PRACTICAL WIRELESS

APRIL 1973

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'SUPER 30' AMP

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R.S.C. SUPER 30 #19-91 £10-50 £88-70

Mk III AMPLIFIER TOTAL \$181-55

FANE 'MODE ONE' HIGH FIDELITY SPEAKER KIT



Incorporating a model 803 8" 13,000 Gauss Bass Speaker with ultra low resonance. P.V.C. surround cone. Printed circuit cross-over assembly with ferrite cored coils. Model 303 Pressure Tweeter, Acoustic damping material, Screws, Panels etc., and in-structive diagrams, Frequency 49.95 post Response 25 Hz-2 KHz. Impedance 8-15 ohms

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Cabinets latest style Satin Teak veneer. Aconstically lined or filled acoustic damping. Ported where appropriate, Credit terms available. acoustic damping. Ported where appropriate, Credit terms available.

DORCHESTER (Illustrated) Size 16×11×91n. appr. Range 46-15,000
c.p.s. Rating 8-10 watts. Fitted High flux 13×8in. 49-45
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MONARCH Size 19×10×91n. approx. Rating 10 watts. Inc. 13×8in. speaker with highly feetible P.V.C. cone surround, long throw voice coil and 10,000 line magnet. High flux pressure tweeter. Handsome design cabinet. Range 35-20,000 c.p.s. 1mp. 8 ohms. Gives amooth realistic sound output.

See 'package offers' for illustration.

Carr. 50p

RSC G66 MkII 6+6 WATT high quality STEREO AMPLIFIER



Individual Ganged Controls: Bass, Treble, Volume and Balance. Printed circuit construction employing 10 Transistors plus Diodes. Output rating I.H.F.M. Frequency range 20-20,000 c.p.s. Bass Control ± 13db. Selector switch for P.U. or Tape/Radio. For loudspeaker output impedances of 3 to 15 ohms. For standard 200-250v. A.C. mains operation. Attractive Black and Silver finished metal facility and proceedings of the process o

fascia plate and matching control knobs.

COMPLETE EIT OF PARTS INCLUDING
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COMPREHENSIVE WIRING DIAGRAMS & INSTRUCTIONS
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Teak veneer finish. Acoustically lined. Sizes approx. Carr. 35p. per enc.

SE10 For outstanding with 10in. Hi-Fi speaker and the speaker



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 Plasticised Cone surround. "D" indicates Tweeter Cone providing extended frequency range up to 16,000 c.p.s. Impedance 3 or 8-15 ohms. PLEASE STATE CHOICE.

 Exceptional performance at low cost.

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R.S.C. TA6 6 Watt HI-FI AMPLIFIER

200-250v. AC mains operated. Frequency Response 30-20,000 c.p.s. —2dB. Harmonic Distortion 0-3% at 1,000 c.p.s. Separate Bass and Treble lift and cut' controls. 3 input sockets for Mike, Gram, Radio or Tape. Input selector switch. Output for 3-15 ohm spikrs. Max. sensitivity 5mV Output rating I.H.F.M. Fully enclosed enamelied case, 91×21×5 im. Attractive brushed silver finish facis plate 10½×3 im. and matching knobs. Complete kit of parts with full wiring diagrams and instructions.

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Response 25 Hz to 15 KHz. Gauss 13,000 Imp 3 or 8-15. £3.85

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FULL DISCOUNT to Genuine Trade Customers. CARR. FREE.

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300-0-300v. 130mA, 6-3v. 4a., 0-5-6-3v. 3a. 22-20
350-0-350v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a. 22-20
350-0-350v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a. 22-20
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150mA, 7-10H, 250 Ω 70p: 100mA, 10H, 200 Ω 60p; 80mA, 10H, 350 Ω 60mA, 10H, 400 Ω 25p

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BUILD AN AMPLIFIER WORTH APPROXIMATELY DOUBLE THE KIT PRICE INCLUDING CABINET Only high grade components by leading manufacturers

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For Magnetic or Ceramic Pick-Ups regardless of Price. Output (per channel) 15 watts RMS



COMPLETE KIT into 8 \(\Omega\$. Frequency Response Carr. 65 p. 7 Hz to 70 KHz Cabinet if req. £5 £25 ± 1½ dB.

FACTORY BUILT UNIT INC. CABINET with 12 months' guar- contained. Or Dep. £7 and 9 monthly £00.75 payments £3.99 (Total £42.91).

'YORK' HIGH-FIDELITY 3 SPEAKER SYSTEM

- ★ Moderate size only 25×14×10in. approx. COMPLETE KIT
- ★ Response 30-20,000 c.p.s. Impedance 15 ohms

★ Performance comparable with units costing coasiderably more Carr. 65p

Consists of (1) 12in. 15 watt Bass unit with cast chassis, Roll rubber cone surround for ultra low resonance, and ceramic magnet.

(2) 3-way quarter section series cross-over system.

(4) High efficiency tweeter, (5) Appropriate quantity acoustic damping material. (6) Handsome Teak veneered cabinet. (7) Circuit and full instructions. Terms: Dep. £4-60 and 9 monthly payments £2-47 (Total £26-83).





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All types 15 Ohms covered in Rexine and Vynair
TYPE C4100 IS ALSO SUITABLE FOR BASS GUITAR OR ELECTRONIC ORGAN

HI-FI AMPLIFIER Highly sensitive. Push-Pull high output, Hum level.—70dB. Response EP86, ECC83, E.134, E.34, G.234. Separate Bass and Treble Controls. Sensitivity 36 millivolts. For High Impedance microphones. For Clubs, Schools, Theatres, Dance Halls, Outdoor Functions, etc. For Elsetronic Organ, Gullar, String Bass, etc. Gram, Pick-up etc. for mixing purposes, 200-250v. 50 c/s A.C. mains. For 3 and 15 ohm passekers. Twin-handled perforated cover 21:90.12 MONTHS GUARANTEE. Carr. 65p
TERMS: Deposit #4 and 9 monthly payments of 22:10 (Total 222-90). Send S.A.E. for leaflet.

LINEAR T40/60D 50W GROUP/DISCO AMPLIFIER

TYPE C312 30-40 WATTS Fitted two TYPE C412S 50 WATTS exceptionally efficient, low feedback how charred accretistic high flux 13° x8° 20 watt 219.95 speakers: Overall size approx. 65 x14 x9in speakers. Terms: Dep. 23 and 9 119.95 rems: Dep. 24 and 9 monthly pay-231 withly payments 22.22 (Total 222.98) Carr. 50p. ments 23.22 (Total 222.98) Carr. 50p. ments 25.32 (Total 232.93) Carr. 75p ments 25.32 (Total 232.93) Carr. 75p

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R.S.C. A10 30 WATT ULTRA LINEAR

£49.50 car

Or Deposit £7-50 and 9 monthly payments £5-87

(Total #55-83)

RSC PHANTOM '50' Combined 50w Amplifier and 12in. Lond-speaker. For Lead Guitar, mic., Gram, Radio, Tape (Not for use with Bass instruments). Inc. 3 inputs and 2 vol. controls plus Treble, Bass and Presence. Output Jack for additional 15 olum Speaker. Attractively finished in black with silver-finished fascia and trimmings. Compact size. Fitted carrying handle.

Units listed below
(a) 100w POWER AMPLIFIER
(b) PAIR OF HI-FI HEADPHONES
(c) HONES

PHONES
(c) MATCHING DYNAMIC
'MIKE' (attached
to headphones)
(d) PAIR 50 WATT SPEAKERS
Black Rexine covered
Cabinets
Size approx.
18" × 18" × 8"
(A(N))

(a)(b)(c)&(d) Carr. £1-25 Terms on Amps. Speakers and Head-phone/Mike. Deposit £15 and 18 monthly payments of £4-00 (Total £87-00).

Mk.III turntables and Sonotone or Acos Cartridges with diamond stylii. Acos Cartridges with diamond stylii, Separate Vol. controls for each turotable. Also MONTORING FACILITIES, plus Treble and Bass Controls. Separate input for 'mike' with vol. control switch. Black Rexine covered Cabinet with lid. see illus. on loft. Genr. 21:25 Cor. Dep. 213:25 and 657:10 and 18 mithly paymes 26:38 (Total: 275:17) or Dep. 215 and 18 mithly paymes 26:38 (Total: 275:17) or Dep. 215 and 18 mithly paymes 26:38 (Total: 280:18)

mthly payments £3-52 (Total £80-16).

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All power ratings are R.M.S. continuous. 2 YEARS' GUARAHTEN
High flux ceramic magnets. ALL CARRIAGE FREE.

'POP' 100 'POP' 60 'POP' 50

£12.90

15" 60 Watt

14.000 gauss



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Simulated black rexine, plastic bonded

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LINEAR

Dep: 26 and 9

Dep: 28 and 9 mthly payments 22-20 (Total 225-80) 21-30 (Total 215). FOR BASS GUITAR, ELECT. ORGAN, ETC

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GROUP/DISCO EQUIPMENT

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A powerful high quality all-purpose unit for lead, rhythin, bass guitar, vocalists, grain, radio, tape. Peak Output rating. Loudapeaker unit either horizontal or

FULL MONITORING PACILITIES

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RSC GP30 HI-FI **AMPLIFIER**

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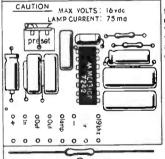
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Stereo radio from your existing tuner.



A complete set of parts from Jermyn to build a stereo decoder module that will convertyour existing mono tuner for stereo reception whilst maintaining a high standard of reproduction.

The distortion is very low (typically 0.3% at 560 mV RMS composite input signal) with 40dB channel separation.

The stereo switching is automatic and there is a light emitting diode which acts as a stereo beacon.

The kit requires no coil and there are no alignment problems.

Fitting. The module requires a 10-16 volt power supply which can normally be, "apped off the existing tuner. The signal input is taken off hefore the de-emphasis circuit which in practice means disconnecting one, or at the most, two capacitors. Any radio engineer will be able to spot these capacitors, but if you're really stuck send the circuit with a SAE to us and one of our engineers will indicate the output point. (This is the full extent of our involvement, no hardware please).

Of course, if you have a modern mono tuner with a multiplex output our module simply plugs in.

The outputs go via a screened twin cable to the tuner inputs of your stereo amplifier.

And the cost? £4.90 for the Kit with 100% tested integrated circuit.

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Please rush me ☐ Kit(s), ☐ made up Stereo decoders. I enclose cheque/postal order for £

Sevenoaks Name
| Kent Address

Block Capitals Please



Apart from the five items shown above, there are another 195 kits to choose from in the vast AMTRON range of electronic kits.

A few examples of equipment you can construct from AMTRON kits are: Power supplies, preamplifiers, amplifiers, L.F. instruments, accessories for musical instruments, amateur and radio control transmitters and receivers, battery chargers, electronic car accessories, psychedelic lighting equipment, measuring instruments, tuners, receivers, I.C. digital equipment.

Only 1st class fully guaranteed components are used —solder is included with every kit.

Prices range from £1.10 to £80 and each kit is sold in protective blister pack containing complete instructions.

Should you experience any difficulty in obtaining AMTRON Kits please contact us direct.

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AMATEUR RADIO EQUIPMENT



R.F. PRESELECTOR

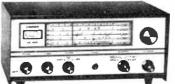
The PR40 R.F. Preselector is the solid state version of the world famous PR30 which it now supercedes. It employs Silicon "N" Channel FET (Field Effect Transistor) front end, followed by silicon NPN Broad Band R.F. Amp., and will substantially improve receiver performance over the range I - 5 to 35 MHz, providing a considerable increase in gain up to an overall average of 30 dB, with improved image rejection and noise ratio.



MULTIBAND-6

SOLID STATE SHORT WAVE RECEIVER KIT

All transistor T.R.F. Receiver tunes 550 KHz to 30 MHz (540 to 10 metres) complete coverage—no gaps, Medium waves—Trawlere—Ship/Shore Telephone—All Six Amateur Bands 160-10 metres—International Broadcast from Australia, Far East, Russia, USA etc. using 4 miniature plug in Coils, Hi-Gain FET Regen. Det./AF/AF Module giving full loudspeaker output to any external 2/3 ohm speaker, Receives AM/CW/SSB. Separate Electrical Bandspread, Calibrated Main Tuning.
A Quality CODAR-KIT with 12 months Guarantee. No technical knowledge required, simple to build, printed circuit and Pictorial Instruction Manual, fully detailed step by step.
Complete Kit with 4 Coils (less standard PP6 battery). £13-20 Carriage 35p. Stamp brings illutrated leaflets.





COMMUNICATION RECEIVER

The CODAR CR70A is an outstanding general coverage communication receiver, ideal for the keen S.W.L.

It tunes from 540 metres medium through to 10 metres with no gaps. Covers shipping, coastguard and distress frequencies, all six amateur bands 160-10 metres, International broadcast, Met. stations etc. etc. giving world-wide reception. Exclusive features include Air-spaced CODAR-COIL Hi-"Q" Aerial input, illuminated Meter and Slide Rule Scale, Two Speed vernier tuning, Switched B.F.O. for CW/SSB signals. Separate output for Tape recorder.
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10K	10 * 10K	10
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Vertic	al or Hori	zontal		S
0 1 wa	itt 5p	0.25 wa	att 7p	
100	1 K 12	10K 12	100K 12	1 M 12
250	2 5K 12	25K 12	250K 12	2 5M !
500	5K 12	50K 12	500K 11	5M 12

Capacitors

dise ceran	nic	low volta-	go op
01µF 18v	5p	0-1µF 30	
·022µF 18v	5p	0-22µF 6	v 5p
047µF 12v	Sp	0-47µF 3	v 5p
ceramic p	late	30 V	
1000pf	10p	4700pf	10p
2200pf	10p	10,000pf	10p
Ceramic	plato	63V (C33	31
1 8pf	8 2of		120pf
		33pt	
2 2pt	10pf	39pt	150pt
3 3pf	12pf	47pf	180pf

2 2pt	4.0	-4	20-	.4	100-4
)pt	39p		150pt
3 3pf	1.2	pf pf	47p	v#	180pf
3 9pf	15	pf	56p	4	220pf
4 7pt	18	pf	68p	d .	270pf
5 6pf	22	pf	82p	4	330pf
6 8pf	27	pf	100p	4	
all 5p. e	ach				
mylar f	ılm		100V		
1000pf	2p	01μF	3p	068µF	4p
2000pf	2p	02µF	3р	1µF	4p
5000pf	2p	04 µ F	3p	2µF	5p
		·05nF	3p		

polystyrene 160V 10pf to 10,000pf in multiples of 10, 15, 22, 33, 47 & 68. 3p each

metallised	polyester	25	OV (C28	0)
01μF 3p	068µF	31p	.47µF	8p
015µF 3p	1 µF	4p	68uF	11 p
022uF 3p	15uF	4p	1 uF	13p
033uF 3p	-22µF	5p	1 5uF	20p
047uF 3p	-33uF	61p	2 2µF	240

0 17 111	op	ooj	0 2 p	-	a. p	
metall	ised	polyester		400	V (C2	31)
01 µF	41p	047µF	6p		22 µF	10p
015µF	43p	068µF	6p		33µF	14p
-022µF	4 p	1 µF	7p		47µF	15p
033µF	5 p	15µF	8p			

 silvered mica 1% (50pf) 500V

 2·2pf—820pf
 7p
 4·7nF—5600pf
 19p

 1nF—2·2nf
 9p
 6800pf—101µF
 29p

mixed	dielec	tric	600V		
01 µF	7p	047µF	7p	22µF	
022µF	7p	068µF	8p	47µF	
033uF	70	1 oF	Bo.	1	

electronics

Hont Cinke

	nei	at sint	45	
(i)	TOS 1018 5p		TO66 TO3 Power Tab	14p 15p 13p
				W
415.14	1	וט	P10/2	

50p	15p
Verob	oard

	Cop	Plain	
	0.1"	0.15"	0.15
2½" x 1" 2½" x 3¾" 2½" x 5" 3¾" x 3¾" 3½" x 5" 17" x 2½" 17" x 3¾" 17" x 5"	6p 20p 24p 24p 27p 67p 90p	6p 16p (9) 21p (7) 21p (8) 27p (10) 50p 70p	10p 12p - 17p 37p 52p 75p
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A F 139	28 p	BF184	25 p	OC45	15p	ZTX531	25 p	2N3903	15p		45p
BC107	10p	8F185	25p	OC71						⊬A723C	95 p
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3300pf 6p	·022µF	9p	47µF	30p
4700pf 6p	-047µF	12p		
Ceramic				
12KV.d.c.	8KV.d.	c.	HI-K 750	IV.
10pf 9p	200pf	9p	1000pf	5p
15pf 9p	220pf	9p	1500pf	5p
22pf 9p	250pf	9p	2000pf	5p
68pl 9p	270pf	9p	3000p1	5p
82pf 9p	300pf	9p	5000pf	5p
100pf 9p	750V O	ISC	10,000pf	5p
120pt 9p	470pf	5p	feed-	
140pf 9p	1000pf	5p	through	
150pf 9p	5000pf	5p		
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	4	6.3	10	16	25	40	63
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5	400	_	_	_	_	_	6.0
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8	_	_	_	_	_	6p	60
1	_	_	_	_	60		60
i	_	_	_	6p	-	6p	60
1	_	_	60	_	6p	_	60
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4	80	_	60	-	6р	60	6p
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				16	25	40	64
-						33p	40p
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4700	21p	-	_	600	75p	13p	_
CAP				VOLTA	GE 25	40	64
500 1250						33p 50p	40p
1600				80p	50p	_	75p
2500				50p	-	75p	93p
3200 4000					75p	93p	_
6400	antha Day			75p	113p	_	_

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1, 2, 4, 8	μF 450V	14p	32 pF	450V	20p
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184		68117		il No		1017		251,667		S. V.		101177		ECHS			40	PLC>9	50	PY82	35	T-CCN4	43
185		6C.1		GK 8G-T		1015		251.5		1,4002	60	DK32		ECH42		EIV so	40	PCC18	9 55	PY85	38	LCC95	40
IT4		60'50		6K 25		101/9		25.64		1500%	60	DK91	40	ECH51		1.7.35		POFSE		PY500		LCFS0	55
3.44		60'6		61,60	50	19F15	50	TOZEC.	5.5	501		DK 92		1001050		EZ 10		Table:		1,1 200		1 CH45	
3Q4		601160	£1.25			1114,101		2010		507		1+K-96		110,150		EZ41		TOTAL		4.7×01		LCH81	
3Q5		6C.H.e		6Q71		101/13		200.1	30			D1.96		ECL82		EZ80		PERM		E:		1101,42	
384		60,4/4		6Q7GT				50C15	80			D1.92		ECLES		EZS1	29			13 154		L CL83	60 60
3Y4		6116		68 A 7 M		12 VT6		300'17		954		11.93		ECL86		G Y 501 G X 30		PCFS		\$130 \$15		UF41 UF89	40
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81'4G 81'4G		6F1		6807M 68117M		12 VU 6		301 1.1		3763		D1.96		1.179		1.Z31	60			SPSI		PESI	40
5Y3GT		61'66		68J7GT		12437		30 F L 15		7195		DM70		EF37A		HN309		PCL				1.3[50]	30
8Z4G		6 F8G		68K7G7		12B \ 6		30 F1.13		1470		DY46		EF39	60			PCL8:			\$10.00	119	50
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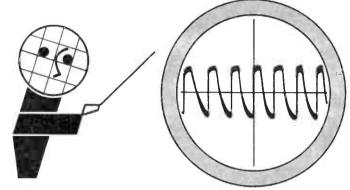
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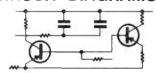
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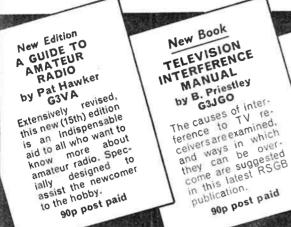
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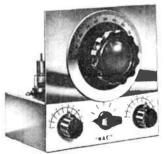
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THIS IS THE FIRST PAGE

0.40 OC19

	AC107	0.20	AD162	0 33	BC148	0.10	BD137	0.45	BFIRE	0.40	OC19	0.35	2G371	0.16	2N2219 (0.20	2N 3054	0.46	2N 4059	0.10
				0 33										0.12		0.22	2N3055	0.50	2N4060	0.12
	ACI13	0.20	AD161 &		BC149	0.12	BD138	0.50	BF194	0.12	OC20	0 · 63	2G371B							
	AC118	0.23	AD162 (3	1P)	BC,120	0.18	BD139	0.55	BF195	0.12	OC22	0.38	201373	0.17		0.20	2N3391	0.14	2N4061	0.12
-	ACI17K	0.20		0.55	BC151	0.20	BD140	0.60	BF196.	0.14	OC23	0.42	20:374	0.17	2N2222	0.20	2N3391A	0.18	2N4062	0 · 12
-0.0		0.12	4 DEL 10				BD155	0.80	BF197	0.14	OC24	0.56	26377	0.30		0 - 17	2N3392	0.14	2N4284	0.17
	AC122		ADTI40		BC152	0.17														0 17
-	AC125	0 17	AFII4	0.24	BC153	0.28	BD175	0.60	BF200	0 - 45	OC25	0.38	20378	0.16		0.14	2N3393	0.14	2N4285	0.17
	AC126	0.17	AF115	0.24	BC154	0.30	BD176	0.60	BF222	0.95	OC26	0.25	2G381	0.16	2N2369A	0 - 14	2N3394	0-14	2N 4286	0.17
-	AC127	0.17	AF116	0.24	BC157	0.18	BD177	0 - 65	BF257	0.45	OC28	0.50	2G382	0.16	2N2411 (0 - 24	2N3395	0.17	2N4287	0.17
									BF258	0.60	OC29	0.50	26401	0.30		0.24	2N3402	0.21	2N4288	0.17
-	AC128	0.17	AF117	0.24	BC158	0.12	BD178	0.65												
	AC132	0.14	AFI18	0.35	BC 159	0.12	BD179	0.70	BF259	0.85	OC35	0.42	20414	0.30		0-47	2N3403	0.21	2N 4289	0.17
-	VC134	0.14	A F124	0.30	BC160	0.45	BD1×0	0.70	BF262	0.55	OC36	0.50	201417	0.25	2N2711 (0 · 21	2N3404	0.28	2N 4290	0.17
-	AC137	0.14	AF125	0.25	BC161	0.50	BD185	0.65	BF263	0.55	OC41	0.20	2N388	0.35	2N2712 (0 · 21	2N3405	0.42	2N4291	0.17
-	1C141	0.14	AF126	0.28	BC167	0.12	BD186	0.65	BF270	0.35	OC42	0.24	2N388A	0.55		0.21	2N3414	0.15	2N4292	0.17
-									BF271		OC44		2N404	0.20		0.17	2N3415	0.15	2N4293	0 - 17
ш	ACI41K	0.17	AF127	0.28	BC168	0.12	BD187	0.70		0.80		0.15								
	AC142	0.14	A F139	0.30	BC.168	0.12	BDIBB	0.70	BF272	0.80	OC45	0.12	2N404A	0.28	2N2904A		2N3416	0.28	2N5172	0 · 12
	AC142K	0.17	AF178	0.50	BC170	0.12	131)189	0.75	BF273	0.35	OC70	0.10	28524	0.42	2N2905 (0 · 21	2N3417	0.28	2N5457	0 · 32
100	AC151	0.15	AF179	0.50	BC171	0.14	BD190	0.75	BF274	0.35	OC71	0.10	2N527	0.49	2N2905A	0 · 21	2N3525	0.75	2N5458	0.82
1200	AC154	0.20	AFIRO	0.50	BC172		BD195	0.85	BFW10	0.60	OC72	0.14	2N598	0.42		0.15	2N3646	0.09	2N5459	0.40
100						0.14			BFX29	0.27	OC74		2N599	0.45		0.18	2N 3702	0.10	28301	0.50
	AC155	0.20	AF181	0.45	BC173	0.14	BD196	0.85				0.14								
	AC156	0.20	AF186	0.45	BC174	0.14	BD197	0.90	BFX84	0.22	OC75	0.15	2N696	0.12		0 20	2N3703	0.10	28302A	0 - 42
	AC157	0.24	AF239	0.37	BC175	0.22	BD198	0.90	BFX85	0.80	OC76	0.15	2N697	0.13		0 · 22	2N3704	0.11	28302	0.42
	AC165	0.20	AL102	0.65	BC177	0.19	BD199	0.95	BFX86	0.22	OC77	0.25	2N698	0.24	2N2925 (0-14	2N3705	0.10	28303	0 - 55
as l	10166	0.20	AL103	0.65	BC178	0.19	BD200	0.95	BFX87	0.24	OC81	0.15	2N699	0.85		0.14	2N3706	0.09	28304	0.70
								0.80	BFX88	0.22	OC81D	0.15	2N706	0.08		0 - 14	2N 3707	0.11	28305	0.84
ပါ	VC167	0.50	ASY26	0.25	BC179	0.19	BD205		DEAGS										28306	0.84
	ACIBB	0.24	A8Y27	0.30	BC,180	0.24	BD206	0-80	BFY50	0.20	OCH2	0.15	2N706A	0.09	2N2926 (G		2N 3708	0.07		
	AC169	0-14	AS Y28	0.25	BC181	0-24	BD207	0.95	BFY51	0.20	OC82D	0.15	2N708	0 · 12		0.12	2N3709	0.08	28307	0.84
	AC176	0.20	A8Y 29	0.25	BC182	0.10	BD208	0-95	BFT52	0.20	OC83	0.20	2N711	0.80	2N2926 (Y)	2N3710	0.09	28321	0.56
O I	AC177	0.24	ASY50	0.25	BC182L	0.10	BDY20	1.00	BFY53	0.17	OC84	0.20	2N717	0.85		Ó·11	2N3711	0.09	28322	0 - 42
							BF115	0 - 24	BPX25	0.85	OC139	0.20	2 N 7 1 N	0.24	2N2924 (O		2N3819	0.28	28322A	0.42
N	AC178	0.28	A8 Y51	0.25	BC183	0.10												0.50	28323	0.56
asil	AC179	0.28	A8Y52	0.25	BC183L	0.10	BF117	0 - 45	BS X 19	0.15	OC140	0.20	2N718A	0.50		0.10	2N3820			
w	AC180	0.17	A8Y54	0.25	BC184	0.12	BF118	0.70	B8 X 20	0.15	OC159	0.25	2N726	0.28	2N2926 (R)	2 N 3 8 2 1	0.35	28324	0.70
_	AC180K	0.20	ABY55	0.25	BC1841.	0 12	BF119	0.70	B8 Y 25	0-15	OC170	0.25	28727	0.28		0-10	2N 3823	0.28	28325	0.70
	AC181	0.17	ABY56	0.25	BC186	0.28	BF121	0.45	B8 Y 26	0.15	OC171	0.25	2N743	0.20	2N2926 (B)	2N3903	0.28	28324	0.70
וש				0.25			BF123	0.50	B8Y27	0.15	OC200	0.25	2N744	0.20		Ó-10	2N3904	0.30	28327	0.70
N.	ACIBIK	0.20	A8Y37		BC187	0.28							2N914	0.14		0.70	2N3905	0.28	28701	0.48
	AC187	0.22	ASYSE	0.25	BC207	0.11	BF125	0 - 45	B8 Y28	0.15	OC201	0.28								
	AC187K	0.20	A8Z21	0.40	130,508	0-11	BF127	0.50	B8 Y29	0.15	OC202	0.28	2N918	0.30		0-14	2N3906	0.27	40361	0.40
м	AC188	0.22	BC107	0.08	BC209	0.12	BF152	0.55	B8 Y34	0.18	OC203	0.25	2N929	0.21	2N3053 (0 · 17	2N4058	0.12	40362	0.45
	ACIBBK	0.20	BCIOS	0.09	BC212L	0.11	BF153	0.45	BS Y 39	0.18	OC204	0.25	2N930	0.21						
0	ACY17	0.25	BC109	0.10	BC213L	0.11	BF154	0.45	BSY+0	0.28	OC205	0.35	2N1131	0.20						
							BF155	0.70	B8 Y41	0.28	OC309	0.40	2N1132	0.22						
	ACY 18	0.20	BC113	0.10	BC214L	0.14			BSY 95	0.12	P346A		2N1302	0.14		DIOD	ES AND I	RECTIF	1ERS	
	ACY19	0.20	BC114	0.15	BC225	0.25	BF156	0.48				0.50					D3*100	0.03	0.110	0.85
	ACY20	0.20	RC115	0.15	BC226	0.35	BF157	0.65	B8Y95A	0.12	1.392	0.42	2N1303	0.14		0 · 08	BY 133	0.21	OAIO	
	ACY21	0.20	BCH6	0.15	BCY30	0.24	BF158	0.55	Bu105	2.00	OCP71	0.48	2N1304	0.17		0.08	BY 164	0.50	OA47	0.07
W)	ACT22	0.16	BC117	0.15	BCY31	0.26	BF159	0.60	CHIE	0 - 50	ORP12	0.48	2N1305	0.17		0 - 08	BYX38/3		O A 70	0 · 07
M	ACY27	0.18	BCITS	0.10	BCY32	0.80	BF160	0.40	C400	0.80	ORP60	0.40	2N1306	0.21	AAY30	0.09		0.42	OA79	0 · 07
ŭ	ACY28		BC119	0.30	BCY33	0.22	BF162	0.40	C407	0 - 25	ORP61	0.40	2N1307	0.21		0.10	BYZ10	0.35	OARI	0.07
M		0.19					BF163	0.40	C424	0.20	ST140	0.12	2N130H	0.23		0.10	BYZII	0.30	OAB5	0.09
٤١	ACY29	0.35	BC120	0.80	BCY34	0.25											BYZ12	0.30	OA90	0.06
ارور	ACY30	0 · 28	BC125	0.12	BC 7.70	0.14	BF164	0.40	C425	0.50	8T141	0.17	2N1309	0.28		0.21				
-	ACY31	0.28	BC126	0.18	BCY71	0.18	BF165	0 - 40	C426	0.85	T1843	0.80	2N 1613	0.20		0.22	BYZ13	0.25	0.491	0.06
10	ACY34	0.21	BC132	0.12	BC'Y'7:2	0.14	BF167	0.22	C428	0.20	UT46	0.27	2N1711	0.20		0 - 14	BYZ16	0.40	OA95	0.07
по	ACY35	0.21	BC134	0.18	BC210	0.20	BF173	0.22	C441	0.80	2G301	0.09	2N1889	0.82	BA154 (0.12	BYZ17	0.35	OA200	0.06
							BF176	0.35	C442	0.30	20302	0.19	2N1890	0.45		0.14	BYZIS	0.35	OA202	0.07
ā	ICY36	0.28	BC135	0.12	BC211	0.25			C444	0.85	20302		2N 1893	0.87		0.18	BYZ19	0.28	8D10	0.05
70	ACY40	0.17	BC136	0.15	BCZ12	0.25	BF177	0.35				0.19					CG62	A 50	SD19	0.05
	ACY41	0.18	BC137	0.15	BD121	0.60	BF178	0.30	C450	0.22	20304	0.24	2N2147	0.72		0.15				
	ACY44	0.85	BC139	0.40	BD123	0.65	BF179	0.30	MAT100	0.19	2G304	0.40	2N2148	0 · 57		0 - 12	(Eg) OA9		IN34	0.07
M	AD130	0.88	BC140	0.30	BD124	0.60	BF180	0.80	MATIOI	0.20	2G308	0.35	2N2160	0 - 60	BY 105 (0-17		0.05	IN34A	0.07
3	AD140	0.48	BC141	0.30	BD131	0.50	BFISL	0.30	MAT120	0.19	2(1309	0.85	2N2192	0.85	BY114 (0 - 12	CG651		1N914	0.06
ы							BF182	0.40	MAT121	0.20	20339	0.20	2N2193	0.35		0.14	(Eq) 0A7	0.	1N916	0.06
O	AD142	0.48	BC142	0.30	BD132	0.60								0.35		0.15	OA79	0.06	IN414B	0.06
	AD143	0.38	BC143	0.30	BD133	0.65	BF183	0 - 40	MPF102	0.42	2G339A	0.16	252194							
70	AD149	0.50	BC145	0.45	BD135	0.40	BF184	0.25	MPF104	0.87	20344	0.18	2N2217	0.22		0.15	OA5	0.35	18021	0.10
S	AD161	0.33	BC147	0.10	BD136	0.40	BF185	0.30	MPF105	0.37	2G345	0.16	2N2218	0.20	BY 130 (0.16	OA5SL	0 · 21	18951	0.08
		2 00.		- 10																

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50 0 23	0.722	0.35	0.35	0.47	0.50	0.53	1 - 15
100 0 25	0.33	0.47	0.47	0.50	0.58	0.63	1 - 40
200 0 - 35	0.37	0.49	0.49	0 57	0.61	0.75	1.60
400 0 43	0.47	0.56	0.56	0.67	0.75	0.93	1.75
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800 0 - 62	0.70	0.80	0.80	0.90	1.20	1.50	4.00

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100 0 04	0 · 0+i			0.16		
200 0 05	0.09			0.20		
400 0 06	0.13	0.07	0.20	0.27	0.37	1.05
600 0 07	0.16			0.34		
800 O-10	0.17			0.37		
1000 0 - 11	0.25			0.46		
1200	0.33			0.57		

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POWER NPN

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KING OF THE PAKS

	Pak !	No.	Description	Pr
1	UI	120	Gives Sub-Min. General Purpose Germanium Diodes	
	Ũ 2	60	Mixed Germanium Transistors AF/RF	
	t 3	75	Germanium Gold Bonded S ab-Win, like OA5, OA47	0.
Į	17 4	40	Germanium Transistor- like OC81, AC128	0.
Ì	Ü 5	60	Office & Sub- Win School Mc OCS1, ACI28	0.
Į	U G	- 30	200mA Sub-Min, Schoon Diodes Sil, Planar Trans, NIN like BSY95A, 2N706	0.
1	1 7	16	Sil. Rectifiers TOP-HAT 750mA VLTG, RANGE up to 100	0.
ı	1.5		Sil. Planer Diodea DO-7 Glass 250mA like OA200/202	-
ı	ē 9	20	Mixed Voltages, I Watt Zener Diodes	0.
ı	1.10	20	BAY50 charge storage Diodes DO-7 Glass	0.
Į	1'11	25	PNP Sil. Planar Trans. TO-5 like 2N1152, 2N2904	0.
١	U12	12	Silicon Rectifiers Epoxy 500mA up to 800 PIV	0.
ł	Ü13	30	PNP-NPN Sil. Transistors OC200 & 28 104	0
ı	U14	150	Mixed Silicon and Germanium Diodes	0.
ı	1'15	25	NPN Sil. Planar Trans. TO-5 like BFY51, 2N697	0.
i	U16	10	3 Amp Silicon Rectifiers Stud Type up to 1000PIV	0.
I	1.17	30	Germanium PNP AF Translators TO-5 like ACY 17-22	0.
ŀ	UIS	8	6 Amp Silicon Rectifiers BYZ13 Type up to 600 PIV	0.
ı	Ū19	25	Silicon NPN Transistors like BC108	0.
I	1'20	12	1.5 Amp Silicon Rectifiers Top Hat up to 1000 PIV	0.
ŀ	U21	30	AF. Germanium Alloy Transistors 2G300 Series & OC71	0.
l	U23	30	MADT's like Milz Series PNP Transistors	0.
ı	1'24	20	Germanium 1 Amp Rectifiers GJM Scries up to 300 PIV	0
ı	U25		300 MHz NPN Silicon Transistors 2N708, BSY27	0.
ı	[†26	30	Fast Switching Silicon Diodes like 18914 Micro.Min	0.
ı	U27	12	NPN Germanium AF Translators TO-1 like AC127	0.1
I	Û29	10	I Anio SCR's TO-5 can, up to 600 PIV CR81/25-600	1.0
ı	1'30		Plastic Silicon Planar Trans. NPN 2N2926	0.8
ı	1.31		Silicon Planar Plastic NPN Trans, Low Noise Amp 2N3707	0.1
ľ	U32		Zener Diodes 400mW DO-7 case 3-18 volts mixed	0.1
ı	1.33		Plastic Case 1 Amp Silicon Rectifiers 1N4000 Series .	0.1
ŀ	l'34	30	Silicon PNP Alloy Trans. TO-5 BCY26 28302/4	0.8
ı	1135	25	Silicon Planar Transistors PNP TO-18 2N2906	0 - 8
ı	U36		Silicon Planar NPN Transistors TO-5 BFY50/51/52	0.8
ı	U37	30 8	Sificon Alloy Transistors 80-2 PNP OC200, 28322	0.8
ı	U38	20	Fast Switching Silicon Trans. NPN 400 MHz 2N3011	0.8
ľ	U39	30	RF. Germ. PNP Transistors 2N1303/5 TO-5	0.8
	U40	10	Dual Transistors 6 lead TO-5 2N2060	0.5
	U41		RF Germanium Transistors TO-5, OC45, NKT72	0.5
	U42		VHF Germanhum PNP Transistors TO-1 NKT667, AP117	0.5
	U43	25 5	3il. Trans. Plastic TO-18 ASC, BC113/114	0.5

Code No's, mentioned above are given as a guide to the type of device in the pak. The devices themselves are normally unmarked.

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Q31	6 Silicon switch transistors 2N708	0.50					
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NFN	NFN	0.50	0.50	0.50			
NFN	NFN	0.50	0.50	0.50			
NFN	NFN	0.50	0.50	0.50			
NFN	NFN	0.50	0.50	0.50			
NFN	NFN	0.50	0.50	0.50			
NFN	0.50	0.50	0.50	0.50			
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NFN	0.50	0.50	0.50	0.50			
NFN	0.50	0.50	0.50	0.50			
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NFN	0.50	0.50	0.50	0.50			
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NFN	0.50	0.50	0.50	0.50			
NFN	0.50	0.50	0.50	0.50	0.50		
NFN	0.50	0.50	0.50	0.50	0.50		
NFN	0.50	0.50	0.50	0.50	0.50		
NFN	0.50	0.50	0.50	0.50	0.50	0.50	
NFN	0.50	0.50	0.50	0.50	0.50	0.50	0.50
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U 3	75	Germanium Gold Bonded Sab-Min. like OA5, OA47	0.50
U 4	40	Germannin Transistor-like OC81, AC128	0.50
Ü 5	6	200mA Sub-Min, Schoon Diodes	0.50
11 6	- 30	Sil. Planar Trans. NPN like BSY95A, 2N706	0.50
U 7	14	Sil. Rectifiers TOP-RAT 750mA VLTG. RANCE up to 100	0.0.50
1.5	56	Sil. Planer Diodes DO-7 Glass 250mA like OA200/202	0.50
0.9		Mixed Voltages, I Watt Zener Diodes	0.50
1,10		BAY50 charge storage Diodes DO-7 Glass	0.50
1'11	25	PNP 84. Planar Trans. TO-5 like 2N1152, 2N2904	0.50
U12	12	Silicon Rectifiers Epoxy 500mA up to 800 PIV	0.50
U13	30	PNP-NPN Sil. Transistors OC200 & 28 104	0.50
U14	150	Mixed Silicon and Germanium Diodes	0.50
1.12	25	NPN Sil. Planar Trans. TO-5 like BFY51, 2N697	0.50
U16	10	3 Amp Silicon Rectifiers Stud Type up to 1000PIV	0.50
1.12	30	Germanium PNP AF Transistors TO-5 like ACY 17-22	0.50
UB	8	6 Amp Silicon Rectifiers BYZ13 Type up to 600 PIV	0.50
U19	25	Silicon NPN Transistors like BC108	0.50
1,50	12	1.5 Amp Silicon Rectifiers Top Hat up to 1000 PIV	0.50
0.51	30	AF. Germanium Alloy Transistors 2G300 Series & OC71	0.50
1,53	30	MADT's like MHz Series PNP Transistors	0.50
U24		Germanium 1 Amp Rectifiers GJM Scries up to 300 PIV	0.50
U25	25	300 MHz NPN Silicon Transistors 2N708, BSY27	0.50
U26		Fast Switching Silicon Diodes like 1N914 Micro-Min	0.50
U27		NPN Germanium AF Translators TO-1 like AC127	0.50
U29		1 Anio SCR's TO-5 can, up to 600 PIV CR81/25-600	1.00
1'30		Plastic Silicon Planar Trans. NPN 2N2926	0.50
f.31		Silicon Planar Plastic NPN Trans, Low Noise Amp 2N 3707	0.50
U32		Zener Diodes 400mW DO-7 case 3-18 volts mixed	0.50
U33	15		0.50
1135	40.5	Silicon PNP Alloy Trans. TO-5 BCY26 28302/4	0.50
U36		Silicon Planar Transistors PNP TO-18 2N2906	0.50
U37	20	Silicon Planar NPN Transistors TO-5 BFY50/51/52 Silicon Alloy Transistors SO-2 PNP OC200, 28322	0.50
(i38		Fast Switching Silicon Trans. NPN 400 MHz 2N3011	0.50
U39		RF. Germ. PNP Transistors 2N1303/5 TO-5	0.50
U40		Dual Transistors 6 lead TO-5 2N2060	0.50
U41	25	RF Germanium Transistors TO-5, OC45, NKT72	0.50
U42		VHF Germanhum PNP Transistors TO-1 NKT667, AP117	
U43	25	Sil. Trans. Plastic TO-18 A.F. BC113/114	0.50
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A must for e ast. Size: 2 c instructions.

Q36 Q37

Q38

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ı		12×7402	0.50	UIC48 =	5×7448	0.50	UIC91 -	5×7491	0.50
l		12×7403	0.50	U1C50	12×7450	0.50	UIC92 =		0.50
	UIC04 -		0.50	UIC51	12×7451	0.50	U1C93 -		0.50
	UIC03 -	12×7405	0.50		12×7453	0.50	UIC94		0.50
	UIC06 →	8 × 7406	0.50		12×7454	0.50	UIC95		0.50
	UICO7 = I	3 × 7407	0.50		12×7460	0.50	UIC96 -		
	UIC10 -		0.50	1'IC70 -		0.50	HICIO	5 × 74100	0.50
	UIC13 - 8		0.50	111072-1		0.50	VICTOU .	0 X 74100	
	UIC20		0.50	UIC73				5×74121	0.50
	UIC30 - 1		0.50			0.50		5×74141	0.50
	I'IC40 - 1			UIC74 = 1		0.50		5 × 74151	
			0.50	UIC75 = 8		0.50		5 × 74154	
	UIC41 = 3		0.50	1.10.19 1		0.50	1 IC193 -	5 × 74193	0.50
	U1C42-5		0.50	UIC80 - 3		0.50	UIC199 =	5×74199	0.50
	1°1C43 = 5		0.50	UIC81-5		0.50			
	U1C44 5		0.50	UIC82 - 2	× 7482	0.50	UICXI =	25 Assorte	d
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Devices may	be mixed	lo qual	Ify for	
quantity price				
on application				

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Anode voltage (Vdo)	170min	178 min	δ
Cathode Current (mA)	2.3	14	8
Numerleal Height (mm)	16	13	9
Tube Height (mm)	47	32	22
Tube Diameter (mm)	19	13	12 wide
I.C. Driver Rec.	BP41 or 141	BP41 or 141	BP47
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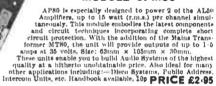
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Three switched stereo inputs, and rumble and scratch filters are features of the PA100, which also has a STELEO/MONO switch, volume, balance and continuously variable base and treble controls.

SPECIFICATION

Frequency Response Harmonic Distortion Inputs: 1. Tape Head
2. Radjo, Tuner
3. Magnetic P.U. 20Hz = 20KHs \pm 1dB better than 0·1% 1·25 mV into 50K Ω 35 mV into 50K Ω 1·5 mV into 50K Ω

All input voltages are for an output of 250mV. Tape and P.U. input-equalised to RIAA curve within \pm 1dB, from 20Hz to 20KHz.

Bass Control Treble Control
Filters: Rumble (High Pass)
Scratch (Low Paus)
Signal/Noise Ratio Input overload Supply Dimensions

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± 15dB at 20Hz ± 15dB at 20KHz ± 15dB at 20KHz 8KHz better than - 68dH + 26dB + 35 volts at 20mA $292mm \times 82mm$

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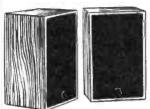
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REALISTIC SA-100B 6-WATT STEREO AMPLIFIER

Here's fabulous, exciting value in miniature! This high quality stereo amplifier measures only 9" wide = 3" high - 5%" deep. And yet it has separate ganged volume, balance and tone con trols Plus speaker in out, mono stered, phono

tuner and power on loff slide switches. The ends are oiled walnut, with match-ing enamelled metal top. The front panel is satin aluminium and walnut-brown enamel. Frequency response is 50 to 10 000 Hz. 348. Output 3 watts r.m.s. per channel into 8 ohms. Inputs are 100mV for both phono and tunes



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STEREO The A-3000 looks as good as it sounds! Giving you e big performance this superb audio emplifier has a full range of facilities on the front and rear panels. On the front -all the controls you're ever likely to need plus a headphone socket. On the rear signal inputs, speaker outputs and a line fuse for circuit protection.

Specifications: 18 watts rms per channel Specifications: 18 watts rms per channel nito 8 ohms. Frequency response 20-35.000 Hz (± 2db) Inputs Magnetic. Ceramic. Tuner, Tape. Aux. Tape Play. Size: 345mm > 300mm > 130mm.

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This is one of the lowest priced stero tuner amplifiers on the market. It covers the full range of both AM and FM broadcast frequencies. And when you're switched to FM, an indicator lights up when a stereo signal is received – that's the time to switch to "Stereo"! The SSA-16 has all the facilities you'd expect to find on tuners costing twice as much - separate vol-ume, bass, treble, balance and tuning controls. Selector switch for tape, phono, AM, FM, stereo, Jack socket on front panel for



incorporates two separate speaker units an 8" wonfer and a 5

mid-range with 2" concentric tweeter. Power handling

OLSON AM-400 4 WATT STEREO AMPLIFIER Here's marvellous value for someone just starting to set them-selves up in audio! At only £10.50, you get a fine amplifier in a scratch resistant metal cabinet, with a smart brushed aluminium front panel. It incorporates separate tona and volume controls for each channel. Inputs are provided for turntable (ceramic cartridge), tuner and tape deck or racorder, Frequency response: 70-20,000 Hz - 3dB, Output 2 watts r.m.s. per channel into 8 ohms. Inputs: phono 80mV, tuner/aux 80mV, Size 8" wide, 2½" high,

for tape, pnono, AM, rM, stereo, Jack socks on front panel 100 stereo headphones, Frequency range: FM 88-106 MHz, AM 535-1605 kHz, Frequency response: 50-10,000 Hz = 346. Power output: 4 watts total music power into two 8 ohm speakers, Size: 16"wide, 4½" nigh, 8" deep. RDC 7-WATT STEREO AMPLIFIER

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OLSON AM-372 16-WATT STEREO AMPLIFIER R Here's a really good amplifier at a really down-to-earth price nearly £7 less than the normal retail value! Just look at what the AM-372 will do for you — reproduce signals from ceramic or crystal cartridges, AM and FM tuners, and tape recorders. And it gives you outputs for two sets of speakers, headphones and tape recorders. Frequency response is 30 to 20,000 Hz 🚣 3dR Output 8 watts r.m.s. ner channel music nower into 8 ohm speakers. Phono input 200mV. Tuner input 200mV. Size: 121" wide, 31" high, 73" deep.

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9	17100	. 40	PCC88	.89		.31	U801	.76	ACY28	.18	BFY50	.23	OC35	. 32
0	EL86	. 38	PCC89	.42	PY801	. 81	174020	.38	AD140	.36	BFY51	.19	OC36	.43
8	EL91	. 23	PCC189	.46	PZ30	.48		.40	AD149	. 50	BFY52	. 20		.10
8	EL95	. 32	PCF80	. 26	QQV03/1		VP41	. 38	AD161	.45	BY 100	.18	OC45	.11
0	ELL80	.75	PCF82	.30		. 20	VT61A	. 85	AD162	.45	BY105	.18	OC46	. 15
9	EM80	.37	PCF84	. 40	Q875/20	. 63	VU111	.44	ADT140		BY114	.18	OC70	. 13
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BUSH A1005	69 - 89	50 95	Input with bullt-in 8-track cart-		
DANSETTE Consort Stereo	34 - 43	23 - 95	ridge player with speakers	69 95 56 25	41 · 50 39 · 95
DANSETTE 4005	71 - 45	49 - 95	GRUNDIG TK 141 (4-track) GRUNDIG TK 141 (4-track) GRUNDIG TK 145 (4-track auto) GRUNDIG TK 146 (4-track auto) GRUNDIG TK 147 (4-track auto) GRUNDIG TK 148 (4-tr. auto 2 spd.)	62 - 10	45.95
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ALBA UA 552 BUSH A1005 DANSETTE COnsort Stereo DANSETTE 4005 DANSETTE 4020 DECCA SOUND 613 DECCA SOUND 613 DECCA COMPACT 2 with Radio S DECCA COMPACT 3 with Radio S DECCA COMPACT 3 with Radio S DECCA COMPACT 3 with Radio S	p. Price	e 97-95	GRUNDIG IN 240 4-Track Stereo		404 5
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PRACTICAL WIRELESS

VOL 48 NO 12

Issue 794

APRIL 1973

The Buyer and VAT

During these last few weeks before Value Added Tax takes effect, readers will be contemplating whether to buy now or wait until after April 1st. It will undoubtedly pay to wait on such items as domestic receivers, some Hi-Fi equipment and electrical goods, but component suppliers are being hard pressed to meet demand before the infliction of VAT.

One way of circumventing purchase tax has been to supply equipment in kit form, but these items in any form will be liable for VAT at one common percentage rate, since VAT is a tax on the basic purchase price or charge

for service.

We would expect that all suppliers will make it quite clear to all customers, at the trading premises and through advertisements, whether quoted prices include VAT. The basic retail price should remain the same as now. Whatever you pay for goods or services from April 1st, you should not be paying any purchase tax or selective employment ax levies; you should be paying VAT on top of the normal retail price, based on the Chancellor's Budget announcement on March 6th.

Kit and component prices should not be raised before April 1st and manufactured goods subject to purchase tax of more than 15% should be noticeably reduced after

April 1st.

Shopkeepers and other traders are not legally bound to show the amount of VAT in cash transactions; neither will they necessarily show special "tax invoices" for retail sales, but it is worth remembering that if you purchase at a cut price rate, the VAT charged will be correspondingly lower. Goods obtained by hire purchase or credit agreements will be subject to tax at the current rate at the time when transaction documents are signed. Interest rates on these terms are not taxable. Private sales between individuals do not attract VAT because neither party is defined as a "taxable person", unless the seller is a trader required to register with H.M. Customs and Excise.

Our advice to readers who are thinking of buying goods by mail order during March is to determine first whether purchase tax is chargeable; if it is then wait until April. Items not subject to purchase tax (such as components and secondhand or used goods) should be ordered early. If of substantial value, send your order by P.O. "Recorded Delivery" and keep the counterfoil of your Postal Order,

Money Order, or cheque.

You should be prepared for a VAT levy on charges for packing service but not for postage.

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Arthur Dow	1124

THE MAY ISSUE WILL BE PUBLISHED ON APRIL 6th

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NEWS...

NEWS...

NEWS...

by Colin Riches

VAT

To the best of our knowledge, the prices quoted in this issue were correct at the time of going to press.

From April 1st 1973, there will be no purchase tax but a large number of goods will carry Value Added Tax. For further details, see our Leader article.

Tulip Time Rally

The 1973 "Tulip-Time" mobile rally will be held on Sunday May 6th at Surfleet, 4 miles north of Spalding on the A16.

The Spalding and District Amateur Radio Society will also be operating a Special Activity station, GB3STF on 12th-13th May from The Grammar School, Priory Road, Spalding, in connection with the 1973 Tulip Festival. Operation will be on s.s.b./c.w. on all bands 160-10m. with a.m. on 2m. All contacts will be confirmed by special QSL cards.

Of interest to "Going Back" fans—the Wireless Preservation Society will have an exhibition of vintage radio on show to the public. I hope to be able to publish further details later.

RSGB "Jubilee Year" President



Pholograph by P. M. Fletcher.

This picture shows Dr. J. A. Saxton, D.Sc., PhD, CEng, FIEE, FInstP, the new President of the RSGB. On the left of the picture is Swedish Amateur Lt. Col. Per Anders Kinman, SM5ZD, who received the Calcutta Silver Key award. Sir John Eden, the P.M.G. is on the right.

In his address, Dr. Saxton said he felt very proud that he had been chosen as President of the RSGB for its Diamond Jubilee Year. He also said that he was extremely delighted that Sir John had been able to attend and that all there were greatly honoured by his presence.

Dr. Saxton went on to say that the Society would continue to do all in its power to continue to deserve the Ministry's support.

Per Anders Kinman has been made an Honoury Vice President of the RSGB in recognition of his outstanding service with the IARU Region 1 in which he has served for many years.

The Calcutta Key he received was first presented 20 years ago and it has been awarded annually by the RSGB to the person they feel has made, in any one year, the most significant contribution to international friendship and goodwill through the medium of Amateur radio.

The Buyer and VAT

continued from previous page

If you order from a current catalogue or advertisement after April 1st, you should add the VAT percentage rate to the basic retail price shown. Then add the estimated or stated charge for postage and packing. If a service is chargeable, such as equipment repair or consultation, VAT will be levied at the standard rate. Trading in second-hand and used goods will also be taxable under VAT.

Finally, good news for P.W. readers: newspapers and magazines will be "zero-rated", which means that no VAT is chargeable on these. Transactions of any kind in the U.K. for the direct exportation of goods and services are exempt from VAT.

M. A. COLWELL-Editor.

Feb P.W. Cover

Many enquiries have been received for information on the book and log book shown on the front cover of the February issue of PW. Both can be obtained from the Radio Society of Great Britain, 35 Doughty Street, London, W.C.1. "How to Listen to the World" costs £2 post paid. The log book shown is intended for transmitting Amateurs and costs 60p post paid but another one, intended for listeners, is available at 45p post paid.

NEWS...

NEWS...

NEWS...

Cordless Iron

This cordless soldering iron comes from the U.S.A. It is completely portable needing no mains power for operation. It has its own power supply which is automatically charged from the stand which itself is connected to the mains. There is a small light near the tip which is very useful for seeing exactly where you are applying heat.

The iron heats up in under 5 seconds and has an "indestructible" iron-plated bit. It costs £9.25 complete with charging stand and fine bit. A heavy-duty bit is also available.

The exclusive distributors in Great Britain are Pact International Electronics Ltd., P.O. Box 19, Royston, Herts, SG8 5HH.



Sonex 1973

The technical author and writer Donald Aldous will be heading a small team to organise the Special Features at "Sonex '73".

Two recital/lecture sessions will be presented each day at the Exhibition's new venue the Excelsior Hotel, London Airport, Heathrow.

Speakers will include Bert Webb, who will lecture on pickups, arms and turntables and Kenneth Shearer, speaking on listening room acoustics.

There will also be a lecture on tape' cassettes and an examination of current loudspeakers and trends

Sonex '73 will run from Friday, March 30th to Sunday, April 1st, inclusive.

Sound '73

"Sound '73" is the exhibition run by the Association of Public Address Engineers. New P.A. equipment and new techniques in the public address and allied fields will be on show.

As in past years, there will be a lecture programme held in the hotel's "City Room". John Maunder from Shure Electronics will give a lecture and demonstration on microphones on Tuesday, 13th March at 14.30hrs.

Mike Beville from Audio and Design Recordings Ltd. will lecture on Components and Limiters (Wednesday at 14.30hrs.)

On Thursday March 15th at 10.30hrs, a member of the Hornsey College of Art will talk on Industrial design of Public Address Equipment.

Venue will be the Bloomsbury Centre Hotel, March 13-15, from 10.00-18.00hrs.

I.E.E. Conferences

The following new conferences to be held in 1973 and 1974 are being organised by the Institution of Electrical Engineers.

"Electrical Signals from the Brain" 27-30 August 1973—in Oxford.

"Symposium on Electromagnetic Wave Theory" 8-12 July 1974—in London.

Further details of the conferences mentioned above are available from the Conference Department, IEE, Savoy Place, London WC2R OBL.

De-soldering Unit

In the February issue we mentioned the Litesold De-Soldering Unit and a misprint stated the price at £.75. This should have read £2.75. Apologies to Light Soldering Developments and any readers that may have been inconvenienced.

Jermyn Inverters

Jermyn Distribution market two inverters, both giving an output of 250V. Input for the 150W version is 12V and for the 300W type, 24V.

A feature of the design enables these inverters to charge the 12/24V batteries up to 10A when plugged into a power socket.

If the mains supply fails, the inverter automatically switches to its "invert mode" providing 240V emergency power immediately.

Should the unit be accidentally overloaded its drive is so adjusted, that the output voltage falls completely, switching the

JERMYN...300...

unit off, eliminating any problems.

An internal 15A fuse blows should the battery leads be connected wrongly. Indicator lights illuminate to show whether the unit is charging a battery or providing a 250V 50Hz output.

Both types of inverter can be obtained in kit form or already built. The kit for 150W costs £25 (£29 built) and 300W £34 (£39 built). Jermyn Distribution, Vestry Estate, Sevenoaks, Kent.



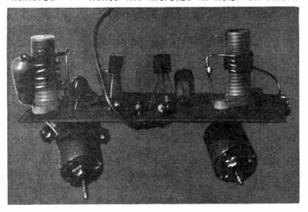


HF radio provides a most useful signal source for any hi-fi enthusiast and, despite the 15 kHz frequency limits, the live BBC broadcasts are certainly up to the standards of the finest records.

The advantages are numerous—being a non-mechanical system the distortion is very low and the self-generated noise is also very low, the result being a large dynamic range and the possibility of encoding two channels on a single signal. This, plus the excellent BBC technique, makes f.m. radio an invaluable source of material. Unfortunately there are several difficulties in securing top quality f.m. regardless of the equipment used.

SIGNAL-TO-NOISE

Referring to Fig. 1, it can be seen that the performance of a receiver depends on the strength of the signal applied to the aerial socket of the receiver. The mono signal-to-noise ratio assumes an optimum value (usually 50 or 60 dB) with only a few μV input—even on cheap tuners. The signal-to-noise performance does not improve so rapidly on stereo, however, and in many cases could be improved on even with inputs in the region of a few hundred μV —hence the increase in noise on stereo



First of the two VHF amplifiers described in the article. This one uses field-effect translators.

in most situations. A person who gets no increase in noise is indeed most fortunate and need read no further!

As regards crosstalk and distortion, these parameters usually reach optimum values with fairly small inputs and usually there is not much improvement to be had by an increase in the signal.

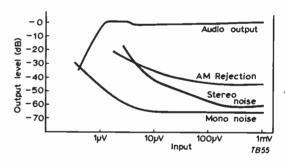


Fig. 1: Graphs comparing receiver performance with the input signal level.

Very few people are fortunate enough to be able to receive "near perfect" stereo without a large aerial, loft or roof mounted. A large aerial, besides having the necessary gain usually has the advantage that it is highly directional and eliminates multipath distortion from reflected signals. In many situations, a reasonably large aerial, three or more elements, carefully sited, and with a low loss feeder gives good stereo but perhaps not of the very highest quality.

The major downfall in domestic stereo reception is that of "stereo" noise—perhaps not excessive but sufficient to mar an otherwise excellent signal. The obvious way to reduce this noise is to increase the signal feeding the tuner by an "aerial amplifier". At present in this discussion we must assume that the amplifier be perfect, having gain but generating no noise itself.

OTHER NOISE

At this point many readers may well be wondering about the other forms of noise, thermostats, car ignition and other spurious signals. These signals are picked up by the aerial and sometimes, even, by the feeder, and consequently will be amplified, together with the f.m. signal, by our "ideal" amplifier, which we are using to combat stereo noise. This brings us to the last important parameter of f.m. receivers, amplitude modulation limiting.

The "ideal" f.m. tuner is designed to respond to f.m. only and a.m. signals are rejected to an infinite degree. Unfortunately, no receiver is perfect and some degree of sensitivity to a.m. is unavoidable.

The a.m. limiting of the receiver improves with increasing signal input, as seen from Fig. 1, so that increasing the signal and spurious a.m. together actually reduces the level of audible interference. Unfortunately, when the receiver is switched to receive a stereo transmission, the stereo decoder in the receiver is actually only sensitive to amplitude modulation of the stereo subcarrier. In the decoder some measure of a.g.c. is applied to the subcarrier amplifier and this maintains a constant level of stereo interference from an a.m. signal regardless of the actual input voltage to the tuner.

