

# Lenry <br> BUILD THE <br> * FREE TEAK CABINET with com- <br> FEATURES. New slim design with 6-IC's, IC Sockets, 10 silicon transistors, 4 rectifiers, 2 zeners. Special Gardeners low field slim line transforme HIO glass PC panel. Complete chassis work <br> HIGH QUALITY \& STABILITY ARE PREDOMINATE FEATURES RELEVELOPED BY TEXAS ENGINEERS FOR PERFORMANCE kelibility and ease of construction. <br> FACILITIES. On/off switch indicator, headphone socket. rumbla filters, bass, volume and balance controts, scratch and Radio Tuner, Aux. Can be altered for Mic., Tape, Tape-head, etc (Parts list Ref. 20 on request) Constructional details Ref. No. 21 30p <br> sutchl £28:50 <br> P \& P 45p <br> COMPLETE WITH FREE TEAK CABINET <br> Designer approved kits distributed by Henrys! within 200 yards - call and see for vourself. <br> YOUR COMPLETE AUDIO-ELECTRONIC STORES <br> everything at the right price, All vour electronic requirements <br> 20 + 20 WATT INTEGRATED I.C. STEREO AMPLIFIER <br>  <br> P.W. Tricolour as per April/May une 1973. Parts list on request (52A). <br> DESIGN ${ }^{\star}$ SUITM SILVER TRIM <br> $4 t^{\prime \prime} \times 6^{\prime \prime} \times 2^{\prime \prime}$ size 

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 E.MP. Size $13 t^{x} \times 8$ 8." Large Cer
TYPE 150 watt. 3,8 or 15
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tweeters and crossover ${ }^{2}$ or 15 ohms. $3-50$. Post 25 p . YPE 35020 watt with eweeter and crossover, $B$ and 15 ohms $£ 750$ : Post 28 p
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Cl. 5 . 35 p
3" Pulse $\begin{array}{ll}\text { Cl.5 } & \text { 3" Pulse Scope } 10 \mathrm{~Hz}-10 \mathrm{mHz} £ 39.00 \text { Carr. } 50 \mathrm{p} \\ \text { TE65 } & \text { Valve Voltmeter } 28 \text {. }\end{array}$ ALL NOMBREX MODEL5 ${ }^{2}$ iN STOCK

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## ASSISTANT EDITOR

Lionel E. Howes, G3AYA
ART EDITOR
Peter Metalli

## TECHNICAL EDITOR

Eric Dowdeswell, G4AR

## PRODUCTION \& NEWS <br> EDITOR <br> Colin R. Riches

## SECRETARIAL

Jenny Maunder
Jill Alflatt
Telephone 01-634 4292

## ADVT. MANAGER

Roy Smith
Telephone 01-634 4293
CLASSIFIED ADVTS.
Colin R. Brown
Telephone 01-634 4301

## SUBSCRIPTIONS

Subscription Rates for one year to any part of the world $£ 2.65$ including Dostage. Enquirles to Subscription Department, IPC Magazines Ltd., Carlton House, 68 Gt. Queen Street, London, WC2 5DD. Phone 01-242 4477 Binders ( $\mathbf{~} 1 \cdot 10$ ) and Indexes (11p) can be supplied by the Binders Dept at the same address.

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Published by IPC Magazines Ltd., Fleetway House, Farringdon Street, London EC4A 4AD. Telephone: 01-634 4444.

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FANE 'MODE ONE' HIGH FIDELITY SPEAKER KIT
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1ndividual Ganged Controls: Bass, Treble, Volume and Balance. Printed circuit construction employing 10 Transistors plus Diodes. Output rating I.H.F.M. Frequency range 20-20,000c.p.s. Bass Control $\pm 12 \mathrm{db}$. Treble Control $\pm 13 \mathrm{db}$. Selector switch for P.U. or Tape/Radio. For loudspeaker output impedances of 3 to 15 ohms. For Attractive Black and Silver finished metal Attractive Black and Silver finished metal COMPLETE KIT OF PARTS INCLUDIMG FULLY WIRED PRINTED CIRCUT AND COMPREHENGIVE WIRING DIAGRAMA \& INATRUCTIONS 42.65 Cart. Or lllustrated 810.50 or dep. 22 and 9 monthly payments


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> Heary construction. Lateat high efficiency ceramic magnetu. Plasticised cone surround. D , jadicates Tweeter Cone providing $\begin{aligned} & \text { ertemied irequency range up to } \\ & 8-16 \text { ohms. PLEASE } 8 T A T E ~ C H O I C E . ~\end{aligned}$

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\begin{aligned}
& \begin{array}{llllllll}
\text { HF808T } & 0^{\circ} & 10 W & 88.30 & \text { HF128 } & 12^{*} & 15 W & 88.35 \\
\text { HF102D } & 10^{\circ} & 15 W & 84.95 & \text { HF12BD } & 12^{*} & 15 W & 88.85
\end{array}
\end{aligned}
$$

FANE 807T HIGH FIDELITY SPEAKER A full range 8in. 10 watt unit for excellent mound quality, in oultable enclosure. Cast chasala Roll P.V.C. cone nurzound and long throw voice cone is fitted to ertend blgh note response. Frequency range 25 Hz to 15 KHz Gauas 10,000. Impedance 3 or 8 - $16 \Omega$.
PLEASE STATE IMPEDANCE WHEN ORDERING $\mathbf{~} 3.70$ $£ 4.95$
$\xrightarrow{\text { Repenene } 25} \mathbf{H z}$ H to 15 KHz Hz
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DORCHEDRisto. Credit terms ivailable. DORCHESTER (Illustrated) Size $16 \times 11 \times 9 \mathrm{in}$. sppr. Iange $45-15,000$
c.p.b. Ratiag $8-10$ watts. Fitted High Gux $13 \times 8 \times 8 \mathrm{a}$. $\mathbf{~ C 9 . 4 5}$ Carr. 40 p .
Dual Cone speaker. Imp. 3 or 15 ohms. Dual Cone speaker. 1 mp .3 or 15 ohms. Rating 10 Fatt Mighy lierible P.Y.C. cone surround, long throw voice coil and 10.000 apener fitb High dux pressure iweeter. Handinme design cablat. Range $35-20,000 \mathrm{c}, \mathrm{p}$. Imp 8 ohms, Gives anooth realistic sound output.
Soe 'package offora' for illantration.
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HI-FI SPEAKER ENCLOSURES MODERN DESIGN

## Teak reneer aniab. Acoustically liner. sizes approx. Carr. 35p. per ene

JE8 Size $16^{\prime \prime} \times 11^{\prime \prime} \times 9^{\prime \prime} . \quad$ SE8 For optimum performPressurised. Gives pleasing ance with any 8 in.


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## R.S.C. TA6 6 Watt HI-FI AMPLIFIER

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 H £6.50 SE12 $9 \times 104 \times 9$ in. performance with 12 in $\mathrm{Hi}-\mathrm{Fi}$ speaker and tweeter ${ }_{25 t}^{\text {Sizt }} \times 16 \times$ 9in. $\quad \mathbf{E 7 . 9 5}$
necomary.

MIDQET CLAMPED TYPE $2 ; \times 2 \| \times 2 \downarrow \mathrm{in}$. 200 F, , $60 \mathrm{~mA}, 6 \cdot 3 \mathrm{~F} .2 \mathrm{a}$
$250-0-250 \mathrm{~F} .60 \mathrm{uA}$
6.3 v

FULLY SHROUDED UPRIGHT MOUNTING $250-0-250 \mathrm{v} .60 \mathrm{~mA}, 6 \cdot 3 \mathrm{y}$. La., 0.5-6.3v. La. $250-0 \cdot 250 \mathrm{~F} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{~s} .3 \mathrm{a}$. $£ 2.45$ $300 \cdot 0-300 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{~F} .4 \mathrm{a} ., 0-5-6-3 \mathrm{v} .3 \mathrm{a} .22 \cdot 45$ $300 \cdot 0 \cdot 300 \mathrm{v}$. $130 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}$. 4 a . c.t., $6 \cdot 3 \mathrm{v}$. 1a.
For Mullard 810 Amplifer ........... 22.95
 $350-0.350 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, 0 \cdot 5 \cdot 6.3 \mathrm{v} .3 \mathrm{~g} .28 .95$
$425-0-425 \mathrm{v}, 200 \mathrm{~mA}, 6.3 \mathrm{v}$. $4 \mathrm{R} .$, c.t., 5 v .3 a .25 .45 $425 \cdot 0-425 \mathrm{r} .200 \mathrm{~mA}, 6 \cdot 3 \mathrm{r} .4 \mathrm{a}, 63 \mathrm{v}$. 38., 5 v .

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R.S.C. STEREO FM III TUNER in cabinet
Visually matches
Super 30 Mk. III
$\mathbf{2 7} \mathbf{5 0}$

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 $250-0.250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{~F} .2 \mathrm{~m}, 6.3 \mathrm{z}$. 1 A. $350-0-350 \mathrm{~s}$. 80 mA , 6.3 s . $2 \mathrm{am}, 0-5-6.3 \mathrm{~F}$.
 $3000.300 .100 \mathrm{~mA}, 6.3 \mathrm{r} .4 \mathrm{a} ., 0-6-6.3 \mathrm{~F} .3 \mathrm{~L}$
 Sultable for Mullard 810 Amplifer.
 $350-0-350 \mathrm{r}$. $150 \mathrm{mAA}, 6 \cdot 3 \mathrm{z}$. 4 A ., 0-5-6-3v. 3a. 22.85 FLLAMEITS or TRANSIBTOR POWER PACK



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Push-Pull Ulra Linear for Mullard 510 , etc. $\mathbf{~} 2.45$ Push-Pull $15-18$ watts, sectionally wound 6 L 6 , KT66, etc., for 3 or $15 \Omega$
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(a) 100 W POWER AMPLIFIER (a) 100 W POWER AMPLIFIER b) PAR ONES
(c) MATCHING DYNAMIC 'MIKE' (attached to h'phone) (d) PAIR 50 WATT SPEAKERS Black Rexine covered Cabinets Size approx (e) $18^{\prime \prime} \times 18^{\prime \prime} \times 8^{\prime \prime}$ (bS TDI DISCO CONSOLE (a) (b) (c) (d) $\&$ (e) f 145

Ferms Deposit $£ 30$ and 18 monthly payments of $£ 8.00$ (Total $£ 17400$ ).

Iocorporating twin Garrard SPRS Mr.M1 turatablee and Sonotone or acol Cartriages with dismond stylii. separate Vol. contror ror ogch arnable. Ano MONITORING Pachimies, plat Troble and Bas Controlr. separate input lor 'mike Vynide covered Gebtnat with lid ree illuatration
Or Dep. 810 and 9 mithly pymts 8.
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R.S.C. COLUMN SPEAKERS IDEAL FOR VOCALISTS All types 15 ohme corered in Perlne end Vrnair TYPE C4I00 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN TYPE CI 32 30-40 WATTS Filtell two TYPE C813 50 WATTS Low feellach
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## $40+1$ <br> 

R.S.C. AIO 30 WATT ULTRA LINEAR HI-FI AMPLIFIER Highls senditive. Puah-Puil blah E9dB $30-20,000$ c/a. All high grade componeatu. Valven EFys
 mitroln. Seniltivity 36 millilvolts. For High Impedance miserothone, etc. For Electronlo Organ, Qultar, Btring Ban, otc. Uranl
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Designed for use with a pair of Player Units and Amplifier with Bass and Treble Controls. Incorporates MONITORING Gram (1) Gram (1)
$16 \xi^{\prime \prime} \times 3^{\prime \prime} \times 4^{\prime \prime}$ deep. Brush Silver finished fascia. Fully enclosed but can be mounted In cabinet

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FULL RANGE AVAILABLE AT ALL BRANCHES
FAL PHASE 50 Mk.III AMPLIFIER 50 WATT soltd atate. \& Maparately controlled linpute Plua tnater vol

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RSC PHANTOM " 50 '






FANE ULTRAHIGH POWER LOUDSPEAKERS

$\left(\begin{array}{l}\left.()^{2}\right)\end{array}\right.$
 $8^{\prime \prime} 100$ Watt $15^{\prime \prime} 60$ Watt $12^{\prime \prime} 50$ Watt 14,000 gauss 13,000 gauss 81150 is
$\pm 14.75$
Dep. 18.80 anl 9 munthly pariments. $\$ 1.50$ (Total $\$ 18.80$ ) Ihep 22 and monthly pay: (Total 218.87 ) PAIR BUTTABLR
FANE SPEAKERS 'POP' 25/2 12 in. 25 WATT Dual Cone $15 \Omega$ (for uses other than Bass Guitar or
f7. 95 or Dep. ©l.28 and Electronic Organ). Carr. Tree

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Or depontt $\mathrm{I} 4-60$ arid 0 monthly payth, of 84.27 .
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Dep $88: 80$

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| Type Pr | Price p | Type | Price p | Tupe r | Price $p$ | Type | Price $p$ | ${ }_{\text {Type }} \mathrm{Pr}$ | Prire $p$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }_{\text {a }}$ | ${ }_{22}$ | AD161 | ${ }_{37}$ | HC145 | 50 | BD1338 |  | B） 18.2 | 4 |
| AC113 | 22 | AD162 | 37 | BC147 | 11 | BD135 | 44 | 13F183 | 44 |
| ACl 15 | 26 | AD181 | ＊ | BCl48 | 11 | BD136 | 54 | $\mathrm{BF}^{\mathrm{B}} 18 \mathrm{l}$ | 33 |
| AC117K | 22 | AD162 | （\＄P） | BCl 49 | 13 | B 1131 B D138 | 50 | $\mathrm{BF}^{\text {Br }} 188$ | 44 |
| AC122 | 13 |  | 81 | BC150 | 20 | BDi39 | 61 | BF194 | 13 |
| $\mathrm{ACl}^{2} 5$ | 19 | ADT140 | － 55 | BCIS | 22 | BDI40 | 68 | BF195 | 13 |
| ACl26 | 19 | AF114 | 27 | ${ }^{13 \mathrm{Cl5}}{ }^{2}$ | 19 | PD155 | 88 | B19198 | 16 |
| AC127 | 19 | AFl15 | 27 | 8C153 | 31 | BDIF | 66 | BF197 | 18 |
| AC128 | 18 | AF116 | 27 | $\mathrm{BCl}^{84}$ | 38 | BD 176 | 68 | 13－200 | 50 |
| ACl32 | 18 | AF117 | 27 | $\mathrm{BCI}^{57}$ | 13 | BD17\％ | 72 | $13 \mathrm{~F}^{2} 222$ | 1.05 |
| AC134 | 18 | AF118 | 39 | BC158 | 13 | BD178 | 72 | B10257 | 50 |
| AC137 | 18 | AF124 | 38 | $\mathrm{BC159}^{\text {BC160 }}$ | 13 | Blolf | 77 | Bros8 | 68 |
| AClil | 18 | AF125 | 28 | ${ }^{\text {BC1 }}$ B60 | 55 | BD180 | 77 | BF259 | 94 |
| AClilk | 19 | AF126 | 31 | ${ }_{\text {BC1F }}$ | 13 | BDI8G | 72 | 13F262 | 61 |
| ACl42 | 16 | AF127 | 31 | BC167 $\mathrm{BC1} 88$ | 13 | BDIRG | 72 | BF963 | 61 |
| ACl42K | K 19 | AF139 | 33 | BC188 | 13 | B1）${ }^{\text {B }}$ | 77 | BF270 | 39 |
| ACl51 | 17 | AF178 | 33 | ${ }^{\text {BCl }} 69$ | 13 | BD188 | 77 | BP971 | 33 |
| AC154 | 22 | AF179 | 55 |  | 16 | HD189 | 83 | 13F272 | 88 |
| AC155 | 22 | AF180 | 55 | $\underset{\mathrm{BCl}}{\mathrm{BC1}} \mathbf{}$ | 16 | 13 D190 | 83 | B $\mathrm{P}^{2} 73$ | 38 |
| AC156 | 22 | AF181 | 50 | ${ }^{\mathrm{BC}} \mathrm{Cl} 172$ | 16 | 13D194 | 94 | B +274 | 39 |
| AC157 | 27 | AF186 | 50 41 | ${ }^{\text {BCl7 }}$ | 16 | BDI9ti | 94 | BFW 10 | 68 |
| AC165 | 22 | AF239 | 72 | BClis | 24 | ［1719\％ | 99 | Bド 29 | 30 |
| AClfi6 | 22 | A Li02 | 72 | RCli7 | 21 | BD1994 | 99 | B19884 | 24 |
| AC167 | 22 | AL103 | 28 | RClif | 21 | B1）194 | 1.05 | BFX85 | 33 |
| ACl68 | 27 | ABY26 | 28 | 8 Cl 179 | 21 | BDEOH | 1.05 | BFX 86 | 24 |
| AC169 | 16 | ASY27 | 28 | $1 \mathrm{CC180}$ | 27 | BD20． | 88 | BFX87 | 27 |
| AC178 | 22 | ABY28 | 28 | 13 C 181 | 27 | BD205 | 88 | BFK88 | 24 |
| AC177 | 27 | ASY－9 | 28 | BC182 | 11 | 13D207 | 1.05 | BFY50 | 22 |
| AC178 | 31 | A8Y60 |  | BC1R2L | － 11 | B Dens | 1.05 | BFY「51 | 22 |
| AC179 | 31 | ASY51 | 28 | ${ }^{\text {BC183 }}$ | 11 | BDY：0 | 110 | BYY52 | 22 |
| AC180 | 19 | ASY5 2 | 28 | ${ }_{\text {BC183L }}$ | － 11 | B1115 | 27 | BFY53 | 19 |
| AC180K | K 22 | ABY04 | 28 | ${ }_{\text {BC1 }}{ }^{\text {RC1 }}$ | － 13 | B171\％ | 50 | BPX25 | 94 |
| ACIRI | 19 | ASY゙55 | 28 | BCIR4L | ＋ 13 | BFIIf； | 77 | 13SX19 | 17 |
| ACl81K | K 22 | ASY56 | 28 | BC186 | － 31 | BF115 | 77 | 48x 30 | 17 |
| AC187 | 24 | ASY57 | 28 | 13 Cl BC 187 | 31 | BFI： | 50 | B8Y－25 | 17 |
| AC187K | K 22 | ASY58 | 28 | $\mathrm{BC}_{2} \mathrm{OO}^{7}$ | 12 | Bパロ | 55 | nSY゙3n | 17 |
| AC188 | 24 | AsZ21 | 44 | $\mathrm{BC}^{\mathrm{BC}} 08$ | 12 | $\mathrm{BFl}_{25}$ | 50 | BSY－27 | 17 |
| AC188K | K 22 | RC107 | 10 | RC209 | 13 | B61辰 | 55 | 13SY28 | 17 |
| ACY17 | 28 | BC108 | 10 | ${ }_{\mathrm{BC} 212 \mathrm{~L}}$ | － 12 |  | 61 | BSY：29 | 7 |
| ACY18 | 22 22 | BCl <br> BC 109 <br> 13 | 11 | $\mathrm{BC}_{\mathrm{BC} 213 \mathrm{~L}}$ | L 12 | BFF5\％ | 50 | B8Y38 | 20 |
| ACY＇0 | 22 | BC114 | 17 | RC214L | L 16 | BF154 | 50 | B8Y39 | 20 31 |
| ACY21 | 22 | BC115 | 17 | BC225 | 28 | BFl5s | 58 | BSY41 |  |
| ACY29 | 18 | BC115 | 17 | BC 226 | 37 | BF157 | 61 | BS495 |  |
| ACY27 | 20 | BC117 | 17 | BCY30 | 27 | BF158 | 81 | 138Y90． |  |
| ACY 28 | 81 | BC118 | 11 | BCY31 | 28 | BF15 | 68 | 181105 |  |
| ACY29 | － 39 | BC119 | 33 | BCY32 | 38 | BFILG4 | 44 | Cl11E |  |
| ACY 30 | － 21 | BCl20 | 88 | BCY33 | 88 | BF102 | 44 | C400 | 31 |
| ACY31 | 131 | BC125 | 13 | BCY 34 | 28 | BF19：3 | 44 | C 407 | 28 |
| ACY34 | 423 | BC126 | 20 | BCF70 | 16 | BFIPA | 44 | C 424 |  |
| ACY 35 | 5 23 | BC132 | 13 | BC： 71 | 16 | BF16．a | 44 | C425 |  |
| ACH36 | 31 | PCl3 4 | 20 | BCY72 | 16 |  | 24 | C426 | 3 |
| ACY40 | － 19 | RC135 | 13 | BC710 | 22 28 | BFF173 | 24 | （428 |  |
| ACY41 | 120 | BC136 | 17 | BCZ11 | － $\begin{array}{r}28 \\ 28 \\ \hline\end{array}$ | ${ }_{13 \mathrm{~F} 175}$ | － 39 | C441 |  |
| ACY44 | 439 | ${ }^{\text {BC1 }} 137$ | 17 | BCX121 | 28 <br> 68 | Briva | － 39 | C443 |  |
| AD130 | 42 | RC139 | 44 | BD123 | ${ }_{72}^{68}$ | BF17\％ | 33 | C444 |  |
| AD140 | － 53 | BC140 | 33 | RD124 | 88 | BF｜79 | －33 | C450 |  |
| AD142 | $2 \quad 53$ | ${ }_{\text {BCl }} \mathrm{BCl42}$ | － $\begin{aligned} & 33 \\ & 33\end{aligned}$ | RD124 RD 131 | 85 | BF189 | －33 | MAT100 |  |
| AD143 | － 58 | $\mathrm{BCH}^{\mathrm{BCL}}$ | － 33 | BD132 | 88 | 3F181 | － 33 | 3ATl01 |  |


| Typer Pr |  |
| :---: | :---: |
|  |  |
|  | NAT191 |
|  | MPP102 |
|  | M $\mathrm{T}^{2} \mathrm{~F}^{104}$ |
|  | 31P105 |
|  | OC19 |
|  | OC 20 |
|  | OC22 |
|  | 0 C 23 |
|  | 0 OC 4 |
|  | 0 C 25 |
|  | OC26 |
|  | OC28 |
|  | OC29 |
|  | OC35 |
|  | OC3 ${ }^{\text {a }}$ |
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|  | 0075 |
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|  | OC8， |
|  | $0 \mathrm{OR4}$ |
|  | OC139 |
|  | 0 C 140 |
|  | 0 Cl 169 |
|  | OC170 |
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|  | P397 |
|  | ST140 |
|  | $8 \mathrm{Tl41}$ |
|  | TIA43 |
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|  | 26301 |
|  | 2G302 |
|  | 2G303 |
|  | 2G304 |
|  | 2G306 |


