing two extra tuned circuits before the receiver. In most cases this will almost completely eliminate second channel interference. VC3 is a panel trimmer to allow peaking the aerial circuit with almost any aerial.
The CA3005 IC operates with a 6 V supply. It is listed as giving 20 dB gain at 100 MHz , but the full gain is not achieved here due to the circuit being arranged for operation from a single power supply, and because of the difficulty of matching the input and output impedances at all frequencies. The input is approximately matched by the centre tap on L2, while the transformer L3/L4 is arranged to give an output impedance suitable for most receivers.
Gain control is provided by VR1, to avoid overloading the receiver on strong signals.

## IC BOARD

The board is wired as in Fig.2. Note that the projection on the IC corresponds to lead 12. Spread the leads slightly so that they may pass through the Veroboard holes as indicated.


Fig. 2. Both sides of the small circuit board that carries the IC.
Two 6BA bolts with tags form the earthing points MC. Leave projecting leads from Cl , for battery positive, VR1 and for VC2. Also solder on R1.

## COILS

These use 24swg enamelled wire throughout, Fig. 3. For the aerial coil, begin at $C$ as near the top of the former as possible, and wind on $4{ }_{2}$ turns. Scrape the wire and twist the centre tap. Wind a further $4^{1}{ }_{2}$ turns and finish at D. Leave a small space and beginning at A wind on 4 turns, finishing at B .

For the second coil, wind 9 turns from $E$ to $F$, leave a space as before, and put on 5 turns from $H$ to $G$.

The ends of the windings can be secured with a loop of cotton lightly smeared with quick-drying adhesive, and given a turn or two round the former. Fix one end by this means, wind on the turns mentioned, and secure the finish of the winding in the same way, pulling it tight by the cotton.


Fig. 3. Details for winding the two coils used in the preselector.

## CHASSIS

The panel for the case listed is approximately $6 \times 4$ in. Punch a clearance hole for the spindle of $\mathrm{VCl} / 2$. As this capacitor has an integral drive and the spindle cannot be cut shorter, it can be spaced back from the panel as in Fig. 4, to bring the knob nearer the front. This requires three 4BA bolts, each with two nuts, locked against panel and capacitor. VRI and VC3 are also set back a little by extra nuts or washers.


Fig. 4. Top view of the chassis showing position of the IC board and major components.

The chassis is a flat plate $4^{1} 2 \times 3 i n$. It is secured by two short 4BA bolts which pass through it and into the threaded holes in the capacitor frame. Place a few washers between plate and capacitor.

## components list

## Resistors

R1 $4 \cdot 7 \mathrm{k} \Omega \ddagger \mathrm{W}$ VR1 $5 \mathrm{k} \Omega$ linear with switch S 1 .

## Capacitors

C1 $470 \mathrm{pF}, \mathrm{C} 20.01 \mu \mathrm{~F}$ disc C3 $0.02 \mu \mathrm{~F}$ disc.
VC1/ $22 \times 365 \mathrm{pF}$ with slow motion drive.
VC3 50pF (Jackson C804) TC1 30pF trimmer

## Miscellaneous

Formers for coils, $\frac{3}{16}$ in dia. with cores (2).
Knobs. ICI, CA3005. Aerial socket and output socket. Instrument case about $6 \times 4 \times 4 \mathrm{in}$.


Finished preselector. Flexible connections are made to battery connector and output socket.

As the receiver employed a co-axial lead, a socket for this was provided as in Fig. 4. An earth circuit to the unit is then available through the co-axial outer conductor. If the receiver does not employ this type of aerial input lead, take a wire from G, L4, to the receiver aerial socket, and connect $H$ and the chassis to the receiver earth terminal.

## OPERATION

TCl can be set at about half maximum capacitance. Tune in a transmission on about 10 MHz , set $\mathrm{VCl} / 2$ nearly fully closed and rotate the cores of the coils for best reception.

Holes are drilled to take the circuit board bolts which are locked with extra nuts. Wiring must be clear of the metal. The coils are held with 8BA bolts and nuts.

## WIRING

Wiring is then completed as in Fig. 4. TCl has its lower tag soldered directly to the frame of $\mathrm{VCl} / 2$, the second tag being connected to VC2, together with the lead from pin 1l, ICl.
The coil leads are cut to length, scraped, and soldered to the points shown. Note that H goes to the chassis at a bolt securing L3/L4.
The battery consists of four HP7 or similar cells, in a 4 -cell holder. The holder is secured in the back of the insulated case, near the top, by a small bolt.

Subsequently check that 30 MHz signals peak with $\mathrm{VCl} / 2$ nearly fully open, and that VC3 also peaks up signals or background noise. If necessary, readjust TCl to allow proper tuning with VC3, and check the core positions, so that little adjustment of VC3 is required, when tuning across the whole band.
Adjustments are best carried out by observing the receiver signal strength meter, or with the receiver AGC switched off, or by selecting weak signals which do not operate the receiver AGC. VRl should be set for maximum gain when doing this. As an aid, a very short aerial may be temporarily taken to $A$. VC3 should then have quite a sharp. peak, but this effect will be reduced with a long aerial when it may be preferable to place a small capacitor in the lead from aerial to A.

## IC of the Month-continued from page 1083

The two amplifiers are used in a 'bridge' or pushpull circuit. The input signal is fed through C2 and R1 to the feedback input (pin 7) of the first amplifier and the same signal also passes through Cl to the non-inverting input ( $\operatorname{pin} 9$ ) of the second amplifier.

When the voltage at the pin 2 output increases, that at pin 13 therefore decreases by the same amount and vice-versa. The speaker is thus driven by this push-pull signal. This circuit has the advantage that no capacitor is required in series with the speaker, since the mean potentials of pins 2 and 13 are almost identical.

The bias from pin 1 is decoupled by C3 and fed through R2 to pin 6. It also passes through R3 to pin 9.

The gain of each amplifier is equal to the ratio of the feedback resistors, namely $\mathrm{R} 4 / \mathrm{Rl}=\mathrm{R} 5 / \mathrm{R} 6$ $=50$. However, the push-pull action gives an effective overall gain of twice this value.

The LM377N is available from Athena Semiconductor Marketing Company Ltd., 140 High St., Egham, Surrey, at $£ 2 \cdot 70$ plus VAT for small quantities, inclusive of $\mathrm{p} \& \mathrm{p}$.

## RADIO BY CABLE \& SATELLITE

-continued from page 1087
Many countries have determined that this is unavoidable within the boundaries of the technical possibilities and it has been recognised by the UNO associated International Telecommunications Union in 1971 in Geneva. At the same time, however, it was established that the use of TV satellites is only possible by observing frequency, positioning and ground coverage plans which are to be drawn up at a special planning conference for this purpose which will take place in 1975/76.

## EXPERIMENTAL WORKSHOP

We regret that due to pressure on editorial space this month, Part 6 of this series has been held over until the April issue.


ALTHOUGH it is a task of exchange technology to handle the signals, in connecting individual communications (telephone, telex), in such a way that the connection is made quickly and reliably, broadcasting must ensure that the primary signal is transported long distances without distortion, be they telephone signals or for telegraphy, music, TV, picture transmission, data transfer or remote control. But what are the problems that arise?

A modern carrier frequency system with 2700 channels for speech has an amplifier spacing of 4.5 km ; at a distance of 4500 km as is found in the trade area between the USA and Canada, 1000 amplifiers are operated one after the other.

Assuming a medium amplification of 30 dB (i.e. the signal output is increased each time by a factor of $10^{3}=1000$, the voltage by around a factor of $31 \cdot 6$ ) the overall amplification over the whole section amounts to the almost unbelievable figure of $10^{3000}$. For comparison: the entire universe contains "only" around $10^{83}$ protons, since the creation of the earth approximately 15 billion years ago a total of "only" $5 \cdot 10^{77}$ seconds has passed.

## Cables

To guarantee the necessary quality over so many stages, extremely high demands must be made, both on the technical equipment (amplifiers, converters, modulators etc.) as well as on the directions of transmission. With regard to the latter there are three "media" which have proved themselves and which are to be found predominantly or exclusively in long-distance traffic: cables, directional radio including satellites and-as a medium of the long-term future, suitably directed laser beams.

Cable, especially coaxial, is already considerably protected by its construction and laying against outside influences from space, the atmosphere and from technical installations, so that in cable transmission systems non-linearity and noise must be kept as low as possible.

Disregarding the "symmetrical" carrier frequency cables, used predominantly with up to 120 speech channels for regional systems, there is a whole series of coaxial types at an impedance of around 75 ohm . There are many various internal sizes, e.g. from 1.2 mm for 300 speech channels or 2.6 mm for a choice of 960,1260 or 2700 channels. If one is prepared to reduce the amplifier spacing even more, one could increase the basic bandwidth considerably (e.g. to 40 to 60 MHz or even higher).
"Hollow" cable recently developed can theoretically provide a transmittable overall bandwidth of around $100,000 \mathrm{MHz}$. It is, in fact, a radio wave guide which should be most suitable for the transmission of digital signals (e.g. for pulse code modulation). Technically hollow cables are well advanced although there are certain reservations with regard to their economic application.