It can therefore be seen that whilst increasing the tuner input with an "ideal" amplifier, the "stereo" interference level remains substantially constant whilst the "mono" component of the audible interference has been reduced by virtue of the amplitude limiting of the f.m. discriminator.

AERIALS

Earlier in this discussion, we talked of elaborate and efficient aerial systems but the previous discussion on aerial signal amplification implies that, with a good amplifier, an aerial providing only a minimal "clean" signal can be used to run an f.m. tuner with a high degree of success.

Unfortunately, some tuners are not so sensitive as others and sometimes require millivolts to function at their best. This means considerable amplification of the few tens of microvolts coming from a rather poor aerial!

The better tuners nowadays use f.e.t.'s in the input circuits to keep noise to a minimum and to keep cross modulation low; so any proposed amplifier should have at least as good a performance as the front end of the tuner.

This is very demanding when tuners such as Sony, Radford and Fisher are considered, but it is possible to improve these tuners on a very poor signal by a remarkable degree.

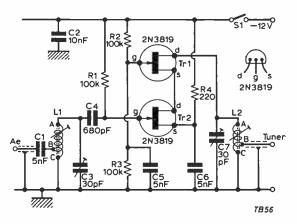


Fig. 2: Circuit of the amplifier using two f.e.t.'s.

To design an amplifier with a front-end comparable to the best tuners use has to made of f.e.t. devices which possess the best noise properties of all the common solid state devices presently available and are responsible for the excellent performance of the best tuners.

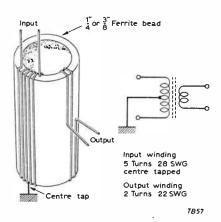


Fig. 3: Details of simple transformer to match balanced 400 Ω feeder to 75 Ω coaxial feeder.

The design chosen for the amplifiers in this article is not often used with solid state devices but was once very common with valve Band III television tuners. The amplifier is a cascode configuration giving reasonable gain with very low noise and good cross modulation.

The input to the amplifier, Fig. 2, is 750 co-axial feeder so Fig. 3 shows a transformer that can be constructed from a small ferrite bead for 4000 balanced feeder.

THE PCB

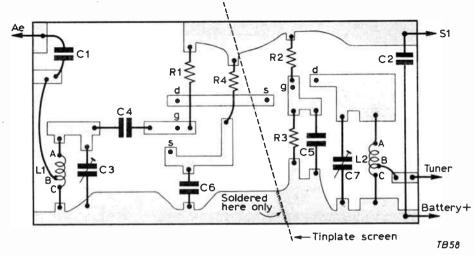
The amplifier can be very easily built on a single piece of printed circuit $4'' \times 2''$ and it is recommended that fibreglass board be used.

To etch the required print design as shown in Fig. 4 (full size), the diagram is traced on to the copper side of the print with carbon paper and the marked areas painted in with high quality enamel. When the paint is dry, the print is immersed in the etching solution and agitated until completely etched (only paint and base material can be seen). The etching solution can be ferric chloride solution but a useful alternative is "Liquor-Ferri Perchloridi Fort" which is obtainable from chemists and should be used undiluted. Rub the copper surface of the board with "Ajax" or similar scourer before painting, to ensure a clean surface.

The enamel paint can be removed with paint stripper once the etching is complete and the board washed and cleaned with wire-wool. The holes for the components should be drilled with a 'x2" drill, preferably in a wheel brace.

Construction is straightforward except that the f.e.t.'s should be left until last and soldered in with the iron disconnected from the mains—surprisingly little voltage will break down the gate junction.

The coils, Fig. 5, are wound on the formers which are located on the board and stuck with Araldite. The 30pF variable capacitors must be connected so that the rotor is connected to the earth line. The author used 30pF Philips beehive trimmers mounted



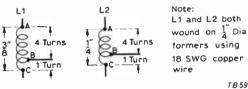


Fig. 5: Winding information for L1 and L2.

★ components list

×	COI	пропенс	1151					
Γ		AMPLIFIER						
	Resis							
	R1	100kΩ R2	100kΩ All	R3 1W 5	3 100kΩ %	. R4	220Ω	
	Capacitors							
i		5nF 400V		C5	5nF 12\	/		
1	C2	10nF 12V		C6	5nF 12\	/		
	C3	30pF Trimme	r ,	C7	30pF Ti	rimmer		
	C4	680pF 12V						
	Miscellaneous							
	Tr1-Tr2, 2N3819. On-off switch. 12V battery. Co-axial							
	sockets (2). PCB, see text. Coll formers.							
	BF200 AMPLIFIER							
!	Resis		50. 0.4			401.0		
			R3 6-8		R5			
	R2	10kΩ	R4 1.5		R6	6·8kΩ		
All &W 5%								
il .		citors						
		1nF_400V		C6				
	C2	30pF Trimme	r	C7	10nF 12	.V		
	C3	10nF 12V			680pF 1			
		680pF 12V			1nF Fee			
	∑ C5	1nF Feed-thre	ougn	C10	30pF	rimme	r	
Miscellaneous								
l	Tr1-Tr2, BF200. On-off switch. 12V battery. Co-axial							
	sockets (2). PCB, see text. Coil formers.							
POWER SUPPLY								
	Capa	citors		-			= 4014	

C3 2000µF 10V

R1, 10Ω $\frac{1}{4}$ W 5%. D1-D2, 1N4002. D3, 12V zener 2W, mounted on aluminium 2" \times 1" minimum. T1, 8V bell transformer. Fuse, 1A. On-off DP mains

switch. LP1, 3-5V 20mA for FET amp + 2 stages or

C2 2000µF 10V C4 1000µF 15V

3.5V 40mA for FET amp + 4 stages.

Fig. 4: Printed circuit board, for the circuit of Fig. 2, shown actual size.

on the copper side of the board. The resistors should be small low noise types and the capacitors need only be low working voltage.

The completed amplifier should be screened by placing tin plate at the position indicated and soldered to the positive line as support.

The amplifier is mounted in a small wooden box, measuring approx. 4" cube internally, covered inside with tin foil, which is connected to the positive supply line. A front panel can be made from a piece of double-sided copper board with the input and output sockets and the on/off switch. The printed board is soldered to the front panel by the positive line, so earthing the front panel.

With a 12V battery connected, the output is fed to the tuner and the input is fed by an "inefficient" aerial, in most cases a short piece of wire.

With the amplifier on, the tuner is switched to the local stereo station and the tuning capacitors C3 and C7 set midway. The cores in the coils (L1 and L2) are then adjusted to give the strongest signal, best observed on a tuning meter or audibly by judging least noise.

The amplifier is then assembled in the case and the capacitors C3 and C7 tuned to give the best signal. The tuning will be sharp and critical, so care should be taken when adjusting.

The amplifier, when connected between the proper aerial and tuner, should have sufficient gain to overcome most of the tuner noise, without introducing significant noise itself. When used on weak local radio stations, the improvement will be very marked, especially in mono. Unfortunately, this usually requires the amplifier to be re-tuned to the local channels. However, connecting 27Ω resistors across L1 and L2 will broaden the bandwidth considerably, enabling the amplifier to be used over a number of channels.

BF200 AMPLIFIER

However, for many of the "poorer" tuners, this amplifier will still not be good enough to fully drive the tuner on a moderate signal. For optimum stereo in such cases two of the amplifiers could be

Č1 100nF 1kV

Miscellaneous

C5 100nF12V

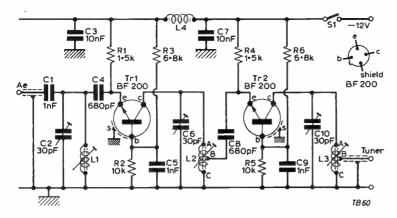


Fig. 6 : Circuit of the second amplifier, using BF200 transistors

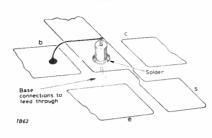


Fig. 8 Method of mounting feed-through capacitors

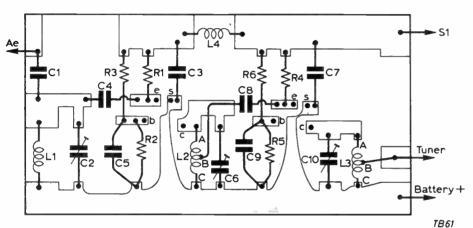


Fig. 7: Illustration, actual size. of the printed circuit board for the BF200 amplifier.

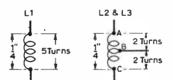
connected in series. The price of f.e.t.'s, however, makes this uneconomical and ordinary low-noise silicon transistors used after the f.e.t.'s work very well. The proposed amplifier, Fig. 6, is two stages of a conventional r.f. amplifier design. Fig. 7 shows a full size print layout for two stages, although for additional gain or bandwidth more stages can be used, although greater than five would be difficult to keep stable.

The board is etched in the same manner as before and a similar front panel and box are prepared. Alignment is the same, tuning the coils and finishing with the capacitors.

The transistors specified are BF200 and these should be used for at least the first two stages to keep the noise level down; after this such transistors as 2N706 work very well. An alternative for the BF200 is BF180 or BF181.

Fig. 8 shows how C5 and C9 are constructed with 1000pF feed-through capacitors. L4 is made by wrapping a few turns of 36s.w.g. d.c.c. copper wire round a ferrite bead. Fig. 9 gives the winding information for 1.1, 1.2 and 1.3.

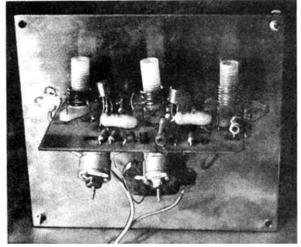
The two amplifiers just described will enable good stereo to be obtained from a mediocre signal without the need for a "fancy" tuner. The improvement that can be expected depends greatly on the individual circumstances. The author has used the amplifiers with a Sony ST5100 tuner and a poor aerial and found the results almost as good as when a proper aerial was correctly installed on the roof. The cost of a pair of amplifiers is comparable to a decent



Note: L1 L2 & L3 wound on $\frac{1}{4}$ Dia formers. L1 use 22 SWG copper wire. L2 & L3 use 18 SWG copper wire.

TB 63

Fig. 9: (above) Details of the three coils shown in Fig. 6. In the photograph (below) the second amplifier board is shown soldered to the front panel consisting of double-sided p.c.b.



aerial less downlead and fitting, so financially it is a viable proposition, although not a substitute for a first class aerial.

In order to split one signal to run several outlets and obtain maximum signal at each of the outlets, a star-splitter is used. This arrangement provides correct impedance matching throughout the system.

Figure 10 shows the circuit of a star-splitter. The value of the resistors R depends upon the impedance of the feeders (Z) usually 75Ω , and on the number of outlets (n) which can be as many as required.

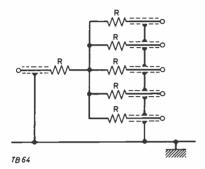


Fig. 10: Circuit of star-splitter enabling several outputs to be obtained from a single input.

The relationship is:— R=Z(n-1)/n+1. For example, for a splitter for a 75Ω system with two outputs the resistors to the nearest preferred value are 27Ω . Small $^{1}4W$ resistors are suitable and indeed preferable to physically larger types.

All of these systems involve a loss of signal and this must be made up by amplification before the splitting. For a distribution system, splitting six or

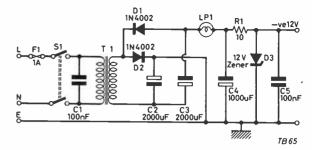


Fig. 11: Suggested power supply for the v.h.f. amplifiers.

eight ways, two f.e.t.'s followed by three transistors should be adequate. One important point to note is that the outputs of the splitter must all be loaded by a 75Ω resistor when not in use, otherwise a loss of signal results and the splitter may form the node of standing waves in the feeder.

If either of the amplifiers is built as a distribution system, it is perhaps a good idea to build a small mains unit to power the whole system. It is desirable that this supply be stabilised to guard against changes in the tuning of the f.e.t.'s if the supply voltage changes.

Fig. 11 gives a circuit of a simple power supply based on an 8V bell transformer with voltage doubling and zener stabilisation. The lamp, LP1, can be used to give on/off indication.

It is hoped that this article has given sufficient information for the home constructor to build an amplifier system to improve the performance of a tuner to reach the very high standards of the B.B.C. stereo transmisions.

EXPERIMENTERS CORNER

NOVEL TONE GENERATOR

HENEVER home constructors and experimenters need to build a source of audio frequency, the choice nowadays is usually a transistor multivibrator. The reasons for this selection are easily understood. It requires few components, avoids the need for a transformer and gives a strong output signal. These virtues outweigh the fact that the square-wave output does not make for a particularly pleasing sound when amplified and fed to a loudspeaker.

In designing the a.f. tone generator to be described, the author set out to devise a circuit which would possess all the aforementioned merits of the multivibrator and at the same time give a better audio tone. In the circuit shown in Fig. 1—which, as a transistor 'circuit, is thought to be original—the writer believes these objectives have been largely achieved.

N. NAUGHTON

It will be noticed that the circuit is actually simpler than a multivibrator and basically it is a sawtooth generator. Like all sawtooth generators it depends upon the charge and discharge times of a

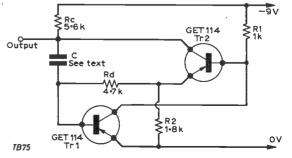


Fig. 1; Circuit of tone generator.

capacitor for its action. But as linearity of the sawtooth ramp is not important for the required purpose, the provision of constant current is omitted in the circuit shown.

In Fig. 1 the two transistors perform the function of switches and the circuit operates as follows:capacitor C charges via the charging resistor Rc and the base-emitter junction of Trl. The charging current flowing through the B-E 'junction turns on Trl and the flow of collector current causes a voltage drop across R1 which results in the potential on the base of Tr2 dropping to a level low enough to turn off Tr2. As the charge on C rises the charging current diminishes so that the potential on the base of Trl decreases to a point where Trl turns off. The base of Tr2 now goes strongly negative causing Tr2 to turn on and C now discharges via Tr2 into the discharge resistor Rd. While discharge current is flowing in Rd it maintains a positive potential on the base of Tr1 thus preventing further switching action during the period of discharge. When C has discharged, it again draws current through Trl once again turning off Tr2. The cycle then repeats.

The foregoing is a simplified description of the operation but many will find it interesting to measure the balance of currents and potentials which exist in the circuit under static conditions when C is removed.

The frequency of oscillation is not readily calculated since it is influenced by several factors one of which will be determined by the type of coupling employed to connect the output. However, for practical purposes values of C ranging between $2\mu F$ and 5000pF will cover the audio spectrum.

APPLICATIONS

A useful feature of the circuit is that it uses only one capacitor. With the values given, the generator should oscillate at any point within the a.f. range the actual point being determined by the value of C selected. Thus it becomes a simple matter to construct a signal generator giving a number of spot frequencies as desired; the only extra components needed being a multi-pole switch and a few capacitors. Many other audio applications will doubtless occur to readers.

For those interested, an interesting feature of the circuit is that because the charge and discharge paths of C are independent, the circuit can readily be made to produce right-handed or left-handed sawtooth waveforms. Moreover, by choice of p.n.p. or n.p.n. transistors, the polarity of either slope can be created as desired at source, thereby eliminating inverting stages. Although some value of Rd is essential for circuit function, in practice this can be less than 1000 thus allowing fast flyback times. There is no reason why C can not be a very large value electrolytic so that the circuit can easily be adapted for timing application.

GENERAL

No constructional details are given since the generator will mostly be incorporated in some larger project. Experimenters can assemble the components on a length of Veroboard or tagboard.

As stated at the outset, the circuit is primarily intended as an a.f. generator and the values given have been chosen to give a roughly pyramid waveform at the collector of Tr2. A strong output signal is also available at the collector of Tr1 but this is a

steep sided pulse and the "softer" toned signal at the Tr2 output can be readily appreciated. Coupling of the output is perhaps best determined to suit the individual case but too tight a coupling to the Tr2 output is best avoided. This is less important if the Tr1 output is used.

With the component values given, the circuit places no critical demands on the transistors' characteristics. Seven widely differing types, in various combinations, have been tried with success. However, experimenters using low values of Rd—especially with a high value of C—should note that Tr2 must then be a device capable of handling the heavier discharge current. Tr1 and Tr2 must both be either p.n.p.'s or n.p.n.'s, the -9V becoming +9V if n.p.n.'s are used.

TELEVISION

APRIL ISSUE

TOUCH TUNING

The latest development in television receiver design is touch-sensitive tuning, using touch-button units which provide a completely non-mechanical means of channel changing. A very high-impedance electronic switching circuit selects the required channel when a finger is placed across a pair of contacts to complete the appropriate circuit. Several models featuring touch tuning are now on the market and this month we are investigating the technique and the circuitry involved. The change from mechanical to all-electronic channel selection should improve the stability and reliability of TV tuning.

BAND III PREAMPLIFIER

Another Bunney wideband aerial amplifier intended for DX work. The two-transistor (BF272) design on test lifted a weak signal from mere traces of line sync pulses to a solidly locked noisy image. Part of Roger's present programme of improving his DX receiving equipment.

SERVICING

Plenty on the servicing front this month. John Law in his new fault-finding series investigates the line timebase used in most KB-STC models. Vivian Capel completes his guide to power supply circuit servicing. Les Lawry-Johns starts on the single-standard Bush-Murphy TV1815/V2016 series. And Caleb Bradley takes us further with the BRC 2000 colour chassis.

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IC POWER AMPLIFIER

D. SILVESTER

THE audio amplifier to be described was designed to deliver in excess of 10W r.m.s. into an 8Ω load, whilst being constructed in a 4½in. x 3½in. x 2in. diecast aluminium box. The size of the box is, in fact, limited not by the size of the i.c. but by the passive components, especially the output capacitor which must be included in the circuit. The use of the i.c. has added one inestimable advantage in that the current through (and the power dissipated by) the output stage under overload conditions can be limited. It is thus possible for the output to be short circuited without disastrous results.

The i.c., although capable of giving a 1 watt output without any other transistors, has been primarily designed for use as the driver stage of an amplifier

capable of delivering up to 35 watts into an 8Ω load.

A description of the working of the i.c. has not been included as it is not necessary for the constructor to completely understand the operation of the device for it to be used successfully.

Two transistors in the i.c. are responsible for the current and power limiting facility. It was calculated that under maximum current limiting and with the normal current gain of a power transistor, the output stage of the i.c. would be overloaded. One way of curing this fault is to use a Darlington transistor. This in fact was done, the Darlington pair being contained in the TO3 metal case of the power transistor. The current gain of the complementary Darlington pairs is in excess of 1000.

CALCULATIONS

The final circuit used for the prototype amplifier is shown in Fig. 1 but since other constructors may wish to use different power supply voltages and load impedances from those used by the author, the method of calculation of the current and power limiting components is given. The basic circuit should be adhered to as it is only the values of R6, R8, R9 and R11 which need to be changed.

The following section shows the worked equations used to give the value of the components in Fig. 1.

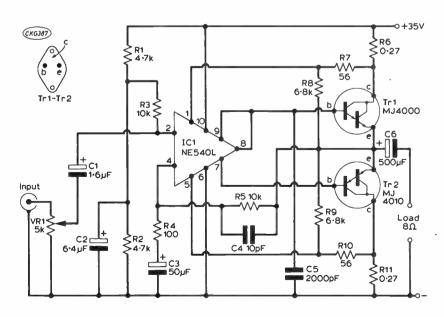
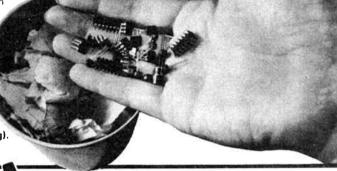


Fig. 1: Circuit diagram of the amplifier and pin connections for the output transistors.

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MODEL CN

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MODEL CN2

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TRAI	NSIS	TORS		2N4931 2N5172	2·70 0·08	AF116 AF117	0-25 0-20	BC307 BC307A	0·10 0·10	BF271 BF272	0-21 0-63
2G801	0.15	2N2924 2N2925	0.18	2N5174	0.22	AF118 AF121	0.50	BC307VI	0.10	BF273	0.25
2G302 2G303	0·15 0·25	2N2926	0-18	2N5176 2N5176	0-28 0-32	AF124	0-22 0-24	BC308 BC_08A	0.08	BF274 BF457	0·28 0·46
2G306 2G309	0-80 0-80	Green Yellow	0·10 0·10	2N5245 2N5190	0-48 0-98	AF125 AF126	0-20 0-19	BC308B BC309	0-09 0-10	BF458 BF459	0-57 0-57
2G344 A 2G345B	0.25 0.25	Orange 2N3053		2N5191 2N5192	0.96 1.24	AF127 AF139	0-20 0-88	BC309A BC309B	0·10 0·10	BF821 BF821A	2·10 2·30
2G371	0.15	2N3054	0.47	2N5193	1.01	AF170	0.25	BC313	0-80	BF828	0.92
2G374 2G381	0·15 0·22	2N 3054 2N 3055	0-46 0-50	2N5194 2N5195	1-10 1-46	AF172 AF178	0·25 0·55	BC327 BC328	0-24 0-23	BP861 BP898	0·27 0·28
2G417 2N109	0-20 0-49	2N3390 2N3391	0.20	2N5245 2N5457	0-48	AF179 AF180	0-85 0-50	BC337 BC338	0-19 0-19	BFW10 BFW11	0-61 0-61
2N174	1.40	2N3391A	0.22	2N5458	0-88	AF186	0.40	BCY30	0-25	BFW15	0.85
2N176 2N274	0-75 0-75	2N3392 2N3393	0·18	2N5459 3N128	0-88 0-68	AF200 AF239	0-85 0-41	BCY31 BCY32	0-40	BFX 13 BFX 29	0-23 0-25
2N335 2N351	0-75 0-95	2N3394 2N3402	0-18	3N138 3N199	1-87 1-86	AF240 AF279	0·78 0·54	BCY32 BCY33	0-75 0-84	BFX30 BFX37	0-25
2N376	1.00	2N3403	0-19	3N140	0.76	AF280	0.54	BCY34	0-85	BFX44	0.88
2N384 2N388A	0-98 0-40	2N3404 2N3405	0-24 0-27	3N141 3N142	0·69 0·54	AFY42 AF211	0·74 0·55	BCY38 BCY39	0·40 1·05	BFX68	2-48 0-80
2N404 2N404	0·28 0·20	2N3414 2N3415	0-10 0-10	3N143 3N152	0-84 0-79	AL102 AL103	0-75 0-70	BCY40 BCY42	0-50 0-15	BFX84 BFX85	0·24 0·29
2N456 2N456A	0-75 0-75	2N3416 2N3417	0·15 0·21	3N153 3N154	0·74 0·74	ABY26 ABY27	0-80 0-86	BCY48 BCY58	0·15 0·21	BFX86 BFX87	0-24 0-25
2N457A	0.80	2N3570	1.25	3N159	1.00	ABY28	0.28	BCY59	0.22	BFX88	0.20
2N491 2N584	8-25 0-28	2N3571 2N3572	1·18 0·97	3N187 3N200	1·80 8·07	A8¥29 A8¥50	0-80 0-20	BCY66 BCY67	0-66 0-94	BFX89 BFY10	0-45 0-85
2N591 2N696	0-84 0-15	2N3702 2N3703	0·10 0·10	3N201	1.05	A8Y55 A8Z21	0-85 0-55	BCY70 BCY71	0·17 0·22	BFY11 BFY17	0-45
2N697 2N698	0-15 0-25	2N3704 2N3705	0·10 0·10	40050	0.78	AU103 BC107	1·25 0·14	BCY72 BCY87	0-18 8-47	BFY18 BFY19	0-25 0-25
2N699	0.29	2N3706	0.90	40251 40309	0-81 0-88	BC108	0.18	BCY88	2-40	BFY20	0.50
2N706 2N706A	0·10 0·12	2N3707 2N3708	0·10 0·70	40310	0.50	BC109 BC113	0·14 0·18	BCY89 BCZ10	0-80 0-85	BFY29 BFY37	0-40 0-20
2N708 2N709	0·18 0·88	2N3709 2N3710	0.90	40313 40316	0-98 0-50	BC114 BC116	0·12 0·15	BCZ11 BD116	0·50 0·75	BFY41 BFY43	0·48 0·68
2N711	0-80	2N3711	0.90	40318 40322	0.92	BC118	0.15	BD116	0.75	BFY50	0.16
2N718 2N718A	0·21 0·80	2N3712 2N3713	0·95 1·08	40360	0-46 0-48	BC116A BC117	0·18 0·21	BD121 BD123	0-75 0-82	BFY51 VFY52	0·16 0·16
2N720 2N721	0-50 0-55	2N3714 2N3715	1-15 1-23	40361 40362	0.44	BC118 BC119	0·11 0·27	BD124 BD130	0·67 0·57	BFY53 BFY56	0-15 0-84
2N914 2N916	0·15 0·17	2N 3716 2N 3773	1-80	43063 40389	0-88 0-46	BC121 BC123	0·23 0·29	BD131 BD132	0-40 0-50	BFY64 BFY75	0.41
2N918	0.30	2N8774	3-83	40394 40395	0-56 0-50	BC125	0.15	BD135	0.48	BFY76	0·40 0·28
2N919 2N929	0.20 0.14	2N3775 2N3776	4-19 5-95	40406 40407	0-44 0-88	BC126 BC132	0.20 0.30	BD136 BD137	0-49 0-55	BFY77 BFY78	0-24 0-86
2N9.0 2N1090	0-14 0-23	2N3777 2N3778	4-84 2-25	40408	0.50	BC134 BC135	0·11 0·11	BD138 BD139	0-63 0-71	BFY90 BRY39	0-60
2N1091 2N1131	0-24 0-20	2N3779 2N3780	8-15 4-50	40409 40410	0-52 0-53	BC136 BC137	0-15 0-15	BD140 BDY10	0-88 1-25	B8X19 B8X20	0·18 0·14
2N1132	0-20	2N3781	8-67	40411 40414	2-00 8-55	BC188 BC140	0-20 0-84	BDY11 BDY17	1.50	B8X21	0.80
2N1184 2N1302	1·27 0·16	2N3782 2N3789	3·37 1·76	40438 40467 A	1-44 0-69	BC141	0.89	BDY18	1·50 1·75	BSX 28 BSX 27	0-84 0-84
2N1303 2N1304	0·16 0·20	2N3790 2N3791	1-90 2-06	40468A	0-44	BC142 BC148	0-24 0-21	BDY19 BDY20	1-97	B8X28 B8X29	0-25 0-47
2N1305 2N1306	0-20 0-22	2N3792 2N3794	8-20 0-10	40600 40601	0-67	BC144 BC145	0-84 0-81	BDY38 BDY60	0-65 0-90	BSX30 BSX59	0-88 0-78
2N1307	0-23 0-25	2N3819	0·26 0·47	40802 40603	0·46 0·58	BC147 BC148	0·11 0·10	BDY61 BDY62	0·85 0·75	BBX 60 BBX 61	0-54 0-42
2N1308 2N1309	0.25	2N3820 2N3928	0.50	40604 40636	0.56 1.10	BC149	0.18	BF115	0.28	B8X76	0-15
2N1483 2N1507	0-90 0-24	2N3824 2N3826	0·75 0·23	40673 AC107	0-56 0-85	BC153 BC154	0·18 0·18	BF117 BF119	0·48 0·58	B8 X 77 A8 X 78	0-20 0-25
2N1613 2N1631	0-20 0-35	2N3854 2N3854A	0-16 0-16	AC113	0.16	BC157 BC158	0·14 0·18	BF121 BF123	0·25 0·27	B8W70 B8Y24	0-28 0-20
2N1637 2N1638	0-80 0-27	2N3855 2N3855 A	0·16 0·16	AC115 AC117	0·16 0·20	BC159 BC160	0·14 0·37	BF125 BF127	0·25 0·27	B8Y25 B8Y26	0-15 0-20
2N1671	1·00 1·10	2N3856	0.16	AC121 AC128	0·18 0·20	BC167B BC168B	0·11 0·18	BF152 BF153	0.20	B8 Y27 B8 Y28	0·15 0·15
2N1701 2N1702	2-15	2N3856A 2N3858	0·16 0·16	AC127 AC128	0-20 0-20	BC168C	0.11	BF154	0.16	B6138	0-15
2N1711 2N1893	0·17 0·84	2N3858A 2N3859	0·16 0·16	AC141K AC142K	0-80 0-25	BC169B BC169C	0·18 0·13	BF158 BF159	0·15 0·27	B8¥39 B8¥51	0·15 0·25
2N2102 2N2147	0-80 0-70	2N3859A 2N3860	0·16 0·16	AC151V	. 0-14	BC170 BC171	0·11 0·18	BF160 BF161	0-23 0-35	BRY52 BBY53	0·25 0·25
2N2148 2N2192	0-60	2N3866 2N3877	0·70 0·25	AC152V AC158	0·17 0·22	BC172 BC182	0-11 0-10	BF163 BF166	0-20 0-85	BBY54 BBY56	0-80 0-79
2N2192A	0.40	2N3877A	0.26	AC153K AC154	0-25 0-20	BC182L BC183	0·10 0·09	BF167 BF173	0.18	BSY65	0.15
2N2193 2N2193A	0-40 0-48	2N3878 2N3879	1-22 1-91	AC176 AC178K	0·18 0·20	BC183L	0.09	BF177	0-19 0-25	BBY78 BBY79	0·40 0·40
2N2194 2N2194A	0·87 0·80	2N3900 2N3900A	0.80 0.81	AC187K AC188K	0-20	BC184 BC184L	0·11 0·11	BF178 BF179	0.25	BSY95A	0-45 0-09
2N2196 2N2195A	0·87 0·18	2N3901 2N3903	0.88	ACY17	0.25	BC186 BC187	0·25 0·25	BF180 BF181	0-85 0-82	BU104 BU105	1-48 2-25
2N2218A 2N2219	0.80 0.87	2N3904 2N3905	0-17 0-21	ACY18	0·15 0·20	BC204 BC205	0·11 0·10	BF182 BF183	0-80 0-40	C111 D40N3	0-58 0-68
2N2219A	0.51	2N3906	0.88	ACY20	0-20 0-18	BC206 BC207	0·11	BF184	0·17 0·17	GETIII GETIII	0.45
2N2221	0.80	2N4038 2N4037	0.68	ACY22 ACY28	0·13 0·18	BC208	0-09	BF194	0.14	GET114	0.20
2N2221A 2N2222	0-33 0-31	2N4058 2N3059	0-12	ACY30 ACY39	0-42 0-55	BC209 BC211	0·10 0·80	BF195 BF196	0·15 0·15	GET115 GET119	0-50 0-85
2N2222A 2N2368	0-41 0-11	2N4060 2N4061	0·11 0·11	ACY40	0.17	BC212K BC212L	0·10 0·12	BF197 BF198	0·15 0·15	GET120	0.25
2N2369 2N2369A	0-89 0-17	2N4062 2N4302	0·11 0·25	ACY41 ACY44	0-17 0-81	BC214L BC238	0-14 0-16	BF199 BF200	0·18 0·85	GET535 GET536	0-20
2N2648	0-41	2N4303	0-88	AD136V AD140	0.96 0.50	BC237 BC238	0.09	BF224J BF225J	0·14 0·19	GET538	0-20
2N2647 2N2711	1·20 0·12	2N4913 2N4914	0-80 0-87	AD140 AD142	0.55 0.50	BC239	0.09	BF257	0.23	GET873 GET880	0-12 0-80
2N2712 2N2713	0·12 0·17	2N4915 2N4916	0-95 0-11	AD143 AD149V	0-45 0-66	BC251 BC252	0·20 0·18	BF238 BF244	0-22 0-16	GET883	0.50
2N2714 2N2904	0·17 0·18	2N4917 2N4918	0·11 0·17 0·50	AD149V	1.26	BC253 BC257	0.23	BF245 BF246	0-88 0-48	GET887 GET890	0·20 0·22
2N2904A 2N2905	0.25 0.26	2N4919	0·58 0·60	AD150 AD161	0-63 0-87	BC258 BC259	0.09 0.09 0.18	BF247	0-49	GET895	0.25
2N2905A	0.28	2N4920 3N4921	0-50	AD162 AD161 \	0-87 PR	BC261	0-20	BF254 BF255	0·14 0·15	RETU	RN
2N2906 2N2906A	0·18 0·23	2N4922 2N4923	0-55 0-60	AD162 }	0-69 1-50	BC262 BC263	0·18 0·23	BF257	0-41	OF	
2N2907	0.18	2N4926 2N4927	0-90 1-00	ADZ12	1.75	BC300 BC501	0·42 0·84	BF258 BF259	0-46 0-48	POS	
2N2907A 2N2918	0·25 0·75	2N4928 2N4929	1.80 8.23	AF106 AF109R	0·27 0·40	BC302 BC303	0-87 0-54	BF261 BF264	0-23 1-45		٠ ١
2N2923	0.18	2N4930	2-25	AF114 AF115	0-25 0-24	BC304	0.48	BF270	0-25	SERVI	
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BN7405	0.20	0-18	BN7438	0.52	0.45	BN7475	0.45	0-24
BN7406	0-80	0.24	BN7439	0.53	0.45	BN 7476	0-44	0.8
BN7407	0.56	0-48	BN7440	0.20	0-18	BN7480	0.75	0.7
BN7408	0-20	0.18	BN7441AN	0-75	0.72	BN7481	1.25	1.0
BN7409	0-20	0-18	BN7442	0.79	0-68	BN7482	0.87	0.6
BN7410	0.20	0.18	BN7443	1.04	0.88	8N7483	1.00	0.8
BN7411	0.22	0.20	BN7444	1.04	0.88	BN7484	0.95	0.8
BN7412	0-48	0-86	BN7445	1.85	1.70	BN7485	2.50	2-3
BN7413	0-80	0.27	BN7446	2.00	1-60	BN7486	0.45	0.4
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BN7417	0.45	0-40	BN7448	1.04	0.98	BN7489	4-97	4.4
BN 7420	0.20	0-18	BN7449	Price	to be	BN7490	0.80	0.7
BN7421	0.22	0.20	annour	ced al	hortly	BN7491	1.20	1.0
BN7422	0.48	0.48	BN7450	0.20	0.18	BN7492	0.75	0.7
BN7423	0.52	0-45	BN7451	0.20	0.18	BN7493	0.75	0.7
BN7425	0-48	0.42	BN7452	0.20	0.18	BN7494	0.84	0.8
BN7426	0.82	0.28	BN7453	0.20	0.18	BN7495	0-80	0.7
8N7427	0-48	0.42	BN7454	0.20	0.18	BN7496	1.00	0.9

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25/25; 32/10; 32/40; 40/16; 60/8-4; 50/25; 50/40; 64/10; 80/18; 80/26;
100/6-4; 12-5/10; 125/16; 200/10.

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PIV	50	100	200	400	600	800	1000	1200
1A SA	8p 15p	9p 17p	10p 20p	11p	19p	15p	20p	
6A	100	-	25p	22 ip 80p	25p 32}p	27p 25p	80p	857
10A	80p	85p	409	47p	56p	66p	75p	
15 A 35 A	86p 70p	45p	48p	55p	65p	75p	87p	_
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l	IN34A	10p	AA119	7p	BAX16	1219	F8T3/4	2219
ı	IN914	7p	AA129	15p	BAY18	171p	OA5	179
ı	IN916	79	AAZ13	12p	BATSI	7p	OAlo	309
ı	IN4007	20p	AAZ15	120	BAY38	259	OA9	109
ı	IB44	7p	AAZ17	109	BY100	15p	OA47	89
ı	18113	15p	BA100	15p	BY103	22p	OA70	79
l	IB120	129	BA102	25p	BY122	471p	OA78	109
i	16121	14p	BA110	25p	BY124	150	OA79	79
ı	18130	8p	BA114	15p	BY126	15p	OA81	89
	18131	100	BA115	79	BY127	179	OA82	109
	18132	12p	BA141	17p	BY164	57p	OA90	79
	18920	7p	BA142	170	BYX10	220	OA91	79
	18922	8p	BA144	120	BYZ10	35p	OA95	79
	18923	12p	BA145	17p	BYZII	82p	OA200	79
	18940	5p	BA154	12p	BYZ12	80p	OA202	109
			BAX13	5p	BYZIS	25p	TIV307	800

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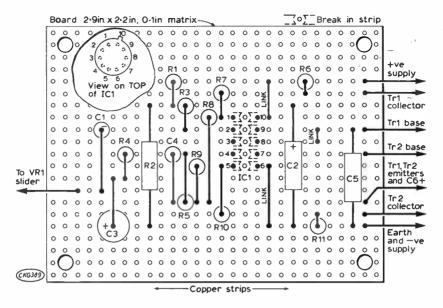


Fig. 3: Component layout on top of veroboard, the copper strips running horizontally underneath.

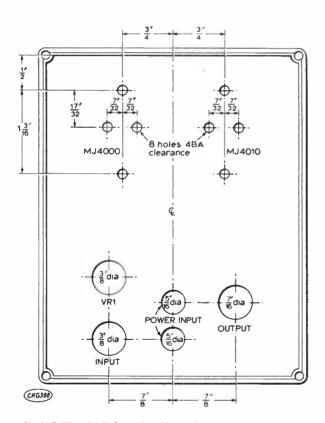
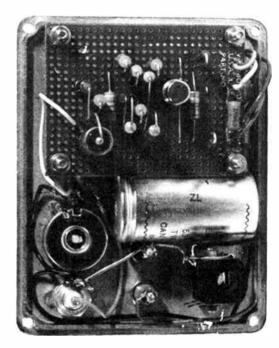


Fig. 2: Drilling details for the box lid on which components are mounted

They are based on a supply voltage (Vcc) of 35V and a loudspeaker impedance of 8Ω (R_L). Before beginning the calculations it must be remembered that there are two limitations imposed by the active devices used; the supply voltage must be in the range 10 to 40V, and the maximum current through the transistors Tr1, Tr2 must not exceed 4A. We can calculate:



This view of the completed amplifier emphasises the restrictions on the physical size of the output capacitor C6.

Peak current in transistors is:

$$\frac{V_{cc}}{2R_L} = 2 \cdot 2A \; (l_{pk})$$

If this value is above 4A we must use either a lower supply voltage or higher load impedance. To provide current limiting of this value and assuming no voltage drop across R7, R10 we calculate the values of R6 and R11 as:

$$R6 = R11 = \frac{650mV}{I_{pk}} = \frac{0.65}{2.2} = 0.296 \Omega$$

The nearest preferred value of resistor, which must be lower in value than the calculated value, is 0.27Ω . The basis of the working of the power limiting facility is difficult to explain in such a short article but works on the principle that both a high voltage across or a high current through a transistor and its network of resistors (Tr1, R6, R7 and R8) will tend to turn off the transistor. The resistor network acts to sense the power dissipation in the transistor and to limit this dissipation. The value of R7 and R10 is 56Ω . In all cases the value of R8 and

$$R8 = R9 = \frac{V_{cc}}{6mA} = 5.8k\Omega$$

The next highest preferred value, $6 \cdot 2k\Omega$, is rather difficult to obtain and the value has been increased to $6.8k\Omega$. The voltage gain of the circuit is 100 and although this may be altered by changing the value of R4, the effect of such a change on the stability of the amplifier is difficult to predict. Under d.c. conditions the capacitor C3 represents an open circuit and the d.c. gain becomes zero, the voltage at the emitters of the two transistors, determined by the ratio of the values of R1 and R2, being at half the supply voltage.

★ components list

Resistors R9 R1 4 · 7kΩ R5 10kΩ 6.8kQ R2 4 · 7kΩ R6 0 \cdot 27 Ω \pm \cdot 02 R10 56Ω R3 10kΩ R7 56Ω R11 $0.27\Omega + .02$ R8 6-8kΩ R4 100Ω VR1 5kΩ log All 1W 5% except R6 and R11 Capacitors C4 .10pF C5 2000pF C6 500µF 50V C1 1-6µF 40V C2 6-4µF 25V C3 50µF 35V Note: C6 should not be over 21" long and 1" dia. Semiconductors Tr1 MJ4000 Tr2 MJ4010 (both with mica washers and bushes) IC1 NE540L Available from SCS Components, POB 26, Wembley, Middlesex Miscellaneous Diecast box, 41 x 31 x 2". Veroboard 2.9" x 2.2", 0-1" matrix. Input socket, Output jack socket.

CONSTRUCTION

The complete circuit is constructed in a diecast aluminium box using the lid to hold all the components and the rest of the box as the cover. Fig. 2 shows the lid marked out for drilling, after which the power transistors are mounted (the NPN transistor Trl, MJ4000 on the left as seen in .Fig. 2) using mica washers with bushes. It is best at this stage to check whether the collectors of the transistors have been accidentally shorted to the box lid. The remainder of components should be fixed to the box lid, a tag washer under the input socket nut providing the main connection to the lid.

The component board is a 2.9in. x 2.2in. piece of 0.1 matrix veroboard, with the copper strips running along the 2.9in. length of the board, Fig. 3. After cutting the strips below the i.c., drilling the mounting holes and cleaning up the rough edges. a few moments should be spent with a meter checking that no lines are shorted together and that the strips below the i.c. are completely severed.

There should be no difficulty in constructing the board, but it is advisable to use different coloured wires for the flexible connections as this assists in the final wiring. The capacitor C6 is held in place by its wire leads, the positive end of the component being connected to the emitter of Trl. The circuit board is held above the transistors on four 4BA screws with either two sets of nuts and washers or lin, long spacers. The nut heads are stuck on the box lid with epoxy resin adhesive.

The final stage of wiring consists of connecting all the leads from the board to their respective terminations, wiring a negative supply earth lead to the earth end of the output socket, the negative supply socket, and the solder tag on the input socket. Lastly a wire is taken from the centre of the input socket to one side of VR1, the remaining potentiometer connection being taken to earth (the slider goes to the input on the board).

A power supply capable of delivering the maximum requirements of the amplifier must be used. In the author's case a supply of 35V at 2.5A. Under these conditions the amplifier was able to deliver nearly 15W r.m.s. into an 8Ω load.

CQ! CQ! CQ! CQ! CQ!

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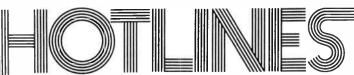
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ON RECENT DEVELOPMENTS

FOR some time now, weather satellites have been happily orbitting the earth some 800 miles up. These animals transmit a picture of the earth and a suitably equipped station below can receive these pictures. They show cloud distribution which is useful in helping to guess whether it will rain or not on the following washday.

3D RAIN?

Now comes news about a satellite built by the RCA. It is equipped with special sensors and boasts the distinction of being the very first operational satellite to provide a three-dimensional picture of the earth's weather. It is equipped with some very impressive sounding equipment; a scanning radiometer, a very high resolution radiometer and a vertical temperature profile radiometer.

The very high resolution radiometer (v.h.r.r.) has two channels and offers images from both the visible and infra-red regions. It can sense the thermal energy given off by objects below, down to half a mile in area.

Resolution is far better than the pictures provided by television cameras or the radiometers used in earlier satellites. The solar cells in the satellite, NOAA-2, generate some 500 watts and over 10,000 individual cells are used to achieve this power. Who knows—television announcers of the future may be forecasting that three dimensional rain is on the way.

LIQUID CRYSTALS

It now seems a certainty that liquid crystal displays will have a big impact on the electronics market. I reported these as being already built into a multi-digit display being marketed at the Electronica exhibition in Germany late last year. Now, the U.S. giant, North American Rockwell is reported to be mass-producing liquid crystal devices.

The liquid crystal phenomenon was first discovered way back, as long ago as 1888. The basic principle is that certain liquids become opaque when they are subjected to an electric field. With no field present, they are transparent. The North American Rockwell displays consist of two small plates of glass. Although

these are bonded together, they are separated by a tiny gap—about a thousandth of an inch. This tiny gap is filled with the special liquid which is affected by an electric field. The cell is thus completely transparent.

However, when a small electric field is applied (this takes about 25V to achieve the desired effect) the cell becomes opaque. Without a field, the molecules in the liquid are uniformly and regularly oriented. The application of the electric field causes this molecular structure to become disoriented and the molecules thus scatter the light giving an opaque effect.

The voids or spaces into which the liquid is put can be formed into figures or letters for the purposes of forming a display. Conductors to the liquid are formed from tin oxide which is a transparent conductor. The liquid crystal display draws almost no power—about 10mW or one hundredth of a watt. Perhaps we will have windows some day which will be clear until we press a button?

OZONE SPEEDS UP RESIST REMOVAL

Integrated circuits (i.c.'s) are delicate little beasts especially during their manufacture. Part of this process is a photographic one. There is a particular stage in the printing of each mask where unwanted photo-resist has to be removed. Considering the size of elements on individual i.c.s this removal is a delicate business. The General Electric Company in the U.S.A. have come up with a new method of removing unwanted photoresist. It consists of exposing the resist to ultra-violet rays in the presence of air. It takes about 40 minutes for a typical film of resist to be removed. The depolymerisation of the resist happens at a rate of about a thousand angstroms per minute. By injecting 2% ozone gas into the chamber with the specimen the process is speeded up some ten times.

Earlier, I talked of liquid crystals and many have leapt in claiming that the solid state flat tube television screen is here. One British manufacturer, however, is obviously unimpressed. Mullard has opened a

new factory in County Durham. The sole purpose is to manufacture shadow mask colour television tubes.

Although only officially opened in December last year, pilot production was already said to be running at the rate of 100,000 tubes delivered from this plant. By the end of this year, production is estimated to be in the region of 500,000 tubes and by the end of this present decade, production will be running at some 900,000 tubes/annum. All this adds up to a lot of colour television receivers—have you got yours yet?

LASERS ARE BACK

Lasers are back in the news again, this time in America where the Optical Physics Division of the National Bureau of Standards is applying one to monitor pollution. A major contributor to atmospheric pollution is nitrous oxide. It is found lurking in such jolly jollop as flue gases and in the exhaust fumes from motor vehicles.

The laser beam is directed through a magnet whose coils are driven by an audio amplifier and is detected by an infra-red device. The amplifier generates a modulating magnetic field which has the effect of sweeping the absorption line through the laser line. The detector produces a signal which has a direct relationship to the amount of nitrous oxide in the sample being investigated.

Concentrations of nitrous oxide as low as 20 parts per million (p.p.m.) can be detected but workers believe that concentrations right down to 0·1 p.p.m. will be detectable as the method is improved.

FLYING SPOT

Useful things oscilloscopes. Have you ever wondered just how fast that tiny spot of light travels across the cathode ray tube? Before you start to make calculations, think of the latest fast writing oscilloscope, the HP 184A. The writing speed for this unit is so fast that the spot travels 400cm in one millionth of a second.





IAN SINCLAIR

VER since the day when Marconi equipped the yacht Elettra with radio to act as a mobile test-bed, electronics and boats have been closely associated. The first really extensive use of radio was at sea, and after the Titanic disaster all ships were required to keep radio watch continuously for distress signals. The requirement for ships to be fitted with radio and staffed with trained operators did not, however, extend to small boats at that time, and it is only fairly recently that radio and electronic aids for pleasure craft have become more of a necessity for serious boating.

MARINE HAZARDS

Electronic devices for use at sea present some design problems which do not appear in land-based equipment. The most obvious hazard is moisture, not the fresh water moisture of a foggy day on land but the salt-laden moisture which corrodes its way through soldered joints, cable terminations, plugs and sockets, and most other metal-to-metal joints in a remarkably short time. As well as the corrosion problem, which can be completely solved only by total encapsulation, there is the problem of insulation resistance.

Salt spray is quite a good conductor and in valve equipment in particular, operating at high voltages, protection of equipment from saline elements is a problem to designer and operator alike.

It was largely the water-spray problem, as well as the cost factor, which has kept electronics out of small craft for so long. In large vessels, the radio and radar equipment could at least be mounted in an enclosed space at a reasonable height above the deck, well away from the direct spray except in the most extreme conditions. In small boats, such sprayfree havens cannot be found, and there is little chance of keeping the equipment free of water by heating coils, as were once used on bridge-mounted radio and radar.

The advent of solid state equipment has opened up a new dimension in marine applications, especially with the possibility of cutting down on interconnections by using integrated circuits. Vibration is one of the most pressing problems in small craft, where the rumble of even a small diesel engine is enough to loosen plugs from sockets or wires from soldered joints.

Some of the most up-to-date equipment used for pleasure craft can be seen at the annual Boat Show, held each year in London in January. This year you would have found amongst other more glaniorous displays, several kinds of communications equipment.

One stand-showed a "triple-standard" television receiver, complete with inverter for use with ship batteries, for use in most yachting centres in the world. But for those who insist on wind in their sails, there was a complete analogue computer, taking information on wind speed and direction, water speed, currents, intended course, and displaying the optimum trim on a model.

RADIO AIDS

Radio is still the mainstay of marine electronics, and it is hardly surprising that there should not be many advances in this direction as there are in instrumentation. The latest ranges of transmitter/receivers are geared to the most recent International regulations, which call for s.s.b. working in the marine bands between 250kHz and 4·IMHz and the use of all solid state equipment nas resulted in very compact apparatus.

A large number of v.h.f. and u.h.f. radiotelephones were also shown, and one interesting new development is the Marconi "Pocketphone" intended for communication on large vessels, such as tankers, and during docking and cargo handling operations.

The v.h.f. and u.h.f. equipment uses frequency modulation. and most make provision for the reduction of channel spacings to 25kHz, which will soon be a Post Office requirement. The bands used are within the range 148MHz to 174MHz in v.h.f. and 440MHz to 470MHz in u.h.f. Communications equipment was being shown by (among others) Marconi Marine, Electronic Laboratories (Marine), Ajax Electronics and S.P. Radio A/S of Denmark.

The latter firm was showing a receiver operating under the spray from a waterfall, whose salt content I did not sample, and also showed the "Dual-watch" facility on receivers. This enables the operator to fulfil the requirements of listening for distress signals along with normal working. The distress frequency is preset, so that the set is tuned permanently to that frequency in the watching circuits.

Working can be continued on other channels, and if a signal is received on the distress frequency (or any other being watched) the receiver output is instantly and automatically switched to the watched frequency. A lamp indicator also shows when a call is being received on the watched channel, and flashes during normal operation to show that the watch is being carried out.

DIRECTION INDICATOR

An interesting device for the small boat is the "Seafix", a hand-held radio direction indicator by Electronic Laboratories (Marine). This consisted of a t.r.f. transistor receiver with "autodyne" detection

over the range 200 to 400kHz, with the calibration most accurate at 300kHz, the centre of the Marine Beacon band.

Switched to NAV, the autodyne circuit is used to receive beacon transmissions, and the highly directional ferrite rod aerial can be used for finding the bearing of the beacon within 2° (at half rated range). Switched to BC, the "Seafix" can be used to pick up the long-wave shipping forecasts broadcast on this band. A stethoscope headset was used in preference to loudspeakers or conventional phones, and water sealing was by the conventional compressed rubber gaskets.

RADAR

Radar has for a long time been one of the most important navigational aids for larger vessels, but is seldom seen on smaller craft. There are several reasons for this: the cost of any radar installation is high, since it must include the cost of modifications to the vessel as well as the provision of the apparatus.

Radar equipment is often unavoidably large, heavy and dependent on high voltages, since the cathoderay tube and the magnetron must use high voltages, although it is now possible to replace the klystron local oscillator by Gunn diodes or other semiconductor devices.



Manufacturers are not dragging their heels over these problems, but are commendably cautious, since they know only too well how much the readings of a radar receiver come to be relied on. Any compression of size or cost must therefore not be made at the expense of accuracy of plotting if we are not to have a rash of "radar-assisted" collisions. All the big names in marine radar (Decca, E.M.I., Marconi Marine) showed small radar outfits, but these were not really intended for the amateur.

The Hepplewhite "Marine Check" is a continuous scanning self-powered instrument designed to minimise risk of collision with other vessels whose radar may not pick up small boats in bad weather or low visibility—the "Marine Check" will however, detect the other vessel's radar transmission and allow you to take avoiding action.

The scanning head is a miniature, precision, solidstate detector and amplifier of continuous, pulsed and modulated X-band radar transmission (9,000 to 11,500MHz) with electronics mounted in a shock-proof case and will receive radar transmissions at sighting distance.

As the sensitivity is reduced, the directional power of the antenna is proportionately increased to a point where the bearing is located on a narrow sector. If this bearing, which is indicated on a compass scale, remains constant, you may be on a collision course, also as the pulse length increases as the distance decreases, it is possible, within limits to determine if the transmitting vessel is approaching or receding.

The "Seascan" radar by Electronic Laboratories (Marine) is designed for the amateur, and has a power consumption of only 48W from 12V, 24V or 48V battery supplies. The only vacuum devices used are the display tube and the magnetron, the local oscillator being a Gunn diode whilst the magnetron modulator uses a thyristor. Unfortunately no circuit details were available and all the units on the stand were dummies.

One interesting new development in radar for the small craft is a passive radar detector by Hepplewhite Marine. This picks up the X-band (9,000 to 11,500MHz) transmissions from other vessels, and has a small directional aerial consisting of a Perspex "horn" on which waves are guided (along the surface) by the effect of the permittivity of the material. The received radar signals are mixed with the output of a local oscillator, and the beat note amplified. The point of strongest signal can be identified by altering the mixer bias so that only a signal of the maximum strength will produce a beat note; this enables the operator to find the bearing of the craft carrying the radar.

SPEED MEASUREMENT

Water and wind speed instruments have for a long time been a weak point in the instrumentation of boats. The traditional methods of measuring speed have depended on anemometers for wind speed and submersible "logs" for water speed. The anemometer is the device using three or four cups at the ends of radial rods pivoted so that the effect of wind is to revolve the assembly about its axis. The



The Electra Magnetic Log is an impellerless speed and distance indicator.

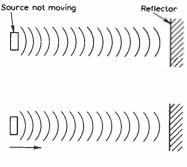
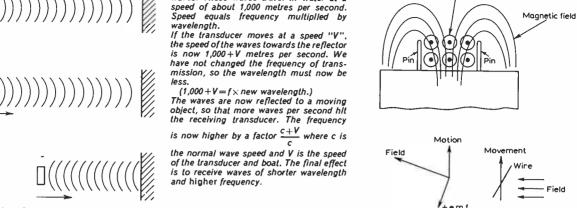


Fig. 1: The Doppler Principle. Imagine a transducer giving out sound waves. These waves travel in water at a speed of about 1,000 metres per second. Speed equals frequency multiplied by wavelength.



speed of rotation, which depends on the wind speed, is measured by counting the number of switching operations of a reed switch under the influence of a magnet on the rotating shaft. This count is converted into an analogue signal which drives a meter. Wind direction is found by using a vane coupled to a potentiometer to show the angular position by voltage detection on a meter.

The traditional submersible "log" consists of a small propeller whose shaft is held in a casing containing a reed switch. The rotation of the propeller as the "log" is towed behind then registers relative water speed just as the anemometer registers relative wind speed. The snag is that the propeller of the log is easily jammed by anything encountered in the water from jellyfish to seaweed, and this can have the effect of making calculation of speed and distance incorrect.

SPEED-LOGS

Two novel speed-logs were shown, each representing refreshingly different thinking about the problem. Space Age Electronics showed their Doppler speed log. This uses a ceramic transducer to project a 1MHz sound beam ahead of the ship. Most of the beam is dissipated in the water, but a small part is reflected from the layer of relatively still water (the boundary layer) close to the boat.

When the boat is moving, the reflected frequency is not the same as the transmitted frequency (Doppler Effect). If the boat is moving ahead, the reflected frequency is higher than the transmitted frequency; if the boat moves astern, the reflected frequency is lower.

Referring to Fig. 1, the transmitter, because of its movement, "packs in" more waves between itself and the still layer than it would if it were not moving. Because more waves are travelling, the wavelength seems shorter. Also, when the waves reflect from the boundary layer, the receiver has also moved towards them, making the frequency of the received waves seem higher.

When the reflected wave is detected, the shorter wavelength appears as a higher frequency (speed = frequency \times wavelength), whose value depends on the difference between the speed of sound in water and the speed of the boat. By beating the transmitted frequency against the reflected frequency, a measure of speed can be obtained.

The method is dependent on obtaining a reflection from relatively still water, and so the transmitting/

receiving head must be located where such a layer is within range. Precise location varies from boat to boat. To allow for variations in installation, the calibration is adjustable, so that the distance log can be checked against accurately known distances (between two land-marks, for example). The circuitry

Right-hand law

Fig. 2: An e.m.f. is produced between two

metal contacts, providing the direction of flow

is at right-angles to the line joining the contacts.

Direction of water flow into

paper shown as (•)

uses three integrated circuits, 17 transistors and eight diodes. A "log" accuracy of better than ± 112% (typical) is claimed.

The "Electra" magnetic log, produced by E.M.I. marine uses the magnetohydrodynamic principle for its operation; this is the generation of a voltage by induction when a conducting liquid flows past a magnetic field.

By arranging a magnetic field to cut the direction of water flow at right angles, an e.m.f. is induced between two metal contacts in the moving water, provided that the direction of flow is at right angles to the line joining the contacts (Fig. 2)

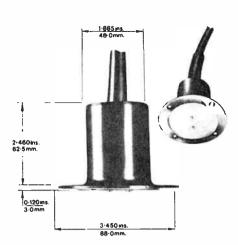
The Electra Magnetic Log operates on this principle, but with some ingenious modifications. The magnetic field used is an alternating field. In this way, the voltage generated is also alternating, which disposes of two problems at once. One problem is polarisation; when a steady voltage exists between two contacts in sea water, an electrolysis action takes place causing corrosion of the metal. The use of a.c. avoids polarisation problems and makes it easy to amplify and display the output from the contacts. As with the previous method, the positioning of the measuring head is critical.

ECHOSOUNDERS

Echosounders have been used for a considerable time, and changes have been in detail rather than in concept. Basically, a marine echosounder consists of a pulse generator working at ultrasonic frequencies in the region 20kHz to 150kHz (the higher frequencies are used for inshore work). A transducer converts the electrical pulses into sound waves directed from the bottom of the boat into the sea, and a receiver, using the same transducer, detects the pulse reflected from the bottom of the sea.

The shape of the received pulse provides a guide to the nature of the sea bed, for example, a muddy





The electro-magnetic transducer for the magnetic log. As the boat moves along, a small e.m.f. is produced and sensed by two probes. This signal is then amplified and displayed in speed and distance units.



The Doppler speed-log does not rely on the flow of water to move a mechanical part like an impeller or paddle wheel. A small streamlined transducer, mounted flush with the underside of the hull, transmits a high frequency ultrasonic signal 70cms ahead. A small part of this signal is reflected back from the boundary layer between the hull and the water.

sea bed is indicated by a broad pulse, a sandy bed by a narrow pulse, a rocky bed gives multiple reflections. Pulses received from intermediate depths can indicate shoals of fish. The time delay between transmission and reception is proportional to the depth of sea.

Because the pulses are travelling in the water at the speed of sound (around 1,000 metres per second) rather than at the speed of radar waves in space (some 30 million metres per second), scanning rates have to be lower than the 1,000Hz commonly used in radar. Scanning rates of once per second are common, although this is rather too low for display on a long persistence cathode ray tube screen.

The display method traditionally used is a rotating wheel carrying, or illuminated by, a neon which flashes on transmission of the pulse and again when the echo is received. The stationary bezel round the wheel is then calibrated in metres of depth (now replacing fathoms on the latest charts).

The large number of echo sounders at the show demonstrated several novel points of design. Most interesting was the use of electro-luminescent diodes to replace neons, so avoiding the need to generate a high voltage supply (Brookes & Gatehouse). A common feature of all the echo sounders was the use of high scan rates for the shallow water ranges (up to six pulses per second) so giving better definition in critical conditions.

Lead zirconate titanate crystals were in evidence as transducers, encapsulated in various plastics. For professional use, chart recording echosounders were shown (these, of course, have been around for a long time). The Marconi Marine chart-maker used electrosensitive paper which changed colour when a small voltage was applied between the front of

the paper and the back.

WATER-LEAK AND WATCH

In addition to the displays of electronics for communication and navigation, there were some interesting exhibits in the "miscellaneous" class. Space-Age Electronics were showing their water-leak and watch alarm, and judging by the sound which could be heard all over the first floor of Earls Court, almost every chandlery firm was demonstrating it.

The instrument is basically a conventional leakage detector using stainless steel pins as probes. If the pins are immersed in water for more than four seconds, an alarm is given, but only if the immersion is for longer than four seconds, a time carefully chosen to avoid continual false alarms in heavy seas. When there is no conductivity between the pins, all transistors are biased off, so ensuring practically no standby current. The sound given out is a rising frequency note which is most easily distinguished amongst other sounds.