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| PIV 300 mA | 750 mA | 1 A | 1.5A | 3A | 10A | 30.4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 50004 | 0.06 | $0 \cdot 06$ | $0 \cdot 08$ | $0 \cdot 16$ | $0 \cdot 23$ |  |
| 1000.04 | 0.07 | $0 \cdot 06$ | 0.15 | 0.18 | 0.26 | 0.83 |
| 2000.06 | $0 \cdot 10$ | 0.07 | 0 -18 | 0.22 | 0.27 | $1 \cdot 10$ |
| 400007 | 0.15 | 0.08 | $0 \cdot 22$ | $0 \cdot 30$ | 0.41 | 1 |
| 6000.08 | 0.18 | $0 \cdot 11$ | 0.26 | 0.38 | $0 \cdot 50$ | 05 |
| $8000 \cdot 11$ | 0. 19 | $0 \cdot 12$ | $0 \cdot 28$ | 0.41 |  | 2-20 |
| 1000 0-12 | 0.28 | 0.16 | $0 \cdot 33$ | 0.51 |  |  |
| 1200 | $0 \cdot 37$ |  | $0 \cdot 42$ | $0 \cdot 63$ | 0. 83 |  |


| triacs |  |  |  |
| :---: | :---: | :---: | :---: |
| VBOM 24 |  | 6 A | 10 A |
| TO-5 TO-66 TO-48 |  |  |  |
|  | \&p | £p | £p |
| 100 | 83 | 55 | 83 |
| 200 | 55 | 68 | 89 |
| 400 | 77 | 82 | 1.21 |
| DIACs |  |  |  |
| FOR USE WITH |  |  |  |
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P.E Organ Metal TO-18 Eqvt. ZTX $3005 \not 5 \mathrm{p}$ each Any Qty

|  | 3 mma ${ }^{30}$ |
| :---: | :---: |
| GP 100 TOS METAL |  |
|  | Furll Tested 1,000 8.90 |
| Vebo $=80 \mathrm{~V}$. Vceo $=80 \mathrm{~V}$. | İteal for Organ Rul |
| 1.C. $=10$ amps. Ptot $=$30 w . hee $-30-170$. |  |
| Replaces the majority of |  |
| Germanium power tran. | SILICON HIGH |
|  | voltage |
| and NK'T range. | Yebo $=2505, \quad$ Vceo $=$ 100 v . I.C. $=6$ amps. Ptot-30W. hife $=$ typ. 20 |
| $25100+$ |  |
| $48 \quad 0.44 \quad 0.40$ |  |
|  |  |
|  |  |
|  |  |  |
|  |  |  |
| I.C. $=15$ amps. Ptot $=$ |  |
| 19Hz. Suitable replace. | $2 N 3000$ |
| ment for 2 N 3055 , |  |
| BDY 11 or BDY 20. | 115 Watt sil |
| 25 | POWER NPN |
| 0. 51 | 55D EACH |

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## Pak No.

Deacription
U 1120 Glass Sub-Min. General Purpose Germanium Dlodes U 260 Mixea Gerinanium Trangistors AF/RF
quality tested semiconductors

| Pak No. |  |
| :---: | :---: |
| Q1 20 Red spot transistors PYP |  |
| Q2 16 | 16 White fpot A.F. transist ors PNP |
| ${ }_{6} 6$ |  |
| Q6 5 OC 72 |  |
|  |  |
| ${ }^{4}$ AC 126 transis |  |
| $\mathrm{Qq}_{\mathrm{Ql} 10} 7 \mathrm{OC} 71$ |  |
|  |  |
| Q10 700 Cl typ |  |
|  | ${ }^{3}$ AF 116 type transib |
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|  | colours |
| Q16 2 GET880 |  |
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| +120 |  |
| Q19 3 M M |  |
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| (en ${ }^{\text {a }}$ |  |
| Q23 10 OA |  |
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| O. |  |
| $\left\lvert\, \begin{array}{ll} \mathrm{Q} 27 & 2 \\ \mathrm{Q} 28 & 2 \\ \mathrm{Q} 29 \end{array}\right.$ | 210 A Piv silicon rectifers 1842 |
|  | 2 2 ${ }^{\text {silcon power rectifif }}$ |
|  | 48 |
| $\left\lvert\, \begin{aligned} & \text { Q29 } \\ & \text { Q30 } \end{aligned}\right.$ | 7 Pllicon switch transistors |
|  | ${ }_{8}$ Sillcon sultch |
|  | $\stackrel{\text { NPN }}{ }$ |
| Q32 | 3 PNP Gllicon tr |
|  | 3 ¢14icon NPN |
|  | 7 Sllicon NPN |
|  | s00M |
|  | ${ }^{3}$ S ${ }_{1} 11 \times$ |
|  | 2 N 3846 TO-18 |
|  | 2n305 |
|  |  |

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hfe $=t 5 \mathrm{p} .100 \mathrm{fT}=3 \mathrm{MHz} \quad$ B1P $19 / 20 \mathrm{Me}$ hfe $=$ typ. $100 \mathrm{fT}=3 \mathrm{MHz} \quad$ B1P $19 / 20 \mathrm{Matched}$ Pair $\begin{array}{cccccc}1 & 25 & 100+ & 1 & 25 & 100+ \\ 0.371 & 0.35 & 0.32 & 0.68 & 0.61 & 0.55\end{array}$

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Msnufacturera "Fall Onte" which include Functional and Part-Functional Unite. These are classed as 'out-of-spec' from the maker's very rigld specifications, but are ideal for learning about I.C's and experimental work

Pak No. Contenta Price PakNo. Contenta Price Pak No. Contenta Price \begin{tabular}{ll|ll}
$\mathrm{U1C00}=12 \times 7400$ \& 0.55 \& UIC46 $=5 \times 7446$ \& 0.55 <br>
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UIC07 $=8 \times 7407$ \& 0.55 \& UIC54 $=12 \times 7454$ \& 0.55 <br>
U1C60 $=12 \times 7460$ \& 0.55 <br>
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$\mathrm{UIC1}$ \& $=12 \times 7410$ \& 0.55 \& $\mathrm{UIC70}=8 \times 7470$ <br>
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\hline 7413 \& 0.55 \& UIC7 $=8 \times 7472$ \& 0.55
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5 mv hito 5
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| $\mathrm{ACl07}$ | 16 p | BCl 38 | 36 p | BF 460 | 29 p | OC44 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| AC 126 | 14 p | $\mathrm{HCl42}$ | 33 p | BF 329 | 18 p | OC 45 |



 ACl 42 K 22 p BCl45 26 p ACl41K 20p | $\mathrm{ACl76}$ | 15 p | BC148 | 9p | RFX86 | 22p | OC83 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathrm{ACH87}$ | 13 p | BC149 | 日p | BFX87 | 280 | OC84 |

 \begin{tabular}{ll|l}
AC 187 A \& 20 p \& $\mathrm{BC153}$ <br>
AC 188 \& 13 p \& BC 154

 

AC188 \& 13 D \& $\mathrm{BCl54}$ <br>
AC188K \& 20 p \& RC157 <br>
ACY17 \& 24 \& <br>
\hline
\end{tabular} ACY

 $\begin{array}{cc:c}A C Y 19 & 25 \mathrm{D} & \text { BC167 } \\ \text { ACY } & 22 \mathrm{~B} & \mathrm{BC1} 68\end{array}$

 | ACY2 | 23p | BC169 | 11p | C407 | 22p | TIP35A |
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$A D 15$
AD1f
AD16
AD
A

## $A \mathrm{~A}$ A A

## AF AF AF

## $A F$ $A F$ $A F$

## AF1

A A 2
AL1

ALl \begin{tabular}{ll|l}
\& <br>
ASY27 \& 31 p \& BD123 <br>
BD130

 

AU103 \& 99 p \& BD130 <br>
BD131
\end{tabular}

## ${ }_{\mathrm{BCl}}^{\mathrm{BCl}}$



| $13 C 109$ | $9 p$ | BD142 | 50 p | OC19 |
| :--- | :--- | :--- | :--- | :--- |
| $\mathrm{BCl13}$ | 151 p | BF159 | 33 p | OC20 |

 \begin{tabular}{ll|ll|l}
BCl 25 \& 16 p \& BF177 \& 28 p \& OC25 <br>
BCl 26 \& 25 p \& BF178 \& 29 p \& OC28

 

$\mathrm{BCl26}$ \& 25 p \& BF178 \& 29 p \& OC28 <br>
BCl 22 \& 16 p \& $\mathrm{HF179}$ \& 35 p \& OC29

 

BCl 34 \& 16 p \& BF 194 \& 15 p \& OC 35

 

BC135 \& 16 p \& BF195 \& 17 p \& OCA
\end{tabular} $\begin{array}{lllll}\text { BC137 } & 18 \mathrm{p} & \text { BF244 } & 27 \mathrm{p} & \text { OC41 }\end{array}$

| 14 p |
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$B$ and W D5 (pair)
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Ditton 15
Ditton 25
Ditton 25
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Ditton 66
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SOLARVOX TKigs iwin speaker
20 watts Teak (pair)
TL 25 Teak (palt) Teak (pair)
TL 50 Teak
THORPE GRENVILLE TGiOO (Dair) TG200 (palr)
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(palr)
Linton Mark il (pair)
Triton III (pair)
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Unit 3 speaker htt (pair)
Unit 4 speaker kit (pair)
5 speaker kit (pal
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Audlom 10P
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$A^{2}$T some time or other, in hire purchase agreements, forms of guarantee, or simple purchases, most people encounter a moment of uncertainty and often wonder if the forms are really worth the paper they are printed on. What are the buyer's rights under signed guarantees or the Supply of Goods Act?
To go some way to tidying up the situation the "Supply of Goods (Implied Terms) Act 1973"' has been introduced. The purpose is to make it a criminal offence to use misleading or invalid guarantees or exclusion clauses in any contract or guarantee, including hire purchase, credit sales and cash sales. Goods must compulsorily correspond with their descriptions, whether in advertisements or on the package, be of merchantable quality and "fit for the purpose intended". The phrase in quotes is often a disputable factor and does not sufficiently define how it is to be applied to technical products. If the magistrate is presumably the deciding authority in the event of such a case being brought to court, he will need authoritative technical advisors to sort this one out, but it is very common for suppliers to exercise their initiative in offering substitute components if the requested item is not currently available. These often serve to enable a project to be made operational but will not necessarily guarantee the optimum performance as achieved with quoted component types. It can be found that faulty conditions occur in a circuit which can cause chain reaction damage to other components. If substandard or substitute components are used, one takes this risk, but the constructor has no redress on the supplier unless the supplier has stated that the substitute component is suitable for that project.

The act stipulates that where redress is justified, the onus is on the seller, usually the retailer. The manufacturer is only responsible for supplying the seller with products that correspond with their trade descriptions. If such a description is inadequate then it is the responsibility of the purchaser to satisfy himself that the goods are what he wants.
Exclusion clauses are made void but not illegal, so that customers should not be led to think that his rights are adversely influenced by such statements. Guarantees should now make clear to the consumer that additional rights are being given; no guarantee that offers less than the implied rights of the Supply of Goods Act will be valid.

> M. A. COLWELL-Editor.
 Further details on page 335.


# Practical Wireless and Television in Berlin 

FOR the first time Practical Wireless and Television will be taking part in an overseas exhibition at the end of August. The "International Radio and TV Exhibition," to be held in Berlin August 31 to September 9 , is one of the largest commercial and public exhibitions of its kind. Of special significance is the celebration of 50 years since the first German radio station began transmitting officially in the former Reich capital.

This will be the 29th national and second international exhibition organised by the "Division Radio and Television" in the German Electrical and Electronic Manufacturer's Association (ZVEI).

There will be 88,000 sq metres of space in 23 halls and 4 pavilions, as well as 40,000 sq metres of open-air grounds. The truly international flavour is due to participation by 20 countries including Hong Kong, South Korea, China, Norway, U.S.A. and several European countries.

Displays will embrace all aspects of electronic home entertainment systems including associated equipment for servicing, studios and transmission installations. Programmes will also be transmitted from a 2,100 seat hall that will be converted into a television studio.
Practical Wireless and Television magazines will participate in the Technical Press section and visitors will be able to see much of the recent work that these two magazines have published as well as some new ideas 'for the autumn.

We cannot possibly tell you everything about this gigantic operation in just a few lines but we hope to be able to publish much of the exciting events that will take place in a future issue. So if you are around West Germany about that time we cordially recommend a visit to this show.

## Texas Instruments Seminar

TEXAS Instruments Ltd. held their successful Interface 73 technical seminar at the Talk of the Town, London on June 12, 13 and 14 .

Richard Mann of "Texan" amplifier fame introduced delegates to the programme. Bob Spoeneman, Marketing Manager (Northern European Semiconductor Div.) then gave a short talk entitled "Market Overview."

A lecture on the TTL system followed and Mick Mimmack and Bob Parsons reviewed new TTL products especially the range of low power Schottky devices.

The next talk was given by Roger Banks, Senior Product Marketing Engineer for military ICs, who spoke on Beam Lead ICs.

Adrian Tarr, Product Marketing Engineer for Metal Can Power Products and Bryan Norris, Applications and Contracts Manager lectured on Power Devices and discussed practical applications of Plastic Power, and High Voltage Transistors, SCRs and Triacs.
A lecture on Optoelectronics followed. This was presented by Millis Miller, a specialist in optoelectronics who also gave a demonstration of solid state targets for low light level TV applications.

Lunch followed at 13.05 and when delegates had finished their steak and tutti fruitti, the lectures continued.

All delegates were presented with a data pack which comprised:
Semiconductor Circuit Design vol. 2, over 200 pages hard bound.
A totally new TTL Data Book providing comprehensive coverage of Texas Instruments 5 families of 54/74 TTL ICs. 640 pages hard bound.
A Seminar Data wallet containing a selection of the very latest product information, together with a book reproducing all the Seminar Slides.


Delegates being presented with data packs, by Mrs Gina Penman.

BSR Award

BSR Limited of Warley, the manufacturer of record changers has received an award for the 810 transcription turntable.

The "Component Design Award" presentation was made recently at a conference held at the Excelsior Hotel, Birmingham Airport. Viscount Caldecote, Chairman of the Design Council presented the Design Award Certificate to Mr. G. R. Wooldridge, Director of BSR Limited.

BSR introduced the 810 transcription turntable into the range of Hi -Fi record changers in late 1971. Its pre-programmed sequential cam system introduces a new experience in featherlight pushbutton operation.

## Logic design for Digital systems

A one week residential Vacation School intended for practising engineers scientists and teachers, who need have no previous knowledge of, but are interested in the fundamentals of logic circuit design is being organised by the Electronics Division of the Institution of Electrical Engineers. The School "Logic design-for digital systems" is intended to give an appreciation of both formal techniques and their application in practice and will be held at the University of Kent at Canterbury from 23-28 September 1973.
Lectures will cover the following subjects: historical and mathematical background; design of memoryless (combinational) circuits; design of circuits with memory (sequential); introduction to automata theory; microcircuit logic; array networks; complete design of a system; CAD techniques; testing and diagnostics; and recent advances in logic design.

Further details are available from Senior Divisional Secretary (Electronics), IEE, Savoy Place, London, WC2R 0BL.

## Noxthern Hi-Ti

THE Northern International Hi-Fi Festival, called "Audio $73^{\prime \prime}$ will be held at the Hotel Majestic, Harrogate, from August 31 to September 2.

## Mobile rally diary

August 19-The Bristol "Mobile Picnic" will be held at Ashton Court, Bristol.
August 19--Preston Amateur Radio Society will be holding their rally at Kimberley Barracks, Deepdale Road, Preston, Lancs. There will be a free car park, trade stalls, bring-and-buy stalls and refreshments. Talk-in stations will be operating on Top Band and 2 m . All the gen from G. W. Earnshaw, G3ZXC, 12 Withy Parade, Fulwood, Peston, Lancashire, PR2 4JN.
August 26-The Town and Country Festival Mobile Rally will be held at the National Agricultural Centre, Kenilworth, Warwickshire.

#  <br> F.G.RAYER <br>  

You do not have to leave this receiver behind when going camping, caravanning, or when pressed for space, as it is small in size, with internal battery and loudspeaker. Despite this, it has a very good performance for the reception of AM, CW and SSB on the short wave bands, in addition to normal medium wave reception.

## CIRCUIT

Fig. 1 is the complete circuit, except for the BFO which is necessary for receiving CW and SSB. As this section is not required for general listening it is wired as a separate unit.

Sockets A1 and A2 are alternative aerial input points. A1 is most suitable for a reasonably long wire aerial, while A2 is better for a telescopic rod or short aerial. The "Blue" aerial coil is tuned by its own 365 pF variable capacitor VC1, so that it can always be peaked up for best results with any aerial, no separate trimming being needed with this arrangement.
Trl is the OCl70 RF amplifier, with the RF gain control VR1. The "Yellow" mixer coil is tuned by VC2, which is one section of a 2-gang tuning capacitor. The panel trimmer VC4 allows this circuit to be trimmed when coils are changed, or at any point of the band covered.

The "Red" oscillator coil is tuned by the second section of the ganged capacitor, VC3. VC5 is the bandspreading capacitor, which greatly simplifies
accurate tuning on the congested SW bands. A 3 -gang component, giving simultaneous tuning of aerial, mixer and oscillator circuits could have been used, but was felt to be unnecessary because aerial and mixer circuits can be peaked up for any setting of VC5, by means of VC1 and VC4, if necessary. There is thus no loss of efficiency with this simplified arrangement-in fact, all circuits can be tuned for best results at any frequency.

Bands are covered by inserting a set of three coils for each waveband. Provision is made for four wavebands. The "Red" oscillator coils require series padders of $350 \mathrm{pF}, 1000 \mathrm{pF}$ (or 1100 pF ) and 3000 pF for the lower frequency ranges, and a direct connection for the highest frequency range. These padders, CP1, CP2 and CP3 are wired to separate holder tags



Fig. 1: Circuit of the Mini-Comm receiver. The circuit of the optional BFO is shown in Fig. 6. The photograph above shows the complete receiver, the speaker being mounted on the righthand side panel.
as in Fig. 1, so the correct padder is automatically included in circuit when the "Red" coils are changed.
The 2-stage IF amplifier has five tuned circuits in all, and although more complicated amplifiers were tried, this one was adopted on the grounds of easy construction, good gain and selectivity. Transistor Tr5 is a grounded base emitter detector with AGC fed from the collector through R11 to Tr 3 .

A 150 mW packaged audio amplifier is fed from the volume control VR2 and gives sufficient output for most circumstances using the small internal speaker. A panel jack allows headphones to be plugged in when preferred.

Using the circuit in Fig. 1, the receiver gives AM reception over all usual short wave and medium wave bands. For the reception of CW and SSB signals on amateur or other frequencies a beat frequency oscillator has to be added, and this is covered later. Should CW/SSB reception be omitted, two panel holes for the BFO "pitch" capacitor and AM-CW/SSB switch will not be necessary.

Capacitor VCl is mounted with three countersunk 4BA bolts, washers or spacers about ${ }_{1}$ in. thick being placed between the capacitor and panel, the spindle passing through a ${ }_{3}$ in. or ${ }^{1}{ }_{2}$ in. dia. clearance hole. Take care that the bolts do not penetrate beyond the thickness of the capacitor front frame. Before mounting VCl , solder a lead to its rotor (chassis) tag, to go to a tag MC bolted at the "Blue" coil holder as in Fig. 2.

Gang VC2/3 is mounted in the same way and two leads are soldered to its central rotor tag. One runs directly to a tag at the "Yellow" coil holder and the other to a tag at the "Red" coil holder. The small drive used for VC5 is fixed to the panel with two 8BA bolts while VC5 itself is fixed to a bracket cut from scrap. Drive and capacitor should be lined up carefully.

