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VOI. 49 NO. 11 ISSUE 805 **MARCH 1974**

BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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IKE many other magazines and paper products "Practical Wireless" has become victim of a world paper shortage resulting in massive increases in the cost of raw materials. In order to maintain the high standard of providing technical information and projects to our readers, we regret that we have been compelled to increase the cover price to 25p.

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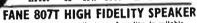
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lef, VA Weight Size cm. P & P Ref. Na. 07 149 150 151 152 153 154 155 156 VA (Watts) 20 60 100 200 250 350 500 750 1000 2000 Weight) 16 oz 1 8 3 12 5 8 0 13 12 15 0 19 8 29 0 38 0 60 0 7-0 × 6-0 × 6-0 9-9 × 7-7 × 8-6 9-9 × 8-9 × 8-6 12-1 × 9-3 × 10-2 12-1 × 11-8 × 10-2 14-0 × 10-8 × 11-8 17-2 × 14-0 × 14-0 17-2 × 14-0 × 14-0 17-2 × 15-5 × 18-1 2-32 3-45 3-79 6-45 8-41 11-22 16-25 22-10 29-87 49-25 36 52 52 67 82



Ref.	VA			AUI	ГС	TR	A	NSF	ORME	RS			
	(Watts)		ight			Size	c	m.	1	luto	Taps	P	& P
113	20	í	0	5.0		5.1	-	4.6	0-115-		240	. £	P
64	75	2	4	7.4	×	6.7	×	6-1				1 · 22 2 · 40	22
.4	150	3	4	8 9	×	7.7				200-	220-240	2.89	36
66	300 500	6	4	9 9				8.6				5.63	52
84	1000	19	8	14.0		11.2		10.2		9	••	8.36	67
84 93 95 73	500	30	2			13.4	×	14.3	**		••	15-19	82
95	2000	32	o	17-2	2	16.6	Č	14.0	••		••	21.99 28.70	-
73	3000	40_	0	21.6	×	13.4	×	18-1	**			39.17	
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		_						N JUM X 4	40.44	-
Ref.	Amps.	W	/eigh	t	Size en	30	VOLT Seconda	RANGE		& P
No.		14	47	7.	A. A. C. M.		occoria.	ry rops		αr
1.12	0.5	10		2041247000		100-2003			£.	D
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79	1.0	2	4	7.0 ×	6.7 ×	6.1			1.92	24
3	2.0	3		0.0	7.7	7.7	**	**		30
20	2.0	- 5	7	0 7 8	/ / X	11	**	••	2.90	36
20	3.0	-	8	9.9 X	8 3 ×	8.6	122	11	3.58	47
2.1	4.0	6	- 4	9.9 x	96 x	8.6	. 92		4.25	52
51	5.0	6	12	12-1 -	0.6	10.5	170	**		32
117	6.0	0	0	12 1 2	0 0 x	10.2	**	19	5 30	52
00	6 0	- 65	0	12 1 ×	9.3 ×	10.2	5.5	20	6.31	52
88	8.0	12	.0	12 1 x	11.8 x	10.2		11.500	8.18	47
89	19.0	13	12	140 -	10.2 -	11.0				0/
									10.33	

	949993	100							TRANG	E	
Ref.	Amps.	W	eight			Size cm		Seconda	ry Tabs	P	R P
No.		ь	oz						,		
102	0.5	1	12	7.0	*	6.4 v	6-1	0.19.25	33-40-50V	1 00	20
103	1.0	2	12	0.3	8	7		0-17-23-	33-40-30 4		30
	2 0	-	1.5	0.3	×	/ 4 X	7.0	10	**	2.80	36
104	2.0	5	- 8	9.9	×	8.9 x	8.6		**	3.87	43
105	3.0	6	12	9.9	v	10.2 -	0.6		**	5.26	74
106	4.0	10	0	12.1	0	10 5	100	**	11		52
	7.0	10	U	12.1	×	10.2 X	10.5	**	**	6.99	52
107	6:0	12	0	14:0	×	10.2 x	11.8	11		10.35	67
118	8.0	18	0	140		13.7 -	11.0	**	**	10.33	07
110	10.0	25	ŏ.	17 3	•	12.0	11.0	**	**	13.51	97
117	10.0	43	U	11.7	×	12:7 ×	14.0	• • •		16.93	•
							- 6	0 VOLT	RANGI	_	

Ref.	Amps.	We	ght	Size c	m.		Second	ary Tat	s P	2 1
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124	0.5	2 .	4 7-0	× 6-	7 ×	6-1	0-24-30	40_428	-69C I ∙93	- 22
126	1-0	3 .	4 8 9	× 7	7 ×	7.7			2.70	30
127	2-0	6	4 9.0	. 0		8-6		* **		36
125	2.0	0 1	12.1	2 9	5 X		1990	(600)	4-25	47
123	3 0				, ×	10.2		**	6.46	52
123	4.0	13 1	2 12 1	x III I	x B	10.2	1930		8.36	67
40	5 0	12 00	14 0	k 10 -	2 ×	11.8	100	200	9 85	87
120	6.0	15 8	140	x 12-1	×	11.8	- 33 -	- 27	12.14	02
121	8.0	25 00		14-7	×	11.8		**	12.46	04
122	10.0	25 0		12 2	, 0	14.0	**	**	13.65	- 3
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20	6.0 15		14-0	× 12-	8-11×1		12:14	82	
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22	10.0 25	0	17-2	x 12	7 x 14.0		20.09		
89	12.0 29	00	17 - 2	x 14 0	× 14-0	22	22.49	- 1	
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20	MINIAI	UKI	TH	ANS	ORME	RS WITH SCRE	ENSP	& P	
ef. 38	MA,	AA.	ight	Siz	e cm	VOLTS	E		
38	200		2		·6×2 ·0	3-0-3	1 31	10	
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35	330,330		4	4 . 8 x 2	9×3-5	0-9, 0-9		10	
07	500, 500	- 1	00	6.1.5	4×4 · 8		1-52	10	
80	IA, IA	- 11			4x6 -1	0-8-9, 0-8-9	2.03	22	
36	200, 200		14			0-8-9,0-8-9	2 73	30	
14			*		9x3 · 5	0-15, 0-15	1-52	10	
	300, 300		4		8×4 8	0-20, 0-20	1.60	22	
21	700 (D.C.)		8	7 · 0×6	1×6·1	20-12-0-12-20	1.41	30	
06	IA, IA	2	12	8 · 3×7	-7×7·0	0-15-20, 0-15-20	3.08	36	
03	500, 500	2			0x7·0	0-15-27, 0-15-27	2.82		
04	IA. IA	3			·7×7·7	0-15-27, 0-15-27		38	
				0 ///	/ ~ / · /	U-13-2/, U-13-2/	2.86	38	

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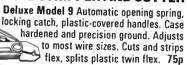
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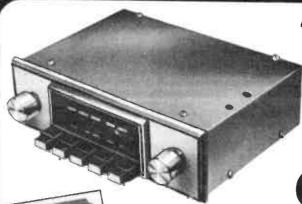
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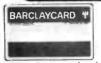


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Huge 19 14 (approx.) high

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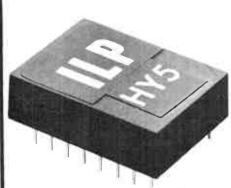
TOTAL HARMONIC DISTORTION: SIGNAL/NOISE RATIO: FREQUENCY RESPONSE: SUPPLY VOLTAGE: SIZE:

25 watts RMS, 50 watts peak music power 4-16Ω Into 8Ω Odb (0.775 volts RMS) 47KΩ

Less than 0.1% at 25 watts typically 0.05 better than 75db 10Hz-50KHz ± 1db + 25 voits 105 x 50 x 25 mm

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Overall size is resucced by the use of a list in the control of the earlier device.

When combined with the HY50 & power supply only potentiometers are required to complete a simple mono amplifier with input & output facilities expected to be found on Hi-Fi amplifiers.

The combination of two HY5's two HY50's sharing a common power supply (PSU50) are linked by a balance control to form a complete stereo system.

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Ceramic Pick-up up 10 3mV
Microphone 10mV
Tuner 250mV
Auxiliary 3-100mV
Input Impedance 47kΩ 1kHz

OUTPUTS Tape 100mV. Main output, Odb (0:775voits)

ACTIVE TONE CONTROLS ACTIVE TONE CONTROLS
Treble ± 120b at 10Mt.
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SUPPLY CURRENT 15mA
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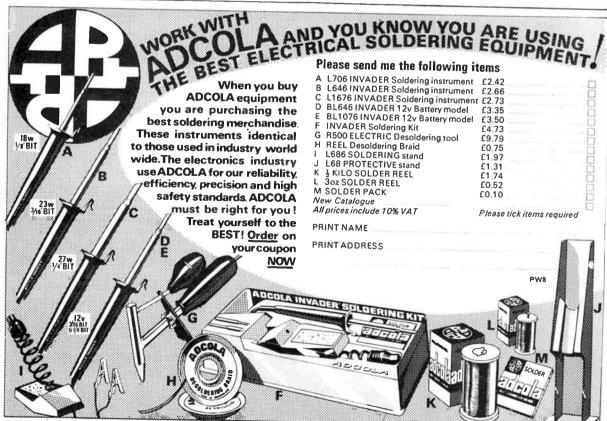
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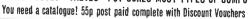


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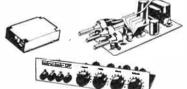
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BC107	15p	BFY64	45p	QA81	10p	T1P29A		2N3054	45p	40408	50p
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B05/40	400v	25 p	
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	dla.		1 1
	1. V.		1 1
		0.5 -	
B1/05	50v	25 p	
B1/10	100v	25 p	
B1/20	200v	28p	
B1/60	600v	30p	
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1 AMP P.	I.V.		
W005	50v	29p	TR1
W01	100v	30p	101/
W02	200v	32p	1111
W06	500v		1111
		35 p	
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2 AMPS P	.1.V.		
B2/05	50v	35 p	1 1
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B2/20	200v	45p	1 1
B2/60	600v	50p	1
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č	3 4	4 · 7-10M	1.5	1 · 2	0.9 nett
Č	1	4 · 7-10M	3 . 2	2 - 5	1 · 9 nett
MO	1/2	10-1M	4	3.3	2·3 nett
ww	1	0.22-3.9	9	9	2
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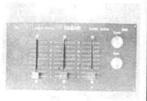
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Z608..23 off BC148. 2 BC158. Z612..12 off ME4102. 2 BC251B. 1 BFY50.

CRYSTAL CALIBRATOR (Second Hand) No. 10 crystal controlled heterodyne wave-meter covering 500KHz-10MHz (harmonics up to 30MHz) power required 300V DC 15mA. 12V 0·3A DC. Test equipment for 62T M/RC. £2·50 each. WIRE-WOUND RESISTORS. Our selection of mixed Ohms and Watts. 25 for £1-50, 50 for £2-50, parcel of 1,000 £30.00.

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- * 4 Transistor Earpiece Radio.
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- 7 Transistor Loudspeaker Radio MW/LW
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Components Include: 24 Resistors ● 21 Capacitors ● 10 Transistors ● 3¼" Loudspeaker ● Earpiece ● Mica Baseboard ● 3 12-way connectors ● 2 Volume controls ● 2 Slider Switches ● 1 Tuning Condenser ● 3 Knobs ● Ready Wound MW/LW/SW Coils ● Ferrite Rod ● 6½ yards of wire ● 1 Yard of sleeving etc. ● Parts Price List and Plans 50p. (Free with parts).

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WITH V.H.F. INCLUDING AIRCRAFT



Nine Transistors, 9 Tuncable wavebands as Roamer Ten Built in ferrite rod aerial for MW/LW. Retractable chrome-plated telescopic aerial for VHF and SW. Push Pull output using 600 mW transistors. 9 Transistors and 3 diodes, tuning condenser with V.H.F. section, separate coil for aircraft, moving coil loudspacker, volume ON/OFF and wavechange controls. Attractive all white case with red grille and carrying strap. 81c. 94" x 7" x 21" approx. Parts Price List and Plans 30p (Free with parts).

Total Building Costs

£6-95 (+ 10% VAT 69p) P P & Ins. 44b (Overseas P & P £1-85)

POCKET FIVE

3 Tunable wavebands, M. W. L.W. and Trawler Band, 7 stages, 5 transistors and 2 dodes, supergensitive ferrite rod aerial, moving coil Total Building Costs builspeaker, attractive black and gold case. Size 5½" × 1½" × 3½" approx. Plans and Paris. 7½" × 15% (* 10% VAT 22p)



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Wavebands, transistors and wavebands, transistors and speaker as Pocket Five. Larger Case with Red Speaker Grille and Tuning Dial. Plans and Parts Price List 15p (Free with parts).

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NEW Everyday Series

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E.V.6. Case and looks as above. 6 Transistors and 3 dlodes. Powered by 9 volt battery. Ferrite rod aerial, 3' londspacker, etc., MVLW coverage. Push Pull output. Parts Price List and Plans 15p. Free with parts.

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E.V.7. Case and looks as above. 7 Transistors and 3 diodes. Six wavebands. MW/LW, Trawler Band, SW1. SW2, SW2, powered by 9 volt battery. Push Pull output. Telescopic aerial for short waves. 3" Loudspeaker. Parts Price List and Easy Build Plans 20p. Free with parts. Overseas P & P £1:05.

Total Building £4.08

P P & Ins. 31p Overseas P & P £1-85 (+ 10% VAT 40p)

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ROAMER EIGHT Mk I

NOW WITH VARIABLE TONE CONTROL

TONE CONTROL

7 Tunable Wavebands: MW1.
MW2, I.W. 8W1, SW2, SW3
and Trawier Band. Built in
Ferrite Rod Aerial for MW and
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Car aerial and Tape record sockets. Selectivity switch
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case in rich chestrut shade with gold blocking. Size 9 × 7 ×
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WITH VHF INCLUD-ING AIRORAFT

10 Transistors. Latest 4 2 watt Ferrite Magnet Loudspeakers. 9 Tunable Wavebands, MW1, MW2, LW, SW1, SW2, SW3, Trawler Band, VHF and Local Stations also Aircraft Band.



Built in Ferrite Rod Aerial for MW/LW. Retractable, chrome plated 7 section Telescopic Aerial, can be augled and rotated for peak short wave and VHF listening, Push Pull output using 600mW Transistors, Car Aerial and Tape Record Bockets. 10 Transistors plus 3 Diodes, Ganged Tuning Condenser with VHF section. Separate coil for Aircraft Hand, Volume m/n/n, Wave Change and tone Controls, Attractive Case in black with silver blocking, Size 9°× 7" × 4". Easy to follow instructions and diagrams. Parts price list and plans 30p (FREE with parts). parts).

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Components include:

Components include:
Tuning Condenser: 2 Volume Controls: 2 Slider Switches:
Fine Tone 3" Moving Voll Speaker: Terminal Strip: Ferrite
Rod Aerial: 2 Plugs and Sockets: Battery Clips: 4 Tag
Boards: 10 Translstors: 4 Diodes: Resistors: Capacitors:
Three 4" Knobs. Units once constructed are detachable
from Master Unit, enabling them to be stored for future
use. Ideal for Schools. Educational Authorities and all
those interested in radio construction.

those interested in radio construction. Parts price list and plans 25p (FREE with parts).

Total building **£5-50** PP & Ins. 33p (Overseas P & P£1-85)

4 169 FAT 53pr

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8 Tunable Wavebands: MW, LW, 8Wl, 8W2, 8W3 and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves. 3In. Speaker, 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with polished metal inserts.

Strag W, AJ, 2 Min. approx. Push-and.

black knobs with pointed nietar interts. Size 9 × 5½ × 2½in, approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and plans 25p (FREE with parts).

£4.48 PP& Ins. 33p

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ROAMER SIX

CASE AND LOOKS AS TRANS-EIGHT

Trawler band plus an extra Medium waveband for easier tuning of Luxembourg, ctc. Sensitive ferrite rod aerial and telescopic aerial for Short Waves. 3in. Speaker's stages—6 transistors and 2 diodes. Attractive black case with red grille, dial and black knobs with polished metal inserts. Size 9 × 9 k × 21m. approx. Plans and parts price list 25p (FREE with parts).

Costs

43 Page 14 Line Vaves. 3in. Speaker's 10 Costs

Total building 25 very 1 costs 25p (Overseas). Total costs 25p (EREE with parts).

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DYNAMIC MICROPHONES B1223. 200 ohms plus on/off switch and 2.5mm and 3.5mm pluss £1.60

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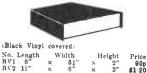
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CAR STEREO SPEAKERS (Angled) 23.85 per pair.

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BAI	51"	×	21"	×	11"	42p
BA2	4"	×	4"	×	11"	41p
BAS	4"	30	21"	×	14"	41p
BA4	51"	×	4"	×	11"	47p
BA5	4"	×	24"	×	2"	41p
BA6	3"	ж	2"	×	1"	34p
BA7	7"	×	5"	×	21"	66p
BA8	8"	×	6"	×	3"	84p
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104 For model CN240 3/16"	38
1100 For model CCN240 3/32"	88
1101 For model CCN240 3/8-	88
1102 For model CCN240 4"	38
1020 For model G240 3/32"	38
1021 For model G240 1/8"	38
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Pack No. Otv.

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18 BALDOCK ST., WARE, Herts. (A10)

C2 200 Capacitors mixed values application by weight C3 50 Precision Resistors 1 %	0.55 0.55
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C4 75 ith W Resistors mixed preferre	d 0-88
C5 5 Pieces assorted Ferrite Rods (0.55
72	0.55
C7 1 Pack Wire 60 metres assor	
C 8 10 Reed Switches	-55
C 9 3 Micro Switches	55
014 15	55
C11 5 Jack Sockets 3 × 3-5m 2 >	55
C12 40 Paper Condensers preferred	55
C13 20 Electrolytics Trans, types 0	55
C14 1 Pack amorted Hardware	55
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C20 4 Sheets Copper Laminate	00
approx. 10" × 7" 0	-55

Ref. J. Tape Head Cleaning Kit 51p Ref. 34. Cassette Case \$1.27 Ref. 56. Hi-Fi Stereo Hints & Tips 32p

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SOCKETS		
P8 35 DIN	2 Pin (Speaker)	0.0
PS 36 DIN	3 Pin	0.10
PS 37 DIN	5 Pin 180°	0.1
PS 38 DIN	5 Pin 240°	0 1
PS 39	Jack 2-5mm Switched	0.0
PS 40	Jack 3-5mm Bwitched	0.1
PS 41	Jack 1" Switched	0.1
PS 42	Jack Stereo Switched	0 2
PS 43	Phono Single	0.0
PS 44	Phono Double	0.10
PS 45	Car Aerial	0.0
PS 46	Co-Axial Burface	0.01
P8 47	Co-Axial Flush	0.1

P8 47	Co-Axial Flush	0.14
INLI	NE SOCKETS	
PS 21	D.I.N. 2 Pin (Speaker)	0 13
P8 22	D.I.N. 3 Pin	0.17
PS 23	D.I.N. 5 Pin 180°	0.17
P8 24	D.I.N. 5 Pln 240°	0.17
PS 25	Jack 2-5mm Plastic	0.10
PS 26	Jack 3-5mm Plantic	0.19
PS 27	Jack 1" Plastic	0 24
PS 28	Jack 1" Screened	0.28
PS 29	Jack Stereo Plantic	0.22
PS 30	Jack Stereo Screened	0.82
PS 31	Phono Screened	0.14
PS 32	Car Aerial	0.18
P8 33	Co-Axial	0.17
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PLU	SS	
P8 1	D.I.N. 2 Plu (Speaker)	0-11
PS 2	D.I.N. 3 Pin	0.12
PS 3	D.I.N. 4 Pln	0.15
P8 4	D.I.N. 5 Pin 180*	0.14
P8 5	D.I.N. 5 Pin 240°	0.15
P8 6	D.I.N. 6 Pin	0.15
P8 7	8.I.N. 7 Pin	0.15
P8 8	Jack 2-5mm Screened	0.10
P8 9	Jack 3-5mm Plastle	0.09
PS 10	Jack 3-5mm Screened	0.12
PS 11	Jack ‡" Plastic	0.13
PS 12	Jack 1" Screened	0.18
PS 13	Jack Stereo Screened	0.29
PS 14	Phono	0.06
PS 15	Car Aeriai	0.15
PS 16	Co-Axial	0.10

i	C	٩B	LES	
	CP	1	Single Lapped Screen	0.0
1	CP	2	Twin Common Screen	0.0
ĺ	CP	3	Stereo Screened	0-0
ì	CP	4	Four Core Common Bereen	0.2
ı	CP	5	Four Core Individually Screened	0.8
ı	CP	6	Microphone Fully Braided Cable	0.1
ı	CP	7	Three Core Mains Cable	0.0
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١	CP	10	Low Loss Co-Axial	0.1
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8 Books comprising
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RPR	Sound and Loudspeaker Manual	50p
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Reactance-Frequency Chart for Audio & RF use 15p Resistor Colour Code Disc Calculator 10p

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ACOS GP91-18C, 200mV at 1-2cms/s	ro #1-16
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ACOS GP96-1, 100mV at 1cm/sec	42-65
TTC J-2005. Crystal/Hi Output	95p
TTC J-20 10C Crystal/Hi Output Com	patible 41-10
TTC J-200 CS Stereo/Hi Output	41-60
TTC J-2105 Ceramis/Med. Output	41.64

CARBON FILM RESISTORS

The E12 Range of Carbon Film Resistors, 1/8th watt available in PAKS of 50 pieces, assorted into the following groups:— R1 50 Mixed 100 ohms-820 ohms 40p R2 50 Mixed 1K ohms-8-2K ohms 40p R3 50 Mixed 10K ohms-82K ohms 40p R4 50 Mixed 100K ohms-1 Meg. ohns 40p THESE ARE UNBEATABLE PRICES-LESS THAN 1p EACH INCL. V.A.T.

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LOW - NOISE CASSETTES C60. 32p C90, 41p C120, 82n

-the lowest prices

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AL10/AL20/AL30 AUDIO AMPLIFIER MODULES



The AL10, AL20 and AL20 units ar-similar in their appearance and in their general specification. However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 warts R.M.S. The versatility of their design makes them ideal for use in record players, tape recorders, sterro amplifiers and casette and cartridge tape players in the car and at home.

Parameter	Conditions	Performance
HARMONIC DISTORTION	Po 3 WATTS (1KHz	0·25°,
LOAD IMPEDANCE		× 16 Ω
INPUT IMPEDANCE	f=1KHz	100 k Ω
PREQUENCY RESPONSE Œ 34B	Po 2 WATTS	50 Hz 25KH:
SENSITIVITY for B VYEU O/P	Vs. 25V RI 8Ω t 1KHz	75mV, RM8
DIMENSIONS		3" > 24" - 1"

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the difference in their working conditions.

Parameter	AL10	AL20	AL80
Maximum Supply Voltage	25	30	30
Power output for 2%, T.H.D. (RL 8Ωt 1 KHz)	3 watts RMS Min	5 watts RMS Min	10 watts RMS Min

AUDIO AMPLIFIER

MOD	ULES		
VL 10	3 watts	RMS	£2 19
AL 20.	5 watts	RMS	£2-59
AL 30.	10 watts	RMS	£3.01

POWER SUPPLIES

POWER SUFFEIL

P8 12. (Use with ALLO & AL20) 88p

8PM 80. (Use with also AL30 & AL50)

£3 25 FRONT PANELS SP 12 with knob

PRE-AMPLIFIERS

PA 12. (Csc with A440 & A420) \$4:35 PA 100 (Use with A430 & A450) \$18:15

TRANSFORMERS

T461 (Use with AL10) £1-38 P & P (5p T538 (Use with AL20) £1-93 P & P 15p BMT80 (Use with AL30 & AL50) £2-15

PA 12. PRE-AMPLIFIER SPECIFICATION

The PA 12 pre-amplifier has been designed to match Into Frequency response most budget sterro systems. It is compatible with the 20Hz 50KHz (3dB) AL 10, AL 20 and AL 30 and/o power amplifiers and it can be supplied from their associated power supplies. There are two stereo liquits, one has been designed for use with "Ceramic cartridges while the auxiliary input will suit most †Magnetic vartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/oil switch, balance, base and treble 81ze 152mm × 84mm - 35mm.

2012 50KH24 3dB)
Bass control
± 12dB at 60H2
Treble control
± 4dB at 14KH2
*Input 1. Impedance
1 Meg. ohin
Sensitivity 300mV
†Imput 2. Impedance
30 K ohins

30 K ohus Sensitivity 4mV

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The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and test-on a one-piece chassis measuring 20 cm + 14 cm + 5.5 cm. This compact unit comes complete with on/off switch volume control, balance, base and treble controls. volume control, balance, base and treble contransformer, Power singly and Power ange. Attractively printed front panel and matching control knobs. The 'Sherce 20' has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively, into a separate cabinet. Output power 20w peak. Input 1 (Cer.) 300mV into 1M. Freq. res. 2511z-25kHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Base control ± 12dB at 40ffz typically 0.25%, at 1 watt. Treble con. ± 14dB at 14kHz.

50W pk 25w (RMS)

0.1% DISTORTION! HI-FI AUDIO AMPLIFIER

THE AL50

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SAVE MONE

So the winter's economic crunch has come as most realistic prophets have forecast. We have read, heard, seen and experienced at first hand some of the revivals of the immediate post-war social and economic problems, not forgetting that dreaded winter of 1947. We do not intend here to rub the salt further into the wound but rather to look at ways and means of

making our lives just a little more bearable.

