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12 V
122
12
12
12
112
12
0
0
1
1
1
2
3 12 or 24 Volts.
Output $Y$. $\$$ Amps.
$12 \mathrm{~V} \times 2250 \mathrm{~mA} \times 2$
Refino.
MT213
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MT108AT
MTT2AT
30 Volts. All tapped at $0.12-15 \cdot 20 \cdot 30 \mathrm{~V}$
Output Ref. No. Price Output Ref. No.
Amps.

| 14 |
| :--- |
| 2 A |

00 miA
 $\begin{array}{llll}60 \text { Volts. All tapped at } 0.24 & 30 \cdot 40-48-60 \\ & 00 \mathrm{ma} \\ \text { MT124AT } & 22 \cdot 33 & 2 A & \text { MT127 }\end{array}$ $1 A$ MTIL6AT 23.28 3A MT127AT 44.36 Power

| output | Winding tapped at | Ref. No. | Price |
| :---: | :---: | :---: | :---: |
| 20 VA | 0-115-210-240 | XMT113CT | 21.28 |
| 75 VA |  | Xmt64at | 82.51 |
| 150VA | 0-115-200-220-240 | XmTat | 28.06 |
| 200 VA |  | XMT65AT | 23.65 |

C.D Igaition 8 ystem by Otpat at 50 BZ .

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|  | 1.8.) | Re1. No. | Price |
| :---: | :---: | :---: | :---: |
| 3-0.3V | 200 mA | MT238Cs* $\uparrow$ | 21.41 |
| 9-0.9 | 100 mA | MT13CS* $\dagger$ | 21-86 |
| 12-0-12 | 50 mA | MT $239 \mathrm{CS}{ }^{\circ} \uparrow$ | 21.41 |
| 20-0-20 | 30 mA | MT241Cs* $\uparrow$ | 21.41 |
| $0.20 \times 2$ | $300 \mathrm{~mA} \times 2$ | MT214CT* | 81.87 |
| $0-8.9 \times 2$ | $800 \mathrm{~mA} \times 2$ | MT207CT* | 28.22 |
| 0-15-20 $\times 2$ | $500 \mathrm{~mA} \times 2$ | MT205AT* ${ }^{\text {¢ }}$ | 28.95 |
| $0 \cdot 15-27 \times 2$ | $500 \mathrm{~mA} \times 2$ | MT203AT* | 18.38 |
| $0-15.27 \times 2$ | $14 \times 2$ | MT204AT* | 83.38 |
| 20-12-0-12-20 | 700 mA (d.c.) | MT221AT* | 11.74 |

AT Indicates open universal fixing with tags; CT is open U.clamp aslog with tags; Cs is open U-clanp axing with P.C. apills; -with interwinding ecreen; $\uparrow$ untapped 240 primary; $\ddagger$ tapped at $210-240 \mathrm{~V}$.; other prinuarics tapped OVER 200 TYP

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| VA | Ret. | Price |  |
|  |  |  |  |
| ${ }^{60}$ | 149 | 2.88 |  |
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| 200 | 151 |  | 0.52 |
| ${ }^{2350}$ | 152 | ${ }^{7} \cdot 0.05$ |  |
| 350 | 153 |  |  |
| 500 | 154 | 18.55 |  |
| 1000 | 156 |  |  |
| - | 1588 | ${ }_{84}^{12} \cdot$ |  |

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Prim:- 800-840V. 8ec:- 19, 25, 88, 40, 60V.

| A пup | Type | Prke | Pa P |
| :---: | :---: | :---: | :---: |
| 0.5 | 102 | 1.60 | 0.30 |
| 1 | 103 | 8.85 | 0.38 |
| 6 | 104 | 8.25 | 0.422 |
| 3 | 105 | 4.40 | 0.52 |
| 4 | 106 | 5.48 | 0.52 |
| 8 | 107 | 8.85 | 0.67 |
| 8 | 118 | 11.87 | 0.97 |
| 10 | 119 | 14.15 | 0.97 |

MINIATURE AND EQUIPMENT
Prim R40V w
Volts
Sec, 1
$3-0-3$
$0-3$
$0-6$
$9-0-4$
$0-9$
$0-8-9$
$0-8-9$
$15-0-13$
$0-15$
$20-0-20$
$0-20$
$0-15-20$
$0-20$
$20-12-0-12$
$0-15-20$
$0-15-97$
$0-15-27$
Sec. 2
$0-6$
$0-6$
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$0-9$
$0-8-4$
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| Miliatnpa |  |
| :---: | :---: |
| Bec. 1 | 8ec. ${ }^{1}$ |
| 200 |  |
| 500 | 500 |
| 1000 | 1000 |
| 100 |  |
| 330 | 330 |
| 500 | 500 |
| 1000 | 1000 |
| 40 | - |
| 200 | 300 |
| 30 | - |
| 150 | 150 |
| 500 | 500 |
| 300 | 300 |
| 700(D/C) |  |
| 1000 | 1000 |
| 500 | 500 |
| 1000 | 1000 |


| Type | Price |
| :---: | :---: |
| No, |  |
| 23 H | $1 \cdot 12$ |
| 234 | 1.18 |
| 212 | 1.28 |
| 13 | 0.95 |
| 235 | 1.28 |
| 207 | $1 \cdot 70$ |
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| 240 | 1.28 |
| $\because 36$ | 1-28 |
| 241 | 1.00 |
| 237 | 1.28 |
| 205 | $8 \cdot 16$ |
| 214 | 1.86 |
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0.10
$0 \cdot 10$
$0 \cdot 20$
0.10
$0 \cdot 10$
0.222
0.30
0.10
0.10
0.10
0.10
0.38
0.24
$0 \cdot 30$
0.38
0.38
0.38
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The AL10, AL20 and AL30 unis are imilar In their appearance and in their seneral specincation. However. careiul resulted in a range of output powers from 3 to 10 watis R.M.s.

| Parameter | Conditions | Pertormance |
| :---: | :---: | :---: |
| HARMONIC DISTORTION | $\mathrm{PO}=3$ WATTS $1=1 \mathrm{KHz}$ | 0.45\% |
| LOAD IMPEDANCE | - | $8-16 \Omega$ |
| INPUT IMPEDANCE | 1-1KHz | $100 \mathrm{k} \Omega$ |
| FREQUENCY RESP'ONSE CE 3H13 | Po-2 WATTS | $50 \mathrm{~Hz}-25 \mathrm{KHz}$ |
| BENSITIVITY for RATED O/P |  | 75 MV. R3s |
| DIMENSIONB | - | $3^{\prime \prime} \times 23^{\prime \prime} \times 1^{\prime \prime}$ | in their working conditions.


| Paramete? | AL10 | AL20 | AL80 |
| :---: | :---: | :---: | :---: |
| Maximum Supply Voltage | 43 | 30 | 30 |
| Power output for 2\% T.H.D. $(R L-8 \Omega i=1 K H z)$ | $\begin{aligned} & 3 \text { watts } \\ & \text { Rys Min. } \end{aligned}$ | $\begin{aligned} & 5 \text { wratts } \\ & \text { RMS Min. } \end{aligned}$ | $\begin{aligned} & 10 \text { watts } \\ & \text { RMS 311n. } \end{aligned}$ |

AUDIO AMPLIFIER
MODULES
$\begin{array}{llll}\text { AL 10. } & 3 \text { wates } & \text { RMS } & 82.19 \\ \text { AL } 20 . & 5 \text { watts } & \text { R3IS } & 82.59\end{array}$

POWER SUPPLIES
PS 12. (Use with AL10 \& AL20) 88p SPM 80. (Usc wjthalso AL30 \& ALSO)
FRONT PANELS SP 12 with K nobs 1.10

The PA 12 pre-amplifier has been deaigned to match into mont buiget atereo aystems. It is compatible with the AL 10. AL 20 and AL 30 audio power amplifers and it can he supplled from thelr ansoctated power supplies. There are two stereo inputs, one hat been dealgned for use with Ceranic cartridges while the auxiliary input will wit most $\dagger$ Magnetic cartridges. Full detalls are given in the specincation table. The four controls are, Irom left to right: Volume and on/off switch, balance, bass and treble. Bize $152 \mathrm{~mm} \times 84 \mathrm{~mm} \times 35 \mathrm{~mm}$.

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## The STEREO 20

The 'Sterco 20 ' anplilier is mounted, ready wired and teated on a one-plece chassis measuring $20 \mathrm{~cm} \times 14 \mathrm{~cm} \times 6.5 \mathrm{~cm}$ This conpact unit comes complete with on/off awitch olume control, balance, ban and treble controls. ransioner, Power supply and Power aups. ing control knobs. The 'Stereo 20 ' has been designed to fit into mont turntable plinths witbout interfering with the mechaninm or, altermatively, into a separate cabines. Output power 20 w peak. Input 1 (Cer.) 300 ml into 1 M . Freq. res. $\mathbf{2} 5 \mathrm{~Hz}-25 \mathrm{Hzz}$. Input 2 (Aux.) 4 mV into 30 K . Harmonic diatortion. Bass control $\pm 12 \mathrm{~dB}$ at 60 Hz typlicalls $0.25^{\circ} \%^{a}$

Frequencs renponse-
$20 \mathrm{~Hz}-50 \mathrm{KHz}(-3 \mathrm{~d} \mathrm{~B})$ Bass controlTreble control- $14 \mathrm{KHz}^{\text {H }}$ -Input ${ }^{ \pm}$. Impedance 1 Meg ohm
Sensitivity 300 mV $\dagger$ Input 2. Impedance 30 K ohms Senalitivit 4 mV

The verastility of their design makes them ideal for use in recorl players, tape recorders, lereo maplinera and cand at home. tape players in the car and at home.

The above table relates to the ALIO, AL20 and AL30 modules. The following table outlines the ulderences

## PRE-AMPLIFIERS

PA 12. (Use with ALIO \& AL20) 24.35 PA 100. (Use with AL30 \& AL50) $£ 13-16$

## TRANSFORMERS

T461 (Une with ALl0) 61.38 P $\$$ P 15 p T538 (Use with AL20) $£ 1.93$ P\&P 15p BMT80 (Lse with AL30 \& ALS0) 28.15
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## PA 12. PRE-AMPLIFIER SPECIFICATION

Frequency Response 15 Hz to $100,000-1 \mathrm{~dB}$.
$\star$ Load-3, 4, 8 or 16 ohms.
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 IPN terices for use in the input atages which and treble controls
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Three suitched stereo hnputs, and rumbie and seratch fitters are featuren of the PA100
SPECIFICATION
Frequency Kesponse
Inputs: 1 Tape Head
$20 H z-20 \mathrm{KHz} \pm 1 \mathrm{~dB}$
Inputs: 1. Tape Head
$1-25$ mvinto $50 \mathrm{~K} \Omega$
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SHORT WAVE RECEIVER KIT


#### Abstract

All transistor T.R.F. Receiver tunes $S S 0 \mathrm{KHz}$ to 30 MHz (S40 to 10 metres) complete coverage-no gaps. Medium waves-TrawlersShip/Shore Telephone-All Six Amateur Bands 160-10 metres-International Broadcast from Australia, Far Eass, Russia, USA etc. using 4 miniature plug in Coils.

Hi-Gain FET Regen, Det./AF/AF Module giving full loudspeaker output to any external $2 / 3$ ohm speaker. Receives AM/CW/SSB.


Separate Electrical Bandspread, Calibrated Main Tuning.
A Quality CODAR-KIT with 12 months Guarantee. No technical, knowledge required, simple to built, printed circuit and Pictorial Instruction Manual, fully detailed step by step.
Complete Kit with 4 Coils (less standard PP6 battery).
E14.90 V.A.T./Carr. Paid.

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 FREE LEAFLETS ON REQUEST.NOTE: These CODAR Receivers meet the B,R.E.M.A. specification for Communication Receivers. Some portable receivers being advertised as Communication Receivers do not meet these requirements.

## TRADE DESCRIPTIONS ACT 1968

It is illegal to make false claims or misleading statements in advertising. The following are just a few extracts from the many letters received from satisfied cuscomers. All are unsolicited and can be inspected at any time.
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I am delighted with the CODAR equipment I am using....everything has come up to your specifications.

Dr. R. E. Wood, Louisiana State University, U.S.A.
Congratulaions on an excellent product. The PR40 Preselector is the first preselector I have found to operate efficiently with ample gain, and without feedback or image problems.

Mr, W, R. Jones, Woy, N.S.W., Australia.
The PR40 peaked signals remarkably and performed as you elaim. ! am very satisfied.
M. G. Bennett, Bath, Somerset.

I am very pleased with my CR70A-results are excellent with many overseas stations I have not heard before and excellent results on the Amateur Bands.

Mr. I. Macdonald, Coningsby, Lincoln.
Received Multiband Kit OK. Assembled it in two hours, worked a treat first time.

Mr, E. Joy, Chesham, Bucks.
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# SPECIALISTS 

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# "STEAM" ROLLING 

ANNUAL Reports and Accounts of major organisations do not usually make exciting reading, but the latest from the IBA is different because of the entries describing the planning of independent commercial radio under the IBA banner.
Most of the information we are either aware of already, or we took for granted as being necessary minimum standards that are laid down to match the existing performance by the BBC. However, one or two interesting points emerge that have an important bearing for the listening audience.

The IBA, with very good reason, intends to encourage the major proportion of listening on v.h.f. The International Telecommunication Union is due to review the allocation of m.f. bands, under the present Copenhagen Convention and Plan, in 1974-5. Any proposed revisions are expected to take effect from 1976 and both the BBC and the IBA are expecting a reduction in the m.f. allocation largely due to "overcrowding". In the meantime both organisations continue to operate sound broadcasting on m.f. as a back-up for v.h.f.

The crunch is in sight for the listeners because it looks as if they must expect, after nearly twenty years of v.h.f. broadcasting, to convert to v.h.f. reception or go without. We have heard the pros and cons of v.h.f. and m.f. so many times that we will not pursue the matter here. Suffice it to say that the IBA are looking ahead to the "day of judgement" by planming in force for circular polarised transmitting aerials to compromise between horizontal and vertical polarised receiving aerials.

The m.f. transmitting aerials will be directional systems using three or four mast radiators so that several stations can transmit over a restricted area on 1151 kHz . The radiated power will vary from one station to another, depending on local conditions, but in London it will be 0.5 to 1 kW ; elsewhere up to 5 kW , with an $8 \mathrm{~kW} \mathrm{mf1}$ and $30 \mathrm{~kW} \mathrm{mf2}$ signal from Saffron Green (not until later next year) for London, when the IBA have finished with the installations at Lots Road Power Station.

The method of m.f. transmission adopted is not commonly used in Europe and it makes one wonder why not, even if large sites are necessary.

The other disturbing thought is the increasing availability of stations broadcasting on v.h.f. With the undesirable side-effects (such as "birdies" and inter-modulation distortion) and the greater sensitivity of tuner front-ends, we forecast a congestion (or indigestion!) problem on v.h.f. in the U.K. within the next five years. Some serious thinking and re-appraisal is therefore going to be needed with a view to extending the broadcast v.h.f. range below 88 MHz ; although we understand that a clash has occurred in Hertfordshire and the police service is expected to be moved to another frequency, it would be wishful thinking to expect the emergency services to be transferred out of their present 97 MHz -plus domain.
M. A. COLWELL-Editor


Mid-Lanark A.R.C.

THE above club has sent us some details of the future programme. There will be a bring-and-buy sale on Nov. 9, a demonstration of stereo radio and quadraphonic sound by GM3UCI on the 23rd and the A.G.M. on December 7th. December 21st is called "Oklahoma" and GM3BVU will give a talk on Amateur radio in the U.S.

Meetings are held at 7.30 in the Wrangholm Hall Community Centre, Jerviston Road, Mother. well.

## Sonex 74

THE venue for Sonex 74 European High Fidelity Exhibition will be The Post House Hotel, London Airport and the dates March 29th to March 31st.

## WIRELESS TELEGRAPHY

## ACT

Readers and advertisers are reminded of the requirements laid down by the Wireless Telegraphy Act. It is an offence in the U.K. to install or operate wireless telegraphy apparatus except under the provisions of the Act and, except in the case of broadcast sound-only receivers, a licence must be obtained from the Minister of Posts and Telecommunications.

Included within the provisions of the Act are any apparatus transmitting deliberate signals for any purpose such as "walkie - talkies", radiocontrolled models or servos and some types of metal detectors. Apparatus radiating interference signals are subject to controls which also come under the administration of the same Ministry. If you require full information, please write to the M/n/stry of Posts and Telecommunlcatlons, Waterloo Bridge House, Waterloo Road, London, SEI 8UA.

Watch P.W. for details

## Open University Course

ELECTROMAGNETICS and Electronics, a Post-experience course by the Open University, aims to provide an understanding of the scientific basis of electronics and electronic circuit design.
The course is intended for those preparing for higher level university study in science and technology and for those who need a knowledge of electronics but who do intend to study at a higher level.
It assumes little prior knowledge of electronics or electromagnetics but does assume a background of scientific or technical education beyond GCE " 0 " Level.
The first part deals with the basic ideas of electricity, magnetism and electromagnetism, semiconductors and the properties of simple circuits. The remainder deals with electronic circuits, stressing the need to design circuits to meet specifications of noise, distortion, output voltage as well as gain and input and output impedance.
Applications are now invited for the course which starts next February and lasts until November. As with all 'Post-experience courses, no formal academic qualifications are needed. They are self-contained courses designed to teach new developments or update knowledge of a subject.
The course consists of 17 written correspondence units linked to 17 television and five radio programmes. Students are required to attend a one week residential summer school and encouraged to attend evening or Saturday tutorial sessions. There are 12 assignments to complete and an examination at the end of the course.
A home experiment kit, including a cathode-ray oscilloscope and a signal generator, is sent to students who are expected to design and build circuits for checking at summer school.

Some elementary mathematics is required for the course. Students should know elementary calculus, the meaning of sine, cosine and imaginary numbers. A preparatory booklet is issued at the beginning.
The course tuition fee is $£ 45$ plus $£ 37$ for the residential summer school. Application forms are available from The Post-experience Student Office, P.O. Box 76, Milton Keynes, MK7 6AA.

## What of D.N.L.?

PHILIPS l.td. will be using the Dolby-B noise reduction systen!!!

## Tyne/Wear radio contract

Aleading contender.
The Authority now proposes, subject to contract, to offer the franchise to Metropolitan, the chairman of which is Sir John Hunter.

The company's programme plans will be published when it begins broadcasting - probably during the summer of 1974.

## More for SQ

MORE manufacturers are getting onto the quadraphonic bandwagon by building SQ decoders into their equipment. Companies like Braun, Grundig, Korting, Philips, Revox, Saba, Sharp, Siemens have taken out SQ licences with CBS.

## New 4-channel system

Afrequencies. 45 kHz on the CD-4 records. making demodulators potentially cheaper.

## Scottish show cancelled

BECAUSE of lack of interest, the Scottish International Hi-Fi Exhibition has been cancelled. Only 12 of the expected 27 firms confirmed their bookings for the show.
The organisers feel that the reason for the lack of interest is that many companies have stretched their budgets by representation at the Harrogate and Olympia shows.

FTER interviewing the six applicant groups for the Tyne/Wear radio contr"ct, and giving full consideration to the written applications, the Independent Broadcasting Authority has announced that it has formed the view that Metropolitan Broadcasting is the

## Physics Exhibition

THE Council of the Institute of Physics has decided that the Physics Exhibition should now be discontinued, and the show arranged for 1975 will now not take place.

In recent years the number of visitors to the exhibition has decreased considerably as have the number of industrial firms and other concerns that used to have exhibits there.

The very first Physics exhibition was held by the Physical Society in 1905. The one held in 1973 was the fifty-seventh in this series. NEW quadraphonic sound system devised by Duane Cooper and developed by Nippon Columbia was demonstrated at the Berlin Radio Show. The new system is called New Discrete or Discrete Matrix. It is said to have certain advantages over other quadraphonic systems because of its dual nature. A typical set-up would use a twochannel matrix for surround sound named BMX. This involves $45^{\circ}$ phase shifts between the speakers rather than conventional $90^{\circ}$ ones.

If increased definition in image placement should be required, a demodulator for the carrier channels on the records would be added, giving the set-up a potential 20 dB separation between channels at mid-

The Discrete Matrix system allows the two extra channels contained on the gramophone record to be of a narrow bandwidth resulting with the maximum frequency of the record being 36 kHz compared with

Noise reduction techniques are not employed with this system, so


THIS receiver employs two transistors and two IC's, one of the latter in the intermediate frequency amplifier section and the second in the driver and output stages. It has band switching and covers all the important short wave ranges, including the low frequency bands, which are not included in some short wave or "all-wave" receivers.

The receiver has a very inexpensive but quite attractive cabinet and operates an internal loudspeaker, a jack allowing headphones to be plugged in when preferred.

## MIXER STAGE

The mixer section is shown in Fig. l and uses six miniature coils, the appropriate coils being selected by the 3 -way 6 -pole rotary switch. Each range is separate from the others and two coils are in circuit for each range. L1. L2 and L3 are the aerial coils, and L4. L5 and L, 6 the oscillator coils.

