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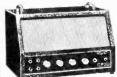
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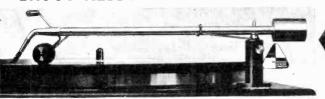
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7 Tunable Wave-bands: MWI, MW2, LW, 8WI, 8W2, SW3 and Trawler Band. Extra Medium waveband provides easier tuning of Radio Luxembourg, etc. Built in ferrite rod aerial for MW and LW. Retractable 4 section 24in. chrone-plated telescopio serial for 8W. Socket for Car Aerial. Powerful push-pull output. 7 translators and 2 diodes, fine tone moving coil speaker. Air staced ganged Powerful push-pull output. 7 translators and 2 diodes, fine tone moving coil speaker. Air spaced ganged tuning condenser. Volume/on/off, tuning and wave change controls. Attractive case with carrying handle Size 9 × 7 × 4 m. approx. Easy to follow instructions and diagrams. Parts price list and casy build plans 15p (PREE with parts).

Total building cook.

Total building costs £5.98 P. P.&



ROAMER SIX

6 Tunable Wave-bands: MW, LW, BW1, BW2, BW3 Trawler, band plus an extra Medium waveband for easier tuning ensier tuning of Luxembourg etc. Bensitive forrite rod nerial and

rite rod aerial and telescopic aerial for Bhort Waves.
3th. Speaker. 8 stages.—I transistors and 2 closes Attractive black case with red grille, dial and black knobs with pollahed netal inverts. Bize 9 × 3; × 2th. approx. Easy build plans and parts price list 15p (FREE with parts).

Total building costs £3*98 P. P. &

POCKET FIVE

3 Tunable Wavebands:
MW, LW, Trawler Band
with extended M.W.
band for easier tuning
of Luxembourg, etc.
7 stages—5 transistors and 2 diodes,
supersensitive ferrite rod aerial, fine
tone moving coil speaker. Attractive black and gold
case. Size 5½ x 1½ x 34 in. Easy build plans and
parts price list 10p (FREE with parts).

Total building costs £2.29 P. P. & P. 63p)

TRANSONA

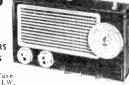


3 Tunable Wavebands: MW, LW and Trawler Band, 7 stage—5 transistors and 2 diodes, ferrite rod aerial tuning condenser volume control, fine tone moving coil speaker. Attractive case with red speaker grille. Size 8\frac{1}{2} \times 4\frac{1}{2} \times 1\frac{1}{2} \times 1\times 1\frac{1}{2} \times 1\frac{1}{2} \times 1\frac{1}{2} \times 1\times 1\frac{1}{2} \times 1\times grille. Size $6\frac{1}{2} \times 4\frac{1}{2} \times 1\frac{1}{4}$ in. Easy by parts price list 10p (FREE with parts).

Total building costs £2°50 P.P. & Ins. 24g

TRANS EIGHT

8 TRANSISTORS and 3 O!ODES



6 Tunable Wavebands: MW, LW, SW1, SW2, SW3 and Trawler Band.
Sensitive ferrite rod acrial for M.W. and L.W. Telescopic acrial for Short Waves. 3in. Speaker. 8 improved type transistors plus 3 diodes. Attractive case in black with red grille, dial and black knobs with polished metal inserts. Size 9 × 51 × 22 in. approx. Push pull output. Battery economiser switch for extended battery life. Ample power to drive a larger speaker. Parts price list and easy build plans 250 (FREE with parts).