The watch facility also provided on this instrument gives an alarm note of gradually increasing amplitude every three minutes. If an alarm button is pressed during the alarm, or before it, the instrument remains silent until another three minutes has passed. If the helmsman is asleep and does not press the alarm button, the alarm warning increases to maximum intensity.

GAS ALARM

The Electra gas alarm, from E.M.I. Marine, is of considerable interest. Unlike previous gas alarms, which used heat conduction from a hot wire to detect changes in the air composition, the Electra gas alarm uses semiconductor sensors. No details were given, but it is possible that the sensors consisted of infra-red electroluminescent diodes and detectors. Any change in the air composition caused by petrol vapour, butane or propane gas, carbon monoxide, smoke, paraffin fumes, diesel fumes is indicated by two visual warnings in the form of a meter reading and a red warning lamp.

In addition, a loudspeaker gives out a 2.5kHz note when the gas concentration exceeds the safe limit. In this way, no panic is caused by small concentrations of gases, since only the discreet visual warning is given, but dangerous amounts operate the audible alarm so that evacuation or other measures can be taken. Remote warnings can also be fitted.

All in all, the Boat Show is developing considerable interest from the point of view of electronic aids. It is unfortunate that so few exhibitors were able to cope with technical queries, but all of them were most helpful.

practically wireless

commentary by HENRY

No. 98
First in the Field

HAD a chap in the shop today, searching for an SP4. It is true: even in the glitter of a hi-fi establishment, where every prospect teases and only valves are vile, we still get enthusiasts with thirty-year-old equipment, hopeful of our being able to provide the missing link.

Which leads us, philosophically, to a contemplation of some of the 'firsts' we nowadays take for

granted.

Example: the quasi-complementary transistor amplifier circuit, which has given us so much trouble since its inception. I have come across the September 1956 copy of *Electronics*, a McGraw-Hill publication, in which R. C. Lin, then of RCA, Princeton, first propounded his output circuit in which, to quote: '... the two upper transistors conduct during the negative half-cycle and the two lower transistors conduct during the positive half-cycle.'

In his summary, he gave amplifier distortion at 100cps (sic) and 400cps as below 1 per cent at six watts, and though he admitted that the distortion might be expected to rise at 5,000cps, he made no mention whatsoever of its fierce spikiness at a fraction of a watt, which is the mariner we've had wrapped around our necks ever since.



The mariner wrapped around our necks.

Inventions, especially worldshaking innovations such as the transistor proved to be, have a habit of spawning themselves much more prosaically than we would like to imagine. No technologist runs screaming through the corridors of the M.I.T. with 'Eureka' echoing behind him. More likely, something as laconic as the 12/29/39: 4.15 p.m. entry in William Shockley's notebook may be handed down to posterity: 'It has today occurred to me that an amplifier using semiconductors rather than vacuum tubes is in principle possible.'

In principle: hardly in practice. He was thinking of a Schottky-barrier FET kind of device, with copper-oxide as the semiconductor. And, as Henry could have told him*, it didn't work. Instead, the experiments of the team included covering metal points with wax and pushing them down on to p-type silicon treated to give an n-type surface. They surrounded the point with water and found they could obtain power amplification.

To quote Brattain: '. . . the group was jubilant that day.'

Trouble was that the water would evaporate. Maybe it was all that heavy breathing. So they switched to glycol borate to reduce evaporation. One trouble: amplification was obtainable only below 8Hz—hardly hi-fi yet.

There were lots more experiments, culminating in evaporated gold spots and germanium, and then, on Dec. 23rd 1947, two gold contacts less than two-thousandths of an inch apart were made to the same piece of germanium and the first transistor happened.

No sudden breakthrough—no inspirational brainchild—and no immediate christening, I may add. It was a month later that a chap called John R. Pierce of the Bell technical staff mooched into Brattain's office and pointed out that the 20dB point-contact amplifier they had made was the



Runs screaming through the corridors.

'. . . dual of a vacuum-tube, circuit-wise.' He mentioned the important valve parameter, transconductance. Then he went on to talk about its electrical dual, transresistance. To quote Brattain once more: '. . . then he said 'transistor', and I said, 'Pierce, that is it!!'

What about a few more firsts in our field? Who developed the first p-n junction? Bet you can't even say his name, let alone remember it. Well Henry can, with the benefit of some help from Edward A. Torrero, who is Associate Editor of Electronic Design. He was William Pfann (with the aid of a chap called Jack Schaff; let's give credit where it is due). They also worked for Bell Laboratories.

But Bell eschewed silicon for germanium, because the impurities, back in the early 1940's, were easier to control. It was left to Texas Instruments to develop silicon types of transistor, and to Motorola to introduce the diffused base transistor.

So I could continue. Henry hasn't the space to name those to blame.

But the "first" we are all concerned with is that original alltransistor radio. And who made that? A firm called Regency, in 1954. How's that for a significant 'first'?

* With the benefit of hindsight. Ed.

EXTRA!!! INNEXTMONTH'S

PRACTICAL WIRELESS

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P.W's reputation for plenty of simple and straightforward constructional projects is excelled next month by an extra large issue. In addition to the usual constructional articles and features, the May issue will include a special extra 8-page coloured supplement describing eight easy projects for the home, designed and described by one of our top designers; you are bound to find at least one of these of interest. This supplement is fully illustrated with all the details on how to build these projects.





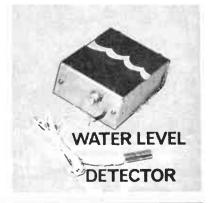












MANY OTHER CONSTRUCTIONAL ARTICLES PLUS ALL THE REGULAR FEATURES. PRICE 20p.

ALL IN THE MAY ISSUE ON SALE 6th APRIL

Following the success of the Texan amplifier published in this magazine during May to August 1972, the applications laboratory of Texas Instruments Ltd. have developed exclusively for P.W., a compatible unit for the control of Psychedelic lights from a sound source. The initial design features zero voltage control. A more sophisticated design incorporating lamp dimming facilities will also be covered in this series of articles. For stereo operation two P.W. Tricolour units are required.

F I had been asked, a couple of years ago, what 'psychedelic lights' were, I could only have made a wild guess: was it perhaps a medical term referring to some sort of ultra-violet treatment for disorders of the mind? Or, possibly, the latest in pet food, some extra tantalising form of offal? The truth, however, dawned slowly. What my "trendy" young friends were talking about was the latest innovation, the offspring of a marriage between light and music. It was not simply a question of a 'pop' version of 'son et lumière' but a more intimate relationship between the two media. Light could be made to respond directly to sound; flashing furnously for a faufare, discreetly dimmed for Debussy. It is, however, unlikely that psychedelic lights will be installed in the Royal Festival Hall, but those of our readers who occasionally frequent the discotheque or dance hall will be familiar with this innovation. It is probable, too, that many have given thought to the incorporation of this feature into their own domestic lighting, systems. What, it might be asked, does this involve?

In essence a 'psychedelic' light system works like this: sound controlled modulators convert bass, middle and treble frequencies into corresponding bursts of light thus adding a new "visual" dimension to the beat of the music. This is achieved by taking a signal from across the loudspeaker terminals and feeding it into a filter circuit whose output provides pulses which correspond to the sound spectrum—bass, middle and treble and any combinations of these three channels. These pulses then pass through an interface circuit and energise appropriate triacs. The latter, as will be seen, act as electronic switches and turn on the lamps.

This article will attempt to explain fully the construction of psychedelic light control units for both mono and stereo equipment. It is aimed at the home constructor who possesses nothing more than an average amount of skill.

Zero Voltage Switching

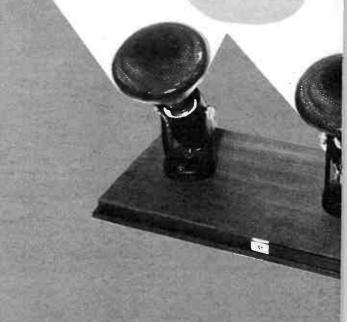
As stated, the lights are turned on and off by utilising a device called a triac, i.e. a semiconductor bidirectional switch (Fig. 1). This replaces two thyristors connected back to back, thus controlling the positive and negative cycle of the supply voltage. Whereas the thyristor requires a positive gate to cathode voltage and will turn on only when the anode voltage is positive with respect to the cathode, triacs will turn on when the gate voltage polarity is the same as voltage between mt2 and mt1 (main terminal 2 and 1), i.e. positive for the positive half cycle and negative for the negative half cycle. In addition a triac will turn on with the gate negative with respect



LAMP OVER-RIDE CONTROL

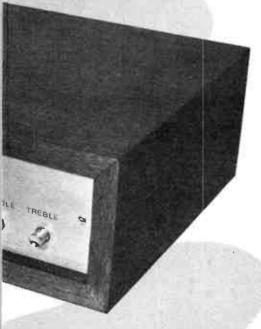
OPT(ONAL LAMP DIMMING

PART ONE



* TEXAS INSTRUMENTS LIMITED.

COLOUR



Lighting System

JUREK BUDEK*



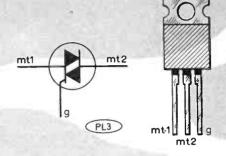


Fig. 1: The TIC226D bidirectional switch

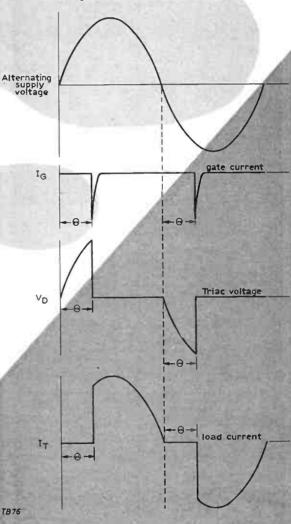


Fig. 2: Waveforms associated with triac switching. Refer to the text for clarification

to the mtl terminal for either polarity of mt2. It is the latter factor which accounts for the techniques used in the circuits to be discussed in this article.

A further point about the triac is that there is only 2-3 volts between the gate and terminal 1, whereas there may be many hundreds or even a thousand volts between terminal mt2 and mt1.

Triacs used in a phase control mode, as shown in Fig. 2, produce considerable radio frequency inter-

ference (r.f.i.) due to the step change in current. The noise thus generated is spread by means of conduction through the wiring system or by radiation. Suppressing r.f.i. becomes more difficult and expensive as the load increases. Uncontrolled switching of "psychedelic" lamps on and off will have a similar effect and will also introduce additional noise in the loudspeakers. A simple solution to this problem is to arrange the switching so that it always takes place at the point where the mains supply voltage crosses zero, as shown in Fig. 3.

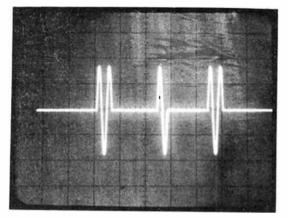


Fig. 3: Waveform depicting zero voltage switching.

This technique is called 'zero voltage switching' or 'burst firing.' In this way isolated numbers of half or full cycles will pass through the lamps and thus avoid step change in currents, which also has the additional advantage of increasing the life of the lamp.

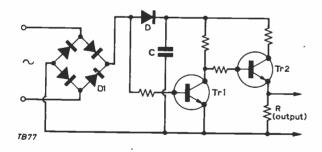


Fig. 4: Basic circuit which generates the pulses at the point of zero voltage crossing.

Fig. 4 shows the circuit used to generate the pulses at the point of zero voltage crossing. Transistor Tr1, whose base is connected to the unsmoothed supply from the bridge rectifier D1 is on most of the time.

However, each time the mains voltage crosses zero, its base voltage is taken below the holding on voltage and it thus turns off, giving positive pulses on its collector. In order to reduce the loading on transistor Tr1, transistor Tr2 has been added. Positive pulses appear as an output across resistor R each time the mains voltage crosses the zero point.

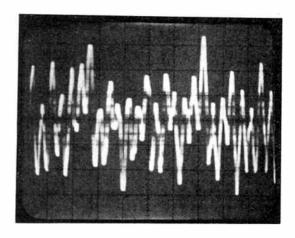


Fig. 5: Typical music voltage waveform at the terminals of a loudspeaker.

In order to control the lamp switching with respect to the frequency bands, we need a circuit which will separate out the low, middle and high frequencies from the voltage waveform appearing at the terminals of a loudspeaker. A typical voltage waveform appearing at this point is shown in Fig. 5.

Filter

A circuit which separates frequencies into bands is called a filter. There are various types of filters which could be employed; e.g. one commonly used is a resistor/capacitor (r.c.) network for high and low pass filters and an inductor/capacitor (l.c.) network for middle frequencies. The elegant way, however, specially developed for the P.W. Tricolour is to employ integrated circuit (i.c.) operational amplifiers, in a positive fixed-gain configuration, as the active filter element and resistors and capacitors as passive elements. By choosing suitable component values a sharp separation between bass, middle and treble frequencies can be obtained.

The shape of the filter response is determined by a factor known as the damping ratio (ζ). The lower this ratio, the sharper the cut-off and there is a peaking effect. This peaking effect is of no importance in our application. As approximately 1.5 volts is required to turn on the interface circuit, and thus to switch on the appropriate lamps, the filter characteristics are expressed in volts against frequency and not in the more usual decibels against frequency.

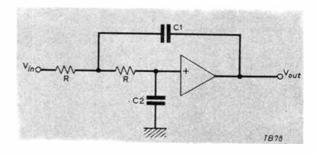


Fig. 6: Basic low pass filter as used in the P.W. Tricolour.

The theory of filter design is quite extensive and complex. We will however only outline the necessary basic concepts and give some simplified formulae.

Let us first look at a basic low pass filter (i.e. one which will stop all frequencies except those below a chosen frequency). The circuit of such a filter is shown in Fig. 6.

Here the angular cut off frequency.
$$\omega o = \frac{1}{R\sqrt{C1 C2}}$$
 and the damping factor
$$\zeta = \sqrt{\frac{C2}{C1}}$$

$$\zeta = \frac{1}{\sqrt{2}}$$

and, for the reason explained before, i.e. to improve the sharpness, this value is reduced to 0.5. From these equations, the filter component values can be established.

The high pass filter (passing all frequencies above a chosen one) is shown in Fig. 7 and again requires only one operational amplifier, two resistors and two capacitors.

Here the angular cut-off frequency,
$$\omega_0 = \frac{1}{C\sqrt{RTR}}$$

$$\zeta = \sqrt{\frac{R1}{R2}}$$

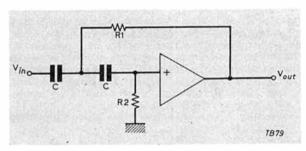


Fig. 7. Basic high pass filter.

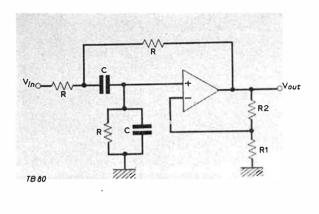


Fig. 8: Basic band pass filter.

Once more from these equations, the filter components values can be established. Finally, the band pass filter; which, of course, as its name suggests, passes a band of frequencies. This, as can be seen from Fig. 8, is a little more complicated than the other two.

The centre angular frequency
$$\omega o = \frac{\sqrt{2}}{RC}$$

and the quality factor
$$Q = \frac{\sqrt{2}}{4 - \frac{R2}{R1}}$$

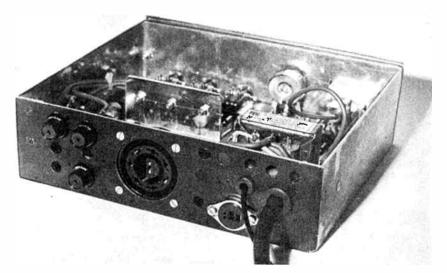
$$Q = \frac{2\Delta f}{fo}, \text{ where } 2\Delta f \text{ is the difference between}$$
 two frequencies at which the voltage output of the

filter is $\frac{1}{\sqrt{2}}$ of its maximum value. From the above

formulae, relevant component values can be obtained.

Musically oriented readers will recall the

Musically oriented readers will recall the 'unisono' note played on the oboe during the orchestra's tuning-up time, just before the concert begins. This note is middle 'A' with a frequency of 440Hz; a frequency which has been chosen as the centre frequency for the middle band-pass filter in



Rear view of the P.W. Tricolour.

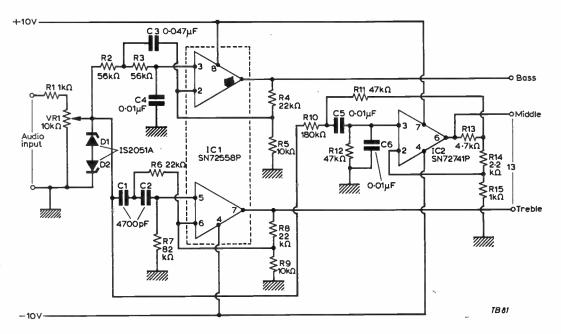


Fig. 9: Complete P.W. Tricolour filter circuit. This unit is used without modification, with either the zero voltage switching unit (Fig. 12) or with the lamp dimming unit, to be described later in this series.

this design. Cut-off frequency for the low pass filter has been chosen to be around 200Hz and that of the high pass filter (treble) about 1kHz.

Based on the above assumptions, a complete filter has been developed with the component values as shown in Fig. 9. The alert reader will notice that some of the component values differ from the figures obtained using the formulae. This has been done intentionally in order to improve the separation between the various frequency ranges.

The input to the filter circuit has been limited to 5 volts peak to peak by using two 5 volt zener diodes connected back to back. Three i.c. operational amplifiers are used. Two of which are contained in one 8 pin package, SN72558P and the other i.c. is contained in a second 8 pin package, SN72741P.

Fig. 10 shows output voltage response of the three filters plotted against frequency for a peak input signal of 0.5 volts. The effectiveness of the filters are obvious. The solid state switches—triacs—turn on their corresponding lamps at filter output voltages equal to and higher than 1.5 volts.

Figs. 11a to 11d show four oscilloscope photographs. These show traces with the vertical axes representing voltages and the horizontal one time. In each instance the four traces were taken simultaneously (i.e. they have a common time axes). In the oscillograms the top trace corresponds to the voltage at the loudspeaker terminal. The other three traces were taken at the outputs of the respective filters.

Fig. 11a was taken at a time when the treble

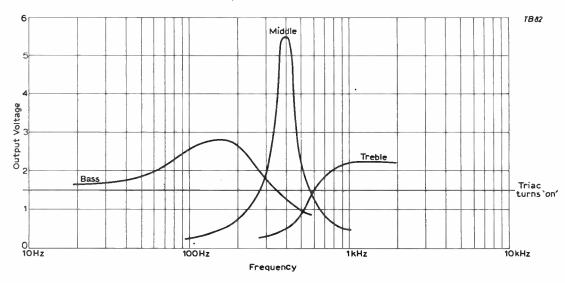


Fig. 10: Output voltage/frequency response of the filter circuit shown in Fig. 9.

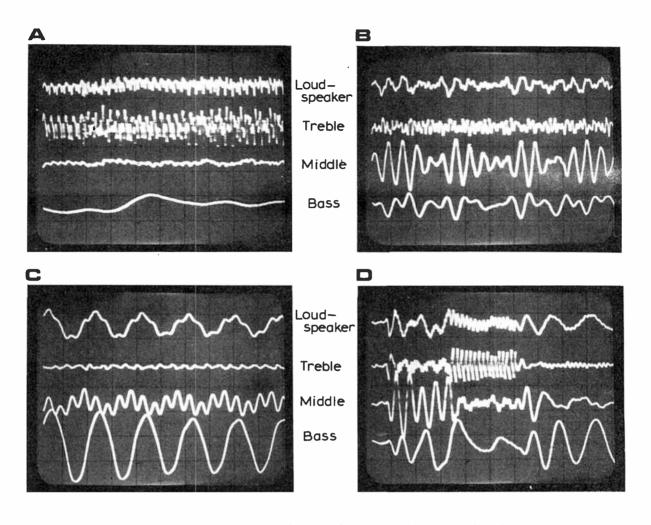


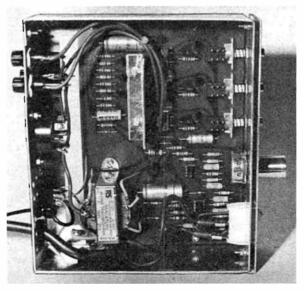
Fig. 11: (a-d) A full explanation of these waveforms is given in the accompanying text.

frequency was predominant. In Fig. 11b the middle frequency is the strongest signal, while in Fig. 11c it is the bass. Fig. 11d shows some interesting combinations of all three frequencies. The middle frequencies predominate at the beginning of the trace, then the treble takes over at the centre of oscillogram and towards the end of the trace it is the turn of the bass to predominate.

A $10k\Omega$ potentiometer has been added at the input to the filter circuit to allow the voltage level at which the lamps are switched to be controlled. In this way it is possible to establish the best effect for 'soft' or 'party' type music.

The $P.W.\ Tricolour$ is suitable for use with 4 to 15Ω loudspeakers. The load represented by the filters is negligible compared to the loudspeaker impedance.

It should be noted that the simple filter circuits illustrated at the beginning of this article used operational amplifiers. An operational amplifier has high input impedance, very high gain, and low output impedance, enabling the filter component values to be determined independent of the amplifier parameters. The amplifiers used were shown having a voltage gain of unity. This means that the output voltage of the high and low pass filters can never



Underside view of the P.W. Tricolour with zero voltage switching.

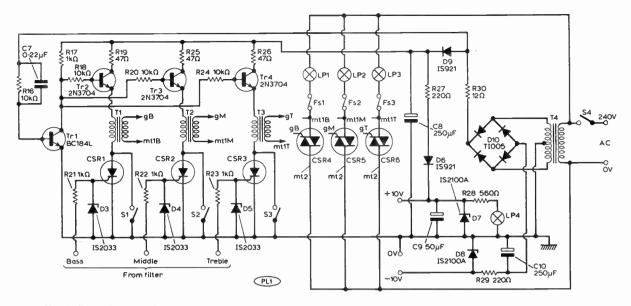


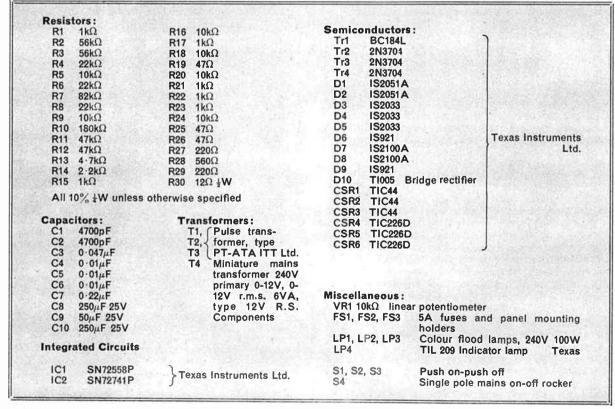
Fig. 12: Zero voltage switching control unit. The positive and negative 10V supply lines are the d.c. supplies to the filter unit (Fig. 9).

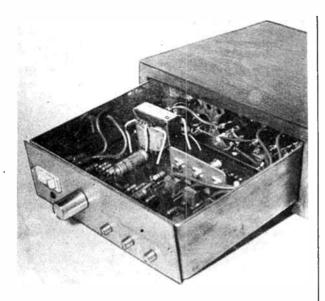
be more than the input voltage. In order to achieve voltage gain so that sufficient output can be obtained to drive the interface circuit at low volume levels, the basic circuit must be modified. This involves reducing the proportion of output voltage from the amplifier that is used as feedback to the filter capacitors and resistors. This is achieved by the use of a resistive potential divider at the output of the

amplifier. This is shown in Fig. 9. The resistor ratio determines the gain of the filter in the pass-band.

The *P.W. Tricolour* is suitable for either mono or stereo record playing. In the case of the stereo system, the lights will flash in accordance with the signals appearing at the terminals of one of the speakers. However, for stereo enthusiasts who wish to use two units, the interconnecting arrangement will

★ components list





Internal view of the P.W. Tricolour.

be explained later.

Fig. 12 shows the circuit which operates the flashing lights according to the frequency ranges.

Switch S4 controls the mains supply to the unit from a 13A domestic socket. When the a.c. mains power is on the gallium arsenide device LP4 lights. A smoothed d.c. supply for transistors Tr1-Tr4 is obtained from a single phase bridge D10, resistor R30, diode D9 and capacitor C8. The $\pm 10V$ power supply for the filter circuit is taken from zener diodes D7, D8 and capacitors C9 and C10.

As described previously, the zero voltage crossing pulses are generated at the collector terminal of transistor Tr1. These pulses turn on transistors Tr2, Tr3 and Tr4 via base resistors R18, R20 and R24. When a voltage signal from the filter circuit appears at the input terminals, the corresponding thyristors CSR1, CSR2 or CSR3 will turn on allowing pulses to be present at the respective gate of CSR4, CSR5 or CSR6 which turn them and thus their lamps on. Pulse transformers T1, T2 and T3 are used only for electrical isolation.

Zener diodes D3, D4 and D5 limit the thyristors gate voltages to 3.3V in the positive direction and to under 1 volt during the negative half cycles.

Facilities are provided for 'by-passing' the psychedelic control by closing switches S1, S2 or S3 to allow the lamps to be used as normal lights. The centre tap of the 12-0-12V mains transformer is connected to the chassis and is earthed. Note that the three triacs are mounted on a common heat-sink, which is at the supply line voltage, i.e. 240V.

The author has made arrangements for the supply of all components for the *P.W. Tricolour* with Henry's Radio Ltd. We understand that a detailed price list will be available from them upon receipt of a stamped addressed envelope.

TO BE CONTINUED

edium ave Column

KING (Edinburgh) asks for the times and frequencies of English speaking foreign stations on the medium waves. Among the stronger there are Radio Sweden which is on 1178kHz every night at 2245hrs; Radio Portugal on 755kHz and 1161kHz, also at 2345hrs and the Vatican Radio on 1529kHz at 2100hrs. There are also the American Forces Network (AFN) outlets on 872kHz, 935kHz and 1142kHz. Try for CJON St John's, Newfoundland on 930kHz—it can be found on the low frequency side of AFN on 935kHz after 2330hrs. CJON has been a strong and consistent signal all winter and it has even been heard when conditions have been poor and no other North American could be heard.

Harold Emblem (Mirfield, Yorkshire) has received a QSL card (verification) from Radio Zagreb Yugoslavia which transmits on 1133kHz. The address is Radio Televizija Zagreb, PO Box 818, Zagreb Yugoslavia and reports in English are answered. Harold mentions hearing PJA6 Radio Victoria on 925kHz, which is located in the Netherlands Antilles in the Caribbean. It broadcasts religious programmes in English and other languages and is usually heard in this country after midnight.

Harry Kenyon (Leeds) has been looking for a published list of medium wave stations. "Broadcasting Stations of the World" published by Iliffe is available in many bookshops price 50p. It covers medium wave stations in Europe and North Africa plus a number of more powerful outlets in other parts of the world, that are usually heard in Europe. There is also a comprehensive list of short wave stations.

Karl Ritz (Bicester) sends a programme schedule of BBC Radio Oxford which is now on 1484kHz. Frequencies in use by BBC local radio are 850kHz R. Blackburn, 998kHz R. Solent, 1034kHz R. Medway, R. Sheffield; 1106kHz R. Leeds; 1457kHz R. London, R. Birmingham, R. Newcastle, R. Manchester; 1484kHz R. Brighton, R. Humberside, R. Merseyside, R. Oxford; 1502kHz R. Stoke; 1546kHz R. Bristol, R. Teeside; 1594kHz R. Leicester.

Kenneth Turner (Edinburgh) has logged R. Birmingham, R. Stoke and R. Bristol and he reports hearing Manx Radio (Britain's only commercial radio) on 1295kHz and 1594kHz.

G. H. Esmail (Bradford) enquires about a suitable receiver for use on the MWs. Serious DXers prefer a communications receiver such as the Trio 9R59DS or the Lafayette HA600 but an ordinary transistor portable will pull-in Europeans and North Africans and if the receiver is rotated to make use of its internal directional aerial, it will be possible to reduce quite a lot of interference.

Please send logs and information about the medium waves to the author at 132 Segars Lane, Southport PR8 3JG.

MW LOOP

S.A.MONEY G3FZX

URING the next two years the minimum of the current sunspot cycle should occur. Although short wave reception usually suffers at the period of the sunspot minimum the conditions will become very favourable for the reception of DX signals on the medium wave broadcast band. Unfortunately, the interference from European stations, many of which now remain on the air all night, is likely to be much worse than it was during the last sunspot minimum. In order to winkle out the weaker DX signals from the QRM it will be important to choose an effective aerial system as well as a good receiver.

In the late 1950's the writer, in collaboration with Reg Dunkley of Havant, Hampshire, carried out a series of tests to investigate the possibility of using a tuned loop aerial for the reception of DX signals on the medium wave band. These tests showed that although the loop aerial is somewhat less sensitive than the usual outdoor wire type aerial it has several advantages which make it attractive for DX work.

Pick-up of background noise and static seems to be rather less on the loop aerial than it is on a wire aerial so that although giving less signal the loop does usually give a better signal to noise ratio.

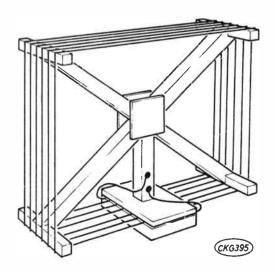


Fig. 1: Configuration of a typical m.w. loop aerial.

By rotating the loop aerial its directional properties can be used very effectively to cut down adjacent channel interference from strong European signals. A further advantage of the loop aerial is that it is very compact and hence attractive to the listener who is unable to use a large outdoor aerial system.

The advantages of the loop aerial have, in the past ten years, made it very popular among the medium wave DX enthusiasts in Britain.

Although the basic loop aerial as used by most of these DX'ers is quite effective it is not the optimum arrangement.

In the past year the writer has experimented with methods of improving the performance of this type of aerial. In this article a system is described consisting of a loop aerial and a matching amplifier capable of giving a performance superior to that of the basic loop aerial.

HOW THE LOOP WORKS

Before going on to describe the improved aerial system it would be as well to consider the make up of the basic loop aerial and the way in which it works. This type of aerial used to be a standard fitting in portable radios before the arrival of the ferrite rod aerial.

The loop aerial usually consists of a number of turns of wire wound in the form of a short coil on a large wooden frame. Typical aerials are square in shape as shown in Fig. 1 although circular or diamond shaped loops will also work. The length of the sides may be from 12in. up to about 4ft. In general, the larger size aerials give greater signal output and rather better directional properties.

Normally the turns of the winding are spaced apart from one another to reduce self capacitance. The whole aerial is then tuned to resonance by a variable capacitor connected across the ends of the loop.

CKG396 From transmitter Vo From transmitter Valags V, by d Phase V0 = V2 sin φ (CKG397) (a) (CKG198) (6)

Fig. 2: (top) Voltages induced in a single turn loop. Fig. 3: (centre) indicates how the output of the loop depends on its position relative to the signal source. Fig. 4: (bottom) illustrates the modified pick-up pattern of a loop due to "antenna" effect.

To see how the loop works let us assume that there is only one turn as shown in Fig. 2. When radio waves pass through the loop a voltage will be induced in each of the vertical sides. These voltages are shown as V1 and V2. The relative polarity of the two voltages is indicated by the arrows. It will be seen that the voltage at the terminals of the loop will be made up of V1 and V2 connected in series. When the two voltages are connected in this way they will be effectively in opposition to one another so that the resultant output voltage at the loop terminals will be the difference between V1 and V2. In practice the two voltages are alternating and therefore the difference voltage will depend not only upon amplitude but also upon the phase of VI relative to V2

Suppose the loop is set up so that it is broadside on to the direction from which the received signal is coming. This is shown in Fig. 3(a) which shows a view looking down on to the aerial. Both vertical sides of the loop will be at exactly the same distance from the transmitter aerial so the induced signal voltages V1 and V2 will be of the same amplitude and in phase with one another. At the output terminals the difference voltage produced will be zero since V1 and V2 will cancel out exactly. This is known as the 'null' position for the loop since there will be no signal output.

Now let us see what happens when the loop is turned so that it is in line with the direction of the signal being received as shown in Fig. 3(b). In this case one side of the loop is closer to the transmitter than the other. Since the width of the loop is very small compared with the distance to the transmitter the amplitudes of the induced voltages V1 and V2 will still be virtually equal. The radio wave will, however, take a finite time to travel from the near side of the loop to the far side so that V2 will lag behind in phase relative to V1. This phase shift of V2 will produce a difference signal output at the loop terminals. In fact at this position the loop will give its maximum output signal.

The resultant pick up pattern for a loop aerial will be as shown in Fig. 4(a). If extra turns are now added to the loop so that it forms a short coil the voltages produced by each of the turns will add together at the output terminals. As a result the output from the aerial will be proportional to the number of turns used. For a multi-turn aerial the pick up pattern will be the same as for a single turn. A further increase in output can be obtained if the aerial is tuned to resonance by connecting a variable capacitor across the ends of the loop winding.

"ANTENNA" EFFECT

One of the difficulties which occurs when using a loop aerial is known as the "antenna" or "vertical" effect. Unless the aerial is exactly balanced electrostatically with respect to earth it will act as a normal vertical aerial. A simple vertical aerial picks up the signal at equal strength from all directions in the horizontal plane. Now we get the condition that when the aerial is broadside on to the direction of the signal the voltages V1 and V2 cancel as before but the output due to "antenna" effect remains constant. This results in a pick-up pattern like that in Fig. 4(b) where the nulls are less marked and much broader than for a perfect loop.

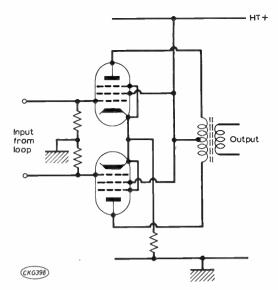


Fig. 5: Basic circuit of an early valve-type balanced input stage.

Perhaps the most obvious method of coupling the loop to the receiver would be to connect it directly across the aerial input terminals of the receiver. This method is rarely successful since the aerial will be unbalanced to earth and "antenna" effect is usually very bad.

For the basic loop aerial used by m.w. DX'ers the usual method of coupling is by means of a link winding. The link usually consists of one turn, or sometimes two, wound on the frame alongside the main winding. This link winding is then connected directly to the receiver input. With a link coupling of this type the aerial usually works quite well except that the link winding itself tends to produce some output due to "antenna" effect.

DIFFERENTIAL MATCHING AMPLIFIER

Wartime d.f. receivers, such as the R1155, made use of a differential or push-pull amplifier at the input. This type of amplifier uses two valves with

* components list

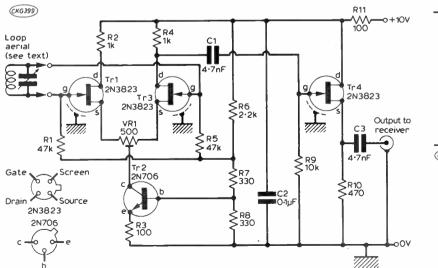
R1	tors 47kΩ	R5	47k	0	R9	10kΩ
100 17 57 188		ALCOHOL:	115,00	T-210000	-01/1/2	470Ω
R2	1kΩ	2/5/2/01/2	2.2	Mar fragilla	R10	
R3	100Ω		330		R11	
R4	1kΩ	R8	330	Ω	VR1	500Ω preset
			All	₩ 5	5%	
	citors					
	4.7nF po	lyeste		C3	4-7nF	polyester
C1			,	СЗ	4-7nF	polyester
C1 C2	4.7nF po	n. foil		C3	4-7nF	polyester
C1 C2	4·7nF po 0·1μF mi conducte	n. foil	r r3	C3		polyester

their cathodes connected together as shown in Fig. 5. The resistor in the cathode circuit is made large enough so that it acts as a constant-current source. This type of amplifier responds only to differences in voltages between the two grids and will reject any signal common to both grids such as that produced by "antenna" effect in the loop aerial.

A balanced input amplifier using transistors instead of valves is shown in Fig. 6. In order to maintain a high value of Q in the aerial circuit a pair of field effect transistors is used for the differential input stage. This type of transistor has similar characteristics to a valve and gives a much higher input impedance than a normal bipolar type transistor. In this circuit 2N3823 'N' channel field effect transistors are used.

A differential amplifier works most effectively when the common-tail circuit of the input pair is fed from a constant-current source. In the valve version this is achieved by feeding the common cathode point through a large resistor from a negative supply voltage. In the circuit of Fig. 6 the transistor Tr2 is used to provide a constant current feed.

Characteristics of the 2N3823 may vary widely from one transistor to another. For optimum results the two transistors Trl and Tr3 in the input stage should either be matched or at least have similar characteristics. This can be checked by using the



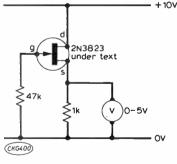


Fig. 6: (left) Complete circuit of the loop matching amplifier. Note that the 2N3823 transistor specified is preferable to the unscreened 2N3823E. Fig. 7: (above) is the circuit of the simple test set-up for checking the characteristics of the f.e.t.'s.

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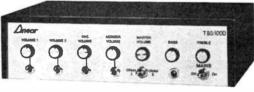
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Fig. 8: Full size illustration of the printed circuit board, from the copper side. Small holes are drilled for component leads and the components mounted from the other side of the hoard.

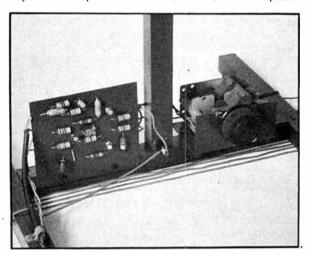
circuit of Fig. 7 to select two 2N3823 transistors giving a similar voltage drop across the $1k\Omega$ resistor in the test circuit. The balanced amplifier itself will tend to level out small differences between the transistors.

Transistor Tr4 acts as a source follower and is used to match the output from Tr3 into the low impedance of the cable and the receiver input circuit. Capacitive coupling is used to the output so that if the cable is accidentally short circuited the transistor Tr4 in the output stage will not be destroyed.

CONSTRUCTION

(CKG401)

It is convenient to build the amplifier on a small circuit board and to mount it close to the tuning capacitor on the main loop frame. A suggested layout for a printed circuit board for the amplifier



Close-up of the matching amplifier and loop tuning capacitor.

is given in Fig. 8. As an alternative the amplifier may be built on a piece of Veroboard. It should be noted that the screen leads of the 2N3823 transistors are connected to earth.

To test the aerial system the input amplifier stage should first of all be balanced. Connect a meter between the drains of transistors Tr1 and Tr3 and adjust the preset resistor VR1 until the voltage is zero. The two transistors will now be drawing equal currents.

Tune in a fairly strong signal from a known direction and rotate the aerial to obtain maximum pick up. At this point the loop should be tuned to resonance by means of the tuning capacitor as indicated by a further increase of signal when resonance is reached.

If the aerial is now rotated so that it is roughly broadside on to the direction of the station being heard a point should be found where the signal falls to a low level. A further small adjustment of VR1 may enable the signal to be reduced even lower.

THE LOOP

The loop aerial used by the writer has 12 turns on a 24in. square frame. To reduce self-capacitance and give more turns for the same inductance the turns are spaced 3in. apart. For the winding 14/0·0076 p.v.c. covered flexible wire is used. Tuning is by a 365pF air spaced variable capacitor across the ends of the loop winding.

Signal pick-up for this loop with its amplifier was found to be some 20dB up on the signal from a 30ft. outdoor wire aerial. Using a Lafayette HE30 receiver the signal reading on the 'S' meter varied from S9+60dB at the maximum pick up point to about S3 when the loop was rotated to the null position. The null point itself is sharp and extends over perhaps only two or three degrees.

"Mobile" dog sledge

In the February 1973 issue of Practical Wireless on page 890 you have a little note about working amateur radio from a dog sledge, stating that this might have been the world's first OSO from a dog sledge mobile installation. I would like to point out to you that there have been a number of radio amateur contacts from dog sledges over the past years. My first contact from a dog sledge installation was made in 1938 and I am quite sure that that was not the first one in the world.

The UK expedition which some vears ago tried to reach the North Pole from Alaska also carried amateur radio equipment and had a number of contacts with the outside world. A Norwegian expedition which also some years ago tried to reach the Pole from the northern part of Greenland had practically all their contacts with the outside world made by amateur radio. Both these expeditions relied on dog sledges for their transportation.

In Norway and no doubt also in other countries with similar snow conditions amateur operations from dog sledges are not infrequent, and I myself have done it many times. I thought you might be interested in knowing this. Lars R. Heyerdahl, LA6A. (Oslo 2, Norway).

Don't get knotted!

A serious error was made by somebody when he knotted the mains input cable, as illustrated and described in the text on the battery eliminator (on pages 920 and 921).

This can be very dangerous and is specifically outlawed by the Institute of Electrical Engineers in their published regulations.

If a cable is rapidly bent from a straight to a highly twisted configuration, as often occurs when an item is knotted and the knot pulled tight rapidly, the core material may suffer from local fatigue causing cracking of the material. The cracking acts as a resistance to the current flowing through the appliances, hence local heating occurs.

The error, though dangerous is so common that M. Wallis could be excused it, provided the suggested warning is printed.

I would suggest that one of the plastic cable clamps, to secure mains leads, should be used. S. A. East, (Enfield, Middlsex).

Midget radio phones

Over the Christmas holiday I assembled the Practical Wireless midget radio, lashed it to the head-band of some wartime crystal 'phones and got good listening for radios 2 and 4 and others between.

The hospital wards being quietish, I set off on some market research: men and women patients listened and all said that such lead-less headphones would be much appreciated, since they currently roll about and pull out the lead, and also cannot use 'phones when sitting out in the middle of the ward. They need to be lighter than my prototype, perhaps built onto a stethophone; and as not a few are hard of hearing, a bit more volume is needed. If we want Radio Humberside or television sound (the ward set provides vision only) we should need something more sophisticated I suppose. Also an experienced Charge Nurse said if 'phones are not on leads I shall need to put them on chains!

Incidentally, when walking home across the common in the fog the wireless 'phones directionality helps personal alignment!—Dr. H. F. Barnard, Pathologist East Riding Group Laboratory, Westwood Hospital, Beverley, Yorks. HU17 8BU.

25 years of transistors

I was especially interested in Mr. R. Collins's article, 25 Years of the Transistor, because he attributed the research and development that led to it to the Bell Company's need for a substitute for the valve in the telephone service, in the 1940's.

I think that there must have been a lot that went before because men were looking for a substitute for the valve as early as

1920, and soon after, in the "Amateur Wireless" of those days, an account was published of a Russian scientist who was experimenting in making crystals perform all the functions of valves.

I remember this well because. as a schoolboy. I put this down as my own scientific basis for an application for an Experimenter's

Licence.

Unfortunately, I went to New Zealand afterwards, and lost touch with radio, but I wonder if any other reader can recall what. if any further developments there were in those experiments.-John Pinches (London, N.W.7).

A semiconductor substitute for the valve is now in production. It has improved characteristics and longer life and uses field effect transistor principles. This device, called a FETRON, will be described in full in next month's Practical Wireless.]-Editor

CO! Gambia

We have been asked by the General Manager of the RSGB to publicise the following letter received by him:-

Whilst on a visit to West Africa recently, I was able to visit the transmitting station of Radio Gambia. I was asked to make an appeal to British S. W. listeners to report to them any reception of Radio Gambia in Britain.

The point is that they have received reports and OSL cards from Australia and America, but would very much like to hear from any British listener. I understand that the transmissions are as follows:-

Radio Gambia, 4.82MHz in the 60metre short wave band.

They tell me the best time for a reception would be between 10.30 p.m. and 11.30 p.m. George Wallace, M.P. (House of Commons).

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t	12AE6	0.60	30 A E 3	0.40	50EH5		DM70	0.60	ECC89	0.50	ELS
ł	12AL5	0.55	30C1	0.80	50L6GT		DM160	0.68	ECC91	0.80	ELS
ĺ	12AQ5	0.50	30C15	1.00	85 A2	0.55	DY51	0.55	ECC189		ELS
١	12AT6	0.40	30C17	1.10	90 A G	2.40	DY86	0.85	ECC807		ELS
ł	12AT7	0.40	30C18	0.90	90 A V	2.50	DY87	0.86	ECF80	0.85	ELS
ĺ	12AU6	0.45	30F5	1.00	90C1	0.75	E88CC	0.70	ECF82	0.85	ELS
ı	12AU7	0.88	30FL1	0.80	90CV	2.40	E180F	1.00	ECF804		ELI
1	12AV6	0.45	30FL12		807	0.50	E810F	2.90	ECH42	0.75	EM
1	12AV7	0.70	30FL14		813	4.00	EABC8		ECH81	0.80	EM'
l	12AX7	0.33	30L1	0.40	866A	0-65	EAF42		ECH83	0.45	EM
ı	12AY7	0.75	30L15	0.95	5642	0.70	EBC33	0.60	ECH84	0.45	EM
1	12B4A	0.65	30L17	0.95	6080	1.75	EBC41	0.65	ECL80	0.50	EM:
ì	12BA6	0.45	30P12	1.00	6146	1.60	EBC81	0.33	ECL81	0.50	EM
ł	12BA7	0.50	30P19	0.95	6146B	2.50	EBF80	0.40	ECL82	0.85	EM:
ı	12BE6	0.50	30PL1	0.95	6360	1.25	EBF83	0.40	ECL83	0.70	EM:
ì	12BH7	0.50	30PL13	1.10	6939	2.25	EBF89	0.32	ECL84	0.55	EN
l	12BY7	0.65	30PL14		7199	0.85	EBL31	1.50	ECL85	0.55	EY
١	12K5	1.00	35A3	0.60	7360	2.20	EC53	0.50	ECL86	0.40	EY
ı	12K7G1		35 A 5	0.75	7586	1.50	EC86	0.60	ECLL80		EY
ı	12Q7GT	0.45	35B5	0.65	7895	1.50	EC88	0.60		2.20	EY
ı	128 R7	0.50	35C5	0.60	A2293	2.20	EC90	0.85	EF37A	1.00	EY
l	20D1	0.60	35 D5	0.75	A21	0.60	EC92	0.45	BF40	0.50	EY
ſ	20L1	1.10	35L6GT	0.75	AZ31	0.55	EC93	0.60	EF41	0.65	EY
ı	20P1	0.50	35W4	0.40	CBL1	0.90	ECC35	1.00	EF42	0.70	EZ4
l	20P4	1.10	3523	0.75	CBL31	1.00	ECC40	0.70	EF80	0.30	EZ4
į	20P5	1.20	35Z4G	0.40	CY31	0.50	ECC81	0.40	EF85	0.85	EZ8
l	25C5	0.60	3525GT	0.70	DAF96	0.50	ECC82	0.88	EF86	0.30	EZ8
I	25L6GT	0.50	50A5	0.80	DF96	0.50	ECC83	0.88	EF89	0.28	GT
l	25Z4G	0.35	50B5	0.70	DK92	0.70	ECC84	0.30	EF91	0.87	GY
Į	25Z6GT	0.75	50C5	0.60	DK96	0.60	ECC85	0.40	EF92	0.85	GZS

	EF98	0.75	GZ33 0	-75	PL33	0.40	U404	0.70
	KF183	0.80		-60	PL36	0.55	11801	0.80
E	EF184	0.85	HABC80		PLSI	0.50	UABCS	0
	EF804	1.25		-55		0.45		0.40
	EK90	0.82	HK90 C	-50	PL83	0.45	UAF41	0.70
	EL33	1.50	KT66 2	35	PL84	0.40	UAF42	
	EL34	0.50		25		0.95	UB41	0.65
	EL36	0.50		-60	PL504	0.75	UBC41	0.55
	EL37	1.70	PABURG		PL508	0.90	CBCSI	
	EL41	0.75		-60	PL509	1-10	UBF80	
	EL81	0.55		-60	PEROL	1.00	UBPRR	
	EL83	0.50		05	P L802	0.95	UBLI	0.70
0.40	EL84	0.25		-50	PM84	0.60	UBL21	
0.50	EL85	0.48		148	PY31	0.35	1,055	0.45
0.80	EL86	0.40		-40		0.63	UCC85	0.45
9 0-65	EL90	0.42		-40	PY80	0.40	UCF80	
7 1-00	EL95	0.85		-55	PYNI	0.80	UCH21	
0.85	EL821	0.60		-55	PY82	0.35	UCH42	
0.85	EL822	1.40	PCC189 (PY83	0.38	UCH81	
41-65	ELL80		PCC805 (PY88	0.40	UCLSI	
0.75	EM34	1.00	PCC806 C		PY800	0.47	UCL82	
0.80	EM71	0.80		-30	PY801	0.50	UCL83	
0.45	EM80	0.45		35	PZ30	0.38	UF9	0.65
0.45	EM81	0.80		-60	QQ V 02-		UFII	0.60
0.50	EM83	0.50		-60		2.25	UF41	0.65
0.50	EM84	0.85		·10	QQ1'03		UP42	0.65
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0.70	EM87	0.70	PCF802 C		667.03		11F80	0.35
0.55	EN91	0.40	PCF805 (5.25	UF85 UF89	0.40
0.55	EY51	0.40	PCF806 0		TT21 TT22	8-40	UL41	0.40
0.40	EY80	0.75	PCF808			8·50 0·75	ULA	0-65 0-48
300	EY81	0.40	PCH2000		U18/20 U25	0.85	UM84	0.30
2.20	EY83	0.55		-50 -35		0.85	UVIN	0.50
1.00	EY86	0.40				0.70	UYII	1.00
0·50 0·65	EY87 EY88	0·43 0·48		-85 -45		6.50	UY4i	0.48
0.70	E 240	0.20		45		0.40	UY82	0.50
0.30	EZ41	0.75		25		0.40	UY85	0.40
	EZ41		PCL800 1			0.40	W729	0.75
0·85 0·80	EZ81	0·28 0·29	PCL800 1			0.75	Y63	0.75
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0.85		0.45		70		0.55		
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6CG7 6CG7 6CH6 6CL6 6CU6 6CW4 6CY5

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THE AMATEUR BANDS David Gibson, G3JDG

Frequencies in kHz Times in GMT

E are running out of frequencies. I know we have certain "Amateur Bands," but some of these are on a shared basis, i.e. we can only use them provided we are not a nuisance to other non-amateur stations using the band.

Many will remember when 40 metres was 300kHz wide-it's now 100kHz wide and intruders still try to drive us off this remaining r.f. island. The only real answer to amateur radio survival is intelligent activity. With a band full of active enthusiasts, intruders will think twice about taking on our "QRM". Those that do would find a few hundred amateurs from dozens of different locations and countries, all suddenly doing tests on that particular frequency. Whether amateur radio loses any more of its r.f. spectrum or indeed a complete amateur band, is entirely up to the people who practise and enjoy our hobby.

A topical example is 4 metres or 70MHz. This band is greedily looked at by many people (nonamateurs) who would like to use the small piece of 4 metres which we still have. Activity on 70MHz is very low from an amateur's point of view, and if activity is not increased, then the authorities may well award the entire 4 metre band to "other services". The argument could well be (and it is a valid one) that since there is so very little amateur activity on 4 metres, then you do not really need that band. So how about some logs for 4 metres?

·A 4 metre converter is not a difficult thing to build and would offer a very useful intermediate step in construction practice between the h.f. bands and 2 metres. Constructing a converter for 70MHz is not difficult but needs a little more care than units constructed for the lower frequencies. One excellent idea would be to use 70MHz as a local net band, which would avoid the interference suffered on 160 metres top band, would keep us clear of Loran, which plagues 160, and would increase the level of 4 metre activity dramatically. We have to start somewhere or we could well lose this band. So, 4 metre enthusiasts forward. Let's hear what vou hear.

A letter from Paul Petty (Canterbury) tells of a useful information service for European stations which transmits on 80 metres between 2100 and 2200 GMT. There is a controller station which is changed daily. Monday's controller is DA1LA. On Wednesdays it is DK8FZ. The purpose of the net is to assemble and disseminate information on DX

stations, i.e. future skeds.

Top band enthusiasts will be delighted to hear that G3SZA has been heard on 160 metres in Australia by a VK3 station. Alas callsigns are still changing. MP4 stations have been heard using a new call sign-A4FA. When will we have some callsign stability? And why change from MP4M to A4FA?

Another strange change is that CT1 stations are to use the prefix CT4 during the CQWPX contest

this month. Why is not made clear. First class licence holders in Japan now have two-letter suffix calls and second class licensees will use a JM suffix followed by three letters.

Old hands will be pleased to hear VR6TC on again from Pitcairn Island, and DX enthusiasts who enjoy hearing/working island stations should listen for VQ9HCS who radiates on 15 metres in the

afternoons from Aldabra Island.

Robert Harpur (Shenfield) tells of two VP8 stations located in South Georgia which can be heard some evenings between 14.125kHz and 14.130kHz. This page commonly informs of stations heard by other short wave listeners and amateurs. The gear is quoted, i.e. receivers, a.t.u. preselectors etc., in this way readers can gauge how their own performance is by direct comparison especially if the report is from someone using similar equipment. It has been suggested it would be nice to actually see some of these stations. Photographs of individual set ups would be of interest to others. Anyone got any really good, sharp photographs of the gear plus themselves. Think of the satisfaction of seeing your trusty old CR100 smiling back at you from the pages of PW.

Peter Franklin (Skegness) received a UNR30 receiver for Christmas and is busily spoiling the brute with a diet of 100ft. end fed. A preliminary listen on eighty metres brought forth a high level of G activity. Peter queries the callsign G4GJ heard testing a transmitter on 3.8MHz one afternoon.

Will the real G4GJ please stand up?

Another eighty metre enthusiast is Peter Reed (Brighton) who is the proud possessor of an FTDX401 receiver which apparently has a Japtick UFP. Sorry Peter, I know of no ointment which can cure that. Perhaps you could scrape it off with a bent screwdriver. Peter's log for eighty reads; FL80M, HS4AGM, I5FLN, JW9QH, M1C, M1I, VE1AIH, VE1IE, VS6DO, VQ9R, W1AA, W1KET, W2APU, W2PV, W3WJD, YA1AH, ZL4KE, ZS1MH, ZS3GH, 5X5N, 9G1DY, 9H1C, 9H5D, all on s.s.b.

Stephen Mayer (Poole) has a CR70A receiver fed with a 90ft. wire. This set up brought in stations from most European countries. From further afield: PY2ZAT, W4AG, W5QGZ, all on eighty metres.

Great rejoicing in South Yardley where David Sharred has found that his blood pressure and country score have increased in direct proportion to the arrival of a new CR150/2. This, together with sharp ears (no, he's not Mr. Spock) and a 140ft. end fed raised these on 3.8MHz; CT2BG, FP8CT, K1DQV, VE1ADV, VE3CDP/W9, VE7SV, W1CF, W4CC, W5SR, W5SW, WA9PRO, ZL3GS, 4X4UF, 5X5NK, 5X5XM, 9HIC.

Logs, in alphabetical order please, to arrive by the fifteenth of the month to:

12 Cross Way, Harpenden, Herts.



MONTHLY NEWS FOR DX LISTENERS

THE first topic for this month is that of aerial wire. In the February column I asked if anyone knew of a good source for aerial wire. The number of replies was very pleasing and I must apologise for not being able to answer them all personally.

In general, your answers seem to bear out my opinion that it is becoming more difficult to find supplies of good quality aerial wire. The wire which I have always used in the past is that manufactured by a firm called 'Aerialite'. This wire consists of seven strands of copper with very strong insulation which is ideal for the purpose.

Mr. A. E. Halladay informs me that this is still available from a shop called 'Al Radio Components' of 14 The Borough, Canterbury, Kent. The wire is available in lengths of 25, 50 or 75 feet and is very reasonably priced at 14p, 2212p and 29p respectively. A charge of 6p is made for post and packing.

Mr. David Porter writes to say that a firm called Chas. H. Young Ltd of 170-172 Corporation Street, Birmingham, B4 6UD sells Stranded 7/·029 and 32/0·2mm Insulated wire in 140 foot lengths for £1·87. This firm is also a good source for aerial insulators and dipole centre pieces.

Mr. A. A. Smith of Preston in Lancashire suggested the use of a particular type of G.P.O. Telephone wire. This consists of a single strand of steel wire which is covered with a film of copper and then a layer of insulation. It is usually supplied as a twin cable, similar to lighting flex, but this is easily split into two separate wires. The advantage of this wire is the superior strength of the steel core. No supplier is known but the wire should be available from Surplus Stores.

A preselector is basically an r.f. amplifier and, as such, it will improve the performance of almost any receiver. Many receivers do not have an r.f. amplifier stage, the first stage being the mixer and it is with these sets that the most significant improvement in performance will be obtained. If the receiver has one or more r.f. stages incorporated the improvement will not be so marked.

The preselector usually provides a gain of 30dB, which in simple terms is a gain of 32 times, this gain being very useful in the reception of weak signals.

It is worth noting that the most common source of lost efficiency in a receiving system is a mismatch between components of the system. The three common components are the aerial, the preselector and the receiver. In the simplest case of aerial and receiver it is essential to have a good match between the two. If a preselector is added there must be a good match between the aerial and the preselector and also between the preselector and receiver.

THE BROADCAST BANDS

Malcolm Connah

Frequencies in kHz • Times in GMT READERS' LOGS

The first log comes from Raymond Mowll, who enquired about preselectors, his equipment is a Trio 9R59DS and 100 feet of wire. The lack of a preselector did not prevent him from hearing:

5047 Togo, French news and music at 2250.

7120 Kiev, with Mailbag programme at 0045. 7180 BBC, Tebrau, Malaysia relay at 1720.

9655 R. Damascus, Syria, in English at 2040.

11710 RAE, Argentina with music at 2330.

11955 FEBA, Seychelles in English at 1745. 15140 R. Havana, Cuba, commentary at 2100.

15375 R. Nederland, Bonaire, English at 1830.

R. M. Witney of Braintree has been active again with his Skywood CX-203 receiver and 110 foot longwire hearing the following stations:

11730 Radio Ceylon at 0140.

11815 Trans World Radio, Bonaire at 0055.

15165 Radio Denmark at 2000.

15448 Radio Nacional de Brazilia in Spanish at 0225.

Peter North of Southport has sent in his first report to the column using his Heathkit RG-1 receiver and 24 foot long-wire to hear:

4979 R. Rumbos, Venezuela in Spanish at 0430.

4995 R. Brazil Central in Portuguese at 0030.

5075 R. Sulatenza, Colombia, Spanish at 0130.

9550 RTB, Belgium in English at 0050.

9730 ETLF, Ethiopia in English at 0400.

9745 R. Baghdad, Iraq in English at 1930.

11710 RAE, Argentina in English at 2300.

11720 R. Nacional de Brazilia in English at 2230.

11805 R. Globo, Brazil in Portuguese at 0030.

11860 R. Canada International, English at 2115.

11880 R. Ankara, Turkey in English at 2200.

11930 WIBS, Grenada in English at 2030.

11955 FEBA, Seychelles in English at 1730.

15300 HCJB, Quito, Ecuador in English at 1900.

15345 R. Kuwait in English at 0500.

Reports should arrive by the 15th of the month and be addressed to me at 59 Windrush, Highworth, Swindon, Wiltshire, SN6 7DT.

NEXT MONTH

ON THE AIR

Our specialist team will present news, views, comment and of course YOUR LOGS on the Broadcast Bands (Short Wave and Medium Wave). The Amateur Bands (Short Wave) and

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(Overseas P. & P. £1)



ROAMER **9** (1) (3) **EIGHT** Mk I NOW WITH VARIABLE TONE CONTROL

7 Tunable Wavebands: MWI, MW2, LW, 8WI, 8W2, 8W3 and Trawler Band. Built in Ferrite Rod Aerial for MW and LW. Retractable chrome plated Telescopic aerial for Short Waves. Push pull output using 600mW transitors. Car aerial and Tape record sockets. Selectivity awitch. 8 transistors plus 3 diodes. Fine tone pushing oil. Selectivity awisen, 8 transistors plus 3 diodes. Fine tone mowing coll speaker, Air spaced ganged tuning condenser. Volume/on/off, tuning, wave change and tone controls. Attractive case in rich chestnut shade with gold blocking. Size 9 × 7 × 4in, approx. Easy to follow instructions and diagrams. Parts Price List and Easy Build Plans 25p (FREE with parts). Earpiece with plug and switched socket for private listening 30p extra.