The six poles of the switch are numbered from Sl to S6. Pole Sl takes the aerial circuit to the aerial coupling windings of the aerial coils and S2 transfers the aerial tuning section of the gang capacitor, VCl , to the correct coil, for aerial tuning purposes. Pole S 3 connects the base of Trl to the base coupling windings, as necessary. The earthed ends of all aerial coupling windings (pin 9) and tuned windings (pin 1) are permanentiy connected to the chassis, while all the base coupling windings are returned to the base bias network R1/R2.

In a similar manner, switch section S 4 selects the collector coupling windings of the oscillator coils L4, L5 or L6, while S5 connects the emitter of Trl to the appropriate emitter winding. S6 selects the muned windings of the oscillator coils which are tuned by the second section of the ganged capacitor. VC2.

All the emitter windings (pin 7 of each coil) are returned to the emitter bias circuit, C2 and R3. In the same way, each collector winding (pin 8) goes to the IF amplifier.

In order to secure proper coverage and tracking, oscillator coil L5 has a padder capacitor CP1 of 3000 pF from pin 4 to chassis. L6 has a 1000 pF capacitor CP2 from pin 3 to chassis while L4 requires no padder, pin 6 being wired to the chassis.

If the circuit in Fig. 1 appears difficult to follow, it is suggested that the switch is set at its middle position and L2 and L5 wired in. The receiver can then be tested on this band. When it is found to be in order L1 and L4 can be added and wired and a check made that this works correctly, before adding L3 and L6. This is much better than wiring in all the coils, then perhaps finding that a mistake has been made with the switch contacts or the operation of the switch, so that some wiring error is difficult to locate and correct. To avoid any possible confusion here, the bands, approximate coverage, and maker's range numbers are as follows:-

| Band | Coverage |  | Maker's Range No. |  |
| :---: | ---: | :--- | :--- | :---: |
| A | $30-10 \cdot 5 \mathrm{MHz}$ | $10-28 \mathrm{~m}$ | 5 T |  |
| B | $15-5 \mathrm{MHz}$ | $20-60 \mathrm{~m}$ | 4 T |  |
| C | $5-1 \cdot 7 \mathrm{MHz}$ | $60-180 \mathrm{~m}$ | 3 T |  |

L1 and L4 are for Band A, L,2 and L5 for Band B and L3 and L6 for Band C.

In order to avoid squegging, or spurious oscillation and hissing spoiling reception, resistors $\mathrm{R} 4, \mathrm{R} 5$ and R6 are included in the individual collector circuits to L4, L5 and L6. The best values for these resistors depend on Trl. Gain is maximum when these resistors are of the lowest values which allow proper working of this stage. The values shown should certainly be satisfactory, but it is an easy matter to have on hand a few resistors of various values between about $100 \Omega$ and $1 \mathrm{k} \Omega$ (say about half a dozen different values) and try these in series with the circuit to pin 9 of each range, while tuning over the range. Excess oscillation is most likely at the high frequency end of any one band (VC2 nearly fully open).

Trimmers TCI, TC2 and TC3 are for aerial circuit trimming and each is adjusted on the appropriate band.


Fig 1, above, and fig 2, belon. give the complete circull of the receiver.


## IF AMPLIFIER

Fig. 2 is the circuit of the intermediate frequency amplifier and audio amplifier, which are constructed on one small circuit board. The IF filter consists of two loosely coupled units, IFT1 and IFT2, tuned to 470 kHz .

Output from IFT2 goes to ICl which provides three stages of amplification at 470 kHz and includes automatic gain control and detection circuitry, giving an audio output which is taken to the volume control VR1.
Resistors R10 and R1l form a potential divider across the 9 V supply and current is taken by ICl
and VR1 through R9. This means that the circuit should not be operated with VRl disconnected and that this potentiometer should be of the value given.

The mixer stage is fed from its own positive supply point at the junction of C3 and R7.

## AF AMPLIFIER

$\operatorname{Tr} 2$ is a high gain pre-amplifier, followed by IC2 which has 6 transistors and 3 diodes in a driver-pushpull output circuit which delivers approximately 250 mW to a $16 \Omega$ speaker. This IC is very economical on battery current and the output is easily adequate for normal loudspeaker reception. The load impedance is not too critical, so that speakers of higher impedance may be used. R14, R15 and R16 provide direct current feedback to stabilise the whole audio amplifier.

## CIRCUIT BOARDS

The mixer board is approximately $l^{1_{4}} \times l^{3}{ }_{16} \mathrm{in}$, Fig. 3 , with a bracket fixed as shown and a tag serving as a return point for $\mathrm{Cl}, \mathrm{C} 2, \mathrm{R} 2$ and R 3 . This bracket must be bolted tightly to the metal chassis so that the board is connected to the negative line.

External connections will be required to a few points. These can be made by providing Veropins, or by leaving a projecting wire. so that leads can be soldered on as necessary.
The small pins of Trl project from the underside of the board and connecting wires are soldered directly to them which will run to the sections of the bandswitch, as indicated in Fig. 3.

Both sides of the IF/AF board are shown in Fig. 4 and it is approximately $3^{3_{4}} \times l^{1} 4 \mathrm{in}$. Holes should first be drilled to clear the pins and can tags of the two IF transformers. If any small error is made when drilling these, they can be enlarged or elongated as necessary with a very small round file. Drill holes for two 6BA bolts. one marked MC is fitted with a tag which forms the negative return


Fig. 3: Layout of components on the mixer board.
to the metal chassis. These bolts should be at least ${ }^{1}$ in. long so that spacers or extra nuts will allow the board to be clear of the metal chassis.

C4 is underneath, directly from pin 4 of IFTl to pin 4 of IFT2, but all other items are on top of the board. Position these as shown. noting the polarity of electrolytic capacitors.

In most places the wire ends of the resistor and other items are long enough to reach the connecting points. Elsewhere, 24 s.w.g. tinned copper or similar connecting wire can be used. Sleeving is put on all leads which cross other wires and anywhere else where this appears necessary.

Two thin flexible leads are soldered on to connect to the speaker. A red flexible lead, with a positive battery clip, is also provided, as shown.

Colour coded leads also run from R9 and the base of $\operatorname{Tr} 2 . \mathrm{C} 7$ is soldered directly on the centre tag of the volume control, VR1. Fit a colour-coded lead from C3, to run on to Rl on the mixer board. A further lead is taken from pin 2 of IFT1, up through the board as in Fig. 4, and will be soldered to the circuit which connects pins 8 on the oscillator coils.


Rear view of receiver showing position of IF/AF board at front left with mixer board immediately behind.

## components list

Resistors

| Resistors |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| R1 | $18 \mathrm{k} \Omega$ | R7 | $1.2 \mathrm{k} \Omega$ | R13 | $33 \mathrm{k} \Omega$ |
| R2 | 15kS | R8 | $100 \mathrm{k} \Omega$ | R14 | $10 \mathrm{k} \Omega$ |
| R3 | $2 \cdot 7 \mathrm{k} \Omega$ | R9 | $10 \mathrm{k} \Omega$ | R15 | $15 \Omega$ |
| R4 | $680 \Omega^{*}$ | R10 | $1.8 \mathrm{k} \Omega$ | R16 | $1 \mathrm{k} \Omega$ |
| R5 | $820 \Omega^{*}$ | R11 | $3 \cdot 3 \mathrm{k} \Omega$ |  |  |
| R6 | $100 \Omega^{*}$ | R12 | $56 \mathrm{k} \Omega$ | VR1 | $25 \mathrm{k} \Omega$ |

Capacitors

| C1 | $0.01 \mu \mathrm{~F}$ |
| :--- | :--- |
| C2 | $0.01 \mu \mathrm{~F}$ |
| C3 | $0.25 \mu \mathrm{~F}$ |
| C4 | 22 p F |
| C5 | $0.02 \mu \mathrm{~F}$ |
| C6 | $0.1 \mu \mathrm{~F}$ |
| C7 | $0.047 \mu \mathrm{~F}$ |
| C8 | $0.01 \mu \mathrm{~F}$ |

Semiconductors $\left.\begin{array}{llll}\text { Tr1 } & \text { BF194 } & \text { IC1 } & \text { ZN414 } \\ \text { Tr2 } & \text { OC71 } & \text { IC2 } & \text { MFC4000B }\end{array}\right\} \begin{aligned} & \text { S.C.S. Components } \\ & \text { POB 26, Wembley. } \\ & \text { Middx.) }\end{aligned}$
Miscellaneous
IFT1/2 (Denco IFT13). L1, Blue 5T. L2, Blue 4T. L3, Blue 3T. L4, Red 5T. L5, Red 4T. L6, Red 3T. (All Denco). Tuning drive (Jackson Type 6/36 Cat. No. 4103). S1-6, 2 wafer switch, each 3 pole 3 way. Speaker, $2 \frac{1}{4} \mathrm{in}, 25$ to $40 \Omega$. Universal chassis members, $8 \times 4$ in (2) (Home Radio). Switched output jack socket. Aerial and earth sockets. Veroboard 0.15 in matrix, $1 \frac{1}{4} \times 1^{3} / 1 \mathrm{e}^{\text {in }}$ approx. and $3 \frac{3}{4} \times 1 \frac{1}{2}$ in approx. Wood for cabinet. Knobs.

1 Cl has three leads, positioned as in the underside view of this component, in Fig. 4. IC2 has four spills, 2 and 3 being longer, as in Fig. 4. If this IC is located as shown, the tags will fit the Veroboard holes correctly and connections being soldered on underneath. Both ICs should be soldered without
undue heating. It should only be necessary to keep the soldering iron in contact with the joint for a second or two. Lengthy heating may damage these items.

This circuit board should not be tested without VR1 and the loudspeaker being connected.

If a signal generator is to be used to adjust the circuits, couple this loosely to the lead running to pin 2 of IFT1. It is only necessary to place the generator lead near this lead with no actual connection. The cores of IFT1 and IFT2 should then be adjusted, with a proper tool, for best output.

When no generator is available, adjustment should prove quite easy as the IFTs are pre-aligned by the maker. It is then only necessary to tune in a stable signal and adjust each core for best volume. The cores should have a sharp resonance peak. Again, it should be stressed that a properly shaped tool must be used, as a wedge-shaped blade may easily break the cores so that they cannot be rotated, while inserting a steel or similar screwdriver will upset correct alignment.

The audio section should be found to provide good amplification and adequate loudspeaker volume. The small internal speaker will give quite reasonable audio quality, for SW listening purposes. A larger, external speaker may be plugged in (as well as phones) and this will naturally give some improvement. It should be of suitable impedance, about 16 to $25 \Omega$. Though a small speaker can give satisfactory results, it cannot be expected to be quite as good as a larger unit operating with its own cabinet or baffle.

## CONSTRUCTION

The chassis is a "universal chassis" flanged member 8 x 4in. with a second similar member used for the panel. The front edge of the chassis is set back ${ }^{1}{ }_{2}$ in. from the panel, as in Fig. 5, using two $1_{2} \mathrm{in}$. spacers and two $3_{4} \mathrm{in}$. countersunk 6BA


Fig. 4: The two sides of the IF/AF board and connections to the remainder of the circult.


Fig. 5: Layout of major components on top of the chassis and interconnections.
bolts, which run through the panel and the front flange of the chassis. (These two bolts with spacers are not absolutely essential, as chassis and panel are held in position by the case sides. However, with the bolts securing these parts together, assembly and testing can be completed before fitting the sides in position, and wiring is thus more easily reached.)

Locate the drive template on the panel and drill the fixing holes for it and for the dual-speed ball drive. A large hole is also punched for the projecting part of the drive which carries the cursor.

Position the bandswitch and VRl as in Fig. 5,
keeping these as low as possible to leave room for the speaker. The speaker opening is made with a large chassis punch or adjustable washer or tank cutter, or by drilling a ring of small holes and clearing up the edge with a half-round file.

Check that the panel and chassis are correctly fixed and at right angles, then fit the ganged capacitor into the drive and drill the fixing holes for the capacitor. Washers are placed under the capacitor to bring it level with the drive. The position of the drive and capacitor should be carefully adjusted as necessary so that they are in line and turn smoothly.


General view of receiver from above to assist in locating components shown in Fig. 5.

Holes $1_{4} \mathrm{in}$. in diameter are drilled for the six coils, which are located as in Fig. 5. Their fixing nuts should be tightened with the fingers only. Pins are counted in a clockwise direction from the space, from 1 to 9 , and wiring is simplified if all the coils are positioned so that their pins are approximately in the same direction.

The IF/AF amplifier board and mixer board are fixed as in Fig. 5, but it is easier to leave these off until most of the wiring has been done to the lower tags of the switch. which are otherwise difficult to reach.


Fig. 6: Method of mounting trimmers on top of the coils
Trimmers TCl, TC2 and TC3 are mounted directly across the coils L1, L2 and L3 as in Fig. 6. Short. stout wires are soldered to pins 1 and 6 of each coil, for this purpose, when wiring the receiver. It is preferable to take the upper plate tag of the trimmer to the earth side of the circuit (pin l) in each case.

The single oscillator trimmer. TC4, is soldered to the ganged capacitor as in Fig. 5, the top tag being connected to the capacitor frame by a stout wire. A check should be made that the tuning capacitor fixing bolts are not too long, or they may touch the fixed plates of the capacitor.

A bandswitch with two wafers was used. The front wafer switches the aerial, base and VCl circuits while the rear wafer is employed for the oscillator coils.

It is not essential to use a two-wafer switch provided the required number of poles are avail. able and the switch is small enough to be accommodated.

Fig. 7 shows connections to the switch. It will be found very helpful to use colour-coded leads here. With the aerial coils, yellow may be used for aerial and Sl circuits, with red for base and S 3 circuits, and green for $\mathrm{S} 2, \mathrm{VCl}$ and associated circuits. For the back wafer, red can be used for S 4. yellow for S5, and green for S6. Chassis returns to the coils can be black and the base bias circuit to $\mathrm{Cl} / \mathrm{R} 2$ may be blue. Whatever colours are used. employ them exclusively for one circuit.

It is also helpful to solder on lengths of wire. before mounting the switch, where the tags will be near the chassis, and hard to reach later. These wires can then be cut to length and taken to the various coils.

If the contacts of the switch cannot be seen, and its operation is not wholly clear, test it for continuity with a meter, in each position. Also it is advisable to wire in the coils for one band only, to confirm that no error is being introduced here. before proceeding with the other ranges.

Pressure should not be imposed on the coil pins when these are hot, so a little care is required when soldering these to prevent them moving when the insulation softens.

The volume control is mounted as in Fig. 5. Connect the lower tag to S7 and to the metal chassis. Run a lead from the other outer tag, under the chassis and up through a hole near the AF amplifier, where it is soldered to R9, Fig. 4. Solder C7 to VR1 slider and take a further insulated lead under the chassis and up through to the junction of R12 and R13.


Fig. 7: Details of the wiring on the bandchange switch wafers.

## ALIGNMENT

Alignment of the IFT's has been described. To align the aerial and oscillator coils, deal with one band at a time. Adjust the coil cores at a low frequency in the band ( $\mathrm{VCl} / 2$ nearly closed) and the appropriate trimmer at a high frequency in the band (VCl/2 nearly open).

TC4 is initially set about half closed. If it is subsequently found that TC1, TC2 or TC3 is fully open for best volume. TC4 should be screwed down slightly. Provided TC1, TC2 and TC3 each have a definite peak giving best volume, there is no need for a separate trimmer for each oscillator coil.

Coverage is primarily determined by the settings of the oscillator coils and TC4. If a signal generator is available, set $\mathrm{VCl} / 25^{\circ}$ from the fully closed position and adjust the core of L4 for reception on $10 \cdot 5 \mathrm{MHz}$; similarly adjust L 5 for reception on 5 MHz , and L 6 for reception on $1 \cdot 67 \mathrm{MH} \%$

Ll should then be adjusted at 11.5 MHz for best volume. L2 is similarly adjusted at $5 \cdot 5 \mathrm{MHz}$, and L3 at 1.83 MHz . VCl/2 is then opened to tune to 28.5 MHz , and TCl is adjusted. TC2 is adjusted at $13 \cdot 5 \mathrm{MHz}$, and TC 3 at $4 \cdot 5 \mathrm{MHz}$.

These adjustments are repeated until no further improvement is possible. These frequencies are the most effective tracking points for the low frequency and high frequency end of each band and result in best tracking throughout the whole range.

## CALIBRATION

The tuning drive listed has a scale marked $0-100^{\circ}$. in addition to scales for individual calibration. Set the cursor to $100^{\circ}$ with the tuning capacitor fully closed. If calibrated as described the following points, read against the $0-100$ scale, may be used as a guide to intermediate frequencies:-

| Range $\mathbf{A}$ |  | Range B . |  | Range C |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 30 MHz | $12^{\circ}$ | 15 MHz | $7^{\circ}$ | 5.0 MHz | $8^{\circ}$ |
| 28 MHz | $15^{\circ}$ | 14 MHz | $10^{\circ}$ | 4. 5 MHz | $12^{\circ}$ |
| 26 MHz | $17^{\circ}$ | 13 MHz | $13^{\circ}$ | 4.0 MHz | $17^{\circ}$ |
| 24 MHz | $19^{\circ}$ | 12 MHz | $16^{\circ}$ | 3.5 MHz | $22^{\circ}$ |
| 20 MHz | $27^{\circ}$ | 11 MHz | $19^{\circ}$ | 3.0 MHz | $29^{\circ}$ |
| 18 MHz | $32^{\circ}$ | 10 MHz | $23^{\circ}$ | $2 \cdot 5 \mathrm{MHz}$ | $41^{\circ}$ |
| 17 MHz | $36^{\circ}$ | 9 MHz | $28^{\circ}$ | 2.0 MHz | $62^{\circ}$ |
| 16 MHz | $40^{\circ}$ | 8 MHz | $35^{\circ}$ | 1. 9 MHz | $70^{\circ}$ |
| 15 MHz | $45^{\circ}$ | 7 MHz | $44^{\circ}$ | 1.8MHz | $79^{\circ}$ |
| 14 MHz | $52^{\circ}$ | 6 MHz | $59^{\circ}$ | 1.7MHz | $89^{\circ}$ |
| 13 MHz | $60^{\circ}$ | $5 \cdot 5 \mathrm{MHz}$ | $71^{\circ}$ |  |  |
| 12 MHz | $70^{\circ}$ | 5 MHz | $85^{\circ}$ |  |  |

## CABINET

Each side of the cabinet is 6 mm plywood, approximately $5^{1} 4 \mathrm{in}$. deep, to give a front projection. The sides are $4^{1}{ }_{2}$ in. high at the back, and 5 in. high at the front, to tilt the panel backwards slightly. (Note, however, that panel and chassis remain at right angles to each other.)

A strip of wood $8 \times 1 \times{ }^{1}{ }_{2} \mathrm{in}$. with a rounded front edge is fitted under the panel by means of two self-tapping screws run into the lower flange of the panel.
The cabinet top is $8 \times 5^{1} 4 \mathrm{in}$. and it is screwed to the back, which is $8 \times 4 \mathrm{in}$., by means of an inner strip about $8 \times 1 \times{ }^{1}{ }_{2}$ in. in size. This completed part (top and back) is secured with two self-tapping screws into the front flange, and two bolts at the back, so that it can be removed to renew the battery. The bottom of the chassis itself may be left open, or closed with a sheet of hardboard.

## PW TECHNICROSS PUZZLE Solution to No. 1 presented last month



## IEEUSTII

## IN THE DECEMBER ISSUE

## VISION MIXER

This easily built unit enables the outputs from two CCTV cameras-or more if extra channels are added-to be faded, switched or mixed. The unit produces a constant sync signal by taking the pulses from the "camera 1 " channel and adding them to whichever video signal is selected.

## ADDITIONAL I.F. AMPLIFICATION

There are several situations in which additional i.f. amplification can be useful. Simple transistor stages can also make it economically worth while. This article shows how.

## SERVICING TV RECEIVERS

The next chassis to be dealt with is the GEC Series 1 single-standard chassis. We shall also be resuming the Philips G6 colour chassis.

## DX RECEIVER SYSTEM

Following the recent article on varicap tuning units last month this article describes some receivers for DX operation.

## COLOUR BRILLIANCE CONTROL

With the three c.r.t. drives necessary in a PAL colour receiver the traditional simple brightness control system is no longer suitable. An examination of the technique used instead provides a valuable insight into video circuit arrangements.

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THERE are a mumber of molegrated circuil audio power amplifiers available at the present time One of these, the 1,M380N device, has a number of features which make it attractive to the aınateur experimenter. In particular, it is very useful in circuits requiring the minimum number of components. The device is manufactured by the National Semiconductor Company, and is available from Ambit International. 37 High Street, 13 rentwood. Essex. or Athena I,td.. 140 High Street. Eyham. Surrey.