## Satellites

The directional radio line, widely used for the transmission of TV modulation (video band) but also for multi-channel speech bands, is physically an ideal transmission medium. However, it requires the application of special "noise reducer" procedures due to the influences of extra-terrestrial, tropospheric and industrial radio signals. Partial bandwidths of up to 30 MHz have shown themselves to be the best for the transmission of television or telephone channels in various frequency ranges between 2 and 12 GHz . Transmitter output is in the area of several watts.

Satellite paths are basically extended directional radio lines with fields of $2 \times 36000 \mathrm{~km}$ length (to and from) with high transmitter outputs, extra large aerials and extremely sensitive receivers (maser) on the terrestrial stations. They are particularly suitable for trans-continental and trans-oceanic relays, operating at frequencies corresponding to those in directional radio technology.

A transmission medium of the future is the laser beam which is strictly monochromatic, polarised and coherent. In a free field of dissemination they are not practicable because of absorption as with normal light, but when suitably guided by lens conduction and glass fibre, it reveals its full potential.

In particular the glass fibre bundle cable, offering an extreme bandwidth even with individual fibres, combined with the multifarious operating possibilities of universal cable, promises to be an important transmitting medium, both in long distance communications and in local traffic in densely populated areas. All of this is of course dependent on a corresponding advance in the components and subsystems in the field of optronics-an advancing technology being fully exploited now.

Satellites providing a country with programmes via only one transmitter can of course be received across borders. Even with rays with a one degree focusing, whose focal area is accommodated within the boundaries of the country cannot prevent this.

# Mreilloreope 

## PART 1

 techniques alanansleIN this series we shall be taking a close look at oscilloscopes of the kind likely to be used by the average electronics enthusiast. This leaves a large range of classes of instruments, but we shall not be too concerned with the developments incorporated in the brand new, four figure price oscilloscopes as these can generally be classed as purely professional in appeal and application.

The instruments to be considered will range from the simplest types of scope, through TV service scopes to the laboratory scopes of a few years ago, now available to the keen amateur-but at a price!

We shall consider design principles, the basis for modifications, and calibration. This last point is rather important as manufacturers can charge a lot for recalibration of their instruments, especially if not of current manufacture.

We shall also look at some oscilloscope applications and at a few pieces of additional equipment in order to carry out an increased range of tests and measurements.

Oscilloscopes fall broadly into four main classes:-

1. AUDIO FREQUENCY
2. TELEVISION AND PULSE
3. LABORATORY
4. SPECIAL PURPOSE

Ignoring the special purpose scopes for the time being, the oscilloscopes are grouped into a convenient scale of ascending bandwidth.

## BANDWIDTHS

As most scopes have a low frequency limit of DC (DC coupled) or a few Hz , the bandwidth figure quoted is the upper frequency limit at 3 dB down (or however else the manufacturer specifies).

The bandwidth information gives an indication of the highest frequency that the scope can predictably handle.

Considering the two curves in Fig. 1, both scopes would have a written bandwidth of 5 MHz , but scope A would in fact perform quite well past this figure whilst scope B drops straight off. Scope A could be used but with loss of calibration up to perhaps 10 MHz or so, scope B being totally useless at this frequency.

Incorporated in any statement concerning bandwidth is an implication of the rise time of the scope.

If we consider an oscilloscope amplifier displaying a 1 MHz signal, and this signal is at the -3 dB point, we can arrive at some justification for the rather mysterious equation used to express rise time in terms of bandwidth.


This imposing array of test equipment in just one corner of the author's workshop will serve to underline the fact that this series of articles on the oscilloscope contains much practical information as well as theoretical discusslon.


Fig. 1. The response curve of the $Y$ amplifier in two different oscilloscopes, to Illustrate the meaning of "bandwidth."

The time period of the 1 MHz signal is $1 \mu \mathrm{sec}$. Thus for one half period the time is 500 ns and for the rising portion 250 ns . If now the slope of the upward going part 'of the cycle is taken to represent the step function applied to the scope, then the rise time of this 1 MHz (3dB down) scope would appear to be 150 ns .

But the 1 MHz signal is not of $100 \%$ amplitude (it is 3 dB down), and as rise time Tr is defined as the time to increase a step function from $10 \%$ to $90 \%$, a correction is required, Fig. 2.
As 3 dB down corresponds approximately to $30 \%$ down, i.e. the trace height at the -3 dB point is only $70 \%$ of what it should be.

It is necessary to bring the $70 \%$ trace to $90 \%$ and in doing this $\operatorname{Tr}$ is increased by $90 / 70$ giving a theoretical rise time of 322 ns .

In practice the figure is found to be between 350 and 390 ns , depending on the shape of the response. The response curve of Fig. 1, scope $A$ would give a faster rise time than that of scope $B$, although both have the same bandwidth.


Fig. 2. First part of a response curve with a step function input to the scope. The rise time is a funclion of the bandwidth of the amplifier.

Taking the rise time to be 365 ns for a 1 MHz scope and applying the laws of proportion we get the expression:-

## Rise Time (ns) $\times$ Bandwidth ( MHz ) $=365$

This expression holds true for the vast majority of cases, but more about that when we come to consider the Y amplifiers in more detail.
Returning to our classification of oscilloscopes it seems reasonable that the audio oscilloscope has but a limited bandwidth ( 1 MHz or so) while the TV or pulse oscilloscope has a bandwidth of perhaps 10 or 15 MHz and is capable of displaying more complex and more rapidly recurring waveforms. The laboratory scope on the other hand has a bandwidth extending from 15 MHz and up and into the hundreds of MHz on the very latest real time oscilloscopes.
Using sampling techniques (imaginary or virtual time) bandwidths into the GHz region have been achieved but this type of scope belongs to the special purpose class. It is interesting to think of the real time response of say a 5 GHz scope, $10 \%$ to $90 \%$ in $7 \times 10^{-11} \mathrm{sec}$, quite fast!

Returning to earth, although it is convenient to classify a scope by bandwidth (or rise time) there are other, perhaps more striking, differences between the classes of scopes.

## TIMEBASES

The uses of an audio oscilloscope are confined usually to periodic waveforms that can be adequately displayed by the use of a synchronised timebase without the need for complex and expensive trigger circuits. The difference between a sync or trig timebase will become clear when we come to consider more fully the numerous methods used to provide a timebase. Suffice to say that the sync timebase is a free running oscillator which is pushed along by a portion of the $Y$ signal applied as sync, whereas the trig timebase waits for a suitable signal before commencing a sweep.

One consequence of the sync mode is that the input signal ( Y ) must have a repetition frequency higher than that of the timebase for a stable image to result, as in Fig. 3. If the timebase is run faster than the repetition rate of the waveform, in order to view detail the trace folds up into a jumble.

Applied to the audio scope this latter effect is not of too great a consequence as there is usually little detail lurking in a signal repeating at 10 kHz . However in TV work we immediately become faced with complex waveforms to lock and also the possibility that the waveform may be required to be investigated more closely.

The triggered timebase becomes a necessity together with the improved $Y$ amplifier bandwidth. The timebase speed ranges are also increased for greater versatility and various modes of timebase operation are employed, including the important addition of an "EXTERNAL TRIG" connection enabling the timebase to be controlled externally. This facility is invaluable in TV work as it enables the frame generator in the receiver to work as a delay timebase generator, the trig level control on the scope selecting the lines to be viewed in isolation on the screen.

This sort of facility necessitates yet another improvement to be made to the simple audio scope, namely the trace brightness.

Fig. 3. The top display occurs when the timebase runs faster than the repetition rate of the input waveform. The consequence of a timebase running slower than the repetition rate is shown in the lower dispiay.

A recurring 1 kHz sine wave may be bright enough, but when the trace is scanning say 10 cm in $64!4 \mathrm{sec}$, and then only 25 or 50 times a second, the trace briliiance falls to almost vanishing point unless high CRT potentials are employed. Usually between 2 and 5 kV are used on oscilloscopes of this nature, as opposed to possibly less than 1 kV for the audio scope.

The TV or pulse oscilloscope then has, apart from an improved bandwidth, a fairly sophisticated timebase system and an improved display mechanism, together with a few other improvements such as DC coupling and the provision of calibrators.

Oscilloscopes intended for reasonably accurate measurement, but that are built to a price, usually incorporate some method of generating standard waveforms of precise voltage and/or time, this being cheaper than trying to stabilise the $Y$ amplifier gain and timebase against variations.

A fairly typical example of the type of calibration provided is the Cossor 2000 oscilloscope, a 5 MHz double beam scope suitable for general TV service and measurement.