Total building cost 26.98 P. P. & (Overseas P. & P. £1)



7 Tunable Wave-bands: MW1, MW2, LW, SW1, SW2,

bands: MW1, MW2,
LW. 8W1, 8W2,
SW3 and Trawler
Band. Extra Medium waveband provides easier tuning
of Radio Luxembourg, etc. Built in ferrite rod aerial
for MW and LW. Retractable 4 section 24in. chrome
plated telescopic aerial for 8W. 80cket for Car Aerial.
Powerful pusb-pull output. 7 transistors and 2 diodes,
fine tone noving coil apeaker. Air spaced ganged
tuning condenser. Volume/on/off, tuning and wave
change controls. Attractive case with carrying handle
81ze 9 × 7 × 46n. approx. Easy to follow instructions
and diagrams. Parls price list and easy build plans
25p (FREE with parls).
Earpiece with plug and switched socket for private
listening 30p extra.

Total building costs £5-98 P. P.A.

6 Tunable Wave-bands: MW, LW, 8W1, 8W2, 8W3 SWI, SW2, SW3
Trawler, bandplus
an extra Medium
waveband for
easier tuning
of Luxembourg
stc. Sensitive ferrite rod aerial and

rite rod acrial and telescopic acrial for Short Waves.
31n. Speaker. 8 stages—6 translators and 2 clodes. Aftractive black case with red grille, dial and black knobs with polished metal inserts. Size 9 × 5½ × 2½n. approx. Easy build plans and parts price list 25p (FREE with parts).

Total building costs £3-98 P. P. &

POCKET FIVE

8 Tunable Wavebands: MW, LW, Trawier Band with extended M.W. band for easier tuning oband for easier tuning of Luxenibourg, etc. 7 stages—5 transistors and 2 diodes, supersensitive ferrite rod aerial, fine tone moving coil syeaker. Attractive black and gold case. Size 5 ½ 1 ½ × 34 in. Easy build plans and parts price list 10p (FREE with parts).

Total building costs £2-29 P.P. & P. 63p) (Overseas P. & P. 63p)

TRANSONA FIVE

5 TRANSISTORS AND 2 DIODES



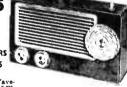
3 Tunable Wavebands: MW, LW and Trawler Band. 7 stage—5 transistors and 2 diodes, ferrite rod aerial. tuning condenser volume control, fine tone moving coll speaker. Attractive case with red speaker grille. Bize 6½ × 4½ × 1½m. Easy build plans and parts price list 10p (FREE with parts).

Total building costs £2.50 P. P. & (Overseas P. & P. 63p)

TRANS EIGHT

ROAMER

8 TRANSISTORS and 3 DIODES



6 Tunable Wavebanda: MW, LW, 8W, 8W, 8W, 8W, 8W, 8W, 8W, 8WS and Trawler Band. Sensitive ferrite rod aerial for M.W. and L.W. Telescopic aerial for Short Waves, 3ln. Spraker. 8 improved type transitors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with pollahed netal inserts. 81ze 9 × 5½ × 2§ln. approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker, Parta price list and easy build plans 25p (FREE with parts).

Total building costs £4.48 P. P. &

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Authorities and all those interested in radio construction

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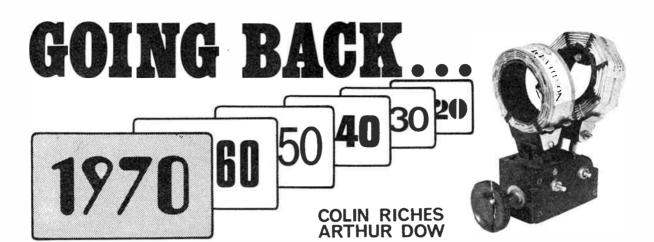
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ROAMER TEN DIESE ROAMER EIGHT TRANSONA FIVE POCKET FIVE	ROAMER SEVEN TRANS EIGHT
Parts price list and plans fo	or
Name	
Address	



THE other month we received a letter from one of our New Zealand readers who informed us that he is an ardent vintage radio equipment collector. He told us that he decided one day to cart all his gear out on to his back lawn (it's baking hot over there at this time of the year) and take some pictures for us to show in the Going Back column.

The reader, George A. Weston, says that he would be grateful if anyone could supply him with the exact dates of the British-made sets, so, if anyone wants to contact him, the address is 179 Rosebank Road, Avondale, Auckland, New Zealand.

The items we show in our pictures have all been fully restored by Mr. Weston and where components had to be substituted, he used parts of the same vintage. Likewise, any valves used were of the same

period and not later replacement types.

Picture No. (1) is a set made by McMichael. It has MH on the panel and is an all-wave superhet. There are five valves inside the unit and one outside.

Date is about 1927.

Next, in picture (2) is a Philips 2516 with valves 506, E415, B443 and date of manufacture is about 1930. The matching speaker is a Baby Grand model 2028 balanced armature cone type that can either hang on the wall or sit on the table as shown.

Set No. (3) is an American "Radiola" model 12/20. Dated about 1925 it has UX199's in all stages except a UX120 as output valve. Case is walnut veneer.

The Gecophone shown in photograph (4) is a 1924 model containing 2 valves and working from batteries. There is one r.f. stage with variometer and a detector stage with condenser-controlled reaction. The valves used are "R" types and the receiver is shown sitting on top of a 2-valve amplifier.

Picture (5) shows a 1924 "B.T.H." crystal set with matching phones. The "driving instructions" are shown in the lid. Also shown is a "Polar Twin" 2-valve battery receiver about 1924 vintage and a Gecophone crystal set c1924 in mahogany case.

The "B.T.H." is called "Radiola"—a name generally associated with RCA in America, indicat-

ing a tie-up between manufacturers.

An "Atwater-Kent" model 30 c1926 6-valve set is shown in picture (6). It uses grid stoppers (Cossor system) in lieu of neutralizing. This was the first single-dial model made by this company. Valves are UX201A's in all stages.

No. (7) is an American 1926 "Grebe" MV1 synchrophase 5-valve neutrodyne battery set. Valves

used are UX201A's. The cabinet is mahogany.

A Philips Dutch 2510 1930 vintage 5-valve mains t.r.f. is shown in picture (8). Valves 2 x E442 screen grid, detector E415, output C443 with a 506 rectifier. The case is a metal frame enamelled black with insert panels mottled rich deep red.

Picture (9) shows an American "Gilfillan GN1 c1926 5-valve neutrodyne battery set. This is a de-luxe model with walnut veneer case. It is 3ft long to accommodate "B" batteries. There is a meter for battery checking and three covers on the front

drop down. In 1926, this set cost £35.

No. (10) shows a "Claritone" re-entry horn speaker (rear left) made by Automatic Telephone Co., England. It has a heavy cast-iron case and was made in 1924. A B.T.H. horn speaker (rear right) can be seen (c1926). This model has a brown flare with a transfer in black and gold.

Also shown are a "Brown" H4 (front left) (c 1926) a Burndept "Peter Pan" (c 192??) and a "True Music Minor" (front left)—date not known and

no information available.

Photograph No. (11) shows an American cone speaker with a balanced armature. It is made from pressed steel and painted gilt. No. (12) is a cone speaker with a reed unit. It is called a "Mellotone" and the cone is made entirely of cardboard. The stem and base are wooden and the date is April 1926.

In some future Going Back articles we hope to show some more of our readers' collections of vintage radio gear.

A reader remembers

R. J. Hall, 7 Darlington Road, Longrock, Penzance, Cornwall, comments on his early days in radio . . .

"In those days the enthusiast enjoyed winding his own solenoid coils and basket coils, building up variable capacitors from threaded brass rod, brass or aluminium plates and nuts and bolts, and even winding transformers, both r.f. and a.f. I myself have wound more than one mains transformer by hand at 7 turns per volt on a sq. inch core and made speech coil formers and wound them.

It was common practice in the early days to plan a set and build it on a 'breadboard' layout when it usually worked perfectly but on being tidied up and put into a cabinet it invariably refused to function. In those days radio was a fascinating hobby but since it has become an exact science half the fun has gone".



McMichael "MH" receiver dated about 1927.



The Philips 2516 dated about 1930 and Philips 'Baby Grand' speaker



R.C.A. model 20 Radiola of 1925.



4 Gecophone 1924 vintage sitting on a 2-valve amplifier



B.T.H. crystal set (1924) with Polar Twin and Gecophone set



The Atwater-Kent model 30.



American Grebe MV1 (1926).



8 Philips 2510 receiver (1930).



American Gilfillan GN1 c1926.



A selection of vintage speakers. 10



11 American cone speaker with balanced armature.



Cone speaker with a reed unit. 12

TAKE 2®

JULIAN ANDERSON

HEN a diode is reverse biased it becomes a low value capacitor. Integrated circuits make use of this effect as in this technology it is far easier to incorporate this than a more conventional component. What is more, the actual value of the capacitance depends on the voltage applied. Special diodes are made to make the best use of this effect and are known as Varicaps but as we have mentioned, all diodes exhibit this affect, the higher the current rating, the better the affect. We can make use of this effect where a small capacity change is sufficient such as in a b.f.o. and it is this which forms the subject of our project this month. Instead of using a variable capacitor, which would be expensive, we are using a simple potentiometer to alter the tuning.

The complete circuit is shown in Fig. 1. The tuned circuit, which operates round about 465kHz, is made up from C4 and L1. This is coupled to Tr1 to form an oscillator, C2 providing the feedback to maintain

oscillation.

L1 is the Repanco DRX1 crystal set coil which has both long and medium wave windings, we only use the medium wave winding in our circuit and the connections should run to the common connection of both windings and to the tag that goes to the start of the smaller winding. In the normal state this would be tuned somewhere in the medium wave band and to increase the inductance (and also to give some control over the operating frequency) we fit a dust core into the centre of the coil.

The tuning side is accomplished by VR1, R1, D1 and C1. If a low value capacitor is connected from the collector of the transistor to the negative line this will alter the frequency. We cannot connect the diode directly here as we would affect the d.c. operating conditions of the transistor and so we have to d.c. block this; C1 performs this function.

To alter the capacity of the diode we have to apply d.c. bias to it and this has to be varied. VR1 can be almost any potentiometer from $5k\Omega$ to $500k\Omega$; all we need is a variable voltage at the slider. R1 has to be included to prevent funny things happening at the extremes of the track.

As regular readers of this column will know, we often use Veroboard but this is of less use at r.f. frequencies and straightforward drilled s.r.b.p. board is better and a layout is shown in Fig. 2. This should cause few problems; the wiring on the reverse side is shown dotted.

When the unit is switched on, the slider of VR1 should be at the centre of the track and then, with the unit near a receiver, the core in L1 should be turned until a whistle is heard on all stations. Whistles may well be heard on one or two stations but this will mean that the frequency, or an harmonic of it, are on top of that station and not on the i.f. When the correct setting has been found VR1 can be adjusted to get the right sort of beat note, it has a fair range both sides of the centre frequency. On the layout a wire is shown marked "To Rx". It will not normally be necessary to make a

No. 47 VARICAP TUNED B.F.O.

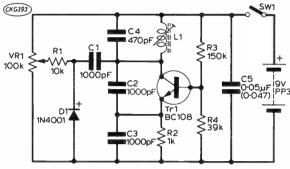


Fig. 1 The circuit instead of using a conventional variable capacitor,

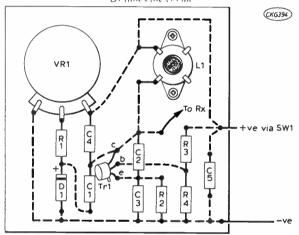


Fig. 2: A suggested component layout on drilled s.r.b.p. board.

* components list

R1	10kΩ ¼W, 5 per cent	1p
R2	1kΩ ,,	1p
R3	150kΩ ,,	1p
R4	39kΩ ,	1p
VR1	100kΩ linear pot	12p
C1	1000pF polystyrene	4p
C2	1000pF polystyrene	4p
C3	1000pF polystyrene	4p
C4	470pF polystyrene	4p
C5	0·05μF Mylar etc.	4p
Tr1	BC108	10p
D1	1N4001	6p
L1	DRX1 crystal set coil	18p
Dust	core to fit L1	3p
SW1	On-off toggle switch	5p
		78p
	es are those recently ad- ged. No allowance is ma	

connection and this wire may not be needed but if the beat note is a bit weak this wire may be dangled among the components of the receiver's i.f. strip.

costs or for postage and packing and these points should be checked carefully before ordering.

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8N7401	0.20 0.18 0.16	8N7451	0.20 0.18 0.16 0.20 0.18 0.16	8N74140	2 · 35 2 · 95 2 · 15
8N7401	0.20 0.18 0.16	8N7453	0.20 0.18 0.18	8N74151	1.10 0.95 0.90
8N7403	0.20 0.18 0.16	8N 7454	0.20 0.18 0.16	9N74153	1.85 1.27 1.20
8N7404	0.20 0.18 0.16	8N7460	0.20 0.18 0.16	8N74154	2.00 1.75 1.55
8N7405	0.20 0.18 0.16	8N7470	0.30 0.27 0.25	8N74155	1.55 1.47 1.35
8N7406	0.80 0.27 0.25	8N7472	0.80 0.27 0.25	8N74156	1.55 1.47 1.35
8N7407	0.80 0.27 0.25	8N7473	0.40 0.37 0.35	8N74157	1.80 1.70 1.50
8N7408	0.20 0.19 0.18	8N7474	0.40 0.87 0.85	8N74160	2.60 2.40 2.25
8N7409	0.45 0.42 0.35	8N7476	0.55 0.52 0.50	8N74161	2.60 2.40 2.25
8N7410	0.20 0.18 0.16	8N7476	0.45 0.42 0.89	8N74162	3-40 3-25 2-70
8N7411	0.23 0.22 0.20	8N7480	0.80 0.75 0.67	8N74163	3-40 8-25 2-70
8N7412	0.42 0.40 0.35	8N7481	1 - 25 1 - 15 1 - 10	8N74164	2.75 2.30 2.10
BN7413	0.80 0.27 0.25	8N7482	0.87 0.80 0.70	8N74165	4.00 3.50 3.00
BN7416	0.80 0.27 0.25	8N7483	1.00 0.90 0.85	8N74166	4.00 8.50 3.00
8N7417	0.80 0.27 0.25	8N7484	0.90 0.85 0.80	8N74167	6-25 5-60 5-10
8N7420	0.20 0.18 0.16	8N7486	0.45 0.41 0.38	8N74170	4-10 8-55 3-05
8N7422	0.48 0.44 0.40	8N7490	0.75 0.70 0.65	8N74174	2.00 1.75 1.80
BN7423	0.48 0.44 0.40	8N7491 A	N1-00 0-95 0-90	8N74175	1-35 1-27 1-15
8N7425	0.48 0.40 0.35	8N7492	0.75 0.70 0.65	8N74176	1.60 1.85 1.20
8N7427	0.42 0.39 0.35	8N7493	0.75 0.70 0.65	8N74177	1-60 1-35 1-20
8N7428	0.50 0.45 0.42	8N7494	0.80 0.75 0.70	8N74180	1.55 1.80 1.20
SN7430	0.20 0.18 0.16	8N7498	0.80 0 75 0.70	8N74181	7-00 5-00 5-50
8N7432	0.42 0.89 0.85	8N7496	1.00 0.97 0.95	8N74182	2.00 1.80 1.60
8N7433	0.70 0.61 0.44	8N7497	6.25 5.50 5.00	8N74184	2-40 2-00 1-80
BN7437	0.65 0.60 0.50	8N74100		8N74185A	
8N7438	0.65 0.60 0.50	8N74104	1.45 1.35 1.20	8N74190	1.95 1.85 1.75
8N7440	0.50 0.18 0.16	8N74105	1 - 45 1 - 85 1 - 20	8N74191	1.95 1.85 1.75
	N 0 - 75 0 - 72 0 - 70	8N74107	0.50 0.45 0.40	8N74192	2.00 1.90 1.80
8N7442	0.75 0.72 0.70	8N74110	0.80 0.70 0.60	8N74193 8N74194	2.00 1.90 1.80 2.50 2.25 1.90
BN7443	1.00 0.95 0.90	8N74118 BN74119	1.00 0.95 0.90	8N74195	1.85 1.70 1.60
BN7445	2.00 1.75 1.60	8N74121	0-60 0-55 0-50	8N74196	1.50 1.40 1.30
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IN4006	800	12
IN4007	1000	15
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PL4002	100	9
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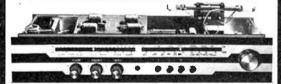
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THIS instrument was designed for use with a photographic enlarger, to determine the exposure required for any particular print. It is cheap to build and easy to use, with a range up to about 40 seconds.

THE CIRCUIT

This is shown in Fig. 1. LDR is a light dependent resistor whose resistance varies with the amount of light falling on its face. LDR and VR1 form a potential divider. The potential at point A is determined by the setting on VR1 and on the resistance of the LDR, hence on the light incident on its surface. Tr1 and Tr2 form a Schmitt trigger. The potential at A determines which of these transistors is on and which is off.

Tr2 has a light emitting diode D1 in its collector circuit, which lights when Tr2 is conducting.

To measure the amount of light incident on the meter, VR1 is altered until the extinguishing (i.e. on-off) point of the diode is found. The setting of VR1 is thus a measure of the exposure time required. A knob with a linear calibration around the outside is used to alter VR1.

The unit is sensitive to voltage supply change, hence a zenor diode D2 is used to regulate the power supply.

SWI is a push button switch which is depressed only when making the exposure, hence eliminating the possibility of forgetting to turn the unit off.

COMPONENTS

Other transistors could be used for Tr1 and Tr2 e.g. 2N2926. VR1 is $50k\Omega$. Increasing the value increases the range of the instrument but decreases its sensitivity.

DI does not have its positive lead marked. This must be found by trial and error or by using a meter.

CONSTRUCTIONAL DETAILS

The whole unit can be fitted into a small plastic box 412in. x 3in. as shown in Fig. 2. Veroboard is used to mount the transistors and resistors. Two small holes can be drilled to take the LDR leads, a dab of

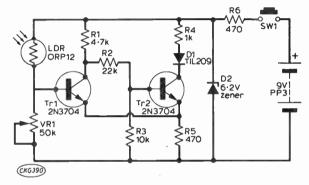


Fig. 1: The complete circuit which is basically a Schmitt trigger.

* components list

Resistors		
R1 4·7kΩ	R4 1kΩ	
R2 22kΩ	-R5 470Ω	
R3 10kΩ	R6 470Ω	
All &W, 5% types		FIRST MARKET
VR1 50kΩ lin. pot.		
LDR ORP12.		
EDR ORF 12.		
Transistors		
TR1 2N3704		
TR2 2N3704		
D1 TIL209 (light en		
D2 6.2V zener diod	e.	
Miscellaneous		
9V battery; Battery	connector; \	eroboard; On-off
switch, push butto	n type: Plasti	c box; Calibrated
knob or dial.		

glue will hold it in place. Further constructional details are not given since the layout is not critical and most constructors will find it is a simple job to assemble the instrument.

The instrument is now ready for calibrating.

CALIBRATION

The scale is calibrated in terms of exposure as follows: a piece of clear blank film is put into the

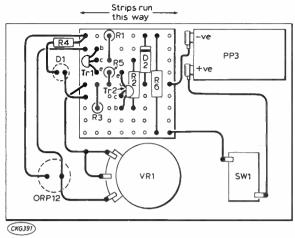


Fig. 2: Constructional details.

For scale readings between 20 and 40 seconds it will be easier if the strips are exposed in multiples of 4 seconds.

A similar calibration graph must be obtained for each different type of printing paper used.

USING THE INSTRUMENT

Having obtained the graphs, the instrument is simple to use. Place it on the easel such that a clear part of the film e.g. the margin between the frames or an unexposed frame, shines onto the LDR. Find the on-off point of the diode DI and note the scale reading. From the graph, read off the required exposure time, if the scale reading is 5 then the exposure time is 19 secs. This will give the correct exposure time for all normal negatives with full tonal reproduction.

CONCLUSION

The instrument is cheap and easy to make, and is

First black strip, i.e. exposure time for this print is 14 secs.

Fig. 3: An example of the gradiations which will appear on the printing paper; the time of each exposure is marked below.



enlarger; all lights in the darkroom are put out except for the enlarger light; the instrument is placed on the easel, SW1 is depressed and VR1 is adjusted so that the diode light just goes from on to off. The reading on the scale is noted. (It is important that the scale reading is always taken from on-to-off since the off-to-on reading is different, owing to hysteresis in the Schmitt trigger.)

2

A narrow strip of paper is then used for a test strip. Parts of the paper are exposed in multiples of two seconds. The developed strip will look like Fig. 3. There is a gradual transition from light to black. The first black stripe can be judged and the corresponding exposure time also. The scale reading and exposure time are then noted.

The procedure is then repeated for different light readings (scale readings) and a graph of scale reading against exposure time is plotted, Fig. 4.

Fig. 4: A calibrated graph relating the knob markings of 1-10 to the time.

reasonably accurate. Its great advantage is the saving in time, since after initial calibration there is no need to make a test strip for every exposure.



25 YEARS MARCH 1973 page 993. At the foot of column three: The I.E.R.E. is publishing a collection of 20 papers in their journal on semiconductor subjects.

DIGITRONIC SOLID STATE DIGITAL CLOCK MARCH 1973 page 1009. The sentence—There is no need . . . harm a LED is to pass too high a *current* through it (most LEDS work operate on 10–15mA).

Back Numbers

We regret to inform readers that owing to the closure by the Company of the department concerned it will no longer be possible to supply back numbers of **Practical Wireless** or **Television**.

Reference to past issues of the magazines may sometimes be obtained at certain public libraries who may hold bound volumes. A few libraries are said to offer a photostat service. Alternatively, we are always willing to insert a free request for specific back numbers in our "CQ" column which appears in most issues.

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Č	1/835	50	4-7 Ω-470 Κ Ω	E24	ĭ	0.8	0.7
C	1/4W	100	4.7 Ω 1031 Ω	E12	ī	0.8	0.7
Č	1/2W	50,	4 7 Ω 1031 Ω	E24	1.2	1	0.9
C	LW.	10%	4-7 Ω 10 M Ω	E12	2.5	2	1.9
310	1/2W	130	10 Ω-1 Μ Ω	E24	4	а	2 nett
M.M.	- 1 W	$10^{\circ}, \pm 1/20 \Omega$	0·22 Ω−3 trΩ	E12	7	7	6
IA II.	314	\$ °.,	ΙΩ~10ΚΩ	E12	7	7	6
W*W'	7 W	5%	1Ω-10ΚΩ	E12		9	8

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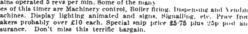
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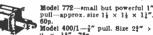
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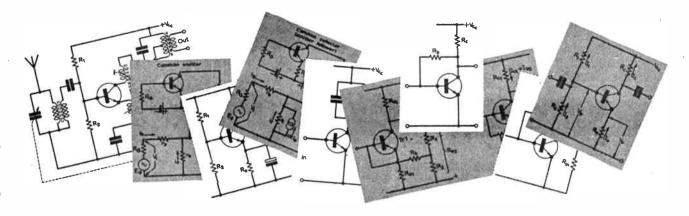
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NSISTOR CIRCUITRY for beginners H.W. HELLYER & MICHAEL HOLLIER

Tone control circuitry

Toward the end of the last part of this series of articles that was published, we were concerned with frequency-dependent feedback. Without being intentionally devious, we skated over some of the finer points and here shall try to keep our promise of digging more deeply into the matter of tone controls. their design and their limitations.

The utter purist will not deign to acknowledge the need for tone controls! Everything should be flat, he says. There should be, he further asserts, no need to alter the frequency response of an amplifier if all the other parts of the audio system are in order. True, but Utopia has not yet arrived, whatever the politicians promise, and there will be nasty pops and crackles from our records, hiss from our tape, peaks and troughs from many a cartridge and even worse deviations by the time the sound escapes from the loudspeakers.

Even then, we are not finished. If the little woman insists on foot-deep rugs and wall-to-wall drapes, or if your pad is scoured to its functional austerity. man, you will need same trimming of the ideally flat response to compensate for-in the first case, the premature absorption of treble, and in the second. the 'hardness' of the sound. Tone controls may be regarded as necessary evil, but as long as we are obliged to have them, let's make sure they do not detract from the best possible performance. And in so many commercial designs, they do.

First steps

Before delving into the tone control circuit as a whole, we must take a look at the effect of the passive components with a change in frequency. Back in the days when Poppa bought his radiogram because it sounded 'mellow', the tone control was simply a network of passive components, usually across the output stage, with variation of the resistive part of a series capacitor-resistor shunt that drained away progressively more and more of the upper frequencies. It was, in other words, a variable treblecut device. One or two more enterprising makers

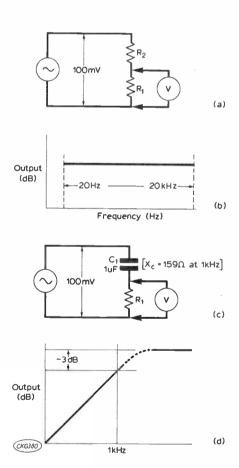


Fig. 74: (a) For a simple resistive network the output shown by the voltmeter is in proportion of the ratio of the resistors to the applied input voltage. In (b) theoretically, the output should not change with frequency, giving a "straight-line" graph. (c) Substituting a capacitor for R2 makes the output frequency dependent while (d) shows an example of the curve we might expect from a simple network such as (c) having a "slope" of 6dB per octave.

fitted alternative resistor-capacitor combinations in the grid circuit of output valves, and others even went so far as to label these Bass or Treble Boost and Cut, but all such passive networks, i.e., those which do not have inbuilt amplification, must attenuate the overall signal.

The point about the passive tone controls is that the attenuation varies the frequency. Take the case of a simple resistive network, as in Fig. 74(a). If we have two resistors of equal value, fed by a signal generator, the output across the measured one will be half the input signal in amplitude, but will not change in frequency. A graph of the situation would be a straight line, as Fig. 74(b).

But if we now substitute the upper resistor with a capacitor, C1 in Fig. 74(c), we find that the measured output will be exactly half the input at

only one frequency. Reactance $X_c = \frac{1}{2\pi f C}$ where X_c

is in ohms, C in farads and f is the frequency an which the test is made, in hertz.

Working out the reactance of a $1\mu F$ capacitor at

1kHz, we get
$$\frac{10^6}{6.28 \times 1000 \times 1} = 159$$
 ohms.

But if we now measure the voltage across a similar-value resistor, we find that instead of half the signal input, we have slightly more. Instead of our attenuator dropping the output by 6dB (to half voltage) at 1kHz, it will have dropped the output only 3dB. This is because the voltage across the capacitor is 90° out of phase with the voltage across the resistor. The output voltage ratio is 0.707:1, not 0.5:1. In fact, if we alter the frequency of the generator, we will find that the measured output drops as the frequency falls. The rate of 'slope', as shown in Fig. 74(d), is 6dB per octave, an octave being a frequency change of 2:1.

This 3dB drop has a further significance when we tackle power output stages, for if the drive voltage to the amplifier fell sufficiently for the power output to drop 3dB, this would be the well-known 'half-power-point'. This is the figure normally quoted in amplifier specifications—a point to which we shall return later. Below this —3dB point in Fig. 74(d), the slope of the curve falls away regularly by 6dB per octave, i.e., a ratio of 2:1, a reduction of output by a half each time the frequency is halved.

Making it active

It helps to regard tone control as a method of frequency correction. The introductory remarks we have made, and references to frequency-dependent

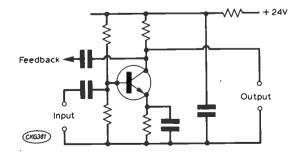


Fig. 75: A collector-follower amplifier arranged so that its output can be measured with and without feedback.

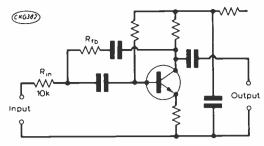


Fig. 76. The basic circuit used for tests.

feed-back in previous articles, should have prepared the regular reader for this approach. Simple tone controls are types of filters. We shall deal thoroughly with filter circuitry later, but at the moment it is necessary to observe that the 'filter' of Fig. 74(c), for example, is called a 'first order filter', having a 'slope' of 6dB per octave. Second order filters have slopes of 12dB/octave and third-order filters, 18dB/octave. As we shall see, real filters, used in well-designed audio amplifiers, should ideally have a third-order slope to be effective.

These filters are passive devices. They contain no amplifying stage or stages to put back the signal attenuated by their action. If we make a marriage of the virtual earth circuitry we talked about in Parts 12 and 13 of this series and the fundamentals of tone control circuitry touched upon in Part 11, we get an amplifier with frequency-dependent feedback, which becomes, if we correctly design it, a better tone control circuit.

First, we need what is known as an 'inverting amplifier'. If you take a look at Fig. 75, you will see that this can be a collector-follower circuit, so arranged that we can measure its gain with or without the feedback. In practice, this is a useful circuit, and the component calculation will be discussed as we go along. It is convenient to use the 24-volt supply described in Part 13, December PW. Fig. 76 shows the circuit devised by Mike and used for tests on the prototype.

With an input from the audio generator, and an output measured with a millivoltmeter, we can measure the open-loop gain. This is the gain of the amplifier with no feedback connected. Here, a word of warning is required: in many erudite theoretical articles, 'open-loop gain' is bandied about freely, but an inspection of the circuit will often show that it would be virtually impossible to measure it in practice. Our aim in this case is to show what we mean by the term, then, by applying the feedback we need, to modify the gain and achieve our controlled response, i.e., effect a tone control.

In our prototype, the open-loop gain, (G₀) was 260. It is absolutely essential when carrying out these measurements to mount the circuit in a screened box, use screened input and output leads and make sure our construction is 'solid'. We use Veroboard for convenience: it allows connection of additional components while retaining the versatility of wired circuitry. We use the very convenient Norman Rose aluminium boxes, because they are inexpensive, easily worked for outlet holes, tag-strip mountings, etc., and have a simple lid which not only completes the screening but also affords an easy access for modifications.

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	3-10
50V, D.C. 40	
	8-10
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100µA, £8:40 15V. A.C £	3-10
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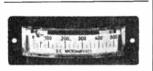
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50-0-50µA £2.85	20V. D.C 22 20		
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100mA £2-20	5 amp. A.C. * #2-20		
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1 amp £2.20	20 amp. A.C. * #2-20		
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Type MR.6	5P. 31	in. x 3‡in. fro	nts
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ImA	£2-40	150V. A.C .	£2 55
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	42 40	VU Meter	
	£2-40	50mA A.C. *	£2 40
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	£2-40		£2-40
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	500-0-500gaA #1		300V, D.C.	£1.75
	1mA £1	.75	500 V. D.C	£1 75
ĺ	1-0-1m \ £1	75	750V. D.C.	£1 75
	2mA #1	-75	15V, A.C	
í	5ta A £1	.75	50V. A.C	£1 85
		-75	150V. A.C	
	20mA . £1	75	300 V. A.C	
	50mA . £1	75	5001'. A.C	
	100mA £1	75	8 Meter ImA	£1.8 ₅
Į	150mA £1	75	VU Meter	£2 30
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50-0-50; A	£2-30	10V. D.C £1 85		
100µA	£2:30	20V. D.C #1-85		
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STREET, SQUARE,	in all	150V. D.C.	42	15
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Completely portable, simple
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50K/Vol. D.C. 5K/Volt A.C.
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1-5/9/ AMP, AC,
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Full capabilities for measuring A, B and ICO. NPN or PNP. Equally adaptable for check-ing diodes. Supplied complete with instructions, battery and



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5 mc/s Pass Band, Separate



5 mc/s Pass Band, Separate YI and Y2 amplifiers. Rectangular 5in. x 4in. C.R.T. Calibrated triggered aweep from 2 u/sec. to 100 milli-sec. per cm. Free running time base 50 c/s-1 mc/s. Built-in time base calibrator and amplitude calibrator. Supplied complete with all accessories and instruction manual 487, Carr. Paid.

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Size 180 × 90 × 90mm.
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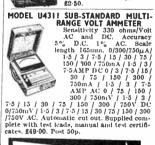
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1-5-1-500v. Resistance up
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Complete with probe and
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150-400 Kc/n. 550 Kc/n-30 Mc/n. FET front end. 2 mech. filters product datactor variable

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band ing 550 Ke/s, to 30 Me/s, con-

80 Mc/s. continuous and wo metres. 8 valve plus 7 diede circuit. 4/8 ohm output and phone jack, 8811-CW. NNL. Variable BFO. 8 meter. Nep. bandspread dial. 17 frequency 455 Kc/s. audio output 1-5w. Variable BF and AF gain controls 116/250°, AC. 87:e: 7 × 13 × 10° with instruction manual. £49 80. Carr. Paid.



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can be panel or bench mounted. Basic meter measures 1 voit D.C. but can be used to measure a wide range of AC and DC voit, current and ohms with optional plug in cards. Specification: Accuracy: ± 0.2, ±1 digit. Resolution: Inv. Number of digits: 3 plus fourth overrange digit. Overrange: 1009, (up to 1:939). Input impelsance: 1000 Meg ohm. Measuring cycle: 1 per second. Adjustment: Automatic zeroing, full scale adjustment against an internated reference voltage. Overload: to 100v. D.C. Input: Fully floating (3 poles). Input power, 110-230v. AC. 50/60 cycles. Overall size: 5½m. × 2 13/16½m. × 3 3/16½m. AVAILABLE BRAND NEW AND FULLY GUARANTEED. \$35-50. Carr. 50p.



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Simply plug in intero-phone, guitar, etc., and output into your amplifier.
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Integrated preamps (output 125 mV) to feed into any stereo amplifier.

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PL12D PL15C

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GA105 21 GA160 21 GA308 Teak 21 GA308PU Teak

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	2200µF	16p	100/1F	7p	1 / iF	61
	3300µF	24p	150,1F	7p	2 · 2 · 1 F	6,
i			220μF 470μF	9р 12р	4.7µF	61
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	10 VO	LT	1000µF	20p	22 ₁₁ F	6; 6;
ı	22,4F	6р	2200/1F	36p	68,1F	9
	47µF	6p	5000µF	62p	100µF	ló
1	100µF	6p	,		150µF	12
1	220µF	7p			220µF	17
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AC141K	18p	BC147	8p		32p	OC81	13p	1N4148	
AC176	14p	BC148	8p		22p	OC83	20p	1844	9 p
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AC188	12p	BC154	16p	BFY50	19p	T1P30A	58p	18120	15p
AC188K	18p	BC157	12p	BFY51	15p	TIP31A	58p	18121	14p
ACY17	21p	BC158	11p	BFY52	15p	TIP32A	66p		8 p
ACY18	19p	BC159	12p	BFY64	35p	TIP33A	95p	18131	10p
ACY19	23p	BC167	11p	BFY90	65p	TIP34A	-	18132	12p
ACY20	20p	BC168	10p	B8 X 20	17p		1.40		7p
ACY21	21p	BC169	10p	C407	20p	TIP35A		18922	8p
ACY22	16p	BC177	14p	C426	30p		2.30	18923	12p
ACY39	62p	BC179	14p	C428	28p	TIP36A		18940	5р
AD140	36p	BC182L	8p	C450	15p		2.90	AA119	10p
AD142	40p	BC183L	8p	MP8111		TIP41A	72p	AA129	10p
A D143	350	BC184L	8p	MP8112		TU142A	83p	AAZ13	10p
AD149	340	BC186	30p	MP8113	32p	2N706	12p	AAZ15	12 p
AD150	55p	BC515F		MPB121		2N930	21p	AAZ17	12 p
A D161	27p	BC213L		MP8122		2N1131	20p	BA100	15p
AD162	27p	BC214L	10p	MP8123	45p	2N1132	25p	BA102	22 ł p
AD M/P		BC258	8p	NKT211	25p	2N1613	20p	BA115	7 t p
AF114	14p	BC259	8p	NKT212		2N1711	24p	BA144	124p
AF115	14p	BC267	12p	NKT214	23p	2N2904	36p	BA145	20p
	14p	BC268	13p	NKT217		2N2904/		BA154	12}p
AF117	14p	BC300	36p	NK T261			40p	BAX13	12 p
AP118	82p	BC301	29p	NKT271		2N2905	42p	BAX16	12 p
AF124	24p	BC302	26p	NKT274		2N2924	16p	BAY18	17 p
	36p	BC303	45p	NKT275		2N 2926	9p	BAY31	71p
	37p	BC304	35p	NKT403		2N3053	24p	BY100	
ALIOO	68p	BCY70	15p	NKT405		2N 3054	50p	BY126	15p
AL102	60p	BCY71	33p	NKY603		2N3055	48p	BY127	174p
AL103	49p	BCY72	15p		60p	2N 3405	40p	BYX10	
A8Y26	27p	BD123	60p	NKT613		2N3663	52p	OA5	17 p
A8Y27	36p	BD130	45p		30p	2N3702	8p		
AU103	90p	BD131	62p	NKT674		2N3703	8p	OA9	10p
	97p	BD132	81p	NKT677	G	2N3704	8p	OA10	221p
AUIIL	67p	BD135	38p		22p	2N3705	8p	0A47	8p
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BC108	8p	BD141 £		NKT773		2N3707	8p		70
BC109	8p	BD142	45p	OC19	50p	2N3708	8p	OA73	10p
	14p	BF159	30p	OC20	50p	2N3709	8p	OA79	7p
BC116	15p	BF173	26p	OC23	30p	2N3710	8p	OA81	8p
	15p	BF177	25p	OC25	25p	2N3711	8p	OA85	10p
BC126	22p	BF178	26p	OC28	30p	2N3794	15p		
BC132	14p	BF179	32p	OC29	30p	2N3819	25p	OA90	7p
BC134	14p	BF194	14p	OC35	25p	40361	45p	OA91	7p
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ALL COMPONENTS CAN BE BOUGHT SEPAR-ATELY, SEND 50p FOR LATEST CATALOGUE, WHICH INCLUDES SPECIALIZED COMPONENTS, HI-FI EQUIPMENT AND ELECTRICAL HOUSE-

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1	1R5	-28	30C17	-76			EM80	-36		-68		.75
ı	185	-22	30C18	-72	EB91	-12		-36	PCL82	-30	UABC80	-81
ı	1T4	-16	30 P5	-64	EBC33	-40	EM84	-32	PCL83	-55	UAP42	-50
ı	384	-26	30FL1	-65	EBC41	-49	EM87	-50	PCL84	-88	UBC41	-45
ı	3V4	-47	30FL12	-69	EBC81	-80	EY51	-36	PCL85	-38	UBF80	-84
ı	5U4G	-81	30FL14	-68	EBC90	-22	RY86	-29	PCL86	-37	UBF89	-88
ļ	5V4G	-85	30L1	-89	EBF80	-32	EY87	-29	PCL88	-80	UCC84	-88
ı	5 Y3GT	-80	30L15	-70	EBF83	-89	EZ40	-89	PCL800	-89	UCC85	-85
1	5Z4G	-35	30L17	-70	EBF89	-29	EZ41	-39	PCL805	-38	UCF80	-80
ı	6/30L2	-54	30P4	-65	ECC81	-17	KZ80	-21	PENA4	•77	UCH42	-58
ı	6AM6	-13	30P12	-69	ECC82	-20	EZ81	-22	PEN36C	•70	UCH81	-80
ı	6AQ5	-22	30P19	-65	ECC83		EZ90	-25		-51	UCL82	-88
ı	6AT6	.20	30PL1	-60	ECC85	-84	GZ30	-84		-48	UCL83	-55
ı	6AU6	-20	30PL13	-89	ECC804	-54	GZ32	-40	PL81	-43	UP41	-52
Į	6LA6	-20	30PL14	-80	ECF80	-30	KT41	-77	PL81A	-47	UF89	-80
ı	6BE6	-21	35 L6GT	-45	ECP82	-26	KT61	-55	PL82	-31	UL41	-68
ı	6BJ6	-41	35W4	-25	ECH35	.55	KT66	-78	PL83	-88	UL84	-80
ı	6BW7	-50	35Z4GT	-25	ECH42	-59	LN319	-68	PL84	-80	UM84	·21
ı	6F14	-35	50CD6G	-68	ECH81	-29	LN329	-80	PL500	-68	UY41	-39
1	6F23	-68	807	-49	ECH83	-38	LN339	-65	PL504	-68	UY85	·25
1	6F25	-50	AC/VP2	•77	ECH84	-35	N78	£1.05	PM84	-30	VP4B	•77
ı	6J5GT	-20	B349	.70	ECL80	-80	P61	-40	PX 25	-95	W77	-48
ı	6J7G	-24	B729	-54	ECL82	-29	PABC		P¥32	- 52	Z77	-23
ı	6K7G	-12	CCH35	-67	ECL86	-35	PC86	-47	PY33	-52	Translat	ors_
ı	6K8G	-36	CY3t	-28	EF39	-88	PC88	-47	PY81	-25	AC107	.17
ı	6Q7G	- 35	DAF91	-22	EF41	-67	PC96	-42	PY82	-25	AC127	-18
ı	68L7(1T	-88	DAF96	-36	EF80	-23	PC97	-38		-26	AD146	-87
ı	68N7GT	-32	DF91	-16	EF85	-28	PC900	-29	PY88	-88	AP115	-20
ı	6 A Q (1	-28	DP96	-36	EF86	-80	PCC84	-29	PY800	-81	AP116	.20
ı	6V6GT	-28	DH77	-20	EF89	-26	PCC85	-28	PY801	-81	AP117	.20
ı	6X4	-83	DK32	-33	EF91	-13	PCC88	-88	R19	-80	AF125	.17
J	6X5GT	-28	DK91	-28	EF92	-27	PCC89	-43	R20	•70	AF127	-17
ı	10P13	-58	DK92	-50	EF98	-65	PCC18		U25	.73	OC26	-25
1	12AT7	-17	DK96	-45	EF183	-27	PCC80		1726	-65	OC44	-13
1	12AU7	-20	DL35	-40	EF184	-29	PCF80		U47 U49	·78	OC45 OC71	·18
ı	12AX7	-22	DL92	-26	EH90	-86	PCF82				OC72	-13
1	19BG6G	-75	DL94	-47	EL33	-55	PCF86		U52	-31	OC75	-13
1	20F2	-67	DL96	-38	EL34	-48	PCF80		U78	·24	0C/b 0C81	-13
Į	20P3	-75	DYS6	-24	EL41	-54	PCF80	1 .28	U191 U193	-88	0C81 0C81D	-13
1	25L6GT	-19	DY87	-24	EL84	-28	PCF80	2 .89	U251	-81	0C81D	-13
1	25U4GT	-57			EL90	-28	PCF80		U201	-88	OC82D	-13
1	30C1	-26	DY802	-83	RL95	-88			U301 U329		OC170	-23
1	30C15	-58	EABC80	-32	EL500	-62	PCF80	0 -96	0.529	.00	00170	.50

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Minimum post/packing on 1 valve 7p., on each additional valve,
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SUPERSOUND 13 HI-FI MONO AMPLIFIER

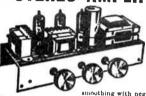


componenta throughout. allicon transistors plus 2 power out-put translators in push-pull. Full wave rectifica-tion. Output

r.m.a. into 8 ohm. Frequency response 12Hz—36Hz ± 34b. Fully integrated pre-amplifier stage with separate Volume, Bass boost and Treble cut controls. Suitable for 8-10 ohm speakers. Input for ceramic or crystalc cartridge. Sensitivity approx. 40mV for full output. Supplied ready built and teated, with knobs, escutcheon panel, input and output plugs. Overall size 3° high x 6° wide x 7½° deep. AC 200/2804. approx. 13 watts

PRICE \$10.50, P. & P. 25p.

DE LUXE STEREO AMPLIFIER



A.C. mains 200-240 v. Using heavyduty heavy duty fully isola-ted mains transform-er with full wave reetl-fication giving ade-

amosthing with negligible hum.

A ua te e

amosthing with negligible hum.

as rectifier. Two duai poteptioneters are provided for

bass and treble control, giving bass and treble boost and
edigit hand channels can be adjusted by means of a separate. Balance control fitted at the rear of the chassis.

Input sensitivity is approximately 3000ty for full peak
output of 4 watts per channel (8 watts mono), into 3 ohm
speakers. Pill negative feedback in a carefully calculated
circuit, allows high volume levels to be used with negligible
distortion. Supplied complete with knobs, chassis size

11"w x 4"d. Overall height including valves 5". Ready
built & tested to a night standard. PRIOF 58.09 P x P 450. built & tested to a nigh standard. PRICE 48-92 P. & P. 45p

POWER SUPPLY UNIT 200/240v. A.C. Input. Four awitched fully amoothed D.C. outputs giving 6v. and 74v. and 9v. and 12v. at 1 amp continuous (1 amp intermittent).

intermittent), Filted insulated output terminals and pilot lamp indicator. Hammer finish metal case overall size 6 × 31 × 21 . Suitable for Translator Radios, Tape Recorders, Amplifers etc. etc. Ready PRICE £4.50 p. & p. 35p. built and leated.

BLACK ABODISED 16g. ALUMINIUM HEAT SINKS. For TO3, complete with mica's and bushes. Size 2% × 3° approx. 25p pair. P. & P. 5p.

HIGH GRADE COPPER LAMINATE BOARDS $8'' \times 6''$ 5 for 50p P. and p. 13p.

BRAND NEW MULTI-RATIO MAINS TRANSPORMERS. Giving 13 alternatives. Primary: 0-210-240v. Secondary combinations 0-5-10-15-20-26-30-35-40-60v. half wave at 1 amp. or 10-0-10, 20-0-20, 30-0-30v. at 2 amps full wave. Size 3in. long × 3jin. wide × 3jin. wide × 3in. long × 3jin. wide × 3jin. long × 3jin.

MAIRS TRANSFORMER, For transistor power supplies, Pri 200/240v, Sec. 9-0-9 at 500m A, 85p. P. & P. 13p. Pri. 200/240v, Sec. 12-0-12 at 1 amp. 85p. P. & P 13p. Pri. 200/240v, Sec. 10-0-10 at 2 amp. £1-45. P. & P 3.0p. SPECIAL OFFER MAINS TRANSFORMER 200/240v. A.C. Input 35v at 1½ amp A.C. output overall size 2½* × 2½* × 3* approx. Suitable drop through or vertical mounting 90p, P. & P. 30p.

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GENERAL PURPOSE HIGH STABILITY
TRANSISTOR PRE-AMPLIFIER
For P.U. Tape, Mike, Guitar, etc. and suitable for
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response 15Hz—25KHz. Gain 26dB. Solid encapsulation size 1½ x 1½ x ½. Hrand new complete
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Prices in this advertisement (incl. p. and p.) will be subject to VAT as from 1st April, 1973.

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LATEST B.S.R. C109/C129 4-SPEED AUTOCHARGER.

With latest mono compatible cartridge 26:97 Carr. 50p.

With stereo cartridge 27-97 Carr. 50p.

GARRARD 8P25 Mk III with heavy precision machined die cast turntable \$10.95, carr. 50p.

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PRECISION EMGINEERED PLINTHS
Beautifully constructed in heavy gauge "Colorcoat"
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142" x 34" high (approx. 7½" high, including rigid
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LATEST ACOS GP91/ISC mono compatible cartridge with t/o stylus for LP/EP/78. Universal mounting bracket. t/o stylus for LP 21-50 P. & P. 8p.

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ONLY 22-50 P. & P. 10p. Also available fitted with twin Diamond T/O stylus for Stereo L.P. 23. P. & P. 10p.

LATEST RONETTE T/O STEREO/COMPATIBLE CARTRIDGE for EP/LP/Stereo/78. 21.63 P. & P. 10p. LATEST RONETTE T/O MONO COMPATIBLE CART-RIDGE for playing EP/LP/78 mono or stereo records on mono equipment. Only \$1.50 P. & P. 10p.

QUALITY RECORD PLAYER AMPLIFIER MK II A top quality record player amplifier employing heavy duty double wound mains transformer, ECCS3, ELS4, and rectifier, Separate Bass, Treble and Volume controls. Corapiete with output transformer matched for 3 ohm speaker, Size 710, while × 31n, deep × 61n, high, Ready built and tested, PRICE \$2.95 P. & P. 40p ALSO AVAILABLE mounted on board with output transformer and speaker ready to 8t into eabinet below. PRICE \$5.95 P. & P. 50p.

DELUXE QUALITY PORTABLE R/P CABINET MK II. DELIGIAL QUALITY FORTABLE BIF GABIRET MA II. Uncut motor board size 14½ x 121n, clearance 21n, below, 5½in, above, Will take above amplifier and any B.S.R. of GARRARD changer or Single Player (except AT60 and 8P25). Size 18 x 15 x 8in, PRICE 24-75, P. & P. 50p.

SPECIAL OFFER! HI-FI LOUDSPEAKER SYSTEMS

Beautifully made teak finish enclosure with most attractive Tygan-Vynair front. Size 16\(\frac{1}{2}\) high x 10\(\frac{1}{2}\) wide x 5\(\frac{1}{2}\) deep. Fitted with E.M.I. Ceramic Magnet 13\(^2\) x 8\(^3\) bass unit, two H.F. tweeter units and crossover. Power handling 10 watts. Available 3 or 8 or 15 ohis impordance. 8 or 15 ohms impedance

OUR PRICE £8.40 Carr. 65p

Cabinet Available Separately 24-50 Carr 60p Also available in 8 ohms with EMI 13" x 8" speaker with parasitic tweeter 26-50 Carr. 65p

LOUDSPEAKER BARGAINS
5in. 3 ohm £1-05, P. & P. 15p. 7x 4in. 3 ohm £1-15, P. & P.
20p. 10 × 6in. 3 or 15 ohm £1-90, P & P. 30p. E.M.I.
8 × 5in. 3 ohm with high flux magnet £1-62, P. & P. 20p E. M.I. 13½ × 8in. with high flux ceramic magnet with parasitic tweeter 3, 8 or 15 ohm £3.20, P. & P. 30p. H.M.I. 13 × 8in. 3, 8 or 15 ohm with two inbuilt tweeters and crossover network £4.20, P. & P. 30p.

BRAND NEW. 12ln. 15w. H/D Speakers, 3 or 15 ohms. Current production by well-known British maker. Now with Hilliux ceramic ferrobar magnet assembly £6.75, Guitar models: 25w. £6.75, 35w. £3.50, P. & P. 35p



SPECIAL OPPED

LIMITED NUMBER OF BRAND NEW ELAC 10' TWIN CONE LOUDSPEAKERS

With large ceramic magnet and plasticised cone aurround.

8 ohm impedance. 22.75, P. & P. 25p.

12in. "RA" TWIN (ONE LOUDSPEAKER, 10 watta peak handling, 3, 8 or 15 ohm \$2:20, P. & P. 30p, 35 ohm SPEAKERS 3in. only 63p P. & P. 13p.

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"POLY PLANAR" WAFER-TYPE, WIDE RANGE
ELECTRO-DYNAMIC SPEARER
Size 11f" x 14f" x 1 4f" deep. Weight 19oz. Power
handling 20W r.m.s. (40W peak), Impedance 8 ohm only.
Reaponse 40Hz-20kHz. (an be mounted on cellings,
walls, doors, under tables, /tc., and used with or without
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P. & P. 25p.

VYNAIR & REXINESPEAKERS & CABINET FABRICS app. 54 in. wide. Usually £1.75 yd., our price 75p yd. length. P. & P. 15p per yd (min 1 yd.) S.A.E. for samples.

HI-FI STEREO HEADPHONES

Adjustable headband with comfortable flexifoam ear-muffs. Wired and fitted with standard stereo [in jack plug. Frequency response 30-15.000Hz. Matching impedance 8-16 ohns. Easily converted for Mono. PRICE 22-95, P. & P. 15p.

HARVERSONIC SUPER SOUND 10 + 10 STEREO AMPLIFIER KIT



NEW FURTHER IMPROVED MODEL WITH HIGHER OUTPUT AND INCORPORATING HIGH QUALITY READY DRILLED FIBER CLASS PRINTED CIRCUIT BOARD WITH COMPONENT IDENTIFICATION CLEARLY MARKED FOR EVEN EASIER CONSTRUCTION

EASIER CONSTRUCTION

A really first-class Hi-F1 Stereo Amplifier Kit. Uses 14 transistors including Silleon Transistors in the first five stages on each channel resulting in even lower noise level with improved sensitivity. Integrated pre-amp with Hasa, Treble and two Volume Controls. Suitable for use with Ceramic or Crystal cartridge—instructions included. Output stage for any speakers from 5 to 15 ohms. Compact design, all parts supplied including drilled metal work, high quality ready drilled fibreglass printed circuit board, smart brushed anodised aluminium front panel with matching knob, wire, solder, nuts, bolts—no extraato buy. Simple step by step instructions enable any constructor to build an amplifier to be proud of. Birtel specification; Power output: 14 watts r.m.s. per channel into 5 ohms. Frequency response 4 3dis 12-30.000 itz Sensitivity; better than Som Into 1M Ω. Full power bandwidth: 4-2dis 12-15,000 itz. Bass board approx. to + 12dis. Technical Solution of the production of the stage of the stage

AMPLIFIER KIT ... £10.50 P. & P. 15p

(Post Free if all units purchased at same time)
Full after sales service

lso available ready built and tested £21-00, Post Free. Note: The above amplifier is suitable for feeding two mono sources into inputs (e.g. mile, radio, twin record decks, etc.) and will then provide mixing and fading facilities for medium powered Hi Fi Discotheque uss, etc.



3-VALVE AUDIO AMPLIPIER HA34 MK II. Designed for Hi-Fi reproduc-tion of records, A.C. Mains operation. Ready built on operation. Ready built on plated heavy gauge metal chassis, size 7½° w. × 4° d. × 4½° h. Incorporates ECUS3, ELS4, EZ80 valves. Heavy duty, double wound mains transformer and output transformer matched for 3 ohm

former matched for 3 shim apeaker, Separate volume control and now with improved wide range tone controls giving bass and treble lift and eut. Negative feedback line. Output 4½ watts. Front panel can be detached and leads extended for remote mounting of controls. Complete with knobs, valves, etc., wired and tested for only £4.95, P. & P. 35p. HSL "FOUR" AMPLIFIER KIT. Bunllar in appearance to HA34 above but employs entirely different and advanced circuitry. Complete set of parts, etc. £4.10. P. & P. 40p.

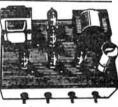
HARVERSON'S SUPER MONO AMPLIFIER

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A super quality grain amplifier using a double wound fully isolated mains transformer, rectifier and ECL82 triode pentode vaive as audio amplifier and power output stage. Impedance 3 ohms. Output approx. 3.5 watts. Volume and tone controls. Chassis size only 7in. wide x 3in, deep x 6in, high overall. AC mains 200/240v. Supplied absolutely Brand New completely wired and tested with good quality output transformer.

P. & P. 35p BARGAIN PRICE £2.95 BARGAIN PRICE £2.95

10/14 WATT HI-FI AMPLIFIER KIT

A stylishly finished monaural amplifier with an output of 14 watts from 2 EL84s in push-pull. F.1.548 in push-pull.
Super reproduction
of both music and
speech, with negligible hum. Separate
inputs for mike and
grain allow records
and announcements
to follow each other to follow each other.



to follow each other.

Pully shrouled section would output transformer to match 3-15 Ω speaker and 2 independent volume controls, and separate base and treble controls are provided giving good lift and cut. Valve line-up 2 ELR4s, ECC83, EF86 and EE80 rectifier Simple instruction booklet EF86 and EZ80 rectifier Simple instruction booklet 13p (Free with parts). All parts sold separately, ONLY 27-97 P. & P. 55p. Also available ready built and tested £10-97 P. & P. 60p.

HIGH IMPEDANCE CRYSTAL STICK MIKES. OUR PRICE 21-05, P. & P. 8p

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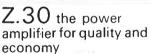
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Sinclair Project 60

Now-the Z.50 Mk.2

with built-in automatic transient overload protection

When originally introduced, the Sinclair Z 50 proved now it was possible to design and produce a popularly priced modular power amplifier having characteristics to challenge the world's costliest amplifiers. Many thousands of Z.50's are now giving excellent service day in, day out. But we have also learned that constructors do not always use their Z.50's ideally. That is why we have introduced modifications whereby risk of damage through mis-use is greatly reduced and performance further enhanced. The Z 50 Mk 2 has improved thermal stability, more accurately regulated D.C. limiting to ensure more symetrical output voltage swing and clipping and still less distortion at lower power. Z.50 Mk, 2 is compatible with all other Project 60 modules, and may be incorporated to advantage in existing systems. Eleven silicon epitaxial planar transistors are now used, two more than in the original Z 50. circuitry has been re-designed making this versatile high performance amplifier better than ever.





with free manual

The Z 30 provides excellent facilities for the constructor requiring a high fidelity audio system of less power than that available from Z 50 s. Using a power supply of 35 volts. Z 30 will deliver 15 watts RMS into 8 ohms, or 20 watts RMS into 3 ohms using 30 volts. Total harmonic distortion is a fantastically low 0.02% at 15 watts into 8 ohms with signal to noise ratio better than 70 dB unweighted. Input sensitivity. 250mV into 100K ohms. Size 80 x 57 x 13 mm (3\frac{1}{8} x 2\frac{1}{8} x \frac{1}{8}) Z 30, Z 50 and Z 50 MK 2 modules are compatible and interchangeable.

Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, you money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sinclair Radionics Ltd.

Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defect arise in normal use, we will service it at once and without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically £1.00) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.

