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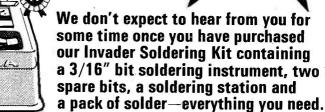


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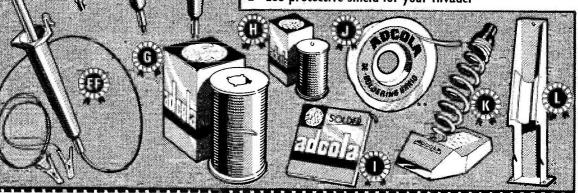
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BRITAIN'S PREMIER MAGAZINE FOR THE DO-IT-YOURSELF RADIO AND ELECTRONICS CONSTRUCTOR

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(b) PAIR OF HI-FI HEADPHONES
(c) MATCHING DYNAMIC
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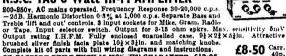


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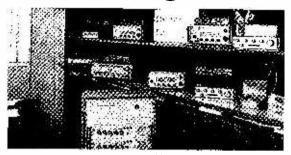
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185	-25	30L1	-29	EBF89	-25	EY87	.29	PCL88	-80		-43
1T4	-20	30L15	-60	ECC81	.20	EZ40	-39	PCL800	-89	CBF80	-34
384	-27	30L17	-70	ECC82	-21	EZ41	39	PCL805	-37	L BESS	-32
3V4	47	30P4	-54	ECC83	-35	EZ80	-21	PENA4	-77	CCC84	-82
5U4G	.31	30P12	-69	ECC85	-31	EZ81	-22	PEN36C	.70		·32
5V4G	-35	30P19	-54	ECC804	-50	EZ90	-25	PFL200	46		-30
5Y3GT	30	30PLI	-56	ECF80	-30	GZ30	-34	PL36	-48	CCH42	-56
5240	-35	30PL13	.78	ECH35	·48	GZ32	40	PLSI	-43	CCHSL	30
6/301/2	-50	30PL14	-80	ECH42	-56	KT41	77	PLSIA	47	UCL82	-32
6 A M 6	-16	35W4	-30	ECH81	-23	KT61	65	PL82	31	UCL83	-50
6AQ5	35	50CD6G	-68	ECH83	-38	K T66	-78	PL83	-33	UF41	-49
6. \ T6	20	807	-55	ECH84	-85	LN319	-56	PL84	27	CF89	25
6AU6	-20	AC/VP2	.77	ECL80	-30	LN329	-80		-58		53
613.46	-20	AZ31	40	ECL82	29	LN339	-65		-58	UL84	-30
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12AU7	-21		27	EF183		PCC189	48	R19	-30	AF115	-20
12AX7	22		47	EF183	27	PCC805	-70		-70	AF116	-20
1933 X 7			-38	EF184 EH90	-36	PCF80	28		70	AF117	.20
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20P2 20P3	75	DY87			65	PCF86	46	U47	73	AF127	.17
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30C1 30C15	·26	EAF42	46	EL90	-35	PCF805	-57		-55	OC72	.12
30C15	76	EB91	12	EL500	-62	PCF806	-56	U 193	31	OC75	·12
30C17 30C18			43		-36		-65		61	OCSI	.12
	24		44	EM81	-36	PCL82	-30		-38	OC81D	·12
30F5	64		.30	EM84	-32	PCL83	-55		-66	OC85	·12
30FL1	65		22		-47	PCL84	-33		.75	OC82D	·12
30FL12	-69	EBF80	-32	EY51	-36	PCL85	-37	CABCSO	-29	OC170	23

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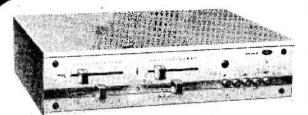
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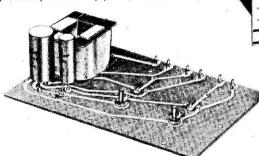


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SPECIFICATION OF UNITS

	110061 003	Plodel 303
Overall Diameter	8"	3"
Natural resonance	30Hz	b-
Main resonance	*35Hz	1200Hz
Magnet Pole Diameter	1"	3"
Magnet Flux Density	13,000 gauss	10,000 gauss
Frequency response	30Hz-8kHz	2kHz-17kHz
Impedance	8-15 ohms	8-15 ohms
Power Handling	*15 watts	*15 watts

Very easy to assemble, this boxed kit comes with acoustic foam damping material, panels, screws, wire, wiring diagrams and instructions to provide a remarkable loudspeaker assembly—a pair is ideal for stereo.

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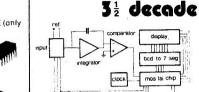
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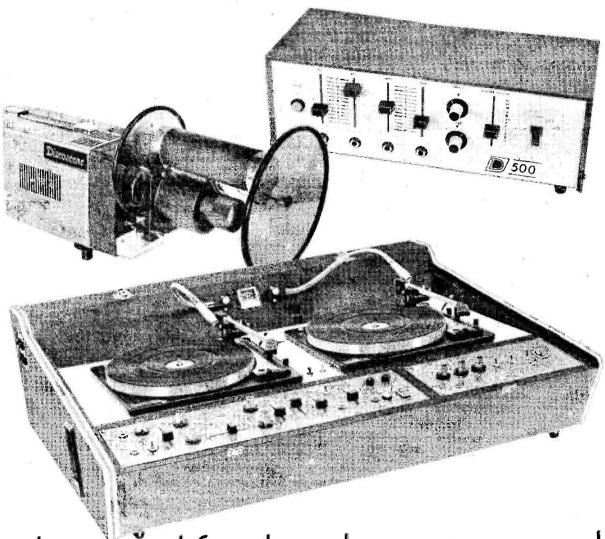
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MIDGET 220 v. 45 mA. 6.3 v. 2 s. 2 v. 24 v. 24c
MIDGET 220 v. 45 mA. 6.3 v. 2 s. 2 v. 24 v. 24c
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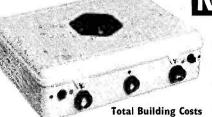
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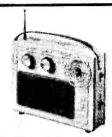
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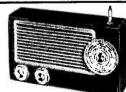


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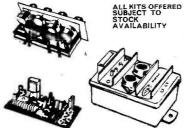
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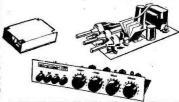
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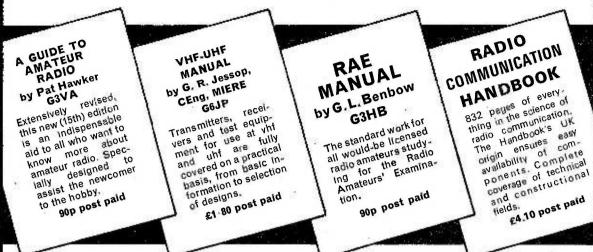
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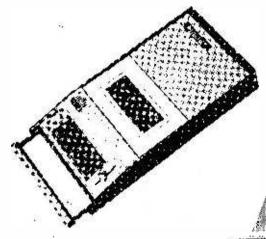
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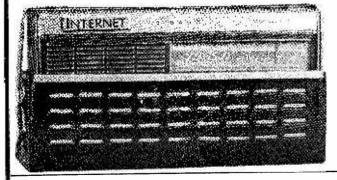
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The Tourist PB can be mounted in any standard size dash panel and it has an illuminated tuning scale. Chassis size is: 7in wide, 2in high and 4½ in deep. Circuit diagram and comprehensive instructions 55p free with parts. Fully retractable and lockable car aerial £1-37 post paid.

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If you can solder on printed circuit board, you can build this push-button car radio kit. It's simple—just follow the step-by-step instructions.

STILL ONLY £49 COMPLETE



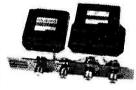
RELIANT MK IV

*5 Electrically Mixed inputs. *3 Individual Mixing controls. *3 Individual Mixing controls. *5 Separate bass and treble controls common to all 5 inputs. *Mixer employing F.E.* (Field Effect Transistors). *Solid Circuitry. *Attractive Styling. Mic. or Guitar 8mV. Inputs. 3, 4-& 5 are suitable for a wide range of medium output equipment (Gram, Tuner, Monitor, Organ, etc.) All 250mV sensitivity. Output 20 watts into 8 \(\Omega\$. \$\mathbb{L} \) \$\mathbb{L

UNISOUND MODULES

ONLY £7.64 + 55p. p & p For the man who wants to design his

own stereo—here's your chance to start, with Unisound—pre-amp, power amplifier and control panel. No soldering—just simply screw together. 4 watts per channel into 8 ohms. Inputs: 120mV (for ceramic cartridge). 120mV (for ceramic cartridge). The heart of Unisound is high efficiency I.C. monolithic power chips which ensure very low distortion over the audio spectrum.



IN-GAR ENTERTAINMENT

With this elegant stereo 8 track add on unit, audio enthusiasts now have the opportunity to extend their systems to include the playing of 8 track cartridges. Simply select your channel, by push button, four digital lamps indicate channel selected. The Viscount III, the

fabulous Stereo 21 and the Unisound Modules 29.90 + 80p. p. & p. will accept this unit, simply connect up.

PE TAPE LINK CONSTRUCTORS

£1 p. & p. £4.00



Suitable 3 speed tape deck, less heads, Caters up to 52 ins. spools. 240V AC mains. Unused but store soiled hence no warranty.

SEE OPPOSITE PAGE FOR ADDRESS DETAILS

ISSUE No.800

THIS issue of *Practical Wireless* is the 800th, in which we take off our hats to our predecessors going back to 1932. In those days *Practical Wireless* was a weekly and cost three old pence, and they certainly crammed in a great deal of material that was the slightest bit related to wireless in almost every sense. We recommend a look at our Going Back feature this month. What an eye-opener!

Today 41 years later things are very different, with changes in technology and a totally different attitude in the politics involved with entertainment electronics.

Readers will probably have noticed this from the international flavour of last month's issue, in which we showed that the whole of the entertainments electronics scene is not, of course, as parochial as it was in the 30's. Commercial competition rages furiously now in what we call the rat-race. To keep up with it, today's magazines have to employ human dynamos, always looking for new or different ways of encouraging readers to exploit new technology and ideas.



Here you are, chief! All 800 issues packed into one integrated circuit. Just arrived on the 8 o'clock carrier pigeon from "Ireland".

DO-IT-YOURSELF QUAD

In this issue we present a do-it-yourself "first". In quadraphonic sound there has been much argument which no doubt you will have heard about. We became fed up with waiting for someone to decide on a standard or universal system. So did the various manufacturers. We confidently predict that the Audio Fair in October will show a very wide variety of equipment that will attempt to satisfy the growing interest in quad.

But to the best of our knowledge this is the first time that a compatible four-system quad design with description and full constructional details has been published in a radio and electronics do-ityourself magazine. A decoder for CD-4 can also be

used with this unit.

In addition to enhancing ambience in reproducing recorded music, quad opens up a whole new form of aural effect that adds an indescribable sensation to recorded pop music of any kind. The listener can get a feeling of complete relaxation in the midst of his music, no matter how off-beat it might be.

There are several ways of getting quad sound and we have exploited all of them. So with Project Q4

you can choose to play stereo records or tapes through the different quad decoding processes; you can also play any currently available quad record through either the decoding process intended for it or through one of the other decoding channels for some different effects.

We have not used valuable magazine space on describing amplifiers and other equipment specially for this decoder, because we believe that most constructors will want to choose their own, whether they are commercial products or home-made. Most constructors will already have a stereo amplifier system of some kind so it is a simple matter to add to this our Q4 Decoder and another identical stereo amplifier and speakers. If you are starting with no equipment you still have the choice. It need not be expensive.

With this set-up, you can start quad straight away with stereo records or tapes, best played through the RM, SQ or QS channels. Even with this, the results will be quite staggering, and we hope you will then be encouraged to invest in quad records and tapes as and when available for the SQ, QS and discrete four-channel systems.

EXPERIMENTING

Also in this issue we start constructors on the trail of phase locked loop circuits. The ideas and theory behind phase locked loops are far from new; we think that many readers will have read enough theory about this subject already. We have therefore cut the theory down to manageable proportions so that constructors can get started on making up some interesting projects.

This month we start off with a.m. and f.m. demodulators and next month we exploit phase locked loop i.c.s for metal detection. Further articles showing their versatility will be published in future issues of Practical Wireless.

At a time when schools and colleges will be commencing new courses and sessions, we are providing a new series of self-contained articles describing how to learn while you build. "Experimental Workshop" explains the theory with working practical projects. You don't have to use soldering irons so you can re-use the components again.

We hope you will all find Issue No. 800 interesting to read and worthy to keep. As a bonus, we have included the first pair of PW Data-cards. Look out for more in this series in the next two issues.

M. A. COLWELL-Editor

The November issue, on sale 5th October, will include for all readers, and specially visitors to the London Audio Fair, an extra 8-page supplement "Dictionary of Audio Terms" to help you understand the language; the "P.W. Ferret" our new metal detector design using a phase locked loop i.c.; the second pair of P.W. Datacards dealing with DIN plugs and decibels. Further details on page 531.

NEWS..

NHWS...

NEWS...

Computerised security network

minicomputer-controlled security network has been put into operation by a major bank in Pittsburgh, Pennsylvania, to watch windows, doors and bank vaults, and to call the police if the bank is robbed. One bandit was recently arrested less than two minutes after police headquarters received a teletype alert printed out on the command of a Computer Automation Alpha 16 minicomputer incorporated in the bank's new Diebold DGM-320 Security System.

This police alarm was an automatic function of the system, which continuously monitors security sensitive areas in the bank's head-quarters and 22 area branch offices, through electronic sensors plugged

into a private data communications network, as well as a CCTV system.

All conditions concerning security contact points are programmed into the minicomputer's 8K 16-bit core memory. The computer knows, for example, when a given area is secured or open for entry, and reacts instantaneously to every deviation from norm, implementing a series of prescribed activities designed to meet the potential 'emergency'. In routine operations, the minicomputer initiates a survey of all security points every 100 milliseconds, and instantly produces a legible teletype status report on every checkpoint.

The information-generating devices installed in security areas cover a broad spectrum of sensors and switches, noting such activities as the opening and closing of doors, windows and vaults. Also included are heat and smoke detectors, ultrasonic and infrared sensors. The system activates alarm devices to alert security personnel and/or the police when the vaults are entered illegally, when the bank or any of its branches are robbed, or when someone tampers with any of the multitude of security devices. The security minicomputer system's matically determines whether a circuit has been cut, shorted or plugged into an external PSU.

When the DGM-320 system detects an emergency condition, it tells security personnel exactly what steps are to be taken to handle the situation by projecting a 35mm slide on a screen mounted in the system console; in addition, a teletype report is printed out and any required audio alarm is sounded.

Price slashed

ENERAL Instrument Microelectronics have slashed the small quantity prices of their single chip calculator series and are now offering their C500 microcircuit for £13.70.

This £18 reduction is such that an individual engineer can now build a complete calculator, using extensive application notes supplied with the microcircuit, for well under the market price. Equally the new pricing structure, resulting from the high volume of production now being achieved by the Glenrothes production unit, will make it extremely attractive for users such as instrument manufacturers to utilise the chip in instrument design, thereby economically deriving from one measurement a wide variety of parameters.

Radio in the N.E.

T the time of going to press it was expected that independent radio for the Tyne/Wear area would be run by Metropolitan Broadcasting. The IBA announced that they are having more detailed discussions with the company and would make a further announcement in September.

Meanwhile the starting date for broadcasting independent radio in London and the South-East was still not available.

Welsh radio

THE I.B.A., after full consideration of the two applications for the Swansea radio franchise, proposes to offer the contract, subject to certain conditions and further detailed discussion, to Swansea Sound Limited (Chairman — Mr. John Allison).

Storage tube

NEW cathode ray tube from Mullard is designed for use with laboratory oscilloscopes which require a half-tone storage facility. Designated L14-110GH/55, it is a 14 cm. rectangular tube with a storage time of at least 1·5 minutes. The scan area is 90 x 72 mm. (10 x 8 divisions of 9 mm.). Correction coils supplied with the tube enable the raster to be aligned with the internal graticule.

P.C.M. in the North

HE BBC has now completed a further stage in its p.c.m. sound distribution system, which will make it possible to start a full stereophonic service from the stations at Holme Moss (near Huddersfield) and Belmont (near Louth, Lincs).

The use of the p.c.m. system means that the standard of technical quality will be appreciably higher than has been possible until now, and this improvement will apply to monophonic, as well as stereophonic reception.

Test transmissions in stereo started from both stations on August 4, and they will be maintained throughout programme hours as far as possible. But it may be necessary to revert to monophonic transmission on occasions, for essential engineering work. The date for the start of the full service will be announced later.

G3UDN

THE Mid-Warwickshire Amateur Radio & Electronics Society, G3UDN, inform us that they will resume full activities at their clubrooms on September 10th after their summer recess.

Meetings will be held each Monday evening at 8.00 p.m. at 28 Hamilton Terrace, Leamington Spa, and further information on club activities can be obtained from Alan Outhwaite, G8GDY, 7 St. Ann's Close, Leamington Spa.

Demodulating AM/FM the easy way or

PHASE LOCKED LOOP TECHNIQUES

W.S.POEL G8CYK

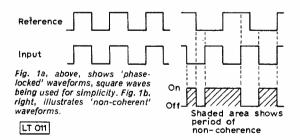
HE phase locked loop (PLL) technique is very little used by amateur radio and electronics enthusiasts. Perhaps too many people are daunted by the rather grandiose images conjured up by the title; which is a great pity, since the theory of operation is very straightforward. Thanks to the range of PLL integrated circuits, notably by Signetics and National, it is a very simple matter to put the theory into practice.

FIRST PRINCIPLES

As the name suggests, the basis of this system is a signal whose phase is the same as another signal, i.e. the reference source. At this point, a diagram will convey far more than a hundred words. There are two viewpoints when considering the reference signal:—

Fig. 1a. The reference may be derived from a crystal controlled oscillator, and may then be divided a number of times, say 'n'. The PLL will then be caused to operate at this frequency: the crystal frequency, divided by 'n'.

Fig. 1b. The reference may be the oscillator in the PLL itself, as in the case where the device is used as a demodulator.



ELEMENTS IN THE LOOP

The purpose of the **phase comparator** section, Fig. 2, is to compare the two signals at its inputs and produce a 'control' voltage at its output which is proportional to the frequency difference, or phase difference, between the input signals.

The low pass filter immediately after the phase detector control voltage output is to smooth out the high frequency components of the control voltage and so improve the stability of the voltage controlled oscillator.

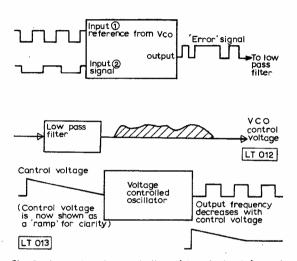
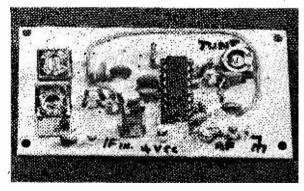


Fig. 2a, top and centre, production of 'error' signal from phase comparator.

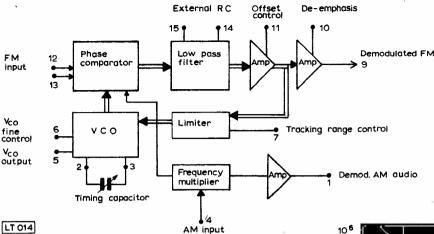
Fig. 2b, bottom, change of output frequency by control voltage to VCO.

The voltage controlled oscillator, see Fig. 2, can be any form of variable frequency oscillator whose output frequency is a function of a controlling voltage. This can be a varicap tuned oscillator, but in the PLL IC described later, it is a voltage controlled multivibrator. The control voltage is derived from the error voltage from the phase detector. It should be noted that increasingly positive control will cause the VCO to go higher in frequency, and vice versa.

A practical loop system is shown in the block diagram of Fig. 3, using the Signetics NE561B IC.



Author's prototype decoder for NBFM at 455kHz. The board, shown full size in Fig.9, includes a mechanical filter and matching transformer.



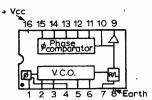


Fig. 3. A phase-locked system using the NE561B IC. Connections are given for the 16pin dual-in-line package, viewed from on top.

APPLICATIONS OF NE561B

Apart from containing the essentials of the loop, the NE561B contains much more beside and can be used for tone decoders, telemetry decoding, signal reconstitution, tracking filters, FSK receivers, wide band detectors, AM and FM receivers.

Before running through the list it is as well to examine this excellent device in closer detail. As well as the classical loop components, there are a number of amplifiers, and a 'multiplier', which will be described when considering the action of the IC as an AM radio.

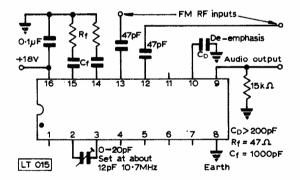
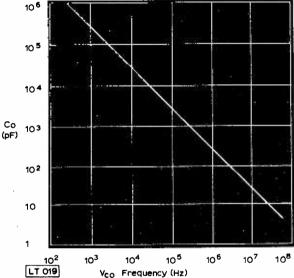


Fig. 4. Basic circuit using the NE561B as an FM demodulator at 10·7MHz.

TABLE 1

1772h -						
10-2006 WILLIA	Min.	Type	Mex	Conditions		
Derection Threshold pV		120	300	Var-		
Demod. Amplifish µV	30.	80		teV RMS		
Distriction % Tieth		113	10	76kHz DevinBoh		
Signal + Noise dB Notes		35		f=1kHz		

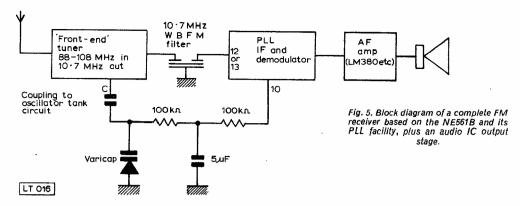


Graph for determining the value of the timing capacitor connected between pins 2 and 3 on the IC.

FM demodulation (includes FSK, telemetry), Fig. 4. The NE561B will demodulate FM to a minimum of 15MHz, and typically up to 30MHz. To take, as an example, a wide band FM demodulator for 10·7MHz, the circuit is supplied with the correct timing capacitor for the VCO, as determined from the graph. For 10·7MHz a small trimmer of 0-20pF is recommended. Signetics specify the results as shown in Table 1.

One of the main advantages of the PLL FM demodulator is the automatic frequency control facility. The PLL itself will track the input signal by a minimum of $\pm 5\%$ of the input frequency, in this case $\pm 535 \text{kHz}$. A typical range of $\pm 20\%$ is given, so be prepared for $\pm 2140 \text{kHz}$!

One proviso though; if the wanted signal happens to drift through a stronger signal, or merely happens to be very close to a stronger signal, the loop will then lock on to this other signal. A ceramic FM filter is therefore a necessity to keep out unwanted signals. The tracking range of the device itself can be restricted by reducing the signal level, since the range is largely a function of the signal amplitude.



The figures given here are for a 5mV signal, the threshold voltage is the input signal where lock just occurs.

Since the VCO control voltage closely follows the deviation on the incoming signal, this can be used as the audio signal, Fig. 5.

With the popularity of NBFM (±2.5kHz) on amateur bands, and not only on VHF, it is useful to realise that the NE561B will also work here. Considering the deviation as a percentage of the signal frequency, the following figures are obtained:—

WBFM at 10·7 MHz = 75kHz
$$\% = \frac{75}{10700} \times 100 = 0.7\%$$

NBFM at 455 kHz =
$$2.5$$
kHz $\% = \frac{2.5}{455} \times 100 = 0.55\%$

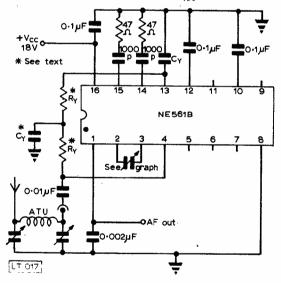


Fig. 6. The NE561B can also be used to demodulate AM signals, as shown in this simple complete receiver.

So, if the value of the timing capacitor is chosen for an IF around 455kHz, then NBFM can be very satisfactorily demodulated without the need for any coils whatever.

Figure 3 showed a fine tune control at pin 6 and by applying a small voltage via a preset the VCO can be tuned in this way. In order to determine the correct value, it is best to refer to the device data sheet before any experimental attempts are made. (Mistakes may be costly!) Similar comments apply when considering the tracking control range.

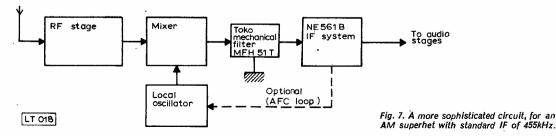
The AFC loop in the IC can also be tapped to provide AFC to the front-end oscillator. By taking the output from pin 10, feeding it via $100 \mathrm{k}\Omega$ and a low pass filter to the AFC varicap, a vast tracking range can be attained, but it is subject to the limitations discussed earlier.

AM demodulation, Fig. 6, is the distinguishing feature of the NE561B. No other IC in the range is capable of AM demodulation. The PLL can only detect FM, so some modification is necessary. It turns out to be a kind of 'quadrature' detector in reverse! By means of the external phase shift network the AM signal is shifted through 90°.

Although the values should change when tuning over the MW band there is sufficient tolerance to allow the band to be tuned from end to end. The minimum (typical) signal to maintain lock is only 100μ V so the device can be used straight away as a receiver, just attaching an aerial as shown. If strong signals predominate, then include a simple aerial tuning device to enhance selectivity. Of course, when used as an IF strip, i.e., after an RF stage, mixer and filter, the NE561B does away with the need for IF coils and all the encumbrances of standard techniques, Fig. 7.

of standard techniques, Fig. 7.

Signal Reconstitution This is the last function of the NE561B that will be considered in detail although other members of the PLL family are more specifically applicable.



With reconstitution, the idea is to salvage a badly distorted, noisy or generally damaged pulse. Fig. 8 gives the idea in detail. The reconstituted pulses are taken from the VCO output and can be processed as required in standard digital circuitry. An interface to TTL is also shown which means that the loop can be locked to one of the standard frequency transmissions, notably Droitwich on 200kHz, and then divided down to provide very accurate frequency markers.

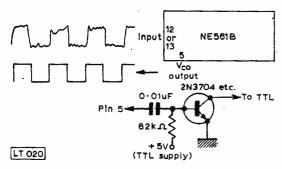


Fig. 8. NE561B used for the reconstitution of 'damaged' signals.