The Y amplifiers are calibrated against an internally generated signal of 300 mV . The $Y$ amplifier control is set to give 3 cm deflection with the input attenuator set at $0 \cdot 1 \mathrm{~V} / \mathrm{cm}$.

The 300 mV signal is obtained from 50 Hz from the scope mains transformer and a small neon is used to provide a reference level of about 70 V from this high voltage AC . The resulting 70 V square wave is then attenuated and is available as the 300 mV calibration signal.

Time calibration is available as a 20 MHz oscillator providing intensity modulation of the beam. This means that a display brightens up at every 50 ns enabling accurate time measurements at the higher sweep speeds.

## LABORATORY SCOPES

The final class of scope that we shall consider is the laboratory scope and in this class we can conveniently consider the special purpose oscilloscopes.

In general one expects to find that a laboratory scope has a good bandwidth, versatile timebase with fast sweep speeds, high tube voltage and is capable of long lasting calibration to within a few per cent, depending on the measurement methods employed.

Intended for use in research and for the investigation of complex waveforms, the laboratory oscilloscope needs to be versatile and has therefore rather a lot of controls and tends to be physically large.

As we shall see later, wide bandwidth deflection systems require a large number of valves passing
fairly high currents. This, together with the number of valves in the timebase (usually two are provided) and the supply regulator needed to maintain calibration, means that the valve count is sometimes over a hundred and a power consumption of almost 1 kW is not uncommon. These big scopes are usually trolley mounted with a fan to keep the operating temperature at a reasonable level.

## TEKTRONIX TRENDS

Pioneers in this field of scopes were undoubtedly the American firm Tektronix and many other manufacturers have done a lot of copying from the Tektronix design. The Tektronix format of tube in the top left corner, $Y$ amplifier below, and timebase down the right-hand side is now familiar to users of laboratory scopes.

With the advent of Tektronix styling came another innovation, perhaps conceived initially by the same company and now copied by many, that of plug-in Y amplifiers, followed by plug-in almost everything! This means that a wideband ( 33 MHz for Tektronix) main frame can be used for a number of special purposes just by changing plug-in units.

The main frame houses the CRT, power supplies, $Y$ drive amplifier, $X$ amplifier and the timebase if this is not plug-in. A range of $Y$ plug-ins would then be used with the scope, providing double beam operation, differential inputs, very high sensitivity or a special function such as a spectrum analyser or four channel display. If plug-in timebases are provided these could be normal timebase, delay plus normal, very slow, or a straightforward amplifier plug-in for XY display.

Whilst appreciating that these plug-ins can cost a great deal of money it is fairly obvious that a selection of plug-ins is cheaper than a selection of scopes! The user is also able to keep in touch with current technology by the purchase of recent plugins offering such facilities as sampled inputs giving very high apparent bandwidths, although not in real time. One other advantage of plug-ins is that the $Y$ amplifier controls probably get the hardest use on a scope and it is an easy matter to remove the plug-in for maintenance without having to disembody the whole scope.




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## SAMPLING TECHNIQUES

The group of scopes classed as "special purpose" can be extended to virtually any scope not corresponding to the norm, and, in a way, most scopes have a little something special since they have to appeal to buyers, just like motor cars.

Perhaps the most important special purpose scope, to be found in few amateur labs, is the sampling oscilloscope.


A close-up of the front panel of one of the author's scopes. This EMI WM16 has plug-in facilities, dual timebases and a bandwidth of better than 40 MHz .

Considered on a real time basis the sampling scope has a bandwidth of a few tens of MHz . However, a special input circuit, usually contained in the probe, samples the instantaneous level of the signal at a rapid rate and the probe output when fed through the $Y$ amplifier produces a display that builds up in a very short space of time to a continuous display.

Various manufacturers use different sampling techniques but the results obtainable represent bandwidths well into the hundreds of MHz and beyond.
A useful result of the development of sampling techniques has been the production of a circuit which when connected to an oscilloscope deflection amplifier's outputs, enables the trace on the screen, perhaps a 5 MHz pulse, to be drawn by a mechanical plotter which takes about 10secs to complete one accurate scan. The technique used is similar to sampling oscilloscopes, the input to the XY plotter being sampled over say 10 seconds. The resulting XY plot is a faithful reproduction, within the plotter resolution, of the trace that was on the scope face, although not in real time as it takes 10 seconds to draw a signal of, say, 100 ns width.

Other special oscilloscopes are designed to do specific jobs and there are such things as spectrum analyser scopes produced. In this scope the $Y$ channel is narrow band, the precise band being determined by the X deflection voltage. Thus as the timebase sweeps, usually fairly slowly, the $Y$ amplifier sweeps a certain range of frequencies, the $Y$ deflection being proportional to the signal at that frequency. The $X$ axis can be calibrated in frequency and such a scope can be used for investigating modulation sidebands etc.
Storage scopes also fall into the category of "special purpose" if only by virtue of the very high price. We shall consider storage tubes in the next section dealing with displays, but suffice it to say here that a special tube is employed which enables a trace to be retained after the scan is completed. These scopes are very useful for low speed servo work and in conjunction with spectrum analyser facilities, as mentioned above, flicker can be completely eliminated.

To be continued


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# No. 58 GRIP TESTER 

## A series of simple transistor projects, using not more than twenty components.

THE objective when using this piece of equipment is to hold a probe (made of aluminium foil folded round a piece of wooden broom handle) in each hand and squeeze the probes as hard as possible. The tighter the grip the more the lamps will become illuminated. But more than this; the lamps come on in a set sequence. A weak grip will make only one lamp glow faintly but a very strong grip could make all three lamps glow brightly. An intermediate grip may only illuminate two lamps. The circuit shown in Fig. 1 is designed to operate three lamps this way but can be extended to operate as many as are required if the instructions are followed.
is reached when it might be more economic to use a zener diode. For more than four indicating stages R2 ought to be reduced to 220 ohm. The sensitivity of the unit is controlled by VR1. Reducing its value lowers the sensitivity and requires a stronger grip to get the lamps to light up.

## $\star$ components list

$$
\begin{aligned}
& \text { R1 } 1 \mathrm{k} \Omega \pm \mathrm{W} \text { R2 } 470 \Omega \pm \mathrm{W} \text { R3-5 } 1 \mathrm{k} \Omega \underset{\ddagger}{\ddagger} \mathrm{~W} \\
& \text { VR1 } 200 \mathrm{k} \Omega \text { linear potentiometer } \\
& \text { D1-6 } 1 \mathrm{~N} 4148 \text { Tr1-4 BC108 LP1-3 } 6 \mathrm{~V} 40 \mathrm{~mA} \\
& \text { Battery 9V Probes Veroboard }
\end{aligned}
$$

## Circuit

Trl is an emitter follower and the potential at its emitter is set by the potential divider effect of R1, VR1 and the body's resistance plus contact resistance between the palms of the hands and the probes. The lower the skin and body resistance the higher will be the emitter potential. Skin contact resistance can, to some extent, be controlled by the pressure of grip on the probes and this affects the emitter potential.

This potential is used to provide base current into each of the following grounded emitter lamp drivers but the silicon diodes in series with each of the bases ensures that in the case of $\operatorname{Tr} 2$ the output from Trl must be higher than 1 -2V while for $\operatorname{Tr} 3$ it must be $1 \cdot 8 \mathrm{~V}$ and for Tr 4 should exceed $2 \cdot 4 \mathrm{~V}$. Thus, when the grip is weak the potential from Trl might only be $1 \cdot 6 \mathrm{~V}$ and in this case LPl will be the only lamp illuminated but if it is $2 \cdot 2 \mathrm{~V} \operatorname{Tr} 3$ will be starting to conduct and LP2 will start to glow while LP1 glows even more brightly. The diodes are there simply to provide potential increments for consecutive stages and the technique of adding one extra to each stage could be continued until some point


Fig. 1, above, is the clrcuil for a four stage lester and a suggested layout on plain veroboard is shown In Fig. 2, below.


