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\author{

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$2 \times \mathbf{Z 3} 3$, Stereo 60, PZ5
$2 \times$ Z30, Stereo 60, PZ6
$2 \times Z 50$, Stereo 60, PZ8
Transiormer for ${ }^{\mathbf{2 0} 28}$
PROJECT 605 KIT 19.95


POWER SUPPLIES FOR

## EVERY PURPOSE

(All cased unless stated chassls)

470C $6 / 7 \frac{1}{2} / 9$ volt 300 MA (Ineludes Multi-Adaptor for Cape Recorders, etc.) $\quad 1.35$ post $20 p$ Car $\quad 1.95$ (state voltage | $6 \mathrm{v}, 7 \mathrm{v}, 9 \mathrm{v})$ |  |
| ---: | ---: |
| $\mathrm{SC} 2023 / 617+19$ volt 400 mA | 1.95 es. post 25 p | HC244R Stabilised version P500 9 volt 500 mA

P11 24 volt 500 mA (chassis)
P15 $26 / 28$ volt 1 amp (chassis) P1080 12v 1 amp (chassis) P1081 45v 0.9 amp (Chassis) P12 $4 \frac{1}{2}-12$ volt $0 \cdot 4$ - 1 amp (Stab.) RP164 6/7t/9/12 1 amp (Stab.) 4.25 carr. 30p 2.30 post 20 p $2 \cdot 80$ post 20 p 2.70 post 20 p
3.25 post 20 p 3.25
4.40 post 20 p
$\mathbf{4}$ post 20 p 4.40 post 200
6.75
post 30 p RP164 6/7t/9/12 1 amp (Stab) $\quad$ g. 15 post 25 post 30 p


STEREO AMPLIFIERS
(carr./packing 50p)

| AKAI | $\begin{aligned} & \text { A A } 5200 \\ & \text { AA } 5500 \\ & \text { A A } 5500 \end{aligned}$ | $\begin{array}{r} 61.70 \\ 78.50 \\ 117.50 \end{array}$ |
| :---: | :---: | :---: |
| AMSTRAD | 1 C 2000 Mk . II | 29.50 |
|  | 4000 | 23.10 |
| EAGLE | TSA149 | 25.10 |
|  | TSA159 | 34.85 |
|  | AA2 | 30.80 |
|  | AA4 | 42.45 |
|  | AA6 | 55.95 |
|  | DA1000 |  |
| HENELEC WEST HENELEC TEXAN | KIt | 28.50 |
|  | Built |  |
|  | TRM300 | 25.95 |
|  | TRM400 | 32.50 |
| PIONEER ROTEL | SA500A | 34.25 |
|  | RA310 | 36.95 |
|  | RA610 |  |
|  | RAB10 | 75.75 |
|  | RA1290 | 92.50 |
| SINCLAIR | 2000 |  |
|  | 3000 | 28.95 |
| TANDBERG TELETON | TA300 | $66 \cdot 10$ |
|  | SAO206B | 22.50 |
|  | SAQ307 | 22.50 |
|  | GA202 | 28.50 |

STEREO RADIO TUNERS
(carr./packing 50p)
AKAl
AMSTRAD
EAGLE
HENELEC Stereo KIt
HENELEC Stereo Bullt HOWLAND WEST DA1000T PIONEER TX500A
ROTEL $\begin{array}{ll}\text { RT320 } \\ \text { SINCLAIR } & \text { RT620 } \\ & 2000\end{array}$ TELETON $\quad 3000{ }^{2}$ DECODERS
SYNTHESIZERS

## (carr. etc. 30p)

AKAI SS1
EAGLE AA10
$\left.\begin{array}{l}\text { TATE } 1 \\ \text { TATE } 3 \\ \text { TATE }\end{array}\right\}$ ChassIs $\left.\begin{array}{l}\text { TATE } 3 \\ \text { TATE } \\ \text { TATE }\end{array}\right\}$
MATCHED SPEAKER

## SYSTEMS

Recommended pairs 8 ohms (Carr. / Packing $£ 1 \cdot 50$ pait)
MARSDEN HALI

## 110 150 150 <br> | 150 |
| :--- |
| 200 |

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DYNACO
DYNACO 250020 watt
A25
WHÁRFEDALE
Denton 2 i8 watt
$\begin{array}{ll}\text { Uinton } 2 & 20 \text { watt } \\ \text { Triton } & 25 \text { walt }\end{array}$
$\begin{array}{ll}\text { LEAK } \\ 160 & 18 \text { watt }\end{array}$
${ }^{250}$ CELESTION ${ }^{18}$ watt
1 COUNTY 20 watt
$\begin{array}{ll}\text { COUNTY } & 25 \text { watt } \\ 15 & 30 \\ \text { watt }\end{array}$
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(carr. etc. 15p)
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Complete with Speakers carp./packlng £1.25)
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$\begin{array}{ll}\text { Sanyo } & \text { GXT4520KL } \\ \text { Sanyo } & \text { GXT4730KL }\end{array}$ $\begin{array}{ll}\text { Philips } & \text { GY908 } \\ \text { Philips } & \text { RH802 }\end{array}$
$\begin{array}{ll}\text { Philips } & \text { RH802 } \\ \text { Philitos } & \text { RF836 } \\ \text { Philins } & \text { GF826 }\end{array}$
$\begin{array}{ll}\text { Philips } & \text { GF826 } \\ \text { Philips } & \text { RH813/RH142 }\end{array}$
$\begin{array}{ll}\text { Philps } & \text { RH811/ } \\ \text { Phillps } & \text { RF839 } \\ \text { Philips } & \text { GF829 }\end{array}$
$\begin{array}{ll}\text { Philips } & \text { G8889 } \\ \text { Philps } & \text { G8815 }\end{array}$
Phillps GF808

| Philips | RH84/RH411 | GF65 |
| :--- | :--- | :--- |
| Phillos | GF603 | 93.50 |

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RECORDERS
(carr. etc. 30p)

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| Amerex | AC104 | 16.00 |
| :--- | :--- | :--- |
| Phillps | N2204 | 20.75 |
|  | N2205 | 29.50 |
|  |  |  |

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CASSETTE RECORDERS
(carr. etc. 30p)
ACR200
ACR201
Ellzabethan LZ416
BASF CC9301
Phllips
$\begin{array}{ll}\text { Sanyo } & \text { M4141 } \\ & \text { M2400W } \\ & \text { M2400FG } \\ & \text { M4400FC } \\ \text { Grundig } & \text { C250 } \\ \text { HItachi } & \text { TRK1240E } \\ & \text { TRS1161 }\end{array}$
TRS1161
KCT1210L
DECKS
(carr./packing 50p)
CASSETTE
Phillps N2506 $\begin{array}{ll}\text { Pye } & 9145 \\ \text { Tandberg } & \text { TCD } 300 \\ \text { Akai } & \text { GXC40D }\end{array}$

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GXC45D
GXC46D
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3055 , ment for 2N 305
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Q3 4 OC 77 type transistors
$\begin{array}{lll}\text { Q4 } & 4 & \text { Matched translato } \\ \text { Q6 } & \text { OC } & \text { OF transistors }\end{array}$
$\begin{array}{ll}\text { Q6 } & \text { B OC } 72 \text { transistors } \\ \text { Q7 } & 4 \text { AC } 128 \text { transistora PNP high gain }\end{array}$
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500 MHz (code P397).............
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U45 7 3A SCR. TO68 up to 600PIV
Code No's. mentioned above are given as a gulde to the type of device in the pak. The dovices themael yes are normally unmarked.


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| PIV | 300 mA | 750 mA | 1 A | 1.5 A | 3 A | 10 A | 30 A |
| ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 50 | 0 | 04 | 0.06 | 0.06 | 0.08 | 0.16 | 0.23 |
| 0 | 0.66 |  |  |  |  |  |  |
| 100 | 0.04 | 0.07 | 0.06 | 0.16 | 0.18 | 0.26 | 0.83 |
| 200 | 0.04 | 0.10 | 0.077 | 0.16 | 0.22 | 0.27 | 1.10 |
| 400 | 0.07 | 0.15 | 0.08 | 0.28 | 0.30 | 0.41 | 1.88 |
| 600 | 0.08 | 0.18 | 0.11 | 0.26 | 0.38 | 0.50 | 2.05 |
| 800 | 0.11 | 0.19 | 0.12 | 0.28 | 0.41 | 0.61 | 2.20 |
| 1000 | 0.12 | 0.28 | 0.16 | 0.33 | 0.81 | 0.70 | 2.76 |
| 1200 | - | 0.37 | - | 0.42 | 0.63 | 0.83 | - |

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| H8/2A | $3 \cdot 3 \mu{ }^{\prime}$ | 25 v | 4 p | H7/5 | $80 \mu{ }^{\prime}$ | 16 v | $4 p$ |
| H8/3 | $3 \mu \dagger$ | 50 v | 4 p | H7/6 | 100 $4 \dagger$ | 25 v | $5 p$ |
| H8/3A | $4 \mu$ | 50 v | 4 p | H7/6A | 10014 | 15v | $4 p$ |
| H8/4 | 4.714 | 25v | 4p | H7/7 | 100 $\mu$ f | 25v | $4 p$ |
| H8/4A | 5 41 | 64v | 4p | H7/8 | 125 $\mu \dagger$ | 16v | $5 p$ |
| H8/5 | $5 \mu 1$ | 10v | 4 p | H7/8A | 100 1 ¢ | 35 v | $8 p$ |
| H8/5A | $5 \mu 9$ | 150 v | 4 p | H7/9 | 100 $\mu 4$ | 83 v | 6 p |
| H8/6A | 104 ${ }^{7}$ | 10v | $4 p$ | H7/9A | 125 $\mu \dagger$ | 4 V | 4p |
| H817 | 1014 | 70v | $4 p$ | H7/10 | 125 $/ 4$ | 25v | 6 p |
| H8/8 | 164 $\dagger$ | 35 v | $4 p$ | H7/10A | 160 $\mu \mathrm{f}$ | 2.5 v | 3p |
| H8/8A | 18/4 ${ }^{\text {f }}$ | 16v | 4 p | H7/11 | 160 ${ }^{\text {f }}$ | 25 v | 6 p |
| H8/9 | $20 \mu 9$ | 6 v | 2p | H7/11A | 1504f | 16v | 5p |
| H8/9A | 2044 | 70 V | 4 p | H7/13A | 2004 | 25v | ep |
| H8/10 | $22 \mu \dagger$ | 50 v | 4 p | H7/14 | $220 \mu 1$ | 50 v | 10 p |
| H8/10A | $22 \mu 4$ | 100v | 4 p | H7/14A | $220 \mu 9$ | 16v | 6 p |
| H8/11 | 25 $\mu$ f | 12v | $4 p$ | H7/15 | 22014 | 25v | 5 p |
| H8/11A | 24 $\mu \dagger$ | $275 v$ | 4 p | H7/15A | 28014 | 35v | 10p |
| H8/12 | $32 \mu \dagger$ | 15v | $4 p$ | H6/1A | 250Mf | 4v | 3 p |
| H8/12A | 3041 | 10v | 4 | H6/3A | 32014 | $2 \cdot 5 \mathrm{v}$ | 3p |
| H8/13A | $32 \mu \dagger$ | 50 v | 40 | H6/4 | $320 \mu 1$ | 10 V | 4p |
| H8/14 | 40, 4 | 25 v | $5 p$ | H6/4A | 33014 | 18 v | 5 p |
| H8/14A | 4014 | 16v | 4 p | H6/5 | 33041 | 25v | 10p |
| H8/15 | $47 \mu \boldsymbol{f}$ | 50 V | 4 p | H6/5A | $330 \mu 4$ | 35 v | 15p |
| H8/15A | 4014 $\dagger$ | 35 v | 4 p | H6/7 | 400 $\mu 1$ | 15v | 5p |
| H7/1 | 5014 | 6 V | 3 p | H6/8 | 47045 | 25v | 10p |
| H7/1A | 5014 | 10 v | $4 p$ | H6/8A | 47014 | 35 v | 20p |
| H7/2 | 50121 | 50 V | 4 p | H6/9A | 400 11 | 40 V | 20p |
| H7/2A | $64 \mu 4$ | $2 \cdot 5 \mathrm{v}$ | 2 p | H8/10 | 75014 | 12v | 5p |
| H7/3A | 64 14 | 25 v | $4 p$ | H6/13A | 100014 | 25 v | 18p |
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| 07215113 | 16 | $11000+11000$ | 13.8 amps | 4 toz | 49p |
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| 07216502 | 25 | $5000+5000$ | 9.6 amps | 3toz | 37p |
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| 07217342 | 40 | $3400+3400$ | 9.1 amps | $3 \frac{1}{2} 02$ | 37p |
| 07217502 | 40 | $5000+5000$ | 12.0 amps | 4102 | 49 p |
| 07118681 | 63 | 680 | 2.1 amps | 102 | $15 p$ |
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| 10615103 | 16 | 10000 | 7 amps | $2 \frac{1}{2} \mathrm{Oz}$ | $65 p$ |
| 10616223 | 25 | 22000 | 17 amps | 1002 | 8.1.12 |
| 10617103 | 40 | 10000 | 12 amps | $7 \frac{1}{2} \mathrm{Oz}$ | 94p |
| 10618153 | 63 | 15000 | 28 amps | 1802 | E.1.79 |
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$14 \times 3 \mathrm{in} .16 \mathrm{p} ; 10 \times 7 \mathrm{in} .19 \mathrm{p} ; 12 \times 5 \mathrm{in} .90 \mathrm{p} ; 12 \times 8 \mathrm{in} .15 \mathrm{p} ;$ $16 \times 6 \mathrm{in}$ ． $28 \mathrm{p} ; 14 \times 9 \mathrm{in} .84 \mathrm{p} ; 12 \times 12 \mathrm{in} .40 \mathrm{p} ; 16 \times 10 \mathrm{in} .60 \mathrm{p}$ PAXOLIN PANEL $10 \times 8 i n .15 p$ ．

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GEHERAL PURPOEE LOW VOLTAGE．Tapped at $2 A, 8,4,5,6,8,9,10,12,18,18,24$ and 80 V
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$8 A, 6,8,10,12,16,18,20,84,30,86,40,48,60 \mathrm{~V}$ $8 \mathrm{~A}, 5,8,18 \mathrm{~V} 21-00$ ，Ditto 5 A $8 \mathrm{~A}, 5,8,10,18 \mathrm{~V}$, B－0 $=5 \mathrm{~V}$ 21P80，Ditto BA 6Y 0.6500 mA
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$500 \mathrm{mF} .12 \mathrm{~F} .15 \mathrm{p} ; 25 \mathrm{~V} .20 \mathrm{p} ; 80 \mathrm{~F} .80 \mathrm{p}$.
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 $30-14,500 \mathrm{c} / \mathrm{h}, 12 \mathrm{in}$ ．Past 85 con，wooler and tweeter cone osether with a BAKER marame magnet sasembly 4000 flar denaity of 145，000 sud a total Anx esonsmee 40 c／s Raiod 90 ratta NOTR C／s Rated 20 15 ohms must be stated．

Module kit， $80-17,000 \mathrm{c} / \mathrm{s}$ with twetter，crosiover，berle and instractions．$£ 12.50$ P．$\$$ p． 85 p ．

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| DY86/7 | 0.42 | EF85 |} $\begin{array}{ll}\text { DY86/7 } & 0.42 \\ \text { DYF8s }\end{array}$ | EABC80 | $\mathbf{0 . 4 5}$ | EF86 |
| :--- | :--- | :--- | :--- | | EB91 | $\mathbf{0} .88$ | EF99 |
| :--- | :--- | :--- | | EBC81 | $\mathbf{0 . 7 8}$ | EF91 |
| :--- | :--- | :--- |
|  | EF92 |  | | EBC81 | $\mathbf{0 . 7 5}$ | EF92 |
| :--- | :--- | :--- |
| EBF80 | 0.60 | EF95 | | EBF80 | 0.60 | EF95 |
| :--- | :--- | :--- |
| EBF83 | $0-62$ | EFIB3 |
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| EL3 | EL3 |  | | ECC81 | 0.45 | EL36 |
| :--- | :--- | :--- |
| ECC82 | 0.48 | EL81 |
| ECC83 | 0.45 | EL8 | | ECC83 | 0.45 | EL81 |
| :--- | :--- | :--- | | ECC84 | 0.55 | EL88 |
| :--- | :--- | :--- |
| ECC85 | 0.53 | EL80 | | ECC85 | 0.63 | EL86 |
| :--- | :--- | :--- |
| ECC88 | 0.75 | RL8 | ECC85 | ECC189 | 0.71 | EL91 |
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| ECF80 | 0.56 | ELL80 | | ECF80 | 0.58 | ELL80 |
| :--- | :--- | :--- |
| ECF82 | 0.73 | EM84 | | ECF82 | 0.78 | EM84 |
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|  |  |  |  |  |  | UCL83 | 0.70 | 6V8GT | 0.45 |
| AZ1 | 0.80 | EF80 | 0.25 | PC86 | 0.60 | UP41 | 0.75 | $6 \times 4$ | 0.40 |
| AZ31 | 0.55 | EF85 | 0.85 | PC88 | 0.60 | UF89 | 0.40 | 6X5G | 0.40 |
| CBL31 | 1.00 | EF86 | 0.80 | PC97 | 0.45 | UL41 | 0.85 | $6 \times 5 \mathrm{G} 7$ | 0.45 |
| CL33 | 1.50 | EF89 | 0.88 | PC900 | 0.48 | UL84 | 0.48 | 786 | 0.76 |
| CY31 | 0.50 | EF91 | 0.37 | PCC84 | 0.40 | UY41 | 0.48 | 7B7 | 0.70 |
| DAF91 | $0 \cdot 30$ | EF92 | 0.85 | PCO88 | 0.55 | UY85 | 0.40 | 706 | 1.00 |
| DAF96 | 0.50 | EF95 | 0.40 | PCC89 | 0.50 | VR105-30 | $0 \cdot 40$ | 7C6 | 0.75 |
| DCC90 | 1.35 | EF98 | $0 \cdot 75$ | PCC189 | $0 \cdot 80$ | VH150-30 | 0.40 | 7H7 | 0.70 |
| DF91 | 0.80 | EF183 | 0.80 | PCF80 | 0.30 | OA2 | 0.40 | 7R 7 | 0.75 |
| DF96 | 0.50 | EF184 | 0.35 | PCF82 | 0.85 | OB2 | 0.40 | 787 | 2 -25 |
| DK91 | 0.45 | EL32 | 0.80 | PCF86 | 0.80 | 1R5 | 0.45 | $7{ }^{4}$ | 0.75 |
| DK92 | 0.70 | EL33 | 1.75 | PCF801 | 0.50 | 185 | 0.30 | 12AT6 | 0.40 |
| DK96 | 0.60 | EL34 | 0.50 | PCF802 | 0.50 | 1 T4 | 0.80 | 12AT7 | 0.40 |
| DLa2 | 0.40 | EL36 | 0.50 | PCF805 | 080 | 384 | 0.40 | 12AU6 | 0.45 |
| DL94 | 0.48 | EL37 | 2.95 | PCFP06 | 0.75 | 3V4 | 0.48 | 12AU7 | 0.88 |
| DL96 | 0.55 | EL41 | 0.90 | PCF808 | 0.85 | $5 \mathrm{R4GY}$ | 0.75 | 12AX7 | 0.88 |
| DY88/B7 | 0.87 | EL42 | 0.00 | PCL 82 | 0.85 | 5U4G | 0.40 | 12BA6 | 0.45 |
| DY802 | 0.87 | EL84 | 0.25 | PCL83 | 0.66 | 5 V 4 G | 0.50 | 12BE6 | 0.60 |
| EABC80 | 0.38 | EL95 | 0.85 | PCL84 | 0.45 | 5Y3GT | 0.45 | 30 Cl | 0.80 |
| EAF42 | 0.75 | ELL80 | 1.00 | PCL85 | 0.50 | 524G | 0.45 | 30 Clb | 1.05 |
| EB91 | 0.22 | EM80 | 0.45 | PCL86 | 0.45 | 8/30L2 | 0.80 | 30 Cl 7 | 1.10 |
| EBC33 | 1.00 | EM81 | 0.60 | PCL805/8 |  | 6AK5 | 0.40 | 30C18 | 0.80 |
| EBC41 | 0.75 | EM84 | $0 \cdot 35$ |  | 0.50 | 6AM5 | 0.90 | 30F5 | 1.10 |
| EBC81 | 0.88 | EM85 | 1.00 | PDS00 | 1.80 | 6AQS | 0.42 | $30 \mathrm{FL1}$ | 0.75 |
| EBF80 | 0.40 | EY51 | 0.40 | PEN45 | 0.75 | 6487\% | 0.85 | 30 FL 2 | $0 \cdot 75$ |
| EBF83 | 0-40 | EY86 | 0.40 | PL36 | 0.55 | 6AT6 | 0.98 | 30 FL 1 | 0.85 |
| EBF89 | 0.32 | EZ40 | 0.75 | PL81 | 0.50 | 6AU6 | 0.80 | 30L15 | 1.05 |
| EBL31 | 1.60 | FEZ41 | 0.75 | PL82 | 0.45 | 68A6 | 0.28 | 30L1 | 0.80 |
| ECC81 | 0.40 | E280 | 0.28 | PL83 | 0.45 | 68E6 | 0.32 | 30 LIV | . 30 |
| ECC82 | 0.38 | E281 | 0.29 | PL84 | 0.40 | 6BH6 | 0.75 | P4M | 130 |
| ECC83 | 0.38 | GY501 | 0.80 | PL500 | 0.75 | 6BJ6 | 0.85 | 30 Pl 2 | 1.05 |
| ECCO4 | 0.80 | GZ30 | 0.45 | PL504 | 0.75 | 6BQ7A | 0.65 | 30P19 | 1.00 |
| ECC8 | 0.40 | GZ32 | 0.50 | PL508 | 0.90 | $6 \mathrm{BR7}$ | 0.80 | 30PLI | 0.95 |
| ECC88 | 0.40 | Q234 | 0.60 | PL509 | 1.55 | 6887 | 1.85 | $30 \mathrm{PL1} 3$ | 1.20 |
| ECH 35 | 1.25 | GZ37 | 1.25 | PL802 | 0.95 | 68W6 | 0.90 | 30 PL 14 |  |
| ECH42 | 1.00 | HN309 | 1.50 | PX4 | 8.00 | 6BW7 | 0.80 | 30 PL 14 | 1.25 |
| ECE81 | 0.80 | K T61 | 1.75 | PX 25 | 8.00 | 6 C 4 | 0.85 | 35 W 4 | 0.40 |
| ECH83 | 0.45 | KT66 | 2.85 | PY33 | 0.62 | 6CD6 | 1.30 | 35Z4GT | 0.70 |
| ECL80 | 0.45 | KT81 ${ }^{\text {7 }}$ | ) | PY81 | 0.80 | 6CH6 | 0.80 | 50CD6G | 1.20 |
| ECL82 | 0.35 |  | 1.18 | PY82 | 0.85 | 6CW 4 | 0.70 | 807 | 050 |
| ECL89 | $0 \cdot 68$ | KT81 | 1.75 | PY83 | 0.38 | $6 \mathrm{~F}^{2} 23$ | 1.05 | 813 IT |  |
| ECLA6 | 0.40 | KT88 | 2.25 | PY88 | $0 \cdot 40$ | 6F26 | 1.00 | 813 IT | 213 |
| ECLISA00 | 2.26 | KTW61 | 100 | PY600 | 0.47 | 6 F 28 | 0.70 | 813 USSR |  |
| EF37A | 1.20 | MU14 | 1.00 | PY81/800 | 0.50 | 6J5M | 0.60 |  | ${ }^{5} 5.75$ |
| EF39 | $1 \cdot 20$ | N78 | 1.80 | PY801 | 0.50 | 6J5G | 0.45 | 866A | 0.85 |

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Each additional Valve add 2 p .

## EXPRESS

 POSTAGE3p for firat Tranalator. for each alditlenal add for

$1 p$

|  |  |  |  |
| :--- | :--- | :--- | :--- |
| AA119 | 0.7 | BD132 | 0.80 |
| AAZ13 | 0.10 | BF115 | 0.25 |
| AAZ15 | 0.10 | BF167 | 0.25 |
| AC107 | 0.35 | BF173 | 0.25 |
| AC128 | 0.25 | BF179 | 0.30 |
| AC127 | 0.25 | BF180 | 0.30 |
| AC128 | 0.25 | BF181 | 0.32 |
| AC178 | 0.25 | BF194 | 0.15 |
| AC187 | 0.25 | BF196 | 0.15 |
| AC188 | 0.25 | BF197 | 0.15 |


| 0.75 | PL84 | 0.66 | 30C15/ |  |
| :---: | :---: | :---: | :---: | :---: |
| 0.75 | PL604 | 0.88 | PCF800 | 1.08 |
| 0.45 | PL608 | 1.05 | 30 Cl 7 | 1.00 |
| 0.58 | PL509 | 1.55 | 30C18/ |  |
| 0.52 | PL802 | 0.86 | PCF80] | 0.80 |
| 0.80 | PY33 | $0 \cdot 68$ | 30F5/PF |  |
| $0 \cdot 65$ | PY81/800 | 0.50 |  | 1.10 |
| 0.85 | PY82 | 0.55 | 30FL1/ |  |
| 0.51 | PY88 | $0 \cdot 60$ | PCE800 | 0.75 |
| 1.80 | PY600A | 1.05 | 30FL2 | 0.75 |
| 0.85 | PY800 | 0.50 | 30FL12 | 1-05 |
| 0.85 | PY80] | 0.50 | 30 FLI 4 | 0.85 |
| 87 | U26 | 1.00 | 30L1/PCC84 |  |
| 65 | U101 | 1.00 | 30L1/PCC | 0.62 |
| 71 | U193 | 0.50 | 30L15/PCC805 |  |
| 0.86 | UABC80 | 0.80 | 30L15/Pし | 1.05 |
| 0.88 | UBC81 | 0.70 |  | 10.90 |
| 0.54 | UBF89 | 0.60 | $30 \mathrm{LL7}$ | 0.90 |
| . 6 | UCC8s | 0.80 | 30 P 4 MR | 1.30 |
| 0.59 | UCE81 | 1.00 | 30PI2/PC801 |  |
| 0.63 | UCL82 | 0.70 |  | 1.05 |
| 0.63 | UCL83 | 0.70 | 30P19/PC802 |  |
|  | UF89 | 0.80 |  | 1.00 |
| 0.63 | U1.84 | 0.95 | 30PL1/PCL801 |  |
| 1.55 | UY85 | 0.50 | 30PL13/ 0.08 |  |
| 0.80 | 6/30L2 |  |  |  |
| 0.88 0.75 | 6F23/EF812 |  | PCL800 | 1.20 |
| 0.88 | - 2 / | 1.05 | 30PL14/ |  |
| 0.50 | $3001 / \mathrm{PCF}$ |  | PCL88 | $1-25$ |
| 0.98 |  | 0.81 | 30PL1 ${ }^{\text {d }}$ | 1.05 |


|  | PC88 | 0.75 |
| :---: | :---: | :---: |
| 0.46 | PC97 | 0.45 |
| 1.03 | PC900 | 0.56 |
| 0.43 | PCO84 | 0.62 |
| 0.90 | PCC88 | 0.80 |
| 0.81 | PCC89 | 0.65 |
| 1.80 | PCC189 | 0.65 |
| 1.40 | PCF80 | 0.51 |
| 1.85 | PCF82 | 1.80 |
| 080 | PCF86 | 0.85 |
| 0.80 | PCF200 | 0.85 |
| $0 \cdot 58$ | PCF201 | 0.87 |
| 0.85 | PCF801 | 0.65 |
| 1.05 | PCFP02 | 0.71 |
| 0.00 | PCF806 | 0.86 |
| 0.47 | PCH200 | 0.88 |
| 0.55 | PCL82 | 0.54 |
| 0.95 | PCL83 | 0.68 |
| $0 \cdot 70$ | PCL84 | 0.50 |
| $1-81$ | PCL8S | 0.63 |
| 2.30 | PCL86 | 0.63 |
| 1.18 | PCL805/85 |  |
| 1.18 |  | 0.63 |
| 0.88 | PD500 | 1.55 |
| 0.42 | PFL200 | 0.80 |
| 0-64 | PL36 | 0.88 |
| 0.51 | PL8I | 0.75 |
| 0.40 | PL81A | 0.88 |
| 0.90 | PL82 | 0.50 |
| 0.78 | PL83 | 0.96 |

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| 0 Cl 6 | 0.76 | ZTX 500 | 0-15 | 2 N 2646 |
| :---: | :---: | :---: | :---: | :---: |
| OC20 | 0.95 | ZTX 601 | 0.16 | 2N2904 |
| OC23 | 0.85 | ZTX 503 | 0-17 | 2N2904A |
| OC25 | 0.40 | ZTX531 | 0.20 | 2N2905 |
| OC28 | 0.85 | ZTX 550 | 0.20 | 2N2906 ${ }^{\text {A }}$ |
| OC35 | 0.80 | IN914 | 0.7 | 2N2906 |
| OC36 | 0.88 | IN 4001 | 0.6 | 2N 2928 |
| $0 \mathrm{C42}$ | 0.40 | IN 4002 | 0.7 | 2N3053 |
| $0 \mathrm{C44}$ | 0.15 | IN4003 | 0.8 | 2N3055 |
| OC48 | 0.15 | IN4004 | 0.8 | 2N3525 |
| OC71 | 0.15 | IN 4005 | 0.10 | 2N3614 |
| 0 C 72 | 0.25 | IN4006 | 0.12 | 2N3815 |
| OC76 | 0.40 | IN4007 | 0.15 | 2N3702 |
| 0 C 77 | 0.45 | IN4009 | 0.5 | 2N3703 |
| $0 \mathrm{C81}$ | 0.95 | IN4148 | 0.8 | 2N3704 |
| OC8ID | 0.25 | 18921 | $0 \cdot 10$ | 2N3708 |
| OC812 | 0.55 | 182039 | 0.20 | 2N3706 |
| $0 \mathrm{C83}$ | 0.25 | 182051A | 0.20 | 2N3707 |
| OC140 | 0.55 | 182100A | 0.20 | 2N3708 |
| OC170 | 0.25 | 183010 | 0.25 | 2N3709 |
| OC171 | 0.80 | 2N698 | 0.15 | 2N3710 |
| OC200 | 0.45 | 2N697 | 0.18 | 2N3711 |
| OC201 | 0.75 | 2N70¢ | $0 \cdot 10$ | 2N3819 |
| OC202 | 0.80 | 2N706A | 0.12 | 2N3820 |
| OC203 | 0.50 | 2N1131 | 0.25 | 2N3823 |
| 0CP71 | 1.25 | 2N1132 | 0.85 | 2N3903 |
| ORP12 | 0.50 | 2N1302 | 0.18 | 2N3904 |
| ORP60 | 0.40 | 2N1303 | 0.10 | 2N3905 |
| T1005 | 0.30 | 2N1304 | 0.28 | 2N3906 |
| TIC44 | 0.85 | 2N1305 | 0.82 | 2N4088 |
| TIC226D | 1.50 | 2N1304 | 0.82 | 2N4050 |
| T1L209 | $0 \cdot 30$ | 2N1307 | 0.25 | 2N4060 |
| TIS43 | 0.85 | 2N1308 | 0.25 | 2N4061 |
| ZTX107 | 0.15 | 2N1309 | 0.87 | 2N4002 |
| 2TX108 | 0.12 | 2N1813 | 0.80 | 3NI41 |
| 2TX300 | 0-12 | 2N1614 | 0.20 | 40360 |
| ZTX 301 | 0.15 | 2N2147 | 0.75 | 40361 |
| 2TX302 | 0.18 | 2N2160 | 0.59 | 10382 |
| ZTX304 | 0.25 | 2N2369A | 0.15 | 40430 |


| 400 | 0.20 | BN7425 | $0 \cdot 48$ | SN7473 | - | 7 |  | 157 | 1.80 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BN7401 | 0.20 | BN7427 | 0.42 | EN7474 | 0.40 | BN74110 | 0.80 | SN74170 | 410 |
| 8N7402 | 0.20 | BN7428 | 0.60 | EN7475 | 0.65 | 8N74111 | 1.48 | 8×74174 | 8.00 |
| BN7403 | $0 \cdot 20$ | 8N7430 | 0.20 | EN7476 | 0.45 | GN74118 | 1.00 | BN74176 | 1.85 |
| 9N7404 | $0 \cdot 20$ | BN7432 | 0.48 | BN7480 | 0.80 | 8N74119 | 1.90 | 6N74176 | 1.60 |
| 8N7405 | 0.80 | 8N7433 | 0.70 | SN7482 | 0.87 | BN74121 | 0.80 | 8N74190 | 1.88 |
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| EN7409 | 0.45 | gN7441. |  | SN7490 | 0.75 | BN74146 | 1.50 | BN74194 | 2.50 |
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| EN7411 | 0.28 | BN7442 | 0.75 |  | 100 | BN74181 | 1.10 | BN74196 | 1.80 |
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| EN7413 | 0.80 | BN745I | 0.20 | BN7493 | 0.75 | BN74155 | 1.55 | GN75198 | 4.60 |
| 8N7416 | 0.30 | 6N7453 | 0.20 | BN7494 | 0.80 | EN74156 | 1.85 | SN74199 | -60 |
| EN7417 | 0.30 | BN7454 | 0.20 | BN7495 | 0.80 |  |  |  |  |
| BN7420 | 0.20 | SN7460 | 0.20 | 8N7496 | 1.00 | DIL |  |  |  |
| 8N7422 | 0.48 | 8N7470 | 0.30 | 8N7497 | 6.85 |  |  |  |  |
| 6N7423 | 0.48 | SN7472 | 0.30 | BN74100 | 2.50 |  |  | 6 pi | P |

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IF you were fortunate enough to obtain last month's special issue of Practical Wireless, and your particular interests are in audio, short wave, broadcast reception, test equipment, or experimental electronics, you will have found at least one item of interest to you. In very general terms, this is what Practical Wireless is about, helping and encouraging its readers to have-a-go. This issue is also special in that it is the largest $P . W$. ever produced, carrying 120 pages and two free colour Datacards.