Total building costs £4-48 P. P. & Ins. 32p

FIVE

5 TRANSISTORS AND 2 DIODES



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METROSOUND HFS 103 (pair) 29 -21 20 -95 METROSOUND 202 21 -50 14 -75 METROSOUND Duplex 15 32 -00 21 -95 METROSOUND Duplex 25 -56 -00 37 -95 PHILIPS RH411 (pair) 21 -80 18 -25 PHILIPS RH412 (pair) 73 -50 29 -50 PHILIPS RH412 (pair) 70 -00 47 -95 PHILIPS RH412 (pair) 70 -00 47 -95 PHILIPS RH412 (pair) 70 -00 47 -95 PHILIPS RH405 (pair) 70 -00 47 -95 PIONEER CS53 46 -72 29 -50 SINCLAIR Q16 8 8-98 6-50 STE-MA 450 25 -00 16 -95 TANDBERG Tan 7 29 -50 24 -95 TANDBERG Tan 11 (pair) 40 -00 32 -95 TANDBERG Tan 12 teak (pair) 44 -00 32 -95 TANDBERG Tan 12 teak (pair) 71 -50 58 -95 TANDBERG Tan 50 teak 68 -00 52 -95 TANDBERG Tan 50 teak 68 -00 52 -95 TELETON 8000 (pair) 21 -08 11 -95 Grenville TG 200 (pair) 55 -95 WHARTED G00 (pair) 55 -95 WHARTED G00 (pair) 40 -95 Dovedale 3 Mark II 47 -50 31 -95 WHARTED G00 (pair) 47 -95 Rosedale 10 -96 -90 46 -95 Unit 3 Speaker Kit 12 -50 8 -95 Unit 4 Speaker Kit 12 -50 8 -95 Unit 5 Speak	KN2100 3-speaker Sys	stem	30.60	19-95
METROSOUND HFS 103 (pair) 29 -21 20 -95 METROSOUND 202 21 -50 14 -75 METROSOUND Duplex 15 32 -00 21 -95 METROSOUND Duplex 25 -56 -00 37 -95 PHILIPS RH411 (pair) 21 -80 18 -25 PHILIPS RH412 (pair) 73 -50 29 -50 PHILIPS RH412 (pair) 70 -00 47 -95 PHILIPS RH412 (pair) 70 -00 47 -95 PHILIPS RH412 (pair) 70 -00 47 -95 PHILIPS RH405 (pair) 70 -00 47 -95 PIONEER CS53 46 -72 29 -50 SINCLAIR Q16 8 8-98 6-50 STE-MA 450 25 -00 16 -95 TANDBERG Tan 7 29 -50 24 -95 TANDBERG Tan 11 (pair) 40 -00 32 -95 TANDBERG Tan 12 teak (pair) 44 -00 32 -95 TANDBERG Tan 12 teak (pair) 71 -50 58 -95 TANDBERG Tan 50 teak 68 -00 52 -95 TANDBERG Tan 50 teak 68 -00 52 -95 TELETON 8000 (pair) 21 -08 11 -95 Grenville TG 200 (pair) 55 -95 WHARTED G00 (pair) 55 -95 WHARTED G00 (pair) 40 -95 Dovedale 3 Mark II 47 -50 31 -95 WHARTED G00 (pair) 47 -95 Rosedale 10 -96 -90 46 -95 Unit 3 Speaker Kit 12 -50 8 -95 Unit 4 Speaker Kit 12 -50 8 -95 Unit 5 Speak	LEAK 250 (pair)		63 · 00	46 - 95
METROSOUND HFS 103 (pair) 29 -21 20 -95 METROSOUND 202 21 -50 14 -75 METROSOUND Duplex 15 32 -00 21 -95 METROSOUND Duplex 25 -56 -00 37 -95 PHILIPS RH411 (pair) 21 -80 18 -25 PHILIPS RH412 (pair) 73 -50 29 -50 PHILIPS RH412 (pair) 70 -00 47 -95 PHILIPS RH412 (pair) 70 -00 47 -95 PHILIPS RH412 (pair) 70 -00 47 -95 PHILIPS RH405 (pair) 70 -00 47 -95 PIONEER CS53 46 -72 29 -50 SINCLAIR Q16 8 8-98 6-50 STE-MA 450 25 -00 16 -95 TANDBERG Tan 7 29 -50 24 -95 TANDBERG Tan 11 (pair) 40 -00 32 -95 TANDBERG Tan 12 teak (pair) 44 -00 32 -95 TANDBERG Tan 12 teak (pair) 71 -50 58 -95 TANDBERG Tan 50 teak 68 -00 52 -95 TANDBERG Tan 50 teak 68 -00 52 -95 TELETON 8000 (pair) 21 -08 11 -95 Grenville TG 200 (pair) 55 -95 WHARTED G00 (pair) 55 -95 WHARTED G00 (pair) 40 -95 Dovedale 3 Mark II 47 -50 31 -95 WHARTED G00 (pair) 47 -95 Rosedale 10 -96 -90 46 -95 Unit 3 Speaker Kit 12 -50 8 -95 Unit 4 Speaker Kit 12 -50 8 -95 Unit 5 Speak	LEAK 600	alr)	49·50 Sp. Price	33·95 13 50
TANDBERG Tan 7 29-50 24-95 TANDBERG Tan 12 teak (pair) 40-00 32-95 TANDBERG Tan 12 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 50 teak 68-00 52-95 TELETON 8000 (pair) 21-08 11-95 Grenville TG 200 (pair) 41-95 25-95 Grenville TG 300 (pair) 55-95 31-95 WHARFEDALE Denton Mark II (pair) 52-00 36-95 Triton III (pair) 65-00 36-95 Triton Mark II 93-00 23-59 Dovedals 3 Mark II 35-00 23-59 Dovedals 3 Mark II 19-00 32-59 Unit 4 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 18-75 CHASSIS SPEAKERS GOODMANS TWIN-AXION 8. 65 6-95 TAIDMAIDM 10 17-68 11-95 Audiom 8P 5-20 4-15 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 19P 36-70 37-75 Audiom 18P 35-70 24-45 Audiom 100 40-94-80 Midax 650 13-59 Super 10/RS/DD 14-00 Midax 650 13-59 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 17-67 AUDIO TECHNICA AT86 6-47 AUS 28-55 GOLDRING 6800 12-21 GOLDRING 6800 12-21 GOLDRING 6800 11-67 GOLDRING 6800 51-69	METROSOUND HFS 1	03 (pair)	90.94	20 - 95
TANDBERG Tan 7 29-50 24-95 TANDBERG Tan 12 teak (pair) 40-00 32-95 TANDBERG Tan 12 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 50 teak 68-00 52-95 TELETON 8000 (pair) 21-08 11-95 Grenville TG 200 (pair) 41-95 25-95 Grenville TG 300 (pair) 55-95 31-95 WHARFEDALE Denton Mark II (pair) 52-00 36-95 Triton III (pair) 65-00 36-95 Triton Mark II 93-00 23-59 Dovedals 3 Mark II 35-00 23-59 Dovedals 3 Mark II 19-00 32-59 Unit 4 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 18-75 CHASSIS SPEAKERS GOODMANS TWIN-AXION 8. 65 6-95 TAIDMAIDM 10 17-68 11-95 Audiom 8P 5-20 4-15 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 19P 36-70 37-75 Audiom 18P 35-70 24-45 Audiom 100 40-94-80 Midax 650 13-59 Super 10/RS/DD 14-00 Midax 650 13-59 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 17-67 AUDIO TECHNICA AT86 6-47 AUS 28-55 GOLDRING 6800 12-21 GOLDRING 6800 12-21 GOLDRING 6800 11-67 GOLDRING 6800 51-69	METROSOUND Duple:	c 15	32.00	21 - 95
TANDBERG Tan 7 29-50 24-95 TANDBERG Tan 12 teak (pair) 40-00 32-95 TANDBERG Tan 12 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 50 teak 68-00 52-95 TELETON 8000 (pair) 21-08 11-95 Grenville TG 200 (pair) 41-95 25-95 Grenville TG 300 (pair) 55-95 31-95 WHARFEDALE Denton Mark II (pair) 52-00 36-95 Triton III (pair) 65-00 36-95 Triton Mark II 93-00 23-59 Dovedals 3 Mark II 35-00 23-59 Dovedals 3 Mark II 19-00 32-59 Unit 4 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 18-75 CHASSIS SPEAKERS GOODMANS TWIN-AXION 8. 65 6-95 TAIDMAIDM 10 17-68 11-95 Audiom 8P 5-20 4-15 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 19P 36-70 37-75 Audiom 18P 35-70 24-45 Audiom 100 40-94-80 Midax 650 13-59 Super 10/RS/DD 14-00 Midax 650 13-59 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 17-67 AUDIO TECHNICA AT86 6-47 AUS 28-55 GOLDRING 6800 12-21 GOLDRING 6800 12-21 GOLDRING 6800 11-67 GOLDRING 6800 51-69	METROSOUND Duple: PHILIPS RH411 (pair)	25	56·00 21·80	18 - 25
TANDBERG Tan 7 29-50 24-95 TANDBERG Tan 12 teak (pair) 40-00 32-95 TANDBERG Tan 12 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 50 teak 68-00 52-95 TELETON 8000 (pair) 21-08 11-95 Grenville TG 200 (pair) 41-95 25-95 Grenville TG 300 (pair) 55-95 31-95 WHARFEDALE Denton Mark II (pair) 52-00 36-95 Triton III (pair) 65-00 36-95 Triton Mark II 93-00 23-59 Dovedals 3 Mark II 35-00 23-59 Dovedals 3 Mark II 19-00 32-59 Unit 4 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 18-75 CHASSIS SPEAKERS GOODMANS TWIN-AXION 8. 65 6-95 TAIDMAIDM 10 17-68 11-95 Audiom 8P 5-20 4-15 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 19P 36-70 37-75 Audiom 18P 35-70 24-45 Audiom 100 40-94-80 Midax 650 13-59 Super 10/RS/DD 14-00 Midax 650 13-59 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 17-67 AUDIO TECHNICA AT86 6-47 AUS 28-55 GOLDRING 6800 12-21 GOLDRING 6800 12-21 GOLDRING 6800 11-67 GOLDRING 6800 51-69	PHILIPS RH412 (pair)		35.00	29 50
TANDBERG Tan 7 29-50 24-95 TANDBERG Tan 12 teak (pair) 40-00 32-95 TANDBERG Tan 12 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 50 teak 68-00 52-95 TELETON 8000 (pair) 21-08 11-95 Grenville TG 200 (pair) 41-95 25-95 Grenville TG 300 (pair) 55-95 31-95 WHARFEDALE Denton Mark II (pair) 52-00 36-95 Triton III (pair) 65-00 36-95 Triton Mark II 93-00 23-59 Dovedals 3 Mark II 35-00 23-59 Dovedals 3 Mark II 19-00 32-59 Unit 4 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 18-75 CHASSIS SPEAKERS GOODMANS TWIN-AXION 8. 65 6-95 TAIDMAIDM 10 17-68 11-95 Audiom 8P 5-20 4-15 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 19P 36-70 37-75 Audiom 18P 35-70 24-45 Audiom 100 40-94-80 Midax 650 13-59 Super 10/RS/DD 14-00 Midax 650 13-59 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 17-67 AUDIO TECHNICA AT86 6-47 AUS 28-55 GOLDRING 6800 12-21 GOLDRING 6800 12-21 GOLDRING 6800 11-67 GOLDRING 6800 51-69	PIONEER CS53		46.72	29 - 50
TANDBERG Tan 7 29-50 24-95 TANDBERG Tan 12 teak (pair) 40-00 32-95 TANDBERG Tan 12 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 52 teak (pair) 71-50 58-95 TANDBERG Tan 50 teak 68-00 52-95 TELETON 8000 (pair) 21-08 11-95 Grenville TG 200 (pair) 41-95 25-95 Grenville TG 300 (pair) 55-95 31-95 WHARFEDALE Denton Mark II (pair) 52-00 36-95 Triton III (pair) 65-00 36-95 Triton Mark II 93-00 23-59 Dovedals 3 Mark II 35-00 23-59 Dovedals 3 Mark II 19-00 32-59 Unit 4 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 48-95 Unit 5 Speaker Kit 19-00 18-75 CHASSIS SPEAKERS GOODMANS TWIN-AXION 8. 65 6-95 TAIDMAIDM 10 17-68 11-95 Audiom 8P 5-20 4-15 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 19P 36-70 37-75 Audiom 18P 35-70 24-45 Audiom 100 40-94-80 Midax 650 13-59 Super 10/RS/DD 14-00 Midax 650 13-59 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 Super 10/RS/DD 14-00 Super 8/RS/IDD 3-75 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 17-67 AUDIO TECHNICA AT86 6-47 AUS 28-55 GOLDRING 6800 12-21 GOLDRING 6800 12-21 GOLDRING 6800 11-67 GOLDRING 6800 51-69	SINCLAIR Q16 STE-MA 450		25:00	6 · 50 16 · 95
THORPE Grenville TG 100 (pair) 28-95 17-95 Grenville TG 200 (pair) 41-95 25-95 Grenville TG 300 (pair) 41-95 25-95 31-95 MHARFEDALE Denton Mark II (pair) 55-95 31-95 MHARFEDALE Denton Mark II (pair) 65-00 46-95 Melton Mark II 35-00 23-5	TANDBERG Tan 7	aleX	29 - 50	24 - 95