CONSTRUCTION

The author's layout of the pcb is shown in Fig. 9. The material used is fibre glass ¹161in. copper laminate since this does not suffer any of the problems experienced with paxolin based board such as the peeling of the strips and general brittleness. The board can be either etched at home or purchased ready made.

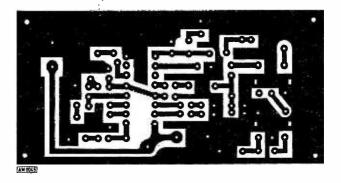
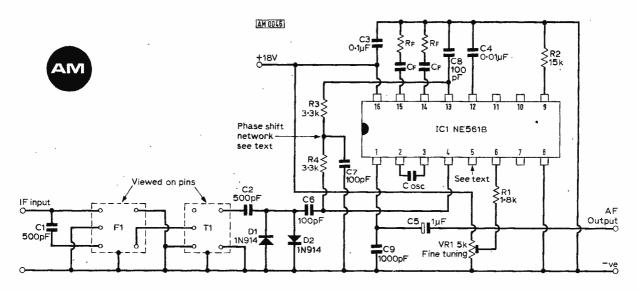
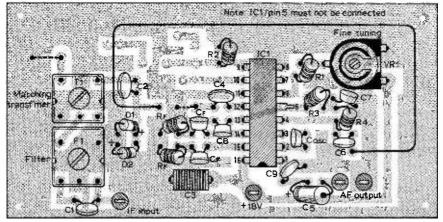


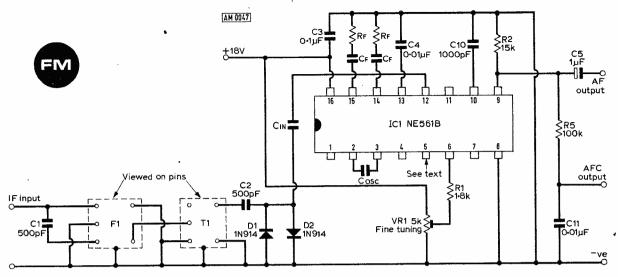
Fig. 9. Full size layout of pcb for those that wish to make their own board.



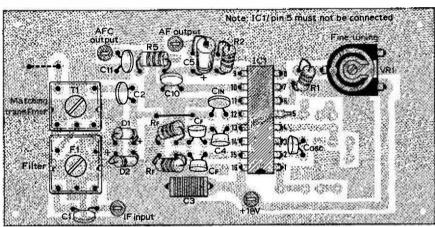
▲ Fig. 10. Complete circuit of the AM decoder board including the mechanical filter F1 and matching transformer T1.



The layout of components on the plain side of the board for the AM circuit shown above.



▲ Fig. 11. The FM decoder circuit using the same printed circuit board as for the AM circuit.



Components on top of the pcb for the FM circuit. ▶

Note that the track under pin 5 of the IC is not in any way connected with that pin. When mounting the IC remember to bend pin 5 inwards. If a socket is used, either bend or remove the pin 5 position.

When the board is prepared solder the components on as shown in Fig. 10 or 11. Two layouts and circuits are shown for the NE561B, one for AM detection, and the other for FM. It is possible therefore to change the operation quite simply, by switching the input and output. The phase shift components need not be removed for FM operation.

There is provision on the board layout for the incorporation of a mechanical filter from the MFH range by Toko. Bandwidths are available from 4 to 7kHz, depending on application. If a too narrow filter is used for NBFM, the signal will be reduced so greatly on deviation peaks that the loop will lose lock and a noise burst will result, making the modulation sound very choppy. Probably the lowest value to choose is 7kHz.

CHOOSING THE CONDITIONS

The filter shown is specifically for 455kHz, so if operation is desired at this frequency, it will be seen from the graph that the value of the VCO timing capacitor is approximately 1000pF. The fine

frequency adjustment can be made on the preset potentiometer.

For AM detection, the values of the phase shift network can be two $3.3 k\Omega$ resistors with 100pF capacitors, though the formula for computing this value allows for an almost infinite combination of values.

Operation at other frequencies can be calculated from the information given, the most probable use is perhaps the WBFM demodulator, at 10.7MHz. Followed by the coil-less PLL FM stereo demodulator, it is possible to produce a formidable array of technology just for "consumer" use. In this case the 455kHz filter is obviously not required, a 10.7 MHz IF transformer being included instead.

TESTING AND ALIGNMENT

Once the assembly is completed, check that the IC is in the right way round. This is an all too easy mistake to make. Clear the swarf from the copper tracks and make certain that there are no stray blobs of solder.

Attach an audio amplifier stage and switch on, whilst monitoring the current. About 10mA is correct if all is well. There should be a quiet hiss from the speaker and if a finger is placed on the PLL input,

it is quite likely that you will pick up general

SW/MW signals.

Now, find some source of IF at 455 kHz, which can be a signal from the IF of a communications receiver or pocket portable, and tune in a station. As the PLL acquires lock a rushing sound will be heard, followed by a click as lock is attained. The 'no lock' noise level will be quite high when operated in the NBFM mode and requires some form of interstation muting if the gain is increased.

* components list

COMMON COMPONENTS C1 SUPPRISE CERSONS C2 SUPPRISE CERSONS R1. 1 8k1/ R2 15k0 580 (2 off) Fo 5kD linear C3 Of UF min. foil C4 +0-01pF disc ceramic C5 1pF 25VW ejectro vic C6 1000pF (2 off) disc cer Cess 1000pF disc ceramic. minimuse pre-set 01/02 (NS14 IC) MESSIG and holder F1, Mochanical files (Toke) (Ambit) T1, Matching (repsformat (Toke (KET667) (Ambit) Prince Terreinal pina (6). * ess text. ADDITIONAL COMPONENTS AM UNIT C5 100pF dies carumic C7 100pF dies carumit C8 100pF dies gerande C9 5000pF dies paramete 3000 FM UNIT Today F disc ceramic distuit disc ceramic se to 200pt (dist critical) 100sC All rearestors \$1, 1 or IW The real repay striked and packind and suitable for although it sentiable from Ambal internations, if high Street Brentween, Essex, for the A basic kill commissing pcb. IC and holds, mechanical files and matching transferred can be applied see in Propes include VAT and pip.

There is very little to do in the way of alignment, since the PLL aligns itself. All that needs to be done is to bring the PLL VCO as close to the operating frequency as possible, by means of the preset on the board. To do this, tune to a weak station and lower the input level slowly until lock is just lost. Now turn the preset until a heterodyne whistle is heard as the VCO sweeps through the carrier. Adjust for zero beat, whereupon the VCO frequency and IF frequency are the same. This means that the PLL has less range to track to capture the desired IF signal and that lock will be maintained on weaker

It is very difficult to list all the possible applications of such a simple IF unit since if used in conjunction with the mechanical filter it forms a complete IF strip, requiring just the input from the mixer. The filter cores should be carefully adjusted for maximum output which will correspond to maximum noise when the loop is off lock.

ELEVISIO

OCTOBER ISSUE

Basic Colour faults Guide ... in full

This issue of Trievision contribs a special contribution properties, which you can put not and lead to reference, showing by means of off-amount colour photographs, the basic colour facts that can accur. The accompanying text explains the passer, and the cures, of the builts.

VARICAP TUNING SYSTEM
Television's correspondent on long melance
TV reception has a equipped his excessing male
ration with varical tuners. These are boused with
the necessary power expenses and inclination, in
compact dieedstriones, with versical fer title
and WHF. Full cessies are given of these units
which have proved very successful in title.

This is an opportunity to get acquainted with the new techniques necessitated by the change to 410 solour tubes. Television has taken a netalled jook at the first 110° polour chassis to come from a UK setmaker. The Mulland Phase II decessive used a expected to be realized in other new generation changes now in the pipeline.

SERVICING TV RECEIVERS

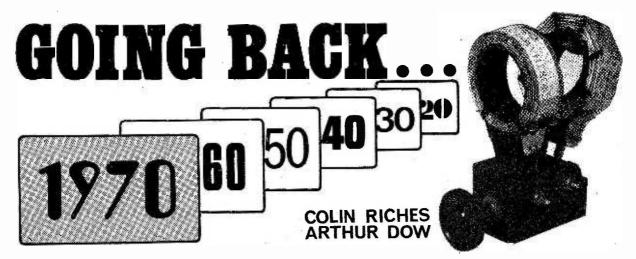
This, leature details, the common leads as presented with the LTT/KB VC300 single details in increasing points of this cause is in the use of prince causeless.

of the CRT. I.
Also in this leave is a fath finding guide covering the timebase recurs awar in the Philose 107 CTSIA. series.

RECEIVER DE BUIGDING
Part 3 in this series describes the effects on the
picture of deficiencies in the characteristics of the
IF and object chickels and the addensates to take to
reduce these to a minimum.

PLUS ALL THE REGULAR FEATURES

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ADDRESS	***************************************				
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Since the Practical Wireless century stepping stones take quite a while to come around perhaps we ought to take the opportunity in this issue No. 800 to look back at earlier marker points along the way. We might not be here for No. 900! In case any reader is doing a quick bit of mental arithmetic, it is of interest to make the point that in the early days of PW it was a weekly magazine, so the 100's rolled round that much faster!

Issue No. 1 Volume 1 of Practical Wireless was dated September 24th, 1932, and went to 68 pages in a 10^3_4 x 8in. format. Published weekly by George Newnes at a cover price of 3d it was edited by the redoubtable F. J. Camm assisted by H. J. Barton Chapple, Frank Preston, W. J. Delaney and W. B. Richardson on the Technical staff. Quoth the Editor "a well equipped laboratory staffed by enthusiastic experimenters closely associated with the home constructor movement will examine and test the latest components, the results of which will be reviewed in Practical Wireless."

The new 200kW Radio Luxembourg transmitter started up on the long wave band "despite international protests on the choice of 1275 metres." One writer affirmed "the variable-mu valve has come to stay and listeners who are troubled with swamping from a powerful local station should fit one if it is humanly possible." Anyone heard yet of a variable-mu transistor? Seems to be badly needed on many modern radios.

An "Experimenter's Baseboard" was fabricated from wood strips to provide slots in which movable bolts could be used for fixing down individual components when mocking up a circuit. Items published on the "Radio Wrinkles from Readers" page were rewarded with half a guinea, provided that the idea was original.

A review appeared of a kit of parts for making what was to become a very famous receiver, the Lissen Skyscraper. With the three valves, loudspeaker and walnut cabinet you would have been set back £5.5.0. in those days! For the constructor starting from scratch there was the Dolphin Straight Three design while W. B. Richardson exploded some commonly accepted notions about wireless on the "Radio Fads and Fallacies" page.

With this first issue of PW went a free blueprint

With this first issue of PW went a free blueprint for making the "Long Range Express Three" proudly described as "The Set of the Year". This blueprint

was the start of a very successful series of blueprints for various wireless sets and auxiliary equipment that went on into the 60's. Even today requests for back numbers of these blueprints are not infrequent. No. 100 came up in Volume 4 and was for August 18th, 1934, and still priced at 3d. A great splash was made on the cover and inside of the National Radio Exhibition held at Olympia at which PW had Stand 8. "How to get there" and stand location information was given as well as a review of the exhibits themselves.

Prominence was given in the issue to the first number of *Practical Television*, "on sale now" price

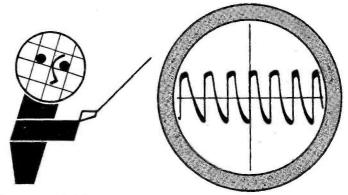


Believe it or not, we could not find a cover for No. 1 of PW, only a bound volume. So here is No. 100 instead.

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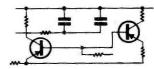
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H8/3	3µf	50v	4p	H7/6	100µf	25v	5p
H8/3A	441	50v	4p	H7/6A	100µf	15v	4p
H8/4	4-7µf	25v	4p	H7/7	100µf	25√	4p
H8/4A	5µf	64v	4p	H7/8	125,41	16v	5p
H8/5	5µf	10v	4p	H7/8A	$100\mu f$	35v	6p
H8/5A	5µ1	150v	4p	H7/9	100µf	63v	6р
H8/6A	1041	10v	4p	H7/9A	125µf	4v	4p
H8/7	10µf	70v	4p	H7/10	125µ1	25v	€p
H8/8	1641	35v	4p	H7/10A	160µf	2·5v	3p
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H8/9	20µf	6v	2p	.H7/11 A	150µ4	16v	5p
H8/9A	20µ1	70v	4p	H7/13A	2004	25v	8p
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H8/11A	24µf	275v	4p	H7/15A	220µ1	35v	10p
H8/12	3241	15v	4p	H6/1A	250µf	4v	3р
H8/12A	30µf	10v	4p	H6/3A	320uf	2+5v	3p
H8/13A	32 µf	50v	4p	H6/4	$320\mu t$	10v	4p
H8/14	40j.tf	25v	5p	H6/4A	330µ1	16v	5p
H8/14A	40µf	16v	45	H6/5	330ut	25v	10p
H8/15	4741	50v	4p.	H6/5A	330µ4	35v	15p
H8/15A	40µ1	35v	4p	H6/7	400µf	15v	. 5p
H7/1	50µ1	6v	3p	H6/8	470µl	25v	7 10p
H7/1A	50µ1	10v	4p	H6/8A	470/4	35v	20p
H7/2	50µf	50v	4p	H6/9A	400µ1	40v	20p
H7/2A	6441	2 ·5v	20	H6/10	750µf	12v	5p
H7/3A	64µf	25v	4p	H6/13A	1000µ4	25v	16p
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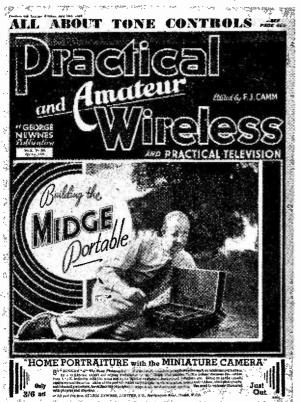
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6d, while in the parent paper W. J. Delaney suggested that the Friday morning experimental TV transmissions from the BBC on 261 metres (yes, on the medium waves!) could very well be viewed out in the country . . "the equipment can easily be accommodated in a car, together with the batteries . . . the set can be one of the portable disc types! A wireless receiver was also carried to get the sound channel. A photograph showed two enthusiasts taking up the suggestion.

A survey of developments in valves noted the QPP (quiescent push-pull) double pentode battery valve having very low standing current, the production of much smaller valves without sacrificing reliability and changes to the shape of the valve envelope to enable it to more rigidly support the electrode assembly.

The constructors among the readership enjoyed themselves with the "Armada Mains Three", a low priced efficient radiogram design or the "Summit" three valve battery receiver which incorporated the WB "Stentorian" loudspeaker which was to become extremely popular probably because of the built-in tapping switch and transformer enabling the speaker to be very quickly matched to any output valve. In an accompanying competition the magazine offered fifty of the speakers to readers who could place a list of the speaker's virtues in the right order.

No. 200 for July 18th, 1936, now had gained a resplendent title! Practical and Amateur Wireless and Practical Television, no less. Obviously there had been some takeovers in the interim! but it was still a weekly and still 3d. Inflation, evidently, was not an "in" word at that time.



By 1936 No. 200 of PW had absorbed both Amateur Wireless and Practical Television.



After six years of publication PW still retained a cover price of 3d. as shown here with No. 300.

The cover and main article spread themselves on the subject of the "Midge" portable receiver with an internal frame aerial, the forerunner of the modern ferrite rod aerial. "Facts and Figures" dealt with components tested in the magazine's new laboratory and reported on the Avo capacity meter and Collaro automatic record changer.

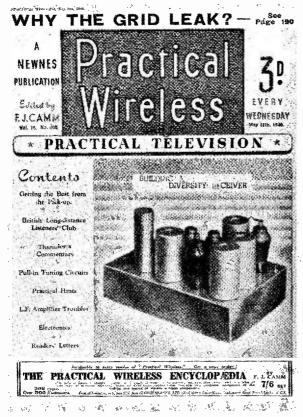
For listeners to the short wave bands Frank Preston described various desirable refinements that could be made to a short wave receiver with a view to obtaining smoother reaction, a highly prized objective. The repairman could glean a lot of useful tips from "Speedy Repairs" which showed how many receiver breakdowns could be diagnosed and fixed "in less than five minutes!" The modern dealer would give an awful lot to have that capability available today!

Practical Television was allowed a whole page to itself leading off with chat on television studio scenery followed by a report from the USA on a new invention that obviated the need for separate receivers for sound and vision frequencies. It was thought that two sets would still be needed for the BBC's TV service, yet to come, accommodating them in the same cabinet.

A Chicago receiver manufacturer managed to produce a set with forty valves. Wireless but not valveless . . . probably also had a valve factory just round the corner!

No. 300, still going strong on June 18th, 1938, at 3d a week featured a 2½-watt battery amplifier on the cover and centrespread. The Class B stage consumed little current without any signal but it must have been a fair load on peaks for the 135 volt high tension battery!

For the summer months the magazine recommended its experimental short wave receiver for the outdoor life. However, Practical Television's two pages reported high winds at Epsom racecourse which interfered with the BBC's efforts to televise the Derby although it all came right in the end. A London cinema fixed up an 8ft x 6ft 6in TV screen to enable viewers to see Bois Roussel romp home. The radio link between Epsom and Alexandra Palace was on 5 metres (60MHz).



Wartime issue No. 400 of 1940 but PW was not to retain its price of 3d much longer. By September it had doubled to 6d.

A newspaper reader was reported to have complained about the frequent use of gramophone records by the BBC. He felt that he was "not getting his 10s. worth"! One reader's wrinkle was to add a lead balance weight to his pickup thus "reducing the weight on the record to about loz." Mind you, it was a 78! In a kind of "Going Back" atmosphere L. Ormond Sparks recalled how he had, in 1923, installed radio equipment in a motor coach for the first time. Being an open coach the aerial system had to be rigged in such a way that it did not interfere with the passengers. These good folk plugged their headphones into a socket located near each seat. The coach company organised strategically planned round trips enabling the passengers to listen to the station at Cardiff during the evening's run.

W. J. Delaney contributed a couple of ideas on improving the PW two valve deaf aid and "News from the Trade" looked at Tungsram valves, a new Hivac cathode ray tube akin to the VCR139, a Cosmocord playing deck and WB transformers for audio and mains use.

No. 400 issue of May 18th, 1940, continued the old price of 3d but by June had gone up to 4d and upward again to 6d by the issue for September, reflecting the new wartime conditions. A "Dig for Victory" photograph showed allotment enthusiasts digging furiously to music from an Ekco portable radio.

The equipment review covered the GEC portable set which used a single battery supplying the 1.5 volts for the filaments and 90 volts HT for the anodes of the valves. The price for the receiver was just £8.18.6.

A very interesting column which had, in fact, been going for some time was the "Replies in Brief" feature. In this a few lines only were devoted to replying to any reader whose query did not justify more detailed treatment or was not considered to be of general interest. Provided one was not in a great hurry for a reply, this system probably served its purpose.

The British Long Distance Listeners' Club had a page to itself for letters from its members describing their activities and experimental work. An interesting article described "pull-in" tuning circuits, or AFC as we would call it today, but these were for use on the medium wave band. W. A. Flint dealt with the construction of his Diversity Receiver. Being dissatisfied with the Home Service on both 391 and 449 metres and the "blasting and distortion" introduced by the AVC he had two separate straight receivers with the detectors feeding into a common audio stage.

No. 500 was in a smaller format, 8^{3}_{4} x 6in., and dated March 1948 having become a monthly publication at a price of 9d. F. J. Camm was still in the chair and in his Editorial pointed out that while other commodities and services had increased in price by 100 per cent the licence fee was the last to be increased, from 10s to a £1 plus £1 for the TV licence. In view of rumours of further rises in the fee FJC wondered "if the time was ripe for the BBC to drop its outmoded belief that publicity is an unclean thing and to remove its ban on commercial broadcasting in this country". Readers will not be slow to note that the BBC policy remains the same in 1973 but commercials will take the air in the autumn on VHF and MW and so cream off the profits which could so well go towards reducing the already astronomic TV licence fee collected for the BBC.

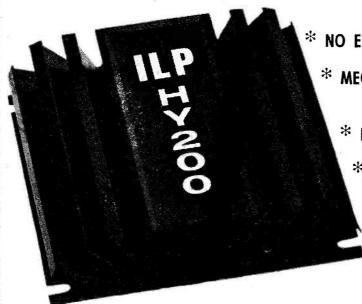
C. L. Orsborne wrote on modifying the wartime Utility Receiver for reception of the Light programme on the long waves since some parts of the country experienced difficulty with the 261 metre signals after dark. Edwin N. Bradley described a test pattern generator for the TV service engineer. This produced a vertical bar pattern using a single valve, double triode 6SN7. Another article dealt with the design of test instruments with particular reference to multivibrators and sub-standard oscillators.

On special application to the GPO radio amateurs could obtain permission to use the six metre band for a limited period. The band was very active at the time but only certain countries, mainly in the Americas, included it in the standard amateur licence

Readers were reminded that if a car had been laid up because of the petrol rationing they could



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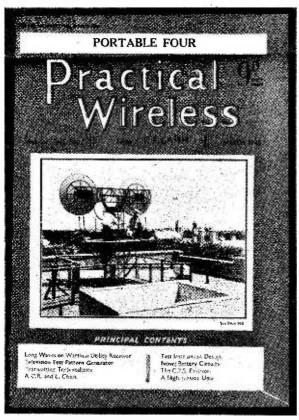
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obtain a refund of 1/8d. a month on the unexpired portion of a car radio licence. Full details were given of the construction of a four valve battery portable using a novel frame aerial which lay flat on the back of the cabinet.

No. 600 came at the festive season of December 1956 but the cover price had increased to 1/3d. The cover featured a front door intercomm system using relays for the switching circuits.



Smaller sized No. 500 in March 1948 had a very poor quality cover that even had a flagrant spelling error! Can you spot it?

Editor FJC wrote . . . "with nearly half a million VHF sets sold since the opening of Wrotham in May 1955 there is no doubt that this is the answer to interference-free reception of very high quality and in the course of a few years the system must inevitably oust the older one . . ." Seventeen years on and there is more MW broadcast activity in this country than possibly ever before!

The first of the Film Shows organised by PW was held at Caxton Hall in the following February and this issue gave full details of the films that were to be shown. These included methods of manufacturing CRT's, valves and transistors. These shows continued until quite recent times.

F. R. W. Strafford resigned from the position of Technical Manager of Belling and Lee Ltd. His claim to fame was as originator of G9AED the first UK Band III pilot television transmitter. Gordon King concluded his series on Servicing Radio Receivers but promised more including "AM/FM models and receivers using transistors".

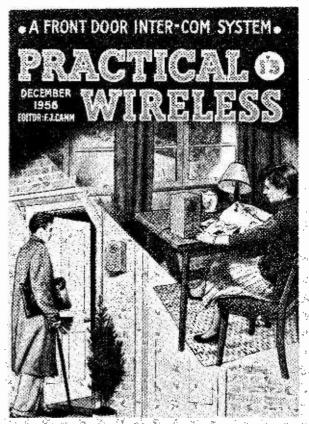
Practical projects included a Versatile Valve

Voltmeter, a Beginner's Shortwave Three for mains operation and an Electronic Metronome, using a transistor of all things! Incidentally an OC71 then cost 24/- compared to 2/6d today. "Matched Crystals" was very misleading since the reference was to germanium diodes as used in FM discriminator circuits.

No. 700 of June 1965 was still in the old, smaller format and "Free Inside" was a double-sided blue-print on how to build the electronic Hawaiian guitar featured on the cover. The blueprint service was still going strong costing from 1/6 to 8/- each including postage and whatever went for VAT in 1965. The service was always very popular and we often wonder if it could ever be resurrected, but like the Back Numbers department, we fear that it has gone forever!

Letters to the Editor numbered no less than nine in strong contrast to the meagre offerings of today. Personally, we'd like to see ninety-nine an issue!

The world's first commercial communications satellite was in stationary orbit and Goonhilly tracking station was busy modifying its equipment to handle the increased volume of traffic expected from "Early Bird". On a slightly smaller scale C. J. McClelland, G6AG, of Chalfont St. Peter in Bucks,



Looking at No. 600 with its colour printing, it would seem that the importance of bookstall appeal was beginning to be appreciated.

had reports from the USA on his 2 metre signals received there via amateur radio's very.own satellite Oscar 3. He also made two way contact with amateurs in Germany, Switzerland and Sweden through the satellite.

—continued on page 530

practically wireless HENRY commentary by

No. 101 Doing it

yourself

NXIOUS to cure his noise without adding to—I quote—'my heap of damaged output transistors', a reader of a very popular audio magazine has written to the Editor, asking for advice. He read 'with interest' an article published a couple of months before, describing an editorial venture into d.i.y.

The relevant point for PW readers is that the kit he had blundered upon was first described in these pages, and has since earned worldwide acclaim as an inexpensive and honest attempt at quality without pretensions.

Henry wished that he had the 'full might' of his employer to enable him to indulge in some of the design problems that beset an ordinary workshop. Such as, making a new comparator, switchboxes and pre-amplifiers that can couple anything to anything else. universal filters which enable specification tests to be made without recourse to the equipment supplier's factory, an intermittent fault testing device that will ring a bell or activate a buzzer when the signal deviates from the normal . . . and so on. In our line of business, such service aids as one acquires are usually made up in the lonely winter evenings.



Intense antagonism between supporters.

Doing it yourself is great fun. especially when you have to surmount the initial difficulty of finding a suitable design. Better still, when you are capable of geting under the writer's skin and determining whether a design is indeed suitable—let alone 'good'—or will be followed in successive months by corrigenda.

Even the mighty lapse sometimes, and current argument in the audio glossies barely covers with politeness an intense antagonism between the supporters of shunt and series feedback.

Worse than this, far too many major makers of wireless and other electronic equipment bring out designs that are advertised as world-shaking, only to follow them, perhaps a year later, with carefully tabulated modifications. These are printed and listed, punched and perforated to be the more easily inserted into the original, elaborate service manual.

With hand on heart, the maker will state (through the mouthpiece of his Press Relations Officer), that he 'reserves the right to make improvements to the original design.' This simply means that he will take note of the feedback of complaints and questions from his dealers and rap his designer over knuckles, producing one or two hasty amendments which will then be published with the usual hoo-ha of trumpets as 'modifications'.

The trouble with modifications in do-it-yourselfery is that so many are made by the constructor, from expediency.