Activities covered by this magazine are, believe it or not, of a seasonal nature and we are always delighted in one sense when the holiday season ends, because we all settle down again after sun-tan(?) and surf-riding to renew our absorbing interest in d.i.y. radio and electronics.

It was often the case in the past when we would expect readers who go away in the summer to leave their tools and $P$.W. at home. Imagine some reader on the Costa Brava wielding a soldering iron on a pair of gritty output transistors-it's just not done is it? We were particularly pleased therefore that the temporary summer recess this year was hardly noticeable; surely the summer was not that bad! And it is known that P.W. is read on beaches.

The autumn, therefore, is just the time when, if not already bitten by the bug, our readers look around as if to court the means to satisfy their instinctive curiosity in the techniques of working circuits. You might say that we also provide the necessary bait to give newcomers encouragement to have a go. You might be right, but then if we did not learn something about our readers we would not be the highest selling British magazine of its kind. Some subjects do come up for renewed treatment but unlike some magazines, they are seldom in the same guise as before.

Take our Metal Detector on page 634; not a scrap like the earlier models and certainly easier to make.

October is also the time for the London Audio Fair; it is natural therefore that those readers who will be going to Olympia will want to sort out some of the technical jargon used in the audio world. Very sad that we cannot be there this year so we expect every P.W. reader visitor to carry this issue in his pocket, so that he can refer to the extra supplement which we have bound in the centre.

Incidentally, we have heard rumour on the "grape vine" that a certain company is biting its tongue for not having published a multi-systems quad matrix decoder as simple as ours.
M. A. COWELL—Editor.


## Paris Component Show

MEASURING instruments will be featured in addition to the usual sections on electronic components, materials, equipment and pro ducts at the Paris Component Show.

Venue is Exhibition Park, Porte de Versailles and date 1st-6th April 1974

## Mullard back out

MULLARD Ltd. have decided to kill off their Educational Service. The service has acted as a valuable aid for the teaching profession for the last 25 years.

## Oxidising agent

ENTHONE Inc. Ebonol C Special is an oxidising agent which increases the strength of the bond in the production of single, double-sided and multi-layer printed circuit boards. The process involves producing many thousands of little cupric oxide needles. The oxide coating is obtained by the immersion of suitably treated copper in a solution of $180 \mathrm{gm} / 1$ Ebonol C at $104^{\circ} \mathrm{C}$

Liquid adhesive may then be brushed or rolled onto the oxidised surface. After the adhesive has "cured" the imbedded needles of cupric oxide maintain a "key", firmly fixing the adhesive to the copper. The prepared copper foil is then affixed to the plastics base.


We settle down when the holiday season ends...

## Packaging for professionals

THE Inter-Nepcon conference at Brighton specialises in broad terms in electronic component packaging and assembly. There is a very strong emphasis on printed circuit techniques and integrated circuit encapsulation.

Although not strictly dealing with electronics techniques, this exhibition has a distinctly practical emphasis because it concerns the making of component assemblies and modules. It is being held at the Metropole Hotel on the sea-front at Brighton, from 16th to 18th October and is organised on an international basis by Kiver Communications Ltd of 149-155 Ewell Road, Surbiton, Surrey. Admission is restricted to those who register as being engaged full-time in electronic circuit packaging and production.

## No more please!

With the Audio Fair about to open its doors on 22nd October (trade only), and 23 rd October to the public, it is interesting to learn that one famous British manufacturer, Armstrong Audio, has had to withdraw because it could not contemplate at present the thought of taking on more orders. It seems that the new 600 series has created so much interest that current orders exceed their present manufacturing capacity.

Rather than spend time and money in exhibiting with the prospect of more orders, Armstrong have decided that they should expand their facilities to cope with the rush.

## Multimeter competition

WE wish to apologise to readers for the omission of information in last month's issue on the Digital multimeter competition. Due to the fact that so many readers sent in answers that were the best according to the considered opinion of the judges, our Competitions Department is at present organising a further contest for these readers. We will be publishing the result just as soon as we have it.

## Derby modellers gel together

D
ERBY and District Amateur Radio Society (G3ERD, G2DJ) are branching into radio control models. The new club is already under way and held its first meeting in September. Anyone interested should contact Ray Webster, č\% 5 Uplands Avenue, Littleover, Derby.

## Slimline digital multimeter

Oand polarity indication.

The heart of the instrument is a "postage-stamp" size thin film hybrid circuit with analogue and digital processing. It is claimed to measure d.c. voltage from $0 \cdot 1 \mathrm{mV}$ to 500 V and a.c. voltages from 3 mV to 500 V . The resistance range measures from 1 ohm to $10 \mathrm{M} \Omega$. The input resistance is stated as $10 \mathrm{M} \Omega$.

## Cassette library system

WITH the current boom in tape cassette recorders, BASF are to show at the Audio Fair two new machines for chromium dioxide tape and a (quote) "unique library system for cassettes", that can be free standing or fitted to the wall.

## BIB's own set-up

MULTICORE Solders Ltd. have set up a subsidiary company, BIB Hi - Fi Accessories Ltd., to look after the interests of growing range of products with the "BIB" trade name, including record and tape cleaning accessories and splicing kits. The board of the new company is selected from the parent company and will continue to operate from P.O. Box 78, Hemel Hempstead, Herts, HP2 7EP.

## Ham Exhibition

THE Midland National Amateur Radio and Electronics Exhibition will be held at the Granby Halls, Leicester from 25th to 27 th October.

## Commercials date

$\boldsymbol{A}^{\mathrm{T}}$ the time of going to press, we have heard that
the London Broadcasting Company will go on the air on Monday 8th October. There will be a special message from the Minister of Posts and Telecommunications. Frequencies 719 kHz , 417 m and $97 \cdot 3 \mathrm{MHz}$. F professional quality, this unusual device is a hand-held digital multimeter from Hewlett-Packard. At £138 (+VAT) this instrument represents a valuable on-line tool for engineers and technicians. A $3_{2}$ digit l.e.d. display uses automatic decimal placement


SUPER-REGENERATIVE receivers may use a simple and easily built circuit, and are highly sensitive. There are no gauging or other alignment problems, and frequency coverage is easily modified. A straightforward circuit of this type is thus completely practical, as an alternative to a complicated v.h.f. superhet, or v.h.f. converter used with a short wave receiver.

On the other hand, the disadvantages of the superregenerative type of circuit should be remembered. One is the lack of selectivity, and another the background hiss which is present when no transmission is tuned in. The lack of selectivity means that a strong, local transmission can prevent reception of a weaker signal on a nearby frequency. The stronger signals are, however, very well received, and any signal which is received at sufficient strength will automatically quiet the background hiss.

A further important point is the extent to which a super-regenerative receiver can cause interference to other receivers. Some radiation of this kind seems unavoidable, but it can be kept within limits by screening the receiver, and using an r.f. stage to help isolate the aerial from the oscillating detector stage. In these circumstances, interference is not caused over a wide area.

Interference is primarily caused on the frequency to which the super-regenerative receiver is tuned, and nearby frequencies. As example, if an unscreened super-regenerative receiver is tuned to 144 MHz this is found to cause no interference at all to a normal receiver in the $88-108 \mathrm{MHz}$ range, with the equipment side by side. On the other hand, interference wou, 1 arise with nearby receivers tuned to 144 MHz or $\mathrm{ad}_{J}$ acent frequencies.

This really means that the super-regenerative receiver should be confined to use in those circumstances where other people are not listening on the same or a near-by frequency. In fact, the receiver described has often been used as the only means of reception for 2 metre amateur band contacts, without any complaint. This does not mean, however, that it would be wise to use it for 2 metre reception when there are other 2 metre receivers or converters in use nearby.


## Receiver circuit

This is shown in Fig. 1. Though actually constructed for 2 metre reception as a portable, it can be used over the 90 MHz to 150 MHz range without any change other than re-adjusting the preset trimmer TC1. Trl is the untuned r.f. stage, with input to the source across the source bias resistor R1. A tuned r.f. stage increases gain, but has to be screened from the detector, and also requires its own means of tuning, unless a small frequency band is adopted. The main purpose of this stage is to reduce radiation caused by coupling an aerial directly to the detector coil L2. The r.f. stage does not provide complete isolation, due to the internal capacitance of Tr1 and other unwanted coupling through leads.
$\operatorname{Tr} 2$ is the detector. The operating frequency depends on the coil L2, trimmer TC1; and VC1. There are of course no alignment adjustments at all. With TC1 fully open, VC1 tuned approximately $130-150 \mathrm{MHz}$. Super-regeneration is maintained until TCl is about two-thirds closed, giving a low frequency limit of about 90 MHz . For lower frequencies it would be necessary to increase the number of turns on L2. The upper limit at which the receiver can be made to operate is largely determined by Tr2.

Regeneration is controlled by VR1, and it is recommended that the values shown for C4, C6, R4 and R5 are as shown, though VR1 can equally well be $20 \mathrm{k} \Omega$ or $25 \mathrm{k} \Omega$. TC2 from source to drain allows


Fig. 1: Complete circuit of the portable v.h.f. receiver.
adjustment of regeneration, and was found of advantage with various transistors employed for Tr2.

A detector of this type is usually considered to have a sensitivity of about $0.5 \mu \mathrm{~V}$, which offers a useful range with a simple aerial.
$\operatorname{Tr} 3$ is an audio amplifier, followed by the i.c, which contains six transistors in a driver-push-pull arrangement. This gives reasonable loudspeaker volume from the internal miniature speaker. The receiver is free from troublesome hand capacity effects, if constructed as shown.

## Circuit board

This is plain Veroboard, $0 \cdot 15 \mathrm{in}$. matrix, and is approximately $2^{5}{ }_{8} \times 3^{1} 4 \mathrm{in}$., see Fig. 2. The detector stage is assembled in close proximity to VCl.

L2 is self-supporting, and is wound with 18 or $16 \mathrm{~s} . \mathrm{w} . g$. wire, with an outside diameter of $\mathrm{l}_{2} \mathrm{in}$. The coil is approximately ${ }_{4} \mathrm{in}$. long, and its ends are shaped so that they may be soldered to the fixed plates tag of VCl , and to $\mathrm{C} 2 . \mathrm{C} 2$ has the shortest possible leads each end. A stout wire supports TCl just clear of the plates of VCl , and the outer tag A of TCl is bent down and soldered to L 2 as shown. L1 is 2 turns of insulated wire near L2, and is soldered to two Veropins.

Coverage can be modified to some extent by stretching L2, or by compressing it so that the turns are closer together. For the coverage mentioned, four turns are used. The coil should be at least ${ }^{1}{ }_{2}$ in. from the metal case.

A small 3-lead holder is fitted for $\operatorname{Tr} 2$, and is of

Fig. 2: Component layout on the circult board.

advantage in allowing this transistor to be changed readily. TC2 and the holder can be soldered almost directly together and to VC1. A stout lead, just clear of VCl moving plates, runs to the rotor tag with C2.
The r.f. choke is self-supporting, and is wound with 22 s.w.g. enamelled wire. It has 35 turns and is 0.3 in . outside diameter. Wind the turns side by side on a suitable object, which is then removed. The ends are scraped and tinned, and soldered to $\operatorname{Tr} 2$ source at the holder, and to a Veropin adjacent to R5.

When inserting $\operatorname{Tr} 2$, always take care that it is placed the correct way, so that leads come as in Fig. 2.

## Underside wiring

A lead passes through the board from VCl rotor, forming the negative line, as in Fig. 3. The metal case or bush of VR1 is grounded by a lead under the control or its fixing nut, Fig. 2.

The resistors and capacitors can then be inserted as in Fig. 2, and connected as in Fig. 3. Place insulated sleeving on leads where required, and keep all the leads and joints close against the board. Here, there will be a clearance of about ${ }_{16} \mathrm{in}$. from the metal panel, so there is no real danger of shorts to the metal if joints are made neatly and excess wire snipped off close to the board.

The i.c. has two long tags, and two short tags, and will fit the matrix of the Veroboard when placed as in Fig. 2. Leads are soldered to the projecting pins underneath, as in Fig. 3.

Solder a black flexible lead to S1, Fig. 2, and fit this with a negative battery clip. A red lead with a positive clip passes through the board to the positive circuit for C10.

A short wire runs from R1, as in Fig. 2, and is later soldered to a tag for the aerial connection. Also bring out leads from C9 and the negative line, for the loudspeaker.

## Metal panel

For the $6 \times 4 \times 2 \mathrm{in}$. universal chassis box, this is $6 \times 4 \mathrm{in}$. The dimensions could be modified to suit a different case.

A $1^{3}{ }_{4} \mathrm{in}$. hole is punched for a 2 in . or $2^{1}{ }_{4} \mathrm{in}$. speaker. A piece of perforated metal is fixed across the opening inside with adhesive, and the miniature

speaker is fixed with more adhesive. Though the speaker is $40 \Omega$, a 75 or $80 \Omega$ unit can be fitted with almost similar results, though the best impedance for the i.c. is in the 15 to $40 \Omega$ range.

Washers are put on the bush of VCl to space the insulated board from the metal panel, and these are then secured together with the capacitor nut. Check that all joints etc. are clear of the metal.

## Final assembly

The receiver should be tested and adjusted before filting it in its case. The box is assembled with 413 A bolts through the holes punched in its flanges, and the panel is fixed with 6BA bolts or self-tapping screws.
A 34in. telescopic aerial is used, bolted to the side of the box near R1, but insulated from the metal. This is done by using insulated washers and bushes, or insulated washers and pieces of sleeving on the bolls. One bolt carries a tag, for the aerial lead mentioned.
The battery rests in the bottom of the box, and folded card can be put round it and between battery and speaker. There must be no contact between the battery clips and metal case.

For 2 metre reception, a ${ }^{1}$-wave aerial is around 19 to 20 inches. But it was found that the exact length of the aerial was not important, there being no noticeable change in volume when changing this

## $\star$ components list


from about 20 in . to 30 in . or so. Some strong transmissions were received with the aerial completely closed.
In many cases it is better to have the aerial sloping or near horizontal, but with a hand-held receiver of this sort it is easy to move around to find the best position for the aerial, if needed.
Indoors, reception is modified by the proximity of objecis such as metal windows. On a few occasions an outdoor dipole, with a co-axial feeder, has been connected, and this naturally increased range.

## Adjustment

Both TCl and TC 2 may be fully unscrewed, for about $\quad 130-150 \mathrm{MHz}$. (Exacl coverage naturally depends on Ll and other factors, but is likely to be near this.)

When VR1 is rotated to switch on, a point should be reached where a loud hiss commences. This is the poinc where super-regencration, upon which sensitivity depends, has commenced. No reception is possible if this is not obtained. Should superregeneration be absent, TC2 may need screwing down slightly. A setting should be found where super-regeneration continues over the whole band tuned by VC1, with only a little re-adjustment of VR1.

When a signal is tuned in, this hiss should cease. Strong signals will produce this effect with most settings of VR1 which permit super-regeneration; but with weak signals VRI may have to be backed off slightly.
L1 should be quite near L2, but if coupling is very tight this may prevent regeneration in some circumstances. It is possible to boost volume by using more turns on L1 so that it is broadly selfresonant at the wanted frequency. However. this adjustment is fairly touchy. Ll may be unsoldered from the pins, and a new winding may be fitted, with a minimum of disturbance.
If all connections are short and direct, and no fault is present, the absence of super-regeneration can only arise from Tr 2 being inefficient at the frequency wanted. Of several quite inexpensive transistors tried here, one failed to operate at any frequency higher than about 100 MHz , while another continued to provide regeneration at over 200 MHz . As $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$ are of the same type, the transistor found to give best regeneration may be used for Tr 2 . Its leads need not be cut down. This test can be made with the aerial temporarily taken to the drain pin of L1.

It is in order to use a 4.5 pF or 5 pF capacitor at VCl , if a narrower band is required, or to fit a 15 pF capacitor for a larger band. The overall drain of the receiver is about $10-20 \mathrm{~mA}$, depending on volume.
The amount of activity on these frequencies varies very considerably in different areas, being least in some isolated parts of the country. Amateur activity on the 2 metre band is most likely at certain times at weekends. It may be considerable during v.h.f. contests, while at other times no stations may be operating. Any amateur in the 2 metre band (144146 MHz ) will provide a tuning calibration point which can be noted as a guide for future reference when listening.

# $1+1$ <br>  L.A.J.IRELAND 

Asimple requirement whose realisation in practice can be rather difficult is the tunable audio oscillator with an accurate sine waveform. At frequencies below 20 kHz the use of inductive tuned circuits is not practical and the most commonly used circuit is the Wien bridge using RC circuits to determine the time constant of the oscillator feedback loop. The impedance of such a circuit is, of course, frequency dependent; the loop gain therefore also tends to be frequency dependent, with the result that the circuit can produce some variation in waveform and amplitude as the operating frequency is varied.

Any departure from a true sine waveform, such as the square wave produced by an oscillator with excessive loop gain, contains harmonics or overtones of the fundamental frequency and is therefore unsuitable for many applications such as the determination of the frequency response of an audio system. Various improvements on the basic Wien bridge circuit have been introduced to overcome these defects, such as the incorporation of an AGC loop with a thermistor to regulate gain.

## Op Amp + Comparitor

This month, however, a completely different approach is outlined, one first introduced by engineers of the National Semiconductor Corp. and employing two integrated circuits. One of these is an operational amplifier, the other a voltage comparator. The standard application of a voltage comparator unit is as a sensing element, operating a relay or switching the state of a logic circuit on the application of a low level input signal.

## Operation

In the oscillator circuit to be described, it is accepted that the output of a comparator will alternate between extreme values irrespective of the waveform of the input signal. If, then, the inpui signal has a fixed period, the output of the comparator will be a square wave with that period and a fixed amplitude. With effective filtering to remove


| $C 1$ and C 2 | Frequency range |
| :---: | :---: |
| $0.47 \mu \mathrm{~F}$ | $18 \mathrm{~Hz}-80 \mathrm{~Hz}$ |
| $0.1 \mu \mathrm{~F}$ | $80 \mathrm{~Hz}-380 \mathrm{~Hz}$ |
| $0.022 \mu \mathrm{~F}$ | $380 \mathrm{~Hz}-1.7 \mathrm{kHz}$ |
| $0.0047 \mu \mathrm{~F}$ | $1.7 \mathrm{kHz}-8 \mathrm{kHz}$ |
| $0.002 \mu \mathrm{~F}$ | $4.4 \mathrm{kHz}-20 \mathrm{kHz}$ |

[^7]harmonics, a sine wave of fixed amplitude will remain. The filter in question is in this case an active` filter incorporating an operational amplifier integrated circuit, with its centre frequency determined by an RC network. In turn, the output of the filter provides the input signal for the voltage comparator, thereby closing the oscillator feedback loop. It is clear that two separate waveforms are available from the oscillator, both stabilised in amplitude and locked together in frequency and phase; a square wave at the output of the voltage comparator, and a sine wave at the output of the operational amplifier.

## Simplified Tuning

There is the further advantage that the frequency is set by a single variable resistor, whereas the Wien oscillator requires matched ganged tuning elements. The audio range from 18 Hz to 20 kHz is covered in five bands with band switching achieved by changing the capacitive elements in the tuned filter. The limitation on the frequency range covered with any given pair of capacitors is applied by the rise in harmonic distortion to some $2 \%$ at the maximum value of R3. Further, the principle is not applicable to the construction of RF signal generators since a sufficiently high Q is not available without the use of inductors.

## Construction

In construction of these oscillators, however, some care is necessary to follow good high frequency design practice, since the individual IC's are wide
bandwidth devices. Careless construction could therefore lead to an oscillator with RF instability, and plagued by parasitic oscillations. Both power supply lines, therefore, should be decoupled by $0.1 \mu \mathrm{~F}$ disc ceramic capacitors. Further, the output of the comparator should be shielded from the op amp input, to ensure that the only feedback occurs via the intended filtered loop.

## Radio Control

For those interested in radio control techniques, it can be seen that a simple modification to the circuit can produce a frequency-operated switch. If the operational amplifier and associated tuned circuit are examined alone, it is clear that an output signal is produced only if the input applied via R2 contains a component at the resonant frequency. That output signal can then be detected by a conventional diode, and the resultant DC level applied to the voltage comparator, thereby operating a relay. Such a system therefore would function on the presence or otherwise of an appropriate AF modulation on a radio control signal.
The National Semiconductors devices are available from: ITT Electronic Services, Edinburgh Way, Harlow, Essex.

The LM101A and LM111 are manufactured to military specifications and therefore somewhat expensive. The 'civilian' equivalents LM301A and LM311 are very much cheaper and should perform quite adequately in this application (Technical Editor).


## ACROSS

## DOWN

2 It has an angle in radio communication (7) All-rounders in coil protection (7) Yes, relay equipment is connected (3) Invitation to part of a French meal? (6) Took a pitch from the animal within? (5) Expression of effective forcefulness (7) A piece of cake in ionization? (5) Too much connection with 25 Across? (7) A circuit may do so, of course (5) Good reception for a type like Rod? (7) Crew formation for co-ordinating adjustment? (7) Revolvers instead of maps for world travellers (6) Aches so about a mere game? (5) Network of transatlantic origin (1, 1, 1)


## GORDON KING <br> PART 3

## AERIAL DESIGN

Accurate design of good FM aerials of multielement composition is complex, and since very good FM aerials of all types are readily available at quite reasonable prices it hardly pays the enthusiast these days to tailor his own design. Discarded television aerials as they stand are useless for FM since their tuned frequency is all wrong. However, it is sometimes possible to make use of some of the components of such aerials in the construction of an FM aerial. The elements and crossboom of a Band I aerial can be cut down to tune Band II, and the insulator at the dipole and other fitments can often be used to advantage. There is no 'standard' design; the absolute dimensions of the elements and their spacings determine the overall bandwidth, the nature of the polar diagram and the correct impedance matching to the feeder over the bandwidth.


Fig. 7: General construction of a folded dipole which can be used by itself or form the basis of a mult-element aerial.

A simple dipole has a centre impedance of about 72 ohms and thus closely matches 72 ohm coaxial feeder, this being necessary for maximum energy transfer from the aerial to the receiver or tuner. However, when the simple dipole is advanced into a multi-element array by the addition of parasitic elements the impedance at the centre of the dipole falls and some artifice has to be employed to increase the coupling impedance to a value matching the feeder.

One such artifice is 'folding' the dipole, as shown in Fig. 7. This quadruples the impedance at the
feeder connecting point, increasing it to about 300 ohms in the simple case. However, when a reflector and directors are added the centre impedance of a simple dipole falls to abou't 24 ohms, so by folding the dipole as shown in Fig. 7 the coupling impedance is restored to about 72 ohms.

## HOME-MADE AERIAL

Fig. 8 gives the dimensions for a home-made fourelement array which will respond pretty well over the whole of Band II. The dipole can be folded as shown in Fig. 7 and 72 ohm coaxial feeder should be used. Notice that the reflector is slightly longer than the dipole and that the directors are shorter. Additional directors can be used, the third then being 4 ft . 3 in . and the fourth 4 ft . with 1 ft . 7 in . spacing.

It should be noted that the element dimensions correspond to length plus diameter, so if they are


Fig. 8: Dimensions for a four element beam using a folded dipole as shown in Fig. 7.

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#### Abstract

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| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| AF115 | 20p | BC187 | 22p | BUY2 | 20p | 2N3702 | 13p | ZTX 108 | 15p |
| AF116 | 20p | RD 13105 | 225p | 2N3703 | 12p | ZTX300 | 15p |  |  | 


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| BZY10 | B00V | 6 A | 25p | OA90 | $5 p$ |
| BZYI3 | 200 V | 6A | 20p | OA91 | $5 p$ |
| IN400\| | 50 V | IA | 7 p | OA202 | $7 p$ |
| IN4004 | 400V | 1 A | 8 p | IN4\| 48 | 5p |
| $1 N_{4007}$ | 1000 V | IA | 10p | BAll4 | 8 p |

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$\begin{array}{lr}22 \mu \mathrm{~F} & 16 \mathrm{~V} \\ 33 \mu \mathrm{~F} & 10 \mathrm{~V} \\ 47 \mu \mathrm{~F} & 6.3 \mathrm{~V}\end{array}$


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A commercial version of a four element array for FM (J-Beam Aerials Ltd.),
composed of, say, ${ }_{2}{ }_{2} \mathrm{in}$. rod the actual lengths are all ${ }_{2}{ }_{2}$ in. less than given on the diagram. The spacings are taken from the centre axis of each rod or element.

## INPUT MATCHING

Most British receivers and tuners destined for the British market have aerial inputs suitable for 72 ohm ' coaxial cable (the British 'standard'). Some imported receivers and tuners have inputs for both 72 ohms coaxial (which is unbalanced) and $240 / 300$ ohms balanced twin feeder, used in European areas and American countries. There are times, however, when the receiver or tuner has only a $240 / 300 \mathrm{ohm}$ balanced input. By connecting the British standard coaxial cable direct to such an input results in a mismatch and hence loss of signal energy transfer.


Fig. 9: A useful'dodge' to perm/t feeding a balanced input with unbalanced coaxial cable.


Fig. 10: An alternative method of feeding unbalanced coaxial cable to a balanced input circuit.

In quite a few cases like this it is possible to achieve matching to coaxial cable by connecting the inner conductor to one of the $240 / 300$ ohm sockets or terminals and the braid to an adjacent earth terminal or to the metal part of the chassis (Important: this must never be done if the receiver is of the 'a.c./d.c.' type which uses no mains transformer for isolation; if in doubt consult a qualified dealer or technician), as shown in Fig. 9.

This matching results from the centre-tapped winding on the primary of the aerial input transformer, giving a $4: 1$ impedance transformation since the turns ratio is $2: 1$.

Should the 300 ohm balanced aerial input circuit of the receiver or tuner be unsuitable for matching this way, then an external impedance matching transformer must be used for the best results. A simple coaxial cable transformer arrangement is shown in Fig. 10. It is also possible to obtain commercially small low-loss balun transformers using ferrite cores.


A multi-element FM aerial can be an awkward brutel Erection of these arrays Is best left to the experts (R. Smith Aerials, Luton).

## INPUT OVERLOAD

When a tuner or receiver is used very close to a powerful station the input stages may be unable to accommodate the multiplicity of strong signals


Fig. 11: Overloading of input circuits can cause all hinds of strange noises on FM. Suitable signal attenuators can be constructed using the above formulae.
without overloading. This is manifested by spurious signals appearing at incorrect tuning points over the scale, and intermodulation may occur between the various programmes.

This trouble can also incite a 'warbling' type of interference on stereo. The solution to the problem is to reduce the level (attenuate) the signal from the aerial to the receiver or tuner. A less elaborate indoor aerial may reduce the signal input, but in some cases this could be undesirable, notably when


The lower mast carries a fixed TV array plus a Stolle rotator for the Arrow 7 FM beam above ( $R$. Smith Aerials, Luton).
a directional aerial is used to reduce distortion due to reflected signals (Fig. 6).

Plug-in coaxial attenuators in a range of values are obtainable from dealers, and there is a similar type available with adjustable attenuation values. Alternatively, it is not a difficult matter to make one's own attenuators for unbalanced circuits, as shown in Fig. 11. The resistors, which should be of non-iriductive type (i.e., cracked carbon), can be mounted in a discarded tobacco tin, using the tin itself as the 'earthy' circuit.

Overloading can also occur under certain conditions at distances of twenty or more miles from a station at elevated sites with open aspects towards the station. It is likely that more overloading problems will occur when the FM commercial stations go on the air, for these may not be co-sited with the regular BBC stations and thus could introduce heavy signal fields in areas where only moderate signals are present' from the BBC stations.
In some cases like this it may be necessary to use frequency-selection attenuation adjusted only to the frequency of the powerful offending station, but this is another story which will be examined in greater detail when the time comes.

## IAEVSH11

## NOVEMBER ISSUE

## TEST SIGNAL EXTRACTOR UNIT

Quite a few test signals are present on the lines transmitted during the field flyback period. These sometimes include experimental Ceefax (BBC) or Oracle (IBA) data transmissions. The lines carrying these test or data signals should not normally be seen since they should appear above the top of the picture. They can be observed however by reducing the setting of the height control. An oscilloscope can be used to display such signals if it has facilities for strobing out particular lines. The test signals themselves are not particularly helpful for general servicing but the ability to strobe out lines can be invaluable for colour servicing since this makes the standard colour bar pattern present at the top of Test Card F available for signal tracing in PAL decoders. The unit featured next month can be used as an economical add-on unit for scopes without strobing facilities and in addition provides good, clean line and field sync pulse outputs.

## TACKLING STICKY FAULTS

Most fault-finding is reasonably straightforward, a matter of clear symptoms and obvious causes. Every engineer has his ration of faults that seem to defy analysis however. There are nevertheless some common mechanisms by which these arise and a number of ways in which a goodly proportion of them can be cleared up without the need to spend hours delving into the "unknown". Next month Vivian Capel describes various steps which can provide a short-cut to solving the more obscure types of fault.

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| AF114 | 12p | BFY50 | 22p | 2N2926O | $9{ }^{\text {p }}$ | IN4004 | 7 p | 14\&16pin 15p |
| AF115 | 22p | BFY51 | 22p | 2N2926V | 9p | IN4005 | 7 p | ZENER |
| AF116 | 12p | OC26 | 40p | 2N2926G | 10p | IN4006 | ${ }^{\text {p }}$ | DIODES |
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$0.02 \mu \mathrm{~F}, 3 \mathrm{p} ; 0.033 \mu \mathrm{~F}, 0.047 \mu \mathrm{~F}, 0.068 \mu \mathrm{~F}, 3 \frac{1}{2} \mathrm{p} ; 0.1 \mu \mathrm{~F}, 4 \mathrm{p} ; 0.15 \mu \mathrm{~F}$ p; $0.22 \mu \mathrm{~F}, 0.33 \mu \mathrm{~F}, 5 \mathrm{p} ; 0.47 \mu \mathrm{~F}, 7 \mathrm{p} ; 0.68 \mu \mathrm{~F}, 10 \mathrm{p} ; 1.0 \mu \mathrm{~F}, 11 \mathrm{p}$

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| :---: | :---: | :---: | :---: |
| $1 \mathrm{k} \Omega-2 \mathrm{M} \Omega$ Singie gang | 12p |  |  |
| $5 \mathrm{~K} \Omega-2 \mathrm{M} \Omega$ s/gang w/switch | 24p | KNOB |  |
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The equally minute IF units at the top of the photograph include the MFH51T mechanical filter and its matching transformer type YXE10857 which together cost around $£ 1 \cdot 50$. The filter is available in 4, 5 and 7 kHz bandwidths $(5 \mathrm{kHz})$ versions being readily available at the moment. The CFU455C and CFT455B are also shown in the group, these being ceramic filters centred on 455 kHz . Details and current prices from Ambit International, 37 High Street, Brentwood, Essex.

## DIGITAL CLOCK

Fonadek have introduced their Copal 602 clock. It shows the day, date and time in white numerals and there is a small fluorescent tube built in which illuminates the digits. The cabinet is finished in simulated Brazilian rosewood and the unit is priced at $£ 15 \cdot 95$ including VAT. Fonadek International Ltd., Harbòrne, Birmingham B17 9JS.