THORPE Grenville TG 100 (pair) 28-95 17-95 Grenville TG 200 (pair) 41-95 25-95 Grenville TG 300 (pair) 41-95 25-95 31-95 MHARFEDALE Denton Mark II (pair) 55-95 31-95 MHARFEDALE Denton Mark II (pair) 65-00 46-95 Melton Mark II 35-00 23-5	TANDBERG Tan 12 tea	k (pair)	44.00	35 - 95
THORPE Grenville TG 100 (pair) 28-95 17-95 Grenville TG 200 (pair) 41-95 25-95 Grenville TG 300 (pair) 41-95 25-95 31-95 MHARFEDALE Denton Mark II (pair) 55-95 31-95 MHARFEDALE Denton Mark II (pair) 65-00 46-95 Melton Mark II 35-00 23-5	TANDBERG Tan 25 tea TANDBERG Tan 50 tea	ık (pair)		52 - 95
Linton Mark II (pair) 52-00 38-95 Triton III (pair) 65-00 46-95 Melton Mark II 35-00 23-50 Dovedale 3 Mark II 47-50 31-95 Rosedale 69-00 46-95 Unit 3 Speaker Kit 12-50 8-95 Unit 4 Speaker Kit 12-50 8-95 Unit 4 Speaker Kit 12-50 18-75 CHASSIS SPEAKERS GODDMANS Twin-Axiom 8 8-65 7-50 Axiom 401 17-68 11-95 Audlom 8P 9-520 4-15 Audlom 8P 5-20 4-15 Audlom 12P 13-00 9-15 Audlom 12P 13-00 9-15 Audlom 18P 35-70 24-45 Audlom 18P 35-70 24-45 Audlom 18P 35-70 24-45 Audlom 19P 35-70 24-45 Audlom 19P 35-70 24-50 Audlom 19P 35-70 35-70 Audlom 19R 35-70 35-70 Audlom 19R 37-70 35-70 Super 3/RS/IDD 36-70 35-70 Super 3/RS/IDD 36-70 35-70 AUDLOM 19RS/IDD 14-00 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 19P 35-70 AUDLOM 19RS/IDD 19-70 GOLDRING 6800 192-21 AUSTRAD 900 EX 11-00 GOLDRING 6800 192-21 AUSTRAD 525 GOLDRING 6800 192-21 AUSTRAD 525 GOLDRING 6800 192-21 AUSTRAD 525	TELETON 8000 (pair)	100 (palr)	21.08	11 - 95
Linton Mark II (pair) 52-00 38-95 Triton III (pair) 65-00 46-95 Melton Mark II 35-00 23-50 Dovedale 3 Mark II 47-50 31-95 Rosedale 69-00 46-95 Unit 3 Speaker Kit 12-50 8-95 Unit 4 Speaker Kit 12-50 8-95 Unit 4 Speaker Kit 12-50 18-75 CHASSIS SPEAKERS GODDMANS Twin-Axiom 8 8-65 7-50 Axiom 401 17-68 11-95 Audlom 8P 9-520 4-15 Audlom 8P 5-20 4-15 Audlom 12P 13-00 9-15 Audlom 12P 13-00 9-15 Audlom 18P 35-70 24-45 Audlom 18P 35-70 24-45 Audlom 18P 35-70 24-45 Audlom 19P 35-70 24-45 Audlom 19P 35-70 24-50 Audlom 19P 35-70 35-70 Audlom 19R 35-70 35-70 Audlom 19R 37-70 35-70 Super 3/RS/IDD 36-70 35-70 Super 3/RS/IDD 36-70 35-70 AUDLOM 19RS/IDD 14-00 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 19P 35-70 AUDLOM 19RS/IDD 19-70 GOLDRING 6800 192-21 AUSTRAD 900 EX 11-00 GOLDRING 6800 192-21 AUSTRAD 525 GOLDRING 6800 192-21 AUSTRAD 525 GOLDRING 6800 192-21 AUSTRAD 525	Grenville TG 200 (pai	r)	41 - 95	25 - 95
Linton Mark II (pair) 52-00 38-95 Triton III (pair) 65-00 46-95 Melton Mark II 35-00 23-50 Dovedale 3 Mark II 47-50 31-95 Rosedale 69-00 46-95 Unit 3 Speaker Kit 12-50 8-95 Unit 4 Speaker Kit 12-50 8-95 Unit 4 Speaker Kit 12-50 18-75 CHASSIS SPEAKERS GODDMANS Twin-Axiom 8 8-65 7-50 Axiom 401 17-68 11-95 Audlom 8P 9-520 4-15 Audlom 8P 5-20 4-15 Audlom 12P 13-00 9-15 Audlom 12P 13-00 9-15 Audlom 18P 35-70 24-45 Audlom 18P 35-70 24-45 Audlom 18P 35-70 24-45 Audlom 19P 35-70 24-45 Audlom 19P 35-70 24-50 Audlom 19P 35-70 35-70 Audlom 19R 35-70 35-70 Audlom 19R 37-70 35-70 Super 3/RS/IDD 36-70 35-70 Super 3/RS/IDD 36-70 35-70 AUDLOM 19RS/IDD 14-00 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 19P 35-70 AUDLOM 19RS/IDD 19-70 GOLDRING 6800 192-21 AUSTRAD 900 EX 11-00 GOLDRING 6800 192-21 AUSTRAD 525 GOLDRING 6800 192-21 AUSTRAD 525 GOLDRING 6800 192-21 AUSTRAD 525	WHARFEDALE	r)		
Unit 3 Speaker Kit	Denton Mark II (pair)			27 · 95 36 · 95
Unit 3 Speaker Kit	Triton III (pair)			46 - 95
Unit 3 Speaker Kit	Dovedale 3 Mark II		47.50	31 - 95
CHASSIS SPEAKERS GOODMANS Twin-Axiom 8. 8-85 5-95 Twin Axiom 10 9-58 7-50 Axiom 401 17-68 11-95 Audiom 8P 5-20 4-15 Audiom 10P 15-67 4-50 Audiom 12P 13-00 9-15 Audiom 12P 13-00 9-15 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 100 40 watts DIN 12-00 8-35 ARU 172 4-50 320 Axent 100 6-90 4-80 Midax 650 13-59 9-50 Attenuator 37-77 3-9-50 Attenuator 37-77 3-30 WHARFEDALE BIN Bronze/RS/DD 4-75 3-30 Super 8/RS/DD 3-50 4-75 3-50 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 19-50 AMSTRAD 900C 19-750	Unit 3 Speaker Kit		12.50	8 · 95
CHASSIS SPEAKERS GOODMANS Twin-Axiom 8. 8-85 5-95 Twin Axiom 10 9-58 7-50 Axiom 401 17-68 11-95 Audiom 8P 5-20 4-15 Audiom 10P 15-67 4-50 Audiom 12P 13-00 9-15 Audiom 12P 13-00 9-15 Audiom 18P 35-70 24-45 Audiom 18P 35-70 24-45 Audiom 100 40 watts DIN 12-00 8-35 ARU 172 4-50 320 Axent 100 6-90 4-80 Midax 650 13-59 9-50 Attenuator 37-77 3-9-50 Attenuator 37-77 3-30 WHARFEDALE BIN Bronze/RS/DD 4-75 3-30 Super 8/RS/DD 3-50 4-75 3-50 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 4-95 AMSTRAD 900C 19-50 AMSTRAD 900C 19-750	Unit 4 Speaker Kit		19 · 00 27 · 50	12 95 18 75
Axent 100 6.90 4.80 MIdax 650 13:59 9-50 Attenuator 3.73 2.60 Crossover Network XO/950 7.77 5-45 VHARREDALE 8In. Bronze/RS/DD 4.75 3.30 Super 8/RS/DD 14.00 9-95 CARTRIDGES AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 3.75 3.75 AUDIO TECHNICA AT86 6.47 3.46 GOLDRING G800 12:21 4.00 3.60 GOLDRING G800 12:21 4.77 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:58 3.55 4.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 3	CHASSIS SPEAKE	RS		
Axent 100 6.90 4.80 MIdax 650 13:59 9-50 Attenuator 3.73 2.60 Crossover Network XO/950 7.77 5-45 VHARREDALE 8In. Bronze/RS/DD 4.75 3.30 Super 8/RS/DD 14.00 9-95 CARTRIDGES AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 3.75 3.75 AUDIO TECHNICA AT86 6.47 3.46 GOLDRING G800 12:21 4.00 3.60 GOLDRING G800 12:21 4.77 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:58 3.55 4.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 3	Twin Axiom 10		9 - 58	7 - 50
Axent 100 6.90 4.80 MIdax 650 13:59 9-50 Attenuator 3.73 2.60 Crossover Network XO/950 7.77 5-45 VHARREDALE 8In. Bronze/RS/DD 4.75 3.30 Super 8/RS/DD 14.00 9-95 CARTRIDGES AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 3.75 3.75 AUDIO TECHNICA AT86 6.47 3.46 GOLDRING G800 12:21 4.00 3.60 GOLDRING G800 12:21 4.77 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:58 3.55 4.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 3	Axiom 401		17 · 68 5 · 20	11 · 95 4 · 15
Axent 100 6.90 4.80 MIdax 650 13:59 9-50 Attenuator 3.73 2.60 Crossover Network XO/950 7.77 5-45 VHARREDALE 8In. Bronze/RS/DD 4.75 3.30 Super 8/RS/DD 14.00 9-95 CARTRIDGES AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 3.75 3.75 AUDIO TECHNICA AT86 6.47 3.46 GOLDRING G800 12:21 4.00 3.60 GOLDRING G800 12:21 4.77 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:58 3.55 4.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 3	Audiom 10P		5 - 67	4-50
Axent 100 6.90 4.80 MIdax 650 13:59 9-50 Attenuator 3.73 2.60 Crossover Network XO/950 7.77 5-45 VHARREDALE 8In. Bronze/RS/DD 4.75 3.30 Super 8/RS/DD 14.00 9-95 CARTRIDGES AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 3.75 3.75 AUDIO TECHNICA AT86 6.47 3.46 GOLDRING G800 12:21 4.00 3.60 GOLDRING G800 12:21 4.77 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:58 3.55 4.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 3	Audiom 12P		21 - 00	14-60
Axent 100 6.90 4.80 MIdax 650 13:59 9-50 Attenuator 3.73 2.60 Crossover Network XO/950 7.77 5-45 VHARREDALE 8In. Bronze/RS/DD 4.75 3.30 Super 8/RS/DD 14.00 9-95 CARTRIDGES AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 4.95 3.50 AMSTRAD 900C 3.75 3.75 AUDIO TECHNICA AT86 6.47 3.46 GOLDRING G800 12:21 4.00 3.60 GOLDRING G800 12:21 4.77 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:57 7.75 GOLDRING G800 Super 2.44 11:58 3.55 4.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 4.55 3.55 3	Audiom 18P	DIN	35 · 70 12 · 00	24·45 8·35
Crossover Network XO/950 7-77 5-45 WHARFEDALE 8In. Bronz/RS/DD 4-75 3-50 Super 8/RS/DD 14-00 9-95 CARTRIDGES AMSTRAD 900C 4-95 3-50 AMSTRAD 900C 7-75 5-50 AMSTRAD 900C 11-00 8-75 AUDIO TECHNICA AT66 6-47 3-45 GOLDRING G850 12-21 4-75 GOLDRING G800 12-21 4-75 GOLDRING G800 12-21 4-75 GOLDRING G800 12-21 4-75 GOLDRING G800 Super E 24-41 15-25 *GOLDRING CS90 Stereo 4-88 3-95 *GOLDRING CS90 Stereo 4-88 3-95	ARU 172		4 · 50	3 · 20
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HEADPHONES—conlinued Rec. KOSS K6. KOSS K6/LC (with volume control) PIONEER SE30 PIONEER SE30A PIONEER SE20A PIONEER SEL20. PIONEER SEL20. ROTEL RH530 ROTEL RH530 WHARFDALE DD1	12:50 9:90 14:00 11:10 21:90 14:20 12:60 8:75 7:88 5:15 10:53 6:80 17:43 11:30 6:50 4:50 9:95 6:75 12:50 8:75
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FERROGRAPH 722		262 · 03 262 · 03	190-15
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2 speed)		74 - 10	56 - 95
		131 - 85	99-95
COLINDIC TK 3200 Hi-Fi (Batte	ry)	141 · 10 39 · 46	105·95 24·95
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4450 4-track stereo 4500 4-track stereo tape dec	k	124 - 30	91-65
PHILIPS 4510 4-track stereo		185 · 00	154 95
deck TANDBERG 2041 4-track (Ster TANDBERG 1841 4-track stere TANDBERG 3021 X twin track s TANDBERG 3041 X 4-track stere	eo)	130 50	108 · 50 49 · 95
TANDBERG 1841 4-track steres	o aeci tereo	113·00 113·00	89-95
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The PR40 R.F. Preselector is the solid state version of the world famous PR30 which it now supercedes. It employs Silicon "N" Channel FET (Field Effect Transistor) front end, followed by silicon NPN Broad Band R.F. Amp., and will substantially improve receiver performance over the range 1-5 to 15 MHz, providing a considerable increase in gain up to an overall average of 30 dB, with improved image rejection and noise ratio.