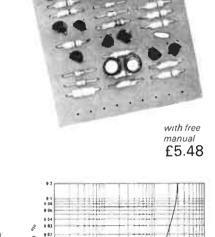


Brilliant new technical specifications

(50v 15Q speakers only)

Input impedance 100 K Ω Input (for 30w into 8 Ω) 400mV Signal to noise ratio, referred to full o/p at 30v HT 80dB or better Distortion 0.02% up to 20W at 8 Ω . See curve Frequency response 10Hz to more than 200 KHz \pm 1dB Max. supply voltage 45v (4 Ω to 8 Ω speakers)

Min. supply voltage 9v Load impedance — minimum: 4Ω at 45v HT Load impedance — maximum: safe on open



Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc	£4.48
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control, etc.	£9.45
12W, RMS continuous sine wave stereo amp-for average needs	2 x Z.30s, Stereo 60; PZ.5	Crystal, ceramic or mag P U , F M. Tuner, etc.	£23.90
25W RMS continuous sine wave stereo amp using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60; PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier (60W RMS into 8 ohms)	2 x Z.50s, Stereo 60; PZ.8, mains transformer	As above	£34.88
Indoor P.A	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43

the world's most advanced high fidelity modules

Stereo 60 Pre-amp/control unit



Designed specifically for use on Project 60 systems, the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxial planar transistors are used throughout, a really high signal-to-noise ratio and excellent tracking between channels is achieved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly

SPECIFICATIONS—Input sensitivities: Rallo up to 3ml. Mag pu 3mV correct to RIAA curve 1dB 20 to 25 000 Hz Ceran pu up to 3ml. Aux - up to 3ml. Output: 250mV Signal to noise ratio: better than 70 dB Channel matching: within 1dB Tone controls: TREBLE 12 to -12dB at 10KHz BASS 12 to —12dB at 100Hz Front panel: brushed aluminium with black knobs and controls Size: 66 x 40 x 207mm,

B. It. lested and quaranteed

£9.98

Project 60 Stereo F.M. Tuner



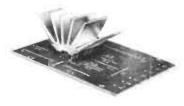
The phase lock loop principle was used for receiving signals from space craft because of its vasily improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit coils, an ŁC in the specially designed stero decoder and switchable squelch circuit for silent tuning between stations. In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems

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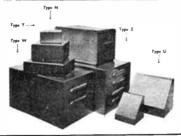
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OA2 0.40	6AR8 0.65	6F5 0.75	7Y4 0.75	Flora A One	alles E	ully Guar	beetee	EF97	0.65	GZ33 0.75	PFL2000.6		0.70
OA3 0.48	6AR11 1.25	6F6G 0.45	9BW6 0.70	First Qu	ality r	uny duai	aillean		0.75	GZ34 0.60	PL33 0.4	0 U404	0.70
OB2 0.40	6A85 0,50	6F11 0.50	10C2 0.60			_			0.80	HABC800.55	PL36 0.5	5 U801	0.80
OB3 0.70	6A87G 0.65	6F13 0.50	10D1 0.65		COLUMN 2007	1977			0.35	11K90 0.50	PL81 0.5		80
OC3 0.40	6AT6 0.38	6F14 0.70	10D2 0.55		ASSESS SIL					KT66 2.85	PL82 0.4		0.40
	6AU6 0.30	6F15 0.65	10F1 0.75		IC II II II	o eu			1.25				
OD3 0.40		6F18 0.50	10F9 0.65		9 11 11 11 11 11 11	4		EK90	0.82	KT88 2.25			
1B3GT 0.45		6F23 0.90	10F18 0.60	1/4		M BRA	IND	EL34	0.50	N78 1.60	PL84 0.4		
11.4 0.25	6AW8A 0.65		101.1 0.60	//	200			EL36	0.50	PABC800.40	PL302 0.b		0.65
1R4 0.50	6BA6 0.28	6F24 0.80			aeru			EL37	1.70	PC86 0.60	PL504 0.7		
1R5 0.45	6BE6 0.82	6F25 1.00	10LD110.70					EL41	0.75	PC88 0.60	PL508 0.9		
184 0.80	6BF6 0.55	6F26 0.35	10P13 0.75			10 1/4	LVEC	EL81	0.55	PC92 0.05	PL509 1.1	0 UBP80	
185 0.80	6BH6 0.75	6F28 0.70	12AB5 0.70	FIFC	TRON	IC VA	LAES	EL83	0.50	PC97 0.50	PL801 1.0	0 UBF89	0.40
1T4 0.80	6BJ6 0.55	6GK6 0.60	12 AC6 0.60	FLLO	, ,, ,,	. •		EL84	0.25	PC900 0.48	PL802 0.9	6 UBLI	0.70
104 0.40	6BK7A 0.75	6J4 0.80	12AE8 0.60			1	ECC88 0.40	EL85	0.43	PCC84 0.40	PM84 0.6	0 UBL21	0.70
11/5 0.75	6BN5 0.43	6J5GT 0.40	12 A L5 0.55	30C1 0.30	50L6GT 0.60	DM160 0.88		EL86	0.40	PCX285 0.40	PY31 0.3		0.45
1 V2 0.55	6BN6 0.60	6.16 0.30	12AQ5 0.50	30C15 1.00	85A2 0.55	DY51 0.55	ECC89 0.50			PCC88 0.55	PY33 0.6		
	6RQ5 0.25	6J7 0.45	12AT6 0.40	30C17 1.10	90AG 2.40	DY86 0.35	ECC91 0.30	E1.90	0.42				
1X2B 0.55	6BR8 0.75	6K4/7 0.60	12AT7 0.40	30C18 0.90	90 A V 2.50	DY87 0.36	ECC189 0.65	E1,360		PCC89 0.55	PY80 0.4		
2021 0.40		6K 6GT 0.75	12AU6 0.45	30F5 1.00	9001 0.75	DY802 0.37	ECC807 1.00			PCC189 0.60	1º Y 81 0.3		
3 4 0.45		6K7 0.43	12AU7 0.38	30FL1 0.80	90CY 2.40	E80F 1.10	ECF80 0.35			PCC805 0.95	PY82 0.3		
3 A 5 0.75	6BW6 0.90		12AV6 0.45	30FL12 1.10	807 0.50	E88CC 0.70	ECF82 0.35	ELL80		PCC808 0.95	PY83 0.8		
3BP1 8.50	6BW7 0.90	6K8G 0.45	12AV7 0.70	30FL14 0.90	813 4.00	E180F 1.00	ECF8041.65	EM34	1.00	PCF80 0.80	PY88 0.4		
384 0,40	6BX6 0.25	6K25 0.75		30L1 0.40	866A 0.65	E810F 2-90	ECH42 0.75	EM71	0.80	PCF82 0.85	PY800 0.4		
3 V 4 0.65	6BZ6 0.45	6L6GT 0.55	12AX7 0.38		5642 0.70	EABC800.38	ECH81 0.80	EM80	0.45	PCF84 0.60	PY801 0.5	0 UCL83	
5R4GY 0.75	6C4 0.35	6L7 0.45	12AY7 0.75	30L15 0.95	6080 1.75	EAF42 0.60	ECH83 0.45	EM81	0.60	PCF86 0.60	PZ30 0.8		0.65
5U4G 0.40	6C5GT 0.55	6L18 0.50	12B4A 0.65	30L17 0.95		EBC33 0.60	ECH84 0.45	EM83	0.50	PCF87 1-10	QQVO2-6	UF11	0.60
5 V 4 G 0.50	6CB6 0.40	6LD20 0.50	12BA6 0.45	30P12 1.00	6146 1.60	EBC41 0.65	ECL80 0.50	EM84	0.35	PCF801 0.50	2.5	25 UF41	0.65
5Y3GT 0.45	6CD6GA	6N7GT 0.55	12BA7 0.50	30P19 0.95	6146B 2.50		ECL81 0.50	EM85	1.00	PCF802 0.50	QQV03-10	UF42	0.65
523 0.75	1.80	6P28 0.65	12BE6 0.50	30PL1 0.95	6360 1.25	EBC81 0.83	ECL82 0.35	EM87	0.70	PCF805 0.90	1.8		0.65
5Z40 0.45	6CG7 0.80	607 0.50	12BH7 0.50	30PL13 1.10	6939 2.25	EBF80 0.40		EN91	0.40	PCF806 0.75	QQV03-20		6.35
6/30L2 0.90	6CH6 0.80	68A7 0.45	12BY7 0.65	30PL14 1.25	7199 0.85	EBF83 0.40	ECL83 0.70			PCF808 0.90	5.8		0.40
6AB4 0.45	6CL6 0.60	68(17 0.45	12K5 1-00	35 A 3 0.60	7586 1.50	EBF89 0.32	ECL84 0.55	EY51	0.40		TT21 3.4		0.40
8AF4A 0.60	6CU6 0:80	68K7 0.50	12K7GT0.50	35 A5 0.75	7895 1.50	EBL31 1-50	ECL85 0.55	EY80	0.75	PCH2000.70	TT22 3.5		0.65
	6CW4 0.70	68L7GT0.45	1207GT0.45	35B5 0.65	A 2293 2-20	EC53 0.50	ECL86 0.40	EY81	0.40	PCL81 0.50			0.48
6AG5 0.25		68N7GT0.45	128 R7 0.50	35C5 0.60	AZ1 0.60	EC86 0.60	EF37A 1.00	EY83	0.55	PCL82 0.85	U18/20 0.7		0.30
6AG7 0.45	6CY5 0.50	68Q7 0.50	20D1 0.60	35 D5 0.75	AZ31 0.55	EC88 0.60	EF40 0.50	EY86	0.40	PCL83 0.65	U25 0.8		
6AII6 0.60	6CY7 0.75	68R7 0.50	201.1 1.10	35L6GT0.75	CBL1 0.90	EC90 0.35		EY87	0.48	PCL84 0.45	U26 0.6		
6AJ8 0.30	6D3 0.55		20P1 0.50	35 W4 0.40	CBL31 1.00	EC92 0.45	EF41 0.65	EY88	0.43	PCL86 0.45	U31 0.7		1.00
6AK5 0.40	6DC6 0.80	6T8 0.38		35Z3 0.75	CY1 0.50	EC93 0.60	EF42 0.70	EZ40	0.50	PCL88 1.25	U37 8.6	50 UY41	0.48
6AK6 0.80	6DK6 0.80	6U4GT 0.70	20P4 1.10	35Z4G 0.40	CY31 0.50	ECC35 1.00	EF80 0.30	EZ41	0.75	PCL200 0.75	U52 0.4	40 UY82	0.50
6AL3 0.48	6DQ6B 0.75	6U5G 0.75	20P5 1.20		DAF96 0.50		EF85 0.85	EZ80	0.28	PCL800 1.10	U76 0.4	10 UY85	0.40
6AL5 0.22	6DS4 1.25	6U8A 0.48	25C5 0.60	35Z5GT0.70		ECC40 0.70		EZ81	0.29		U78 0.4		0.75
6AM5 0.40	6EA8 0.65	6V6GT 0.45	25L6GT 0.50	50 A5 0.80	DF96 0.50	ECC81 0.40	EF86 0.80	GTIC	3.00	PCL801 0.95	U191 0.3	75 17129	
6AM6 0.87	6EH7 0.30	6X4 0.40	25Z4G 0.85	50B5 0.70	DK92 0.70	ECC82 0.83	EF89 0.28	GY501		PCL805 0.50	U201 0.4	50 153	0-75
6AQ5 0.42	6EJ7 0.35	6X5GT 0.45	25Z6GT0.75	50C5 0.80	DK96 0.60	ECC83 0.33	EF91 0.37	GZ30	0.45	PD500 1.80	U281 0.		8.00
6AQ6 0.70	6EW6 0.70	6 X 8 0.65	30A5 0.60	50CD6G1.20	DL96 0.55					PF88 0.70	U282 0.		1.35
6AR5 0.55	6F1 0.75	6 Y 6G 0.80	30 A E 3 0.40	50EH5 0.65	DM70 0.60	ECC84 0.30	EF92 0.85	GZ31	0.40	1 7 7 00 0.70	0202 0.	, 2000 C	
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2N697	0.	.15		132	0.8		BD12	4	0.60	
2N698	0.	.80	AC	153	0.2	ō	BD13	i	0.75	
2N705		.70		154	0.1	2	BD13		0.80	
2N706		.10		157 169	0.1	á	BFII	5	0.20)
2N708 2N753	Ų.	.15	AC	176	0.1	ž	BF16		0.18	
2N929	0	20	AC	187	0.2	5	BF17		0.20	
2N930	0.	.20	AC	188	0.2	5	BF18		0.30	
2N997	0.	.80	AC	Y17	9.0	5	BF18	1	0.30)
2N113	1 0	.25	AC	Y18 Y19	0.2	6	BF18		0.20)
2N113	2 0	25 25		Y20	0.2		BF18		0.20	
2N118 2N130		.17		Y21	0.2		BF19 BF19		0.14	
2N130	3 0	.17		Y22	0.1		BFIS		0.15	
2N130	4 0	.20		140	0.5	0	BFIS		0.15	ē
2N130	15 0	.20	ΑŢ	149	0.4	5	BF20		0.8	5
2N130		.25	ΛI	161 162	0.8	15	BFW		0.2	
2N130 2N130	9 0	.25		Z11	1.2		BFW	88	0.20	
2N130	9 0	.25	AL	Z12	1.2	5	BFW	01	0.20	
2N 161	3 0	.17		114	0,1	17	BFX	86	0.2	Ď
2N171	1 0	.20		115	0.1	2	BFY	17	0.4	0
2N175	6 0	.75		116	0.1	4	BFY		0.2	5
2N214 2N216	17 0	60		118	0.3	30	BFY		0.2	
2N221		.25	Al	125	0.9	0.5	BFY		0.2	ň
2N221	18 0	.20	AI	127	0.5	90	BSY	26	0,1	7
2N221		.20	Al	180	0.3	35	BSY	27	0.1	5
2N236		.15		186	0.4	10	BSY		0.1	7
2N247 2N264	16 0	,40		239	0.3	36	BSY	65 05 A	0.2	9
2N290		.25	Al	Z11	0.4	45	OCI	sau S	0.5	Ď
2N292	23 0	1.12		Z12	1.4	00	OC2	2	0.5	0
2N292	24 0	.13		Y26 Y27	0.1		OC23	3	0.6	0
2 N 292 2 N 305	76 (0.10		Y28	0.1		OC2	4	0.6	ō
2N305	54 0	.50		Y29	0.		0C2	6	0.3	a K
2N30	55 (0.60	- A8	3Y54	0.9	DΚ	OC2	8	0.5	
2N313	33 (25.0		3Z15	0. 0. 0.	70	OC2	9	0.6	0
2N31	34 (.25		3Z16 3Z17	٧.	70	OC3	5	0.5	
2N331	91 (0.17	A	Z18	0.	75	OC3	6	0.4	5
2N33	93 (0.15		3Z20	0.	25	0C4	4	0.2	5
2N33	94 (1.15		3Z21	0.		OC4	5	0.1	2
2N33	95 (0.20		JYIO		00	OC7		0.1	0
2N34	U2 (n. 10	B	2107	0.	10	OC7		0.1	2
2N34		0.15 0.32	R	C108	0.	10	OC7		0.1	2
2N34		0.20	B	C113	Ö.	10	0C7	3	0.3	5
2N34	15 (0.15	B	C118	0.3	20	007	ĸ	0.1	5
2N34	17 (0.25		C134	0.	20	0C7	8	0.2	5
2N37	03 (0.10		C147 C148	0.	10	OC7	8D	0.9	0
2N37	03 (0.10 0.12		C149	Ň.	10 12	OC8	1,	0.9	20
2N37	07	0.12	l B	C152	ő.	15	OC8		0.9	20
2N37	09 (0.10	B	C158	0,	15	oci		0.5	
2N37	10 (0.10		C175	0.	20	OCI	40	0.3	15
2N38	19	0.35		C186		25	OC1	41	0.6	30
2N39 2S70		0.25	B	CY30 CY31		25 30	OC1	70	0.1	
2874	ŝ	0.50		CY31	ů.	25	0C1 0C2	41	0.1	30
ACII	3	0.25 0.15	l ß	CY34		30	0C2	01	0.6	
AC12	5	0.30	B	CY72	0.	.15	OC2	02	0.0	85
AC12	:6	0.20		CZ10		30	OC2	03	0.4	0.2
AC12	7	0.17	ī B	CZ11	0.	40	OC2	04	0.4	10











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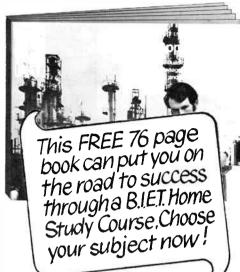
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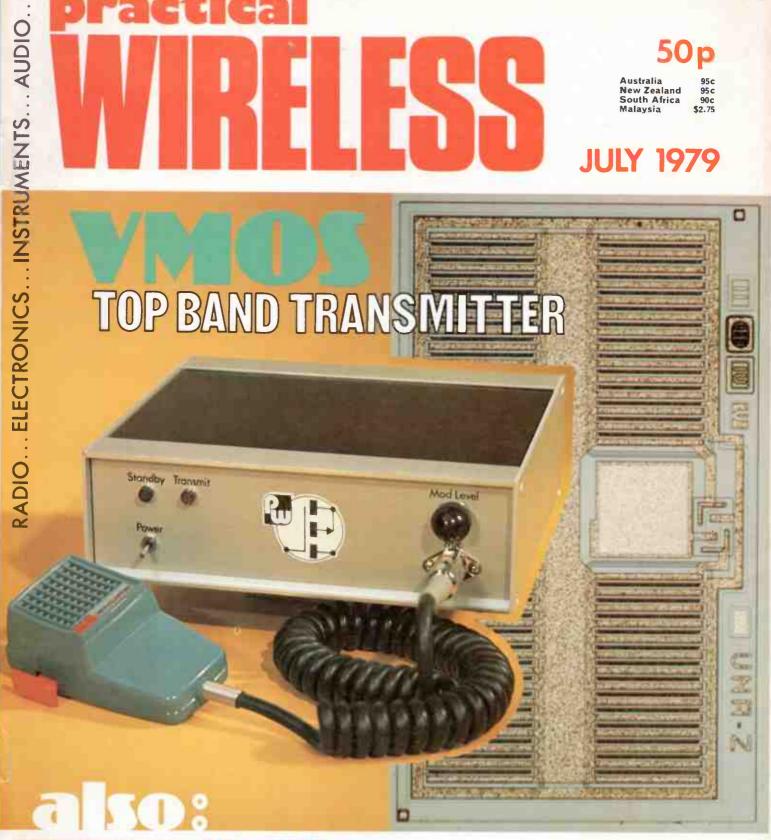
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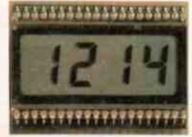
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w	e regret that Part 2 of the PW ''Trent'' has had to be held over, due to production difficulties

OUR COVER

The object looking rather like a ventilation grille is in fact a much-enlarged view of the "works" of a power f.e.t. Photograph courtesy Siliconix Ltd.

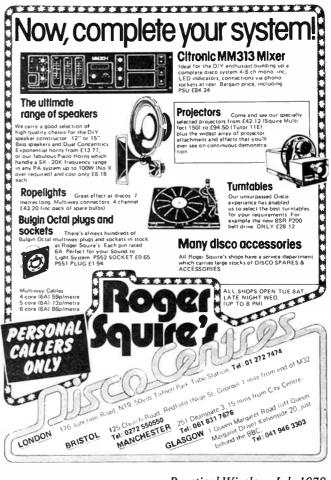
Our August issue will be published on 6 July (for details see page 43)



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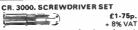
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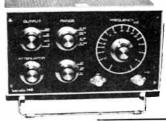
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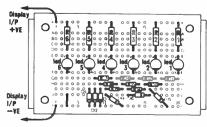
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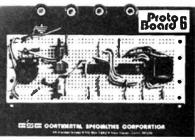
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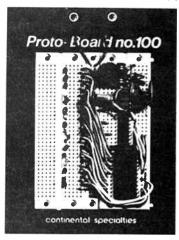
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ı	4021	82p	4082	20p	4556	77;
1	4022	90p	4085	82p	4557	3866
1	4023	17p	4086	82p	4558	117;
1	4024	76p	4089	150p	4559	388
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000	LIDE	4527	15/
1063	109p	4528	102
1066	53p	4529	141
067	400p	4530	90
068	25p	4531	141
069	20p	4532	125
070	20p	4534	614
071	20p	4536	380
072	20p	4538	150
073	20p	4539	110
075	20p	4541	141
076	90p	4543	174
077	200	4549	399
078	20p	4553	440
081	20p	4554	153
082	20p	4556	771
085	82p	4557	386
086	82p	4558	117
089	150p	4559	388
093	50p	4560	218
094	190p	4561	65
096	105p	4562	530
097	372p	4566	159
098	110p	4568	281
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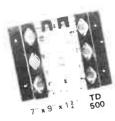
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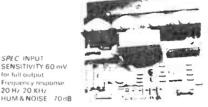
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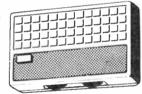
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ı	CA3018	£0.76	SLB12C	€2.75	SN76008KE	€1.05	TAA521	£1.18	TAA930B	CLAS
ı	CA3018A	£1.10	SL620C	£3.85	SN76013N	£2.04	TAA522	€1.85	TBA120	€0.60
į	CA3020	€2.20	SL621C	€3.75	SN76013ND	£1.72	TAA550	€8.48	TBA331	€0.90
ı	CA3020A	£2.50	SL623C	€8.25	SN76018KE	£1.90	TAA611B	£2 30	TBA341	£0 95
į	CA3021	€2.40	SL63DC	£2.50	SN760234	£2.05	TAA621	€2 50	TBA395	€1.80
ı	CA3022	£2.20	SUB4DC	£4.40	SN76023ND	£1.72	TAA661A	£1.65	TBA396	£1.20
ı	CA3023	£2.20	SL641C	€4.48	SN76033N	(100	TAA661B	£1.45	TBA400	€2.20
ı	CA3026	£0.70	St701C	£2 50	SN76110N	£1.30	TAA790	€1.85	1BA440	£1.88
ı	CA3028A	60.60	CA3086F	£1.87	SN76115N	£1.65				
J	CA3028B	£1.25	CA3069E	£2 90	SN78116N	€1.80		_	1	
Ì	NEW	1979	CATA	LOG	UE					

ACCESS AND BARCLAYCARD.

I	VALVE	S — I	MULLA	RD				
П	QY87/802	£1.17	EL86	£2.43	PCF 200	[2,77]	PL 63	£2.87
- 1	ECC62	€1.38	EL95	£1.71	PCF 201	£2.77	PL 64	£1.78
	ECC83	€1.31	EY86/802	€1.17	PCF801	£1.77	PL 95	£1.48
	ECC84	£1.51	GY501	€2.87	PCF802	£1.77	PL504	£2.50
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il	ECL82	€1.71	PC900	£2.43	PCL84	£1 67	PY800	£1.78
	ECL86	€1.78	PCC8	€1,51	PC186	£1.76	PY88	€1.58
	EF85	€1.17	PCC85	€1.71	PCL805/85	£1.80	PY 500A	€2.48
ŀ	EF183	£1.51	PCC89	€1.75	P0510	€4.40	UCL82	£1.86
-	EF184	£1.82	PCC189	€2.15	PFL 200	£2.25	UCL83	€1.86
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Unusually stable trouble-shooter — for TV, Radio, amp, etc. £5.30.

TINNED COPPER WIRE Available on 2 oz. reels in the following guages:

SWG Price SWG Price SWG Price

18	£0.55	26	£0.60	32	€0.73	
22	£0.55	30	£0.65	36	£0.80	
MULTICORE SOLDER - SAVBIT 1.2mm						

Approx. 13.7 metres of size 12 SAVBIT solder, Ideal for Radio, TV and similar work — £2.28.

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ı	CD4000	£0.20	CD4012	£0.20	CD4021	€1.06	C040318	(2.21
ı	CD4001B	€0.20	CD40138	€0.52	C040228		CD40348	£2.44
ı	CO4002		CD4014	£1.00	CD40238	£0.20	C040358	£1.30
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ı	CD4007		CD4016	£0.62	CD40258	€0.20	CD4040	€1.12
ı	CD4008B		CD4017B	£1.05	C040278	CO 55	CD40418	£0.86
ı	CD4009	£8.58	CD4916B	£1.05	CD40288	£0.60	CD40428	£0.80
ı	CD4010		C040198	£0.52	CD40298	€1.10	CO4043	€105
ı	CD40118	£0.20	CD40208	£1.15	CD4030	€8.64	C04044	€1.00

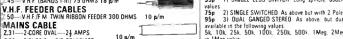
1.30 .55 1.30 1.30 .70 1.25 .86 .85 1.65 1.70 .18 .15 .18 .22 .22 .21 .26 7.41-U.H.F. (BANDS I-V) 75 DHMS 18 n/m

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ARY POTENTIOMETERS. All standard ½" spindles

1) SINGLE LESS SWITCH Long spindle double wiper, available in following

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minimum £10.

TTL (see catalogue for full range)



			_
	30 VOLT	RANGE	
	/240 sec 0-		
Voltages	s available 3,	4, 5, 6, 8,	9, 10,
	18, 20, 24,	30V or 12V	-0-12V
	/-0-15V.		
Ref	Amps	Price	P&P
112	0.5	2.64	0.78
79	10	3.57	0 96
3	2 0	5.77	0 96
20	3 0	6.20	1 14
21	4 0	7.99	1 14
51	5 0	9.87	1 32
117	60	11.17	1 45
88	80	14.95	1 64
89	100	17.25	1 64
90	12 0	19-17	1 95
91	150	21.96	2 08
92	2 0	20.45	O A.

45 VHF (BANDS I-III) 75 0HMS 18 p/m

-FIGURE 8-RIB POLARISED

MAINS CABLE

U A.
33-40-
0, 13,
DV and
P&P
0 78
0.96
1 14
1 32
1 50
1 64
2 08
O.A
O A.

109	12 0	20.50	U.A.
		ORS (SCREE	CT
Ref	VA	Price	P & P
*07	20	4.40	0 79
149	60	6.70	0 96
150	100	7.62	1 14
151	200	11.16	1 14
152	250	13.28	1 50
153	350	16.43	1 84
154	500	20.47	2 15
155	750	29.06	0.A
156	1000	37.20	OA
157	1500	51.38	O A
158	2000	61.81	O.A.
159	3000	86-66	O.A.
		Sec 115 or	
	sec volts req		

		ANSFORM USA flat pir	
VA Cab	Price	P&P	Ref
20	5.95	0 90	56W
75	7.73	1 14	64W
150	10.01	1 14	4W
200	10.92	1 45	65W
250	11.59	1 45	69W
500	19-17	1 64	67W
1 K	27.88	2 30	84W
1.5K	26.02	O.A.	93W
2 K	49.97	O.A.	95W

EX-510CK				
SAME DAY DESPATCH	4			
VAT 8%				

VAT 8%
TRANSFORMERS

END OF LINE OFFERS	226	60	30	
Ref				
30-Isolator 240V:240V 200VA	£4	-54 P	&P£1	04
62-Isolator 240V:240V 250VA	£5	-62 P	&P £1	04
63-Isolator 240V:240V 500VA	£11	-50 P	&P£2	15
6-250-0-250 a 100ma 1) Sec	6 3V	₹ 3 5	A 2) 5	Sec
0-5V, 6 3V > 2/1 amp		£3-20	P& P 7	78p
7-350-0-350V a 100ma 1) Sec 6	-3V = 3	-5A 2)	Sec 0-	5V,
6 3V @ 2/1 amp		£4-10	P&PS	96 p
218-250 0-250V a 150ma 1) 5	Sec 6 3	V = 4A	2) 0-	5V.
C 21/ 2/1		C2 EA	DOD T	700

6 3V = 2/1 amp	£3.50 P&P 78p
27-250-0-250 a 60ma 1) Se	c 6-3V • 2 5A 2) Sec 6 3V
■ 1 amp	£3.00 P&P 78p
220-410-0-410V a 180ma	1) Sec 6 3V = 4 amp CT 2)
Sec 6 3V a 2A 5V a 2 amp	£5.30 P&P 96p
82-4 amp lead acid 8attery C	harger (transformer only)
	£4-81 P&P f 1 04

86-6 amp lead acid 8attery Charger (transformer only)
	£5.80 P&P£1 04
59-0-240V, 25-0-25 a 4A	£6.32 P&P£1 62
M184 - To match EL84 15W	£1-62 P&P 32p
M616 - 0-240V: Screen 1) 13-0-13	14 2) 12V 150ma

	0 2 10 1 10 0 10 0 11 17 10 0 10	
		£2-10 P&P 60p
M489 -	0-240V: 1400V a 150ma, 6	3 3V 4 4A
		£5.50 P&P £1 04
M708 -	6K to 3KΩ matching transfe	ormer 5 watt
		00 000 40

	SUP	P&P	4Up
M679 - 120V x 2; 36V 1 6A	£3.00	P&P	78p
$M865 - 100V$ Line to 4Ω 10 watts	£1.90	P&P	60p
M973 $-$ 100V Line to 8Ω 40 watts	£2.90	P&P	60p
M1015 - Choke 8A = 5 watt 150A	Serge		
	£1.50	P&P	45p

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M1130 - 0-240 4500V a 10ma	£4.86 P&P £1 08
M1165 - 0-115-240V; 14V 50ma	75p P&P 30p
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Pri 220-240 volts				
	4	mps		
ef .	12V	24V	Price	P&P
11	0.5	0 25	2.20	0 45
13	1 0	0.5	2.64	0.78
71	2	1	3.51	0.78
18	4	2	4.03	0 96
85	0.5	2 5	5.00	0 96
70	6	3	6.35	0 96
80	8	4	7.42	1 14
72	10	5	8.12	1 14
16	12	6	8.99	1 32

12 OR 24V OR 12-0-12V

111 213 71 18 85 70 108 72 116 17 115 187 226	0 5 1 0 2 4 0 5 6 8 10 12 16 20 30 60	0 25 0 5 1 2 2 5 3 4 5 6 8 10 15 30	2·20 2·64 3·51 4·03 5·00 6·35 7·42 8·12 8·99 10·72 13·98 17·93 36·74	0 45 0 78 0 78 0 96 0 96 0 96 1 14 1 14 1 32 1 32 2 08 U.C.

ı	65 W Metal Oxide Resistors
ı	65 W Metal Oxide Resistors
	150 Mixed Value Capacitors
	10 Reed Switches
	50 Wire Wound Resistors
	10 3000mf 30V Capacitors
	25 Assorted presets
	50 3 tag terminal strips
	Hardware BA nuts bolts
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	32 mf to 2000 mf.
	70p + 121% VAT
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COMPONENT PACKS

100V 200V 400V 400V 500V PM7A6 1 VAT 123 P &		
AMPLIFIE 10W (AL6 25W (AL6 35W (AL6 125W (AL Power Supply Power Supply VAT 12 P & P 35p	R MOD (0) (0) (0) (250) (PS12 (SPM8)	£3-75 £4-95 £7-79 £18-74 £2-05 £4-25 £6-70

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All accessories available.	
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MINI-MULTIMETER	
DC 1000V AC 1000V DC 100mA Res	
1000Ω/V Bargain £7-20 P&P 62p VAT 8	%

	ohm/V			
Ranges	AC DC to	1000V DC	current to	250mA
Resistar	ice to 3 Mc	hms		
5° x 3	4" x 13" £	14-36 P&P	£1 05 VA	T 8%

Pr.		W RANGE 1				to aive
36	0 36V	48 0 48V 72	V or 92V	P	g P	to give
	Ref 3A	14.70)	1	48	
	4A 5A	18-77 26-64			84 15	
		200	VATE			

	PANELN	IETERS	
43mm -	43mm	82mm -	78mm
	6.20	0 50/A	6.70
0 500MA	5.95	0 500AA	6.70
0 1mA	5.95	O 1mA	6.70
0 30V	5.95	0 30V	6.70
VU ind. Pan	el 48mm •	45mm	3.36
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54mm - 14	mm 250µa	FSD	2.60
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250µA F S		11537	TIP
		LTANI	

Carriage 65p VAT 8%

Send 15p for Catalogue

15V RANGE			
0 C T Ref 171	15V 500 mA	2.09	P&P 0.45
172	1A 2A	2.96 3.59	0 78 0 78
174	3A 4A	3.75 5.73	0 86 0 96 AT 8

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Solderless bread boarding	
S Dec 70 contacts	€3.55
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Home electronic starter Start
simply and progress to a TRF
radio or electronic organ No
soldering All parts included in
presentation box. Full instructions.
£8-29, P & P 96p VAT 8%

ABS	PLAST	C B	OVE	turn. 2
	nuts, inter			
	flush fitti			
	180mm -			6 5 p
PB2	100mm -	75 .	40	73p
	120mm -			
	215mm -			
P & F	29p. VA	T 8 6 (• P &	P 40p)

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15W	3.95
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20 x 20 WATT STEREO AMPLIFIER

Viscount IV unit in teah simulate cabinet. Silver finish rotary controls and pushbuttons with marching fascual red in inits indicator and stereo jack nocket functions switch for inc magnetic and crystal pictuos, fape funer and auxiliary. Rear panel features two mains outlets DIN speaker and injurt sockets plus fuse 20x20 watts RMS 40x40 watts peak for use with 8 to 15 ohm speakers.

£29.90

30x30 WATT AMPLIFIER IN KIT FORM

For the experienced constructor com plete in every detail, same facilities as Viscount IV but with 30x30 output 60x60 watts peak For use with 4 15 ohms speakers





SPECIAL OFFER

30 x 30 WATT AMPLIFIER KIT with BSR P200 belt drive

deck and Shure M75 cartridge.

£55.00 + p&p £5.00

EMI SPEAKER BARGAIN

Stereo pair 350 kit System consists of 13" x 8" approx wooter with rolled surround 2";" approx Audax tweeter crossover components and circuit diagram frequency response 20 Hz to 20 KHz Power handling 15 waits RMS 20 automatics. 20 watts max 8 ohm impedance

£14.95

BSR P200

Belt drive chassis lurntable unit semi £24.95

A D C OLM 30 Mk III Magnetic Cartridge



BSR Planual single play record deck with auto return and cueing lever. Littled with stereo ceramic cartridge 2 speeds with 45 r.p.ni endle adaptor ideally suited from home OUR PRICE £10.95

GARRARD DECK **MODEL CC 10A**

Record changer with cueing device fitted with stereo ceramic cartridge ready to lit into your own plinth

£7.95 pap 12 00 Size 12" x 8"

SANYO Nic/cad battery, with mains charger equivalent in mains charger equivalent size and reptaces 4 SP11 type batts Size 34."x 1%

£7.50 £1 50p





Features 8 watt total output Full size BSR manual turntable with cueing and auto return. Socket for tape in and out and stereo headphones complete with speakers £34.95

Micro Cassette Recorder

Packet size—home or office use or when travelling

£13.95 **Battery operated fluorescent** camping lamp.

Runs off 8 U2 batteries

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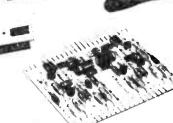
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ACCESSORIES ARE ONLY

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ACCESSORIES

Suitable mains power supply parts consisting of mains transformer bridge rectifier, smoothing capacitor and set of rotary stereo controls for treble bass, volume and balance £2.90

Two Way Speaker Kit Comprising of two 8" x 5" approx 4 ohm bass and two 312" 15 ohm mid fange tweeter with two

per stereo pair plus £1 50 p&p

10 + 10 AMPLIFIER KIT

An opportunity to buy a 10 waits per channel stereo amplifier kit which is suitable for use with a ceramic cartridge. The amplifier utilises proven Mullard modules and is available at a very competitive price. The amplifier kit comes complete with instructions and includes a Mullard tP1183 stereo preamplifier module, two tP3173 power amplifiers with integral heatsinks, a power supply. Zobel networks, front and back mounting panels, a finished fascia panel, all control potentiometers (bass, treble, volume and balance) switches input output and headphone sockets, wire, and an easily assembled wrap around cabinet

to house the finished unit Size approximately

p&p £2 05 £11.95

£5.95

£6.95

£12.95

£2.95

£13.95

£3.50

£1.50

£20.00

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91," x 81," x 4" **BARGAINS FOR PERSONAL SHOPPERS**

LED 5 function men's digital watch stainless steel finish LCD 5 function men's digital watch

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POCKET CALCULATOR With LEO display meniory and percentage key

AM/FM DIGITAL CLOCK RADIO Accurate 4 Digi Electronic Clock with A." display Buzzer and

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125 Watt Power Amp Module

Mains power supply for above unit MULLARD Built power supply

DECCA 20w Stereo speaker kit comprising 2.8" approx. bass units + 2.3A" approx. weeter inc crossovers VIDEOMASTER Super Score TV Game with pistol mains operation

PORTABLE RADIO/CASSETTE RECORDER, AM/ FM with clock LW MW SW VHF mains/battery operation £41.95

VIDEOMASTER COLOUR **SHOT TV GAME**

Choice of three games—Football, Tennis and Squash Ready to play—one or two players MAINS OPERATED OPPO



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ACTON: Mail Order only, No callers ALL PRICES INCLUDE VAT AT 123% All items subject to availability. Price correct at 1/5/79 and subject to change without notice **50 WATT MONO DISCO AMP** £29.95 P&P £2 50

Size approx 134," x 54," x 64

50 watts rms 100 wasts peak output. Big features include two disc inputs, both for ceramic cartridges, tape input and microphone input Level mixing controls fitted with integral push-pull switches. Independent bass and trehle controls and master volume.

70 & 100 WATT **MONO DISCO AMP**

Size appròx 14" x 4" x 10"4" Brushed aluminium

lascra and rotary controls

Five vertical slide controls, master volume,
tape level, mic level, deck level, PLUS INTER DECK FADER for perfect graduated change from record deck No. 1 to

No. 2, or vice versa. Pre-fade level cont-ol-(PFL) lets YOU near next disc before fading it in .VU meter monitors output level. Output 100 watts RMS 200 watts peak.

70 watt 140 watt peak **£57** p&p £4 00 100 watt £65

DUO II SPEAKERS

Attractive teak finish, modern design incorporating 2 separate speaker units - 6" approx wooter and 215" approx tweeter 45 to 1800 Hz Impedance 8 ohms Power 15 watts RMS 20 watts max Per stereo pair

For personal £17.00 callers only.



FOR PERSONAL SHOPPERS ONLY STEREO RADIOGRAM CABINET

Finished in a natural teak veneer with opening top. Easily modified to accommodate stereo equipment of vour choice. Price £10.95

Size approximately 47" x 151/2" x 15"

Personal Shoppers EDGWARE ROAD LONDON W2 Tel: 01-723 8432. 9.30am-5.30pm. Closed all day Thursday ACTON: Mail Order only. No callers GOODS NDT DESPATCHED OUTSIDE UK

Quality audio modules and accessories for

S450

Fitted with phase lock-loop

£26.14 + 440 040



FREQUENCY RANGE	88-108 Mhz
SENSITIVITY	3 0 µV
BANDWIDTH	250 kHz
SPURIOUS REJECTION	50 dB
SELECTIVITY ± 400 kHz	55 dB
AUDIO OUTPUT (22 5 kHz devi-	ation) t00 mV
STEREO SEPARATION	30 dB
SUPPLY REQUIREMENTS	20 to 30V (90mA max)
AERIAL IMPEDANCE	75 ohms
DIMENSIONS	240mm - 110mm - 32mm

The 450 Tuner provides instant programme selection at the touch of a button ensuring accurate tuning of 4 pre-selected stations, any of which may be altered as often as you choose, simply by changing the settings of the pre-sel controls. Features include FET input stage. Vari-Cap diode tuning. Switched AFC LED Stere dicators.

Stereo 30 COMPLETE AUDIO CHASSIS

£21.57 + 660 080



1	OUTPUT POWER	7 Watts RMS
	LOAD IMPEDANCE	8 ohms
	TOTAL HARMONIC DISTORTION	Less than 5% (Typically 3%)
	FREQUENCY RESPONSE	50 Hz to 20 kHz ± 3dBs
	TONE CONTROL RANGE	± 12 dBs at 100Hz and 10kHz
1	SENSITIVITY	190 mV for full output
ı	INPUT IMPEDANCE	1 M ohms
1	TRANSFORMER REQUIREMENTS	22 V.A.C. rated at 1A
	DIMENSIONS (Less controls and panel)	200mm - 130mm - 33mm

The Stereo 30 comprises a complete stereo pre-amplifier, power amplifiers and power supply. This, with only the addition of a transformer or overwind will produce a high quality audio unit suitable for use with a wide range of inputs i.e. high quality ceramic pick-up, stereo tuner, stereo tape deck etc. Simple to install, capable of producing really first class results, this unit is supplied with full instructions, black front panel, knobs, main switch, fuse, and fuse holder and universal mounting brackets.

AL60

AUDIO AMPLIFIER MODULE 25 Watts RMS

£5.27 + 3

-	25 W
Sp pap	

1	OUTPUT POWER	25 Watts RMS
1	SUPPLY	30-50 V
ì	LOAD IMPEDANCE	8-16 ohms
1	TOTAL HARMONIC DISTORTION	Less than 1% (Typically 06%
١	FREQUENCY RESPONSE	20 Hz to 30 kHz < 2 dBs
1	SENSITIVITY	280 mV for full output
-	MAX. HEAT SINK TEMPERATURE	90°C
	DIMENSIONS	103mm - 64mm × 15mm

This high quality audio amplifier module is for use in audio equipment and stereo amplifiers and provides output powers up to 25 RMS with distortion levels below 0.1%

AL80

AUDIO MAMPLIFIER MODULE

£7.92 + 350 060



OUTPUT POWER	35 Watts RMS
SUPPLY	40-60 V
LOAD IMPEDANCE	8-16 ohms
TOTAL HARMONIC DISTORTION	Less than 1% (Typically 06%)
FREQUENCY RESPONSE	20 Hz to 30 kHz × 2 dBs
SENSITIVITY	280 mV for full output
MAX, HEAT SINK TEMPERATURE	90°C
DIMENSIONS	103mm - 64mm - 15mm

The AL80 is similar in design to the AL60 above and is of the same high quality but provides output powers up to 35W with distortion levels below 0.1%

AL250



OUTPUT POWER	125 Watts RMS continuous
OPERATING VOLTAGE	50-80 V
LOADS	4-16 ohms
FREQUENCY RESPONSE	25 Hz 20 kHz measured at 100 Watts
SENSITIVITY FOR 100 WATTS	450 mV
INPUT IMPEDANCE	33 K ohms
TOTAL HARMONIC DISTORTION 50 WATTS into 4 ohms 50 WATTS into 8 ohms	0 1% 0 06%

This unit, designated AL250, is a power amplifier providing an output of up to 125W RMS, Into a 4 ohm load.

AL30A AUDIO AMPLIFIER MODULES

£4.26 + 35p p4p



1	MAXIMUM SUPPLY VOLTAGE	30 V
I	POWER OUTPUT for 2% THD	10 Watts RMS
1	TOTAL HARMONIC DISTORTION	Less than 25%
ı	LOAD IMPEDANCE	8-16 ohms
ı	INPUT IMPEDANCE	100 K ohms
ı	FREQUENCY RESPONSE	50 Hz-25 kHz ± 3 dBs
ı	SENSITIVITY	75 mV for full output
ı	DIMENSIONS	74mm - 63mm - 28mm

These low cost 10 watt modules offer the utmost in reliability and performance, whilst being compact in size.

SPM80 STABILISED POWER SUPPLY £4.95 + 35p p4p



INPUT A.C. VOLTAGE	33-40V
OUTPUT D.C. VOLTAGE	33 V nominal
OUTPUT CURRENT	10 mA-1 5 amps
OVERLOAD CURRENT	1 7 amps approx.
DIMENSIONS	105mm - 63mm - 30mm

FREQUENCY RESPONSE 20 Hz to 20 kHz × 1 dB

TOTAL HARMONIC DISTORTION Less than 1% (Typically 07%)

1. TAPE 2. RADIO TUNER 3. MAGNETIC P.U.

Designed to power two AL60s at 15 Walts per channel simultaneously. Circuit Techniques include full short circuit protection.

EQUALISATION

INPUT OVERLOAD

BASS CONTROL RANGE

TREBLE CONTROL RANGE SIGNAL/NOISE RATIO

PA100 STEREO PRE-AMPLIFIER



110	
£18-05	

DIMENSIONS A top quality stereo pre-amplifier and tone control unit, the PA100 provides a comprehensive solution to the front end requirements of stereo amplifiers or audio units. The six push button selector switch gives a choice of inputs together with two filters for high and low frequencies.

MPA30

MAGNETIC CARTRIDGE PRE-AMPLIFIER



£3.35

Enjoy the quality of a magnetic cartridge with your existing ceramic equipment using the MPA 30 which is a high quality preamplifler enabling magnetic cartridges to be used where facilities exist for the use of ceramic cartridges only. +350 040

SENSITIVITY	3 5 mV for 100 mV output
EQUALISATION	Within ± 1 dB from 20 Hz to 20 kHz
INPUT IMPEDANCE	50 K ohms
SUPPLY	18 to 30 V-re earth
DIMENSIONS	110 - 50 - 25mm (inc DIN socket)

PA12



£8.75 + 350 080

The PA12 Stereo Pre-Amplifler chassis is designed and recommended for use with the AL 20/30 Aution Amplifler Modules, the PS12 power supply and the TS38 Transformer. Features include on/off volume, Balance, Bass and Treble controls. Complete with tape output.

	and fredie controls. Complete	Till tape colpan
	FREQUENCY RESPONSE	20 Hz-20 kHz (-3dB)
	BASS CONTROL	± 12 dB at 60 Hz
	TREBLE CONTROL	± 14 dB at 10 kHz
Ī	INPUT IMPEDANCE	1 Meg. ohm
	INPUT SENSITIVITY	300 mV
Ī	CROSSTALK	60 dB
Ī	SIGNAL/NOISE RATIO	-65 dB
_	OVERLOAD FACTOR	± 20 dB
	TAPE OUTPUT IMPEDANCE	25 K ohms
	DIMENSIONS	152mm > 84mm · 25mm

PS12 POWER SUPPLY MODULE

Power supply for AL20A-30A. PA12, S450 etc. Transformer T538.

input A.C. Voltage 15-20V. Output D.C. Voltage 22 30V approx. (Dependent upon input.) Output Current 800mA maximum. Dimensions 60 x 43 x 26mm



£2.13 + 350 080

BP124 SIREN ALARM

American Police screamer powered from any 12 volt supply into 4 or 8 ohm speaker. Ideal for car burglar alarm freezer break-down, and other security purposes.

ONLY £3.78

5 WATTs -

MA60 HI-FI AMPLIFIER KIT

Build you own top quality amplifier, save yourself pounds. The MA60 kit comprises the following Bl-kits modules, 2 - AL60 amps, 1 × PA100 pre-amp, 1 - SPM80 stab. power susply; 1 × BM180 trans1, giving 15 watts RMS per channel STEREO. All modules covered by the Bl-PAK satisfaction or money back guarantee. Details of the above modules are in this ad.

Price £36-00 + 62p p&p.

TC60 KIT

A beautifully designed genuine TEAK WOOD veneered cabinet to put the professional touches to your home built amplifler. Full set of parts incl. Front & Back Panels, Knobs, Chassis, Fuses, Sockets, Noen, etc. Ideal for the MA60. Size: 425mm - 290mm >

TRANSFORMERS

T538 For use with S.450 AL30A MPA30
Order No. 2836
T2050 For use with Stereo 30
Order No. 2836
MT80 For use with AL60 SPM80
Order No. 2835
Price:£3.68 + 55pp&p.
BMT250 For use with AL250
Order No. 2835
Price:£7.14 + £1.10p&p.
2040 For use with AL60 2040. For use with AL60 Order No. 2040 Price: £5,85 + 800 p&p. 2041. For use with AL80, AL120 and AL250 Order No. 2041. Price: £7-6 Price: £7-65 + 86pp&p.

CASES
TEAK 30, 32 x 23 x 8cm, designed mainly for use with our stereo 30 Audio System but has proved very helpful to home constructors. Fitted with solid uncut front and back, 0/n 139, £6-89, p8p 70p.

TEAK 60, 42 \times 29 \times 9cm, for use with AL60/MK60 Audio Kit, Useful for the home constructor requiring an amplifier sleeve – has no front or back panel, o/n 140. £7-87, p8p B5p.

+ 40p p&p

100 mV/100 K ohms } For an 100 mV/100 K ohms } output 3 5 mV/50 K ohms 250 mV

± 15 dBs at 75 Hz

10-20 dBs at 15 kHz

Better than 65 dBs (All inputs)

Better than 26 dBs (All inputs)

300 · 90 · 33mm (less controls)

Professionals and Enthusiasts from BI-PAK

AL120

AMPLIFIER heat sink and short-circuit

£12.91

+ P. & P. 35p



OUTPUT POWER	50 Watts R.M.S.
SUPPLY	70 Watts
LOAD IMPEDANCE	B-16 ohms
TOTAL HARMONIC DISTORTION	05% Max. (Typically 02%)
FREQUENCY RESPONSE 1 1dB	25Hz-20kHz
SENSITIVITY	500mV
MAX HEAT SINK TEMP.	45 deg C
DIMENSIONS	192 x B9 x 49 mm

Introduced to fulfill the demand for a fully protected power amp, capable of driving high quality speaker systems at up to 50w with distortion levels below 05%. Ideal for domestic use, Discos, P.A. systems, electronic organs etc. The generously rated com ponents ensure continuous operation at high output levels

SPM120 STABILISED POWER SUPPLIES

SPW120/45 SMP120/55 SMP120/65



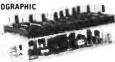
AC INPUTS		
SPM120 45	40-4Bv	
SPM120/55	50-U5v	
SPM120/65	60-65v	
OUTPUT CURRENT	2.5A	
RIPPLE	1A 100mV	
	2A 150mV	

SPM120 is a fixed voltage stabiliser available with an or 9061 1/0 ge of either 45v, 55v, or 65v. Designed primarily for use in audio applications, the stabiliser which provides output currents up to 2.5A., operates direct from a mains transformer requiring only the addition of 2 Electrolytic capacitors to complete the s/c protection.

GE100 Mk2.

10 CHANNEL MONOGRAPHIC EQUALISER

£22.50 + P. & P. 35p



Control Range	±12dB	
Dynamic Range	110dB	
Maximum Output	+ 15dB	-
Frequency Response	30Hz-20KHz (±1dB)	
Power Supply	15 0-15v	
Voltage Handling Input	3v R.M.S	
T H.O.	005%	

Only 155mm x 65mm x 50mm including the 10 x 10K 1in slider potentiometers and knobs which are mounted on a board positioned above the circuitry. In the frequency range of 31Hz to 20KHz you can cut and boost ±12dB with the 10 sliders each of which has its frequency marked on the circuit board. The GE100 has numerous uses including mixers PA systems and discost it will also greatly improve the sound reproduction of your existing audio equipment. Power Supply for GE100 o/d SG30 E3 B0

VPS30 REGULATED VARIABLE STABILISED POWER SUPPLY



AC Input Maximum	25v	
Voltage Regulation	2-30v	
Regulated Current	0-2A	

This NEW versatile Regulated Variable Stabilised Power Supply with short circuit protection and current limiting is a must for all electronics enthusiasts. It incorporates adjustable voltage from 2v-30v, with a current limiting range of 0-2A. With this module there is no need to build a separate power supply for each of your projects, with the simple addition of a transformer (ord 2033). 0-1ma (ord 1310 or 1305), plus a suitable shunt, a voltmeter (ord 1311 or 1306), a 470ohm pot (ord 1896), a 4K7 pot (ord 1899), it can be used again and again as a self-contained bench, power supply, eliminating the use of batteries and thus saving

PA200

PRE-AMPLIFIER



£16.55
+12}% V.A.T.

FREQUENCY RESPONSE TOTAL HARMONIC DISTORTION		20Hz to 20kHz × 1dB Less than 1% (Typically 70%)		
EQUALISATION		Within + 1dB from 20Hz to 20kHz		
BASS CONTRO	DL RANGE	15dBs at 75Hz		
TREBLE CONTROL RANGE		+ 10 20dBs at 15kHz		
SIGNAL NOISE RATIO		Better than 65dBs (All inputs)		
INPUT OVERLOAD		Better than 2dBs (All inputs)		
SUPPLY		35 to 706v		
DIMENSIONS		300 x 90 x 33mm (less controls		

The PA200 is basically our popular PA100. Modifications have been made to make it compatible with the higher output AL120 and

HEADPHONES
A top quality headphone with cushioned earpads and headband. Separate balance/rolume controls. Stereo or Mono switch Impedance 8 ohms. Frequency. 30-18,000Hz. o/n884. £9-78. p&p 70p.

A brilliant compromise between price and performance. Superb stereo reproduction for the newcomer to Hi-Fi. Impedance B ohms. Frequency 30-15.000Hz. o/n BB5. £4-95. p&p 50p.

HI-FI ACCESSORIES

Parallel Tracking GROOV KLEEN
The very latest in automatic record cleaning. Designed to suit all modern single play decks. Simple to fit, it is extremely efficient. Complete with two types of base and three height extensions, o/n 8101, £3-97, p&p.35p.

Cassette Tape Editing Kit

Casante Tape colling NT Enables cassette tapes to be edited and joined easily quickly and accurately. At comprises Tape Spicer F (3 2mm) 2 Precision Tape Cutters Tape Piercer 9 Self-adhesive Labels. Reel of Spicing Tape 3 Winders and removers and instructions, all in a Winders and removers and instructi handy wallet. o/n 811. £2-59. p&p 35p.

GROOV-STAT
The BIB Groov Stat static reducer neutralises the static charge on records and other plastic surfaces o/n8103. £5-89. p&p35p.

Cassette Head Cleaner
Essential for cleaning of tape heads, capstans and rollers Pack contains Tape Head Applicator and tape head polisher tools. Plus bottle of special formula cleaning fluid and full instructions. o/n 832. £0-72. p8p 35p.

METERS

Miniature Balance & Tuning Meter
Miniature moving-coil meter for stereo balance
indicator tuning indicator for FM or similar
application. Pointer at centre indicates zero or null
position. Robust construction. Sensitivity
100.0.100M. Dimensions. 23 x 22 x 26mm
o/n 1318. £2-11. p&p.35p.



Balance and Tuning Meter Clear view edgewise meter. Centre zero application. Sensitivity 100 0 100UA Dimensions. 45 x. 22 x. 34mm. o/n 1319,£2-16.p&p35p.



Miniature Level Meter
Moving coil, for accurate level indication for tape
recorders amplifiers etc Neat design rugged con
struction
will withstand live times rated value
Sensitivity FSD 200UA OdB 130UA Omen
sions: 23 x 22 x 26mm, o/n 1320. £3-02.
p&p35p.



Vu Meter Calibrated 20 to +3 and 0 100%, making it suit able for use as a recording level meter or as a power output indicator. Sensitivity, 130uA Dimensions: 40 x 29mm. o/n 1321. £2-16. p&p35p.



ADAPTORS

AC-DC enables a large range of battery powered radios, recorders, calculators to be run off the mains. (220-240v AC). Switchable for 3-6-9-12 volts. Current rating 300mA. Polarity reversing switch. Universal plug incorporated. o/n 137. £4-05. p&p 35p.

DC-DC for use in all cars, boats etc., with pos. or neg. earth for a regulated output of 6, 7-5 or 9 volts DC at 300mA. For radios, recorders etc. o/n 138.£3-15.p&p35p.

CROSSOVER NETWORKS

2-WAY channels for high and low frequencies to correct speakers – high to tweeters, low to woofers. Complete with instructions. Frequency: 3,000Hz. o/n 1904.£1-24.p&p 35p.

2-WAY for B ohm speakers up to 30 watts. Frequency: .3KHz. o/n 1905.£1-B1.p&p35p.

3-WAY for B ohms speakers up to 30 watts. Frequency: BOOHz and 4.5KHz. o/n 1906. £3-32.p&p35p.

MICROPHONES

DYNAMIC CASSETTE

For equipment requiring a high quality microphone. Sturdy, solid
moulded body in black with neat chrome surround. Pick-up pattern is
omnidirectional. OniOff switch. I metre of tough lead with floating 2.5
and 3.5mm plugs. Matching moulded strut. Impedance: 200 ohms.
Sensitivity. 90dB. Frequency. 90-10.000Hz. Size; 20mm dia. x 120mm, o/n 1326, £1-80, p&p 35p.

DYNAMIC MICROPHONE

DYNAMIC MICROPHONE
Superior quality portable cassette recorder mike with built-in remote control switch and lead fitted with 5-pin 240° DIN plug (remote switch) and 3-pin DIN plug (imcrophone). Provides a direct replacement for those supplied with recorders. With detachable stand. Omnidirectional impedance 200 ohms. Freq response: 100 to 10,000Hz, Sensitivity: 79dB at 1,000Hz, o/n 1327, £2-9B.

PRE - 317: DYNAMIC MICROPHONE
Highly sensitive, high-grade desk or hand mike suitable for use with
many popular cassette decks. Incorporates On/Off switch and 1 metre
lead with moulded standard jack plug. Complete with desk stand.
Omnidirectional Impedance 5,000 ohms. Freq response; 100 at
12,000Hz. Sensitivity: (-7dB at 1,000Hz). o/n 1336. £4-48.
p86,0350.

OMNIDIRECTIONAL CARDIOID

OMNIDIRECTIONAL CARDIOID
Powered by a 1½ battery located within the aluminium body. Satin silver finish with front disk protection to the diaphragm housing. On 0ff switch Also with Busby type windsheld, "U" bracket and stem and extremely supple cable Consumption 0.2mA from 1½ battery providing approx. 8-10,000 hours continuous life. Impedance: 600 ohms. Sensitivity 70dB Frequency 30-16,000Hz, Size: 23mm dia + 267mm. o/n 1329, £14-40, p&p 35p.

UNIDIRECTIONAL CARDIOID
Dual imp 600 and 50,000 ohms Response 50 to 14,000Hz.
Sensitivity 54dB at 50Kiohms Size 1½" dia x 6½" long Weight approx., 190gm. o/n 1328. £12-32. p&p 35p.

STANDS

GOOSENECK CHROME FLEXIBLE HOLDERS Length 320mm. o/n 1333.£2-70. p&p 35p. Length 515mm. o/n 1334.£3-83. p&p 35p.

ELIOOR STAND Heavy chrome. Stow-away feet with rubber ends for maximum stability. Draws to a height of 5' maximum. o/n 1335. + £10-69.p&p.B5p.

BOOM ARM for use with the above stand. Heavy chromed metal, it gives 30" reachfrom the stand. o/n 1337.£10-35.p&p70p.

WINDSHIELD COVERS

n 1331 Medium per pair £1-35, p&p 35p, o/n 1332 Large rpair£2-03.p&p35p.

AUDIO LEADS

107	FM Indoor Ribbon Aerial 3 5mm Jack plug to 3 5mm jack plug Length 1 5m	£0-68 £0-84
114	5 pin DIN plug to 3 5mm, Jack connected to pins 3&5. Length 1.5m	£0.95
115	5 pin DIN plug to 3 5mm. Jack connected to pins 1&4 Length 1.5m	
116	Car aerial extension. Screened insulated	£0.96
117	lead. Fitted plug & skt. AC mains connecting lead for cassette.	£1-24
	recorders & radios 2 metres	£0.76
118	5 pin DIN phono plug to stereo headphone jack socket	£1-18
119	2 + 2 pin DIN plugs to stereo jack socket	20
	with attenuation network for stereo headphones. Length 0.2m	£1-01
120	Car stereo connector Variable geometry	
	plug to fit most car cassette, 8 track cartridge & combination units, Supplied	
	with inline fused power lead and instructions.	£0.68
123	6 6m Coiled Guitar Lead Mono Jack Plug	***
124	to Mono Jack Plug BLACK 3 pin DIN plug to 3 pin DIN plug, Length 1.5m	£1-62 £0-84
125	5 pin DIN plug to 5 pin QIN plug Length 1.5m	£0.84
126	5 pm DIN plug to Tinned open end Length 1.5m	£0.84
127	5 pin DIN plug to 4 Phono Plugs.	
	All colour coded Length 1.5m	£1-46
128	5 pin DIN plug to 5 pin DIN socket. Length 1.5m	£0.90
129	5 pin DIN plug to 5 pin DIN plug mirror image Length 1 5m	£1-18
130	2 pin DIN plug to 2 pin OIN inline socket Length 5m	£0.76
131	5 pin DIN plug to 3 pin DIN plug 184	
	and 3&5 Length 1 5m	£0.93
132	2 pin DIN plug to 2 pin DIN socket Length 10m	£1.10
133	5 pin DIN plug to 2 phono plugs.	
134	Connected pins 3&5. Length 1.5m 5 pin DIN plug to 2 phono sockets	£0.84
134	Connected pins 3&5 Length 23cm	£0.76
135	5 pin DIN socket to 2 phono plugs.	LU-70
	Connected pins 3&5 Length 23cm	£0.76
136	Coiled stereo headphone extension lead.	
1.20	Black Length 6m	£1-97
178	AC mains lead for calculators etc	£0.54
	ALL PRICES INCLUDE V.A.T.	

DEPT.PW7, P.O. Box 6, 18 Baldock Street, Ware, Herts.



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LTHOUGH we have, over the years, reviewed quite a number of kits, for items ranging from intruder alarms to ignition systems, it has long been editorial policy that reviews of ready-built equipment were confined to pieces of test equipment which were likely to appeal to the electronics or radio enthusiast. This was considered to be the right approach for a magazine which was aimed principally at constructors.

We have recently been receiving a growing stream of letters from readers, asking for advice and comment on currently-available communications receivers and other radio equipment for the short-wave listener and amateur, and it is to meet this demand that we are now embarking on a series of reviews. You may rest assured, however, that this change in policy does not mean that we shall be devoting less attention to designs for home-constructed equipment.

It is not our intention to carry out any Which-style comparative tests, nor to suggest a "Best Buy". Neither shall we be carrying out full-scale specification testing, in the way that the hi-fi magazines do on tuners, amplifiers and the like. We shall simply try to convey the feel of the equipment as gained from user tests, to give an idea of how good the instruction manual, etc. is, and to say what accessories or options may be available.

In choosing items for review, we have selected what seem to be the most popular, plus any others available within roughly the same price bracket. This month it is the turn of the Yaesu FRG-7 receiver-future plans include several more receivers, transmitters, transceivers, aerials and various pieces of ancillary equipment. We also hope to comment on some professional receivers now available on the second-hand market. We hope that you will find the reviews interesting and useful, and would be glad to receive suggestions for items to include in the future.



Charles Molloy G8BUS—"On the Air" Contributor

Trained as a telecommunications engineer, Charles worked abroad for several years and became an associate member of the IEE. He is now a technical author in electronics.

Interest in the medium waves began when a schoolboy in the mid-1930s. after constructing a receiver for domestic use. He later turned to the short waves after building a one-valve receiver from a design by F. J. Camm in Practical Wireless, and became a regular SWL while living in the Middle East.

Although a holder of a class B amateur licence, appearances on 70cm and 2m are infrequent as the main interest in radio these days is in broadcast band DXing.

Charles collects books on the early days of radio, and enjoys messing about in boats. Other interests include classical music, opera and attending ballet with wife Mary, who is a devotee. He is looking forward to retirement and the opportunity to catch up with a number of outstanding radio projects.

Marshall's Bristol move

Subsequent to the recent publishing of Marshall's 1979 product range catalogue their Bristol retail shop has moved.

From 24 April 1979, the new shop will be in larger premises at 108A Stoke's Croft, Bristol. This new location is approximately 5 minutes walk from the main shopping centre of Bristol.

At the same time they announce that they have been appointed sole specialist distributors to the constructor market for the new Mullard Teletext chips—SAA 5000, 5010, 5012, 5020, 5030, 5040 and 5050. These will be available shortly.

Further information from: Mardata, Kingsgate House, Kingsgate Place, London NW6 4TA. Tel: 01-624 0805.

Conferences

An IERE/RSGB colloquium is to be held on Tuesday, 5 June 1979 starting at 2 pm at The Royal Institution, Albemarle Street, London W1.