## ADVANTAGES

The LM380N automatically 'centres' its output at one half of the power supply voltage. This eliminates the need for additional circuitry (including a pre-set potentiometer) which is required with some other types of amplifier for adjusting the bias so that maximum voltage swing (and hence a maximum power output) can be obtained.

The LM380N device also incorporates internal protective circuits. If the silicon chip becomes too hot (above about $150^{\circ} \mathrm{C}$ ) owing to incorrect operation. the circuit automatically becomes inoperative for a time until the chip has cooled. Protection is also incorporated against excessive current in the output stage; such currents will occur if the output is accidentally short-circuited. The limiting curvent in the output stages is about $1 \cdot 3 \mathrm{~A}$.

The I.M380N can feed up to 2.5 W to an 88 loudspeaker when operated from all 18 V supply. The absolute maximum permissible supply voltage is 22 V , but it is wise to use a somewhat lower value to allow a margin for error. The writer has found that satisfictory loudspeaker volume can be obtained using the minimum recommended supply voltage of 8 V . 'the total harmonic distortion is $0.2 \%$ at 2 W output using an 18 V supply.

It is normally convenient to use the L.M380N in a standard 14 pin dual-in-line socket so that it can

[^6]be removed easily from the circuit. However, one can solder directly to the terminals of the device.

## CONNECTIONS

The connections of the L,M380N are shown in Fig. 1. The input signal can be fed either to the nodinverting input or to the inverting input. Generally it is more convenient to feed the signal to the noninverting input and to leave the inverting input unconnected.

If, however, the sigmal is fed to the inverting input, the non-inverting inpul should be returned to earth through a capacitor or a resistor or directly carthed. This will prevent positive feedback from the output to the non-inverting input causing instability. A capacitor is preferable when the signal source has a high impedance, but with a source of moderate impedance a resistor approximately equal in value to this source impedance is preferable to maintain the balance of the differential stage. When the source impeditice is low. the non-inverting inpul may be eartherd.

## GAIN

The voltage gaill of the LM380N is lixed at 50 (or 34d13) by the internal circuitry of the device. Although this fixed gain limits the versatility of the amplifier, it does resull in a minimum number of external components bring required for its use.

## HEAT SINK

The LM380N device itself can dissipate up to $1 \cdot 25 \mathrm{~W}$ when operated without any heat sink al anbient temperatures of up to $25^{\circ} \mathrm{C}$; this is adequate for many applications. For example, Fig. 2 shows that the power does not exceed $1 \cdot 25 \mathrm{~W}$ at supply voltages up to 14 V when an $8 \Omega$ speaker is employed. Even if a higher supply voltage is used, it is not likely that the dissipation will exceed 1.25 W for an appreciable time.

Fig. 3 shows that there is still less chance of overheating when a $16 \Omega$ speaker is employed. In this case, the supply voltage would have to exceed 20 V for the dissipation to exceed $1 \cdot 25 W$.

In the case of a $4 \Omega$ speaker, however, Fig. 4 shows that the dissipation can reach 1.25 W when a 10 V supply is used. If a much higher supply voltage is enployed, the pins $3,4,5,10,11$ and 12 of the device should be soldered to a copper heat sink of


Figs. 2, 3 and 4: These graphs show dissipation of the LM380N against output power for various values of supply voltage and loudspeaker impedance
area about six square inches.
The three per cent total harmonic distortion line shown in Figs. 2 to 4 is approximately the onset of clipping.

## POWER SUPPLY

If there is hum or noise on the power supply line, a hum rejection of about 38 dB can be obtained by connecting a $5 \mu \mathrm{~F}$ capacitor from pin 1 to earth. A smaller capacitor will also provide some measure of hum reduction.
If the power supply leads from a battery or filter capacitor are longer than two or three inches, a $0 \cdot 1 \mu \mathrm{~F}$ capacitor should be connected between pin 8 and earth to prevent oscillation.

In addition, a $2 \cdot 7 \Omega$ resistor in series with a $0 \cdot 1_{\mu} \mathrm{F}$ capacitor may be connected between pin 8 and earth to suppress any high frequency oscillations.


Fig. 5: A simple circuit using the LM380N.

## SIMPLE CIRCUIT

The simplest circuit using the LM380N is shown in Fig. 5. The $470 \mu \mathrm{~F}$ capacitor must be placed in series with the loudspeaker to prevent a steady current from flowing through the speaker from pin 8. A smaller capacitor than that shown will result in inferior bass response.


The input pin operates with a mean potential equal to the earth potential. A capacitor in series with the input pin is therefore required only if the


Fig. 6: A record player amplifier suitable for use with a crystal or ceramic plck-up cartidige.
mean potential of the signal source is not also at earth potential.

The writer has used the circuit of Fig. 5 in a radio receiver. Fig. 6 shows how a similar circuit may be used as a record player amplifier with volume and tone controls. The input impedance of the LM380N is about $150 \mathrm{k} \Omega$.

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Fig. 7: A high inpul impedance achieved by use of a common-mode volume control.

## HIGH IMPEDANCE INPUT CIRCUIT

An amplifier with a high impedance input is shown in Fig. 7; it is suitable for use with high impedance signal sources such as a crystal microphone. This circuit employs a 'common mode' volume control. When the potentioneter slider is at the bottom of its travel in Fig. 7, the input signal is fed to both the inverting and the non-inverting inputs. In this case the signals will almost cancel in the device and the output will be small. When the potentiometer is at the lop of its travel, however, only pin 2 will receive an appreciable input voltage and maximum volume will be obtained.

The circuit of Fig. 8 shows how a common mode volume control circuit may be used with a common mode tone control to maintain the high input impedance.

A very high input impedance amplifier can be made using the field-effect transistor input circuit shown in Fig. 9. At low frequencies the inpul impedance is 22 megohms, but at high frequencies the input impedance is reduced by the gate to drain capacitance of the field effect transistor

## INTERCOM SYSTEM

A simple circuit for an intercom system is shown in Fig. 10. The transformer ratio of $25: 1$ multiplied by the gain of the LM380N produces a loop gain of 1250 . The roles of the input and output speech transducers are reversed when the switch is operated.


Fig. 8: This circuit features common-mode controls for both volume and tone.


Fig. 9: The addition of a FET input stage gives a very high input impedance.


Fig. 10: An intercom system in which the loudspeakers double as microphones. The view above shows the amplifier with controls attached.



## DUAL POWER SUPPLY

Another simple circuit using the LM380N is shown in Fig. 11; it provides a dual voltage supply balanced with respect to ground from a single supply. If the input is 20 V , outputs of +10 V and -10 V can be obtained. The potentiometer can be used to balance the outputs relative to ground, but may be omitted if exact balance is not required.
An advantage of this circuit is that a high quiescent current is not taken when little current flows in the outputs.

## EXTRA GAIN

Although the gain of the LM380N is fixed at 50 by the internal components, higher gain can be obtained by using additional positive feedback. For example, Fig. 12 shows how a gain of 200 can be obtained.


Fig. 11: A circuit to provide a spift power supply from a single source.


Fig. 12 : Increased gain may be obtained by the use of positive feedback.
The maximum gain is around 300, since attempts to obtain still higher gain may merely result in oscillation.

## SUPPLY POLARITY

As in the case of most integrated circuit audio amplifiers, if the power supply to the LM380N is applied with the polarity reversed, a large current will flow and the device will almost certainly be destroyed within a few milliseconds.

Readers may therefore wish to incorporate a diode in one of the power supply lines (normally the positive line). If a supply of reverse polarity is accidentally applied to the circuit at any time, the diode will prevent any appreciable current from flowing and will thus protect the LM380N. It is, of course, essential that the diode is connected with the correct polarity, see Fig. 12.


## Microwave distance Record

On Thursday, 13th September a
 between GW8CKT/P on Snowdon and GM8AZU/P on the Cairnsmrore of Fleet. We believe that, at 212.5 km , this is a new British distance record.

Weather conditions were far from ideal, with gale force winds and both ends of the link well above the cloud base. Visibility
on Snowdon at 3560 feet was only 15 yards, and on the Cairnsmore of Fleet at 2300 feet was only 20 yards. The high wind on Snowdon made it impossible to use a dish aerial and so a 10 dB horn was used. At the Scottish end a 32 in . dish was used, and a considerable amount of luck was in evidence when the beam heading, estimated using a cheap plastic compass, turned out to be correct to better than $0.5^{\circ}$. Earlier attempts to find a signal using a 10 in . dish at the Scottish end had failed. Signal reports exchanged were readability 5 and strength 6/7.

Equipment used at GM8AZU/P: Tx, Mullard CXY19 Gunn device, output approximately 100 mW ; Rx, Mixer CS10B, Local Oscillator, Mullard CL8370; i.f., 70 MHz ; ANT, 32 inch dish with horn feed.

Equipment used at GW8CKT/P: TX, Mullard CXY 19 Gunn device, output approximately 120 mW ; RX, Mixer, balanced pair of Mullard BAW95, Local Oscillator,

Mullard CL8380; i.f., 70 MHz ; ANT, Small horn.

The equipment, which was all solid state, was carried to the summits of the two mountains concerned. Pundits who ask why the GW team did not use the train, may be interested to know that the train was not running due to the bad weather so it's just as well that they bargained on climbing!

80 m talkback was used between the two base camps in order to co-ordinate the departure for the climb to the summit.

2 m talkback was used from summit to summit.

Those involved were:-
At the GM end: G3VUQ, G3YCQ, G8AMG, G8APZ, G8AZU, G8DKK. At the GW end: G3XSO, G3YMV, G8BPN, G8CKT, G8ENX, G8FTB, G8HCO.-Michael H. Tooley, G8CKT, (Weybridge, Surrey).


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## Zetter from $\mathfrak{A m e r i c a}$

FOR several years I have read your column religiously and at long last decided to write to you. Needless to say I have an avid interest in Vintage Radio. However, I have had to content myself with vintage parts, valves, radio books and magazines. Additionally I construct simple vintage radios out of antique parts using my own circuits or those from Hugo Gernsback publications from the early ' 30 's. My valve collection fortunately contains many good useable valves. At present I am constructing a short wave receiver (semi-antique) using types ' 35 and ' 27 (U.S. tubes) and meant for mains operation.

I started my radio hobby in 1928 with a commercial crystal set (Vario Couple Type). I made crystal sets until 1932 when I started on valve short wave and medium wave receivers. My hobby continued through 1935 and 1936. It was interrupted in 1937 by my joining the U.S. Army. I did only occasional short wave listening thereafter until 1946 when I went back to radio construction.

My recent vintage radio construction includes a one tube SW receiver (using a transmitting type '30). The coils (plug-in) are my originals from 1932. These are about the only parts surviving from that era. While I was in the army in pre-World War 2 days, a relative threw the rest away! I also have two surviving books.
The other receivers are a Short Wave Portable which is a good copy (including original vernier dial) from an article in a 1933 Short Wave Craft Magazine. I had been planning to build it for decades and only made it last year. Also I have a breadboard type Medium Wave receiver using a type '99. (A very good performer with one modern part-a ferrite rod aerial in it). I use it mostly for a quick test of old tubes. Much better than the tube tester!

I possessed one vintage radio in recent years (an RCA Radiola) but an avid collector got it away from me. All I have at the moment is a vintage tube tester, Signal Generator and Output meter (Weston, circa 1929). The trouble is that some collectors in this country possess 100 to 300 radios leaving none for us pickers.-Chester A. Beck, K6DFP, ( 9045 Margaret Street, Downey, California, 90241, U.S.A.)

Mr. W. H. Quick tells us that he has been given an old one-valve radio which he would like to get going. He would like to know what the L.T. and H.T. voltages are. There is a $1 \cdot 5 \mathrm{~A}$ fuse fitted and we show in the diagram the front panel and a plug-in coil which fixes to the side of the set.

If anyone can help Mr. Quick, they can contact him at 15 Beechwood Grove, Horbury, Wakefield, Yorkshire.


Mr. Quick's plug-in coll and the front panel of his vintage receiver.

(1) = Brass terminals

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## PART 3-TRIGGER CIRCUITS

LAST month we saw that there is, at least, one circuit which is sensitive to the rate of voltage change, i.e. the divider circuit would only respond correctly if we caused rapid changes in lighting level at the photo cell; slow changes would not make the divider work. There are other circuits


Fig. 14a. If PCCI and RI are used as alternatives, omit VR1 and link in PCCI on the "left-hand" end of R2.
which like to see what are known as "fast going edges" to signals; as a result, a range of circuits has been developed which will accept slow changing inputs and convert these into signals having fast rise and fall times.

These eircuits are called triggers because their


Fig. 15 a. The extra stage of amplification effectively improves the rise time of the outout signal between the power rall extreme voltages.

Fig. 14b: T-Dec layout for Fig. 14a.


Fig. 15b: T-Dec layout for Fig. 15a.
output will always be in a certain state (say zero volts) until the input signal rises to a certain level and, irrespective of the time it takes the input to get to this level, when the critical voltage has been reached the output changes to a higher level (say +9 V ) instantaneously.
In practice everything takes a certain amount of time to happen, so "instantaneously" is, perhaps, too strong a term to use. Nevertheless, as you will see if you do some of the following experiments, we can make extremely slow voltage changes trigger a circuit to give edges to waveforms that change from one level to another in a few millionths of a second.

## Fast and slow "edges"

First of all we had better look at what we are calling an "edge" so that we can compare the difference between fast and slow edges. Fig. 14a is a very simple transistor amplifier stage which gives an output inversely proportional to the voltage at the wiper of VRl (or, if you are using the photocell alternative, the junction of PCCl and R1).

Measure the voltage at the collector of Tr 1 with VR1 set to the bottom of the track (Alternatively completely shade PCC1). You should read about +9 V because the transistor, in the absence of base current, is not conducting. Slowly increase the voltage at the wiper of the potentiometer by rotating it (or slowly increase the amount of light falling on PCC1); base current will start to flow and the voltage at the collector will start to fall.

The thing to notice is that you can control the level of the measured voltage quite easily and get any value you like by careful adjustment of VR1 or the amount of light falling on PCC1. Try and get a "feel" for the rate at which the measured voltage changes for given rates of moving the potentiometer or illuminating the cell.

You can use the wires $A$ or $B$ in the layout and transfer one, or other, of them to point X-depending on whether you were using the cell or the potentiometer. Fig. 15a shows an extra stage of amplification. Carry out the same experiment but now measure the voltage at the collector of Tr 2 . Obviously the extra stage gives us inversion so when the potentiometer is down the measured voltage is low.

Now slowly increase VRl until the voltage starts to rise and then try and control it in the same way as before. It should be very apparent that, for the same rate of change in position of the wiper of


Fig. 16: Note the increased amplification appears to enhance the slgnal's rise time between the supply voltage limits.


Fig. 17a. True trigges action is oblamed by using positive feedback via R4.


Fig. 17b: T-Dec layout for Fig. 17a.
the potentiometer, the voltage at Tr 2 goes from zero to +9 V very much quicker than it did before.

It is, however, still possible to set it mid-way between the two extremes by careful adjustment. The effect is even more pronounced using the photocell and you should start to appreciate the increase in the rate of change of the signal at the output.

## Amplification

The signals we have been talking about can be described as waveforms as shown in Fig. 16. The portion of the signal between the low and high voltages of the output is called an edge and you can see that it has become much steeper with the extra amplification.

Simple amplification thus increases a signal's rise time but there is still the possibility of getting a mid-rail voltage during the transition-especially if the input signal was unusually slow. Ideally we


Fig. 18a: Schmilt trigger circuil. The trigger level can be controlled over small limits by changing R1 in the range $1 \mathrm{k} \Omega$ to 470 ks .


Fig. 18b: T-Dec layout for Fig. 18a.
would like to have a circuit that gives a fast change irrespective of the rate of change of input. The circuit in Fig. 15a has been modified in Fig. 17a with a resistor coupling the output back to the input. We have introduced a positive feedback loop.
If VR1 is slowly increased the voltage at $\operatorname{Tr} 2$ collector will, at some time start to rise; when this happens current starts to flow through R4 back into the base of Trl and effectively increases the base current we are already applying from the potentiometer. The effect is to make the voltage at $\operatorname{Tr} 2$ rise even more enhancing the effect until eventually Tr2 is totally non-conducting. All we needed to do was set the operation in motion by initiating base current into Trl; once that was started the voltage at Tr 2 collector would move from zero to +9 V without any further movement of the potentiometer-the feedback loop did the rest.
The feedback cycle occurs extremely rapidly (the speed is limited only by certain internal parameters of the transistors) so the output changes level at a speed set by the circuit and no longer by the rate at which we turn the knob on VRI. Try it for your.
self and you will find it impossible to set a mid rail voltage at the output.

When VR1 is at the limit of its travel. try turning it down; the same thing happens on the downward going edge of our input signal. Notice that there is a sort of "no-mans-land" between the positioning of the wiper for upward going triggering and downward triggering. This is known as "hysteresis" and is very useful in differentiating between the two levels we are considering.

## Hysteresis

In this circuit, you can control the amount of hysteresis by means of the value for R4. A $470 \mathrm{k} \Omega$ resistor will give the smallest differential between upward and downward triggering levels but by reducing it to $100 \mathrm{k} \Omega$ you can widen the gap between the levels. This circuit is operating as a true trigger and the feature to take note of is the use of positive feedback to speed up the edge. If you think about the circuit a bit you will find it is not very different from the bistable described last month.

## Schmitt trigger

Probably the best known trigger circuit is the Schmitt trigger shown in Fig. 18a. When the voltage


Fig.19a: Basic monostable multivibrator. Capacilor C1 can be increased to $3,000 \mu \mathrm{HF}$ to extend the dwell time.


Fig. 19b: T-Dec layout for Fig. 19a.
at the wiper of VRI has reached a certain level base current will start to flow in Trl and the voltage at its collector falls slightly; this reduces the base current into Tr 2 . The two emitters are, however, connected together and as Trl starts to conduct the voltage at the "top" end of R3 starts to rise.
Because this is connected to the emitter of Tr 2 we reduce-even more-the potential difference. between Trl collector and Tr2 emitter thus the base current into Tr 2 becomes less. Here again we have a positive feedback loop caused by emitter coupling and the effect of this is to accelerate $\operatorname{Tr} 2$ going out of conduction and the output voltage drops very rapidly.
Again this occurs independently of the rate we are applying signal at the input and the speed is limited only by the transistors' parameters. Reduce the input voltage slowly and the opposite happens.

## Monostable multivibrator

Another circuit which often comes into the category of trigger circuits is the "monostable multivibrator" shown in Fig. 19a. Unlike the Schmitt trigger it is a little bit more complicated to initiate triggering but it offers a useful bonus. It has a "short term memory". We can design it so that it will trigger rapidly on the receipt of a suitable signal but the output from it stays at the new level for a fixed period of time before rapidly returning to its original state.


Fig. 20a: Touch-sensitive child's room-light. Supply current is approximately imA rising to aboul 80 mA when the lamp is on. Duration of $3 \frac{1}{2}$ minutes can be oblained by making $\mathrm{Cl} 3.000 \mu \mathrm{~F}$ and C2 $50 \mu$ F. The capacitor shown dotted, across C2, indicates how It is connected-plus to R2.


## Touch switch

The monostable thus gives us trigger action and a timing function which can be put to many uses. A novel circuit for a safe child's bedside light is shown in Fig. 20a. It is a touch sensitive switch coupled to a monostable that switches on a lamp for a pre-determined period of time (Warning: the novelty is more likely to keep a child awake than get him off to sleep!).

## ON RECENT DEVELOPMENTS

## THE YEN

HAVE you ever had a yen to do something?-the Japanese have. My ageing eyeballs have recently scanned a report which comes from the Orient from an "impeccable source". In February of this year, the Electronic Industries Association of Japan found that the total sales of electronic parts and components from Japan amounted to 101,079 million yen - which is a lot of yen for just one month's effort. It is interesting to see how this figure breaks down. For example, electron tubes (that's valves in English or Toobs in American) in February amounted to 17,841 million yen and showed an increase in February 1972 of over $10 \%$. Integrated circuits accounted for 8,483 yen and showed an increase over the same month last year of a staggering $92 \%$. On these figures, the Western comics who chant "Ha so?" might easily find the answer to be "Velly well thank you".
Other news from Japan is equally interesting. One snippit from spies is that Sony are to withdraw from the electronic calculator market altogether. Another is that Government approval (Japanese) has been given for the joint enterprise between Alps Electric and Motorola for the manufacture and sale of ICs. This American/Japanese Company is aiming to sell 3,000 million yen's worth of ICs in 1974.

## KEEPING A WATCH!

Still in yen land, the Japanese watch industry is claiming that some 200,000 watches using piezo-electric crystals, will be produced there this year. Production lines are eagerly being set up to manufacture C-MOS ICs and there is a hive of activity in the liquid crystal readout sector. If all this activity goes through, then clearly now is the time to watch Japan.