Practical Wireless showed foresight in the autumn of 1973 which paid off. The power crises ever looming in our midst, we grabbed at the expected misfortunes in the electricity supply industry by publishing at the right time an emergency lighting unit to operate from a car battery. This proved so popular that we are now short of copies for office use. For those of you who missed it we publish in this issue a slightly different version (suggested by a P.W. reader) that uses a ready-made oscillator coil.

If you have thoughts about visiting the SONEX or other hi-fi exhibitions in the vicinity of London Airport in March, but are seriously wondering where the money to buy is going to come from, because of the Chancellor's mini-budget restrictions, again take a crumb of comfort from P.W. For less than a pound you can have not only the widest variety of do-it-yourself designs over the next three months, but also the freedom to control your own spending over whatever period you choose. You can purchase components and build your own equipment at leisure without worrying about interest charges.

This month's issue sees the start of a new hi-fi project with a difference. We do not recall ever seeing a similar project before in a magazine that incorporates a cassette recorder. We could then be justified in claiming yet another first for the do-it-yourselfer. The result is that you can save on the cost of a system for the home that gives you a.m. and f.m. radio, tape record/playback, the playing of pre-recorded cassettes, and with an added pick-up you can play back stereo discs. This quality system is in stereo and the cassette machine is left to your choice to suit your requirements and, most important, your pocket. If you are seriously interested in quadraphonic sound there is ample room in the unit to include a second pair of amplifiers and an uprated mains transformer.

If you have your own hi-fi set-up already, but you could do with a useful piece of test gear to help you set it up or locate some of those obscure faults, you will be interested in the Trouble Tracer that we published in the last two issues and the

Waveform Generator in this issue.

Finally, most of you will already be hooked on our P.W. Datacard system; numbers 7 and 8 in this issue are specially designed for those who require "finger-tip" information on local reception and guidance on aerial installations.

M. A. COLWELL-Editor.

The April issue will include a new unique portable 5-band radio receiver; a "short-wipe" unit for clearing April showers from your car windscreen; an article that explains impedance matching in audio equipment; a special tool kit arranged by Practical Wireless for its readers at a favourable price. Cut your costs again—order the April issue of P.W. now. See the footnote and further details on page 1075.

NEWS...

IMPORTANT MESSAGE TO ALL READERS

Readers of "Practical Wireless" and most other magazines will be aware of the restrictions imposed by the Government and as a result of Trades Union action in various industries. To ensure that you receive your copy of "Practical Wireless" at the earliest possible date, we have to rely on effective communications and delivery through the post and by railway. We also depend on the operation of electrical equipment and printing machinery. Petrol and diesel oil are vital to the needs of our job in quick and effective processing of editorial and advertising material.

We are sure that you will understand the many problems that confront all of us. We therefore request your patience and understanding during any temporary period when publication may be delayed.

We regret that due to the effects of the current industrial situation, the number of pages in this issue has had to be limited. We apologise to advertisers who were unable to insert their full allocation of product announcements and to those unable to appear at all in this issue. Such is the "pulling-power" of Practical Wireless and its advertisements that we recommend booking early for the next available issue.

Plessey IC book

LESSEY Semiconductors has produced a comprehensive 235-page Databook giving details of its extensive range of silicon integrated circuits.

Continuous emphasis on the development of processes and circuits by Plessey has been demonstrated by the successful intro-duction of Bipolar Process III circuits and MNOS electricallyalterable non-volatile memories. The first products from these new processes are detailed in the Databook along with the wide range of both special and standard products currently available.

Copies of the Integrated Circuit Databook are available on application to Plessey Semiconductors Limited, Cheney Manor, Swindon, Wiltshire.

Sonex rival

I-FIDELITY '74 is a rival exhibition which will run concurrently with Sonex at the Heathrow Hotel. More details next month.

NEWS...

NEWS...

NEWS...

ISB for broadcast radio?

ORK on the problems of a.m. broadcasting on medium and long waves has been carried out at Siemens laboratories in West Germany. The independent sideband (ISB) system, proposed by the Hamburg Institute of Radio Engineering is being seriously considered to overcome some of the problems of increasing mutual interference.

Siemens engineers are quick to point out that the review of broadcasting frequency allocation, due within the next eighteen months, should recommend ISB to enable expansion up to double the number of programme channels for the same number of transmitters. An added advantage is that ISB offers the equivalent to SSB in terms of interference, bandwidth and fading, and could be implemented locally without the need for international agreement.

The major drawback is that receiver design will have to be altered so that a phase shift network can be employed for the 150 to 4kHz band to separate the two side-bands by at least 40dB. ISB receivers would be capable of processing signals in the SSB and DSB modes, with improved reception on DSB by listener selection. Transmitters would probably handle signals with the dynamic range reduced by 30dB.

Modules and valves

T a recent visit to the huge Mullard manufacturing complex at Blackburn recently, we were privileged to see the making of those "liquorice allsorts" coloured capacitors that are now familiar on printed circuit assemblies. Readers will also be pleased to learn that valves, mostly for television, are still being made in millions although the range of types has been rationalised to fit the economic needs of setmakers and servicemen.

We also saw the assembly of Mullard modules: the LP1185 f.m. i.f. strip; LP1186 d.c. voltage controlled tuner for Band II; LP1159 a.m. i.f. strip; LP1162 4 watt amplifier; LP1164/1 r.f./i.f. amplifier for a.m./f.m. radio; LP1402 f.m. tuner with capacitor tuning. Mullard are working on a modular design stereo decoder for release soon.

Our picture here shows the polyester foil type capacitor going through the colour code dip painting process. These are only a few of the vast activities on this 46 acre site employing approximately 4,000 people.

Torbay A.R.S.

HE Torbay Amateur Radio Society, G3NJA, has produced its first magazine. One of the main features is that of v.h.f./u.h.f. conversions of commercial equipment for the Amateur. This has been written by E. Hayman, G3ABU.

The T.A.R.S. are willing to add any readers' names to their magazine mailing list. Alternatively readers may become Associate Members for the sum of 50p annual subscription. They would then receive a free copy.

The magazine will be produced on alternate months and further gen may be obtained by sending a s.a.e. to Frederick J. E. Bolton, G3VTQ, Top Flat, 23 Waverley Road, Newton Abbot, Devon.

Rad<mark>ar pio</mark>neer dies

SIR Robert Watson-Watt, C.B., F.R.S. died on 5th December at the age of 81. Sir Robert will be one of those famous names in the U.K. associated with great electronic inventions and in his case radar.

Early in his career he worked on the use of radio to detect thunderstorms. Radio direction finding found fame for him in World War II. Civil applications include airlines and shipping; a fitting tribute being the recently opened computer assisted radar tower and communications system for shipping within a 20 mile range of Liverpool.

The communications system was installed by Decca Radar Limited.



A Versatile WAVEFORM GENERATOR

J. B. DANCE M. Sc

THE Signetics NE566 integrated circuit function generator can be used to construct a simple unit which will provide a variety of waveforms over a very wide frequency range.

The prototype unit will be described in detail. However, a number of variations will be discussed so that individual readers can make modifications which may make the unit more useful for their own particular purposes.

The basic waveform generator produces triangular waves and square waves, and it is especially suitable for use in audio amplifier testing. An additional circuit can be used to produce sine waves in addition to the other two waveforms. The circuit can be modified to produce rising or falling waveforms of high linearity instead of the triangular waveforms. In this case short rectangular pulses are available at the output which previously provided square waves.

THE BASIC CIRCUIT

The circuit of the basic function generator is shown in Fig. 1. The voltage at the slider of VR1 is applied to pin 5 of the NE566V and also pin 6 via C1. The

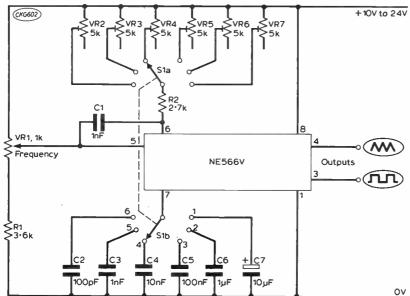
current passing to this latter pin is determined by the value of the voltage at this pin and by the resistance between it and the positive line. This current is used to charge and discharge the capacitor selected by S1b.

A Beckman 'Helipot' precision ten-turn helical potentiometer is employed for VR1 together with a Beckman turns counting dial; this enables the frequency of oscillation to be set reasonably accurately. The value of R1 has been chosen so that the potential at pin 5 never falls below three-quarters of the positive power supply line potential (as recommended by the manufacturers of the integrated circuit).

The frequency of oscillation is proportional to the voltage between the positive power supply line and pin 5; this voltage is in turn proportional to the resistance of VR1 between the positive line and the slider. In the circuit of Fig. 1, the frequency of oscillation is set to 10Hz, 100Hz, 1kHz, 10kHz, 100kHz



▲ The finished waveform generator with its direct reading dial. The necessary components to produce a ramp waveform can be added to the circuit board. For converting triangular waveforms to sinewaves a separate unit is required.



◀ Fig. 1: Circuit of generator producing square and triangular waves over a wide range of frequencies.

or 1MHz (depending on the range) when the slider of VR1 is set at $10 \cdot 0$. At other settings of the dial, the frequency is closely proportional to the dial setting. For example, a dial setting of 5.67 on the

1kHz range produces an output of 567Hz.

Many types of capacitor (especially electrolytic types) have very wide tolerances in their capacitance value. It is therefore necessary to calibrate the frequency at one point on each range to obtain accurate frequency readings. In the circuit of Fig. 1 this is accomplished by the adjustment of a different trimmer potentiometer (VR2 to VR7) for each range used. The switch which selects the trimmer, S1a, is ganged with that which selects the range capacitor, S1b.

FREQUENCY COVERAGE

The frequencies available from the six adjustable ranges employed are shown in Table 1. The upper frequency limit of 1MHz is determined by the characteristics of the integrated circuit used. In the table it has been assumed that a frequency range of 20:1 may be covered using any one capacitor. However, more accurate frequency settings may be obtained by limiting the coverage of each range to 10:1, as was done in the prototype.

RANGE	CAPACITOR	FREQ. COVERAGE
1	10µF	0·5Hz- 10Hz
. 2	1µF	5Hz-100Hz
3	100nF	50Hz- 1kHz
4	10nF	500Hz-10kHz
5	1nF	5kHz-100kHz
6	100pF	50kHz- 1MHz

TABLE 1. Total frequency coverage possible with six capacitors. In practice each range is reduced to a ratio of 10:1.

The writer has found that a frequency range of about 30:1 is about the limit with any one capacitor. At settings of the frequency dial of less than about 0.3 the output waveforms become distorted, whilst oscillation ceases at settings below about 0.25. It was noted that the square waveform at 1MHz was somewhat distorted. The lowest frequency range in the prototype was 0.5 to 10Hz and it is assumed that most readers will not require frequencies below this value. Extra ranges can easily be added if required. However, an additional trimming potentiometer must be included in the Sla circuit for each extra range. A 100 µF capacitor in the S1b circuit can be used to produce a range of 0.05 to 1Hz, a 1000 µF capacitor a range of 0.005 to 0.1 Hz and a 10000 μF capacitor a range of 0.0005 to 0.01Hz (0.0005Hz is one cycle in about 33 minutes).

When using very large capacitors, check that their leakage current is not excessive. The lowest possible frequency is probably about one cycle every few hours, but the writer has not tried to obtain frequencies quite as low as this. Some industrial applications may be found for generators of extremely

low frequencies.

CONSTRUCTIONAL NOTES

The basic oscillator circuit of Fig. 1 was constructed in an Eddystone die-cast box of approximate dimensions $4^{1}_{2} \times 3^{1}_{2} \times 2^{1}_{4}$ in. (Cat. 6908P). The Helipot VR1 and switch S1 are mounted in the base of the box and the circuit board along one of the

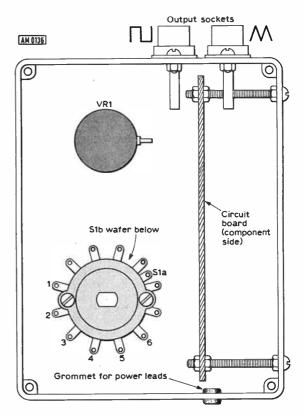


Fig. 2: General layout of components in the die-cast box.

longer sides Fig. 2. No components were mounted on the lid of the box since this procedure enables the lid to be removed without the inconvenience of having wires between it and the main part of the

The six miniature Beckman trimmer potentiometers are mounted on the circuit board Fig. 3, their connecting tags being inserted through holes in the board and bent over before the connecting wires are soldered. The integrated circuit socket is also mounted on the circuit board by passing the pins through holes in the board and soldering the connections to them.

C1 is mounted on the circuit board, but C2 to C7 are mounted around the switch S1. No power supply was included in the box, since it is generally more convenient to employ an external 12V battery. However, a mains power supply could be included if a rather larger box is employed.

If the circuits for the ramp and short pulse generator are required, they must be included in the basic oscillator unit itself. However, if the triangle-to-sine wave converter is made, it will probably be more convenient to construct it on a separate circuit board.

CALIBRATION

The best way of calibrating the frequency settings involves the use of a digital frequency meter which automatically counts the pulses from the oscillator over a timed period. Alternatively a pulse counter may be used with a manually operated stop watch.

Calibration may also be carried out using a good oscilloscope with a calibrated time base. Alternatively the calibration may be set by adjusting the trimming potentiometers so that the output 'zero beats' with the signal from a calibrated generator. At higher operating frequencies harmonics of the square wave output may be allowed to beat with a radio signal, using a receiver.

If very low frequency ranges are incorporated in the unit, the operating frequencies are best determined by connecting a voltmeter across the square wave output and timing the movements of the meter needle.

It is normally best to calibrate the unit at a point near to the highest frequency on each range. The linearity of the resistance of VR1 with the dial setting is very good (better than 0.25%). However, the writer has found that the frequency of oscillation of the NE566V may depart from linearity by up to about $\pm 1\%$ at the lower frequencies in each range.

If a constructor does not like an instrument in which the oscillation ceases at the very low frequency end of each range, it is possible to set the dial so that it reads from 1.0 to 11.0. In this case a 100 ohm resistor, preferably of 0.5% tolerance, should be inserted between the upper end of VR1 and the positive supply line in Fig. 1 so that the readings are directly related to the frequency of oscillation. Operation in this way is likely to increase the errors in the frequency settings, since the percentage linearity tolerance of a precision helical potentiometer is typically about ten times better than the resistance value tolerance.

OUTPUTS

The circuit of Fig. 1 provides good square waves and also linear triangular waves, both at 50 ohm output impedance. These outputs are adequate for many applications, since the triangular waves can

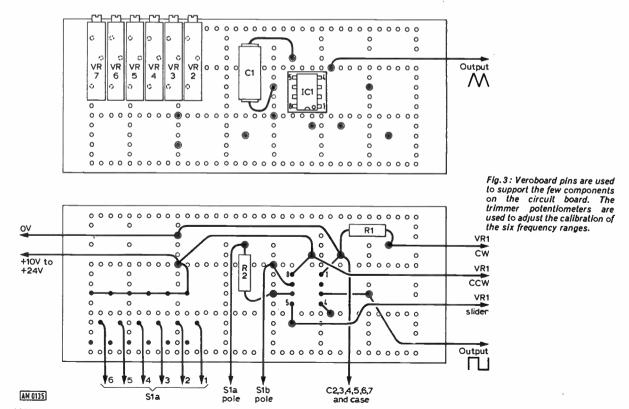
often be used instead of sine waves when their harmonic content is not disadvantageous.

Both of these output waveforms are superimposed on steady positive potentials. The latter can be removed by capacitive coupling except at low frequencies where it is difficult to obtain an adequate time constant to preserve the waveform. The average potential of either of the output waveforms can be made equal to earth potential by employing a power supply consisting of suitable positive and negative supply voltages both isolated from earth.

TRIANGLE-TO-SINE CONVERSION

If a sine wave with a relatively low harmonic content is required, a diode-resistor shaping network may be employed. A fairly complex circuit is required if the shaping must be carried out reasonably accurately. A simpler solution involves the use of the conversion circuit described below.

At a fixed gate voltage, the first part of the drain characteristic of a junction field effect transistor (FET) approximates to half a sine wave. However, further increase of the drain voltage produces little effect on the drain current. The first part of this characteristic can be employed to shape a triangular wave into a reasonably good sine wave. If a triangular wave is applied to this circuit the positive going part of this waveform will produce a drain current of half a sine wave. In order that both the positive and negative parts of the triangular wave shall produce the corresponding parts of a sine wave, the type of circuit shown in Fig. 4 may be employed. This utilises the fact that the drain and source electrodes of an FET are essentially interchangeable.



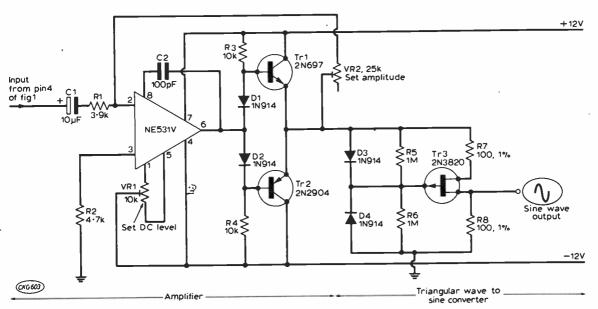


Fig. 4: Suitable circuit for converting a triangular wave to a sine wave.

PRACTICAL SINE CONVERTERS

It should be clear that the amplitude of the triangular wave applied to the circuit of Fig. 4 is quite critical if one requires a good sine wave output. If the input to this circuit is too large in amplitude, the output pulses will have fairly flat sections in place of the normal sine wave peaks. If the input amplitude is too small, the output will be approximately the same form of triangular wave as the input.

It must therefore be possible to alter the amplitude of the triangular wave fed to the circuit of Fig. 4. In addition, the output impedance of the source of the triangular waves must be small and there must be no steady voltage superimposed on the triangular waves. An amplifier of variable gain and of low output impedance is therefore employed between the output of the 566 circuit and the input of the triangle-to-sine converter.

CONVERTER CIRCUIT

The circuit of a practical triangle-to-sine wave converter is shown in Fig. 4. The triangular wave input from the circuit of Fig.1 is capacitively coupled to the input of a Signetics NE531V high slew rate operational amplifier; it therefore follows that this circuit is unsuitable for use at very low frequencies with the values shown, since the coupling time constant would be inadequate.

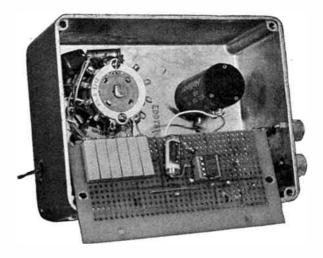
The complementary output transistors Tr1 and Tr2 provide a low impedance output to the converter circuit of Tr3. The preset potentiometer VR1 is set so that the potential at the emitters of Tr1 and Tr2 is zero volts when no input is applied to the circuit.

The voltage gain of the circuit of Fig. 4 from the input to the emitters of Tr1 and Tr2 is equal to the resistance of VR2 divided by R1. The amplified triangular wave is applied to the circuit of Tr3, the operation of which has already been discussed. The author found that the sine wave output voltage was of the order of 0.7V peak to peak and that it has no steady component superimposed on it.

The gain control, VR2, must be set carefully so that the output waveform shows minimum distortion, adjusting the gain whilst examining the output waveform by means of an oscilloscope. If, however, a waveform analyser is available, VR2 may be adjusted for minimum third harmonic distortion.

A satisfactory sine wave was obtained using fixed resistors for R7 and R8. However, one of these resistors may be replaced by a 50 ohm resistor in series with a 100 ohm preset trimmer so that the output may be adjusted for minimum second harmonic distortion (preferably using a waveform analyser). It should then be possible to obtain a sine wave output with very low distortion.

The writer tried replacing the NE531V integrated circuit with a μ A741V which has the same connections. It was found that the NE531V could operate at higher frequencies, but in neither case could satisfactory operation at 1MHz be obtained.



The secret of the direct frequency read-out lies in the use of the multiturn Helipot potentiometer, right centre.

A simple circuit using two cascaded emitter followers for driving an FET triangle-to-sine converter was published in the February 1973 issue of *Wireless World*. However, a circuit with voltage gain is required when the triangular wave output from a 566, operated from a 12V supply, is to be converted into a sine wave.

RAMP WAVEFORM GENERATORS

The circuit of Fig. 1 can be easily converted into a generator which produces either a rising or a falling linear ramp waveform. At the end of each ramp the output quickly returns to its initial level and another ramp commences.

In order to produce a rising ramp waveform, the capacitor connected to pin 7 is allowed to charge, but at the end of the charging period it is rapidly discharged. The ramp waveform appears at pin 3 of the 566 in place of the triangular wave. A falling ramp is produced in a similar way; at the end of the discharging period, the capacitor connected to pin 7 is rapidly re-charged.

RAMP CIRCUITS

Fig. 5 shows the components which must be added to the circuit of Fig. 1 to allow either rising or falling ramps to be produced. When the switch S2 is in position 1, the additional components shown dotted are not used and the circuit therefore provides the normal square and triangular output waveforms. When S2 is in position 2, a falling ramp waveform is generated, whilst in position 3 a rising ramp is formed. Short negative going pulses are available at pin 4 when S2 is in position 2 and short positive pulses when S2 is in position 3.

Let us now consider in detail the operation of the falling ramp generator when S2 is in position 2.

If the output from pin 4 is in its high voltage state, little current passes through D1 of Fig. 8. The base and emitter of Tr1 are therefore at about the same potential and this transistor passes little

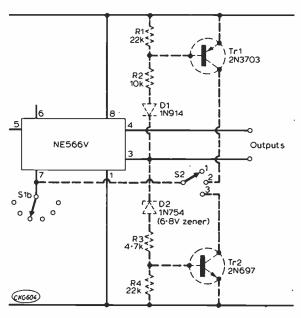
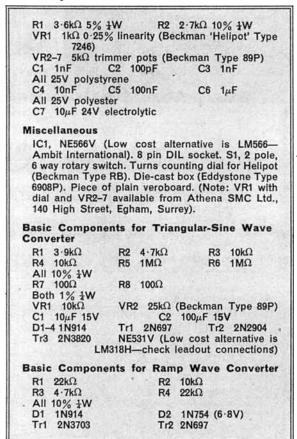


Fig. 5: Additional circuitry, shown dotted, to produce rising or falling ramp waveforms.

* components list



current. The output from pin 3 therefore falls linearly with time, unaffected by the additional components.

When the output from pin 4 falls to its low voltage state, however, D1 conducts and the base of Tr1 becomes negative. This PNP transistor therefore conducts and rapidly charges the capacitor selected by S1b. The voltage at pin 3 therefore rises rapidly to its maximum value before a further falling rampis generated.

The output from pin 4 consists of short negative going pulses which occur each time the ramp waveform at pin 3 rises to its maximum value. These waveforms are shown in Fig. 6. When the capacitor selected by S1b is small, the negative going pulses at pin 4 were found to be about $0.2\mu s$ in length.

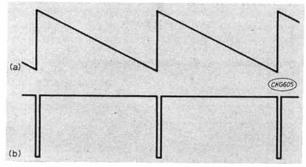
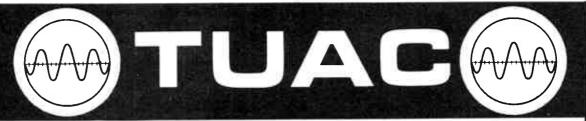
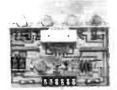


Fig. 6: Waveforms obtainable from the circuit of Fig. 5.





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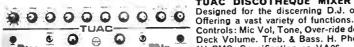
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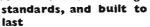
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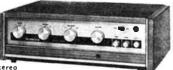




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When a large capacitor is in circuit, however, it takes longer to charge from the current passing through Trl. Nevertheless, the time for which the waveform at pin 4 is in its low voltage state is a very small fraction of the total operating time.

The operation of the rising ramp generator, when S2 is in position 3, is rather similar. When the output at pin 4 is in its low voltage state, the zener diode D2 passes little current and Tr2 remains cut off. During this time the ramp waveform at pin 3 is rising.

When the voltage at pin 4 switches to its upper level, however, the zener diode conducts and Tr2 receives a positive bias at its base. This NPN transistor therefore conducts and rapidly discharges the capacitor selected by S1b. The potential at pin 3 therefore returns quickly to its lowest level and the ramp commences to rise again.

The output from pin 4 consists of short positive pulses which occur each time the ramp at pin 3 returns to its lowest level.

The rising ramp generator was found to give a poor waveform on the 1MHz range. However, the rising and falling ramp generators both operated satisfactorily on the other ranges and also at very low frequencies. The writer tried them at frequencies down to about 0.01Hz and at such frequencies the waveform takes a fraction of a second to return at the end of each ramp.

When either of the ramp generators is employed, the one half of the triangular waveform is eliminated. The frequency of oscillation of the 566 is therefore approximately doubled when S2 is in position 2 or 3. Constructors who intend to use the unit mainly for ramp waveform generation may wish to calibrate the unit so that the ramp frequency can be read directly from the Helipot dial. The dial reading must then be halved to obtain the frequency of the triangular or square wave.