## AMATEUR RADIO AWARDS

This new book from the R.S.G.B. compiled by the Society's HF Awards Manager contains details of the world's major awards, where and how to apply for them and illustrations of a number of the certificates.

## USEFUL FASTENERS

Hedlock II fasteners are the latest from 3M. They consist of interlocking "twin" parts which just push together to give a strong bond. They can be screwed to two surfaces, ie: car parcel shelf and speaker (see picture), and make a good push fit. A sharp tug releases the fasteners. $3 M$. United Kingdom Limited, $3 M$ House, Wigmore Street, London W1A. $1 E T$.


## 20 MHz COUNTER/TIMER

Meteronic announce this latest addition to their range of low-cost test instruments. The Type 410 may be used as a frequency meter, multiperiod meter or timer. Timebase stability is typically 1 part in $10^{6}$ per ${ }^{\circ} \mathrm{C}$. Time units are $10 \mu \mathrm{~S}$ to 1 sec and frequency can be measured to over 20 MHz with a resolution of 1 Hz . The high impedance input accepts waveforms with slow transition rates. Range selection is manual, with automatic positioning of the decimal point, and allows up to 8 digits to be examined on the large 4 digit display. Overflow indication is provided. Timer start, stop and reset may be operated electronically or by push buttons. The U.K. price exclusive of VAT, is $£ 85$. Meteronic, 114/116 Shipbourne Road, Tonbridge, Kent.

## HIGH-QUALITY STEREO DECODER

A recent addition to the Mullard range of modules for use in radio and audio amplifiers is a stereo decoder, type LP1400. It is intended for use by setmakers in high-quality equipment.

The LP1400 uses the sum and difference separation principle, which allows de-emphasis to be applied to the difference signal before demodulation. This attenuates interference from adjacent channel transmissions and noise components in the 114 kHz and 190 kHz regions which in a time multiplex system are frequently demodulated by harmonics of the 38 kHz signal and transposed to produce unwanted components in the audio outputs.

The LP1400 offers good stereo separation and a better overall performance than is generally obtained with time multiplex systems. Mullard Ltd., Mullard House, Torrington Place, London WC1E 7HD.

## QUADRAPHONIC PHONES

You don't have to have four ears to listen to quadraphonic sound on headphones, because in the new Eagle FF29, four 50 mm .transducers are so arranged that the effect is similar to four strategically-placed loudspeakers.
The FF29 phones use two coded jack plugs which are also ideally suited for use with the AA26 quadraphonic adaptor. This unit converts any stereo set-up into a 4 -channel system with the addition of 2 extra speakers.

Frequency range of the phones is $20 \mathrm{~Hz}-20 \mathrm{kHz}$, impedance $8 \Omega$ per channel and matching impedance 8 to $16 \Omega$. The retail price is $£ 16.80$ excluding VAT. Eagle International, Precision Centre, Heather Park Drive, Wembley, HAO ISU.


0NE of the latest additions to the electronic home construction market is a pocket calculator available as a complete kit or fully assembled. The Sinclair Cambridge weighs $3 \frac{1}{2}$ ozs and measures $4 \frac{1}{2} \times 2 \times \frac{11}{16}$ in and has an 8 digit LED display.

The LED display is an 8 digit 7 segment gallium arsenide/ phosphide device being driven via diodes directly from the calculator chip. The 8 diodes, D3-D10, and the flat pack resistor package RN1 form both isolation and an integral part of the keyboard's electronic routine. The cathodes of each digit are driven by a sixteen pin integrated circuit.

The keyboard is made from a single sheet of stainless steel with 18 'click fingers' chemically etched into it to enable the keys to have mechanical hysteresis and a positive click action.

The power supply (incorporating $\operatorname{Tr} 1$ functioning as an oscillator) generates a stabilised 15 volt d.c. supply for the two IC's. The action of Tr1 is such that it switches fully on and off thereby producing a square wave at the emitter thus providing the clock pulse, which is required to drive the calculator chip.

The algebraic logic of this calculator-which enables calculation a to be entered as you would write it down, or in other words logically, acts together with an advanced constant function to give, in effect, a limited memory, thus
extending the calculations which can be carried out as true chains. The constant facility may be used on all four functions-addition, subtraction, multiplication and division $(+-\times \div)$. These functions are often referred to in calculator terminology as operators.

In addition, the calculator operates across a wide exponent range from $10^{-20}$ to $10^{78}$ enabling it to handle large or small numbers without becoming overloaded. Calculations are to 8 significant digits, and incorporate a fully floating decimal.

A dual purpose clear button will remove only the last entry when used in conjunction with a function.
The calculator is battery powered by four cells. These may either be ordinary U16 cells (which give limited life) or the MN2400 mercury cells to give the calculator an extended

$\triangle$ Basic circuit of the Sinclair Cambridge. A brief description of circuit function is given in the text.

## The Catalogue you MUST have!




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## XEROZA RADIO

1 EAST STREET, BISHOPS TAWTON, DEVON


THE first surprise to the reader brought up on radio in the fifties and sixties is to find the TRF (tuned radio frequency or "straight") radio circuit making a comeback in the 1970s. This type of circuitry was discontinued in the thirties, with the development of the superhet, for several good reasons. First, the selectivity of the tuned circuits of the time became inadequate as the number of transmitters on the air increased, with the result that the ability to discriminate between stations closely separated in frequency was impaired. Improved selectivity required more sharply tuned coils, or alternatively the application of reaction or positive feedback. Further, with a series of tuned circuits operating at the same frequency, stray coupling could itself provide sufficient positive feedback to produce instability.
In any event, excessive positive feedback whether due to stray coupling or deliberate application of reaction could, quite simply, cause the circuit to radiate rather than receive and thereby render impossible reception of a broadcast on that frequency, for some distance around. The superhet, in which amplification of the signal occurs mainly at an intermediate frequency separated from that of the received signal, not only guarantees improved selectivity and stability but also permits the easy application of such refinements as automatic gain control (AGC).

The above observations apply generally to valve or transistor systems; it will be noted that, although TRF circuits have a deceptive simplicity, and avoid the purchase, installation and alignment of intermediate frequency transformers, they achieved only a very restricted popularity among the home constructors of the sixties. Also, despite the fact that quality in broadcast sound had been transferred to the FM channels, even the cheapest commercial AM receivers retained the superhet scheme. To be a credible contribution to the radio scene, therefore, the Ferranti ZN414 unit must have featured as distinctly novel in TRF circuits.


It should be clear, though, that the technology of the monolithic integrated circuit is better adapted to the TRF format. In every single operational amplifier or other high gain IC, methods have had to be developed and applied to enable the transfer of signals through several stages of amplification within a single chip without instability developing through stray capacitances. An integrated circuit IF amplifier for a superhet, however, must either lump all the frequency-selective tuned circuits before or after the amplification stage, or alternatively transfer the signal several times between the chip and external discrete circuitry, each time incurring the risk of instability problems which the superhet was intended to avoid. Further, with the high grade ferrites and litz wire, the tuned aerial circuit currently available has a higher " $Q$ ". and therefore an inherently improved selectivity, on the circuits of over thirty years ago. Further, a high input impedance can be developed, in the case of the Ferranti ZN414 typically over $1.5 \mathrm{M} \Omega$, so that this selectivity is not degraded by the loading presented by the following circuit. Finally, it has been found possible to incorporate an adequate AGC system.

## Low current consumption

The unit incorporates the equivalent of ten transistors packaged in a three pin TO-18 can identical with that used for small NPN transistors. The required power source is a single 1.5 V dry cell though the unit will function adequately over the range $1 \cdot 1$ to $1 \cdot 8 \mathrm{~V}$; economy of operation is assured by the very low current drain, some 1 mA being typical. Under such conditions, and with the AGC system operating on an incoming signal, the circuit produces an output of some 40 mV quite adequate to operate a medium impedance magnetic earpiece (about $500 \Omega$ ) or a crystal earpiece through a coupling capacitor. In general, though, the unit will be used to drive an audio amplifier, for which the output is adequate.

## Constructional details

Now for one or two constructional points. The small capacitor from the output pin to earth bypasses to earth any radio frequency signal appearing at the output. It is therefore necessary that it be mounted as close as possible to the output and earth leads of the ZN414. It will be noted that the time constant of the output circuit, determined by this capacitor and the AGC resistor, is some 4 kHz a feature tailored to the characteristics of the AM signal, for which a passband of some 10 kHz (double sideband) is allowed.

The aerial used, which may be any of those advertised to cover the medium waveband with an appropriate capacitor, should have its ferrite rod at least an inch away from the IC, otherwise all leads should be as short as possible. Due to the high input impedance already mentioned it is not necessary to tap the tuned coil on the ferrite rod to find a matching point to feed the circuit input. However, on commercial rod aerials employed with this unit, such a tap, or a small secondary winding, may be available; this may be used experimentally for the connection of an external aerial, if so desired.


THIS lightweight metal detector operates at a frequency of 120 kHz and uses a phase locked loop to provide both an audible and a visual indication of a find. Most detectors use either a variable inductance or a variable mutual inductance as the sensing element. The Ferret is no exception, the inductance of the search coil changing in the presence of metal. Ferrous and non-ferrous metals cause opposite changes in inductance and it is a unique feature of the Ferret that a visual indication of this is provided. The meter deflection is in opposite senses for the two types of metal.

Another feature not found on previous metal detectors is the use of harmonic mixing. Although the two oscillators in the Ferret are both operated at about 120 kHz the beat note is derived from their fifth harmonics and the sensitivity is accordingly five times as great.

## Main Oscillator

The electronics of the metal detector breaks down into four functions: the Main Oscillator, Beat Frequency Oscillator, Phase Locked Loop and DC Amplifier. Powered by two PP3 batteries the circuit


The star coil Ll and the series combination of C4, C5 3 Ha C6 form a tuned circuit with Tr 1 acting as an oscillator taking the voltage at the C4-C5 junction, amplifying it, and feeding it back to the C6-L1 junction in the correct phase for maintaining the oscillation. Diode D1 clamps the gate of Trl below earth potential and provides AGC action to stabilise the output and prevent it from being clipped. DC power is fed to the amplifier through the choke L2 the value of which is not critical, but 25 mH should be considered a minimum and the value chosen $(40 \mathrm{mH})$ happened to be available to the author in a convenient size. An output of at least 5 V peak to peak should be available, the frequency being adjusted by altering the number of turns on L1.

## Beat Frequency Oscillator

An NE555 timer IC is used in astable mode to provide a variable frequency oscillator. Suppose Cl is charging up through R1, R2 and VR2; when the voltage across Cl , sensed by pin 6, reaches ${ }^{2}{ }_{3} \mathrm{Vcc}$ pin 7 is earthed and C1 begins to discharge through R1. When the voltage across C 1 , sensed by pin 2 , has fallen to ${ }^{1}$ V Vcc pin 7 is allowed to float and Cl begins to recharge. The switching applied to pin 7 is amplified and presented at the output, pin 3, as a squarewave which swings between earth and Vcc.

Cl charge time $=0 \cdot 685(\mathrm{R} 1+\mathrm{R} 2+\mathrm{VR} 2) \mathrm{Cl}$
Cl discharge time $=0 \cdot 685 \mathrm{RlCl}$
Frequency $=1 /($ Charge time + Discharge time) $=1 /(2 R 1+\mathrm{R} 2+\mathrm{VR} 2) \mathrm{C} 1 \times 0 \cdot 685$
Substituting the circuit values gives a range of frequencies, as VR2 is varied, of $103-160 \mathrm{kHz}$. The upper frequency is not reached due to stray capacitances and internal resistances (the chip is only specified to 100 kHz ) but an adequate band to either side of 120 kHz can be swept.

## Phase Locked Loop

The operation of the NE561B phase locked loop was described last month, but is outlined again below owing to the unconventional used made of it in the Ferret.


When the PLL has no input signal, the Voltage Controlled Oscillator (VCO) frequency resulting is called the free-running frequency and is determined by C12 and the current injected into pin 6 from VR3 and R6.

In Fig. 2, Vc assumes a quiescent value. On applying the main oscillator output to the FM input, pin 13, the phase sensitive detector and low pass filter cause Vc to change just enough to make the VCO frequency equal to the input frequency ( $5 \times \mathrm{Fo}$ ).

The amount that Vc changes depends on the difference between the free-running frequency and $5 \times$ Fo. In this circuit the free-running frequency is fixed so Vc can be regarded as a function of Fo only.

$$
\frac{\text { Change in Vc }}{\text { Change in Fo }}=200 \mathrm{mlV} / \%
$$

Thus changes in the inductance of Ll have been transformed into changes in Fo which have in their turn been transformed into changes in Vc.

The VCO frequency, which by PLL action is exactly equal to $5 \times \mathrm{Fo}$, is mixed with the Beat Frequency Oscillator output $5 \times \mathrm{Fb}$ in the internal multiplier intended for AM demodulation, Fig. 2. An audible beat note, Fa , results where $\mathrm{Fa}=(5 \times \mathrm{Fo} \pm 5 \times \mathrm{Fb})$ $=5$ ( $\mathrm{Fo} \pm \mathrm{Fb}$ ).


Fig. 3: Block diagram illustrating circuit function.

Fig. 3: The printed circuit board-to scale.

If $\mathbf{F o}$ and Fb are very large compared with Fa , and are nearly equal to each other then very small changes in Fo will produce larges changes in Fa. Suppose Fo changes from 120 kHz to $120 \cdot 120 \mathrm{kHz}$, with $\mathbf{F b}=119 \cdot 9 \mathrm{kHz}$.

Vc will change by

$$
\left(\frac{120 \cdot 120-120}{120}\right) \times 100 \times 200 \mathrm{mV}=20 \mathrm{mV}
$$

and Fa will change from $5\left(120-l^{\prime} 19 \cdot 9\right)=500 \mathrm{~Hz}$ to $5(120 \cdot 120-119 \cdot 9)=11100 \mathrm{~Hz}$.
The output from the Beat Frequency Oscillator is dropped by the volume control VR1 to a level suitable for the phase locked loop and C2 tailors the frequency response of the coupling network to attenuate the fundamental of 120 kHz but pass the required harmonic of 600 kHz . An input of more than two volts will cause damage to the IC. The mixed output is fed directly into a crystal eargiece, and is quite sufficient for all but the most noisy surroundings. As mentioned above, VR1 acts as a preset volume control.
DO NOT attempt to drive a magnetic earpiece directly from the IC as this will seriously overload it. If it is required to run a magnetic earpiece or speaker then it is quite permissible to add a suitable amplifier stage, remembering that the AM output of an NE561B has a DC level of about +14 V .

Capacitors $\mathrm{C} 7-\mathrm{Cll}$ perform coupling and bypass functions and any value between $0 \cdot 01 \mu \mathrm{~F}$ and $0 \cdot 1 \mu \mathrm{~F}$ should be adequate.

## D.C. Amplifier

A 741 operational amplifier is used as a variable gain inverting amplifier. By altering the value of VR5, the preset sensitivity control, the gain of the amplifier can be adjusted from $\times 1$ to $\times 500$. At maximum gain an output swing of 1 volt is obtained for a $0.01 \%$ change in Fo.

Because the normal output level at pin 9 of IC2 is +12 V a voltage divider VR4 and R8 is provided to give a zero-set control. The meter M1 will give a zero indication when the voltage at pin 3 of IC3 equals the voltage at pin 9 of IC2.

Resistors R10 and R11 are equivalent to a single resistance in series with the meter and connected to +9 V . Their values should be adjusted so that

full scale deflection of the meter occurs when the amplifier output is either at earth or $+18 \mathrm{~V} .150 \mathrm{k} \Omega$ was found to suit the miniature meter used in the prototype. Power supply decoupling is provided by C13 and C14.

Transistor enthusiasts may be interested to know that the three integrated circuits contain about seventy-five semiconductor devices although it is not often clear which of these are transistors and which are diodes!

## Circuit Board

A printed circuit board $4 \times 2^{3}{ }_{8}$ in. has been designed to take the Ferret, see Fig. 3. Only one interconnecting wire is used on the board and all terminations


Fig. 4: Component layout and interconnections.
are taken to convenient points. The meter is intended to be positioned over the large clear area at one end of the board. Two holes are drilled to enable the board to be bolted into the box, one being positioned to take the integral screw of the specified pot core L2.

All the component holes except those for the preset potentiometers VR1, VR3 and VR5 are positioned on a $0 \cdot$ lin. matrix so the circuit could be made up as shown on perforated paxolin with pins and underboard connecting wires. Component positions are shown in Fig. 4.

If a new component layout is contemplated then the only precaution to take is to keep the leads to IC2 as short as possible and the circuit basically split up into its four sections, as depicted in Figs. 1 and 4.

## Assembly

A small aluminium box $5^{1}{ }_{4} \times 4 \times 1^{1}{ }_{2}$ in. has the remaining components mounted inside it with the meter in the lid. It is important to use a metal box in order to keep down stray radiation. Fig. 5 shows the positions of VR2, VR4, S1 and SK1. The cutting details for the meter will depend on the actual type used.
A 6BA bolt is used to augment the 6BA bolt in L2 for holding the circuit board. It is important to see that the case is earthed via the copper conductor pattern by at least one of these screws. The best way to ensure that the component wires do not short out on the case is to introduce a couple of extra nuts on the bolts between the board and the case.

If plastic electrical conduit, as described later, is used to construct the shaft of the Ferret then a hole large enough to accommodate the fixing bush must be punched or cut in the base of the case and a similar one for the handle.


Fig. 5: The positions of the main controls can be clearly seen above.

The search coil, Ll, must be wound for an inductance which gives a frequency of 120 kHz in the main oscillator. It can be shown that the inductance is proportional to $N^{2} D$, where $N$ is the number of turns and D the diameter of the search coil. Many different coils have been wound for the prototype using this formula based on an original made with the aid of a digital frequency meter. All have fallen well within the band that can be tuned in by the rest of the circuitry.

Fig. 6a shows a small coil for localised searches and Fig. 6b a larger coil, which is slightly less sensitive, for extended searches. The number of
turns are respectively 90 and 65 . To wind the coil, first nail a few small pins into the upper rim of the top plate and carefully wind the required number of turns from any thin insulated copper wire. When this is complete push the coil down on to the hardboard and secure with a dozen or so blobs of glue. When the glue is dry the pins can be removed and the two pieces of hardboard sandwiched together. Drill four holes in the complete assembly, as shown in Fig. 6, and bring the plates together with 4BA bolts.

The connection to the circuit board is made by a length of coax cable and a terminal block inside the case.

One of the easiest materials to use for the shaft is a length of plastic conduit intended for electrical wiring. Having been bent to the shape shown in Fig. 7, by gently heating the relevant section, it is fixed into the base of the box and the search coil top plate with termination pieces. The fixing to the search coil should be completed before it is finally screwed together.

A short length of conduit, fixed as described above into the end of the case, covered with a bicycle handlebar grip will suffice for a handle.

## * components list

| Resistors |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| R1 $2 \cdot 2 \mathrm{k} \Omega$ | R5 | $10 \mathrm{k} \Omega$ | R9 | $10 \mathrm{k} \Omega$ |
| R2 4.7 kS 2 | R6 | $1.8 \mathrm{k} \Omega$ | R10 | $150 \mathrm{k} \Omega$ |
| R3 1 kS | R7 | 10 kS 2 | R11 | $150 \mathrm{k} \Omega$ |
| R4 68 kR 2 | R8 | $47 \mathrm{k} \Omega$ |  | 150k』 |

All $\frac{1}{2}$ or $\frac{1}{t}$ watt, $20 \%$ or better, see text
VR1 $25 \mathrm{k} \Omega$ pre-set pot., horizontal, miniature
VR2 $5 \mathrm{k} \Omega$ pot., standard
VR3 $10 \mathrm{k} \Omega$ pre-set pot., horizontal, miniature
VR4 $100 \mathrm{k} \Omega$ pot., standard
VR5 5M 2 pre-set pot., horizontal, miniature

## Capacitors



C8 $0.02 \mu \mathrm{~F}$ ceramic
C9 $0.02 \mu \mathrm{~F}$ ceramic C10 $0.02 \mu \mathrm{~F}$ ceramic C11 $0.02 \mu \mathrm{~F}$ ceramic C12 1000 pF polystyrene C13 $50 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic C14 $50 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic C15 $0.01 \mu \mathrm{~F}$ ceramic
Polystyrene capacitors 5\% or better

## Semiconductors

ICI NE555 8 pin DIL.
IC2 NE561B 16 pin DIL
IC3 741 C 8 pin DIL

$$
\begin{array}{ll}
\text { D1 } & \text { 1N914 or similar } \\
\text { Tr1 } & \text { 2N3819 or similar }
\end{array}
$$

## Miscellaneous

L1, L2 see.text. Jack socket, 3.5 mm . Crystal earplece and plug, 3.5 mm . S1, 2 pole c/o slide switch. Aluminium box $5 \frac{1}{4} \times 4 \times 1 \frac{1}{2} \mathrm{in}$. (AB10). Batteries PP3 (2) and 2 pairs battery clips. Knobs (2). Plastic conduit, 36 in , approx. and conduit terminations (3). Plastic handlebar grip. Terminal block, 2 way. Hardboard and wire for heads. Co-axial cable. Printed circuit board. M1, centre-zero edge panel tuning meter (Henrys F11).

Ambit international, 37 High St., Brentwood, Essex, can supply the pcb for 78p inc., the three IC's and transistor for $£ 4.90 \mathrm{inc}$, or a complete kit consisting of the pcb, three IC's and transistor, all remaining components, aluminium box and wire for search head for $£ 9.50$ inc.


Fig. 6(a): A small coil used for localised searches and Fig. 6(b) a larger coil, although less sensitive, used for extended searches.


Fig. 7: The handle is formed as shown above.


Photograph shows two of the coils made by the author.


Close-up view showing the inside of the PW Ferret. Compare this photograph with Fig. 4.

## Setting Up

With the search coil connected, set all the preset pots to mid-rotation and switch on. Adjust VR2 for a strong and constant beat note. If only weak and varying notes can be obtained then the loop is not locked and VR3 must be rotated until the required note is heard. Set VR3 in the middle of the portion of its travel over which the beat note is clear. VR1 can then be set for the required volume in the earpiece.

Adjust VR4 to zero the meter, this will be a sensitive setting, and move the Ferret towards a large metal object. An indication should be both heard and seen. VR5 will then determine the strength

## SPECIAL PRODUCT REPORT-continued from page 630

life. Sinclair Radionics claim that mercury cells will give 12 hours continuous operation. Certainly a small mains unit would be an advantage if continuous use of the calculator is contemplated.

The kit is intended for constructors with previous soldering experience. Estimated assembly time is approximately 3 hours. Tools required-and the most important item-is a properly earthed sub-miniature soldering iron with a $\frac{1}{16} \mathrm{in}$. bit or smaller. Other items are wire cutters, tweezers and instrument type pliers.

The 15 page step-by-step assembly instruction booklet contains a section on special safety precautions which should be observed before and during assembly of the kit.

Attention is drawn to the point, that static electricity can be a hazard unless proper precautions are taken. The manufacturers instructions should be carefully read and fully understood before assembly is contemplated.

Care is necessary when assembling the kit, especially because of the numerous tiny solder connections to be made. Blobs of solder must be avoided and close inspection of the completed printed circuit board is essential after soldering has been completed. Examination of the finished p.c.b. with a magnifying glass is recommended to ensure a clean product.

Those constructors who after purchasing the kit and then having read the assembly instructions find that they are 'stumped' may return the kit (untouched) plus a cash balance
of the meter reading when an object comes within range.

It may be possible to obtain beat notes from harmonics other than the fifth. It is sufficient, however, to select that beat note which gives the most sensitive audible response when the Ferret is brought near to some metal test object.

As has been already suggested in the text, a lot of the component values are non-critical and, in general, all except the polystyrene capacitors can have $20 \%$ tolerance. It is recommended that first grade integrated circuits are used, especially the NE555. If required, integrated circuit mounting pins can be used.
in exchange for a built version. What could be more fair? Sinclair Radionics state that full service facilities are available for kits and ready built units.

Also included with the calculator is an informative 32 page booklet detailing the wide range of calculations that can be carried out. From simple arithmetic, compound interest, logarithms, trigonometric functions, roots, polynomials, hyperbolic functions and so on. In addition a credit card size aide-memoire with calculations summarised in formula form is included.
Calculations of all types were performed with the Cambridge and it is surprising how simple it is to use. It brings about a new and refreshing interest to calculations. In the calculation of square roots the iterative Newton-Raphson method is used. This sounds quite complex, but you simply take a (wild) guess at the square root and enter it on the keyboard, using the procedure outlined in the instruction booklet. We tried this method many times-feeding way-out guesses to the keyboard. The correct answer came up every time.

The kit is attractively packaged and includes all necessary components to complete the calculator. Even solder is supplied.

A full money refund guarantee applies to untouched kits if returned within 3 weeks.

At $£ 27.45$ (including VAT) for the complete kit, the Sinclair Cambridge provides excellent value for money. Sinclair Radionics Ltd., London Road, St. Ives, Huntingdonshire PE14 17HJ.

## INNETTMONTH'S 



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## WDBE

or anywhere that a.c. mains is not readily available.

5. RESISTOR AND CAPACITOR CALCULATOR
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Pick up those unusual broadcasts and amateur transmissions that are found on the short wave band. This receiver is designed to tune 1.7 MHz to 30 MHz in three bands, using two transistors and two integrated circuits.

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This fascinating feature shows how you can use one i.c. in any of seven dififerent simple amplifier circuits, including examples for a record player, radio, intercom, or tape player.

DECEMBER ISSUE ON SALE 2nd NOVEMBER

# dicionary of audio terms 8 hi.fi specificeations 

## PRAGTICAL WIRELESS 8.PAGE SUPPLEMENT NOV. 1973

A
A-B. This is the kind of audio comparison test where any differm ences in sound quality can be assessed immediately upon switchover, i.e. on "A-B" comparison between items of equipment $A$ and 8 . Often the left and right-hand channels or the record and replay sound signals are designated $A$ and B.
ACOUSTICS. The study of the behaviour of sound. The "acoustic characteristics" of a room are dependent on its size, shape and the reverberation time according to the reflective or absorbent items present.

## ACOUSTIC FEEDBACK. Cycling

 of sound build-up to a continuous squeal as the microphone picks up a signal from a loudspeaker connected to the same microphone amplifier.ACOUSTIC SUSPENSION. Some loudspeaker systems employ a sealed cabinet. This enables the acoustic pressure of the air enclosed therein to provide the principal restoring force for the diaphragm of the speaker.
A.F.C. Automatic frequency control. A control circuit in a receiver or tuner which compensates for small variations in the carrier signal frequency to provide a stable audio output. A circuit function in a tuner
or receiver which keeps the unit accurately tuned to the desired station, eliminating any tendency to drift.
A.G.C. Automatic gain control. A circuit which stabilises a large variation in the strength of an incoming signal.
A circuit function in a tuner or receiver which maintains the mean amplitude of the modulated signal at almost a constant level. A.G.C. or A.V.C. (Automatic volume controi) as it is sometimes called is also used to describe the audio compression system employed in automatic tape recorders, in which the recording signal level is adjusted to compensate for widely differing sound levels.

## ALIGNMENT PROTRACTOR.

 Indicates errors in a pickup's lateral alignment. It fits on the centre spindie of the turntable, and the pick-up stylus fits into a small hole on the device. The correct indication is shown when the angle of lateral movement of the pick-up head is at $90^{\circ}$ to the tangent of the groove at any point, although minimal tracking error is expected with most pick-up arms.AMBIENCE. The "feeling" given to sounds by a room. The effect of the environment on the coloration of sounds produced.
AMBIENT NOISE. Unwanted background noise picked up by a microphone, we. any extraneous
clatter in a room. Also any acoustic caloration that influences sounds, krought about by the acoustic proparties of a loom in which a recording is being made or replayed.
AMPLIFICATION. An increase in the magnitude of a signal brought about by passing "it through an ampl fier
AMPLIFICATION FACTOR. The symkol used to signify this is " $\mu$ ". It is the measurement of amplification in a circuit usualiy in voltage or current terms calculated by dividng the output by the innut. This figure is often converted to decibels (which see).
AMPLIFIER. A device for increasing the magnitude of a signal by means of a varying control voltage, maintaining the signal's characteristic form as closely as possible to the original.
AMPLITUDE. The level of an audie or other signal in voltage or current terms.
AMPLITUDE DISTORTION. The distartion of a signal by the undesirable influence of a circuit or component and takes place when the is a change of amplitude in fart of the input signal bringing about harmonic distortion and intermodulation distortion. This part is expressed as a percentage of the whole waveform at any given period of time.
AMFLITUDE MODULATION.
Commonly known as a.m. and
refers to the method of radio transmission where the audio modulating signal is made to vary the amplitude of the radio carrier wave.


The audio information is carried on a high frequency radio wave.
ANECHOIC CHAMBER. A special room used for testing audio transducers, where all wall surfaces have been covered with acoustically absorbent materials so that reflections of the sound waves are eliminated. Otherwise known as a "dead room".
ANTI-PHASE. Where two identical signals are disposed in $180^{\circ}$ phase opposition. When superimposed, they tend to cancel each other because their waveform patterns are of equal magnitude but opposite polarity.
ANTI-SKATING DEVICE. A device found on many modern pick-ups which provides an "outward" force on a pick-up arm. This counteracts the arm's tendency to move towards the turntable centre due to offset geometry, and reduces stylus/groove friction.
ANTISTATIC CLEANER. Substance used on gramophone records which helps to prevent the build-up of a static charge which attracts dust.
ATTENUATOR. A device which reduces the amplitude of a signal by known proportions.

## AUDIO FREQUENCY SPEC-

 TRUM. Mainly the full range of sounds we can hear. In a person with good hearing the range of sounds in the audio spectrum is usually between 30 Hz and $16,000 \mathrm{~Hz}$. In older people this is usually 50 Hz to $10,000 \mathrm{~Hz}$.AUDIO OUTPUT. The output signal from any audio equipment. It is generally measured in volts or watts r.m.s.
AUTO-CHANGER. A device on a record-playing turntable which facilitates the automatic positioning of a disc and pickup ready for playing.
AUX. Abbreviation of auxiliary. Often applied to amplifier inputs and refers to an extra input facility as distinct from "mic", "tuner", "pickup", etc.
AZIMUTH. The angle which recording and playback head gaps make with the line along which the tape moves. The head is oriented until this angle is $90^{\circ}$.

BAFFLE. The mounting for a loudspeaker usually comprising a flat non-resonant panel. It is used to increase the length of the path of the sound waves between the front and rear of the speaker to minimise bass losses.
BALANCE. Equality of amplifier gain or signal level from right and left channels of a stereo amplifier. In theory the balance between each channel should be electrically perfect but there may be mismatch of nominal signal level from one or other channel which is compensated by adjustment of the "balance control".
BALANCE CONTROL. A variable resistor used to compensate for any slight loss of signal in the right or left channel of a stereo amplifier. To some extent, this control can compensate for unbalanced speakers and be used for adjustment when the listener is not in an equidistant position between the two loudspeakers.
BANDWIDTH. The range of audio frequencies over which an amplifier or receiver will respond and provide a useful output.
BASS. The lower end of the sound spectrum (usually 150 Hz and below). An amplifier "bass control" usually provides a variance of decrease or increase in response at frequencies below 1 kHz .
BEL. A ratio of two signal levels, such as at the output and input, in logarithmic terms. It is too large a unit to use for precise measurement and we use tenths or "decibels". These are defined in power terms as $10 \log _{10} \frac{\text { output }}{\text { input }}$ or in voltage or current terms as $20 \log _{10} \frac{\text { output. }}{\text { input. }}$
BIAS. A high frequency signal applied to the audio signal at the tape recording head to make the audio signal magnetise the tape over the linear part of head's magnetic characteristic. The bias signal is usually above 40 kHz to avoid audible intermodulation distortion. Bias is also a term used to denote the sideways thrust of a pickup arm.
BIAS COMPENSATOR. A device which counteracts the inward bias of a pick-up arm as it tracks the disc. The compensator exerts an outward force on the arm and generally can be adjusted to have a definite relationship to the playingweight of the pick-up.

BI-RADIAL STYLUS. Also known as elliptical stylus. This is used with lightweight pick-up arms to reduce tracking distortion. The stylus tip has a small radius where it touches the walls of the record grooves as distinct from a conventional stylus which has a hemispherical tip.
BOTTOMING. A situation in which a stylus reaches the bottom of a record groove because its tip radius is smaller than optimum for the groove. Also the opposite of the pinch effect.
BULK ERASER. An instrument which erases recordings from a whole tape at once while it is still on the spool. It does this by producing an a.c. magnetic field of high intensity.


CAPSTAN. The drive spindle in a tape recorder, which in conjunction with the pinch-wheel, pulls the tape across the heads at constant speed.
CARDIOID MICROPHONE. A microphone which has a sensitive response to sounds on one side.