If only, in their avid desire to do it themselves, the electronic builders of this world would either take basic principles and evolve from there, or trust those whose experience and expertise has paved the way for them, the tangled travesties of published ideas would not land on the doorsteps of Henry and his ilk, to be, most uneconomically, unravelled.

In other words, brothers, if you must do it yourselves, please gen up on the underlying principles, or leave the job alone. If you simply want to build—and impress your more gullible neighbours, then buy some reputable kit, follow each instruction to the letter, and please do not try to circumvent the designers' intentions. That way, you may save yourself, at least, a heap of damaged output transistors.

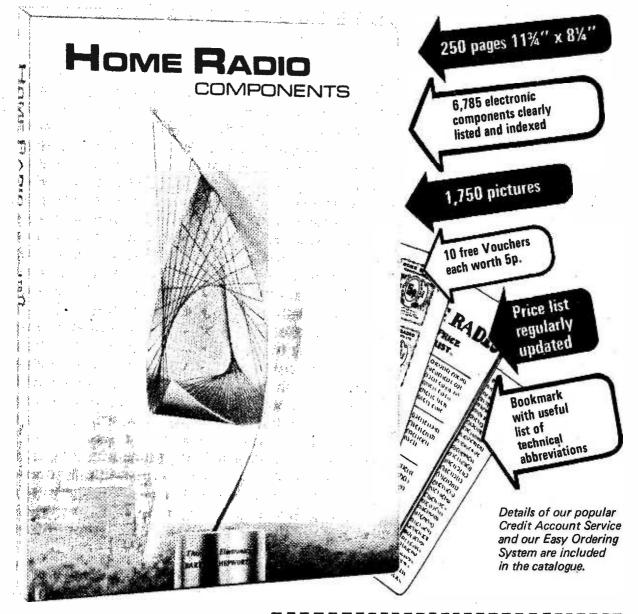
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P AX—man of peace, or man of many pieces. Has survived the handling of editors for 55 vears, and hopes to be around for at least another couple of weeks. Draws part-time, to earn enough to keep alive, though it looks doubtful if he has succeeded. Has illustrated a couple of books (editors do have incautious moments) and done many bits and pieces with pens and things. Born in Aberdeen, Scotland, probably the only town with no Jewish residents—they couldn't hope to make a living up there. Unmarried, to the best of his knowledge. Has lived many long years in London, almost a Scotch Cockney by now. Likes drawing cars, animals and Pax characters. Gets mixed up with music when he isn't drawing, with disturbing results.



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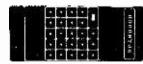
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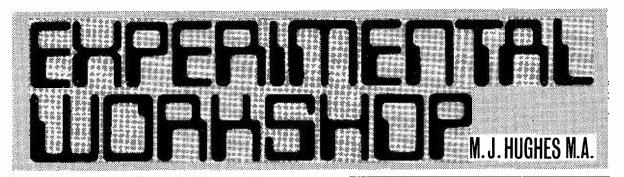
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THIS new series is designed to give the lesser experienced reader an interesting set of potential projects that can be taken to several stages of complexity. It will follow along the lines of instructional articles but will be of a practical nature. Each month a series of experiments (which may be simple projects in themselves) will lead logically from one step to another and by combining the reading of the text and participating in the experiments the relative newcomer to electronics will not only get some very useful practical knowledge of various types of circuitry but could—if he wants to—make a number of useful novelties en route.

Economy will be very much in mind and we recommend that readers build the experimental circuits on T-Dec; as far as possible we shall

arrange the circuits to re-use components over and over again although there is no reason why any circuits that catch the eye should not be "permanised" on Veroboard or some other assembly.

To be involved in the experiments all you will need is T-Dec, a 9V battery (two 4.5V bell batteries in series are ideal) and an assortment of components that can be bought as you go along. A multi-range meter will be useful but separate voltmeters and milliammeters will do. Voltage measurements should only be made with $20,000\Omega|$ volt instruments or better. You should not cut the leads of the transistors if you want to re-use them; in fact it is advisable to lengthen the leads with about 1in. of 20 or 22 s.w.g. tinned copper wire to permit easy insertion in the T-Dec.

PART 1—ELECTRONIC SWITCH

THE heart of modern electronics is the transistor, so let us start with this and see what we can do with some surprisingly simple circuits. This month we shall look at the transistor as an electric switch.

A transistor is made to conduct between collector and emitter by passing a current into its base. To make base current flow you have to have a voltage at the base that is greater than the voltage at the emitter with respect to the common line or "earth". In the case of the more common npn silicon transistors, this voltage has to be at least 600mV more positive than the emitter. The amount of base current is controlled by a resistor in series between the base and the main voltage rail of the circuit in question. There are two factors which control the amount of current that flows between collector and emitter, these are (a) the value of resistor in the collector/emitter circuit and (b) the amount of base current that is permitted to flow. The maximum collector current one can control for a given base current can be calculated by multiplying the base current by hFE or beta of the transistor in question. For a BC108 \hat{h}_{FE} is between 100 and 250—depending on how lucky or unlucky you were in your purchase. You can see the effect of a transistor's current gain from the experimental circuit of Fig. 1. Measure the voltage between the collector and ground with $R1 = 2 \cdot 2k\Omega$ and $R2 = 220k\Omega$. Before point A is connected to the positive rail the potential at B should be virtually +9V. When 9V is applied to A we have arranged values so that sufficient base current flows to provide a collector current that will make the voltage at B fall to almost zero. We say that the transistor is in full conduction or in saturation. Change the value of R2 to 2.2M\Omega and see what happens then. The base current is much less (down by a factor of ten) hence the maximum collector current will also come down by a factor of ten. This will be insufficient to give a 9V drop across R1 and the voltage you read will be by no means as low as zero. The actual value will be dependant on the hFE of your transistor. If you now increase the value of R1 by a factor of ten to 22kΩ you will revert to a reading of zero because the smaller collector current is again able to give a 9V drop across the higher value resistor. Try reducing R1 to 220Ω and see by trial what is the highest value of resistor you need for R2 to get back to the reading of zero at Tr1's collector.

The circuit that gives you a full 9V swing at the collector when 0V or 9V is applied at point A is sometimes called an inverter because when the voltage level is high at the input it is low on the collector output and vice versa. It is much used in logic systems. You can directly couple one inverter

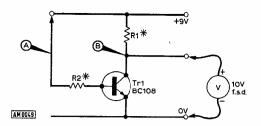


Fig. 1: *See text for experimental values. Experiment to show how collector current and voltage at B is controlled by the values R1 and R2 respectively.

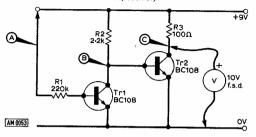


Fig. 1a: Double inversion. When point A is connected to r9V Tr1 goes into conduction and effectively shorts point B to ground so no base current flows into Tr2. Hence point C goes to +9V. Connect point A to ground (or leave it disconnected) and point C goes to OV.

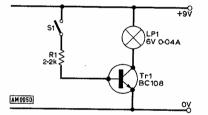


Fig. 2: Basic practical lamp driver circuit. Close the switch and the lamp lights

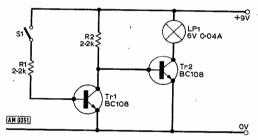


Fig. 3. Lamp driver preceded by an inverter. Close the switch and the

to another—Fig. 1a—so that the sense (or level) of the output signal is the same as the input. Not at first a very likely thing to want to do but it does have a "not so obvious" application. The 9V of the first stage input is being fed through a $220k\Omega$ source resistor (very small current is being drawn) whereas the output at the collector of Tr2 is coming through a collector load resistor of 100Ω . We have thus got the same voltage signal out as we put in but there is considerably more current being switched and this could be useful in itself or for driving other circuits.

The inverter if often used to drive low voltage lamps-which need a reasonable amount of current to make then glow. Because the maximum collector current rating for a BC108 is 100mA we can only control bulbs up to this capacity. For experimental purposes a 6V 0.04A bulb is ideal. You can liken this bulb to a 100Ω resistor for the purposes of calculating base current required to make it go on when it is in a collector circuit. Either by experimental methods or calculation you should find that 9V applied through a $2 \cdot 2k\Omega$ resistor as base current is ample to make LP1 (Fig. 2) turn on. If S1 was a push button, when you pressed it the lamp would go on. It might be you wanted the lamp to go off when you pressed the button. To do this it is only necessary to insert another inverter stage into the circuit-Fig. 3. Notice that the collector load of Tr1 has the same ohmic value that will supply the necessary base current for Tr2-when Trl is not conducting.

You can use two inverter circuits connected together to make a simple form of "snap" detector—these are frequently used in television quiz games to decide who was first to press their button. We have to modify the circuitry a bit so that when one button is pressed it makes it impossible for the opposition's light to go on when they press their

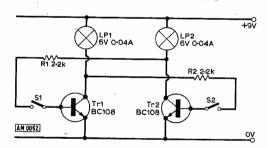


Fig. 4: Basic workable quiz "snap" detector.

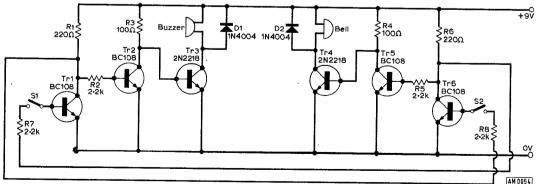


Fig. 5: Snap Indicator with direct drive to the bell and buzzer. Coil resistance of each should not be less than 12%. R2 and R5 are included so that the collector potentials of Tr1 and Tr6 are not held down by Tr2 and Tr5 drawing their respective base currents. For lower resistance coils use 2N3055's for Tr3 and Tr4.

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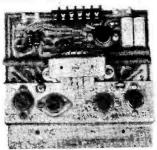
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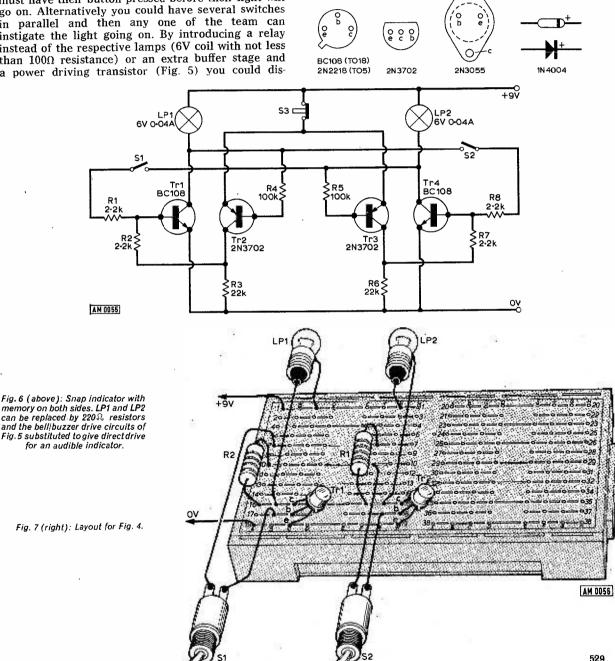
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Age.....CV BPW20 BRITISH INSTITUTE OF ENGINEERING TECHNOLOGY button; of course the converse must hold true—depending on who presses first. See Fig. 4.

Tr1 draws its base current from the collector of Tr2 via the push switch. Initially neither transistor will be conducting therefore the collectors of both will be at +9V and the lamps will be off. Say that S1 is pressed first; base current can flow through LP2 via the switch and R1 into Tr1's base. LP1 will light up and the potential at Trl's collector falls to nearly zero. If S2 is now pressed there is not sufficient potential at Trl's collector to drive base current into Tr2 hence as long as S1 is pressed LP2 cannot be lit. As an indicator for a game you can make it more interesting if, say there are two teams competing, you have two-or more-switches in series on each side. Every member of the team must have their button pressed before their light will go on. Alternatively you could have several switches in parallel and then any one of the team can instigate the light going on. By introducing a relay instead of the respective lamps (6V coil with not less than 100Ω resistance) or an extra buffer stage and a power driving transistor (Fig. 5) you could dispense with the lights and have a buzzer and bell (low voltage types with coil resistances of *more* than 12Ω) on opposing sides. It is necessary, in the latter case to include a diode across the buzzer bell to prevent any high voltages (caused by the sudden breaking of the inductive circuit) damaging the output transistor.

The snag with these circuits is that they lack memory. If the player was to take his finger off the button his light goes off and he leaves things open for the other side. If the judge was not quick enough there might be a few cries of "cheat". This can be overcome by building in a little more complexity—

AM 0059



Underside views

without introducing any new major concepts. We need another transistor on each side of the basic indicator—as shown in Fig. 6. Note that these are pnp types. We have established that when S1 is pressed the potential at Trl's collector falls zero: this zero voltage is, in fact, a high base drive for the pnp transistor Tr2 so the latter switches on and its collector rises to about +9V. This level is applied back to the base of Trl through R2 so that, when the finger is taken from the button, base current is maintained and LP1 stays on-inhibiting the other side. Exactly the same reasoning would apply to the other side of the circuit if S2 was operated first. To cancel the indication for the start of the next game the emitters of Tr2 and Tr3 have to be momentarily disconnected from the positive rail by depressing

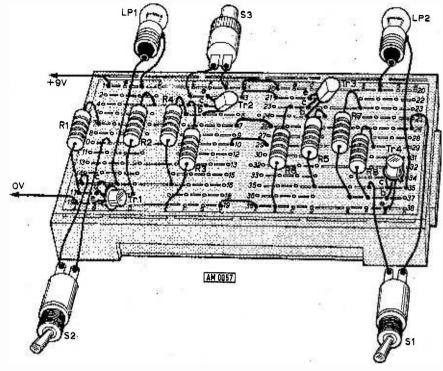


Fig. 8: Layout for Fig. 6.

the normally closed switch S3—this would (presumably) be under the control of the judge.

All these circuits will work and you can build any of the versions—obviously some have more refinements than others and of course that will cost a bit more. We leave it to you to go as far as you like!

Next month we shall look at more aspects of the transistor as a switch including the emitter follower (not a switch in itself) and some trigger circuits.

GOING BACK—continued from page 521

A two transistor radio, which today would be built on a small piece of veroboard, was assembled on a board $6\times5\times1_2$ in. so it seems that even transistors had to go through the breadboard stage! The PCR ex-government communications receiver was revamped by W. V. Woods by adding a mains operated power supply and rearranging the circuitry around more modern valves.

Increasing solar activity in 1965 led to informationpacked reviews of the short wave broadcast bands by John Guttridge and of the amateur bands by "ol faithful" Dave Gibson, G3JDG. And, guess what? Here's Henry with his Practically Wireless No. 10 lashing out at the gimmicks at the International Audio Fair held at the Russell Hotel. He even mentions a Quad decoder! Did he mean quad or Quad??

Brian Robinson was churning out Part 8 of his series on preparing for the Radio Amateurs Examination. Since the exam is still going strong a repeat of the series or something like it might not come amiss. A whole page of Club News in 1965 has sadly dwindled out of existence although we are sure that the Clubs are just as numerous and active today as they were then.

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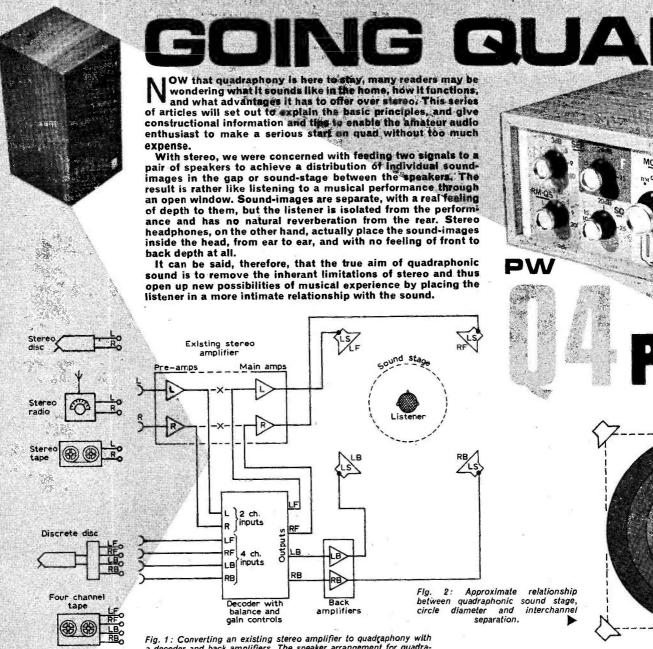
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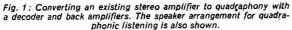
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ERHAPS the most striking demonstration of the effectiveness of quadraphonic equipment in a home setting is when a familiar and well recorded stereo disc or tape is played through four speakers in the 'surround-sound' mode. The enhanced detail and realism is astonishing, to say the least. Actual quadraphonic recordings offer the promise of even better results, but with the limited amount of quadraphonic material to choose from at the moment, most of which is ineptly recorded 'muzak', it is difficult to arrive at a valid comparison.

It has been said that listeners prefer to hear their quadraphonic music at about half the normal stereo output level, but this could be attributed to a desire to remain apart from the performance, or to equipment defects. An experiment conducted by the

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writer on a flumber of they slowly adjust to fou The initial response is to as 'frightening' or 'uncann' best describe quadraphonic If you prefer music as an u conversation then you mis stereo.

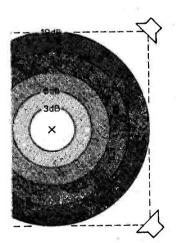
One snag with quadrapl realism emphasises defect on the part of the musicians distortion, dust and scratc rumble, etc., but this is greater fidelity. With son systems it is difficult for

DRAPHONIC

1 QS recordings **2** SQ recordings **2** Dicemete CD-A

Discrete CD-4 recordings
SURROUND SOUND





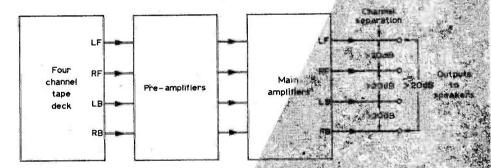


Fig. 3a: Discrete tape aparent

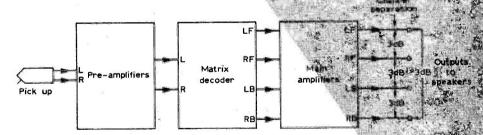


Fig. 3b. Matrix disc system.

BOLLEN

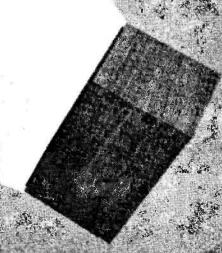
riends suggests that as r speaker listening they ad higher output devels describe the experience but the word that may listening is 'involvement nontrusive background to the just as well stick to

ony is that the greater so such as lack of skill and recording engineers, her on discs, tape hist, siways the penalty of the quadraphonic more than one listener.

in a small room to hear the performance in perfect balance.

How does it work?

The new standard arrangement for quadraphonic listening is to have feelt speakers placed in a square array—preferably in the corners of the room—and facing inwards along diagonals, with the listener seated at the centre of the square, set Fig. 1. Abbreviations LF RF, LB and RB, define left and right, front and back channels. The curtain sound stage, shown adotted in Fig. 1. Is a subjective



boundary which is felt as a 'hole' in the sound, or as a clear area of floorspace where few sound-images occur. There is, however, no limit to the apparent location of sound-images outside the circle. Many of them seem to be a long way off, beyond the walls of the listening room.

The old idea of coupling four speakers to a stereo amplifier is just not on these days. Each of the quadraphonic speakers needs to be fed with an adequate signal of low distortion. An economical and versatile way of going quadraphonic, with the least equipment redundancy, is to add a pair of back amplifiers and speakers, and a decoder, to an existing stereo set-up, as shown by the block diagram of Fig. 1 Stereo disc and tape decks, with their associated pre-amplifiers and tone controls, can then be employed for playing surround-sound stereo, and two-channel quadraphonic discs and tapes without modification, using the decoder circuit to split the two channels into four. Four-channel tape sources can also be played direct through the decoder gain and balance controls to the four main amplifiers, and it would be a simple matter to add on a CD4 disc demodulator and decoder in the same way. Thus, several quadraphonic systems can be catered for at the same time, with the vital controls

Discrete versus Matrix

centralised in the decoder unit.

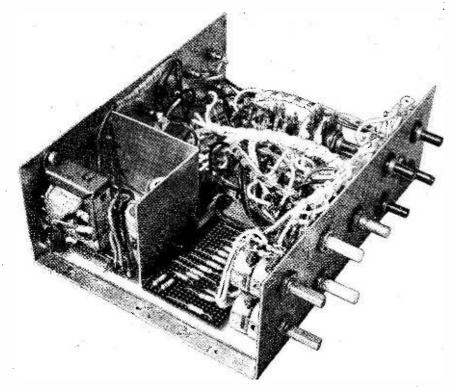
A discrete four-channel recording medium, such as multi-track tape, offers the best in quadraphonic sound. Each channel is free from crosstalk with other channels and signals are relayed direct to the main amplifiers after suitable pre-amplification, see Fig. 3a. Another less satisfactory approach is to encode four signals on a two-channel disc or tape

Q4 MATRIX DECODER SPECIFICATION

Two-channel input impedance 43-47kΩ Four-channel input impedance 100kS2 Output impedance Maximum gain 100a¥ Equivalent input noise 2V r.m.s. Maximum Input signal 2V r.m.s. Maximum output signal Distortion at 1kHz 500mV 0-1% or less Phase shift error 90" 10% 100Hz-10kHz Maximum channel separation 30Hz 60d8 50dB 20kHz 25dB 30Hz-30kHz =1dB Frequency response

and then decode the resulting pair of signals with a mixing circuit or matrix to reconstruct the original four signals, Fig. 3b. Notice that separation between channels in the discrete case will be 20dB or more, while the matrix may offer as little as 3dB separation.

Poor separation with two-speaker stereo reduces the distance between sound images, and at zero separation the images would be piled on top of each other as a mono sound centrally placed between the speakers. The situation is slightly different with quadraphony because poor separation reduces the apparent size of the sound-stage circle without affecting the distribution of sound-images. All that happens is that balance adjustments become more critical and movement of the listener in relation to the speakers is more restricted.



Internal view of the P.W. Project Q4 matrix decoder.

Fig. 2 shows the approximate sound-stage diameter for several values of separation. Assuming the speakers are ten feet apart then a 3dB sound-stage will be 2ft. in diameter, and a 9dB stage 6ft. If a critical listener moves his head one quarter of the sound-stage diameter in any direction this will throw a musical performance out of balance, so in the above case the listener would be confined to an area 1ft. in diameter with 3dB matrix separation, and 5ft. in diameter when separation is virtually discrete and exceeds 19dB.

Matrix techniques also introduce undesirable phase shifts in the speakers, which will tend to blur and shift those sound images having a smooth, rounded tone. Images of sharp sounds are much less affected, due to the inability of the ear to detect phase shifting above about 8kHz, this is probably why matrixed quadraphonic recordings tend to favour the use of plenty of percussion instruments. When a matrixed recording is correctly decoded, image width and channel separation are optimised. Incorrect decoding not only alters the intended location of sound images and tonal balance, but it can also boost the sound level of some instruments and reduce others, with peculiar results in some instances.

To achieve widespread acceptance a quadraphonic system must be able to offer convenience of use, low cost per playing time, low noise, low distortion, a wide frequency response, and plenty of programme material, and these requirements are most easily met at the moment by vinyl discs. It is significant that the technically excellent, but inconvenient, four-channel open-reel tape recorder has been around for some time now and that little effort has been made to supply users of these machines with pre-recorded quadraphonic tapes. The quadraphonic snowball only started rolling when the matrix appeared, because this allowed highly developed stereo disc techniques to be readily adapted to quad.

The present position is, therefore, that matrix users can now quite literally surround themselves with surprisingly good sounds from disc, tape, and radio, and play those favourite old recordings to maximum advantage, despite the shortcomings of the system, while advocates of discrete systems must wait, and content themselves with a very limited range of good programme material.

Which system?

At the moment in the UK a serious choice exists between the following systems: discrete Q8 tape cartridge, discrete Victor-RCA CD4 disc, Sansui-Pye QS matrix disc, CBS-EMI SQ matrix disc, with RM or 'regular matrix' being employed as a 'back-up' system for stereo surround-sound playback. There are other systems in other countries, and new systems under development, but these are not likely to become established for some time. The Philips quadraphonic cassette is still under development, and may go discrete or matrix. A choice of system made by the BBC for FM radio will depend on the outcome of long-term listening tests, and many areas still await the coming of FM stereo.

The currently available quadraphonic systems will now be discussed in greater detail.

O8 TAPE

Discrete four-channel Q8 tapes and playback equipment are at present marketed mainly for the motorist, and are not stereo compatible. The recorded tracks on quadraphonic Q8 do not match up with the tracks on a stereo Q8, but this problem can be solved by tape head swiching. Provided that hiss and tape wear can be kept within reasonable bounds, and the manufacturers of pre-recorded tapes make some effort to extend frequency response, then this system could enjoy widespread popularity in the home as well as in the car. There is a rapidly increasing amount of quadraphonic programme material available for Q8.

VICTOR-RCA CD4

A conversion kit is available for this discrete disc system at a cost of around £90. The kit includes a special stylus and cartridge, low capacitance pick-up cables, and a pre-amplifier combined with decoder. CD4 is capable of providing a really good quadraphonic performance but uses complex circuitry which is prone to noise and distortion when incorrectly aligned. With less than fifteen discs available (at the time of writing), CD4 is still very expensive in terms of pleasure for money. Additional equipment would be needed to play surround-sound stereo or quadraphonic matrix discs.

RM (REGULAR MATRIX)

The main use for this system is to enhance ordinary stereo programme material with four speakers by 'bending' the stereo sound-stage around the listener giving the "surround-sound" effect. This is not true quadraphonic sound in its strictest sense, but a very acceptable compromise, giving subjectively better results than 'one-wall' stereo. The presence of 180° phase shifts in the speakers causes serious blurring of some sound images. With RM, the sound-stage can only occupy a 270° sector, leaving a 90° hole behind the listener. Basic channel separation is 3dB, but this can be modified by the use of a variable separation matrix. QS and SQ recordings played through RM will suffer slight to moderate image mislocation.

SANSUI-PYE QS

This Japanese sysem uses the same matrix values as RM but employs 90° phase shifts to give more distinct images and a 360° sound-stage. Results can be good, with an even distribution of images around the listener. Basic channel separation is 3dB, but this can be altered in the same way as RM and Sansui have now introduced an automatic separation enhancement circuit called Variomatrix. QS recordings are available under the Pye label and from import record stores. There is slight to moderate image mislocation from a stereo record played through QS, and serious image mislocation from an SQ record.