APPLICATIONS

The fundamental frequencies from the waveform generator can be used to test the functioning of audio amplifiers; they also cover the long wave band and the low frequency end of the medium wave band. In addition, the outputs contain harmonics (mainly odd harmonics) which can be used to test the functioning of radio receivers throughout the medium wave band and also at somewhat higher frequencies.

Both the triangular waves and the ramp waveforms are very suitable for the detection of crossover distortion in audio amplifiers, since these waveforms are essentially linear. If the triangular wave output is fed to the input of an audio amplifier which introduces cross-over distortion in its output stage, the type of waveform shown in Fig. 7a is obtained. The values of the resistors in the audio amplifier which control the quiescent current in the output stage may be altered so as to increase this current slightly; the cross-over distortion should disappear when the quiescent current is sufficient.

It is easier to detect cross-over distortion when using the triangular or ramp waveforms than when the more conventional sine wave is employed. A frequency in the mid-audio region is ideal for this test (perhaps 1kHz). The linearity of the waveform on the oscilloscope screen may be measured by placing a straight edge along the tips of the waveform.

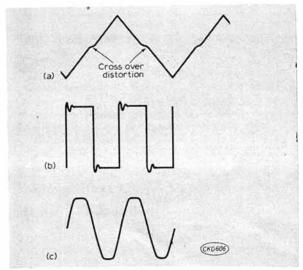


Fig. 7a-b-c: Waveforms at the output of an audio amplifier using input signals from the waveform generator.

The square wave output is also very useful for testing audio amplifiers. At fairly high frequencies one may examine the output from an amplifier for ringing of the type shown in Fig. 7b. Ideally there should be no overshoot or ringing. An audio amplifier which can faithfully reproduce a square wave at a frequency of about 10kHz must have a good frequency response in the high audio frequency region since square waves contain many harmonics and will be reproduced satisfactorily only if the amplifier has a fairly level response at frequencies of up to at least three times the fundamental frequency of the square wave.

If an audio amplifier has only a moderately good high frequency response, the corners of the output waveform will be rounded off at 10kHz, as shown in Fig. 7c. An approximate value for the frequency response of the amplifier may be obtained by estimating the time taken for the output waveform from the amplifier to rise from 10% to 90% of its final value. The maximum frequency at which the response is reasonably constant is of the order of 1/(3 x the rise time). If the rise time of a square wave is very short, one sees only the lines at the top and bottom of the oscilloscope display, the rising and falling parts of the waveform being so short that they are barely visible.

One can also use the square wave output from the 566 unit to examine the low frequency response of audio amplifiers. As one reduces the frequency of the square wave, the upper and lower parts of the output waveform do not remain horizontal, but develop a definite slope. At very low frequencies, a differentiated waveform will be obtained. The input of the oscilloscope marked 'DC' should be used for these low frequency tests, since the 'AC' input is connected to a series capacitor inside the oscilloscope which may distort the waveform.

In the audio amplifier tests discussed above, it has been assumed that the amplifier under test has a volume control at its input which can be adjusted to provide the required signal output level. At high levels it will be necessary to include a series canacitor in the input circuit to block the steady voltage at the 566 outputs. In this case care should be taken to ensure that the coupling time constant is adequate for the lowest frequency to be employed.

DRY BATTERY CHARGER

R.A.Butterworth

OST of us either make or buy a mains supply unit to operate our battery tape recorders, receivers etc., when used at home to save the cost of dry batteries. However batteries are still needed around the home and unfortunately they seem to cost more each time. One could of course use rechargeable cells but they are expensive and need a rather special charging unit which is also expensive.

If we could get a few more hours out of our dry battery we could cut our costs considerably, even one more 'run' would be equivalent to cutting the cost by a half. With the charging units described here two, three or more 'lives' can be given to a set of batteries, perhaps not quite as long a period of operation as the first but certainly for periods long enough to make the building of a charger show an economical return for the effort involved.

The idea of reforming dry cells is by no means new. Investigation of the possibilities were made as long ago as the early 1950's with encouraging results. With modern methods of manufacture and materials, the life of the primary cell can be considerably extended if a few basic rules are born in mind. These are:

1 The battery must be charged before its voltage (on load) drops from 1.5V to below 1V.

2 It must be put on charge as soon as possible after being removed from service and put into service as soon as possible after re-charge.

3 It is not economical to charge a single unit, a 1.5V 'pen light' HP7 for example. Therefore it is better to have one set of batteries in service and another on charge.

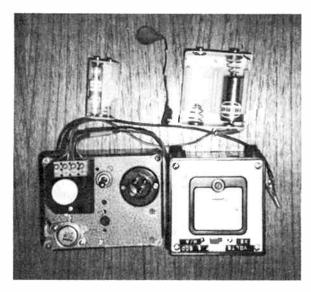
4 The charging rate should be adjusted to distribute the charge, in other words avoid heating up the cell by charging at too high a current.

5 If there is the slightest suspicion of battery leakage throw them away or you will have a horrible mess to clear up.

The cylindrical types like the U2, U11 and HP7, respond much better than the layer batteries, such as the PP3. The use/charge cycle is less than half that of the cylindrical types. The table gives details for popular zinc-carbon types which have responded successfully to several use/charge cycles with the equipment shown.

Battery holders

Standard battery holders can be used to hold the cells whilst charging in blocks of 2, 4, or 6. From experience it would appear that, after setting at the current shown, if after the first couple of hours there

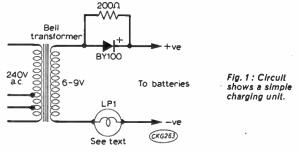


is no drop in the charging current, then discard the battery as the electrolyte has probably dried out. If the batteries get appreciably warm or show signs of leaking throw them out. Different sets of batteries have given a different number of cycles. This, the author believes, is due to 'freshness' of the unit cells when first purchased; in other words how long they had been on the shelf in store.

DRY BATTERY CHARGING

Battery		No. of Cells	Charging Current mA Min. Max.		Approx. hours of charging	No. of cycles
U2	Torches, Hand lamps Rádios	2 4 6	150	300	5	3
U7	Small Torches, Radios	1 or 2	100	150	4	4
U11	Cassette Tape Recorders	4	100	250	5	4

In the circuits shown in Figs. 1 and 2 it will be noted that very little smoothing of the d.c. output has been incorporated. This is deliberate; investigation has shown that it is advantageous to have a little a.c. present. This "dirty d.c." appears to shake up the electrolyte and therefore assists in the reforming.



-continued on page 1061

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BC107	10p	T1843	28p	1N 4002	640
BC108	10p	2N1711	24p	1N4003	70
BC109	10p	2N2219	25p	1N4004	740
BC147	10p	2N2646	45p	1N4005	81
BC148	10p	2N2905	33p	1N4006	810
BC149	12p	2N2907	25p	1N4007	91
BC168	13p	2N2926O	10p	W O 0 5	302
BC169C	12p	2N2926Y	10p	W-04	331
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Charger units

Fig. 1 shows a simple unit which can be easily put together and used to try out the idea. A good quality bell transformer, BY100 diode, m.e.s. lamps, lamp holder and a 220Ω 1W resistor and you are in business. The writer found this unit successful but it lacked flexibility. If the bell transformer shown in Fig. 1 has various outputs then the number of cells to be charged can be varied and by changing the lamp the charging current can be varied within limits.

Fig. 2 is a more elaborate unit and in the author's case serves two purposes; A dry battery charger and mains unit for various equipment used in the shack. Should additional smoothing be required then it is a simple matter to add this. It is advisable to install the meter permanently so that the charging current can be monitored. A d.p.d.t. switch with a suitable shunt series resistor would enable both voltage and the current to be monitored. Diode D6 provides for reversal protection and prevents the battery discharging through the 470Ω resistor.

Zinc-carbon batteries are very amenable to recharging.

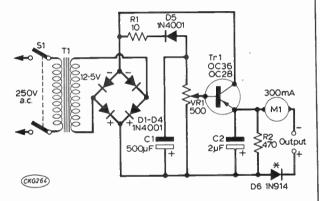


Fig. 2: A more elaborate design.

★ components list (Fig. 2)

R1	10Ω ½W
R2	470Ω 1W
VR1	500Ω 3 W linear wirewound
C1	500µF 20V
C2	2μF 20V
Tr1	OC36, OC28 or similar rating
T1	Mains transformer 12.5V 1A secondary
D1-D4	1N4001 diodes
D5	1N4001 diode
D6	1N914 diode (see text)
M1	Meter 300mA f.s.d.
S1	Double-pole on/off toggle switch
LP1	3.5V or 6.5V 0.1/0.2A (Fig. 1)

NEXT MONTH

An Automatic Battery Charger for 12 volt car batteries.

TELEVISION

IN THE

ASSEMBLING A MODULAR COLOUR SET

There are various ways of going about building a colour receiver. One approach is to make use where possible of manufacturers' surplus units. David Robinson describes the set he built on this basis and how the various problems of interfacing different units not originally intended for use together were overcome.

LOG-PERIODIC SET-TOP AERIAL

A simple log-periodic set-top aerial can be made using printed circuit board. Full constructional details will be provided.

TV SET SAFETY

With the introduction of the BEAB television receiver testing system and BS415:1972 there has been a tightening up in safety requirements. It is essential that anyone handling TV sets should be aware of what is involved. A detailed account starts next month.

FAULT FINDING

John Law looks at the power supply and line timebase circuits used in BRC 15in. dualstandard portable models. These make excellent second sets.

PHASE IN COLOUR TV

The phase of the chrominance signal indicates the colour being transmitted: phase is thus the key to colour television. A special article next month describes the basic technique and PAL signal processing, paying particular attention to practical points that are not always made clear.

PLUS ALL THE REGULAR FEATURES

Details of the March issue are subject to the current national situation at the time of going to press.

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JOSTY KITS

Our Advertisement Manager has asked me to point out that Swanley Electronics will not be supplying "Josty" kits as per their December advertisement.

HEATHKIT CATALOGUE

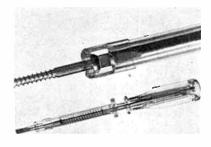
The latest catalogue from Heath (Gloucester) Limited contains details of the company's kits and some new models featured for the first time include the GR-990 12in. Black and White Television kit for either 12V or mains operation; the GD-39 Home Intrusion Alarm, disguised as an unobtrusive book — an ultrasonic burglar alarm/surveillance system; the CR-1008 a.m. Radio and the CM - 1045 Small Engine Tune - up Meter.

Also included are the 10-104 Solid State 15MHz Oscilloscope; IB-1103 180MHz Frequency Counter; the GC-1005 Electronic Digital Clock which incorporates a 'snooze' alarm; the CR9502 Push-Button a.m. Car Radio and the IC-2108 Desk Top Electronic Calculator.

Readers may obtain their free catalogue by writing to Heath (Gloucester) Limited, Bristol Road, Gloucester, GL2 6EE.



SCREW DRIVING BOON



Thunder Screw Anchors Ltd. announce an addition to their range of screwdrivers by the introduction of four screwholding screwdrivers. Two are suitable for slotted head screws and two for recessed head screws, their dimensions being 81/in. and 91in. overall length, 3/16in. and in, blade diameter respectively. The screw is firmly held at the tip of the screwdriver by sliding the springloaded shank over the head of the screw, (see picture) leaving one hand free to hold the article to be fixed. It is possible to fix screws or bolts in the most difficult of places, where to hold a screw in the hand might normally be impossible.

Prices, excluding V.A.T. are 20372 and 20376 69p each, 20374 and 20378 79p each.

We understand that due to the shortage in the foreign plastics industry, supplies of these screwdrivers may be subjected to extended delay. However, this firm does have some further useful and novel tools that would be of interest to readers. Supplies are through retail outlets. Thunder Screw Anchors Ltd., Victoria Way, Burgess Hill, Sussex, RH15 9NF.

MICROELECTRONICS

We apologise to Microelectronics for being unable to include their advertisement in the Feb. issue. If readers refer to this month's issue, page 1028, they will see that the company markets the Minicomp 100 Random Number Selector. When the button on the front panel is pressed, numbers are displayed at high speed on a Nixietube read-out before a random number is displayed—in effect a miniature "ERNIE".

The circuit includes 6 TTL logic i.c.'s and three transistors and the manufacturers say that typical applications include number selection for dice, roulette, bingo etc. Price of the Minicomp 100 kit is £42·50. A fully assembled version is available at £45·00.—Microelectronics, 51 Mexfield Road, London, SW15 2RG. (Tel. 01-870 2368).

ONE-HAND DESOLDERER

When desoldering, have you ever wished you had three hands? Well, here is something that will brighten your day!

Only one hand is required to operate the Picard soldering / desoldering iron. The whole body of the tool forms a suction tube which is pressed down towards the job during heating and released to produce suction.

The unit has a rating of 20W and uses an 8V supply, a transformer being available if required. For desoldering, it reaches a temperature of 340°C in four minutes. Only three minutes' heating is however required for soldering. The heating element is sealed with a ceramic insulating paste which, by preventing burning and corrosion, prolongs its life quite considerably.

The bit is made of alloy steel and molten solder is sucked through it by the release of the spring-loaded body. The faster the release, the stronger the suction. The solder collecting chamber is easy to clean out while the bit is still warm.

A soldering stand is supplied with every tool and the price of the complete unit is £6.49. Henry Picard & Frere Limited, 357/359 Kennington Lane, London, S.E.11.



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H38	30	Short lead Transistors, NPN Silicon Planar types	55p
H39	6	Integrated Circuits. 4 Gates BMC 962, 2 Flip Flops BMC 945	55p

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H16	15	Experimenters' Pak of Integrated Circuits, Daja supplied	55p
H20	20	BY126/7 Type Silicon Rectifiers 1 amp plastic. Mixed volts.	55p
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Plastic Power Transistors 6

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The object was to design a unit which would provide 1MHz, 100kHz, 10kHz markers at good strength to at least 30MHz or higher. The calibrator to be described will, when used with the average receiver, provide strong frequency markers to above 30MHz and will give markers as high as 144MHz at reduced level.

OPERATION

The crystal oscillator runs at 1MHz and is based on the Colpitts circuit. In the design, good stability results in respect of both temperature variation and variation of supply rail voltage. In order to maintain this performance silver mica capacitors are specified for C2 and C3. The crystal in the prototype required about 40pF in series and this is made up by C1 plis TC1. If necessary, C1 can be altered to suit different

The output from the crystal oscillator is taken from the collector of Trl. The waveform is roughly a sine wave and in order to drive the dividers must be squared. Tr2 acts as a buffer amplifier and is biased into saturation on positive half cycles. This gives a square wave output of five volts peak to peak, which is used to drive the dividers.

The SN7490N (IC1-1C2) are TTL logic binary dividers and contain two gates and four bistables. They are used in this circuit to divide the 1MH2 square wave by a factor of ten, giving in the first case 100kHz and in the second 10kHz. The output is a square wave of five volts (approx.).

The three outputs, one from each divider and the 1MHz waveform from Tr2 buffer are selected by S1 and are used to drive 1C3 and Tr3. These stages form the harmonic generator.

HARMONIC GENERATOR

From a pulse rising at an infinite rate an infinite frequency spectrum could be derived, and if the pulse were to be repetitive at some frequency, say 1MHz, then the spectrum would be related to the repetition rate of the pulse. However after the rise the pulse amplitude must decay again in time for next transition. If the decay is fast and at half the pulse repetition time then obviously a square wave would result. This could be shown to contain, in a pure case only, odd harmonics of the basic repetition rate. Now if the decay point were to be shifted from the half repetition rate time, then the even harmonic content would become apparent. Therefore in generating both odd and even harmonics of a fre-

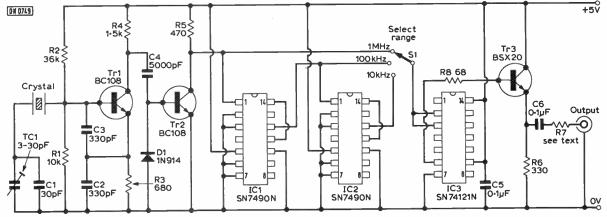
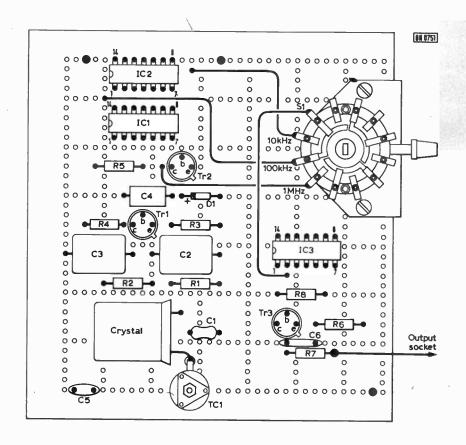


Fig. 1: Circuit of the calibrator



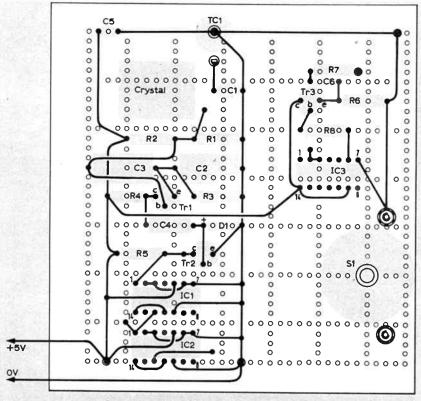


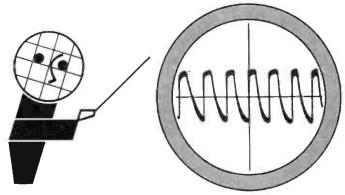
Fig. 2: Veroboard layout for the i.c. crystal harmonic calibrator

-continued on page 1069

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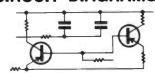
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ECC81	I2p	PCL85	20p	6F23	15p
ECC82	12p	PL36	17p	30FS	12p
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quency or rate, the main functions governing them are the rise or transition time of the pulse and its duration with respect to repetition rate.

It can now be seen that the principal requirement for a harmonic generator is that it must generate a pulse with a rapid transition or rise time which is as narrow as possible with respect to the repitition rate.

A number of methods exist whereby a fast pulse may be generated, these include tunnel diodes, reverse recovery effect of diodes, fast switching transistors etc.

For ease and cheapness the method used here is a standard SN74121N monostable (IC3) which drives Tr3 the emitter follower into saturation. The SN74121N has provision for external timing components, but none are used here. This gives a pulse width of 30-40nS. The output rise time (transition time) is quoted as 10nS, but this is speeded up considerably by Tr3, which is a high speed switching device. Tr3 also provides a low output impedance.

The 75Ω resistor R7 is worth mentioning. The output impedance of the emitter follower (Tr3) is not governed directly by R6. It is in fact much lower than this and for matching purposes may be taken as zero. If it is desired to pass the signal along a coaxial line or to use an attenuator then R7 should be chosen to match the impedance of the cable in use, in the range of $50\text{-}300\Omega$. However, many people will simply want to connect receivers or to squirt the output into a few feet of wire in which case make R7 50 Ω .

POWER SUPPLIES

The limiting factors here are the integrated circuits. The voltage required is five volts $\pm 10\%$. The design of the oscillator assures stability to within a few Hz for a $\pm 20\%$ change in supply potential. This should not however present too great a problem as many constructors now run some form of equipment from which a five volt supply could be borrowed to operate the calibrator.

Fig. 3 shows the circuit of a simple stabiliser for use with this calibrator.

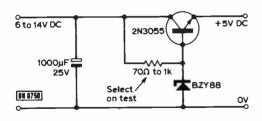


Fig. 3: Simple stabiliser

CONSTRUCTION

Building the calibrator should not present any problems, all components may be assembled on perforated board of suitable matrix. However in order to realise the best h.f. performance the leads around 1C3 Tr3 should be kept as short as possible and the output socket wired direct to Tr3 emitter. In particular, ensure that the output lead from pin 6 of 1C3 is short and direct to Tr3 base.

The crystal, if of a miniature type, may be fastened to the board and secured with a loop of wire. Solid

vibration free wiring in the crystal oscillator circuit will avoid microphony. If S1 cannot be wired direct to the board, all leads to it should be kept short. When completed and tested the board may be fitted in a small metal case or die-cast box.

* components list

C1 30pF silver mica C2 330pF silver mica 2% C3 330pF silver mica 2% C4 5000pF polystyrene C5 0·1µF ceramic C6 0·1µF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	Resist	ors			
R3 680Ω R7 50-300Ω R4 1-5kΩ R8 68Ω Capacitors: C1 30pF silver mica 2% C3 330pF silver mica 2% C4 5000pF polystyrene C5 0-1μF ceramic C6 0-1μF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments	R1	10kΩ			
R4 1·5kΩ R8 68Ω Capacitors: C1 30pF silver mica 2% C2 330pF silver mica 2% C4 5000pF polystyrene C5 0·1μF ceramic C6 0·1μF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N IC3 SN74121N	R2	36kΩ	R6	330Ω	
Capacitors: C1 30pF silver mica C2 330pF silver mica 2% C3 330pF silver mica 2% C4 5000pF polystyrene C5 0·1µF ceramic C6 0·1µF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	R3	680Ω			
C1 30pF silver mica C2 330pF silver mica 2% C3 330pF silver mica 2% C4 5000pF polystyrene C5 0·1µF ceramic C6 0·1µF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	R4	1-5kΩ	R8	68Ω	
C2 330pF silver mica 2% C3 330pF silver mica 2% C4 5000pF polystyrene C5 0·1μF ceramic C6 0·1μF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	Capac	itors:			
C2 330pF silver mica 2% C3 330pF silver mica 2% C4 5000pF polystyrene C5 0·1μF ceramic C6 0·1μF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	C1	30pF silver	mica		
C3 330pF silver mica 2% C4 5000pF polystyrene C5 0·1µF ceramic C6 0·1µF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N					
C5 0·1µF ceramic C6 0·1µF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N			r mica 2%		
C6 0·1µF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N					
C6 0·1µF ceramic TC1 3-30pF Philips trimmer Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	C5				
Semiconductors: Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	C6	0·1μF cerar	nic		
Tr1 BC108 Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	TC1	3-30pF Phil	ips trimmer		
Tr2 BC108 Texas Instruments Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	Semic	onductors:			
Tr3 BSX20 Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	Tr1	BC108			
Integrated Circuits IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	Tr2	BC108	Texas Instru	iments	
IC1 SN7490N IC2 SN7490N Texas Instruments IC3 SN74121N	Tr3	BSX20			
IC2 SN7490N Texas Instruments IC3 SN74121N	Integr	ated Circuits			
IC3 SN74121N	IC1	SN7490N			
	IC2	SN7490N	Texas Ins	truments	
Miscellaneous	IC3	SN74121N			
	Misce	llaneous			
S1 1 pole 3 way	S1	1 pole 3 wa	y		

TESTING

Connect a suitable five volt supply to the calibrator and couple the output to a receiver (b.f.o. on) tuned to 1MHz. If all is in order a marker will be heard. Tune the receiver throughout its range and check that markers are present. Switch S1 to 100kHz and check that there are 100kHz markers present. Switch to 10kHz and carefully check that 10kHz markers are present.

If no markers are present on any range first check the oscillator circuitry. If markers appear only at 1MHz intervals check the dividers for a fault.

The simplest way of controlling the injection of markers to a receiver is to vary the coupling. Obviously the markers are less strong around 30MHz and the coupling may have to be increased. Direct coupling without the use of an attenuator is likely to overload the receiver and may introduce spurious responses. A little experiment will reveal the best method of operation.

Once the unit has been checked the frequency may be accurately set against WWV or MSF on either 2.5, 5.0 of 10MHz. The calibrator should be rechecked from time to time against the standard frequency services to maintain its accuracy. TC1 may be adjusted as necessary to maintain this accuracy.

We regret that the December 1973 issue of Practical Wireless is now out of print

FURTHER DESIGN PAUL COOPER

12volt d.c. portable flourescent lamp unit is a very useful piece of equipment to own—especially in these days of power cuts! This article describes an alternative to the unit described in the December 1973 issue of Practical Wireless. There is the bonus that it is easier to build the circuit on a standard piece of veroboard than to produce a special printed circuit board and, by using a ready made transformer, reduces the cost.

TRANSFORMER

A transformer specifically for '12 volt inverters to run flourescent tubes from car batteries is available from G. F. Milward* for only 50p + post packing & VAT. It saves the time taken to wind the transformer, which is something which might put off the inexperienced amateur from building the project.

The revised circuit diagram is shown opposite.

The circuit is basically the same as in the original article except for the extra tertiary winding on the transformer which is connected in parallel with capacitor C3. The unit will work without this winding connected but in the circuit shown it tunes the transformer thus producing a better output.

It is most important that terminals 1, 2, 3 & 4 of the transformer are connected to the right points on the circuit diagram (as shown by the dots) since if, say, 3 and 4 are reversed the circuit will not oscillate. To cure this, should it occur, connections 3 and 4 should be interchanged and the circuit should then oscillate. (For the complete setting-up procedure see the original article.)

LAYOUT

The Veroboard layout is shown opposite for $0\cdot 1$ inch matrix veroboard. The board size is the same as for the original printed circuit board so no problems should occur in mounting this board in the completed unit. Note that the fixing hole in this circuit board is in a different place to that of the original board, so a different hole will have to be drilled in the unit case.