This makes the response very directional. It is called "cardioid" because it has a heart-shaped polar diagram.
CARTRIDGE. The electro-mechanical transducer of a pick-up head that converts stylus vibrations to an electrical signal. It is generally detachable and fits into the headshell of a pick-up.
CERAMIC. Piezo-electric part of a pick-up, speaker or microphone that acts as a transducer. It has characteristics similar to a crystal transducer but is more robust.
CHANNEL SEPARATION. The degree to which the two signals in a stereo system are electrically isolated. Usually expressed as a ratio in decibels.

CLASS-A. An amplifier where the output transistors or valves are operating permanently on linear portions of their transfer characteristics. Efficiency is low, but a constant current is drawn from the power supply whatever the signal level. Usually recognised by the use of a single transistor or valve driving the loudspeaker.
CLASS-B. An amplifier where two transistors or valves operate on positive and negative half cycles of the signal wave form. Each operates from a low initial current but this rises as the signal level increases. Usually recognised by the use of two transistors or valves operating in antl-phase to drive the loudspeaker.
CLIPPING. Severe distortion caused by overloading the input of an amplifier. A sine wave signal waveform has a flat top and bottom at the peaks when clipping occurs. COAXIAL CABLE. A screened cable where the inner conductor is surrounded by a concentric outer screen. Commonly known as "coax' the cable is carefully manufactured so that it has a constant characteristic r.f. impedance of $70-80 \Omega$. It is used for aerial downleads and for sending r.f. from one unit to another. Also used to inter-
connect audio stages or equipment of high impedance to minimise the risk of hum inducement.
COLUMN SPEAKER. A loudspeaker cabinet of long "column" shape. Usually the loudspeaker is at one end so that the rear of the drive unit is loaded by a column of air. Often columns are made from drain-pipes. Also the name given to a long speaker cabinet containing several loudspeakers for public address work.
COMPARATOR. Often found in audio showrooms, it is a unit which by switch selection, will connect up a combination of speakers, amplifier, tuner, pick-up, tape player, etc. For comparing different types. Also the name of a circuit which compares two signals and provides a "difference" signal.
COMPATIBILITY. The ability of one unit to be used with another without detrimental effect on the signal through mismatch. A compatible pick-up will play both mono and stereo records.
COMPLIANCE. The ability of a stylus to respona to both horizontal and vertical movement. The degree of compliance is a measure of the
capability of the stylus to follow rapid variations in the groove surface.
COMPRESSION. This occurs when the dynamic range is reduced electronically so that quiet sounds are raised and loud sounds lowered. The most common application is an "automatic" recording where it is important that all sounds recorded are made intelligible when played back. Also used where necessary to avoid over recording and distortion, or to lift the signal level clear of background noise or hum.

## CONDENSER MICROPHONE.

A microphone which contains a metal plate and a thin metal diaphragm set close together. A polarising voltage is applied to the plates. The capacitance of the microphone is thus affected by movement of the diaphragm from air pressure waves.
CONTROL UNIT. A pre-amplifier unit in an audio set-up. Signals from audio sources, i.e. tuner, pickup microphone, are fed into it. Equalisation (where necessary) is applied, then the signal is fed to the main amplifier. Volume and tone controls are usually incorporated together with any necessary programme selection switch.
COUNTERBALANCE. Counterbalance is a weight, usually adjustable, fitted at the pivot end of a pickup arm. It counters the weight of the pickup head and cartridge unit and allows adjustment of the stylus pressure to the desired value. CROSSOVER NETWORK. A circuit usually employing capacitors and coils which feeds low notes to a low frequency speaker (woofer) and high notes to a high frequency speaker (tweeter). The crossover frequency is that at which frequency bands divide. Sometimes the audio spectrum is divided into more than two bands to drive more than two speakers.
CROSSTALK. Breakthrough of the signal from one channel to another by conduction or radiation. CUT-OFF FREQUENCY. The frequency response Imitation, either upper or lower end, of a given component or piece of apparatus where the response falls off by 3 dB , then is even lower beyond this frequency.


DAMPING FACTOR. The ratio of the impedance of a speaker to the amplifier impedance. A high damping factor is desirable to

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subdue speaker resonances.
DECIBEL. One tenth of a Bel (which see).
DE-EMPHASIS. Reduction of the level of the higher audio frequencies during f.m. reception or tape replay, so that they compensate for the pre-emphasis (which see) applied to the transmission. This restores an overall uniform resjonse, with improved signal-to-noise ratio.
DEMAGNETISER. A cevice which removes residual magnetism from tape heads. This magnetism, if not removed can introduce noise on recordings and cause high frequency loss.
DEVIATION. In f.m. transmissions and reception deviation is the increase or decrease of signal carrier frequency from the nominal; also applied to drifting. Standard maximum deviation rating is $\pm 75 \mathrm{kHz}$ for f.m. radio.
DIN. Stands for Deutsche Industrie Normenausschus. This is an organisation in West Germany (similar to the British Standards Institution) which sets certain industrial standards.

A well-known standard is the DIN 45,500 which applies to domestic hi-fi equipment. Various plugs and sockets are popularly known

as "DIN plugs". They have DIN standard geometry and connections.
DIPOLE. An aerial generally used for v.h.f. receivers.
DNL. Dynamic noise limiter. A compatible circuit designed by Philips Ltd. primarily for use with tape recorders. It improves the effective signal-to-noise ratio during replay by selective filtering at low signal levels.
DOLBY SYSTEM. A njise reduction system which compresses signals before they are recorded on tape and expands them again on replay. This results in a reduction of background noise and is particularly designed for use with tape recorders.
DRIFT. Variation of r.f. signal carrier frequency above and below the nominal due to unstable reception conditions. It can be alleviated to a great extent by applying automatic frequency control.

DECODER. A circuit built into an f.m. tuner to enable it to translate stereo signal information into two matched audio outputs. Also a

means to extract and process recorded quadraphonic sound information from a complex signal into four matched outputs.
DISTORTION. Unwanted changes in the purity of sound being reproduced or in iff. signals. In audio it generally implies intermodulation and/or harmonic distortion. These are derived from phase differences and/or amplitude distortion where the amplitude of the output does not bear the same proportion to the input at all frequencies.
DROP-OUT. Sudden decrease in the recorded signal level due to tape imperfections.
DVNAMIC RANGE. The range of signal amplitudes from the loudest to the quietest that can be reproduced effectively by the equipment. The upper limit is set by inherent distortion leval, and the lower limit by background noise and/or hum.

## EARTH LOOP

The wiring of the interconnections between items of audio or radio equipment such that there is more than one neturn path for the "ground" side of the signal-carrying


Eakth Loop caused ar this earth crumerigu berween fwe Two chassis as well as by the screil of TME showal cable
wiring. This generally results in a loud hum from the speakers.
ELECTROSTATIC. Applied to loudspeakers and microphones (condenser type). An electrostatic force is used to activate the diaphragm. The charged diaphragm is suspended between two perforated plates. As an a.c. signal is applied to the outer plates, the diaphragm vibrates.
EQUALISATION. A pre-arranged circuit that applies correction to a given recording characteristic dur-
ing replay to result in a uniform frequency response at the output terminals.
ERASE HEAD. A head on a tape recorder which applies a strong high frequency alternating magnetic field to the tape so that earlier recordings may be "erased" as the tape runs past the head.

## $\square$

FADING. A drift in the level of received radio signals beyond intelligability. It is often caused by changes in the upper atmosphere. Also applied to deliberate slow reduction of signal level by means of the volume control.
FEEDBACK. A system where part of the output signal from an amplifier is applied to the input. When in antiphase (i.e. negative feedback) this results in reduction of distortion, lowering of the amplifier output impedance, improvement in signal stability.
F.E.T. Field Effect Transistor often used in early stages of an amplifier or tuner to give a high input impedance for minimum loading of the programme source, lie. aerial or pick-up.
FLUTTER. Rapid variations of pitch or frequency caused by inconsistent speed of a turntable or tape iransport mechanism.
F.M. Frequency modulation is a system of transmitting a radio signal where the frequency of the carrier wave is altered by changes in the amplitude of speech or music.

F.M. is applied to v.h.f. sound broadcasting above 87 MHz .
FREQUENCY. The number of complete cycles in one second of alternating current, voltage, electromagnetic or sound pressure waves. FREQUENCY RESPONSE. A graphical characteristic showing relative signal levels at different frequencies with respect to a given reference level. A "flat" frequency response is one that has a uniform level at all frequencies within a given band width.
FRONT END. Refers to the first stage of an amplifier or tuner.


GAIN. The increase in the power or voltage level of a signai due to amplification, i.e. the ratio that

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exists between the output signal level and the input signal level, usually quoted in decibels (which see).
GROOVE. A record "track" which carries the audio signal information in two $45^{\circ}$ displacements (stereo). In a long-playing record, groove dimensions could be: width 2.5 mils.; depth 1 mil. and pitch 250-350 groove revolutions per inch.

## R

HARMONIC. A harmonic of a fundamental frequency is the frequency of its exact multiple. Thus twice the fundamental frequency is the second harmonic (one octave up) and so on. If the fundamental trequency is $1,000 \mathrm{~Hz}$, the second harmonic would be 2 kHz , the third 3 kHz , and the fourth harmonic 4 kHz (two octaves up from the fundamental).

## 雨

IMPEDANCE. Opposition to a.c. current presented by capacitors, ind ctors and resistors. This effect is measured in ohms and is related to frequency.
INFINITE BAFFLE. A loudspeaker mounting where ideally there is no path of air between the back and front of the speaker diaphragm. An infinite baffie improves the forward radiation of sound at-low frequencles and preferably should be a very large plane surface like the wall of a room or a screen of very rigid material (e.g. $\frac{3}{4}$ in wood) on which a loudspeaker is mounted. In practice truly infinite baffles are rarely accomplished except in sealed boxes, but these give rise to problems of resonance.
I.P.S. Inches per second. Used for signifying the speed of a tape travelling past the heads of a tape recorder. The most common speeds used in this country are $1 \frac{7}{8}$ i.p.s. ( $4.75 \mathrm{~cm} / \mathrm{s}$ ); $3^{\frac{3}{4}} i . p . s .(9.5 \mathrm{~cm} / \mathrm{s})$ and $7 \frac{1}{2}$ i.p.s. $(19 \mathrm{~cm} / \mathrm{s})$.


JACK. A type of two-or more-ways concentric contact socket for carrying audio signals.
JOHNSON NOISE. A frying or sizzling sound produced by thermal agitation voltages generated in amplifier circuits. It usually occurs
in the input circuit (or front end) of an amplifier.
L
LEVEL. The voltage or power of a signal, or the relative voltage or power compared with a reference. LIMITER. A circuit in an amplifier or tape recorder which reduces volume when over-modulation or distortion is likely to occur.
LINE SOURCE SPEAKERS. A chain of speakers used in public address work that are driven from an amplifier with 100 V or 600 ohm output line.
LOUDNESS. The intensity of a sound as subjectively judged by the human ear. Loudness levels are measured in "phons" and may differ in effect from one person to an other.
LOUDSPEAKERS. A transducer which converts a.c. electrical energy into acoustic energy by movement

of the diaphragm causing air pressure waves.
M
MAGNETIC PICK-UP. A pick-up which employs an electro-magnetic transducer. An armature bears the stylus. The armature is pivoted between the poles of a riagnet and stylus movement make!; the magnetic field change, inducing a variable voltage in coils wound on the magnet.
The name refers to pick-ups of the moving coil type, moving magnet, moving iron, induced magnet and variable reluctance types.
MATCHING. Equalisation of the input impedance of one unit to the output impedance of another connected to it. Also used to refer to pairs of loudspeakers, microphones or other components which have similar characteristics and which are employed in the two channels of a stereo system.

MICROPHONE. An electroacoustic transducer which converts sound energy into electrical energy. The method depends on the material used in the microphone.
MIXER. A device which combines two or more separate signals into a common output.
MODULATION. The process whereby an r.f. or other signal is mixed with and caused to vary in accordance with an audio signal. The degree to which a tape or disc recorder is made to record without introducing distortion.
MONITORING. Listening to a signal as it is being recorded so that a check can be made on the quality. MONOPHONIC. Thereproduction of sound through a single channel amplifier.
MUSIQUE CONCRETE. A musical work comprising natural sounds which are recorded, then edited or manipulated and treated so that they do not sound like the original recording, but present an artificial form of musical composition.
MULTIPLEX TRANSMISSION.
The transmission of two or more simultaneous signals on a common carrier wave. Used for transmitting stereo broadcasts. A multiplex decoder is needed before these transmissions can be resolved into stereo of ather muitiple channeh audio.


NEGATIVE FEEDBACK-See "Feedback".
NOISE. Unwanted sounds of multiple and irregular frequencies and heard as a hiss or click.
-
OFFSET ANGLE. The angle at which the pick-up head is offset from a line through the centre of the arm. Correctly set, it minimises wear on stylus and record groove, and distortion of reproduction by keeping the tracking error down to a minimum.
OMNIDIRECTIONAL. Generally refers to a microphone which has approximately uniform sensitivity in all directions, the polar response being completely spherical.
OVERLOADING. An amplifier or piece of equipment operated beyond its signal-handling capability so as to create a distorted output.
QUTPUT STAGE. A power amplifier's final stage which feeds

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the audio signal to a oudspeaker or ather device.

## $\square$

PARALLEL TRACKING. A pickup cartridge's movement which is exactly parallel to the radius of the record, with the sty us always positioned on that radius for zero lateral tracking error.
PEAK PROGRAMME METER. A meter and associated circuitry which is used for indicating the peak levels of programme volume. Commonily referred to as P.P.M.
PHASE. Phase is the angular relationship in time of an alternating voltage or current with reference to zero voltage (or current) or another comparative waveform. Sound waves are said to be in phase when the voltage of one at any instant is the same polarity and angular displacement as the other and when crossing the zero voltage line in the same direction. "In-phase" soundwaves are identical in frequency and polarity at any instant; out-ofphase, waves may be idertical in frequency (but not necessarily) and of opposite polarlif at some instant. Anti-phase waves are identical in frequency and exactly opposite in polarity, i.e. $180^{\circ}$ out of phase.
PHASING. The arrangement of of loudspeaker or connestions in a stereo set-up so that-when an identical signal is fed to the two speakers, the speech coils are so connected that the cones both move in the same direction at the same time.
FHON. A unit of measurement of loudness allowing for the difference in sensitivity of the ear at differing frequencies. The phon is related to the decibek, but is in terms related to one frequency and determined from sound pressure measurements.
PHONO PLUG. A connecting plug often used in audio equipment. It has a centre "live" pin and an outer "earth" shield. Used with

screened cable for cennecting pickups and tuners to an amplifier or control unit.
PICK-UP. The part of a gramophone which extracts recorded information from a disc and
changes it to an electrical signal.
PICKUP ARM. The cantilever support for the pickup head with counterbalance weights, pivots etc. for carrying the cartridge.
PICKUP HEAD. The end of the pickup arm containing the cartridge. It is often removable from the arm and is usually called the "head shell" which carries the actual cartridge.
PIEZO ELECTRIC. An effect whereby a substance generates an electrical current when it is subjected to mechanical stress. This characteristic has been made use of in the design of pickups, microphones and loudspeakers.
PILOT TONE. A 19 kHz tone used in stereo broadcasting at the equivalent of $10 \% \mathrm{f} . \mathrm{m}$. modulation $\pm 7.5 \mathrm{kHz}$. It is transmitted with the sum-and-difference signals to assist in the stereo decoding process in the f.m. receiver.
PINCH EFFECT. The vertical movement of a stylus which takes place during record reproduction when irregularities in groove width occur.
PINCH WHEEL. The rubberised wheel in a tape transport mechanism that holds the tape against the capstan so as to ensure that the tape does not slip.
PITCH. The pitch of a sound is the masicai term for sound vibrations. Standard U.S. and European pitch is based on $=440 \mathrm{~Hz}$. When the pitch is raised one octave, the frequency is twice the original.
PLAYBACK. The reproduction of a tape recording or disc through an amplifier and loudspeaker or phones.
PLAYING WEIGHT. Downward force of a pickup on a record. Sometimes called stylus pressure. POLAR RESPONSE. Polar diagram or circular graph which shows the sensitivity of an aerial or microphone or the output from loudspeakers in an angular mode through $360^{\circ}$.
POLYESTER BASE. A base material used for magnetic tape on which is coated the magnetically sensitive substance. Widely used for long playing tape, it is less prone to stretching than acetate film.
POWER. The energy dissipated in an electrical or electronic circuit or component that is conducting either a.c. or d.c.
POWER AMPLIFIER. The stage of an amplifier which supplies audio signals to a loudspeaker or phones.
POWER-HANDLING CAPA CITY. The maximum power rating of a loudspeaker or other
component which determines how much current can be passed safely through without adverse effects. PRE-AMPLIFIER. An amplifying system for low signal levels. It boosts a low-level signal from a cartridge, for instance, and feeds the signal to a power amplifier. It may contain additional circuitry that affects the frequency response in some way.
PRE-EMPHASIS. The boosting of high frequencies in f.m. broadcasting or recording. Uniform frequency response is restored by "de-emphasis" in the receiver or replay amplifier. The purpose is to reduce the noise level that arises through transmission and tape recording.
PRESSURE PAD. A felt pad which applies a gentle but firm force to keep a moving tape in good contact with the heads of a tape recorder.
PRESSURE UNIT. A movingcoil speaker drive unit which usually has as its diaphragm a small dome of plastic or metal. It is designed for use in the throat of a horn.


QUADRA TURE. Two a.c. signals of equal-frequency are said to be in quadrature when they are phase displaced by $90^{\circ}$.
QUADRAPHONY. Four matched discrete audio channels are employed in true quadraphony; four matched microphones are used in the recording process, four-track tape or "quad" records are used for replay through a four-channel amplifier which feeds four loudspeakers.


Various modulation or matrix systems are sometimes used so that four channels can be obtained by using some two-channel (stereo) equipment. The signals are then "decoded" so that four channels of sound can be reproduced through four speakers.

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Systems known as "surround sound" are used to produce "synthetic" quadraphonic effects. These units use matrix circuits in conjunction with conventional stereo equipment and records.
QUADRUPLE PLAY. Magnetic recording tape which is thinner than "standard play" tape and consequently enables one to make recordings four times longer than with 'SP' tape.
Q4. The name given to the Practical Wireless quadraphonic decoder to enable quadraphony to be reproduced from stereo or quadraphonic recordings.

## R

RADIO FREQUENCY. A term describing incoming radio signals to a receiver or outgoing signals from a radio transmitter. There are no finite limits in the r.f. range but it is usually considered to denote frequency above 150 kHz and extending up to the infra-red range.
RAKE. The "rake" angle of a stylus is the angle that the stylus bar makes with a gramophone record when viewed from the side.
RANDOM NOISE. Noise generated in a circuit by random movement of electrons caused by thermal agitation. In tape recording it can be caused by uneven distribution of magnetised particles and is reproduced as a background "hiss".
REAR SUSPENSION. Used in moving-coil loudspeakers, it is a pliable support situated near the apex of the cone, and assists in keeping the coil in a concentric position in the air gap between the magnet poles.
REFLECTOR. An element in a v.h.f. aerial which is situated to the rear of the main dipole. It helps to reflect radio waves on to the dipole. Also the name given to the "dish" often employed to reflect quiet or distant sounds in the open air on to a microphone.
REFLEX CABINET. A type of speaker enclosure fitted with a vent or port through which out-of-phase signals from the rear of the cone are "reflexed" by allowing the enclosed air in the cabinet to be tuned for a coupled resonance effect with the cone of the drive unit. The signals are then brought into phase with the front radiation from the cone of the speaker so as to reduce the "boomy" effect of resonance.

REJECTOR. Filter or part of a circuit which rejects a particular frequency or band of frequencies.
RESONANCE. The nature and dimensions of any object or enclosed volume of air will vibrate at a calculable frequency when disturbed by striking. This frequency is said to be the resonant frequency. When the object is made to vibrate at this frequency by a corresponding sound pressure wave the resonance is enhanced, producing a "boomy" effect, i.e. the volume at that frequency is apparently louder than at any other.
RESPONSE CURVES. Usually measured in decibels, with reference a given level, on a vertical scale, the response curve is a graphical representation of frequency response


When the response curve of an amplifier, pick-up, microphone, etc. is accurately plotted it represents the relative levels of amplitude at all frequencies within a specified bandwidth.
REVERBERATION. Reflected sound. It is produced by the gradual decay of sounds being reflected from ceilings, walls, floors and furniture.

Reverberation units create an artificial representation of the decay of the sounds electronically.
RIBBON MICROPHONE/
SPEAKER. Uses a narrow corrugated aluminium alloy strip suspended in a magnetic field. Sound makes the strip vibrate in a direction perpendicular to the magnetic field, resulting in an a.c. current being induced in a coil.
The natural response of a ribbon unit is bi-directional and a ribbon microphone has certain areas of minimum sensitivity. Only a very small response is produced by quite loud noises from the sides, the polar diagram for this type is known as "figure of eight".

A few ribbon microphones will give cardioid and hypercardioid responses.
RMS VALUE. The "root-meansquare" value of a.c. voltage, cur-
rent, or power is calculated as 0.707 of peak amplitude at the given frequency. It represents for mathematical purposes an acceptable level by which relationships between these units can be accurately established.
RUMBLE. Low frequency noise produced by the turntable bearings and motor of a record player, and transmitted mechanically by vibrating the pick-up. These vibrations are then detected by the transducer in the cartridge for conversion into an electrical signal.
RUN-IN. The start of a groove at the beginning of a side of a gramophone record which "runs in" to the recorded section.

SCRATCH FILTER. A low-pass filter, often an integral part of an amplifier circuit, which attenuates the higher frequency noise derived from disc recordings. The scratch filter is also suitable for the suppression of background noise produced by tape background hiss.
SCREENED LEAD. A cable which has an outer sheath of braiding which provides electrostatic screening of the inner conductor and so makes it ideal for connecting high impedance pick-ups microphones and tuners to the input of an amplifier. Its purpose is to reduce the effects of hum caused by radiation from a.c.-carrying wiring or components.
SELECTIVITY. A tuner's ability to discriminate between a wanted signal and an interfering signal on adjacent frequency settings of the tuning dial.
SENSITIVITY. The ability of any communications equipment, including audio to reproduce very low signals.
SEPARATION. The degree to which right and left stereo signals are isolated in pickup or stereo amplifier.
SHELL. Refers to that part of the pick-up which carries the cartridge. The head shell can often be detached from the pick-up arm.
SIBILANCE. The strong emphasis in pronunciation of the letters "S" and "SH" in speech. It can be exaggerated by microphones having peaks in their high frequency response.
SIDE-THRUST. The tendency of the stylus to "skate" towards the centre of a record causing increased wear on the inner groove wall. With low tracking weight, side thrust can cause the stylus to "jump" the record's groove.

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SIGNAL-TO-NOISE RATIO. The difference, measured in decibels, between a specified signal reference level and the level of unwanted noise. The higher the ratio, the better the equipment.
SINE WAVE. A waveform (often viewed on an oscilloscope) of a pure alternating current or voltage. It is drawn on a graph of amplitude versus time or radial degrees and follows the rules of sine and cosine values in relation to angular rotation of an alternator. It can be simulated by means of an electronic oscillator.
SOLID-STATE. A general term that applies to any semiconductor device such as transistors, diodes, an integrated circuit. Can also be used to describe equipment that employs miniaturised modules or building blocks, integrated circuits or micre-circuits.
SOUND STAGE. The area between the two or more loudspeakers of a stereo or quad set-up where subjective sound images or imagin-

ary loudspeakers seem to be, providing a wide area of apparent sound source.
SPEECH COIL. The moving coil in a dynamic loudspeaker. It is suspended in the field of a permanent magnet and is fixed to the speaker diaphragm.
SPLICE. A joint in a length of magnetic tape. For a good strong splice, the two ends of tape should be cut at an angle of $45^{\circ}$ so that they butt together in line without any gaps.
SQUARE WAVE. An a.c. periodic waveform in which voltage alternates rapidly from a positive peak value to the negative peak value, and vice versa after a delay.

A waveform with these characteristics is ideal for testing audio equipment with an oscilloscope to test for good transient and frequency response. Square waves are also used in switching circuits.

STANDARD PLAY. An arbitrary description given to identify a spool of thick recording tape with a specified playing time according to reel size. For example, a 7in. spool will hold $1,200 \mathrm{ft}$ of "standard play" tape a 5 in , spool 600 ft . The actual playing time is then dependent on tape speed.
STANDING WAVES. The behaviour of air pressure waves in an enclosed room or box, giving rise to resonances which occur. They are created by the effects of multiple sound reflections between opposite walls and cycle at frequencies determined by the distance between them. In effect, the room acts as a resonator.
STEREOPHONY. A two channel recording and reproduction system more popularly referred to as "stereo". At the recording studio separate microphones are used for each recorded channel. The correct reproduction of stereo signals in the home gives to the listener a sense of direction of sound and thus enhances the realism.
STYLUS. A small piece of industrial grade diamond or artificial sapphire, conically-shaped, which tracks the groove in a gramophone record.
SLIOE-OUT FIXIGG SCAEW PLUG FOM ARM Sirles
SSEMELY ASSEMELY


STYLUS ARM/BAR. Cantilever which carries the pickup stylus. It is suspended at one end so that it can be allowed to vibrate in a magnetic field or transmit mechanical stresses through a piece of piezo-electric material.
SUPERIMPOSE, To record one or more signals over another without erasure, so that when a tape is played back, all recordings can be heard simultaneously. This is particularly useful if one wishes to have a spoken commentary with a musical background.
SURFACE NOISE. Nolse generated by contact of a gramophone stylus with minute particles of dust or other irregularities in a record groove. Can also be caused by excessive wear of a disc or by poor quality coating on recording tape.


TANGENT, A straight line that meets a curve or circumference at
one point only, such that it is at $90^{\circ}$ to the radial line between the centre of the circle and that point. A tangential pick-up arm is one that maintains this condition throughout its tracking across a disc.
TAPE DECK. The mechanical part of a tape recorder. It comprises the complete tape transport system, motors and drive mechanisms. It may also include the heads.
TAPE HEAD. The transducer on a tape recorder past which the tape runs during record or replay. It applies a magnetic field to the tape during the recording process and provides electrical output during replay.
T.P. Triple-play tape. Very thin recording tape of which it is possible to wind $3,600 \mathrm{ff}$. onto a 7 in . spool. This would give 180 minutes of playing time at $3^{\frac{3}{3}}$ i.p.s.
TRACING. The ability of a stylus to follow the variations or modulation pattern of a record groove.
TRACKING. The movement of the record player stylus across a gramophone record.
TRACKING ERROR. The deviation of angle between the stylus bar axis and the radial line between the disc centre and stylus point.


This is a factor applied to pickup arms with offset angle heads.
TRACKING WEIGHT. The downward force of a pick-up stylus which ensures optimum reproduction of recorded groove modulation with minimum wear of groove wall and stylus.
TRANSCRIPTION. Word commonly used to describe high quality pick-up and turntable units. Literally it is a copy or a recording of an audio programme onto tape or disc.
TRANSIENT RESPONSE. The ability of an amplifier or transducer to handle and faithfully reproduce rapid changes in signal amplitude. A very short "rise-time" is a measure of this characteristic.
TREBLE. The high frequency end of the audin spectrum.
TWEETER. A Inudspeaker de-

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signed specially for reproducing high frequencies. It is used in conjunction with a "woofer" (bass speaker) and a crossover unit for audio reproduction.

V
VARIABLE RELUCTANCE. Principle employed in certain pickups. Deflections of the stylus when playing a record, make an armature vibrate between the poles of an electromagnet. The reluctance is the ratio of magnetic force to magnetic flux in a magnetic field. Variatlons due to stylus movement create variations in the current through the electromagnet.
VERTICAL TRACKING. Stylus motion path which is near "vertical". Applies to "hill-and-dale" recordings on stereo discs.
V.H.F. Very high frequency radio band. Broadcast v.h.f. Band 2 is the 87 to 108 MHz range. Also applies to frequencies above 30 MHz for radio or television.

W
WAFER SPEAKER. Thin compact loudspeaker with an "inverted" cone where the magnet is sited forward of the cone.
WATT. Unit of electrical power, aften used to signify the signal power output from an amplifier.
WAVEFORM. A graphical representation of the relationship between voltage, current or power against time. It also provides a picture of the behaviour of signals at given frequencies.
WHITE NOISE. The random motion of electrons in a conductor which, when reproduced through a loudspeaker or phones, sounds like noise and covers a wide frequency range. It is used to test loudspeakers and phones for resonance and sensitivity.
WOOFER. A low-frequency or bass loudspeaker for reproducing musical notes in the approximate range of $25-2,500 \mathrm{~Hz}$. Employed with a "tweeter" and crossover network to reproduce a range of frequencies for audio reproduction.
WOW. Slow regular variations in the speed of a record turntable or tape transport mechanism. It is heard through a loudspeaker system as a wavering of musical pitch.

# EHPERMTEПTRL ШСR 

## Ledining By Pragical Prodebi sters

## PART 2-THE BISTABLE

WE are going to look at a very fundamental switching circuit this month that is based on the principles we developed in the last part. It is called the bistable switch-the reason for this name should become clearer as its story progresses. If you look at the basic circuit in Fig. 9a you will notice a marked similarity to the experiments we did last month; two transistors are cross connected-the base current for each being drawn from the collector circuit of the other. Notice, however, that both base resistors (R2 and R3) are permanently connected in and we are not using switches this time!

## Basic assumptions

For those who like to sweat over puzzles try this one before reading on. Assuming that the circuit is completely wired up and power is supplied use your knowledge regarding base current and driving voltages to work out whether $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$ are conducting or not conducting!

Unless you have made an assumption you should be completely stuck because the system does not seem to make sense. In stages you could have said that when power is not applied both transistors must be non-conducting hence at the instant you apply power both points A and B will be at +9 V . This set of circumstances, however, provides base current for the opposite transistor and the effect of this is to make each transistor go into conduction and both the respective voltages will fall cutting off the base current; the result of this would be to make both collectors rise back to +9 V and we are again at the start point of a vicious circle! To arrive at a sensible result we must make a practical assumption-that there is bound to be a slight difference in the current gains of the two transistors used and the one that has the higher value will go more rapidly into conduction when power is applied. Let us assume Tr 1 has a nominally higher current gain than Tr2.

When power is applied Trl will draw base current from point $B$ through R3 and the voltage at A will fall rapidly -cutting off the supply of base current to

Tr2. The latter therefore will not go into conduction and the voltage at $B$ will stay at +9 V while that at A will fall to nearly zero. Try this with your experimental circuit making and breaking the power line and you should find that it is always the same transistor that goes into conduction-in your case, of course, it might be Tr2.

Anyway we shall carry on with our assumption that after switch on point $A$ is at zero volts and we have-after all-a stable state. Let's assume


Fig. 9a: A conventional bistable circuit.


Fig. 9b: T-Dec layout for Fig. 9a.


Fig. 10a: A bistable with components modified to drive lamps direct.


Fig. 10b: T-Dec layout for Fig. 10a.
that we really wanted point $B$ to go to zero volts. For this to happen we must, somehow, make base current flow into Tr2. To do this we must make the voltage at A rise to +9 V by momentarily removing Trl's supply of base current-conveniently done by short ing point C to ground. Do just that and watch the voltage at $B$ as you make the short. Sure enough, it falls to zero while you make the short, but notice that when you have removed the shorting link from C point B stays at zero volts-not only that, but A is now at +9 V and the system is again stable. You can make the circuit revert to its original state by momentarily shorting point $D$ to ground. The circuit has two possible stable states (hence its name) and we can make it go into either of them by externally tampering with the base current supplies.

## Alternative loads

The rules of current gain apply in this circuit without undue complication and taking into account the normai current limitations of transistors you can use collector loads other than pure resistors. Fig. 10a is an identical circuit in which lamps are used; the cross coupling resistors have to be of lower values to ensure that enough base current flows to control the larger load. Alternatively connect the flying lead to points C and D and you will see that you can make LP1 go on-and stay on -when point D is quickly shorted to ground and similarly with LP2 and point C.


Fig. 11a: Alternative ways of driving low voltage lamps from a bistable. Low voltage relays (requiring less than 100 mA ) can be substituted for the lamps provided protection diodes are inserted (see part 1, last month).

If you wish to you can use the voltage swings at the collectors of the bistable transistors to drive other circuits. A selection of lamp drivers are shown in Fig. lla. Any of the single transistor driver stages (with inputs marked X1, 2, 3 and 4) can be connected to either points A or B . (We shall assume they are connected to B.) Take driver (a) which is a simple grounded emitter inverter stage. When point $B$ is $+9 V \operatorname{Tr} 3$ can draw base current through R5 and the lamp will light. Notice that we have to put a $10 \mathrm{k} \Omega$ resistor in to prevent the base emitter circuit of $\operatorname{Tr} 3$ pulling the voltage at $B$ down to +600 mV ; if that were to happen the action of the bistable would be interferred with.