## MINI FREQ. COUNTER

What other interesting things are happening in Japan? Well, quite apart from the considerable amount of electronics business that's taking place (would you believe that this country sold 83,349 million yen's
worth of communications equipment in 1972?) there is always the neatness, the preciseness of some of the products. Perhaps an excellent example is in the field of frequency counters-feed a signal in and the frequency is flashed up on a digital readout. Well, one Company (and I'm talking about a production item, not a prototype laboratory wonder) is marketing a miniature but professional standard frequency counter. It gives a digital readout of frequency from 15 Hz to 50 MHz although there is an optional pre-scaler which extends this to 220 MHz at the upper limit. It's completely portable and uses internal rechargeable cells. The internal oscillator is accurate for the majority of applications having a stability of $\pm 0.0005$ at $25^{\circ} \mathrm{C}$. The size is particularly impressive- $120 \times$ $175 \times 25$ millimetres. Just grab yourself a ruler or do a quick mental conversion and you'll see that this slips into your pocket (there's $25 \cdot 4$ millimetres to the inch!).

## LASER TELEVISION

One could hardly look at the Japanese electronics scene without taking in the television industry. Latest thing in this sector to catch my eye is a large screen laser colour television projector. This beasty is a considerable improvement over its younger sister which made a debut at the World Exposition in Osaka in 1970. The earlier model had a resolution of 525 lines. The latest version has a resolution of 1,125 scanning lines. A krypton ion laser is used to generate the red, while an argon ion laser emits the green and blue spectrums. Perhaps we're not at the home use stage yet, but maybe the time will come when an entire wall will light up with a full colour, 3D life-size TV screen-so real you'll be able to step through your kitchen wall and join in a quick romp with Noddy or a punch-up with Ena Sharples; the mind boggles.

In serious terms, the new laser colour television projector has some very real advantages. The image is very clear and sharp. It is also very bright and there is very little divergence, too. One feature which my Japanese contact did not highlight but which is of interest is that the
polygonal mirror used for horizontal scanning rotates in magnetic bearings. These have certain advantages over conventional bearings, notably reductions in noise and vibration.

## CHINESE PUZZLE?

How many characters or words do you think there are on this page? How about a page in a Chinese newspaper then? No, I haven't nipped across on the Kowloon ferry, I'm still in Japan where a leading electronics manufacturer has just launched a very high-speed printer which prints out the Chinese language. It will produce some 600 lines of Chinese in 60 seconds which, as I'm sure you know, works out at 12,000 Chinese characters every minute. A computer is used to hold information prior to printout but manual over-ride can be used. The printout can be in either lateral or vertical rows so it doesn't matter which way you want to read it-the machine can oblige. Damn clever, those Chinese, or should that be Japanese? I'll have to get myself properly orientated.

## EARTH STATIONS

In the early days, the Japanese electronics industry suffered (rightly or wrongly) from a "cheap goods" brand. It is now no longer possible to regard all its products as in this category. An earth terminal is no small thing, neither is there any room for sub-standard effort. In this field, one Japanese Company alone has built, supplied and/or installed very nearly 50 (fifty) earth stations.

## GET ORGANISED!

A little gem from England to finish with. In a church at the Royal Naval Air Station Yeovilton, Somerset, an electronic organ began to play itself-a radar beam was being picked up by some of the internal components. About time the Navy got itself organised!
Cimbers

# ARETOU wiritie-on? make this UTTRASONIC Renote CONTROLER 

 By the flick of a switch from your armchair you can switch on the television, radio, lamps, intruder alarm, electric kettle, electrically operated curtains, operating rotating aerials, darkroom lights. For bedridden patients, handicapped and elderly people, there is a multitude of uses for this valuable tool, from remote signalling to opening electrically operated doors-without the need for them to go near the mains supply. Your son can have a lot of fun, too, if you make it for a Christmas gift.
## AF/HF/VHF TROUBLE-TRACER

Our Trouble-Tracer will provide you with a test signal ranging from audio to VHF. Test probes pick up signals from the equipment under test and feed them into an amplifier and speaker. All in the one cabinet-What else could you want?


# RORTABLE FITISTENTLAMPU ofromyour 1ev batn 



## FOR: EMERGENGY LIGHTING,GAR

 HE battery operated 15 W fluorescent lamp unit described here is of simple construction, being designed around readily available components. The whole assembly is made up in aluminium, consisting of a framework which supports the tube and houses the oscillator module. A cover plate acts as reflector and dust cover.
## CIRCUIT DESIGN

Fig. I shows the circuit. A 2 N 3055 silicon power transistor operates as a transformer coupled class ' C ' oscillator. The fluorescent tube is supplied from a third winding on the transformer. Satisfactory operation is obtained from 10 to 15 V .

A variable resistor provided in the base circuit of the transistor ensures correct operation with devices having any gain within normal spreads. The



## WHW \& GARS,LOFTS,SHEIS, GABAGES, MDBILE RALIES, ETC...

Wansformer is designed around Mullard FX2242 pot cores. The collector winding is tuned by a $0.22 \mu \mathrm{~F}$ capacitor. Bias for the transistor is provided by a 200s resistor from the positive supply rail.

The operating frequency is determined by the $0.47{ }^{\prime \prime} \mathrm{F}$ base timing capacitor Cl , the variable resistor, the tuning capacitor and the load conditions. Since the load (the fluorescent tube) is a high resistance until alight, the circuit has a "soft" start, the oscillations starting at low frequency and amplitude and building rapidly over a few seconds until settling down at steady amplitude and high frequency once the tube 'strikes'.

## CONSTRUCTION

The tube and oscillator housing is made up from aluminium strip and sheet as shown in Fig. 2. This
construction method allows assembl with the tools normally available in a small workshop. The cover plate is the most complicated piece, but being fabricated from sin. sheet this makes the work quite casy. Culting is accomplished with a Stanley knife using a laminate cutting blade (Stanley No. 5194). The cut edges should be filed smooth. The original cover plate made by the author was bent up in a normal small metalwork vice. extra long 'jaws' being made up from $2 \times$ lin. hardwood.
The oscillator housing is bent up from 'rin. sheet as is the tube mounting bracket. The power transistor is mounted on the oscillator housing so that the base and emitter pins are inside the casing, directly above the circuit board. One bi-pin tube connector is also firmly nounted to a bracket bent up from this housing. Two side struts are bolted on to this oscillator housing. The smaller ' $U$ ' bracket supports them at the far end and also holds the



Fig. 3: Details of the spring-loaded tube connector.
other bi-pin tube connector. This connector is mounted on a lin. 4BA bolt and spring, Fig. 3, to facilitate easy fitting of the fluorescent tube by pulling back the connector and then pushing it over the tube pins.

## OSCILLATOR PCB

Fig. 4 shows full size layouts for both the component and the copper side of the circuit board. The board can be made by laying the drawing over a piece of copper clad board ready cut to size, and drilling through all the holes. It is essential that the drawing does not move during this operation. The layout can then be copied on to the board using a fine brush or mapping pen and cellulose paint. The board can then be etched off in ferric chloride (strong) solution. (A 500 ml bottle is adequate and may be obtained from most chemists to order.) After etching the board should be washed thoroughly in warm water. The paint can be removed with thinners or rubbed off with scouring powder. The components can them be mounted in place and soldered. Flying leads are required for the three transistor connections. Veroboard terminal pins are used for the four connections to the fluorescent tube.

## VARIABLE RESISTOR

The variable resistor VRI used here is primarily intended for use as a convergence control in Colour TV receivers. If difficulty is experienced in obtaining this control, it should be ordered from a TV dealer as a spare part (e.g. Decca CTV25 Part No. 535167). This control is mounted near the edge of the board so that adjustment may be made by turning the knob edge with a forefinger from the end of the lamp unit.

## THE TRANSFORMER

The transformer is wound on a Mullard DT2180 bobbin. Enamelled copper wire is used throughout and all windings are wound in the same direction.

The collector winding is put on first and consists of 12 turns of 28SWG wire, the start labelled (1) and the finish (2). The turns should be wound close together. The base winding is wound directly on top of the collector winding and consists of 18 turns of 28SWG wire, also closely wound. Label the start (3) and the finish (4). Next a single turn of insulating tape is put round the bobbin to isolate the low voltage windings from the tube supply winding.

Finally the high voltage winding is put on consisting of 310 turns of 32SWG wire with taps brought out after 5 and 305 turns. This winding is layer

## components list

| C1 | $0.47 \mu \mathrm{~F} 250 \mathrm{~V}$ polyester |
| :--- | :--- |
| C 2 | $0.22 \mu \mathrm{~F} 250 \mathrm{~V}$ polyester |
| R 1 | $200 \Omega 5 \mathrm{~W}$ wire-wound |
| VR17 | $5 \Omega$ pot. wire-wound (see text) |
| Tr1 | 2 N 3055 with insulating kit |
| LP1 | 15 W fluorescent tube |

Miscellaneous
Pot core ( $2 \times$ half cores) Mullard FX2242 and bobbin DT2180 (available complete from Hawnt Electronics Ltd., 112 Pritchett St., Birmingham, B6 4EN for $£ 1$ - 20 inc.).
Bi-pin tube connectors (2). 28 and 32SWG enamelled copper wire. PCB, $3 \times 1 \frac{1}{4} \mathrm{in}$. Length of twin 5A wire, as required, with two large crocodile clips.
Aluminium: 4 ft of $1 \times \frac{\mathrm{in}}{}$. strip (Part A), $6 \times 5 \mathrm{in}$. of $\frac{1}{16}$ in. sheet (Part B), $24 \times 3 \mathrm{in}$. of $\frac{1}{32}$ in. sheet (Part C).
wound, with a turn of insulation put right round the finished bobbin. The start, tap 1, tap 2 and finish should be labelled (5) (6) (7) and (8) res. pectively. The two ferrite cores can then be placed around the bobbin and the transformer loosely bolted on to the circuit board.

The leadouts can now be cut to length, scraped clean at the ends and soldered to their respective points on the circuit board. Once this has been


All holes drill No. 55 uniess otherwise stated.
Fig. 4: Full size layout of printed circuit board and component location on board.


A view of the oscillator assembly at one end of the lamp unit.
done, the fixing bolt may be removed and the top ferrite core taken off. A small piece of Sellotape should be stuck on to the centre pole-piece of the core. This provides a small gap which ensures that the core cannot be saturated by the primary magnetic flux. The upper core is then replaced and held into place with a further piece of Sellotape around the join (the cores are finally held together by the module mounting bolt).

An 'exploded' view of the transformer is shown in Fig. 5 which also shows the method of mounting the module.

## TESTING

The power transistor should be mounted on the module housing with a mica washer and two nylon bushes, usually supplied with the transistor. A smear of silicone grease should be applied to each side of the mica washer to ensure good thermal contact. The flying leads should be connected to the transistor, ensuring that the base and emitter leads are not reversed. The supply lead should also be connected to the copper side of the circuit board. Do not fit the tube or module into the framework yet.

Connect the power leads to a 12 V supply, ensuring correct polarity. The oscillator should 'whistle' loudly, since without a load the operating frequency is lower. If the circuit does not oscillate it is probable that the phasing between the collector and base windings is incorrect. Reversing either winding should ensure correct operation.

## ASSEMBLY

Once it is established that the oscillator is functioning correctly, the fluorescent tube connectors


Fig. 5 : An exploded diagram of the oscillator transformer and mounting.
may be wired up and the module bolted into the framework. Care must be taken not to overtighten the mounting bolt as the ferrite cores are very brittle and easily fractured. The nut can be sealed with a drop of paint or varnish. The tube can now be fitted into place and final adjustments made.

Reconnect the 12 V supply, ensuring correct polarity. The oscillator should start up at a medium frequency, increasing rapidly in pitch until the tube strikes and lights. The oscillator should then be inaudible. Adjust VR1 for maximum brightness. At one end of its travel the light will be dim and at the other extreme excessive base drive will cause squegging with consequent flickering of the lamp. Once the oscillator is correctly set operation should be satisfactory over the range 10 to 15 V . The current consumption should be between 1.3 and 1.5 A at 12 V input.

The cover plate should now be clipped on at the oscillator end and pressed home. Two self tapping screws hold the cover in place.

NOTE 1 Connecting the lamp to the battery with reverse polarity will not cause any damage since the transistor is reverse biased and cut-off, resulting in practically zero current flow.

NOTE 2 The metal framework has been left completely isolated. Slight radio interference may be caused in the immediate vicinity of the lamp unit. To reduce this interference to a negligible level (field localised to within 4 ft .) the frame should be connected to either the positive or the negative supply line. Connect a short lead from either to the soldering tag on the module mounting bolt.

## EXPERIMENTAL WORKSHOP-Part 3-

Trigger Circuits-continued from page 749
If the gap between the touch wires is bridged with the fingers a minute current flows into the base of emitter follower Trl. This produces a considerably larger current into Tr 2 and its collector falls to zero. The junction of R3 and R4 is momentarily pulled down by C 2 from about +4.5 V to $-4 \cdot 5 \mathrm{~V}$. This negative going signal is coupled to the base of $\operatorname{Tr} 3$ of the monostable through D1 and this switches off Tr 3 starting the monostable cycle.

The lamp goes on for the period set by Cl and R7. Capacitively coupling the touch-sensitive switch with C2 allows the user to keep his finger on the touch wires without interfering with the monostable action.

The values shown in the circuit only give a dwell time of a few seconds-for experimental purposesbut a reasonable period of time of $31_{2}$ minutes can be arrived at by increasing Cl to $3,000 \mu \mathrm{~F}$, and C 2 must be increased to about $50 \mu \mathrm{~F}$.

Next month we shall look at a development of the monostable; the astable multivibrator.
> coming soon fos Matr

## Multimeter Competition BESUM

In our June "Multimeter" Competition readers were invited to place eight features of the new Sinclair Radionics multimeter DM1 in order of appeal to the average P.W. reader.

Having considered all entries, the judges decided that the best received were a large number of identical attempts which had placed features in the following order:
1st-E; 2nd-D; 3rd-L; 4th-J; 5th-K ; 6th-B; 7th-A; 8th-C.
In accordance with the rules, these tying competitors then participated in a postal eliminating contest from which the eventual winners were judged to be Mr. J. Bertram, of Fenham, Newcastle-upon-Tyne; Mr. R. Harris, Knowle, Bristol; Mr. J. R. Mann, Knaresborough, and Mr. G. Rider, Hythe, Southampton.
These four readers each win a Sinclair digital multimeter and 12 months' free copies of Practical Wireless.
The tying competitors who entered the final postal eliminating contest, and were subsequently unsuccessful, each receive a consolation prize and 12 months' free copies of Practical Wireless.


The next series of special issues of P.W. will be in the Spring 1974.

In the coming months we shall be giving advance information on our new

# Successfus <br> Soldering 

WITHOU'I a doubt one of the most important tools for either professional engineer or amateur hobbyist is the soldering iron. Nearly every component has to be soldered, so whether constructional work or repairs are being carried out, the iron has to be called intc use. There are a considerable number of soldering instruments of all sorts and sizes available, so in this article we will take a look at some of them to see which are most suitable for particular applications, and their respective advantages and disadvantages.

## BASIC REQUIREMENTS

We will start off with what could be called the basic workshop instrument. This is an iron with the element operating at mains voltage and a wattage of between 25 and 40 watts. The size allows for most printed-circuit and general component soldering, but the bit may be rather large for some of the finer printed boards. For this reason, most irons have a variety of interchangeable bits so that a thinner one can be fitted for fine work.

In practice though, bits are not often changed according to the requirements of the job. For one thing they have a habit of getting seized-up and difficult to remove. They should really be loosened from time to time to facilitate changing, but in practice this precaution is usually neglected. Also, most workshop irons are kept on contimually in order 10 be instantly available, so 10 change the bit for a particular job would mean allowing the iron to cool down and waiting for it to warm up again after the change, plus of course a repeat performance for the re-fitting of the normal bit. Going to the other extreme, irons of this type and wattage have a limited heat output and so cannot tackle rarge jobs.
The difference between temperature and heatvolume must be noted here. All soldering irons attain a temperature which exceeds the melting point of solder ( $168^{\circ} \mathrm{C}$ for the high-quality $60 / 40$ grade) otherwise they would be useless for their purpose, but some deliver a greater quantity or volume of heat than others. This is determined largely by the wattage of the instrument. Hence, a soldered joint to a punched-out chassis tag may be impossible with some smaller irons because the chassis conducts the heat away faster than the element can produce it, and so the bit cools rapidly to below the required temperature. Any large area of metal will have the same effect.

Another factor is the size of the bit. The bit effectively stores heat and so acts as a reservoir. Heat flows out of the bit when the iron is used and more heat is supplied by the element. However, the outflow can be greater than the input for a short period until the stored heat is exhausted. Thus larger areas
can often be soldered than would be feasible with a particular element-wattage. if the iron is fitted with a large bit. When the iron has been thus used, it will take longer for the bit to return to correct operating temperature than would a smaller bit because it has what is termed, a slow heat recovery time.

## IDLING TEMPERATURE

A further consideration is the heat loss when the iron is switched on but is not in use, as is the case in most workshops for the greater wart of the time. While the iron may get hotter than needed because there is no heat conduction by application to a work area, it must not get so hot as to damage the element or cause premature deterioration of the bit. Hence the physical size of the iron barrel and bit must not be too small for the element size so that heat losses by convection and radiation are insulficient to keep the temperature to a safe dimit. It follows then, that physical size is closely related to element rating and should not be too small or too large.


Stiron 20 W and 60W irons, made in Sweden and featuring ironcoaled bils.

In order to keep the temperature of an iron down when it is not being used for long pericds, it is the practice in some workshops to operate a half-heat arrangement, whereby a lamp is switched in series with the iron. The temperature will gradually rise to not far short of the correct operating level, then when the iron is needed, the lamp is switched out and the temperature comes up within a few seconds. Another method is to stand the iron on a large cliunk of metal which keeps it from overheating by conduction. An old speaker magnet is sometimes used for the purpose, as this also attracts the iron and keeps it in place.

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## Sinclair

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*Four operators $(+,-, x, \div)$, with constant on all four.

* Constant acts as last entry in a calculation.
*Constant and algebraic logic combine to act as a limited memory, allowing complex calculations on a calculator costing less than $£ 30$.
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6. Printed circuit board.
7. Keyboard panel.
8. Electronic components pack (diodes, resistors, capacitors. transistor).
9. Battery clips and on/off switch.
10. Soft wallet.


This valuable book - free!
If you just use your Sinclair Cambridge for routine arithmetic- for shopping. conversions, percentages, accounting. tallying, and so on - then you'll get more than your money's worth.

But if you want to get even more out of it, you can go one step further and learn how to unlock the full potential of this piece of electronic technology.


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Because of the limnitations of the 25 to 40 watt iron, most workshops have at least one or two other types and sizes of iron available. For larger jobs, an iron with a rating of 60 to 100 watts is required. These irons are similar to their smaller counterparts in general construction and appearance except for the size and element rating. The bit may be square instead of the usual pencil-type. As only occasional use would be expected, the iron would not normally be left on for long periods, so there would be no overheating problems.


Work on integrated circuits requires a very small iron such as the Micro Soldering Pencil, shown here.

For the smaller and more intricate jobs, there are irons that are little bigger than pencils with element ratings of 10 to 15 watts. These are ideal for some of the tiny printed circuits that are now encountered and for the wiring of I.C.'s where the connections are close and damage could be caused by excessive heat. Heat output is obviously limited and many larger jobs could not be tackled. The element wire for these mains-operated low-wattage irons is necessarily very fine and so they are less reliable than the higher-rated ones. They should not be run continuously but only when a particular job calls for their use. Because of their small bit size, they are usually quite fast in warming up. This and their size also makes them suitable for outside service work.

## LOW VOLTAGE IRONS

Another type which has achieved a measure of popularity is the low-voltage iron. While these can be run from a low-voltage source such as a car battery, the more common method is to operate them from a mains transformer. The main feature is a very quick heating time, just a matter of seconds, and a rapid heat-recovery time. This means that the iron can be used for outside service work where delays waiting for a conventional iron to warm up are thus eliminated.

One type of low-voltage iron is constructed very similarly to the normal iron and fed from a separate transformer, which also serves as an irnn-rest. Other types have the transformer built-in, either over the top of a pistol-grip handle, or in one make, actually inside the handle. With these the element is also the bit, consisting of a loop of wire connected across the transformer secondary, Fig. 1.

In either of these low-voltage types, the bit can very quickly become overheated, even when being used on large areas, so a switch is incorporated in the iron so that the operator can keep switching it on and off and thereby maintain the tool at about the


Fig. 1: Circuit of a transformer iron with element/bit consisting of a wire loop.
right temperature. In one make that uses a separate transformer, a thumb ring is used as a switch on the handle; while most of the built-in types, being pistol-like in construction, use a trigger switch.

This need for constant switching can be a drawback, especially if the switches are stiff as some are, and need considerable finger pressure. The danger of overheating due to switching on for too long can also be a hazard for transistors and other semiconductor devices.

A yet further drawback of the built-in transformer type is their weight. This is of little consequence for occasional use, but when used continuously, as in the professional workshop, they can be very tiring. The wire-loop bits are not very durable and need frequent replacement; while owing to their flexibility they cannot be used to unpick joints as can the conven-


A plstol-grip soldering gun with integral transformer. The We/wyn KL3000.