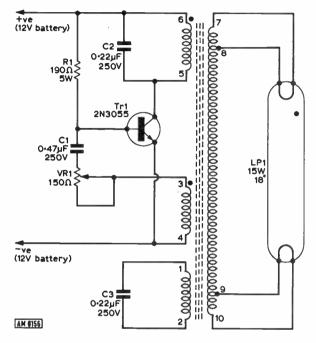
The transformer is fixed to the circuit board by two links of insulated copper wire as shown in the circuit board layout diagram.

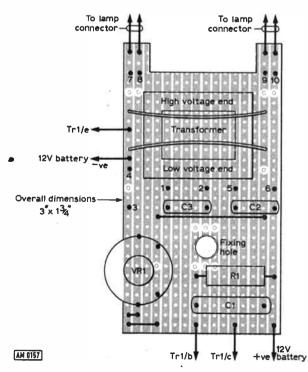
Resistor R1 should be mounted about ¹4in clear of the circuit board and clear from C1 as it gets hot! Since drilling of the holes for the legs of potentiometer VR1 cuts the circuit board tracks completely, care must be taken to ensure contact when soldering the legs in.

Exact values of R1 and VR1 are not very critical. Values were chosen because of availability.

As my unit was built primarily as an emergency light for use in power cuts, the case has been designed to stand on a table with the tube vertical, and it is made of wood.

* G. F. Milward, 369 Alum Rock Rd, Birmingham, B8 3DR.





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'SIMINI' 5-BAND RECEIVER

This unusual receiver is designed to give five ranges from 160kHz to 27MHz, using simple plug-in coils to cover broadcast and amateur transmissions. Only eight transistors are used, and, with a telescopic aerial the "Slimline" becomes a versatile a.m. receiver to take almost anywhere.



GASSETTE 8 (CORDER) IND UNER !!!



THIS constructional feature describes a stereomultiplex AM/FM tuner-amplifier providing 10 watts RMS output per channel into 8Ω loads with facilities for incorporating a cassette tape recorder. The integrated unit provides very good results which, although not to true high fidelity standards, will give satisfying listening for a moderate outlay.

Facilities on the prototype included full Band II FM coverage together with one preset AM station and an input for a ceramic cartridge. Additional circuitry and printed boards are shown in this article so that inputs for magnetic cartridge and tape heads can be accommodated, together with record/play-back connections for a cassette or reel-to-reel tape recorder. Additional tuning capacitors may also be fitted along with a selector switch to provide more extensive AM coverage. The AM section uses an internal ferrite aerial, but an external aerial may be added if required. The stereo decoder incorporates automatic mono/stereo switching and stereo beacon lamp drive.

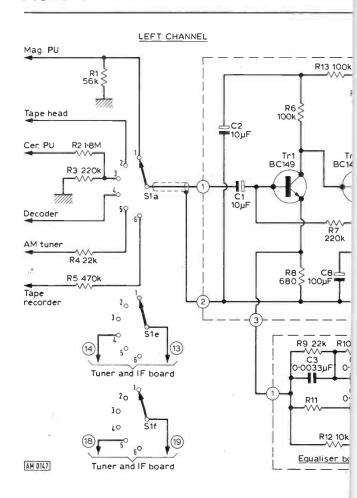
The complete unit is built up on five main circuit boards. The power supply is built directly onto the chassis which is constructed from aluminium angle and strip. The following unit numbers will be used as a prefix to identify components which are mounted off the circuit boards:—

- 1 Pre-amplifiers
- 2 Power amplifiers
- 3 Tuner and IF
- 4 Stereo decoder
- 5 Power unit and input/output sockets.

The front panel is fashioned from 3mm Perspex, using Letraset marking and gives a very professional finish to the unit.

The complete circuit uses 3 integrated circuits, 19 transistors and 7 semiconductor diodes. The FM tuner head is a Mullard module, simplifying construction and greatly reducing alignment problems.

PART 1





RICHARD COLLIN

* Performance Specification

AMPLIFIER

Power output: 10 watts RMS per channel into 8Ω Frequency response: 20Hz to 30kHz \pm 3dB at full

power 50Hz to 20kHz ± 1dB (power

amplifier)

Channel separation: 54dB at 1kHz and 10 watts Noise: -60dB at 10 watts (ceramic cartridge input)

Total harmonic distortion: < 0.2% at 1kHz and

10 watts

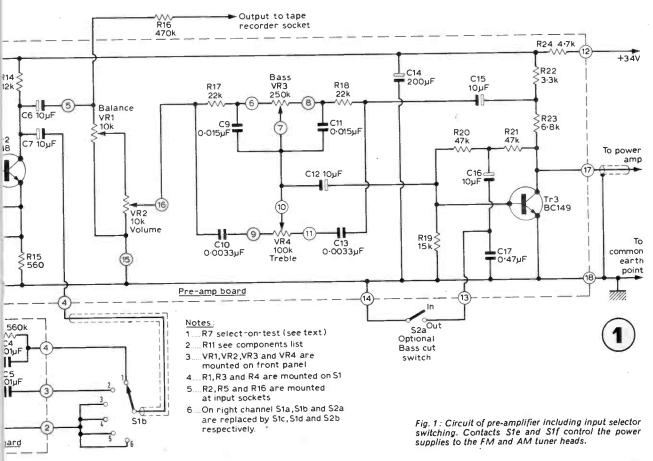
Tone controls: Bass ± 16dB at 50Hz Treble ± 14dB at 15kHz

F.M. TUNER

Frequency range: 88 to 104MHz Channel separation: 40dB

PRE-AMPLIFIER (UNIT 1)

The inputs from the various programme sources, attenuated and matched as necessary by R1-R5, are selected by S1a (S1c for the Right channel). Transistors Tr1 and Tr2 are connected as a highgain pair and amplify the input signals to a level sufficient to drive the tone control circuit. The bias resistor R7 for the first stage may need to be selected for optimum operation. This will be dealt with in a later part of the article. Its final value should lie between 120 and 270kn.



* components list

		PR	E-AMPLIFIERS		
Res	istors				
R1	56kΩ	R10	560kΩ	R17	22kΩ
R	2 1·8MΩ	R11	22kΩ for 12ips	R18	22kΩ
R	3 220kΩ		12kΩ for 3∄ips	R19	15kΩ
R4	22kΩ		6.8kΩ for 71ips	R20	47kΩ
R	5 470kΩ	R12	10kΩ	R21	47kΩ
Re	5 100kΩ	R13	100kΩ	R22	3⋅3kΩ
R7	7 220kΩ*	R14	12kΩ	R23	6 · 8kΩ
R	3 680Ω	R15	560Ω	R24	4 · 7kΩ
R	22kΩ	R16	470kΩ	* Se	e text
A	Il resistors	‡W	5% carbon film		
VI				250ks	2 dual lin
VI	$R2 10k\Omega$	dual lo	g VR4	100kΩ	2 dual lin

Capacitors

C1	10µF 16V	C7	10µF 16V	C13	3300pF
C2	10μF 16V	C8	100µF 10V	C14	200 uF 30V
C3	3300pF	C9	0·015µF	C15	
C4	0.01/4F	C10	3300pF	C16	
C5	0.01µF	C11	0.015µF	C17	0.47µF
C6	10uF 16V	C12	10 uF 16V		3 - 3 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -

Non-electrolytic capacitors should be polyester or polystyrene

Semiconductors

Tr1 BC149 Tr2 BC148 Tr3 BC149

NOTE—With the exception of the four dual-ganged potentiometers, two sets of the above components are required for the two channels.

Miscellaneous

S1 6 pole, 6 way, 3 wafer rotary switch S2 DPST miniature toggle switch Pre-amplifier printed circuit board Equaliser printed circuit board

POWER AMPLIFIERS

Resistors

R2		$\begin{array}{c} \text{R6 10k}\Omega \\ \text{R7 47}\Omega \\ \text{R8 100}\Omega \ 2.5\text{W} \end{array}$	w/w	R12 R13	0·47Ω 2· 0·47Ω 2· 10Ω	5W w/w
	470Ω 470Ω	R9 100Ω 2·5W R10 10Ω	w/w	All film	↓W 5% unless rwise	

VR1 50kΩ

VR2 100Ω miniature presets (horizontal mounting)

Capacitors

C1 25µF 25V	C4 0.01µF 100V	C7 200µF 30V
C2 47/1F 40V	C5 0.22µF 100V	C8 1,500µF 25V
C3 1 000 "F 25V	C6 0.001. E 750V	

Semiconductors

Tr1	BC158	Tr4	2N6288	(RCA)
Tr2	BC148		2N6111	

Tr3 2N6288 (RCA)

Tr3, 4 and 5 are supplied with the necessary mounting hardware

NOTE—Two sets of the above components are required for the two channels.

Miscellaneous

Printed circuit board. Heat sinks and brackets (see Figs. 8 and 9)

NOTE—RCA Semiconductors for this project are available from E.C.S. (Windsor) Ltd., Thames Avenue, Windsor, Berks.

Total requirements are: 2 2N6111 at 50p

5 2N6288 at 54p 1 CA 3089 E at £1.96

1 CA 3090 Q at £4 · 23

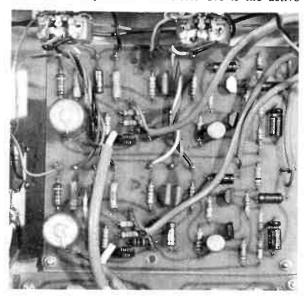
Add 40p post and packing per order and 10% VAT

Feedback around Tr1/Tr2 provides high stability and is also used to set the gain and, for the magnetic pick-up and tape-head inputs, the frequency response. The appropriate feedback path is selected by S1b (S1d for the Right channel). The value of R11, which with C5 provides equalisation for the tape-head input, must be chosen according to the tape speed to be used.

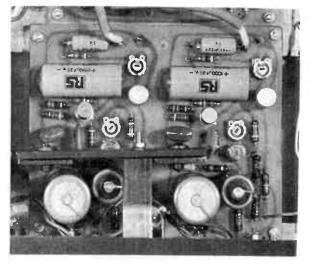
A constructor not requiring the full complement of input facilities may of course omit the unwanted circuitry and connectors.

An output is taken via R16 for connection to a tape recorder, allowing recording of a programme being played through the amplifier (subject to the provisions of the Copyright Act, 1956). The signal at this point is equalised but is unaffected by the Volume and Tone controls. Because of the high value of R16, the two channels can be paralleled at the input of a mono recorder with only slight worsening of stereo crosstalk within the amplifier.

The tone controls are in the familiar Baxandall configuration, providing both lift and cut at bass and treble frequencies. Transistor Tr3 is the active

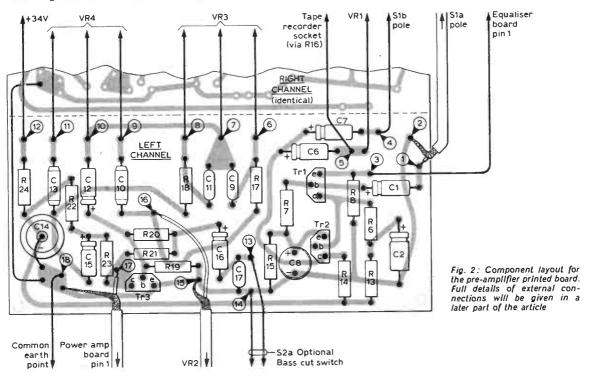


Prototype boards for the pre-amplifier (above) and power amplifier (below)



element of this stage and also makes up for the losses incurred by the frequency selective circuits. A bass cut or rumble filter may be provided by removing the short circuit from across C17.

Ensure correct polarity of the electrolytic capacitors when assembling the circuit boards. In the R7 position fit $220k\Omega$ resistors, leaving the wires long as the value may need to be changed later. Once



AM 0148

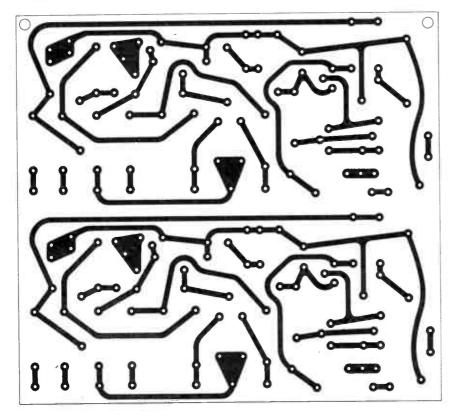
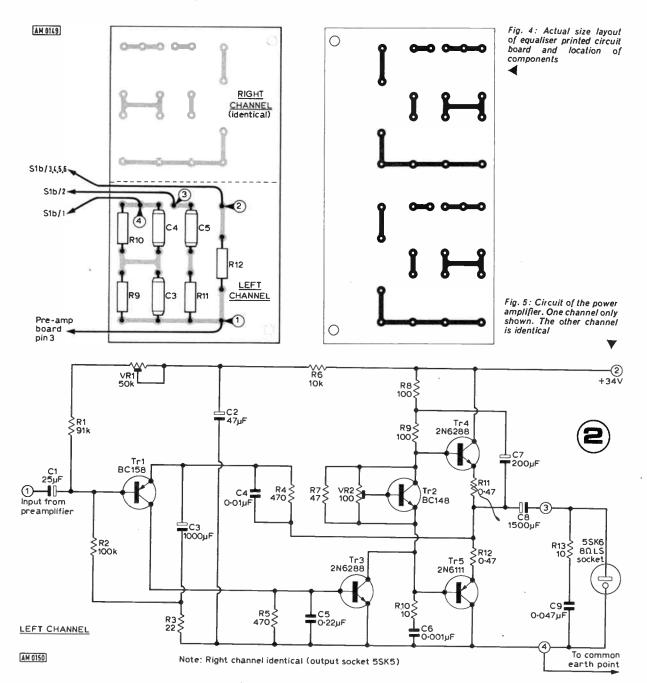


Fig. 3: Actual size layout for the pre-amplifier printed circuit board



complete, these boards may be placed in a safe place until the chassis and power unit are completed. A number of components included in the pre-amplifier circuit diagram are not mounted on the boards. These are dealt with in a subsequent part of the article.

POWER AMPLIFIER (UNIT 2)

The familiar complementary—symmetry configuration is used and designed around silicon transistors. Good low frequency response and stability is ensured by the use of DC coupling throughout the amplifier. The output pair, RCA plastic packaged 'Versawatt' devices, deliver 10 watts RMS into an 8Ω load. A similar device Tr3 operates as a class 'A' driver.

The small forward bias required to minimise crossover distortion is provided by a small signal transistor Tr2 connected between the bases of the output pair. The first stage Trl provides amplification of the input signal and in addition acts as a DC comparator, enabling the output stage to be set up for symmetrical clipping under overload conditions. The DC potential at the output mid-point is connected to the emitter of Trl via R4. The base potential of Trl is determined by the potential divider Rl, R2, VR1 and R6. The high loop gain of the circuit keeps the small difference between Vb and Ve constant, so that the output mid-point voltage is defined by the base potential of Tr1 regardless of component tolerances. Negative feedback is provided by R4, C3 and R3.

Fig. 6: Component location for the power amplifier printed board

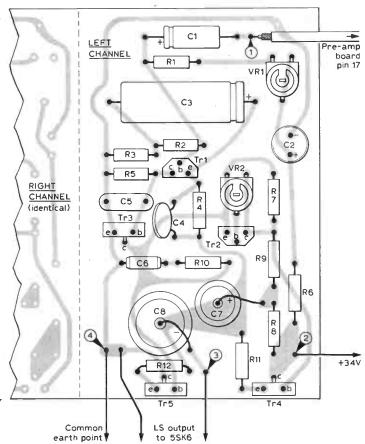
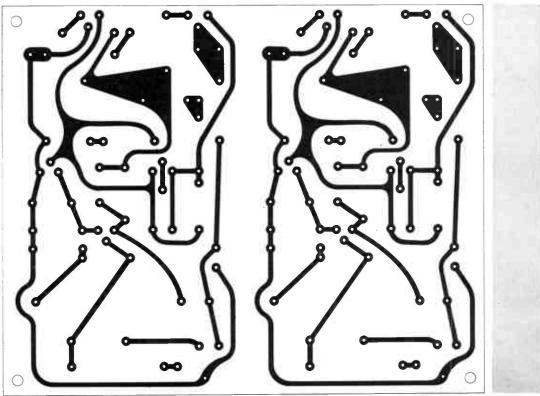


Fig. 7: Actual size layout for the power amplifier printed circuit board

AM 0151



-continued on page 1080

The Sinclair Cambridge... no other calculator is so powerful and so compact.

Complete kit-£24-95! (PLUS VAT)

The Cambridge – new from Sinclair

The Cambridge is a new electronic calculator from Sinclair, Europe's largest calculator manufacturer. It offers the power to handle the most complex calculations, in a compact, reliable package. No other calculator can approach the specification below at anything like the price – and by building it yourself you can save a further £5.50!

Truly pocket-sized
With all its calculating capability, the Cambridge still measures just $4\frac{1}{2}$ " x 2" x $\frac{11}{16}$ ". That means you can carry the Cambridge wherever you go without inconvenience — it fits in your pocket with barely a bulge. It runs on ordinary U16-type batteries which give weeks of life before replacement.

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All parts are supplied – all you need provide is a soldering iron and a pair of cutters. Complete step-by-step instructions are provided, and our service department will back you throughout if you've any queries or problems.

Total cost? Just £27.45!

The Sinclair Cambridge kit is supplied to you direct from the manufacturer. Ready assembled, it costs £32-95 – so you're saving £5-50! Of course we'll be happy to supply you with one ready-assembled if you prefer – it's still far and away the best calculator value on the market.



Features of the Sinclair

Cambridge

A complete kit!

The kit comes to you packaged in a heavy-duty polystyrene container. It contains all you need to assemble your Sinclair Cambridge.
Assembly time is about 3 hours.

Contents:

- 1. Coil.
- 2. Large-scale integrated circuit,
- 3. Interface chip.
- 4. Thick-film resistor pack.
- Case mouldings, with buttons, window and light-up display in position.
- 6. Printed circuit board.
- 7. Keyboard panel.
- Electronic components pack (diodes, resistors, capacitors, transistor).
- Battery clips and on/off switch.
- 10. Soft wallet:



This valuable book - free!

If you just use your Sinclair Cambridge for routine arithmetic – for shopping, conversions, percentages, accounting, tallying, and so on – then you'll get more than your money's worth.

But if you want to get even more out of it, you can go one step further and learn how to unlock the full potential of this piece of electronic technology.



How? It's all explained in this unique booklet, written by a leading calculator design consultant. In its fact-packed 32 pages it explains, step by step, how you can use the Sinclair Cambridge to carry out complex calculations.



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Take advantage of this money-back, no-risks offer today

The Sinclair Cambridge is fully guaranteed. Return your kit within 10 days, and we'll refund your money without question. All parts are tested and checked before despatch – and we guarantee a correctly-assembled calculator for one year.

Simply fill in the preferential order form below and slip it in the post today.

Price in kit form: £24.95 + £2.50 VAT. (Total: £27.45) Price fully built: £29.95 + £3.00 VAT. (Total: £32.95)

	,
To : Sinclair Radionics Ltd, London Road, St Ives, Huntingdonshire, PE17 4HJ	PW 3 74
Please send me	Name
☐ a Sinclair Cambridge calculator kit at £24·95 + £2·50 VAT (Total: £27·45)	
a Sinclair Cambridge calculator ready built at £29·95 + £3·00 VAT (Total: £32·95)	Address
*I enclose cheque for £, made out to Sinclair Radionics Ltd, and crossed.	
*Please debit my *Barclaycard/Access account. Account number	
*Delete as required.	PLEASE PRINT

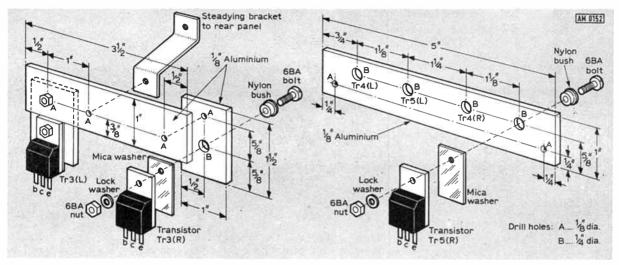


Fig. 8: Design and assembly of driver transistor heatsink

A Zobel network C9/R13 is connected across the output terminals. The purpose of this network is to ensure that the loudspeaker load always appears essentially resistive to the output transistors. This means that the output stage is protected against inductive transients which could exceed the breakdown voltage of the transistors.

Fig. 9: Design and assembly of output transistor heatsink

PART 2 next month will describe the Tuner/IF and FM Decoder units

DWTECHNICROSS UZZLE No.3

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 17 18 20 21 22 23 24 25 28 29

ACROSS

- 1 Employs a coupling of ferrous esters (4)
- 4 A shaker in the transformation scene (8)
- 9 A stick-up in the rockery (4)
- 10 Radio engineers meet with such resistance? (8)
- 11 Come back to fix a little drink (3)
- 12 The Spanish miss her in the end (4)
- 13 Already fixed on the wavelength? (3-3)
- 14 A key piece of mechanism (4)
- 15 As familiar as Liz (4)
- 17 Bell's slowest ringing tone (4)
- 20 Basso loudspeakers amplify this single? (4)
- 21 How to dispense with an earth! (6)
- 23 You talk nonsense about defeat (4)
- 24 Dipole once connected with him! (3)
- 25 If about to bewail a valve component! (8)
- 27 Not so hot in acoustic editing (4)
- 28 Salty type's crystallization at the mike! (8)
- 29 Collections of old wirelesses (4)

DOWN

- 2 Land in court with such maintenance? (7)
- 3 Glass in pieces from these transmissions? (7)
- 5 Jim pleased about the little rascal (3)
- 6 The longest-ever tape? (6)
- 7 They're well up about antennae (5)
- 8 A composed musical performance (7)
- 10 Such a charge about a cathode? (5)
- 15 The more hearty kind of con-man (7)
- 16 Birds do such load-shedding? (5)
- 17 Do riots break such coils? (7)
- 18 Told Sue about being so noisy! (7)
- 19 More I'd swap for a position in golf (6)22 Classification of a crystal-set? (5)
- 26 Nickel-coating is zero-rated? (3)

FOR AMUSEMENT ONLY ANSWERS NEXT MONTH

ON RECENT DEVELOPMENTS

WATCH IT!

AM looking at a Swiss electronics journal. There's a circuit which uses two ICs, a readout chip, and a one-transistor oscillator. Connected together they form an electronic clock complete with digital readout. The only circuitry which needs "building" is the single transistor oscillator and this comprises five resistors, five capacitors, a crystal and one of the ICs mentioned. For the record, the two chips are the SCL5437F (oscillator) and SCL5424F which drives the liquid crystal readout direct.

UNIVERSITIES HELP

One of the major criticisms levelled at universities is that their experiments are all too often of academic value only. While this may be true in some instances, it certainly is not true in the case of the University of Utah in the U.S. This establishment has a section devoted to making blind people see again. Although in the experimental stages, blind people have been able to see light patterns which have been simulated by an external "eye" and fed into their brains by small electrodes.

The light images or patterns are called phosphenes and are stimulated (in these experiments) by the generation (and careful control) of pulses, in other words, the vision has been created by purely electronic means. The width of the pulse and its duration determined the intensity or "shades" of the image which the totally (otherwise) blind person can "see". Researchers see no reason why some form of imaging device (like a solid state t.v. camera) should be used and the impulses fed into the brain—after suitable processing, of course. This latter idea is well within the realms of readily available electronics which one can obtain today.

Embedded image sensors could even be controlled by the eye muscles themselves. Aiready, computer-generated images have been drawn quite accurately by a totally blind person. The image was viewed on a c.r.t. so that a fair comparison could be made.

If you know of a blind person, it would be unkindly premature to mention these experiments with too great an enthusiasm because it may well take many years to perfect it into a practical device.

A TOOTHGRAPH?

Still in the realms of medicine—well, almost, is the latest use of lasers. Now, the dental profession have taken an interest. By using a small laser it is possible to take holographic photographs of a person's teeth. One interesting thing to emerge from this useage is not that it will offer an invaluable aid in dental practice (although this is very true) but its use for security purposes. Apparently no two peoples teeth are the same so instead of fingerprints one could have toothgraphs or teggypix.

Criminals of the future will do well to heed the old addage—when in doubt, keep your mouth shut. In any case the idea should give Scotland Yard something to get its teeth into.

LARGE-SCREEN COLOUR

Perhaps one of the most interesting battles currently being fought is the one for television screens/tubes/systems. All sorts of ideas are currently under examination including a flat screen solid state beasty. News has arrived about another contender. This one is called a Video-Beam projector and houses optics inside the colour tubes. It shows promise for large screen colour television and claims the advantages of doing away with colour dots, lattices and shadow masks.

Each electron beam (one for each of the three colours) is fired at a "target" which has the relevant colour phosphor. This beam is reflected back inside the tube to a concave mirror which in turn reflects the image out of the tube onto the screen. Extremely good results are reported, however,

there is a snag—the projection distance is fixed at eight feet and is unalterable. The company working on the device do not see this as a problem and claim that once the colour tube "projector" has been adjusted at the manufacturing facility, it requires no adjustment or fiddling by the user.

No mention is made of the power requirements but one presumes that they are considerably lower than the 25–30kV needed for the earlier black-and-white projection systems where many people expressed concern about radiation from such a set up.