Circuit (b) is a simple form of emitter follower and in this case we can do away with the $10 \mathrm{k} \Omega$ resistor. The reason for this is that when point $B$ goes "high" we immediately pass base current into Tr4 and it starts to conduct, but when this happens the voltage at its emitter rises as current flows through the lamp. The voltage rises to a value 600 mV less than the voltage at B ; the difference in voltage is due to the standard base emitter forward voltage drop associated with silicon transistors. If, say, point $B$ went to +9 V we would end up with approximately 8.4 V across the bulb. The only drawback of this circuit-although it does not bother us in this application-is that we will always lose 600 mV of driving voltage across the bulb and it will not glow quite so brightly.

In both these two drivers the lamp went on when point B went to +9 V . The remaining two drivers use pnp transistors in grounded emitter and emitter follower configurations and because they are sensitive to opposite polarity signals the lamp goes off when point $B$ goes high. In circuits it is often useful to make use of opposite polarity transistors to get this type of inversion. It is not very impressive in this application because if we had wanted any inversion we could have used point $A$ as the driving source.

## Dividing

An interesting development of the bistable circuit is the divider shown in Fig. 12a. The basic circuit of Fig. 9a is still there and you can ignore $\operatorname{Tr} 3$ because it is only a lamp driver. We have added a couple of diodes and capacitors and a few more resistors. The object of the circuit is to make Tr 1 and $\operatorname{Tr} 2$ take up their alternative stable states each time we make a single short circuit path to ground (we shall be shorting point $G$ to ground as a signal).

Let's assume that point A is at +9 V ( B will be zero and so will C , and D will be at approximately +600 mV ). The voltage at A effectively reverse biases D1, and D2 is just on the edge of conduction through R6 to point B-which is just slightly more

Fig. 12a: A bistable with built in gating so that it switches in alternate directions each time point $G$ is connected to ground. This is is connected to ground. This


Fig. 12b: T-Dec layout for Fig. 12a.



Fig. 13c: Veroboard layout for Fig. 13a.
negative than $D$. The potential at $G$ (without the shorting link made) will be just under IV because of the potential divide action of R7 and R8.

By repeated dabbing of the shorting link to ground you can make the lamp go on and off alternatively. There is something that you have to note, however. The circuit is very sensitive and you must make very good clean makes and breaks of the shorting operation; it is very easy to accidently give a double "pulse" when you think you have, in fact, only made one. R7 has deliberately been made a high value to allow time for the voltage at G to recover and this
helps to eliminate what appears to be erratic action. Nevertheless the time constant of $1 \mathrm{M} \Omega$ with the $0 \cdot 1 \mu \mathrm{~F}$ capacitors is still quite short so do not be too surprised if sometimes the lamp appears not to respond. What actually happens is that the lamp switches on and back to off so quickly you do not see it happen! Try reducing R7 to $100 \mathrm{k} \Omega$ and R8 to $10 \mathrm{k} \Omega$ and you will deliberately aggravate the problem. In a circuit of this nature it is wiser to use some form of non-mechanical switch to do the triggering so that we lose the "bounce' problem.
When you short point $G$ to ground there will be a change in voltage at point E by about 0.8 V in a negative direction but because D1 is reverse biased there will be little effect on the base circuit of Trl. On the other hand the similar drop developed at point $F$ will put D2 into sufficient conduction to momentarily drop the voltage at D and hence remove the base current from $\operatorname{Tr} 2$. The voltage at B will rise and bistable action will take place and the voltage at A will fall as the circuit takes up its other stable state. The set of circumstances is now reversed and if the shortening link is removed to allow the two capacitors to regain their original equilibrium the operation can be repeated to make the circuit flip back to its first stable state.

## EXPERIMENTAL WORKSHOP

-continued from page 644
Fig. l3a shows a very crude electronic form of trigger for the divider. A sudden transition of from near darkness to full room light on PCCl will make Tr 4 go suddenly into conduction and the voltage at the junction of C 1 and C 2 will fall rapidly to zerostimulating the divider. Switch off the room light and switch it on again and the circuit reverts. The reason for doing this experiment is to show that it needs two complete operations of switching the room light on and off to make the lamp in the circuit go on and off once. We are effectively dividing the number of operations by a factor of two-the reason why the circuit gets its name. While doing this experiment it is worth noting that slow signals do not have any effect on the divider; slowly covering and uncovering PCCl will not be an effective trigger-you need the very fast action of switching a light on and off to get reliable results. The reason for this is that Cl and C2 are not able to pass slow waveform signals. You need a wide range of lighting levels to make this circuit switch rapidly but there are a range of switching circuits called "triggers" which speed up the action of slow stimuli. We shall be looking at this effect next month.

## TO BE CONTINUED

## DO YOU HAVE A STANDARD SIZE "COMPACT CASSETTE" TAPE RECORDER ?

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We can still accept handwritten letters, tool *We can only send cassettes to U.K. addresses.


## Mum writes in

I am writing as a 'Mum' of one of your enthusiastic readers. Do you by any chance know the ages of some of your younger readers?

My son Edward is $6^{1}{ }_{2}$ years old and has taken Practical Wireless for over a year now. It is used for bedtime stories together with Aesop's Fables (I insist on that!)

Thus one outcome of the enthusiasm of one small boy is that his mother now knows the difference between a diode and a triode, step-up transformers and step-down transformers.

I must confess I find the whole subject of wireless very difficult and show no enthusiasm myself but if you could see a certain little boy's eyes light up when "P.W." as it is affectionately called arrives, it persuades me once more to plough through details of digital multimeters and who is selling what component at the cheaper price!

Through your magazine, Edward bought a pocket multimeter from an advertiser, so we are all having our resistance tested!Mrs. Pat Russell (Herts.).

## Darkroom thermometer

Some time ago, you published an article by R. A. Bottomley on the construction of a darkroom thermometer. I have built this unit with great success but I found it was necessary to increase R3 to obtain balance at the mid-point on the scale. I arranged for $24^{\circ}$ and $29^{\circ}$ by duplicating R3, VR1 and R4. R3 then became $1 \cdot 5+2 \cdot 2 k$ and $1 \cdot 5+3 \cdot 3 \mathrm{k}$. A changeover switch completed the revised arrangement, the two temperatures being respectively for developing colour film and colour prints. The meter I used was a Japanese Henelec 0-100uA.-C. G. Dahl (Surrey).

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6. Printed circuit board,
7. Keyboard panel.
8. Electronic components pack (diodes, resistors, capacitors, transistor)
9. Battery clips and on/off switch.
10. Soft wallet


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# GOING QUADRAPHONIC <br> PW  <br> PART2 D.BDLLEN <br> <br> © 0 recardings <br> <br> © 0 recardings SO pearrings SO pearrings $\square$ Discrete CD-4 recordings $\square$ Discrete CD-4 recordings SURROUNO SOUND 

 SURROUNO SOUND}

It is easy to see how several resistance networks, plus variable separation, could be combined by switching to offer multi-system decoding, but before considering this it would be as well to look first at the circuits of Units A and B.

## Unit A circuit

The circuit of unit A is shown in Fig. 12. Trl and Tr2 act as unity gain phase splitters, with an input impedance of $47 \mathrm{k} \Omega$ and an output impedance of about $1 \mathrm{k} \Omega$. Mixers Tr3-Tr6 are of the virtual earth type, with an output impedance of $2 \mathrm{k} \Omega$, and a gain of two when employed with input resistors of a nominal $100 \mathrm{k} \Omega$.

Apart from matrixing, the mixers will accept additional input resistors for mixing in other signals such as reverberation or echo. To keep noise to a minimum, and maintain the correct working point for each transistor, it is advisable to use metal oxide resistors of 5 per cent tolerance or better in the circuit of Fig 12.

## Unit B circuit

A constant phase shift of $90^{\circ}$ throughout the audio spectrum presents circuit problems. It is arguable how wide the frequency bandwidth needs to be. Some authors maintain that the ear is incapable of detecting phase differences from loudspeakers beyond the limits of $100 \mathrm{~Hz}-8 \mathrm{kHz}$, while decoder manufacturers are currently aiming at a constant phase shift bandwidth of $20 \mathrm{~Hz}-20 \mathrm{kHz}$. Some commercial decoders seem to get by with a bandwidth of $100 \mathrm{~Hz}-10 \mathrm{kHz}$, with a variation of $\pm 10$ per cent on $90^{\circ}$ so this standard was adopted for the PW Q4 decoder. The graph of Fig. ll shows the phase shift characteristic of the unit B circuit.

A $90^{\circ}$ phase shifter consists of a phase splitter followed by a network of resistors and capacitors, but a simple splitter of the type used in unit A has insufficient power output to drive such a network

effectively, so IC operational amplifiers were employed instead.

In the circuit of unit $B$, left and right channels are identical and it will suffice to examine the left channel only. ICl package contains two operational amplifiers of the 741 type, here labelled A and B. The inverting input of amplifier $B$ is connected to the output of amplifier A, which also inverts. Operational amplifier A has a gain of $2 \cdot 3$ and $\mathbf{B}$ a unity gain, so the combined outputs of the amplifier pair will be $180^{\circ}$ out of phase and $2 \cdot 3$ times the level of the input signal; this gain is just sufficient to offset the gain loss in the following phase shift network.


Fig. 11 : Phase shift characteristics.


Fig. 12: Circuit of unit A.


Fig. 13: Circuit of unit B.


## Q4 COMPONENTS LIST

| Resistors | UNIT A |  |
| :---: | :---: | :---: |
|  |  |  |
| R1 $180 \mathrm{k} \Omega$ | R13 | $43 \mathrm{k} \Omega$ |
| R2 100ks | R14 | $330 \mathrm{k} \Omega$ |
| R3 $1 \mathrm{k} \Omega$ | R15 | $4 \cdot 7 \mathrm{k} \Omega$ |
| R4 1k $\Omega$ | R16 | $100 \Omega$ |
| R5 180k $\Omega$ | R17 | $43 \mathrm{k} \Omega$ |
| R6 100k $\Omega$ | R18 | $330 \mathrm{k} \Omega$ |
| R7 $1 \mathrm{k} \Omega$ | R19 | $4.7 \mathrm{k} \Omega$ |
| R8 $1 \mathrm{k} \Omega$ | R20 | $100 \Omega$ |
| R9 $43 \mathrm{k} \Omega$ | R21 | $43 \mathrm{k} \Omega$ |
| R10 330k $\Omega$ | R22 | $330 \mathrm{k} \Omega$ |
| R11 $4 \cdot 7 \mathrm{k} \Omega$ | R23 | $4.7 \mathrm{k} \Omega$ |
| R12 100 2 | R24 | $100 \Omega$ |
| All $\frac{1}{2}$ W metal oxide |  |  |

## Capacitors

C1-C8 $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic
Transistors
Tr1-Tr6 BC109
Miscellaneous
0.1 in pitch Veroboard $0.9 \mathrm{in} \times 4 \mathrm{in}$; terminal pins.

| Resistors |  | UNIT B |  |
| :---: | :---: | :---: | :---: |
|  |  |  |  |
| R25 | $43 \mathrm{k} \Omega$ | R42 | 240S |
| R26 | $43 \mathrm{k} \Omega$ | R43 | 4-3k $\Omega$ |
| R27 | $100 \mathrm{k} \Omega$ | R44 | $4 \cdot 3 \mathrm{k} \Omega$ |
| R28 | $100 \mathrm{k} \Omega$ | R45 | $30 \mathrm{k} \Omega$ |
| R29 | 100k $\Omega$ | R46 | $30 \mathrm{k} \Omega$ |
| R30 | $100 \mathrm{k} \Omega$ | R47 | $3 \cdot 6 \mathrm{k} \Omega$ |
| R31 | $100 \mathrm{k} \Omega$ | R48 | $1 \cdot 5 \mathrm{k} \Omega$ |
| R32 | $100 \mathrm{k} \Omega$ | R49 | $3.6 \mathrm{k} \Omega$ |
| R33 | $100 \mathrm{k} \Omega$ | R50 | $1.5 \mathrm{k} \Omega$ |
| R34 | $100 \mathrm{k} \Omega$ | R51 | $100 \mathrm{k} \Omega$ |
| R35 | $100 \mathrm{k} \Omega$ | R52 | $39 \mathrm{k} \Omega$ |
| R36 | $100 \mathrm{k} \Omega$ | R53 | $100 \mathrm{k} \Omega$ |
| R37 | $5 \cdot 1 \mathrm{k} \Omega$ | R54 | $39 \mathrm{k} \Omega$ |
| R38 | $5 \cdot 1 \mathrm{k} \Omega$ | R55 | $1 \mathrm{k} \Omega$ |
| R39 | $620 \Omega$ | R56 | $1 \mathrm{k} \Omega$ |
| R40 | $240 \Omega$ | R57 | $1 \mathrm{k} \Omega$ |
| R41 | $620 \Omega$ | R58 | $1 \mathrm{k} \Omega$ |

## Capacitors

| C9 | $0 \cdot 12 \mu \mathrm{~F}$ |
| :---: | :---: |
| C10 | $0.022 \mu \mathrm{~F}$ |
| C11 | $0.12 \mu \mathrm{~F}$ |
| C12 | $0.022 \mu \mathrm{~F}$ |
| C13 | $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |
| C14 | $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |
| C15 | $0.12 \mu \mathrm{~F}$ |
| C16 | $0.022 \mu \mathrm{~F}$ |
| C17 | $0 \cdot 12 \mu \mathrm{~F}$. |
| C18 | $0.022 \mu \mathrm{~F}$ |
| C19 | $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |
| C20 | $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |
| C21 | $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |
| C22 | $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |
| C23 | $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |
| C24 | $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic |

All capacitors $\pm 5 \%$ polycarbonate unless otherwise specified

## Transistors

Tr7 BC109 Tr8 BC109

## Integrated Circuits <br> IC1 747C 14 pin DIL <br> IC2 747C 14 pin DIL

## Miscellaneous

0.1 in pitch Veroboard $1.8 \mathrm{in} \times 3 \mathrm{in}$; terminal pins

Additional components for multi-system decoder
Resistors

| $R 59$ | $100 \mathrm{k} \Omega$ | $R 66$ | $110 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- |
| $R 60$ | $100 \mathrm{k} \Omega$ | $R 67$ | $100 \mathrm{k} \Omega$ |
| $R 61$ | $100 \mathrm{k} \Omega$ | $R 68$ | $100 \mathrm{k} \Omega$ |
| $R 62$ | $100 \mathrm{k} \Omega$ | $R 69$ | $140 \mathrm{k} \Omega$ |
| $R 63$ | $110 \mathrm{k} \Omega$ | $R 70$ | $140 \mathrm{k} \Omega$ |
| $R 64$ | $110 \mathrm{k} \Omega$ | $R 71$ | $140 \mathrm{k} \Omega$ |
| $R 65$ | $110 \mathrm{k} \Omega$ |  | $R 72$ |

All resistors $\frac{1}{2} W$ metal oxide
Potentiometers
VR1 $100 \mathrm{k} \Omega$ linear dual-gang
VR2 $100 \mathrm{k} \Omega$ linear dual-gang
VR3 $100 \mathrm{k} \Omega$ linear
VR4 $100 \mathrm{k} \Omega$ linear
VR5 $22 \mathrm{k} \Omega$ linear
VR6 $22 \mathrm{k} \Omega$ linear
VR7 $22 \mathrm{k} \Omega$ linear
VR8 $22 \mathrm{k} \Omega$ linear
VR9 $22 \mathrm{k} \Omega \log$ (two dual-gang, see text)
Capacitors
C25 $0.22 \mu \mathrm{~F}$
C26 0.22 $\mu \mathrm{F}$
C27 $0.1 \mu \mathrm{~F}$
C28 $0.1 \mu \mathrm{~F}$
C29 $0.1 \mu \mathrm{~F}$
C30 $0.1 \mu \mathrm{~F}$
C31 $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic
C32 $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic
C33 $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic
C34 $1 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic
All capacitors tubular polyester unless otherwise specified

## Switch

S1 12 pole 3 way (RS Components miniature Makaswitch with three 4 pole 3 way wafers)
Sockets
SK1-SK10 phono panel mounting
SK11 $\quad 0 \cdot 1$ in pitch edge connector cut down to 19 way (see text)

## Miscellaneous

$0 \cdot 1$ in pitch Veroboard 1.9 in $\times 3$ in and 2 in $\times 1-2 \mathrm{in}$; knobs; phono plugs; 18 s.w.g. aluminium sheet $20 \mathrm{~cm} \times 29 \mathrm{~cm}$ and $14.5 \mathrm{~cm} \times 35 \mathrm{~cm}$.

## POWER SUPPLY

## Resistors

R77 $1 \mathrm{k} \Omega 10 \% \frac{1}{2} \mathrm{~W}$ carbon

## Capacitors

C35 $1000 \mu \mathrm{~F} 35 \mathrm{~V}$ electrolytic
C36 $1000 \mu \mathrm{~F} 25 \mathrm{~V}$ electrolytic
C37 $0 \cdot 1 \mu \mathrm{~F}$ tubular polyester
Transistors
Tr9 BFY52
Diodes
D1 1N4001
D2 1N4001
D3 BZX61 (1-3W zener)

## Transformer

T1 0-20V, 0-20V (RS Components L.td. miniature mains transformer)

## Miscellaneous

0.1 in pitch Veroboard $1.9 \mathrm{in} \times 2.1 \mathrm{in}$; TO5 heat sink; terminal pins.

The phase splitters in Fig. 13 are Tr7 and Tr8. Phase shift capacitors for the left channel are C9, C10, C15, and C16, and these must have a tolerance of $\pm 5$ per cent or better if the performance indicated in Fig. 11 is to be realised. All resistors used in the Unit B circuit should also be 5 per cent or better and preferably of the metal oxide type.

The input impedance of unit B is $43 \mathrm{k} \Omega$ and the output impedance from the phase splitters approximately $1 \mathrm{k} \Omega$. As the $0^{\circ} \mathrm{L}$ and R outputs are only to be connected to the phase splitters of unit A their impedance may be ignored.

## Multi-system decoder

Fig. 14 shows the circuit of a multi-system decoder based on units A and B. In the RM position of switch S1, with VR1 and VR2 set to mid-track the circuit adheres to the Schieber code with constants of 0.92 and 0.38 , giving 3 dB separation with a similarly coded recording. When VR1 and VR2 sliders are at the earthed ends of their tracks, left to right separation is virtually infinite. and front to back separation is zero, thus giving centre of the room stereo, and an effect similar to stereophones. At the other extreme, with sliders at the live ends of tracks, left to right separation will be zero and front to back separation is infinite, giving a stereo recording as centre front mono with centre back ambience.

Adjustment of VR1 and VR2 will cover the codes of all early American material, and will also compensate for the widely differing recording techniques used for stereo, to give a well balanced surroundsound result. The resistors associated with the RM decode are R63-R66 and R73-R76.

With Sl switched to QS, the RM resistors are rearranged for Sansui-Pye decode, when VR1 and VR2 are at mid-track. Here, adjustment of VR1 and VR2 can be used to alter the sound stage proportions and to compensate for an oblong speaker array.

In the SQ decode S1 position, resistors R67-R72 are brought into circuit to satisfy the CBS decode constants of 1 and 0 on the front channels, and 0.707 on the back channels, with the required phase shifts in the back channels. At the same time, the controls and resistors associated with RM and QS are rendered inoperative, and VR3 and VR4 are brought in to control SQ front and back separation. With VR3 and VR4 at mid-track, left to right separation will be 10 per cent or 20 dB , and this setting will give satisfactory results with SQ recordings where a strong centre front image is not important. The blend values may be varied to compensate for an unusual speaker layout, or to boost a centre front image.

SK3 to SK6 in Fig. 14 are for discrete inputs, and may be used at any setting of Sl when the twochannel inputs to SK1 and SK2 are switched off. Using two and four channel inputs simultaneously would give a mix between the two, so SK3-SK6 can also be employed for mixing in other signals while decoding matrixed material. An output from a reverberation unit could be fed into SK5 and SK6 for increased ambience on certain recordings, or a voice announcement could be mixed into any one of the four channels while music is playing.


Fig. 15 : Power supply circuit.

## Power supply

The supply requirements of units $A$ and $B$ together are $33-40 \mathrm{~mA}$ at 20 V with a low ripple content and a low supply impedance throughout the frequency range. This is provided by the semiregulated supply circuit of Fig. 15.

C36 and R77 time constant ensures a slow-rise switch on to prevent loudspeaker 'plop' and at the same time keeps impedance down at very low frequencies. C37 offers a low impedance at high frequencies.

The article to follow next month will give constructional details of the multi-system decoder, with notes on testing and setting up.


## P.W. STUDENT OSCILLOSCOPE

On page 340 of the August issue a Veroboard layout was shown. To assist constructors, the co-ordinates of the conductor breaks are listed below:

| A43 | B1 | C4 | E15 | F24 | G15 | H5 | K66 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
|  | B4 | C76 | E24 | F28 | G19 | H15 |  |
|  | B27 |  | E36 | F33 |  |  |  |
|  | B83 |  |  |  |  |  |  |
| L54 |  | M57 | N34 | O39 | P24 | Q48 | R8 |
| L67 | S14 |  |  |  |  |  |  |
|  | M63 | N39 | O43 | P39 | Q74 | R23 |  |
|  | M66 | N51 | O48 | P48 | Q80 |  |  |
|  | M72 | N57 | O76 | P51 |  |  |  |
|  |  | N63 | O80 | P76 |  |  |  |
|  |  | N66 |  | P80 |  |  |  |
|  |  |  |  |  |  |  |  |
|  | T5 | U13 | V36 | W1 | W63 | X43 |  |
|  | T25 | U75 | V53 | W5 | W67 |  |  |
|  | T32 | U80 | V75 | W40 | W73 |  |  |
|  |  |  | V80 | W50 | W80 |  |  |
|  |  |  |  | W59 | W83 |  |  |
|  |  |  |  |  |  |  |  |

## ON RECENT DEVELOPMENTS

ON ANIMPULSE

WHILE it is always interesting to record the latest developments in electronic components, instruments; etc, it often works out that an application of established principles and equipment is equally fascinating.
One such application is that of amplifying tiny-really tiny-electrical signals or impulses and causing these to control things. Human beings have been doing this since the year one. Signals from the brain control limbs, etc. The twist in this story comes when you take signals generated by the body and couple them to external sources.
A series of experiments has been conducted (another series is in current progress) which shows that well over a dozen different muscle patterns can be produced on cue. The idea is that the subject thinks of.raising (s.ay) his right thumb but does not actually move it upwards. Gold electrodes taped to the hands are able to detect these impulse commands.

The experiments to date have involved a subject causing diffierent patterns in an array of lights. Consider the possibilities. You could think that the grass needed cutting-and immediately a radiocontrolled E-type lawn mower would belt out of the shed. Obviously there are limits. Imagine being introduced to Raquel Welch, an experience which should produce an impulse or two in most men. Perhaps a built-in manual control could restrict reaction on such occasions to a.well willed wink.

## PACEMAKERS

Pacemakers, those devices which keep an internal eye on hearts which don't function as reliably as they should, have to be replaced surgically about every two years. Nuclear-powered pacemakers can last ten times as long but can cost five times as much compared to "conventional" ones. They also radiate and are more bulky and heavier than their "conventional" counterparts.

A new pacemaker has arrived. It can be implanted in the patient using only a local anaesthetic. This unit triggers and "fires" only if the heart doesn't beat after a predetermined time. There's more to come too. The unit may be recharged by the patient! The user has a portable recharging unit and a special "vest" which is donned. A special acoustic coupler also enables the wearer to telephone his doctor and transmit heart signs and signals directly for study.

## TEMPIS FUGIT

In a previous issue, I wrote of electronic clocks and watches. This seemed to stir a chord in some people and a few even wrote to me. Prices for these items will doubtless come down as production goes up. Not all electronic time pieces cost hundreds of pounds. An electronic stop-watch about to launch itself onto the American market is reckoned to sell there for less than $\$ 200$. It has a crystal oscillator, LED display and a rechargeable battery. A 28 -pin C.M.O.S. chip is employed and the watch measures $0 \cdot 5 \mathrm{in}$. wide, $1 \cdot 4 \mathrm{in}$. long and 0.75 in . deep. The 24 hr readout will happily stay illuminated for about 12 weeks before the battery needs recharging and there is a small button which will switch off the display if it is desired to conserve power.
The electronic watch market in the U.S. alone is estimated at $\$ 50$ million for this year which might account for all the activity. One manufacturer has recently introduced what is claimed to be the first watch ever which employs field effect liquid crystal displays.

One of the interesting things about the particular display used in these watches is that it is the reverse of the image usually associated with liquid crystal displays. Normally, these adopt a frosted-glass effect for the legends against a mirror background. The field effect LCD's absorb the incident light via polariser filters and the legends (figures, letters, etc) are easily
seen as dark outlines against a diffused white background. The lowest price model in this range of wrist watches is around $\$ 150$. The field effect displays are guaranteed by the manufacturer for 3 years, but it is expressed that they will last for nearer 10 years. Looks as though proud owners will be taking their timepieces to electronic beauty salons every so often for a face change?
One of the most vital parts in the electronic watch, employing a crystal oscillator, is the crystal itself-the electronic heart of the beast. Favourite crystal frequency is 32 kHz which is then divided down to supply pulses which in turn feed the displays via display drivers. But there's a snag. Difficulty is being experienced in some areas because the clock/watch maker cannot get enough crystals at 32 kHz .

## THEY'RERESISTANT!

One company offers some intriguing resistors which are described as ceramic-insulated and flame-proof. Apparently, these will not burn even if the open flame of a blow-lamp is played on them. Well I'm blowed! Resistance values range from $1 \Omega$ to $60 \mathrm{k} \Omega$ in wattage ratings from 1-10 Watts.

## POWER STRUGGLE

Remember the first transistors? Red spot for a.f. with a cut-off around 800 kHz . Then White spot transistors which, with luck, managed the $1 \cdot 8-2 \mathrm{MHz}$ Amateur band. They were delicate and couldn't handle too much power. The latest power transistors from one manufacturer are rated to handle 400 V at 60 A (down to 100 V at 200A). A 500 V 100A component is in the design stage. Note: these are transistors not thyristors. Perhaps we have a struggle for Power here?
Gimberz

# TAKE 2® 

## A series of simple transistor projects, using not more than twenty components.

Before you complain that you have been misled by this month's title I had better explain that this device enables you to play records via any type of transistor portable radio without having to make any internal connections to the radio. Thus it is ideal for use with the modern miniature portables that do not have pick-up sockets and thus might save Dad a bit of money when "junior" demands a record player! Apart from the unit to be described you will, of course, need a turntable unit with a CRYSTAL CARTRIDGE pick-up. We stress crystal cartridge not only because it is the cheapest but because the "Radio-Gram" will not work with other types.

## Circuit

The circuit shown in Fig. 1 is basically an oscillator that can be tuned with TC1 to operate between about 700 kHz and 1.5 MHz (i.e. across the range of the medium wave band). The amplitude of oscillation is modulated by direct connection of the pick-up across R2. The modulation process works simply by shifting the bias level of the transistor at audio frequencies and this is remarkably effective. C1 is necessary to help decouple the junction of R1 and R2 to r.f. and it also prevents overmodulation at high frequencies.

## Construction and Testing

The coil is wound on a 4 to 6 in length of $3_{8}$ in diameter ferrite aerial rod, Fig. 2, but when doing this be careful to take note of the sense and start points of the windings; if the connections from the 5 turn feedback coil are reversed the circuit will refuse to operate! The BC108 used should have a gain in the order of 200 , which is in the centre of the production spread, but the circuit will operate with devices of widely differing gain.

If, on test, the signal is distorted it is likely that the transistor has too high a gain and the carrier is being clipped. To prevent this increase the value of R3 and reduce R4, keeping the sum of the two about $2 \mathrm{k} \Omega$, to introduce a little more negative feedback. Conversely, if the signal strength is weak change the values in the opposite direction. No problem should be encountered here, however, so we have made R3 and R4 fixed values instead of using a more expensive preset.

The unit can be built on veroboard and fitted within a screened metal box. The signal is fed out via a screened lead (very loosely coupled to the ferrite rod as shown) and the centre conductor connected into the aerial socket of the transistor radio. To operate it, select a quiet portion of the medium waveband, put on a record and adjust TCl until the music is clearly received. First tuning is best carried out on the receiver.
The current drawn by the Radio-Gram is minute, less than 100 microamps, so any small 9 V battery will operate it for almost the battery's shelf life.


Fig. 1 above, shows the circuit of the Radio Gram. One end of the output coupling coll Is leff free.
Fig. 2, below, is a suitable layout on veroboard.

$\star$ components list


# is this the price you pay? 

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Baker Me Luxe
Baker Major 12
Kef T27
Kef TIS
Kef 8110
Kef B200
Kef B139
Kef DN8
Kef DN9
Kef DNi3
Fane. Pop 100 watt $8 / 15$ ohm Fane Pop 60 watt $8 / 15 \mathrm{ohm}$ Fane Pop 50 watc $8 / 15$ ohm Fane Pop 25/2 25 watt 8/15 ohm Fane Pop 15 watt $8 / 15$ ohm Fane Crescendo $15^{\prime \prime} 8$ or 15 ohm Fane Crescendo 12A 100 w 8 or 150 hm Fane 807T $8^{\prime \prime} \mathrm{d} / \mathrm{croll} / \mathrm{s}^{2} 8$ or 15 ohm Fane 808T $8^{\prime \prime} \mathrm{d} /$ cone 8 or 15 ohm Goodmans Axent 100 tweeter Goodmans 8P 8 or 15 ohm Goodmans IOP 8 or 15 ohm Goodmans 12P 8 or 15 ohm Goodmans 15P 8 or 15 ohm Goodmans 18P 8 or 15 ohm Goodmans Twinaxiom 8 Goodmans Twinaxiom 10
Elac $9 \times 55^{\prime \prime} 59$ RM 109 ! 5 hm .
59 RMII 148 ohm
Elac $6 \frac{1}{2}$ " $\mathrm{d} / \mathrm{c}$ roll/s 8 ohm
Elac $6{ }_{3}^{\prime \prime}$ " d/cone 8 ohm
Wharfedale Bronze 8 RS/DD
Wharfedale Super 8 RSIDD Wharfedale Super 10 RS/DD
Coral $6 \frac{1}{2}$ " d/cone roll/s 8 ohm Siran $6 \frac{1^{\prime \prime}}{} 3$ or 8 ohm
Richard Allan $12^{*} \mathrm{~d} / \mathrm{c} 3$ or 15 ohm $10^{\prime \prime} \times 6^{\prime \prime} 3,8$ or 15 ohm
$8^{* *} \times 5^{*} 3$ or 8 ohm
$21^{\prime \prime} 64 \mathrm{ohm}$ or 70 mm 80 ohm Adastra Hiten $10^{*} 10 \mathrm{w} 8$ or 15 ohm Eagle DT33 dome tw
Eagle HT 15 tweeter
Eagle CT5 tweeter
Eagle CTIO tweeter
Eagle MHT10 tweeter
Eagle FR4
Eagle xover CN23, 28, 216
Sp. matching transformer 3-15 ohm Celestion MFIOOO 25 w harn 8 or 15 oh

Celestion PS8 (for Unilex) Celestion GI2M 8 or 15 him Celestion G12H 8 or 15 ohm Celestion GI5C 8 or 15 ohm Celestion GI8C 8 or 15 ohm Car Stereo speakers-ask for leaflet.


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## W.S.POEL G8CYK

THERE can be little doubt that the wobbulator method is by far the best means of setting up an IF strip for optimum bandpass characteristic, combined with optimum sensitivity. There are a number of commercial units made, aimed mainly at the 'trade' and priced accordingly. However, the wobbulator described here costs about £l, whilst providing all the necessary features. An oscilloscope is necessary and preferably one with a simple means of getting at the timebase. (Horizontal X output).

## PRINCIPLE OF OPERATION

The wobbulator consists basically of a voltage controlled oscillator whose frequency is being constantly swept across the IF band of the receiver in question. The control is by means of a varicap diode, which can either be one of the purpose-made devices, or more simply, a power rectifier, such as the 1N4001/2/3.


Fig. 1: Typical waveform of a timebase oscillator, used to control the sweep of the wobbulator.

The timebase output on an oscilloscope looks like Fig. 1, which is applied to the diode so that the voltage on the diode is constantly changing in step with the oscilloscope trace. So we have three variables coordinated, namely:-

1. The trace.
2. The voltage on the varicap diode.
3. The varicap capacity and consequently the wobbulator frequency.


Fig. 2: Interconnections of the scope, wobbulator and If strip being aligned.