The controls are positioned as in Fig. 3. As mentioned, S2 and VC6 will be required for the BFO only so if these items are not wanted VR1 can be moved to the VC6 position, for a symmetrical layout.


Fig. 2: Layout of the major components on top of the chassis.

## GENERAL CONSTRUCTION

The receiver chassis is an 8 x 4 in . "universal chassis" flanged member punched to take the coilholders as in Fig. 2. A second 8 x 4 in . flanged member forms the panel. The end flanges of the chassis member are cut so that they fit inside the flanges of the panel and bolts pass through the front flange to secure the chassis at a height of $11_{4} \mathrm{in}$.

Both sides are ${ }^{1}$ in. or similar hardboard, $4^{3_{8}} \mathrm{x}$ $45^{8}$ in. Bolts hold the sides to the chassis and panel flanges. The right side has an aperture for the speaker with perforated zinc or speaker material placed behind the opening. It is as well to leave the speaker off until construction is otherwise finished.

The case back is a third $8 \times 4$ in. member. A bracket is cut from scrap or a spare member so that a PP9 battery can be placed as shown. Both top and bottom are $8 \times 4_{2}$ in. and can be metal or other material such as hardboard, paxolin sheet, or plywood. Self-tapping screws hold these parts to the front and back flanges.

As there is not much spare space under the chassis, the panel holes for these items come almost against the front flange of the chassis. In order that the controls are not tilted by this, it is necessary to fit one or more washers on each bush and to cut the flange to clear these. Alternatively, use five washers such as those punched out for the coil holders and cut a flat on each to clear the chassis flange.

Most of the wiring in Figs. 2 and 3 can then be done, mounting resistors and capacitors directly on the coil holder tags, as shown. Some 20 or 22 swg tinned copper wire is suitable for other connections, with insulated sleeving.

The leads from $\operatorname{Tr} 1$ and Tr 2 are left almost full length. It may be preferred to use coloured sleeving on the wires say green for emitter, blue for base, and orange for collector, with the shield wire bare or red.

The small circuit board in Fig. 3 carries the components shown in Fig. 4 and is wired separately. For external connections, insert Veropins or leave a projecting wire.

## components list



A ${ }^{1} 2 \mathrm{in} .6 \mathrm{BA}$ bolt is fixed to the chassis in the position shown in Fig. 3 and an extra nut put on it, so that the board will be clear of the metal. The board is then placed as in Fig. 3, and fixed with a further nut.

The tag MC (Fig. 4) under the board is the chassis return.


Fig. 4: Layout of the RF board.

## IF AMPLIFIER

A piece of Veroboard is cut having 7 rows of holes one way, and 23 rows the other way, or $31_{2} \times 11_{8}$ in. Components and leads can then be placed exactly as in Fig. 5 with the minimum of difficulty.

Drill holes for 6BA bolts to fix tags MC, place the board on the chassis as in Fig. 2, and drill matching holes in the chassis. Holes have to be drilled for the IFT's so that the pins are located as in Fig. 5. Probably the easiest method is to secure the board by one long edge in a vice and drill the holes, then if some do not match the pins with sufficient

Fig. 3: Arrangement of parts and wiring underneath the receiver. Top centre is seen the audio module and to its right the BFO board. The board at centre right carries some of the RF components and wiring.

accuracy, to use a very small round file to enlarge the holes until the IFT's fit. A central hole is necessary under IFT1 and IFT2 to reach the lower cores.

Components can then be placed as in Fig. 5. In most places the wire ends of resistors and capacitors are long enough, so they are bent over, soldered and snipped off. Sleeving is put where needed to avoid shorts. The tags MC are secured tightly with ${ }^{1}{ }_{2} \mathrm{in}$. 6BA bolts and nuts and one screening can tag of each IFT must also be wired to this earth circuit.

Fit four Veropins or wires as shown. At the righthand end of the board " 9 V negative" has a black flexible lead and negative battery clip. A lead from C14 positive will run to VR2, as shown. At the other end of the board, IFT1 pin 2 will be connected to tag 8 of the "Red" coil holder. A wire from the
pin "negative for RF and mixer" will run to R3 and R7 on the under-chassis board.

Pieces of sleeving about $3_{8} \mathrm{in}$. long on the transistor wires will prevent shorts here and raise them a little above the board. Solder these wires directly to the points in Fig. 5 and snip off excess wire.

The IF amplifier can be tested by connecting a battery and phones (or AF amplifier) and injecting a signal at pin 2 of IFT1 from a signal generator. As the IFT's are pre-aligned by the maker, the cores should be left as they are until proper results are obtained, and only touched up as required afterwards.

The IF amplifier is mounted with lock nuts, making sure that there is no possibility that leads or joints will touch the chassis. Leads can then be connected as shown.


Flg. 5 : Details of the wiring and construction of the If strip. This can be tested and roughly aligned before being fitted into the chassis,


A useful view of the recelver with the back removed to enable the IF strip to be seen.


Fig. 6: The circuit of the optional BFO. The leadout connections for the OC 45 can be found on Fig. 5.

## AF AMPLIFIER

Figs. 1 and 3 show the packaged amplifier from the top. It is mounted clear of the chassis by a ${ }^{1}{ }_{2}$ in. 6BA bolt with extra nuts, also securing a tag which forms the positive or chassis return connection as in Fig. 3.

Run the lead to VR2 slider (centre tag) against the chassis. Take two blue wires as shown for the speaker circuit. The one connecting point here also has a black lead, which passes to the 9 V negative pin of the IF board, and thus to battery negative.

## IF ALIGNMENT

This is carried out with a weak but stable signal, from a signal generator, or from a BBC MW station. VR2 should be at maximum, but signals can be reduced with VR1 so that the AGC action does not mask adjustments.

Adjust each core, if necessary, using a properly fitting tool (such as the Denco TT5 trimmer tool). Each core should have a quite sharp peak, but much adjustment ought not to be necessary.

Once this has been done, no further adjustment to the IF amplifier is necessary.

## TUNING

As the coil cores are screwed right in for packing purposes they require adjusting so that some length of brass thread projects. Band coverage is set by means of the core of the "Red" coil. This adjustment is made at the low frequency end of the band.
Tune in a signal near the high frequency end of the band, and rotate VC4 for best volume. Now tune to a signal near the LF end of the band. Leave VC4 untouched and rotate the core of the "Yellow" coil for maximum volume. It should then be found that VC4 will require only a little adjustment, for best
volume, at any frequency in the band. To retain dial calibration, the core of the "Red" coil is locked with a 6BA nut.

In all cases VC1 should peak up signals when in a similar position to VC2/3. Adjust the core of the "Blue" coil at the LF end of the band so that this condition is obtained. It is then only necessary to keep VCl approximately in step with VC2/3, while tuning, and to adjust VCl for maximum signal strength with the wanted station, or for the narrow band of frequencies to be tuned by VC5.
The listed single capacitor VC1 and 2-gang capacitor VC2/3 have integral reduction drives and direct and slow-motion $1_{4} \mathrm{in}$. shafts. An "Electrovalue" type CK4 knob was fitted to the direct drive part of each spindle, by tapping out the metal insert or disc. A type JV18 knob was then fitted to the slow-motion part of the shaft. An alternative is to fit pointers to the direct drive part of each shaft, or to use direct drive (not slow motion) capacitors, with pointer knobs or scales.


Fig. 7: The two sides of the board for the BFO components.

Coverage of the sets of "Blue", "Yellow" and "Red" coils is approximately as follows, and only those coils necessary for the frequencies wanted need be obtained.

Range $2 \mathrm{~T} 515-1545 \mathrm{kHz}$ ( $580-195 \mathrm{~m}$ )
Range $3 \mathrm{~T} 1 \cdot 67-5 \cdot 3 \mathrm{MHz}(180-57 \mathrm{~m}$ )
Range $4 \mathrm{~T} 5-15 \mathrm{MHz}(60-20 \mathrm{~m})$
Range $5 \mathrm{~T} \quad 10 \cdot 5-31 \mathrm{MHz}(28 \cdot 9 \cdot 7 \mathrm{~m})$


## BEAT FREQUENCY OSCILLATOR

The circuit for this is shown in Fig. 6. When switched on, it produces an oscillation which can be tuned to approximately the receiver's intermediate frequency by the panel control VC6. This signal is coupled into the IF amplifier.

When CW is being received VC6 is adjusted so that the difference between the signal received and the BFO frequency will produce the wanted audio tone. With VC6 tuned to the receiver IF, no tone is produced. Moving VC6 either way produces a tone which rises in pitch. In some cases placing the BFO one side or the other of the IF may give greater freedom from interference.

When receiving SSB (single sideband) the BFO frequency is adjusted with VC6 so that it simulates the carrier which was removed before transmission. The speech will then be resolved. For this purpose, VC6 has to be adjusted carefully as required, for if the BFO (or carrier oscillator) is the wrong side the SSB signal, the latter cannot be resolved.
As the receiver has no separate product detector, it is essential to keep the level of the received signal down on SSB, as required, by means of the RF gain control VR1. For AM reception, VR1 will usually be at near maximum, while volume is controlled by VR2. But for SSB, VR2 will usually be at maximum (except when using phones) and gain will be reduced by VR1. (An exception is when strong AM signals cause cross-modulation of other AM signals, when VR1 should be turned back.)

The stabilising diode D1 is not absolutely necessary but as the current drawn by the AF amplifier varies considerably with audio level this can tend to cause modifications to the oscillator frequency due to fluctuations in oscillator voltage. A $100 \mu \mathrm{~F}$ or $250 \mu \mathrm{~F}$ capacitor from battery negative to chassis will help reduce this. For a similar reason, connections to Tr2 can be modified so that this stage is supplied from the regulated 6.8 V line, though this again is not by any means essential.

## BFO CONSTRUCTION

Fig. 6 shows wiring and components on the small BFO board. This is positioned as in Fig. 3, so that a short, stiff lead can run from pin 3 of the BFO coil to VC6. When first setting up the BFO, tune in a weak but stable AM signal. Put VC6 half closed, switch on the BFO, and rotate the VFO coil core until a strong audio heterodyne is produced, which is then adjusted to zero. Turning VC6 either way from this position should then cause an audio tone which rises in pitch.

When the BFO is in use, this produces some AGC voltage which reduces the IF gain. The second pole of the 2 -way switch is wired as in Fig. 6 to avoid this. R11 is disconnected from the pin of IFT1 and colour coded leads are run from R11 and pin 6 through the chassis. A $68 \mathrm{k} \Omega$ resistor is added at the IF board, connected to the IF board negative line. These circuits are connected as in Fig. 6 so that AGC is only applied to the first IF amplifier when the switch is in the AM position.
At the same time R13 can be disconnected from the positive line and a lead can be soldered on to run to VR1, as also in Fig. 6. This gives manual control of the gain of both the RF and the IF stages.



## BBC ENGINEERING 1922-1972

By Edward Pawley, OBE, M.Sc.Eng., C.Eng., CIEE<br>Published by the British Broadcasting Corporation,<br>35 Marylebone High Street, London, WIM 4AA. 569 pages $10 \times 7 \downarrow$ in. Price $£ 7.00$ HIS book is one of those "Bibles" that should be on the bookshelf of any man whose interest is in the earlier days of radio.

Chapter 1 explains what broadcasting is and takes the reader through the pioneering days of radio transmission. Chapter 2 tells of the period between 1922 and 1926 and is sub-divided into sections which include such things as transmitters and reception, studios, outside broadcasts, international relations and the Keston Receiving Station.

The years 1927 to 1939 are covered in chapter 3 and such items as the forming of the Corporation and short wave broadcasting are covered together with the story of the regional scheme of transmitters and the beginnings of television. There is also a section covering the BBC's preparation for the war.

The whole of chapter 4 is devoted to the war years and chapter 5 covers the post-war reconstruction of the BBC from 1946 to 1955.

The sixth and final chapter is entitled "The Years of Expansion" (1956-1972) and tells how the Corporation has progressed to the present day. A rather interesting section in this chapter deals with research and development.

Mr. Pawley has comprehensively covered the growth and progress of broadcasting throughout the six chapters of this book and traces the history from the experiments of Hertz, Marconi, Oliver Lodge and other great pioneers right through to the present day.

This is a text that it is well worth putting on the "birthday present" or "Christmas present" list as it will, I am sure, provide many many hours of interesting reading to anyone who regards radio as his hobby.

CRR
TELEVISION INTERFERENCE MANUAL By B. Priestley G3JGO Published by Radio Society of Great Britain 35 Doughty Street, London, WC1
92 pages, $8 \pm \times 6 \mathrm{in}$. spiral bound. Price: 80p HE average transmitting amateur in this country is beset by two major problems-the complaints of neighbours who will persist in wanting to watch interference-free TV programmes and, having reluctantly agreed that the neighbours have a point, finding the relevant technical information to enable him to fix his transmitter and/or the TV set and live in peace ever more.

Unlike the United States, TV set manufacturers here are under no legal obligation to fit any kind of filter to their sets so the poor amateur is forced to do a PR job for them by visiting the complainant and, hopefully, finding a solution. The amateur soon finds out that every TV set has its own particular problems and that the filter that clears the X model set is useless on the Y model. So far, information on the subject for the amateur has only appeared in dribs and drabs, mainly in "Radio Communication" the monthly magazine for members of the RSGB and not on general sale. However, this new RSGB publication, long overdue, is a welcome collation of such information from many sources on just about every method of TV interference suppression that has ever been tried on transmitters and TV sets.

The eight chapters of the manual are packed with practical information ranging from an all-important explanation of the nature of TV signal through preliminary investigation of TVI to the design of transmitters. With the deluge of hi-fi gear that has now descended on the populace the amateur is often faced with the problem of audio breakthrough and this has been given a chapter to itself. The author makes much, and rightly so, of the great tact and diplomacy needed between the parties involved if there is to be a successful conclusion to TV breakthrough investigations. The Radio Interference Service of the Post Office usually comes into the act and their actions and responsibilities when investigating complaints are very clearly laid down in this manual.

So far, very little concerted effort has been made to form effective TVI investigation groups among the amateur fraternity and those that do exist are no doubt sitting on masses of useful information. For the amateur who must go-it-alone, this excellent manual will be his greatest ally. With some 18,000 licensed amateurs in the UK the RSGB should be able to sell at least that number of copies without any trouble at all.

AED

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Number 40

## LP1000 STORED ENERGY REGULATOR

Visual power indication in battery operated equipment is usually absent so as to conserve power, except in the case of equipment incorporating high capacity or re-chargeable batteries. In some cases the power drain from a small filament incandescent bulb would be greater than the total consumption of the set. With the advent of the LED with its far greater light output efficiency it was possible in some cases to incorporate these as visual indicators but even here a 30 mW or so power drain would be quite typical.

An alternative approach to reduce power drain even further to a mere 300 microwatts or so would be to pulse operate the LED every few seconds in addition to keeping it in operation only for a specified portion of the peak pulse thereby giving rise to maximum light output for minimum energy consumption.

A new monolithic integrated circuit type LP1000 manufactured by the Lithic Systems Inc. Co. of America performs just this function and is described as a 'Stored Energy Regulator' or 'Miser' for short, due to its extremely low power drain. This, however, is only one of a number of very interesting applications of this particular IC to be considered this month.

## Circuit

A circuit diagram of the LP 1000 IC together with a functional block diagram is illustrated in Fig. 1. Power for the device is usually obtained through a resistor capacitor network. The output power gate consisting of $\operatorname{Tr} 4$ is kept biased off as long as $\operatorname{Tr} 1$ is kept in a non-conducting state set by the voltage drop across D4 which is in series with the Dl-D3 diode chain. As soon as Tr conducts the voltage drop produced across R2 saturates $\operatorname{Tr} 2$ which in turn forces the power gate $\operatorname{Tr} 4$ to change state.

The feedback signal to the base of $\operatorname{Tr} 3$ via R1, reduces further the voltage drop across D4 as it saturates $\operatorname{Tr} 3$ which is connected in parallel with D4 and this accentuates the turn-on time resulting in a sharply rising output pulse at the collector of Tr4.

As the LP1000 then discharges the capacitor Cl through the load, the voltage across Cl begins to drop but before it can reach zero level $\operatorname{Tr} 3$ will be biased off giving rise to an equally abrupt turnoff pulse. The peak and valley voltages for the LP1000


Fig. 1 : Circuit diagram of the LP1000, together with a functional block diagram. The IC is produced in a TO-18 package.
lie between $2 \cdot 4 \cdot 1 \cdot 9 \mathrm{~V}$ so peak power is only consumed with the inherent advantage of maximum efficiency. This sequence of events continues so long as power is suppled to the device with the flashing rate set by the external RC time constant.

A high intensity light flash visible even in direct sunlight is possible using a $500 \mu \mathrm{~F}$ capacitor. However, as the maximum voltage applied across this capacitor is in the region of 3 volts, the actual physical dimensions of the capacitor can be kept quite small. Less intense flashes are produced with
smaller value capacitors with a corresponding increase in the flashing rate provided the charging resistor remains constant.

## Other uses $=\because$

Due to the built in load resistor in the collector circuit of $\operatorname{Tr} 4$ the IC can also act as a free-running multivibrator with the frequency again controlled by the RC time constant. Frequency rates from as low as one cycle per minute to as high as 20 kHz are possible using this simple arrangement with a typical power consumption of a mere 500 microwatts. Fig. 2 shows the LPl000 connected as a 1 kHz oscillator.


AM0008
Fig. 2: LP1000 in a multivibrator circuit at 1 kHz .
A further development from the oscillator application above is to power the IC from a solar cell giving rise to a self-contained unit which could find interesting applications as an aid to the blind. By replacing the load resistor with a miniature earphone an audible tone is available as a light indicator with the frequency of the note indicating the intensity of the light. Turning the cell towards brighter areas will be reflected by a corresponding increase in the pitch of the note. Solar cells capable of delivering 500 microwatts are relatively inexpensive and the light-to-sound indicator could prove to be a invaluable asset to any blind person, Fig. 3.


Fig. 3: Circuit using the LP1000 in a light-to-sound indicator.
Finally the last application to be considered is again a rather unusual one but the experimental possibilities it opens up are intriguing. If the load is replaced by a small step-up transformer voltages as high as 90 volts or so are obtainable. Naturally the available current from such a source is small but it does offer the possibility of trickle charging small capacity batteries from solar energy in a pretty efficient manner.

The Lithic Systems Inc. Co. have also recently released one of the first monolithic microtrans-mitters-a complete radio transmitter on a single chip with a 100 mW output. In the near future it is hoped that an article featuring this IC type LP2000, will be published in this column.

## AUGUST ISSUE

## RECEIVER DEBUGGING

When you've built a TV receiver and tested it you will probably find all sorts of faults present. The aim of this new series is to run through the likely faults and to pinpoint the areas where action needs to be taken. The series will aid the understanding of fault-finding generally of course, and is a follow up to our series earlier this year on assessing receiver performance. In the first part the operation of the timebases is considered and the resons for non-linear scanning outlined.

## UHF FAULTS

When a dual-standard set is first switched over to 625 -line operation all sorts of unsuspected faults are often encountered. George Wilding runs through the common ones and their causes, and the action necessary. Reception on u.h.f. has proved to be rather more troublesome generally than at v.h.f.

## VALVE AND TRANSISTOR SUBSTITUTION GUIDE

It is not always necessary, and sometimes impossible, to fit exact valve and transistor replacements. This guide has been compiled to indicate generally what can and can't be done, list numerous helpful substitutes and lay down guidelines for the more difficult situations.

## SERVICING TELEVISION RECEIVERS

This month Les Lawry-Johns deals with problems on the final GEC group dual-standard chassis, the GEC/Sobell 2032/1032 series.

## SBF AERIAL FOR BAND V

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## EXPERIMENTERS CORNER



IN some applications, such as in small pocket receivers, only comparatively small output powers are required, and small modern loudspeakers produce adequate volume for a small room from only a few milliwatts of power. In fact most miniature speakers have a maximum power handling capability of only $100-200 \mathrm{~mW}$.

While in the interests of battery economy class B amplification is usually used in the output stage of battery operated equipment, where only low output powers are involved, a simple class A circuit is quite suitable. Bearing these points in mind, the simple amplifier described below was constructed.

## Circuit Explanation

A circuit diagram of the amplifier constructed by the author is shown in Fig. 1. This uses three inexpensive silicon n.p.n. transistors.

VR1 is the volume control, and CI the input coupling capacitor. $\mathrm{Tr} 1-\mathrm{Tr} 2-\mathrm{Tr} 3$ are direct coupled. R2, and R5 bias the input transistor (Trl) so that the voltage present at its collector (approximately 0.65 V ) is at the correct level to in turn bias Tr2. Likewise, Tr 2 is biased to just the right level to produce a voltage at its collector which is suitable to bias the output transistor, $\operatorname{Tr} 3$. In effect $\operatorname{Trl-R1}$ form a potential divider which biases $\operatorname{Tr} 2$, and $\operatorname{Tr} 2-\mathrm{R} 3$ form a potential divider which biases $\operatorname{Tr} 3$.
As each transistor inverts the signal between its base, and collector terminals, the input and the output of the entire amplifier are $180^{\circ}$ out of phase. The two biasing resistors, R2, and R5 being connected between the input and the output therefore introduce a considerable amount of d.c., and a.c. negative feedback. While the d.c. feedback is very
desirable as it gives stable biasing to a system which would otherwise be very critical, the a.c. negative feedback decreases the gain of the amplifier. This does however, give the amplifier improved quality (hi-fi).
The gain of the amplifier can be increased by connecting a capacitor of a suitable value between the junction of $\mathrm{R} 2-\mathrm{R} 5$, and earth. This decouples the a.c. signals through the biasing resistors, and virtually eliminates the a.c. feedback at audio frequencies.