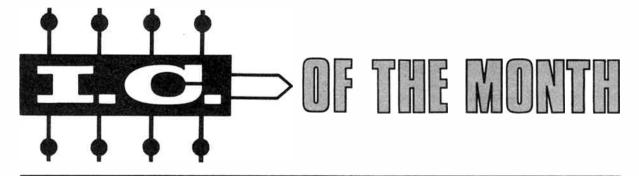
MULTI- CHIPS

A new IC chip, the 2240, is claimed by its makers to do just about anything. It is currently hailed as a programmable timer, binary counter, music synthesiser, A/D converter, ultra-long delay generator, digital sample and hold circuit, frequency synthesiser, pulse counter, binary pattern. generator, precision oscillator... etc., all in one innocent looking sixteen-pin dual in-line package. I have contacted the company with a view to obtaining further information which I will pass on as and when it arrives. It may be possible to include some circuitry of the more practical applications for the home constructor.

BIG CHIPS!

Remember the days when semiconductor devices were fragile and sensitive to fluctuations in power. Contrast that with the latest beast from International Rectifier. This is a silicon controlled rectifier which handles 2,500 Amps r.m.s. at up to 1,200 volts. A 2,000V version is already planned. The wafer for this device is almost 2½ inches in diameter. This is probably the largest chip which has ever been employed in any semiconductor device.





Number 44

National LM377N 2 + 2W AUDIO AMPLIFIER

HE LM377N is an IC, manufactured by the National Semiconductor Company, which contains two separate two-watt amplifiers in a single device. The connections are shown in Fig.1. A 14 pin dual-in-line encapsulation is employed which can be fitted into a socket or soldered into a printed circuit board. A similar device, the LM377N-10, has metal tab connections which may be soldered to a printed circuit board. Pins 3, 4 and 5 and also 10, 11 and 12 of Fig. 1 are replaced by metal tabs on each side of the device. These are very convenient for soldering to a heat sink.

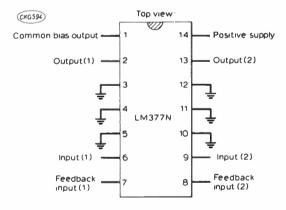


Fig. 1. Pin connections to the 14 pin DIL LM377N.

The LM377 devices are intended mainly for use in stereo equipment where the output power required does not exceed 2W. However, they can also be used in a bridge circuit where the two amplifiers in the device are used in push-pull to provide a monaural output of up to 4W.

Advantages

The following features make the LM377N especially attractive to the amateur constructor as well as to the professional circuit designer:—

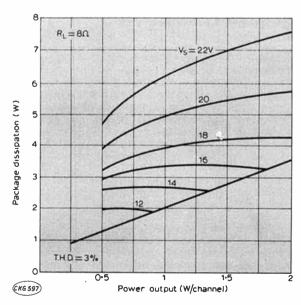
(i) The output stages are automatically centred at the correct bias so that the output voltage can swing an equal amount in either direction resulting in maximum power output at a given distortion level. (Some power amplifiers circuits require a preset potentiometer so that the bias can be adjusted manually.)

- (ii) The LM377N contains internal circuits which protect it from overheating. If the silicon chip becomes too hot, the device switches itself off until it becomes cooler.
- (iii) Protective circuits prevent the device from being damaged by excessive current. Such currents are likely to flow if either of the outputs is accidentally shorted to earth.
- (iv) The input impedance is relatively high, 3MΩ, and this increases the versatility of the device.
- (v) Any hum on the power supply line is reduced by 80dB. The separation between the two channels is typically 70dB.

Circuits

In all circuits the inputs of both amplifiers should be biased by the voltage from pin 1. The bias current is typically 0.5μ A to each amplifier.

In addition, feedback from each output should be applied to the feedback input of the same amplifier. The amount of feedback controls the gain.



Graphs relating supply voltage to output power for the LM377N.

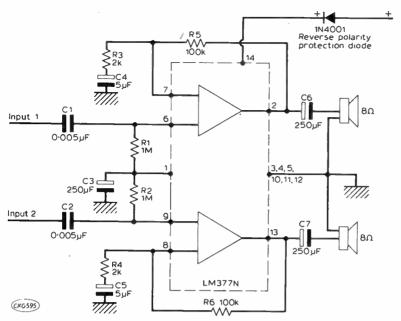


Fig. 2. Circuit of a practical stereo amplifier suitable for a record player. A volume control will be required on the input circuit.

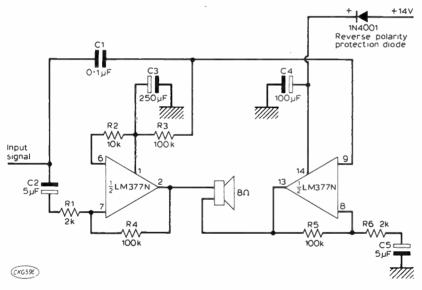


Fig. 3. This mono circuit utilises both amplifiers to provide 4W output.

A typical circuit for the use of the LM377N as the two power amplifiers of a stereo system is shown in Fig. 2.

Bias from pin 1 is decoupled by C3 and applied to the inputs at pin 6 and 9 via R1 and R2. The input signals are capacitively coupled through C1 and C2 respectively in order to prevent the bias from being affected by the impedance of any previous stage. The input impedance of the LM377N is relatively high and therefore the coupling capacitors can be fairly small in value.

In the upper amplifier of Fig. 2, the feedback is taken from the output at pin 2 through R5 to pin 7. The voltage gain is equal to R5/R3 which is 50 times or 34dB. The gain may be increased by reducing R3 but the distortion will increase.

Similarly, the gain of the lower amplifier is R6/R4=50. The typical gain of an amplifier without any feedback is 30.000 (90dB).

The mean output potential is equal to approximately half the supply voltage. An electrolytic capacitor (C6 and C7) must therefore be placed between the outputs of the device and each speaker so that direct current cannot flow. If the value of the capacitors is reduced, an inferior bass response will be obtained.

Power supply

The LM377N can be fed from a supply line having any value between 10V and 22V. The absolute maximum supply voltage is 26V, but one should always allow a safety margin to avoid the risk of damage to the device.

A current of about 15InA is taken from a 20V supply when no signal is applied to either input, but the current rises towards 1A when full output power is being delivered to the speakers.

The maximum output power which can be obtained from each channel depends on the supply voltage used and also by the speaker impedance. A typical LM377N provides 2.5W per channel when fed from a 20V supply into 8Ω speakers, whilst all devices should provide a minimum of 2W per channel under these conditions.

The LM377N can dissipate up to about 2.5W continuously without a heat sink, but if the centre pins

of the device are soldered to $2\cdot 5$ sq. in of copper on a printed circuit board, the maximum dissipation is increased to about $4\cdot 2W$. Some form of heat sink seems required when an 8Ω speaker is employed, unless the power supply voltage does not exceed about 14V. In practice, however, the device is seldom operated at maximum power level for more than a moment (unless one likes to listen to sine waves!). Normally one is not likely to require a heat sink when using supply voltages of up to 18V provided that the speaker impedance is not less than 8Ω .

, Mono Amplifier

A single LM377N device can be used in a single channel system to provide an output power of 4W, Fig. 3.

continued on page 1086

PRESELECTOR for

10-30MHz

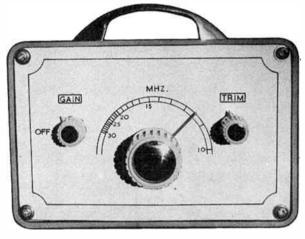
F. G. RAYER G30GR

ANY receivers are susceptible to second channel interference when working on the higher frequencies. This means that if the receiver employs an intermediate frequency of 470kHz, the oscillator is working at a frequency 470kHz higher than that of the wanted transmission and signals which are 470kHz higher than this, or 940kHz higher in frequency than the wanted transmission, can beat with the receiver oscillator frequency, to produce a signal which passes through the 470kHz amplifier, interfering with the wanted signal. On the lower frequencies, there is usually sufficient selectivity ahead of the mixer to avoid difficulty from this cause. But on higher frequencies, the receiver is unable to totally eliminate the offending signals which cause interference and whistles.

Even a well-designed receiver with one RF stage may not provide second channel rejection better than 15dB at 30MHz. If a signal strength scale of 6dB per S-point were used, as is quite usual, this would mean that if a wanted signal read S9, an unwanted signal of equal strength 940kHz higher in frequency would read S6+, which is a severe level of interference.

Such interference can be greatly reduced by raising the receiver intermediate frequency, or by increasing the second channel rejection ahead of the mixer. Changing the IF is probably impossible, but the unit here will enormously increase the second channel rejection.

The maximum benefit will be found with receivers which have no tuned RF stage, or only one RF stage, and employ a 455-470kHz intermediate



Completed preselector in its 6x4x4in cablnet.

frequency. With such receivers, 19m broadcasts may greatly mar reception of 20m amateur signals, for example. The unit can also be employed with other receivers including those with a 1.6MHz or other IF.

CIRCUIT

This is shown in Fig. 1. As second channel interference is not usually troublesome at signal frequencies lower than about 10MHz, the unit covers approximately 10MHz to 30MHz in a single band, thus avoiding any need for band switching. L2 and

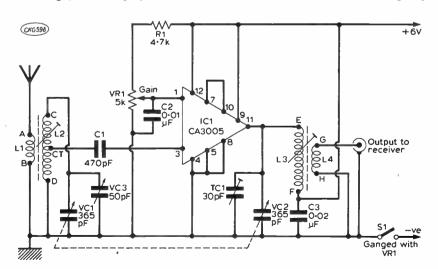


Fig. 1. Circuit of preselector using a single integrated circuit. Input, output and battery connections are at the rear. When placed between aerial and receiver useful galn will result as well as a reduction in second channel interference

L3 are tuned with the ganged capacitor VC1/VC2 providing two extra tuned circuits before the receiver. In most cases this will almost completely eliminate second channel interference. VC3 is a panel trimmer to allow peaking the aerial circuit with almost any aerial.

The CA3005 IC operates with a 6V supply. It is listed as giving 20dB gain at 100MHz, but the full gain is not achieved here due to the circuit being arranged for operation from a single power supply, and because of the difficulty of matching the input and output impedances at all frequencies. The input is approximately matched by the centre tap on L2, while the transformer L3/L4 is arranged to give an output impedance suitable for most receivers.

Gain control is provided by VR1, to avoid overloading the receiver on strong signals.

IC BOARD

The board is wired as in Fig.2. Note that the projection on the IC corresponds to lead 12. Spread the leads slightly so that they may pass through the Veroboard holes as indicated.

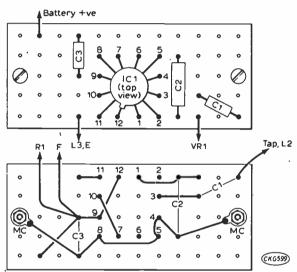


Fig. 2. Both sides of the small circuit board that carries the IC.

Two 6BA bolts with tags form the earthing points MC. Leave projecting leads from C1, for battery positive, VR1 and for VC2. Also solder on R1.

COILS

These use 24swg enamelled wire throughout, Fig. 3. For the aerial coil, begin at C as near the top of the former as possible, and wind on 4^{1}_{2} turns. Scrape the wire and twist the centre tap. Wind a further 4^{1}_{2} turns and finish at D. Leave a small space and beginning at A wind on 4 turns, finishing at B.

For the second coil, wind 9 turns from E to F, leave a space as before, and put on 5 turns from H to G.

The ends of the windings can be secured with a loop of cotton lightly smeared with quick-drying adhesive, and given a turn or two round the former. Fix one end by this means, wind on the turns mentioned, and secure the finish of the winding in the same way, pulling it tight by the cotton.

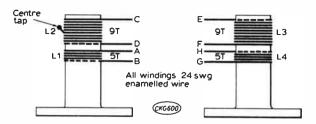


Fig. 3. Details for winding the two colls used in the preselector.

CHASSIS

The panel for the case listed is approximately 6 x 4in. Punch a clearance hole for the spindle of VC1/2. As this capacitor has an integral drive and the spindle cannot be cut shorter, it can be spaced back from the panel as in Fig. 4, to bring the knob nearer the front. This requires three 4BA bolts, each with two nuts, locked against panel and capacitor. VR1 and VC3 are also set back a little by extra nuts or washers.

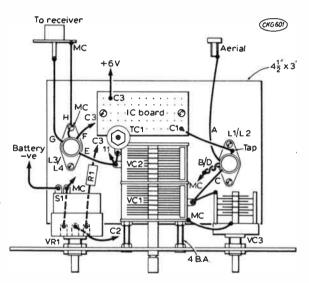


Fig. 4. Top view of the chassis showing position of the IC board and major components.

The chassis is a flat plate 4^{1}_{2} x 3in. It is secured by two short 4BA bolts which pass through it and into the threaded holes in the capacitor frame. Place a few washers between plate and capacitor.

* components list

Resistors

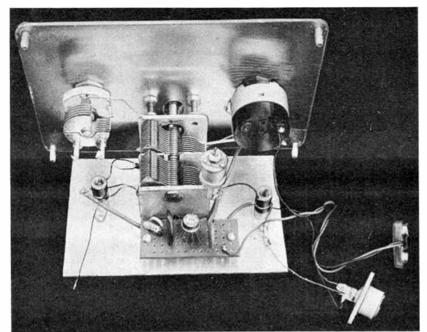
R1 4.7kΩ ‡W VR1 5kΩ linear with switch S1.

Capacitors

C1 470pF, C2 $0\cdot01\mu\mathrm{F}$ disc C3 $0\cdot02\mu\mathrm{F}$ disc. VC1/2 2 x 365pF with slow motion drive. VC3 50pF (Jackson C804) TC1 30pF trimmer

Miscellaneous

Formers for coils, %in dia. with cores (2). Knobs. ICI, CA3005. Aerial socket and output socket. Instrument case about 6 x 4 x 4in.



Holes are drilled to take the circuit board bolts which are locked with extra nuts. Wiring must be clear of the metal. The coils are held with 8BA bolts and nuts.

WIRING

Wiring is then completed as in Fig. 4. TCl has its lower tag soldered directly to the frame of VCl/2, the second tag being connected to VC2, together with the lead from pin 11, ICl.

The coil leads are cut to length, scraped, and soldered to the points shown. Note that H goes to the chassis at a bolt securing L3/L4.

The battery consists of four HP7 or similar cells, in a 4-cell holder. The holder is secured in the back of the insulated case, near the top, by a small bolt.

Finished preselector. Flexible connections are made to battery connector and output socket.

As the receiver employed a co-axial lead, a socket for this was provided as in Fig. 4. An earth circuit to the unit is then available through the co-axial outer conductor. If the receiver does not employ this type of aerial input lead, take a wire from G, L4, to the receiver aerial socket, and connect H and the chassis to the receiver earth terminal.

OPERATION

TCl can be set at about half maximum capacitance. Tune in a transmission on about 10MHz, set VCl/2 nearly fully closed and rotate the cores of the coils for best reception.

Subsequently check that 30MHz signals peak with VC1/2 nearly fully open, and that VC3 also peaks up signals or background noise. If necessary, readjust TC1 to allow proper tuning with VC3, and check the core positions, so that little adjustment of VC3 is required, when tuning across the whole hand.

Adjustments are best carried out by observing the receiver signal strength meter, or with the receiver AGC switched off, or by selecting weak signals which do not operate the receiver AGC. VR1 should be set for maximum gain when doing this. As an aid, a very short aerial may be temporarily taken to A. VC3 should then have quite a sharp peak, but this effect will be reduced with a long aerial when it may be preferable to place a small capacitor in the lead from aerial to A.

IC of the Month-continued from page 1083

The two amplifiers are used in a 'bridge' or pushpull circuit. The input signal is fed through C2 and R1 to the feedback input (pin 7) of the first amplifier and the same signal also passes through C1 to the non-inverting input (pin 9) of the second amplifier.

When the voltage at the pin 2 output increases, that at pin 13 therefore decreases by the same amount and vice-versa. The speaker is thus driven by this push-pull signal. This circuit has the advantage that no capacitor is required in series with the speaker, since the mean potentials of pins 2 and 13 are almost identical.

The bias from pin 1 is decoupled by C3 and fed through R2 to pin 6. It also passes through R3 to pin 9.

The gain of each amplifier is equal to the ratio of the feedback resistors, namely R4/R1=R5/R6=50. However, the push-pull action gives an effective overall gain of twice this value.

The LM377N is available from Athena Semiconductor Marketing Company Ltd., 140 High St., Egham, Surrey, at £2.70 plus VAT for small quantities, inclusive of p & p.

RADIO BY CABLE & SATELLITE

-continued from page 1087

Many countries have determined that this is unavoidable within the boundaries of the technical possibilities and it has been recognised by the UNO associated International Telecommunications Union in 1971 in Geneva. At the same time, however, it was established that the use of TV satellites is only possible by observing frequency, positioning and ground coverage plans which are to be drawn up at a special planning conference for this purpose which will take place in 1975/76.

EXPERIMENTAL WORKSHOP

We regret that due to pressure on editorial space this month, Part 6 of this series has been held over until the April issue.



LTHOUGH it is a task of exchange technology to handle the signals, in connecting individual communications (telephone, telex), in such a way that the connection is made quickly and reliably, broadcasting must ensure that the primary signal is transported long distances without distortion, be they telephone signals or for telegraphy, music, TV, picture transmission, data transfer or remote control. But what are the problems that arise?

A modern carrier frequency system with 2700 channels for speech has an amplifier spacing of 4.5 km; at a distance of 4500 km as is found in the trade area between the USA and Canada, 1000 ampli-

fiers are operated one after the other.

Assuming a medium amplification of 30dB (i.e. the signal output is increased each time by a factor of $10^3 = 1000$, the voltage by around a factor of $31 \cdot 6$) the overall amplification over the whole section amounts to the almost unbelievable figure of 10^{3000} . For comparison: the entire universe contains "only" around 10^{83} protons, since the creation of the earth approximately 15 billion years ago a total of "only" $5 \cdot 10^{17}$ seconds has passed.

Cables

To guarantee the necessary quality over so many stages, extremely high demands must be made, both on the technical equipment (amplifiers, converters, modulators etc.) as well as on the directions of transmission. With regard to the latter there are three "media" which have proved themselves and which are to be found predominantly or exclusively in long-distance traffic: cables, directional radio including satellites and—as a medium of the long-term future, suitably directed laser beams.

Cable, especially coaxial, is already considerably protected by its construction and laying against outside influences from space, the atmosphere and from technical installations, so that in cable transmission systems non-linearity and noise must be kept as low

as possible.

Disregarding the "symmetrical" carrier frequency cables, used predominantly with up to 120 speech channels for regional systems, there is a whole series of coaxial types at an impedance of around 75 ohm. There are many various internal sizes, e.g. from 1.2 mm for 300 speech channels or 2.6 mm for a choice of 960,1260 or 2700 channels. If one is prepared to reduce the amplifier spacing even more, one could increase the basic bandwidth considerably (e.g. to 40 to 60MHz or even higher).

"Hollow" cable recently developed can theoretically provide a transmittable overall bandwidth of around 100,000MHz. It is, in fact, a radio wave guide which should be most suitable for the transmission of digital signals (e.g. for pulse code modulation). Technically hollow cables are well advanced although there are certain reservations with regard to their economic application.

Satellites

The directional radio line, widely used for the transmission of TV modulation (video band) but also for multi-channel speech bands, is physically an ideal transmission medium. However, it requires the application of special "noise reducer" procedures due to the influences of extra-terrestrial, tropospheric and industrial radio signals. Partial bandwidths of up to 30MHz have shown themselves to be the best for the transmission of television or telephone channels in various frequency ranges between 2 and 12GHz. Transmitter output is in the area of several watts.

Satellite paths are basically extended directional radio lines with fields of 2 x 36 000 km length (to and from) with high transmitter outputs, extra large aerials and extremely sensitive receivers (maser) on the terrestrial stations. They are particularly suitable for trans-continental and trans-oceanic relays, operating at frequencies corresponding to those in directional radio technology.

A transmission medium of the future is the laser beam which is strictly monochromatic, polarised and coherent. In a free field of dissemination they are not practicable because of absorption as with normal light, but when suitably guided by lens conduction

and glass fibre, it reveals its full potential.

In particular the glass fibre bundle cable, offering an extreme bandwidth even with individual fibres, combined with the multifarious operating possibilities of universal cable, promises to be an important transmitting medium, both in long distance communications and in local traffic in densely populated areas. All of this is of course dependent on a corresponding advance in the components and subsystems in the field of optronics—an advancing technology being fully exploited now.

Satellites providing a country with programmes via only one transmitter can of course be received across borders. Even with rays with a one degree focusing, whose focal area is accommodated within the boundaries of the country cannot prevent this.

-continued on page 1086

Vicillo/cope

PART 1

techniques alan ainslie

In this series we shall be taking a close look at oscilloscopes of the kind likely to be used by the average electronics enthusiast. This leaves a large range of classes of instruments, but we shall not be too concerned with the developments incorporated in the brand new, four figure price oscilloscopes as these can generally be classed as purely professional in appeal and application.

The instruments to be considered will range from the simplest types of scope, through TV service scopes to the laboratory scopes of a few years ago, now available to the keen amateur—but at a price!

We shall consider design principles, the basis for modifications, and calibration. This last point is rather important as manufacturers can charge a lot for recalibration of their instruments, especially if not of current manufacture.

We shall also look at some oscilloscope applications and at a few pieces of additional equipment in order to carry out an increased range of tests and measurements.

Oscilloscopes fall broadly into four main classes:-

- 1. AUDIO FREQUENCY
- 2. TELEVISION AND PULSE
- 3. LABORATORY
- 4. SPECIAL PURPOSE

Ignoring the special purpose scopes for the time being, the oscilloscopes are grouped into a convenient scale of ascending bandwidth.

BANDWIDTHS

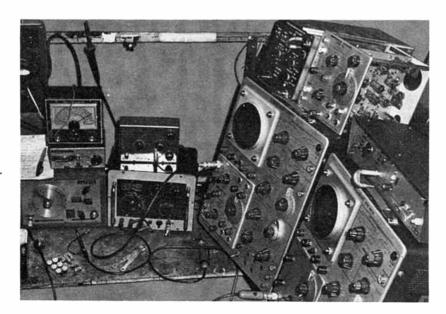
As most scopes have a low frequency limit of DC (DC coupled) or a few Hz, the bandwidth figure quoted is the upper frequency limit at 3dB down (or however else the manufacturer specifies).

The bandwidth information gives an indication of the highest frequency that the scope can predictably handle.

Considering the two curves in Fig. 1, both scopes would have a written bandwidth of 5MHz, but scope A would in fact perform quite well past this figure whilst scope B drops straight off. Scope A could be used but with loss of calibration up to perhaps 10MHz or so, scope B being totally useless at this frequency.

Incorporated in any statement concerning bandwidth is an implication of the rise time of the scope.

If we consider an oscilloscope amplifier displaying a 1MHz signal, and this signal is at the -3dB point, we can arrive at some justification for the rather mysterious equation used to express rise time in terms of bandwidth.



This imposing array of test equipment in just one corner of the author's workshop will serve to underline the fact that this series of articles on the oscilloscope contains much practical information as well as theoretical discussion.

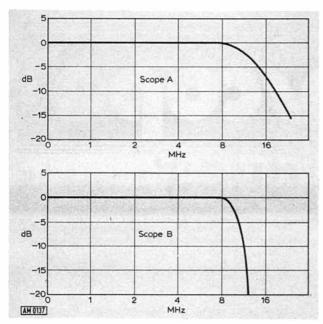


Fig. 1. The response curve of the Y amplifier in two different oscilloscopes, to illustrate the meaning of "bandwidth."

The time period of the 1MHz signal is 1μ sec. Thus for one half period the time is 500ns and for the rising portion 250ns. If now the slope of the upward going part of the cycle is taken to represent the step function applied to the scope, then the rise time of this 1MHz (3dB down) scope would appear to be 150ns.

But the lMHz signal is not of 100% amplitude (it is 3dB down), and as rise time Tr is defined as the time to increase a step function from 10% to 90%, a correction is required, Fig. 2.

As 3dB down corresponds approximately to 30% down, i.e. the trace height at the -3dB point is only 70% of what it should be.

It is necessary to bring the 70% trace to 90% and in doing this Tr is increased by 90/70 giving a theoretical rise time of 322ns.

In practice the figure is found to be between 350 and 390ns, depending on the shape of the response. The response curve of Fig. 1, scope A would give a faster rise time than that of scope B, although both have the same bandwidth.

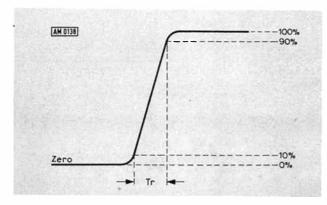


Fig. 2. First part of a response curve with a step function input to the scope. The rise time is a function of the bandwidth of the amplifier.

Taking the rise time to be 365ns for a lMHz scope and applying the laws of proportion we get the expression:—

Rise Time (ns) \times Bandwidth (MHz) = 365

This expression holds true for the vast majority of cases, but more about that when we come to consider the Y amplifiers in more detail.

Returning to our classification of oscilloscopes it seems reasonable that the audio oscilloscope has but a limited bandwidth (1MHz or so) while the TV or pulse oscilloscope has a bandwidth of perhaps 10 or 15MHz and is capable of displaying more complex and more rapidly recurring waveforms. The laboratory scope on the other hand has a bandwidth extending from 15MHz and up and into the hundreds of MHz on the very latest real time oscilloscopes.