The subject for discussion will be amateur work on microwave propogation and techniques over the last five years, which have made the professionals look hard.

There has been some fascinating work, particularly in the UK, e.g. "s.s.b. at 10GHz" and the colloquium will describe these great developments which are currently going on.

Further details from: The Conference Secretariat, IERE, 99 Gower Street, London WC1. Tel: 01-388 3071.

The programme for the Consumer Electronics Symposium, announced by the Society of Electronic and Radio Technicians (SERT) last autumn, has now been finalised, and is to be held at the University of Essex between 8 and 10 July 1979.

Copies of the programme/registration form are being widely distributed and applications from nearly 100 potential delegates have already been received.

As can be seen from the programme, there is a wide representation of authors from industry, broadcasting authorities and servicing organisations who are providing an extremely varied programme of lectures and discussion covering all aspects of electronics in the consumer field.

Further details from: SERT, Faraday House, 8–10 Charing Cross Road, London WC2H OHP. Tel: 01-240 1152.

Club News

The North England Radio Club has a national and European membership, with the heart of the club on Merseyside.

They publish a monthly magazine called 'Spectrum' and meet monthly, usually at The Sports Centre, Grange Road West, Birkenhead.

New members from anywhere in the world would be very welcome. A copy of 'Spectrum' and club information may be obtained for two $9\frac{1}{2}p$ stamps, in the UK, or two IRC's from abroad.

The man to contact is: Norman Monti, 66 Chesnut Grove, Birkenhead, Merseyside L42 OMZ.

TI 9900 data book

A self-teaching microprocessor design manual—written for beginners and experts alike—is now available from Texas Instruments.

The soft-cover "9900 Family Systems Design and Data Book", will offer in more than 1000 pages a comprehensive selection of educational and applications information that can help users develop a deeper understanding of the complex technology and tremendous potential available in microprocessors.

Combining hardware and software information, the data book should assist both the engineer doing advanced m.p.u. design work and "interested" people who simply want to know more about the subject. It is a complete reference book containing the basic knowledge and data a novice might need to become better acquainted with m.p.u.s.—and it carries that knowledge through into complete technical and systems design data needed to use TI's 9900 family of 16-bit microprocessor and microcomputer circuit boards.

The "9900 Family Systems Design and Data Book" costs £8.00 plus P&P, and is available from: *The Modern Book Co., 19–21 Praed Street, London.*

SERT

The Society of Electronics and Radio Technicians is pleased to announce that Mr T. Bryce McCrirrick has become a Vice-President of the Society.

Mr McCrirrick has recently been appointed Director of Engineering to the British Broadcasting Corporation in

succession to Sir James Redmond.

The current President of SERT is Air Vice Marshal Alec Morris and the other Vice-Presidents are Mr Michael Clark (Deputy Group Chairman of the Plessey Company) and Sir Edward Fennessey.

Rally Dates

The Royal Naval Amateur Radio Society's Mobile Rally, will take place at HMS Mercury, Petersfield, Hampshire, on Sunday, 17 June 1979. It will be open to the general public between 1000 and 1700 hours.

The rally is intended as an outing for the whole family, with stands, arena events and displays of interest to all ages. There will also be the usual trade stands.

Further details from: Wally Walker G4DIU, 9 Woodstock Road, Bedhampton, Havant, Hants PO9 3HX.

The "East Suffolk Wireless Revival" Amateur Radio Mobile Rally will take place on Sunday, 3 June, 1979, at the I.A.C.S.S.A. Sports ground, Bucklesham, near Ipswich. Commencing at 1100hrs and admission will be 40p, which includes a free raffle ticket.

In addition to talk-in stations on 2m, 70cm f.m. and 80m s.s.b., there will be trade stands, technical displays (featuring Prestel, RTTY and m.p.u.s), refreshments and a licensed bar.

Further details from: C. P. Ranson G8LBS, 67 Tranmere Grove, Ipswich, Suffolk IP1 6DU.

"Nunsfield House Community Association Amateur Radio Group" of Derby, hold their 10th Rally, at Elvaston Castle Country Park, on Sunday, 10 June 1979.

It is expected to be their largest rally yet, with over 50 trade stands, along with many other attractions of interest to all the family.

Talk-in stations will be available on callsign GB2ECR, on 2m f.m. Ch. 22, and 70cm f.m. Ch.s SU8, SU20.

Further details from: Chris Wallace G8PTW, QTHR. Tel: Derby 752358.

"Bangor & District Amateur Radio Society" hold their mobile rally on 24 June 1979, at the Castlewellan Forest Park. There will be all the usual events including trade stands and a "bring and buy" stall.

Further details from: W. H. Langtry GI4AMM, QTHR. Tel: Bangor 65394.

OM/FM. Frequency readout

William POEL

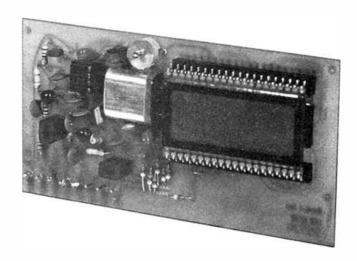
If you can think of an application for an arrangement of c.m.o.s. logic with a potential sale of a million plus, then the chances are that some enterprising manufacturer of l.s.i. has got a dedicated chip either on the drawing board, or in the market place. The application described here is an ideal candidate, since it is yet another instance of age-old analogue technology being swept aside with digital technology. For a long time past, an accurate readout of a radio receiver's tuned frequency has only been available with large amounts of logic, and large amounts of patience to work out the various i.f. offset programming steps. Such systems have also cost considerably more than the best analogue arrangements, and have consequently been restricted to the very expensive exotica in both consumer and communications applications.

Just as Intersil have revolutionised the concept of the instrument type counter with their ICM7216, OKI Electric of Japan have introduced a family of c.m.o.s. for consumer and communications digital frequency readouts which render all other approaches now quite simply obsolete. For in a 40-pin l.s.i. the counter gives both a.m. and f.m. frequency readout, plus straight kHz frequency count (no offset); drives an l.c.d. directly with no r.f.i. to the radio in question and all this with a current consumption of 4mA with the prescaler off, or 15mA with it on. The unit described here is conceived and designed as a universal readout for long wave through medium wave to a maximum a.m. count of 2.999MHz, including the popular marine DF band where digital readout is almost essential for reasonable operation in congested waters. The f.m. range operates from about 20MHz to 200MHz (with SP8629 prescaler) with a resolution of 100kHz—e.g. a typical readout is 88·1MHz. In the direct mode, the display shows kHz from the a.m. input, and 100s of kHz from the prescaled input.

Purists will complain that 100kHz is insufficient for f.m. resolution—but the display flicker brought about by further resolution is very tedious, and the small number of stations not on 100kHz channels makes the exercise rather pointless for the nuisance involved. And not many f.m. receivers would show up too well from the point of view of oscillator drift.

The Circuit

The full circuit (Fig. 1) reveals a remarkably simple overall approach compared to previous endeavours to produce this type of unit. Nearly all functions are carried



on within the MSM5526 i.c.—and the few remaining peripheral components are included as an extra for maximum flexibility. On f.m. the divide-by-100 prescaler is an obvious essential, but the input sensitivity of both the SP8629 and the MSM5526 is such that, if the unit is wired into many receivers directly, the pre-amps are not required. However, with these pre-amps using the high f BF274 type of transistor, typical sensitivities of 800μV on a.m. and 10-15mV on f.m. can be achieved—thus permitting connection of the digital display with the barest minimum of coupling. In the case of one portable radio tried by the author, it is sufficient simply to couple in via a single-ended wire loosely draped around the relevant oscillator section for either a.m. or f.m. So, even if your set doesn't possess specific local oscillator drive, a small piece of wire poked into the oscillator section will work in almost all applications.

The SP8629 has a very useful 6.3V Zener on-chip, permitting a simple but adequate 5.5V stabiliser stage to be built with an external pass transistor. The National Semiconductor equivalent DS8629 does not incorporate this facility, and a separate external Zener must be used. The stabiliser stage has an 82Ω resistor in the output—and this is the result of a mistake when assembling the prototype, since 8.2Ω should have been used. However, the whole circuit worked perfectly when switched on—and it was only when a check was made on the current drain, that this error was discovered, since the unit took a sur-

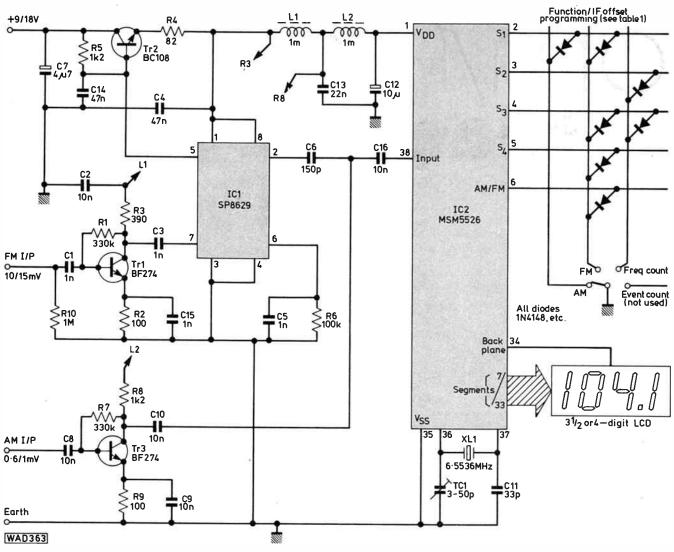


Fig. 1: Complete circuit diagram of the a.m./f.m. frequency readout based on the OKI MSM5526 i.c.

LCD 3½ Digit			LCD 4 Digit				
PIN		PIN		PIN		PIN	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17	Back Plane - Bar b ₄ , c ₄ nc nc nc nc DP3 e ₃ d ₃ c ₃ DP2 e ₂ d ₂ c ₂ DP1 e ₁	40 39 38 37 36 35 34 33 32 31 30 29 28 27 26 25 24	Back Plane Bar Over Range nc n	1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	Back Plane nc nc nc e4 d4 c4 DP3 e3 d3 c3 DP2 e2 d2 c2 DP1 e1	40 39 38 37 36 35 34 33 32 31 30 29 28 27 26 25 24	Back Plane nc nc g ₄ f ₄ a ₄ b ₄ nc g ₃ f ₃ a ₃ b ₃ DP4 (colon) g ₂ f ₂ a ₂ b ₂
18 19 20	d ₁ c ₁ b ₁	23 22 21	9 ₁ f ₁ a ₁	18 19 20	d ₁ Ե ₁ Ե ₁	23 22 21	9 ₁ f ₁ a ₁

Table 1

Display Select	Input AM/FM	conditions S1S2S3S4	IF offset value			
АМ	H H H H H	H H H X L H H X H L H X L L H X H H L X L H L X	-452·5kHz -454·5 -456·5 -465·5 -467·5 -469·5			
FM			+10.68 +10.71 +10.75 +10.79 +10.82 -10.60 -10.61 -10.62 -10.63 -10.65 -10.66 -10.69 -10.70 -10.72 -10.73			
direct	Н	HLLX	none			
event counter	Н	LLLX	impulses			
"H" = open (or	Vdd)		"H" = open (or Vdd)			

⁼ open (or Vdd)

prisingly low 15mA from a 9V source. The SP8629 is rated at a typical 30mA—so investigation with a voltmeter revealed that both prescaler and display i.c. were happily clocking away with only a 3.8V rail—as a result of the 82Ω mistake. A second unit was built with the same values, and worked just as well—and so it is assumed that most others will too—but if faulty counting is experienced, this 82Ω should be gradually reduced until the circuit

The input to the counter i.c. is common for both a.m. and f.m. count, and the drives from the f.m. prescaler and a.m. pre-amp may be simply paralleled. The output of the SP8629 settles either high or low, depending where the last count cycle left it—and so whilst the outputs were originally paralleled via 10nF capacitors, the f.m. coupling capacitor has to be reduced to 150pF—otherwise the a.m. signal can easily be shunted through the prescaler output stage when it has settled to the low state. A value of 150pF

is still quite enough to pass the very fast edges of the logic output of the prescaler, since counting of the l.s.i. occurs on edges, the actual waveform (which looks quite distorted) is immaterial.

The input to the 8629 must be disabled when reading a.m., and it is important to follow Plessey's application advice, and tie the unused differential input down via a $100k\Omega$ resistor to ground, to prevent spurious oscillation occurring under no-input conditions.

The i.f. offsets are all pre-programmed via a diode matrix, set according to Table 1. Just about every standard offset is available, although occasional 500Hz compromises are called for, e.g. 454.5kHz not 455kHz. With an a.m. resolution of 1kHz, and an average i.f. filter tolerance of 1kHz, this sort of error is unlikely to be at all

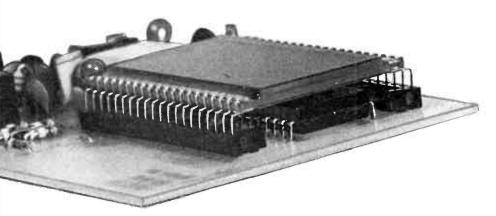
The functional setting is likewise matrix controlled, enabling selection via the simplest of all devices, a groundto-operate switch. As well as the three modes available on this board, a straightforward event counter is also available for batch counting to a maximum of 2999 units, but this feature is not used in this instance.

Had this been a description of a "discrete" approach c.m.o.s. unit, the circuit description would have just about reached the oscillator stage, but instead, there is nothing more to say!

Construction method

The printed circuit board layout, Figs. 2 and 3, employs a useful technique when using direct drive to l.c.d.s from l.s.i., namely placing the i.c. under the display. This technique saves space—and cuts the only marginal area of possible interference (from the l.c.d. backplane strobe) to a bare minimum. Construction on anything but the properly made p.c.b. is not really feasible. Fixing holes for mounting are provided so that the unit may be fitted directly behind the receiver front panel. The c.m.o.s. MSM5526 is not a particularly fragile device, but the usual care should be taken when soldering, to avoid static damage, caused by poorly earthed soldering implements, or earth leakage currents. The p.c.b. is laid out for either HC13 or HC18 style crystals, and since 6.5536MHz is a standard binary frequency, the supply is not generally a problem.

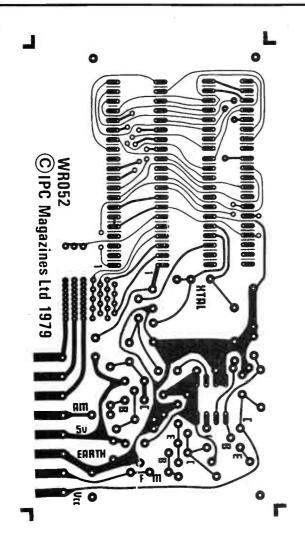
Great care must be taken when mounting liquid crystal displays, since these are not only costly, but very fragile if pressure is applied unevenly. A socket must be used to raise the l.c.d. above the rest of the components, and either socket strip or a 40-pin d.i.l. socket cut in half is suitable for the purpose. Molex i.c. pins are not a good idea since in strips of 20, it is very difficult to accurately locate the pins of the display. The electrical contact is also somewhat more chancy at this sort of length, since a small displacement of one pin can cause a lot of trouble.



The MSM5526 is mounted directly on the board and the liquid crystal display is mounted over it, using i.c. sockets to space it from the p.c.b. (see text)

^{&#}x27;'L'' = ground (Vss)

X'' = either



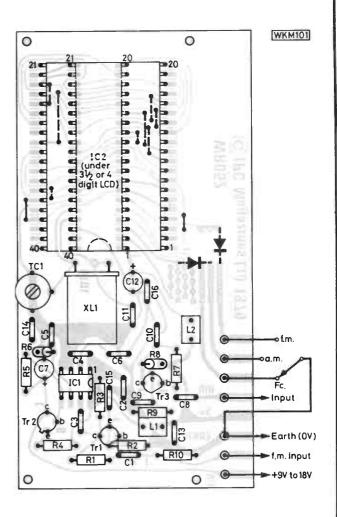
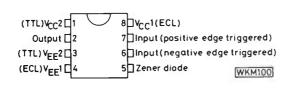
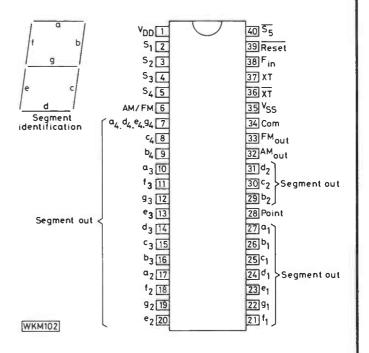


Fig. 2 (above): Full-size track layout of the p.c.b.

Fig. 3 (above right): Component layout and details of external connections to the p.c.b. The switch will normally be part of the wave-change switch of the associated receiver. When using a $3\frac{1}{2}$ -digit l.c.d., two "U"-links of insulated wire should be soldered to the track side of the p.c.b., linking pins 2 and 5/6, and pins 3 and 7 of the display

Fig. 4: Pin-outs of the SP8629 (below) and the MSM5526 (right)





* components

Resistors			Semiconducto	rs	
0.25W 5%			Transistors		
82Ω	1	R4	BF274	2	Tr1, 3
100Ω	2	R2, 9	BC108	1	Tr2
390Ω	1	R3			
1-2kΩ	2	R5, 8	Diodes		
100kΩ	1	R6	1N4148	as requ	uired for programming (see
330kΩ	2	R1,7		Table 1)	
1ΜΩ	1	R10			
			Integrated circu	its	
			MSM5526	1	IC2 (OKI Electric)*
Capacitors			SP8629	1	IC1
	plate (lead s	pacing 5mm max.)	0.0020		
33pF	1	C11	Inductors		
150pF	1	C6	1mH	2	L1, 2 (Toko 7BA
1nF	4	C1, 3, 5, 15			144LY-102)*
10nF	4	C2, 8, 9, 10, 16			
22nF	1	C13	Miscellaneous		
47nF	2	C4, 14			stal, Style HC13 or HC18
			wire-ended	j*	
			4-digit (or 3½	-digit) lic	quid crystal display
Tantalum bead			Socket for I.c.	.d. (see to	ext)
4.7µF	1	C7	Printed circui	t board F	Ref. WR052
10μF	1	C12	Terminal pins	(8 off)	
Sub-min trimme	er		*Available fro	m Ambit	International and
3-50pF	1	TC1	Watford Elec	ctronics	

Switch-on and test

Provided the components are located correctly, then there is nothing to go wrong apart from your soldering. Check the very fine tracks for splashes, and clean the board with flux remover if available. Using a current-limited power supply (for extra security), apply 5 volts at first, gradually turning up to 12V if the current drain is not excessive—indicating a short circuit somewhere. Switch to the desired input, and place a finger on the relevant preamp input, when some stray counting should occur from the pickup thus provided. Remember, this is very sensitive.

With a suitable radio to hand, place a pickup coil near the oscillator, and feed this to the counter input via r.f. coaxial cable. Something is almost certain to happen, and usually no more trouble than this is necessary. In fact, a single-ended pickup is frequently enough, though not suitable if more than 150mm long. If you don't know the exact i.f. offset, assume 10.7MHz high for f.m., and in the f.m. mode, tune to a station of known frequency. If the display reads incorrectly—say 89.2 instead of 89.1 with the tuning indicator zeroed—then the i.f. offset should be adjusted to 10.79MHZ (the closest to 10.8MHz available) by diode programming. Many of the finer variations of offset will not be apparent unless you have a very accurately calibrated signal source handy.

To set the internal clock accurately, switch to Direct Count and with a signal generator and reference counter, tune to 999kHz so that the generator output reads 999·4999kHz. Tuning to 999·501 should cause the counter to change over to 1000kHz, and the trimmer capacitor on the crystal input to the MSM5526 may then be adjusted to provide this threshold point. With the trimmer approx 30 per cent enmeshed, the whole unit is sufficiently accurate to be self calibrating anyway, so do not worry too much about these very fine adjustments if you cannot

get access to appropriate equipment. Another way is simply to count the crystal oscillator frequency on a separate counter so that it is trimmed for exactly 6.5536MHz (take care not to load the crystal—try to use inductive coupling if possible).

To set the a.m. offset, tune to a known frequency with the offset pre-programmed for 469.\$kHz (nearest available to 470kHz) for most UK- and European-made sets, and 455kHz for most Japanese sets, and check the error. Simple maths will tell you what to do—e.g. if the station is known to be on 910kHz, and the counter says 905 when the i.f. is set for 470kHz, then reprogramme the offset for 465.5 and all will be well.

Applications

Apart from new equipment, there is obviously a large retrofit application for improving existing equipment—since the accuracy of frequency display has let down many otherwise good designs. Varicap diode designs can occasionally put strains on analogue scale design, since the end-point capacitance can vary widely, although the diodes themselves remain well matched. This display takes away those problems, and does away with the last remaining mechanical headaches of the set designer.

One point which is very important about the MSM5526 is the fact the display is totally static. This means that there is no multiplexing interference—and the only potential source is in the shape of the backplane strobe, which is very, very low power for an l.c.d. Thus without screening, this device can readily be used without problems in any radio environment, from supplies ranging from 8V to 20V d.c. (thanks to the regulator on board). So next time the drive cord snaps, forget about a replacement and fit a digitally accurate alternative.

SPECIAL PRODUCT REPORT



LOGIC PROBE KIT

If you are involved in digital electronics it is essential that you have some means of detecting pulses and logic states. Without this necessary equipment you will be totally in the dark when trying to find out why your latest creation does not work.

There are many logic probes on the market but for the amateur they tend to come a touch on the pricey side. Continental Specialties Corporation, who also make a range of logic probes, have recently introduced a kit for a probe which will detect and display logic levels, pulses and voltage transients.

The kit is complete down to the last piece of wire and even includes a length of solder. All the components appeared to be of good quality and fitted the holes drilled in the glass fibre printed circuit board without any problems.

The instruction manual is very comprehensive and covers not only the building of the probe but also notes on how to use it.

★ specifications

Input impedance: 300kΩ

Threshold: Logic 1 (Hi-l.e.d.) 70% Vcc

Logic O (Lo-l.e.d.) 30% Vcc

Detectable pulse width: 300 nanoseconds min.

Input signal frequency: 1.5MHz max.

Pulse detector: High-speed pulse train or single

events (positive or negative transitions), active 0.1 second pulse

stretcher

Input voltage: ± 50V continuous, 120V a.c. for less

than 15 seconds

Power requirements: 5 volt Vcc at 30mA

15 volt Vcc at 40mA

25 volts max., with power

lead reversal protection

Physical size: 147 x 25.4 x 17.8mm

Weight: 85 grams



Construction proved to be very simple and straightforward, the step-by-step assembly instructions proving easy to follow. Unlike traditional British component placement drawings however this one did not show the copper track pattern of the p.c.b. and no holes are shown so that it is very important to check twice that the components are correctly placed.

No problems were encountered and the probe worked first time, but if you are unfortunate a page is devoted to trouble-shooting and two pages to testing the probe following construction.

The plastics case, which is available separately and has been used for the *PW* Car Test Probe, is very neat and the two labels supplied with the kit are self-adhesive giving the finished probe a professional look.

The probe is simple to use, requiring the power leads to be clipped to suitable voltage rails on the circuit under test and the probe tip to be held against the test point.

Indication of the status of the point is by a combination of three l.e.d.s which light, or pulse, depending upon the logic state being investigated.

As a simple means of determining logic states this kit is very good value for money.

Dick Ganderton

SEE NEXT MONTH'S ISSUE OF PRACTICAL WIRELESS FOR DETAILS OF A SPECIAL INTRODUCTORY OFFER FEATURING THIS KIT



publication elsewhere.

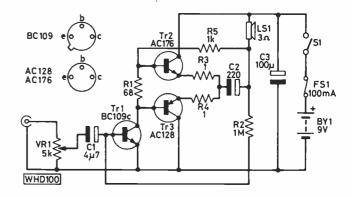
WORKBENCH AMPLIFIER

Although there are plenty of amplifier i.c.s and modules available, there are many applications where discrete circuitry can hold its own on cost and simplicity. One of these is a battery-powered audio amplifier for workbench use.

The input signal goes via the volume control VR1 to Tr1, which is a high-gain voltage amplifier. Its output is applied to the bases of Tr2/Tr3, the complementary output pair, with R1 providing the necessary standing bias. For reasons of simplicity and cost, no form of temperature compensation has been included.

Two negative feedback paths are included. Resistor R5, which is basically the collector load for Tr1, also provides bootstrapping for the output stage. Resistor R2 provides base bias for Tr1 and also overall negative feedback. Audio quality may be improved at the expense of reduced output by lowering the value of R2. Capacitor C3 decouples the supply, and helps to maintain audio quality when the battery approaches the end of its life.

Transistors Tr2 and Tr3 should be purchased as a



Each idea should be accompanied by a declaration that it is the original work of the person submitting it, and that it has not been accepted for

matched pair, and must be fitted with heat-sinks—the push-on, finned type should suffice. With no signal applied, the total consumption of the amplifier should be less than 35mA.

D. L. Jones, Denbigh, Clwyd.

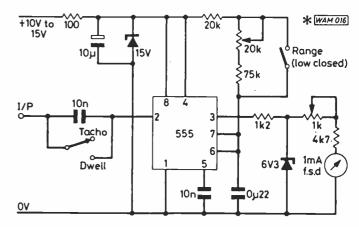
TACHOMETER/DWELL METER

This circuit utilises a 555 timer chip in a dual function as a tachometer or dwell meter. In the tachometer mode, the input signal is taken from the car's contact breaker as a square-wave and fed via a capacitor to pin 2 of the timer, realising a high mark/space ratio. The two switched ranges, 0 to 1000 r.p.m. and 0 to 5000 r.p.m., are calibrated by a $20k\Omega$ and a $1k\Omega$ potentiometer.

In the "dwell" mode, the input capacitor is by-passed, maintaining a square-wave at the input of the device, which means that the output at pin 3 is an inverted version of the input waveform. In the "dwell" mode, only the lower of the two tacho ranges should be switched in.

The circuit requires a minimum supply of 12V for consistent operation.

R. J. Jenkins & M. E. Taylor, Knebworth, Herts.



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Brushed Aluminium Fascia Front Panel.	£32.99
Pack (E) Semiconductors (including HITACHI MOS Power	
Fets)	£30.53
Pack (F) Toroidal Mains Transformer	£17.22
Complete Kit of all parts necessary to built the WINTON	£120.00

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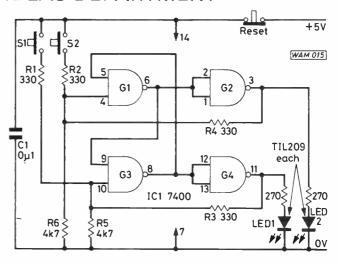
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IDEAS DEPARTMENT



TTL "SNAP" INDICATOR

At switch-on R6 holds the input to gate 1 low, making the output high. This is coupled to inverter gate 2, the output of which is low and is coupled back to pin 4 by a 330 ohm resistor. These gates remain in this state as do gates 3 and 4 and in this condition no l.e.d.s are lit.

Note that the high at pins 6 and 8 are cross-coupled to the inputs of gates 1 and 3. Suppose S2 is pressed: pin 4 is connected to a high via R2. As pin 5 is also high the output of gate 1 goes low causing gate 2 to change state at pin 3, which goes high causing l.e.d. 2 to be lit.

Pin 4 is kept high via R4 so that the l.e.d. is "latched" on when S2 is released. Since pin 9 of gate 3 is held low by the output of gate 1, closing of S1 cannot change the state of gate 3 and l.e.d. I cannot be lit.

A complementary sequence occurs if S1 is pressed first. The power supply must be broken by the reset button to restore the circuit to its original state. C1 decouples the supply lines and prevents random triggering of the l.e.d.s at switch-on.

J. Bloxham, Stratford-on-Avon, Warwickshire.

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UNICOM 21

To celebrate the 21st anniversary of the birth of their company, South Midlands Communications Ltd. are holding an Exposition and Symposium on Communications, called Unicom 21, on 22/23 June at Kempton Manor, Sunbury-on-Thames. Opening hours for the general public are 6pm-10pm on the Friday and 10am-8pm on the Saturday. Kempton Manor is adjacent to the M3 and A305, alongside Kempton Park Race Course.

There will be demonstrations of equipment by SMC, Strumech, Ascot Antennas and Microwave Modules, with experts on hand to answer all your questions. *Practical Wireless* will be there too, showing a selection of recent projects for the radio enthusiast.

The programme of lectures includes such subjects as: "A Single-chip Frequency Synthesiser". "FM vs SSB Bandwidths", "WARC 79", "Direct Conversion Receivers" and "Working more DX".

There will be a talk-in station operating on channel S22 with the special call-sign GB3SMC. Full bar and buffet facilities will be available.

Exhibitions

"The Great British Electronics Bazaar" is to be held at Alexandra Palace between 28 and 30 June 1979. The Bazaar is aimed at attracting the amateur, hobbyist and small professional buyer.

Among the stands booked by both large and small companies and organisations, will be demonstrations of building electronic circuits and home computer systems, to suit virtually everyone.

It is hoped that the event may be televised and application has been made for an amateur radio station with its own callsign.

Free tickets for the exhibition are available (send s.a.e.) from: The Great British Electronics Bazaar, 34–36 High Street, Saffron Walden, Essex CB10 1FP

Computer shop

Since Friday, 16 March 1979, London's West End shoppers have been able to walk up to a counter and say "Can I have a computer, please?" And

that's precisely what they can do at The Byte Shop, located in the capital's home electronics heartland, Tottenham Court Road.

At The Byte Shop, the fascinating world of computers is only a counter's width from the man in the street. For the first time, businessmen in Central London will be able to nip out at lunchtime for an impromptu demonstration. Everything needed to computerise a small to medium sized business is now on show—from the smaller self-contained systems costing a few hundred pounds to the most professionally-configured systems incorporating external printers and visual display units priced up to around £15 000.

The Byte Shop also offers a broad selection of advanced computer games, with shoppers being invited to pit their skills against chess, poker and backgammon programs compiled by experts. Further information from: *The Byte Shop, 48 Tottenham Court Road, London WC1*.

Cartoon computer

A unique computerised system to expedite the production and lower the costs of making animated films is now being used by the Swedish Broadcasting Corporation (SBC) for its television services.

Conventional methods of preparing animated films are enormously time-consuming. Most of the work is very repetitive since each second of finished film requires from 20 to 25 almost similar drawings.

Under the new system, utilising a Sperry Univac 1100/11 computer, SBC uses a technique developed by Alan Kitching, an animation and data processing specialist, who manages Grove Park Studios in Camberwell.

The technique, known as ANTICS, begins with a basic drawing being prepared and entered into the computer using a special light pen. By means of special command words and codes, direction, speed and position specifications are also fed into the computer. The basic drawing can then be modified in different ways, for example, it can be shrunk, enlarged, panned, skewed, shaken or reversed. It can also be induced to rotate, jump, rock, etc. The system now contains some 40 commands, but Alan Kitching is working on further expansion.

One of the latest concepts within ANTICS is the Skeleton command. In response to a Skeleton command, a part of the basic drawing—such as a human character—will move in a natural manner. Using single skeletal figures the operator can specify a pattern of movements based on key positions. The computer then automatically creates all the intervening pictures needed to complete the overall sequence of movements and the final result appears as a smooth natural motion which matches the position of the skeletal figures entered into the computer.

With the new ANTICS system, sophisticated films that would have taken more than six months to produce by conventional means can be made in a few man-weeks. Sperry Univac, 65 Holborn Viaduct, London EC1.



PRODUCTION LINES alan martin

Mighty Midget

Toolrange, distributors of the Panavise range, announce availability of the Model 502 Precision Panapress. This small but tough arbor press, less than



178mm high, is ideal for pressing bearings, forming and assembling small parts, staking rivetting and broaching. Built to stand the rigours of daily production line usage, the press has a rated capacity of 500psi.

The arbor and table plate are pressure die cast in high strength Zamak III alloy. The operating mechanism and operating lever are hardened ground steel, leverage ratio 13-25:1. Throat depth is 64mm and vertical capacity is 89mm. Ram ends are supplied unfinished for custom tooling by the user and the operating ram is fully reversible. A unique feature of the Panapress 502 is the four self lubricating adjustment gibs which give fine directional control of the ram/plate alignment.

The Panapress 502 is available at £36 plus VAT, from *Toolrange Ltd.*, *Upton Road, Reading RG3 4JA. Tel:* (0734) 29446 or 22245.



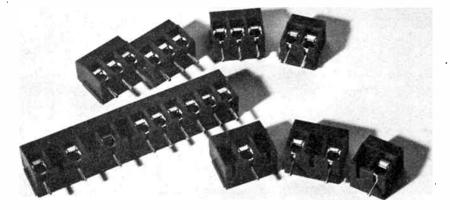
The new Kaffka range of connectors being imported from Germany by West Hyde consists of six types, made in 5mm or 10mm spacing. They dovetail together to form a connector of any desired configuration.

They are of high-quality precision manufacture in red Nylon 66. The connector bodies are of zinc-plated brass with leaf springs to avoid conductor damage from the chromed nickel

plated clamping screws.

Behind each screw there is a hole for a 2mm test prod. Current rating is 13 amps and accept cables of 2.5mm², with temperature range of from -30°C to +120°C.

Prices range from 7p to 23p each and are available from: West Hyde Developments, Unit 9, Park Street Industrial Estate, Aylesbury, Bucks HP20 1ET. Tel: (0296) 20441.





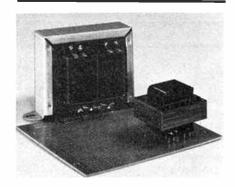
Handy Stripper

Recently introduced into the Carel Components catalogue, is the "Kabifix" DBP cable stripper which can effectively and accurately end or centre strip cables up to 25mm diameter.

Complete with a blade which easily adjusts to the insulation thickness and swivels automatically, the tool can be snapped closed over the cable, rotated round the insulation or pulled longitudinally to expose the cable.

Durable and easy to operate, this handy stripping tool supplied with an instruction leaflet and plastic pouch, costs £8.25 plus VAT.

Carel Components, 40–44 The Broadway, Wimbledon, London SW19. Tel: 01-540 7186.



Transformers

A new range of high quality competitively priced transformers, designed to conform generally to BS2214, is now being stocked by Verospeed.

All the transformers are fitted with full shrouds and are varnish protected. Two 120V windings are provided for the primary and they may be connected in series or parallel for operation at 50 and 60Hz. Two secondary windings are provided for series or parallel connection. Various output voltages from 0–3V to 0–20V are available within a range from 1-2VA to 50VA.

Further details are contained in the new Verospeed catalogue, available direct from: Verospeed, Barton Park Industrial Estate, Eastleigh, Hampshire SO5 5RR. Tel: (0703) 618525.

Learning to spell

The latest learning aid from Texas Instruments, known as "Spelling B", uses proven word/picture association techniques to help children progress in spelling regardless of their basic writing skills. Using an alphabetical calculator-type keyboard and display, combined with a picture book containing 264 carefully selected, colourful pictures of familiar objects, "Spelling B" is designed to provide an early introduction to word recognition, and also incorporates a series of simple and entertaining word games to improve basic reading skills.

In operation, the "Spelling B" selects and displays a picture number, the child finds the numbered picture in the book, and then spells the name of the picture by pressing the letter keys. As the letters are keyed they appear in the display, and at the end of each word the display signals "right or wrong". If the word is misspelled, the

child is given a second attempt, and if this is wrong the correct answer is displayed. The number of correct answers is displayed as a "score" at the end of each set of five words.

"Spelling B" is programmed so that one of three different levels of difficulty can be selected. In addition, a variety of pre-spelling activities for younger children plus word games for all ages are available.

Among the games which add fun and variety to "Spelling B" are: "Starts with", a pre-spelling exercise in which the child only has to enter the first letter of the displayed word; "Missing letter", in which a word is selected at random and displayed with letters missing; "Mystery word", a variation of "Hangman" in which players have to guess words one letter at a time; and "Scramble", in which up to five words can be put into a memory in anagram form and recalled for "unscrambling" at a later stage.



The "Spelling B" costs £19.95 (r.r.p. including VAT), and is available through the usual distributors.

Texas Instruments Ltd., European Consumer Division, Manton Lane, Bedford MK41 7PA

Portable 'scope

The new Model SB15M lightweight portable oscilloscope from Albol Electronic is claimed by the makers to break all records for cost-effectiveness for a professional/amateur instrument.

Albol say that the bandwidth goes up to 15MHz within 3dB limits and nine ranges cover, with an accuracy of 5% 10mV to 20V/cm on the 45 by 60mm measuring area of the c.r.t. Input impedance is $1M\Omega\pm3\%$ in parallel with 30pF, and the maximum input voltage is 400V.

The timebase can be freely running or triggered, and is displayed on 19 calibrated ranges from $0.5 \mu s/cm$ to $0.5 \mu s/cm$. Synchronisation can be either internal or external, with the a.c. mode giving 20Hz to 1MHz, and the h.f. mode 1 to 15MHz. Trigger sensitivity is said to be 0.5 cm of the display on "internal", or 0.5 V p–p on "external".



Bandwidth of the X amplifier, within 3dB, goes from d.c. to 3MHz, with an input impedance of $1M\Omega$ in parallel with 45pF. The X deflection coefficient varies from 0·3 to 1·5V/cm. An attractive feature of this truly portable scope is that it can operate from 220 to 240V mains (using the optional adaptor) at 50 to 400Hz, with a power consumption of 40VA, or else from internal 1·5V cells giving 12V d.c. (rated then at 27W).

The width of the SB15M is 150mm, depth 340mm, and height 280mm, and it weighs only 7.6kg. Price is £150 plus VAT.

Available from: Albol Electronic & Mechanical Products Ltd., 3 Crown Buildings, Crown Street, London SE5 OJR. Tel: 01-703 2311.

New Sinclair DFM

Latest from Sinclair's new instrument product range, is a high specification, low cost, digital frequency meter, called the PFM200.

Designed to provide the performance of high quality bench-style instruments with the portability of a 158 \times 76 \times 45mm unit in a light (6oz) but rugged case, the PFM200 is priced at only £49.80 plus VAT, which should permit most laboratory engineers, service technicians, students and hobbyists to possess their own personal digital frequency meter.

Its bright, sharp 8-digit display with variable accumulation period gives high resolution coverage from low audio frequencies right up to v.h.f.

without the need for complex range changing and with exceptional sensitivity of 10mV. Guaranteed range is 20Hz to 200MHz, typically higher, with a frequency resolution down to 0·1Hz. Power is from a 9V battery or approved a.c. adaptor.

Supplied complete with test leads and probes, protective wallet and operator's manual, optional extras are a.c. adaptors for 117V, 220V or 240V; de-luxe padded carrying case with lead storage compartment; and a connector pack comprising BNC, coaxial, DIN and phono adaptors plus telescopic aerial for direct signal pick-up from nearby transmitter.

A technical information leaflet on the PFM200 is also available from: Instrument Sales, Sinclair Radionics Ltd., London Road, St Ives, Huntingdon, Cambs PE17 4HJ. Tel: (0480) 64646.



Practical Wireless, July 1979

numbers without tears

Dr G. BROWN

The aim of this design was to produce an educational toy capable of teaching rapid number recognition to children of $2\frac{1}{2}$ years and upwards. The absolute minimum of instruction should be necessary, the idea being that the child learns as he plays, without external influence. The toy should thus be interesting to play with.

To a young child this means: (a) visual stimulation—things should be seen to happen; (b) tactile stimulation—the instrument should respond to touch, to pressure—there should be something to turn, something to switch.

This simple unit has all these facilities and can hold a child's attention for remarkably long periods. It can also double as a single die for use with other games.

General Features

Fig. 1 shows the basic design blocks. A swept-frequency clock generator feeds the first decade counter, the digit outputs of which are used to drive ten light-emitting diodes (l.e.d.s) arranged in a circle. A second decade counter, fed from the same clock source, drives a single 7-segment l.e.d. numeric display. As the clock frequency rises from zero, the circular l.e.d. display assumes a rotating motion with a visible acceleration. As the clock frequency then falls to zero, the "flywheel" effects slows and stops at a random position.

The l.e.d.s are labelled 0 to 9, as are the positions on the manual number selector, which is a rotary switch. Provided that both decade counters are reset to zero initially, they will always remain synchronised, i.e., if the flywheel stops at position "4", then the 7-segment outputs will correspond to the figure 4 also.

The number selector is wired such that the 7-segment display is only illuminated when this switch is turned to the same number at which the flywheel has stopped. The normal fixed-frequency clock is used when the device is

employed as a die.

Some simple logic is included to make the toy more interactive with the child, and will be described in the appropriate sections.

The Swept-frequency Clock Generator

For this particular application, a manually-initiated frequency sweep was required from zero up to about 100Hz and back again to zero. The circuit is shown in Fig. 2.

The clock is designed around the ubiquitous NE555V integrated circuit connected in the astable mode.

If the circuit to the left of the dashed line is studied, the timing components R1 and C1 are easily recognised. C1 is

charged up through R1, and IC1 will discharge C1 when the voltage at point A reaches 0.67Vdd. The negativegoing edge corresponding to the discharge of C1 retriggers the cycle and the system becomes astable, the frequency of oscillation being given by:

$$f = \frac{1.44}{R1 \times C1} Hz$$

In the circuit to the right of the dashed line Tr1 and Tr2 are connected as a Darlington pair controlled by the touch plate connected to the base of Tr2. The quiescent-state voltage at point A is controlled by resistors R1, R2, and R3, the two transistors being effectively open-circuit. A simple Ohm's Law calculation shows that point A is held at 0.65Vdd and, because IC1 will not discharge C1 until point A reaches 0.67Vdd, the clock oscillator is biased off, its output being a logic "1" in this condition.

When a finger is applied to the touch plate, charge flows into the electrolytic capacitor, C2. As this charges up, the potential at point B rises. With C2 fully charged (after about one second), both transistors are turned fully on and point B is taken almost to Vdd. Thus the Darlington pair may be regarded as a variable resistance, Rt, between point B and Vdd, this resistance varying from infinity to near zero. As soon as Rt becomes finite, point A is lifted above the threshold value of 0.67Vdd and oscillation begins.

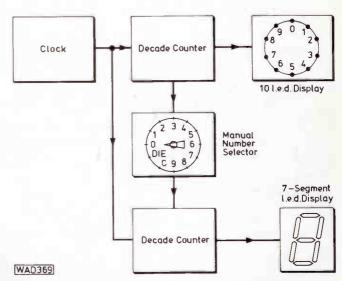


Fig. 1: The basic block diagram of the numbers toy

The frequency of oscillation is still given by the above equation, except that R1 must be replaced by the effective instantaneous value of R1, R2 and Rt. In the limit, with Tr1 and Tr2 turned fully on, R1 and R2 are virtually in parallel between Vdd and point A, and have an effective resistance of $24.8k\Omega$. This gives a theoretical upper frequency limit of:

$$f = \frac{1.44}{2.48 \times 10^4 \times 3.3 \times 10^{-7}} = 176 Hz$$

This figure is not attained in practice because Rt never falls completely to zero.

When the finger is removed from the touch plate, C2 discharges slowly through Tr1 and R3, and Rt increases correspondingly. The frequency of oscillation falls and finally reaches zero when point A falls again below its threshold value. This decay time is of the order of 10 to 15 seconds.

Switching R4 into the biasing network by closing S1 holds point A just above threshold and a constant-frequency output of about 15Hz is produced. The use of this clock frequency is described in a later section.

The touch plate is very sensitive in its action, and this encourages the child to experiment as he watches the effects of his finger's pressure illustrated on the flywheel display.

The Decade Counters

Apart from the NE555V oscillator, this instrument employs c.m.o.s. devices which are relatively cheap and are ideal for this purpose. Fig. 3 shows the circuit diagram of

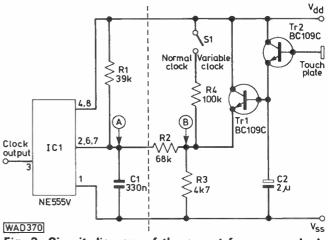
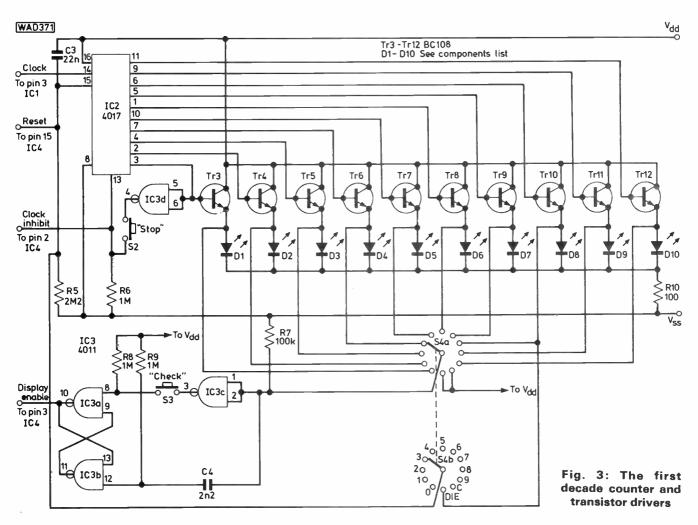


Fig. 2: Circuit diagram of the swept-frequency clock generator

the first decade counter and the transistor drivers for the 10-l.e.d. flywheel display. The 4017 decade counter is fed from the clock generator described above. In order to drive the flywheel l.e.d.s at 20mA, ten transistors operating as emitter followers are used. As only one l.e.d. is illuminated at any instant, only one current limiting resistor, R10, is necessary. It will be noted from Fig. 3 and Fig. 4 that the "reset" and "clock inhibit" functions are made common to both decade counters. This is to ensure complete synchronism of the two counters at all times. The combination of C3 and R5 resets both counters to zero when power is first applied.



Switching Logic

The switching logic provided by S3, S4 and IC3 has two important effects, which are now described.

Suppose the flywheel display has stopped at "4". It would be trivial to connect the pole of S4a to the "display enable" pin of the second counter (see Fig. 4) to illuminate the 7-segment display when S4a is turned to position "4". This operation would not require any numerical knowledge on the part of the child: he would just turn S4 until the 7-segment display came on. To avoid this, IC3a, b and c are interposed between S4a and the "display enable" pin of the second counter. IC3a and b form a toggle whose normally-off output is taken to the "display enable" input of the 4026 counter, thus keeping the 7-segment display off under normal conditions.

Taking pin 8 of IC3 to Vss will turn the toggle on and, with it, the 7-segment display. Similarly, taking pin 12 of IC3 to Vss will reset the toggle and extinguish the

7-segment display.

Signals to control the state of the toggle are taken from the pole of S4a. The "on" state of toggle and display is controlled by the position of S4a, by the inverter IC3c, and by the push switch S3. If S4a is turned to position "4" to match the flywheel display, then the pole is taken to logic "1"; logic "0" thus appears at pin 3 of IC3.

If S3 is momentarily pressed, the resulting logic "0" applied to pin 8 of the toggle will switch both itself and the 7-segment display on. Thus the child must not only select a number, but must press the CHECK button, S3, to see if

his selection was correct.

What happens if the selector switch is turned after the 7-segment display has been illuminated? If the display were to remain illuminated with the electro-switch now showing a different number, the child would be confused, so provision is made to extinguish the display (a) when the selector switch is turned from the correct position, and (b) when the flywheel is started again. These requirements are simultaneously fulfilled by connecting the pole of S4a via C4 to the "reset" input of the toggle, pin 12.

Suppose the previous procedure has resulted in a "4" being indicated by both the displays. If S4a is turned away from "4" the pole is taken from logic "1" to logic "0", and the negative-going edge so produced is passed by C4 to

reset the toggle and extinguish the display.

Similarly, if the flywheel is started, the negative-going edge produced as l.e.d. "4" goes out resets the toggle via

C4 and the 7-segment display is extinguished.

Thus, in normal use, there can never be any ambiguity between the numbers on the displays and the number set on the selector switch.

The presence of R7 from the pole of S4a to Vss is worth

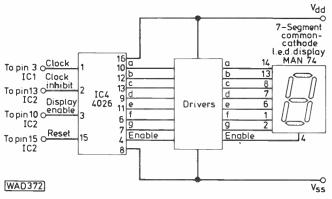


Fig. 4: The second decade counter

nothing. There is no reason why the digit positions on the S4a wafer should not go direct to the digit outputs of the 4017 counter: in this case R7 would be unnecessary. However, there is a very good practical reason why this is not done. The ten l.e.d.s and the selector switch S4 are mounted on the front panel. The integrated circuits and transistors are on a single circuit board mounted on the base of the metal box. Thus there are ten flexible leads from the emitters of Tr3-Tr12 to the l.e.d.s on the front panel. Ten more flexible leads would be needed from the S4a wafer to the digit outputs of IC2, but these leads can be eliminated by simple wiring to \$4a from the anodes of the l.e.d.s, which are on the same panel. When this is done, a pull-down resistor, R7, to Vss is needed for the inputs of IC3c to keep them at logic "0" except when a logic "1" is fed to the pole of S4a from the flywheel display.

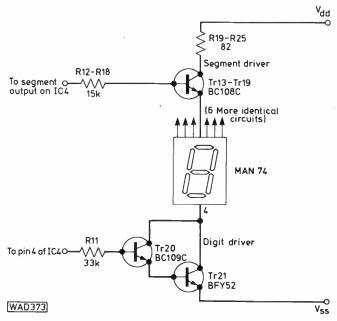


Fig. 5: Driver circuits for the second decade counter

The second decade counter and its associated circuitry are shown in Figs. 4 and 5. The counter is a Type 4026 c.m.o.s. device which has outputs for a 7-segment display. These figures require very little explanation. The 4026 counter operates in parallel with the 4017 counter, and the 7-segment common-cathode display is fed by seven segment driver stages, Tr13-Tr19, and one digit driver stage, Tr20-Tr21. The current-limiting resistors, R19-R25, give segment currents of 19mA. To. "enable" the display, the digit driver Darlington pair, Tr20-Tr21, is switched on by a logic "1" from pin 4 of the 4026 counter, thus providing a low-resistance path from the display cathodes to Vss. Tr21 must be capable of carrying $7 \times 19 = 133$ mA, and the Darlington configuration has been used so that Tr21 can be very conservatively rated, ensuring high reliability.

Provision has been made to illuminate the 7-segment display while the flywheel is running. This adds to the visual appeal of the instrument before the child is ready to tackle number recognition and matching. This is the function of position "C" (continuous display) on the selector switch S4. When "C" is selected and S3 pressed, the display will remain on throughout the flywheel cycle.

A final word now about the use of the instrument as a die. On the "DIE" position of the selector switch, S4a provides a constant logic "1" on its pole (as in the "C" position), and when S3 is pressed the 7-segment display is

constantly illuminated. S4b comes into operation at this point and connects the "7" digit of the l.e.d. flywheel to the "reset" pins of both counters. Thus both of the displays count repetitively from "0" to "6" when the clock runs. The swept-frequency clock can be used for this, but it has been found that the use of a constant 15Hz clock (selected by S1) is more satisfactory, in that the procedure is less involved for the child.

To "throw" the die, all that the child does is press S2: both displays stop immediately, showing a number between "1" and "6". On releasing S2, counting begins again. This function utilises the "clock inhibit" pins of both counters. When these pins are taken to logic "1", counting will cease, even though the clock is still running. The last NAND gate of IC3 is used for a rather devious purpose in this mode. Both IC2 and IC4 are counting from "0" to "6" yet it would clearly be incorrect to allow the die to stop at "0".

Instead, the die is slightly "weighted" such that it can never be stopped at "0"! The probability of throwing a given number on a die is 1:6. On this die, the probability of throwing a number between 2 and 6 is 1:7 and the probability of throwing a 1 is 2:7.

In use by young children, or even unsuspecting adults, this would never be noticed. To prevent a "0" being thrown, the signal to inhibit the clock is taken from the "0" digit output (pin 3) of the 4017 counter. If, at the moment S2 is pressed, a number from "1" to "6" is being displayed, pin 3 will be at logic "0". IC3d inverts this to logic "1" and inhibits the clock. However, if "0" is being displayed when S2 is pressed, pin 3 is at logic "1" and the logic "0" produced by IC3d will not inhibit the clock. Instead, it waits for the next clock pulse which increments both counters to the digit "1", at which instant pin 3 of the 4017 goes to logic "0" and IC3d then inhibits the clock with logic "1" at its output.

Power Supply

A single-polarity, stabilised 5 volt supply is used, employing an integrated circuit regulator. Stabilisation is to be preferred here, because the current taken from the supply varies between about 23mA with only the flywheel display on, to about 160mA with the 7-segment display showing an "8". Fig. 6 shows the circuit used. The regulator is mounted on the metal box to dissipate the small amount of heat generated. The use of 15V d.c. supply for the regulator may seem excessive. In fact, this supply rail will drop to 12 volts on full load and, as the regulator needs a supply of at least 8.5 volts, the supply is not too conservatively rated. A transformer with a 9-0-9 volt secondary could be used, provided that the supply rail for the regulator did not fall below 9 volts on full load.

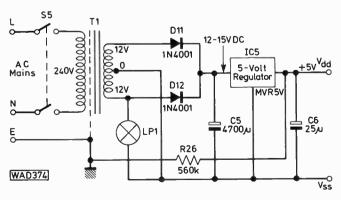


Fig. 6: Power Supply

★ components

¹ ₄ W 5% carbon film 82Ω	7	R19, 20, 21, 22, 23, 24, 25
100Ω	1	R10
4.7kΩ	1	
1.5kΩ	7	R3 R12, 13, 14, 15, 16, 17, 18
33kΩ	1	R11
39kΩ 68kΩ	1	R1 R2
100kΩ	2	
560kΩ	1	R4, 7 R26
1ΜΩ	3	R6, 8, 9
2.2ΜΩ	1	R5
Capacitors		
Electrolytic		
2μF 6V	1	C2
25μF 6V	1	C6
4700μF 25V	1	C5
Polycarbonate or pe	olyeste	
2.2nF	1	C4
22nF	1	C3
0.33μF	1	C1
Semiconductors		
Diodes	2	D11 12
1N4001 LED	10	D11, 12 D1, 2, 3, 4, 5, 6, 7, 8, 9, 10
Transistors		
BC108C	17	Tr3, 4, 5, 6, 7, 8, 9, 10, 11,
BC100C		12, 13, 14, 15, 16, 17,
		18, 19
BC109C	3	Tr1, 2, 20
BFY52	1	Tr21
		10 man
Integrated circuits		
MVR5 regulator	1	IC5
NE555V	1	IC1
4011	1	IC3
4017	1	IC2
4026	1	IC4
Switches		
s.p.s.t.	1	S1
Push to make	2	S2, 3
2p 12w rotary	1	S4
s.p.d.t. slide	1	S5
Miscellaneous		
12-0-12V 200r	nA tra	ansformer T1 (1); 12V panel red l.e.d. display, common

Constructional Notes

Apart from the power supply, displays and switches, the entire circuit was constructed on a single piece of Veroboard measuring 95×63 mm. The layout is not important, so no details are given, but it is advisable to take all Vss leads to a common point.

In general, this precaution is unnecessary, but in this circuit the emitter connection of the digit driver Tr21

Continued on page 60



This unit was developed after I was asked by a friend to build a device with which he could turn a light on by clapping his hands.

Obviously this could be done by using a simple sound operated switch comprising a microphone, audio amplifier and trigger circuit, but such a simple circuit would respond to any sound of sufficient volume. Clearly something more

sophisticated was required.

After a number of tests had been made, it was found that satisfactory operation could be obtained by making the circuit respond only after receiving two sounds with a fixed time interval between them of around one second. This achieves a good compromise between simplicity, spurious operation from background noise and ease of use. The human brain is very bad at estimating short time intervals and a sequence of more than two sounds becomes impossible to generate with any accuracy. The circuit also incorporates a filter and a level trigger so only sounds of the correct pitch and sufficient volume will be detected.

Circuit Operation

IC1 and associated components amplify the sound picked up from the microphone and include rough frequency filtering. VR1 is a gain control and VR2 adjusts the d.c. level of the output from this stage. This is fed to a Schmitt trigger comprising Tr1 and Tr2 and also has a time delay (C4, R2) to prevent multiple triggering. The components following (Tr3-Tr5) form a driver stage for the logic circuit, and the l.e.d. D2 indicates when a sound has been detected. The circuit gives a logical '0' on receiving an input above a preset threshold set by VR2.

The output from this stage is first fed to a monostable comprising G1 and associated components which in turn triggers two more monostables G3, G4 and associated components. Monostable G1 has a period of about 5 seconds and is included to prevent the other two monostables re-triggering before the circuit has finished its cycle. G3 has a period of about 1 second and G4 about 3 seconds.

The circuit comprising G6-G11 and FF1 looks for the state in which, after a pulse has triggered the monostables, a second pulse arrives during the period when G3 has turned off again and G4 is still on, i.e. 1-3 seconds after the first pulse. When this happens a logical '1' is sent to FF2 which then changes state and opens or closes the relay via Tr9 and Tr10. If the second pulse arrives before or after

the allowed period it is ignored and will also work the latch G9, G11 to make the circuit ignore all further inputs until G1 has reset. Thus on receiving two sounds with a time interval of about 1 second between them the circuit will operate the relay, turning the load circuit on or off.

Construction

Construction is simplified by the use of printed circuit boards. Start by soldering in the smallest components, i.e., resistors and diodes and add the tallest components (capacitors and transistors) last. The c.m.o.s, integrated circuits (IC2-IC5) should be connected using i.c. sockets, installing them in after all the other components have been soldered. Standard c.m.o.s. handling precautions should be used. Sockets should also be used for the other integrated circuits. Take great care to connect all components such as diodes, transistors, i.c.s and electrolytics the correct way round as incorrect connection can cause a large range of puzzling faults.

At this point, something should be said about the microphone and the mains transformer. The microphone used is a high impedance balanced armature earpiece which is better than a crystal microphone in this application. There is also space on the circuit board for putting a resistor in series with C2 to adjust the low

frequency characteristics (10-100 Ω).



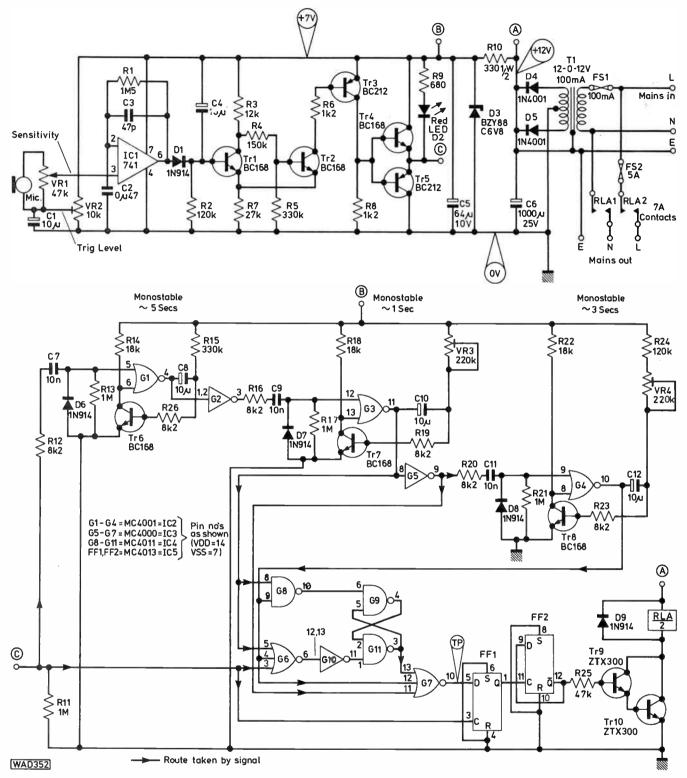
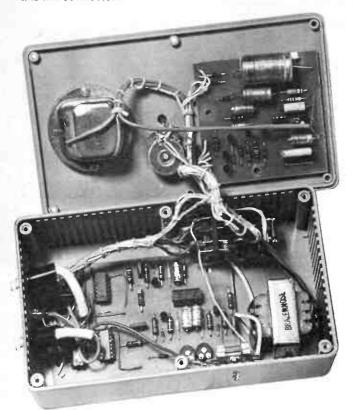


Fig. 1: Circuit diagram of the selective sound operated switch

The mains transformer is a 12-0-12V type designed to supply up to 100mA d.c. from a full-wave rectifier. Most of the current is drawn by the relay (60-80mA) with the rest taking less than 20mA. Thus if a relay is used which draws more than 80mA a larger transformer will be needed. A 100mA fuse is shown connected to the primary of the transformer and this is necessary for safety. If it is found that the fuse blows on switch-on an anti-surge fuse can be fitted. The other fuse supplying the appliance being controlled should be rated according to the relay contacts and mains cable used.