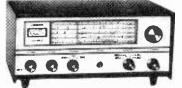
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MULTIBAND—6

SOLID STATE SHORT WAVE RECEIVER KIT

All transistor T.R.F. Receiver tunes 550 KHz to 30 MHz (540 to 10 metres) complete coverage—no gaps. Medium waves—Trawlers—Ship/Shore Telephone—All Six Amateur Bands 160–10 metres—International Broadcast from Australia, Far East, Russia, USA etc. using 4 miniature plug in Coils. Hi-Gain FET Regen. Det./AF/AF Module giving full loudspeaker output to any external 2/3 ohm speaker. Receives AM/CW/SSB. Separate Electrical Bandspread, Calibrated Main Tuning.
A Quality CODAR-KIT with 12 months Guarantee. No technical knowledge required, simple to build, printed circuit and Pictorial Instruction Manual, fully detailed step by step.
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The CODAR CR70A is an outstanding general coverage communication receiver, ideal for the keen S.W.L.

It tunes from 540 metres medium through to 10 metres with no gaps. Covers shipping, coastguard and distress frequencies, all six amateur bands 160-10 metres, International broadcast, Met. stations etc. etc. giving world-wide reception. Exclusive features include Air-spaced CODAR-COIL Hi-"Q" Aerial input, illuminated Meter and Slide Rule Scale, Two Speed vernier tuning, Switched B.F.O. for CW/SSB signals, Separate output for Tape recorder. Ready to plug in to 200/240 volts A.C. it only needs your aerial and a 2/3 ohm loudspeaker to bring the world to your finger tips. 12 months full suggested.

full guarantee.

Complete ready built £27.50, Carriage 70p. Ask the chap who's got one, there's lots of them!

NOTE: These CODAR Receivers meet the B.R.E.M.A. specification for Communication Receivers and are FREE of Purchase Tax. Some portable receivers being advertised as Communication Receivers do not meet these requirements.



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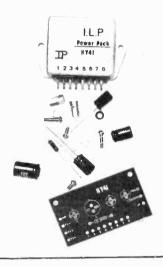
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THE HY41

The HY41 supersedes the popular HY40 introduced by ILP last year. This highly improved module achieves true High Fidelity with a dramatic reduction in distortion (typically 0.05% at 1KHz into 8 ohms!) and is electronically and mechanically compatible with the HY40.

With this important improvement the HY41 retains all of the quality characteristics found in the earlier version and P.C. board, Resistor, Capacitors, Hardware Mountings and comprehensive manual are included in the basic kit. No further components are required to construct a complete power amplifier of extremely high performance sufficiently versatile to provide power not merely for Hi-Fi but also for public address systems and industry.

The free manual gives a full circuit diagram of the HY41 and its various applications including a complete stereo amplifier.

Like its predecessor the HY41 is based on conventional and proven circuit techniques developed over recent years.

OUTPUT POWER: British Rating 40 WATTS PEAK, 20 watts

R.M.S. continuous.

LOAD IMPEDANCE: 4—16 ohms.
INPUT IMPEDANCE: 30K ohms at 1KHz.

VOLTAGE GAIN: 30db at 1KHz

TOTAL HARMONIC DISTORTION: less than 0.15% (typical 0.05%)

FREQUENCY RESPONSE: 5Hz-50KHz + 1db.

SUPPLY VOLTAGE: + 22.5volts D.C. SUPPLY CURRENT: 0.8 amps maximum.

PRICE: inc. comprehensive manual, P.C. board, five extra components and P. & P.:-MONO: £4.90 STEREO: £9.80

UNIQUE HYBRID PRE-AMPLIFIER

The HY5 has rapidly established a position in the WORLD as the sole hybrid pre-amplifier to contain all feedback and equalization networks within an integrated pre-amplifier circuit.

Supplied with the HY5 are two stabilizing capacitors and by the addition of volume, treble and bass potentiometers it is ready for use.

Internally the HY5 provides equalization for almost every conceivable input, the

desired function is achieved by use of a multi-way switch or by direct interconnection, Two distinctive features of the HYS are its inbuilt stabilization circuit, allowing it to be run off any unregulated power supply from 16–25 Volts and a balance circuit which, when linked by a balance control to a second HYS, forms a complete stereo

pre-amplifier. Specifically and critically designed to meet exacting Hi-Fi standards, the HY5 combines extremely low noise with a high overload capability. When used in conjunction with the HY41 and PSU45 forms a completely intergrated system.