Using sampling techniques (imaginary or virtual time) bandwidths into the GHz region have been achieved but this type of scope belongs to the special purpose class. It is interesting to think of the real time response of say a 5GHz scope, 10 % to 90% in 7×10^{-11} sec, quite fast!

Returning to earth, although it is convenient to classify a scope by bandwidth (or rise time) there are other, perhaps more striking, differences between the classes of scopes.

TIMEBASES

The uses of an audio oscilloscope are confined usually to periodic waveforms that can be adequately displayed by the use of a synchronised time-base without the need for complex and expensive trigger circuits. The difference between a sync or trig timebase will become clear when we come to consider more fully the numerous methods used to provide a timebase. Suffice to say that the sync timebase is a free running oscillator which is pushed along by a portion of the Y signal applied as sync, whereas the trig timebase waits for a suitable signal before commencing a sweep.

One consequence of the sync mode is that the input signal (Y) must have a repetition frequency higher than that of the timebase for a stable image to result, as in Fig. 3. If the timebase is run faster than the repetition rate of the waveform, in order to view detail the trace folds up into a jumble.

Applied to the audio scope this latter effect is not of too great a consequence as there is usually little detail lurking in a signal repeating at 10kHz. However in TV work we immediately become faced with complex waveforms to lock and also the possibility that the waveform may be required to be investigated more closely.

The triggered timebase becomes a necessity together with the improved Y amplifier bandwidth. The timebase speed ranges are also increased for greater versatility and various modes of timebase operation are employed, including the important addition of an "EXTERNAL TRIG" connection enabling the timebase to be controlled externally. This facility is invaluable in TV work as it enables the frame generator in the receiver to work as a delay timebase generator, the trig level control on the scope selecting the lines to be viewed in isolation on the screen.

This sort of facility necessitates yet another improvement to be made to the simple audio scope, namely the trace brightness.

Fig. 3. The top display occurs when the timebase runs faster than the repetition rate of the input waveform. The consequence of a timebase running slower than the repetition rate is shown in the lower display.

A recurring 1kHz sine wave may be bright enough, but when the trace is scanning say 10cm in 64 sec, and then only 25 or 50 times a second, the trace brilliance falls to almost vanishing point unless high CRT potentials are employed. Usually between 2 and 5kV are used of oscilloscopes this nature, as opposed to possibly less than 1kV for the audio scope.

The TV or pulse oscilloscope then has, apart from an improved bandwidth, a fairly sophisticated timebase

system and an improved display mechanism, together with a few other improvements such as DC coupling and the provision of calibrators.

Oscilloscopes intended for reasonably accurate measurement, but that are built to a price, usually incorporate some method of generating standard waveforms of precise voltage and/or time, this being cheaper than trying to stabilise the Y amplifier gain and timebase against variations.

A fairly typical example of the type of calibration provided is the Cossor 2000 oscilloscope, a 5MHz double beam scope suitable for general TV service and measurement.

The Y amplifiers are calibrated against an internally generated signal of 300 mV. The Y amplifier control is set to give 3 cm deflection with the input attenuator set at 0.1 V/cm.

The 300mV signal is obtained from 50Hz from the scope mains transformer and a small neon is used to provide a reference level of about 70V from this high voltage AC. The resulting 70V square wave is then attenuated and is available as the 300mV calibration signal.

Time calibration is available as a 20MHz oscillator providing intensity modulation of the beam. This means that a display brightens up at every 50ns enabling accurate time measurements at the higher sweep speeds.

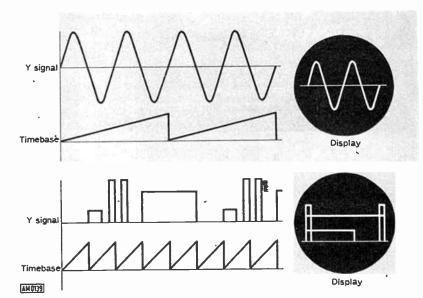
LABORATORY SCOPES

The final class of scope that we shall consider is the laboratory scope and in this class we can conveniently consider the special purpose oscilloscopes.

In general one expects to find that a laboratory scope has a good bandwidth, versatile timebase with fast sweep speeds, high tube voltage and is capable of long lasting calibration to within a few per cent, depending on the measurement methods employed.

Intended for use in research and for the investigation of complex waveforms, the laboratory oscilloscope needs to be versatile and has therefore rather a lot of controls and tends to be physically large.

As we shall see later, wide bandwidth deflection systems require a large number of valves passing



fairly high currents. This, together with the number of valves in the timebase (usually two are provided) and the supply regulator needed to maintain calibration, means that the valve count is sometimes over a hundred and a power consumption of almost 1kW is not uncommon. These big scopes are usually trolley mounted with a fan to keep the operating temperature at a reasonable level.

TEKTRONIX TRENDS

Pioneers in this field of scopes were undoubtedly the American firm Tektronix and many other manufacturers have done a lot of copying from the Tektronix design. The Tektronix format of tube in the top left corner, Y amplifier below, and timebase down the right-hand side is now familiar to users of laboratory scopes.

With the advent of Tektronix styling came another innovation, perhaps conceived initially by the same company and now copied by many, that of plug-in Y amplifiers, followed by plug-in almost everything! This means that a wideband (33MHz for Tektronix) main frame can be used for a number of special purposes just by changing plug-in units.

The main frame houses the CRT, power supplies, Y drive amplifier, X amplifier and the timebase if this is not plug-in. A range of Y plug-ins would then be used with the scope, providing double beam operation, differential inputs, very high sensitivity or a special function such as a spectrum analyser or four channel display. If plug-in timebases are provided these could be normal timebase, delay plus normal, very slow, or a straightforward amplifier plug-in for XY display.

Whilst appreciating that these plug-ins can cost a great deal of money it is fairly obvious that a selection of plug-ins is cheaper than a selection of scopes! The user is also able to keep in touch with current technology by the purchase of recent plug-ins offering such facilities as sampled inputs giving very high apparent bandwidths, although not in real time. One other advantage of plug-ins is that the Y amplifier controls probably get the hardest use on a scope and it is an easy matter to remove the plug-in for maintenance without having to disembody the whole scope.

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AC176 AC187 AC188	14p 12p 12p	BC108 BC109 BC147 BC148	10p 11p 12p 12p	MJE370 MJE520 OC26 OC28	57p 52p 40p 40p	2N1307 2N2926 2N3014 2N3053	9p 10p 20p	O A 200 O A 202 1 N 91 4 1 N 4 0 0 1 / 2	8p 8p 5p 6p
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AF116 AF117 AF118 AF124	12p 12p 40p 22p	BC179 BD131 BD132 BF194	14p 49p 49p 15p	OC45 OC70 OC71 OC72	10p 10p 10p 10p	2N3705 2N3706 2N3707 2N3819	11p 11p 11p 25p	1N4148 BYZ11 WO1 WO6	5p 18p 30p 34p

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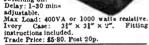
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0-6	0-6	1000	1000	212	1.28	0.22
9-0-9	_	100	_	13	0 - 95	0.10
0-9	0-9	330	330	235	1.28	0.10
0-8-9	0-8-9	500	500	207	1.70	0.22
0-8-9	0-8-9	1000	1000	208	2.80	0.30
15-0-15	_	40	_	240	1.28	0.10
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20-0-20		30	_	241	1.09	0.10
0-20	0-20	150	150	237	1.28	0.10
0-15-20	0-15-20	500	500	205	2.16	0.38
0-20	0-20	300	300	214	1.36	0.22
20-12-0-1	12-20	700(D/	C)	221	1 · 21	0.30
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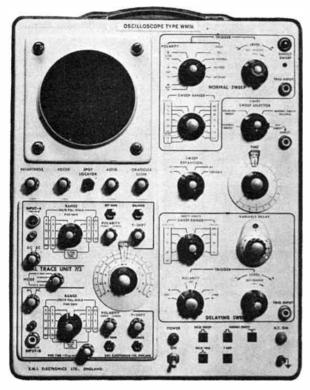
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SAMPLING TECHNIQUES

The group of scopes classed as "special purpose" can be extended to virtually any scope not corresponding to the norm, and, in a way, most scopes have a little something special since they have to appeal to buyers, just like motor cars.

Perhaps the most important special purpose scope, to be found in few amateur labs, is the sampling

oscilloscope.



A close-up of the front panel of one of the author's scopes. This EMI WM16 has plug-in facilities, dual timebases and a bandwidth of better than 40MHz.

Considered on a real time basis the sampling scope has a bandwidth of a few tens of MHz. However, a special input circuit, usually contained in the probe, samples the instantaneous level of the signal at a rapid rate and the probe output when fed through the Y amplifier produces a display that builds up in a very short space of time to a continuous display.

Various manufacturers use different sampling techniques but the results obtainable represent bandwidths well into the hundreds of MHz and

beyond.

A useful result of the development of sampling techniques has been the production of a circuit which when connected to an oscilloscope deflection amplifier's outputs, enables the trace on the screen, perhaps a 5MHz pulse, to be drawn by a mechanical plotter which takes about 10secs to complete one accurate scan. The technique used is similar to sampling oscilloscopes, the input to the XY plotter being sampled over say 10 seconds. The resulting XY plot is a faithful reproduction, within the plotter resolution, of the trace that was on the scope face, although not in real time as it takes 10 seconds to draw a signal of, say, 100ns width.

Other special oscilloscopes are designed to do specific jobs and there are such things as spectrum analyser scopes produced. In this scope the Y channel is narrow band, the precise band being determined by the X deflection voltage. Thus as the timebase sweeps, usually fairly slowly, the Y amplifier sweeps a certain range of frequencies, the Y deflection being proportional to the signal at that frequency. The X axis can be calibrated in frequency and such a scope can be used for investigating modulation sidebands etc.

Storage scopes also fall into the category of "special purpose" if only by virtue of the very high price. We shall consider storage tubes in the next section dealing with displays, but suffice it to say here that a special tube is employed which enables a trace to be retained after the scan is completed. These scopes are very useful for low speed servo work and in conjunction with spectrum analyser facilities, as mentioned above, flicker can be completely eliminated.

To be continued



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... Detailed instructions required for filting new belt to Akai 4000D tape deck.—T. Fieldhouse, 100 Wortley Heights, Leeds LS12 1JF.
... Any info on BUSH EBS 4 RADIO all replies answered.—K. Eskriett, 63 Paley Road, Bradford, Yorks, BD4 7EL.
... For, AF61335 Freq. Swept Generator, CT202. Handbook BR1771(14) or circuit diagram. Buy loan of copy, any info welcome.—T. E. Wicks, 12 Kensington Ave, Watford, Herts. WOI TRY.
... ang gen on the U.S.N. transceiver Type CR1-4344—a unit of Model TBY-B made by Colonial Radio Corporation, Buffalo, N.Y. Even band-coverage gen would help.—H. W. Boyett, G6CZG, 66 Freshbrook Road, Lancing, Sussez BN15 6DA.
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No. 58 GRIP TESTER

A series of simple transistor projects, using not more than twenty components.

THE objective when using this piece of equipment is to hold a probe (made of aluminium foil folded round a piece of wooden broom handle) in each hand and squeeze the probes as hard as possible. The tighter the grip the more the lamps will become illuminated. But more than this; the lamps come on in a set sequence. A weak grip will make only one lamp glow faintly but a very strong grip could make all three lamps glow brightly. An intermediate grip may only illuminate two lamps. The circuit shown in Fig. 1 is designed to operate three lamps this way but can be extended to operate as many as are required if the instructions are followed.

is reached when it might be more economic to use a zener diode. For more than four indicating stages R2 ought to be reduced to 220 ohm. The sensitivity of the unit is controlled by VR1. Reducing its value lowers the sensitivity and requires a stronger grip to get the lamps to light up.

* components list

R1 1kΩ ‡W R2 470Ω ‡W R3-5 1kΩ ‡W VR1 200kΩ linear potentiometer
D1-6 1N4148 Tr1-4 BC108 LP1-3 6V 40mA Battery 9V Probes Veroboard

Circuit

Trl is an emitter follower and the potential at its emitter is set by the potential divider effect of R1, VR1 and the body's resistance plus contact resistance between the palms of the hands and the probes. The lower the skin and body resistance the higher will be the emitter potential. Skin contact resistance can, to some extent, be controlled by the pressure of grip on the probes and this affects the emitter potential.

This potential is used to provide base current into each of the following emitter lamp grounded drivers but the silicon diodes in series with each of the bases ensures that in the case of Tr2 the output from Trl must be higher than 1.2V while for Tr3 it must be 1.8V and for Tr4 should exceed 2.4V. Thus, when the grip is weak the potential from Trl might only be 1.6V and in this case LP1 will be the only lamp illuminated but if it is 2.2V Tr3 will be starting to conduct and LP2 will start to glow while LP1 glows even more brightly. The diodes are there simply to provide potential increments for consecutive stages and the technique of adding one extra to each stage could be continued until some point

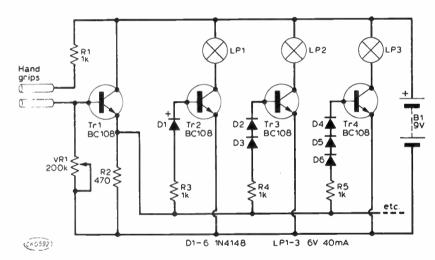
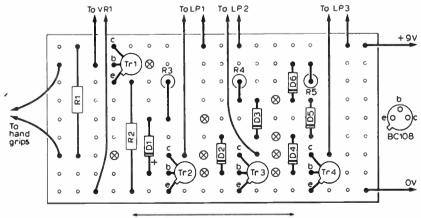


Fig. 1, above, is the circuit for a four stage tester and a suggested layout on plain veroboard is shown in Fig. 2, below.



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				PC88	0.75	PL504	0.88	PCF800	1.05
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DY51	0.85	EF83	1.03	PC900	0.58	PL509	1.55	30C18/	
DY86/7	0.42	EF85	0.43	PCC84	0.52	PL802	0.96	PCF805	0.90
DY802	0.45	EF86	0.90	PCC88	0.80	PY33	0.66	30F5/PF8	318
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EB91	0.88	EF91	1 80	PCC189	0.65	PV82	0.55	30FL1/	
EBC81	0.75	EF92	1.40	PCF80	0.51	PY88	0.60	PCE800	0.75
EBF80	0.60	EF95	1-35	PCF82	1.80	PY500A	1.05	30FL2	0.75
EBF83	0.62	EF183	0.60	PCF86	0.65	PY800	0.50	30FL12	1.05
EBF89	0.58	EF184	0.60	PCF200	0.85	PY801	0.50	30FL14	0.85
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ECC81	0.45	EL36	1-05	PCF802	0.71	U193	0.50	201101	
ECC82	0-43	EL81	0.90	PCF806	0.66	UABC80	0.90	30L15/PC	
ECC83	0.45	EL84	0-47	PCH200	0.88	UBC81	0.70		1.05
ECC84	0.55	EL85	0.55	PCL82	0.54	UBP89	0.80	30L17	0.80
ECC85	0.58	EL86	0-95	PCL83	0-66	UCC85	0.60	30P4MR	1.30
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ECH83	1.00	EY86/87	0.42	PFL200	0.80	6/30 L2/			0.95
ECH84	0.78	EY88	0.64	PL36	0.88	ECC804	1.00	30PL13/	
ECL80	0.53	EZ80	0.51	PL81	0.75	6F23/EF8		PCL800	1.20
ECL82	0.61	EZ81	0.40	PLSIA	0.88	,	1.05	30PL14/	
ECL83	0.68	G Y501	0.90	PL82	0.50	30C1/PCF		PCL88	1.25
ECL86	0.63	GZ34	0.78	PL83	0.96	,	0.51	30PL15	1.05

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DL92 0-4		50 PCF802 50 PCF805	0.50	1T4	0.30	12AT7	0.40
DL94 0.4		50 PCF806	0.75	384	0.40	12AU6	0.45
DL96 0-1		90 PCF808	0.90	3V4 5R4GY	0.70	12AU7	0.88
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EABC80 0-		40 PCL84	0.45	5 Y3GT	0.45	30C1	0.80
EAF42 0:		-00 PCL85	0.50	524G	0.45	30C15	1.05
EB91 0-9		45 PCL86	0.45	6/30L2	0.90	30C17	1.10
EBC33 1-0		60 PCL805/		6AK5	0.40	30C18	0.90
EBC41 0-2 EBC81 0-2		85 00 PD500	0.50	6AM5	0.80	30F5	1.10
EBF80 0-4		00 PD500 40 PEN45	1·80 0·75	6AQ5	0.45	30FL1	0.80
EBF83 0		40 PL36	0.55	6AB7G 6AT6	0.85	30FL2	0.75
EBF89 0.		75 PL81	0.50	6AU6	0.45	30FL14	0.90
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BC184L	0.13	MPF103	0.36	T1005	0 20	2N1304	0.22	2N3906	0.16
BCY32	1.20	MPF104	0.35	TIC44	0.29	2N1305	0.22	2N 4056	0.15
BCY33	0.38	MPF105	0.46	TIC226D		2N1306	0 28	2N4059	0.10
BCY34 BCY70	0.45	NKT404	0.60	TIL209	0.25	2N1307	0.28	2N4060	0.18
BCY70	0.15	OA5	0.60	T1843	0.26	2N1308	0.28	2N4061	0.13
BCY71 BCY72	0.20	OA10 OA79	0 40	ZTX 107 ZTX 108	0.12	2N1309	0.30	2N4062	0.14
BCZ11	0 65	OA81	0·10 0·10	ZTX300	0·10 0·14	2N1613 2N1614	0.20	3N141	0.81
BD121	1.00	OA91	0.7	ZTX301	0.14	2N1614 2N2147	0·45 0·75	40360	0.40
BD124	0.80	OA200	0.08	ZTX 302	0.20	2N2160	1 00	40361 40362	0.45
BD131	0.45	OA202		ZTX304	0.24	2N2369A		40430	0·40 0·85
	_								0.99
BN7400	0.20	8N7425	0.37	BN7473	0.44	8N74107	0.51	8N74157	1.09
8N7401	0.20	8N7427	0.37	8N7474	0.48	BN74110	0.57	BN 74170	2.88
8N7402	0.20	BN7428	0.43	8N7475	0.59	8N74111	0.86	8N74174	1.80
BN 7403 BN 7404	0.20	8N7430 8N7432	0·20 0·37	8N7476 8N7480	0.45	8N74118	1.00	8N74178	1.29
8N7405	0.20	8N7433	0.43	8N7482	0.80	8N74119	1.92	8N74176	
BN7406	0.40	8N7437	0.48	8N7483	1.20	8N74121 8N74122	0.57	8N74190	
8N7407	0.40	BN7438	0.43	BN 7484	1.00	8N74123	0.80	8N74191	2.30
BN7408	0.25	8N7440	0.20	BN7486	0.50	8N74141	1.00	8N74192 8N74193	2:30
8N7409	0.33	BN7441A1	N .	BN7490	0.75	BN74145	1.44	BN74194	
8N7410	0.20		0 85	8N7491A	N	8N74150	2.30	BN74195	
8N7411	0.28	BN7442	0.85		1.10	8N74151	1.15	BN74196	1.58
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8N7417	0.80	8N7453 8N7454	0.20	8N7494	0·85 0·85	8N74156	1.15	8N74198 8N74199	2.88
8N7420	0.20	8N7460	0.20	8N7496	1.00	DIL			
BN7422	0.28	BN7470	0.33	8N7497				14 pin	15p
BN7423	0.40	8N7472	0.38	8N74100	2.16	SOCKET	rs	16 pin	17p
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BROADCAST

SHORT WAVE DX by MALCOLM CONNAH

HE receivers used by Broadcast Bands listeners vary enormously; they may be ex-government sets or brand-new commercial units; but all receivers have one thing in common: They will not give their best performance until they are used with a good aerial system.

When we talk of an aerial system we include any devices, such as aerial tuning units, which are placed

between the aerial and the receiver.

In order to get optimum reception the aerial system must be resonant at the frequency of reception. Amateur Bands listeners, and operators, have an advantage here because their bands, with the exception of 15 metres, are closely related. These bands are 10, 20, 40, 80 and 160 metres. If an aerial system is resonant on 80 metres it is a relatively simple matter to get it to resonate on 40, 20 and 10 metres.

The Broadcast Bands, however, are completely unrelated being 11, 13, 16, 19, 25, 31, 41, 49, 60, 75, 90 and 120 metres. If one of these bands is of particular interest a half-wave dipole may be erected for that band. The only practical solution for all band reception is to use some form of end-fed aerial. It should be noted that the term 'long-wire' is often used incorrectly, a misuse of which I have been guilty, as this is strictly an end-fed aerial which is long in relation to the wavelength being received.

The length of aerial that can be erected depends on the amount of space available, but the usual compromise is between 50 and 100 feet long. Theory dictates that the aerial should be straight, but many people have had very good results with aerials that have been bent in order to fit them into the space available.

The aerial should, preferably, be an outdoor one erected at a reasonable height and located as far away as possible from such obstructions as buildings and trees. A very simple aerial tuning unit (such as that described by David Gibson in the January 1974 issue) should then be constructed in order to make the aerial system resonant on the desired bands.

Readers' Logs

David Kernick of Prescot, Lancashire used his Grundig TR600A portable with only just the built-in telescopic antenna to hear the following.

6070 R. Sofia, Bulgaria at 1930.

7145 R. Kiev in English at 0030.

7215 All India Radio in English at 2000.

9550 R. Finland noted at 1805.

9670 Adventist World Radio at 0930.

9695 V. of Saudi Arabia, Arabic at 0405.

9745 R. Baghdad, Iraq noted at 1945.

9770 R. Australia, English at 1605.

9833 R. Budapest, Hungary at 1615.

11920 R. Algiers noted at 1900.

11970 R. Tunis in Arabic at 0920.

15140 R. Havana, Cuba in French at 1935.

15165 R. Denmark in Danish at 1850.

15240 R. Belgrade, Yugoslavia at 1530.

15410 United Nations Radio at 1600.

17755 HCJB, Quito, Ecuador at 1930.

17780 RSA, South Africa noted at 1600.

17845 WYFR noted in English at 1730.

17865 WINB, Red Lion, music at 1930.

21630 V. of Saudi Arabia, testing at 1110. Richard Staples has found an Eddystone 680X in the loft (excuse me whilst I return my ladder to garage)

and the addition of a 100 foot end-fed aerial produced:

3999 R. Godthab, Greenland in Danish at 0840.

4820 Voz Evangelica, Honduras at 1805.

4940 R. Yaracuy, Venezuela, Spanish at 1740.

5920 R. Kiev, news in English at 1800.

9590 R. Australia noted in English.

9610 R. Canada in English at 2115.

11720 R. Nacional, Brazil, Portuguese at 0705.

11935 R. Pakistan, news in English at 1715.

15200 RSA, South Africa in English at 0840.

21695 Greek Military Radio, Athens at 0905.

Christopher Hodgson of Sunderland reports that Radio WYFR (Family Radio Inc.) broadcasts in English to Europe at 1810 GMT on 15130kHz. The station replied to his report in about two weeks and the address for reports is: WYFR, 290 Hegenberger Road, Oakland, California 94621, U.S.A.

With his usual equipment: Codar Multiband 6, P.W.

A.T.U. and 50 foot end-fed; Christopher also heard:

7080 Voice of Vietnam, Hanoi at 1820.

7210 Red Cross Broadcasting at 1700.

9505 VOA, Tangier, in Rumanian at 1930.

9525 All India Radio at 2010.

9540 Radio Tashkent noted at 1210.

9545 Radio Ghana, s/off at 2215.

11805 WYFR-Family Radio at 2100.

15130 WYFR—Family Radio at 1810.

15175 RSA, South Africa, s/off at 1850.

15185 R. Finland noted at 1830.

15290 ORTF, Paris, s/off at 1115.

15415 Radio Kuwait, s/on at 1730.

15420 BBC, East Med. relay noted at 1600.

17820 R. Canada, s/on in Polish at 1530.





VHF/FM

by SIMON DAVID

HOGMANAY was celebrated in Scotland in a different way than usual. No doubt the timing was deliberate for Radio Clyde, Scotland's first commercial radio station, broadcast on 95·1MHz on December 31st. The station started at 10.30 p.m. with news and introductions to the staff. The 4kW transmitter is at Black Hill.

The criticisms and doubts surrounding London Broadcasting, the London news stations, resulted in the resignations recently of the Managing Director and Chief Editor. Former Lord Mayor of London, Sir Charles Trinder, also walked out issuing an admission that the finances had not lived up to expectations. One thing evident is the difference between some commercial and BBC local radio broadcasts from a technical standpoint and although both have severe financial restrictions, it is only to be expected that the latter has the advantage of drawing on the resources of its "great-auntie".

I have been informed that BBC Radio Derby is still operating on 96.5MHz from Sutton Coldfield using slant polarisation. The 94.2MHz transmitter that I mentioned recently is installed at the studio to fill-in the town centre area because of surrounding high ground. It uses a vertically polarised aerial and 10 watt transmitter.

The Radio Derby aerial at Sutton Coldfield is a 5-element Yagi array 500 feet above ground level. It provides a maximum e.r.p. of 5kW in the Derby direction.