A suitable case for the unit can be made from a plastics Bimbox. When fitting components into the case, it is important to keep all the high voltage components (relay, transformer and fuse holders) well away from the other components so that there is no chance of any live connections touching any other part of the circuit. Holes are drilled in the case for the microphone, the l.e.d. and the gain control VR1. The circuit boards should be positioned within the case such that the presets VR2-VR4 can easily be reached to be adjusted. The boards are held in place using self-adhesive pads. When wiring up between the

circuit boards, it is very important that all the supply rails are connected up correctly because the c.m.o.s. chips can be damaged if an input is fed to them before the power rails are connected.



The components and p.c.b.s are fitted into a plastics Bimbox. The two p.c.b.s are attached to the box base and lid using self-adhesive foam pads

Setting Up

First set VR3 and VR4 midway along their tracks. Set the gain control VR1 to minimum. It should be found that as VR2 is moved the l.e.d. will light at one end of the track and be extinguished at the other. Adjust VR2 until it is just extinguished. Then turn the gain control VR1 up a little. It should now be found that any loud sound near the microphone will cause the l.e.d. to flash on for just under a second. If it stays on or does not come on at all then adjust VR2 until the response is satisfactory. Next, connect a voltmeter between the OV rail and pin 10 of IC3 (marked TP in the diagram) or, if no meter is available, disconnect R25 from IC5 and make a temporary connection from that end of the resistor to pin 10 of IC3.

It should now be found that if, after at least 5 seconds of silence, a sound is made near the unit loud enough to make the l.e.d. flash, then a short pulse of approximately +7V will be indicated on the meter, or the relay will close momentarily about one second after the sound. If this does not happen adjust VR3 and VR4 until it does. This is the period during which the device is sensitive and it will switch the load if a second sound is made during this period. Adjust VR3 and VR4 until the time period is satisfactory. Note, however, that if the values of the presets are made too low then the monostables will stop working, so that if a satisfactory time period cannot be achieved then it may be necessary to change C8 or C12. Do not make the "sensitive" period too short or it will be found very difficult to estimate the required time interval.

After R25 has been replaced in its correct position and the lid has been attached, then the unit is ready for use.

* components

Resistors		
½W 5%		
680Ω	1	R9
1 · 2kΩ	2	R6, R8
8-2kΩ	6	R12, 16, 19, 20, 23, 26
12kΩ	1	R3
18kΩ	3	R14, 18, 22
27kΩ	1	R7
47kΩ	1	R25
120kΩ	2	R2, 24
150kΩ	1	R4
330kΩ	2	R5, 15
1ΜΩ	4	R11, 13, 17, 21
1·5MΩ	1	R1
½W 5%		
330Ω	1	R10

Potentiometers

Horiz. miniature	prese	t
10kΩ Lin.	1	VR2
220kΩ Lin.	2	VR3,
1/4 inch shaft		
47kΩ	1	VR1

Capacitors

Disc ceramic		
47pF	1	C3
10nF	3	C7, 9, 11
Polyester		
0.47µF	1	C2
Electrolytic		
10μF 25V	5	C1, 4, 8, 10, 12
64μF 16V	1	C5
1000μF 16V	1	C6

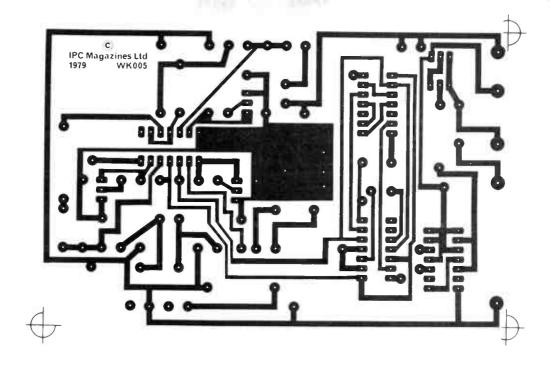
Semiconductors

Diodes

1N4001	2	D4, 5
1N914	5	D1, 6, 7, 8, 9
Red I.e.d.	1	D2
BZY88 C6V8	1	D3
Transistors		
BC168	6	Tr1, 2, 4, 6, 7, 8
BC212	2	Tr3, 5
ZTX300	2	Tr9, 10
Integrated circu	its	
741	1	IC1
4000	1	IC3
4001	- 1	IC2
4011	1	IC4
4013	1	IC5

Miscellaneous

Bimbox (190 x 110 x 60mm BIM 2006/16); Mains transformer 12-0-12V 100mA (1); Relay 12V 80mA max. 7A 240V d.p.c.o. (1); Fuse holder (2); Fuses 100mA and 5A; Balanced armature earpiece (see text) (1); Printed circuit board (2 in set); Sockets, 14 pin d.i.l. (4); 8 pin d.i.l. (1); Knob (1); Mains cable, socket and cable clamps.



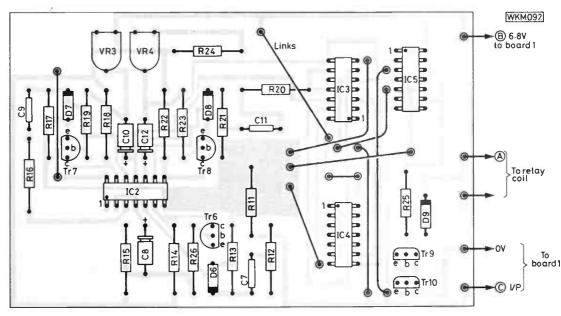


Fig. 2: The copper track pattern and component placement drawing for Board 2 shown full size.

Using the Switch

Adjust VR1 so that the l.e.d. will not flash from background noise in the room, but will reliably respond to a hand clap. The l.e.d. will be found very useful for indicating whether the unit has "heard" a sound or not, when setting the sensitivity.

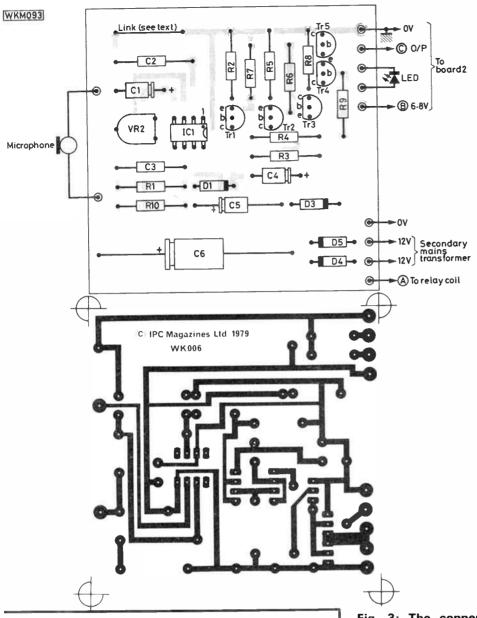
Although originally intended purely as a gimmick, the device has been found to be extremely reliable and may well have more practical uses. The prototype was left in an average sitting room for a week without triggering spuriously, but would immediately respond on hearing the correct sound sequence.

There could be practical uses where it is necessary to operate equipment remotely, possibly by a disabled

person, or in other cases where it is not possible to operate a switch directly.

Fault-finding

Once the design had been finalised, it was found that the units could be relied upon to work correctly immediately they had been assembled and adjusted. Most faults are likely to be caused by wire links in the wrong places and diodes or transistors the wrong way round. Remember that the circuit uses both *npn* and *pnp* transistors. A puzzling intermittent fault in one unit was traced to C6 being open-circuit. This resulted in the supply rails



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For details and coupon see page 30

Fig. 3: The copper track pattern and component placement drawing for Board 1 shown full size

carrying unsmoothed a.c. and played havoc with the logic functions.

Provided that the l.e.d. flashes in response to sounds then faults are best traced by first checking the outputs of the monostables (pins 4, 10, 11 of IC2) and then following the voltage levels through the rest of the circuit. Remember that the monostables give an inverse output, i.e. "1" in the quiescent state and "0" when active, and remember also that the circuit takes 5 seconds to complete its cycle and if it receives an input before G1 has reset it will ignore it.

If the l.e.d. does not light up then first check IC1. The voltage on pin 6 (output) should equal that on the wiper of VR2, except at extreme settings of VR2. The Schmitt trigger, Tr1, Tr2 should turn on when the voltage on Tr1 base exceeds about 5V, turning on the l.e.d. via Tr3-Tr5, and should turn off sharply as the voltage is lowered. These functions can easily be checked with a multimeter and should show up the location of any fault. However, provided the unit is constructed carefully, there is no reason why it should not work first time.

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Ultrasonic Remote Conti

A short introduction to the use of ultrasonics for cordless on/off control of domestic appliances etc. The article suggests some suitable circuits based on i.c.s intended for use in other fields, allowing the construction of very small transmitters and receivers





erial Design

Aerial designs can be tested and developed easily by building scale models of the proposed systems and making measurements at u.h.f. This article describes how a surplus marine adar display can be adapted to plot the resulting polar diagrams automatically





Plus SPECIAL PRODUCT REPORT on the LOWE SRX~30 Receiver

top band tran

J.R.Green BSc, G3WVR*

This low-power a.m. transmitter design illustrates the use of power f.e.t. devices—in particular, the VN66AF recently introduced by Siliconix Ltd.—and takes full advantage of modern semiconductor technology. The unit is particularly suitable for use within the 160-metre band, although operation at higher frequencies is quite possible.

Design Considerations

The Author has carried out a great number of experiments with low-power transmitter circuitry using bipolar (i.e. "conventional") devices over the last few years. Some degree of success was achieved in later designs, using the now-defunct BD123, but en route many pitfalls for the unwary were uncovered.

Technically, however, the bipolar device fell down on

several counts, notably:

1. High drive power was required; typically 10%, even

at low frequencies.

 Difficulty was experienced in achieving really linear amplitude modulation, even when modulating both the driver and p.a. stages. Modulation of the p.a. only, by swinging the supply rail, was unsuccessful. Modulation of the driver as well was essential and far more modulator power was required.

3. Problems were encountered in achieving stability in the transmitter r.f. strip. Often appreciable "slugging" was called for to prevent h.f. or v.h.f.

parasitics.

4. Modulation excursions also tended to introduce instability, often producing undesirable steps of modulation non-linearity in the modulated r.f. carrier envelope.

5. It proved remarkably easy to destroy the p.a. transistor(s) if instability occurred or the transmitter was

mis-tuned.

These difficulties led the Author to the conclusion that solid-state transmitter design could be much simplified if a *Senior Development Engineer—Gould Instruments Division

device existed which exhibited the characteristics of a thermionic valve. In particular, low drive power, modulation linearity and stability were desirable in addition to the ability to operate from low voltages. In other words, a high-power f.e.t. was needed.

During 1978, Siliconix Ltd. produced the VN66AF and samples were supplied to further the Author's experiments. The ultimate results are incorporated into the transmitter featured in this article. Whilst the published form is for 160-metres, the basic circuit could be used to produce a transmitter capable of at least 10MHz and possibly more.

Circuit Description

The transmitter employs a crystal oscillator which incorporates a twice-frequency, parallel-resonant crystal, with a TIS88A f.e.t. as the oscillator transistor (Care with substitutes! The circuit may fail to oscillate with devices requiring different d.c. conditions.). This stage provides sufficient drive to switch Tr2, a 2N2369A switching transistor which provides a twice-frequency 5 volt peak-to-peak square-wave to drive IC1. This i.c. is a 7473 flip-flop wired to divide-by-two, thus producing the output frequency "f".

The 7473 limits the "2f" crystal to around 6MHz (therefore the output frequency "f" to 3MHz) but this may be extended by substituting a Schottky 7473 (i.e. a 74S73).

From IC1 the signal is passed to Tr3, another 2N2369A switching transistor, to present 12 volts peak-to-peak square-wave drive to the output devices. With Tr3 looking into 100Ω the two VN66AF p.a. devices are easily driven. Their input capacity of 50pF each is the prime limiting factor with untuned drive, although a BFY50 could be substituted for Tr3 and R11 reduced in value to increase the operating frequency or drive more than two p.a. devices. A power output of 6 watts is typical for a 10 watt d.c. input.

A simple "constant K" type low-pass filter is provided, together with transformer matching to transfer the output power effectively into a 50Ω load and remove harmonics.



Note that since a 1:1 mark-space square-wave drive is derived for the p.a., optimum efficiency with minimal second-harmonic radiation in the unfiltered output is assured, with the filter biting hard at the third and subsequent harmonics.

Filter values shown are for a cut-off frequency of 2500kH2, but others may be calculated from the expressions:

$$\begin{split} C &= \frac{1}{f_c \pi z} \quad \text{and} \quad L = z^2 C \\ \text{where } z &= 50 \Omega \quad \text{and} \quad L = L1 = L2 = L3 \\ C &= C_{10} = C_{11} \quad \text{and} \quad C_9 = C_{12} = \frac{C}{2} \end{split}$$

f is the cut-off frequency.

The modulator circuit is merely a modified version of the Author's hi-fi amplifier design and should not present any problems. A speaker matching transformer rated at 10 watts (T2) is used to transfer the modulator power to the p.a. This should have a core area of around 25mm square and a winding resistance between the 0 and 16Ω taps of not more than 1Ω . The modulator input sensitivity is in the order of 100 mV, so a pre-amplifier will be necessary for microphone level signals.

The r.f. matching transformer T1 was wound on a Mullard binocular "balun" ferrite block, measuring approximately 25 × 20 × 8mm and consists of three turns on the primary (transistor) side and nine on the secondary (filter) side. Experiments using these baluns showed a power-handling capability of 100 watts peak! Substitutes

should have the following characteristics:

1. Suitable for the intended operating frequency.

2. 1:3 turns ratio for 6 watts, 50Ω output with wire gauge as large as possible.

3. 50Ω secondary reactance to be $\gg 50\Omega$ at operating frequency.

4. Peak power rating of at least 20 watts.

If a suitable ferrite block cannot be found, three Mullard FX2249 blocks can be used.

No Adjustments Needed!

It will be apparent from the r.f. circuitry that no tuning is required on the r.f. strip, which should work from switch-on. Trimmer VC1 is used for very fine frequency adjustment and could well be omitted, replacing it with a fixed capacitor of 18pF if the facility is not required. The pre-set potentiometer VR2 should be rotated until Tr11 and Tr12 just start to conduct—say 50mA of standing current.

The VMOS VN66AF devices performed very impressively throughout the development of the prototype transmitters. Only very low drive was necessary and very linear upward and downward modulation was produced. In every respect, the devices performed entirely to specification and simply shut down if an unacceptably-low load was connected.

Possibly it will be found that the modulator output is not quite sufficient to achieve 100% upward modulation but with a suitable transformer the quality is very good indeed and certainly far superior to so-called "communications quality", which covers a multitude of sins!

Construction

The construction techniques are clearly seen in the photograph, most of the components being soldered and mounted on one side of a double-sided "earth-plane" printed-circuit board, measuring 160×100 mm. The top of the board, the component side that is, forms an earth-plane and the copper should be cleared (using a drill and an outsized bit) around the larger holes indicated in Fig. 2. The remainder form earth-plane connections. Details of the p.c.b. are given in Fig. 2 and the component locations are shown in Fig. 3.

The modulation transformer T2 is mounted on the bottom panel of the West Hyde Developments instrument case, as are Tr4 and 5 (on insulated washers). Transistors Tr11 and 12 are mounted on the extrusion as shown in the photograph. (In fact, the VMOS devices could also be

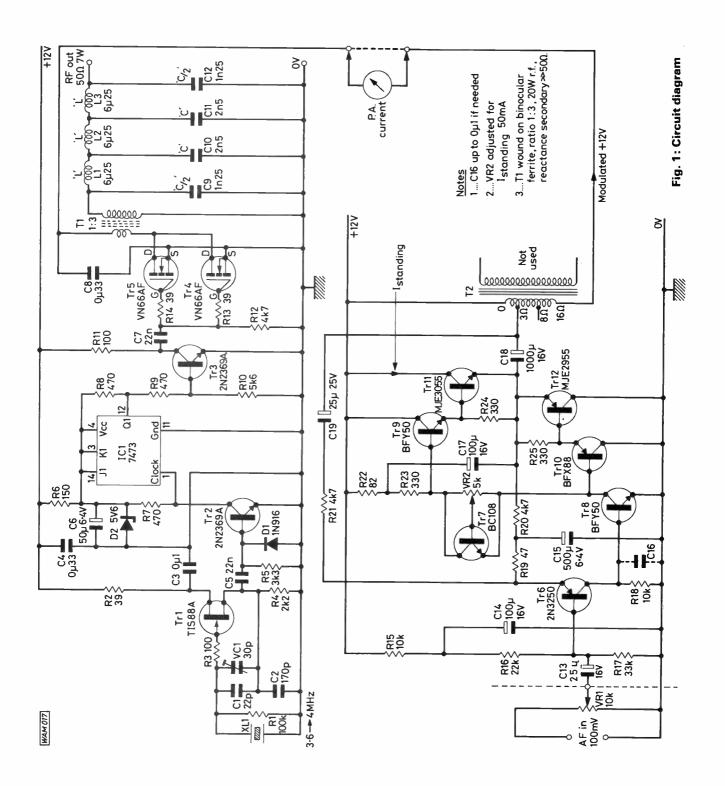
fixed in the same manner, if preferred).

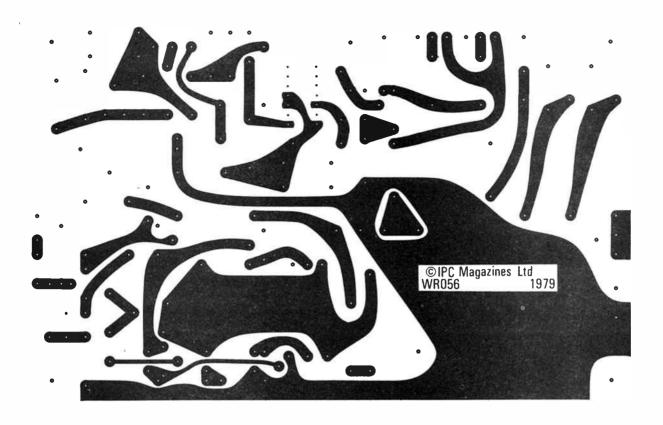
For the prototypes, the p.c.b.s were made by the rather laborious drilling-painting-etching-cleaning techniques, which are more arduous than difficult. However, constructors who wish to purchase ready-made boards will find them available from advertisers.

Components used in the output filter should be exactly as specified—i.e., abnormally high voltage capacitors to take high circulating currents and air-cored inductors to

avoid the saturation which would occur with the smaller type of ferrite cores. Remember that the filter is passing 6-7 watts of r.f. energy and retaining 1-2 watts of harmonic energy.

Loss of harmonic power and the bottoming resistance of the power f.e.t.s are the principal causes of efficiency loss in this transmitter. The filter values may be "scaled" for other frequencies.





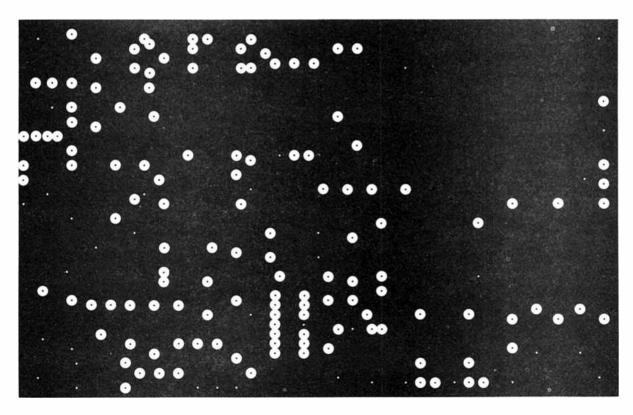


Fig. 2: The copper track side of the p.c.b. is shown full size at the top with the copper ground plane on the component side below it.

* components

Resistors		न	Semiconductor	18 %	
1 watt 5% Metal	Oxide		Diodes	3	de la
39Ω	3	R2, 13, 14	1N914 - 1	1 5	D1 1N916 may be used
47Ω	1	R19	1N5339B	1 -	D2 5.6 volt Zener
82Ω	1	R22	71100005		•
			Transistors		
100Ω	2	R3, 11—see text		4	T-1
150Ω	1	R6	TIS88A	1	Tr1
330Ω	3	,R23, 24, 25	2N2369A	2	Tr2, 3
470Ω	3	R7, 8, 9	VN66AF	2	Tr4, 5 (from C. Bowes & Co.)
2-2kΩ	1	R4	2N3250	1	Tr6
3-3kΩ	1	R5	BC108	1	Tr7
4.7kΩ	3	R12, 20, 21	BFY50	2	Tr8, 9
5-6kΩ	1	R10	BFX88	1	Tr10 °
10kΩ	2	R15, 18	MJE3055	1	Tr11
22kΩ		R16	MJE2955	1	Tr12
	1		WI3E2955	'	1112
33kΩ	1	R17			*
100kΩ	1	R1	Integrated circui		104 CN74C7C11 / 111
			SN7473N	1	IC1 SN74S73N for higher
					frequency operation
Potentiometers		VIDO 61 1			
5kΩ	1	VR2 Skeleton pre-set	Crystal		* 9
10kΩ	1	VR1 Log. Panel mtg. pre-set		fragus	ency HC6U type, parallel-resonan
		with locking nut and cap	ALI IVVICE-I	reque	mey 11000 type, parallel-lesolidii
Capacitors			Inductors		
Silver Mica			Calculated filter	r valu	ues for 160 metres:
22pF	1	C1	$6.25\mu\text{H}$, fc = 2.		
				2	
170pF	1	C2 180pF may be necessary	L1, 2, 3	20	turns of 26 s.w.g. enamelled
			L1, Z, 3		per wire on 25mm long 8mm
Ceramic disc	_				
22nF	2	C5, 7		diar	neter former, air cored.
0·1μF	2	C3, 16 see text			
0.33μF	2	C4, 8			· · · · · · · · · · · · · · · · · · ·
					m / 1 / 1 / 1
Polystyrene 350	volt		Transformers		· 8
1.25nF	2	C9, 12 (Use 1·2nF)		rating	g r.f. transformer (peak). Turns
2.5nF	2	C10, 11 (Use 2·2nF)			ndary reactance $\gg 50\Omega$, wound on
Z-511F	2	CTU, TT (USE 2.2HF)	ratio 1.3,	incou	lar balun-block ferrite (or 3 type
Tomas house has a fire	101	4			
Tantalum bead, 1			FX2249,		•
25μF	1	C13			speaker matching transformer
47μF	1	C14 100µF may be used			$\delta\Omega$ taps. The step-up ratio using
					1.3Ω as input and 16Ω (or 15Ω)
Electrolytic, axial	leads		as output	is a fr	action in excess of 1:2.
25μF 25V	1	C19			
50μF 6·4V	1	C6			
100μF 16V	1	C17			
220μF 16V	i	C15 470µF may be used			
		C18	Hardware	140 -	In VINCEAE PROSTER /21
1000μF 16V	1	CIO	Insulating k	its f	or VN66AF transistors (2),
			MJE3055 an	d MJ	E2955. Socket for crystal. 50Ω
			BNC conne	ector	(or SO239). West Hyde
Trimmers			Development	s ins	strument case type "Classic"
Dau type cerami	c		CL2ADK (Se	e ad	vertisers' index). Printed-circuit
		VC1 see text (from J. Birkett)			

Setting Up

A very short section this! No tuning is required and the r.f. strip should work straight away. The d.c. input current to the final stage can be monitored and should be about 800mA when looking into 50Ω . Other loads will affect the p.a. current and in extreme cases may require some sort of matching transformer.

Poor quality "inactive" crystals will reduce the oscil-

lator drive level and this may reach proportions where Tr2 will not switch and consequently there will be no output.

The quiescent current of the modulator should be set at around 50mA by means of VR2. If this adjustment is a smooth one all is well, but if the current flicks up to a high value check for amplifier instability. This can be cured by fitting C16, which also helps to keep r.f. from reaching the modulator.

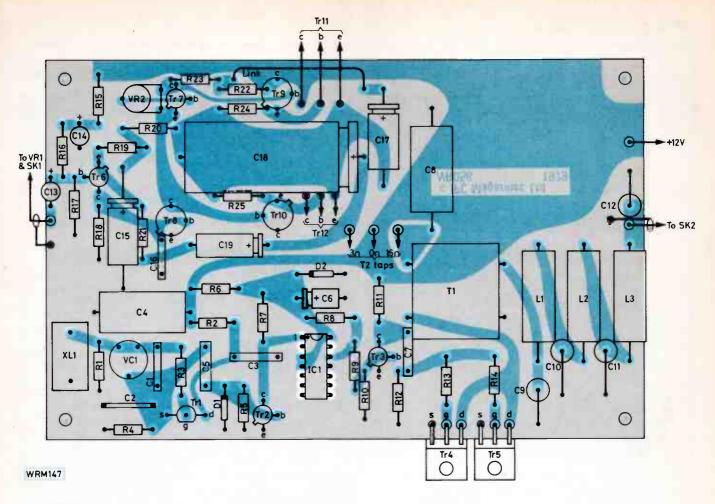
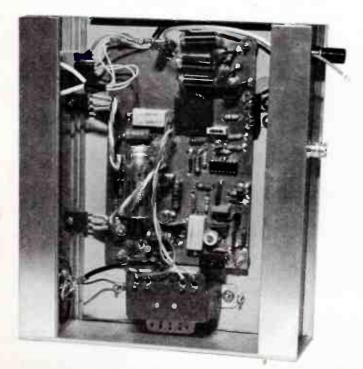


Fig. 3: The component placement drawing of the p.c.b. showing the ground plane (component) side of the board.



Aerial Matching

Most low-frequency aerials in amateur use are unlikely to present a good 50Ω match due to their small electrical size. The following techniques, based on a little theory and a lot of experimentation, are suggested.

The transmitter filter is quite tolerant of a mis-match—say $30-80\Omega$ —but placing a low impedance load on the output may violate the d.c. input power requirements. A really low load will cause the VN66AFs to overheat, but do not worry if this should occur; adequate protection is afforded within the devices, and they will merely shut down.

VFO Operation

Those who develop the transmitter may well wish to add the facility of v.f.o. operation. This is easily achieved by feeding the twice-frequency v.f.o. signal, at 2 volts peak-to-peak, into C5, in place of the injection from the crystal oscillator.

No problems with f.m. pulling should be encountered, as the v.f.o. and output frequencies are not the same.

Well, now you know how to build and operate your VMOS transmitter. Incidentally, the VN66AFs should only cost around £1 each. We hope it brings you enjoyment.

Changes in

BROADCAST-BAND LISTENING

on Short Waves

PART 1

Jonathan MARKS

If you follow Practical Wireless regularly, then by now you may have put together or bought a short-wave general coverage receiver. Tuning around between 3 and 30MHz it soon becomes apparent that the spectrum is divided into blocks which are used for various purposes. If you listen between the frequencies 5950-6200, 7100-7300, 9500-9775, 11700-11975, 15100-15450. 11700-11975. 9500-9775. 17 700-17 900. 21 450-21 750 and 25 600-26 100kHz you'll hear radio programmes originating from broadcasting organisations all over the world. These radio stations are obviously different from the BBC or IBA domestic broadcast channels that the general public are used to, since their target audience is often a whole continent if not the world, rather than a single country or indeed a particular town.

A first flick through any short-wave (usually abbreviated to s.w.) broadcast band may prove disappointing. Many stations seem to be talking in foreign languages and are all crowded together. The secret with this hobby though is slow, careful tuning and frequent checks on "who's around". Most stations put out a magazine-style programme of about half-an-hour's duration in a number of languages, and with English the most common international language there are few stations without an English section. Indeed many s.w. stations broadcast specifically to Great Britain and Ireland every evening with programmes in English.

Station Types

Short-wave broadcasting stations fall into two main categories. The first group of stations aim to provide their listeners with news which is unlikely to hit world headlines (and therefore overseas newspapers and radio bulletins), yet never-the-less would be interesting to people with a

ABOUT THE AUTHOR

Jonathan Marks is a broadcaster/journalist who formerly worked in Vienna for the Austrian Radio Short Wave Service, becoming involved with the weekly SWL news programme "Austrian SW Panorama", broadcast world wide every Sunday. Since returning to the UK, he has continued to make regular contributions to the programme, and is an active DX enthusiast desire for information on world events and culture. Such stations are usually given a grant by their government, but the journalists and broadcasters are given a free hand to make programmes without government censorship. Hence the programmes give an objective, often critical insight into current affairs in the country, the reaction of its people to world events and a sample of the culture, music and perhaps even language. Stations in this category include Radio Finland, the Swiss Broadcasting Corporation, Radio Canada International, Austrian Radio, Radio Sweden and the BBC World Service.

In the second category are the government-run stations, whose main aim is to put over the political views of the government in power. As a result programming is rather one-sided, promoting only national achievements and churning out masses of statistics. That aside, such stations can be a source of quite fascinating information, and it is often interesting to compare their version of a news story with others, either in your national newspaper or on TV. Such government-run stations include Radio Moscow, Radio Peking, Radio Berlin International, Radio Tirana and the Voice of Vietnam.



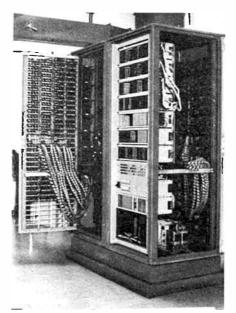
A view of the BBC Monitoring Service listening room, as seen from the console

Photo courtesy BBC



Austrian Radio studio centre in Vienna, with s.w. section in foreground

Photo courtesy ORF, Vienna



Computer-controlled switching gear selects appropriate transmitters and aerials to suit propagation conditions

Photo courtesy ORF, Vienna



Continuity suite for Radio Sweden.
The cartridge machine on the left provides multi-lingual station identifications

Photo courtesy Arne Skoog, R. Sweden

Reception Reports

While reading PW's "On the Air" feature you may have heard of QSLs and reception reports. These are really terms adopted by the broadcasting stations from the amateur radio world, and go back to the early thirties when many s.w. stations started up. In those days, stations didn't know if they were being heard in the target areas at all, and so in return for a listener sending in a report of reception (containing details of time, date, frequency and quality of reception, plus notes on the programme heard and receiving equipment used), stations would issue a confirmation card or QSL. This consisted of a picture postcard with the time, frequency and date of the transmission heard confirmed in writing on the back.

Many stations still send out QSLs, but since the thirties there have been a lot of changes on the technical side. Stations now use very much higher power (many in the order of 500kW), and because of the existence of professional monitoring stations, the larger broadcast stations know exactly how they are being received in target zones. Thus, as far as these stations are concerned, listeners' reception reports are now of marginal interest and the QSL card is more of a public relations venture since the reports are not checked. However, the smaller stations operating in only a few languages (especially religious stations), still need reception reports from listeners. They have only a limited budget and very much lower powered equipment, so regular reports on more than one frequency remain very important.

How can you judge if the station wants your report? The answer is to look in an excellent annual publication called the *World Radio and Television Handbook* which is available through most bookshops. It lists all known radio organisations in the world and where and when to listen out for them. It will give you a clear idea as to the size of the station, its QSL policy and the exact address to send your report to. In general, the smaller the station the more welcome your reception report, with the exception of small stations in West and Central Africa and South Amercia. Stations in these areas use s.w. for domestic broadcasting

in much the same way as v.h.f. is used in Europe, and distant reception reports are usually QSLd only out of courtesy.

Programmes

All international broadcast stations, large or small, welcome your comments on the programmes heard. Over the last 10 years, programming standards have improved enormously compared with the sixties when most stations were of the "cold war" variety, deadly dull and boring. Then, the hobbyist could do little but send a technical reception report. In 1979, though you'll still find some pure propaganda stations, most stations in the Western world (and even a few in the Eastern Bloc) have woken up to the fact that sheer political fact switches Mr Average SWL off. Instead you can now find interesting, wellpresented cultural material, whether it be tips on hitchhiking across Sweden, eating out in Brussels, getting around in Tokyo or exploring caves in the Alps of Austria. Younger listeners too are catered for, with music programmes which broaden one's outlook on the pop music scene and enable one to get world-wide contacts. It is also important to point out that listeners who provide stations with critical constructive comments are well respected by the editorial staff.

Who listens to these international s.w. programmes? In the UK, s.w. broadcast listening is not widely known. Radios sold today in the average British hi-fi shop have no facilities for s.w. listening, but this is not the case in other parts of Europe. In West Germany or Finland for example, thanks to publicity of SWL clubs and the availability of suitable sets, SWL means more to the man in the street. There are signs though that the UK may be catching up on its European neighbours, as good s.w. receivers become cheaper thanks to integrated circuits. and digital readout eases the tuning problem. Also with more holidays being taken abroad, people like to keep in touch with countries they've seen. In the USA and Canada, s.w. is catching on simply because listeners are fed up with their local station full of commercials, time and weather men and rip-and-read news.

The more factual style of s.w. is also important in the developing countries, where radio is very different to Europe. There is usually no v.h.f. or m.w. service, and s.w. radio is the only means for the government to reach listeners in its own country. Thanks to ionospheric propagation though, signals from other countries (e.g. in Europe) can also reach developing countries. The BBC's African Service for example, thanks to a network of onthe-spot correspondents, provides a very fast, accurate picture of what is going on in Africa for African listeners, often before the national radio station reports it. Of course politics comes into play here. Many stations in the Western world beam vernacular programmes towards a developing country which disagree with what the national government station in that country is saving; something which often worries the latter if it is trying to influence its population.

Local Stations

Most stations in Latin America broadcast on the 60 metre tropical s.w. band (4750–5060kHz) instead of medium waves, which are full of static due to tropical thunderstorms. Propagation is such that from about midnight until dawn in the UK you can hear these stations broadcasting to their local population: an excellent insight into Latin America with wide opportunities to study the language or simply enjoy the music. Such small stations in the jungle run on a shoe-string and provide amusing stories for those who've visited them.

The official time signal on one station in Peru for example, turned out to be made by a simple audio oscillator triggered by the DJ watching the second hand on an ancient clock. A station in Bolivia came up on the wrong frequency for over a month because the station engineer had plugged in the wrong crystal. Similar stories come from Asia where the national station in Nepal sometimes comes on the air late when they forget to switch on the carrier of the transmitter. All this added together makes for a fascinating hobby.

The secret is to know when and where to look. One of the best ways is to contact one of the UK Broadcast DX Clubs as well as reading "On the Air". In addition stations themselves put out SWL programmes to assist listeners, for example: Sweden Calling DXers (Radio Sweden), World Radio Club (BBC World Service), Austrian SW Panorama (Austrian Radio), World DX News (AWR, Portugal) and DX Juke Box (Radio Nederland) to name just a few. In addition, an organisation exists in the UK, called the Handicapped Aid Programme, to help introduce this hobby to the disabled. Undoubtedly, broadcast listening can open up new horizons for a person who is house-bound, and no licence is needed.

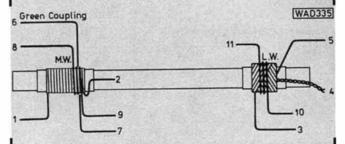
Finally, if you would like to combine your hobby with a holiday, then you might consider joining a DX camp for a few days. These take place during the summer months in Austria, West Germany, Sweden, Finland and, starting in 1979, in the UK. These meetings offer an excellent chance to try out new equipment and antennas as well as meeting fellow DXers and SWLs. Such camps are often coordinated under the European DX Council which acts as an umbrella organisation for European clubs and has a number of useful publications for broadcast band listeners. Meetings on a local basis also explode the myth that a typical SWL is someone who hibernates in his shack, to find friends all over the world but none in his own country!

CONTINUED NEXT MONTH

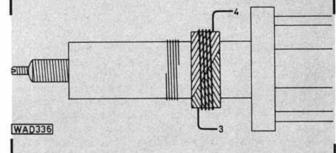
KINDLY NOTE!

PW Imp 3-Waveband Receiver May 1979

The details of the extra windings to be added to the coils were unfortunately omitted from Figs. 5 and 6. They are given below.



Additional reaction windings. 38s.w.g. enamelled copper wire. 8-9, 2 full turns in sense shown above; 11-10, 2 full turns in sense shown above. Note that the coils should be on the rod as shown so that the windings are in the same direction from the 'live' ends (1 and 3).



Reduce winding 5-7 to 2 turns. Add 12 turns of 38s.w.g. enamelled copper wire on top (3-4) in direction shown above.

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RADIO

SPECIAL PRODUCT REPORT

FRG-7



GENERAL COVERAGE RECEIVER



There are many types of communications receivers currently available, the choice of which is initially determined by where the user's interests lie. General-coverage receivers, as the name implies, cover a range of frequencies which include broadcast bands, amateur bands and other communications channels, and the Yaesu FRG-7 falls into this category.

On the other hand, if only the amateur bands are required, then receivers for this purpose, offering a greater bandspread over these frequencies, are available.

In both instances, the tuned frequency may be displayed by "conventional" analogue means, or a digital readout, which gives the tuned frequency in illuminated digits.

The FRG-7 tested by PW was already fitted with a digital readout when supplied by SMC Ltd. This is an option which can be retro-fitted to existing FRG-7s and replaces the original dial unit with a $4\frac{1}{2}$ -digit red l.e.d. display. The digital display indicates the kilohertz part of the frequency to which the receiver is tuned, while the megahertz part is set using the original MHz knob in conjunction with the "Lock" indicator lamp and the "Band" switch.

A Preselector control is provided which enables the r.f. circuits to be tuned for optimum signal. This control operates a vertically mounted drum which has four bands marked on it. The Band switch selects the basic range over which the Preselector and MHz controls operate, at the same time illuminating the appropriate preselector band.

The "Lock" indicator lamp is extinguished when the MHz tuning control is correctly set to mid-band.

The main tuning control is fitted with a large diameter handwheel knob which has a large felt washer fitted behind it to provide a measure of friction although by no stretch of the imagination could the control be described as flywheel. The fine tune control is fitted just to the right of the main tuning knob and was positioned too close to the main knob for comfort. It proved to be annoying when, after getting the main control set, operating the fine tune meant that one's thumb or index finger caught the large knob putting the set off tune. The fine control also seemed to be much too coarse in operation making precise adjustment of setting, so

essential for successful s.s.b. listening, very difficult. In fact with an adjustment of $\pm 6 \text{kHz}$ over 180° swing it was only four times better than the main control and it was almost as easy to set the tuning using only the main control and ignoring the fine one. As supplied the fine control operated in reverse to the main control but this was easily altered by slackening the grub screw of the knob and turning the mab through 180° .

An input attenuator is fitted with a three position which labelled DX, NOR, Local. The handbook indicates that the DX position a station which is swamping the set cat be attenuated to enable a weaker distant station to be received. We were not able to verify this as in the Bournemouth area no signals seemed strong enough to overload the front-end. All the attenuator seemed to do was cut down the signal strength, so the set was operated with the attenuator in the normal position.

The Tone switch changes the audio response of the receiver and has three positions, 250Hz to 3kHz, 400Hz to 2.5 kHz and 250Hz to 1.5 kHz.

The other front panel controls fitted are a volume control and the Mode switch. A horizontal scale S-meter is fitted above the tuning dial. The dial lamps can be switched off independently of the main power, which cuts down on current drain from the battery pack when running from batteries.

The audio output, rated at 2 watts, is not hi-fi but is presentable and enables the receiver to be used on the broadcast bands.

A pair of phones can be used instead of the speaker fitted, the phone jack being on the front panel together with the jack for the record output.

The performance of the FRG-7 on a.m. was excellent with a very good single-signal response. However, on s.s.b. and c.w. the set lacked selectivity with the standard filters. Alternative filters are available as optional extras but were not tried in this test.

Three sockets are provided on the rear of the case for aerials. Two of these are push-type terminals for long-wires while the third is a SO239 socket for use with a coaxial type

THE WADLEY LOOP

The FRG-7, in common with many other contemporary communications receivers, employs the Wadley Loop, triple-conversion superheterodyne system. This offers a number of advantages in terms of performance.

A high first intermediate frequency can be used, in this case around 55MHz, giving good image (second-channel) rejection. The problems inherent in achieving satisfactory frequency stability in the first oscillator ("MHz Set"), which must operate in the v.h.f. band and tune over a range of some 30MHz (55·5–84·5MHz), are overcome by mixing its output in twice, so that any errors due to drift are self-cancelling.

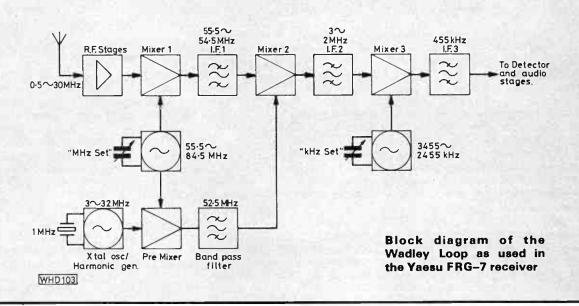
As shown below, this is done by mixing the first oscillator output with a spectrum of harmonics from a stable 1MHz crystal oscillator. The product at 52.5MHz is selected by the Band-pass Filter and mixed with the 1MHz-wide band of signals coming from IF1 to translate them to the band 3-2MHz for IF2.

The output of IF2 is mixed with the output of the "kHz Set" oscillator in Mixer 3. Because this oscillator operates at a reasonably low frequency, and over a band just one megahertz wide, it is not too difficult to make it adequately stable. The output of Mixer 3 is at 455kHz, and is passed to a conventional i.f. filter/amplifier chain, detectors and a.f. stages.

Because there are no conventional band switches other than in the r.f. preselector stage, problems due to varying contact resistance in the oscillator circuits (a common cause of instability) are eliminated. Because the whole range of 0.5–30MHz is tuned in bands 1MHz wide, the tuning resolution of the receiver is the same at 1MHz as at 30MHz.

Disadvantages of the system are the large number of mixing stages employed, calling for careful screening and filtering if spurious products are to be kept low, and the need to design efficient filters operating in the v.h.f. band, for IF1 and the Band-pass Filter.

The actual frequencies adopted in the early stages of receivers using the Wadley Loop principle vary between different models; those shown here are as used in the FRG-7. Anyone checking the sums for themselves may wonder about the fact that the "MHz Set" oscillator tunes down to 55.5MHz, which is within the passband range of IF1, inferring that the receiver will tune down to zero frequency! In fact the lowest band is cut off at just below 0.5MHz by the response of the r.f. stages, and on that band, the signals passed to IF1 are limited to 55-54.5MHz and those in IF2 to 2.5-2MHz. The "kHz Set" oscillator only tunes over 2955-2455kHz on this band. In many Wadley Loop receivers, IF2 is fixed-tuned with a 1MHz passband, but in the FRG-7 it is tuned in step with the "kHz Set" oscillator.



feeder and this is electrically common with the push terminal labelled SW1. This can cause confusion since the coaxial socket is labelled SW1 on the circuit diagram, SW2 on the receiver back panel and to add to the confusion a label immediately above the aerial sockets gives the ranges as SW1, SW2, SW3 and SW4.

The handbook provided with the set was generally good, with an adequate circuit description, a full circuit diagram drawn reasonably well and very legible, a block diagram of the set and a comprehensive components listing.

The operating instructions were generally good but there

were some omissions. The English was very good for a Japanese model with none of the usual funny sentences which seem to occur during translation from the original.

Maintenance and alignment information together with a voltage chart and p.c.b. component layout drawings should help if it is ever necessary to overhaul or repair the set.

As well as the operating manual, the FRG-7 is supplied with two lengths of copper flex for use as aerials, all the necessary plugs and two spare fuses.

The maker's guarantee is for twelve months but does not include the semiconductors.

Practical Wireless, July 1979

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Input Impedance: 0.5MHz - 1.6MHz High

Impedance

 $1.6 MHz - 29.9 MHz 50-75 \Omega$

unbalanced

Output Impedance: 4Ω

Audio Output: More than 2 watts

Power requirements: 100/110/117/200/220/234V

a.c. 50/60Hz or 13.5 d.c.

Negative ground

Batteries: Type UM-1 x 8

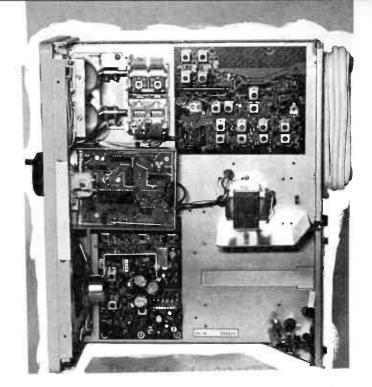
Dimensions: 340 x 153 x 285mm

Weight: 7kg without batteries

The standard of engineering is excellent as can be seen from the photograph of the inside of the set we tested.

The receiver was subjected to several air-tests, using a variety of antennas, ranging from a 132ft long wire to a multi-element rotary beam. On the broadcast bands the receiver performed very well indeed and the s.s.b. capability for amateur reception was also quite good. (The latter mode can be quite dramatically improved, incidentally, by the inclusion of the mechanical filter, produced for the FRG-7 by Ambit International.)

The Wadley Loop provides a good degree of stability in the receiver. This is especially necessary for acceptable sideband resolution—at 29MHz, for the receiver to remain within about 25Hz of the tuned frequency, a stability factor of about one part per million is called for. Long-term stability is perhaps less important to the amateur than stability in the short-term, and the FRG-7 performs quite well in this respect. However, since the Wadley Loop system involves multiple conversion, it is difficult to achieve a wide dynamic range, a problem which is overcome to some extent in this receiver by the use of a balanced mixer.



Internal view of the Yaesu FRG-7

Used in conjunction with a 400 watt p.e.p. transmitter, the receiver performed well. Many contacts were made with W, VK, ZL, ZS and so on, some of these on a simple end-fed long-wire antenna. Copy on the h.f. bands was good, but on the more congested frequencies—such as 40m—it was often felt that a little more selectivity would have been nice. Still, "You pays your money . . ." as the old adage goes, and the FRG-7 represents particularly good value.

A 2.4kHz mechanical filter to improve the s.s.b. performance is available from Ambit International, 2 Gresham Road, Brentwood, Essex, priced at £15.30 (inc VAT). We understand that a Yaesu approved s.s.b. filter may be available from SMC in the very near future.

Prices

Basic FRG-7 receiver £210.37 FRG-7 receiver with digital readout £270.00 Yaesu approved digital readout (SMC) £56.25 (All prices quoted include VAT and carriage)

The FRG-7 receiver reviewed was kindly loaned by South Midlands Communication Company Ltd., Osborne Road, Totton, Southampton SO4 4DN. Tel: 04216 7333, and we would like to thank them for their invaluable assistance in this respect.

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Continued from page 37

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should not be taken to Vss via any wire connecting the c.m.o.s. to Vss. When Tr21 is switching a full 140mA, some very strange arithmetic may be evident from the counters if some of the wiring to Vss is common! Anyone contemplating a p.c.b. design is especially warned of this point.

In order to make the touch plate as mechanically simple as possible, a 6BA cheeseheaded bolt was mounted on (but insulated from) the metal front panel and recessed so that the head was flush with the panel. The entire box was earthed and connected to the mains transformer screen, and connected to Vdd via R26 (see Fig. 6).

In this way, a finger placed on the head of the bolt must also touch some of the surrounding painted panel, and this provides sufficient base current to operate the Darlington pair, Tr1 and Tr2. The instrument is thus electrically safe while providing 100 per cent reliable touch operation of the swept-frequency clock.

Fault-finding

It may be found that, on closing S1, the clock does not run. Decreasing R4 to $82k\Omega$ will solve the problem. Similarly, in the swept-frequency mode, it may be found that the clock is still "ticking over" even when C2 is discharged. Increasing R1 to $47k\Omega$ should stop the clock.

These problems arise because of the 5% tolerance resistors used to derive quite a precise voltage at point A (Fig. 2). The author has not found this to be a problem, but theory shows that it is quite possible.

The mains switch, S5, is a d.p.d.t. slider switch mounted on the side of the box adjacent to the top of the front panel. It is thus normally out of sight, reducing the temptation to tamper with it.

Summary

This instrument is designed to appeal to children of $2\frac{1}{2}$ years upwards. The visual effects produced by it are pleasant and interesting. There are switches to use, buttons to press, a knob to turn, and a touch-controlled flywheel display. It aids in the teaching of rapid number recognition and matching, without obviously being a "teaching" toy.

It can also be used as a die for other board games when the numbers themselves have become of secondary importance.

With a little judicious help, the child will soon grasp the cyclic nature of counting in the decimal system—the progression from single-digit numbers to dual-digit numbers, the second (tens) digit being the number of complete revolutions of the flywheel, the first (units) digit being the number at which the flywheel stops.

A REVIEW OF RECENT DEVELOPMENTS

In general, the author does not have any more information on products than appears in the article.

Microprocessor Miscellany

People have long been chanting that microprocessors are going to end up in "everything". One of the latest applications to reach my ageing eyeballs is in typewriters. The new ET 221 for example is not the established "golfball" but a "daisywheel". Built-in is a Z80-based system that uses a number (note: not just one) of 8-bit, single-chip microcomputers. To be sold in the US for under \$2000, this new wonderwriter has a 20-character display for showing what you've been typing in line at a time. It can also store lines and page formats too, so it appears to be bordering on a form of word processor.

Another microprocessor application to loom is in controlling motors. When one considers that there are virtually millions and millions of motors in so many different applications, the enormous market becomes apparent.

There are some very good reasons, too, for using microprocessors in this application. The first is that old chestnut-money. For example, many motors rely on costly feedback loop circuitry required for close speed control. It has been claimed that just over £1 worth of digital chip can replace £5 worth of analogue circuitry to do the same job. The microcomputer can also do far more than adjust speed. For example, it can check the motor current against a table of maximum values which it holds safely stored in its ROM. This very same ROM can contain a program that limits both the instantaneous and surge currents drawn by the motor at any given time. This, besides offering a safety factor, also allows the manufacturer to use smaller, and probably cheaper motors to do exactly the same job.

Big Bang Theory

A few Ginsbergs ago I mentioned Lithium batteries. They appeared to offer advantages, but I now hear of disadvantages—like they explode. Perhaps not all Lithium batteries do this, but it is reported from America

that the powerful Federal Aviation Administration has ordered that Lithium-Sulphur-dioxide batteries must be removed from emergency aircraft locator transmitters within 30 days. Apparently half a dozen or so reports were received of LiSO₂ batteries exploding. Some 6000 aircraft in the US carry equipment that uses LiSO₂ batteries.

Mon Dieu

I note with great interest that a British company has come up with an i.c. certain to cause a linguistic stir. By adding it to your teletext/viewdata decoder set, you can have the potential to display the whole lot in one of 28 different languages—Ha so! Perhaps you don't get the whole 28 in one go, but an order has already been received for the chip from across the pond in Canada, where the new i.c. is to enable delighted viewers to see viewdata information in a 20-row format (32 characters/row) in English and French. Had this happened when de Gaulle was in office, the designers would have been given the Legion of Honour and free wine for life. How about it. Giscard?

Stable Arrays

And pleased I am, too, to tell of another British achievement. A well-known establishment has come up with a new way of addressing twisted nematic liquid crystals. The liquid crystal display matrix can be driven continuously over the whole of its area and thus the annoying flicker associated with multiplexed arrays is eliminated.

Complementary m.o.s. (CMOS) powered by only 15V is used to drive a 100 x 100 matrix at around 5kHz. Researchers believe that 1000 x 1000 element arrays are possible. This, coupled with the low voltages and flicker-free display, could have great impact on the small screen TV and scope development. A pocket oscilloscope with а power consumption of, say, 500mW becomes a reality.

Bye-Bye Noise

The Dolby system of noise suppression in audio and hi-fi equipment is now very well entrenched. But a German company has arrived with an alternative—and the claims are that it's better, too. The new system is called High Com and it claims to be an improvement over the Dolby system in two areas. The first is that it removes an extra 10dB of noise. It is also said to perform this kind act over the audio spectrum—that's 30Hz to 20kHz, not just over a narrow band.

The immediate area of obvious improvement is at the l.f. end. The Dolby system starts to be effective at around 300Hz, so it isn't so effective against our old audio enemy "mains hum" at around 50Hz. The name High Com derives from "high fidelity compander" and during compression the lowest level signals are amplified. Thus any noise that is picked up or contributed by either the storage medium employed or the actual transmission path finds the amplified signal that much stronger and therefore that much higher above the noise level.

The immediate application for such a device is in consumer audio goods and it is rumoured that some 20 European electronics manufacturers are very interested indeed, as are four of the big Japanese producers. One claim is that when the High Com was used on an audio cassette tape recorder, the measured noise was found to be no less than 20dB down. The magic i.c. that helps achieve all these wonderful things is designated U401B and it comes disguised in a 24 pin d.i.l. plastic package. It has been suggested that the new device could be very usefully employed in radio and television. Although it will cost a little more than the Dolby counterpart at present, volume production will doubtless bring the prices tumbling down. Please note: you cannot buy one yet.

Ginsberg

INEXPENSIVE AF electronic voltmeter

M.TOOLEY BA G8CKT

Most multi-range meters offer a rather mediocre performance on the a.c. voltage ranges. The Avo 8 MkIV, which has long been one of the writer's favourite test instruments, exhibits an internal resistance of only 250 ohms on the most sensitive (2.5V) a.c. range. This is clearly very unsatisfactory regarding sensitivity and circuit loading when measurements are to be made on today's electronic circuits. The instrument described was therefore developed as a replacement for the Avo on the a.c. voltage ranges and it offers the advantages of a $1 M\Omega$ constant input impedance on all ranges and a frequency response which is substantially flat from 10 Hz to well over 100 kHz. Six voltage ranges are provided, with a maximum sensitivity of 100 mV r.m.s.

The unit uses low cost readily available components and can be built for an outlay of around £10. Battery consumption is minimal and a small 9V battery will provide for many hours of operation.

Circuit Operation

The a.c. voltage to be measured is applied to a switched potential divider, R1 to R6. The range is selected by S1 and capacitor C1 is used to remove any d.c. level present on the input voltage. R7 provides a measure of protection for the field effect transistor, Tr1, and C2 provides a degree of high frequency compensation. Tr1 operates as a

source follower and exhibits an extremely high input impedance (greater than $100M\Omega$) thus minimising the loading effect on the potential divider. Tr1 provides a voltage gain of slightly less than unity, the output voltage being developed across R8.

Silicon transistors, Tr2 and Tr3, form a two-stage high-gain amplifier. Both transistors are operated in the common emitter mode. The amplifier incorporates three feed-back loops which help to ensure unconditional stability, a wide operating bandwidth and a high degree of linearity. Stabilisation of the transistor bias is provided by means of direct current feedback from the emitter of Tr3 to the base of Tr2 using R9. C4 provides negative feedback in the second stage of the amplifier. This helps reduce any tendency to oscillation at high frequencies and also ensures that the frequency response "rolls-off" beyond a few hundred kilohertz. VR1, the emitter resistor of Tr2, is used to set the overall voltage gain by controlling the amount of negative feedback present.

Germanium diodes, D1 and D2, from a voltage doubler rectifier arrangement. The arrangement of C6 and C7 provides a means of reducing the surge current through the meter movement during switch-on. Silicon diodes, D3 and D4, provide a "last ditch" protection for the meter movement by offering a shunt path to current when a 600mV voltage drop of either polarity appears at the meter terminals; this corresponds to an eight times overload.

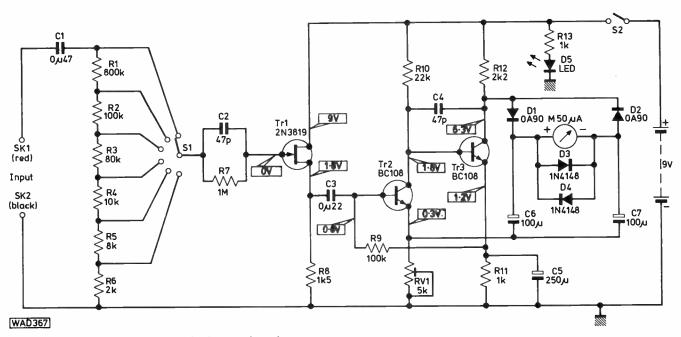


Fig. 1: Circuit diagram of the a.f. electronic voltmeter



★ specifications

Voltage ranges: 100mV, 500mV, 1V, 5V, 10V,

50V

Input resistance: $1M\Omega$ on all ranges

Frequency response: Typically 5Hz to 250kHz at

3dB down

Accuracy: ±5%

Supply: 9V d.c. at 10mA

Construction

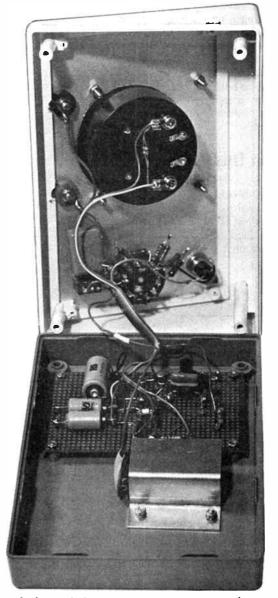
The impedance converter and the amplifier circuit are constructed on a p.c.b. The circuit board layout is shown in Fig. 3. The range selector switch, S1, is mounted on the front panel of the instrument together with the meter movement, power on/off switch, l.e.d. indicator and input sockets. The potential divider resistors, R1 to R6, are most conveniently wired directly to the tags of S1. C1 is wired directly between the input terminal and top end of R1, which is located on S1. Note that the high frequency response of the instrument will depend very much on the stray reactance associated with the input and potential divider wiring. It is essential that all connecting leads be kept as short and direct as possible. The front panel wiring layout is shown in Fig. 4.

Earthing of the metal front panel is achieved by means of the body of \$1, which may be soldered to directly in order to provide a common earth point. If an alternative switch is substituted for the recommended type, it may be necessary to locate a separate earth tag on the front panel. This may be most conveniently accomplished by using one of the meter securing nuts. The front panel is labelled by means of dry transfers, and then sprayed with clear lacquer to protect the transfers. During this operation the meter should either be removed from the front panel or be protected using several layers of masking tape.

The instrument is housed in a standard Vero case. Any other suitable case may of course be substituted provided that any metal parts are connected to the earth or common rail. It was not found necessary to use a totally screened enclosure for the instrument, as with careful wiring there should be no pick-up of hum or stray signals within the unit. The unit will not, however, give accurate indications in the presence of very strong r.f. fields such as may be experienced when measurements are made on medium or high power transmitters.

Testing and Calibration

After completing the assembly of the instrument it is advisable to carry out a thorough visual check of the wiring. Connect a 9V battery to the instrument and measure the d.c. current supplied. If the circuit is functioning correctly this should be approximately 10mA and will vary slightly according to the setting of RV1. Due to a slight difference in the charging currents of C6 and C7, the meter pointer



Internal view of the complete instrument. This is the prototype which used a matrix board instead of a p.c.b.