A compromise between gain, and output quality can be achieved by placing a feedback limiting resistor in series with the decoupling capacitor. In Fig. 1, C3 is the decoupling capacitor, and R6 the feedback limiting resistor. The value of R6 is the highest one which gives adequate gain for the amplifiers intended purpose, a value of $22 \mathrm{k} \Omega$ being used on the prototype. Its value can be varied to suit individual requirements, the required value being found by experimentation.



A
Fig. 2: Component layout on the Veroboard.

Fig. 1: The low power class A amplifier.

R4, and C2 are the supply decoupling components. The loudspeaker itself forms the collector load for Tr3. Speakers of other impedances can be used, but must have an impedance of at least $35 \Omega$. Due to the large amount of d.c. negative feedback used in the circuit, altering the speaker impedance should not drastically change the operating parameters of the circuit.

The low value capacitor, C 4 , is required in order to reduce the upper frequency response of the circuit, and so maintain good stability. Without this component, direct pick-up of radio signals can become a problem.

Sl is the on-off switch, and can be ganged with VRl if preferred.

The unit requires a $4 \cdot 5 \mathrm{~V}$ supply, an Ever Ready 1289 battery being a very economical source of power for the amplifier, although if small size is required, three U16 batteries connected in series can be used.

As the amplifier uses only a few components all
of which are of a small size, it is easily miniaturised. A diagram giving a suitable Veroboard layout for the unit is shown in Fig. 2. The prototype built to this layout measures only $1.4 \times 0.9 \times 0.75 \mathrm{in}$. For obvious reasons miniature resistors, and components must be used. On the prototype a tantalum bead capacitor was used in the Cl position, but a miniature electrolytic of $8-10 \mu \mathrm{~F}$ can be used providing it will fit into the available space.

There is only one break which has to be made in the copper backing strips, this being between the negative side of C 1 , and the collector of Tr 1 . A soldering iron with a fine bit is required when soldering the components to the board, and a continuity tester should be used to ensure that no excess solder is shorting two adjacent copper strips together.

One cannot expect too much in the way of output quality from the amplifier, mainly because such a small speaker is used, but the unit is economical to run, small, inexpensive to build, and sensitive, and is very useful for many purposes.

## CASSETTE RECORDER IN THE CAR

ON a long trip it is often desirable that one can play one's cassette tape-recorder, but then it's battery life becomes very short. Since most cars use a 12 volt battery, the tape recorder cannot be run directly from the car's electrical system. One often used method is to connect a heavy resistor in series with the tape-recorder, but on a radio-cum-tape-recorder this method does not work since the tape recorder draws far more current than does a radio.
This problem can be overcome by using a very simple stabilising voltaged supply consisting of only three components-a transistor, resistor and a zener diode. Before one selects any components, one must know exactly what one's requirements arethe figures given at the end of this article are for a typical cassette tape-recorder that draws a maximum of 350 mA . It is however easy to modify one's design to cope with almost any portable tape-recorder.

Firstly, what is the voltage of the machine? This is easily determined by counting the batteries and multiplying by $1 \cdot 5$,-most recorders are either 6 , $7 \cdot 5$ or 9 volts. Once the voltage has been determined, it is neccessary to find the maximum current that the machine will draw. To do this, remove one battery and solder wires onto the ends of it. Connect an ammeter in series with the battery and by dabbing the wires where the battery was and by playing the tape recorder with it's volume fully turned up, the maximum current can be determined.

Our next job is to choose a transistor. The only specifications that need concern us are it's power and current rating and it's current gain ( $h_{f e}$ ). For a tape recorder, a 2N3054 is normally sufficient, but for a large machine, a 2 N 3055 might be neccessary, while for a small radio, a 2 N 1611 might suffice. To determine the power rating, we use the formula Power $=\mathrm{IxV}$

$$
=I\left(V_{\text {in }}-V_{\text {out }}\right)
$$

The zener diode is a low power device ( 250 mW ) and it's breakdown voltage is the required output voltage plus $0 \cdot 6$ volts, the latter being the emitter-

## M. Vlietstra

base voltage of a silicon transistor. The zener need not be specially selected, since a volt either way will have very little effect on the tape-recorder.


AMOOOL
Fig. 1: Stabilising circuit for cassette recorders.

The resistor ( R ) is the most difficult to calculate. The current that passes through it performs two functions:
i) A current of normally at least 5 mA to maintain the voltage across the zener diode.
ii) The base current of the transistor. As a rule of thumb, this should be twice the maximum required output current divided by the current gain of the device.
Adding these two we get that the current through the resistor is ( $5+2 \mathrm{I}_{\text {out }} / \mathrm{h}_{\text {fe }}$ ) mA and assuming that the car uses a 12 volt battery, the value of the resistance, using Ohm's Law, is found to be:

$$
\mathrm{R}=\left(\frac{\left(12-\mathrm{V}_{\mathrm{out}}+0 \cdot 6\right)}{\left(5+2 \mathrm{I}_{\mathrm{out}} / \mathrm{h}_{\mathrm{fe}}\right)}\right) \mathrm{k} \Omega \quad\left(\mathrm{R}=\frac{\mathrm{V}}{\mathrm{I}}\right)
$$

The components given below are for a typical tape-recorder that draws 350 mA . No list of prices is included as a person who can't build this for less than $£ 1$ just isn’t trying!

| Components. | 6 V | $7 \cdot 5 \mathrm{~V}$ | 9 V |
| :--- | ---: | ---: | ---: |
| Resistor $\left(\mathrm{I}_{2} \mathrm{~W}\right)$ | $330 \Omega$ | $270 \Omega$ | $180 \Omega$ |
| Zener diode | $6 \cdot 6 \mathrm{~V}$ | $8 \cdot 1 \mathrm{~V}$ | 10 V |
| Transistor. |  | 2 N 3054 | $\square$ |

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moving coil mpeaker. Attractive case with red speaker grille. Bize 6$\} \times 4\} \times 1 \frac{1}{2}$ in. Easy bulld plans and paris jrice list 10 g (FREE with parts).
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of Luxembourg etc. Bensitive fer
 riterodaerial and telescopic seria
3in. Speaker. 8 . 2 nioues. Attractive black case with red grille, dial anm black knobs with pollshed metal inserts. Size $9 \times 5!\times 2 \sharp$ in approx. Easy build

Total building costs $54.39 \mathrm{P} . \mathrm{P} .8$ Overseas P. \& P. \&1.05) \& 0

bands: MW, LW
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black with red grille, dial and black knobs with polished metal inserts. Size $9 \times 5 \frac{1}{2} \times 28 i n$. approx. Push pull output. Rattery economiser switch ior extenced battery life. Ample power to drive a larger speaker. Part. Total building costs $8: 9$ F. P. $\%$

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ACOMMON circuit arrangement in the popular construction journals is that which allows temperature to control something-a sort of electronic thermostat.

Perhaps the most featured circuitry is that which has some form of temperature sensor (say, a thermistor) followed by a transistor or two which, in turn, drives a meter (for temperature to be read from a pre-calibrated dial) or a relay to actuate some form of control circuit.

Out on to the electronics market has come a new type of reed switch which can perform this kind of func-tion-and without the need for any further electronic circuitry.

Basically, the reed switch has two contact blades which form a simple on-off switch. Around the glass tube which houses these contacts is a coil. Energising the coil causes the contacts to open (or close) while remova of the energising source causes the blades/contacts to return to their original state.

The new devices have the glass capsule and reed relay blades. Instead of a simple coil of wire, the capsule is surrounded by torroidal magnets which are separated by a ferrite material. Because the ferrite material separates the magnets, it also has the effect of separating their individual magnetic fields.

However, the particular make-up of the ferrite employed is such that there is a certain critical temperature point called the Curie point. Below this point, the ferrite no longer isolates the magnetic fields of the separate magnets and thus the switch can be caused to activate.

Once the temperature rises above the Curie point, the magnetic fields are again separated. Thus there is a complete switching action actuated only by temperature, and the reed blades themselves can be used to form a switch. There are many uses which will come to mind; standard units in the range extend from $0^{\circ} \mathrm{C}$ to $100^{\circ} \mathrm{C}$ in $5^{\circ} \mathrm{C}$ steps.

## LIGHTS UP

Turning to the "lighter" side of smoking, solar cells are being used in electronic lighters to keep the batteries charged. One set of experiments shows that some 50 cigarettes
a day can be lit for a month before the batteries need recharging by exposing the light-cells to a light source. It seems reasonable to assume that one could leave such a lighter out in the open for various periods of time and thus the batteries would remain charged for far longer than a month.

Work is proceeding to improve the efficiency of solar cells as a means of supplying energy from ordinary daylight, i.e. without any sunshine at all. This should be a useful project for people living in or around Manchester on a rainy day.

## ALL TOGETHER

Electronic calculators have become very real practicalities over the past few years. Progressing from the realms of theory they are now offered by the van load in a wide variety of shapes and sizes. Many things have contributed to the progress of electronic calculators not the least of which is the development of the i.c. which does all the calculating. The aim has been to be able to boast " $A$ calculator on a chip".

Well, the dream gets closer every hour. A company has now brought out a chip which very, very nearly achieves this title. The low power calculator circuitry is on the same glass panel as the liquid crystal display. Thus the thing is literally a complete calculator on a single substrate.

But what of the buttons or keys which input the information? Well, the manufacturers have thought of that too-yes, and it's on the same panel. The inter-digitised contacts are shorted by a conductive rubber button whenever a key is depressed. Standby power is only 12 mW and the calculator runs for about 100 hours from a single pen-sized cell. Sorry, they are not for sale in the U.K. as yet.

## VERY HIGH-BROW

Capacitors are one type of component which seems to be getting ever smaller. The photograph on this page shows five tantalum chip capacitors from the range manufactured by Union Carbide. The T 400 series has nine case sizes; values range from $0.1 \mu \mathrm{~F}$ and can withstand temperatures of up to $300^{\circ} \mathrm{C}$. Those

shown in our photograph are for a very "high-brow" application - at least, "eye" think they are.
Down in the forest something stirred, so we're told. In a certain Bavarian forest it is more than stirring. Laser equipment, supplied by Siemens, measures the trajectory of survey satellites. Power of this laser is 100 MW ( 100 megawatts or one hundred million watts). One wonders if, in the decades to come, this type of equipment will be towed away from Lisle Street shops as surplus stock by delighted Amateurs who may have just given £1.75 for them. If this happens one must ask whatever will replace such equipment?

## LITTLE THINGS

Little things please little minds so we're told, but sometimes it's not that cynically simple, Cramming a few thousand semiconductors into a dual in-line package is a common occurrence today, but what of the devices which are very difficult to integrate? Items such as tuned circuits are a problem. However, solutions are on the way, in the form of subminiature inductors or "coils".

Described as monolithic chip inductors, these minute devices are made by stacking $U$-shaped conductor patterns which have been screened onto a special ferrite tape. The U-shaped patterns are stacked such that when the individual ends of each $U$ are connected to the $U$ 's above and below, a continuous "coil" pattern is achieved. When this has been done, the complete stack is "fired" resulting in a monolithic structure.
Cimbers

##  COMMPONIENTSHOW

THE four-day London Electronic Components Show at Olympia, London opened on Tuesday 22nd May, the guest of honour at the inaugural luncheon being H.R.H. The Duke of Kent, who later made quite an extensive tour of the Show.

The Show's sponsors, the Radio and Electronic Components Manufacturers Federation, celebrating their 40th anniversary this year, managed to get no less than 480 companies to exhibit the very latest developments in electronic components and associated instruments, equipment and services.

Olympia's two main halls were utilised for this massive event and special preparations were made to receive and attend to the needs of the many visitors from abroad. Almost one-fifth of the stands belonged to exhibitors from overseas with representatives from more than sixteen countries including Australia, Austria, Belgium, Canada, Denmark, Hungary, Japan, West Germany, Spain, Sweden and the USA.

During the Show three discussion and question sessions were held outside at the Royal Westminster Hotel, being arranged jointly by the RECMF and the Institution of Electronic and Radio Engineers. The subject "European Component Survey" covered the aspects of component testing, evaluation and development.

Visitors to the Show were invited to try their luck in various competitions in which very attractive prizes such as an 8 -track tape recorder, a $£ 100$ watch and even bottles of whisky could be won, not to mention a holiday for two in Rome!

All the components in the world would not be of much use if the many units into which they are fitted could not be connected together by means of efficient


Spectrol Reliance Ltd. were justifiably proud of this large number of permutations of their Model 534 'Universal' potentiometer.
connectors. In 1971 over $£ 22$ million of the electronic components market was accounted for by the sale of just such connectors.
About every possible variation of connector was on show with Amphenol making them their main theme on their stand together with switches, lamps, relays and indicators. Ultra Electronic Components featured a new range of connectors and accessories for use with printed circuit boards as well as an improved version of their $0 \cdot 1$ in. pitch modular edge connector. Other products on their stand included plugs and sockets, terminal blocks, rotary wafer switches and water activated batteries.

AMP of Great Britain also had a wide range of low cost pin and socket and flat flexible cable connectors. They manufacture just about everything needed in solderless, crimped terminations and can supply everything from a single terminal to computerplotted wiring system components.


In spite of their long and world wide reputation for testmeters, only now have AVO Ltd. started producing a line of panel mounting meters. Two of the new Dinline series are shown above.

AVO celebrated their Golden Jubilee with the introduction of their first-ever range of panel mounting meters. The new Dinline Fifty range marks, not only fifty years of Avo, but also their entry into Europe, with styling based on the rectangular DIN (IEC 51) specification. The matching series of eight models is available in two presentations, a moulded black finish and glass window or clear Macralon ensuring entirely shadow-free readings.

Sealectro's stand had their complete range of products which includes RF connectors, multi-pin connectors, plugboards, insulated terminals, rotary switches and punched card readers. Centre piece of this display was the new series of punched card readers, the new 4 mm grid plugboard system and the new FR/SR series of two-piece insulated terminals. New items in the RF range include a high isolation coaxial switch and a range of 75 ohm connectors to

DIN 47295. Sealectro's technical staff demonstrated a miniature RF connector assembly using flexible and semi-rigid cables.

Piher International Limited, were exhibiting in the United Kingdom for the first time. Piher are already among the world's leading suppliers of carbon film resistors with a daily output of some seven million resistors from their headquarters at Badalona near Barcelona. Over 90 per cent of their production goes to export markets, principally the United States, Germany and the United Kingdom. On Piher's stand could be seen many samples from their range of carbon film resistors, trimming potentiometers, small signal and medium power transistors and capacitors, and particular interest centred on a new range of preformed resistors.


One of the Series C16 Cermet pocentiometers by AB Electronic Components Ltd. Standard models range from $100 \Omega$ to $2.5 \mathrm{M} \Omega$, linear, but speclal models down to $50 \Omega$ and up to $10 \mathrm{M} \Omega$ are available, with soldering tags or printed circuit terminals.

Hungary was represented by Elecktromodul who were showing components for telecommunication, engineering and electronics. Products on display included ferrites, electrolytic capacitors and ceramic capacitors.

Audax SA, from France, exhibited examples from a wide range of loudspeakers, while Societe Francaise de l'Electro-Resistance had on display metal film and hi-rel resistors, carbon and cermet track potentiometers and trimmers, plastics potentiometers and cermet film micro-circuits.

Cosmocord-Stolec Limited were showing, for the first time in the United Kingdom, a range of lowcost multimeters and insulation testers, plastics mouldings and audio transcription transducer equipment.


One ltem from the vast range of drives, dials and tuning capacitors from Jackson Bros. Ltd., a miniature ball drive with a 10:1 reduction, Type 5870.

New ranges of DIN plugs and sockets and instrument components were featured by Tape Recorder Spares Limited. Audio and electronic components, switches, mains units, wire measuring and storing equipment and wire cutting and stripping equipment were among other products shown.

Watson Anodising Limited had a range of nameplates, labels, instrument panels, plain and printed chassis as well as examples of the general printing they undertake for the electronics industry.

Rectifiers, thyristors and triacs from Raytheon-TAG Components Limited included glassivated and planar plastics encapsulated thyristors and triacs, plastics encapsulated 10 A rectifiers to 1300 V , fast turn-off rectifiers and diffused SCRs up to 35A and triacs up to 25A RMS.

Radiatron Components Limited stand had a display of components and accessories ranging from collet knobs, instrument cases and housings to relays, connectors, switches and automation modules.

For visitors to the show interested in television, AB Electronic Components Limited makers of the only touch tuner made in the United Kingdom, which, when announced last year was the only one made anywhere in the world, is perhaps the best known of their products. Connectors, potentiometers, switches and thick film microcircuits are among others. Sharing AB's stand was Wolsey Electronics, a division of $A B$, showing various aerials and their range of radio and television master aerial and amplifier systems.


This 25-turn preset potentiometer by AB Electronic Components Lid. is of carbon composition construction intended for use with var/cap tuners. Resistance ranges up to $100 \mathrm{k} \Omega$ in linear, logarithmic or diode characteristic law.

Solder, one of the most important materials used in electronics, was shown in all its forms by Multicore Solders Limited. Cored solder, solder creams, bar solders as well as liquid fluxes and chemicals for hand and wave soldering were included in their display. Some 50 per cent of Multicore products are exported to 107 countries throughout the world-onequarter of the exports going into the competitive U.S.A. market.

Soft solder, fluxes, chémicals, solder preforms and samples from a wide range of solder products were to be seen on the stand of Enthoven Solders Limited.

A heavy duty aerial rotator was among communications, marine, television and radio aerial equipment featured by J-Beam Engineering Limited.

Communications cables, instrumentation cables, equipment and connecting wires, winding wires, mineral insulated heating cables and thermocouples, solder coated copper wire, silicone insulated fine wires and connectors were displayed by BICC.

The wire-wound component is one of the oldest devices used in electronics and remains an important adjunct in the industry. Gardners Transformers Limited, who specialise in this field, have orders currently valued at $£ 450,000$-a quarter of which come from overseas. They were displaying transformers, inductors, filters, delay lines, inverters, converters, power supplies and modules.

Having recently merged with the Allen-Bradley Company of Wisconsin, USA, Morganite Resistors Limited had a wide range of resistors, potentiometers, switches, thin film and thick fiim networks, capacitors,


A Tekdata Lid. flat flexible cable in FibaTEK p.v.c. material. This custom-made cable uses $7 / 0.193$ and $14 / 0.193$ wires.
fllters and industrial controllers from both of their product lines. Not previously shown in the United Kingdom, the Morganite cermet single turn potentiometer, type 90 , with a power rating of 0.5 watt and a resistance range of 10 ohms to 2 megohms, is designed for commercial and industrial applications. New from Allen-Bradley is the "Mod-Pot", a variable resistor available in single, dual, triple and quadruple construction plus potentiometers, line switches and vernier drive modules.
A. F. Bulgin \& Company Limited commemorate 50 years as electrical and electronic component suppliers. During the last 12 months some 40 new products have been introduced, the complete range now containing over 15,000 items. Examples on show included fuses, fuseholders, knobs, switches, signal lamps, and plugs and sockets.

Custom-built specialists in MOS, bi-polar and hybrid thick film technologies, GEC Semiconductors Limited had a new phase control circuit for controlling triacs when driving small electric motors. One interesting device also on display was the MA1705, a MOS integrated circuit developed for use in electronic musical instruments and synthesisers. It generates four notes on an equally tempered scale by dividing successively by $1 \cdot 0595$


[^1]from a single master oscillator. Three packages can be cascaded to produce a complete octave of semitones, while further octaves can be generated by using compatible six-stage binary divider circuits.

Among new transistors by Mullard for use in highpower, high-quality audio amplifiers are families of complementary pairs that can give outputs of up to 100 W . For example, in applications where an output of 6 to 15 W is required, pairs from the transistor family BD433 to BD438 are suitable. (Odd numbers are n-p-n types, and even p-n-p.) These have a maximum $V_{\text {CEO }}$ rating of 22 to 45 V and a total dissipation of 36 W .

Silicon power transistors type BD266 and BD267 form a complementary pair that can give a highquality, audio output of 25 W ; they are also suitable for use in general purpose amplifiers and switching applications. Both are monolithic epitaxial-base Darlington transistors.

Other new Darlington devices seen were types BDX62 to BDX67, which are power transistors with TO-3 encapsulations. Complementary pairs selected from these for use in audio amplifiers will give outputs of 25 to 100 W .


Rather large but a component never-the-less! The A51-160X Precision In-Line colour TV tube assembly features a slotted shadow mask, integral neck components and factory-set static/dynamic convergence and purity adjustments. The June issue of our companion magazine Television featured a technical article on the new Thorn tube.

The use of Mullard circuit modules and integrated circuits can reduce the design costs and assembly times of good radio receivers, a.m. and f.m. Different arrangements, demonstrating the ease with which a variety of receivers can be designed, were shown.