Also from Derby, Roy Patrick reports that the Lichfield IBA transmitter for the Birmingham area is due on the air on 94.8MHz in February; the Manchester commercial station is due on 97.0MHz (2kW) in March; the Swansea station is expected to start transmitting on 95.1MHz (1kW), using the circular type of aerial, later on in the summer of 1974.

Last month I reported on the results of using the Antiference FM264T six-element aerial. Results since then have been repeated with the addition of Rouen on 96 6MHz. Unfortunately conditions have not favoured reception from Rheims.

MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

AVE KERNICK (Prescot, Lancs) has a Grundig TR600A transistor portable with a built-in ferrite rod antenna, which he has found to be an excellent receiver for pulling-in distant stations. He reports hearing programmes in English from AFN Frankfurt 872kHz; Deutschlandfunk, West Germany 1268kHz at 1745hrs; Radio Norway 1578kHz at midnight; Radio Sweden 1178kHz at 2245hrs; Radio Tirana, Albania 1457kHz (additional frequency for the English Service) at 0330hrs; together with Sud Radio, Andorra in French at 2245hrs on 818kHz and Tripoli, Libya in Arabic at 0025hrs on 1250kHz. Dave asks if it is possible to hear North America on the medium waves using a portable receiver. This is unlikely as a ferrite rod aerial does not have enough pick-up to receive really distant stations. DXers who want to try for North Americans should use an external aerial or a medium wave loop such as the DXers MW Loop Aerial described in the April 1973 issue of Practical Wireless.

Readers' Logs

Roy Patrick (Derby) reports hearing the new Independent Broadcasting Authority (IBA) station at Manchester testing on 1151kHz at 1100hrs on December 1st and IBA Birmingham using test tones on the same channel. IBA stations in the provinces are expected to use 1151kHz for stations at Manchester, Birmingham and Glasgow (R. Clyde); 1169kHz for Swansea and 1546kHz for Liverpool and Edinburgh.

R. B. Callwood (Munich, West Germany) reports hearing BBC Radio 1 (1214kHz) at 1300hrs on his

car radio while driving on the autobahn between Munich and Frankfurt. Reception was on a single occasion only and he wonders if any other reader has received BBC Radio 1 in Germany.

Bill Thorne (London) asks for information about the French broadcasts on 584kHz (513m) which he listens to regularly. The station on this frequency produces programmes for the Paris area for the greater part of the day and has a power of only 5kW. The address is O.R.T.F., 116 Avenue du President Kennedy, Paris 16eme France.

Brian Murray has heard IBA Radio Clyde testing on 1151kHz at 1345hrs and he reports that this station is due on the air on December 31st, 1973. Brian has been busy again with his Astrad VEF 204 receiver using an old band 1 TV aerial as a medium wave antenna. His log includes programmes in English from Radio Warsaw 1502kHz at 0115hrs; Radio Sweden 1178kHz at 0025hrs; Manx Radio, Isle of Man 1295kHz at 1350hrs; Radio Eireann 1250kHz at 2120hrs; Trans World Radio, Montecarlo 1466 kHz at 2325hrs and Radio Portugal 755kHz at 2312hrs.

A last-minute phone call from T. McCann (Belfast) reports reception of Newfoundland on 930kHz (CJON in St. John's) with the comment "I was surprised at the strength of this station." Propagation on the North American path is rather variable with periods of a week or more when nothing can be heard. At other times, many stations in Canada and the United States can be heard, the limiting factor being interference from Europeans. During the winter listen around midnight on 600kHz, 640kHz, 710kHz, 930kHz, 940kHz, 950kHz, 1070kHz, 1130kHz. North Americans are easy to identify as all stations are allocated callsigns which are used frequently together with the name of the town or city where the studios are located.

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50/50V 10p 16+16/450V 40p	8/450V . 18p 16/450V 22p 82/450V 35p 82/500V 50p 25/25V . 10p	500/25V . 20p 1000/25V . 35p 1000/50V . 47p 8+8/450V . 22p 8+16/450V . 25p	60+100/850V 82+83/850V 82+83/450V	50 85 20 60 55 55

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AMATEUR BANDS

SHORT WAVES by DAVID GIBSON, G3JDG

thank you to the many sharp-eared r.f. sleuths who sent in logs. Everyone seems to have bagged far more DX than I did—well done.

John Powell (Essex) sends in some useful information regarding "who's where and when". John says look out for VQ9HCS on Astove Island (look it up; I had to!). New Ham on Campbell Island is ZL4NJ/A.

A listening MUST. Havering Amateur Radio Club are running a station in Rutland from Saturday, March 30 to Monday April 1 1974. Listen on topband, eighty and v.h.f. Why? Because after that date there will be no County of Rutland, its being absorbed into the surrounding counties so this is your very last chance. Full marks for initiative to the Havering A.R.C.

Michael Watson (Kent) tells that a station in Teheran, EP2BQ, has put up an inverted V for topband. Listen for the EP2 callsign in the bottom 5kHz of 160 metres. Who will hear him first?

Several people have written taking me to task for omitting the list of Happenings in the radio world. It appears that we have a number of keen Contest types among us. The calendar for February is as follows: 9-10, 1.8MHz contest; 16-17, ARRL Contest (c.w.); 23-24, REF contest (phone); March 3-4, 144MHz Open and s.w.l. contest; March 3-4, ARRL DX contest (phone). National Field Day this year will be on June 1-2.

Robert Beebe (Derby) reports hoards of G stations on topband. He tells that members of the Derby club have worked some juicy DX around 1830kHz and quotes calls like W1, KV4, DJ and OK etc.

Vice Chairman (wonder what sort of vice?) David Andrews writes to tell of the Droitwich High School Radio Club. Ten members so far and all going in for the R.A.E. The Club has both Rx and Tx but no antenna up as yet. (How about a base-loaded Maths Master—a sure sine of success).

Keith Rowlings (Herts) has a UR1A, PR40, 75ft. long wire—and a problem. He's heard N20 and L50 on 7MHz and wants to know where they are (and so do I). Anyone any information on these or are they Japanese postal districts?

Graham Nicholls (Oxon) has a homebrew 70cm converter feeding a homebrew 144MHz converter which feeds an R107 (not homebrew). His 15 element 70cm Parabeam rests in his bedroom, but it still heard the following; F1CTH, G3BA, G3COJ, G3DAH. G3YXN, G3KEQ, G3UHT, G3WSN, G3ZFP, G3ZMD. G3YC, G4ABF, G4AHU, G4BEL, G4BMP, G6XM. G8ADC. G8FMK, GW8AWS/P, HW6BQH/P, HW7FY, ON5FF, ON5HN. On two metres with a hamebrew 6—ele Yagi (also in the bedroom) Graham logged; GW8HEZ, HW1CS, HW5SY. PA0ADY, PA0CIO, PA0EZR/A. PA0FHV, PA0PEP. PA0PRY, PA0TAR, SM7DT.

Ye fantastic logge has been sent in by Stanley Sharred. I note that it's on IBM paper—it's cheating if you get the computer to listen and log. No gear is mentioned (bet it's a regenerative cats whisker feeding a 100 Watt light bulb) but the following are claimed for 160 metres; GM3ANO, GM4ALK. GW3UCB, DK3BJ, GM4ASY. EI8H, K2ANR. KV4FZ, OE5KE, OK1AXD, K3RUQ, OK1FCW. OKIKRS, OKIKPU, OK2BKT, OK5KWA, OL6AQJ. OL8CCS, PA0HIP, VE1CD, VEIMX, VEIASJ. VOIKE, WIDX, WIMX, W2DED, W2LWI, W2UEZ. WA2WLN/2, WA8IJI, WB8APM. On 3.5MHz. Stanley excelled with; CT1ADV, CT2BG, EL7D. K2BT, VE1AIH, VO1FG, 7X2MD, 9Y4HR. An excursion to 7MHz revealed DX like; C3IMO, CR4BS. CR6TP, EP2TW, K4DX, PY4MA, PY6WF, PY6AOV. SV1CH, TY1ABE, YV1BI, 5U7BB, 9G1HE.

Eighty metres found Martin Ward listening with a JR500S and 60ft. end fed plus an "L-match device" (Oh L). Squeaks of s.s.b. reported from; CT1GC, LX1GC, KG4CB, VE1AIH, VO1FG, 9H1CE. 9J2AE, and a late arrival—CN8CG. Martin reports hearing the Panama City Radio Club on 21MHz with the callsign 3E1KC.

Stephen Day (Suffolk) made an "adjustment" to his R1155 and claims the signals went up by some 20dB. (You can come and make the same adjustment to my receiver—anytime). Antenna is 50ft. end fed and main interest is eighty metres. Stephen bagged mostly G stations but managed foreign signals from; ZK5AFZ and 9H4L.

John Turner says, "I have been giving the Pye" Cambridge a rest". What a thoughtful lad. This compassion for a trusty friend has not prevented John from listening with his homebrew t.r.f. (P.W. November 1963). The bandspread is the small tuning capacitor from the 235MHz section of an Ex-19 set. The t.r.f. 85ft. end fed and lots of patience produced; CT2BK, EA6CK, EA8IH, EL7C, HB0LL. HI3XCP, HK3AVK, HRIRSP, HZISH, JX4GN JY6UMS, K4PWC/AM, KP4BBW, PY2ELV, PY4LW. PZ1DR, TF5TP, TG8KT, VE1AF, VE3AII/SU. VK2AHM, VK2LW, VK2SG, VK3AD, VK3AX. VK3XJ, VK5FH, VK6SB, VS9MJ, VU2GBG, YV4AGT, ZB2CS, ZB2DL, ZD7SD, ZD7SS, ZM3FO. 3A2CP, 4Z4MQ, 5B4F, 7X2MD. Think what could have been received if Stephen Day (above) had made an "adjustment"!

BROADCAST BANDS

Short Wave Reports by 15th of the month to Malcolm Connah, 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.

Medium Waves Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.

VHF/FM Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

AMATEUR BANDS Short Wave/VHF

Logs in alphabetical order please by 15th of the month to David Gibson, G3JDG, 12 Cross Way, Harpenden, Hertfordshire.



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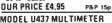
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MODEL 500

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OUR PRICE £10.95 Carr, paid Leather case for above £1.75

KAMODEN 360 MULTIMETER

KAMODEN 360 MULTIMETER
High sensitivity.
DC 100kohm/v o
AC 10kohm/v o
AC

P&P 25p

OUR PRICE £13.95

HIOKI MODEL 700X

HUKI MUUEL /UUJ 100,000opw, Overload protection, Murror scale 0.3/0.6/1.2/1.5/3/6/ 12/30/60/120/300/ 600/1200V DC. 1.5/3/6/12/30/60/150/ 300/600/1200V AC. 15/30b.4/3/6/30/60/ 150/500m.A/6/12A DC 2k/200k/2M/20MOmms –20 to +63dB.



KAMODEN HM720B FET VOM

NAMUUEN HM7201 Input impedence 10 Megohms. Ranges -0/.25/1/2.5/10/50/ 1000V DC. 0/2.5/10 50/250/1000V AC 0/25uA/2.5/25/250 mA DC. 0/5k/50k/500k/5 M 500 Megohms **DUR PRICE** F14 95 PRP 30m



TMK MODEL 117 FET **ELECTRONIC VOLTMETER**



OUR PRICE £17.50

P&P 20p KAMOOEN 72200 Multitester

K AMUUEN /22U High sensitivity tester. 220,000 opp Overload protected Mirror scale. Ranges: -0/.06/.3 3/30/120/600/ 1200V DC. 0/3 12/60/300/1120V VAC. 0/8UA/ 1.2mA/120mA/ 600mA/12A DC 0/12A AC. -20 to 6-53d8. 0/2K/200k/ 2 Meg/200 Megohm (g s



370WTR MULTIMETER

37/WH R MUL IIME I Features AC current ranges. 20,000 opv. 07(0.5/2.5/10/50/ 250/500/1000V DC 07(2.5/10/50/250/ 500/1000V AC. 07(504A)/11/01 D0 mA/1/10A DC. 07/50wA/11/01 AC. 07/50/50/500/500W 5 Meg/50 Meg. Decibels: -20 to 42d8.



U4317 MULTIMETER

U4317 MULTIMETER
High sensitivity
instrument for field
and laboratory work
Knife edge pointer,
Knife edge pointer,
Semm, mirror scale,
Semm, Semm, Mirror Semm, Mirror
Semm, Sempled in cerrying case complete with leads.
Semm, Sempled in cerrying case com-

OUR PRICE £15.00

TE40 HIGH SENSITIVITY AC VOLTMETER

AC VUL IME 1 10 Meg input. 10 ranges: 0,001/ 0,03/0,1/0,3/ 1/3/11/30/100/ 300V RMS. 5cps-1,2MHz. -40 to +50dB supplied brand new complete with leads and instructions



P&P 25p

100

re s

TE85 VALVE VOLTMETER 18:05 VALVE VI 28 ranges. DC volts 1.5–15:00V. AC volts 1.5–15:00V. Resistance up to 10:00 Megohms, 200/240V AC operation. Com-plete with probe and instructions.

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TMK LAB TESTER

TMK LAB TESTER
100,000-ppv. 64"
scale, Buzzer
short circuit check,
Sensitivity 100,000
opv OC, Skr/ NaC
000/1000/ NaC 3/10/50/250/
OC 2017-0100/ NaC 3/10/50/250/
000/10000/ DC,
current 10/100uA/10/
10/100/50mA/2.5/10A, Resistence:
1k/10k/100k/10 Meg/ 100 Meg ohms.
Oecibels: -10 to +4586, Plastic case
with carrying handle, Size: 190 x 172
x 99mm.

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M0 0EL U4311 Sub-standard Multi-range Volt-Ammeter Sensitivity 330 Ohms/Volt AC and DC. Accuracy 0.5% DC, 1% AC. Scale Inenth: 10/300/750-0.4/ 1.5/31/.5/15/30/75/30/75/

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1000 100

LB3 TRANSISTOR TESTER Tests ICO and B. PNP/NPN. Operates from 9V battery. Complete with all **OUR PRICE** £3.95 P&P 20p

LB4 TRANSISTOR TESTER
Tests PNP or NPN
transistors. Audio
indication. Operates
on two 1.5V
batteries. Complete
with instructions ex

OUR PRICE £4.50



U4341 MULTIMETER TRANSISTOR TEST 27 ranges, 16,700opv Overload protected. Ranges: 0.3/1.5/6/ 30/60/150/300/990\ DC. 1.5/7.5/30/150/ 300/750V AC.

Current: 0.06/0.6/ 8/60/600mA DC. 0.3/3/30/300mA AC.

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0.3/3/3/3/3/00mA AC. Resistance: 0.06/ 0.6/2/6/20/60/200k ohms/2 Mohms. Bettery operated, Supplied complete with probes, leads and steel carrying case. Size: 115 x 215 x 90mm.

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S100TR MULTIMETER-TRANSISTOR TESTER

100,000opv. Mirror scale. Overload 100,000opv, Mirror scala, Overload protection, 0/0.12/ 0.6/3/12/30/120/ 600V DC, 0/6/30/ 120/600V AC, 0/12/600u A/12/ 300mA612A OC,



OUR PRICE £14.95

Model 449A In Circuit TRANSISTOR TESTER

Checks true AC, Beta in/out, Checks ICO, Checks diodes in/out, Checks SCR etc, Beta HI 10-500 LO 2-50, ICO 0-5000uA, 220/ 240 V AC operation.



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P&P 25p

KAMODEN HMG500

insulation resistance tester Range 0-1,000 Megohms, 500V Megolims, sour-Battery operated Wide range clear meter 4"x 4%". Complete with deluxe carrying case, batteries an

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SIGNAL GENERATOR 5 ranges, 400kHz to 30 MHz, An inexpensive instrument for the handy-man. Operates on 9V battery, Wide partery, Wide easy to read scale, 800kHz

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Sine 20cps to 200kHz



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ARF 300 AF/RF SIGNAL GENERATOR GENERATOR
All transitorised
compact fully
portable. AF sinewave 18Hz to 220
kHz. AF square
wave 18Hz to 100k
kHz. AF square
wave 18Hz to 100k
LOUDT Square
AF 100kHz to
200MHz. Output
1V maximum.
220/240V AC operation. Complete
with instructions and leads.
PRESENTING SPEECE.

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GRIO OIP METER
Transistorised. Operates as Grid Dip,
Oscillator, Absorttion Wave Meter and
Adolthic John Street
A400Hz – 280MHz
in six cold. 500uA
meter. 9V battery
operation, Size:
180 x 80 x 40mm.

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£8.75 £10.00 £14.70 £25.50 £28.10 £29.50 £72.50 £72.50 £103.10 1A 2.5A 5A 8A 10A 12A 20A 25A 40A

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BV05 Vernier TUNING OIAL App. 7:1 ratio planetary drive vernier dial. Log scale 0—180 degrees.
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BELCO Sine Square Wave

CR OSCILLATOR
Sine 18 x 200 000 Mr
Square 18 x 20,000
Hz. Maximum output +10dB (10b
ohmid Operates
from internal batteries. Attractive to
tone case. Size: 198 x 127 x 50mm

SWR METER Model SWR3

Frequency range 0– 200kHz, Attenuator 0–111dB, 0.1dB steps. Impedence 600 ohms, Inpur power maximum 30dBm, Size: 180 o 90 x 55mm

P&P 37p

P&P 17p

3

P&P 25p

P&P 20p

P&P 15

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200uA 500uA 50-0-50uA 100-0-100 1mA 5mA	63.35 63.30 63.25 63.35 63.30 63.20 63.20		A	
100mA	 €3.20 €3.20 €3.20	20V DC 50V DC		**
1A DC 5A DC	 £3.20 £3.20	300V DC		
10A DC 5V DC	 £3.20 £3.20	300V AC VU Meter		

4	-
	200
20V DC 50V DC 300V DC	£3.20 £3.20 £3.20

CLEAR PLASTIC MODEL SW100

50uA			€4.55	
100uA			£4,35	
500uA	**		£4.10	
50-0-50u			€4.35	
100-0-10	Ou/	۸	£4.30	
1mA			£3.95	
1A DC			£3.95	
5A DC		**	£3,95	
20V DC			£3,95	
50V DC			€3.95	3
300V DC			£3,95	١



EOGWISE MODEL PE70

344. 30 x 3411111	
50uA	£4.15
100uA	£3.95
200uA 500uA	£3.75
50-0-50uA	£3,50 £3,95
100-0-100u A	€3.85
1mA	£3.50
300V AC	€3.50
VU Meter	€4.25



MODEL E0107 EQUICATIONAL METER Size: 100 x 90 x 150mm including terminals

A range of high quality moving coil instruments ideal for school experi-ments and other bench applications. 3" mirror scale. The meter move-ment is easily seasible.

ment is a to demo- working.	nstr nstr	y ac	cessible internal
50uA			€7.60
100uA			£7.05
50-0-50u	Α		£7.05
1A DC			£6.55
5A DC			€6.55
5V DC			£6.55
10V DC			£6,55
15V DC			£6.55



-0-50u	Α	 £7.05		
DC		 €6.55		
DC		 66.55		
DC		 €6.55	300V DC	£6.55
V DC		 €6.55	500mA/5A DC	£7.70
V DC		 €6.55	EV//EOV/ DC	€7.70
V DC		 €6.55	5V/15V DC	€7.70
V DC		 £6.55	1A/15A DC	£7.70

CLEAR PLASTIC MODEL 85P Size: 120 x 110mm

50uA			£4.85	
100uA		••	£4.70	
200uA			£4.45	
500uA		••	£4.30	
50-0-50u	٠	**		
30-0-500	Δ.		£4.70	
100-0-10	Ou/	۹	€4.45	
500-0-50	Du A	١	£4.30	
1mA			£4.30	
1-0-1mA			£4.30	
5mA			£4.30	
10mA			£4.30	
50mA			£4.30	
100m A		**	£4.30	-
500mA			£4.30	3
1A DC	••	**		,
	••		€4.30	3
5A DC			€4.30	S
15A DC			£4.30	١
30A DC			£4.35	1
10V DC			€4.30	5
20V DC			€4.30	- 1



£4.30	NE - 12-
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£4.30	The second secon
£4.30	
€4.30	300V DC £4.30
£4.30	15V AC £4.35
€4.30	300V AC £4.35
£4.30	S Meter 1mA £4,30
£4.30	VU Meter £5.00
£4.35	14 40 8 64 20
£4.30	EA 40 4 64 00
€4.30	10A AC
£4.30	204 40 + 64 20
£4.30	
L=.30	30A AC • £4.30

*Items with asterisk are Moving Iron type, all others are Moving Coil

CLEAR PLAST	TIC MO	OEL S0830	
50uA	£3.75		
100uA	€3.70		7
200u A	€3.65	The same	
500uA	£3.45	100	100
50-0-50u A	€3.75		
100-0-100uA	£3.70	200	- 1
1mA	£3,40	THE RESERVE THE PERSON NAMED IN	10000
5mA	€3.40	Name and Address of the Owner, where the Owner, which is the Owner, where the Owner, which is the Owner	100
10mA	€3,40		
50mA	€3.40	10V DC	€3.40
100mA	€3.40	201/ DC	£3.40
500mA	£3.40	EOV DC	£3.40
1A DC	£3.40	200V DC	£3.40
5A DC	£3.40	16V AC	23.65
SOA DC	£3.40	300V AC	£3.65
5V DC	€3.40	VU Meter	£3.85
34 00,	23.40	A O INSTAL	£3,80

5	*	2
	10V DC 20V DC	£3.40 £3.40
)	50V DC 300V DC	£3.40 £3.40
)	15V AC 300V AC	£3.65 £3,65
)	VU Meter	£3,85

100-0-10 1mA ... 5mA ... 10mA ... 100mA 500mA 1A DC 5A DC 10A DC 5V DC CLEAR PLASTIC MODEL 45P Size: 50 x 50mm

50uA 100uA .. 200uA .. 500uA .. 50-0-50uA

50uA

£3.00 £2.85 £2.75 £2.70 £2.90 £2.75	
£2.65 £2.65 £2.65 £2.65 £2.65 £2.65	
£2.65 £2.65 £2.65 £2.65 £2.65 £2.65	300V AC £2 S Meter 1mA £2 VU Meter £3 1A AC * £2 5A AC * £2 10A AC * £2
£2.65 £2.70	20A AC £2.

	À
300V AC	£2.70
S Meter 1mA	£2.75
VU Meter	£3.00
1A AC	• £2.65

CLEAR PLASTIC MODEL 38P £2.80

100uA	**		£2.70	6	
A u009			£2.65		- 1
500u A			£2.50	Local Confession and	. 1
50-0-50u	Α		£2.75	1000	200
100-0-10	Ou 4	١	€2.65	100	~
00-0-50	Child		£2.50		
mA	00,	• ••	€2.50	2	9
-0-1mA	••		£2.50	1111111	
mA	**		£2.50	1111111	
	••	••		11111111	THE R. P.
	• •	**	€2.50	CHINA THE PARTY OF	
10mA	**	••	£2.50		
Am0	**	**	€2.50		
0mA			€2.50	15V DC	£2.50
00mA	**	**	£2.50	20V DC	£2,50
50mA			£2.50	50V DC	£2,50
Am00			£2.50	100V DC	£2.50
Am00			£2.50	150V DC	€2.50
OOm A			£2.50	300V DC	€2.50
50mA			£2.50	FOOV DC	£2.50
A DC		•••	£2.50	750V DC	
A DC			€2,50	15V AC	£2.50
A DC	••	**	£2.50		£2.55
OA DC	••	**		50V AC	£2.55
5A DC	**	**	£2.50	150V AC	£2.55
	**	••	€2.50	300V AC	£2.55
OA DC	**	**	£2.50	500V AC	£2.55
V DC	••	••	€2.50	S Mater 1mA	£2.55
OV DC	••	••	€2.50	VU Meter	€2.90

20A DC 3V DC 10V DC CLEAR P

CLEAR PLAS	TIC MO	DEL SD460
Size: 59 x 46mn	п	
50uA	£3.10	
100uA	£3.05	
200u A	€3.00	1 12700
500u A	£2.80	10
50-0-50u A	£3.10	Α
100-0-100u A	£3.05	
1mA	£2.85	THE REAL PROPERTY.
5m A	£2.85	M CONTRACTOR OF
10mA	€2.85	
50mA	£2.85	
100mA	£2.85	10V DC £2.85
500mA	£2.85	50V DC £2,85
1A DC	£2.85	300V DC £2.85
5A DC	£2.85	15V AC £3.00
5V DC	£2.85	300V AC £3.00
0 V DC	£2.85	VU Meter, £3.20

100-0-16 1mA ... 5mA ... 10mA ... 100mA 500mA 1A DC 5A DC 10A DC 5V DC POSTAGE & PACKING 15p

P&P 23n

CLEAR PLASTIC MODEL 65P

Size: 86 x 78mm	MODEL 65P
100uA	86 85 85 85
S00mA E2 14 DC C2 C3 C3 C3 C3 C4 C4 C4 C4	85 50V AC

5A AC 10A AC 20A AC 30A AC 50mA AC 100mA AC 200mA AC BAKELITE MODEL S80 Enlarged Window

2158: 90 X	BU	mm	
50u A			£3.85
			£3.75
	••		€3.35
50-0-50u /			£3.75
100-0-100	λuΑ	١	€3.65
1mA			£3.00
1A DC			£3.30
5A DC	**		€3.30
20V DC		**	£3.30
50V DC	••		£3.30
300V DC	**	**	£3.30
300V AC	••	••	£3.30
VU Meter			£4.05



CLEAR PLASTIC MODEL 52P

24ZE: PO 2	(01	лт	1
50uA			€3.85
100uA		**	മ്.30
500uA	**		€2,90
50-0-50u			£3.35
100-0-10	Ou A	١	€3.25
1mA			£2.75
5mA			£2,75
10mA	**		£2.75
50m A		**	£2,75
100mA			£2.75
500mA			£2.75
1A DC			£2.75
5A DC			£2.75
10V DC			£2.75
20V DC			£2.75
50V DC			€2.75
300V DC			€2.75
15V AC			£2.85
300V AC			€2.85



MILITA	100
S Meter 1mA	. £2.85
VU Meter	. £3.95
1A AC 5A AC	. • £2.75
10A AC	£2.75
20A AC	

BAKELITE	MOOEL 65	Size: 80 x 80mm
25uA 50uA 100uA 500uA 50-0-50uA 100-0-100uA 500-0-500uA	£5.05 £3.90 £3.30 £3.00 £3.35 £3.30 £2.85	Size. BUX BUMM
1-0-1mA	£2.85 £2.85 £2.85	
100mA	£2.85 3 £2.85 5 £2.85 1	0V AC • £2. 0V AC • £2. 50V AC • £2. 00V AC • £2.
2A DC 5A DC 15A DC	. £2.85 5 . £2.85 V . £2,85 1	00V AC • £2, 00V AC £2, 'U Meter £4, A AC • £2,
30A DC 50A DC 5V DC	. £2.85 1 . £2.85 2	A AC
20V DC 50V DC 150V DC 300V DC	. £2.85 5 . £2.85 5 . £2.85 5	0A AC • £2: 00mA AC • £2: 0mV DC £3: 00mV DC £3:

£2.85 £2.85		
£2.85	30V AC	* £2.85
£2.85	50V AC 150V AC	• £2.85
£2.85	300V AC	• £2.85
£2.85 £2.85	500V AC VU Meter	£2.85
£2.85	1A AC	• £2.85
£2.85	10A AC	£2.85
£2.85	20A AC	• £2.85
€2.85	50A AC	£2.85
£2.85 £2.85	500mA AC 50mV DC	£2.85
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20084	£4 50

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5000W

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For display of pulsed
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forms in electronic
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VRMS/mm: 0.1—25
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VRMS/mm: 0.3—26
1—3000usec. Free running 20—200
kHz in nine ranges. Calibrator pips.
220 x 360 x 430mm. 115—230V AC.
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3" tube. Y amp OSCILL
3" tube. Y amp OSC

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Calibrator and amplitude Calibrator, Supplied complete with all accessories and instruction manual.