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| DL92 | 0.40 | EL36 | 0.50 | PCF805 | 0.90 | 1 T | 0.30 | 12AT7 | 0.40 |
| DL94 | 0.48 | ELS 7 | 2.50 | PCP806 | 0.76 | 3V4 | 0.70 | 12AU7 |  |
| DL9* | 0.65 | EL41 | 0.90 | PCF808 | 0.90 | ER4GY | 0.80 | 12AX7 | . 88 |
| DY86/7 | 0.38 | EL, 42 | 0.90 | PCL82 | 0.85 | bU49 | 0.40 | 12BAB | 5 |
| DY802 | 0.87 | EL84 | 0.28 | PCL83 | 0.68 | 8V40 | 0.50 | 12BE6 | . 50 |
| EABC80 | 0.88 | EL,95 | 0.40 | PCLE4 | 0.45 | 5Y30T | 0.46 | 30 Cl | - 80 |
| EAF42 | 0.75 | ELL80 | 1.00 | PCL85 | 0.50 | 8240 | 0.45 | 30 Cl 15 | 1.05 |
| E891 | 0.29 | EM80 | 0.48 | PCL86 | 0.45 | 6/30L2 | $0-80$ | 30 C 17 | 1-10 |
| EBC33 | 100 | EM81 | 0.80 | PCL805/85 |  | BAKB | 0.40 | 30 C 18 | 0.90 |
| EBC41 | 0.75 | EM84 | 0.85 |  | 0.50 | 6A35 | 0.90 | 30P5 | $1-10$ |
| EBC81 | 0.88 | EM85 | 1.00 | PD500 | 1.80 | 8AQS | 0.45 | 30FL1 | 0.80 |
| EBF80 | 0.40 | EY51 | 0.40 | PEN 45 | 0.75 | $6 \mathrm{AB7C}$ | 0.85 | 30PL2 | 0.75 |
| EBP83 | 0.40 | EY86 | 0.40 | PL,36 | 0.85 | 6AT6 | 0.45 | 30FL14 | 0.90 |
| 89 | 0. | EZ40 | 0.75 | PL81 | 0.50 | 6AU6 | 0.80 | 30L15 | 1.05 |
| PCC81 | 0.40 | E280 | 0.78 0.88 | ${ }_{\text {PLL8 }}$ | 0.45 | 6BA6 | 0.28 | 30 L 17 | 0.95 |
| ECC82 | 0.83 | EZ81 | 0.89 | PL84 | 0 | BBE6 | 035 | 30P4M | 1.30 |
| ECC83 | 0.81 | GY801 | 080 | PL500 | 0.75 | ${ }_{6}^{68146}$ | 0.75 0.55 | 30P12 | 1.05 |
| ECC84 | 0.80 | O230 | 0.45 | PLS04 | 0.75 | 6BQ7A | 0.55 | 30 PJ 9 | 1.00 |
| eccss | 0.40 | O232 | 0.50 | PL508 | 0.90 | ${ }^{6887}$ | 1.00 | 30 PL 1 | 0.98 |
| ECC88 | 0.40 | 9234 | 0.65 | PLS09 | 1.55 | 6887 | 1.85 | 30 PL 13 | 1.80 |
| CE35 | $1 \cdot 25$ | G2, ${ }^{\text {\% }}$ | 1.85 | PL802 | 0.95 | 6BW\% | 0.90 | 30 PL 13 | 1.80 |
| CHE42 | 12.00 | HN309 | 1.50 | PX4 | 3.50 | 68w7 | 0.90 | OPL14 | 1.25 |
| ECL80 | 0.55 | ET81 (7C5) |  | PY33 | 0.68 | 6CD6G | 1.80 | 35240T | 0.70 |
| ECL82 | 0.85 |  | $1 \cdot 30$ | PY81 | 0.80 0.85 | ${ }^{6} \mathrm{CH} 6$ | 1.40 | 50CD6 | 1.20 |
| ECL83 | 0.70 | KT81 | 1.75 | ${ }_{\text {PY'83 }}$ | 0.85 0.88 | ${ }^{6 \mathrm{FP}_{23}}$ | 1.00 | 807 | 0.80 |
| CLS8 | 0.40 | Кт88 | 2.90 | PV88 | 0.40 | 6 F 25 | 1.00 | 813 ITT | 118 |
| FCLL 800 | 3.20 | KTW61 | 1.00 | PY500 | 1.00 | $6 \mathrm{~F}^{2} 8$ | 0.70 | 813 U88R |  |
| EF37A | 1.20 | MU14 | 1.00 | PY81'800 | 0.60 | 6.55M | 0.85 |  | 15.75 |
| EF39 | 1.20 | Ni\% | 2.75 | PY801 | 0.50 | 6J56: | 045 | 96ifil | 0 | EXPRESS $5 p$ for 1 Valve. Each addtitonel veive

add 2p. add 2 D

| PL84 $\quad 0.68$ | 30C151 |  |
| :---: | :---: | :---: |
| PL504 0.88 | PCF800 | 1.05 |
| PI.508 1.05 | 30 Cl 7 | 1.00 |
| PL509 1.55 | 30 Cl 181 |  |
| PL80: 0.98 | PCF805 | 0.90 |
| PY33 0.88 | 30F3/P | 18 |
| PY81/800 0.50 |  | $1 \cdot 10$ |
| PV82 0.55 | 30FLI/ |  |
| $\begin{array}{ll}\text { PY88 } & 0.80\end{array}$ | PCE800 | 0.75 |
| PY500A 1.05 | 30FL'2 | 0.75 |
| PY800 0.50 | $30 \mathrm{FL12}$ | 1.05 |
| PY801 0.50 | 30FL14 | 0.85 |
| [26 1.00 | 30L1/PCC84 |  |
| U101 1.00 |  | 0.52 |
| $\begin{array}{ll}U 193 & 0.50\end{array}$ | 30L15/PCC805 |  |
| UABC80 0.90 |  |  |
| UBC81 0.70 |  | 1.05 |
| UBF89 0.60 | 30 LI 7 | 0.90 |
| UCC8s $\quad 0.60$ | 30P43R | 1.30 |
| UCH81 1.00 | 30P12/PC801 |  |
| $\begin{array}{ll}\text { UCL82 } & \mathbf{0 - 7 0}\end{array}$ |  | 1.05 |
| UCL83 $\quad 0.70$ | 30P19/PC802 |  |
| UF89 $\quad 0.80$ |  | 1.00 |
| U1.84 0.98 | 30PL1/PCLS01 |  |
| $\begin{array}{ll}\text { UY85 } & 0.50\end{array}$ | $30 \mathrm{PL} 1 / \mathrm{PC}$ | 0.95 |
| 6/30L2] 1.00 | 30P L131 |  |
| ECC804 1.00 | PCL800 | 1-20 |
| 1.05 | 30PL14/ |  |
| 30C1/PCF80 | PCL88 | 1.25 |
| 0.51 | 30 PLIS | 1.05 |




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| ACl |
| :--- |
| ACl |
| ACl |
| ACl |

AC18
AC18
ACY
ACH
ACY

| ACY39 | 0.22 | BFI |
| :--- | :--- | :--- |
| BF200 |  |  |
| AD140 | 0.65 | BF881 |

AD1
ADI
APl
APl
APll
APll

|  | AP1 | 0.25 | BYY51 |
| :--- | :--- | :--- | :--- |
|  | 0 |  |  |
| AF117 | 0.25 | BPY52 | 0 |

AF18
AF 23
A 8 Y 2


|  | BY |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| $\mathrm{BC1}$ |
| :--- |
| BCl |

$\mathrm{BC10}$
$\mathrm{BCl1}$
$\mathrm{BCl1}$


|  | CC147 | 0.18 | MJE340 |
| :--- | :--- | :--- | :--- |
| MJE370 | 0.50 |  |  |
| BC148 | 0.10 | MJE |  |


| BCI 89 C | 0.10 | MJE520 | 0.65 |
| :--- | :--- | :--- | :--- |
|  | 0.14 | MJF.2955 | 1.10 |



| BC182L | 0.18 | MPP102 | 0.40 | ORP60 | 0.45 | $2 N 1303$ | 0.28 | $2 N 3904$ | 0.20 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| BC184L | 0.13 | MPF103 | 0.38 | T1005 | 020 | $2 N 1304$ | 0.28 | 2N390 | 0.26 |
| BCY32 | 1.20 | MPF104 | 0.35 | TIC44 | 0.20 | $2 N 1304$ | 0.28 | 2N306 | 0.16 |


| BCY32 | 1.20 | MPF104 | 0.35 | TIC44 | 0.29 | $2 N 1305$ | 0.22 | $2 N 3906$ | 0.16 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| BCY33 | 0.38 | MPF105 | 0.46 | TIC226U | 1.50 | $2 N 1308$ | 028 | $2 N 4059$ | 0.15 |
| BCY34 | 0.45 | NKT404 | 0.60 | TIL20H | 0.95 | $2 N 1307$ | 0.28 | $2 N 4080$ | 0.18 |


| BCY70 | 0.15 | OAS | 0.60 | TI843 | 0.28 | 2N1307 | 0.28 | $2 N 4080$ | 0.18 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| BCY71 | 0.20 | OA10 | 040 | ZTX107 | 0.12 | 2N1308 | $0-28$ | 2N4081 | 0.13 |
| BCY72 | 0.15 | OAT9 | 0.10 | ZTX108 | 0.10 | 2N1613 | 0.20 | $2 N 4062$ | 0.14 |