New to the United Kingdom and exhibited by Bird Electronic Limited, was the Bird model 4370 wide-band Thruline wattmeter and model 4342 com bined power meter and VSWR monitor. Coaxial load resistors, attenuators, coaxial switches, filters and calorimeters were also shown.

Included in the Spear Engineering Company Limited's display were power transistor holders, connectors, valve and tube base mouldings and printed circuit assembly fixtures.

on. This causes the voltage at the collector of Trl to be at a very low level, and Tr2 receives only a very small amount of base current through R3. This means that $\operatorname{Tr} 2$ is turned off, and the relay will not operate.

When light falls on the ORP12, its resistance will decrease and it will have an earthing effect on the base of Trl. This will cause a decrease in the current flowing through Tri, and the voltage at the collector will swing to a high level. Tr2 can now obtain quite a heavy base current and will turn on, operating the relay. The voltage at the collector of Tr 2 will now be at a low level, and it is $\operatorname{Tr}$ that is unable to obtain any appreciable base current, and will thus be turned off. Even if the light is now taken off the photocell, the circuit will still remain in the same state, as Tr 1 will still be unable to draw sufficient base current due to the low voltage at the collector of Tr 2 .

The circuit may be reset by two methods. A pushbutton switch may be connected between $\operatorname{Tr} 2$ base and earth. When this is operated it will have the same effect as when light fell upon the photocell, except it will have the opposite result. Alternatively the unit may be turned off, and then turned on again.

A protective diode is connected across the relay in all the circuits shown. This is to prevent the high reverse voltage, which is induced into the relay coil by the collapsing magnetic field as the relay is turned off, from damaging the transistor. Almost any diode will work in this position.


Fig. 1: Typical photoelectric switch.


Fig. 2: Circuit suitable for applications where the relay must remain on once operated.

The circuit of Fig. 2 does lack sensitivity and the ORP12 has to be almost fully illuminated before the relay is triggered. A more sensitive circuit is shown in Fig. 3. This circuit requires an extra transistor, and although BC183L is specified, the circuit should work equally well with any high gain, silicon, n.p.n. transistor.


Fig. 3: Sensitive circuit using three transistors. A 25k $\Omega$ potentiometer may be placed in series with the ORP12 to control sensitivity.

With no light falling on the photocell it will have a high resistance. Trl will receive very little base current, and will have a high resistance between the collector and emitter. Rl also has a fairly high resistance and this will prevent much current flowing to the base of $\operatorname{Tr} 3$. This transistor will cut off while Tr 2 is turned on, as occurred in the circuit of Fig. 2 when a small amount if light falls on the photocell, its resistance will fall, causing the resistance of Tr 1 to fall by a far greater amount.

When this resistance reaches a low enough value, the voltage at the collector of $\operatorname{Tr} 2$ will be at a fairly high level. A large base current will now flow, turning on $\operatorname{Tr} 3$, and operating the relay. The voltage at the collector of $\operatorname{Tr} 3$ will drop, turning off $\operatorname{Tr} 2$. If the light is now taken away from the photocell, the resistance between the collector and the emitter of Trl will again be very high. The resistance of Tr 1 and R1 will be just sufficient to give enough base current to $\operatorname{Tr} 3$ to hold the relay on.

## Broken light beam alarm

Another type of alarm sometimes used is one in which a beam of light is aimed from one side of a room, or a doorway, to a photocell the opposite side. If anyone then passes between the two, breaking the beam, the alarm is sounded. A suitable circuit for an alarm such as this is shown in Fig. 4.

This works in very much the same way as the two previous circuits. When light is falling on the photocell it will have a resistance very similar to that of R2 in Fig. 2, and the circuit will behave in the same way initially. When the light to the photocell is


Fig. 4 : Circuit for operating in a dark room.
interrupted, it will exhibit a high resistance. Tr 1 will receive very little base current, the voltage at its collector will rise, $\operatorname{Tr} 2$ will be able to obtain a large base current, and will turn on. The voltage at the collector of $\operatorname{Tr} 2$ will drop and, even if light is now restored to the photocell, Tr 1 will be unable to draw any appreciable base current. Thus $\operatorname{Tr} 2$ is able to draw a heavy base current and the relay remains on.
The circuit may be reset in the same way as the two previous circuits. For the circuit to function correctly, the room in which the photocell is situated has to be fairly dark, of course, or the light in the room will keep the relay off, regardless of the light beam.

These circuits are all fairly simple, and inexpensive, but should prove useful and interesting. With a little imagination a number of uses, other than those mentioned, may be found for the circuits.

## OCTOBER is IS5IE No. 800 Will youbecelelonatingwithus?

If so you will receive with your October copy of Practical Wireless the first pair of PW Datacards. absolutely free. A special "Going Back" feature? with reproductions from early issues of Practical Wireless; the introductory article in our new series * on Q4; "Experimental Workshop" and many other special and regular features will also appear. Further details next month.

The October issue is on sale September 7th.

. . . will give full details of how to make our two-band, two-i.c. "pop" radio receiver, . . . will give full details of the PW Datacard System announced elsewhere in this issue. ... will reveal the identity of Q4,
. . . will contain straightforward constructional projects designed around integrated circuits,


Specially designed to simplify construction, this smart looking radio uses two integrated circuits: a ZN414 for processing radio signals and an SL403D as the amplifier to drive an 8- or $\mathbf{5 5 - o h m}$ loudspeaker. Medium wave stations and Radio 2 (long wave) are covered with a very simple aerial coil; no alignment problems arise. The amplifier is designed to give 1 to 3 watts of output power and is ideally suited for a teenagers' room, kitchen, bathroom. in fact almost anywhere.


This very simple instrument is based on the popular 741 i.c. and with a minimum of other components is capable of voltage measurements up to 100 volts d.c. in five ranges. Accuracy on low voltage ranges is very good and the input sensitivity is much greater than in the conventional multimeter.

## THE FIRST OFOUR SPECIAL AUTUMN ISSUES....

$\stackrel{*}{\text { SII }}$

DON'T MISS ANY ISSUE OF PRACTICAL WIRELESS - SEPTEMBER ISSUE ON SALE AUGUST 3rd

IT occurred to the writer that many readers, being 'brought up' on transistors, would not have had the opportunity to learn about the oscilloscope from the 'bottom up' and that a basic transistorised design, with modern construction methods, would be welcomed.

An oscilloscope should be a substantial piece of equipment, and in view of the high voltages employed $(700 \mathrm{~V}$ for the e.h.t. and 300 V for the deflection amplifiers) it must be emphasised that the rather solid nature of the model is deliberate.

Another feature is the simplification of the controls on the front panel, these being; brilliance, focus, $Y$ attenuation ( Y amp), Y shift, timebase coarse control in 6 ranges, timebase fine control (fine), timebase amplitude ( X amp), and sync on/off.

There is a Y input socket and an external timebase input socket.

The writer has noticed that it is usually necessary to attenuate the input signal rather than amplify it, and with transistorised equipment the signal which is being examined can be dealt with quite effectively by an attenuator of the 'volume control' type. This makes it necessary to turn the $Y$ attenuator down to zero before connecting a signal to the $Y$ input socket but once this habit has been formed, the simplification of having just one continuously variable gain control with a d.c. amplifier is evident. The d.c. amplifier is necessary to maintain a good low frequency response, especially with square wave signals.

## The Cathode Ray Tube

The cathode ray tube (c.r.t.) itself is a form of valve, having a heater and a cathode, a control grid and anode-which must be at a high positive potential (e.h.t.) with respect to the cathode.

For a 3 in. c.r.t. the e.h.t. should be of the order of $900 / 1000 \mathrm{~V}$.

Between the control grid and the final anode are the first and focusing anodes. There are also two pairs of deflection plates, one pair-the Y platesfor vertical deflection, and the other pair-the X plates-for horizontal deflection. The deflection plates are usually operated in push-pull and with 1000 volts across the c.r.t. the push-pull voltage swing needs to be about 150 V . This makes it necessary to have a 300 V supply to the deflection amplifiers and the deflection transistors must be able to withstand this voltage.

The design utilises the 3BP1, c.r.t. which has a heater requirement of $6 \cdot 3 \mathrm{~V}$ at 0.6 A . The c.r.t. has a 14 pin base with a locating spigot and the base connector should be obtained (if possible) when purchasing the c.r.t.

The tube gives a green trace of medium short persistence and a useful trace height is 5 cms . The c.r.t. is approximaiely 10 inches in length including the base.

Cathode ray tubes are sensitive to stray magnetic fields, such as those produced by mains transformers, and even when a mu-metal shield is utilised to screen the c.r.t., transformers on the same chassis usually cause some interference to the spot. Mu-metal shields are quite expensive (when available).

In the present design, the mains transformers are fitted on a separate chassis, connected together by a multiway lead. By using this method, the problem of interference from the mains transformers was eliminated.

## The $Y$ (Vertical) Amplifier

The input to the Y amplifier is through a volume control' type attenuator VR1, and it is taken directly to the base of Tr 1 , which with Tr 2 forms a boot-

strapped amplifier with an input impedance of about $1 \mathrm{~m} \Omega$. If the reader wishes, a $0 \cdot 1 \mu \mathrm{~F}$ capacitor ( Cx ) can be inserted in the lead from the slider of VR1 to the base of Trl, with a shorting switch across it, to give a.c./d.c. facilities, but it must be pointed out that this is a sensitive part of the circuit, and all leads must be kept as short as possible to avoid stray pick up.

The output from the signal amplifier is passed through a resistor network to the long tailed pair which form the vertical deflection amplifier Tr3 and Tr 4 . This stage performs two functions:

1. To give two outputs which are $180^{\circ}$ out of phase and supply the push-pull voltages to the vertical deflection plates.
2. To provide a voltage swing of 150 V at each deflection plate.

When the base of $\operatorname{Tr} 3$ goes positive its collector goes negative. That is, the signal is inverted at $\operatorname{Tr} 3$ collector.

Also $\operatorname{Tr} 3$ emitter goes positive. This means that Tr 4 emitter goes positive. The base bias of Tr 4 is held at a fixed level by the bias network VR2 R15. As the potential difference between $\operatorname{Tr} 4$ base and emitter is decreasing the base of $\operatorname{Tr} 4$ is in effect going negative.

This causes the collector of $\operatorname{Tr} 4$ to move in a positive direction, which is the same as the original signal at $\operatorname{Tr} 3$ base. Thus $\operatorname{Tr} 3$ collector is the inverting output and $\operatorname{Tr} 4$ collector is the non inverting output.

The network R7, R8, R9 is designed to bias the base of $\operatorname{Tr} 3$ and prevent overloading, and the base bias of Tr 4 is made variable to balance with Tr 3 base and centre the trace on the screen. VR2 is therefore the Y shift. C2 by-passes any a.c. signals present at Tr4 base.
The collectors of $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$ are connected directly to the Y plates. The values of the collector resistors were chosen by trial to balance the collector outputs, and the emitter resistors R11 and R14, and the coupling resistor R12, which controls the gain of

the stage, may also be altered to match the transistors. When the trace is centred and no signal is present the collector voltages shoud be 180 V . The maximum height of the Y trace when using a 100 mV input signal (VR1 at maximum) is 3 cms .

## The Timebase Generator and $X$ Amplifier

The timebase waveform generator $\operatorname{Tr} 7$ is a unijunction transistor (TIS43) with Tr6 acting as a constant current device to regulate the charging of the timing capacitors ( $\mathrm{C} 5, \mathrm{C} 6, \mathrm{C} 7, \mathrm{C} 8, \mathrm{C} 9$ and C 10 ) and to give a linear rise time.

The fine frequency control (VR3) should be wirewound and it should be possible to steady the trace at any part of the frequency range without using synchronisation. There is some loss of amplitude on the upper timebase range.

The sawtooth signal is taken from the emitter of $\operatorname{Tr} 7$ to the base of Tr8, via a closed circuit jack JK1 and a $0 \cdot 1_{\mu} \mathrm{F}$ capacitor C12. The output signal from Tr 8 collector is fed via capacitor C13 to the timebase amplitude control VR4.

The horizontal deflection amplifiers $\operatorname{Tr} 9$ and $\operatorname{Tr} 10$ are a long tailed pair with a common emitter resistor R3l. Bias for Tr 9 is by potentiometer network R28 R29 and as in the Y amplifier, the base bias of the second transistor Tr 10 is made variable to act as a shift control to centre the trace on the c.r.t. screen. C 17 by-passes any a.c. signals and stabilises the trace.

## Synchronising

The purpose of synchronisation is to lock the timebase frequency to the $Y$ signal and so hold a given number of complete waveforms steady on the screen.

The $Y$ signal is taken from the emitter of $\operatorname{Tr} 3$ and is passed via C 4 to the base of $\operatorname{Tr} 5 . \operatorname{Tr} 5$ is driven hard by the $Y$ signal and this produces a square wave at the collector of Tr5.
C3 and R16 form a pulse shaper and the diode D1 passes the positive going pulse to b2 of the unijunction sawtooth generator $\operatorname{Tr} 7$.

The d.c. potential to b 2 is stabilised by the zener diode D2. R24, C11 and the decoupling resistor R23 all contribute to improved synchronisation of the timebase.

## The Power Supplies

Five a.c. supplies are required from the mains transformers, they are:

1. $6 \cdot 3 \mathrm{~V}$ at $0 \cdot 6 \mathrm{~A}$ for the c.r.t. heater (T2)
2. 250 V at 2 mA for the e.h.t. multiplier circuit (T2)
3. 15 to 22 V at 500 mA for the low voltage line (T3)
4. 250 V at 50 mA for the high voltage 300 V d.c. line (T1)
5. $6 \cdot 3 \mathrm{~V} 0 \cdot 6 \mathrm{~A}$ for indicator lamps (T1)

The leads from the oscilloscope chassis are taken to the transformer subchassis and terminate in a multiway plug. It is suggested that constructors utilise a 10 way Jones plug and socket, for the inter-connection.

## components list

| Resistors |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | $4 \cdot 7 \mathrm{k} \Omega$ | R25 | 10M $\Omega$ |
| R2 | $2 \cdot 2 \mathrm{k} \Omega$ | R26 | $12 \mathrm{k} \Omega$ |
| R3 | $47 \mathrm{k} \Omega$ | R27 | $12 \mathrm{k} \Omega$ |
| R4 | $100 \Omega$ | R28 | $3 \cdot 3 \mathrm{M} \Omega$ |
| R5 | 8.2k $\Omega$ | R29 | $18 \mathrm{k} \Omega$ |
| R6 | $1 \mathrm{k} \Omega$ | R30 | 47k 11 W |
| R7 | 8.2kS | R31 | $120 \Omega$ |
| R8 | 2.2k $\Omega$ | R32 | 47k 1 1W |
| R9 | $1.8 \mathrm{k} \Omega$ | R33 | $3 \cdot 3 \mathrm{M} \Omega$ |
| R10 | 68k $\Omega$ | R34 | 2.2M $\Omega$ |
| R11 | $390 \Omega$ | R35 | $2 \cdot 2 \mathrm{M} \Omega$ |
| R12 | $56 \Omega$ | R36 | 10k 1 W |
| R13 | $82 \mathrm{k} \Omega$ | R37 | $10 \mathrm{k} \Omega 1 \mathrm{~W}$ |
| R14 | $470 \Omega$ | R38 | 1-2kS 1 W |
| R15 | 5-6k | R39 | $390 \Omega 1 \mathrm{~W}$ |
| R16 | $1 \mathrm{M} \Omega$ | R40 | $1 \cdot 2 \mathrm{k} \Omega$ 1 W |
| R17 | 22k $\Omega$ | R41 | $1 \cdot 2 \mathrm{k} \Omega$ 1 W |
| R18 | 1-5M $\Omega$ | R42 | 390 kS 1 W |
| R19 | 10k $\Omega$ | R43 | 8.2k $\Omega$ |
| R20 | $82 \mathrm{k} \Omega$ | R44 | $1 \mathrm{M} \Omega$ |
| R21 | 8-2kS | R45 | $680 \mathrm{k} \Omega$ |
| R22 | 47 $\Omega$ | R46 | $100 \mathrm{k} \Omega$ |
| R23 | $470 \Omega$ | R47 | $100 \mathrm{k} \Omega$ |
| R24 | $680 \Omega$ |  |  |

All $\pm 10 \% \frac{1}{2} W$ carbon except where stated otherwlse.

## Transistors:

Tr1, Tr2, Tr5, Tr8 BC109
Tr3, Tr4, Tr9, Tr10 MJE340
Tr6 ASY26
Tr7 TIS43

## Diodes:

D1 1N4148 or 1N914
D4, D5, D6 1N5054 or PL4007
D7, D8 400 p.i.v. 1 A
D2 12 V 1 W
D3. 18 V 1 W

## Transformers:

T1, T2 Primary $200-250 \mathrm{~V} 50 \mathrm{~Hz}$
Sec. 250V $60 \mathrm{~mA}, 6.3 \mathrm{~V} 2 \mathrm{~A}$
T3 Primary 200-250 50 Hz
Sec. 18V1-25A