CBS-EMI SQ

90° phase shifts are also used in this American system, but matrix values are quite different to RM and QS. Excellent left to right separation is achieved at the expense of centre front to back separation, which means that a centre front or back soundimage will tend to be located close to the listener's head. A better image distribution can be achieved by deliberately introducing a measure of crosstalk between left and right channels, called blending, or

by the use of additional gain-riding 'logic' circuits. A stereo or QS record played through SQ will exhibit serious displacement of images, generally towards the back and to one side. The SQ system currently offers the largest number of quadraphonic recording in the UK, under CBS and EMI labels, and from import stores.

If the reader is wondering why an SQ record sounds reasonably good through an RM matrix, and a stereo record sounds bad through an SQ matrix, this seeming contradiction can be explained by so called 'psychoacoustic' factors. The ear does not behave in a predictable way when confronted by phase shifts and sounds issuing from point-source loudspeakers.

One must accept that SQ records played through an RM (or surround sound) system is only the poor man's substitute for real quadraphonic sound. It does not clearly define the position of the performers or the listener.

Back amplifiers and loudspeakers

All main amplifiers and the four speakers should be as closely matched as possible in terms of power output and frequency response. The task of installing a pair of back amplifiers is now made easy by readily available modules with matching power supplies. It is only necessary to house these modules in a suitable box and wire them up according to the manufacturer's instructions to achieve results not far removed from the best in hi-fi at power levels ranging from a few watts to more than a hundred watts r.m.s. per channel.

One very important point to check when setting up the back amplifiers and speakers is that these are in-phase with the front channels. This can be tested by feeding a low level signal of around 1kHz into a front and back amplifier via separate gain controls, see Fig. 4a, and adjusting those controls for identical output levels as measured with an a.c. voltmeter between amplifier outputs and earth. Do not use a high level test signal as this could damage the amplifiers or loudspeakers. If the voltmeter is now linked between the two amplifier outputs, Fig. 4b, a small or zero reading will indicate that phasing is correct, and a large reading that the amplifiers are incorrectly phased and that the polarity of the rear speakers should be reversed.

If speaker polarity is not indicated—usually by a red dot beside one speaker terminal—it can be found by applying a 1.5V battery to the terminals and noting the resulting cone movement. In most cases, when battery positive is applied to speaker positive there will be an outward movement of the cone, but check that this is so with the other speakers.

Room shape and furnishings may dictate a departure from the ideal square speaker array, in which case aim for a rectangular configuration with speakers equidistant from the listening position. The speakers should preferably radiate at head height.

Looking next at the stereo amplifier used for the front channels; if this is a modern unit it will almost certainly have pre-amplifier left and right outputs brought out to the rear panel, and bridged to the main amplifier inputs with a switch or plug. If not, then the unit will have to be modified to provide

this facility, and it would be a good idea to contact the manufacturers to see if they can supply a circuit diagram of the amplifier with suitable take-off points shown.

The PW Project Q4 that follows examines matrix circuits more closely, and describes a decoder circuit which offers switch selection of RM and QS, both with variable separation and SQ with variable blend. There is also provision for inputs from discrete sources, such as a Q8 tape-deck or a CD4 decoder. Switched modules are used in the decoder to allow for individual modifications or the construction of a simplified version which caters for one system only.

The decoder design to be described in this series uses readily available components and will cater for several quadraphonic systems without adversely affecting the intended location of sound images or tonal balance. Correct decoding is achieved by switch selection of matrix parameters and infinitely variable adjustment of front and back crosstalk.

In addition to handling all available quad matrixed recordings, including Pye-Sansui QS and CBS-EMI SQ, the decoder will also operate in regular matrix (RM) surround-sound stereo with variable 'wraparound' and ambience—conventional two speaker stereo, two or four speaker mono, and will serve as a common control centre for discrete signals from a tape player or CD-4 decoder. If desired, the decoder can be built in a simplified form to cater for one system only.

The matrix

A matrix circuit is a special kind of mixer with four outputs which responds to the amplitude and phase of a pair of input signals. When fed with appropriate left and right input signals, a symmetrical matrix circuit will phase cancel an output signal to one loudspeaker when the sound image associated with that signal is located diagonally opposite that speaker.

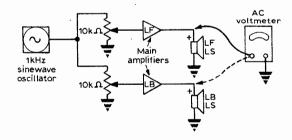
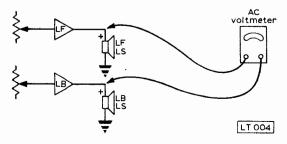


Fig. 4a: Checking amplifier phase, Step 1. Adjust input potentiometers for equal low-level outputs from LF and LB main amplifiers.

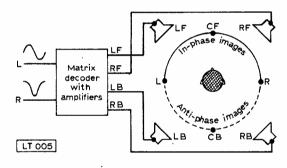
Fig. 4b: Checking amplifier phase, Step 2. If voltmeter reading is higher than Step 1, reverse connections to LB and RB speakers.



The experienced stereo listener may have noticed that in-phase left and right signals create sound images in the gap between the two loudspeakers, while anti-phase signals cause sound images to extend outside the speakers. Anti-phase is sometimes used deliberately in stereo recordings to produce artificial effects, and it also occurs naturally in the form of ambience or reverberation, but in matrixed quadraphonic recordings phase should be carefully controlled.

When a two-channel recording is played through a matrix to four loudspeakers, the in-phase images will be distributed around a semi-circle to the front of the listener; this is equivalent to a 'wrap-around' stereo sound stage with a left only signal producing an image to the left of the listener and a right only signal to the right. Anti-phase images will then be located around a semi-circle to the rear of the listener. So, if there is any anti-phase content on a conventional stereo recording, this will be routed to the back speakers when played through a matrix.

Fig. 5 shows the circular quad sound stage made up of in-phase and anti-phase images, and also lists the properties of input signals for four selected image locations.



Input signals of the same amplitude and frequency	Sound-image location
L and R in-phase	CF
R only	R
L and R anti-phase	СВ
L only	L

Fig. 5: How phase affects matrix image location.

The subject of separation between matrix channels is full of apparent contradictions. For example, a QS disc displays a separation of 7.7dB when played in two speaker stereo, and a simple QS decoder circuit also offers a left to right separation, of 7.7dB, but when the QS recording is played through the QS decoder the resulting separation is 3dB. Furthermore, although QS separation is 3dB between adjacent channels, it is not, as one might suppose, 6dB between alternate channels, that is, across the diagonals of the listening area. Instead, diagonal separation is infinite!

With the basic SQ matrix, on the other hand, left to right separation is infinite, but front to back and diagonal separation is only 3dB. All rather confusing, but explainable in terms of code and decode formulas.

Various tricks can be employed to increase separation with a matrix, such as the Sansui automatic matrix adjuster or 'Variomatrix' and the SQ gain-riding 'logic' circuit, but these will only operate effectively with simple sound sources and would be confounded by a full orchestra. Fortunately for the listener, the net effect of poor separation with a matrix is merely to make balance adjustments and the listening position more critical, without otherwise influencing the location of sound images and tonal balance, but if programme material coded for one matrix system is decoded by the equipment of another matrix system results will nearly always be disappointing.

Matrix decoders

If matrix decoders are compared, and are broken down into basic circuit elements, they can be seen to consist of similar phase splitters, phase shifters, and mixers. The phase splitting and shifting circuits take the left and right input signals and process them to give a group of phase related outputs which are then added and subtracted by the mixers in proportions depending on the system code being handled. It is possible to cater for all available

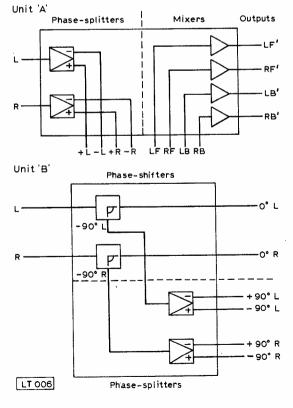


Fig. 6: The arrangement of units A and B.

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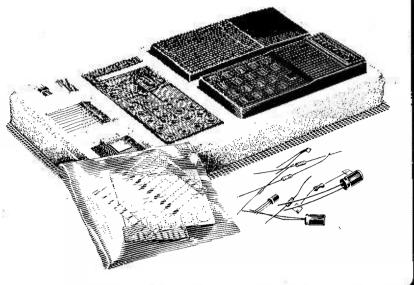
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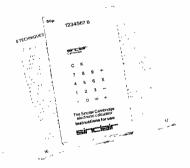
- 1. Coil.
- 2. Large-scale integrated circuit.
- 3. Interface chip.
- 4. Thick-film resistor pack.
- Case mouldings, with buttons, window and light-up display in position.
- 6. Printed circuit board.
- 7, Keyboard panel.
- Electronic components pack (diodes, resistors, capacitors, transistor)
- Battery clips and on/off switch.
- 10. Soft wallet.



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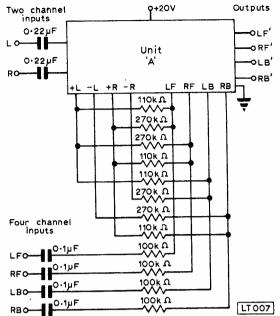


Fig. 7: Unit A as an RM surround-sound decoder with additional discrete inputs.

matrix systems with four phase splitters, two phase shifters, and four mixers.

In the PW Q4 decoder, these circuits are grouped into two units, see Fig. 6. Unit A contains a pair of phase splitters and the four mixers, with the splitters providing non-inverted and inverted (180° phase difference) outputs denoted by a plus and a minus sign respectively.

Unit A can be employed on its own for surroundsound stereo decode by connecting the splitter outputs via a suitable resistance network to the mixer inputs, and additional mixer input resistors would serve for discrete inputs also.

Unit B in Fig. 6 is designed to be coupled to unit A, and contains two phase shifters and two phase splitters. The shifters impart a lagging phase shift

of approximately 90° to the left and right input signals (leading is signified by a plus sign and lagging by a minus) which is then fed to the splitters to give leading and lagging outputs in relation to the 0° left and right outputs. For practical purposes the phase relationship between shifter and splitter outputs and the original left and right inputs may now be ignored as the 0° outputs serve as reference signals. Another way of looking at this is to assume that the 0° output has been shifted $+45^\circ$ in relation to the input signal and a -90° output has been shifted -45° in relation to the input.

When unit B is combined with unit A, and interconnected by a suitable resistance network, they will offer a basic QS or SQ decode.

With only two circuit modules, it is therefore possible to individually decode one of three systems

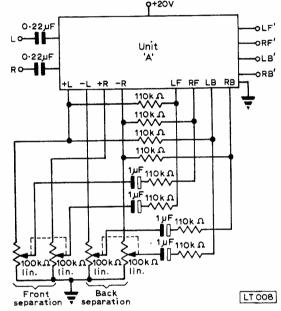
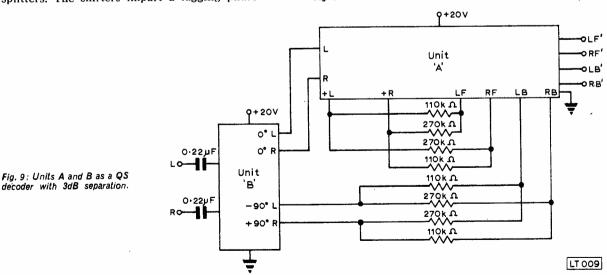


Fig. 8: Unit A as a surround-sound decoder with variable separation.



540

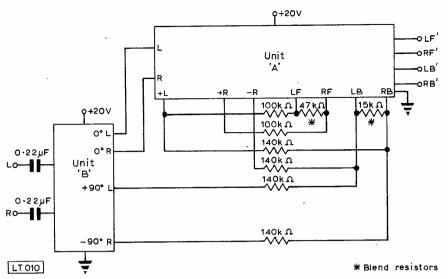


Fig. 10: Units A and B as an SQ decoder with 20dB front separation and 8dB back separation.

with a minimum of additional components, or to cover a wide range of codes and programme material by the use of a switched and variable resistance network. Suppose a user requires a surround-sound RM decode for his stereo tapes, plus discrete inputs for his four-channel tapes, he could employ the circuit of Fig. 7. An alternative RM decoder, which is suitable for surround-sound experimentation, with variable left to right separation set by dual-gang pots. is shown in Fig. 8. Yet another user might only be interested in a straightforward QS decoder, and he could combine units A and B with the resistance network values shown in Fig. 9. The circuit of Fig. 10 would give an SQ decode, with 10% (20db) front and 40% (8db) back blends to ensure a strong centre front image.

The circuits of Figs 7-10 all have a throughput gain of two and will function as shown, without additional components other than gain and balance controls and a power supply.

For those who wish to experiment with resistance

network values, they can be arrived at by dividing the code figure into $100k\Omega$. Thus, for the Scheiber code the values are $100k/0.92=108.7k\Omega$ rounded off to $110k\Omega$, and $100k\Omega/0.38=263.1$ rounded off to $270k\Omega$. In the circuit of Fig. 8 the potentiometers cover code values of 0-0.92, and are loaded by the $110k\Omega$ resistors so that 0.38 occurs close to centre track.

The SQ decoder of Fig. 10 can also be modified for blend on the basis of blend resistor Rb=480/% blend, so if a blend value of 15% is required this will be $480/15=32k\Omega$ rounded off to $33k\Omega$. Since SQ blend resistors tend to reduce the outputs from a pair of blended channels the above formula become increasingly inaccurate above about 30% blend, hence the value of $15k\Omega$ in Fig. 10.

The loudspeakers shown on this month's cover are the AUDIOTRONIC CRITERION.

Next month, full circuit details will be given.

RAE Courses

We give below some of the centres which are running courses for the Radio Amateurs Examination.

BATH City Technical College, Avon Street. The instructor is P. A. Bubb, G3UWJ.

BOSTON College of Further Education, Rowley Road. Lecturer is D. Byrne, G3KPO, Home House, Quadring Watergate, Spalding, Lines

BRIDGNORTH College of Further Education, Stourbridge Road. Starts September 17. Lecturer is P. Edwards, G3DKJ and M. Jones, G3JCX.

BRIGHTON Technical College, Faculty of Engineering, Richmond Terrace.

CANNOCK Technical College, Stafford Road. Further gen from Principal, Cannock 5811. **CANTERBURY** College of Technology, New Dover Road. Lecturer: D. J. Bradford G3LCK.

FARNBOROUGH (North and West) Further Education Centre, St. John's Road, Cover, Farnborough. Lecturer is John Hardy, G3KND.

GOSFORTH The Grammar School, Gosforth, Northumberland. Tutor: D. R. Loveday, G3FPE.

LIVERPOOL College of Technology, Riverside Road. Details from the Head of Department of Electronics and Radio Engineering.

LONDON (Beckenham) Adult Education Centre, 28 Beckenham Road. Tutor is R. E. Piper, G3MEH.

LONDON (Chingford) Community Centre, Friday Hill House, Simmons Lane. Instructor is E. Johnson G2HR.

LONDON (Holloway) Shelburne Youth Centre, Hornsey Road, London N.7. Phone 01-607 8522. LONDON (Wembley) Copland Evening Institute, Cecil Avenue, Wembley. Further gen from I. J. Bayliss, G8CZQ, 4 Aintree Close, Hillingdon, Middlesex. UB8 3HS. MANCHESTER Adult Evening Centre, Moorside County High School. Swinton. Instructor is P. Whatmough, G8BFP, and further information may be obtained from: T. Honeyford, 2 Gorsefield Drive, Swinton, Manchester.

NEWPORT College of Further Education, Nach Road, Newport, Mon.

PETERBOROUGH Electronic and Engineering Dept., Peterborough Technical College, Enfield Road. Further details from D. Byrne G3KPO, Homa House, Quadring Watergate, Spalding, Lincolnshire.

ON RECENT DEVELOPMENTS

TV MAGNIFIER

AVE you ever wished you could take a closer look at some television programme? How about a television magnifier? One European research establishment has come up with a device which is based on closed circuit television (c.c.t.v.) principles. The unit can enlarge from $5 \times$ to $25 \times$ and could be used to help people with poor vision or, perhaps, for educational applications.

It must be confessed that the thought of having Raquel Welch on the television is exciting enough, but the prospect of having a gadget which could magnify her left toenail by $25\times$ is positively unbearable, although it might put your scribes' viewing habits on a firm footing.

ALPHA-NUMERICS

Alpha-numeric displays have been with us for quite some time. There are many types, i.e. l.e.d., hot wire, liquid crystal etc. Someone has just found another type and they are calling it "Electrochromic". The basis of operation is to take a colourless organic material and transfer electrons to it from an electrode.

A small, flat glass cell is filled using viologen bromide in aqueous solution. The display is formed by arranging a suitable pattern of working electrodes plus a common electrode inside the cell. The viologen ions receive electrons at the working electrodes by the application of only one volt between the common electrode and relevant working electrode. This causes the solution in the immediate vicinity of the working electrode to assume a blue/purple colour. Thus a shape (number, figure etc.) is shown coloured against a clear background.

By applying the voltage again, but in the reverse polarity, the viologen ions are forced to give up their captured electrons and thus the display is erased.

These displays can exhibit a memory effect and offer good contrast which is claimed to be independent of the direction of viewing.

AGAINST THE LAW!

Many people are becoming increasingly alarmed about the use of computers to store vast amounts of "personal" information. It is commonly felt that a great deal of private information about the individual can

be accessed by all and sundry. So, three rousing and sincere cheers for Sweden, the Swedish Government and for Prime Minister Olof Palme. A law has been passed which gives at least some protection to the man in the street. In Sweden, you are not allowed (now) to even compile a personal register of names etc. without the express permission of the newly appointed Data Inspection Board (D.I.B.). It is now against the law to keep "sensitive" information about people in computers, such as psychiatric notes, arrests, alcoholism etc. unless you have permission from the D.I.B. And you are not allowed to keep computer notes about an individual's political or religious views.

Two of the best items are a) An individual can sue a Data Bank which gives out wrong information about him or her and b) Every individual has the right to receive a free printout of all information which a Data Bank has on him—and that such a printout shall be in an understandable form. Government Departments can still keep Data information, but it is a very good start. At present, Sweden is the only country in the world to have such a system. Lets hope it's catching.

ENERGY CRISIS

The energy resources of the world are going fast, so we're told. Other methods of supplying power must be found. One possibility which has been with us for sometime is sunlight/daylight plus the photoelectric cell. I predict some really hot developments in this field, especially from the United States where people are becoming acutely aware of the energy crisis which is approaching.

One company over there currently markets a unit composed of five cells which has a 1·5 Watt capability and sells for around 30 dollars for quantities of 1,000 plus. Solar cells are already being employed in a variety of applications—to drive a small television receiver and to power a navigational beacon, the latter requiring 50 Watts.

A European company is manufacturing a unit which comprises 64 cells and measures just over 1.5 inches in diameter. It gives 8 Watts but before you get too excited the price in the States is around 310 dollars for 1,000 up

quantities. The U.S. is mentioned here because it uses such a colossal amount of energy. One official body in the U.S., the Solar Energy Panel, advises that 20% of the electrical energy required by the U.S. during the next three decades could be obtained from solar energy—but only if sufficient funds were made available for research.

THE T.S.D.

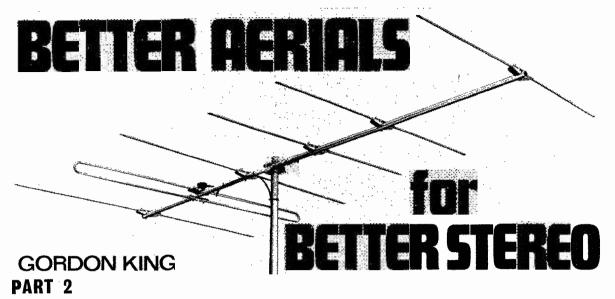
In London recently a company demonstrated what it called a Touch Sensitive Digitiser. This touching display involves a piece of glass. Two edges of the glass (at right angles to each other) have piezoelectric transducers bonded to them thus forming X-Y axes. The transducers are fed alternately with a signal which causes them to produce a pulse modulated surface wave. Frequencies involved are around 4,000kHz.

When not energised the relevant transducer is connected to a receiver circuit. Special counter circuitry carefully measures the intervals between transmission of the wave and the reflection from a finger in contact with the glass (or any other object in contact with the glass). Thus, by putting a finger on the surface, its position can be accurately determined.

Because the glass is clear and has nothing internal added (i.e. electrodes etc.) it can be simply laid over images such as photographs, maps or even have an image projected onto it. A finger may then be pointed to any part, and that portion of the image can be stored in a computer. Thus a complete image can be put into the computer memory just by using a finger.

Some of the applications are interesting and very practical. How about using the idea for an electronic keyboard for typewriters or even electronic organs—no contacts and no noise. Clearly the solution to many problems will soon be in everyone's hands.

Ginsberg



SIGNAL PROPAGATION

The FM programmes are carried on very high frequency (v.h.f.) channels in Band II which extends from approximately 88 to 108MHz. The signals thus have some similarity between those used for television in Bands I and III. They are propagated in a similar manner, and the service area of a transmitter spans a radius little more than 40 to 50 miles (sometimes more in one direction than others owing to deliberately engineered transmitting aerial directivity or due to topographic features).

Thus consistent reception, particularly of stereo, cannot be normally expected much beyond this maximum range. However, this is not to imply that FM reception over greater distances is impossible. Indeed, under favourable conditions reception is not unknown over hundreds of miles, but then the propagation is enhanced by signal refraction in the troposphere (upper atmosphere) and sometimes in the ionosphere (the electrical layers above the Earth's local atmosphere).

However, reception due to such propagation is singularly unreliable and occurs (tropospherically) during spells of fine weather (i.e., during an anticyclone when the pressure is high). Fading is experienced as the refractive index of the troposphere varies.

LONG-DISTANCE RECEPTION

Reasonably consistent reception can sometimes be achieved over a path up to about 100 miles or so at an elevated receiving site and with a very sensitive tuner (IHF usable sensitivity in the order of $1.5\mu V$, p.d. 75 ohms) coupled to a high-gain multi-element aerial accurately orientated and connected to the tuner through low-loss feeder. The author is currently receiving stereo from his nearest stereo-encoded station over a distance of about 100 miles on the Goodmans Module 90 tuner-amplifier (receiver) in conjunction with a six-element Antiference aerial at a site with a good outlook towards the station at an elevation of about 200ft. Reception is not one hundred per cent reliable even then, but for most of the time 'entertainment quality' stereo reception is possible.

Readers who may be contemplating establishing a system to receive stereo at such extreme ranges must ensure that the tuner is of good quality and that it is endowed with good selectivity (IHF alternate channel selectivity not less than about 45dB) as well as high sensitivity, especially if the distant stereo station is close to the frequency of the much more powerful 'local' signal.

Moreover, if the 'local' signals are very strong the tuner or receiver must have a high immunity against input (or front-end) overload, this generally calling for two or more variable tuned circuits in front of the mixer and field-effect transistors for r.f. amplification, if not for mixing.

The aerial required for good stereo thus depends on the distance of the site from the transmitter, amongst the other factors already noted. In the inner service area, up to about 20 or so miles from a transmitter, a relatively simple aerial might extract sufficient signal strength from the passing radio signal, provided there is not a lot of local screening or electrical interference (e.g., car interference from a nearby main road!).

FM DIPOLE

The simplest FM aerial is the dipole. This is a length of wire or rod conductor of about 5ft. in overall length broken in the centre for feeder connection, as shown in Fig. 2. The actual length depends on conductor diameter and on the part of the FM band where it is desired to 'peak' the response. The length, in fact, tunes the aerial. The wavelength of an

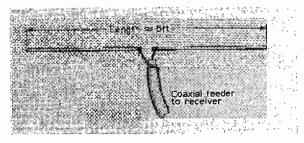


Fig. 2. The simple dipole aerial, useful in close proximity to the transmitter.

electromagnetic wave in metres is equal to the wave velocity divided by the signal frequency. The velocity is very close to 300×10^6 metres/sec., so the wavelength of a 100MHz signal is 3 metres.

The simple dipole is useful when its length corresponds to about half the wavelength, which in this case is $1\cdot 5$ metres, which is close to 5ft. However, the velocity is reduced slightly as the wave is extracted by the aerial, depending on the velocity factor (a function of the length/diameter ratio), so a practical dipole is generally made a little shorter and tuned to a slightly lower frequency, such that it works out to approximately 5ft. again.

The FM signals are horizontally polarised (mostly, anyway, though 'slant' polarisation is used in some parts to facilitate response on FM car aerials which are vertically disposed). This means that the receiving aerial has to be disposed horizontally to secure maximum 'capture' of the signal. So arranged, the aerial has a so-called 'figure-of-eight' polar diagram, as shown in Fig.3, where there are two maxima and two minima response directions, the aerial picking up most signal when broadside on to the station and least when end on.

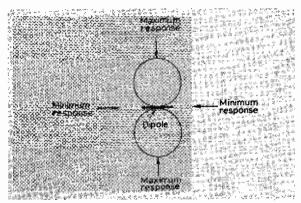


Fig. 3. Diagram showing the pickup characteristics of a dipole aerial.

This sort of aerial may be all right up to ten miles from a powerful station, even when placed indoors or in the roof space, though towards the edge of the inner service area it may have to be mounted outside

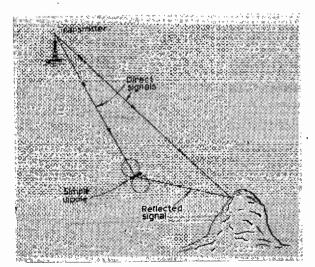
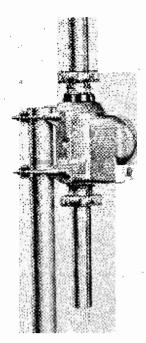
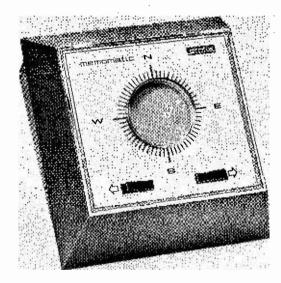


Fig. 4. Regardless of signal strength unwanted reflections of the signal can cause distortion on FM.



In some areas several FM programmes are receivable but usually only if it is arranged to rotate the aerial system. In the Stolle system the motor-driven rotator, left, is remotely, controlled by the 'Memomatic' control box, below, thus showing the direction in which the aerial system is pointed. (J-Beam Ltd.)



on a bracket, fixed to a wall for example. However, since it is wide-open to signals arriving from all directions it is of little use for discriminating against unwanted signals and interference.