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£11.97



P&P 50p

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ourrLY UNIT
Solid state, Output
6, 9 or 12V DC up
to 3 Amp. Meter to
monitor current,
Input 220/240V AC.
Size: 100 x 82 x
159mm.



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SUFFLY UNITS
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up to 2 Amp. Inde
pendent meters to
monitor voltage and
current. Output
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98mm.



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Nine wave-bands covering 1.8–29.7 MHz, 144–146MHz and 10MHz WWV SSB, CW, AM and FM. AF output is more than 1 watt. S Meter. Squelch control. BFO. Variable AF and RF controls. 4–16 ohm output and jeck for phones. Power requirement 100/240V AC, 12/14V DC, Size: 270 x 140 x 310mm.

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	-	1000µF	17p	1000µF	25p			
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$33\mu F$	6 p	2000µF	43p	. 200,2.	119			
68µF	₿₽p		-					
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470µF	11p	10µF	6ip					
680µ F	13p	22µF	6 p	63 VO	1 7			
1500µF	18p	47µF	6 p					
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RESISTORS

W Iskra high stability carbon film—very low noise—capless construction.
W Mullard CR25 carbon film—very small body size 7:5 x 2:5 mm.
W 2% ELECTROSIL TR5.

Power			Values	Pr	ice	l
Watts	Tolerance	Range	available	1-99	100+	l
+	5%	4·7 Ω-2·2M Ω	E24	lo.	0 · 8p	l
*	10%	$3.3M \Omega = 10M \Omega$	E12	lp.	0.8p	l
*	2%	10 M I - 12 0 I	E24	3 · 5p	30	ł
*	10%	1Ω-3-9Ω	E12	lp.	0 · 8p	l
*	5%	4·7 Ω-IM Ω	E12	·lp	0.8p	ı
A 4.	10%	1 Ω –10 Ω	E12	6p	5 · 5p	
Quantity	Drice applies	for any selection	langua (magaina.			ı

MULLARD POLYESTER CAPACITORS C296 SERIES 400V: 0.001/nf, 0.0015/nf, 0.0015/nf, 0.0022/nf, 0.0033/nf, 30.0047/nf, 0.0033/nf, 30.0047/nf, 0.068/nf, 0.015/nf, 40.0052/nf, 0.033/nf, 11p, 0.047/nf, 0.068/nf, 0.016/nf, 40.005/nf, 11p, 0.047/nf, 13p, 0.047/nf, 0.068/nf, 3p, 0.1/nf, 31p, 0.15/nf, 0.022/nf, 0.022/nf, 0.022/nf, 0.022/nf, 0.022/nf, 0.022/nf, 13p, 1.0/nf, 13p, 0.1/nf, 13p, 0.022/nf, 0.022/nf, 0.022/nf, 13p, 0.047/nf, 0.068/nf, 13p, 0.047/nf, 0.068/nf, 13p, 0.047/nf, 0.015/nf, 0.022/nf, 3p, 0.033/nf, 0.047/nf, 0.068/nf, 13p, 1.5/nf, 4p, 0.15/nf, 0.022/nf, 5p, 0.047/nf, 81p, 0.068/nf, 11p, 1.0/nf, 13p, 1.5/nf, 4p, 0.15/nf, 0.022/nf, 61p, 0.047/nf, 81p, 0.068/nf, 11p, 1.0/nf, 13p, 1.5/nf, 20p, 2.2/nf, 5p, 0.33/nf, 61p, 0.047/nf, 81p, 0.068/nf, 11p, 1.0/nf, 13p, 11/nf, 4p, 0.15/nf, 0.02/nf, 5p, 0.047/nf, 81p, 0.068/nf, 11p, 1.0/nf, 13p, 11/nf, 4p, 0.15/nf, 0.02/nf, 0.000/nf, 0.0000/nf, 0.000/nf, 0.000/nf, 0.000/nf, 0.000/nf, 0.000/nf, 0.000/

MYLAR FILM CAPACITORS 100V 0.001μF, 0.002μF, 0.005μF, 0.01μF, 0.02μF, 2½p. 0.04μF, 0.05μF, 0.068μF, 0.1μF, 3½p. CERAMIC DISC CAPACITORS 100pF to 10,000pF, 2p each.

ELECTROLYTIC CAPACITORS $(\mu F|v) | 1/63, 1 \cdot 5/63, 2 \cdot 2/63, 3 \cdot 3/63, 4 \cdot 7/63, 6 \cdot 8/40, 6 \cdot 8/63, 10/25, 10/63, 15/16, 15/40, 15/63, 22/10, 22/25, 22/63, 3 \cdot 3/63, 3/16, 3/140, 47/4, 47/10, 47/25, 47/40, 68/6-3, 68/16, 100/4, 100/10, 100/25, 150/6-3, 150/16, 22/04, 22/06, 3/20/16, 3/30/4, 6p. 47/63, 100/40, 150/25, 22/0/25, 3/30/10, 470/6-3, 7p. 68/63, 150/40, 220/140, 3/30/16, 1000/4, 10p. 470/10, 6/80/6-3, 11p. 100/63, 150/63, 220/63, 1000/10, 12p. 470/25, 6/80/16, 1500/6-3, 11p. 470/40, 6/80/25, 1000/16, 1500/10, 2200/6-3, 18p. 3/30/63, 6/80/40, 1000/25, 1500/16, 2200/10, 3/300/6-3, 4700/4, 21p.$

JACK PLUGS AND SOCKETS

D.I.N. PLUGS AND SOCKETS 2 pin, 3 pin, 5 pin 180°, 5 pin 240°, 6 pin Plug 12p. Socket 8p.
4 way screened cable, 15p/metre, 6 way screened cable, 22p/metre.

Standard screened 18p 2.5mm insulated 12p 3.5mm insulated 12p 3.5mm screened 15p 3.5mm screened 15p 2.5mm socket 15p 2.5mm socket 18p 3.5mm socket

BATTERY ELIMINATOR 61.50 9V mains power supply. Same size as PP9 battery.

-1,000 VOLT 0·22μF 0·47μF

4500μF 16V 50p 4500μF 25V £1·68 5000μF 50V £1·10

8p 13p 8p

DEVELOPMENT PACK

0.5 watt 5% iskra resistors 5 off each value 4.7 Ω to IMΩ. E12 pack 325 resistors £2.40. E24 pack 650 resistors £4.70,

POTENTIOMETERS Carbon track $5k\Omega$ to $2M\Omega$, log or linear (log $\frac{1}{2}W$, $\lim_{n\to\infty} \frac{1}{2}W$), Single, 12p. Dual gang (stereo), 40p. Single D.P. switch, 24p.

SKELETON PRESET POTENTIOMETERS
Linear: 100, 250, 500 \(\Omega\$ and decades to 5M \(\Omega\$. Horizontal or vertical P.C. mounting (0-1 matrix).
Sub-miniature 0-1W, 5p each. Miniature 0-25W, 7p each.

TRANSISTORS

AC107 AC126	15p	AFI26 AFI39	20p	BFI15	25p	OC42	12p	2N3707	12p	l
AC127	15p	AFI78	32p	BF173	20p	OC44	12p	2N3708	10p	ı
AC128			32p	BF177	28p	OC45	12p	2N3709	Hp	ı
	15p	AF180	40p	BF178	32p	OC70	12p	2N3710	Hp	ł
AC131	12p	AFIBI	40p	BF179	32p	OC71	12p	2N3711	Hp	ł
ACI32	12p	BC107	I2p	BF180	32p	OC72	12p	2N3819	32p	ł
AC176	15p	BC108	12p	BFIBI	32p	OCSI	12p	2N4062	12p	ł
AC187	22p	BC109	120	BF194	14p	OC82D	120	2N4286	20p	Ė
AC188	22p	BC147	12p	BF195	14p	2N2646	60p	2N4289		ı
AD140	50p	BC148	120	BF197	15p	2N2904	20p	40360	20p	ı
ADI49	45 p	BCI49	120	BF200					35p	ı
ADI6I	33p	BC157			32p	2N2926	10p	40361	35p	ı
AD162			I4p	BFY50	20p	2N3054	58p	40362	40p	l
	36p	BC158	14p	BFY51	20p	2N3055	60p	40408	40p	l
AEL14	20p	BC159	14p	BFY52	20p	2N3702	13p	ZTXIOS	15p	
AFI15	20p	BC187	22p	BUY105	225p	2N3703	12p	ZTX300	15p	
AFI16	20p	BD131	75p	OC26	45 p	2N3704	130	ZTX302	20p	
AFI17	20p	BD132	75p	OC28						
AFIIB	38p	BD133	75p	OC35						
AFIIB					50p	2N3705 2N3706	12p	ZTX500 ZXT503	15p	

ZENER DIODES 400mW 5% 3-3V to 30V, 12p.	1	WIRE WOUND POTS. 3W, 10, 2 50 Ω and decades to 100k Ω , 35p.
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DIODES					
RECTIFIE	ER			SIGNAL	
BY127	1250V	IA	12p	OA85	7-
IN4001	50V	IA	7p	OA90	7p
IN4002	1007	ÍÁ '	8p	OAPI	5p
IN4004	400V	IA	8p	OA202	5p
1N4006	800V	ÍÁ	100	IN4148	7p
IN4007	1000V	iÂ	10p	BA114	5p

SMOKE AND COMBUSTIBLE GAS DETECTOR-GDI

 SOLID TANTALUM BEAD CAPACITORS

 0·1μF
 35V
 2·2μF
 35V

 0·22μF
 35V
 4·7μF
 35V

 0·47μF
 35V
 6·8μF
 25V

 1·0μF
 35V
 10μF
 25V

0.15 16p 24p 24p 27p 57ip 78p 82p 60p 42p 11p 52p 42p 20p

| 1600µF 64V 74p | 2500µF 64V 80p | 2500µF 64V 74p | 2800µF 100V 62-60 | 2500µF 40V 74p | 2800µF 100V 62-60 | 2500µF 50V 36p | 3120µF 16V 50p | HIGH | VOLTAGE TUBULAR CAPACITORS—0-01µF 10p | 0-047µF 13p | 0-022µF 12p | 0-1µF 13p | 0-047µF 1

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0.1 22p 24p 24p 27p 75p 100p

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VEROBOARD

2† x 3‡ 22p 2† x 5 24p 3‡ x 3‡ 24p 3‡ x 5 27p 17 x 2‡ 100p 17 x 2† 100p 17 x 5 (plain) — 17 x 3‡ (plain) — 17 x 5 (plain) — 2† x 5 (plain) 2† x 5 (plain) — 2† x 3‡ (plain) — 2† x 3‡ (plain) 2† x 5 (plain) 2† x

The GDI is the world's first semiconductor that can convert a concentration of gas or smoke into an electrical signal. The sensor decreases its electrical resistance when it absorbs deoxidizing or combustible gases such as hydrogen, carbon monoxide, methane, propane, alcohol, North Sea gas, as well as carbon-dust containing air or smoke. This decrease is usually large enough to be utilized without amplification. Full details and circuits are supplied with each detector. Detector GDI, £2. Kit of parts for detectors including GDI and P.C. board but excluding case. Mains operated detector £5.20, 12 or 24V battery operated audible alarm £7.30, As above for PP9 battery, £6.40.

PRINTED BOARD MARKER

Draw the planned circuit onto a copper laminate board with the P.C. Pen, allow to dry, and immerse the board in the etchant. On removal the circuit remains in high relief.

SLIDER POTENTIOMETERS

86mm x 9mm x 16mm, length of track 59mm. 5INGLE 10K, 25K, 100K log. or lin. 40p. DUAL GANG, 10K + 10K etc. log. or lin. 60p. KNOB FOR ABOVE, 12p.

BRUSHED ALUMINIUM PANELS 12in x 6in, 25p 12 in x 2½in, 10p 9in x 2in, 7p

FRONT PANEL, 65p. 18 Gauge panel 12in x 4in with slots cut for use with slider pots. Grey or matt black finish complete with fixings for 4 pots.

Į	THY	RISTO	RS	
1	2N506	0 50V 4 200V	A8.0	30p
ı	2N506	4 200 V		
l	106F		4A	40 p
6	106D	400V	4A	55p

ALUM	INIUM BOXE	S			
AB7 AB8 AB9 AB10 AB11 AB12	22" x 5½" x 1½" 4" x 4" x 1½" 4" x 22" x 1½" 4" x 5½" x 1½" 4" x 5½" x 1½" 3" x 2½" x 2" 3" x 2" x 1"	50p 50p 50p 50p 60p 44p	AB14 AB15 AB16 AB17 AB18 AB19	7" x 5" x 21" 8" x 6" x 3" 10" x 7" x 3" 10" x 41" x 3" 12" x 5" x 3" 12" x 8" x 3"	84p 108p 122p 108p 120p 160p

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HEA 2W 3W	TSINKS 24p 36p	-REDP	OINT 45p 60p	TO5 Clip TO18 Clip		TOI	5ingle Double	5p 8p

	ORMERS All have 2401	V primar	'у	
MT30/2	0~12-15-20-24-30	2A	62 - 85	
MT50/1	0-19-25-33-40-50V	+A	£1 -90	
MT50/1	0-19-25-33-40-50V	ĬA	62 - 55	
MT50/2	0-19-25-33-40-50	2A	63-50	
MT60/4	0-24-30-40-48-60V	±A.	62-10	
MT69/1	0-24-30-40-48-60V	ÍA.	62 80	
MT60/2	0-24-30-40-48-60V	2A	63 80	

METERS	1‡" 5cale-500uA, 1mA, 1	10mA, 100mA	£1 ·90
BULGIN MAINS		9:- 114 G	

3 Pin	IţА	Chassis Plug Line Socket	10p 13p	3 Pin	ΗA	Chassis Socket Line Plug	18p
3 Pin	3A	Chassis Plug Line Socket	10p 14p	3 Pin	3A	Chassis Socket Line Plue	
3 Pin	5 A	Chassis Plug	16p			Line ring	23p
		Line Socket	15p	2 Pin	5A	Line Plug	20p

THERMISTORS VA1005 15p VA1026 15p VA1033 15p	D.P. 2A 32p
VA10555 13p VA10665 13p VA1077 13p R53 41 35	LINEAR IC's 709 14 pin DIL 40p 741 8 pin DIL 40p 741 14 pin DIL 38p 723 14 pin DIL 95p
WAVECHANGE SWITCH 23p Ip I2W, 3p 4W, 2p 2W, 2p 6W, 4p 3W	747 14 pin DIL 85 p 748 8 pin DIL 45 p DIL 50ckets 14 pin and 16 pin

TRANSISTORS, ZENER DIODES etc. **Fully guaranteed** 25p ORP61 45p 2N2411 25p ORP90 95p 2N2646 45p OR 93 2110 2N2904 25p RA£31)AP 2N2989 25p 35p 2N3053 ALL valves 20p NKT222 80p OC75 11p OA5 60p OC75 18p OA10 40p OC77 15p OA70 10p OC78 45p OA71 10p OC78 25p OA73 15p OC81 25p OA74 15p OC81 2N2411 56p 2N2646 45p 2N2904 20p 2N2908 24-00 2N3053 20p 2N3054 45p 2N3055 55p 2N3730 65p 2N3730 65p 2N3731 70p 2N3819 25p Individually packed VALVES AC 07 AC113 AC126 AC 27 B(1) 18 22 309, 00.75 259, 0R.P61 409 | 00.776 259, 0R.P61 409 | 00.77 459, 0R.P90 109 | 00.778 259, 18.48.31.Ni 109 | 00.781 259 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 209 1159 | 00.781 20 guaranteed 6H6M 25p 12Q7GT 6Y4WA 21-00 128G7 6Y5 55p 1487 ECLE 4 400 N78 2 EP36 600 OA2 EP37A 21-00 OB2 EF40 620 PABCAO EF41 650 PCS7 EF80 250 PCS9 EF83 21-00 PCCS4 EF85 21-00 PCCS4 EF85 21-00 PCCS4 EF85 21-00 PCCS4 EF96 27 PCCS8 EF96 27 PCCS8 EF91 379 PCCS EF183 350 PCF80 EF183 350 PCF80 EF183 350 PCF80 EF183 350 PCF80 ELS4 379 PCF80 ELS4 389 PCF80 ELS4 389 PCCS T 40p 6064 40p 6063 80p 6080 50p 6146 £7:00 8020 £5:75 9001 £6:25 9002 £1:00 9003 T 60p 9004 6Y4W A 6Y5 6Y5GT 6Y6 6Y7G 6Y7M 6K6GT 6K7G 6K8GT 6K25 6L6M £ 6SA7 6SA7GT 6SC7GT 6SY7 85p 21p 25p 65p £2:20 £2:00 BD136 ACT28 20p 25p AC132 AC176 AC187 AC188 ACY17 BF115 19AQ5 20p BF167 25p BF173 25p BF173 35p BF177 35p BF180 25p 25p 25p 25p 20p 85p CY31 25p OA74 25p OA79 25p OA81 20p OA91 35p OA200 30p OA200 20p OAZ200 20p OAZ201 75p OC16 19G3 £8.75 50p 30p 25p £1:00 DAF96 19G6 19H4 30p 50p 55p 25p DE96 DE96 DE92 DE94 45p 60p 35p 45p 55p 41p 2N3731 2N3819 28303 28304 28307 28703 40594 ACY17 ACY28 AD139 AD149 AD161 AD162 AF118 AP127 AF139 AF178 25p 70p 80p 21.60 75p 65p 75p 9 50 BFY51 200 0A22 1 350 BFY52 200 0A22 2 350 BFY52 200 0A22 2 350 BFY52 200 0A22 3 350 BFY52 200 0A22 3 350 BFY52 350 0C22 3 350 BFY96 750 0C25 4 350 CR51/10 350 0C25 4 350 CR51/10 485 0C25 4 3 36p 40p 55p 45p 50p 25p 35p 75p 50p 90p 45p 90p 55p 55p 55p 65p 55p DL96 **DM70** 35p EF86 DY86 50p 50p 20p 65p 75p 37p 43p 22p C.R. 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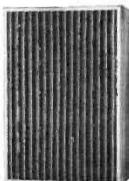
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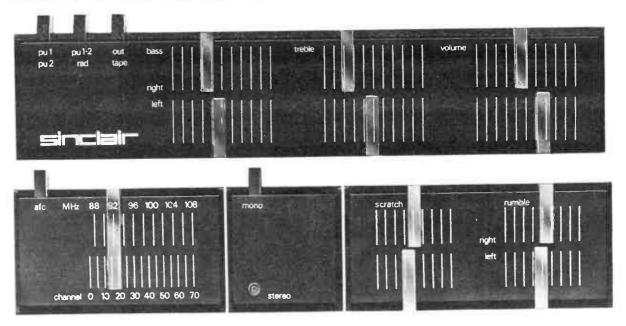
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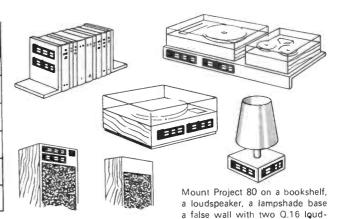
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System	The Units to use	Units cost
Simple battery record player	Z.40	£5-45 - 54p V.A.T.
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30W. RMS continuous sine wave stereo amp.	2 × Z.40s, Stereo 80; PZ.6	£30-83 +£3.08 V.A.
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Project 80 FM tuner, decoder, and A.F.U. may be added as required



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TECHNICAL SPECIFICATIONS

Size - 260 - 50 = 20mm (103 = 2 × 3 ins)

Finish - Black with white indicators and transparent sliders

Inputs - Magnetic pick-up 3mV RIAA corrected; Ceramic pick-up 300mV

Radio 300mV; Tape 30mV

Signal/noise ratio = 60dt. Frequency range = 20Hz to 15KHz ± 1dB: 10Hz to 25KHz ± 3dB

Power requirements - 20 to 35 volts

Outputs – 100mV + AB monitoring for tape
Controls – Press button for tape radio and P U Sliders for volume,
bass (+ 12dB to - 14dB at 100Hz) treble (+ 11dB to - 12dB at 10KHz)

R.R.P. £11.95 HE1-19

Simplest ever fixing

Project 80 FM tuner and stereo decoder





Twin dual varicap tuning: 4 pole ceramic filter: switchable A.F.C.

 On the decoder, solid state stereo indicating beacon.

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TECHNICAL SPECIFICATIONS OF TUNER

Size = 85 × 50 × 20mm (3½ × 2 × ½ins)
Tuning range = 87-5 to 108 MHz
Detector = I.C. balanced coincidence for good A.M. rejection

One I.C. equal to 26 transistors Distortion - 0.2% at 1 KHz for 30% modulation

4 pole ceramic filter in I.F. section

Aerial impedance - 75 Ω or 240-300 Ω

Sensitivity - 4 microvolts for 30dB quieting

Output - 300 mV for 30% modulation

Power requirements - 23 to 33 volts

Size-47 × 50 × 20mm (1 × 2 × ½ ins)

One 19 transistor I.C.

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Z.40 TECHNICAL SPECIFICATIONS

Size $-55 \times 80 \times 20$ mm ($2\frac{1}{8} \times 3\frac{1}{8} \times \frac{3}{8}$ ins) 9 transistors

Input sensitivity - 100mV

Output - 15 watts RMS continuous into 8 Ω (35v)

Frequency response - 10Hz = 100KHz - 1dB

Signal/noise ratio - 64dB

Distortion – at 10 watts into 8 Ω less than 0.1%

Power requirements - 12 to 35 volts

Z.60 TECHNICAL SPECIFICATIONS

Size $-55 \times 98 \times 15$ mm ($2\frac{1}{8} \times 3\frac{3}{4} \times \frac{3}{4}$ ins) 12 transistors Input sensitivity $-100 \cdot 250$ mV

Output - 25 watts RMS continuous into 8 Ω (45V). Distortion - typically 0.03%

Frequency response - 10Hz to more than 200KHz 2 1dB Signal/noise ratio - better than 70dB

Built in protection against transient overload and short circuiting

Load impedance - 4 Ω min, max safe on open circuit Z.40 R R P. £5.45 + 0.54 V A T , Z.60 R R P. £6.95 - 0.69p V.A T.

Project 80 active filter unit

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TECHNICAL SPECIFICATIONS Size - 108 x 50 x 20mm ($4\frac{1}{4}$ x 2 x $\frac{1}{4}$ ins)

Voltage gain - minus 0-2dB Frequency response - 36 Hz to 22 KHz controls minimum Distortion - at 1 KHz - 0.03% using 30V supply HF cut off (scratch) - 22KHz to 5.5KHz, 12dB/oct, slope L.F. cut off (rumble) - 28dB at 20Hz, 9dB/oct. slope

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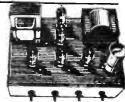
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