| BC1 | 0.18 | OA79 | 0.10 | ZTX108 | 0.10 | $2 N 1613$ | 0.20 | $3 N 141$ | 0.81 |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BCZ11 | 085 | OA81 | $0-10$ | ZTX300 | 0.14 | $2 N 1614$ | 0.45 | 40360 | 0.40 |
| BD121 | 1.00 | OA91 | 07 | ZTX 301 | 0.14 | $2 N 2147$ | 0.76 | 40361 | 0.45 |
| BD124 | 0.80 | OA200 | 0.08 | ZTX 301 | 0.20 | $2 N 0160$ | 100 | 40862 | 0.40 |


|  |  |  |  |  | 0.2 |  | 0.16 | 40436 | 0.85 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| EN7400 | $0 \cdot 20$ | 8N7425 | 0.37 | 8N7473 | 0.44 | 8N74107 | 0.51 | 37 | 0 |
| 8N7401 | 0.20 | 8NT427 | 0.37 | 8 87474 | 0.48 | 8NT4110 | $0-67$ | 8N74170 | 2.88 |
| 8N7402 | 0.20 | 8N7428 | 0.43 | 8N7475 | 0.59 | 8N74111 | 0.86 | 8N74174 | $1-80$ |
| 8N7403 | 0.20 | 8N7430 | 0.20 | 8 ¢ 7476 | 0.45 | 8N7418 | 1.00 | BN74175 | 1.29 |
| 8NT404 | 0.20 | 8N7432 | 0.37 | 8N7480 | 0.80 | SN74119 | 1.98 | 8N74176 | 1.44 |
| 8N7405 | 0.20 | 8N7433 | 0.43 | 8N742 | 0.87 | 8N74121 | 0.57 | BN74190 | 8.30 |
| 8N7406 | 0.40 | 8N7437 | 0.48 | $8 \mathrm{S7483}$ | $1-20$ | 8N74122 | 0.80 | 8N7419 | 8.30 |
| 8N7407 | 0.40 | 8N7438 | 0.43 | ON7484 | 1.00 | 8N7423 | 1.44 | BN7419 | $8 \cdot 30$ |
| SNT408 | 0.25 | 8N7440 | 0.20 | 8N7486 | 0.50 | 8N74141 | 1.00 | 8N7 | 2.30 |
| SN7409 | 0.38 | SN7441AN |  | 8N7490 | 0-75 | 8N7414 | 144 | BN 74 | 78 |
| 8NT410 | 0.20 |  | 085 | EN7491AN |  | 8S 74150 | 2.30 | 8N74195 | 1.44 |
| 8N7411 | 0.23 | 8N7442 | 0.85 |  | 1.10 | 8N74151 | 1.15 | BN74198 | 1.58 |
| 8N7412 | 0.28 | 8N7450 | 0.20 | 8N7492 | 0.75 | 8N74154 | 2.30 | 8N74197 | 1.58 |
| SN7413 | 0.80 | 8N7481 | 0.20 | 8N7493 | 0.75 | 8NT4185 | 1.15 | 8N74198 | 3.18 |
| 8N7416 | 0.80 | 8N7453 | 0.80 | 8N7494 | 0.85 | 8574156 | 1.15 | 8N74199 | $2 \cdot 88$ |
| 8N7417 8N7420 | 0.80 | 8, 7454 | 0.20 | 8×7495 | 0.85 |  |  |  |  |
| 8N7420 | 0.20 | 8N7460 | 0.80 | 8N7496 | 1.00 | IL |  |  |  |
| BN7422 | 0.28 | 8N7470 | 0.33 | 8N7497 | 4.38 |  |  | 16 |  |
| 8N7423 | 0.40 | 8N7472 | 0.38 | 8N74100 | $2 \cdot 16$ | SOCKET |  | 16 pin | $7 p$ |

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$24^{\prime \prime} \times 24^{\prime \prime}$ ；FULL SHEET $43^{\prime \prime} \times 37^{\prime \prime}\left(11^{\mathrm{sq}}\right.$ ．it．）．SIngle． sided Copper with thickness of $1 / 32^{59}, 3 / 64^{\prime \prime}, 3 / 32^{\prime \prime}$ ．

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| 1バ・ |  | 111c＊＊ |  | 11－55 |
| 12゙ |  | －13＊ |  | E1．89 |
| 121 | $\because 1.1$ MT | T716 ${ }^{\text {a }}$ |  | 22．45 |
| 12－ |  | T人页 |  | 2308 |
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| 12v． | $3{ }^{3} \mathrm{O}$ ，MT | $7 \% .17$ |  |  |
| 30 Volts． 111 tappril at（1－12－15－30－3030． |  |  |  |  |
| Ointput | Ref．Sir．P＇ricer | Output | Ref．Nor | ＇rler |
| Ampe． |  | 11川か． |  |  |
| 50074 | 3T1121＇Tキ 21．81 | 4 | MT：JIT | 25－22 |
| 14 |  | 3.1 | MT．alt | 26．10 |
| $\because 1$ | HT 3．1T 23.77 | N．I |  | \％9－88 |
| 3 A | MT：01T 8431 | 161 | MTmgAT | ¢11－97 |
|  | 50 Volts．ill tappuel at | $0 \cdot 19.23 .33 \cdot 40 \cdot 504$ |  |  |
| S00\％n． | MT10：．1T $\ddagger 28.38$ | 3.1 | MT10．at | ¢6．34 |
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|  | 60 Volts．All tapued at | （0）－24．30－4）－4x－501． |  |  |
| S10\％ma | 9T1：4AT $22 \cdot 60$ | $\because \wedge$ | MTIEAT | E5－15 |
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| AUTO－WOUSD RANGE |  |  |  |  |
| Pinver |  |  |  |  |
| Hutput | Nimeling tapied at |  |  | e |
| 20） | 0．115－210－240 |  | $31^{\circ} \mathrm{T}$ | 21.48 |
| 73－A |  | MT | IT | 1295 |
| biovis | 0．115－2（4）－230．241） | 11 T |  | 23．61 |
| 200才， |  | MT |  | ¢4 31 |
| 400 V ．Ontput at 50 Hz ． |  |  |  |  |
|  Wirelew W＇orda． |  |  |  |  |
| Referen | nce 1T3AT |  |  | 84－26 |
| EQUIPMENT RANGE |  |  |  |  |
| Hec．Ou | utput（r．m．ッ．） | Ret． | No． | Prie |
| $3-0.3 \mathrm{~V}$ | 200m． 1 | MT： | 34＊＊＊ | 1139 |
| 0．0．9 | 100 ml | 3 T | （＂\＄＊ | 11．39 |
| 1：0．1：3 | － 50 m 1 | MT | 14＞0＊ | 2130 |
| $20.00 \cdot 30$ | 30 mal | MT： | 1 （＂x－＊ | 21.39 |
| $0-30$ \％ | $\because 30 \%$ ¢1 | 3 T | $4{ }^{\text {T }}$＂ | 28．13 |
| 0．8．9 ${ }^{\text {\％}}$ | －301m．－－ | MT： | な「＊＊ | 22－53 |
| 0－15－20 |  | MT： | ST＊＊ | 23.39 |
| 0．1．5－27 | 7 ．${ }^{2}$ shom－－ | 11 T | 03．AT＊ | ¢3．78 |
| 0－1．1－23 | ＊ $11 \times 2$ | 1 T | 04，${ }^{\text {c }}$ | $23 \cdot 78$ |
| $30.12 \cdot 0$ |  | 3 T | $1 \mathrm{~T}^{*}$ | 21.98 |
| AT milleater fipen uthemal thing with tags：CT in sipw <br>  <br>  primary；$\ddagger$ tappent at $210-2401$ ；onther prituarien tappes <br>  |  |  |  |  |
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SHORT WAVE DX

## by MALCOLM CONNAH

THE receivers used by Broadcast Bands listeners vary enormously; they may be ex-government sets or brand-new commercial units; but all receivers have one thing in common: They will not give their best performance until they are used with a good aerial system.

When we talk of an aerial system we include any devices, such as aerial tuning units, which are placed between the aerial and the receiver.

In order to get optimum reception the aerial system must be resonant at the frequency of reception. Amateur Bands listeners, and operators, have an advantage here because their bands, with the exception of 15 metres, are closely related. These bands are 10, 20, 40, 80 and 160 metres. If an aerial system is resonant on 80 metres it is a relatively simple matter to get it to resonate on 40,20 and 10 metres.

The Broadcast Bands, however, are completely unrelated being $11,13,16,19,25,31,41,49,60,75$, 90 and 120 metres. If one of these bands is of particular interest a half-wave dipole may be erected for that band. The only practical solution for all band reception is to use some form of end-fed aerial. It should be noted that the term 'long-wire' is often used incorrectly, a misuse of which I have been guilty, as this is strictly an end-fed aerial which is long in relation to the wavelength being received.

The length of aerial that can be erected depends on the amount of space available, but the usual compromise is between 50 and 100 feet long. Theory dictates that the aerial should be straight, but many people have had very good results with aerials that have been bent in order to fit them into the space available.