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Capacitors:
C1 \(100 \mu\) F elect 25 V
C2 \(0.47 \mu \mathrm{~F} 250 \mathrm{~V}\)
C3 \(0.1 \mu \mathrm{~F}\)
C4 \(0.022 \mu \mathrm{~F}\)
C5 \(0.68 \mu \mathrm{~F}\)
C6 \(0.1 \mu \mathrm{~F}\)
C7 \(0.02 \mu \mathrm{~F}\)
C8 \(0.005 \mu \mathrm{~F}\)
C9 \(0.001 \mu \mathrm{~F}\)
C10 \(0.0005 \mu \mathrm{~F}\)
C11 \(100 \mu \mathrm{~F}\) elect 25 V
C12 \(0.1 \mu \mathrm{~F}\)
C13 \(100 \mu \mathrm{~F}\) elect 25 V
C14 \(100 \mu \mathrm{~F}\) elect 25 V
C15, C16, C17 \(0.47 \mu \mathrm{~F} 250 \mathrm{~V}\)
C18, C19, C24 \(50 \mu \mathrm{~F}+50 \mu \mathrm{~F}+50 \mu \mathrm{~F}\) elect 350 V
\(\mathrm{C} 20, \mathrm{C} 26 \quad 32 \mu \mathrm{~F}+32 \mu \mathrm{~F}\) elect 350 V
C21, C22 \(500 \mu \mathrm{~F}\) elect 25 V
C23, C25 \(250 \mu \mathrm{~F}\) elect 50 V
C27, C28, C29, C30 0.47 F F 1000 V
Cx see text
```

Potentiometers:
VR1 2M $\Omega$ carbon
VR2 $2 \cdot 5 \mathrm{k} \Omega \mathrm{w} . \mathrm{w}$. linear
VR3 $50 \mathrm{k} \Omega \mathrm{w} . \mathrm{w}$. linear
VR4 $25 \mathrm{k} \Omega \mathrm{w} . \mathrm{w}$. linear
VR5 $25 \mathrm{k} \Omega \mathrm{w} . \mathrm{w}$. linear
VR6 $250 \mathrm{k} \Omega$ carbon
$\left.\begin{array}{ll}\text { VR7 } & 250 \mathrm{k} \Omega \\ \text { VR8 } & \text { carbon } \\ \text { VR } & 250 \mathrm{k} \Omega \\ \text { carbon }\end{array}\right\}$ good quality well insulated
VR9 50k $\Omega$ carbon

CRT: 3BP1

Switches:
S1 2 pole c/o slide
S2 1 or 2 pole 6 way rotary. Only 1 pole used
S3 On/oft mains toggle switch
JK1 Closed circuit p.o. type jack

## Miscellaneous :

Veroboard, $0 \cdot 15$ in matrix 3 tins. $\times 17$ ins. Veropins. 2, 4, 6BA screws, nuts, washers and spacers, panel lamps, coaxial sockets, systoflex, cleats, grommets, chipboard, laminated plastic sheet, 4 instrument handles, 8 rubber feet, aluminium for metalwork.



Fig. 2 The complete Veroboard layout for the oscilloscope.

The tube heater winding must withstand 1000 V to the chassis. If the insulation breaks down it will put the whole e.h.t. voltage between heater and cathode of the c.r.t. The writer has not had this fault occur on any standard mains transformers that he has used. Well insulated twin flex of the type used for mains wiring is suitable for the c.r.t. heater leads.

Three rectifier diodes are used in the e.h.t. multiplier circuit. Although this type of circuit suffers from poor regulation, in this case, where the current required is only about 1 mA it is quite stable.

The capacitors C28, C29 C30 help to maintain good regulation. The diodes are arranged to give a negative output, the positive end of the chain is at earth potential.

The circuit is so arranged that the 700 V e.h.t. supply and the 300 V line are in series. Therefore the voltage across the c.r.t. from the grid to the final anode, is equal to the sum of the two voltages.

The c.r.t. resistance network acts as a bleeder across the e.h.t. and the smoothing resistor R47 and the network should be fitted before the circuit is tested. It will limit the e.h.t. voltage and prevent possible damage to the smoothing capacitor C27.

The $1 \mathrm{M} \Omega$ resistor R 44 may be included in the circuit if flyback blanking is to be added later. Because of the unusual layout of the e.h.t. multiplier circuit extra care must be taken in layout and wiring.
The low voltage line is supplied from transformer T3 which gives an output of between 15 and 22 volts, the bridge rectifier being rated at 400 V p.i.v. at 1 A and the reservoir and smoothing capacitors at 50 V . The smoothing resistor R42 has a value of $390 \Omega$ and the zener diode D3 stabilises the line at 18 V . The Y amplifier and the timebase circuit have separate smoothing components to reduce inter-action.

The high voltage 300 V d.c. line is supplied by the bridge rectifier D8 which is rated at 400 V 1 A . The reservoir capacitor C 26 is $32 \mu \mathrm{~F}$ and is of the can variety. Each deflection amplifier has its own decoupling components to prevent crosstalk and the astigmatism and $X$ shift potentiometers are in parallel across the 300 V d.c. line and act as bleeders.

When the writer commenced his experiments with this oscilloscope, the method used for X and Y shift was similar to that employed in valved instruments, where the deflection plates were coupled to the valve anodes through capacitors and the shift voltages were determined by potentiometers across the positive end of the network. This method has been retained for the $X$ deflection plates, the $X$ amplifier being a.c. coupled throughout.

The $Y$ amplifier is d.c. coupled and the $Y$ shift is determined by the potential at the collectors of Tr3 and Tr4. This means that the signal level at Tr3 base must be matched by that at $\operatorname{Tr} 4$ base to keep the trace on the screen. The X shift can be set and needs no further attention, but the $Y$ shift must be adjusted for positive or negative going signals and for changes in amplitude.

## The Veroboard Panel'

The Veroboard panel is 24 holes (or strips) wide and 83 holes long. This is cut from a standard 17 in . $x \quad 3^{3}$ in. Veroboard panel. The matrix is $0 \cdot 15 i n$. When working on the panel it is essential to make all joints with the minimum of solder. Where flexible leads are taken to components on the Veroboard, Veropins or the wire ends of components already attached to the copper strips should be used as anchoring points.


Photograph showing the completed oscilloscope. The three controls on the right hand side of the chassis are $x$ linearity, $X$ shift and astigmatism.



## SHORT WAVE DX

## by MALCOLM CONNAH

JUDGING from some of the letters and enquiries that I receive it would appear that many of you do not know of the existence of The World Radio and TV Handbook.

The book contains a list, by countries, of all the Broadcasting stations in the world. Each entry shows details of the station schedule including frequencies and language used; other details given are the station address and its QSL policy. The interval signal of the station is given along with the opening announcement which is the easiest way of identifying the station.

The first section of the book has various articles on Broadcasting subjects, which are useful to beginners and experienced DXers alike. The final pages of the book contain a listing, by frequency, of all the stations complete with call-sign and transmitter power.

The book is available through most good bookshops, the price is $£ 3$ which is a small price to pay for such a mine of information.

## DX News

BANGLADESH: Radio Bangladesh now starts the English service at 1700 instead of 1715 on frequencies of 11650 and 15520 kHz .

GABON: Plans are afoot for the installation of several 300 kW shortwave transmitters to be used by both ORTF and. Radiodiffusion TV Gabonaise. Libreville has been heard on the new frequency of 7130 from 1230 to 1430 .

GRENADA: Radio Grenada, formerly Windward Islands Broadcasting Service, has moved from 11930 to 15105 kHz for its transmissions to the U.K. at 1945-2130.

MONGOLIA: Radio Ulan Bator now also broadcasts programmes in English and French to Africa at $2000-2030$ on 17780 and 17860 kHz . The programmes in English are broadcast every Wednesday and Saturday, and in French every Tuesday and Friday. There are also programmes in English daily, except Sunday evening and Monday morning, at $1200-1250$ on 17780 and 17860 , and at $2200-2230$ on 11810 and 11860 kHz .

## Readers' Logs

The first log this month comes from Roy Patrick of Derby who returns to the page after a considerable absence, Welcome back OM. Roy's equipment consists of a Trio 9R59D receiver and an Eddystone 840. Stations logged included:

3240 R. Baghdad, Iraq in Arabic at 2000.
4945 R. Colosal, Colombia at 0700.
4980 Ecos del Torbes, Venezuela at 0605.
4995 R. Brazil Central at 2200.
11650 R. Bangladesh in English at 1700.
11710 RAE, Argentina noted at 2300.
11720 R. Nacional, Brazil, fair at 2100.
11725 R. Ceylon in English 1800-1830.
11790 R. Australia to SE Asia at 1800.
11800 R. Ceylon in Hindi, good at 1830.
Michael Johnson of Hockley in Essex describes his equipment as follows: "I use an ex-radiogram, 6 valve, Ferguson receiver; coupled with the dipole of an old 405 line TV aerial which works better than my 50 foot dipole on 31 metres!" This equipment enabled him to hear the following stations:
6050 RAI, Italy in English at 1935.
6070 R. Sofia, Bulgaria in English at 1930.
6185 R. Norway in English at 1700
6580 R. Pyongyang, N. Korea at 1900.
7290 Trans World Radio in English at 1045.
9545 R. Ghana, Accra in English at 2145.
9670 R. Trans-Europe in English at 2000.
9840 Voice of Vietnam at 1915.
11880 Voice of Turkey, Ankara noted at 2200.
15185 R. Finland in English at 1800.
15415 R. Kuwait in English at 1645.
Messrs. Wormleighton and Fletcher of Rencomb College, Cirencester have sent in another excellent $\log$ using the following equipment: HRO with 8 metre folded dipole; Astrad-Altair with 150 foot longwire, Bush PB63 with 35 foot long-wire.
5990 HCJB, Quito, Ecuador in English at 0825.
6050 RAI, Italy in English at 2030.
7235 R. Australia in English at 1500.
9525 RSA, South Africa noted at 2215.
9710 HCJB, Quito, Ecuador in English at 0715.
9715 R. Nederland, Bonaire, English at 0845.
9805 R. Cairo, U.A.R., in English at 2200.
11745 HCJB, Quito, Ecuador in English at 0730.
11880 Voice of Turkey, Ankara. English at 2200.
11920 RNE, Spain in Spanish at 1300.
11945 R. Voice of the Gospel, Ethiopia at 1930.
11970 RSA, South Africa at 1900, News in English.
15415 R. Kuwait in English at 1730.
21545 R. Ghana, Accra in English at 1500.
21595 R. Canada International noted at 1640 .



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MEDIUM WAVE BROADCASTS by CHARLES MOLLOY

John thorburn (Glasgow) has used his Vasco Gold Star radio to hear CHER Sydney, Nova Scotia on 950 kHz ; WBT Charlotte, North Carolina on 1110 kHz ; Radio Bermuda 1340 kHz ; Voice of America Kavalla, Greece 791 kHz ; Radio Zagreb, Yugoslavia 1133 kHz . John also logged the BBC local radio outlets at Blackburn on 850 kHz . Sheffield 1034 kHz ; Leeds 1106 kHz ; Newcastle 1457 kHz ; Stoke 1502 kHz ; Bristol 1546 kHz and Manx Radio, Isle of Man on 1594 kHz .

Dominic Glynn (East Grinstead) has a Philips transistor receiver and a 100 ft . longwire antenna. He reports hearing programmes in English from Radio Sweden 1178 kHz at 2300 hrs GMT; Trans World Radio Montecarlo 1466 kHz at 2230 hrs and Radio Berlin International 1511 kHz at 1815 hrs . Dominic has also logged Radio Tirana, Albania 1394 kHz at 2230 hrs and BBC Radio Stoke 1502 kHz at 1045 hrs .

From the BBC comes news that Radio Solent is now broadcasting on two frequencies, 998 kHz and 1594 kHz . The new outlet on 1594 kHz brings the

## VHF/FM

## by SIMON DAVID

HAVE you been suffering from "Sporadic-E" lately? If so we would like to hear from you. Sporadic-E is the name given to a disturbance in the " $E$ " region of the ionosphere. It is most likely to occur in the summer months (U.K.) and gives rise to some odd goings-on on the v.h.f. bands up to about 100 MHz .

Although almost impossible to predict accurately, such manifestations are in long distance reception, interference on television and radio and interaction between signals from one source and another, often several hundreds or even thousands of miles apart. Stations operating on close frequency allocations are susceptible and in particular those on v.h.f. mobile radio systems often fall victim.

Greetings in particular this month to listeners who can now pick up local radio on their portables and in cars in Leeds, Huddersfield, Barnsley, Dewsbury, Wakefield, Castleford, parts of Halifax, Bradford and Harrogate, Barnsley, Doncaster, Worksop, East Retford and Rotherham. In case you are not aware, you should now be able to drive to the lilt of BBC Radio Leeds ( $92 \cdot 4 \mathrm{MHz}$ ) or Radio Sheffield ( $97 \cdot 4 \mathrm{MHz}$ ).

The old Meanwood Park transmitter on $94 \cdot 6 \mathrm{MHz}$ and Boston Park, Rotherham, transmitter on $95 \cdot 05 \mathrm{MHz}$ have closed and all transmissions from these two stations now come from Holme Moss near Huddersfield. Sheffield listeners can still tune in on 88.6 MHz , but all others tuning to 97.4 MHz may need to turn their aerial round so that it is directed at Holme Moss (also home of BBC television). Aerials that are already rigged on the roof or chimney outside and directed at Holme Moss for Radios 2, 3 and 4 are likely to be suitable for the local radio stations also.
service to Bournemouth, Poole and Wimborne Minster while the existing service on 998 kHz for the Southampton and Portsmouth areas is unaffected

Medium wave DXers who go abroad for their holidays have the opportunity to try the band from a new location. In Spain there are many low power local stations, some of which would be rarities if heard in this country and even a pocket sized transistor portable will pull them in. For those interested in keeping in touch with events at home there is the BBC Radio 2 transmission on 200 kHz ( 1500 m ) on the long waves which can be heard over a large part of Europe after dark. Visitors to Majorca can hear Radio Mallorca (EAJ13) on 800 kHz ; Radio Popular de Mallorca (EAK18) on 1268 kHz ; Radio Juventud de Palma Mallorca (EFJ45) on 1385 kHz . On the Costa Brava there are Radio Barcelona (EAJl) on 827 kHz ; Radio Juventud Barcelona (EFJ15) on 1025 kHz ; Radio Espana de Barcelona (EAJ15) on 1124 kHz ; Radio Sabadell (EAJ20) on 1475 kHz ; Radio Gerona (EAJ38) on 1520 kHz . At Benidorm there are Radio Popular de Alicante (EAK31) on 1394 kHz ; Radio Gandia (EAJ23) on 1457 kHz ; Radio Alicante (EAJ31) on 1520 kHz and La Voz de Alicante (EFE8) on 1570 kHz . Those going to the Costa del Sol have the opportunity to hear Radio Gibralter on 1484 kHz which broadcasts in English and Spanish; Radio Ceuta (EAJ46) on 1106 kHz which is located in a Spanish enclave in Morocco; Radio Juventud de Malaga (EFJ56) on 1133 kHz ; Radio Popular de Malaga (EAK11) on 1430 kHz and Radio Costa del Sol (ECS15) on 1570 kHz .

Some transmitters use slant polarisation to assist where vertical receiver aerials are used (such as on cars). One such is used for Radio Derby which is transmitted from Sutton Coldfield, Birmingham, on $96 \cdot 5 \mathrm{MHz}$. If you are not sure on the polarisation for your area you can ask at any local BBC radio offices or write to the Engineering Information Dept., BBC, Broadcasting House, London W1A 1AA; please enclose a stamped addressed envelope.

Now for some quick quotes from some of the letters received: W. F. Kitching in Shropshire has a Grundig "Yacht Boy" 210 with telescopic aerial and has picked up Radio Telefis Eirean $95 \cdot 3 \mathrm{MHz}$. He looks forward to police inactivity so that he can hear Radio Na Gaeltachta, Eire, on $97 \cdot 0 \mathrm{MHz}$.

On the other side of the Irish Sea, Des Walsh in Tipperary uses a Leak Troughline-3 and a BASF CC9300 Radio recorder and points a J-Beam FM6S and FM4S at South Wales and South West England. He has bagged Wenvoe, Haverfordwest, Blaen-plwyf, North Hessary Tor, Redruth and Radio Bristol. Turning north-east he can pick up Belfast and Radio Merseyside. Here's the crunch! With the help of tropospherics he can hear ORTF from N. W. France.
D.J. is a 14-year-old from Egham, Surrey, and is one of many who has heard the London Independent Radio transmissions on Radio Classic $94 \cdot 4 \mathrm{MHz}$. Hope his parents won't get annoyed when they find out that he was listening to "an extra programme" at $01 \cdot 05$ Easter Sunday morning. Was this a "Jolly Roger" operation?

Anybody heard broadcasts from the North Sea Radio Telephone Company? Graham Wilson has in Bordon Hampshire and wonders who was responsible. The transmission was heard on much of the $88-108 \mathrm{MHz}$ band (but was strongest at 91 MHz ) on March 5th.


## SHORT WAVES

## by DAVID GIBSON, G3JDG

IT'S getting hotter in more senses than one. The summer season brings great hotness with it and it is known in this scribe's shack as the Equinox of the molten ear'ole-a disease common to all wearers of headphones during periods of great warmth.
The other sense is a rumour to ban a.m. from the Amateur bands, notably the l.f. regions of 1.8 and $3 \cdot 5 \mathrm{MHz}$. What do readers think about this? Shall we settle for s.s.b. and c.w. only?

A staggering piece of news for professional callsign changers. The latest act in the callsign circus is to change it just for a particular contest. The result is CR6 becoming CQ6 (a really clever choice$\mathrm{CQ})$ for the WPX contest. A little bird also tells me that MP4TEE is now A6XF.

Best piece of news on the callsign front, and one for some genuine rejoicing in Amateur circles, is that the People's Republic of China will probably be allowing/issuing callsigns in the not too distant future. It'll make the bands even more crowded but

a big welcome to the Chinese Amateurs as and when they appear on the bands.

In the April issue, mention was made of photographs showing readers' stations. First person to take up the gauntlett is Graham Bleakley who is 15 and lives in Cumbernauld New Town, Scotland. The gear shown is a "trusty old CR100". Graham is the one on the left with all the hair, and the CR100 is on the right, with all the knobs. No mention of what the tape recorder is for but Graham does say he reckons to become a 68 with a bit of help from the May 1974 RAE. No word of the antenna, but whatever it is, it pokes out of the windows of 82 Ash Road.

Info from G3RPJ that the Stratford on Avon Radio Club will have rigs working on $1 \cdot 8 \mathrm{MHz}, 14 \mathrm{MHz}$ and 144 MHz (a.m. f.m. and r.t.t.y.) at the Town and Country Festival on August $25 / 26 / 27$. Place is the Royal Showground, Stoneleigh, Kenilworth, Warwickshire. The stations will stay on the air in the evenings after the show.

Karl Muller (Mbabane, Swaziland) has a JR-500SE 7 MHz inverted V and a lot of patience. Rewards for same has given him 148 countries heard on 7 MHz . On 7 MHz c.w. Karl bagged; CE3ED, CE5HP, CX1BBL, CX9BT, FC9VN, FG7TG, FH8CY, KøALL, KH6AQ, KH6RS, SV1DO, TI2PZ, VP9GR, WN3TGR, WNøHYN, ZP5AL, 4K1A, 9F3USA, 9L1GC. On s.s.b., the latest log reads; CT2AJ, KC6SK, MP4BJP, OY7BD, WB6VGI/VQ9, ZC4EJ, ZD9GC, 4W1AF, 6W8DY.

Before going on with logs, I see that the May 1973 issue of Radio Communication, the journal of the RSGB, publishes a full list of intruder stations complete with all sorts of information; frequency, date, location, source etc. This seems a useful coincidence in view of previous remarks made in this column. Single copies of the journal are available to nonmembers at 30 p plus postage.
J. Wright (Loughborough) homebrew converter, 960 receiver, 3 -element beam at 30 ft . sends in a log for 70 MHz (Yippee). Stations bagged include: G3CDG/P, G3HCW/P, G3HVI, G3LVP/P, G3NQV/P, G30NP, G3SFT/P, G3TOM/P, G3VER/P, G3VPF/P, G3VPK, G3WMR/P, G3ZVK, G4ALE/P, G4BEZ/P, G4BLQ, G4BPY, G4BZO, G5DF, GD2HDZ, GW3MHR, GW30BD/P, GW3WOS, GW4ABR/P, GW4BGG/P.
P. Newman (Thame) sends in a "Heard in the 144 MHz and 70 cm Contest" log. Pickings on 70 cm ; G8DOR/P, G88GHR/P, G3NNG/P, G5DF, G8FBG/P. Two meter goodies were; G8DWC/P, G2DRT/A, G8CIB/P, G8GSX/P, G8GTD, G8FBG/P, G8FTL, G8FZL/P, G3FZL/P, G3KIN/P; G3OSS, G3NNG/P, GW4ABR/P.
Contests for the month of July include: July 7/8, v.h.f./u.h.f. Jubilee contest (R.S.G.B.); $14 / 15$, s.s.b. field day; $15, \mathrm{DF}$ qualifying round at Coventry; 22, 432 MHz portables contest; August 4/5, YO DX Phone and c.w. contest; August 5, DF qualifying round (Salde).

[^3]
## AMATEURBANDS Short Wave/VHF

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| 6AQS | . 24 | 35W4 | . 25 | ECH42 | . 69 | KT01 | -65 | PL82 | $\cdot 81$ | UF41 | -58 |
| 6AT6 | . 20 | 35Z4GT | - 25 | ECH81 | . 29 | K T66 | .78 | PL63 | -8 | UF89 | . 80 |
| 6AU6 | -20 | 50CD6 | -68 | ECH83 | . 88 | LN 319 | . 56 | PL84 | -30 | UL41 | -4 |
| 6BA6 | -20 | 807 | . 55 | ECH84 | . 88 | LN829 | . 80 | PL500 | . 68 | UL84 | - 0 |
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| $6 \mathrm{BJ6}$ | $\cdot 41$ | AC/VP2 | -77 | ECL82 | . 29 | N78 | 41.05 | PM84 | -30 | UY41 | 87 |
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| 6 JSGT | -20 | DAF91 | . 25 | EF80 | . 28 | PC97 | - 85 | PY82 | . 26 |  |  |
| 6J7G | . 24 | DAF96 | . 86 | EF85 | . 28 | PC800 | . 29 | PY83 | . 86 | Trena |  |
| 6V6GT | -28 | DF91 | - 80 | EF86 | . 80 | PCC84 | . 29 | PY88 | . 3 | AC107 | . 17 |
| $6 \times 4$ | . 80 | DF96 | . 86 | EF89 | . 26 | PCCBS | . 28 | PY800 | .11 | AC127 | -18 |
| $6 \times 5 \mathrm{CT}$ | -88 | DH77 | . 20 | EF91 | . 18 | PCC88 | . 88 | PY801 | - 81 | AD140 | -87 |
| 10P13 | .58 | DK91 | . 80 | EF92 | . 80 | PCC89 | . 48 | R19 | .80 | AF115 | -2 |
| 12AT7 | . 20 | DK92 | . 48 | EF98 | .70 | PCC189 | - 48 | R20 | .70 | AF116 | 0 |
| 12AU7 | . 21 | DK96 | - 48 | EF183 | . 27 | PCC805 | - 70 | U25 | .70 | AF117 | -90 |
| 12AX7 | . 82 | DL92 | 80 | EP184 | . 89 | PCF80 | . 26 | U26 | - $4^{4}$ | AF125 | -17 |
| 19BGAG | . 78 | DL94 | -47 | EH90 | .36 | PCF82 | . 88 | U47 | .78 | AF127 | -17 |
| 20 Fr 2 | -67 | DL96 | . 88 | ELS3 | . 85 | PCF88 | . 46 | U49 | -70 | OC44 | . 18 |
| 20P3 | . 75 | DY86 | -28 | EL34 | . 50 | PCF800 | . 18 | U52 | . 81 | OC45 | . 18 |
| 25LbgT | . 19 | DY87 | . 28 | EL41 | -68 | PCF801 | . 28 | U78 | -80 | OC71 | -18 |
| 25U4CTT | . 67 | DY 802 | . 30 | EL84 | . 88 | PCF802 | . 80 | U191 | . 85 | $0 \mathrm{C72}$ | -18 |
| 30 Cl | . 26 | EABC80 | . 82 | EL90 | -24 | PCFB05 | - 87 | U103 | . 81 | $0 \mathrm{C75}$ | -1 |
| 80 Cl 15 | . 58 | EAF42 | . 50 | EL500 | . 68 | PCF808 | . 50 | U251 | -81 | 0 Cal | -18 |
| $30 \mathrm{C17}$ | .78 | EB91 | . 12 | EM80 | .86 | PCF808 | - 65 | U301 | -88 | OCs1D | -18 |
| 30 Cl 8 | . 57 | EbC33 | . 45 | EM81 | .38 | PCL82 | - 80 | U329 | - | OCaz | -19 |
| 30 Fs | -64 | EBC41 | . 49 | EM84 | .82 | PCL83 | . 56 | U801 | . 75 | OC82D | -18 |