REFLECTIONS

Like television signals, FM signals are vulnerable to reflection from hills and large structures. On television we get the well known ghost image or picture. On FM we get severe harmonic distortion, and, when the system is stereo, impairment of the stereo separation and consequent loss of stereo effect.

What happens is shown in Fig.4. The simple dipole receives the direct signal at one side and a reflected signal from a hill on the other side, where the response is still high. The reflected signal arrives a small fraction of a second after the direct signal owing to its longer route, and it is this which results in the distortion (and ghosting on television). An aerial of greater directivity is thus required to eliminate or reduce the response to the reflected signal or signals.

AERIAL DIRECTIVITY

A dipole is given directivity by the addition of socalled parasitic elements (meaning that they are not in actual effective electrical connection with the dipole). Such an element behind the dipole is called a reflector and elements in front are directors. There is usually one director (or director system, depending on aerial design)and one or more reflectors.

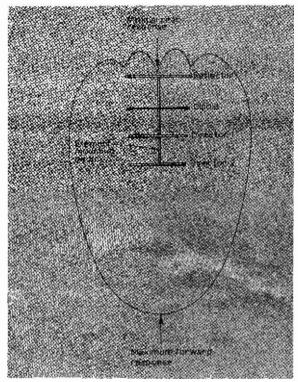


Fig. 5. Polar diagram of a typical four element FM beam aerial.

A simple horizontal 'H' type aerial could be composed of the dipole and one reflector or one director. With the former the dipole would face the station (reflector behind) and with the latter the director would face the station (dipole behind). Usually, however, the parasitic of an 'H' aerial is a reflector.

The greater the number of elements used in a design (up to a certain number governed by technical and practical factors), the greater the directivity, and with four elements (reflector, dipole and two directors) we might obtain a polar diagram as shown very approximately in Fig.5. Here is indicated that the

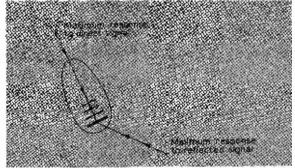
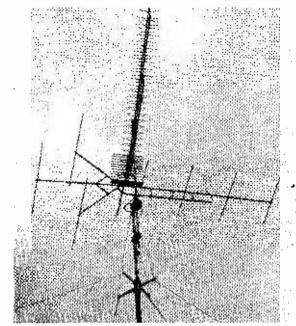


Fig. 6. Positioning of beam to avoid reflected signals can be quite



The FM aerial here is an Arrow 'Eight' by R. Smith Aerials of Luton. The accompanying TV array is one of the Zodiac range by the same company.

response has been 'pushed' from the rear and sides towards the front (rather like a stressed balloon), and resulting from this the front of the aerial picks up more signal than a simple dipole.

The aerial is thus said to have 'gain'. Such an aerial, therefore, could be used to advantage in a situation as shown in Fig.4 to reduce the response to the reflected signal (Fig.6) and also in an area of weak signal field, where the intrinsic gain yields a greater signal than a simple dipole at the feeder.

Thus, even in areas relatively close to a transmitter a high-gain directional aerial may be required to discriminate against unwanted signals arriving at bearings off the main beam, while at locations towards the edge of the primary service area and into the outer service area a high gain array might be required to produce sufficient signal strength for noise-free stereo reception.

No hard and fast ruling can be given, but as a rough guide a simple dipole might prove adequate up to ten or so miles from a station, a two-element aerial from ten to twenty-five miles, a three-element aerial from twenty-five to about thirty-five miles and a four-element array at the extremes of the service area; but as already expounded, much will depend on the sensitivity of the tuner or receiver, on the site elevation and height of aerial above ground. For extreme fringe working an aerial of six elements could make all the difference between just about acceptable stereo reception and good, noise-free stereo reception.

PART 3, NEXT MONTH, WILL CONCLUDE THE SHORT SERIES BY SHOWING HOW TO CONSTRUCT A FOLDED DIPOLE AND A FOUR ELEMENT BEAM FOR FM. MATCH-ING DEVICES AND ATTENUATORS ARE ALSO DISCUSSED.

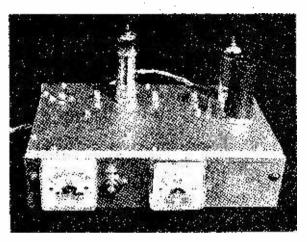
10 Wcits For Secretary 10 Wcits For Secretary 12 Metres

THE transmitter described here has only three stages, is crystal controlled, and gives a very useful RF output, running at about 10 watts. This, with a simple dipole aerial, will give solid contacts over a fair radius so for local working a rotary beam aerial is not necessary.

CIRCUIT

Fig. 1 is the circuit. The lowest frequency present is 72MHz, followed by a doubler to 144MHz. This results in an output free from unwanted frequencies. With a 144MHz transmitter it is quite usual to employ an 8MHz oscillator followed by multipliers (such as $3\times3\times2$) to obtain $18\times$, or 144MHz. This can result in the presence of unwanted frequencies with the output. But with a 72MHz oscillator, followed by a doubler, incorrect adjustments, which will produce frequencies outside the band, are extremely unlikely.

A 72.2MHz crystal was fitted for output on 144.4MHz, but other frequencies can be used. V1, a 6C4, is employed with an overtone crystal with L1 tuned to about 72MHz. With this type of oscillator



the circuit does not oscillate at the crystal fundamental and so no lower frequency energy is present. Oscillation is directly at the overtone frequency for which the crystal is made.

Experiments with this kind of circuit show that it is almost useless trying to press old surplus

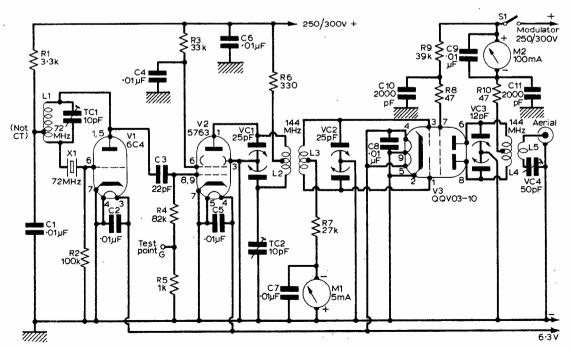


Fig. 1. Complete circuit of the 2m transmitter using spot frequency crystal control.

crystals into service even if a harmonic works out at the required frequency. These crystals may fail to oscillate or may give only a very small output or not provide the expected frequency when operating in an overtone mode. It is thus virtually useless to try the circuit with any crystal except the correct type.

Feedback depends on the position of the tapping on L1, and the small trimmer TC1 allows ad-

justments to tuning.

V2, a 5763, receives drive at 72MHz and doubles this to 144MHz so no problems of stability arise. It was not found necessary to operate this stage at maximum dissipation in order to get enough grid drive for the power amplifier. However, maximum ratings for the

5763 used may be noted, in case it is wished to raise the output. When operating as a doubler, 300V may be applied to the anode when R3 can be reduced to $12.5 \mathrm{k}\Omega$. Maximum anode current should then be $40 \mathrm{mA}$ resulting in a maximum anode dissipation of 12 watts.

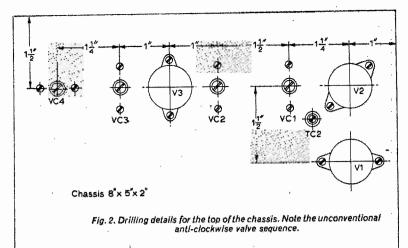
L2 is tuned to 144MHz by VC1, and TC2 compenstates for stray capacitance in V2. Tap G is a test point allowing grid current to be checked without

having to disconnect R4.

The QQV03-10 is an internally neutralised double beam tetrode, working as a straight through PA at 144MHz. L3, tuned by VC2, drives the grids in push-pull and, as bias is obtained by grid current through R7, a grid current meter M1 is permanently fitted. The actual maximum rating of this stage is 76mA anode current at 300V, or 23 watts input, with 3mA grid current. Normally, a somewhat lower input has been used, around 10 to 15 watts.

* components list

Resistors	
R1 3 3 3 2 4 W	R6 3390 1W)
R2 100k(1+W	
R3 3360 34V	
R4 82651 4W	R9 3060 1W
R5 The TW	R10 470 W
Capacitors	
C1, C4, C6	0.01µF 350V disc ceramic
C2, C5, C7, C8,	C9 0-01µF 150V disc ceramic
C3	22pF mica
C10, C11	2000pF 600V disc ceramic
TC1 10nE trin	nmer (Jackson Tetfer)
TC2 100F 015	
VC13958F Bist	birfly 6-015" spacing (Jackson C713)
VC2 25oF but	terfly 0 015 spacing (Jackson C713)
VC3 120F but	torny 0 046" spacing (Jackson C713)
VC4 50gF (Ja	
Values assesses	
V1-6C4 V2	5763: V3 QQVO3-10
2022020202020	
Miscottaneous	i j∌d. M2, meter 100m A fsd.
MIT HISTORY OF STREET	x 2in. with 5 x 2in. screen.
CB33565 0 2 0	t. On-off toggle switch.
Constant Socke	J (or HC25U, see text) (Senator
Children of M	alleyfield Road, London, SW16).
that single so w	B7A (1) ceramic with skirt and



L4 is tuned by VC3, and M2 is permanently connected to show anode current. HT for this stage is drawn from the modulator so S1 can be opened during tune-up, so that HT is not applied to the PA.

TC3 adjusts PA loading and the output is fed into a co-axial cable which runs to the aerial. The original transmitter could be operated without the least disturbance to TV reception in the same house, but this depended on various factors and it is impossible to say that this happy state would remain so in all circumstances.

CHASSIS WORK

Drilling dimensions for the $8\times5\times2$ in. chassis are shown in Fig. 2, V1 requiring a skirted holder with screening can, but screens must not be used on V2 or V3. A screen is required across the holder of V3, below the chassis. If a "universal chassis" is used, an extra 5×2 in. flanged side can be used for this purpose its flanges being cut to fit inside the front and back flanges.

Holes are cut or punched in the front runner to take the meters and switch, the back runner taking the co-axial aerial socket and a grommet for the

power supply leads.

The capacitors VC1/4 are readily available each being mounted by two 6BA bolts. The exact values shown need not be used and some slightly smaller surplus capacitors of similar type have been cheaply available and are quite suitable.

WIRING

Fig. 3 shows all wiring and components and Fig 4 the construction of the coils. All by-pass capacitors (C1, C2, C4, etc.) should be connected with the shortest practical leads.

One end of L1 is soldered to the insulated tag of a small tag strip, which also supports TC1. A lead from the second tag of TC1 runs to pin 5 on V1 and this lead supports the other end of L1.

A wire-ended crystal was used its leads going to pin 6 on V1 and the junction of L1 and TC1 at the

tag strip.

Keep heater and HT leads against the chassis, but RF leads, such as to C3, clear of the metal. TC2 is a tubular trimmer, mounted by a nut which forms the chassis return.

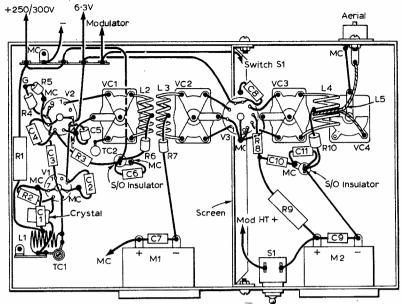


Fig. 3. Layout of components and wiring underneath the transmitter. See note at end of article with reference to crystal mounting.

R6, R7 and R10 have a very short lead to the centretap of the appropriate coil. Position L2 and L3 so that they are almost touching each other.

The junction of R3, C6 and R6 is supported by an insulated tag or pillar as is the junction of C10, C11 and R10.

Position the holder for V3 so that pins 1 and 3 come to the left of the screen, as in Fig. 3. Cut the screen to pass closely over the valveholder, while adequately clearing tags 1, 3 and 4. Note that the screen passes completely across the holder. It is secured by bolts fixing the valveholder and is also bolted to the front and rear of the chassis.

The ends of L5 are shaped so that they can be

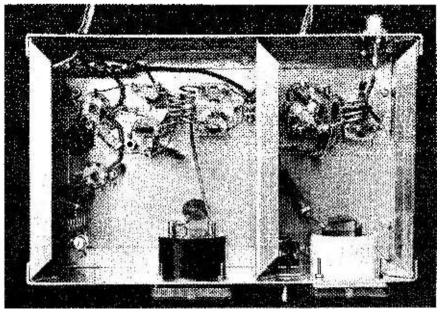
soldered to VC4 and the aerial socket, when L5 is pushed between the middle turns of L4.

Check that the capacitors can be adjusted without fouling leads or resistors. Chassis returns should be stout and as short as possible.

Fit flexible leads from the tag strip for power connections. The jumper between HT tags is to allow easy disconnection of V2.

The heaters require 1.73A at 6.3V. For HT purposes, a 300V 120mA or similar supply is most suitable, though the equipment will work satisfactorily at reduced input with a lower voltage.

If the HT voltage for V1 and V2 is too low, it may be difficult to obtain enough grid drive for V3.



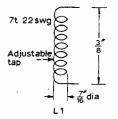
Photograph of author's prototype transmitter which may be compared with Fig. 3, above.

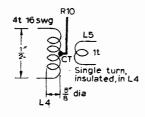
A voltage of under 250V is not recommended for V3. With 250V it is better to keep to about 6W to 8W input, rather than trying to load V3 to a greater input, which may actually reduce RF output, when the HT voltage is low. Anode current is shown by M2.

A small push-pull modulator will do very well with the transmitter. Good results can also be secured with an economical modulator consisting of a twin triode such as a 12AX7, followed by a single 6BW6 or similar output stage, but the PA input should then be kept down to 8 or 9W.

ALIGNMENT

It is obviously necessary to adjust the circuits for proper working. However, wrong adjustment is more likely to result in no RF output, rather than an output which is outside the permitted band. The PA is not switched on by S1 until 1 to 2mA grid current has been obtained, as shown by M1. In any case correct operation of the crystal oscillator must first be checked.





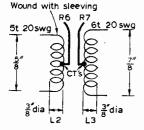


Fig. 4. Winding information for the four coils. See text for position of tap on L1.

Temporarily disconnect the HT jumper so that HT is on V1 only. V2 must however be in place. A meter should be included in the HT lead to V1. Ideally, rotation of TC1 should now show a point where the anode current of V1 falls, showing that oscillation has begun. Turning TC1 away from this position, either way, should result in anode current rising again, due to oscillation ceasing. In these circumstances, the frequency of oscillation is controlled by the crystal and all is well. In addition, checking with a receiver will show that the oscillator frequency does not change, no matter what setting is used for TC1. Wrong adjustment of TC1 merely causes oscillation to cease.

It may be found that current remains relatively low, say 7 to 8mA, for all settings of TCl and that the oscillator frequency moves over the band as TCl is adjusted. If so, the oscillator is not controlled by the crystal. This must be corrected by moving the tapping on Ll a little nearer the crystal end of the coil.

On the other hand, it may be found that no adjustment of TC1 produces oscillation and that current remains around 15mA or so. In this case, the tapping must be moved a little nearer the anode end of L1.

TC1 is purposely small, so that it is practically impossible to tune to wrong overtones of the crystal. It might thus be necessary to compress or stretch L1 a little to get the circuit on frequency. If a grid dip oscillator is available, adjust L1 so that this shows resonance at 72MHz with TC1 about half screwed down.

This type of oscillator is not particularly tricky, but may require a little care and patience. Once adjusted, it is reliable and will not need any more attention.

When oscillation is obtained, clipping a meter across R5 (meter negative to G) should show a little grid current in this stage, rather less than 1mA. HT can then be applied to V2.

Rotating the capacitors VC1 and VC2 should now show grid current on M1. If VC1 is fully closed without a peak being reached, compress L2 slightly, and vice versa. Coverage of these circuits is quite small, and it is impossible to tune them to wrong harmonics, if made as described. Coils L3 and L4 can also be adjusted in the same way, if necessary, so that each trimmer has a definite tuning point.

TC2 can be set about half open. Subsequently adjust it a little at a time, while correcting tuning with VC1, until the best grid current reading on M1 is obtained.

Should the best obtainable grid current be too small L2 may be moved nearer to L3. It may also be necessary to increase the HT voltage to V2 in particular, if this is rather low, or to reduce the value of R3, or to make a small adjustment to the tap on L1, to secure more drive. Final adjustments are made with all stages tuned up and working. Where grid current is more than adequate, L2 and L3 may be separated a little, or tuning slightly staggered.

PA ADJUSTMENT

As mentioned, HT must not be applied to V3 until at least 1mA is shown by M1. A load such as a 12V 6W lamp can then be plugged into the aerial socket, VC4 is opened and S1 is closed. Adjusting VC3 to resonance should light the lamp. If L4 needs adjustment, make this as described for L2 and L3.

Closing VC4 will increase loading. As is usually the case with VHF equipment of this type, an accurate indication of PA tuning cannot be obtained by observing the dip in anode current shown by M2. A slight re-adjustment of VC2 and VC1 may be required as the PA is loaded and tuned.

It should be found that the circuit works reliably when switched on. If the oscillator does not start, tune TC1 slightly off peak, until this is overcome.

For local working, a dipole is easily made which has the advantage of minimal directivity. It can be constructed from alloy tubing, flattened and drilled at the inner ends and secured here in an ordinary junction box. The overall total length should be about 38^{1} ₂in. A co-axial cable is attached to the inner ends of the elements, in the junction box, The aerial can be raised on a light post or pole, or can be fixed to a support arranged as convenient on the house.

As the use of a wired-in crystal severely restricts the versatility of the transmitter constructors may wish to use the similar plug-in crystals, type HC25U, with a suitable socket.—Tech. Ed.

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A very simple project this month, based on our old friend the astable multivibrator. Although it uses only small-signal transistors it gives a surprisingly high output signal level into a 35 ohm loudspeaker.

Circuit

Transistors Tr1 and Tr2 are the active components of the multivibrator, the frequency of oscillation being being set by C1 with R2 and C2 with VR1 and R3. The signal at the collector of Tr2 is directly coupled to Tr3 which works as an emitter follower to provide sufficient current drive for the loud-speaker.

Note that the circuit runs from a 4.5V battery. It would be very unwise to exceed this voltage because, as the circuit stands, Tr3 is working on the limit of its power dissipation; an increase in supply voltage could easily destroy this transistor. Because of the lower-than-usual supply voltage it is not necessary

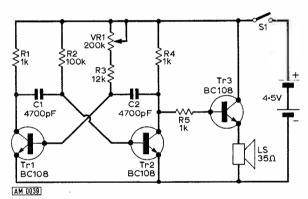
R1	∵ 1kΩ	.1p
R2	100kΩ	1p
R3	12kΩ	1 p
R4	1kΩ	1 p
R5	1kΩ	1p
C1	4700pF	4p
C2	4700bF	4c
VR1	200k() (linear)	25p
Tri	SC198	10p
Tr2	SC198	10p
Tr3	BC108	10p
SWI	Push switch	15 p
		83p

LST is a 35 ohm loudspeaker and is not allowed for in the above list.

No allowance is made for minimum order costs or for postage and packing and these points should be checked carefully before ordering. to protect the base/emitter junctions of Tr1 and Tr2 with diodes. Thus the circuit is probably as simple as it could possibly be.

Operation

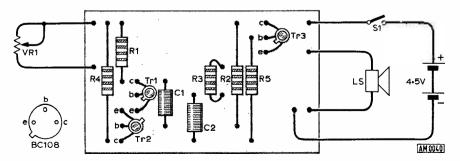
Operation is effected by the push button in the supply line and provided this is of reasonable quality clicks should not be too troublesome. It would be possible to use a slider potentiometer for VR1 and make quite a smart looking instrument that would operate in much the same way as a real Swanee Whistle. If the frequency of operation is not in the



Circuit of the Swanee Whistle

range desired it can be dropped by about one octave by doubling the values of C1 and C2; conversely, halving the values of these two capacitors raises the frequency by about one octave.

A word of warning: it is not advisable to run the circuit with a loudspeaker having an impedance of less than 35 ohms but higher values may be used at the expense of power output.



Suggested layout of circuit on veroboard and connections to external components.

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AF139 nnp germanium medium power 40p
AF139 nnp germanium medium power 40p
AF139 pnp germanium medium power 40p
BC107 12p; BC108 12p; BC108 12p;
BC107 12p; BC108 10p; BC108 11p
BC107 12p; BC108 11p; BC108 13p
BC107 12p; BC108 11p; BC208 13p
BC107 12p; BC208 11p; BC208 13p;
BC107 12p; BC208 11p;
BC107 12p;
BC208 12 DIODES
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OA200 9p; OA202 10p
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Full lists and technical data will be found in Catalogue No. 6. See also amendments list.

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1W	5%	4·7 Ω-10M Ω
1/2W	2%	10 Ω-1M Ω
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MEDIUM WAVE BROADCASTS by Charles Molloy

BC RADIO NOTTINGHAM is now broadcasting on 1520kHz (197m) from a temporary installation which is expected to provide satisfactory reception up to about 8 miles from the centre of the city. This brings the total number of BBC Local Radio Stations transmitting on the medium waves to eighteen, only Carlisle 755kHz (main) and 1457kHz (relay) and Derby 1115kHz have still to come on the air to complete the network of stations in England. The following are currently on the air:-Radio Blackburn 854kHz; Radio Solent (main) 998kHz; Radio Medway, Radio Sheffield 1034kHz; Radio Leeds 1106kHz; Radios Birmingham, London, Manchester, Newcastle on 1457kHz; Radios Brighton, Humberside, Merseyside, Oxford on 1484kHz; Radio Stoke-on-Trent on 1502kHz; Nottingham 1520kHz; Bristol, Teeside 1546kHz; Leicester, Solent (relay) 1594kHz.

Ian Gordon (Birmingham) has tried the medium waves with his Codar CR70A receiver, aerial tuning unit and 80ft longwire aerial. He reports hearing Radio Nacional Espana, Madrid, on 584kHz; Radio Prague 1286kHz at 2200hrs; Radio Tirana, Albania 1394kHz in German at 2200hrs and Trans World Radio Montecarlo 1466kHz with sign-on at 2115hrs.

His daytime loggings of BBC Local Radios are Nottingham 1520kHz at 1430hrs; Bristol 1546kHz at 1240hrs and Leicester 1594kHz at 1000hrs.

Richard Tubridy (Bickley, Kent) has been listening to North Africa on the medium waves and he reports hearing Algeria with its Arabic Service on 533kHz from Ain Beida and on 548kHz from Oran. The French Service was heard from Alger Chaine 3 on 890kHz and also during the daytime from Tipaza 251kHz on the long waves. Richard has been having difficulty with Radio London 1457kHz at night owing to interference from a station playing Chinese music and he asks if this could be coming from China itself. The 500kW transmitter at Durres in Albania operates on 1457kHz and as this station relays the External Service of Radio Peking every evening it is the most probable cause of the interference. A similar high power transmitter which operates on 1214kHz has caused trouble with reception of BBC Radio One in some parts of the U.K.

Radio 4 medium wave broadcasting is to be restored to the south-west of England. In a recent written parliamentary answer the Minister of Posts and Telecommunications stated that he has authorised the BBC to install low-power transmitters at Exeter, Barnstaple, Torbay, Plymouth and Redruth to broadcast on medium frequencies the programmes carried on the VHF transmissions of Radio 4, which include regional items. Redruth is now on 908kHz but so far there is no information as to the frequencies of the others. During 1973 it is likely that Radio 4 transmitters at Stagshaw and Scarborough will change from 1151kHz to 908kHz, according to the BBC.

VHF/FM

by SIMON DAVID

AM not quite sure how the editor would react to my mentioning Pirate Radio stations yet again especially after I mentioned that one of our readers had picked up Radio Classic recently. Another reader **Peter Welton** has sent information to me about some of these stations.

The reason I mention this is not so much to give these stations publicity but rather to highlight an increasing problem that could occur on the v.h.f. band which is already existing on the a.m. band. That is the increasing congestion of broadcasting stations coming in on particularly sensitive receivers especially around the 95MHz region.

Chris Webstor sends me an interesting letter in which he lists several stations which can be picked up from the continent. He says that he is in rather too steep a valley to enjoy tropospheric DX except from due north and south. He is at Ringwood, Hants.

On 16th June he says that several f.m. stations in France were completely swamped by Yugoslav signals and this report bears out what has been the experience of several readers of late. He uses an FM6S aerial a home made pre-amp and a Teleton tuner and lists several frequencies ranging from 87·7 up to 99·6MHz. These have all been the result of sporadic-E interference. Examples he mentions are Radio Beograd on 90 and 99·6MHz, the largest signal he claims comes from Celevac, Croatia, on 95·1MHz. This and Novi Sad, Serbia on 87·7MHz both transmit at 50kW. Most of the real DX, Chris says, comes from Russia around 70MHz but Russian television sound comes in on 91·75 and 99·75MHz.

Mr. G. M. Christie writes to me from Orkney, north Scotland. When there is a high pressure area situated to the East and South of his home he is able to receive clear and strong signals from the Norwegian f.m. stations, wiping out some BBC v.h.f. transmissions from local stations about 10 miles away.



He has received second channel images from Grampian television sound and the vision carriers from channel 9 Aberdeen and channel 8 Rumster.

Have you noticed the lack of v.h.f. frequency information-with the radio programmes in some newspapers? The wavelength on the medium or long wave is usually given but they seem to ignore the v.h.f. band. Perhaps the BBC could help to rectify the situation in the near future, or at least recommend through all newspaper editors that they include all broadcasting bands for their stations in the information provided opposite their programme material.

It is well worth recommending once again the use of good aerials, particularly near the edge of normal reception areas if you want to pick up a good stereo signal. Elsewhere in this issue you will find part two of an excellent article which Gordon King started last month on improved stereo reception which I would recommend to all enthusiasts of the v.h.f./ f.m. band whether stereo biased or not.

Although modern receivers are extremely sensitive it is necessary to improve on background noise and to make sure that you lock on correctly to the stereo signal. This is not always possible if your aerial system is inefficient and in particular does not employ the correct matching cable between the aerial array and your receiver. Furthermore the interference from car ignition is a particular problem with f.m. so justifying the use of a highly directional aerial of high gain.

SHORT WAVE DX by MALCOLM CONNAH

A good receiver for the newcomer to the hobby is the ex-RAF R1155 which can be obtained in good working order for as little as £5. Other receivers which are commonly available include the early HRO and the AR88. The latter is probably the most wellknown of these sets and can be obtained for about £25.