The aerial should, preferably, be an outdoor one erected at a reasonable height and located as far away as possible from such obstructions as buildings and trees. A very simple aerial tuning unit (such as that described by David Gibson in the January 1974 issue) should then be constructed in order to make the aerial system resonant on the desired bands.

## Readers' Logs

David Kernick of Prescot, Lancashire used his Grundig TR600A portable with only just the built-in telescopic antenna to hear the following.
'6070 R. Sofia, Bulgaria at 1930 .
7145 R. Kiev in English at 0030.
7215 All India Radio in English at 2000.
9550 R. Finland noted at 1805.
9670 Adventist World Radio at 0930.
9695 V. of Saudi Arabia, Arabic at 0405.
9745 R. Baghdad, Iraq noted at 1945.
9770 R. Australia, English at 1605.
9833 R. Budapest, Hungary at 1615.
11920 R. Algiers noted at 1900.
11970 R. Tunis in Arabic at 0920.
15140 R. Havana, Cuba in French at 1935.
15165 R. Denmark in Danish at 1850.
15240 R. Belgrade, Yugoslavia at 1530.
15410 United Nations Radio at 1600.
17755 HCJB, Quito, Ecuador at 1930.
17780 RSA, South Africa noted at 1600 .
17845 WYFR noted in English at 1730.
17865 WINB, Red Lion, music at 1930.
21630 V . of Saudi Arabia, testing at 1110.
Richard Staples has found an Eddystone 680X in the loft (excuse me whilst I return my ladder to garage) and the addition of a 100 foot end-fed aerial produced:
3999 R. Godthab, Greenland in Danish at 0840.
4820 Voz Evangelica, Honduras at 1805.
4940 R. Yaracuy, Venezuela, Spanish at 1740.
5920 R. Kiev, news in English at 1800.
9590 R. Australia noted in English.
9610 R. Canada in English at 2115.
11720 R. Nacional, Brazil, Portuguese at 0705.
11935 R. Pakistan, news in English at 1715.
15200 RSA, South Africa in English at 0840.
21695 Greek Military Radio, Athens at 0905.
Christopher Hodgson of Sunderland reports that Radio WYFR (Family Radio Inc.) broadcasts in English to Europe at 1810 GMT on 15130 kHz . The station replied to his report in about two weeks and the address for reports is: WYFR, 290 Hegenberger Road, Oakland, California 94621, U.S.A.

With his usual equipment; Codar Multiband 6, P.W.
A.T.U. and 50 foot end-fed; Christopher also heard:

7080 Voice of Vietnam, Hanoi at 1820.
7210 Red Cross Broadcasting at 1700.
9505 VOA, Tangier, in Rumanian at 1930.
9525 All India Radio at 2010.
9540 Radio Tashkent noted at 1210.
9545 Radio Ghana, s/off at 2215.
11805 WYFR-Family Radio at 2100.
15130 WYFR-Family Radio at 1810.
15175 RSA, South Africa, s/off at 1850.
15185 R. Finland noted at 1830.
15290 ORTF, Paris, s/off at 1115.
15415 Radio Kuwait, s/on at 1730.
15420 BBC; East Med. relay noted at 1600.
17820 R. Canada, s/on in Polish at 1530.


## VHF/FM

by SIMON DAVID

HOGMANAY was celebrated in Scotland in a different way than usual. No doubt the timing was deliberate for Radio Clyde, Scotland's first commercial radio station, broadcast on $95 \cdot 1 \mathrm{MHz}$ on December 3lst. The station started at 10.30 p.m. with news and introductions to the staff. The 4 kW transmitter is at Black Hill.

The criticisms and doubts surrounding London Broadcasting, the London news stations, resulted in the resignations recently of the Managing Director and Chief Editor. Former Lord Mayor of London, Sir Charles Trinder, also walked out issuing an ad-
mission that the finances had not lived up to expectations. One thing evident is the difference between some commercial and BBC local radio broadcasts from a technical standpoint and although both have severe financial restrictions, it is only to be expected that the latter has the advantage of drawing on the resources of its "great-auntie".

I have been informed that BBC Radio Derby is still operating on 96.5 MHz from Sutton Coldfield using slant polarisation. The $94 \cdot 2 \mathrm{MHz}$ transmitter that I mentioned recently is installed at the studio to fill-in the town centre area because of surrounding high ground. It uses a vertically polarised aerial and 10 watt transmitter.

The Radio Derby aerial at Sutton Coldfield is a 5-element Yagi array 500 feet above ground level. It provides a maximum e.r.p. of 5 kW in the Derby direction.

Also from Derby, Roy Patrick reports that the Lichfield IBA transmitter for the Birmingham area is due on the air on 94.8 MHz in February; the Manchester commercial station is due on $97 \cdot 0 \mathrm{MHz}$ ( 2 kW ) in March; the Swansea station is expected to start transmitting on $95 \cdot 1 \mathrm{MHz}$ (lkW), using the circular type of aerial, later on in the summer of 1974.

Last month I reported on the results of using the Antiference FM264T six-element aerial. Results since then have been repeated with the addition of Rouen on 96.6 MHz . Unfortunately conditions have not favoured reception from Rheims.

## MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

DAVE KERNICK (Prescot, Lancs) has a Grundig TR600A transistor portable with a built-in ferrite rod antenna, which he has found to be an excellent receiver for pulling-in distant stations. He reports hearing programmes in English from AFN Frankfurt 872 kHz ; Deutschlandfunk, West Germany 1268 kHz at 1745 hrs ; Radio Norway 1578 kHz at midnight; Radio Sweden 1178 kHz at 2245 hrs ; Radio Tirana, Albania 1457 kHz (additional frequency for the English Service) at 0330hrs; together with Sud Radio, Andorra in French at 2245hrs on 818 kHz and Tripoli, Libya in Arabic at 0025 hrs on 1250 kHz . Dave asks if it is possible to hear North America on the medium waves using a portable receiver. This is unlikely as a ferrite rod aerial does not have enough pick-up to receive really distant stations. DXers who want to try for North Americans should use an external aerial or a medium wave loop such as the DXers MW Loop Aerial described in the April 1973 issue of Practical Wireless.

## Readers' Logs

Roy Patrick (Derby) reports hearing the new Independent Broadcasting Authority (IBA) station at Manchester testing on 1151 kHz at 1100 hrs on December lst and IBA Birmingham using test tones on the same channel. IBA stations in the provinces are expected to use 1151 kHz for stations at Manchester, Birmingham and Glasgow (R. Clyde); 1169 kHz for Swansea and 1546 kHz for Liverpool and Edinburgh.
R. B. Callwood (Munich, West Germany) reports hearing BBC Radio 1 ( 1214 kHz ) at 1300 hrs on his
car radio while driving on the autobahn between Munich and Frankfurt. Reception was on a single occasion only and he wonders if any other reader has received BBC Radio 1 in Germany.

Bill Thorne (London) asks for information about the French broadcasts on $584 \mathrm{kHz}(513 \mathrm{~m})$ which he listens to regularly. The station on this frequency produces programmes for the Paris area for the greater part of the day and has a power of only 5 kW . The address is O.R.T.F., 116 Avenue du President Kennedy, Paris l6eme France.

Brian Murray has heard IBA Radio Clyde testing on 1151 kHz at 1345 hrs and he reports that this station is due on the air on December 31st, 1973. Brian has been busy again with his Astrad VEF 204 receiver using an old band 1 TV aerial as a medium wave antenna. His log includes programmes in English from Radio Warsaw 1502 kHz at 0115 hrs ; Radio Sweden 1178 kHz at 0025hrs; Manx Radio, Isle of Man 1295 kHz at 1350 hrs ; Radio Eireann 1250 kHz at 2120 hrs ; Trans World Radio, Montecarlo 1466 kHz at 2325 hrs and Radio Portugal 755 kHz at 2312 hrs .

A last-minute phone call from T. McCann (Belfast) reports reception of Newfoundland on 930 kHz (CJON in St. John's) with the comment "I was surprised at the strength of this station." Propagation on the North American path is rather variable with periods of a week or more when nothing can be heard. At other times, many stations in Canada and the United States can be heard, the limiting factor being interference from Europeans. During the winter listen around midnight on $600 \mathrm{kHz}, 640 \mathrm{kHz}, 710 \mathrm{kHz}, 930 \mathrm{kHz}$, $940 \mathrm{kHz}, 950 \mathrm{kHz}, 1070 \mathrm{kHz}, 1130 \mathrm{kHz}$. North Americans are easy to identify as all stations are allocated callsigns which are used frequently together with the name of the town or city where the studios are located.

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SHORT WAVES by DAVID GIBSON, G3JDG

Athank you to the many sharp-eared r.f. sleuths who sent in logs. Everyone seems to have bagged far more DX than I did-well done.
John Powell (Essex) sends in some useful information regarding "who's where and when". John says look out for VQ9HCS on Astove Island (look it up; I had to!). New Ham on Campbell Island is ZL4NJ/A.