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WIth the Short Wave Bands becoming more crowded every year it becomes increasingly necessary for the listener to be able to determine the frequency to which his receiver is tuned. Conversely, if the receiver is accurately calibrated the listener is able to tune to a desired frequency to listen for a particular station.


Fig. 1 Circuit showing the bandspread ganged capacitor added to the exist/ing circuit.

The latter part of this article deals with a method of receiver calibration which costs less than a pound. The only requirement is that the receiver has a band-
spread control with a reasonable scale. The first part of the article, therefore, deals with adding a suitable bandspread control to a receiver which is lacking in this respect.

## ADDING BANDSPREAD

The addition of a bandspread control to a receiver which does not have this facility is probably the most effective, yet simple. method of improving the performance of the set. The total cost is little more than $£ 1$ so the project is well within the means of the average listener.

All superhet receivers have a main tuning control which is either a two or three gang variable capacitor. This is shown as VC1/VC2/VC3 in Fig. 1. The bandspread control required for the project is a two or three gang (depending upon the number of gangs of the main tuning) miniature variable capacitor each section having a capacitance of approximately 15 to 20 pF . The most suitable type is that often used for the tuning of v.h.f. receivers, usually having a capacitance of 17 pF per section.
The bandspread control is represented by VC4/ VC5/VC6 in Fig 1. Each section of the bandspread


Fig. 2 A typical calibration chart produced by the method described in the article.
capacitor is wired in parallel with a section of the main tuning control. The new control should be mounted as near as possible to the existing variable capacitor with the wiring as short and straight as possible. In order to retain the previous calibration of the receiver, the bandspread control should be half closed and the trimmers TC1/TC2/TC3 unscrewed slightly to compensate for the additional capacitance of the bandspread control.

## BANDSPREAD CONTROL

The bandspread control should be fitted with a knob which has a 0 to 100 scale; the larger the knob that can be accommodated on the receiver the better the tuning performance will be. A knob with integral slow motion is better still.

## CALIBRATION

The lowest cost method of calibrating a receiver is by drawing calibration charts for the various frequency ranges of interest, using the bandspread control. The best graph paper to use is that which has each large division sub-divided into ten smaller divisions. A separate chart should be drawn for each band but some of the wider bands will require two charts as the bandspread control will not cover the entire band with one setting of the main tuning.

The main tuning is adjusted so that the bandspread will cover the band being calibrated. This position of the main tuning is noted by sticking a piece of tape on the dial or by reference to the receiver's logging scale if one is fitted. As an example, the author's receiver was calibrated on the 19 metre band, being fitted with a 0-100 logging scale, and with the main tuning set at 37 the bandspread control covered the whole band.

The next stage is to do some concentrated listening on the band, trying to hear those stations of which the frequency is known and plotting these on a graph similar to Fig. 2. The stations heard by the author were as follows:

Station
WWV
Radio Cairo
RSA, S. Africa
VOA, Tangier
RAI, Rome
Radio Moscow

| Frequency | Bandspread Setting |
| :--- | :---: |
| 15000 kHz | 0 |
| 15150 kHz | 19 |
| 15200 kHz | 26 |
| 15300 kHz | 43 |
| 15400 kHz | 65 |
| 15450 kHz | 80 |

When all these points have been plotted a smooth curve is drawn between them giving the result shown in Fig. 2. This procedure is repeated for all the bands required by the listener.

The method of calibration by plotting frequencies is tedious but, once done, the graph can be used again and again very simply. One of the basic ideas behind the article was that the minimum of expense was involved. The reader will have to spend some time drawing up the graphs but will have spent very little money.

The use of a crystal calibrator would, of course, speed up the process of drawing the charts. The The 3 -range Crystal Marker by R. F. Graham was published in the February 1973 issue of PW and this is ideal for the job, being both simple and inexpensive.

## USING THE CHARTS

It is possible to use the charts by simply returning the main tuning to the marked position from which the chart was drawn. This is not very accurate however, and the following method is recommended. When returning to a given band a search is made for one particular station the frequency of which is known, say 15250 kHz . Reference to the graph shows that this should appear at 34 on the bandspread scale. Both the main tuning and the bandspread are then adjusted until the station appears at this bandspread setting. The controls are now set for accurate listening on the band.

Having set up the receiver it is possible to use a chart in two ways. First, it is possible to determine the frequency of a station which has been tuned in by converting the bandspread reading to frequency, secondly, it is possible to tune to any particular frequency, to look for a station, by determining the correct bandspread setting for that frequency and adjusting the control accordingly.

## 

Practical Wireless will be launching a new series of PW Datacards in the autumn. These will provide the radio, television, audio and electronics constructor with some of the background information he needs to understand his subject.

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| 6ATK | -18 | DH77 | - 18 | ECH81 | - 26 | EY86 | 27 | PCL84 | -81 | U329 | * |
| 6AQ5 | -23 | DK91 | . 28 | ECLs0 | -27 | E280 | -19 | PCL85 | . 86 | UABC80 | 29 |
| $6 \mathrm{BW7}$ | . 48 | DK92 | -47 | ECL82 | -27 | EZ81 | 21 | PCL86 | -36 | UBF89 | -28 |
| 6 F1 | -57 | DK96 | -43 | ECL86 | $\cdot 32$ | KT61 | . 88 | PFL200 | $\cdot 45$ | UCC85 | -32 |
| $6 \mathrm{~F}^{2} 23$ | -64 | DL92 | -28 | EF39 | . 43 | KT86 | -75 | PL36 | $\cdot 45$ | UCH42 | . 56 |
| 6 F 25 | -49 | DL94 | -46 | EF41 | . 56 | N78 | 81.00 | PL81 | -41 | UCH81 | -28 |
| 12AU7 | -17 | DL96 | -36 | EF'80 | -22 | PC86 | . 42 | PL8: | -29 | UCL82 | 88 |
| 25L6GT | . 18 | DY86 | . 21 | EF85 | -26 | PC88 | - 42 | PL83 | -81 | UF41 | -49 |
| 30 Cl 5 | . 68 | DY87 | . 21 | EF86 | -27 | PC97 | . 84 | PL84 | . 28 | UF89 | 28 |
| 30 Cl 17 | $\cdot 78$ | DY802 | . 28 | EF89 | -24 | PC900 | -28 | PL500 | -58 | UL41 | -5\% |
| 30 Cl 18 | -55 | EABC80 | -28 | Ef91 | -15 | PCC84 | -27 | P1.504 | . 58 | UL84 | -87 |
| 30 F 5 | . 80 | EBC33 | $\cdot 43$ | EF94 | -26 | PCU89 | 41 | PY81 | -28 | UY41 | -25 |
| $30 \mathrm{FL1}$ | - 59 | EBC41 | -47 | EF183 | . 25 | PCC189 | - 46 | PY82 | . 28 | UY85 | . 88 |
| 30FL14 | . 63 | EBF89 | -27 | EF184 | -27 | PCF80 | -25 | PY800 | . 80 | W77 | -4 |

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MR. J. TURNER tells us that he managed to purchase a Marconiphone model V2 receiver at a local auction. He has restored it to work. ing order and it performs very well-especially on long waves. Tuning is accomplished by sliding in various ebonite slabs-each covering a different range. Each contains an "embedded" coil which is tuned by copper "spades." There is a "regenerator' unit" which does not seem to fulfil any useful purpose and Mr. Turner would like to hear from any readers who can comment on this. The valves are of the D.E.R. type (dull emitters). The h.t. supply is 90 V and l.t. 3 V . The set still bears its original transfers and is in very good condition throughout. Inside the lid there is an ivorine plate giving the serial number of the set as "installation no. S/A 2535.

Mr. Turner would like any information on this set that readers could supply.

We found a reference to the V2 in a catalogue kindly lent to us by Dr. Brodribb-another vintage radio collector. It reads: "The Marconiphone V2 gives excellent results as a long-range instrument. By its reflex circuit, two valves do the work of three. It holds a remarkable record of results from overseas stations, including America. Cost of upkeep is comparatively negligible, and is perfectly simple to operate."
In c1926 the V2 could be obtained from Upfield and Sons (Motors) at Hastings, for the sum of $£ 10.5 \mathrm{~s}$.

The receiver complete with accessories, including two D.E.R. valves cost $£ 14.11 \mathrm{~s} .2 \mathrm{~d}$ and a dry cell combination including two D.E.3. valves cost £14.13s.8d. There was also a Marconi royalty of $£ 1.5$ s to pay.

Our old friend Chris Petsikopoulos from Greece tells us he has recently returned from holiday and writes:
"During that time I had the opportunity to make a great search which brought great finds, the most important of all was a French radio-set of the era 1917-1918, made by "DUCRETET", Paris, providing a 100 watt spark Transmitter and crystal detector receiver connected in a common tuning circuit through a change-over switch.

The tuning circuit consists of an Oudine coil with a slider for the aerial and a variable capacitor used only for reception, this meaning that the transmitter works on a standard wave length $(450 \mathrm{~m})$. The whole unit is housed in a compact wooden case $17 \times 12$ inches, and is in nice condition. In the case are housed the tuning coil, variable capacitor, sendreceive switch, mica condenser, high tension coil with interrupter, and a 10 amp . meter. Also connectors for key and headphones. On top of the set are aerialearth connectors, crystal detector, and spark-gap. Connectors for 12 V d.c. are on the right side of the case.

Connecting a 12 V battery, a 100 foot aerial and an earth, the set was able to work. The aerial was


Fig. 1: The circuit of the Marconi $V 2$ receiver re-drawn from the information supplied by Mr. J. Turner.


Chris Petsikodoulos" "Ducretet" $T x / R_{x}$.


The "Thomson-Houstor" receiver.
tuned with the slider for maximum current, 5-6 amp. giving a nice audible buzzing signal in a range of about 5-8 miles depending on the position of the car which was used for checking the range. The receiver has a range from $250-600 \mathrm{~m}$ and the reception of several broadcasting stations was able with good volume, the only difficulty being in finding a sensitive position on the crystal although the change-over switch provides a third position where the tuning circuit is off and the buzaing of the interrupter is then used to adjust the detector.

Shown are pictures of the above set and of a 1922 two valve Heterodyne made by "ThomsonHouston", Paris, valves are type R-5 of "La Radiotechnique" still working. The set is accompanied with a band switching frame aerial covering a wave length from 400 m to 3.000 m in three ranges "

Mr. H. E. Hunt, 68 Oundle Road, Thropston, Northants, quotes some prices he noticed for making one's own components.
"Your feature "Going Back" has caused me to reach for Vol. IV of "The Amateur Mechanic" whose mildewed covers contain the inspiration that set me building my first "Wireless Telegraph" set (1920-21).

There is no "Components List" because there were no components in those days but a "Specification of Materials" and I quote that portion for the variable condenser only:-

| 1 sq. ft of ${ }^{4} 4$ inch teak (to make box) | s. | d. |
| :--- | :--- | :--- |
| 1 sq. ft. of thin sheet zinc | 6 |  |
| 2 small nuts and bolts | 2 |  |
| 1 knob (off rubber stamp or screwdriver) | 2 |  |
| 2 small brass terminals | 3 |  |
| 8 ins. electric light flexible wire | 2 |  |
| 6 old quarter plate negatives | . |  |

Total cost 13
(The last item was for di-electric, not P.C.Bs.) 'These were the days of ebonite, teak, brass turning and 2lb. soldering irons (gas heated).

Such was the success of this "Long Distance Receiver"-Poldhu, Eiffel Tower and numerous spark transmitters were received-using a 6 ft . twin spreader aerial, 50 ft . long and 30 ft . high, that I was able to obtain parental financial backing (30/-) to build a single valve receiver.

The valve was an ungettered one of Dutch manufacture ( $15 /-$ ) which not only furnished sufficient light to work to but formed the nucleus of a receiver that occupied one half of the work bench.

But what a new world it opened up, the Hague concerts on Sundays, and England's first and unsurpassed compere P. P. Eckersley from 2.MT, at Writtle, Essex on Tuesday evenings.

There were also at this time some excellent telephony transmissions from local Northampton amateurs (2.TV.-5XH-5XG).

I started using the d.c. mains for h.t. long before eliminators were on the market, except that one had to put up with a complete loss of signals every time a tram passed 200 yards away.

One could write a book on the early days of amateur "wireless' but for myself I must hurry off to change an under-rated thyristor in the speed control of my wheel chair (or something like that). Tempus fugit!!

## FUTURE PLANS

Let us tell you why you should know about some of our future plans in Practical Wireless.
First, our autumn issues are being planned as the best yet; secondly, we will be doing what no other magazine has ever done before; thirdly, if you don't find out about these and order your copies" in advance, your newsagent is very likely to sell out before you get there.
Naturally, we cannot tell you everything now, but we can tell you what to look for next month, and in the following issues. Want to know more? Then keep your eyes on our "Leader" page and turn to pages 320, 334, 335 and 350 for further details in this issue.

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| ACY21 | 20D | BCY:2 | 15p | MJE340 | 50D | 0 C 201 | 75p | 2N696 | 15p | 2N3790 | 2.25 |
| ACY39 | 55p | BCY87 | 299 | MJE370 | 70p | 0 C 202 | 80p | 2N697 | 15p | 2N3819 | 35p |
| AD140 | 50, | BCZ11 | 60p | MJE520 | 75p | 0 C 203 | 50D | 2N706 | 100 | 2N3820 | 50p |
| AD149 | 50p | BD124 | 80p | MJE295 |  | OCP71 | 1.25 | 2N930 | 20p | 2N3866 | 85p |
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| AF188 | 40p | BF180 | 30p | NKT 217 | 740 p |  | 55p | 2N1307 | 25p | 2N5457 | 30 p |
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| BCl07 | 10p | BFY50 | 20p | $0 \mathrm{OC16}$ | 75 D | TIP3AA |  |  | 25p | 40250 | 50p |
| BC108 | 10p | BFY51 | 20p | $\mathrm{OC}_{2} 0$ | 95 p |  | 150 | 2N2:69 A |  | 40360 | 40 p |
| BC109 | 10p | BFY52 | 20p | $0 \mathrm{OC2} 3$ | 85 p | TIP35A |  |  | 15p | 40361 | 40p |
| BCl09C | 12p | BFY64 | 50 p | $0 \mathrm{OC} 2 \overline{5}$ | 40p |  | 2.50 | 2N2406 | 20D | 40362 | 50p |
| BC113 | 15 D | BFY90 | ${ }^{590}$ | OC28 | 65 p | TIP36A |  | 2N2926 |  | 40408 | 60p |
| BC117 | 20p | BLY 36 BSX20 | 8.00 150 | OC35 | 50p | TIP41.4 | 3.00 750 | ${ }_{2}^{\mathrm{cal}_{4} \mathrm{~N}_{4}}$ | 10p | 40486 40636 | 75 p 1.10 |
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No. 51
TOUCH-SENSITIVE SWITCH

## A series of simple transistor projects, using not more than twenty components.

Nowadays there is a tendency to veer away from electro-mechanical switches to electronic versions which have no moving parts. The reason is twofold; first there is less likelihood of failure and secondly there is a strange fascination in setting something in motion or switching on something without any apparent mechanical intermediary. This is already happening in applications such as lift control buttons and desk calculator keying so why not in a few domestic situations, or as a replacement for the Morse operator's key?

This month's circuit is a very simple way of providing touch sensitive keying and is capable of several types of output including an output that illuminates a low voltage lamp but the circuit can be quite easily modified to provide a relay drive
(rather negating the original sentiment of avoiding mechanical components!) or, better still, a logic (TTL) compatible output.

## Operation

Touch sensitivity is achieved by detecting the minute current that passes through the finger when a pair of contacts is bridged by the touch of the operator. The touch transducer in the prototype was made from a 1 in . square of 0.1 in . pitch Veroboard, with alternate copper strips paralleled together to form a contact pattern.

A more attractive touch plate could be made by printed circuit techniques and if this is done it is better to use a fibre-glass base. In either case the copper contacts need some protection from corrosion and this can be effected by lightly tinning the strips with solder.

The touch plate is connected between the supply


Circuit of the touch-sensitive switch, with alternalive TTL output circuit.


Layout of components on the Veroboard with details of the touch plate.
rail (through R1) and base of Tr 1 which should have low leakage current (beware of cheap "reject" transistors). When the plate is touched a very small current flows in the base/emitter circuit of $\operatorname{Tr} 1$ and this in turn permits a much higher current to flow between collector and emitter. Tr2 and Tr3 are connected as a Schmitt Trigger circuit; the emitter current from Trl flows mainly into the base of Tr2 and turns it on; this causes Tr3 to turn off and the potential at its collector starts to rise until base current in Tr4 is established. When this occurs the lamp LPl=lights. Alternatively, considering the TTL version, the output level falls to " 0 ".

## $\star$ components list



Removing the finger from the touch plate causes the base current to stop flowing in Trl ; current into the base of $\operatorname{Tr} 2$ thus stops and the latter starts to turn off. As this occurs Tr3 starts to draw base current through R3 and R5 and begins to turn on. As this happens the potential at Tr3's emitter starts to rise slightly and this (due to the feedback inherent in a Schmitt Trigger) causes $\operatorname{Tr} 2$ to turn off faster. At the same time the potential at $\operatorname{Tr} 3$ 's collector falls until sufficient base current into Tr4 can no longer be maintained. Tr4 thus turns off and the lamp goes out. Alternatively the TTL output goes to a logic level " 1 ".

## TTL Output

To obtain the TTL output version R 7 and zener diode D1 should be in circuit and lamp LPI omitted For relay operation LP1 should be replaced by a 6 volt relay. The components list has not taken the alternative versions into account.

## Note

A word of warning-the touch plate should not be used out of doors or with wet fingers because droplets of moisture bridging the conductors will provide sufficient current to make the circuit switch. Possibly this problem could be overcome' by carefully painting in the gaps between the strips with a good quality water repellent paint having a high gloss finish.

THE easily built unit to be described is used to provide a signal in the 2 metre Amateur band ( $144-146 \mathrm{MHz}$ ). When constructing or modify. ing apparatus for 2 metre use it can be very difficult indeed to locate the band or any part of it. Indeed in some areas, amateur activity is so low that many hours of experimenting may be wasted in tuning for non-existent transmissions. Experienced constructors will know to their cost that at v.h.f. finicky adjustments are often required and in the case of a tuning coil for example just one half turn too little or too much may result in the circuit being so far off frequency as to be useless for the purpose required. To overcome problems such as these this unit was quickly assembled-and at small cost.

The circuit of the device is shown in Fig. 1; it is by no means unique but rather the practical outcome of some earlier experiments. Basically a crystal-
controlled oscillator-Tril and associated itemsprovide harmonic output which is lightly audio modulated due to Tr 2 circuitry. The modulating section is by no means essential but it does enable the user to aurally recognise the v.h.f. signal being generated which is, in the case of the 6025 kHz crystal utilized, the twenty-fourth harmonic ( 6025 x $24=144 \cdot 6 \mathrm{MHz})$. Whether or not the final generated frequency is exactly at this figure is not too important provided it is in the 2 metre amateur band.

Inductor Ll is tuned by trimmer TCl to the crystal harmonic frequency, L2 merely being a low impedance untuned output link closely coupled to L1. In the f.e.t. source circuit inductor L3 is tuned to the crystal frequency by capacitor Cl , final fine tuning being accomplished by means of the dust core which when once set can be so left. The drain current taken by Trl when oscillating correctly is approximately 2 mA from a 9 V d.c. supply.


Fig. 1: Circuit of the complete unit


Fig. 2 : Component layout and wiring.

The circuitry around $\mathrm{Tr}_{\mathrm{r}} 2$ enables audio oscillations to be generated, transformer T1 providing the required collector-base feedback. The transformer used is a sub-miniature type driver transformer removed from a defunct broadcast band receiver. Such items are not difficult to come by and in any case the type is not critical provided the primary and secondary windings have measured resistance values approximating to 500 and 150 ohms respectively. If difficulty exists in finding a suitable surplus transformer for T1 a readily available item is the Ardente type Tl079 interstage model. In some cases-and particularly if the Ardente transformer is used-it may be necessary to increase the value of resistor R 3 to say $100 \mathrm{k} \Omega$. The frequency due to the audio generator is of little consequence provided it is recognizable.

## Constructional

Since it is essential to screen the apparatus the ubiquitous 2 -oz tobacco tin provides a cheap and convenient housing which also leaves sufficient internal space for a small battery if desired. The location of components is shown in Fig. 2 which is