Magnetic Pick-up (within ±1db RIAA curve) $2mV. 47K \Omega$ Tape Replay (external components to suit

head). 4mV. $47K\Omega$

head). 4mV. 47K χ 0 Microphone (flat) 10mV. 47K χ 0 Ceramic Pick-up (equalized and compensatable) 20–2000mV. variable. Tuner (flat) 250mV. 100K χ 0 Auxiliary 1 250mV. 47K χ 1 Auxiliary 2 2–20mV. 100K χ 2

OUTPUTS

Main Pre-amp output 500mV. Direct tape output 120mV

ACTIVE TONE CONTROLS (Bexendall) Treble ± 12db. Bass ± 12db.

Bass + 1/20.
INTERNAL STABILIZATION
Enables the HY5 to share an unregulated supply with the Power Amplifier.

SUPPLY VOLTAGE

16-25 volts MONO: £3.60

SUPPLY CURRENT 6mA approx.

OVERLOAD CAPABILITY

IPHY5

better than 26db on most sensitive input infinite on tuner and auxl.

OUTPUT NOISE VOLTAGE: 0.5mV

STEREO: £7.20



POWER SUPPLY PSU45

The versatile P.S.U.45 is designed to supply your HY41's +HY5's in stereo or mono format.

Specification

Input: 200–240 Volts. Output: \pm 22.5 Volts at 2 amps. Overall Dimensions: L. 7"; D. 3.8"; H. 3.1"

PRICE: £4.50 inc. P. & P.

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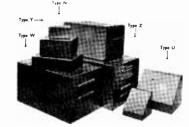


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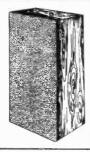
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AUDIO & ELECTRONIC EQUIPMENT EW & SECONDHAND MUSICAL INSTRUMENTS, MAIN ISTRIBUTORS FOR A.K.G. HIGH QUALITY MICROPHONES.

SA25-SA35-SA100

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SA35 £4·45

35 WATTS RMS. 7 Iransistors 7 diodes

SA100 £10[.]9

100 WATTS RMS. 11 transistors 6 diodes

ALL THREE MODULES HAVE OPEN & SHORT CIRCJIT PROTECTION, AND THE SAMM IS PROOF AGAINST OVER-DISSIPATION & FAULTY INDUCTIVE LOADS. ONLY ADVANCED DESIGN TECHNIQUES MAKE THESE EXTRA-ORDINARILY LOW PRICES POSSIBLE.

BRIEF SPEC. FOR ALL THREE MODULES

Freq. response 15-40,000 Hz ± 1dB 0-2% at 1 kHz Distortion

Loads 4 to 16 ohms

Quiescent current 15 mA

Better than - 75 dB Supply voltage

25-45 volts SA25/35 40-70 volts SA100 4½" x 4" x 1" (SA100) 4" x 3" x 1" (SA25/SA35)

Circuits, connecting Instruction and application data are supplied free with all modules.

POWER SUPPLIES FOR THE SA25/35 & SA100 AUDIO MODULES

Stab PS45 Stabilized module for 2 SA25's or two SA35's £3-50 carr, free

Transformer for above, heavy duty £2.85 carr. 20p MT45 Transformer for unstabilized supply complete with rectifier diodes mounted £3.50 carr. 20p MT30

Unstabilized supply for one or two SA100 £6.75 carr. 40p P1170

Stabilized supply module for one or two SA100's £4.90 carr, free PS70 £4.90 carr. 40p MT70 Transformer for PS70

> ALL MODULES ARE BUILT ON GLASS FIBRE P.C. BOARD

OTHER SAXON PRODUCTS. .

120 WATT HEAVY DUTY MODULE £13.90 + 20p carr. or with supply

£18 95 + 40p carr.

Featuring a rugged class A driver stage, this module will run from all our mixers, etc., and most other makes of mixer. It delivers 120 watts into an eight ohm load and employs 4 T03 can (115 watt) output transistors.

SPECIFICATION

Power output
Freq. response
Input sensitivity
Construction
Size
Low distortion parallel push-pull output stage.



SINGLE CHANNEL SOUND/LIGHT CONVERTER

This compact and reliable unit operates from amplifiers with outputs from 5-100 watts. Does not impose a heavy load on the amplifier, or, if connected in the wrong polarity, cause any damage, as with some units.

Operation is simplicity itself and the unit is fully fused. The unit is supplied to function from bass notes but may easily be converted to respond only to treble or mis-range notes by the addition of components costing less than 5p.



carr. £8·90 free

THREE CHANNEL SOUND TO LIGHT UNIT

Handling the total of 3000 watt (3kw) this unit is unique for its price in that not only bass, middle a nd treble but also master controls are provided. Two amplifier sockets eliminate the need for split le ads, etc. Supplied in tough white steel case with a blue stelvette hooded cover. Fully guaranteed.

SAXON STEREO CONTROL UNIT



£15·80 carr. 30n MONO VERSION

£6-50 carr. 20p (As illustrated left S.A.E. details 9 voit

operation) Outputs up to 1 voit RMS

Two deces, and tan neadphone monitoring. The unit is mains operated and measures 17½" x 3" x 4" deep and is finished with a smart white on black facia. The controls are: Left/Right deck fader, volume, bass, treble, Headphone Selector and volume, Microphone volume, bass, treble, mains onloft. THIS IS A MUST FOR THE HOME BUILT HIGH QUALITY DISCOTHEQUE AND IS COMPARABLE TO UNITS AT OVER TWICE THE PRICE.

COMPLETE AMPLIFIERS

The CSE 100, £34.90 carr, free

This versatile unit is now available in a black vynide case and so represents even better value than ever delivering speech and muslc powers of up to 100 watts RMS and continuous sine wave outputs of 70 watts. Two individually controlled inputs with wide range bass and treble controls. Ideal for small groups D.J.S., etc.

The SAXON 100 £48-50 carr. free



With an RMS output of 120 watts speech and music, 100 watts continuous power, four individually controlled FET Input stages and wide range bass and treble controls, this amplifier has established itself as a unit offering quality and reliability at low cost.

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This is real value for money! We have designed 2 systems and the heart of them all is the Viscount III amplifier. A unit of great eye appeal with teak finished cabinet. FET's (Field effect transistors) are incorporated on the input stages, just like top priced units. FET's give you more of the signal you want and almost none of the hiss you don't. Both units have output sockets for headphones and tape recorder. Filters and tone controls give a wide range of bass and treble adjustment.

For both systems we have chosen the famous Garrard SP25 Mk. III deck which comes with fitted magnetic cartridge, simulated teak plinth and tinted accrylic dust cover. The exclusive Duo loudspeaker systems are incomparable for quality within their price range. Large speakers in extremely substantial cabinets. There's a choice of the Duo II's for the smaller room or the big Duo III's for real bass response.

SPEAKERS

Duo Type II Size approx. 17in. \times 10 \pm in. \times 6 \pm in. Drive unit 13in. \times 8in. with parasitic tweeter. Max. power 10 watts, 8 ohms. Simulated Teak cabinet. £14 pair + £2 p&p.

PRICES: SYSTEM 1

Viscount III R101 amplifler 2 × Duo Type II speakers Garrard SP25 Mk. III with MAG. cartridge plinth and cover

£22.00+90p p&p £14.00+£2 p&p £23.00+£1.50 p&p

£59-00

Available complete for only £52 + £3:50 p&p

PRICES: SYSTEM 2

Viscount R101 amplifier 2 × Duo Type III speakers Garrard SP25 Mk. III with MAG, cartridge plinth and cover

£22.00+90p p&p £32.00+£3 p&p £23.00+£1.50 p&p

Total £77:00

Available complete for £69 + £4 p&p



MUSIC MAKERS



UNISOUND FOR THE NEV

The whole system is complete including superb cabinets in simulated teak—just simply screw together

The whole system is complete including superb cabinets in simulated teak—just simply screw together the components and you save pounds!

Amplifier is based on the famous Mullard Unlitex system, Garrard 2025TC turntable complete with stereo ceramic cartridge, teak simulated plinth and tinted acrylic cover. Plus the big 13" x 8" EMI Twin-cone speakers ready for mounting in their elegant cabinets, which simply need screwing and glueing together. All glue and screws supplied.

Easy to follow step-by-step instructions g-ride you quickly and effortlessly to taking the wraps off truly realistic stereo sound.

E25 complete plus £2.80 p. & p.

Dlamond Stylus £125 extra.

Power output: 4 watts per channel into 8 ohms. inputs: 120 mV (for ceramic cartridges).

Stereo headphones with adaptor £4.00

UNISOUND MODULES ONLY £6-95

If you prefer, you can buv the three modules—pre-amplifier, power supplydual power amplifier, and control panel—by themselves for only £6-95. P. & P. 50p extra.

No soldering, just simply screw together with screwdriver supplied. Their overall specification is the same as shown for the complete Unisound console, using the high efficient I.C. monolithic power chips to ensure very low distortion at all power levels, correct operation in all ambient temperatures. full power over the audio spectrum.