A listening MUST. Havering Amateur Radio Club are running a station in Rutland from Saturday, March 30 to Monday April 1 1974. Listen on topband, eighty and v.h.f. Why? Because after that date there will be no County of Rutland, its being absorbed into the surrounding counties so this is your very last chance. Full marks for initiative to the Havering A.R.C.
Michael Watson (Kent) tells that a station in Teheran, EP2BQ, has put up an inverted V for topband. Listen for the EP2 callsign in the bottom 5 kHz of 160 metres. Who will hear him first?

Several people have written taking me to task for omitting the list of Happenings in the radio world. It appears that we have a number of keen Contest types among us. The calendar for February is as follows: $9-10,1 \cdot 8 \mathrm{MHz}$ contest; 16-17, ARRL Contest (c.w.); 23-24, REF contest (phone); March $3-4,144 \mathrm{MHz}$ Open and s.w.l. contest; March $3-4$, ARRL DX conteśt (phone). National Field Day this year will be on June 1-2.
Robert Beebe (Derby) reports hoards of G stations on topband. He tells that members of the Derby club have worked some juicy DX around 1830 kHz and quotes calls like W1, KV4, DJ and OK etc.

Vice Chairman (wonder what sort of vice?) David Andrews writes to tell of the Droitwich High School Radio Club. Ten members so far and all going in for the R.A.E. The Club has both Rx and Tx but no antenna up as yet. (How about a base-loaded Maths Master-a sure sine of success).
Keith Rowlings (Herts) has a UR1A, PR40, 75 ft . long wire-and a problem. He's heard N20 and L50 on 7 MHz and wants to know where they are (and so do I). Anyone any information on these or are they Japanese postal districts?

Graham Nicholls (Oxon) has a homebrew 70 cm converter feeding a homebrew 144 MHz converter which feeds an R107 (not homebrew). His 15 element 70 cm Parabeam rests in his bedroom, but it still heard the following; F1CTH, G3BA, G3COJ, G3DAH. G3YXN, G3KEQ, G3UHT, G3WSN, G3ZFP, G3ZMD. G3YC, G4ABF, G4AHU, G4BEL, G4BMP, G6XM. G8ADC. G8FMK, GW8AWS/P, HW6BQH/P. HW7FY, ON5FF, ON5HN. On two metres with a hamebrew 6-ele Yagi (also in the bedroom) Graham logged; GW8HEZ, HW1CS, HW5SY. PAOADY, PAOCIO, PAOEZR/A. PAOFHV, PAOPEP. PA0PRY, PA0TAR, SM7DT.
Ye fantastic logge has been sent in by Stanley Sharred. I note that it's on IBM paper-it's cheating if you get the computer to listen and log. No gear is mentioned (bet it's a regenerative cats whisker feeding a 100 Watt light bulb) but the following are claimed for 160 metres; GM3ANO, GM4ALK. GM4ASY. GW3UCB. DK3BJ, EI8H, K2ANR. K3RUQ, KV4FZ, OE5KE, OK1AXD, OK1FCW. OK1KRS, OK1KPU, OK2BKT, OK5KWA, OL6AQJ. OL8CCS, PA0HIP, VEICD, VEIMX, VEIASJ. VOIKE, W1DX, WIMX, W2DED, W2LWI, W2UEZ. WA2WLN/2, WA8IJI, WB8APM. On $3 \cdot 5 \mathrm{MHz}$. Stanley excelled with; CT1ADV, CT2BG, EL7D. K2BT, VE1AIH, VOIFG, 7X2MD, 9Y4HR. An excursion to 7 MHz revealed DX like; C3IMO, CR4BS. CR6TP, EP2TW, K4DX, PY4MA, PY6WF, PY6AOV. SV1CH, TYlABE, YV1BI, 5U7BB, 9G1HE.'
Eighty metres found Martin Ward listening with a JR500S and 60ft. end fed plus an "L-match device" (Oh L). Squeaks of s.s.b. reported from; CTIGC, LXIGC, KG4CB, VElAIH, VOIFG, 9H1CE. 9J2AE, and a late arrival-CNBCG. Martin reports hearing the Panama City Radio Club on 21 MHz with the callsign 3EIKC.

Stephen Day (Suffolk) made an "adjustment" to his R1155 and claims the signals went up by some 20dB. (You can come and make the same adjustment to my receiver-anytime). Antenna is 50 ft . end fed and main interest is eighty metres. Stephen bagged mostly G stations but managed foreign signals from; ZK5AFZ and 9H4L.
John Turner says, "I have been giving the Pye Cambridge a rest". What a thoughtful lad. This compassion for a trusty friend has not prevented John from listening with his homebrew t.r.f. (P.W. November 1963). The bandspread is the small tuning capacitor from the 235 MHz section of an Ex 19 set. The t.r.f. 85 ft . end fed and lots of patience produced; CT2BK, EA6CK, EA8IH, EL7C, HB0LL. HI3XCP, HK3AVK, HRIRSP, HZ1SH, JX4GN JY6UMS, K4PWC/AM, KP4BBW, PY2ELV, PY4LW. PZ1DR, TF5TP, TG8KT, VE1AF, VE3AII/SU. VK2AHM, VK2LW, VK2SG, VK3AD, VK3AX. VK3XJ, VK5FH, VK6SB, VS9MJ, VU2GBG. YV4AGT, ZB2CS, ZB2DL, ZD7SD, ZD7SS, ZM3FO. 3A2CP, 4Z4MQ, 5B4F, 7X2MD. Think what could have been received if Stephen Day (above) had made an "adjustment"!

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| Transistori／ Dlodes |  | BC109 | 11p | BC303 |  |
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|  |  | $\mathrm{BCl}_{13}$ | 15tp | BC304 | p |
|  |  | 13C1 16 | 16 p | BCY70 | 17p |
| 10 | 18p | 18C128 | 18p | BCY71 | 370 |
| C126 | 140 | ${ }^{3} \mathrm{Cl} 126$ | 250 | BCY72 | 17 p |
| ${ }^{\text {AC127 }}$ | 13p | BC132 | 16D | BD131 | 680 |
| $\mathrm{ACl}^{2} 8$ | 130 | $\mathrm{BCl}^{34}$ | 16p | BD132 | 90p |
| ACl42K | 220 | HC135 | 16 D | BDi3s | 420 |
| AClilk | 20g | ${ }^{13 C 137}$ | $18 p$ | BD138 |  |
| $\mathrm{ACl}^{\text {c }} 8$ | 150 | $\mathrm{BCl}^{\text {Cl }} 38$ | 38 p | $\mathrm{HDI}^{\text {D }}$ | 187 |
| AC187 | 18p | HC142 | 83 p | BDI 4 | 50p |
| AC187K | 20p | BC143 | 330 | BF159 | 33 |
| $\mathrm{ACl}^{\text {c }}$ | 180 | BC14． | 30 g | BF゙173 | 290 |
| AC188K | 20 D | $\mathrm{BCl}^{45}$ | 28p | BF177 | 280 |
| ACY17 | 24D | 1 BCl 47 | 97 | Br゙178 | 28 |
| ACY18 | 21p | HC148 | 98 | BF179 | 35 p |
| ACY19 | 25p | HC149 | 9 p | BF194 | 150 |
| $\mathrm{ACY}^{20}$ | 22p | ${ }^{3} \mathrm{C} 153$ | 16p | BF19 | 17D |
| ACY21 | 23 p | $\mathrm{BCl}^{4} 4$ | 170 | BF24 | 270 |
| ACY＇2 | 18p | BCl57 | 13 p | BF260 | 29p |
| ACY39 | 68p | BC158 | 12p | 13F329 | 18 |
| AD140 | 40p | ${ }^{\text {BCL }} 69$ | 14 p | 13F330 | 18 |
| AD142 | 44D | ${ }^{\mathrm{BC}} \mathrm{Cl} 67$ | 13p | B F＇390 | 37 |
| AD143 | 39p | BC168 | $11 p$ | BFX84 | 28 p |
| AD143 | 38p | BC169 | 11. | BFX85 | $35 p$ |
| AD150 | 60 p | BC17 | 15p | 13FX86 | 22 p |
| ADl61 | 38p | BC179 | 15p | BFX87 | 28p |
| ADIG2 | 38p | BCIR2L | 10p | BFX8S | 260 |
| AF114 | 180 | HC183L | 110 | BFY50 | 210 |
| AF115 | 18p | BC184 | 11p | BFY51 | 17D |
| AF116 | 18． | BC186 | 33 p | BPY52 | 17p |
| AF117 | 18p | BC212L | 11. | BFY64 | 38 D |
| AF118 | 92p | BCO13L | 11 p | BFY90 | 72p |
| AF124 | 27D | BC214L | 110 | BSX2 | 18D |
| AF＇139 | 39p | BC258 | 8p | $\mathrm{C4} 07$ | 22p |
| AF：239 | 41p | HC259 | 9 p | C4． 26 | 33p |
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| AL102 | 66 p | BC268 | 18p | C450 | 17p |
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| $\mathrm{BCl}^{0 .}$ | 11p | BC301 | 32p | MP811？ | 42p |
| 3C108 | 110 | BC302 | 30 p | MP8113 | ， |

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Single. 12p. Dual ganz (stereo), 40 p . Single D.