One receiver of particular interest is the CR100 which was made by Marconi for Services use during the last war. This set is ideal for both medium and short wave listening. The coverage is in six bands from 60kHz to 30MHz and the set has two r.f. and three i.f. stages, a crystal filter, a b.f.o. and an internal mains power supply.

The main shortcomings of the CR100 are its lack of sensitivity above 20MHz and the absence of an 'S'-meter. The high frequency performance can be improved by modifying the r.f. stages to use modern valves such as the 6BA6 and an 'S'-meter is a very simple addition. The CR100 can be obtained for about £5 to £15 depending on condition, and fully reconditioned sets have been seen for £20-£25.

Readers' Logs

The first log this month comes from D. A. Lavender of Gravesend in Kent who used his Teleton TF182 receiver and a 75 foot inverted 'L' aerial to hear the following:

3997 SABC, South Africa in English at 2330.

DX enthusiasts usually use a rotating aerial which is controlled from the receiver location but excellent results can be achieved by careful and strategic sighting of your aerial in the first place. If it is directed at a local high power British broadcasting station you are not likely to achieve very good results from long distance reception and you are also inclined to have difficulty in separating one station from an adjacent one.

The BBC issues local maps for v.h.f. radio services with average field strength contours of 60 and 48dB relative to $1\mu V/m$ for a receiving aerial height for 30ft above ground level. These are average figures and contours and do not take into account steep hills or any other such violent variations in the local topography. However very good and satisfactory results can be achieved in many places with sensitive receivers using telescopic aerials but one must not expect to get good stereo signals in this

"Birdies"

One of our frequent correspondents, Hugh Cocks, of Mayfield, Sussex, reports that on June 20th RNE Spain came in well on 87.75MHz. On July 13th, he reports. Spain and Yugoslavia was received and Genk -97.9MHz-from Belgium on August 2nd.

In certain parts of the country, reception is affected by transmitters operating on adjacent channels, i.e. on frequencies close to that of the wanted services. This interference can result in an audible effect known as "birdies"-a varying highpitched background to the programme heard from the loudspeakers. A carefully positioned multi-rod aerial may help to eliminate the interference but it is also important that the receiver should incorporate a low-pass filter. All stereo receivers should have such filters.

4765 C.R.E. Guayaquil, Ecuador noted at 0435.

4820 La Voz Evangelica, Honduras, English at 0355.

4832 R. Capital, Costa Rica in Spanish at 0445.

4905 R. Relogio, Brazil in Portuguese at 2300. 4915 Nairobi, Kenya in Swahili at 2000.

4995 R. Brazil Central in Portuguese at 0035.

5047 R. Lome, Togo in French at 2130.

6020 R. Nederland, Bonaire relay at 0025.

11745 HCJB, Quito, Ecuador in English at 0158. 11810 Beirut, Lebanon in English at 0230.

Andrew Dutfield of South Brent in Devon has a Trio 9R-59DS receiver and with this he connected to a 100 foot long-wire he was able to hear:

3335 BCC, Taiwan in Japanese at 2050.

3999 Godthab, Greenland in Danish at 2120.

4755 RRI, Makassar, Indonesia at 2105.

4865 R. Ponta Delgada, Azores, music at 2115.

5345 Voice of Free Yemen with music at 1840.

7690 R. Espana Independiente, music at 1910.

9870 R. Bangladesh in Bengali at 1935.

11415 Peyk-e-Iran, identification at 1945.

Harold Emblem of Mirfield in Yorkshire used his Lafayette HA-63 receiver and 18 metre long-wire aerial to hear the following interesting stations:

6020 R. Nederland, Lopik noted at 1515.

6065 R. Sweden, Horby noted at 2055.

9475 R. Cairo, N. American Service at 0300.

9515 Voice of Turkey, Ankara at 2210.

9625 CBC, R. Canada noted at 0230.

9745 R. Baghdad, Iraq noted at 1940. 11620 All India Radio from Delhi at 2120.

15205 VOA, Tangier noted at 2000.

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71b BARGAIN PARCELS

Hundreds of new components - capacitors, resistors, switches, crystals, pots, PC boards, etc., etc. Outstanding value £1 65 (37p).

COMPUTER PANELS: Type E: 4 OC29, 4 ACY19, 8 other transistors 35 diodes etc. £1 (10p). Parcel of 12 top quality boards, inc. power transistors, trimpots. IC's, etc. £2 (25p), 31b of lower quality £1 (25p), 71bs £2 (40n). 56lbs £12 (c.nd). Pack of boards containing at least 500 components including 50 transistors. 50p (15p).

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SHORT WAVES by DAVID GIBSON, G3JDG

Thas been another month where 28MHz has provided some surprises. Signals from ZP5, 5U7, CR6 and VU have been logged by more than one listener. Best periods to listen on ten metres appears to be late afternoons and early evenings but with this band one is never quite sure. The VU, for example, was heard around 1400 hours and quite a few African stations were logged around 1200 hrs.

Incidentally, on ten metres, there are a number of very useful beacon stations which operate and give an indication of what's happening on the band. On 28.180MHz is ZC4CY located in Cyprus, and on 28.190MHz there's 3B8MS on the island of Mauritius. Other beacon stations on ten metres are: VP9BA, 28.165MHz (Bermuda); VE3TEN, 28.175MHz (Ottawa, Canada); DL0IGI 28·195MHz and 28·200MHz -note this station is on 28.200MHz each hour between five minutes past the hour and 30 minutes hour (Salzburg, Germany); past the 28·185MHz (Crowborough, Sussex). Seems that you can log some quite good DX in beacon stations alone. Why not have a go this month and see just how many of these you can log-you might hear some other DX too.

Readers' Logs

Paul Newman (Thame), listens on 144MHz and 70cms. Best on 70cms; G2CXT, G3ISO/P, G3KEQ, G3WIR/P, G3YXZ/P. On 144MHz; PA0ZAZ/P, F0AKD, F6BHI/P, GC2FZC, GC8AWE. Paul uses an 8-element Yagi at 23ft on 144MHz and an 8-over-8 at 18ft. for 70cm. Gear consists of 'Sentinel' converters feeding an RA1 tuning 28—30MHz with an n.b.f.m. discriminator fitted. He also has an aerial in the loft called a turnstile—do you mean you actually charge the signals for admission?

Another 70cm enthusiast is Nicholas Richardson (Wendover, Bucks). The antenna is a 46-element Yagi at 37ft. Signals are down-converted to 144MHz and another converter is then used to feed an EC10 MkII receiver tuning 28—30MHz. Stations logged on 70cm include: G3s—BNL/P, EHM, LTF/A: RPE/P, THQ/A, TTV/P, VER/P, WDG/P, XJS, G4AJW,

G4ARD/P, G8s—ACE, ATD/P, ATP/P, AZU/P, FMK. Nicholas informs me that he is licensed to receive artificial Earth satellites and uses a MOSFET converter (136MHz-138MHz) feeding the EC10.

Michael Bolton (Banbury, Oxon) has been on ten metres for four weeks. The station consists of a homebrew MOSFET converter feeding a BC348RX tuning 4-6MHz. Antenna is a homebrew 6-element Yagi plus rotator at 30ft. Two-metre signals were heard from: F0AKD, F1AGV, F1CBH/A, F6BCK, F6BHI/P, G3IVE/M, G3TIR/P, G4AKA/P, GW3ONP/P, GW8PFU/M, PA0AKK, PA0VTR, PA0VV.

Stanley Sharred (South Yardley, Birmingham) sends in a super log for top band. His receiver is a CR150/2 and the antenna a horizontal Vee with 60ft. in each leg. "Ears" are Sharred Mk II's and the 160-metre stations heard: GM3TMK, GM3YOR, GW3VLX/P, GW3WSU/A, GW3ZQN, DL1FF, EP2BQ, HB9NL, K2ANR, LU5HFI, PY1DVG, 5Z4KL. A listen on 3·5MHz s.s.b. raised: GD6IA, C3IFO, CN8MN. KP4AN, LU2AFH, PY2CIQ, PY7BLV, V01FG.

D. Dance (St. Boswell, Roxburghshire) claims to have logged the following stations using a CR7OA, PR40 preselector, a.t.u. and a 264ft. end fed at 20ft. Topband c.w. signals from: DJ3CY, DL1FF, EI9J, GW3TLW, GW3UCB, OK1ATP, OK1MAC. On eighty c.w.; W4ZMQ, and W80N, while on eighty s.s.b.; CT1ADV, CN8MN, CT2BG, G3SKR/KP4, K2LWR, KP4AN, LU4CAM, OA4AKL, A OA4SS, VE1AHP, VE1ED, VO1BT, W3EGA, YV5AMW. Stanley even had a go on 7MHz and managed: LU5HFI, VK2BPN, ZL2BFU all on c.w., and VK3XI on s.s.b.

J. Eagland (Brighouse, Yorkshire) sends in a long, long log of G stations heard on 3.5MHz with the aid of his CR45 and 80ft. end-fed high up in the loft.

"I am a newcomer to Amateur Radio at the age of sixteen", says John Hughes (Gee—all those wasted years). John's equipment consists of an AR88LF, PR30 preselector "and a crude 60ft. of wire". The log for 14MHz reads: CT2BG, MP4BJR, OY3H, VK2MZ, VK3XI, VK5FM, VK6NM, VK8KK, ZE4NEB, ZD7SS, ZD7SD, ZK1PA, 5B4ES, 5X5FS, 6Y5ED, 7G1CD, 7Z3QR, 9F3USA, 9X5PK. John's best on eighty metres were: CX3BH, PJ2CW, PY2SUS, PY3GIQ, TF5TP, 3X2AX, 9G1DY, 9H1BX, 9J2WR. As a P.S. he asks where XK4 is hidden. Perhaps it's 20 miles each of XL4—anyone know for certain?

Stephen Fletcher (Bromsgrove, Worcester), has a 150ft. long wire in the loft and a homebrew, unaligned Heathkit SW717. Pick of Steve's best on eighty metres s.s.b.: CN8FL, VO1EL and 9H5D. Up on twenty metres Steve logged: CR4BS, CT1KA, EA2RAZ, EA3GN, HB9J, I0SNI, PJ2CW, PZ1DR, VE1HX, VE1WF, VK6JJ, VO1BT, VU2MX, YV3UN/P, YV5DER, 4X4UK, 7X2BK, 9H4E, 9Y4AVC, 9Y4VU, 9Y4VV, all on s.s.b. Ten metres produced: EA6BG and HB0AWQ, both on s.s.b.

BROADCAST BANDS

Short Wave Reports by 15th of the month to Malcolm Connah, 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.

Medium Waves Logs to Charles Molloy, 132 Segars Lane, Southport, PR83JG. VHF/FM Reports to Simon David, c/o Practical Wireless, Fleetway House, Farringdon Street, London, EC4A 4AD.

AMATEUR BANDS Short Wave/VHF

Logs in alphabetical order please by 15th of the month to David Gibson, G3JDG, 12 Cross Way, Harpenden, Hertfordshire.

The 'CONST-AMP'

a constant-current-source

D. T. GOODWIN B. Sc.

A LTHOUGH a constant-current generator is not an essential piece of apparatus in the amateur's workshop, it is not without its uses. The "Const-Amp" is a simple yet effective constant current source which can be connected to almost any low voltage power supply. The circuit described has been designed to supply up to 100mA but with the data provided it is a simple matter to alter it to individual requirements.

CIRCUIT OPERATION

In the circuit of Fig. 1 it can be seen that the base voltage is accurately controlled by the zener voltage Vz. Thus, taking into account the base-emitter drop of the transistor Vbe, the voltage across Ra is set and so its current is also set. This current Vz-Vbe/Ra can be assumed to flow completely into the collector circuit. By suitable choice of Ra the load current can be accurately set.

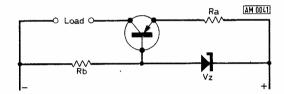
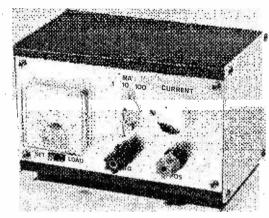


Fig. 1: A simple circuit for providing a constant current in a load.

The value of Rb must be chosen so that the current drawn through it, determined by the supply voltage minus the zener voltage, is greater than the zener operating current plus the transistor base

current. Assuming the transistor is of the OC28 family (Rfe=25) then the base current is Ic/25. Thus the current through Rb must be greater than Iz nominal + Ic/25 but not so great that an excessive current is drawn through the zener. The only limit on Ra is that the maximum collector current of the transistor is not exceeded.



The 'Const-Amp' completed and ready for the workshop.

THEORY INTO PRACTICE

The completed circuit as shown in Fig. 2. The main control is VR1/2 which controls the amount of current flowing in the load, R1 being inserted so that the maximum collector current can be set. R2 has been calculated so that the zener is not overrun when VR2 is at minimum. VR2 ensures that when

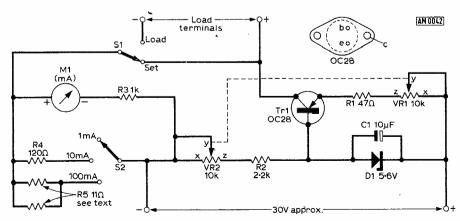


Fig. 2: Circuit of the 'Const-Amp'. R1 should be 1W, the remaining resistors ½W at 5% or better. The author used a 1mA meter of 75Ω resistance but 100Ω is suitable. The zener diode rating is 400mW (BZY88 series).

RECORD PLAYBACK HEADS TRUVOX

(TRUVOX: Individual prices of these arc. 2 track record playback heads 50p each track record playback heads 72p each Frase heads are also as allable separately—2 track 39p. 4 track 55p. MU-metal mounting shields 39p each. 2 track-heads already fixed on heavy mounting plate with shield £122.



DRILL CONTROLLER

NEW IKW MODEL Electronically change speed from approri-mately 10 revs. to maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instruc-tions. £1.95. Made up model also available. £2.95.

MIGHTY MIDGET

Probably the finest possible radio, as described in Practical Wireless, January 78. All electronic parts 22 20 post paid.



TIME SWITCH

IIME SWITCH
Smith's mains arrived clock with
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I CHIP RADIO

Ferrant's latest device ZN414 gives results better than superhet. Supplied complete with technical notes and circuits. £1.38 each. 10 for

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For experimenting with the ZN414.
KIT NO. 1. Plessey Miniature Tuning Condenser
with built-in LW switch and 3" Territe slath and

MIT NO. 1. Plessey Minhaure Tuning Condenser with built-in LW switch and 3" Ferrite slab and litz wound MW coil, 72p. KIT NO. 2. Air spaced tuning condenser 6" ferrite rod litz wound MW and LW coils, 94p. KIT NO. 3. Air spaced TC with slow motion drive 8" ferrite rod, with litz wound LW and MW coils, 61 and 10 and 1 coils, £1.10. KIT No. 4

KIT No. 4. Permeability tuner with fast and slow motion drive and LW loading colls, 50p.

13 amp self-fixing into an oblong hole Size approximately 1" . ‡" 9p cach, 10 for 82p.



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Slide Switch, 2-pole changeover panel
mounting by two 6B.A. screws. Size
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8p each, 10 for 78p. Ditto as above but
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Sub Miniature Slide Switch, DPDT 19mm

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10.000 cubic ft. per hour.

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casing with 5,''' fan blades.

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1 pole	44p	44p	44p	44p	44p	44p	44p	44p	44p
2 poles	44p	44p	44p	44p	44p	44 p	44p	77p	77p
3 poles	44p	44p	44p	44p	77p	77p	77p	£1.04	£1 04
4 poles	44p	44 p	44p	77p	77p	77p	77p	£1 32	£1 32
5 poles	44p	44p	77p	77 p	£1.04	£1.04	£1.04	£1.60	£1.60
6 pole-	44p	77p	77p	77p			£1.04		21 87
7 poles	77p	77p	77p		£1.32				£2·15
8 poles	77p	77p	77p		£1.32	£1.32			£2.42
9 poles	77p	77p	£1.04		£1.60	£1.60	£1 60	£2·70	£2.70
10 poles	77p	77p	£1.04	£1.32	£1.60	£1.60	£1.60	£3.00	£3.00
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and announcements to follow
each other. Fully shrouded section wound output transformer

each other. Fully shrouded section wound output transformer to match 3-15 \(\Omega \) speaker and 2 independent volume controls, and separate bass and treble controls are provided giving good lift and cut. Valve line-up 2 EL24s. ECC38. EF86 and E280 rectifier. Simple instruction booklet 15p + SAE (Free with parts). All parts sold separately, ONLY 28-80 P. & P. 55p. Also available ready built and tested £12-10 P. & P. 60p.

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the base current drops the current drawn through the zener does not increase to a dangerous amount. The zener diode that was used was a 400mW one and tests have shown that although the manufacturers recommended working current is 5mA the voltage remains steady with less than 1mA flowing.

The capacitor Cl has been added to ensure that rapid changes in supply voltage, such as from a poorly stabilised supply, do not adversely affect the zener voltage. In the meter circuit it was deemed necessary to add the switch Sl to the original design thus enabling the current to be set before it is allowed to flow through the load, thus eliminating costly mistakes. The power transistor is of the OC28 family, so the maximum collector current is of the order of 1A but if any significant current is likely to be drawn, say above 250mA, a heat-sink will be required.

CIRCUIT LIMITATIONS

The maximum load that can be supplied by this circuit will vary and is dependent on the current drawn and the supply potential. The prototype was designed for a 30 volt supply and thus the maximum load resistance (R) which can be supplied with a load current (I) is given by the following equation R=Vs-Vz+Vbe/I. So for a load current of 100mA the maximum load for the prototype would be approximately 250Ω , for 10mA it would be $2.5k\Omega$ and for 1mA it would be $2.5k\Omega$.

The circuit of Fig. 2 will supply up to 100mA with the minimum current being 0.5mA. If a higher supply voltage is used the designer must ensure that the zener is never overrun and if a higher current is desired the meter circuit and base current circuits must be altered.

The meter circuit needs little explanation. It has been designed to give an accuracy of about 5% and this should be an acceptable error for such a device and needs no alteration. If a meter of a greatly different resistance is used it may be necessary to alter some of the resistor values, but a meter of 100Ω should also give satisfactory results.

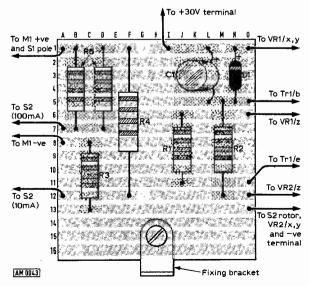
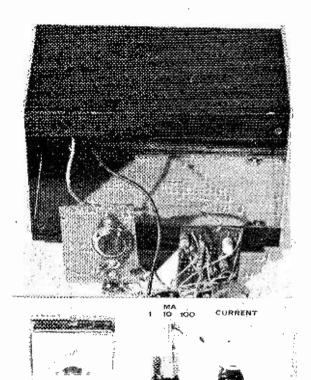


Fig. 3: A small piece of 0·1in. matrix veroboard will take the few components. The board could be omitted and the components wired directly between the panel components.



General construction of the 'Const-Amp' can be seen here.

CONSTRUCTION

The circuit, apart from the output transistor, was built on a small piece of veroboard, shown in Fig. 3, R5 consisting of 2 x 22Ω resistors in parallel to obtain the 11Ω required. The whole instrument was built into a case 6 x 4 x 3^12 in. and was very light and sturdy.

The OC28 transistor was mounted on a piece of s.r.b.p. board. If a heat-sink is fitted ensure that it is electrically isolated from the rest of the circuit.

OPERATIONAL NOTES

Before switching on the device the meter selector switch should be switched to its maximum value of 100mA. Linear potentiometers for VR1 and VR2 give a rapid rise in current towards the end of their travel so log potentiometers may be preferred. R1 may need to be reduced in value because the potentiometers minimum resistance may reduce the maximum obtainable current.

If possible a well regulated DC supply would be preferred but a simple supply as shown in Fig. 4 should suffice and give little ripple on the output current.

APPLICATIONS

Many types of equipment require a constant current supply. One application is the testing of semiconductor devices and the measurement of



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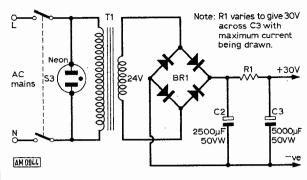


Fig. 4: Suggested circuit for power supply for use with the 'Const-Amp'.

transistor parameters. For example, in the evaluation of zener diodes it is important to use a constant current source. Also, most tunnel diode circuits perform at their best when operated from a source possessing constant current characteristics.

Ordinary diodes can be tested simply by placing them across the output terminals and watching the meter. In one direction the current should flow and in the other there should be very little or no current flow. It can also be used in conjunction with a voltmeter, to measure low values of resistance. A suitable current is chosen and applied to the resistor and the voltage across it is measured. Ohm's Law then provides the resistance value. Finally, it can also be used as a constant current battery charger, within the current limitations, with the advantage that the terminals may be shorted together without damaging the charger circuit.

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Because of problems associated with colour printing, the colour mauve, representing 7 in the colour code on the Datacards, is not as accurate as we would have liked it to be. In poor or artificial light it could be confused with brown (1), so take care! This warning is also applicable to the reading of colour on resistors and capacitors themselves in poor light.

PW for November will contain **Datacards Nos. 3** and 4 having a special appeal to those who need to inter connect audio equipment but can never find the DIN plug and socket information when they want it! Decibels come into the limelight with a simple explanation and a chart that will enable readers to decipher some of the weird terms used in some audio equipment brochures.

Datacards Nos. 5 and 6 will appear in the December issue of P.W. providing one chart for the rapid determination of current, voltage, power and resistance in DC circuits and another chart to assist in obtaining that odd value of resistance that is sometimes required, by connecting two or more resistors in parallel. The same chart can also be used for capacitors in series.

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BCY71	9.20	OA10 0.3		0.15	2N1309	0.27	2N4062	0.12
BCY72	0.15	OA79 0-1		0.12	2N1613	0.20	3N141	0.81
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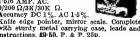
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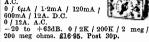
Features A.C. current ranges, 20,000 o.p.v. 0/-5/2-5/10/50/250/500 1000 V. D.C. 0/2-5/10/50/250/500/1000V AC 0/50uA/1/10/100mA/1/10 Amp

0/50uA/1/10/100niA/1/10 Amp D.C. 0/100mA/1/10 Amp AC 0/5K/50K/500K/5 MEG/ 50 MEG. -20 +62db. £15. P. & P. 25p.



KAMODEN 72.200 MULTITESTER

High sensitivity tester. 200,000 o.p.v. Overload protection. Mirror scale. Ranges: 0/-06/-3/3/30/120/600/1200V. D.C. 0/3/12/60/300/11,200V. A.C.



TMK LAB TESTER.

TMK LAB TESTER.

100,000 O.P.V. 6fin.
Scale Buzzer Short Circuit Check. Sensitivity:
100,000 O.P.V. D.C. 5K/
Volt A.C. D.C. Volts:
5, 2-5, 10, 50, 250, 1,000
V. A.C. Volts: 3, 10, 25,
50, 250, 500, 1,000V.
D.C. Current: 10, 100µA,
10, 100, 500mA, 2-5, 10 amp. Resistance:
1K, 10K, 10K, 10KB, 10MBG, 100MBG O.
Decthels: -10 to +49 db. Plastic Case with Carrying Handle. Size: 7jin.×6qin.×
3jin. £18*95. P. & P. 25p.



Model S-100TR MULTIMETER/ TRANSISTOR TESTER

100,000 o.p.v. mirror scale/ overload protection. 0/12/ 6/8/12/80/120/600 V DC. 0/6/30/120/600. V AC. 0/12/ 600µA/ 12/300mA/12 AMP DC. 0/10 K/1 MEG/100MEG. -20 to +50db. 0-01-2 MFD. Transistor tester measures Transistor tester measures Alpha, beta and Ico. Complete with batteries, instructions and leads. £13.50. P/P 25p.



KAMODEN HM.350 TRANSISTOR TESTER

KAMODEN HM. 350 Tr. High quality instrument to test Reverse Leak current and DC current. Amplification factor of NPN, PNP, transistors, diodes, SCR's etc. 4" x!" clear scale meter. Operates from internal batteries. Complete with instructions, leads and carrying handle. £12-50. Post 30p.



MODEL 449A IN CIRCUIT TRAN-SISTOR TESTER

Checks true A.C. beta in / out. Checks Icbo. Checks diodes



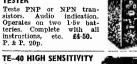
in / out. Checks SCR, etc. Beta H1 10 - 500, L0 2 - 50. Icbo 0-5000µA. 220/240 V A.C. operation £17-50. Post 25p.

LB3 TRANSISTOR TESTER

Tests ICO and B.
PNP | NPN. Operates
from 9v battery. Complete with all instructions, etc. £3.95.
P. & P. 20p.



LB4 TRANSISTOR TESTER



TE-40 HIGH SENSITIVITY A.C. VOLTMETER

10 meg. input 10 ranges: 01/-03/-1/-3/1/3/1/3/0/30/100/)
300V. R.M.S. 4eps.-1-2 Mc/s. Decibels -40 to +50dB. Supplied brand new complete with leads and instructions. Operation 230V. A.C. £17-50. Carr. 25p.



TE-65 VALVE VOLTMETER
28 ranges. D.C. volts
1.5-1,500v. A.C. volts TE-65 VALVE VOLTMETE 28 ranges. D.C. volta 1-5-1,500v. Resistance up to 1,000 megohms. 200/240v. A.C. operation. Complete with probe and instructions. 217-50. P. & P. 30p. Additional probes available: R.F. \$212\frac{1}{4}; H.V. \$2.50.

KAMODEN HM. 720B

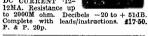
F.E.T. V.O.M. Input impedance 10 meg

ohms.
Ranges:
0 / -25 / 1 / 2-5 / 10 / 50/
250 / 1000V. D.C.
0 / 2-5 / 10 / 50 / 250
1000V. AC.
0 / 2-5 / 10 / 50 / 250
1000V. AC.
0 / 25µA / 2-5 / 25 / 25 / 250
MA D.C.
20 to +62dB
0 / 5K / 50K / 500K / 5meg
600meg ohms.

500meg ohms. £14.95. Post 30p

TMR MODEL 117 F.E.T. ELECTRONIC VOLTMETER

Battery operated, 11 meg input, 26 ranges. Large 4%" mirror scale. Size 5%" × 4%" × 2%". DC VOLTS 0-3-1200V AC VOLTS 3-300V RMS. 8.0-S00V P-P. DC CURRENT ·12-



MODEL L-55 FET V.O.M.