The separate transformer type of low-voltage iron is therefore the more convenient, but for outside work the built-in type is probably the best. Neither though, really is as suitable as the mains-voltage type for workshop use.

## CONTROLLED TEMPERATURE

Of recent years we have seen several thermostatically controlled irons which overcome some of the snags inherent with the uncontrolled types, whether high or low voltage. One, rather ingeniously, uses the Curie effect of iron. Iron, when it is heated beyond a certain point loses its magnetic properties. A small
iron disc is fixed to the base of the soldering-iron bit and this has an attraction for a bar magnet which holds a switch in the 'on' position by means of a push-rod, Fig. 2. When the iron temperature reaches the Curie point of the disc, it loses its attraction, the magnet is released and the switch is opened. As the temperature drops to below the Curie point, attraction is re-established and the switch returns to the 'on' position.

Each bit has its own iron disc, which can be made with different Curie points, hence with its own temperature setting. This particular iron is a low voltage model and is operated from a separate transformer. It has a very rapid warm-up time and good heat recovery, but, because of being thermostatically controlled, does not overheat nor need switching attention by the operator. The barrel is a little short though, for some types of work.


Fig. 2: Mechanism of a heat-controlled iron using the Curie effect.

Another thermostat iron is called the 'Litestat.' This is a mains-operated instrument, hence it is not encumbered with a transformer, either built-in or attached by lead. It has a 70 watt rating, but is only little larger than the average 25 to 40 watt instrument, the thermostat preventing it overheating. As with other thermostat irons, when there is a heavy outflow of heat from the bit due to working on a large heat conductive area, any loss of temperature is compensated by the switch remaining on longer than usual, and the larger element quickly supplies the extra heat volume. Thus we have the best of both worlds, a moderate sized iron that will handle reasonably small jobs (quite small if the extra-small bit is used) and will also tackle the big ones. Although the occasional user will probably get on quite well with a normal uncontrolled iron, the advantages of the thermostat control really make this type of iron a 'must' for professional workshops.

These then are the basic types of soldering instrument and their respective features. Within each category there are many makes and models and engineers and hobbyists alike of ten have a particular favourite that handles well and seems to produce good work for them.

## SOLDERING BITS

Bits are available in several types. There are of course the various shapes and sizes that are produced for specific applications, most irons having a number of alternative bits obtainable as extras. There are though, differences in material. The most common is copper, which because of its high heat conduction is the best material (excluding precious metals) for the purpose. When clean it can be tinned quickly and easily, another great advantage. A disadvantage with copper bits is their deterioration with use. Prolonged periods of operation at high temperatures causes oxidization and flaking of the metal. In
addition, at the bit face where the solder is melted, cavities begin to form due to the chemical affinity of solder for copper, which absorbs it each time the bit is used.

Little can be done to stop the flaking other than running the iron at a lower temperature during standby periods, but the cavities can be almost eliminated by using the Savbit solder developed by Multicore. This contains minute traces of copper which satisfies the affinity of the solder without it taking more from the bit.

Other types of bit are made from alloys, or are nickel or chromium plated to achieve longer life. One method used by some manufacturers is to clad the copper bit with iron which is harder and more durable than copper, yet has the copper core for its thermal properties. A disadvantage with all these bits is that they cannot be filed without ruining them, thus once the plating or cladding has gone the bit must be discarded, whereas a copper bit can be filed flat at its face many times before filing and flaking reduces the size to inoperative proportions.

The superior thermal qualities and ease of tinning make the copper bit still the favourite, especially since its life can be prolonged with special solders.

## USING THE IRON

Now just a point or two on using the iron. It is surprising the number of people who are technically well qualified, professional engineers included, who cannot seem to produce a good soldered joint. It is very important to do so, as all sorts of faults can arise from poor soldering. It is noteworthy that all candidates for the RTEB servicing exams had to undergo soldering tests and failure led to automatic disqualification for the whole of the practical and theoretical examinations.


Litesold Conqueror iron and stand with bit-cleaning sponge and range of interchangeable bits.

There is nothing really difficult in making a good joint, just observing a few straightforward rules. The first one is to make sure that both surfaces are clean. In the case of wires, this can be done by pulling the wire a couple of times through the blades of a pair of side-cutters, as though one were stripping insulation. Terminals and tags can be scraped with a screwdriver blade. In most cases wires and terminals will be already tinned, but do not rely too much on it. Next both surfaces should be tinned. This is done by applying the iron to the surface for a few seconds, and then introducing the solder to bit and


Fig. 3: The iron should heat the whole joint-not just the solder.
surface so that it runs easily over it, Fig. 3. If the solder is thick and slow to run, the bit temperature is too low, either because the iron has not been switched on long enough, or the iron is too small for the work. The solder may not run over the surface readily at first because insufficient heat has been transferred from the bit, and it is just not hot enough to melt the solder. This could be due to poor contact between bit and surface, but a little solder introduced at the junction of the two, will give a good thermal conduction, and the surface should then quickly attain sufficient temperature to itself melt solder when applied.
When both surfaces have been thus tinned, they are brought together in mechanical contact, and the iron applied again to both. More solder is then introduced so that it runs freely over both surfaces.
then the iron is withdrawn. Do not move the work until the solder has solidified otherwise a weak joint will result; this will take only a second or two. Where possible the joint should be mechanically sound before soldering. No external flux should be used as these are often corrosive and will give trouble in the future. Sufficient of the correct type of flux is contained in the cores of solders intended for electronic wiring, to do the job.


Fig. 4: (a) A 'dry' joint, showing the blob of solder due to insufficient heat or dirly surfaces.
(b) A good joint, showing smooth flow of solder over joined surfaces.

Do not use too much solder as this is not only unnecessary but could form a short to adjacent terminals. In appearance, the joint should be bright and smooth. A lumpy or pitted appearance shows the solder was not hot enough. It should also appear as a 'mound' rather than a blob. The illustration Fig. 4 shows what is meant by this. If the solder surface comes down and curls under as shown, it has not taken to the surface and we have a 'dry' joint. By observation of these points and a little practice, perfect joints can be made every time.

LETTERS-continued from page 742

## Value for money

I greatly appreciated the article on 'Going Back' as it is full of nostalgia. I have taken P.W. off and on since the early beginnings, but only since 1967 have I bought it every month and I only started then because a free record of audio faults was given away, but on reading the articles on transistorised equipment, and particularly details of a transistor SW receiver by F. G. Rayer. 1 was astonished at the transformation in building techniques (being brought up on $3_{B}$ " thick breadboards and ${ }^{1} 16$ " dia. connecting wire!) and plunged up to the neck in transistor circuits and have been building them from $P . W$. projects ever since.

Though the price of P.W. has greatly increased, the contents have kept in step and I think it is still good value for money. It is improving all the time, as reference back to only a few years ago will show, and even in the last few months there have
been detailed improvements, such as better layout and the contents page being put on the first page. Long may you continue!

Incidentally, radio parts seem to be one of the few things which have not greatly increased in price, and some, like transistors and i.c.s, have actually gone down.-R. A. Read (Salisbury).

## A Fly in the Ointment?

Do any readers know how to build an electronic fly-catcher? We are driven crazy with flies in the summer and we are sure that it is the sheep that bring them in.

I was born in the UK and lived many years in Africa but the flies were never as bad as here. I have taken P.W. for over 20 years now but have not seen any details of fly catchers. Also, we are a bit lost out here for getting components especially as we can only get a $£ 2$ British P.O. here on demand at the Post Office.-J. S. Skeels (One Tree Point, Rukaka, Northland, New Zealand).

## Short Wave Converter

I have built the Radio Nederland converter, Practical Wireless, September 1973, and am very pleased with the results, however, I should like to point out an error in publication which would result in disappointment to those to quote your preamble - "with little experience in electronics."

Reference page 409 figure 1 circuit diagram oscillator $\operatorname{Tr} 2$ AF 124 and page 410 drawing AM0022. Note the emitter and base connections are shown reversed so there could be no conduction in the collector circuit due to reverse polarity at the base.

As a note of interest $I$ used Wearite $\mathbf{P}$ coils either PA4 or P'HF4 which very nearly approximate the coil data given for L 1 and L2, a similar coil was slightly modified to make up L3. A PHF6 coil tuned by a 200 pF silver mica in parallel with a 250 pF trimmer was used for L4. The unit is used with a BUSH TR130 receiver tuned to the extreme h.f. end of the m.w. band.-A. J. Birkinshaw (Telford, TF2 6RA).

# GOING <br> QUADRAPHONIC <br> PART3 D.BOLLEN <br> OS reardilins Sir reamrining $\square$ Discrete CD-4 reemriling $\square$ Suhrouna souno 

THE article last month gave circuit descriptions single and multi-system matrix decoders based on two circuit modules, Units A and B. There now follows constructional details of these two units, and of the additional units and components needed to build a multi-system decoder with infinitely variable front and back separation.
Readers are reminded that they will require, in addition to the decoder, a stereo outfit plus a pair of back amplifiers and speakers for quadraphonic reproduction from discs and tapes.

## Unit A construction

Unit A is assembled on a piece of $0 \cdot$ lin. pitch Veroboard 0.9 in . wide by 4 in . long, see Fig. 16. Begin by making breaks in the copper strips, where shown, with a spot face cutter, and then insert and solder the terminal pins.

During assembly, it is important to ensure that the transistors are not overheated as this could have a detrimental effect on noise performance. A clip made of aluminium sheet should serve to conduct away heat when placed around the transistor can during soldering. Constructors who are not accus-

tomed to $0 \cdot 1 \mathrm{in}$. Veroboard should also make sure that solder blobs do not bridge between the copper strips. It is a good idea to run a sharp knife blade along the gaps between strips to remove excess flux and any particles of solder. When inserting capacitors in the unit A circuit board, check that the polarity is as shown in Fig. 16.


Fig. 16: Component layout of unit A circuit board. Note breaks in copper strips.


Fig. 17. Component layoul of unit B circuit board. Note breaks in copper strips

(a)

20
AM 0001 All dimensions in cm Drill all holes 1 cm diameter


Fig. 18(a): Drilling details of front of chassis tray. Fig. $18(b)$ : Front panel layout


Fig. 19: Multi-system decoder layout showing earth wiring.


Fig. 20: Dimensions and fixing details of the chassis cover.


Fig. 21 : A method of securing the circull boards.

## Unit B construction

A piece of $0 \cdot 1 \mathrm{in}$. pitch Veroboard $1 \cdot 8 \mathrm{in}$. wide by 3in. long is employed for unit $B$, and the layout is shown in Fig. 17. Left and right hand channels are identical and are arranged one above the other on the circuit board.

Make breaks in the copper strips according to the diagram of Fig. 17 and insert and solder all terminal pins. Commence with the ICs, leaving pins $3,5,8,11$, and 14 unsoldered, and then position and solder the remaining components. Use a heat clip on $\operatorname{Tr} 7$ and $\operatorname{Tr} 8$ and ensure that the polarity of the electrolytic capacitors is correct.

## Checking units A and B

As a preliminary check, wire the earth and +20 V terminal pins of unit A circuit board to an 18 V battery (two PP9s in series) and with a testmeter measure the voltages between the earth terminal and the transistor cans. Tr 1 and $\operatorname{Tr} 2$ should show a voltage of about 14 V , and $\operatorname{Tr} 3-\mathrm{Tr} 6$ a voltage of 9 V . If there is a serious discrepancy, look for a short circuit between the copper strips on the underside of the circuit board, or an error in component positioning.

To check unit B , connect the 18 V battery to earth and +20 V terminals and measure the voltage at ICl and IC2 pins 10 and 12, which should be at 9 V relative to the earth terminal pins. The can voltage of $\operatorname{Tr} 7$ and $\operatorname{Tr} 8$ will be about 14 V if there are no constructional faults.

Small piece of 16 swg aluminium to engage in slot at the back of the front pots. and slot in the spindle.


Fig. 22: VR9 assembly utilising two dual-gang polentiometers.

If the user intends to experiment with a singlesystem decoder, units A and B can be employed with an 18 V battery, or the power supply of Fig. 15, with $22 \mathrm{k} \Omega$ balance controls (VR5-VR8 Fig. 14) wired to the LF, RF, LB, and RB outputs of unit A. It is advisable to connect a $1000 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic capacitor across the supply rails when operating units $A$ and B from a battery.
Where an oscilloscope with X-Y facilities is available, unit B can be tested for $90^{\circ}$ phase shifting by injecting a signal of 2 kHz into the left input, with the $X$ input of the scope linked to the $0^{\circ} \mathrm{L}$ output, and the $Y$ scope input connected to each of the $90^{\circ} \mathrm{L}$ outputs in turn. The resulting display should be a near perfect circular trace. Repeat the test for the right hand channel.


Fig. 23 : Component layoul of resistor network board.

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## Multi-system decoder construction

Fig. 19 shows the layout of a multi-system decoder based on the circuit of Fig. 14. Additional circuit boards serve to accommodate the resistor network, input capacitors and resistors, and power supply components; these will be described later.
A start can be made by making up the chassis tray from 16s.w.g. aluminium sheet, to the measurements shown in Fig. 19. Allow 7 cm of space for the power supply, and mark out and drill the rear of the chassis tray to take sockets SK1-SK10. Next, mark out and drill the holes to mount transformer T1, the power supply screen, and mains lead grommet.

Drilling details for the front of the chassis tray are given in Fig. 18a, and Fig. 18b shows a front panel made of 20.5 cm by 7.5 cm brushed aluminium or white Formica, which is drilled to match the holes in the chassis tray. The dimensions and fixing details of the chassis cover are shown in Fig. 20.

Glue a sheet of Formica or s.r.b.p. inside the base of the chassis tray to insulate the circuit boards from the chassis; this should measure 19 cm by 14.5 cm . A method of securing the circuit boards is shown in Fig. 21.
Make up switch S1 from three 4-pole 3-way wafers, with a three spacer gap between wafers. Mount the assembled switch on the front of the chassis tray, along with controls VR1-VR8.

In the absence of a four-gang component for VR9, this can be made up from two dual-gang potentiometers, as shown in Fig. 22. A small piece of sheet aluminium engages with the spindle slot at the rear of the front pair of pots, and with a slot in the


Copper strip breaks occur at the following points:- $\mathrm{C} / 6.5 / 6,1 / 5,1 / 8$, L/5,L/9,0/5.0/4,R/5,R/9.
spindle of the back pots. To align VR9, set the front pots to mid-track and measure the resistance between a slider and the earthed end of its track. Rotate the body of the rear pots to give a similar resistance reading on a rear pot slider and its track end, and then tighten the mounting nuts. VR9 can now be mounted on the chassis.

## Resistor network board

The resistor network components are assembled on a piece of 0.1 in . pitch Veroboard 1.9 in . wide by $3 \cdot$ lin. long, and this is designed to plug into a $19-$ way edge connector (SK11) to facilitate easy modification of matrix parameters. The layout of the resistor network board is shown in Fig. 23.

A suitable edge connector, such as the RS Components $0 \cdot 1$ in. 25 -way, may be cut down to 19 ways with a small saw. When the resistor network board is completed it can be inserted in SK11, and the latter glued to the insulating board on the chassis tray.

## Input circuit board

Fig. 24 shows the input circuit board with components mounted on 0.1 lin . Veroboard, which measures 2 in . wide by $1 \cdot 2 \mathrm{in}$. long.

In Fig. 14 (last month) the lower unit board should have been designated unit B . We regret, that due to pressure on space, final constructional details, wiring and setting up, have had to be held over until next month.

## TO BE CONTINUED



# No. 55 <br> TRIPLEX SIGNALLING UNIT 

DAVID ANDREWS

## A series of simple transistor projects, using not more than twenty components.

THIS project can be used as quite a useful gadget for signalling between the house and a shed or to illuminate signs outside an office door. Signals are produced by two lamps either. or both, of which can be switched on and off. This does not, in itself, sound very clever but the circuit to be described enables one to do this with a single pair of wires. Thus, over two wires one can display three separate codes on the two lamps.

## Circuit

The trick is to make use of positive going half cycles of the mains supply to switch on one lamp. In Fig. 1 D6 is forward biased for positive going cycles and LP2 will light but when SW2 is switched to the centre position the polarity of these half cycles is reversed and D5 becomes forward biased, turning on LP1 (D6 becomes reverse biased and 1,P2 goes out).
The third code, having both lamps on at the same time, is obtained by turning SW2 into the third position which applies a.c. to the signal wire pair direct from the transformer. LP1 and LP2 will now each light up, LP2 on positive and LP1 on negative half cycles.

## Variations

There are many variations to this circuit, and relays could be used instead of the lamps. Provided limiting resistors were inserted into the lines and the voltage reduced to below the reverse breakdown level, light emitting diodes could be. used instead of the lamps, diodes D5 and D6 being omitted. For those who do not wish to bother with a.c. and a transformer one can still transmit two codes down the pair of wires by dispensing with the control unit. All that is needed in its place is a suitable battery and a reversing switch on the control end of the signal wires. One polarity will turn on one of the lamps, reverse the polarity of the supply and the other lamp will light. Apart from the diodes most of the components can be
salvaged from old equipment. Any 6.3 V transformer will do for Tl and probably the best source is an old valved radio.

Fig. 2 shows a suggested layout for the unit, on a metal or insulating material panel, which can be the lid of a box.


A Fig. 1. Circuits of Control Unil and Remote Signals
$\nabla$ fig. 2. Author's suggested layoul for the two units.

(CKG537)

## components list

| D1-6 | Diodes 1N4001 |
| :--- | :--- |
| LP1-2 | 6V Lamps |
| SW1 | 2 pole mains switch |
| SW2 | 2 pole 3 way wafer switch |
| T1 | Mains transformer, 240/6.3V |
|  | Mounting box, tag strip, etc. |





SHORT WAVE DX
by MALCOLM CONNAH

AS many of you will know, propagation conditions vary according to the time of day, the time of year and the position in the 11-year sunspot cycle; as well as other minor factors. This means that, at any particular time, there is an optimum band for reception from any part of the world.

Forecasting these optimum bands is a relatively simple matter once one has collected all the necessary information. The following forecast is for reception in Western Europe and is listed by transmitter site.
North America During the late afternoon the most suitable band will be 25 metres, by 1900 GMT this will have changed to 19 metres but will return to 25 metres by 2300 . During the early hours of the morning the most useful frequency will drop still further reaching 31 metres by 0300 .

Central \& South America The optimum frequency during the late afternoon will be 16 metres and this will drop gradually during the evening to be 19 metres at 1900; 25 metres at 2300 and $49 \& 60$ metres at 0300 .

Middle East The late afternoon finds 19 metres as the best band dropping to 31 metres at 1900 and 41 metres at 2300 .

Far East \& Australasia Reception for this area will be much the same as the Middle East except that the best band will not drop below 31 metres.

Africa Late afternoon reception will be best on 16 metres dropping to 25 metres at 2000 and 31 metres at 2300 .

## DX News

COSTA RICA: Radio Capital de Costa Rica has been heard on 4832 kHz at 0130 GMT. Reception is poor due to the low power of 1 kW .

ECUADOR: Radio Nacional del Ecuador has been noted with a programme of news and Latin-American music on 6170 kHz at 0500 GMT.

EL SALVADOR: La Voz del Comercio, Colonial Sta. Lucia, Santa Ana, is asking for reception reports on 9545 kHz . The best time for reception being 1600 GMT.

MEXICO: XERMX has been heard in Spanish on 15195 kHz at 0330 GMT , this is a change from the usual frequency of 15125 kHz .
TUNISIA: Radio Tunis has been noted on 15226 kHz at 2345 GMT and at 0910 GMT on 11970 kHz . (Some of the above items by courtesy of Sweden calling DXers.)

## Readers' Logs

John D. Porter of Bakewell (No jokes about Bakewell tarts-please) in Derbyshire has nine transistors and a few other components built into his superhet receiver. This, in combination with a 45 metre longwire and some attention to the higher frequency bands, produced the following results:
11710 R. Nacional d'Espana at 0005.
151110 R. Grenada, Windward Is., English at 2100.
15150 R. Pyongyang, N. Korea noted at 2030.
15375 HCJB, Quito, Ecuador at 2210.
15415 R. Kuwait in English at 1850.
15450 R. Nacional de Brasilia in English at 2355.
17820 R. Canada Int., in Polish at 1540.
17885 HCJB, Quito, Ecuador noted at 2250.
Andrew Brown of Maidenhead in Berkshire is fourteen years of age so both his National HRO and R107 receivers are older than he is. The connection of a 10 metre long-wire antenna enabled the following stations to penetrate Andrew's shack:
7275 RAI, Italy in English at 1936.
9005 Tehran, Iran in English at 2000.
9560 R. Jordan, Amman in English at 1600.
9655 R. Damascus, Syria in English at 1930.
9745 R. Baghdad, Iraq in English at 1930.
11765 Radio Australia noted at 0710.
15165 R. Denmark in Danish at 0945.
15325 R. Pakistan, Karachi in English at 1530.
15520 R. Bangladesh in English at-1715.
17825 NHK, Japan in English at 0800.
21520 RSA, South Africa noted at 0755.
21655 R. Norway, Oslo in English at 2000.
David Thornley of Dukinfield, Cheshire has a Trio 9R59DS receiver and a Joystick antenna with ATU; which enabled him to hear:
7125 R. Peking in English at 0120.
9020 R. Iran in English at 2000.
9610 R. Kiev in English at 0030.
11672 R. Pakistan with news in English at 2000.
11880 Voice of Turkey in English at 2000.
15425 Israel with news in English at 1200.
17735 R. Havana, Cuba in English 2035.
21605 RSA, South Africa with quiz show at 1305.


## MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

ROY PATRICK (Derby) has been busy with his National 1400 receiver on the medium waves. He reports good reception of Radio London on 1457 kHz and the two IBA London transmitters on 557 kHz and 719 kHz . While on a visit to Farnborough (Hants) Roy logged Radio Brighton 1484 kHz , Radio London and Radio Solent on 998 kHz .

Richard Livesey (Guildford) has used his Audiotronic multiband receiver with internal ferrite aerial to hear Radio Portugal 755 kHz at 2310 hrs ; Radio Prague 1286 kHz ; Trans World Radio Monte Carlo 1466 kHz at 2230 hrs ; Radio Moscow 1493 kHz at 2230 hrs ; Radio Warsaw 1502 kHz at 2230 hrs . All of these broadcast in English.

Ian Gordon (Birmingham) has a Codar CR70A receiver, a 25 metre longwire antenna and an aerial tuning unit (ATU). He reports hearing Radio Tirana 1394 kHz with sign-on at 2000 hrs ; Radio Blackburn 854 kHz ; R. Leeds 1106 kHz ; R. Stoke 1502 kHz ; R. Nottingham $1520 \mathrm{kHz} ;$ R. Bristol 1546 kHz plus the American Forces Network in Germany on 611 kHz (Grafenwohr / Kaiserslautern / Nürnberg), $872 k H z$ (Frankfurt), 935 kHz (Berlin), 1106 kHz (Munich),

1142 kHz (Bremerhaven/Stuttgart). The AFN can also be heard on 1034 kHz (Karlsruhe), 1304 kHz (Heidelberg), 1394 kHz (Augsburg).
M. Laugharne (Didcot, Berks) reports hearing R. Solent $998 \mathrm{kHz}, \mathrm{R}$. London $1457 \mathrm{kHz}, \mathrm{R}$. Oxford 1484 kHz and R. Bristol 1546 kHz on his Philips portable receiver. T. D. Wilson (Hemel Hempstead) used a Grundig Mariner to hear R. Sweden 1178 kHz and R. Portugal 755 kHz , both in English at 2300 hrs . He mentions receiving WINS, New York City on 1010 kHz last February. Gary Celand (Southall, Middlesex) would like to listen to North American stations on the medium waves and when reception is possible. A path of darkness between transmitter and receiver is required for medium wave propagation. Listen for North Americans some five to six hours after sunset in the UK. From November to February they can be logged as early as 2330 hrs when conditions are favourable. Those most frequently heard are CJON St. John's in Newfoundland on 930 kHz ; CHER Sydney, Nova Scotia on 950 kHz ; WINS New York City on 1010 kHz ; CBA Moncton, New Brunswick on 1070 kHz and WNEW 1130 kHz New York City.

The BBC have announced the location of the first four low power medium wave stations which will improve the Radio 4 service to the south-west of England. Torquay 854 kHz ( 351 m ), Barnstaple 683 kHz ( 439 m ), Plymouth 1457 kHz ( 206 m ) should come into service before the end of 1973 and Redruth 755 kHz (397m) by the Spring of 1974. The Barnstaple service will replace the present one on 692 kHz ( 434 m ) while the others will be additional to the existing Radio 4 medium wave service.

## VHF/FM DXING

## by SIMON DAVID

T. J. Clamp of Cranbrook in Kent lists among other stations in the U.K., Markelo 2 on $98 \cdot 4 \mathrm{MHz}$ and Roermond 1 on $88 \cdot 3 \mathrm{MHz}$, both from Holland, as well as Aalter, Belgium on 98.5 MHz . He uses a Grundig Melody Boy 1,000 receiver and the in-built 86 cm telescopic aerial. He also says "How about a list of BBC local radio station frequencies on f.m?" Other readers have also asked for this information, so I have included it in this month's column. The BBC Engineering Information Department issues complete lists with frequencies, powers, and polarization on Information Sheets 1034(24) and 1919(21) for any one with a technical interest. In the not too distant future I shall be giving details of some of the European frequency allocations. Details on Radio Telefis Eireann were given last month.

Igor Hájek has given me some very interesting gen on East European bands. With reference to my comments in the September issue, he points out that East European countries (including U.S.S.R.) use the $65-73 \mathrm{MHz}$ band, possibly with a view to making it difficult for their local population to have access to Western broadcasts. In spite of this, Czechoslovakia have tuners that cover West Europe (CCIR) and East Europe (OIRT). How long before we have this facility as commonplace in the U.K.? (see Leader article-Ed.).

This lower frequency band is in the 4 metre area of the dial and does lend itself very well to DX reception, as my colleague David Gibson will testify.

Future plans for stereo on v.h.f./f.m. include Wenvoe and Kirk O'Shotts next year, Pontop Pike and Sandale (near Carlisle) in 1975. It is surprising that Norfolk and Huntingdon areas are not yet planned, especially in view of the flat terrain.

The following is a list of BBC Local Radio stations. Birmingham, Blackburn, Manchester and Teesside will have transmission powers increased. Slant polarisation is employed at Blackburn, Derby, Leeds, Leicester, Manchester, Nottingham, and Sheffield (main). All others use horizontal polarisation. Medium wave shown in brackets.

Birmingham $95 \cdot 6 \mathrm{MHz}$ (206m)
Blackburn $96 \cdot 4 \mathrm{MHz}$ ( 351 m )
Brighton $95 \cdot 3 \mathrm{MHz}$ (202m)
Bristol $95 \cdot 5 \mathrm{MHz}$ (194m)
Carlisle $95 \cdot 6 \mathrm{MHz}$ ( $397 \mathrm{~m}, 206 \mathrm{~m}$ )
Derby $96 \cdot 5,94 \cdot 2 \mathrm{MHz}$ (269m)
Humberside $96 \cdot 9 \mathrm{MHz}$ (202m)
Leeds $92 \cdot 4 \mathrm{MHz}$ ( 271 m )
Leicester $95 \cdot 1 \mathrm{MHz}$ ( 188 m )
London $94 \cdot 9 \mathrm{MHz}$ ( 206 m )
Manchester $95 \cdot 1 \mathrm{MHz}$ (206m)
Medway $96 \cdot 7 \mathrm{MHz}$ ( 290 m )
Merseyside $95 \cdot 8 \mathrm{MHz}$ (202m)
Newcastle $95 \cdot 4 \mathrm{MHz}$ ( 206 m )
Nottingham $95 \cdot 4 \mathrm{MHz}$ ( 197 m )
Oxford $95 \cdot 2 \mathrm{MHz}$ (202m)
Sheffield $97 \cdot 4,88 \cdot 6 \mathrm{MHz}$ (290m)
Solent $96 \cdot 1 \mathrm{MHz}(301,188 \mathrm{~m}$ )
Stoke-on-Trent $96 \cdot 1 \mathrm{MHz}$ ( 200 m )
Teesside $96 \cdot 6 \mathrm{MHz}$ ( 194 m )

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## SHORT WAVES

## by DAVID GIBSON, G3JDG

I'T'S an interesting period for Amateur Radio. The sunspot count continues to creep lower and the longer, darker (colder) nights are making $14 / 21 \mathrm{MHz}$ less favourite for DX working. For the s.w.l. who reckons he's up to tackling something a little more difficult, then I suggest a serious DX assault on 7 MHz . This will assume more and more the role of the major DX band. Further down, on $3 \cdot 5 \mathrm{MHz}$, more DX is becoming apparent so it could well be an l.f. DX winter.

On $3 \cdot 5 \mathrm{MHz}$ this past month, goodies like OA4OS, ZS6TE and 9J2DT have been heard while up on 7 MHz the air has been buzzing with c.w. offerings from calls like CM2JA, CR6AI, FG7XC, VK3MR, ZS5AN and 8P6DR.

Hair-raising happenings on top band. Several G stations have worked VP8KF in the Falklands. A few years back, this station would never have been thought about on 1.8 MHz . Even now, a VP8 would cause excited s.w.l. squeaks if heard on 14 MHz . Topband sleuths are invited to lay in wait for r.f. travellers like ZLIMQ and a few JA stations who are known to be loitering. One station in Japan (JA7AO) has worked all continents (WAC) except Europe so it would be a safe bet to reckon his signal is there somewhere-who'll be first to report it?

Up on ten metres things seem to be fairly static Long periods when one hears a noise like frying eggs (cheaper variety) and then, suddenly, an S9 plus five million dB's (well, it sounds like it) comes out of nowhere. South African stations are logged with out too much effort and the South American continents comes romping in at times. Don't forget to listen first for the beacon stations since these will give a useful indication of what the bands are doing.

Before we take a peep at the logs sent in this month, let's open up the JDG little black book for contests in November. According to my crystal ball, the following are on: November $10-11$, OK DX contest (c.w./phone); 10-11, topband contest; 11, four metre contest; 24-25, CQ WW (c.w./phone) contest.

First event in December is on the 9th and is a two metre contest for fixed stations-you've just got time to tie that 40 -element Yagi beam to the chimney pot and switch on!

## Readers' Logs

Dave Gregory (Plymouth) confesses, "I have been a Broadcast Bands maniac (is there any other kind?) for some months now". Brethren will be pleased to know that my Brother Gregory has seen the light and cleansed his sins by purchasing a 9R-59DS, RA-1 and CR100. With a homebrew a.t.u, and "DX processing unit" Dave repents on 14 MHz with the following log; A51PN, A6XP, AR1RSP, EA7PS (an XYL-O'lay); WA5FW, ZB2BL, 3A2EE, 4Z4MQ, $5 Z 4 \mathrm{~GB}, 5 \mathrm{Z} 4 \mathrm{GK}$
A. McNeill (Newbury), comments on the many eastern europeans loose on 14 MHz . He also praises the DX'ers processing unit which was featured in P.W. and queries the callsign NI3A who keeps popping up. Are there NI takers to answer this?

Derek Harding (Godstone) says he's 23 years old and has been an s.w.l. for four days (What a waste of 22 years, 361 days). Derek asks how he can filter out the various loud whistles which beset him? Anyone got any thoughits other than the on/off switch?

John Turner sends in a 21 MHz selection from a log made during his school holidays (think of all the conkers you missed). Gear in his bedroom at Doncaster includes a Pye Cambridge receiver with an 85 ft end fed supplying the microvolts to the tune of; A2CCY, CE3OE, CN8CG, CPlHL, CR6AD, CT1BY, CX2CS, CX7BM, DUlFE, EA8CS, EA8HH/M, ELIG, ET3USA, HK3CDW, HS4AJL, JA4PE, JA6PIC, JA7KHZ, JH1DEV, KP4AD, KZ5EK, LU5MAO, M1C, PZ1DR, TI2IO, TR8VT, TU2D0, VK4PU, VP2MF, VP8ML. VP9CB, VQ9BP, YN1AZ, YV5EED, ZD3D, ZD8MH, ZS4JW, 4Z4LM, 7X0WW, 8R1J, 9GlAF, 9H1DP 9M2DQ, 9U5CR, 9X5VA.
Tam Large (Hassocks) lives on a farm in Sussex. His favourite animal is a 9R-59DE. Feed it a staple diet of mains electricity and put it on a 200 ft . end fed lead and it yields the following twenty metre tweets; CR6LX, HP1TG, K2LZQ/OH0, M1C, PZ1DR, 4WlAF. Similar treatment brought forth the follow. ing from 21 MHz ; TG9CQ, XElGR, ZD3D, 9M2CX.

Paul Davies (Blackpool) is learning to read c.w. (good lad). Meanwhile, he listens with baited breath on 14 MHz to the following juicy jingle; CR6GA, EL8J, EP2SP, ET3GA, HR2WTA, IB0PV, JA4JUV/ MM, JY6HCT, KA6HQ, 9H1CQ, 9H4B, 9K2AL, 9M2DW, 9X5NA, all on s.s.b. Gear used is S' Heath HR-10B, Joystick antenna and an a.t.u.
S. Eldridge (Crawley), has a CR70A, 132 ft . end-fed looped round the bedroom and a ven to listen on 15 metres. Here's the gen on his yen; A6XB, CE3PY, CR6AG, CR6HZ, CT2AB, HI8LC, JA8ISK, JElMUM, JFIIUA, JH3EXI, JR1TAM, KA2PJ, LU6FEP, PT2JB, TI2STI, TR8VE, VQ9M, VU2DK, ZP5VO, ZS1J, ZS4JW, 5N2ESH, 5U7BA, 9X5VA

## BROADCAST BANDS

Short Wave Reports by $15 \%$ of the month to Malcolm Connah, 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.
Medium Waves Logs to Charles Molloy, 132 Segars Lane, Southport, PR8 3JG.
VHF/FM Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

## AMATEUR BANDS

Short Wave/VHF
Logs in alphabetical order please by 15th of the month to David Gibson, G3JDG, 12 Cross Way, Harpenden, Hertfordshire.

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| 213 | 1.0 | 0.5 | 1 | 4 | $6.1 \times$ | $5.8 \times$ | 4.8 | 0.12 V | at | 0.5 A .2 |

$\qquad$ 22

 $\begin{array}{r}8 \\ \hline 22 \\ 22 \\ \hline 22\end{array}$

$\begin{array}{lll}6.1 \times 5.8 \times & 4.80 .12 \mathrm{~V} \text { at } 0 \cdot 5 \mathrm{SA} \cdot 2 \\ 7.0 \times 64 \times & 6.1 & 0.12 \mathrm{~V} \text { at } 1 \mathrm{AA} .2\end{array}$
_ $\begin{array}{lllll}7.0 \times & 6.4 \times & 6.1 & 0.12 V \text { at } 1 A-2 & 1.60 \\ 8.3 \times & 7.7 \times & 7.0 & 0.12 V \text { at } 2 A-2 & 2.2 \\ 8.9 \times 8.0 \times & 7.7 & 0.12 V \text { at } 3 A-2 & 2.70 \\ 9.9 \times 8.9 \times & 8.6 & 0.12 V \text { at } 4 A .2 & 3.00\end{array}$ $\begin{array}{llll}8.9 \times 8.0 \times 7.7 & 0.12 \mathrm{~V} \text { at } 3 \mathrm{~A} .2 & 2.70 \\ 9.9 \times 8.9 \times 8.60 .12 \mathrm{~V} \text { at } 4 \mathrm{~A}-2 & 3.00 \\ 9.9 \times 9.6 \times 8.60 .12 \mathrm{Vat} 5 \mathrm{-} & 3.55 \\ 12.1 \times 9.9 \times 10.2 & 0.12 \mathrm{~V} \text { at } 8 \mathrm{~A} .2 & 5.48\end{array}$ $\begin{array}{llll}2.1 \times & 9.9 \times 10.2 & 0.12 \mathrm{~V} \text { at } 8 \mathrm{~A} .2 & 5.48 \\ 1.0 \times 9.6 \times 11.8 & 0.12 \mathrm{~V} \text { at } 10 \mathrm{~A} .2 & 6.98\end{array}$ $\begin{array}{llll}4.0 \times 12.1 \times 11.8 & 0.12 \mathrm{~V} \text { at } 15 \mathrm{~A}-2 & 12.90 \\ 17.2 \times 15.3 \times 14.0 & 0.12 \mathrm{~V} \text { at } 30 \mathrm{~A}-2 & 23.72\end{array}$ 30 VOLT RANGE 30 VOLT RANG



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MYLAR FILM CAPACITORS IOOV CERAMIC DISC CAPACITORS $0.001 \mu \mathrm{~F}, 0.002 \mu \mathrm{~F}, 0.005 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}, 0.02 \mu \mathrm{~F} . \quad 100 \mathrm{pF}$ to $10.000 \mathrm{pF}, 2 \mathrm{p}$ each. 2 1 P, $0.04 \mu \mathrm{~F}, 0.05 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 3 \frac{1}{2} \mathrm{p}$.

ELECTROLYTIC CAPACITORS
$(\mu F / V) 1 / 63,1 \cdot 5 / 63,2 \cdot 2 / 63,3 \cdot 3 / 63,4 \cdot 7 / 63,6 \cdot 8 / 40,6 \cdot 8 / 63,10 / 25,10 / 63.15 / 16,15 / 40$,
 $\begin{array}{lll}68 / 16,100 / 4.100 / 10,100 / 25,150 / 6 \cdot 3,150 / 16,220 / 4, & 220 / 6 \cdot 3,220 / 16,330 / 4,6 p .47 / 63, \\ 100 / 40,150 / 25,220 / 25,330 / 10,470 / 6.3,7 p, 68 / 63,150 / 40,220 / 40,330 / 16 / 1000 / 4,10 p\end{array}$ $100 / 40,150 / 25,220 / 25,330 / 10,470 / 6 \cdot 3,7 \mathrm{p} .68 / 63,150 / 40.220 / 40,330 / 16,1000 / 4,10 \mathrm{p}$,
$470 / 10,680 / 6 \cdot 3,11 \mathrm{p} .100 / 63,150 / 63,220 / 63,1000 / 10,12 \mathrm{p} .470 / 25,680 / 16,1500 / 6 \cdot 3,13 \mathrm{p}$, $470 / 10,680 / 6 \cdot 3,11 \mathrm{p} .100 / 63,150 / 63,220 / 63,1000 / 10,12 \mathrm{p} .470 / 25,680 / 16,1500 / 6 \cdot 3,13 \mathrm{p}$.
$470 / 40,680 / 25,1000 / 16,1500 / 10.2200 / 6 \cdot 3$, 18p. 330/63, 680/40, 1000/25, 1500/16, $2200 / 10,3300 / 6 \cdot 3,4700 / 4,21 p$

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$0 \cdot 1 \mu \mathrm{~F} \quad 35 \mathrm{~V}$
$2 \cdot 2 \mu \mathrm{~F} \quad 35 \mathrm{~V}$

| $0.1 \mu \mathrm{~F}$ | 35 V | 35 V | $2.2 \mu \mathrm{~F}$ |
| ---: | ---: | ---: | ---: |
| $0.22 \mu \mathrm{~F}$ | 35 V |  |  |
| $0.47 \mu \mathrm{~F}$ | 35 V | $4.7 \mu \mathrm{~F}$ | 35 V |

$0.22 \mu \mathrm{~F} 35 \mathrm{~V}$
$\begin{array}{ll}.8 \mu \mathrm{~F} & 25 \mathrm{~V} \\ 10 \mu \mathrm{~F} & 25 \mathrm{~V}\end{array}$
$\begin{array}{lr}22 \mu \mathrm{~F} & 16 \mathrm{~V} \\ 33 \mu \mathrm{~F} & 10 \mathrm{~V} \\ 47 \mu \mathrm{~F} & 6.3 \mathrm{~V}\end{array}$
VEROBOARD

| VEROBOARD |  |
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| $2+33$ | 0.15 |
| $27 \times 32$ | 16p |
| $2 \mathrm{~m} \times 5$ 24p | 24p |
| $3 \times 31$ 24p | 24p |
| $34 \times 5$ 27p | 27p |
| $17 \times 2 t \quad 75 p$ | 571p |
| $17 \times 331000$ | 78p |
| $17 \times 5$ (plain) | 82p |
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| Pin insertion tool 52p | 52p |
| 5pot face cutter 42p | 42p |
| Plet. 50 pins 20p | 20p |

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2500 \mu \mathrm{~F} & 40 \mathrm{~V} & 74 \mathrm{p} & 2800 \mu \mathrm{~F} & 100 \mathrm{~V} & 62.60 & 4500 \mu \mathrm{~F} & 25 \mathrm{~V} \\
2500 \mu \mathrm{~F} & 50 \mathrm{~V} & 58 \mathrm{D} & 3200 \mu \mathrm{~F} & 16 \mathrm{~V} & 50 \mathrm{D} & 5000 \mu \mathrm{~F} & 50 \mathrm{~V} \\
\mathbf{C l} \\
\hline 1.10
\end{array}
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# NELSON-JONES FM TUNER KIT 



## VARICAP TUNING

as in 'W.W.' June '73

Now avaitable to readers of 'Practical Wireless'. The Nelson-Jones tuner uses dual gate MOSFET's in the RF stages, integrated circuits and ceramic filters in the IF stages, for very high performance and quick assembly. Do not confuse with tuners using only bipolar transistors and IF coils!
Tuning is accomplished by variable capacitance diodes and a Push Button Unit with 6 positions. AFC disable is incorporated as well as a pointer for each button showing tuning position in the range $87.5-108 \mathrm{MHz}$, i.e. each 'button' is fully tuneable simply by turning.