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| AC107 | 15p | AFI 26 | 20p | BFIIS | 25p | OC42 | 12p | 2N3707 | 12p |
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excluding case. Mains operared der detectors including GDI and P.C. board but excluding case. Mains operated detector 65-20, 12 or 24 V battery operated audible

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Draw the planned circuit onto a copper laminate board with the PC. Pen allow 97 dry, and immerse the board in the etchant. On removal the circuit remains in hish relief.

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## Stereo 80 pre-amplifier and control unit



Each channel has ths own separate tone and volume controls operated by shders. enabling ideal environmental matching to be obtained. A virtual earth input stage forms part of the up-dated circuitry that ensures the finest possible quality from all signal sources. Generous overload margins are allowed on all inputs. Clear instructions with template are supplied. TECHNICAL SPECIFICATIONS
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Finish - Black with white indicators and transparent sliders
Inputs - Magnetic pick -up 3 mV RIAA Corrected: Ceramic pick-up 300 mV
Radio 300 mV : Tape 30 mV
Signal/noise ratio - 60dt
Frequency range -20 Hz to $15 \mathrm{KHz}=1 \mathrm{~dB}: 10 \mathrm{~Hz}$ to $25 \mathrm{KHz}=3 \mathrm{~dB}$ Power requirements - 20 to 35 volts
Outputs $-100 \mathrm{mV}-\mathrm{AB}$ monitoring for tape
Controls - Press button for tape radio and $\mathbf{P}$ U Siders for volume, bass ( $* 12 \mathrm{~dB}$ to -14 dB at 100 Hz ) treble ( -11 dB to -12 dB at 10 KHz )

## Project 80 FM tuner



Making the Project 80 F.M. tuner and decoder available separately gives wider chorce of systems and saves money where stereo reception may not be required. The tuner is a triumph of electronic design and assures excellent performance. The decoder gives a 40 dB channel separation with 150 mV output per channel. Both units may be used with other than Project 80 systems.
TECHNICAL SPECIFICATIONS OF TUNER
Size $-85 \times 50 \times 20 \mathrm{~mm}\left(3 \frac{1}{2} \times 2 \times 1 \mathrm{~ns}\right)$
Tuning range -87.5 to 108 MHz
Detector-I.C. balanced cancidence for good A.M. rejection
One I.C. equal to 26 transistors
Distortion $-0.2 \%$ at 1 KHz for $30 \%$ modulatıon
4 pole ceramic filter in I.F. section
Aerial impedance-75 $\Omega$ or 240-300 $\Omega$
Sensitivity - 4 microvolts for 30 dB quieting
Output - 300 mV for $30 \%$ modulation
Power requirements -23 to 33 volts
DECODER
One 19 transistor I.C.

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Input sensitivity -100 mV
Output - 15 watts RMS coninuous imo $8 \Omega$ ( 35 v )
Frequency response $-10 \mathrm{~Hz} \quad 100 \mathrm{KHz}=1 \mathrm{~dB}$
Signal/noise ratio -64 dB
Distortion - at 10 wattsinto $8 \Omega$ less than $01 \%$
Power requirements - 12 to 35 volts
Z. 60 TECHNICAL SPECIFICATIONS

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Input sensitivity $-100 \cdot 250 \mathrm{mV}$
Output - 25 watts RMS continuous into $8 \Omega(45 \mathrm{~V})$.
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Signal/noise ratio - better than 70 dB
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$160 \mathrm{~V}: 0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 2 \not 2 \mathrm{p}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 3 \nmid \mathrm{p} .0 .1 \mu \mathrm{~F}, 0.15 \mu \mathrm{~F}, 4 t \mathrm{p}$. $0.22 \mu \mathrm{~F}, 5_{p, 0} \cdot 33 \mu \mathrm{~F}, 6 \mathrm{p} \cdot 0 \cdot 47 \mu \mathrm{~F}, 7 \ddagger \mathrm{p}, 0.68 \mu \mathrm{~F}, 11 \mathrm{p} .1 \mu \mathrm{~F}, 12 \nmid \mathrm{p}$.
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| CF-High |  |  |  |  |  |  |  |  |
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| H. | CF | 22.1 M | 0.8 | 0.65 | 0.62 | 0.55 | 0.5 | 0.45 |


|  | C | 22-1M | 1 | 0.8 | $0 \cdot 65$ | $0 \cdot 62$ | $0 \cdot 55$ | $0 \cdot 5$ | 0.45 | $2 \cdot 4 \times$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | CF | 22-2M2 | 1 | 0.8 | $0 \cdot 65$ | 0.62 | 0.55 | 0.5 | 0.45 | $3.9 \times 10$ |
|  | CF | 22.1M | , | $0 \cdot 8$ | 0.65 | 0.62 | 0.55 | 0.5 | 0.45 | $5 \cdot 5 \times 16$ |
|  | MF | 10.2 M 7 | , | 0.9 | 0.8 | 0.7 | 0.65 | 0.65 | 0.6 | $3 \times 7$ |
|  | MF | 10.2 M 2 |  | 0.9 | 0.8 | 0.7 | 0.65 | 0.65 | 0.6 | $4.2 \times 10$ |
|  | MF | 10.10 M | $1 \cdot 5$ | $1 \cdot 25$ | 1. 25 | 1.1 | , | 0.95 | 0.88 | $6 \cdot 6 \times 13$ |
| 2 | MF | $10+10 \mathrm{M}$ | 3 | $2 \cdot 5$ | $2 \cdot 5$ | 2 | 1.75 | 1.75 | 1.6 | $8 \times 17 \cdot 5$ |

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| 1.0رF | 63 V | 6 p | $68 \mu \mathrm{~F}$ | 16V 6p |
| 1. $5 \mu \mathrm{~F}$ | 63 V | 6p | $68 \mu \mathrm{~F}$ | 63V 12p |
| 2. $2 . \mu \mathrm{F}$ | 63 V | 6 p | $100 \mu \mathrm{~F}$ | 10V 6p |
| 3-3 $\mu \mathrm{F}$ | 63 V | $6 p$ | 100 LF | 25V 6p |
| $4 \cdot 0 \mu \mathrm{~F}$ | 40 V | 6p | $100 \mu \mathrm{~F}$ | 63V14p |
| 4.7 $\mu \mathrm{F}$ | 63 V | 6 p | $150 \mu \mathrm{~F}$ | 16V 6p |
| 6.8 2 FF | 63 V | 6 p | $150 \mu \mathrm{~F}$ | 63 V 15 p |
| 8. $0 \mu \mathrm{~F}$ | 40 V | 6 p | $220 \mu \mathrm{~F}$ | $6.4 \vee 6 p$ |
| $10 \mu \mathrm{~F}$ | 16 V | 6 p | $220 \mu \mathrm{~F}$ | 10V 6p |
| $10 \mu \mathrm{~F}$ | 25 V | 6 p | 220 F | 16V 8p |
| $10 \mu \mathrm{~F}$ | 63 V | 6p | $220 \mu \mathrm{~F}$ | 63 V 21 p |
| $15 \mu \mathrm{~F}$ | 16 V | 6p | 330 LF | 16V12p |
| $15 \mu \mathrm{~F}$ | 63 V | 6p | $330 \mu \mathrm{~F}$ | 63 V 25 p |
| $16 \mu \mathrm{~F}$ | 40 V | 6p | $470 \mu \mathrm{~F}$ | $6.4 \vee 9 p$ |
| $22 \mu \mathrm{~F}$ | 25 V | 6p | $470 \mu \mathrm{~F}$ | 40V 20p |
| $22 \mu \mathrm{~F}$ | 63 V | 6 p | 680 4 F | 16 V 15 p |
| $32 \mu \mathrm{~F}$ | 10 V | 6p | $680 \mu \mathrm{~F}$ | 40V 25p |
| $33 \mu \mathrm{~F}$ | 16 V | 6p | $1000 \mu \mathrm{~F}$ | $16 \vee 20 p$ |
| $33 \mu \mathrm{~F}$ | 40 V | 6p | $1000 \mu \mathrm{~F}$ | 25V 25p |
| $32 \mu \mathrm{~F}$ | 63 V | 6 p | $1500 \mu \mathrm{~F}$ | $6.415 p$ |
| $47 \mu \mathrm{~F}$ | 10 V | 6p | $1500 \mu \mathrm{~F}$ | 16V25p |
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| :---: | :---: | :---: | :---: |
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