'NATURAL' ONLY FRO **TOURIST PB CAR RADIO KIT** If you can solder on printed circuit board

Apart from the output stage, which is an integrated circuit, the only other electronic components that need soldering are some capacitors, resistors, etc. The kit includes a pre-built RF tuner unit, and fully modulised IF stages which are pre-aligned before despatch. As well as electronic components, this kit also contains 2 diamond-spun aluminium knobs, elegant matching front panel, dial, washers, screws and wire.

The Tourist PB is suitable for 12 volt working on both negative and positive earth vehicles. It covers the full medium and long wave bands. Four push-buttons for medium wave, one for long wave. It is permeability tuned and sturdily constructed. Output is a full 2.5 watts into an 8 ohm speaker. But the Tourist PB will operate into any loudspeaker from 8 to 15 ohms. Power consumption is less than 1 amp.

The Tourist PB ran be mounted in any standard size dash panel and it has an illuminated tuning scale for easy reading at night. Chassis size is: 7in. wide, 2in. high and 4#in deep (excluding front panel, etc.).

★ Circuit diagram and comprehensive instructions 50p, free with parts.

★ Fully retractable, lockable, Car aerial £1.25 post paid.

Price only £7:00 + 50p p&p. 8 ohm speaker with baffle and fixing strips £1.50 post free if bought with kit + 25p p&n.

you can build this push-button car radio kit, It's simple-just follow the step-bystep instructions.







SIZE:-121" × 6" × 31".

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★ 5 Electronically Mixed Inputs. ★ 3 Individua! Mixing Controls. ★ Separate bass and treble controls common to all 5 inputs. * Mixer employing F.E.T. (Field Effect Transistor). ★ Solid State Circuitry. ★ Attractive Styling. * Sides Finished in solid teak

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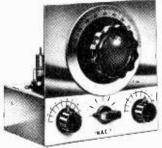
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Press to start button. Stereo headphose and Left and Right Mic sockets on front panel. Qual recording level meter, and Left and Right volume riignt Nick sockets on tront panel. Usal recording level meter, and Left and Right volume controls. Builtin pre-amp. Taps speed 33, pp. (9-5 cms.). Frequency response: playback 30-10,000 Hz, recording/playback 30-8,000 Hz. Line output: fully variable 0-500mV. The RP-1000ST incorporates all the features you'd expect on a top quality Cartilled Tape Oeck. Stre 16' wide. 4' high. 3' deep. Cabinet in walnut. Including connecting leads.

REALISTIC 30 WATT STERED A superb hi-fi amplifier with all the fea-

February 1972 tures you've ever wanted - for under - £46 00. Saving over £10-00 on the normal retail value. Up-to-the-minute slider controls for bass and treble £35.20 volume and balance controls. Headphone socket on front panel. Push-button input controls — magnetic phono (high/low) tuner, aux, mono, monitor. Loudness push-button control for perfect sound at low output levels. Lett and right push-button on/off switches for speakers. Noise filtering ℓ and tape monitoring facilities. Two auxiliary AC outlets. Frequency response 20-20,000 Hz \pm 1 db at full power. 15 watts rms per channel. Walnut cabinet with £55.50 satin aluminium trims. Inputs. phono 2-5mV and 5mV RIAA; tuner/aux 250mV. Hum and noise: phono - 50db; tuner/aux - 65db. How's that for a soecification! Size 14½" wide, 3½" high, 10½" deep



OLSON RA-310 AM/FM/MPX
STEREO TUNER This ROC Tuner is especially designed to match the Olson AM-395

Signed to mater the Usion Ann-333
Stereo. Amplifier. In price and
value, as well as it's good looking design! But of course it's also
the normal retail value and yet it is a highly sophisticated unit, incorporating the latest solid state techniques. Operation is drift free for sup-50.00 reme station-holding capability. You can connect this Tuner to a stereo amplifier, to a tape deck or a tape recorder, And of course it covers all the stations in the AM and FM bands. FM. 87-108 MHz; AM: 525-1605 kHz.

FM Sensitivites: FM, 3µV. AM, 250µV. Stereo separation 30dB at 1kHz, image rejection 60dB. Size: 11 ½ wide, 4 high, 7½ deep.



REALISTIC SA-100B 6-WATT STEREO AMPLIFIER

Here's fabulous, exciting value in miniature! This high quality stereo amplifier measures only 9" wide × 3" high × 5%" deep. And yet it has sepa ate ganged volume, ballance and tone con

trols. Plus speaker in/out, mono/stereo, phono, juner and power on/off slide switches. The ends are oiled walnut, with match ing enamelled metal top. The front panel is satin aluminium and walnut-brown enamel. Frequency response is 50 to 10,000 Hz + 3dB. Output 3 watts r.m.s. per channel into 8 ohms. Inputs are 100mV for both phono and tune



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the radio all by yourself. Then this will solve the problem. Separate volume and tuning controls with easy-to-use knobs. Frequency range is 535 to 1605 kHz medium wave band. Maximum output is 300 mW. Normal Price £7:50 ROC PRICE £5:80

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Here's your opportunit for the price of a ceramic! Is specially de signed to match top quality tone arms, and to get the very best from your hi-fi amplifier. 0-7 mil diamond stylus. Output: 7mV per channel, Frequency range: 20-21,000 Hz. Channel balance: 4 1db, Channel separa-Channel balance: tion: 28dB. Compliance: 12 - 10-6 cm/dyne ROC PRICE £6 37

OLSON AM-395 40-WATT STEREO

An ideal unit for your new stereo separate system. It is more than £10.00 below the normal retail price! Making the AM, 395 one of Britain's best hi-fi

buys. It takes in signals from magnetic or ceramic pick-ups tuners (see Olson RA-310) and tape decks. And it's got outputs for taping and for headphones. There are separate bass and treble controls, separate Left and Right channel volume controls. And a loudness switch for boosting the bass and

treble notes when listening at low output levels. Frequency response: 20-20,000 Hz ± 3dB. Output: 20 watts r.m.s. per channel into 8 ohms. Inputs: magnetic phono 3-0mV RIAA, crystal phono 180mV: tape 160mV; tuner 160mV. Size $11\frac{\pi}{7\pi}$ " wide, 4" high, $7\frac{\pi}{2}$ " deep. The specification reads well – sounds even better!



A-3000 36-WATT
SOLID STATE STERED AMPLIFIER
The A-3000 looks as good as it sounds!
Giving you a big performance this superb audio amplifier has a full range of facilities on the front and rear panels. On the front -all the controls you're ever likely to need plus a headphone socket. On the rear -signal inputs, speaker outputs and a line fuse for circuit protection.

Specifications: 18 watts rms per channel into 8 ohms. Frequency response 20-35.000 Hz (± 2db) Inputs Magnetic, Ceramic, Tuner, Tape, Aux. Tape Play, Size: 345mm × 300mm × 130mm.

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KIT

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Q 25-WATT 3-WAY CRYSLER TIVING AUDIO SPEAKER CE-5b

This binh quality speak er has its own built-in A.way sound response switch giving you the ideal frequency response for hi-fi, natural or mood music listening. Its

beautiful, heavy, oiled walnut cabinet incorporates two separate speaker units an 8" mid-range with 2" concentric tweeter. Power handling capacity: 25 watts rms into 8 ohms. Overall frequency res ~ ponse: 35-20,000 Hz. Cabinet size: $10\frac{1}{2}\%\times7\frac{1}{2}\%\times8\frac{2}{4}\%$. Exactly right for matching the most modern decor. 25 watts r.m.s. into 8 nhms. Overall frequency res

OLSON AM-400 4 WATT STEREO AMPLIFIER Here's marvellous value for someone just starting to set them-selves up in audio 1 At only £10-50, you get a fine amplifier in a scratch resistant metal cabinet, with a smart brushed aluminium front panel, it incorporates separate tone and volume controls for each channel. Inputs are provided for turntable (ceramic cartridge), tuner and tape deck or recorder. Frequency response, 70-20,000 Hz ± 3d8. Output: 2 watts r.m.s. per channel into 8 ohms. inputs: phono 80mV, tuner/aux 80mV, Size 8" wide, 2½" high.



PALACE AM/FM/MPX STERED TUNER AMPLIFIER SSA-16

This is one of the lowest priced stero tuner amplifiers on the market. It covers the full range of both AM and FM broadcast frequencies. And when you're switched to FM, an indicator lights up when a stereo signal is received – that's the time to signist up when a steeled signol is releaved. — Intak she three which to 'Stereo!' The SSA-16 has all the facilities you'd expect to find on tuners costing twice as much—separate volume, bass, treble, balance and tuning controls. Selector switch for tape, phono. AM, FM, stereo. Jack socket on front panel for stereo headphones. Frequency range: FM 88-108 MHz. AM Stereo Headphilles, Frequency response: $50-10,000~{\rm Hz}~\pm~3{\rm dB}$. Power output: 4 waits total music power into two 8 ohm speakers. Size: 16% wide, 4% high, 8% deep.