Our complete metalwork system is supplied with nuts, bolts, board standoffs, push button mains on/off and stereo mute assembly, sockets, fuse and holder. Printed and Anodised Front Panel and Veneered Teak case. Power supply kits are supplied with complete kits of parts, or separately. LED tuning ind. is also supplied.

Prices for complete kits start at $£ 23.95+50 \mathrm{ppp}$. + VAT for mono tuners, (phase locked decoders are also available to fit in the cabinet). Please send large SAE for complete details of special offers and our complete lists.
GREEN LED's-the latest for 'stereo' lamps. 1-9 69p, $10+59 \mathrm{p}$.

## TEXAN AMPLIFIER

The Cabinet of the Nelson-Jones Tuner is specially designed to match the Texan amplifer cabinet, see photographs, so that owners of Texan's are assured of compatibility, both in superb pertormance and appearance.

Texan amplifier kits are available at $£ 28-50+50 \mathrm{p} \mathrm{pp} .+$ VAT.
Worried about tuner alignment? then let our alignment service take over.
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| NEW! NEW! NEWI NEW! <br> An esposol epray providing a convenient means of producing any number of coples of a printed circuit both simply and quickly. <br> Method: Spray copper laminate board whith light sensilive spray. Cover with transparent fllm upon which circuit has been drawn. Expose to light. (No need to use ultra-violet.) Spray with developer. rinse and etch in normal manner. Loht senstive aerosol spray .. .. .. Es.0 plus Oeveloper and Etchant |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NEWER THAN NEWI:I <br> Fibre Class Board pre-treated with light-sensitive Imequer enabling you to produce prototype printed circults within flve minutes. |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| SILICON N.P.N |  |  |  |  |  |  |  |
| Type Volts Frequency Price Type Volts frequ |  |  |  |  |  |  |  |
| BC 10 | 30 |  |  | 2N 697 | 60 | 40 M |  |
| QC $100 \quad 30 \quad 150 \mathrm{MHz}$ 10p ${ }^{\text {a }}$ |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| BF 180 | 30 | 625 MHz |  | 2N 753 | 25 | 250 MHz |  |
|  |  |  |  |  |  |  |  |
| $\times 43$ | 30 | 500 MHz |  | 2N 1613 | 75 | 60 MHz |  |
|  |  |  |  |  |  |  |  |
| FY $53 \quad 30 \quad 50 \mathrm{MHz}$ 10p 2 N 305360 |  |  |  |  |  |  |  |
| 85x 87 | 40 | 500 | 10p | 2N 37 |  |  |  |
|  | 30 | 200 MHz |  | 2N 51 | 20 | 900 MH |  |
| SPECEAL OFFER |  |  |  |  |  |  |  |
| Uni-Junction Transistor Similar to |  |  |  |  |  |  |  |

POSTAGE (MINIMUM) 20p PER ORDER ALL GOODS $10 \%$ V.A.T.


SILICON P.N.P.
Type 71 Voltco
$\begin{array}{ll}\text { TYDe } & \text { Vo } \\ \text { BCY } 71 & 45\end{array}$

| Ype | Voltape |
| :--- | :--- |
| CY 71 | 45 |
| FS 92 | 100 |

BFS 95
BFX 12
$2 N 2906$

$\begin{array}{lll} & & \\ & & 10 \\ & 100 \\ \text { BLY89A } & 35 & 1,200 \\ \text { BLY } 83 A & 60 & 650 \\ & 35 & \end{array}$
$\begin{array}{lll}\text { BLY } 93 A & 60 & 650 \mathrm{M} \\ & 36 & 500 \mathrm{M}\end{array}$
BLY 218
$2 N 709$
$2 N 3926$

| Firequency | Price |
| :---: | :---: |
| 200 MHz | 120 |
| 70 MHz | 21p |
| 70 MHz | 17p |
| 210 MHz | 10p |
| 200 MHz | 15p |
| 100 MHz | $11 p$ |
| 100 MHz | 12p |
| POWER |  |
| 1,200 MHz | ¢1 |
| 650 MHz | 55 |
| 500 MHz | 55 |
| 1,200 MHz | $\underline{51}$ |
| 800 MHz | 15p |
| 250 MHz | ¢1 |

ST YERO-BOARO CUTTER $52 \frac{1}{2 l}$. $x i \ln . x \cdot 15$ BOARD 50 SO. INS. "ODD PIECES"
VERO


20 ASSORTED UHUSEO
MARKED, TESTED TRANBISTORS
BCIN ETC.

## POSTAGE 20p

PACKNo. 5
ITRAMSISTORISEO SIGNAL TRACER KIT 1 TRANGISTORISED
SIGNAL INJECTOR KIT

| GERMANIUM P.N.P. |  |  |
| :---: | :---: | :---: |
| Vollage | Frequency | Price |
| 50 | 1 MHz | 10p |
| 80 | 75 watts | E1 |
| 20 | 75 MHz | 20 p |
| 32 | 350 MHz | 29 p |
| 25 | 5 MHz | 10p |
| 15 | 450 MHz | 20p |
| 32 |  | 10p |
| 32 | 2 watts | 10p |
| 50 | 1 MHz | $10 p$ |
| Light-sensitive |  | $20 p$ |
| 30 | 10 MHz | $15 p$ |
| 30 | 15 MHz | 15 |
| 60 | 150 watts | E |

Type
ACY 44
AOY 26
AF 124
AFY 19
ASY 32
ASZ 21
GET 113
GET 120
OC 123
OCP 70
$2 N 1307$
2N 1309
2N 443
$\square 150$ wats

RECORD PLAYBACK HEADS (TRUVOX)
individual prices of these are:-
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Erace heads are aleo avaltable separ.
ately-2 track $38 \mathrm{p}-4$ track 55 p
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2 track heads alrcady fixed on heavy
mounting plate with shield $\$ 1.28$.
 Brade up model also avallable. se:ps.

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## TIME SWITCH

Bmitb's mains driven clock with 15 mmp swltch. also notes showing how you can wake up with music playing. kettie boilling or come home to a warm
house, warn of burglars, keep house, warn off burglars, keep peta warm, hal

## CHIP RADIO

Ferranti' lateat device 2N:14-gives results better than superhet. Supplled complete with technical notes and circuits. 21.88 esch. 10 for

HI-Q TUNER COMPONENTS
For experimenting with the ZN414.
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EIT NO. 2. Alr spaced tuning condenser $6^{\circ \prime}$ Karrite rod litz wound MW and LW colle, 94p. drive $8^{\prime \prime}$ territe rod, with litz wound LWW and Mw colle, 81.10 .
KIT No. 4. Permeablity tuner Fith tast and
siow motlon drive and LW loading colls 80 .

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TELESCOPIC for portable, car radlo or
namitter. Chrome platedsix tranmitter. Chrome plated47ta. ITole in bottom for 6BA acrew. 429. KNUCKLED MODEL FOR F.M. 659.


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Cleans the air at the rate of 10,000 cuble ft. per hour.
8uitable for kitchens, bath. gultable for kitchens, bath.
rooms, factories, changing rooms, factorica, changing hardly be heard. Compect, 5t ${ }^{\circ}$ casing with $5 t^{\prime \prime}$ fan bladee. Kit compriscs motor, fan bwitch, mains connector, pull fixing bracket, fis.75 plus 20 p post and ins.

MAINS OPERATED SOLENOIDS
 model 772 - mand but ifze $1 / \times 1 \mathrm{l} \times 1 \mathrm{in} .66 \mathrm{p}$,
$\mathrm{Model} 4001 /-1 \mathrm{n}$.



## MAINS TRANSISTOR

## POWER PACK

Denigned to operato tranistor sets and amplifiera. Adjutable output $6 \mathrm{v} ., 9 \mathrm{v}$., 12 volte for up to SoumA (clate B working). Takes the place of any of the following batterien: PP1, PPS, PP4, PP6, Priniformer rectiner, smoothing comprises: maina ranalormer rectitier, smoothing and load realatos $\$ 1 \cdot 10$ plus 20 p poatage.

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 Ez G.P.O. Black thandard model with dithling dial but no internal bell. 8upplied with con. nection diagram El emeh. Ditto Tlial bell but wlthout dialling Flth boll and dial e1.50 anch plue 50 p post for single then 65 p per pair.

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| Standard aize $14^{\prime \prime}$ wafer-shver-plated 5 amp contact, atandard $7^{\prime \prime}$ epindle $2^{\text {N }}$ long-with locking waher and nut. |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 pole | 449 | 410 | 410 | 44p | , | D | 48 |  |  |
| 2 polea | 44 | $4{ }^{19}$ | 410 | 44 | 49 | 419 | 448 | 770 | 770 |
| 3 poles |  | 44 | 410 | 14 | 770 | 770 | 770 | 21.04 | 21.04 |
| 4 polea | 440 | 440 | 410 | 77 | 77 | 770 | 778 | E1.32 | 21.82 |
| ${ }_{5}$ poles | 44 | 44 | 77p | 779 | 81.04 | 21.04 | 21.04 | 81.60 | 21.60 |
| 6 poles | 44 | 770 | 77p | 770 | [1.04 | \$1.04 | 21.04 | 21.87 | 81.87 |
| 7 poles | 770 | 770 | 77 | 21.04 | 21.88 | \$1.88 | t1.82 | 28.15 | 28.15 |
| 8 poles | 770 | 779 | 77p | 31.04 | 21.38 | \$1.88 | t1.82 | 22.48 | 28.48 |
| 9 poles | 770 | 77. | 21.04 | 21.04 | 81.80 | 21.80 | \$1.80 | 2e. 70 | 28.70 |
| 10 poles | 77 p | 770 | 21.04 | $\underline{1.88}$ | 21.60 | 21.60 | 21.80 | 28.00 | 88.00 |
| 11 poles | 77 | 81.04 | 21.04 | 1-82 | 21.87 | S1.87 | 21.87 | 23.25 | 28.25 |
| 12 poles | 77p | 21.04 | 81.04 | 11.82 | 21.87 | 21.87 | 21.87 | 23.68 | 23.68 |

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 Hoover and buiet ruanlag. In as hited in Hoover and blower heatera coating $\$ 15$ and more. We have a rew only. Comprises motor allowing switching 1,2 and $3 \Sigma W$. elemen thermal saftety cut-out. Can be fitted into

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Thia aritem which has proved to be amazingly Brctionc ievino and rellabla ma frat described in th Fireless Forld abont a year ago. Wa can aupply verolon (Proctical Improved and aven more eftelent $20 p$ post. When ordering plesees state De-luxe model including printed clrcuit board, etc. if P- 8 .

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Made by $8 \mathrm{~m} / \mathrm{th}$, , the are AC malas operated, NOT or can be bullt into box mounting on rack of ahelf pletely adjustable tim period. per 24 hours $\overline{\text { om }}$ changeover contecte will witch ofreult on or of during these perfods. 88.75 poet and ins. 25 p . Additions time contect bor palr.


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\hline 1000 ．．．．．．34p \& 1000 ．．．．．．10p <br>
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\hline 25 ．．．．．．12pea \& OC35 <br>
\hline 100 ．．．．．10p \&  <br>
\hline  \&  <br>
\hline 1000 ．．．．．． \&  <br>
\hline \multicolumn{2}{|l|}{\multirow[t]{2}{*}{ZENER DIODES $400 \mathrm{~m} / \mathrm{w}$ BZYB8／}} <br>
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\hline \multirow[t]{2}{*}{BZX83．From $3 \cdot 3$ volt－ 33 volts 10p each} \& LINEAR I．C． <br>
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\hline IN4700 serles． \& 709C（D．l．L．）31p <br>
\hline \multirow[t]{2}{*}{From $3 \cdot 3$ volt－ 33 volt isp each．} \& 723C（T099）＊p <br>
\hline \& 723C（D．I．L．）＊p <br>
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\hline \& 728C（T099）45p <br>
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P／001／IN5400} <br>
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(carr. etc. 30p)
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250 V P.C. Mounting: $0.01 \mu \mathrm{~F}, 0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 34 \mathrm{p} .0 .068 \mu \mathrm{~F}$, $0.1 \mu \mathrm{~F}, 41 \mathrm{p} .0 .15 \mu \mathrm{~F}, 4 \not \mathrm{p} .0 .22 \mu \mathrm{~F}, 54 \mathrm{D} .0 .33 \mu \mathrm{~F}, 8 \mathrm{p}, 0.47 \mu \mathrm{~F}, 9 \mathrm{p} .0 .68 \mu \mathrm{~F}$, 11 p . $1 \mu \mathrm{~F}$. 15p. 1. $5 \mu \mathrm{~F}, 22 \mathrm{p} \cdot 2 \cdot 2 \mu \mathrm{~F}$, 25p.
MULLARD POLYESTER CAPACITORS C296 SERIES
$400 \mathrm{~V}: 0.001 \mu \mathrm{~F}, 0.0015 \mu \mathrm{~F}, 0.0022 \mu \mathrm{~F}, 0.0033 \mu \mathrm{~F}, 0.0047 \mu \mathrm{~F}, 2$ tp. $0.0068 \mu \mathrm{~F}, 0.01 \mu \mathrm{~F}$, $0.015 \mu \mathrm{~F}, 0.022 \mu \mathrm{~F}, 0.033 \mu \mathrm{~F}, 3+\mathrm{fP} .0 .047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}, 41 \mathrm{p} .0 .15 \mu \mathrm{~F}, 04 \mathrm{p}$. $0.22 \mu \mathrm{~F}, 81 \mathrm{p} .0 .33 \mu \mathrm{~F} .12 \mathrm{p} \cdot 0.47 \mu \mathrm{~F}, 14 \mathrm{p}$.
 $0.22 \mu \mathrm{~F}, 5 \mathrm{p} .0 .33 \mu \mathrm{~F}, 6 \mathrm{p} .0 .47 \mu \mathrm{~F}, 7 t \mathrm{p} .0 .68 \mu \mathrm{~F}, 11 \mathrm{p} .1 \mu \mathrm{~F}, 12 \mathrm{pp}$.
MINIATURE CERAMIC PLATE CAPACITORS
$50 \mathrm{~V}:(\mathrm{p} F) 22,27,33,39,47,56,68,82,100,120,150,180,220,270,330,390,470$. $560,680,820,1 K, 1 K 5,2 K 2,3 K 3,4 K 7,6 \mathrm{~KB},(\mu \mathrm{~F}) \mathrm{O} .01,0.015,0.022,0.033,0.047$, $2 \mathrm{fp} . \mathrm{cach}, 0 \cdot 1,30 \mathrm{~V}, 4 \mathrm{fp} \cdot 0 \cdot 1: 100 \mathrm{~V}, 5 \mathrm{fp}$.
POLYSTYRENE CAPACITORS 160 V $5 \%$
( $p$ F) $10,15,22,33,47,68,100,150,220,330,470,680,1000,1500,2200,3300$,
470040.6800 .10 .000 . 1 p .

SPECIAL RESISTOR KITS
IOEI2 W KIT: 10 of each EI2 value, 10 ohms- 1 M , a total of 610 (CARBON FILM $5 \%$ ), 63 , 10 net IOE12 W KIT: 10 of each EI2 value, 10 ohms- 1 M , a total of 610 (CARBON FILM $5 \%$, $63 \cdot 20$ net $25 E 12$ W KIT: 25 of each E12 value, 10 ohms-1M, a cotal of 1525 (CARBON FILM $5 \%$ ), $67 \cdot 20$ net $25 E 12$ WW KIT; 25 of each EI2 value, 10 ohms-IM. a soral of 1525 (CARBON FILM 5\%), e7-35 net $20 E 12$ W K KT: 20 of each E 12 value, 10 ohms-1M, a total of 1220 (METAL FILM $5 \%$. E7. 50 net
 RESISTORS

CF—High Stab Carbon Film, $5 \%$ MF-High Srab Meral Film. $5 \%$. W. Type Range $1-9 \quad 10.49 \quad 50.99 \quad 100.249 \quad 250.499 \quad 500-999 \quad 1000-$ Sizemm $\begin{array}{llllllllll}\text { W. Type Range } & 10.49 & 50-99 & 100.249 & 250.499 & \text { So } \\ \text { CF } & 22-1 M & 1 & 0.8 & 0.65 & 0.62 & 0.55 & 0.5 & 0.45 & 2.4 \times 7.5 \\ \text { CF } & 22.2 M 2 & 0.8 & 0.65 & 0.62 & 0.55 & 0.5 & 0.45 & 3.9 \times 10.5\end{array}$ $\begin{array}{llllllll}\text { CF } & 22.2 M 2 \text { I } & 0.8 & 0.65 & 0.62 & 0.55 & 0.5 & 0.45 \\ \text { CF } & 22.1 M & 0.8 & 0.65 & 0.62 & 0.55 & 0.5 & 0.45 \\ \text { MF } & 10.2 M 7 \text { I } & 0.9 & 0.8 & 0.7 & 0.65 & 0.65 & 0.6\end{array}$ | MF | $10.2 M 2$ | 0.9 | 0.8 | 0.7 | 0.65 | 0.65 | 0.6 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| MF | 0.10 M | S | 1.25 | 1.25 | 1.7 | 0.65 | 0.65 | $5.5 \times 16$

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$8 \times 17.5$ For value mixing prices, please refer to our catalogue. (price in pence each) VALUES AVAILABLE-E12 Series only.