As the frequency sweeps through the IF' frequency of the receiver, the IF response curve is displayed on the scope, which is itself monitoring the output from the receiver detector, Fig. 2.

## CIRCUIT

The heart of the device is the single FET Vackar VFO, Fig. 3. The choice of FET is very large, and almost anything in the standard N -channel series will do, e.g. 2N3819, 3823E, TIS88, BFW10. Remember to check the base connections.

The centre frequency is mainly determined by L1, C3 and C5 and VC1. By experimentation with values, it is possible to make the VFO operate past 50 MHz , though most sets designed for $A M$ operation use an IF between 455 and 470 kHz . An ordinary 455 or 470 kHz IFT can be used for L1, the internal capacitor being disconnected.

It is advisable to check the timebase output from the 'scope when choosing the varicap diode, since many scopes have a high voltage at the $X$ output. (The author found out the hard way!) Choose a diode with adequate PIV ratings.

## CONSTRUCTION

It will be seen from the diagrams that the layout is quite straightforward. A printed circuit board layout is given, Fig. 4, though at 455 kHz there is no objection to Veroboard if that is considered


General view of the prototype wobbulator. Co-axial sockets could be used instead of the terminal block.

Fig. 3: Circuit of the wobbulator. VCl may be any suitably sized variable of about 200pF

Fig. 4: The printed circuit board, actual size, with component layout.


more convenient. Relative positions are not critical, and the wobbulator can very largely be adapted to fit any convenient case.

No particular types of sockets are necessary since most people seem to have adopted their own 'standard,' most probably the standard TV coax system. Reraembering the comments on the timebase output it is best to use either a shielded plug or directly soldered connections to avoid shocks when se.aing up.

## OPERATION

The current drawn by the wobbulator is typically 5 mA , and any big discrepancy should be investigated before going further. When the system is coupled


The p.c.b. is mounted in the box with bolts and spacing nuts. General layout is not at all critical. An on/off switch could form part of VRl.


Fig. 5 : Various i.f. response curves, oblained with the set-up of Fig. 2.
together as shown in Fig. 2, set the frequency of the wobbulator approximately by the variable capacitor, until a trace of the IF is seen on the scope screen. The sweep frequency should be set at around 50 Hz for best results when a 50 Hz buzz from the set's loudspeaker will be heard when the wobbulator is correctly aligned. The centre frequency of the IF can then be determined by using an accurately calibrated signal generator, Fig. 5 a.

The output from the signal generator is coupled to the IF strip in the same way as the wobbulator, namely a few turns of wire placed near to the mixer input/output. Remember to disable the set's local oscillator before alignment, since this will
otherwise lead to spurious traces. A few traces likely to be seen are shown in Fig. 5b-e.

The sweep width potentiometer determines the length of sweep, which may represent from 0 to 20 kHz . The narrower the sweep, the more of the IF is displayed on the scope, but it must sweep at least as far as the ends of the IF bandwidth, Figs. 5f-g.

There only remains to align the IF by adjusting the cores in the IFT's to get the desired response, Bandwidth can be determined by using the signal generator to determine the points on the response curve corresponding, say, to 452 and 458 kHz ( 455 kHz centre frequency).

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[^9]


THE International Short Wave Club conducts a poll every three years to determine the most popular short wave stations.
Listeners are asked to participate by sending to the ISWC, 47 Harridge Road, Leigh-on-Sea, Essex SS9 4HE; a list of their five most popular short wave stations in order of merit, together with a short note of not more than 30 words why they consider their No. 1 choice to be their most popular station. More than 30 words will automatically disqualify any listener from any award that may be given in connection with the Poll. The final date for voting is December 31st. 1973.

## Ex-W.D. Equipment

The short paragraph at the end of the September column announcing that I would be devoting some space to the subject of ex-government Communication receivers has sparked off an even larger than usual postbag. The problem has become so bad that I have had to install a larger letterbox to assist the postman. I would, however, like to remind you all that any letter requiring an answer should be accompanied by a stamped addressed envelope.

I still require information on some of the rarer receivers and if any of you can supply me with this I can assure you that it will be well treated and returned as soon as possible. In particular I would be grateful for any information on the ex-Admiralty B40 receiver.

## Readers' Logs

The first log this month comes from Alan Carpenter who lives in Aborfield near Reading. Alan's equipment consists of a Heathkit 'Mohican' GC-1U receiver and its 50 inch telescopic aerial. However, a 70 foot long-wire: inas added to pull in Radio Ceylon.
4915 Radio Ghana, Accra, nx. in English at 2245.
6250 World Music Radio in English at 0900.
7310 Radio Vilnius, Lithuania. English at 2230.
11725 Radio Ceylon with Religious programme at 1700.

11725 R. Free Europe, Lisbon. Pop music at 2315.
11730 R. Tashkent, Uzbek in English at 1400.
15445 R. Nacional de Brasilia. English at 2230.
A. W. Guzelian of Coniston in Lancashire has an HRO receiver and a 45 foot long-wire aerial which enabled him to hear:
7105 R. Nacional de Espana, in Spanish at 1300.
9555 R. Baghdad, Iraq in English at 1940.
11350 R. Pyongyang, N. Korea, English at 2100.
11765 R. Yerevan, Armenia noted at 2030.
11880 Voice of Turkey, in English at 2200.
15115 R. Tashkent in English at 1400.
15415 R. Kuwait in English at 1730.
Simon Wormleighton and J. P. Fletcher of Rendcomb College, Cirencester, Glos. have again sent in a report using the following equipment, Astrad-Altair with 80 foot long-wire; HRO with 8 metre folded dipole; Bush PB63 with 35 foot long-wire. Stations logged included:
6010 R.T.B., Belgium in French at 1505.
9022 Voice of Iran in English at 2005.
9600 R. Kuwait. Nx. in English at 1730.
9670 Adven!ist World Radio, Lisbon at 0935.
11730 R. Vilnius, Lithuania in English at 2250.
11850 R. Norway in English at 0824.
15325 R. Canada International at 1634.
Chris Greenway and John Greenlees sent in a combined log from Brandiston in Norfolk. The equipment used being a Lafayette HA600A receiver; Codar PR40 preselector; 100 foot long-wire; 15 MHz dipole and homebrew A.T.U. An extract from their $\log$ with more than 60 entries is as follows:
9545 R. Ghana, Accra in English at 2135.
9655 R. Damascus, Syria, English at 2000.
11650 R. Bangladesh with music at 1715.
11710 R. Kiev, Ukraine noted at 1945.
11725 R. Ceylon in English at 1700.
11935 R. Pakistan, news in English at 1725.
15105 R. Grenada, Windward Islands at 2120.
15105 BBC, Ascension Is. relay noted at 1510 .
15185 R. Nigeria, Lagos, in English at 0715.
15195 R. Japan, news in English at 2215.
15265 R. Afghanistan in English at 1800.
15310 BBC, Tebrau, Malaysia relay at 1745.
The last log for this month comes from Christopher Hodgson of Sunderland who used a Codar Multiband6 receiver, the PW A.T.U. and a 50 foot long-wire aerial to hear the following stations:
6130 Radio Norway at 1800. (Sundays).
9005 R. Tehran, the Voice of Iran at 2000.
9840 Voice of Vietnam, Hanoi noted at 1815.
15012 Voice of Vietnam, Hanoi noted at 1800.
15165 Radio Denmark in Danish at 1400
15185 Radio Finland at 1810.
15325 R. Canada International, s/off at 1313.

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## MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

AW. GUZELIAN (Coniston, Lake District) has been trying his H.R.O. receiver and 45 ft outdoor aerial on the medium waves. His log includes BBC local radio stations at Blackburn on 854 kHz ; Sheffield 1034 kHz ; Leeds 1106 kHz ; Merseyside 1484 kHz ; Stoke 1502 kHz ; Nottingham 1520 kHz ; Teesside 1546 kHz ; together with programmes in English from the Voice of America (VOA) Munich 173 kHz ( 1734 m ) on the longwaves at 1600 hrs ; Milan, Italy on 899 kHz at 2300 hrs ; American Forces Network (AFN) Berlin 935 kHz at 2325 hrs ; Radio Eireann 1250 kHz at 1430 hrs (low power relay at either Dublin or Cork).
Keith Lavelle (Manchester) has a 10 transistor radio and an outdoor spring-loaded whip antenna. He reports hearing BBC Radio Leeds on 1106 kHz ; Sheffield 1034 kHz ; Stoke 1502 kHz ; Bristol 1546 kHz ; Manx Radio (Isle of Man) 1594 kHz ; Trans World Radio, Montecarlo 1466 kHz .
J. Hallos (Warrington, Lancs) has built the Practical Wireless General Coverage receiver which he is using with a 12 ft indoor aerial attached to a 6 ft curtain rail. He reports hearing Manx Radio 1594 kHz at 0800 hrs ; Radio Eireann 1250kHz; Radio Leicester 1594 kHz at 1400 hrs ; Bristol 1546 kHz ; Nottingham 1520 kHz ; Stoke 1502 kHz .

Tim Thorpe (Lowbands, Glos.) has become intrigued with the performance of his Murphy transistor portable after dark. Using its internal aerial he has logged programmes in English from AFN Germany on 872 kHz and 1142 kHz ; Vatican Radio 1529 kHz at 2045 hrs ; TWR Montecarlo 1466 kHz at 2100 hrs ; Radio Berlin International 151 kHz at 2145 hrs ; Radio Tirana, Albania 1394 kHz at 2200 hrs ; Radio Prague 1286 kHz at 2200 hrs ; Radio Warsaw 1502 kHz at 2230 hrs ; Radio Portugal 755 kHz at 2245 hrs ; Radio Sweden 1178 kHz at 2245 hrs .
Harold Emblem (Mirfield Yorkshire) has received a verification from the low power Radio Rabat, Morocco 818 kHz and he mentions that this station signs off at 0300 hrs GMT with "Huna Rabat". This is a good time of year to listen to medium wave stations from North Africa and the Middle East. During the period of Ramadhan, which falls between the 28th September and 27th October this year, many stations are on the air all night and some of them are quite conspicuous after 2300 hrs GMT. Listen for Algeria on $533 \mathrm{kHz}, 548 \mathrm{kHz}, 890 \mathrm{kHz}$ and 980 kHz ; Tunisia on 629 kHz and 962 kHz ; Libya 1124 kHz and 1250 kHz ; Egypt on 620 kHz ; Kuwait 1345 kHz ; Baghdad 760 kHz ; Beirut 836 kHz ; Morocco 935 kHz ; Saudi Arabia 587 kHz ; Syria 957 kHz ; Turkey 1061 kHz . On the long waves look for Azilal, Morocco on 209 kHz ( 1435 m ) in Arabic and Tipaza, Algeria 251 kHz ( 1195 m ) in French.
The BBC transmitter at Moorside Edge on 692 kHz ( 434 m ) is being increased from 150 kW to 300 kW to help listeners whose reception is affected by interference from a station in East Germany. The Radio 4 transmitter at Swindon on 692 kHz has been changed to 1340 kHz ( 224 m ) which is marked "Northern Ireland" on many tuning scales.

Charles Molloy

## VHF/FM DXING

## by SIMON DAVID

FOLLOWING a report a few months ago, David Gardner of Dublin has kindly forwarded to me a copy of RTE Guide which covers v.h.f. and television broadcasts from the Republic of Ireland. Radio Na Gaeltachta has only recently opened, broadcasting news, local events and Irish music. Stations have been set up to transmit from Truskmore $91 \cdot 90 \mathrm{MHz}$, Maghera 97 MHz , Mullaghanish $91 \cdot 30 \mathrm{MHz}$, Kippure $89 \cdot 10 \mathrm{MHz}$, and Mt. Leinster $90 \cdot 40 \mathrm{MHz}$ all on the v.h.f./f.m. band. Others are on medium wave $240 \mathrm{~m}, 556 \mathrm{~m}, 312 \mathrm{~m}$. Irish is spoken throughout while RTE maintains a mainly English speaking service on $89 \cdot 7 \mathrm{MHz}, 94 \cdot 1 \mathrm{MHz}, 95 \cdot 3 \mathrm{MHz}$, $94 \cdot 9 \mathrm{MHz}$ respectively.
David says that RTE will verify reception reports, but is still awaiting acknowledgement from R. Na Gael, who have small studios at Casla, Connemara, Co. Galway, Eire. They are a part of RTE, but do not carry commercials. It apparently arose following the setting up of a "pirate" station in the west. This resulted in the "pirate" operator being engaged officially to run R. Na Gael.
Roy Patrick of Derby has taken his v.h.f. receiver on holiday with him on the East Coast (keen DXer!), but unfortunately did not have much DX success. Moving on to Farnborough, Hampshire he picked $\mathrm{up}_{9}$ Rouen $96 \cdot 5 \mathrm{MHz}$ (loud and clear), Boulogne $99 \cdot 9 \mathrm{MHz}$ (excellent quality) and back in hometown just managed to pick up Boulogne again.

Mr. Patrick used a Grundig "Music Boy" receiver.
In some places it is possible for the aerial to pick up not only the direct signal from the transmitter but also signals which have been reflected from tall buildings, hills or other large objects. This is known as multipath interference and it can cause very unpleasant distortion. The directional properties of a carefully-positioned multi-rod aerial can often be exploited to reduce the pick-up of the reflected signals and thus eliminate the interference. If the received signals are too strong this could give rise to 'intermodulation' or interaction between two or more received signals which may result in a 'birdie' background noise on one of the channels-usually Radio 3. Modern receivers are tending to overcome this effect by using special circuitry.

If this form of interference is experienced, it is better to reduce the signal input by using an attenuator in the aerial lead, other than by using a less efficient, and therefore less directional, aerial. Variable attenuators are available and the value to choose is the one which reduces the signal input just sufficiently to remove the 'birdies' without allowing background hiss to be introduced.

If any readers have taken a v.h.f. f.m. receiver on holiday with them, especially when travelling abroad, I shall be pleased to hear from them. We are particularly interested in reception, DX or otherwise, from foreign stations. I would also welcome cassette tape recordings of readers' f.m. reports. Please enclose your full name and address and 4 p stamp for the return of your cassette.


## SHORT WAVES

by DAVID GIBSON, G3JDG

THE summer is now firmly behind us. No more mobile rallies and outings. Which means, 1 hope, that everyone will have a concentrated onslaught of listening on the Amateur Bands. How about making it a 40 metre autumn/winter? A listen for a minimum of fifteen minutes on 7 MHz before you nip off to the more lucrative DX segments of 14 and 21 MHz . Spare a thought too for ten metres. Could be interesting bearing in mind that we are only a couple of years away from a sunspot minimum.

One person keeping an r.f. eye on the l.f. end of things is Stanley Sharred (Birmingham). He managed to locate a "good" CR100 for the princely sum of $£ 2$. He uses it as a back-up to his CR150/2. Using a horizontal Vee antenna ( $60 \mathrm{ft} . / \mathrm{leg}$ ) the following c.w. titbits were logged on topband; GM8MJ, EI9J, LU5HFI, OL1API, PY1RO, ZP9AY, with a couple of GW's and PAOHHV on s.s.b. A sniff around 3.5 MHz raised s.s.b. squeaks from; C31DM, FP8DH, KP4AN, PY2FUS, VO1FG, WIFVD, WA30VC, 3A2EE, 7X2MD. Even the dreaded forty metres was given a "Sharreding" to yield goodies on the c.w. like; CM2BG, CP5GM, K4JO, LU5HFl. WA5WPB. YV3TMD, ZI,2MM, ZM2AFH, and s.s.b. from; LU713DZ, PY7BHX. VK2WC, YV5CYS.

## Readers' Logs

Guy Dean (Ringwood) is the proud possessor of a FR50B amateur bands receiver plus a PR30 preselector. Antenna is an inverted Vee trap dipole with the apex at 44 ft . Three band log is as follows. Eighty metres; HC1HA, K2LWR, K4CYU, OY5NS, VE1DI, VE1ED, VOIBT, VO1FG, PY1HA, WA2CLQ, W2NR, W3HFV, W5BS. Twenty inetres; CE3AEV, CP1WB, CR6RJ, EP2MJ, ET3DS, ET3USA, HC2WF, HC7RD, HP1IW, HR1RSP, HZ1AB, JA4ZA, JY3ZH, JY6GT, JY8LE, KG4CA, KG4FS, KP4DSC, OA4HI, PZ1DR, TF3SV, TI2KF, VE8RC, VE8RCS, VK3BJB, VK3PA, VK5AS, VP3MKE, VU2DK, VU2JM, WA7UKQ, W6KMC, W7IJZ, YV4TY, YV5EED, 5Z4JE, 6Y5GB, 9J2DC, 9X5NA, 9Y4BO. Fifteen metres; A4XFJ, A6XP, CE3ABZ, CE3EGW, CP1FG, CR6AD,

CR6AG, CR7OL, ELIG, EL9C, HK3AUE, HK3LT, KP4AOW, KZ5USA, LUIDAB, LU3KAX, OJ0AM, PY2BFJ, TR8AF, VQ9BP, YV3VU, ZD7FT, ZD8AW, ZE1AD, ZE4JW, ZE7JR, ZP5HJ, ZS1FH, ZS4GF, ZS5EL, ZS6QD, 5H3JL, 5T5DY, 5Y4XNH, 5Z4JE, 3D6AU, 9K2JM.
Listening on a CR70A receiver, PR40, a.t.u. and 264 ft . end fed, D. Dance (Roxburghshire) heard some nice tweets on the h.f. bands. On twenty metres c.w., for example; CN8BO, CR6BX, DU1OR, OA4XK, PY2BOS, PY7VOU, PZICP, VP9CB, with s.s.b. from; DU1JMG, EL9C, HV3SJ, VE8RCS, 7X2MD, 9M2LN. Up on fifteen metres c.w.; CN8BO, CR6AL, CR6MX, EA8FE, EA8FS, EL0S/MM (near the Brazilian coast), FG7TG, KZ5EK, LU1HDC, VP9CB, YV3VU, ZC4BI, 9 X 5 NA . Best on ten metres were; ZC4CY, 9 H 1 CH on c.w. with LXIPD, M1C and 9J2DT on s.s.b.
J. Eagland (Brighouse) has a " 30 ft . long wire aerial, arranged as a spiral in the loft". Dizzy signals arriving from it are fed unmercifully into a CR45 receiver. The log for twenty metres reads; CE3AIU, HCISS, HK6CPS, LU3FAQ, LXIDAV, PZ6AA, VE2WF, VE7XF, VK2BHR, VK3MO, VR1FL, VP1TB, W9XRP, XE1PO, ZD3D. The same gear on eighty metres managed to locate; CN8HD, CT2AK, OY7JO, OY2X, VE1ZAN, VE3GCS, W2NIN, XE1CV, 4 X 4 KT .

Signals arriving at the ears of L. Large (Hassocks) have to walk a 600 ft . tightrope. At least that's the length of the antenna which can truthfully be described as a long wire. Apparently it was $1,000 \mathrm{ft}$. long but low-fiying motor vehicles proved a hazard. At the end of the line is a 9R59DS receiver and a page in the $\log$ marked 14 MHz which reads; EI6S, F9JA, GI3GRD, HZ1SH, LX1RR, K6UA, VO5BZ, TF5TP, VE1AM, VE8RCS, YV5AS, 3A2C. On 21 MHz the best were CR6QR, and TR8VE.

Loose on 14 MHz with an R107, homebrew a.t.u. and 132 ft . end fed is D. Douglas (Leicester). His best on 14 MHz were; CE3AX, CNBBO, CP5CW, CR3WB, CR7EH, EA6BG, EA8CR, EP3SP, ET3RS, ET3USA, HM1AQ, HR1BS, HZ1AB, JW1SO, JY6ZZ, KG6JBE, KP4DDO, KZ5JM, MP4BJP, OX3BH, VE1PV, V01JR, YN9GL, YV3VU, ZB2BZ, ZE4JG, ZL3UY, ZP5GE, 3V8CA, 4S7BR, 4W1BC, 4X4BA, 4Z4BA, 7X2MD, 9J2DT, 9LIVW, 9Y4PL.

Bernard Hughes (Worcester), JR310 receiver, dipole, bagged these on 14MHz; CR7AG, HR1RSP, HZ1AB, HM1AQ, JX3P, JY6KAM, JA3AJW, KG6JAP, KZ50H, LG5LG, VQ9MC, VP2VAP, VP2VS, VK2BKG, VK3ALL, WA7PMI, WA7BPS, ZL1JJ, ZD7FT, ZD3D, ZK1DX, 5W1AU, 9V1Q0, (9G1HE, 9J2EP. Curses, all Gibbies best gone for a chop-

## Events

Contests and events for October include: October 6-7, Oceana contest (phone); 6-7, u.h.f. national field day; $6-7,432 / 1296 \mathrm{MHz}$ contest; $13-14$, Oceana contest (c.w.); 13-14, fifteen/ten metre contest; 20-21, WADM contest (c.w.); 20-21, forty metre contest (c.w.). November 3-4, forty metre contest (phone); 3-4, two metre and 70 cms contest.

## BROADCAST BANDS

Short Wave Reports by 15th of the month to Malcolm Connah, 59 Windrush, Hlghworth, Swindon, Wiltshire, SN6 7DT.
Medium Waves Logs to Charles Molloy, 132 Segars Lane, Southport, PR83JG.
VHF/FM Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.
AMATEURBANDS Short Wave/VHF Logs in alphabetical order please by 15th of the month to David Gibson, G3JDG, 12 Cross Way, Harpenden, Hertfordshire.

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WE'D like some help and information as soon as possible on early wireless equipment manufactured by "H.P.R. Wireless Ltd." Mr. R. J. I. Moon, lately of Guildford, Surrey, has, in the process of moving down to Cornwall, kindly passed on to us some single valve units comprising tuners, detectors and audio stages. These used to be connected together to form a complete receiver and we even have the original heavy copper wires used for that purpose, with end loops perfectly formed.

So far we have not been able to trace the makers in any of our old catalogues but we believe the units are typical of the early 1920's. The units are housed in the inevitable mahogany boxes with black ebonite panels and the equally inevitable brass terminals, each panel being engraved "H.P.R. Wireless Ltd."

Mr. Ray Williams of Grantham, Lincs, thinks enough of our humble efforts to have extracted all the Going Back pages from past issues of the maga zine and to have bound them together to form a 'useful reference work'. Another reader wonders if we are going to do a reprint of our offerings! Any
more letters like that and we shall have enough evidence to demand of the Editor that something be done!

Not quite vinlage but of great interest to Ray Williams are two Utility receivers of the last war, both in perfect working order. In view of the vast numbers of these sels that must have been turned out at the time there must still be many thousands out of sight in attics, storerooms, garages etc. So, go to it, Going Back'ers and follow Ray's favourite haunts, 'derelict buildings, under wood piles and in odd corners'. One ancient set was brought round by a neighbour who thought it was a war-time bomb!
Mr. Williams was also kind enough to send along a photograph, reproduced herewith, of some of his treasures which number twenty eight, so far. He specialises in cally crystal sets and has collected some specimens in mint condition. The apple of his eye is an Ediswan crystal set, as new, in its original carton! This was featured on BBC TV in 'Nationwide' in July last year. So . . oh, when you buy that transceiver keep the carton, it could be worth a bomb in fifty years time?


Mr. Ray Williams from Grantham is pictured here with some items from his vintage radio collection.

# $\mathfrak{C O}$ CO! CO! CO! CO! 

## Information delanteo

any information appreciated on this meter. Front dial reads 70-0-70 Edison and Swan No. 116371916. Top terminals read I and Q.-R. J. Goodman, 26 Killarney Road, Wandsworth, London, SW 18 2DX.


I wish to restore a Gecophone 3 -valve a.c. receiver, Frequency is $50 / 80 \mathrm{~m}$ and voltage input $200-250 \mathrm{~V}$. Number is BC 3130 . Inst. No. 7327 . I would be glad of any information on this set and a suitable speaker to use with it.-Maurice Dean, 29 Lea Road, Dronfield, Sheffield, Yorks.
information regarding valves in a two-valve Gecophone model BC 3250 (cl926)-David James, 12 Circus Street, Greenwich, London, S.E. 10 .


This BBC photograph shows an Outside Broadcast commentator at the Brooklands Race Track in 1922.

## TRANSFORMERS

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 $\begin{array}{lllllllllllllll}213 & 1.0 & 0.5 & 1 & 4.8 \times & 2.9 \times & 3.5 & 0.12 V \text { at } 0.25 A-2 & .02 & 22 \\ 71 & 2 & 1 & 12 & 7.1 \times & 5.8 \times & 4.8 & 0.12 V \text { at } 0.5 A .2 & 1.22 & 22\end{array}$ $\begin{array}{lllllllllll}18 & 2 & 1 & 1 & 12 & 7.0 \times & 6.4 \times & 6.1 & 0.12 \mathrm{~V} \text { at } 1 \mathrm{~A} \cdot 2 & 1.60 & 22 \\ 70 & 6 & 3 & 2 & 12 & 8.3 \times & 7.7 \times & 7.0 & 0.12 \mathrm{~V} \text { at } 2 \mathrm{~A} \cdot 2 & 2.24 & 30\end{array}$ Also available a 20 W att version 12.02 P \& P 27 p

| 18 | 4 | 2 | 2 | 12 | $8.3 \times 7.7 \times$ | 7.0 | $0.12 V$ at $2 A \cdot 2$ | 2.24 | 30 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 70 | 6 | 3 | 3 | 8 | $8.9 \times 8 \times 0 \times$ | 7.7 | $0.12 V$ at $3 A \cdot 2$ | $2 \cdot 70$ | 42 |
| 108 | 8 | 4 | 5 | 8 | $9.9 \times 8.9 \times$ | 8.6 | $0.12 V$ at $4 A \cdot 2$ | $3 \cdot 00$ | 52 |


| 72 | 10 | 5 | 5 | 8 | $9.9 \times$ | $8.9 \times 8.6$ | 0.12 V at $4 \mathrm{~A} \cdot 2$ | 3.00 | 52 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 17 | 16 | 0 | 8 | 12 | $12.1 \times$ | $9.6 \times 8.6$ | 9.12 V at $5 \mathrm{~A} \cdot 2$ | 3.55 | 52 |


| 15 | 20 | 10 | 11 | 8 | $12.1 \times 9 \times 9.9 \times 10.2$ | 0.12 V at $8 \mathrm{BA} \cdot 2$ | 5.48 | 52 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 187 | 30 | 15 | 15 | 8 | $14.0 \times 12.1 \times 11.8$ | 0.12 V at $10 \mathrm{~A} \cdot 2$ | 6.98 | 67 |



## TRANSMIT/RECEIVE CONTROL BOX

R. H. LONGDON

THIS device is intended to control a transmitter and receiver, but can be used for other purposes, as explained. It gives complete control of suitable home-built equipment, without the need for any relay, or relay supplies.
Fig. 1 is the circuit, based upon the use of a 4 -wafer 3 -way rotary switch. Switch positions are numbered 1,2 and 3 . The back wafer Sla transfers the circuit from co-axial socket Sk1 to either co-axial socket Sk2 or Sk3. Wafter Slb closes the circuit in position 3. Wafer Slc closes in positions 2 and 3, while the front wafer Sld closes in positions 1 and 2.

## METHODS FOR USE

Uses for the control box in an amateur station include the following:

## Rx/Tx Control

Plug the aerial or tuner lead into Sk1. Run a coaxial lead from Sk2 to the receiver, and a similar lead from Sk3 to the transmitter. Disconnect the transmitter p.a. h.t. lead from the power pack, and take to A , running a lead from the second terminal A to the power pack. Similarly place B-B in the v.f.o. or v.f.o. h.t. circuit. Disconnect one receiver speaker lead from the speaker and take to C , adding a lead from the speaker to the second terminal C.
Position 1 then provides reception. Position 2 allows the v.f.o. to be turned to the receiver frequency. Position 3 puts transmitter on, and receiver off.

## Aerial Selection

A dipole may be available for one band, and an end-connected wire for other bands. For such purposes, or a direct comparison of aerials, connect one aerial to Sk2, the other aerial to Sk3, and the receiver to Sk 1 .

## Aerial/dummy load

It is sometimes convenient to run a transmitter output temporarily into a dummy load. For this, connect the Tx to Sk1, the aerial (or tuner) to Sk2, and dummy load to Sk3. For modulation and other tests the dummy load can be a household lamp. Should the dummy load be of known impedance, such as 75 ohms, it can be useful to load the transmitter into this correctly. Then switch to the aerial tuner and adjust the tuner for the same Tx p.a. input reading. A dummy load with r.f. meter is also very useful for obtaining optimum transmitter output.

## Receivers

It is sometimes convenient to switch from one receiver to another, for comparison, or because they are most suitable for different purposes (such as general coverage and amateur band only receivers, or h.f. band and I.f. band receivers). This can
be done by using Sk2 for one receiver, and Sk3 for the other. Where necessary, the speaker of the receiver not in use can be muted by using terminals $\mathrm{A}-\mathrm{A}$, and $\mathrm{C}-\mathrm{C}$.

## Transmitters

Sometimes a 10 W Tx may be used for 160 m , and a larger transmitter for other bands. Sk2 can then go to one Tx, Sk3 to the other Tx, and Sk1 to the aerial tuner.

## Transmitting Aerials

It is sometimes useful to compare one transmitting aerial with another (e.g., a vertical and long wire) while transmitting. This can be done by taking the Tx to Skl, and the aerials (with tuners, where required) to Sk2 and Sk3. Other uses will no doubt suggest themselves.

## EFFICIENCY

When this method of change-over was first used, there was some doubt about r.f. efficiency, and the possibility of switching high voltages.
R.F. efficiency was compared by feeding r.f. from a Tx to an r.f. wattmeter direct, then through the control box, on 28 MHz and lower frequencies. No difference in wattmeter readings could be seen.
R.F. feedthrough from Tx to Rx when transmitting depends on the equipment and layout elsewhere. as well as on stray coupling in the box. It was never large enough to cause trouble. An extra wafer was tried with the control of a large transmitter, to short Sk2 (receiver aerial) to earth, when transmitting. This was not incorporated in the control box as it was felt to be unnecessary.


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Input impedance 10 meg ohms.
Ranges:
Ranges: $0 / .25 / 1 / 2.5 / 10 / 50 /$ $250 / 1000 \mathrm{~V}$ D.C. $0 / 2.5 / 10 / 50 / 250$ $0 / 25 \mu \mathrm{~A} / 2.5 / 25 / 250$ mA D.C. -20 to +62 dB
$0 / 5 \mathrm{~K} / 50 \mathrm{~K} / 500 \mathrm{~K} / 5 \mathrm{mog}$ 500 meg ohms.
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Volt Bats, 500 Volt. Wide range clear moter $4!^{\prime \prime} \times 4^{\prime \prime}$.
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AC
$0.5 \%$
and
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D. $\quad 1 \%$ Accuracy $\begin{array}{ll}0.5 \% & \text { D.C. } 1 \% \text { AC. Scale } \\ \text { length } & 165 \mathrm{~mm} . \\ 0 / 300 / 750 \mu \mathrm{Ma}\end{array}$ length 105 mm .
$1-6 / 8 / 75 / 15 / 80 / 75 /$
$160 / 300 / 750 \mathrm{~m} / 1.5 / 8 /$ $160 / 300 / 750 \mathrm{~mA} / 1.6 / 8 /$
$7.5 \mathrm{AMPDCO/3/7.5/15}$ $80 / 75 / 150 / 800 / 1$
$750 \mathrm{~mA} / 15 / 3 / 7.5$
AMP AC $0 / 75 / 150$ $\mathrm{AMP} \mathrm{AC} 0 / 76 / 150 /$
$300 / 750 \mathrm{mV}$
$70 / 1-6 / 3 /$

$7.5 / 15 / 80 / 75 / 150 / 300 / 750 \mathrm{~V}$ DC $0 / 750 \mathrm{mV} / 1 \cdot 5 / 3 / 7-5 / 15 / 30 / 75 / 160 / 300$ 1750 V AC. Automatic cut out. Supplled com-
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+10 dB. $(10 \mathrm{~K}$
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 3 in , tube, Y amp. Senaltivity$0.17 \quad$ p-p/CM. Bandwidth 1.17
$1.5 \mathrm{cps}-1.5$
2 MHz. Input imp. $\begin{array}{llll}2 & \text { meg } & \Omega & 25 \mathrm{pF} \\ \text { sensitivity } & 0.9 \mathrm{y} & \mathrm{X} & \mathrm{mmp} \text {. } \\ \text { s/CM }\end{array}$ $\begin{array}{lll}\text { sensitivity } & 0.9 \mathrm{v} \text {. } \mathrm{p} \text {-p/CM } \\ \text { Bandwidth } \\ 1.5 \mathrm{cps}-800 \mathrm{H}\end{array}$ Bandwidth $1.5 \mathrm{cps}-800 \mathrm{kHz}$. Input imp. 2 meg $\Omega 20 \mathrm{pF}$. 500 kHz . Synchrontzation.
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For dlaplay of pulsed and periodic waveforms in electronle circuits. VERT. AMP. Band-
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## Frequency 200 KHz.