ROC 7-WATT STEREO AMPLIFIES CHASSIS SK-317 This exclusive completely self-contained, and it costs £2-25 less than the normal re tail value! TI SK-317 is a really

compact unit measuring only 5½" wide. 1½" high and 6½" deep. It contains its own mains power supply, and has a ganged volume control and separate power supply, and has a going of volume treble controls for each channel. Specification: frequency response 40-17 000 Hz \pm 3dB; output 3-5 watts music power per channel into B ohms; input, phono, 600mV, signal-to-noise ratio better than 45dB

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AC117K	0.20		0.55	BC151	0.20	BD140	0 - 60	BF196	0.14	OC23	0.42	20374	0.17		0·20 0·17	2N3391A 2N3392	0·16 0·14	2N4062 2N4284	0·12 0·17
AC122	0.12	ADT140	0.50	BC152	0.17	BD155	0.80	BF197	0.14	OC24 OC25	0 56	2G377 2G378	0·30 0·16		0.14	2N3393	0.14	2N4285	0 - 17
AC125	0.17	AF114	0.24	BC153	0.28	BD175 BD176	0 · 60 0 · 60	BF200 BF222	0 45	OC25	0.25	2G381	0.16		0.14	2N 3394	0.14	2N4286	0.17
AC126 AC127	0·17 0·17	AF115 AF116	0 24	BC154 BC157	0.18	BD177	0.65	BF257	0.45	OC28	0.50	2G382	0.16		0.24	2N3395	0 - 17	2N4287	0.17
AC128	0.17	AF117	0.24	BC158	0.12	BD178	0.65	BF258	0.60	OC29	0.50	2G401	0.30		0.24	2N3402	0·21 0·21	2N4288 2N4289	0·17 0·17
AC132	0.14	AF118	0.35	BC159	0.12	BD179	0.70	BF259	0.85	OC35	0.42	2G414 2G417	0·30 0·25		0-47	2N3403 2N3404	0.21	2N4289 2N4290	0.17
AC134	0.14	AF124	0.80	BC160	0.45	BD180	0.70	BF262 BF263	0.55	OC36 OC41	0 · 50 0 · 20	2N388	0.35		0.21	2N3405	0.42	2N4291	0.17
AC137	0.14	AF125 AF126	0 · 25 0 · 28	BC161 BC167	0·50 0·12	BD185 BD186	0.65	BF270	0.35	OC42	0.24	2N388A	0 - 55	2N2714	0.21	2N3414	0.15	2N4292	0 17
AC141 AC141K	0·14 0·17	AF127	0.28	BC168	0.12	BD187	0.70	BF271	0.30	OC44	0.15	2N 404	0.20		0.17	2N3415	0.15	2N4293	0·17 0·12
ACI41	0.14	AF139	0.30	BC169	0.12	BD188	0.70	BF272	0.80	OC45	0.12	2N404A	0 · 28 0 · 42		0.21	2N3416 2N3417	0 · 28 0 · 28	2N5172 2N5457	0.12
AC1 3K	0.17	AF178	0-50	BC170	0.12	BD189	0.75	BF273	0.35	0C70 0C71	0·10 0·10	2N524 2N527	0.42		0.21	2N3525	0.75	2N5458	0.32
ACIL	0.15	AF179	0.50	BC171	0.14	BD190 BD195	0·75 0·85	BF274 BFW10	0.35	OC72	0.14	2N598	0.42		0.15	2N 3646	0.09	2N5459	0 - 40
AC154	0·20 0·20	AF180 AF181	0 · 50 0 · 45	BC172 BC173	0·14 0·14	BD196	0.85	BFX29	0.27	OC74	0.14	2N599	0.45	2N2906A		2N3702	0.10	28301	0.50
AC155 AC156	0.20	AF186	0.45	BC174	0.14	BD197	0.90	BFX84	0.22	OC75	0.15	2N696	0.12		0.20	2N3703	0.10	28302A 28302	0 · 42 0 · 42
AC157	0.24	AF239	0.87	BC176	0.22	BD198	0.80	BFX85	0.30	OC76	0.15	2N697	0·13 0·24	2N2907A 2N292a	0 22	2N3704 2N3705	0·11 0·10	28302	0.55
AC165	0.20	AL102	0.65	BC177	0.19	BD199	0.95	BFX86 BFX87	0·22 0·24	OC77 OC81	0.25	2N698 2N699	0 35	2N2924	0.14	2N3706	0.09	28304	0.70
AC166	0.20	AL103	0 · 65 0 · 25	BC178	0·19 0·19	BD200 BD205	0.80	BFX88	0.22	OC81D	0.15	2N706	0.08	2N2925	0.14	2N3707	0.11	28305	0.84
AC167 AC168	0.20	ASY26 ASY27	0.80	BC179 BC180	0.24	BD206	0.80	BFY50	0.20	OC82	0.15	2N706A	0.09	2N 2926 (C		2N3708	0.07	28306	9 84
AC169	0.14	A8Y28	0.25	BC181	0.24	BD207	0.95	BFY51	0.20	OC82D	0.15	2N708	0.12	0370006 /1	0.12	2N3709	0.09	28307 28321	0·84 0·56
AC176	0.20	A8Y29	0.25	BC182	0.10	BD508	0.95	BFY52	0.20	OC83	0.20	2N711 2N717	0·30 0·35	2N2926 (0.11	2N3710 2N3711	0.09	28322	0-42
AC177	0.24	ASY50	0 25	BC182L	0.10	BDY20	1·00 0·24	BFY53 BPX25	0·17 0·85	OC84 OC139	0.20	2N718	0.24	2N2926 (C		2N3819	0.28	28322A	0.42
AC178	0.28	ASY51 ASY52	0 · 25	BC183 BC183L	0·10 0·10	BF115 BF117	0.45	B8X19	0.15	OC140	0.20	2N718A	0.50		0.10	2N3820	0.50	28323	0 - 56
AC179 AC180	0·28 0·17	A8 Y54	0.25	BC184	0.12	BF118	0.70	BSX20	0.15	OC169	0.25	2N726	0.28	2N2926 (2N3821	0.35	28324	0·70 0·70
AC180 K		ASY56	0.25	BC184L	0 12	BF119	0.70	B8 Y 25	0.15	OC170	0.25	2N727	0.28	0310000 (1	0.10	2N3823 2N3903	0.28	28325 28326	0.70
AC181	0.17	ASY56	0.25	BC186	0.28	BF121	0 - 45	BSY26	0.15	OC171 OC200	0 · 25 0 · 25	2N743 2N744	0.20	2N2926 (1	0-10	2N3904	0.30	28327	0.70
AC181 K		A8Y57	0.25	BC187	0.28	BF123 BF125	0 - 50	BSY27 BSY28	0·15 0·15	OC200	0.28	2N914	0.14	2N3010	0.70	2N3905	0.28	28701	0 42
AC187	0.22	ASY58 ASZ21	0.25	BC207 BC208	0·11 0·11	BF127	0.50	BSY29	0.15	OC202	0.28	2N918	0.30	2N3011	0.14	2N3906	0 27	40361	0.40
AC187 B AC188	0.22	BC107	0.09	BC209	0.12	BF152	0.55	BSY38	0.18	OC203	0.25	2N929	0.21	2N3053	0.17	2N 4058	0-12	40362	0 - 45
1 C188 K		BC108	0.09	BC212L	0.11	BF153	0.45	BSY39	0.18	OC204	0.25	2N930 2N1131	0 21						
ACY17	0.25	BC109	0.10	BC213L	0.11	BF154 BF155	0.45	BSY41	0·28 0·28	OC205 OC309	0 85	2N1131	0.22		DIAL	ES AND	וזייים ס	POST	
ACY18	0 · 20 0 · 20	BC113 BC114	0·10 0·15	BC214L BC225	0 · 14 0 · 25	BF156	0.48	B8Y95	0 12	P346A	0.20	2N1302	0.14						
ACY19 ACY20	0.20	BC114	0.15	BC226	0.35	BF157	0.55	B8Y95A	0.12	P397	0.42	2N1303	0.14	AA119	0.08	BY 133	0.21	OA10 OA47	0.35
ACY21	0.20	BC116	0.15	BCY30	0.24	BF158	0.55	Bu105	2.00	OCP71	0.43	2N1304 2N1305	0 17	AA120 AA129	0.08	BY164 BYX38/3	0 - 50	OA70	0.07
ACY22	0.16	BC117	0.15	BCY31	0.26	BF159 BF160	0.80	C111E C400	0.50	ORP12 ORP60	0.43	2N1305	0.21	AAY30	0.09	21200/	0.42	OA79	0.07
ACY27	0.18	BC118	0·10 0·30	BCY32 BCY33	0·30 0·22	BF162	0.40	C407	0 25	ORP61	0.40	2N1307	0.21	AAZ13	0.10	BYZ10	0.35	OA81	0.07
ACY28 ACY29	0·19 0·35	BC119 BC120	0.80	BCY34	0.25	BF163	0.40	C424	0.20	ST140	0.12	2N1308	0.23	BA100	0.10	BYZ11	0.30	O A 85	0.09
ACV30	0.28	BC125	0.12	BCY70	0.14	BF164	0.40	C425	0.50	ST141	0.17	2N1309	0.23	BA116 BA126	0 · 21 0 · 22	BYZ12 BYZ13	0.30	OA90 OA91	0.08
ACY31 ACY34	0.28	BC126	0.18	BCY71	0.18	BF165	0.40	C426 C428	0.35	T1843 UT46	0.30	2N1613 2N1711	0.20	BA148	0.14	BYZ16	0.40	OA95	0.07
ACT34	0.21	BC132	0.12	BCY72	0.14	BF167 BF173	0.22	C428	0.30	2G301	0.09	2N1889	0.32	BA154	0.12	BYZ17	0.35	OA200	0.08
ACY35 ACY36	0·21 0·28	BC134 BC135	0·18 0·12	BCZ10 BCZ11	0.25	BF176	0.85	C442	0.30	2G302	0.19	2N1890	0 - 45	BA155	0.14	BYZ18	0.35	OA202	0.07
4CY40	0.17	BC136	0.15	BCZ12	0.25	BF177	0 - 35	C444	0.85	2G303	0 19	2N1893	0.37	BA156	0.13	BYZ19 CG62	0.28	8D10 8D19	0·05 0·05
ACY41	0.18	BC137	0.15	BD121	0.60	BF178	0.80	C450	0.22	2G304	0 24	2N2147 2N2148	0 · 72 0 · 57	BY100 BY101	0·15 0·12	(Eg) OA	91	1N34	0.07
ACT44	0.85	BC139	0.40	BD123	0.65	BF179 BF180	0.30	MAT100 MAT101	0 19	2G306 2G308	0.40	2N2148	0.80	BY 105	0.17		0.05	IN34A	0.07
A D130	0.38	BC140 BC141	0.80	BD124 BD131	0.60	BF181	0.30	MAT120	0.19	2G309	0.35	2N2192	0.35	BY114	0.12	CG651		1N914	0.06
AD140 AD142	0 · 48 0 · 48	BC141	0.30	BD132	0.60	BF182	0 - 40	MAT121	0.20	2G339	0.20	2N2193	0.35	BY126	0.14	(Eq) OA OA79	70- 0-06	1N916 IN414B	0 · 06
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AD149	0.50	BC145	0.45	BD135	0.40	BF184	0 25	MPF104 MPF105	0.37	2G344 2G345	0·18 0·16	2N2217 2N2218	0.20	BY130	0.16	OASSL	0.21	18951	0.06
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8N7433	0.80	0.75	0.70 8N7495	0.77	0.74	0.68 SN74184 £3:50	£3 · 25	£3.00
SN7437	0.64	0.62	0.60 8N7496	0.87	0.84	0 78 SN74190 £1 95	£1 · 90	£1 85
SN7438	0.64	0.62	0.60 8N7410	0£1.65	£1.60	£1-55 8N74191£1.90	£1 · 85	£1.80
SN7440	0.15	0.14	0.12 SN7410	4 0.97	0.94	0.88 SN74192 £1.95	£1 · 90	£1 85
8N7441	0.67	0.64	0.58 SN7410	5 0.97	0.94	0.88 SN74193 £2.00	£1 80	£1.75
8N7442	0.67	0.64	0.58 SN7410	7 0.40	0.38	0 · 36 SN74194 £2 · 70	£2 60	£2·50
SN7443	£1 · 30	£1 · 25	£1 · 20 8N7411	0 0.55	0.53	0.50 SN74195 £2.00	£1 · 90	£1.80
SN7444	£1.30	£1 · 25	£1 -20 SN7411	1 £1 · 25	£1 · 15	£1 · 10 SN74196 £1 · 80	£1.70	£1.60
8N7445	£1.80	£1 · 77	£1.75 8N7411	8 £1 · 00	0.95	0.90	£1 · 70	£1 · 60
8N7446	0.97	0.94	0.88 SN7411		£1 · 25		£5.00	£4 50
BN7447	£1 · 00	0.97	0.95 8N7412	0 40	0.37	0.34 SN74198 £5.50		
SN7448	£1 · 00	0.97	0.95 SN7412	2£1-40	£1 · 30	£1 · 10 8N 74199 £5 · 50	£5 · 00	£4 · 50
								1