V.U.F.

Input impedance 10 meg ohms. 0 /-3 / 1-2 / 6 / 30 / 120 / 6600 V. D.C. 0 / 3 / 12 / 660 / 120 / 6600 V. D.C. 0 / 3 / 12 / 660 / 120 / 6600 V. D.C. 0 / 1 K / 100 K / 10 meg / 100 meg ohms £15-97. Post 15p.



KAMODEN HMG-500 INSULATION RESISTANCE TESTER Range 0-1000 Meg-oinms, 500 Volt. Battery operated. Wide range clear meter 44" × 4". Complete with deluxe carrying case, batteries, instructions. 219-95. Post 30p



tions. 219-95. Post 30p

MODEL U4311 SUB-STANDARD MULTIRANGE VOLT AMMETER
Renstitivity 330 ohms/Volt
AC and DC. Accuracy
5% D.C. 1% AC. Seale
length 165mm. 0/500/750µA/
1-5 / 3 / 7-5 / 15 / 30 / 75 /
150 / 300 / 750mA / 1-5 / 3 /
7-5 AMP ACO 0 / 5 / 150 /
750mA / 1-5 / 3 / 7-5 / 15 /
30 / 75 / 150 / 300 /
750mA / 1-5 / 3 / 7-5
AMP ACO 0 / 75 / 150 /
300 / 750mV / 1-5 / 3 /
7-6 / 15 / 30 / 75 / 150 / 300 / 750v DC
0/750mV / 1-5 / 3 / 7-5 / 15 / 30 / 75 / 150 / 300 /
//50V AC. Automatic cut out. Supplied complete with test leads, manual and test certificates. \$49-00. Post 50p.

BELCO AF-5A SOLID STATE SINE SQUARE WAVE C.R. OSCILLATOR Sine 18 × 200,000 Hz; Square 18 × 50,000 Hz (10 K ohms) Operation Internal batteries Attractive 2-tone case 7½ × 5″ × 2″. Price \$217-50. Carr. 17½p.

T0-3 PORTABLE OSCILLOSCOPE

3in. tube, Y amp. Sensitivity
0·1v p-p/CM. Bandwidth
1.5 cps-1-5 MHz. Input imp.
2 meg Ω 25pF X amp.
sensitivity 0·9v. p-p/CM.
Bandwidth 1.5 cps-800kHz.
Input imp. 2 meg Ω 20pF.
Time base. 5 ranges 10 cps
300 kHz. Syndronization.
Internal/sexternal. Illuminated scale 140×215×330 mm. Weight 154lb.
220/240v. A.C. Supplied brand new with handbook. £52·50. Carr. 50p.

CI-5 PULSE OSCILLOSCOPE



OSCILLOSCOPE
For display of pulsed and periodic waveforms in electronic circuits. VERT. AMP. Bandwidth 10MHz. Sensitivity at 100KHz. VRMS/mm. 1-25; HOR. AMP. Bandwidth 500KHz. Sensitivity at 100KHz. V RMS/mm. 3-25; Preset triggered sweep 1-3,000usec.; free running 20-200,000Hz in nine ranges. Calibrator pips. 220 × 360 × 430mm. 115-230V. AC. operation, 239-90. Carr. paid. Calibrator pips. 220 × 360 × 430mm. 115-230V. AC operation. £39-00. Carr. paid.

RUSSIAN CI-16 DOUBLE BEAM OSCILLOSCOPE

SEAM OSCILLOSCOPE

5 mc/s Pass Band. Separate
Y1 and Y2 amplifiers.
Rectangular 5 in. × 4 in. 5 in.
C.R.T. Calibrated triggered sweep from 2 u/sec.
to 100 milli-sec. per em.
Free running time base 50 c/s-1 mc/s. Bulltin time base calibrator and amplitude
calibrator. Supplied complete with all
accessories and instruction manual
287. Carr. Paid.



£87. Carr. Paid.

MODEL AT201 DECADE ATTENUATOR

Frequency range 0-200KHz. Attenuator 0-111db, 0-1db step. Impedance 600 ohms. Max. input power 30dbm. Size 180 × 90 × 55mm. 425.0 Page 379. £12.50. Post 37p.



ARF-300 AF/RF SIGNAL GENERATOR

ARF.-300 AF/RF SIGNA
All transistorised, compact, fully portable. AF sine wave 18 Hz to 220 KHz. AF square wave 18 Hz to 100 KHz. Output sine / square 10v. F-P. RF 100 KHz to 200 MHz. Output 1v. maximum. Operation 200/240v. AC. Complete with instructions and leads. £29-95. Fost 50p. Post 50p.



MODEL TE.15 GRID DIP METER

Transistorised. Operates as Grid Dip, Oscultator, Absorp-tion Wave Meter and Oscil-lating Detector. Frequency range 440Kc/s-280Mc/s in 6 coils. 309µA Meter. 9V battery operation. Size 180 × 80 × 40mm. 60 x 40mm. £15.00. Post 20p.



TE-20D RF SIGNAL GENERATOR

TE-20D RF SIGNAL
Accurate wide range signal
generator covering 120
Ke/s 500 Me/s on 6 bands.
Directly calibrated Variable R.F. attenuator, audio
output. Xtal socket for
calibration. 220/240V. A.C.
Brand new with instructions £17.50. Carr. 37p.
Star 140. 2015 × 170. tions £17.50. Carr. 37p. Size 140 × 215 × 170 mm.



TE22 SINE SQUARE WAVE AUDIO GENERATORS

Sine: 20cps to 200 kc/s on 4 bands. Square: 20cps to 30 kc/s. Output impedance 5,000 ohms, 200/250V. A.C. operation. Supplied brand new and 200/200 eration. Su new



brand new and guaranteed with instruction manual leads. £17.50. Carr. 37½p.

AUTO TRANSFORMERS

0/115/250V. Step up or step down. Fully

80 W	£2.35 P. & P. 18p	
150 W	£3.00 P. & P. 18p	
300 W	£4.00 P. & P. 23p	
500 W	£5.80 P. & P. 33p	
1000 W	£8.25 P. & P. 38p	
1500 W	£11.25 P. & P. 43p	
2250 W	£19.00 P. & P. 50p	
5000 W	£40.00 P. & P. £1	

MCA. 220 AUTOMATIC VOLTAGE STABILISER

Input 88 125 VAC or 176, 250VAC. Output 120VAC or 240VAC. 200VA rating. £11.97. Carr. 50p.





HIGH QUALITY CONSTRUCTION KITS ppointed stockists at all brance mplette with comprehensive, easy to follow instructions, and covered by full guarantee Post and packing 15p per kit

AF20	Mono transistor amplifier.	£4.80
AF30	Mono transistor pre-amplifier , , ,	£261
AF310	Mono amplifier (use two for stereo	£5 91
AT5	Automatic light control	£2.58
AT30	Photo cell switching unit	£\$ 70
AT50	400W Triac light dimmer/speed control .	£4.80
AT55	1 300W Triac light dimmer/speed control	£5.70
AT56	2,200W Triac light dimmer/speed control	£6 90
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AT65	Psychedelic light control, 3 channel	£14.55
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HF75	FM transistor receiver	€2.88
HF310		£15 81
HF325		
HF329	Stereo decoder for HF310/HF325	£9 96
HE395	Aerial amplifier for AM/FM bands I, II, III .	£1.77
GP310		£21.27
	Tremola unit for guitars etc	£7 50
NT10		
NT300	Professional stabilized power supply	20.15
161300	2x 30 Voit, 2 2 Amp	£12.51
NITZOE	Transistor converter 12/15V AC/DC to 6V,	
161202	7 5V or 9V DC.	£4 50
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161210	at 3 American	£4.80
NT315	at 2 Amps . Power supply 240V AC to 4.5- 15V DC	14.00
181313	500 m a	€9.57

RP214 REGULATED POWER SUPPLY

Solid state. Variable output 0-24V DC up to 1 amp. Dual scale meter to monitor voltage and current input 220/240V AC.

105mm. 25-97

P. & P. 25-97

P. & P. 25-97



PS.200 REGULATED P.S.U.

Solid state. Variable output 5-20 volt D.C. up to 2 amp. Independent meters to monitor voltage and current. Output 220/240 V. A.C. Size 7'# × 5'# × 3'*.

219-95. P. & P. 25p.



PS.1000B REGULATED POWER SUPPLY

Solid state. Output 6, 9 or 12 volt DC up to 3 amps. Meter to monitor current. Input 220/240v AC. Size 4" × 3½" × 6½". £11.97. P. & P. 25p.

"YAMABISHI" VARIABLE VOLTAGE TRANSFORMERS

Excellent quality at low cost. All models— Input 230V. 50/60 c/s. Variable output 0-260V.



MODEL S-260 GENERAL PURPOSE BENCH MOUNTING

1	\mathbf{Amp}	• •	#7-00
2.5	\mathbf{Amp}		£8.05
5	Amp		£11.75
8	Amp		£15.90
10	Amp		£22.50
12	Amp		£23-60
20	Amp		£49.00
25	Amp		£58-00
40	Amp		£82·50



MODEL S-260B

Panel Mo	untin	g.
1 Amp		£7.00
2.5 Amp		£8-05

Carriage and Packing Extra



POWER RHEOSTATS

High quality ceramic con-struction. Windings emstruction. Windings embedded in vitreous enannel. Heavy duty brush wiper. Continuous rating. Wide range available ex-stock. Single hole fixing. In. dia shafts. Bulk quantities available

25 WATT. 10/25/50/100/250/500/1000 ohms. 95p. P. & P. 10p.

50 WATT. 10/25/50/100/250/500/1000/2500 or 5000 ohms. £1-35. P. & P. 10p.

100 WATT. 1/5/10/25/50/100/250/500/1000 or 2500 ohms. £1.95. P. & P. 15p.

230V/240V SMITHS SYNCHRONOUS GEARED MOTORS

Built in gearbox. All braud new and boxed. 30 RPH CW; 2 RPH CW; 20 RPH CW; 2 RPH ACW; 30 RRH CW;

50p each Post 12p.



SEW CLEAR PLASTIC PANEL METE

USED EXTENSIVELY BY INDUSTRY, GOVT. DEPTS., EDUCATIONAL AUTHORITIES, ETC.

ock—other ranges to order. Quantity discounts available. Send for fully illustrated brochure. Over 200 ranges in stock-

Turns CW 100 100 v 90

I The 3	77.100	IOO X OO HOIL
50µA	£4 15	
500-50µA	£3.95	4
100μΑ	£3.95	
100-0-100µA	£3.90	An /
500μΑ	£8.70	
lmA 20V. D.C	£3.60	
50V. D.C	£3 60	5 amp. D.C. 23
300 V. D.C.	£3.60	300V. A.C #3
amp. D.C.	£3.60	VU Meter £4
-		•

Type SD.830 82.5mm x 110mm Fronts



.. ... £3.10

nr	n x 110mm r	ronts
1	10mA	£8.10
	50mA	£3·10
1	100mA	£3·10
;	500mA	£3·10
i	1 amp	£3·10
÷	ŏ amp	£3·10
i	10 amp	£3·10
1	5V. D.C	£3·10
1	10V. D.C	
1	20V. D.C	£3·10
1	50V. D.C	
1	300V. D.C.	
П	15V. A.C	£3.30

Type SD.640 63.5mm x 85mm Fronts £2.90 50uA £3.05 | 500mA

50-0-50μA	#8.02	1 amp	EZ-90
100μΑ	£3.00	5 amp	£2·90
100-0-100µA	£8·00	10 amp	£2.90
200μΑ	£3.00	5V. D.C	£2.90
500μA	£2-95	20V. D.C	£2.90
1m A	£2.90	50V. D.C.	£2.90
5mA	£2.90	300V. D.C.	£2.90
10mA	£2·90	15V. A.C	#8.00
50mA	£2·90	300V. A.C	£8.00
100mA	£2.90	VU Meter	£3·15

Type SD.460 46mm x 59.5mm Fronts 50μA £2.80 | 1 amp..... £2.60

50-0-50µA	£2 80	5 amp	#2-60
100µA		10 amp	£2:60
100-0-1004A	£2.75	5V. D.C	£2 60
200µA	£2.70	10V. D.C.	£2-60
500µA	£2.55	20V. D.C	£2-60
lmA	£2.60	50V. D.C	£2·60
5mA	£2.60	300V. D.C.	£2·60
10mA	£2.60		
50mA	£2·60	15 V. A.C	£2.70
100mA	£2.60	300V. A.C	£2.70
500m A	42.60	VII Mater	49.00

"SEW" EDGWISE METERS

TYPE PE.70.		32in. X 1 15/3/ deep	un. x
50μΑ	£3·75	, 5 0 0μΑ	£3·20
50-0-50μA 100μA		lmA	£3-20
100-0-100µA		300V. A.C	£3.25
200μΑ	£8.40	VU Meter	£3.85

*MOVING IRON-ALL OTHERS MOVING COIL

Please add postage

Type MR.85P. 41in. x 41in. fronts



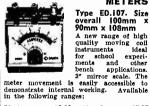
2.4	Į.	0 amp	#2.AA
20.	2000	15 amp	£3.90
L man Talker	210	30 amp	£3.95
46.00		20V. D.C.	£8-90
		50V. D.C.	£3.90
50μA	£4-40	150V. D.C.	£3.90
50-0-50µA	£4.25	300V. D.C.	£3.90
100UA	£4.25	15V. A.C	£3·95
100-0-100µA	£4.05	300V. A.C	£3.95
200μΑ	£4.05	8 Meter 1mA	£3.90
500µA	£3.90	VU Meter	£4.55
500-0-500µA	£3.90	1 amp. A.C.*	£3·90
1mA	£3.90	5 amp A.C.*	£3.90
1-0-1mA	£3.90	10 amp. A.C.*	£3.90
5mA	£3.90	20 amp. A.C.*	£8.90
10mA	£3.90	30 amp. A.C.*	28 90

Type MR.52P, 23in, square fronts

1,50 1111521			
£8.50	10V. D.C \$2.50		
£3.05	20V, D.C \$2.50		
£8.00	50V. D.C #2.50		
£2.95	300V, D.C. 42.50		
£2.65	15 V. A.C \$2.60		
£2.50	300V. A.C \$2.60		
£2.50	8 Meter lmA £2.60		
£2.50	VU Meter 48.60		
£2.50	l amp. A.C. * £2.50		
£2·50	5 amp. A.C. # 22.50		
£2.50	10 amp. A.C. * \$2.50		
£2.50	20 amp. A.C. * \$2.50		
£2·50	30 amp. A.C. * 22.50		
	£3.50 £3.05 £3.05 £2.95 £2.65 £2.50 £2.50 £2.50 £2.50 £2.50 £2.50		

Type MR.65P. 3fin. x 3fin. fronts			
50μA	£3.70 1	10V. D.C 22.60	
	28 15	20V. D.C #2-60	
100μΑ	€8-15	50V. D.C 22-60	
	£3-10	150V. D.C. #2.60	
200μΑ	£3.05	300V. D.C. 42.60	
	£2.76	15V. A.C 22.80	
500-0-500µA	£2 60	50V. A.C 42-80	
1mA	£2·60	150V. A.C 42.80	
Бт А	£2.60	300V. A.C #2.80	
10mA	£2.60	500V. A.C. 42.80	
50mA	£2:60	8 Meter ImA 22.85	
100mA	£2·60	VU Meter \$8.70	
500mA	£2.60	50mA A.C. * #2.60	
1 amp	£2·60	100mA A.C. * #2:60	
5 amp	£2.60	200mA A.C. * £2.60	
	£2.60	500mA A.C. * \$2.60	
15 amp	£2·60	1 amp. A.C. * \$2.60	
	£2.60	5 amp. A.C. * \$2.60	
	#2·80	10 amp. A.C. * #2.60	
	£2.90	20 amp. A.C. * £2.60	
5V. D.C	£2-80	30 amp. A.C. * \$2.60	

"SEW" EDUCATIONAL METERS



50μA	£6.90	20V. d.c £5.9
100μΑ	£6·40	50V. d.c £5.9
	£6-40	300 V. d.c £5.9
1mA	£5.95	
1-0-1mA	£5-95	Dual range
1A d.c	£5-95	500mA/5A d.c. £7.0
5A d.e	£5.95	5V/50V d.c. 27.0
10V d.c		

1. Type MR.38P. I 21/32in. square fronts 200mA £2.25 300mA £2.25

£2.55 £2.50 £2.45 £2.40 £2.25 £2.25 £2.25



50µA 50-0-50µ.A

100μA ... 100-0-100μA 200μA ... 500μA ... 500-0-500μA

1mA 1-0-1mA ..

1-0-1m 2mA 5mA 10mA 20mA 50mA 100mA

1	500mA	£2.25
i	750mA	£2·25
ľ	1 amp	£2.25
	2 amp	£2.25
1	5 amp	£2.25
1	10 amp	£2.25
ı	3V. D.C	£2.25
ı	10V. D.C	£2.25
ì	15V. D.C	£2.25
1	20V. D.C	£2·25
- [50V. D.C	£2.25
ì	100V. D.C.	£2.25
ı	150V. D.C.	£2.25
-	300V. D.C.	£2.25
-	500V. D.C.	£2·25
1	750V. D.C.	£2.25
-1	15 V. A.C	£2·30
H	50V. A.C	£2:30
-	150V. A.C	£2·30
١	300V. A.C	£2·30
-	500V. A.C	£2·30
-	S Meter ImA	£2.80
- 1	VU Meter	£2.65

£2 40 £2 40 £2 40 £2 40

MR.45P. 2in. square fronts

Type Fig. 43F. Aill. Square itoit			
50μA	£2.70	5 amp	
50-0-50µA	£2-65	10V. D.C	
100μΑ	£2·60	20V. D.C	
100-0-100µA	£2·50	50V. D.C	
200μΑ	£2.50	300 V. D.C.	
500µA	£2·45	15V. A.C	
500-0-500µA	£2.40	300V. A.C	
ImA	£2·40	8 Meter 1mA	
5mA	£2-40	VU Meter	
10mA	£2.40	l amp. A.C. *	
50mA	£2-40	5 amp. A.C. *	
100mA	\$2.40	10 amp. A.C. *	
500mA	£2·40	20 amp. A.C.	
1 amp	£2-40	30 amp. A.C. *	

"SEW" BAKELITE PANEL METERS

Type MR.65, 31in, square fronts



Б ЦА	£4·60
0 <u>i</u>	£8.55
0-0-50 ₄ A	£3-05
00μA	£3.00
00-0-100µA	£3.00
Au00	£2.70
00-0-500μA	£2-60
mA	£2.60
-0~lmA	£2.80
m.A	£2 60
0m.A	£2.60
0mA	£2-60
00mA	£2-60
00mA	£2-60

1. square fronts
1 amp. 22:80
5 amp. 22:80
15 amp. 22:80
10 amp. 22:80
30 amp. 22:80
50 amp. 22:80
60 Amp. 22:80
10 V. D.C. 22:80
50 V. D.C. 22:80
50 V. D.C. 22:80
50 V. D.C. 22:80 30 amp. 50 amp. 50 amp. 50 amp. 50 amp. 50 amp. 50 mp. 60 300 V. A.C. * 22-65 500mA A.C. * 22-65 500mA A.C. * 22-60 5 amp. A.C. * 22-80 10 amp. A.C. * 22-80 20 amp. A.C. * 22-80 30 amp. A.C. * 22-80 50 amp. A.C. * 23-80 VU Meter . . . 33-65

Type S-80 80 mm. square fronts

50µA
50-0-50µA
100μΑ΄
100-0-100µA
500µA
lm'A
20V. D.C
50V. D.C
300V. D.C.
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£3.00 £3.00 £3.70 300V. A.C. VU Meter

HAND HELD 2-WAY WALKIE **TALKIES**

Battery operation. Volume and squelch controls. Call button and press to talk button. Telescopic aerial. Complete carrying

100mW £24.95 Pair. Post 50p.

2 channel £52.50 Pair. Post 50p. 3 channel £71.25 Pair. Post 50p.

Licence required for operation in U.K.

240° Wide Angle ImA Meters



MW 1-6 60mm square MW 1-8 80mm square £3.97 £4.97 P. & P. extra

230 VOLT A.C. 50 CYCLES RELAYS

Brand new. 5 sets of changeover contacts at 5 amp rating. 40p each. P. & P. 10p (100 lots £30) Quantities available.

SEND SAE FOR NEW 8 PAGE LIST SEMI CONDUCTORS & VALVES

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4 Bands covering 550 kc/s-30 m c/s B.F.O. Built-in Speaker 220/240 v. A.C. Brand new with instructions. Our £15.75 Carr.

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Bands covering 550 kc/s-30 mc/s. ET, S Meter. Variable BFO for SB. Built-in Speaker, Band-SSB. Built-in Speaker, Bar spread, Sensitivity Control. 22 240 v. A.C. or 12 v. D.C. 122 in. 42 in. × 7 in. Brand new wiinstructions.

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SKYWOOD CX203 RECEIVER



Solid state, 5 bands covering 200-420 KHz and -55 to 30 MHz. Illuminated slide rule dial. Bandspread. Aertal tuning. BFO, AVC, ANL, "St" meter, AM/CW/SS B. Integrated speaker and phone socket. 220/240 v. A.C. or 12 v. D.C. Size 325 x 266 x 150 mm. Complete with instructions and circuit. circuit.

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LAFAYETTE HA-600 RECEIVER



General coverage 150-400 kc/s, 550 kc/s-30 mc/s, FET front end, 2 mech. filters, product detector, variable B.F.O. noise limiter, 8 Meter Bandspread. RF Gain. 15in. × 9\frac{2}{3}in. × 8\frac{2}{3}in. 18 lb. 220/240 v. A.C. or 12 v. D.C. Brand new with instructions.

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TRIO 9R59DS RECEIVER



bands covering 550 kc/s to 30 mc/s continuous and electrical bandspread on 10, 15, 20, 40 and 80 metres. 8 valve plus 7 diode circuit. 4/8 ohm output and phone jack. SBs-CW, AML, Variable BFO. 8 meter. Sep. bandspread dial. IF frequency 445 kc/s, audio output 1-5w. Variable RP and AF gain controls 115/250 v. A.C. Size: 7in. × 13in. × 10in. with instruction manual.

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Model 350. 13" × 8" with single tweeter/ crossover. 20-20,000 Hz. 15 watt RMS. Available 8 or 15

Hz. 15 watt RMS.
Available 8 or 15
chms. 27.25 each.
P. & P. 37p.
Model 450, 13" × 8"
with twin tweeter/
crossover. 55-13,000
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Available 8 or 15
chms. \$28.62 each.
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Matched pair of stereo bookshelf speakers. Deluxe teak veneeredfinish. Size 14½" × 9" × 7½". 8 ohms. 8 watt RMS.

16 watt peak. Complete with DIN

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All silicon transistor

transistor amplifier operates from magnetic, ceramic or tuner inputs with twin stereo headphone outputs and separate volume controls for each channel. Operates from 9v battery. Inputs 5MU/100MU. Output 50MW.

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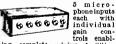
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STATION

Our £2.25 P. & P.

MP7 MIXER PREAMPLIFIER



5 micro

ing complete mixing facilities.

Battery operated. 9½" × 5" × 3".

Inputs Mics: 3×3mV 50K; 2×
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Self contained, transistorised, battery operated. Simply plug in microphone,

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wainut cabinet. 7½ × 3 × 4½in. with headphone/ speaker selector. 4-32 ohms. 2015p 24,000 Hz. 21

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RANGE OF HIGH QUALITY EQUIPMENT Audiotronic Products are manufactured exclusively for the Audiotronic Group of Companies and as a member of the group we are pleased to ofter you this fabulous range of high quality equipment. Made to our own specifications each item provides outstanding performance and reliability at a value for money price!

ACD.660 Stereo Cassette | AUDIOTRONIC DOLBY 'B' Deck

A beautifully

A beautifully styled 4 track stereo deck with an outstanding specification offered at a remarkably low price. Incorporates a host of features including switchable noise filter normal/chrome tape selector, twin VU meter, slider record/playback level controls, front panel headphone socket, recording indicator lamp, phono/Din line input sockets, 3.5mm mike input sockets etc. etc. Frequency response sected, 3.5min make input sockets, etc. etc. Frequency response 100-8KHz Cr023 [100-12KHz Cr02] S/N-45dB. Crosstalk 45dB. Separation-25dB. Noise limiter-6dB at 10KHz. Complete with phono connecting leads.

connecting OUR £39.50 Carr. & PRICE £39.50p

AHP-8D 8 Track Stereo Tape Deck

Can be used with most hi fi amplifiers.

amplifiers.
Push button
track selector
and illuminated track
indicators. Attractive cabinet with
black and silver trim. Output level
750mV. AC 220/240v.

UUR #11.95 P. & P. 50p.

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Incorporates built in amplifiers giving 2\(\frac{1}{2} + 2\) watts rms output. Push button track selector, illuminated track indicators, slider controls for volume, balance and tone. Attractive cabinet with black and silver trim. Output impedance 8 ohms. AC 220/240v. OUR 217-25 P. & P. 50p. PRICE \$17-25

Stereo Headphones

LSH.20 Individual volume controls Stereo mono switch. 8 ohms, 40-19,000 Hz. 23:50 P & P 30p

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LSH.40 Two way speaker system.
Individual volume controls. 8 ohms.
20-20,000 Hz.
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NOISE REDUCTION UNITS Reduce tape hiss by 3dB at 600Hz, 6dB at 1200Hz and 10bB for all frequencies above 3000Hz.
Size 16 % × 8" × 3" AC 200/250v



FRUGESS FOUR
For use with semi-professional tape recorders. Freq. res. 30Hz-20KHz ± 2dB. S/N better than 70dB. Full source tape monitoring. Record/Replay metering. Switchable multiplex filter. Supplied with test tape.

Our £50.00 P&P

PROCESS TWO

PROCESS TWO
For use with cassette and tape
recorders. Freq. res. 30Hz-20KHz
± 2dB. Off tape monitoring,
switchable multiplex filter. Two
Dolby calibration meters. S/N
better than 70dB.
Supplied with test cassette or tape
as required.

Our £34.50 P&P

ACR.14 Battery Mains Cassette Recorder

Portable twin track mono recorder with automatic recording level control. Built in speaker. Earpiece socket. Input

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Fast forward and rewind.
Output 500mW. AC 220/240v or 6v DC operation. Complete with remote control microphone, mains lead, earpiece and batteries.
OUR PRICE £10.50 P. & P. 50p.