## 200 KHz .

$0-111 \mathrm{db}$. 0.1db
Impedance 600 step.
Max. input power
30 dbm . Slize $180 \times 90 \times 55 \mathrm{~m}$
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te/b on
4 ke/s on 4 bandq.
Square: 20 cps to 30 Square: 20cps to
ke/s. Output impe ${ }_{200 / 250 \mathrm{~V} \text {. }}^{\text {dance }}$ eration. Supplier

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AUDIOTRONIC AHA- 101 STEREO HEADPHONE AMPLIFIER

 tranalictor amplifer operaten from ceramio or tuner ithputs with twin ateren headphone outputs and separate volume controly for esch channel. Operates from $y^{2}$ hattery. INPUTS: $5 \mathrm{mv} / 100 \mathrm{mV}$. nel. | Our | 57.50 |
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more than 1 watt. B Meter. gquelch more than watt. B Meter. Bqueich AF controls. 4-16 ohm output and phone jack. Power requirementa $100 / 240 \mathrm{v}$. AC. $12-14 \mathrm{v}$. DC.
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Fully transistor: Bed portable Will transmit and receive on 6 channels between 144 traugmitter. 12 v DC Internal o
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Solld state moblle transcelver for 12y DC neg. use. Transnits and between 144 and 146 MHz . Power output 10 w and 1 w switchable. Interal $3^{\prime \prime}$ speaker. Complete w'th dynamic mike, PTT switch, three sets of crystals for
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15 MHz . SSB, $A M$ and CW. $A F$ output more than 1 watt. Crystal
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Price $\mathbf{\$ 2 5 . 0 0} \begin{gathered}\text { Carr. } \\ 37 \mathrm{p}\end{gathered}$

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Master and two sub stations. Can be used on desk or wall mounted. Complo Our
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AHP-8D 8 Track Stereo Tape Deck Can be used with most bj $f$
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Incorporates built in amplifers giving $21+2 \dagger$ watts rms output. illuininated track Indicators, allder controle for volume, balance and tone. Attractive cabinet with black and silver tritn. Outpnt impedance 8 ohms. AC 220/240v. OUR
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For conventional or Chronium Dioxide tape. 4 track record/ playbsck. volume and tone 16 kHz (using CrOy response 40 . tion better than $2 \%$ wow and flutter better than $0.2 \%$ RMS. Complete with pair of matchlng Akai C8s8 speakers.

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Carriage and Paching 75p. Complete units with Stereo cart-
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SP25 111 Module/M75-8 8P25 IV Module/M75-6EM AP76/G800 AP76/G800E AP76/M44E
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 $210 / \mathrm{SC} 7 \mathrm{M}$$\mathrm{MP} 60 / \mathrm{G} 800$ MP60/TPD1/G800 M P60/M44-7 HT70/TPD1/G800

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610/TPD1
710
810
810
11
MP60/GB00
MP60/TPDI
HT70
HT70/TPD1
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BD1 Kit
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SP 25
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Size only 4 d $^{\prime \prime}$
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sine wave
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Specification on all three power modules :
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|  |  | 25 |  |  | 25 |  |  | 25 |  |  | 25 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SN7400 | 0.17 | 0.18 | SN7426 | 0.50 | 0.48 | 8N7454 | $0-17$ | $0 \cdot 18$ | 8N7494 | ． 85 | －82 |
| SN7401 | $0 \cdot 17$ | 0－16 | SN7427 | 0.50 | 0.46 | 8N7460 | $0 \cdot 17$ | 0.18 | 8N7495 | 0.85 | －82 |
| 8N7402 | 0.17 | 0.16 | 8N7428 | 0.77 | 0.78 | 8N7470 | $0 \cdot 32$ | 0.29 | 8N7496 | 0．98 | ． 08 |
| 8N7403 | 0.17 | $0 \cdot 18$ | 8N7430 | 0.17 | $0 \cdot 16$ | SN7472 | $0 \cdot 32$ | 0.29 | SN74100 | 21.82 | 21.7 |
| BN7404 | 0.17 | 0.18 | SN7432 | 0.50 | 0.48 | 8N747 | 0.41 | 0.39 | SN74104 | 21.07 | E1． |
| 8N7405 | 0.17 | 0.18 | SN7433 | 0.88 | 0.83 | EN747 | 0.41 | $0 \cdot 39$ | GN74105 | 81.07 | 21.04 |
| 8N7406 | 0.89 | 0.84 | 8N7437 | 0.71 | 0.88 | 8N747 | $0-50$ | 0.48 | SN74107 | 0.44 | 0.42 |
| 8N7407 | 0.38 | 0.34 | gN7438 | 0.71 | 0.88 | N747 | 0.4 | 0.48 | SN74110 | 0.81 | － 5 |
| 8N7408 | 0.20 | 0.19 | 8N7440 | 0.17 | 0.18 | N7480 | 0.74 | 0.71 | SN74111 | 41．38 | 21．87 |
| 8N7409 | 0.20 | 0.19 | gN7441 | 0.74 | 0.71 | N7481 | 81－88 | 21－27 | SN74118 | 21.10 | 21.05 |
| gN7410 | 0.17 | 0.16 | SN7442 | 0.74 | 0.71 | N748 | 0.96 | 0.95 | SN74119 | 11.49 | 21.38 |
| SN7411 | 0.28 | 0.27 | 8N7443 | 21.43 | 21－38 | N7483 | 21．81 | 21.16 | SN74121 | 0.44 | 0.41 |
| gN7412 | 0.38 | 034 | SN7444 | 21.43 | 21.38 | N7484 | 21.10 | $\pm 1.05$ | 8N74122 | \＄1．84 | 21.48 |
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| gN7417 | 0－48 | 0.44 | 8N7447 | 0.98 | 0.88 | N7489 | 18.05 | 25.78 |  |  |  |
| 8N7420 | 0.17 | 0.16 | 8N7448 | 21.10 | \＆1－07 | SN7490 | 0.68 | 0.60 |  |  |  |
| 8N7422 | 0.55 | 0.53 | 8N7450 | $0 \cdot 17$ | $0-18$ | 8N7491 | 21.10 | E1．05 |  |  |  |
| SN7423 | 0.55 | 0.58 | 8N7451 | 0.17 | 0.18 | 8N7492 | 0.74 |  | － 100 plus lesar $10 \%$ of |  |  |
| SN7425 | 0－55 | 0－53 | SN7453 | － |  |  | 0.74 |  |  |  |  |

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| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 301 | T099 | 0.55 | 307 | 8 Pin | DIL $0 \cdot 66$ | 723 C | DIL | 0.89 | 748 C | T099 | 0 |
| 301 | 8 Pin DIL | $0 \cdot 48$ | 308 | T099 | 28．90 | 723 C | T099 | $21 \cdot 00$ | 1437 | DIL | 1 |
| 301 A | DIL | 0.69 | 308A | T099 | $27 \cdot 40$ | 741 C | 8 Pin | L 0.35 | 1458 | T099 | 12 |
| 301A | T099 | 0．69 | 709 C | DIL | $0 \cdot 35$ | 741 C | 14 Pi | IL0．88 | 3046 | DIL | 0. |
| 301A | 8 Pin DIL | $0 \cdot 68$ | 709 C | T099 | 0.34 | 741 C | T099 | 0.38 |  |  |  |
| 307 | DIL | 0.69 | 710 C | DIL | 0.44 | 747 C | DIL | 0.80 |  |  |  |

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| :---: | :---: | :---: | :---: | :---: |
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| 220 2 F －61p | 100 F F 61p | 2000 $\mu \mathrm{F}$－ 43 p |  | $4 \cdot 7 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ |
|  | 220 FF －8p | $3300 \mu \mathrm{~F} \quad 38 \mathrm{p}$ |  | $6.8 \mu \mathrm{~F}$－ $6 \frac{1}{2} \mathrm{P}$ |
| $1000 \mu \mathrm{~F} \quad 13 \mathrm{p}$ | $330 \mu \mathrm{~F} \quad 10 \mathrm{p}$ | $6800 \mu \mathrm{~F} \quad 65 \mathrm{p}$ | 40 VOLT | $10 \mu \mathrm{~F}$ |
| $4700 \mu \mathrm{~F} \quad 29 \mathrm{p}$ | 470 FF F 10p |  | $6.8 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | $22 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{p}$ |
|  | 1000 $15 \mathrm{~F} \quad 11 \mathrm{p}$ |  | 15 5 F （ $6 \frac{1}{2} \mathrm{P}$ | $68 \mu \mathrm{~F} \quad 10 \mathrm{p}$ |
| 6－3 VOLT | 1500 FF 20p | 25 VOLT | $33 \mu \mathrm{~F}$－61P | $100 \mu \mathrm{~F} \quad 11 \mathrm{p}$ |
| $\begin{array}{ll}33 \mu \mathrm{~F} & 6 \frac{1}{2} \mathrm{p} \\ 68 \mu \mathrm{~F} & 6 \frac{1}{p}\end{array}$ | 2200～F 24p | $10 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ |  | $150 \mu \mathrm{~F} \quad 13 \mathrm{p}$ |
| $68 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ |  | $22 \mu \mathrm{~F}$（ $6 \frac{1}{2} \mathrm{P}$ | $100 \mu \mathrm{~F}$（ 9 p | 220 F F 19p |
| $150 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | 16 VOLT | $47 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | $150 \mu \mathrm{~F} \quad 10 \mathrm{p}$ | $330 \mu \mathrm{~F} \quad$ 22p |
| $470 \mu \mathrm{~F}$（ IIP | $15 \mu \mathrm{~F} \quad 6 \frac{1}{2} \mathrm{P}$ | $100 \mu \mathrm{~F}$－8p | $220 \mu \mathrm{~F} \quad 11 \mathrm{P}$ | 470 F F 26p |
| $\begin{array}{ll}680 \mu \mathrm{~F} & 13 p \\ 1500 \mu \mathrm{~F} & \text { 18p }\end{array}$ | $\begin{array}{ll}33 \mu \mathrm{~F} & 6 \pm \mathrm{p} \\ 68 \mu \mathrm{~F} & 61 \mathrm{p}\end{array}$ | $150 \mu \mathrm{~F} \quad 8 \mathrm{p}$ | $470 \mu \mathrm{~F}$－19p | 1000 F －44p |
| $\begin{array}{ll}1500 \mu \mathrm{~F} & 18 p \\ 2200 \mu \mathrm{~F} & 18 \mathrm{p}\end{array}$ |  | $220 \mu \mathrm{~F}$－10p | 680 $\mu \mathrm{F} \quad 25 \mathrm{p}$ |  |
| 2200んF 18p | $150 \mu \mathrm{~F}$ 1－8p | 470んF 13 P | $1000 \mu \mathrm{~F}$ 25p |  |
| 3300 2 F 26p | 220 2 F 9p | $680 \mu \mathrm{~F}$ 20p | 2200 $\mu \mathrm{F}$－44p |  |
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 ACl41K 28p

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AC188 \& 14 p \& BC108 \& 9D \& BC212 \& 12 D \& OC45 \& 14 p \& 2N3707 \& 11 p \& 1N4002 \& 1N <br>
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 AC187K 25p 

AC188K 24p \& BC147 \& 11 p \& BC214 \& 12 p \& OC81 \& 14 p \& $2 N 3709$ \& 11 p \& 1 N 4005 \& 8 p
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Normal Price Our Price
 Type $S W 100 \times 80 \mathrm{~mm}$ ．

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| ＂－500 ${ }^{\text {a }}$ | 23．45 | \＄2．80 |
| ＂VU＂meter | 23．85 | \％2．09 |
| Meter： <br> n $\times 1-15 / 32$ in $\times 2$ 2in deep |  |  |
|  |  |  |
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## the slimmest,most elegant hi•fi modules ever made



Living with hi-fitakes on new meaning now that Project 80 is here. These amazing new modules mark a brilliant technical advance all round; their size and presentation bring exciting"new opportunities to install systems in ways hithertis only dreamed about but never before made practical. You can build a Project 80 system virtually anywhere and it is unbelievably simple to install and connect up. Everything that could possibly be wanted in a top quality do-it-yourself domestic hi-fi system will be found in Project 80 - compactness, eiegantly ultra-modern styling, ease of fixing and operation, new control methods, and above all superb performance. New as well as popular established ideas on installation are featured on page four of this announcement to provide just
a few examples of the system's fantastic versatility a few examples of the system's fantastic versatility.


## Stereo 80 pre-amplifier and control unit

As with other Project 80 units, the Stereo 80 is mounted by means of two bolts fixed at the rear which pass through holes drilledin the wood or plastic on which modules are to be mounted. All the electronics are contained within the $\frac{3}{4}{ }^{*}$ deep front panel! Connecting leads are taken away simularly out of sight. Each channel in the Stereo 80 has its own independent tone and volume controls operated by sliders. This enables exceptionally good environmental matching to be obtained. Provision is made for magnetic and ceramic pick-ups. radio and tape in and out. A virtual earth input stage forms part of the up-dated circuitry of the Stereo 80 to ensure the inest possible quality from all signal sources. Generous overload margins are allowed on all inputs Clear instructions with template are supplied.

TECHNICAL SPECIFICATIONS
Size $-260 \times 50 \times 20 \mathrm{~mm}$ ( $10 \frac{1}{4} \times 2 \times \frac{3}{3}$ ins)
Finish - Black, with white markings
Inputs-Mag. P.U. 3 mV RIAA corrected: Ceramic P.U. 300 mV
Radio 300 mV : Tape 30 mV
$\mathrm{S} / \mathrm{N}$ ratio- 60 db
Frequency range -20 Hz to $15 \mathrm{KHz} \pm 1 \mathrm{~dB}: 10 \mathrm{~Hz}$ to $25 \mathrm{KHz} \pm 3 \mathrm{~dB}$
Power requirements -20 to 35 volts
Outputs $-100 \mathrm{mV}+\mathrm{AB}$ monitoring for tape
Controls - Press button for tape, radio and $P$ U. selection Volume.
Bass +12 dB to -14 dB at 100 Hz : Treble $+11 \mathrm{~dB} 10-12 \mathrm{~dB}$ at 10 KHz


R R.f. $£ 11.95$


## Project 80 FM tuner smaller, more efficient

A truly remarkable tuner in every way - its unbelievably compact size its original circuitry - its dependable performance - all this in a boldly designed modern case measuring $85 \times 50 \times 20 \mathrm{~mm}$ ( $3 \frac{1}{2} \times 2 \times \frac{3}{8}$ ins). Greater adaptability (and possibly financial convenience) results from the tuner and stereo decoder section being made avallable separately.

TECHNICALSPECIFICATIONS
Size $-85 \times 50 \times 20 \mathrm{~mm}$ (approx. $3 \frac{1}{2} \times 2 \times \frac{3}{4}$ Ins)
Tuning range -87 to 108 MHz
Detector-I.C. balanced coincidence, for good A.M. rejection
AFC - Switchable, with thermistor control to prevent from dift
One 26 transistor I.C.
Twin dual varicap tuning
Distortion- $0.3 \%$ at 1 KHz for 75 KHz deviation
Ceramic filter in I.F. section
Aerial impedance - $75 \Omega$ or 240-300 $\Omega$
Sensitivity - 4 microvolts for 30 dB queting
Power requirements - 12 to 45 volts

## Project 80 stereo decoder

Making the Project 80 decoder separate from the F.M. tuner gives the constructor a wider choice of systems as well as saving money in cases where stereo reception may not be required. This unit gives a 40 dB channel separation with an output of 150 mV per channel. The gallium arsenide light emiting beacon automatically lights up to show when a stereo transmission is tuned in. Des!gned essentially as an integral part of Project 80 systems. this multiplex stereo demodulator may be used in many cases with existing single channel frequency modulated tuners to provide stereo reception.
Size $-47 \times 50 \times 20 \mathrm{~mm}$ ( $1 \frac{1}{1} \times 2 \times$ 揉ns)
One 19 transistor I.C.


## new constructional techniques

## and again Sinclair leads the world

1962 Micro-minıature power amp small enough to stand on a 10p. piece. Slimline pocket receiver smaller than a 20 cigarette pack
1963 Micro-6 receiver, smaller than a matchbox
1964 Pocket F.M. receiver: PWM amp.
1965 Z. 12 power amplifier module. PZ. 3 power supply
1966 Stereo 25 pre-amp/control unit
1967 Micromatic Q. 14 loudspeaker: the first Neoterıc
1968 IC. 10 . the first ever integrated circuit for constructors use

## Project 80 active filter unit

This efficiently designed unit makes a highly desirable part of any worthwhile system where inputs may be from record. radio or tape. As with Stereo 80. separate controls are applied to each channel thereby making it easier to obtain ideal stereo balance in any kind of indoor environment

TECHNICAL SPECIFICATIONS
Size $-108 \times 50 \times 20 \mathrm{~mm}$ ( $4 \frac{1}{4} \times 2 \times \frac{3}{4} \mathrm{~ns}$ )
Voltage gain-minus 02 dB
Frequency response -36 Hz to 22 KHz . controls minımum
Distortion - at $1 \mathrm{KHz}-0.03 \%$ using 30 V supply
HF cut off (scratch) -22 KHz to $5 \cdot 5 \mathrm{KHz} .12 \mathrm{~dB} /$ oct slope
L.F. cut off (rumble) -28 dB at $20 \mathrm{~Hz} .9 \mathrm{~dB} /$ oct. slope

## Z. 40 \& Z. 60 power amplifiers totally short-circuit proof

Etther of these entirely new power amplifiers is intended for use in Project 80 installations although. of course, they are readily adaptable to an even wider range of applications. Both $Z .40$ and $Z .60$ incorporate builtin protection against shortcircuiting and risk of damage arising from mis-use is greatly reduced. Comprehensive instructions are supplied with each of the modules.
Z.40 Technical Specifications Size $-55 \times 80 \times 20 \mathrm{~mm}$ (21 $\times 3 \frac{1}{8} \times$ fins) 9 transistors Input sensitivity -100 mV Output - 15 watts RMS contınuous into $8 \Omega(35 \mathrm{~V}) .30$ watts music power into $4 \Omega(30 \mathrm{~V})$
Frequency response -10 Hz $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$
Signal to noise ratio -64dB Distortion - at 10 watts into $8 \Omega$ less than 0 1\%
Power requirements $-12-35$ volts

Z 60 Technical Specifications Size-55×98×20mm ( $2 \frac{1}{6} \times 3 \frac{3}{3} \times \frac{3}{3}$ ins) 12 transistors Input sensitivity $-100-250 \mathrm{mV}$ Output - 25 watts RMS into $8 \Omega(45 \mathrm{~V}) .50$ watts music power into $4 \Omega$ (50V)
Distortion- typically 0 03\% Frequency responsé -10 Hz to more than $200 \mathrm{KHz} \pm 1 \mathrm{~dB}$ Signal to noise ratio - better than 70dB
Built-in protection against transient overload and short circuit
Load impedance - $4 \Omega$ min; max safe on open circuit

## Sinclair power supply units PZ.8

the worlds most
advanced unit in its class
Stabilised power supply unt Reentrant current limiting makes damage from overload or even direct shorting impossible. a principle never before inorporated in a commercially available constructor mod. ule. Normal working voltage (adjus. table) 45 V .
R.R.P. $\mathrm{f} 7.98+0.79 \mathrm{p}$ V.A.T. Without mains transformer PZ. 530 V unstabilised
R.R.P. $€ 4.98+0.49$ p V.A.T.

PZ. 6 35V. stabilised
R.R.P. $£ 7.98+0.79$ p V.A.T.


1969 Q. 16 - improved version of Q. 14 Systems 2000 and 3000: Project 60 launched
1970 IC. 12 Project 605
1971 Project 60 stereo $F M$ tuner. Z. 50 PZ 8
1972 Improvements to Project 60 with Z.50 MK. 2 and PZ. 8 Mk. 3 The Executive Calculator: Digital multi-meter Q. 30 speaker

1973 Cambridge Calculator
PROJECT 80 LAUNCHED


Recommended Project 80 applications

| System | The Units to use | Units cost |
| :---: | :---: | :---: |
| Simple battery record player | 2.40 | $\begin{aligned} & £ 5.45 \\ & +54 p \vee A T \end{aligned}$ |
| Mains powered record player | 2.40. P2.5 | $\begin{aligned} & £ 10.43 \\ & +£ 1.04 \text { V.A.T. } \end{aligned}$ |
| 30W. RMS continuous sine wave stereo amp | $\begin{aligned} & 2 \times 2.40 \mathrm{~s}, \text { Stereo } \\ & 80 ; \text { PZ.6 } \end{aligned}$ | $\begin{aligned} & £ 30.83 \\ & +£ 308 \mathrm{~V} \text { A.T } \end{aligned}$ |
| 50W ( $8 \Omega$ ) RMS continuous sine wave de luxe stereo | $\begin{aligned} & 2 \times 2.60 \mathrm{~s}, \text { Stereo } \\ & 80 ; \text { PZ.8 } \end{aligned}$ | $\begin{aligned} & £ 33.83 \\ & +£ 338 \vee A . T \end{aligned}$ |
| amplifier Indoor P.A | 2.60, PZ.8 | $\begin{aligned} & £ 14.93 \\ & +£ 1.49 \text { V.A.T. } \end{aligned}$ |
| Car Radio | F.M. tuner. <br> 2.40 | $\begin{aligned} & £ 16.40 \\ & +£ 1.64 \text { V.A.T } \end{aligned}$ |

## From Sinclair the worlds most advanced hi-fi modules

Sinclair Project 80 tre ultra-modern non-obtrusive hi-fi
 end


The modules mount very easily onto a playing plinth

A novel application would be to build around the base of a

hade

## Project 80 could

 be easily mounted onto a loudspeaker cabinet

A $2 \frac{1}{2}$ " strip aiong the edge a shelf could be sufficient to contain a complete

lampshade

Two Sinclair Q. 16 loudspeakers suitably positioned together with Project 80 could be
mounted on to a false wall.

> When you have seen for yourself how fantastically slim and cleverly designed these modules are, further ways will suggest themselves in which they can become a pleasing part of vour particular domestic environment.

## To SINCLAIR RADIONICS LTD. ST. IVES, HUNTINGDON PE17 4HJ <br> 

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Should any defect arise in momal use. we will service 11 without charge. For damage árismg from mis-use a small charge (typically £1.00) will be made.

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## CAPACITORS

Sub-miniature

| Axial lead electrolytic |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Md V Price Mid V Price |  |  |  |  |  |  |  |
|  | 63 | ${ }^{\text {B }}$ D | 68 | 6.36 p |  |  |  |
|  |  | 6D | 68 | 10 6p |  |  |  |
|  | 63 | 8D | 68 | 63 10p |  |  |  |
|  | 63 | 6D | 100 | 4 6p | Mid |  | Price |
|  | 63 | 80 | 100 | 10 6p | 470 | 6.3 | 6p |
|  | 40 | 6 D | 100 | 25 6p | 470 | 10 | 10p |
|  | 63 | 6p | 100 | 40 䂙 | 470 | 25 | 12D |
| 10 | 25 | 6D | 100 | 63 12p | 470 | 40 | 18p |
| 10 | 63 | 8p | 150 | 5.3 6p | 680 | 1.3 | 10p |
| 15 | 16 | 6p | 150 | 16 BD | 680 | 16 | 12p |
| 15 | 40 | 6p | 150 | 25 8D | 680 | 25 | 18p |
| 15 | 63 | 6p | 150 | 4010 p | 680 | 40 | 22p |
| 22 | 10 | 8p | 150 | 6312 p | 1000 | 4 | 10p |
| 29 | 25 | 6p | 220 | 4 6p | 1000 | 10 | 12p |
| 22 | 63 | 8p | 220 | 10 Bp | 1000 | 16 | 18p |
| 33 |  | $3{ }^{6}$ | 220 | 16 6p | 1000 | 25 | 22p |
| 33 | 16 | 6p | 220 | 2510 D | 1500 | 6.3 | 12p |
| 33 | 40 | 80 | 220 | 4012 D | 1500 | 10 | 18p |
| 47 | 4 | 6D | 230 | 63 18p | 1500 | 16 | 22p |
| 47 | 10 | ${ }^{8} \mathrm{p}$ | 330 | 4 6p | 2200 | $6 \cdot 3$ | 18p |
| 47 | 25 | 6 d | 330 | 10 6D | 2200 | 10 | 22p |
| 47 | 40 | 8p | 330 | 16 10p | 3300 | $6 \cdot 3$ | 22p |
| 47 | 63 | 6p | 330 | 63 22p | \$700 | 4 | 22 p |

## PLUGS AND SOCKETS



## WIRE © CABLES

Hook-up wire. 7 strand 0-2mm. PVC ec-vered tinned copper witre for light general connexions up to $1-4 \mathrm{~A}$. 11 colours: black, blue brown, green, grey, orange, plnk, red, violet
white, yellow. 10 metrea of any one eolour Thite, yellow. 10 metres of any one eolour 15p. Pack of 11 ( 1 of each colour) 10 m .
colls $£ 1.50$.

Single core sereened 6p per metre. Twin indivldually screetied 8 p per metre. High quality single acreened $50 \Omega \quad 100 \mathrm{pF}$ per metre, ideal for high grade audto con-
nexions lip per metre.


Extra flezible 55 atrand 0.1 mm . PVC covered plain copper wire rated at 6A. Ideal for test leads etc. Red or black 41p per maetre.

Matns 3-core miniature 2.5A black PVC covered 13 atrand 0.2 mm . per condnctor
$7 \not \equiv p$ per metre.

## POTENTIOMETERS

Rotary minlature carbon track t" spindle
Single gang Lin or Log $5 \mathrm{k}, 10 \mathrm{k}, 26 \mathrm{k}, ~ 50 \mathrm{k}, 100 \mathrm{k}, 250 \mathrm{k}$,
$500 \mathrm{k}, \mathrm{IM}, 2 \mathrm{M}$ (and 1 k Lhu) 12g


Wirewound $10 \%$ 1W
33p; $10 \mathrm{k}, 37 \mathrm{p} ; 25 \mathrm{~s}$ indle $10,50,100 \mathrm{R} 34 \mathrm{p} ; 250,500,1 \mathrm{k}, 5 \mathrm{k}$
44 p .

## RESISTORS



All $t^{n}$ shatt. Grub acrew fixing
Diameter shown in brackets


POLYESTER FILM METALLISED R50VDC $0.01 \mathrm{uF}, 0.015 \mathrm{uF}, 0.022 \mathrm{uF}$ 8p; 0.033uF, $0.22 \mathrm{uF} 5 \mathrm{p}: 0.33 \mathrm{uF} 7 \mathrm{D} ; 0.4781 \mathrm{p} ; 0.68 \mathrm{uF}$ 12p: luF 14p: 15 uF 21p; 2-2uF 25p.

Wide range of transistors, flodes and I.C.'s in stock see our catalogue for detalls.

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$1000 \mathrm{VDC} ; 300 \mathrm{VAC}$; Non-inductive
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VAT
Please add 10\% to the final total.

Tantalum Bead

| Mid | V | Price | 11fd | V | Price | - |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.1 | 35 | 12p | 10 | 16 | 14 p |  |
| 0.22 | 35 | 12p | 10 | 25 | 16p |  |
| 0.47 | 35 | 12D | 15 | 16 | 16p |  |
| 1.0 | 35 | 12p | 22 | 16 | 16D |  |
| $2 \cdot 2$ | 35 | 12 p | 47 | 6.3 | 18p |  |
| 4-7 | 35 | 14D | 100 | 3 | 18p |  |

Trimmers-compression type $\begin{array}{rrrrr}3 \text { to } 40 \mathrm{pF} & 13 \mathrm{p} & 20 \text { to } 250 \mathrm{pF} & 18 \mathrm{p} \\ 30 \text { to } 140 \mathrm{pF} & 13 \mathrm{p} & 100 \text { to } 500 \mathrm{pF} & 21 \mathrm{p}\end{array}$

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 1800 11p: 2200 13p: 2700 15p; 3600 18p; 4700, 5000 20p; $680027 \mathrm{p} ; 8200,10,00034 \mathrm{p}$.

k
Rotary with adjustable stop 1 pole 2 to 12 way; 2 pole 2 to 6 way; 3 pole 2 to 4 way; 4 pole 2 or 3 way, each 24 p . Mains rotary DPDT 250 V 2A 20 p .

Carbon Film
carbon Fillon
it
$5 \%$$\frac{1 \Omega}{} 1 \Omega$ to $1 \mathrm{M} ; 10 \% 1 \cdot 2 \mathrm{M}$ to 10 M E12 Carbon Film tW $5 \% 1 \Omega$ to $10 \Omega ; 10 \%$ 1-2M to 10 M E12 Carbon Film iW $5 \% 11 \Omega$ to 910 k Metal Oride tW $9 \% 10 \Omega$ to 10 M Wirewound 2 \& W $10 \% ~ 0.220 \mathrm{hms}$ to 0.47 ohm E12\& E24 4D Wirewound 2 FW $5 \%$ 1ohm to 270 ohms E12 101 E12 values 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and decades E24 values 11, 13, 16, 20, 24, 30, 36, 43, 51, $62,75,91$ and decades


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non-locking Slide
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DPDT Sub-mintiature toggle DPDT Toggle 250V 1.5A
 with ON/OFF plate 25p.


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AUDIO MDXER MODULES for hi-fi applications. Catalogue free, large S.A.E.; Hillcrest Electronics, 123 Harestone Hill, Caterham, Surrey.

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| MINIATURE HALF WAVE SILICON RECTIFIERS |  |  |  |
| :---: | :---: | :---: | :---: |
| IAB029（Avalanche） | 1000 P．I．V． | 1．6A | 0.30 |
| IN540 | 400 P．I．V． | 750 mA | $0 \cdot 30$ |
| IN645 | 225 P．I．V． | 400 mA | 0.16 |
| IN649 | 600 P．I．V． | 400 mA | 0.85 |
| IN3193 | 200 P．I．V． | 750 mA | 0.15 |
| IN3194 | 400 P．I．V． | 750 mA | $0 \cdot 17$ |
| IN4001 | 50 P．I．V． | 14 | $0 \cdot 06$ |
| IN4002 | 100 P．I．V． | 1A | 0.07 |
| IN4008 | 200 P．I．V． | 14 | 0.075 |
| IN4004 | 400 P．I．V． | 1A | 0.08 |
| IN4005 | 600 P．I．${ }^{\text {P }}$ ． | 1A | $0 \cdot 10$ |
| IN4006 | 800 P．I．V． | 14 | $0 \cdot 12$ |
| IN4007 | 1000 P．I．V． | 1A | $0 \cdot 14$ |
| IN5390 | 1000 P．I．V． | 1．5A | 0.25 |
| IN5408 | 1000 P．I．V． | 3 A | 0.80 |
| BY100 | 700 P．I．V． | 450 mA | $0 \cdot 15$ |
| BY101 | 450 P．I．V． | 1－1A | 0.15 |
| BY100 | 800 P．I．V． | 1.14 | 0.15 |
| BY125 | 200 P．I．V． | 425 mA | $0 \cdot 10$ |
| BY126 | 650 P．I．V． | 14 | $0 \cdot 10$ |
| BY127 | 1250 P．I．V． | 14 | 0.18 |
| DD000 | 50 P．I．V． | 500 ma | 0.15 |
| DD006 | 400 P．I．V． | 500 mA | 0.25 0.85 |
| DD058 | 800 P．I．V． | 500 mA | 0.85 |

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"Completing your course, meant going fronı a job, I detested to a job that I love, with unlimited prospects".-Student J.A.O. Dublin.
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## ORT WAVE TWO




Resistors:

| RI | $2 \cdot 2 M \Omega$ | $R 6$ | $220 k \Omega$ |
| :--- | :--- | :--- | :--- |
| R2 | $150 k \Omega$ | R7 | $2 \cdot 2 k \Omega$ |
| R3 | $220 k \Omega$ | R8 | $470 k \Omega$ |
| R4 | $20 k \Omega$ | $R 9$ | $1 k \Omega$ |
| R5 | $33 k \Omega$ | $R 10$ | $2 \cdot 2 k \Omega 3$ |

R5 $33 \mathrm{k} \Omega \quad$ R10 $2 \cdot 2 \mathrm{k} \Omega 3 \mathrm{~W}$ w.w
All $10 \%$, $\frac{1}{2} W$ carbon, except where otherwise indicated
VRI $100 \mathrm{k} \Omega$ wire-wound potentiometer
VR2 $500 \mathrm{k} \Omega$ carbon potentiometer
Capacitors:

| C | 50 pF mica or ceramic |
| :--- | :--- |
| C 2 | 50 FF mica or ceramic |
| C 3 | $0.1 \mu \mathrm{~F}$ paper |
| C 4 | 500 pF mica or ceramic |
| C 5 | $4 \mu \mathrm{~F}$ electrolytic 350 V |
| C 6 | $0.01 \mu \mathrm{~F}$ paper |
| C 7 | $0.01 \mu \mathrm{~F}$ paper |
| C 8 | $12 \mu \mathrm{~F}$ electrolytic 25 V |
| C 9 | $16 \mu \mathrm{~F}\{$ dual electrolytic 350 V |
| ClO | $8 \mu \mathrm{~F}$ |
| VCl | 150 FF air dielectric variable |

Transformers:
T1 Output transformer 60: 1
T2 Small mains transformer. Tapped primary. Secondaries: $250-0-250 \mathrm{~V} 40 \mathrm{~mA}$; 6.3 V IA
Valves:
VI 954 V2 I2AT7
Other Circuit Components:
LSI $2 \frac{1}{2}$ in. diameter loudspeaker $2-3 \Omega$
SI Toggle switch s.p.s.t.
MRI, 2 Contact cooled rectifier 250 V 40 mA

## Miscellaneous:

Ball drive 6: I ratio. Knobs: one 2in. diameter. two lin. diameter. One B9A valveholder. Ribbed 4-pin plug-in coil formers (Eddystone). Coil holder (Eddystone). Aerial-earth socket strip.
Tag strip (2 insulated). Chassis 7in. $\times 4 \mathrm{in} . \times 2 \frac{1}{2} \mathrm{in}$. approx. Panel Gin. $x$ tin.