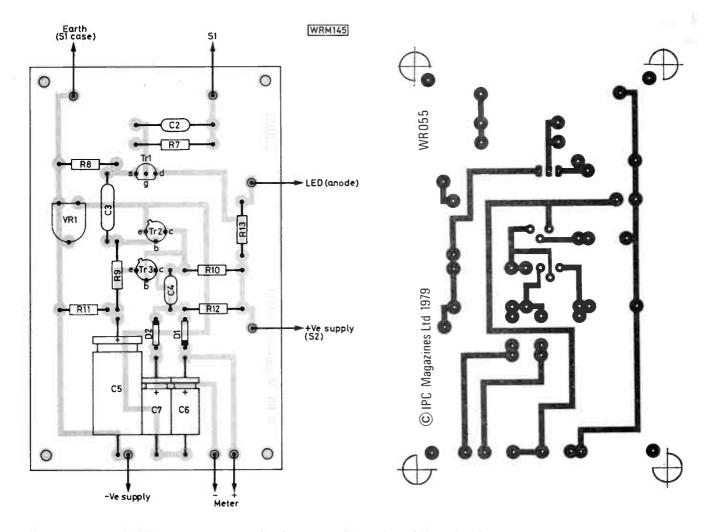
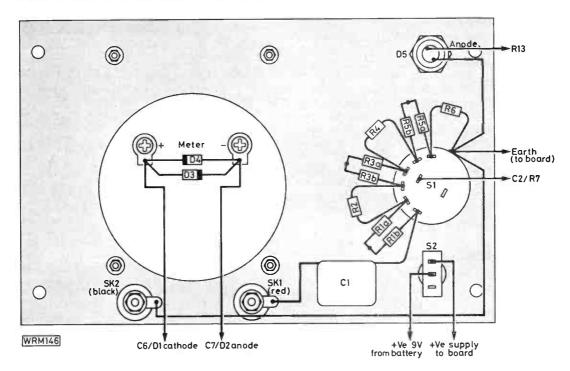


Fig. 2: (above left) The component overlay for the p.c.b. version of the a.f. voltmeter

Fig. 3: (above right) The copper track layout of the p.c.b. shown here full size

Fig. 4: (below) The wiring and layout of the front panel. The resistors on S1 are soldered directly to S1 tags and the end of R6 is soldered directly to the body of the switch



* components

Resistors		
½W 2% metal oxide		
1.2kΩ	1	R5a
2kΩ	1	R6
6.8kΩ	1	R5b
10kΩ	1	R4
12kΩ	1	R3a
68kΩ	1	R3b
100kΩ	1	R2
120kΩ	1	R1a
680kΩ	1	R1b
½W 5% carbon film		
1kΩ	2	R11, 13
1.5kΩ	1	R8
2·2kΩ	1	R12
22kΩ	1	R10
100kΩ	1	R9
1ΜΩ	1	R7
Capacitors		
Electrolytic axial leads		
100μF 25V	2	C6, 7
250μF 25V	1	C5
Polystyrene		
47pF	2	C2, 4
Polyester		
0-22μF	1	C3
0-47μF	1	C1
Potentiometers		
Miniature horizontal pre		
5kΩ lin.	1	VR1
Semiconductors		
Diodes		Park the Story
OA90	2	D1, 2
1N4148	2	D3, 4
LED	1	D5
Transistors		
BC108	2	Tr2, 3
2N3819	1	Tr1
Switches		
1p6w rotary	1	S1
s.p.d.t. min. toggle	1	S2
Miscellaneous		
Case Vero 75-1798-	k 171	\times 121 \times 75mm (1
4mm terminals 1	red, 1	black; Meter, 50p
4 inch scale 110 v	82mm	Printed circuit boar

may give a momentary indication when switching on. The pointer should however return to zero fairly quickly, and if this is not the case the wiring should be re-checked for faults.

To calibrate the instrument a known source of a.c. voltage is required. A signal generator with a calibrated output level may be used, alternatively a comparison may be made with an existing a.c. voltmeter. If neither is available,

a rough calibration can be carried out using a low voltage transformer of known output. A 6.3V filament transformer or the 9V transformer of a power supply is ideal for this purpose. The instrument should be switched to the 10V range and RV1 adjusted for the correct reading. The calibration on the other ranges should follow automatically provided that the potential divider has been wired correctly. If a signal generator is available a check can be carried out on each range. The calibration should be consistent to within ±5% on all ranges. If a signal generator is used, it is suggested that calibration be carried out at a frequency of 1kHz. Where a mains transformer is used the calibration will, of course, be at 50Hz. The frequency response of the instrument should be "good" over a wide frequency range, at least 10Hz to 100kHz at the 3dB points, and the frequency response of the prototype instrument on the 1V range is shown in Fig. 5.

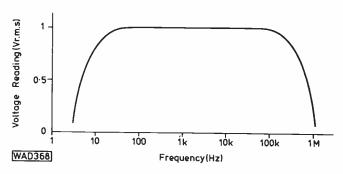


Fig. 5: The frequency response of the instrument

Note that, due to the high input impedance of the instrument, false readings can sometimes be produced on the more sensitive ranges. This is due to pick-up of hum and stray signals on the input leads. The input leads can be screened if desired; the inner lead of the coaxial cable is connected to SK1 (red) and the outer screen to SK2 (black). It is important to note that coaxial cable possesses an appreciable shunt capacitance between the inner conductor and screen (often as much as 100pF per metre). Long screened cables should therefore be avoided since they will impair the high frequency response of the instrument.

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by Eric Dowdeswell G4AR

The problem of identifying correctly an amateur callsign can present a problem to anyone unaccustomed to listening on the amateur bands. It often seems to be a jargon incapable of being decoded! The answer is not always obvious even if the station is in the clear, but if it is being clobbered with QRM then there really is a problem.

Although there is an ITU phonetic alphabet, given below, it is seldom adhered to by amateur operators who seem to use part of this alphabet and part of their own invention. In a perfect phonetic code the word used to represent a letter, such as "alfa" for A and "bravo" for B, must be neutral, one without any particular connotation and generally understood world-wide.

The approved code starts off all right but then uses "Charlie" for C, although personal and place names ought to be avoided since these can be misleading, especially in amateur use, where station locations and operator's names

are constantly being exchanged.

Α	Alfa	J	Juliett	S	Sierra
В	Bravo	K	Kilo	T	Tango
C	Charlie	L	Lima	U	Uniform
Ď	Delta	M	Mike	V	Victor
Ē	Echo	N	November	W	Whiskey
F	Foxtrot	O	Oscar	X	X-Ray
Ğ	Golf	P	Papa	Y	Yankee
H	Hotel	0	Quebec	Z	Zulu
ï	India	· R	Romeo		

There are several words in the phonetics list which I do not agree with personally, but the problem is to find suitable alternatives.

What causes most confusion however is the amateur's own version of the phonetic code, especially the use of "George" for the G in UK callsigns, particularly where the operator is called "Fred"! Might not matter too much among lads and nets on 2m or u.h.f., but used on the DX bands can only make identification of a callsign all that more difficult.

On numbers, the recommended procedure is to use the word "figure" before any number, to indicate that a figure is to follow, thus "Golf, figure four, alfa romeo". This can only help but it is seldom employed by amateurs unless they have been trained on a military or commercial network of some kind. The use of phrases like "Red Hot Momma" for RHM in the suffix of a call may be amusing to some but meaningless to the amateur with little or no knowledge of the English language.

I appreciate that this little homily will have no effect whatsoever, but I hope it will serve to demonstrate to the innocent listener to the amateur bands that there is little or no "system" with amateur phonetics. Initially, it is better to write down in full what is heard and then the callsign ought to become apparent, aided by a good list of prefixes, but, as ever, experience will prove the best teacher.

Here and There

Well known to this column for his SSTV reports in the past, Paul Barker of Sunderland is now busy on c.w. and s.s.b. with his new callsign G4HPS, having started off with G8OVD. Paul's first s.s.b. QSO was with FG7AS/FS7 on 10m, which is enough to make anyone's mouth water! He uses a TS520S transceiver to an 18AVT multiband vertical, plus an FT221R on 2m to an indoor 4-element quad. Paul managed to get QSLs from all six continents for SSTV reports before getting his ticket.

In Southport, Peter Hawks has got going with a DX160 but, like others, found the manual's calibration chart did not match up to reality. He's talking about a digital readout unit but I think he would be better off initially with a crystal calibrator. Philip Charlesworth (Southport) has got going with an outside aerial which he finds "staggering" after his indoor one. As he lives on the only hill in Southport he will find the advantage of much greater importance when he gets his ticket in due course. Philip mentions the PAOAA transmissions on 3750kHz for amateurs, followed by slow Morse transmissions. Details of the latest schedules would be appreciated.

Peter Lucas of Newport, Salop, has dumped his R207 and settled for an AR88 but needs to rewire a lot of it. A circuit or manual would be appreciated at 3 Queen's Drive if anyone can help. Pete's been hearing plenty on 10m of late with only a 16ft vertical. In Chiswick, London, George Gizebieniak BRS 41733 has bought an old SX24 receiver for £20 and found it worked fine on the 10m band, with converters for 2m and 70cm.

An appeal from Jim Timoney ZS1TK for a spare for his KW2000 transceiver, not having had any success with the descendants of KW in this country. He wants the 3-gang tuning capacitor on the pre-selector, part number C40 on the circuit diagram. Any offers of help to me direct please. Another reader in need of help is M. David of 46 Pentathlon Way, Cheltenham, Glos, who has got hold of a Star SR550 for just a £1! It works fine but he'd like a manual for copying and return. He's heard an HK on the 10m band and threatens to send in some logs in future.



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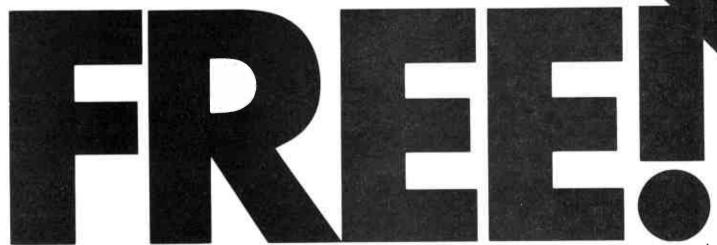
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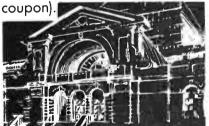
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World Radio History

Mike Stollov of Blackley, Manchester, has not deserted the column although active as G4HWB. Flu laid him low but he was able to drag his FRG-7 to the bedside and keep in touch with the bands on c.w. and s.s.b. Good finds on 15m c.w. were HH2T, HK0BKX, HM1DM and H44LW while on 10m s.s.b. FM7AY, HC1FM, KZ5AS and 6W8AAD were fairly rare ones. After some blush-making comments R. Beswick of "Hillhouse", Yatton-Keynell, Chippenham, Wilts, mentions that he has run through quite a few receivers and now has a Trio 9R59D and a Minimitter MR44, but is sadly in need of a circuit or manual for the latter. Any help direct please to him, all expenses paid of course.

We don't often get any RTTY news but here is **Dennis** Sheppard of Sheppey, Kent, with a long log of stations copied in this mode with Creed page printer, tape printer, tape reader and home-made terminal unit driven from a JR310 receiver. Any other RTTY enthusiasts are invited

to write in with logs, etc.

Australian J. Clark arrived here with his equivalent to the "B" licence and wrote to the RSGB for info on clubs in the Reading area and on the licensing regulations in order to get a full licence while over here. He says: "The RSGB HQ was not particularly forthcoming about licensing exam procedures, nor even too certain about the active status of clubs in this area". Needless to say, he got a full reply from me in a couple of days!

DX Notes

Bill Rendell (Truro) has the solution to the S79MC mystery, straight from the horse's mouth! It is the Seychelles after all. Although Bill heard him some time ago, it was only in the middle of March that the QTH was given, seemingly. Bill has been up at sunrise to find the DX still rolling in on 80m such as C6AFR, CT2SH, HC1NJW, VP1KG plus three ZLs one of whom was mobile "out salmon fishing"! 40m revealed Bill's first GD logging, GD3KGC but little else. On 20m CT2YB on St Michael popped up, with D4CBS, J3ABN, M1D, VP2VBK and VP8SO on Signy Island, not to mention VK3MO reputed to have eight quads in a 4-over-4 arrangement!

The 10m band has been very good at times but several readers comment on weird and variable skip at times, which makes it all the more interesting! P. Lucas of Newport, Salop mentioned HH2LD, H44CF and S79MC on the band, all good catches in the early evening, on his AR88 and vertical. Looking at the c.w. end of bands can produce some unusual prefixes if one is interested in that direction. Mike Stollov found a CP5, EA8, HC2, HP1, OY9 on 20m and HH2, VS6 on 15m, plus KZ5, SV1, 6W8 and 8P6 on 10m. More c.w. logs would be very

welcome.

As usual lan Marquis sorted out the better ones at Leigh-on-Sea, Essex, on his FRG-7, 100ft wire and 28MHz dipole, such as M1C and ZB2CJ on 80m, VP2KF, XE1FU and YN1S on 40m, C6ANX and TR8AC on 15m with HC1FM and HL9KE on 10m, all s.s.b.

Club Activity

Let's start with the **Bury RS** which meets every Tuesday evening at Mosses Centre, Cecil Street, where visitors are more than welcome. June 12 sees G8SCA talking on the joys of medium-wave DXing (how did that get in?) and on July 10 there is a foxhunt for those keen on DFing. QRP-lovers may like to know that **Yeovil ARC's** transmitter G3CMH is reputed to have made the first

solid-state s.w. DX QSO in the UK in 1954, working 90 miles on 80m with 30mW input to a single transistor. The station is still active with QRP so pop along any Thursday evening to Building 101, Houndstone Camp, Yeovil and meet the gang, or write: D. McLean G3NOF, 9 Cedar Grove, Yeovil.

The second and fourth Thursdays of the month, see the Edgware and District RS (Middx), at the Watling Community Centre, 145 Orange Hill Road, Burnt Oak, Edgware. On June 14 a "Bring & Show" your favourite test gear, tools, etc., is a pleasant twist while on June 28 there is a junk sale. Contact: D. Lisney G3MNO, 119 Draycott Avenue, Kenton, Middx. Fridays is the day to find the West Kent ARS at the Adult Education Centre, Monson Road, Tunbridge Wells. On June 22 a Mr Constable will talk on the British Vintage Wireless Society and its work.

Trevor Tugwell G8KMV reports his retirement as Sec of the Stevenage & District ARS and I hope his replacement Ted Godfrey of 94 Common View, Letchworth, will be equally forthcoming with the club's news. June 14 is devoted to a DF hunt, with G4DDX talking about his Top Band DF receiver on June 21.

Don't forget the deadline for copy, the 15th of the

month without fail.

Log Extracts

lan Marquis:—80m M1C ZB2CJ 40m HC4JQ
VP2KF, XE1FU YN1S 20m VP8ML VR3AH VS5XU
8Q7AH 15m C6ANX TR8AC VP9JA 10m HC1FM
HL9KE

R. Bell:—20m OA8ODE 15m JY5ZM P29MF 10m CT2CP KZ5FF YB0ADW

P. Hawks:—20m VK7OH A9XBS CT4UU M1D VP9CP XT2AV

P. Charlesworth:—20m JY8AQ JY0OZ VP9BB 7X2LS 9V1TX

M. Stollov:—20m CP5NK EA8FO FY7BF HC2FN HP1XGL OY9J 15m HH2T H18MOG HM1DM H44LW KL7PJ VS6EN 10m FM7AY HC1FM KZ5AS VS6DT 8P6JQ (Bold are c.w.)

P. Lucas:—10m HH2LD HI8XEA H44CF S79MC

VQ9JJ ZF2CL 9J2LL 9L1KB

W. Rendell:—80m C6AFR CT2SH EA8PP HC1NJW PJ2AAX VP1KG YS9RVE ZF1CL ZL3GS ZL4AP 40m EA8QY 20m D4CBS HP6JB J3ABN J6LFZ M1D VK7AE VP2VBK VP8ML VQ9JJ ZD7PL 15m CT2CP HC6FC J6LDE (St Lucia) S79MC VP5JFH VP8SB (Adelaide Is.) VQ9RL YB0WR ZB2DV

D. Sheppard:—All RTTY 20m A4XFW FP8DF 9G1JX 9J2KD 15m JA1ACB KC6CB LU1NH VE7DIA W7WHY YU3KAA 10m AG2M C5AAN FG7XT JA2JHR KZ5JA VK3KF ZS6AKO 3D6AD 5Z4PD

Reports on the various bands are welcome and should be sent direct, by the 15th of the month, to:

AMATEUR BANDS Eric Dowdeswell G4AR, Silver Firs, Leatherhead Road, Ashtead, Surrey KT21 2TW, Logs by bands, each in alphabetical order.

MEDIUM and SW BANDS Charles Molloy G8BUS. 132 Segars Lane, Southport PR8 3JG. Reports for both bands must be kept separate.

VHF BANDS Ron Ham BRS15744, Faraday, Greyfriars, Storrington, Sussex RH20 4HE,



MEDIUM WAVE DX

by Charles Molloy G8BUS

Are you going abroad for your holidays this year? Then why not take along a portable receiver? As well as providing entertainment, it will give you the opportunity to listen to the medium waves from a new location. I had this experience while on holiday in Bulgaria a few years ago where the medium-wave scene was totally unrecognisable. I could have been on another planet! I even tried to do some DXing but could not pick up either the BBC or Luxemburg on the medium waves, though a weak unidentified on 200kHz might have been Droitwich. It would have been very interesting with a decent receiver and a loop.

Holidays abroad these days generally mean Spain, a country which is very interesting from the radio standpoint. As well as having an official government network, there are several chains of privately-owned local radio stations spread across the country. In most locations there are at least three to be heard during the day-time, while after dark many more are just waiting to be picked up. The holidaymaker also has the opportunity to hear "difficult" outlets such as Radio Gibraltar on 1458kHz.

DXing Spain

No need to visit Spain to listen to Spanish radio. A lot of it can be heard from the UK, and it is quite an interesting area to explore at this time of the year. A loop should sort out much of the co-channel QRM, since the DX is coming from the south while much of the QRM is from the east. The easiest stations to pick up are the high-powered RNE outlets at the l.f. end of the band. Listen to 585, 639, 684, 729, 738, 774 and 885kHz for the call Radio Naçional España.

The real interest for the DXer is with the local radio stations which operate on a number of channels between 792kHz and 1602kHz. The best time to listen for them is between 2300 and 0100 GMT when European QRM slackens off and many Spanish locals themselves close down leaving the frequencies clear for other weaker stations to appear in their place. Try on 1026kHz, 1107, 1134, 1224, 1260, 1314, 1395, 1521, 1539, 1584 and 1602kHz.

Identification

Station identification includes the name of the town or city preceded by one of four titles depending on the particular network such as Radio Barcelona, Radio Popular Malaga, Radio Juventud Murcia, La Voz (pronounced Voth) de Granada. A callsign is allotted to each station which is generally used in the sign-off announcement but it can present a problem to the DXer unless he is familiar with the alphabet and numerals in Spanish. Four sets of three letters plus figures are in use depending on the network. For example, EFE14 is in Madrid, ECS5 in Granada, EFJ56 in Malaga and EAJ1 in Barcelona.

A list of Spanish frequency allocations extracted from the Boletin Oficial del Estado of the 13 November 1978 is available from Keith Hatcher, Duquesa de la Victoria 50bis, Logroño, Spain in return for 2 IRCs or 25 Pesetas in unused Spanish stamps. At the time of writing this is the most up-to-date list available, though it does include some stations not yet on the air.

Reception Reports to Spain

Spanish locals are usually good verifiers even to a report written in English, though a Spanish Report Form (obtainable from DX clubs) is better. A full list of callsigns and addresses is to be found in the World Radio and TV Handbook though the frequency information in the 1979 edition is quite out of date. No need to worry too much about the full address. A report sent to El Gerente, Radio Popular Malaga, Malaga, Spain will certainly find the station. El Gerente being the station manager. Always include return postage, either unused Spanish postage stamps which are obtainable from stamp shops or an International Reply Coupon (IRC). These are on sale in main post offices.

Region 2 Station Separation

According to a report in *DX Monitor*, the Daylight Broadcasters Association (USA) is asking the US government to press for 9kHz station separation plus a slight extension of the m.w. band, as an alternative to the current proposal to the WARC-1979, to extend the band to 1850kHz. The suggestion is that the band should start at 530kHz with stations spaced at 9kHz intervals up to 1610kHz, which would provide an additional 14 channels.

The DBA just cannot be serious! It would mean that the majority of stations in Region 2—North, Central and South America—would be on the old pre-Geneva channels, which incidentally are at the moment occupied by many broadcasters in the Middle East who have not (yet?) changed over. 1kHz heterodynes would be commonplace and a 1kHz audio notch filter would be an essential item in the m.w. DXer's shack. A more reasonable proposal would be to start at 540kHz and follow the Geneva frequencies right up to 1602kHz. This would give 12 additional channels and would not require approval by the WARC as the m.w. band would not have to be extended. It would only require approval by the countries in Region 2.

It is to be hoped that the DBA will not be successful. At present Region 2 is on 10kHz separation starting at 540kHz which is also a Geneva frequency. Coincidence between the two systems occurs at 90kHz intervals across the band but there are other parts where the separation between the two systems is as much as 4kHz and these are the "DX slots" that would disappear if the Geneva Plan becomes world-wide. Fortunately there is likely to be opposition within the USA to the DBA's proposals, as many stations would be put to considerable expense, not just in changing frequency but with modifications to directional aerials which are in widespread use in that country. None-the-less, m.w. DXers will await further developments with apprehension.

Loops in New Zealand

The Loop becomes Respectable is the title of a short, amusing article sent to me by its author Tony King, who is the Mailbag editor of Radio New Zealand. It seems that RNZ decided to restrict its racing coverage, which led to the experimental use of a DXer's loop to get better reception. Soon, a commercially produced "punter's loop"

appeared which was investigated by the NZ Consumers Council, who had to acknowledge its effectiveness. A competitor, the Space Raker soon turned up. This was a loop built into a briefcase for convenience of use and acceptability in domestic surroundings. Finally "the national TV network screened a programme on the loop, the a.t.u. and on erecting an outside aerial, all in the quest for better reception".

DXing does have a large following in New Zealand but I once knew a Kiwi who was a great leg puller, so you can take your choice. Either way, it is an interesting story.

Readers' Letters

Stephen Donnelly wonders how DXers identify foreign language broadcasts. His method is to look for key words (Voiçi=French). This is alright if you have a list of key words but an easier way is to listen for place names. Most countries carry local items in their news bulletins and if, for example, you hear Ankara mentioned several times then you may be listening to Turkey. Stephen has recently acquired a Trio 9R59D and he would like to hear from other users of this receiver. Replies direct to Stephen Donnelly, 25 Church St, Addlington, Lancs PR7 4EX.

From Pensilva in Cornwall comes another letter from reader K. Lewis who has modified the r.f. pre-amplifier intended for use with the PW "Dorchester" Tuner. He used it along with a long wire, a.t.u. and Realistic DX160 to pull in WINS on 1010kHz, Radio Margarita, Venezuela 1020, Radio Coro, Venezuela 1210 and Radio Paradise, St Kitts on 1265kHz, all heard between 0250 and 0330 during March. Listen in mid-summer during the hour before sunrise for this type of DX; results are sometimes very good.

DX Circle is the name of the weekly DX programme in English carried by Deutschlandfunk on 1269kHz each Tuesday at 1900 GMT. It is compiled and presented by DXer Alan Thompson and it has been running now for over 10 years, the session on the last Tuesday of the month being designed especially for newer members of the hobby.

It is nearly 10 years since I met Alan at the DX Convention he organised in his home town, Neath. It was attended by Arthur Cushen who was on a tour from New Zealand at the time, and this was the first gathering of Broadcast Band DXers to take place in this country so far as I know. Alan is the UK/Europe representative for the NASWA/FRENDX, Indian DX Clubs International and the Union of Asian DXers, which means that subscriptions to those bodies can be made through him. Alan can be contacted via the DX Circle, Deutschlandfunk, 5 Koln 51, Raderberggürtel 40, West Germany.



SHORT-WAVE BROADCASTS

by Charles Molloy G8BUS

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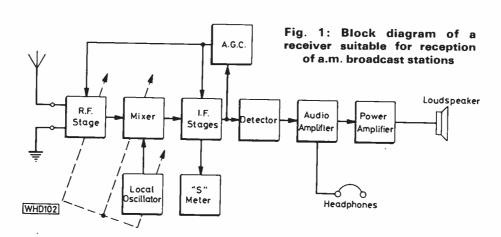
Questions asked by a number of readers recently have prompted me to produce the following few notes written in non-technical language which will, I hope, show how a receiver converts the incoming radio signals into the sounds heard from the loudspeaker or headphones. An understanding of what is happening should help the DXer to get the most out of the quite sophisticated gear that is under his control.

The Superhet Receiver

A block diagram of a superhet receiver suitable for broadcast reception is shown in Fig. 1. Facilities for s.s.b. and c.w. are not included, as these are not generally used for broadcast band DXing. Each square represents a particular job the receiver has to do. Starting at the left-hand side, radio signals are picked up by the aerial and applied to the aerial socket where they pass into the r.f. stage and out again to earth. The r.f. stage selects the wanted signal, amplifies it and applies it to the mixer where a further stage of frequency selection is encountered. The local oscillator is maintained at a frequency 465kHz higher than the incoming signal by the tuning control. The mixer, which is aptly named, mixes the two together and supplies a 465kHz difference frequency complete with modulation (programme) to the intermediate frequency (i.f.) stages. Here the signal is amplified and further selectivity is encountered.

The output from the i.f. stages is applied to the detector where the audio is extracted and applied to the audio amplifier. The output goes either to headphones or to a further amplifier which drives a loudspeaker. The output from the i.f. stages is also fed to the automatic gain control (a.g.c.) circuit, which adjusts the gain of the amplifiers in the r.f. and i.f. stages in sympathy with the strength of the signal.

That, very briefly, is the make-up of the supersonic heterodyne receiver, to give it its full name. In this case the



heterodyne is 465kHz which is the standard value used in the UK. Anyone interested in the history and development of the superhet should try to get hold of a copy of *The Superhet Receiver* by Witts, first published in 1935. There are a number of later editions and although long out of print, copies can be found in secondhand bookshops. This book contains a fascinating account of the efforts of the early radio experimenters to produce a design that is now regarded as standard throughout the world.

Images

To get back to the block diagram. It is important that a receiver intended for DXing should have an r.f. stage. The majority of domestic receivers do not have one, the aerial going straight to the mixer. As well as increasing sensitivity, the r.f. stage helps to reduce what is known as second-channel or image interference. The mixer can produce the 465kHz heterodyne in two ways—by beating with a station 465kHz lower than itself, and also by beating with one 465kHz higher. The second is the image. For example, if the receiver is tuned to 6180kHz (49m band), the local oscillator will be generating 6645kHz and the image will be 7110kHz (41m band). The selectivity in the r.f. stage reduces the strength of the image compared with the wanted signal.

It is easy to tell if a receiver has an r.f. stage. Have a look inside at the tuning capacitor. It should be a threegang, one section for the r.f., one for the mixer and one for the oscillator, all under the control of the main tuning knob. The dotted lines in Fig. I represent the 3-gang tuner. If it is only a twin-gang then there is no r.f. stage. Paradoxically, a receiver without an r.f. stage will sound a lot more lively than one with an r.f. stage. It picks up many more stations, in the example quoted, in the 49m band plus the stronger images in the 41m band. A receiver with poor image rejection will pick up the stronger stations at two points on the dial and this effect becomes worse the higher in frequency you go.

Automatic Gain Control

The a.g.c. does electrically what you can do for yourself manually—turn down the volume when listening to a strong station; turn it up to hear a weak one. The a.g.c. does it much faster and is therefore useful for dealing with fading. There are occasions, though, when you are better off without a.g.c. When two stations are operating on the same frequency, there will probably be a beat of a few hertz, equal to the slight difference between them. This can occur even if one station is a lot weaker than the other. The a.g.c. will follow the beat and may produce an unpleasant blasting effect at the loudspeaker. If you are searching for a weak station close to a strong one then the a.g.c. may respond to the strong station, reducing the receiver gain, so that the weak one is missed.

A.G.C. ON/OFF Switch

An a.g.c. on/off switch is fitted to communications receivers but seldom to other types. If you switch off the a.g.c. then you must be able to adjust the r.f. and i.f. gains, otherwise strong stations will cause overloading, therefore a separate r.f. gain control will have to be provided. In spite of the name, the r.f. gain control usually controls the gain of both r.f. and i.f. stages. To operate a receiver with the a.g.c. switched off; adjust the volume (a.f. gain) to a comfortable level and follow the strength of the incoming signal with the r.f. gain control, which replaces the a.g.c.

To sum up, a receiver for DXing should have an r.f. stage to provide adequate sensitivity and freedom from images. You can check by examining the tuning capacitor. It is also desirable to be able to switch off the a.g.c. but if you do this then you must have a manually operated r.f. gain control as a replacement.

Radio Finland QSLs

From Tullebody in Scotland comes a note from James Thompson who is a civilian instructor on radio with the ATC and a keen DXer. He sent a reception report to Radio Finland expecting to get a listener card in return, but much to his surprise he received a proper QSL giving the date, time, frequency and verifying that the report was correct. Whether this is the result of a genuine change of policy or the result of an error is not clear but let's hope it is the former.

Readers' Letters

The National Panasonic RF1105 is in the news again with a report from E. Roper who obtained his first experience of s.w. listening with this receiver and is more than satisfied with its performance. He finds that by increasing the diameter of the tuning control to 75mm, a more sensitive touch was obtained when tuning. Fitting a large knob to the tuning control is an old dodge, but it can spoil the appearance of the receiver. DX picked up with the RF1105 included Pakistan on the 16m band at 1100, Afghanistan on 19m at 1600 and Radio Australia on 25m at 1900.

"I am at present compiling a survey of the FRG-7 as there seem to be so many conflicting reports about these receivers," writes George Tyler from 41 Park Crescent, St George, Bristol BS. 'AY. George has already contacted about 20 FRG-7 owners and he would like to hear from more as he thinks some hints and guidelines could emerge from his survey. In particular he would like to know the good points, the faults and how the FRG-7 performs with an a.t.u., audio filter, etc. George has promised me a copy of the survey when complete and a summary of it will appear in this column. See also Special Product Report this month. Ed.

Arthur T. Cushen, MBE, writes from New Zealand to say that his book *The World in my Ears* will be published in August or September 1979. It is the story of a blind radio listener who has become a world authority in his hobby and who is a regular broadcaster on RNZ and Radio Nederland. The book, which is partly autobiographical and partly a guide to short-wave listening, can be obtained direct from Arthur Cushen, 212 Earn St, Enwood, Invercargill, New Zealand, at a pre-publication price of £7 until June 30.

DX Heard

Japan has been heard on 9585kHz at 2000, SIO 433 by Chris Howles (Lichfield) using his Vega 206 and 40ft loft aerial. David Stevenson (Thurso) has a National Panasonic receiver and a 100ft length of wire wound round his bedroom and he picked up Afghanistan on 11 805 at 1900 and Taiwan on 15 425 and 15 345 at 0100. Bob Bell (Blyth) reports hearing Radio RSA on 25 790kHz in the 11m band at 1520. According to a recent report in Sweden Calling DXers, IBA Jerusalem is now on 25 640kHz as well as on 25 645, Radio Nederland is on 25 650 at 0800 and the VOA is also on 25 880kHz.

A newly-acquired Sanyo RP 8880 is in use by new-comer to the s.w.s Alan Curry (Stockton-on-Tees) who

pulled in Japan on 15 195 in English at 2300 using the telescopic aerial. All India Radio was logged on 11620 at 2225, SIO 444 with a programme in English about the Indian fishing industry. Mark Hattam (Hereford) is amazed at propagation on the 13m and 16m bands (the higher frequencies are really opening up now). His Realistic DX160 and 45ft long wire pulled in VOA Philippines on 17 780 at 1500, Chile on 17715 at 2330 and Peking 17 680kHz all in the 16m band. P. R. Sixe (Cambourne) is puzzled by Radio Nacional de Colombia which was noted on 13 848kHz and he wonders if this could be the first station to appear on the new 22m band. This band has not (yet) been authorised and you may have heard a harmonic. Craig Kelly (Walsall) has been unable to identify a station on approx 31.2m with the call Hebra Radio (anyone any ideas?). David Grimshaw (Bury) has an FRG-7, long wire and a.t.u., and he reports that Radio Japan comes in well on 17 795 and 17 825kHz, in English, at 0800.



by Ron Ham BRS15744

The propagation of radio waves between two points is a complex subject, because, whatever the wavelength of the transmitted signal it must travel somewhere through the earth's gaseous atmosphere, which, in a variety of ways can be upset by the sun. Every month, with the help of my readers, I endeavour to show what natural events have taken place and how our terrestrial radio communications are affected. New readers to my column often ask about basic reading matter so they can better understand such words as aurora, meteor scatter, sporadic-E, sunspots and solar radio noise, so, my first suggestion is, Chapter 11, in Volume 2 of the RSGB's Radio Communication Handbook (Fifth edition), and secondly, J. A. Ratcliffe's Sun Earth Radio, World University Library.

Solar Activity

On March 21, Cmdr Henry Hatfield, Sevenoaks, recorded bursts of solar radio noise at both 136 and 1296MHz, on the 22nd he saw an active plage through his spectrohelioscope and on the 23rd he counted between 30 and 40 sunspots, in 8 groups, in addition to a long ribbon flare. Nigel Fisher, South-East Essex Astronomical Society, recorded a solar burst at 60MHz during the morning of the 27th and I heard strong solar noise in the 10m band at midday on the 30th. During the BBC's World Radio Club programme on April 8, Lucian Prechner said that ionospheric conditions were disturbed between April 2 and 6, mainly on the western paths, which was no doubt caused by the very large sunspot group, about 35 spots, and a long arched filament which occupied almost a quarter of the sun's diameter. This was a massive affair, bearing in mind that the sun's diameter is about 865 000 miles.

It was not surprising that Henry Hatfield, John Smith, Rudgwick, Sussex, and myself, were recording a solar noise storm, Fig. 2, at 136, 142 and 146MHz during the

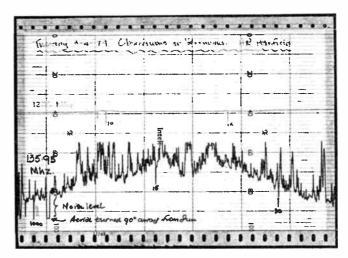


Fig. 2: Chart recording of solar noise received on 135-95MHz on 3 April 1979 by Henry Hatfield

morning and early afternoon of the 3rd. On the 5th, Henry noted that the large sunspot group was declining and the filament was much less active, explaining why we recorded only a few small bursts on the 4th and a slight noise storm on the 5th. Bursts of about 5 minutes duration were recorded around midday on the 8th and 11th, one 1.5 minute burst at 1310 on the 14th, and a 4 minute burst during the midday observation on the 16th.

The 10 Metre Band

Apart from the relatively few disturbed periods, 10m conditions were generally good between March 19 and April 16. On March 22, Harold Goble G4FDQ, Lancing, worked all Continents, UA6, VE, ZL3, 4S7, 5N2, and 8P6, on 10m using his KW 2000A into a 66ft end-fed long-wire aerial. The band was so good on the 22nd, a VK station told Harold, that they were burning the midnight (local time) oil working DX. "The band was running wild," said Harold; too true it was, around 1900, I was at a meeting of the Mid-Sussex ARS and listened to Alan Baker G4GNX, have a 59 contact with WB4HHY, Utah, using the club station G3ZMS. At 0843 on the 22nd, Ern Hoare G3RZD, Hove, and Harold had a joint QSO with 9H1CD who has established a beacon, using his own callsign on 432.25MHz, for use during the sporadic-E season, reports, of course, are welcome. Back in July 1976, Ern worked 9H1CD on 2m phone, during a sporadic-E disturbance.

From my own observations the 10m band was blacked out during the early mornings of March 23, 28, 30, and April 4, 6, 7, 15 and 16. The event on March 30 was reported by the BBC World Service and on April 4 the disturbance persisted for most of the day. On the majority of days throughout the period I received signals, averaging 549, from the International Beacon Project stations in Bahrain A9XC, and Cyprus 5B4CY, but, unlike previous months, the signals from the German beacon, DL0IGI, were much less frequent. During the afternoon, on the good days, signals, about 559, were heard from the Bermuda beacon VP9BA. The RSGB are responsible for the IBP service and in the April issue of Radio Communication they say: "The establishment of the beacon stations has stimulated scientific interest in the propagation paths revealed by reception of the beacons. In addition, they fulfil a practical role by providing signals on what may

otherwise be a dead band.

Aurora

The aurora borealis which followed the big solar storm on April 3 began around 2300 and ended during the early hours of the 4th. Alan Baker noticed that the 20m band was almost dead towards the late evening of the 3rd, and what weak stations there were had an auroral tone. He soon checked the 2m band, turned his beam just east of north and had an auroral contact with G8BHH, Wolverhampton, and heard GM4COK, GM4DSZ and GI4GID. John Cooper G8NGO, Cowfold, Sussex, using his 14-element beam, had 59A contacts with G4HSS, GM4DSZ, GM8EYB, and weaker contacts with G8LHT, Doncaster, and G8RHI. John also heard GM8NET and tried to contact GI4GID who was very strong in southern England, but the pile up to work him was too great.

During the event I heard G8ODN, GI4GID, GM4COK and GM8NET. Up in Scotland the aurora affected v.h.f. signals earlier in the evening and between 1700 and 2000 GMT John Branegan GM8OXQ. Saline, Fife, heard 5 Gs, 4 GIs, 7 GMs, 2 LAs, 1 PA0 and the 2m beacons in Germany DLOPR, Northern Ireland GB3GI, and Cornwall GB3CTC. Dermot Cronin EI9DC/G4GRO, who normally reports from the Royal Sovereign Light, heard, at his home in Killiney, tone-A signals from G, GI, GM and LA during the evening of March 29. John Branegan said it was "A very odd aurora", and between 1700 and 1830 he heard signals from EI, DL, LA, G, GI, GM, OZ, SM and the beacons from Cornwall and Germany. At 1746, John heard EI3S, OZ1OF, GM3UU and GI5AJ all calling at once and writes: "they all appeared at or near the same tuning point but they were clearly not hearing one another. However, the OZ called the EI and was answered by the GI so at

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least he got a QSO eventually". Auroral signals, mainly confined to GM, were heard by John during the early evenings of March 22, 26 and 27 and, around 1115 on April 13, Alan Baker noticed that some 10m signals had an auroral tone.

European DX

While at the BBC on April 6, I met Rudolf Heim, Secretary General of the European DX Council, who was visiting Bush House to see a recording of World Radio Club. The EDXC has some 35 member organisations throughout the world, among whom are several international broadcasters acting as observers. Rudolf told me that only about 10 per cent of broadcast DXers are interested in v.h.f. and TV DX, but the number is growing. The Dutch are well ahead in this field however, and have some remarkable aerial systems. Some German clubs are moving in this direction and the German DX Federation, AGDX, frequently publish their own v.h.f and TV DX Bulletin. The use of Citizens' Band in Germany is popular among people of all age groups.

Radio Astronomy

John Smith is experimenting with a receiver to record the bursts of radio noise which come from Jupiter between 20 and 30MHz. So far he has built a pair of 4 half-wave dipoles on a 300 metre baseline, the signals being fed to an FRG-7 followed by a d.c. amplifier to drive a pen recorder. John is also working on a microprocessor, based on the SC/MP chip, to drive his 30ft dish which he intends to use for astronomical observations at 1420MHz.

Satellites

As a result of John Branegan's article about 70cm propagation from satellites, published in the quarterly journal of AMSAT-USA, he has been busy answering letters, one of which came from JR1SWB, editor of the Japanese OSCAR NEWS. John is pleased to do this and play his part in the international co-operation of the OSCAR project. His talk on satellites to the Mid-Lankark ARS was well received. Recently, John's first QSL card arrived from OK3CDI for a contact through the Russian satellite, RS-1 and another card from W4AXR, Florida, confirming his best DX to date, 4300 miles, via OSCAR 7B. So far, John has had nearly 50 satellite QSOs with W2BXA who was the first amateur to work 100 countries via satellite and the one who helped John through his first transatlantic QSO via OSCAR.

Tropospheric

The predominantly poor weather conditions and the low atmospheric pressure between March 19 and April 12 gave little help to the v.h.f. enthusiast, in fact at midnight on March 27 it was 29.1in and only just reached 30.1in for a few hours on the 23rd, when a brief improvement in conditions took place. Suddenly, on Good Friday, April 13, the weather turned warmer, the pressure began to rise and by midday on Easter Sunday it was 30.2in and rising. At 2200 on March 23, Alan Baker heard DB5KGI and PA3ALK on 2m s.s.b. and at 2320, ON6CP on c.w. At 1931 on April 13, Alan had a difficult QSO with F3CF, Lille, and heard G3BDQ in nearby Hastings working a German station on 2m s.s.b. Later, Alan, from his home in east-Sussex, worked stations in Bedfordshire, Hampshire and Kent, via the London repeater GB3LO, R7. At 0853 on the 15th, I heard a QSO between GB2RN, HMS Belfast, London and G4EVI, Yeovil, Somerset, via the Hampshire repeater GB3SN, R5 and both stations were saying that they had not heard SN so strong for a long time.

Around 0730 on the 16th, I heard signals through GB3BC on R6, received a picture from Lichfield on Ch. 8, (189MHz) and noted some continental interference to the BBC stations in Band II. During the day Barry Ainsworth G4GPW, Sompting, Sussex and Roy Bannister G4GPX. in nearby Lancing, had a QSO via the French repeater FZ2THF on R9 and around 1530, G4GNX worked DJ0JW/A and DL0GO, who were both at their club station, DD8EE and using 4 × 21-element beams on 2m s.s.b.

DX Television

On April 1, Andrew Coetzee, one of my readers in Transvaal, SA received Ch.1 BBC TV, 45MHz on his KB receiver with a dipole aerial. Although the vision was only good enough to make out the figures, the sound was very strong. Congratulations are also due to Andrew, who has passed his amateur exams, and now has a restricted licence, callsign ZR6OP.

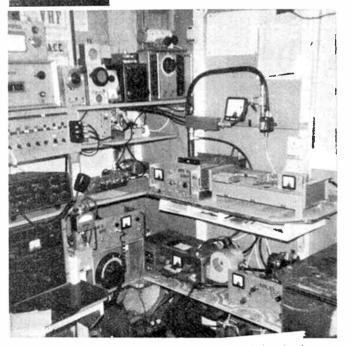
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JOHN TYE

by RON HAM



Part of John Tye's shack, on the right is home constructed equipment for 13 and 23cm

John Tye's interest in radio began around 1940 when, at the age of 14, he assisted with the servicing of broadcast receivers. His fascination for communications was fostered through listening to the short-wave bands on the government surplus receivers, R107 and R1155, which became available soon after the war. Later he joined the RSGB and, as BRS 27622, expanded his listening activities, with home-brew equipment, into the v.h.f. bands. John passed the RAE in May 1968 and, although he was soon active on 2m as G8BYV, his mind was set on building gear and experimenting on the centimetric bands. He passed the Morse test in 1973, and was then granted the callsign G4BYV.

John's signals have been heard in many European Countries on 70, 23 and 13cm from his home in Dereham, Norfolk and in September 1976 he earned the No. 1, Four Metres and Down, Microwave award from the RSGB for a contact of 883km on 1.3GHz with SK6AB. By the end of that year, he had achieved enough confirmed QSOs to qualify for the Society's 23cm award and the 70cm Senior award. One of John's overseas honours came in October 1973 when he received the Mirabel II certificate for sending a tape recording of Mirabel's 1296MHz beacon to F2LM. Mirabel II was a transponder with an up and down link on 144-432MHz, and a beacon on 23cm. It was launched from Nancy, France, by balloon and descended by parachute.

John's present aerial array, consisting of a 13-element Yagi for 70cm, an 8-element Yagi for 2m and separate 4ft dishes for 23cm and 9/13cm, is mounted on a tower which can be raised if required. For almost 30 years, John, a carpenter by trade, has been a reader of Practical Wireless and is supported in his amateur radio activities by his wife, Joan, who enjoys listening to the h.f. bands when driving their car. For the future, John plans to stay on the centimetric bands, use s.s.b. on 9cm and develop gear for 6cm.

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7406	32p	74110	55p	74285	400p	74LS243	175p	74C175	210p	*AY5-1320 320p *CA5019 80p	NE543K 225	- 6		10p	*BU108 250p	*ZTX300	116	*2N4125/6	22p	*OA200	9p
7407	32p	74111	70p	74290	150p	74LS245	175p	74C192	150p	*CA5046 70p	NE555 25			10p	*BU205 220p	°ZTX500	15p	°2N4289	20p	*OA202	10p
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7410	19p 15p	74119	210p	74294	200p	74LS257	120p	74C194	220p	CA3080E 72p	NE561B 425	p .;		12p	*BU406 145p	°ZTX504	30p	2N4427	90p	*1N916	7p
7411	24p	74120	110p	74298	200p	74LS259	175p	74 C195	110p	*CA3089E 225p	NE562B 425	D D		17p	MJ481 175p		250p	*2N4871	60p	*1N4148	4p
7412	20p	74121	28p	74365	150p	74LS298	249p	74 C221	175p	*CA3090AQ375p	NE565 130p	PIR	C179	180	MJ491 200p	2N696	35p	*2N5087 *2N5089	27p	1N4001/2	5p
7413	30p	74122	40p	74356	150p	74LS373	200p		RIES	CA3130S 100p	NE566 155	D i es		100	MJ2501 225p	2N697	25p	*2N5089	27p 27p	1 N4003/4 1 N4005	6p 6p
7414	60p	74123	55p	74367	150p	74LS374 81LS95	195p 120p	4000	15p	CA3140E 70p	NE567 175	P •8	BC184	11p	MJ2955 100p	2N697 2N706A	45p	2N5179	27p	1N4005/7	7p
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7437 7438	35p 35p	74154 74155	190p 90p	74LS20 74LS22	22p 28p	9368	200p	4018	80p 89p	*LM389N 140p	*TBA820 90			200p	*R2008B 200p	2N2904/5	25p	2N6292	65p	RCA 2N30)55
7440	17p	74156	90p	74LS27	38p	9370	200p	4019	45p	LM709 38p	*TCA940 175	1 10	F200	32p	*R2010B 200p	2N2906A	24p	2N128	120p	£36	
7441	70p	74157	70p	74LS30	22p	9374	290p	4020	100p	LM710 50p	*TDA1022 600		BF244B	35p	*TIP29A 40p	2N2907A	30p	3N140	100p	BRIDGE	
7442A	60p	74159	190p	74LS47	90 p	9601	100p	4021	110p	LM733 100p	XR2206 400 p		BF256B F257/8	70p	*TIP29C 55p	*2N2926	9p	3N201	110p	RECTIFIE	
7443	112p	74160	100p	74LS55	30p	9602 9603	175p	4022	100p 22p	LM741 29p LM747 79p	XR2207 400p	PIR	F259	32p 36p	*TIP30A 40p *TIP30C 60p	2N3053 2N3054	20p 65p	3N204 40290	100p 250p		21p
7444	112p	74161	100p	74LS73	50p	INTERF		4023	22p	LM748 35p	*XR2216 675p	P∣∘E		30p	TIP31A 50p	2N3055	40p	40360	40p		22p 36p
7445	100p	74162	100p	74LS74	40p	I.C.s	ACE	4024 4025	50p 20p	LM3800 70p	XR ₂ 240 400 p	p eg	BFR40	30p	TIP31C 62p		140p	40361/2	45p		30p
7445A 7447A	93p	74163 74164	100p 120p	74LS75 74LS83	50p		100p		130p	LM3911 130p	*ZN414 90p	P o i	BFR41	30p	TIP32A 68p		240p	40364	120p		35p
7448	70p	74165	130p	74LS85	100p		100p	4027	50p	LM4136 120p	ZN424E 135p	D og	BFR79	30p	TIP32C 62p	*2N3565	30p	40408	70p		65p
7450	170	74166	140p	74LS86	40p	75107	160p	4028	84p	*MC1310P 150p	ZN425E 400p			30p	TIP33A 90p	*2N3643/4	40p	40409	65p		60p
7451	170	74167	200p	74LS90	60p	75182	230p		100p	MC1458 55p	ZN1034E 200p		BFR81	38p	TIP33C 114p	°2N3702/3	12p	40410	65p	*3A 600V	72p
7453	170	74170	240p	74LS93	60p	75450	120p	4030	55p	MC1495 400p ¹	95H90 800p		FX29	30p	TIP34A 115p	°2N3704/5		40411	300p		95p
7454	17p	74172	720p	74LS107	45p	75451/2	72p	4031	200p	WALTAGE BEG			FX30	34p	TIP34C 160p	*2N3706/7		40594	97p	*4A 400V 1	
7460	17p	74173	120p	74LS112	100p	75491/2	96p		188p	VOLTAGE REGI				30p	TIP35A 225p TIP35C 290p	*2N3708/9 2N3773	300p	40595 40603	105p 50p	6A 50V 6A 100V 1	90p
7470	36p	74174	93p	74LS123	75p		I.C.s		200p				FX38	30p	TIP36A 279p	*2N3819	25p	40673			20p
7472 7473	30p	74175 74176	85p 90p	74LS132 74LS133	900p	74 C 00 74 C 02	25p 25p		110p	1A +ve 5V 7805 75p	1A —ve 5V 7905 100c		FW10	90p	TIP36C 340p	°2N3820	50p	40841		10A 400V 2	
7474	30p	74177	90p	74LS138	60p	74 C04	27p	4041	80p		12V 7912 100c	V -	FY50	22p	TIP41A 65p	2N3823	70p	40871/2		25A 400V 4	
7475	30p	74178	160p	74LS139	60p	74C08	27p	4042	64p	15V 7815 75p	15V 7915 100c					- 1					- 1
7476	350	74180	93p	74LS151	100p	74C10	27p	4043	90p	18V 7818 90p	18V 7918 190g	5 I	REDLI	EDS		VA.	T RA	ATES: All	l items	at 8%	
7480	50p	74181	200p	74LS153	60p	74C14	90p	4044	90p	24V 7824 90p	24V 7924 100p	p	0.125	12p				marked *	which	are at	
7481	100p	74182	90p	74LS157	60p	74C20	27p		110p	100mA TO-92	100mA TO-92	2	0.2"	12p	50 · 10p	12	1%.				
7482	64p	74184 A		74LS158	120p	74C30	27p		100p	5V 78L05 35p	5V 79L05 60p										
7483A	90p	74185	150p	74LS160	100p	74 C32	38 p	4048	55p	12V 78L12 35p	12V 79L12 80p										\equiv
7484 7485	190p	74186 74190	700 p	74LS161 74LS162		74 C42 74 C48	110p 250p	4049 4050	32p	15V 78L15 35p			lease			TIN	HIN	INM	M	C LT	nı
7486	34p	74191	100 p	74LS163	100p	74 C 73	75p	4051	80p	OTHER REGUL	ATORS	P	o&p an	d V	AT at		ΗN	11 I IVI. <i>1</i>	м	1. I I	***
7489	210p	84192	100p	74LS164	120p	74C74	70p	4052	80p	LM309K 13\$p	TBA625B 120p	p a	Doron	riate	rates.	ILU	ш	IUW	111	ULI	U I
7490A	33p	74193	100p	74LS165	80p	74C85	200p	4053	60p	LM317T 200p	TL430 65p	0 I									- 1
7491	80p	74194	100p	74LS173	110p	74C86	65p	4055	125p	LM323K 625p	78HO5KC 675p				eges, etc.	17 BUR	INLE	EY ROA	AD.		- 1
7492A	40p	74195	95p	74LS174	110p	74C90	95p	4056	135p	LM723 37p	78MGT2C 135p	2 o	orders :	acce	epted.				_		
7493A 7494	33p 64p	74196 74197	95p 60p	74LS175 74LS181	110p 320p	74C95 74C107	130p 125p	4059 4060	600p	OPTO-ELECTRO	ONICS	- I C	Callers	we	lcome	LOND	ON !	NW10			
7495A	70p	74198	150p	74LS190	100p	74C150	250p	4063	120p	2N5777 45p ORP	12 90p ORP61 90g	p M	ON-FR	1 9.3	30-5.30		45 4-	. 4500	· ·	0000	,, I
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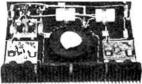
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AF115 0.81 8C135 0.16 8CY34 0.97 AF116 0.81 8C136 0.17 8CY39 3.24 AF117 0.81 8C137 0.17 8CY40 1.08 AF139 0.43 8C147 0.10 8CY42 0.27 AF186 1.30 8C148 0.09 8CY43 0.27 AF239 0.49 8C149 0.10 8CY58 0.17 AF211 2.97 8C157 0.10 8CY70 0.18 AF212 2.97 8C158 0.09 8CY71 0.18	8F179 0-27 8F180 0-32 BU205 1-97 N 8F181 0-32 BU206 2-53 N 8F182 0-32 BU208 2-25 O 8F183 0-27 BY100 0-49 O 8F184 0-27 BY126 0-15 O	KT401 2-46 OC73 1-08 TIP422A 0.76 15920 0.08 2N2906 0.23 KT403 1-87 OC74 0.70 1792956 0.72 15921 0.08 2N2907 0.23 KT404 1-87 OC75 0.70 1792955 0.60 26301 1.08 2N2927 0.24 A5 1.03 OC75 0.70 1792055 0.60 26301 1.08 2N2924 0.24 A5 1.03 OC76 0.59 17543 0.51 26302 1.08 2N2925 0.25 A7 0.59 OC77 1.30 ZS140 0.28 26306 1.19 2N2925 0.25 A7 0.65 OC81 0.70 ZS140 0.28 26306 1.19 2N2926 0.26 A10 0.65 OC81 0.70 ZS170 0.24 2N404 1.08 2N3053 0.27	2N4126 0.18 2N4286 0.23 2N4288 0.25 2N4289 0.27 2N5457 0.39 2N5458 0.39 2N5459 0.39
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7400	0.12	0.21	7485	0.88	0.97	74164	0.89	1.20	74386	0.58	22 pin		0.2	
7401	0.12	0.21			4LSN	74165	0.89		74390 1.92		24 pin		0.31	D .
7402	0.12	0.21	7486	0.26		74166	0.99		74393 2.00		28 pin		0.44	l .
7403	0.12	0.21	74586	1.50			74817	4LSN	73670	2.30	40 pin		0.5	5
7404	0.13	0.21	7489	2.00		74167	2.70		LINEARS		. ,			-
7405	0.13	0.21	7490	0.35	0.85	74169		2.10	CA3045 -14	0.45	CMOS	5		
7406	0.28		7491	0.65		74170	1.68	1.94	CA304614	0.70	4000	0.14	4067	3.50
7407	0.28		7492	0.44	0.82	74172	4.00		LM380N -14		4001	0.15	4068	0.24
7408	0.14	0.21	7493	0.40	0.85	74173	1.18	1.12	LM381N -14		4002	0.16	4069	0.17
74508	0.40		7494	0.80	0.00	74174	0.89	1.12	LM710N -14	0.32	4006	0.82	4070	0.17
7409	0.14	0.21	7495	0.54	1.05	74175	0.68	1.12	LM711N -14	0.32	4007	0.16	4071	0.17
7410	0.13	0.22	7496	0.60	1.30	74517		1.12	MC1310P -14	1.50	4008	0.92	4072	0.17
7411	0.16	0.21	7497	2.00	1.30	74176			NE555N -8	0.30	4009	0.45	4073	0.17
7412	0.21	0.21	74100	0.94		74177	0.82		NE556N -14	0.65	4010	0.48	4075	0.17
7413	0.25	0.46	74104	0.40			1.20		NE2501B -14	2.00	4011	0.15	4076	1.05
7414	0.54	1.05	74105	0.40		74176 74179	1.10		SN72702N	0.50	4012	0.16	4077	0.48
7415	0.54	0.21	74107	0.40	0.40				SN75110N	0.50	4013	0.42	4078	0.22
7416	0.27	0.21	74109		0.40	74180	0.90		SN76003N	1.85	4014	0.80	4081	0.17
7417	0.27			0.45	0.40	74181	1.75	3.38	SN76013N	1.35	4015	0.40	4082	0.20
7420	0.13	0.21	74110	0.46		74182	0.75		SN76023N	1,35	4016	0.77	4085	0.72
		0.21	74111	0.70		745182			SN76033N	1.35				
7421 7422	0.28	0.21	74112		0.40	74H18			TAASSO8		4017	0.77	4066 4089	0.76
	0.17	0.21	74113	0.30	0.40	74184	1.20			0.35	4018	0.87	4093	1.55
7423	0.25		74114		0.40	74185			TAA661B		4019	0.42	4094	0.65
7425	0.20		74116	1.60			7.20		TBA120S	0.64	4020	0.92	4095	1.60
7426	0.25	0.26	74118	0.82		74188	2.70		TBA641A	1.88	4021	0.82		1.10
7427	0.25	0.30	74119	1.25		74189		3.80	TBA800	0.75	4022	0.82	4096	1.10
7428	0.34	0.34	74120	0.82		74190	1.05	0.96	TBA810S	1.04	4023	0.15	4097	3.50
7430	0.13	0.21	74121	0.25		74191	0.89	0.96	TCA270S0	2.00	4024	0.66	4098	1.12
74530	0.30		74122	0.40		74192	0.99	1.50	TDA2020	3.20	4025	0.15	4099	1.90
7432	0.24	0.31	74123	0.50	0.59	74193	1.05	1.50	ZN414	1.00	4026	1.28	4404	1.00
7437	0.24	0.26	74124		1.25	74194	0.90	2.00	OP AMPS		4027	0.50	4412	0.30
7438	0.24	0.26	74125	0.40	0.48	74195	0.84	1.40	CA3130 -T099	1.00	4028	0.87	4428	0.80
7440	0.13	0.22	74126	0.45	0.48	74196	0.80	1.15	LM301A -8	0.30	4029	0.86	4445	1.50
7441	0.52		74128	0.62		74197	0.80	1.15	LM301A-T099	0.48	4030	0.48	4449	0.30
7442	0.55	0.70	74132	0.68	0.82	74198	1.48		LM348N -14	1.00	4031	2.34	4501	0.17
7443	0.90		74134	0.36		74199	1.48		LM709 -8	0.48	4033	1.25	4502	0.88
7444	0.80		74135	0.68		74221	1.50	1.05	LM709 -14	0.42	4034	2.00	4507	0.50
7445	0.70		74136	0.55	0.40	74247		0.80	LM709 -T099	0.50	4035	1.00	4508	2.25
7446	0.70		74137	0.94		74248		0.85	LM741 -8	0.22	4036	2.40	4510	1.05
7447A	0.60	0.94	74136		0.62	74249		0.85	LM741 -14	0.20	4037	0.89	4511	0.88
7448	0.60	0.94	74139		0.62	74251	1.00	0.85	LM741 -T099	0.45	4038	1.00	4512	0.82
7449		0.94	74141	0.56		74253		1.10		0.70	4039	2.80	4514	285
7450	0.13		74142	2.00		74257		1.12	LM3900N	0.50	4040	0.88	4515	2.80
7451	0.13	0.21	74143	2.00		74258		1.15	MC1458P -8	0.42	4041	0.77	4516	1.02
7453	0.13		74144	2.00		74260		0.26	VOLTATE REG		4042	0.72	4518	0.89
7454	0.13	0.21	74145	0.64	1.20	74261		3.26	LM300 -T099	1.00	4043	0.82	4519	0.50
7455		0.26	74147	1.30		74266		0.43	LM309K -T03	1.30	4044	0.82	4520	1.05
7460	0.13		74148	1.15	ĺ	74273	2.15	1.80	uA723 -14	0.40	4045	1.40	4521	2.00
7470	0.26		74150	0.99		74279	1.25	0.55	7805 T0220	0.85	4046	1.32	4522	1.35
7472	0.22		74151	0.60	0.80	74263	1.70	1.05	7812 T0220		4047	0.98	4527	1.60
7473	0.26	0.36	74153	0.60	0.56	74284	6.85	1.03	7815 T0220	0.85	4048	0.60	4528	0.82
7474	0.26	0.38	74154	1.00	1.32	74289	0.00	192	7824 T0220	0.85	4049	0.42	4529	1.10
73574	0.50	50	74155	0.63	0.96	74290		0.85	7905 T0220	1.10	4050	0.42	4538	3.58
7475	0.30	0.42	74158	0.82	0.98	74293	1.35	1.00	7912 T0220	1.10	4051	0.84	4553	4.20
7476	0.26	0.39	74157	0.83	0.60	74298	1.92	1.40	7915 T0220	1.10	4052	0.84	4555	0.85
7478	-20	0.39	74158	0.58	0.82	74352	1.02	1.00	OIL SOCKETS		4053	0.84	4556	0.85
7480	0.45	4.32	74159	1.70	U.82	74353		1.05	8 pin	0.11	4054	1.10	4558	1.25
7481	0.80		74160	0.80	1,30	74365		0.52	14 pin	0.12	4055	1.00	4566	1.40
7482	0.75		74161	0.80	0.80	74365		0.52	16 pin	0.13	4060	0.96	4583	0.75
7483	0.72	0.97			1.30				18 pin	0.23	4066	0.48	4585	1.03
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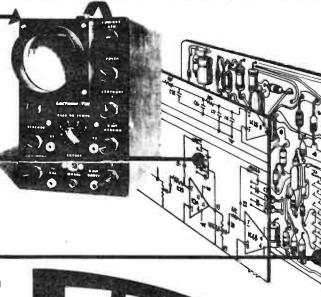
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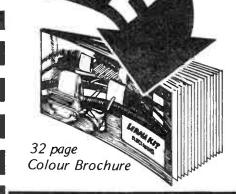
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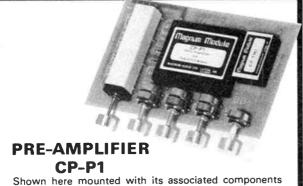
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M9

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M14

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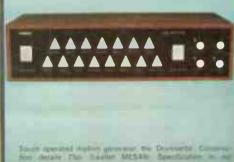




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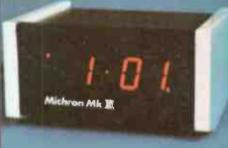
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