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| Miniature Mullard Electrolytics |  |  |  |  | VEROBOARD 0.1 0.15  <br> 2 $\times 5^{\prime \prime}$ $28 p$ <br> $28 p$   <br> $23^{\prime \prime}$ $26 p$ $19 p$ | POTENTIOMETERS <br> Carbon Track SK $n$ to 2 Ma , log or lin. Single, $16 \nmid p$ Dual Gang 46p. Log Single with switch 26p slider Pors. $10 \mathrm{~K}, 100 \mathrm{~K}, 500 \mathrm{~K}, 30 \mathrm{~mm}, 34 \mathrm{p} .45 \mathrm{~mm}, 47 \mathrm{p}, 60 \mathrm{~mm}, 53 \mathrm{p}$. |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1.5 \mu \mathrm{~F}$ | 63 V | 6p | $68 \mu \mathrm{~F}$ | $63 \vee 12 p$ | $3 \times 5$ 年 32 p 31 p |  |  |  |  |  |  |
| $2 \cdot 2 \mu \mathrm{~F}$ | 63V | $6 p$ | $100 \mu F$ | 10V 6p | 3 ¢ 3 \%" $28 p 28 p$ | DIODES |  | UGS ${ }^{\text {ap }}$ |  |  | S. Tubular a Large Cans |
| 3.3uF | 63 V | 6p | $100 \mu \mathrm{~F}$ | 25V 6p | 2f $\times 1$ 1' $7 p 7 p$ | IN4001 6 P |  | 2 Pin 12p |  |  |  |
| $4 \cdot 0 \mu \mathrm{~F}$ | 40V | 6p | $100 \mu \mathrm{~F}$ | 63V 14p | $2 \times 5{ }^{\prime \prime}$ (Plain) - 14p | 1N40027 7 |  | 3 Pin $11 p$ | 200/10. |  | . |
| 4.7 4 F | 63 V | 6p | $150 \mu \mathrm{~F}$ | 16V 6p | $2 \mathrm{~F} \times 32^{\prime \prime}$ (Plain) - 12p | IN4003 op |  | in $180^{\circ}$ 15p | 200110. |  |  |
| $6 \cdot 8 \mu \mathrm{~F}$ | 63 V | 6p | $150 \mu \mathrm{~F}$ | $63 \vee 15 p$ $6.4 V 8 p$ | $5 \times 34^{\prime \prime}$ (Plain) - 22 p | IN4004 91 p |  | mm lack $\left.14\right\|_{\text {P }}$ | $\begin{aligned} & 500 \\ & \mathbf{3 9}, 10 \end{aligned}$ | $0 / 2$ | 2500/12, 17p. 2500/25, 33p. |
| $8.0 \mu \mathrm{~F}$ $10 \mu \mathrm{~F}$ | 40 V 16 V | 6p | $220 \mu \mathrm{~F}$ $\mathbf{2 2 0 \mu F}$ | 6.4 V 6p 10 V 6p | Insertion tool 59p 59p | IN4005 12p IN4006 14p |  | nom Jack $\mathrm{lip}_{51 \mathrm{p}}$ | $\begin{aligned} & \text { 39p. } 1000 / 100,88 \mathrm{p} \\ & 2500 / 50,62 \mathrm{p} .3000 / 5 \end{aligned}$ | $\begin{aligned} & 0 / 25,27 \\ & 2 p .5000 \end{aligned}$ | 66p. 5000 50, 94p. 700050 . |
| $10 \mu \mathrm{~F}$ | 25V | 6p | $220 \mu \mathrm{~F}$ | 16V 8p | Pins, Pkt. 25 10p | IN914 7p |  | CKET | 60p. 25,000/25, 74p. | OLT: 8 | 0. 14p. 16/350, 19p. 32/350, |
| $10 \mu \mathrm{~F}$ | 63 V | 6p | $220 \mu \mathrm{~F}$ | 63V21p | Pins, Pkt. 25 10p | IN916 7p |  | in 10p | 25p. 50 250, 18p 100 | 0, 33p. |  |
| $15 \mu \mathrm{~F}$ | 16 V | 6p | $330 \mu \mathrm{~F}$ | $16 \vee 12 p$ |  | BA100 10p |  | 3 Pin 10p | METALLISED PA | R CA |  |
| $15 \mu \mathrm{~F}$ | 63 V | 6p | $330 \mu \mathrm{~F}$ | $63 \vee 25 p$ | AC127 16+p BC212L 12p | OA5 42p |  | Pin $180^{\circ} \quad 12 p$ | 2SOV: $0.05 \mu \mathrm{~F}, 0.1 \mu \mathrm{~F}$ | p, 0.2 | 54p, $0.5 \mu \mathrm{~F},{ }^{6} \mathrm{p}_{\mathrm{c}} 1^{1} \mu \mathrm{~F}, 9 \mathrm{p}$. |
| $16 \mu \mathrm{~F}$ | 40 V | 6p | $470 \mu \mathrm{~F}$ | $6.4 V 9 p$ $40 \vee 20 p$ | $\begin{array}{llll}\text { AC127 } & 164 p & B C 212 L & \text { 12p } \\ \text { AC128 } & 22 p & \text { BC213L } & 12 p\end{array}$ | OA47 9p |  | Jack 14.p | $500 \mathrm{~V}: 0.025 \mu \mathrm{~F}, 0.05 \mu \mathrm{~F}$ | . | tp, $0 \cdot 25 \mu \mathrm{~F}, 6 \not$ pp. $0 \cdot 5 \mu \mathrm{~F}, 9 \mathrm{p}$. |
| $22 \mu \mathrm{~F}$ | 25V | 6p | $470 \mu \mathrm{~F}$ $680 \mu \mathrm{~F}$ | $40 \vee 20 p$ $16 \vee 15 p$ | $\begin{array}{lll}\text { AC128 } & \text { 22p } & \text { BC213L } \\ \text { BC107 } & 11 p & \text { BC214L } \\ \text { 17p }\end{array}$ | OAB1 IIp |  | mm Jack $11 p$ | 1000V: $0.01 \mu \mathrm{~F}, 10 \mathrm{p}$ | 222 F, 12 | F. |
| $22 \mu \mathrm{~F}$ | 63 V | 6p | $680 \mu \mathrm{~F}$ $680 \mu \mathrm{~F}$ | $16 \vee 15 p$ $40 \vee 25 p$ | $\begin{array}{lll}\text { BC107 } & 11 p & \text { BC2 } \\ \text { BC108 } & 12 \mathrm{p} & \text { OC4 } \\ \text { 17p }\end{array}$ | OA200 8p |  | $0 \quad 5 \dagger$ p | $31 \mathrm{p}, 0.47 \mu \mathrm{~F} .39 \mathrm{p}$ |  |  |
| $32 \mu \mathrm{~F}$ $33 \mu \mathrm{~F}$ | 10 V | 6p | $680 \mu \mathrm{~F}$ $1000 \mu \mathrm{~F}$ | 16 V 20 p | BC109 13p OC7! 13p | Integrated |  | Treened | Fietr |  | NTITY DISCOUNT |
| $33 \mu \mathrm{~F}$ | 40 V | 6p | 1000 4 F | 25V 25p | BC148 12p OC81 16p | Circuits |  | Twin Seree | Wire, Metre | 10p | PECIAL BULK BUY PRICES |
| $32 \mu \mathrm{~F}$ | 63 V | 6p | $1500 \mu \mathrm{~F}$ | $6.415 p$ | BC149 12p OC170 23p | [A709C | 50p | Stereo Scree | ed Wire, Merre | 10p | ARE AVAILABLE BY |
| $47 \mu \mathrm{~F}$ | 10 V | 6p | $1500 \mu \mathrm{~F}$ | $16 \vee 25 p$ | BCI82L 12p TIS43 33p | HA741C | 35p | Connecting | ire, All colours, Merre W Wire Ended |  | ON FOR LARGE |
| $47 \mu \mathrm{~F}$ | 25 | 6 p | $2200 \mu \mathrm{~F}$ | $10 \vee 25 p$ | $\begin{array}{lll}\text { BC183L } & 12 p & \text { 2N2926 11p } \\ \text { BC184L } & 11 p & \text { 2N3702 }\end{array}$ | wA723C | 45 | Neon Bulb, Panel Neon | Wire Ended $40 V$ Red Amber. Clear | $5 \text { for 24p }$ $161 p$ | PROJECTS AND TRADE |

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## Fun With HI-FI

In this book Gilbert Davey defines exactly what high fidelity sound is. He describes the different links In the hi-fi system-the playing deck, cartridge, tuner, amplifier, loudspeaker and loudspeaker assemblyand the part each plays in the reproduction of hi-fi sound. He tells the reader what kind of equipment is available today, and concludes with the latest developments in stereo headphones and four-track stereo'quadraphonic sound'. Fully illustrated, £1-15.

PUBLISHED BY KAYE \& WARD

[^8]

Stereo 80 pre amplifier/control unit

## the slimmest,most elegant hi•fi modules ever made



Living with hi-fi takes on new meaning now that Project 80 is here. These amazing new modules mark a brilliant technical advance all round: their size and presentation bring exciting new opportunities to install systems in ways hitherto only dreamed about but never before made practical, You can build a Project 80 system virtually anywhere and it is unbelievably simple to install and connect up. Everything that could possibly, be wanted in a top quality do-it-yourself domestic hi-fi system will be found in Project 80 - compactness, elegantly ultra-modern siyling, ease of fixing and operation, new control methods, and above all superb performance. New as well as popular established ideas on installation are featured on page four of this announcement to provide just


# Project 80 new modules 

## Stereo 80 pre-amplifier and control unit

As with other Project 80 units, the Stereo 80 is mounted by means of two bolts fixed at the reat which pass inrough holes drilled in the wood or plastic on which modules are to be mounted All the electronics are contaned within the ${ }^{3}$ " deep front panel' Connecting leads are taken away similarly out of sight Each channel in the Stereo 80 has its own independent tone and volume controls operated by sliders This enables exceptionally good environmental matching to be obtained. Provision is made fo magnetic and ceramic pick-ups, radio and tape in and out A virtual earth input stage forms part of the up-dated circuitry of the Sterea 80 to ensure the finest possible quality from all signal sources Generous overload margins are allowed on all inputs Clear instructions with template are supplied

## TECHNICAL SPECIFICATIONS

Size - $260 \cdot 50 \cdot 20 \mathrm{~mm}\left(10_{4} \times 2\right.$ : ins $)$
Finish - Black, with white markings
Inputs - Mag P U 3 mV RIAA corrected: Ceramic P U 300 mV
Radio 300 miV : Tape 30 mV
S/N ratio - 60db
Frequency range -20 Hz to $15 \mathrm{KHz}=$ idB 10 Hz to 25 KHz . 3 dB
Power requirements -201035 volts
Outputs - 100 mV .- AB monitoring for tape
Controis - Press button for tape. radio and $\mathrm{P} U$ selection Volume
Bass- 12 dB to -14 dB at 100 Hz . Treble -11 dB to -12 dB at 10 KHz


## Project 80 FM tuner smaller, more efficient

A truly remarkable tuner in every way - its unbelievably compact size its original circuitry - its dependable performance - all this in a boldly designed modern case measuring $85.50 \cdot 20 \mathrm{~mm}$ ( $3 \frac{1}{2} \times 2 \times 3 \mathrm{ins}$ ) Greater adaptability (and possibly financial convenience) results from the tuner and stereo decoder section being made avalable separately

TECHNICALSPECIFICATIONS
Size-85 $50 \quad 20 \mathrm{~mm}$ (approx 3: 2 3 3ns)
Tuning range -87 to 108 MHz
Detector-1 C. balanced coincidence, for good A M rejection
AFC - Switchable. with thermistor control to prevent from dift
One 26 transistor I.C.
Twin dual varicap tuning
Distortion - $03 \%$ at 1 KHz for 75 KHz deviation
Ceramic filter in I.F. section
Aerial impedance - $75 \Omega$ or $240-300 \Omega$
Sensitivity - 4 microvolts for 30 dB quelıng
Power requirements - 12 to 45 volts

## Project 80 stereo decoder

Making the Project 80 decoder seoarate from the FM tuner gives the consiructor a wider choice of systems as well as saving money in cases where stereo reception may not be required This unit gives a 40 dB channel separation with an output of 150 mV per channel The gallum arsenide light emitting beacon automatically lights up to show when a stereo transmission is iuned in. Designed essentially as an integral part of Project 80 systems. this multiplex stereo demodulator may be used in many cases with existing single channel frequency modulated tuners to provide stereo reception.
Size $-47.50 \times 20 \mathrm{~mm}$ (1: 2. Zins)
One 19 transistor I.C.


## new constructional techniques

## and again Sinclair leads the world

1962 | Micro-miniature power amp small enough to stand on a |
| :--- |
| 10p. piece. Slimiline pocket receiver smaller than a 20 |
| cigarette pack |

1963 Micro-6 receiver. smaller than a matchbox
1964 Pocket F.M. receiver. PWM amp.
1965 Z.12 power amplifier module. PZ. 3 power supply
1966 Stereo 25 pre-amp/control unit
1967 10 p. piece Slimiline pocket receiver smaller than a 20 cıgarette pack
1963 Micro. 6 receiver. smalier than a matchbox
1964 Pocket F.M. receiver. PWM amp
1965 2.12 power amplifier module. PZ. 3 power supply
1966 Stereo 25 pre-amp/control unit
1968 IC. 10. The first ever integrated circuit for constructors use

## Project 80 active filter unit

This efficiently designed unit makes a highly desirable part of any worthwhile system where inputs may be from record, radio or tape. As With Stereo 80. separate controls are applied to each channel thereby making it easier to obtan ideal stereo balance in any kind of indoor environment

## TECHNICALSPECIFICATIONS

Size-108 $50 \cdot 20 \mathrm{~mm}(4: 2$. lins)
Voltage gain-minus $020 B$
Frequency response -36 Hz to 22 KHz . controls minumum
Distortion - at $1 \mathrm{KHz}-003 \%$ using 30 V supply
HF cut off (scratch) - $22 \mathrm{KHz} 1055 \mathrm{KHz}, 12 \mathrm{~dB} / 0 \mathrm{Cl}$ slope
L.F. cut off (rumble) -28 dB at 20 Hz . $9 \mathrm{~dB} / 0 \mathrm{Ct}$ slope

## Z. 40 \& Z. 60 power amplifiers totally short-circuit proof

Either of these entirely new power amplifiers is intended for use in Project 80 installations although. of course they are readily adaptable to an even wider range of applications Both $Z 40$ and $Z 60$ incorporate builtin protection against shortcricuiting and risk of damage arising from mis-use is greatly reduced Comprehensive instructions are supplied with each of the modules.
Z.40 Technical Specifications

Size-55. $80 \cdot 20 \mathrm{~mm}$
(21 - 31 子ins) 9 transistors Input sensitivity -100 mV
Output-15 watis RMS continuous inio $8 \Omega(35 \mathrm{~V}) 30$ watis music power into $4 \Omega(30 \mathrm{~V})$
Frequency response $-10 \mathrm{~Hz}-$ $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$
Signal to noise ratio -64 dB Distortion - at 10 watts into $8 \Omega$ lessthan 0 \%
Power requirements -12.35 volts

Z 60 Technical Specifications
Size-55 $98 \quad 20 \mathrm{~mm}$
(21-3! - Ins) 12 transistors Innut sensitivity $-100-250 \mathrm{mV}$ Output - 25 watts RMS into $8 \Omega(45 \mathrm{~V}) 50$ watis music power mint $4 \Omega(50 \mathrm{~V})$
Distortion-typically $003 \%$ Frequency response -10 Hz to more than 200 KHz - 1 dB Signal to noise ratio - better than 70dB
Built-in protection against transient overload and short circuit
Load impedance $-4 \Omega$ min. max safe on open crecuit

## Sinclair power supply units PZ. 8

the worlds most
advanced unit in its class
Stabilised power supply unit Reentrant current timiting makes dam. age from overload or even direct shorting impossible. a principle never bufore inorporated in a com. mercially avalable constructor mod. ule Normal working voltage (adjus table) 45 V
R R P £7.98+079p P A T
Without mains transformet PZ. 5 30V unstabilised
R R P 〔4.98 + 049 p VA T
PZ. 635 V stabilised
RRP $\mathbb{7} .98+079 p \vee A . T$.


Recommended Project 80 applications

| System | The Units to use | Units cost |
| :---: | :---: | :---: |
| Simple battery record player | 2.40 | $\begin{aligned} & £ 5.45 \\ & +54^{\prime} \mathrm{D} V A T \end{aligned}$ |
| Mains powered record player | Z.40, PZ.5 | $\begin{aligned} & £ 10.43 \\ & +£ 104 \mathrm{VAT} . \end{aligned}$ |
| 30 W . RMS continuous sine wave stereo amp. | $\begin{aligned} & 2 \cdot Z .40 \mathrm{~s}, \text { Stereo } \\ & 80: P Z .6 \end{aligned}$ | $\begin{aligned} & £ 30.83 \\ & +£ 308 \vee \text { A.T. } \end{aligned}$ |
| $50 W(8 \Omega)$ RMS continuous sine wave de Juxe stereo | $\begin{aligned} & 2 \cdot Z .60 \mathrm{~s}, \text { Stereo } \\ & 80: P Z .8 \end{aligned}$ | $\begin{aligned} & £ 33.83 \\ & +£ 338 \vee A T \end{aligned}$ |
| amplifier Indoor P.A | Z.60, PZ. 8 | $\begin{aligned} & £ 14.93 \\ & +€ 149 \vee A T \end{aligned}$ |
| Car Radio | F.M. tuner, $2.40$ | $\begin{aligned} & £ 16.40 \\ & +£ 164 \vee A T \end{aligned}$ |

## From Sinclair the worlds most advanced hi-fi modules

## Sinclair Project 80 tre ultra-modern non-obrusuive hi-fi



A Project 80 system could be built into a book-shelf end
 a shelf could be sufficient to contaın a complete system


The modules mount very easily onto a playing plinth


Two Sinclair Q .16 loudspeakers
suitably positioned together with Project 80 could be mounted on to a false wall

When you have seen for yourself how fantastically slim and cleverly designed these modules are, further ways will suggest themselves in which they can become a pleasing part of your particular domestic environment.


## Guarantee

if. Within 3 months ot purchasmy any froxduct durat frome us, you are dissatis. ford with it. Yout money will ber efunded (an) praduciton of recerpt of payment Miany Surclan apponnted Strockısis also after this guatantec

Should amy dele lanse im menmal use. we will service it withoul charge for damage arising from bus use at smalk - harge (ivpically f 100 ) will be made.

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| :---: | :---: | :---: |
| DY81 | 0.85 | EF83 |
| DY88/7 | 0.42 | EF85 |
| DY802 | 0.45 | EF96 |
| EABC80 | 1.00 | EF89 |
| EB91 | 0.38 | EF91 |
| EBC81 | 0.75 | EF92 |
| EBF80 | 0.80 | EF95 |
| EBF83 | 0-82 | EF183 |
| EBF89 | 0.88 | EF184 |
| EC88 | 0.75 | EH90 |
| EC88 | 0.77 | EL34 |
| ECC81 | 0.45 | EL36 |
| ECC82 | 0.48 | EL81 |
| ECC83 | 0.45 | ELA4 |
| ECC84 | 0.85 | EL85 |
| ECC85 | 0.58 | FL86 |
| ECC88 | 0.75 | EL95 |
| ECC189 | 0.71 | EL91 |
| ECF80 | 0.58 | ELL80 |
| ECF82 | 0.78 | E3184 |
| ECF86 | 0.71 | E*87 |
| ECH81 | 1.00 | FY51 |
| ECH 83 | 100 | EY86/A |
| ECH84 | 0.78 | EY88 |
| ECLB0 | 0.53 | EZ80 |
| ECL82 | 0.81 | EZ81 |
| ECL83 | 0.88 | GY501 |
| ECL8 6 | 0.63 | GZ34 |


|  | PC88 |
| :---: | :---: |
|  | PC88 |
| 0.48 | PC97 |
| 1.03 | PC900 |
| 0.43 | PCCA |
| 0.80 | PCC88 |
| 0.81 | PCC89 |
| 130 | PCCI89 |
| 1.40 | PCFP80 |
| 1.35 | PCF82 |
| 0.60 | PCF88 |
| 0.80 | PCF200 |
| 0.56 | PCF201 |
| 0.95 | PCF801 |
| 1.05 | PCF802 |
| 09 | PCP806 |
| 047 | PCH200 |
| O55 | PCL82 |
| 0.70 | PCL4 4 |
| 1.31 | PCLA5 |
| $1 \cdot 30$ | PCL8 ${ }^{\text {P }}$ |
| 1.18 | PCL805/8 |
| 1-18 |  |
| 0.83 | PD500 |
| 0.42 | PFL200 |
| 0.64 | PL36 |
| 0.61 | PL81 |
| 0.40 | PL81A |
| 0.90 | PL82 |
| 0.78 | PL83 |

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| :---: | :---: | :---: | :---: |
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\hline 6AKB & 0.40 & 6いKも & 0.60 & firs： \\
\hline BAK \({ }^{\text {c }}\) & 0.80 &  & 0.80 & oftir \\
\hline ＊AL． 3 & 0.43 & 13648 & 1.35 & \({ }_{6} \mathrm{~N}\) \\
\hline BAIS & 0.25 & 6fids & 0.70 & \(6 . \mathrm{S}\) \\
\hline 6A\＄16 & 0.37 & 6，E：H： & 0.30 & 6． S \\
\hline 6AqS & 0.45 & tifli & 0.38 & fye \\
\hline 6 A96 & 0.70 & 6FWG & 0.70 & 784 \\
\hline 6ARS & 0.60 & ¢ド！ & 0.78 & \\
\hline 6AR6 & 0.68 & \(65^{6} 5\) & 0.75 & 9 m \\
\hline GAM5 & 0.85 & nFind & 0.50 & 10 \\
\hline
\end{tabular}

\section*{TRANSISTORS \\ \section*{ISTOR}}


2 N 696
2 N 69
2 N 69
2 N 69
\(2 \times 608\)
\(2 \times 708\)
\(2 \times 708\)
\(2 N 708\)
\(2 \times 768\)
2N708
2N708
2N929
\(2 \times 030\)
\(2 \times 947\)
 \(2, ~\)
\(2 \mathrm{~V} / 1\)
2 y 1 \(2 \times 113\)
2 N 118
2 N 130
2 N 130
2 N
\(2 \mathrm{~N}_{1}\)
\(2 \mathrm{~N}_{13}\)
\(2 \mathrm{~N}_{13}\)
aN13 \(2 \times 1\)
\(2, ~ v 18\) \(2, N 1\)
2.216 2.1
\(2 . N 1\) \(2 \times 2\) \(2{ }_{2}^{2} 2\) \(2 \mathrm{~N}_{2}\) 2 N
\(2 \mathrm{~N}:\) \(2 \mathrm{~N}: 4\) \({ }^{2} \mathrm{~N}_{2} 29\) \begin{tabular}{ll} 
\\
2.2923 & 0.12 \\
\hline
\end{tabular} \(\mathrm{N} 2 \mathrm{p} 24 \mathrm{O}^{0.18}\) \(\begin{array}{ll}2 \times 19053 & 0.20 \\ 2 & \\ 2 & \\ 2\end{array}\) \begin{tabular}{ll|}
\(2 \times 3054\) & 0.80 \\
2 & 0.80 \\
\(2 \times 3055\) & 0.80
\end{tabular} \(\begin{array}{lll}2 \times 3085 & 0.80 & A \\ 2 \times 3133 & 0.25 & \end{array}\)


41113：1

\subsection*{0.85} 111123
180124
1113131 0.80
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 0.20
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0.10 \begin{tabular}{l|ll}
5 & 28746 & 0.25 \\
\hline & A 1113 & 0.18
\end{tabular} \(\begin{array}{lll}0.16 & \text { AC113 } & 0.18 \\ 0.30 & \text { AC125 } & 0.30 \\ 0.70 & A C 127 & 0.17\end{array}\) 0.70
0.10
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\begin{tabular}{ll|}
\(2 \times 3391\) & 0.25 \\
\(2 \times 17\) & A \\
\(2 \times 3922\) & 0.17
\end{tabular}

\section*{\(\begin{array}{ll}2 \mathrm{~N} 3393 & 0.16 \\ \mathrm{~N} 3394 & 0.16\end{array}\)}

\section*{－}

2 N 3
2 N 3
2 N 3
\(\begin{array}{ll}2 \times 3403 & 0.15 \\ 2 \times 3404 & 0.32 \\ 2 \times 3 & 0.20\end{array}\)
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