## COIL WINDING DATA

$1 \cdot 2-4 \mathrm{Mc} / \mathrm{s}$ (250-75 metres)
100 turns 34s.w.g., tap at 2 turns. Aerial coupling, 20 turns.
$2.5-7.5 \mathrm{Mc} / \mathrm{s}$ ( $120-40$ metres)
50 turns 32 s.w.g., tap at $1 \frac{1}{2}$ turns. Aerial coupling, 15 turns.
$6.75-22 \mathrm{Mc} / \mathrm{s}$ (44 13.6 metres)
16 turns 30 s.w.g., tap at $\frac{3}{4}$ turn. Aerial coupling. five turns.
$14.5-50 \mathrm{Mc} / \mathrm{s}$ ( $20.6-6$ metres)
$5 \frac{1}{2}$ turns 30 s.w.g., tap $\frac{1}{3}$ to $\frac{1}{2}$ turn. Aerial coupling, two turns.
$40-100 \mathrm{Mc} / \mathrm{s}$ (7.5-3 metres)
$2 \frac{1}{2}$ turns 20 s.W.g., double spaced, tap at $\frac{1}{2}$ turn.
Aerial coupling, one turn.
The two larger coils are close wound. The other coils are on threaded formers, and spaced 21 turns per inch. Aerial windings are near the tuned winding as indicated in Fig. 4(d).



Fig. 3 - Below-chassis wiring


II
$T$ Tuning


Aerial coupling, one turn.
The two larger coils are close wound. The other coils are on threaded formers, and spaced 21 turns per inch. Aerial windings are near the tuned winding as indicated In Fig. 4(d).
V2 12 AT7 (B9A)
(b)

(c)

(d)

Fig. 4 - Coil and valve details.


Fig 5-Chassis drilling details.

## BROADCASTING STATIONS

T-HIS list is not intended to be a complete guide to the many hundreds of short wave broadcasting stations in operation, but it does indicate the stations which, in normal conditions, are most easily heard.

## Frequency Wavelength <br> (kcs) (mecres)

| (kes) | er |  |
| :---: | :---: | :---: |
| 5930 | 50.57 | Prague, Czechoslovakia |
| 5960 | 50.34 | Rome, Italy |
| 5990 | 50.08 | Bucharest. Roumania |
| 6005 | 49.96 | R.I.A.S., Berlin, Germany |
| 6010 | 49.92 | Rome, Italy |
| 6025 | 49.79 | Radio Nederland, Holland |
| 6025 | 49.79 | Lisbon, Portugal |
| 6030 | 49.75 | Muhlacker. W. Germany |
| 6035 | 49.71 | Monte Carlo. Monaco |
| 6055 | 49.55 | Schwarzenburg. Switzerland |
| 6065 | $49 \cdot 46$ | Horby, Sweden |
| 6070 | 49.42 | Sofia, Bulgaria |
| 6075 | $49 \cdot 38$ | Osterloog. W. Germany |
| 6090 | 49.26 | Radio Luxembours |
| 6100 | 49.18 | Belgrade, Yugoslavia |
| 6140 | 48.86 | Voice of America, Tangier |
| 6145 | $48 \cdot 82$ | Allouis, France |
| 6160 | 48.70 | Voice of America, Munich, W. Germany |
| 6165 | 48.66 | Schwarzenburg, Switzerland |
| 6175 | 48.58 | Allouis, France |
| 6190 | $48 \cdot 47$ | Bremen, W. Germany |
| 6190 | $48 \cdot 47$ | Vatican City |
| 7050 | $42 \cdot 55$ | Cairo, Egypt |
| 7105 | $42 \cdot 22$ | Madrid, Spain |
| 7125 | $42 \cdot 11$ | Warsaw, Poland |
| 7135 | 42.05 | Monte Carlo, Monaco |
| 7180 | 41.78 | Baghdad, Iraq |
| 7195 | 41.70 | Bucharest, Roumania |
| 7200 | 41.67 | Belgrade, Yugoslavia |
| 7220 | $41 \cdot 55$ | Budapest, Hungary |
| 7255 | 41.35 | Sofia, Bulgaria |
| 7275 | 41.24 | Rome, Italy |
| 7280 | $41 \cdot 21$ | Allouis, France |
| 7285 | 41.18 | Ankara, Turkey |
| 9009 | 33.03 | Tel Aviv, Israel |
| 9410 | 31.88 | B.B.C. Overseas Service |
| 9475 | 31.66 | Cairo, Egypt |
| 9505 | 31.56 | Prague, Czechoslovakia |
| 9510 | 31.55 | B.B.C Overseas Service |
| 9515 | 31.53 | Rome, Italy |
| 9520 | 31.51 | Voice of America, Tangier |
| 9535 | 31.46 | Schwarzenburg, Switzerland |
| 9540 | 31.45 | Warsaw, Poland |
| 9570 | 31.35 | Shepparton. Australia |
| 9575 | 31.33 | Rome, Italy |
| 9585 | $31 \cdot 30$ | Allouis, France |
| 9620 | $31 \cdot 19$ | Horby, Sweden |
| 9630 | $31 \cdot 15$ | Sackville. Radio Canada |
| 9645 | $31 \cdot 10$ | Vatican City |
| 9665 | 31.04 | Schwarzenburg, Switzerland |
| 9675 | 31.01 | Warsaw, Poland |
| 9700 | 30.93 | Sofia, Bulgaria |
| 9715 | 30.88 | Radio Nederland, Holland |
| 9720 | 30.86 | Radio Nacional, Rio de Janeiro, Brazil |
| 9735 | 30.82 | Deutsche Welle, W. Germany |
| 9745 | 30.78 | Ankara, Turkey |
| 9770 | 30.71 | Vienna. Austria |
| 9780 | $30 \cdot 67$ | Cairo, Egypt |
| 9865 | $30 \cdot 40$ | Djakarta, Indonesia |
| 11705 | 25.63 | Horby, Sweden |
| 11715 | 25.61 | Schwarzenburg, Switzerland |
| 11720 | 25.60 | Sackville, Radio Canada |
| 11755 | 25.52 | Leopoldville, Congo |
| 11800 | 25.42 | Accra, Ghana |
| 11810 | 25.40 | Rome, Italy |
| 11820 | 25.38 | B.B.C. Overseas Service |
| 11830 | 25.36 | Voice of America, Munich, W. Germany and Tangier |
| 11835 | 25.35 | Algiers, Algeria |
| 11865 | 25.28 | Schwarzenburg, Switzerland |
| 11865 | 25.28 | Havana, Cuba |
| 11900 | 25.21 | Paradys, South Africa |
| 11910 | 25.19 | Armed Forces Radio Service, Greenville, U.S.A. |
| 11915 | 25.18 | Voice of the Andes, Quito, Ecuador |
| 11920 | 25.17 | Allouis, France |
| 11925 | 25.16 | Radio Bandeirantes. Sao Paulo, Brazil |
| 11965 | 25.06 | Conakry, Guinea |
| 11990 | 25.02 | Prague, Czechoslovakia |
| 12095 | 24.80 | B.B.C. Overseas Service |
| 15070 | 19.91 | B.B.C. Overseas Service |
| 15080 | 19.89 | Paradys, South Africa |
| 15115 | 19.85 | Voice of the Andes, Quito, Ecuador |
| 15125 | 19.83 | Lisbon, Portugal |
| 15155 | 19.80 | ELWA, Monrovia, Liberia |
| 15165 | 19.78 | Damascus, Syria |
| 15190 | 19.75 | Brazzaville, Congo |
| 15205 | 19.73 | Voice of America, Greenville, U.S.A. |

THIS is a far from easy task on which to give specific information. Forecasting propagation on short waves is, in some ways, as difficult as forecasting the weather. There are certain overall patterns but there are very many variable factors which can affect conditions at any one time. The main changes to be borne in mind are the seasonal ones, the difference between daytime and night-time conditions and, above all, the II-year sunspot cycle.

From now until around 1966 conditions will not change greatly in their main features as we are in a period of low sunspot numbers, and the information given below is meant to apply to this period. Once sunspot numbers begin to increase, the pattern of band usage will change in many ways.

One useful pointer co remember is that broadcasting stations will beam their transmissions to Britain at the time and on the frequencies giving the best chance of good reception. Thus, if Radio Australia broadcasts to us around 07.00 G.M.T. on the 31 and 25 metre bands, that is when expert opinion expects best conditions for the path, although reception from Australia may be possible at other cimes.

All times quoted below are in G.M.T., using the 24 -hour clock system. Let us consider various areas of the world and suggest the best times and frequencies for receiving stations in those areas.

I North America and Caribbean area The best time for this area is between 15.00 and 23.00 during the whole year; in winter the peak is around 18.00 but in summer it is around 20.00/21.00. Western North America is harder to hear, and usually best around 15.00 to 18.00 . For broadcast stations, the best bands in winter are 19 metres in the afternoon. then 25 metres after dark in the summer period. 19 metres is usually best. For the amateur bands, 20 metres is the most reliable all the year, during the winter 40 metres and 80 metres can provide North American stations between 23.00 and 05.00 .
2. Central America This can be an awkward area to hear and the best times are similar to those for North America. For the broadcast bands, as there are not many stations in this area which use the higher frequencies, the best band tends to be 49 metres around 04.00 to 06.00 . On the amateur bands, 20 metres is again the most useful, but this area can come through on 15 metres at times when no North Americans can be heard.
3. South America The best times are around 09.00 to 11.00 and from 17.00 to 01.00 . The Pacific coast tends to be best around 07.00 to 10.00 and later around 20.00 to 02.00 . On the broadcast bands, during spring, winter and autumn, 19 metres is best for the morning period, with 25 and 31 metres best for the evening and night. In summer, the early period is not usually feasible, and 19 metres is best for the evening, but this area is not usually heard too well during the summer. On the amateur bands, 20 metres is usually best, with 40 metres possible later at night, and 15 metres is also a good possibility for the early evening.
4. North A 12.00 to 23.00 , the clock. On usually good ir after dark. usually best, or
5. Central are between I: daylight 19 me better, especial metres is likely to 20.00. This heard during a
6. North A and around 20 Japan. On the On the amateu while recomme
7. South an 11.00 to 17.00 . for the earlier towards the en 20 metres must that 15 metre During the wir extend on to a casting bands $b$
8. Australa: 10.00 and in $w$ New Zealand around 09.00 tc winter and aut the best broads 31 and 41 metr opening which is the favourite
9. Pacific 06.00 to 11.00 . in the area, an Of the amateur
10. Europe day. On the Southern Euro Europe, 19 met day. On the ar and 80 metres occurs on 15 a

## Signal Reporting Systems

|Thas become the usual practice to use some type of code for giving signal reports. The most usual system in use on the amateur bands is a Readability, Signal Strength code, using a scale from 1 to 5 for readability and from 1 to 9 for signal strength. These are not always used correctly and often when incorrectly adjusted "signal strength meters" are used, reports such as "S9 plus 40 dB " are heard. As will be seen below, 99 means "extremely strong" which can hardly be improved on! Following are the scales for readability and signal strength:

## Readability:

## RI Unreadable

R2 Only just readable, and only occasional words heard
R3 Readable, but with considerable difficulty
R4 Readable with almost no difficulty
RS Perfectly readable

## Signal Strength: <br> SI Signals only just perceptible <br> \$2 Very weak signals <br> S3 Weak signals

S6 Good signals
S7 Moderately strong signats
S8 Strong signals
For reporting on celegraphy (CW) signals, an additional scale for "tone" is used to indicate the quality of the note. This is also a I to 9 scale, as follows:

THE "C

THE "Q" C and other its full form. two letters) "what is your location is groups to the usual ones wi QRA Full ad QRH Your QRK Signal price ously)
QRL RM Man-m QRN Atmos ence; QRO High p QRP Low $p$ QRT Closed ORU Nothir QRV Ready

Tone:

## here To Listen

4. North Africa and Near East This area is best around 12.00 to 23.00 , although it is possible to hear it almost round the clock. On the broadcast bands. 16, 19 and 25 metres are usually good in daylight, with 31 and 41 metres being better after dark. On the amateur bands, 15 and 20 metres are usually best, on 15 metres 08.00 to 11.00 is often a good time.
5. Central and South Africa The best times for this area are between 13.00 and 22.00. On the broadeast bands, during daylight 19 metres is best, but after dark 25 and 31 metres are better, especially in the winter half. On the amateur bands 15 metres is likely to be useful, with 20 metres best around 17.00 to 20.00. This area is possibly one of the few which will be heard during any openings on 10 metres.
6. North Asia The best times are around 06.00 to 09.00 and around 20.00, this is not an easy area to hear, especially Japdn. On the broadcast bands, 19 and 25 metres are the best. On the amateur bands, 20 metres is probably the only worth. while recommendation.
7. South and South-East Asia This is usually best around 11.00 to 17.00 . The best broadcast bands are 16 and 19 metres for the earlier part, with 25 metres being most useful later towards the end of the best period. On the amateur bands 20 metres must again be the best suggestion, with just a chance that is metres might occasionally open in that direction. During the winter half it is likely that the best period may extend on to around 21.00 with the 31 and 41 metre broadcasting bands being best for this.
8. Australasia The best times for this area are 06.00 to 10.00 and, in winter, around 14.00 to 17.00 and around 22.00 . New Zealand is not too easy to hear, and is usually better around 09.00 to 11.00 . Reception is much better in the spring, winter and autumn than in the summer. In the better seasons, the best broadcast bands are 25 and 31 metres for the morning, 31 and 41 metres in the afternoon and 19 metres for the night opening which is less reliable. On the amateur bands, 20 metres $r$ is the favourite with 40 metres useful in winter in the mornings.
9. Pacific This is a difficult area usually, and is best around 06.00 to 11.00 . There are few high power broadcasting stations in the area, and 19 and 25 metres are the most likely bands. Of the amateur bands, 20 metres is best.
10. Europe Obviously, this area can be heard 24 hours a day. On the broadcast bands, 25 and 31 metres are best for Southern Europe with 41 and 49 metres best for Northern Europe. 19 metres can provide European reception during the day. On the amateur bands 20 metres during the day, and 40 and 80 metres after dark are best, but in summer short skip occurs on 15 and 10 metres at times.

## THE "Q" CODE

$\mathrm{T}^{+}$HE "Q" Code is used by aeronautical and maritime services and other commercial services and is very comprehensive in its full form. In its correct use, each group (made up of $Q$ and two letters) can stand either for a question (e.g. QTH? means "whot is your location?"), or the answer (e.g. QTH means "my location is ..."). Amateurs have adopted certain of the code groups to their own use and the following list shows the more usual ones with their meanings.

QRA Full address
QRH QRX Wait
QRK Your frequency varies QRK Signal strength (also price or value, humorously)
QRL Busy
QRM Man-made interference
QRN Atmospheric interference; static
QRO High power
QRP Low power
QRT Closed down
QRU Nothing further to say
QRV Ready to operate

## STANDARD FREQUENCY STATIONS

THE frequencies 2500, 5000, 10000, 15000, 20000 and 25000 $\mathrm{kc} / \mathrm{s}$ are set aside for station transmitting accurate frequency standards and also time signals in many cases. Some of these stations are:

QSA Readability of signal
QSB Fading
QSL Acknowledgement of receipt; confirmation of contact
QSO Contact
QSP Pass on a message
QSY Change frequency
QTC Telegram, message
QTH Location
QTR Time check

## THE SHORT WAVE SPECTRUM

THE International Telecommunications Union is the controlling body over the whole of the radio frequency spectrum and allocations have been made from $10 \mathrm{kc} / \mathrm{s}$ to $40 \mathrm{kc} / \mathrm{s}$. The accompanying chart shows the allocations between 1605 $\mathrm{kc} / \mathrm{s}$ and $30000 \mathrm{kc} / \mathrm{s}$, which is the range generally known as the "short waves". The I.T.U. divides the world into three regions for frequency allocation purposes; Region I comprises Europe, Africa, the Near East and the whole of the U.S.S.R.; Region 2 is made up of North America, Central America, South America and Greenland; and Region 3 contains Asia (except the U.S.S.R.) Australasia and the Pacific.

In the main, the allocations in the s.w. range are fairly uniform over all three Regions, but there are a few differences which should be noted.
I. The amateur band 1800 to $2000 \mathrm{kc} / \mathrm{s}$ is only available in a limited number of countries.
2. The broadcasting bands 2300 to $2500 \mathrm{kc} / \mathrm{s}, 3200$ to $3400 \mathrm{kc} / \mathrm{s}$ and 4750 to $5060 \mathrm{kc} / \mathrm{s}$ are classed as "tropical" and are limited to countries in these regions.
3. In Region 2 the amateur band beginning at $3500 \mathrm{kc} / \mathrm{s}$ extends through to $4000 \mathrm{kc} / \mathrm{s}$.
4. In Region 2 the amateur band beginning at $7000 \mathrm{kc} / \mathrm{s}$ extends through to $7300 \mathrm{kc} / \mathrm{s}$ and the allocation 7100 to 7300 $\mathrm{kc} / \mathrm{s}$ is not available for broadcasting.
The chart obviously has to leave out several minor points of difference, but these are mainly confined to the lower frequencies. The main classes of service are indicated as follows:


| 11865 | 25.28 | Schwarzenburg, Switzerland |
| :---: | :---: | :---: |
| 11865 | 25.28 | Havana, Cuba |
| 11900 | 25.21 | Paradys, South Africa |
| 11910 | $25 \cdot 19$ | Armed Forces Radio Service, Greenville, U.S.A. |
| 11915 | 25.18 | Voice of the Andes, Quito, Ecuador |
| 11920 | 25.17 | Allouis, France |
| 11925 | 25.16 | Radio Bandeirantes, Sao Paulo, Brazil |
| 11965 | 25.06 | Conakry, Guinea |
| 11990 | 25.02 | Prague, Czechoslovakia |
| 12095 | 24.80 | B.B.C. Overseas Service |
| 15070 | 19.91 | B.B.C. Overseas Service |
| 15080 | 19.89 | Paradys, South Africa |
| 15115 | 19.85 | Voice of the Andes, Quito, Ecuador |
| 15125 | 19.83 | Lisbon, Portugal |
| 15155 | 19.80 | ELWA, Monrovia, Liberia |
| 15165 | 19.78 | Damascus, Syria |
| 15190 | 19.75 | Brazzaville, Congo |
| 15205 | 19.73 | Voice of America, Greenville, U.S.A. |
| 15220 | 19.71 | Shepparton, Radio Australia |
| 15250 | 19.67 | Voice of America, Bethany, U.S.A. |
| 15260 | 19.66 | B.B.C. Far Eastern Station, Malaya |
| 15280 | 19.63 | Armed Förces Radio Service, Greenville, U.S.A. |
| 15290 | 19.62 | Voice of America, Tangier |
| 15305 | 19.60 | Voice of America, Greenville, U.S.A. |
| 15320 | 19.58 | Sackville, Radio Canada |
| 15330 | 19.57 | Voice of America, Greenville, U.S.A. |
| 15370 | 19.52 | Radio Tupi, Rio de Janeiro, Brazil |
| 15385 | 19.50 | WRUL, Boston, U.S.A. |
| 15400 | 19.48 | Rome, Italy |
| 15445 | 19.43 | Brazzaville, Congo |
| 15475 | 19.38 | Cairo, Egypt |
| 17695 | 16.95 | B.B.C. Overseas Service |
| 17780 | 16.87 | Voice of America, Bound Brook, U.S.A. |
| 17795 | 16.86 | Schwarzenburg, Switzerland |
| 17820 | 16.84 | Sackville, Radio Canada |
| 17895 | 16.76 | Lisbon, Portugal |
| 17920 | 16.74 | Cairo, Egypt |
| 21470 | 13.97 | B.B.C. Overseas Service |
| 21495 | 13.96 | Lisbon, Portugal |
| 21560 | 13.91 | Rome, Italy |
| N.B.-N | ncies of thes eard | given for Radio Moscow or Radio Free Europe gations vary more often than others, but they veral frequencies in each band. |

Readability:
RI Unreadable
R2 Only just readable, and only occasional words heard
R3 Readable, but with considerable difficulty
R4 Readable with almost no difficulty
R5 Perfectly readable
Signal Strength:

SI Signals only just
S2 Very weak signals
S3 Weak signals
S4 Fair signals

| S5 | Fairly good signals |
| :--- | :--- |
| S6 | Good signals |
| S7 | Moderately strong signals |
| S8 | Strong signals |
| S9 | Extremely strong signals |

For reporting on telegraphy (CW) signals, an additional scale for "tone" is used to indicate the quality of the note. This is also a I to 9 scale, as follows:
Tone:
TI Extremely rough ,ote
T2 Very rough note
T3 Rough, low pitched note
T4 Rather rough note
T5 Musically modulated note
T6 Modulated note, slight whistle
T7 Fairly good note, smooth ripple
T8 Good note, slight ripple

T9 Pure DC note
(If the note seems to be crystal controlled, an " $x$ " is added, if the note is chirpy, a " $c$ " is added.)

The readability/strength code can be used for reporting to broadcasting stations, but a better system for this purpose is the SINPO code. This has five scales, each of $I$ to 5 , as indicated by the letters S (Signal Strength). I (Interference), N (Noise, i.e. static), P (Propagation Disturbance, i.e. fading) and O (Overall quality of reception).

The scale for signal strength is: 1-barely audible; 2-poor; 3-fair; 4-good; 5-excellent. The scales for Interference, Noise and Propagation Disturbance are: I-extreme; 2-severe; 3-moderate; 4-slight; 5-nil. The scale for Overall quality is: 1-unusable; 2-poor; 3-fair; 4-good; 5-excellent. Thus, in the SINPO code, a perfectly received signal would be given 55555.

QRL $\begin{gathered}\text { ously) } \\ \text { Busy }\end{gathered}$ $\begin{array}{ll}\text { QRL } & \text { Busy } \\ \text { QRM Man-m }\end{array}$ QRN Atmos ence; QRO High p QRP Low p QRT Closed QRU Nothir QRV Ready

ATA, New
BPV, Pekin
FFH. Paris,
HBN. Neue
IAM, Rome
IBF, Turin.
JJY, Tokyc
is 500 kc
LOL, Buend 15000 kc , MSF, Rugby
OMA, Prag RWM, Mo 15000 kc
WWV, Wa 15000, 20
WWVH, H
ZUO. Joha 10000 kc In addition. and 14670 kc ;
Most of il intervals, and time checks a

## AMATEUR CALLSIGN PREFIXES

AMATEUR radio stations, in common with all other communications stations, have to identify themselves by callsigns. Each station has an individual officially allocated callsign which follows a standard pattern, being made up of a prefix, a numeral, and a suffix. The prefix may be one letter, two letters or a numeral and letter, but it is derived from the international list of callsign allocations. The numeral may have some geographical significance, but this is not always so. The suffix may be one, two or three letters; in the bigger countries they are issued in alphabetical order, but in smaller countries they are often issued haphazardly, a popular idea being to allow the operator to use his initials as his call.

To take an example of a callsign-G3AKA. The $G$ is the prefix allocated to England, the figure 3 has no special meaning and the AKA is the suffix. In another case-say W7XYZ. Here the $W$ is the U.S.A. prefix, but in this case the figure 7 indicates that the station is located in a particular area of the U.S.A., and the $X Y Z$ is the suffix. One final example-say $5 N 2 A B C$. In this case 5 N is the prefix for Nigeria, the figure 2 has no significance, and the $A B C$ is the suffix.
The following is an up-to-date list of prefixes, the numeral is only given here where it is necessary to distinguish between countries, for instance $V Q$ is the general prefix for Commonwealth countries in East Africa, but VQI is Zanzibar and VQ2 is Northern Rhodesia, so the numeral is virtually part of the prefix in these cases. This list is not intended to be an "official" list of countries, the various clubs and societies each issue their own lists of this kind, which only differ where some of the more out of the way places are concerned.

Occasionally, stations can be heard with additional letters, such as $/ P$ or $/ M$ after the callsign. Examples of these and their meanings are: /A indicates the station is being operated from another address than that given in the licence. /P means the
station is being operated "portable", i.e. not from a mains electricity supply;'this letter is usually heard when Field Day contests are being held. M means that the station is "mobile". i.e. in a car or other vehicle. /MM means "maritime mobile", on board a ship. /AM is "aeronautical mobile", on an aircraft In the U.S.A., however, /P and /A are not used; instead, the call area in which the station is temporarily operating is added, for instance W2ZZZ operating portable in the W2 area would sign $W 2 Z Z Z / 2$, if he went over to California he would sign $W 2 Z Z Z 16$. If he crossed into Canada, he might sign $W 2 Z Z Z$ | VE3 and so on.

## CALL AREAS

As mentioned above, in certain countries, there is a subdivision into call areas, indicated by the figure in the callsign. Most of the South American countries use this system, and it also applies in Australia, Canada, New Zealand and the U.S.A. Details for these latter four countries are:
Australia VKI-Canberra; VK2-New South Wales; VK3Victoria; VK4-Queensland; VK5-South Australia; VK6Western Australia; VK7-Tasmania; VK8-Northern Territory.
Conado VEI-Nova Scotia, New Brunswick and Prince Edward Island; VE2-Province of Quebec; VE3-Ontario; VE4Manitoba; VES-Saskatchewan, VE6-Alberta; VE7-British Columbia; VE8-Yukon and North West Territories; VOI-Newfoundland; VO2-Labrador.
New Zealand ZLI-Auckland; ZL2-Wellington; ZL3Canterbury; ZL4-Otago.
United Stotes of America K/KN/W/WA/WB/WN/WV prefixes: I-Connecticut, Maine, Massachusetts, New Hampshire, Rhode Island and Vermont. 2-New Jersey and New York. 3-Delaware, Maryland. Pennsylvania and District of Columbia. 4-Alabama, Florida, Georgia, Kentucky, North Carolina, South Carolina, Tennessee, Virginia. 5-Arkansas, Louisiana, Mississippi, New Mexico, Oklahoma and Texas. 6-California. 7-Arizona, Idaho, Montana, Nevada, Oregon, Utah, Washington and Wyoming. 8-Michigan. Ohio and West Virginia. 9-lllinois, Indiana and Wisconsin. O-Colorado, lowa, Kansas, Minnesota, Missouri, Nebraska, North Dakota, South Dakota.

| AC3 | Sikkim | CO | Cuba |
| :--- | :--- | :--- | :--- |
| AC4 | Tibet | CP | Bolivia |
| AC5 | Bhutan | CR4 | Cape Verde Islands |
| AP | Pakistan | CR5 | Portuguese Guinea, |
| BY | China |  | Principe Is., and Sao |
| BV | Taiwan |  | Thome |
| CE | Chile | CR6 | Angola |
| CE9 | Chilean Antarctic | CR7 | Mozambique |
| CED | Easter Island | CRB | Portuguese Timor |
| CM | Cuba | CR9 | Macao |
| CN | Morocco | CTI | Portugal |

CTZ
CT3
CX
DJ
DL
DM
DU
EA
EAG
EA8
EA9
Azores Islands
Madeira Islands
Uruguay (West)
Germany (Wet
Germany (West)
Germany (East)
Philippine Islands
Spain
Balearic Islands
Canary Islands

EAD Spanish Guinea and

| FG | Corsica Guadeloupe |
| :---: | :---: |
| FH | Comoro Isla |
| K | New Cale |
| FL | French So |
| M | Martinique |
| FO | Marquesas |
|  | $\mathrm{Cl}$ |
| FP | St. Pierre and |
| FR | Re |
|  |  |
| I | St. Marti |
| FU' | New Hebr |
| FW | Wallis and |
| FY | French Guian |
| G | England |
| GB | United Kin |
|  | (special stat |
| GC | Channel Isla |
| GD | Isle of Man |
| Gl | Norther |
| GM | Scotland |
| GW | Wales |
| HA | Hungary |
| HB | Switzerland |
| HBD | Liechtenstein |
| HC | Ecua |
| HC8 | Galapago |
| HH | Haiti |
| HI | Dominican |
| HK | Colombia |
| HL | Korea |
| HM | Korea |
| P | Panama |
| HR | Honduras |
| HS | Thai |
| HV | Vatican |
| HZ | Saudi Arabia |
| 1 | Italy |
| IL | Pelagian |
| IP | Pantellaria |
| IS | Sardinia |
| IT | Sicily |
| JA | Japan |
| JT | Mongolia |
| JY | Jordan |
| JZO | Netherla |
|  | Guinea |
| K | United Stat |
|  | America |
| KA | Japan (U.S |
| KB | B |
|  | Amer |
| KC4 | U.S. Antar |
|  | Navassa Islan |




EVERY PACKET CARRIES A GOVERNMENT HEALTH WARNIN(


[^0]:    275 West End Lane, London NW6 1GS. 01-794 9611

[^1]:    Send S．A．E．for full delails，a brief description of all Ktts and Projects．

[^2]:    

[^3]:    5

[^4]:    5

[^5]:    5

[^6]:    Order by post to Uxbridge Road address or call at either store．Bargains
    galore at both stores－（COMMERCIAL TRAVELLERS PLEASE NOTE：
    Merchandising office at Holborn store．）

[^7]:    Practical circuit for an audio signal generator based on the LM101A/ LM111 combination. Capacitors C1/C2 may be mounted on a range switch and should be of close tolerance and best quality. The frequency control VR1 should be large, physically, and again, of highest quality, if accurate calibration is to be achieved.

[^8]:    VEROBOARO
    $2 \frac{1}{2} \times 3$ in $\begin{aligned} & 0.1 \\ & 24 \mathrm{p}\end{aligned}$
    $2 \frac{1}{3} \times 5$ in $26 p$
    26p
    3) x 3ain $26 p$
    $3 \frac{2}{2} \times 5$ in 30 p
    $2 \frac{1}{2} \times 17$ in 80p
    $3 \frac{3}{2} \times 17$ in 110p $5 \times 17 \ln 140 p$ $2 \frac{1}{2} \times 17$ in (plaln) $3 \frac{1}{2} \times 17$ in (plain) $5 \times 17 \ln$ (plain) Pht. 50 pins Spot face cutte

    | 0.15 | Standard Screened <br> JACK PLUGS (chrome) |
    | :---: | :---: |
    |  | Stereo Screened 30p |
    |  | 2.5 mm Screened Ip |
    | 180 | 3.5 mm Screened 10 p |
    | 26p | DIN PLUGS, SOCKETS |
    | 26p | COUPLERS |
    | 32p | Pin: 2, 3, 4, $5\left(180^{\circ}, 240^{\circ}\right), 6 \& 7$. |
    | 60p | Plugs 12p. Sockets 8p, Couplers10p. |
    | $86 p$ |  |
    | 45p | PHONO PLUGS, SOCKETS, COUPLERS |
    | 63p |  |
    | 89p | PLUGS (Assorted Colours) 5p, |
    | 20p | COUPLERS 6p SOCKETS: Single 5p, Double 7p |
    | 42p |  |
    | 52p | Triple 10p |

    

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[^9]:    Also in the October Issue:
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[^10]:    

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