MR-900 GLOBA AM/FM PORTABLE RADIO



10 wavebands covering AM: 535-1605 kHz,

AM: 5331605 kHz,
LW: 150380 kHz,
MB 1-6400 MHz,
SW1: 4-08 MHz,
SW1: 4-0108 MHz,
PSB1: 30-50 MHz,
PSB2: 148-174 MHz, FM 88108 MHz, AIR: 108-136 MHz.
Features time zone map and timing dial. Large clear scale.
Telescopic aerial and built in aerial. AFC or FM. 6" × 4"
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Battery/mains operation. Size: 345 × 133 × 305mm.
OUR
PRICE £36-00 P. & P. 50p.

AR.1000 SPORTSMAN AM/FM PORTABLE RADIO 5 wavebands covering

AM 535 1065KHz. FM 88-108MHz. AIR 108-135MHz. 174MHz. WB 162



WB 102.

SMHz. Large horizontal slide dial with logging scale. Slider volume and squelch controls. 7 section telescopic aerial for FM and built refresher to the first and built in ferrite bar for AM. AFC. 3in. speaker. Earpiece socket. Green leatherette covered cabinet with metal side panels. Size 152 × 79 × 219mm. Battery/mains operation. OUR EII.50 P. & .P 35p.

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covering MW 535-1605KHz and FM 88-175MHz. All transistor transistor.
Battery or
mains operation. Built in
aerial and 8
section telescopic aeria!

complete with batteries, shoulder strap and earpiece.

OUR
PRICE

COMPLETE CONTROL CHEST
LOW NOISE TAPE CASSETTES TOP HI-Fi quality in library cases TYPE 5 10 25 060 21:29 22:53 25:99 090 21:85 23:62 23:59 0120 22:29 24:48 210:63

Cassette Tape Head Cleaner 80p

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Manual tuning of Medium and Handai tuning of Medium and Long waves. 12v pos. or neg, earth. Complete with speaker. mounting brackets and instruc-

Price £6.50 P&P



12v neg. earth. Slider controls for Volume, Tone and Balance. Channel selector button with red pilot lamp, with speakers, mounting brackets and instructions.

Our P&P

£12.50 Price

ACRI PUSHBUTTON CAR RADIO



Push button tuning of one LW and five MW stations of your and five MW stations of your choice. 12v pos. or neg. earth. Complete with speaker, mounting brackets and instructions.

£8.95 P&P Our Price 50p





50p

5 section. Fully automatic. 12v DC. Extends to approx. 40". Complete with switch, all leads and

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TO 33%% OR

SUPER AKAI HIFI BARGAINS



RECONDER

For conventional or Chromium Dioxide
tape, 4 track record/playback, Volume and
tone controls. Frequency response 4016kHz (using Cr02 tape),
distortion better than 2%, wow
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Rec. Price £96:10. £56.50 P.&P. OUR PRICE

CS35D STEREO DECK

4 track record/playback deck. Accepts chrome/regular tape cassettes.

Rec. Price £68-30

GWS PRICE £44-45

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SUPER HEADPHONE BARGAINS!

Our

Our

Price

Price

SH628 STEREO HEADPHONES



Outstanding value. Soft ear-pads, adjustable headband. 8-16 ohms, 20-20,000 Hz. Com-

plete with lead and stereo plug. Our

£1.87 P. & P. Price 30p

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Lightweight headphones with padded earpieces. 4-16 ohms. 4-16 onno. 20-20,000 Hz. Complete with

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Our £1.95 30n

SPECIAL PURCHASE! BSR 8 TRACK PLAYER CHASSIS

Famous BSR 8 track chassis as used in Model TDSS complete with silver and black exentcheon ready to fit into cabinet. Output 125mV. AC 240v. Overall size approx. 185 × 215 × 80mm.

OUR 28.95 P. & P. 50p.



TEI018 DE-LUXE MONO HIGH IMPEDANCE HEADSET

headset with soft earpads. Impedance 2,690 ohms (d.c. 600 ohms), Fre-quency response 200-4,000 Hz.

BH.001 HEAD SET AND BOOM MICROPHONE

£2.25 P. & P.

Moving Coil. Ideal for language teaching, com-munications. Headphone imp.

16 ohms. Micro

phone imp. 200

30p

£4.95 P. & P.

Sensitive magnetic headset with

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Complete units with Stereo cart-ridge ready wired in plinth cover.

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Station £2-97, P. & P. 15p. Station £5-25, P. & P. 15p. Station £6-62, P. & P. 17p.

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Carriage and Packing 50p

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	G99			
	G101P/C		• •	
	GL69/2	• •		٠.
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£22.50 £22.50 £15.75 £25.45 £33.75

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4 speed autochanger unit fitted with stereo ceramic cartridge. Our Carr. Price_

SP25 III **GP 104**

SP25 MK.II. 4 speed single player fitted with Acos stereo ceramic cartirdge. Carr.

Our £8.50 Price

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as in 'W.W.' June '73

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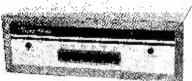
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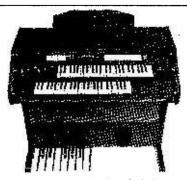
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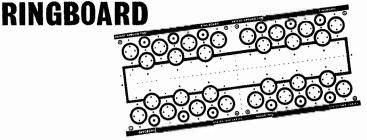
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BA3	4"	×	4"	×	11"	41p
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1	1020 For model G240 3/32"
1	1021 For model G240 1/8"
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AL10/AL20/AL30 **AUDIO AMPLIFIER MODULES**



The ALl0, AL20 and AL30 units are similar in their appearance and in their general specification. However, careful selection of the plastic power devices has resulted in a range of output powers from 3 to 10 watts R.M.S. The versatility of their design makes them ideal for use in record players, tape recorders, stereo amplifiers and cassette and cartridge tape players in the car and at home.

Parameter	Conditions	Performance
HARMONIC DISTORTION	Po = 3 WATTS f=1KHz	0.25%
LOAD IMPEDANCE	_	8 – 16 Ω
INPUT IMPEDANCE	f=1KHz	100 kΩ
FREQUENCY RESPONSE Œ 3dB	Po=2 WATTS	50 Hz - 25KH
SENSITIVITY for RATED O/P	Vs=25V. Rl=8Ω f=1KHz	75mV. RMS
DIMENSIONS	_	3" × 21" × 1"

The above table relates to the AL10, AL20 and AL30 modules. The following table outlines the differences in their working conditions.

Parameter	AL10	AL20	AL30
Maximum Supply Voltage	25	30	30
Power output for 2% T.H.D. (RL = $8\Omega f = 1 \text{ KHz}$)	3 watts RMS Min.	5 watts RMS Min.	10 watts RMS Min.

AUDIO AMPLIFIER MODULES

AL 10. 3 watts AL 20. 5 watts AL 30. 10 watts

POWER SUPPLIES

PS 12. (Use with AL10 & AL20) SPM 80. (Use with also AL30 & AL50) 88p FRONT PANELS PA 12 with Knobs

PRE-AMPLIFIERS

PA 12. (Use with AL10 & AL20) £4.85 PA 100. (Use with AL30 & AL50) £13.15

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T461 (Use with AL10) 51-38 P & P 15p T538 (Use with AL20) 51-93 P & P 15p BMT80 (Use with AL30 & AL50) £2-15 P & P 25p

PA 12. PRE-AMPLIFIER SPECIFICATION

The PA 12 pre-amplifier has been designed to match into most budget stereo systems. It is compatible with the AL 10, AL 20 and AL 30 audio power amplifiers and it Bass control can be subplied from their associated power supplies. There are two stereo inputs, one has been designed for use with "Ceramic cartridges while the auxiliary input will suit most 'Magnetic cartridges. Full details are given in the specification table. The four controls are, from left to right: Volume and on/off switch, balance, bass and treble. Size 152mm x 84mm x 35mm.

Bass control—

± 12dB at 60Hz
Treble control—

± 14dB at 14KHz
*Input 1. Impedance
1 Meg. ohm
Sensitivity 300mV
†Input 2. Impedance
30 K ohms
Sensitivity 4mV

Sensitivity 4mV

EA1000 AUDIO AMP MODULE 3 WATTS R.M.S.



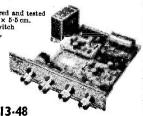
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SPECIAL OFFER £2 each while stores last

The STEREO 20

The 'Stereo 20' amplifier is mounted, ready wired and tested on a one-piece chassis measuring 20 cm × 14 cm × 5·5 cm. This compact unit comes complete with on/off switch volume control, balance, bass and treble controls, Transformer, Power supply and Power amps. Attractively printed front panel and matching control knobs. The 'Stereo 20' has been designed to fit into most turntable plinths without interfering with the mechanism or, alternatively. Into a separate cabinet. Output power 20w peak. Input 1 (Cer.) 300mV into 13A. Freq. res. 25Hh-25kHz. Input 2 (Aux.) 4mV into 30K. Harmonic distortion. Bass control ±12dB at 50Hz typically 0:25% at 1 watt. Treble con.



50W pk 25w (RMS)

0·1% DISTORTION! HI-FI AUDIO AMPLIFIER

THE AL50

- ★ Frequency Response 15Hz to 100.000-1dB.
- * Load-3, 4, 8 or 16 ohms
- ★ Distortion-better than ·1% at 1 KHz.
- * Signal to noise ratio 80dB.

- ★ Supply voltage 10-35 Volts.
- ★ Overall size 63mm 105mm × 13mm.

Tailor made to the most stringent specifications using top quality components and incorporating the latest solid state circultry and ALSO was conceived to fill the need for all your A.F. amplification needs.

FULLY BUILT—TESTED—GUARANTEED.

STABILISED POWER **MODULE SPM80**

AP80 is especially designed to power 2 of the AL50 Amplifiers, up to 15 wait (r.m.s.) per channel simultaneously. This module embodies the latest components and circuit techniques incorporating complete short circuit protection. With the addition of the Mains Transform M 180, the unit will provide outputs of up to 1:5 amps at 36 volts. Size: 63mm × 105mm × 30mm. These units enable you to build Audio Systems of the highest quality at a hitherte unothainable price. Also ideal for many other applications including:—Disco Systems, Public Address, Intercom Units, etc. Handbook available 10p PRICE £3.25

TRANSFORMER BMT80 £2.15 p. & p. 28p.

STEREO PRE-AMPLIFIER TYPE PA100

Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon planar translators, two of these are specially selected low noise NPM devices for use in the input stages.

Three switched stereo inputs, and rumble and scratch filters are features of the FA100, which also has a STEREO/MONO switch, volume, balance and continuously variable bass and treble controls.



SPECIFICATION Frequency Response
Harmonic Distortion
Inputs: 1. Tape Head
2. Radio, Tuner
3. Magnetic P.U.

Bass Control
Treble Control
Filters: Rumble (High Pass)
Scratch (Low Pass)
Signal/Noise Ratio
Input overload nput overload Supply

 $\begin{array}{l} 20 \mathrm{Hz} - 20 \mathrm{KHz} \pm 1 \mathrm{dB} \\ \mathrm{better\ than\ 0.1\%} \\ \mathrm{1.25\ mV\ into\ 50 K\ \Omega} \\ \mathrm{35\ mV\ into\ 50 K \cdot \Omega} \end{array}$

2. Radio, Tuner
35 mV into 50KΩ
All input voltages are for an output of 250mV. Tape and P.U. inputs equalised to BIAA curve within ± 1dB. from 20Hz to 20KHz.

Bass Control
Treble Control
Filters: Rumble (High Pass)
Signal/Noise Ratio
Dignal/Noise Ratio
Eight Signal/Noise Eight Signal/Noise Eight Signal/Noise Eight Signal/Noise Eight Eight Signal/Noise Eight Ei + 26dB + 35 volts at 20mA

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with Co-Axial Tweeter 2.7
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64" 8 ohm. 10 watt 2.6
8" 8 ohm. 10 watt 3.9
12" 8 ohm. 20 watt 5.7
8" x 5" C/Mag. 5 watt 1.4
Twin Tweeter
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FANE 7" × 4" 3 or 8 ohm 1.15	GOLDRING G800
8" Dualcone 8 ohm 2-50	G850
CELESTION 8" 15 ohm 1.75	STYLI For Above Cartric
IDASTIDA 10" 8 or 15 ohm	Sapphire
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24" 8 ohm of 64 ohm 60	CM70 Planet stick metal,
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WHARFEDALE SPEAKERS ALSO	DM160 Dynamic uni dir
AVAILABLE.	metal UD130 50K/600 ohm, u
KIT FORM CABINETS -TEAK	UD130 50K/600 ohm, u
$12 \times 12 \times 6$ with 8", 8" \times 5",	ball metal
or 61" and 31" cutout 2-75	TW206
17 × 10 × 6 with 8" or 13" × 8"	CONDENSER MIKE 600
	uni-dir
eutout	Cassette STICK MIKE w.
out for EMI 350 4-60	Control on/off switch (
WEETER & CROSSOVER	3.5 mm J/Ply)
EMI 31" 3 or 8 ohm C/Mag. 1-10	MIKE MIXERS Mono
Cone Tweeter 8 or 15 ohm, 10 watt 2:00	Mono/stereo
Cone Tweeter 8 ohm. 3 watt 1.10	Lapel type, crystal
Horn Tweeter 8 ohm, 20 watt 5.60	CASSETTES Type Low Pin- Phil-
Dome Tweeter 8 ohm, 30 watt 4.00	Type Low Pin- Phil- noise nacle lips
Crossovers CN23 (3 phm), CN28	noise nacie lips
(8 ohm), CN216 (16 ohm) . 1·10	C45 — — —
CARTRIDGES	C60 85p 40p 50p C90 45p 55p 69p
ACOS GP91/2SC or GP91/3SC	C90 45p 55p 69p
Stereo comp 1.05	C120 55p 75p 105p
GP93/1 Stereo crys 1.35 GP94/1 Stereo crys 1.75	Cassette Head Cleaner
GP94/1 Stereo crys. 1.75	BIB Stereo Test Cassette
GP95/1 1.35	AMPEX Head Cleaner
GP96/1 1.75	magnetiser
GP104	PLASTIC LIBRARY C
SONOTONE	for 5" Reels 20p. 52" Re
9THAC Stereo ceramic, diam. 1.80	7" Reels 80p.
9THAC/G Slim fit, stereo cer.	CASSETTE CASES
diam 1.80	
19-TI Stereo crystal 85	5" 55p 65p
BSR SCom Stereo ceramic 2.25	51" 65p 751
	n// ME- 81.00
SX5H Stereo crystal . 1 65 SX5M Stereo crystal . 1 65	AKAI TAPE DECK
X5H Mono/stereo . 1.30	4000DS Tana
X5H Mono/stereo 1.30 X5M Mono/stereo 1.30	4000DS Tape GXC40D Cassette
Aom mono/stereo 1.00	GACIOD Gassette

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Sapr	hire				.80
D. I	hire Diamon	đ			1.25
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unj-e	e STIC	TT 36 T	77 md	41 D	7.80
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Lonel					
	type, c	rystai		• •	43
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Type	Low	Pm-	Phil-	mein-	Am.
045	noise	nacie	nps	orex	pex 45p
C45	054	40		oup	4op
C60	app	4UP	Sup	oop	Sob
C90	35p 45p 55p	oop	08b	700	75p
C120	aap	70p	Toob	TIOD	TIUP
Cassett	tereo 1	1 Clear	ier		-45
RIBS	tereo 1	est Ca	ssette	~'.	1.65
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mag	netiser				1.65
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CASSE	TTE	CABES			12p
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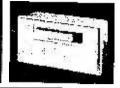
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	33μF 68μF 150μF	6½p 6½p 6½p	25 VC	LT		
	470µF	lip	10μF	6 <u></u> 4p		
	680μF	I3p	22μF	6 3 p		
ı	1500µF	18p	47μF	6∯p		
1	2200μF 3300μF	18p 26p	100μF 150μF	8p 8p	63 VC	NI T
١	3300 pa	ZOP	220μF	10p	IμF	6 ^½ p
1			470µF	13p	2 · 2 μF	$6\frac{2}{2}p$
İ			680μF	20p	4 · 7µF	6-∮p
I	10 AO	LT.	1000μF	22p	6 ⋅ 8μF	6-∮P
1	22 μF	6 ∮ P	2200µF	39p	10μF	6½p
ı	47μF 100μF	6 <u>1</u> p 612p	5000μF	68p	22μF 68μF	6 <u>∓</u> p 10p
١	220μF	8p			100μF	Пр
ł	330µF	10p			150µF	130
1	470µF	IOp	40 VO	LT	220µF	19p
1	1000µF	HP	6 · 8µF	6-5p	330µF	ZZDI
1	1500µF	20p	15μF	6 ½ p	470μF	26p
1	2200μF	24p	33 <i>μ</i> F	6½p	1000μF	44p
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200	37p	60p	£1.98p	£2.31p
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Sinclair Project 60

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Z.50 Mk.2 SPECIFICATIONS

Input impedance 100 KΩ Input (for 30w into 8Ω) 400mV Signal to noise ratio, referred to full o/p at 30v HT 80dB or better Distortion 0.02% up to 20W at 8Ω. See published curve Frequency response 10Hz to more than 200 KHz - 1dB Max. supply voltage 45v (4Ω to 8Ω speakers) (50v 15Ω speakers only)

Min. supply voltage 9v

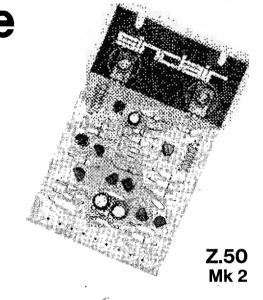
Load impedance - minimum: 4Ω at

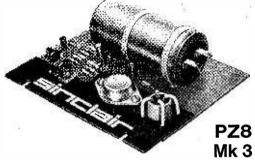
Load impedance - maximum: safe on open circuit £5.48 + V.A.T.

PZ.8 Mk.3 SPECIFICATIONS Nominal working output 45V. Adjustable between 20 & 50V

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Mains Transformer £5.98 - V A.T. 59p





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PZ.6 35 volt, stabilised (Not suitable for Super

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Typical Project 60 applications

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Mains powered record player	Z.50, PZ.5	Crystal or ceramic P.U. volume control etc.	£10.46 + V A.T. £1 04	
12W. RMS continuous sine wave stereo amp. for average needs	2 x Z.50, Stereo 60; PZ.5	Crystal, ceramic or mag. P.U., F.M. Tuner, etc.	£25.92 + VAT £2.59	
25W. RMS continuous string wave stereo amp using low efficiency (high performance) speakers	2 x Z.50, Stereo 60; PZ.6	High quality ceramic or magnetic P.U., F.M Tuner, Tape Deck, etc.	£28.92 + V.A.T. £2,89	
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms)	2 x Z.50 Mk.2, Stereo 60 ; PZ.8 Mk.3 transformer	As above	£34.90 + V.A.T. £3.49	
Indoor P.A.	Z.50 Mk.2, PZ.8 Mk.3 transformer	Mic., guitar, speakers, etc., controls	£19.44 + V A T. £1.94	



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SPECIFICATIONS

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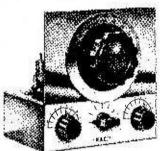
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5Z4G 0.45 6/30L2 0.90	6CG7 0.65	68A7 0.45 68G7 0.45	12E1 3.00 12K5 1.00	30PL13 1.10	6360 1.25 6939 3.00	EBC81 0.83	ECL80 0.55 ECL81 0.55		0.40	PCF806 0.75 PCF808 0.90	QQV03-1			0.65
6AB4 0.45	6CL6 0.65	68K7 0.50	12K7GT0.50	30PL14 1.10	7199 1.00	EBF80 0.40	ECL82 0.35		0.40	PCH200 0.70			UF85	0.40
6AB5 1.00	6CU6 0.80	68L7GT0.48	12Q7GT0.45	35A3 0.65	7586 2.50	EBF83 0.40	ECL83 0.70		0.55	PCL81 0.50				0.40
6AF4A 0.65	6CW4 1.00	68N7GT0.48	128R7 0.50	35A5 0.75	7895 1.50	EBF89 0.32	ECL84 0.55		0.40	PCL82 0.35				0.65
6AG5 0.25	6CY5 0.50	68Q7 0.50	20D1 0.60	35B5 0.65	A2293 2:50	EBL31 1.50	ECL85 0.55		0.43	PCL83 0.65				0.48
6AG7 0.45	6CY7 0.75	6SR7 0.50	20L1 1.10	35C5 0.60	AZ1 0.60	EC53 0.50	ECL86 0.40		0.48	PCL84 0.45				0.80
6AH6 0.60	6D3 0.55	6T8 0.38	20P1 0.50	35D5 0.75	AZ31 0.55	EC80 2.65	ECLL800	EZ40	0.50	PCL86 0.45	U31 0.	70 1	UYIN	0.50
6AJ8 0.30	6DC6 0.85	6U4GT 0.75	20P4 1.10	35L6GT 0.75	CBL1 0.99	EC86 0.60	8-20		0.75	PCL88 1.10				0.48
6AK5 0.40	6DK6 0.60	6U8A 0.48	20P5 1.20	35W4 0.50	CBL31 1.20	EC88 0.80	EF37A 1.00		0.28	PCL200 0.75				0.50
6AK6 0.60	6DQ6B 0.80	6V6GT 0.50	25C5 0.70	35Z3 0.75	CY1 0.50	EC90 0.35	EF40 0.55		0.29					
6AL3 0.43	6DS4 1.35	6X4 0.40	25L6GT 0.60	35Z4G 0.40	CY31 0.50	EC92 0.45	EF41 0.65		4.00	PCL800 1.10				0.40
6AL5 0.25	6EA8 0.70	6X5GT 0.45	25Z4G 0.40	35Z5GT 0.75	DAF96 0.50	EC93 0.65	EF42 0.70		0.70	PCL801 0.95			W729	0.75
6AM6 0.37	6EH7 0.30	6X8 0.70	25Z6GT0.75	50A5 1.00	DF96 0.50	ECC40 0.70	EF80 0.25	GZ30	0.45	PCL805 0.50	U201 0	.50	XC12	0.60
6AQ5 0.45	6EJ7 0.35	6Y6G 0.80	30A5 0.60	50B5 0.85	DK92 0.70	ECC81 0.40	EF85 0.35	GZ31	0.50	PD500 1.30	U281 0	.55	Z759	4.00
6AQ6 0.70	6EW6 0.70	7Y4 0.75	30AE3 0.40	50C5 0.60 50CD6G1.20	DK96 0.60	ECC82 0.33	EF86 0.30		0.50	PF86 0.70	U282 0			4.50
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6AS5 0.55	00.00	100/2 0.00	, 50015 1.00	OPA 0.00	. DILIU 0.00	. 250004 0.00	. TOT 31 U.3/	ILADUS	00.00	1 TTL200 0.60	0403 0	.70 ()	Z803U	1.35

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			٠.	BD124	0.60
2N696		28746.	0.25	BD131	0.40
2N697	0.15	AC113	0.15 0.30	BD132	0.50
2N698 2N705	0.80 0.70	AC125 AC126	0.20	BF115	0.20
2N705	0.10	AC127	0.17	BF167	0.25
2N708	0.15	AC128	0.15	BF173 BF179	0.28
2N753	0.25	AC132	0.95	BF180	0.80 0.85
2N929	0.20	AC153	0.30	BF181	0.85
2N980	0.20	AC154	0.15	BF185	0.20
2N987	0.45	AC157	0.17	BF194	0.10
2N1131 2N1132	0.25 0.25	AC176 AC187	0.25	BF195	0.10
2N1184	1.25	AC188	0.20	BF196	0.11
2N1302	0.17	ACY17	0.35	BF197 BF200	0.12
2N1303	0.15	ACY18	0.20	BFW87	0.25
2N1304	0.20	ACY19	0.25	BFW88	0.20
2N1805	0.20	ACY20	0.20	BFW89	0.20
2N1806 2N1807	0.27	ACY21 ACY22	0.20 0.10	BFW91	0.20
2N1308	0.25	AD139	0.40	BFX88 BFY17	0.20
2N1309	0.30	AD149	0.40	BFY19	0.40
2N1613	0.30 0.17	AD161	0.35	BFY50	0.20
2N1711	0.20	AD162	0.85	BFY51	0.20
2N1756	0.75	ADZ11	1.25	BFY52	0.20
2N2147	0.75	ADZ12 AF114	1.25 0.17	BSY26	0.17
2N2160 2N2217	1.00 0.25	AF114 AF115	0.17	BSY27	0.20
2N2218	0.20	AF116	0.17	BSY28 BSY65	0.17
2N2369A	0.15	AF117	0.17	BSY95A	0.20
2N2477	0.85	AF118	0.25	OC16	1.00
2N2646	0.40	AF180	0.50	OC22	0.50
2N2905	0.82	AF181	0.50	OC23	0.60
2N2923 2N2924	0.12	AF186 AFZ12	0.40 1.00	OC24	0.60
2N2926	0.18 0.10	ASY26	0.25	OC25	0.85
2N3053	0.20	ASY27	0.80	OC26 OC29	0.25
2N3054	0.50	ASY28	0.25	OC35	0.50
2N3055	0.60	ASY29	0.80	OC36	0.65
2N3133	0.25	ASY54	0.25	OC42	0.30
2N3134	0.25	ASZ15 ASZ16	0.80 0.80	OC44	0.15
2N3391 2N3392	0.17 0.17	ASZ17	0.80	OC45	0.12
2N3393	0.15	ASZ18	0.80	OC70 OC71	0.10
2N3394	0.15	BC107	0.10	OC72	0.12
2N3395	0.20	BC108	0.10	OC73	0.30
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2N3404 2N3414	0.82	BC118	0.20	OC78	0.25
2N3415	0.15	BC134	0.20	OC78D OC81	0.20
2N3417	0.25	BC147	0.10	OC81D	0.20
2 N3646	0.36	BC149	0.11	OC83	0.20
2N3702	0.10	BC152	0.19	OC139	0.80
2N3703	0.10	BC158	0.11	OC141	
2N3704 2N3705	0.12	BC175	0.20		0.60
2N3705 2N3706	0.10 0.10	BC186	0.25	OC170	0.25
2N3707	0.12			OC171	0.30
2N3709	0.10	BCY30	0.85	OC200	0.30
2N3710	0.10	BCY31	0.45	OC201	0.60
2N3711	0.10	BCY33	0.35	OC202	0.65
2N3819	0.25	BCY34	0.35	OC203	0.40
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