## components list


self-explanatory. As will be appreciated only the crystal, output socket and supply connectors exist outside when the tin lid is placed in position. In the prototype the negative supply lead is soldered direct to the case, the nearby positive supply being taken inside via a small feed-through capacitor.
The inductors are home-made, L1 consisting of 3 turns of $24 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. copper wire wound on to a $3_{8}$ in. diameter 'former' and allowed to spring off; L2 is similarly made using but $1^{11_{2}}$ turns. Both windings are spaced wire thickness. Some 24 turns of fine d.s.c. wire ( $30-38$ s.w.g.) are close-wound on to a $1_{4} \mathrm{in}$. dust-cored former to make L3.

## Testing

With one end of R2 temporarily disconnected and a crystal plugged in, a meter set to read 0.10 mA placed in series with a 9 V battery supply may initially read full scale or thereabouts, this indicating, as is likely, a non-oscillating condition. The core of L3 is then carefully adjusted until the current being monitored falls suddenly to around 2 mA , this indicating correct functioning.

With R2 reconnected the current reading obviously increases whereupon the secondary winding of Tl is briefly short-circuited with a metal blade whilst carefully noting the test meter pointer. If no current change is detected as the short-circuit is made and broken the audio oscillator is not working and it will be necessary to reverse the connections to either the primary or the secondary windings of Tl-but not both-to phase the feed-back correctly.

If a short rod aerial is then plugged into the output socket, SK1, and is brought close to a 2 -metre receiver-or as is more likely a 2 -metre converter working with a receiver-a signal due to the unit should be tunable whereupon trimmer TCl may be peaked for maximum output.
Thereafter crystals in the frequency range of $6005-6083 \mathrm{kHz}$ may be used to give harmonic output between $144-146 \mathrm{MHz}$. Alternatively crystals in the frequency range of $8005-8111 \mathrm{kHz}$ may be utilized provided inductor L3 is retuned to this region thus affording eighteenth harmonic output.


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## SELF-SATURATING MAGNETIC AMPLIFIERS <br> (continued)

If the control current is zero, the core is taken through a small magnetisation cycle and has an inductance determined by the average flux contributed by the secondary current. If the control current is in the opposite direction, the flux due to control current opposes it and the core can be made to change from negative to positive saturation when signal current flows. In this state, flux change is maximum and inductance is large so that the voltage drop across the secondary winding is large.

In a core operated in this way, the amplification obtained depends mainly on the shape of the magnetisation B-H curve, and a steep sloped curve with a very low value of saturation magnetic field strength is desirable. To obtain this shape of curve, cores are usually made by winding tapes of suitable material (permalloy etc.) round a former to form a toroid and winding the coils round these cores.

When such materials are used in such a core, the B-H curve is of the type shown in Fig. 6, where the scales of the graph are such that the values of $B$ are large and those of H small. Saturation occurs at


Fig. 6 : B-H curve for material used for cores of magnetic amplifiers.
such a low value of flux (measured in milliamps of current $X$ turns of coil) that the cores will saturate with the output current even with no control current applied, and so the control current must be applied so that its flux always opposes the output flux.

The circuit of a full-wave self-saturating magnetic amplifier is shown in Fig. 7. Since the secondary current in each core must be in one direction, a
rectifier is used in series with each secondary winding and two windings are used so that control can be exerted over the whole of one cycle. Note that the voltage across the load is alternating, despite the rectifiers. The output waveform of such an amplifier is also shown in Fig. 7; except for the value of voltage at minimum signal, the waveform is similar to that obtained from a thyristor circuit.

The transfer characteristic (voltage out plotted against current in control winding) is shown in Fig. 7. The precise form of this curve can be calculated if the $\mathrm{B}-\mathrm{H}$ curve for the core in use is known, and it is one of the considerable achievements of core manufacturers that cores and core materials can now be made with reproducible values of $\mathrm{B}-\mathrm{H}$ curve. The greatest sensitivity can be obtained if the control current is biased to the point 0 on this control curve, and for this purpose, if the bias signal cannot be obtained from the source, a separate bias winding may be used.

The self-saturating magnetic amplifier will give an a.c. voltage output across a load almost independent


Fig. 7: Circuit of fullwave self-saturating magnetic amplifier with output waveform and amplifier characteristic curve.
of load impedance and determined only by the d.c. control current, so that a d.c. signal at the control winding produces an amplified a.c. output. The output power obtained depends on the size and type of core used.

## DC OUTPUT FEEDBACK

The magnetic amplifiers described so far give an a.c. output for a d.c. input. Where the load of the amplifier must be supplied with d.c., or where one magnetic amplifier feeds a second (as when very large power amplification is required) the output of the magnetic amplifier must be rectified. This may be done by taking the output terminals to a bridge rectifier and connecting the load across the other two terminals of the rectifiers (Fig. 8a). A more economical method is to make use of the rectifiers which feed the cores, and add two more to form a bridge rectifier circuit (Fig. 8b) or to use a centre tapped transformer as power source and use the core rectifiers to provide the d.c. output (Fig. 8c).

When linearity of control is particularly important, this may be improved by feedback. To apply feedback to a magnetic amplifier a direct current must be obtained from the output and applied to a feedback winding in the direction opposite to the current in the control winding. The feedback ratio which by the usual feedback theory is approximately the new gain of the amplifier, is the ratio of control winding ampere-turns to the feedback ampere-turns.

## DESIGN AND CONSTRUCTION OF PRACTICAL AMPLIFIERS

Because magnetic materials vary so much, it is not easy to give a "circuit" for a magnetic amplifier for home construction; it is rather like giving a circuit for a radio in which all the transistors had to be made at home as well! We can, however, outline the steps in design, so that the experimenter can construct reactors, determine their characteristics and make use of them in the circuits shown earlier. Since commercially obtainable reactors are $£ 10$ and upwards, there is a strong incentive for home construction!

## CORES

The type of core material which can be used depends on the power available to drive the control winding. When large powers (about 1 kW ) are being controlled, and several watts can be used to drive the amplifier, an old transformer core can be rebuilt, provided that the transformer was rated to take such power loads. This requires some trial and error unless the core material is known and information on it is available. If this is not the case, the best cut-and-try method is to keep the original windings on the bobbin and reassemble the core with no gap, by replacing the $\mathbf{E}$ and I sections facing alternatively in opposite directions. The inductance of the main winding should then be checked for saturation point; this is easily done if an oscilloscope is available by feeding the winding from an a.c. supply through a large variable resistor and checking the voltage across the winding with an oscilloscope. As the current is increased, the voltage waveform becomes flat-topped when saturation point is reached, and the current flowing at this point is saturation current (the saturation current
here is peak current $=1.4 \times \mathrm{rms}$ meter reading). Alternatively an a.c. voltmeter and ammeter can be used and voltage plotted against current on a graph, saturation being when the graph becomes flat-topped. Note that the a.c. current must be varied by a resistor, if a constant voltage source such as an auto-transformer is used, the current waveform will be the one which appears distorted.


Fig. 8a, top, shows rectifiers needed to rectify $A C$ output of amplifier when the load requires a DC supply. Fig. 8b, centre, and Fig. 8c, bottom, illustrate alternative methods of achieving $D C$ output.

Once saturation current in the main winding is known, the saturation current in the other windings can be calculated, for it is inversely proportional to the voltage of the winding when used as a transformer. For example, if the saturation current in a 250 V winding is 100 mA the saturation in a $350-0-350$
winding, total 700 V is

$$
100 \times \frac{250}{700} \mathrm{~mA}=36 \mathrm{~mA}
$$

and this 700 V winding can be used as the control winding. If the control winding has resistance of $100 \Omega$, the voltage across it at saturation is 36 V and this will be able to control currents of $\pm 100 \mathrm{~mA}$ at 250 V in the other winding. The voltage gain in this case is not impressive, but the power gain is fairly high and is achieved at less cost than many comparable devices.

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Fig. 9: The cross sectional area of the core can be obtained by multiplying ' $a$ ' and ' $b$ ' measured in cms.
(in $s q . \mathrm{cm}$ ) in the bobbin, $B$ is the saturation flux density of the core in Teslas (Weber per sq.m) and $f$ is the frequency in Hertz (cycles per second).

The wire size may then be selected if the output current is known. Using a table of wire size which shows area in "circular mils" choose a wire size of about 1 circular mil for each milliamp of output current. The number of turns for the voltage required at the output is then $\frac{25 \mathrm{~V}}{\mathrm{~A}}$ where the area of cross-section of the core (Fig. 9) in sq.cm and $V$ is the voltage of the winding in volts.

After this, the design depends on the core material used, whose characteristic must be known. The ampere-turns for control should be obtained from the maker's information, and the control winding designed to suit amplification required and to fill the available bobbin shape.

In the case of a commercial design, considerably more would be done to calculate leakage flux, winding thickness, etc. but a cut-and-try approach is better for the amateur who is more interested in making a working device than in establishing a production line.

## FINAL NOTES

Voltage gains are of the order of 8-40 with straight saturating circuits and up to 1200 with self-saturation. Feedback lines should include a choke to prevent a.c. feedback.

The frequency of the input signal should not be more than one-tenth of the frequency of the operating a.c.; for 50 Hz operation, the input signal bandwidth is d.c. to 5 Hz .


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The colour-
coded sections of the Mullard Data Book list all you'll want to know about valves, integrated circuits, semiconductors, picture tubes and other components. It also contains equivalents and comparables lists.
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## STEREO 21

I didn't think it was possible, but, for the amazingly low price of $£ 17 \cdot 95$, Radio and TV Components are marketing a stereo record playing outfit.

In kit form, it comprises a BSR C129R 3-speed record deck with cartridge, a pre-assembled amplifier module, giving 2.7 W per channel, two 8 in . $x 5 \mathrm{in}$. speakers, easy-toassemble woodwork for the plinth, cover and speaker cabinets and all the wire, nuts and bolts, etc.

The "Stereo 21" is particularly suitable for beginners to home construction because no soldering is required. All electrical connections are made through push-on tags. The plinth and speaker enclo sures employ pre-mitred, wood grain covered chipboard sections, the mitres being cut in such a manner that a hinge is formed. Glue is applied to the mitred sections which are then simply folded over to form a cabinet.

Another new item from the R \& TV stable is an 8-track cartridge player retailing at $£ 9 \cdot 90$. Housed in a smart wooden cabinet, the unit claims a frequency range better than 50 10 kHz . Four track-indicator lights show which track is being played and the unit switches automatically from one channel to the next. This unit can easily be played through the Stereo 21 system, making it a comprehensive good-value-for-money stereo set-up.

Further information by sending s.a.e. to Radio \& TV Components (Acton) Ltd., 21 High Street, London, W3 6NG.

## ADVANCE TIMER/COUNTER



Mentioned last month, the TC17 measures frequencies from d.c. to 50 MHz with resolution of $0 \cdot 1 \mathrm{~Hz}$.

## GL78/P/C

This is the latest addition to the range of Goldring/Lenco Turntable Units. The Model GL78/P/C incorporates an automatic shut-off switch which stops the motor at the end of the record and simultaneously raises the pick-up. A manual override control is built in, in case the shut-off facility is not required. Goldring Ltd., 10 Bayford St., Hackney, London, E8 3SE.


## NEW 'TERRY' CLIPS

The picture shows the range of 'clipco' securing clips. 'Clipco' is versatile, easily fixed and no screwing is required. It is made of unbreakable, resilient rust-free nylon, which prevents damage to articles. 'Clipco' solves many fixing problems around the home and is a specially designed dual purpose plug which ensures efficient fixing to walls, tiles, wood and pegboard etc.

The clips are available in three choices of visual blisters, containing 8,9 or 10 clips dependent on size and shape. The recommended retail price of blisters is 21 p to 23 p . They are also available in bulk-100 at $£ 2 \cdot 18 \mathrm{p}$. Herbert Terry and Sons Ltd., Redditch, England.

## S.W. CRYSTAL SET

Partridge now market a short wave crystal set (see picture). Further information from: Partridge Electronics, Broadstairs, Kent.


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*)
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## VACUUM RECORD CLEANER

The manufacturers, R.I. Audio, claim that their new "Groovac" record cleaner is the only unit available which removes dust from records by vacuum cleaning.
A tracking force of only 0.7 gram has been achieved by using a lightweight design with lubricated-for-life bearings throughout. This is considerably below the 3 to 6 grams force of simple brush cleaners. Low tracking force allows fine hairs to be incorporated in the Groovac cleaning nozzle which ensure efficient removal of dust from the bottom of record grooves-most brush cleaners have hairs with a diameter which is larger than the width of the record grooves. Low tracking force also means an almost immeasurable reduction in turntable speed, a reduction which is at least 3 times less than that caused by brush cleaners.
The Groovac consists of a precision lightweight arm, and a suction

unit which is acoustically isolated in a special enclosure. The suction unit has been designed to be inaudible at a distance of 2 metres; it has a mains switch and indicator, and is attractively finished in teak. Price is $£ 6 \cdot 90$ p plus V.A.T. and it is available from hi-fi retailers or direct from RI Audio, Kernick Road, Penryn Cornwal/.

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## technical specifications

Input impedance 100 Ks
Input (for 30 w into 8 s ) 400 mV
Signal to noise ratio, referred to full $0 / \mathrm{p}$ at
30 v HT 80 dB or better
Distortion $0.02 \%$ up to 20 W at 8 s . See curve
Frequency response 10 Hz to more than
$200 \mathrm{KHz} \pm 1 \mathrm{~dB}$
Max. supply voltage 45 v ( 4 s s to $8 s$ speakers)
( $50 \vee 15 \Omega$ speakers only)
Min. supply voltage 9 V
Load impedance-minimum • 412 at 45 v HT Load impedarice - maximum : safe on open circuit

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## Typical Project 60 applications

| System | The Units to use | together with | Units cost |
| :---: | :---: | :---: | :---: |
| Simple battery record player | 2.30 | Crystal P.U., 12 V battery volume control.etc | £4.48 |
| Marns powered record player | Z.30.PZ.5 | Crystal or ceramic PU. volume control, eic. | £9.45 |
| 12 W. RMS continuous sine wave stereo amp for average needs | $\begin{aligned} & 2 \times \text { Z.30s, Stereo } \\ & 60 ; \text { PZ. } 5 \end{aligned}$ | Crystal, ceramic or mag P.U., F.M Tuner, etc | $£ 23.90$ |
| 25 W . RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers | $\begin{aligned} & 2 \times 2.30 \text { s, Stereo } \\ & 60 ; \text { PZ. } 6 \end{aligned}$ | High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck. etc | £26.90 |
| 80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W RMS into 8 ahms) | $2 \times 2.50 \mathrm{~s}$, Stereo 60; PZ.8, mains transformer | As above | £34.88 |
| Indoor P.A. | Z.50, PZ.8, mains transformer | Mic., guitar. speakers. etc., controls | £19.43 |

F.M. Stereo Tuner (£25) \& A.F.U. (£5.98) may be added as required
2.50.PZ.8,mains Mic..guitar.speakers
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SPECIFICATIONS-Input sensitivities: Radio -up to 3 ml$)^{\circ}$ Mag. p.u. 3 mV correct to R.I.A.A curve - 1 dB .20 to $25,000 \mathrm{~Hz}$. Ceramic p. u. - up to 3 mV . Aux-up to $3 \Pi V$ Output : 250 mV . Signal to noise ratio : better than 70 dB . Channel matching: within 1 dB Tone controls: TREBLE +12 to -12 dB at 10 KHz : BASS -12 to -12dB at 100 Hz Front panel : brushed aluminum with black knobs and controls. Size: $66 \times 40 \times 207 \mathrm{~mm}$

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## Project 60 Stereo F.M. Tuner



The phase lock 1000 principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now. Sinclair have appliec the principle to an F.M. tuner with fan tastically good results. Other advanced features include vancap diode tuning, printed circuit coils, an I.C. in the specially designed stero decoder and switchable squelch circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower lavel of distortion than any other tuner we know. Stereo broadcasts are received automatically. a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems. SPECIFICATIONS—Number of transistors: 16 plus 20 inl . C. Tuning range: 875 to 108 MHz Sensitivity: $7 \mu \mathrm{~V}$ for lock-1n over full deviation Squelch level: Typically $2 \mathrm{C} \mu \mathrm{V}$. Signal to noise ratio: $>65 \mathrm{~dB}$. Audio Stereo decoder operating level: $2 \mu \mathrm{~V}$. Cross talk: 40 dB Ourput voltage: $2 \times 150 \mathrm{mV} \mathrm{RM} \mathrm{S}$ maximum Stereo decoder operating level: $2 \mu \mathrm{~V}$. Cross talk: 40 dB . Output voltage: $2 \times 150 \mathrm{mV}$ R.M S. maximum
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90 dB ( $1,000,000.000$ times) after feedback. $90 d B$ (1,000,000.000 times) after feedback.
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| OA2 | 0.40 | 6A376 | 0.85 | 6F13 | 0.50 | 10D1 | 0.85 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OA8 | 0.48 | 6AT6 | 0.88 | 6F14 | 0.70 | 10D2 | 0.55 |
| OB2 | 0.40 | 6AU6 | 0.80 | 6F15 | 0.65 | 10F1 | 0.75 |
| OB3 | 0.70 | GAV8 | 0.40 | 6 F18 | 0.50 | 10F9 | 0.85 |
| OC3 | 0.40 | 6AW8A | 0.05 | $6 \mathrm{~F}^{23}$ | 0.90 | 10F18 | 0.60 |
| OD3 | 0.40 | 6BA6 | 0.88 | 6 F24 | 0.80 | 10 Ll | 0.00 |
| 1836 T | 0.45 | 6BE6 | 0.82 | 6 F 25 | 1.00 | 10LD11 | 0.70 |
| 1 L 4 | 0.25 | 6BF6 | 0.55 | $6 \mathrm{~F}^{6} 6$ | 0.85 | 10P13 | 0.78 |
| 284 | 0.50 | 6BH6 | 0.76 | 6 628 | 0.70 | 12AB5 | 0.70 |
| 1Rs | 0.45 | 6BJ6 | 0.56 | ${ }^{6} \mathrm{GK} 6$ | 0.80 | 12AC6 | 0.60 |
| 184 | 0.80 | 6BK7A | 0.75 | 6 J 4 | 0.60 | 12AE6 | 0.00 |
| 185 | 0.80 | 6BN5 | 0.48 | $6 J 56$ | 0.40 | 12ALS | 0.55 |
| 1T4 | 0.80 | 6BN6 | 0.80 | ${ }^{6} 56$ | 0.80 | 12AQ5 | 0.50 |
| 104 | 0.40 | 5 BQ5 | 0.85 | ${ }^{6} 517$ | 0.45 | 12AT6 | 0.40 |
| 105 | 0.75 | $6 \mathrm{BR8}$ | 0.75 | $6 \mathrm{~K} 4 \Pi$ | 0.60 | 12AT7 | 5 |
| 1 V 2 | 0.65 | $6 \mathrm{BE7}$ | 1.85 | $8 \mathrm{6BBJT}$ | 0.75 | 12AL6 | 8 |
| $1 \times 2311$ | 0.55 | ABW6 | 0.90 | ${ }^{6} \mathrm{~K} 7$ | 0.48 | 12AU7 | 8 |
| 2D21 | 0.40 | 6BW7 | 0.90 | 6 KBC : | 0.45 | 12 A | 5 |
| 8 A 4 | 0.45 | 6BX6 | 0.85 | 6 K 25 | 0.75 | 12 | 0 |
| 8AB | 0.75 | 6 BZG | 0.45 | 6L6GT | 0.65 | 12AX7 | 0.88 |
| 884 | 0.40 | ${ }^{6 C 4}$ | 0.85 | 6 L 7 | 0. | $12 \mathrm{AY7}$ | 0.75 |
| 3 V 4 | 0.70 | 6C5GT | 0.65 | 6L18 | 0.60 | 12 B | . 65 |
| ER4GY | 0.75 | 8CB6 | 0.40 | ${ }^{6 L D}{ }^{2} 0$ | 0.50 | $12 \mathrm{BA6}$ | 0.45 |
| BU4 ${ }^{\text {d }}$ | 0.40 | 5CDilia |  | 6N7 ${ }^{\text {ciP }}$ | 0.55 | 12BA7 | 0.50 |
| -5V40 | 0.50 |  | 1.80 | $6 \mathrm{CP}^{2} 8$ | 0.65 | 12BE6 | 0.60 |
| 6Y8GT | 0.45 | ${ }^{8} \mathrm{Ca} 7$ | 0.60 | $6 \mathrm{Cl}^{7}$ | 0.50 | 12BH7 | 0.50 |
| 523 | 0.75 | 6CL6 | 0.60 | 68A7 | 0.45 | 12 BY 7 | 0.65 800 |
| 5244 | 0.45 | 6UUR | 0.80 | 6867 | 0.45 | 12E1 | 0 |
| $6 / 30 \mathrm{~L} 2$ | 0.80 | 6CW4 | 0.70 | 68 K 7 | 0.60 | 12 K 5 |  |
| 6AB4 | 0.45 | 6CY6 | 0.50 | 68L7 | 0.45 | 12K |  |
| 6AF4A | 0.60 | ${ }^{6047}$ | 0.75 | 6 S | 0.45 |  |  |
| 6AG5 | 0.95 | ${ }^{6} \mathrm{D} 3$ | 0.55 | 6897 | 0.50 | 12 BF | 0 |
| 6AG7 | 0.45 | 6 CHCb | 0.80 | $68 \mathrm{R7}$ | 0.50 | 2001 | 0.60 |
| 6AB6 | 0.80 | 6DK6 | 0.60 | $6 T 8$ | 0.88 | 20 LJ | 1.10 |
| 6AJ8 | 0.80 | 6DQ6B | 0.75 | 6 CHGT | 0.70 | 20P1 | 0.80 |
| 6AKE | 0.40 | HD84 | 1.25 | 6Ubu | 0.75 | 20 P 4 | 1.10 |
| 6AK6 | 0.80 | 6 LAB | 0.65 | 6U8A | 0.48 | 20 P 5 | 1.20 |
| 6AL3 | 0.48 | 6EE7 | 0.80 | 6 VBGT | 0.45 | ${ }^{25 C 5}$ | 0.60 |
| 6ALS | 0.22 | 6EJ7 | 0.35 | $6 \times 4$ | 0.40 | ${ }^{25 L 6 G T}$ | 0.80 |
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| 6AQS | 0.42 | 6F1 | 0.75 | ${ }_{6}^{6 \times 8}$ | 0.85 0.80 | 3045 | 0.60 |
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