LINEAR I C's-FULL SPEC

LINEAR I.C S-I OLL SI LC.						
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BP 201C-SL201C	63p	53p	45p			
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BP 702C-8L702C	63p	50p	45p			
BP 702-72702	53p	45p	40p			
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BP 71072710	44p	42p	40p			
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TAA 263-	70p	60p	55p			
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8.G.S. EA1000 2-62

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BP933		135	12p	11p
BP935		135	12p	11p
BP936		135	12p	11p
BP944		13p	12p	11p
BP945		25 p	24p	22p
RP946		12p	11p	10p
BP948		25p	24 p	22p
BP951		655	60p	55p
BP962		125	11p	10p
BP9093		40p	38p	35 p
BP9094		40p	38p	35p
BP9097		400	38p	35p
BP9099		40p	38p	35p
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Devices may be mixed to qualify for quantity price. Larger quantity prices on application. (DTL 930 Series only)

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MODEL	CD66	GR116	3015F Minitron
Anode voltage (Vdc)	170min	175min	5
Cathode Current (mA)	2.3	14	8
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Tube Height (mm)	47	32	22
Tube Diameter (mm)	19	13	12 wide
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All indicators 0-9 + Decimal point. All side viewing. Full data for all types available request.

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- * Signal to noise ratio 80dB.

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TRANSFORMER BMT80 £1-95 p. & p. 25p.

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Built to a specification and NOT a price, and yet still the greatest value on the market, the PA100 stereo pre-amplifier has been conceived from the latest circuit techniques. Designed for use with the AL50 power amplifier system, this quality made unit incorporates no less than eight silicon planar transistors, two of these are specially selected low noise NPN devices for use in the input stages.

Three switched stereo inputs, and rumble and scratch filters are features of the PA100, which also has a STEREO/MONO switch, volume, balance and continuously variable base and treble controls.



SPECIFICATION

Frequency Response Harmonic Distortion Inputs: 1. Tape Head
2. Radio, Tuner
3. Magnetic P.U.

better than 0.1% 1.25 mV into 50 K Ω 35 mV into 50 K Ω 1.5 mV into 50 K Ω

All input voltages are for an output of 250mV. Tape and P.U. inputs equalised to RIAA curve within ± 1dB, from 20Hz to 20KHz. Bass Control

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20Hz - 20KHz ± 1dB

292mm × 82mm × 35mm ONLY £11.95

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Garrard 40B deck only	***	£9·50
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complete with KS40A ste	reo ceramic	

... £39·95 .. £37 · 50 C & P £1 · 50 Garrard ZERO 100S Single Player

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VVB4 Mk, II Plinth	1		 	€5 · 45
SPC4 Mk. II cover			 	£4·25
Price together		***	 	£8·70
WBI Plinth			 100.0	£3 · 70
SPCI cover			 20.5	£3 · 60
Price together		100	 	£6·50

Garrard Module Series Modules are complete wired units with cartridge, plinth and cover.

SP25 Mk. III Module SP25 Mk. III with SHURE M75/6 cart. €23-95

AP76 Module AP76 with SHURE M75/6 cartridge £33-95

AP96 Module

ngle play version of SL95B with SHURE M75/6 cartridge ... €38-75 Zero 100S Module

ZERO . 100\$ with SHURE M93/E cartridge

CARRIAGE—all units DECK ONLY 50p. PLINTH & COVER ONLY 25p. DECK WITH PLINTH AND COVER 75p.

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€45 .00

C & P

BSR McDONALD MP60 High precision low-

mass counter balanced piets ed pick-up heavy balanc ble, simple balanced turntable, simple to operate controls, viscous cueing device, slide in cartridge carrier, 4 pole motor. LASKY'S £10.40

LASKY'S £10-40 C& P50p
BSR McDONALD UNITS & PACKAGES
A. Chassis only. B- Complete with Lasky's plinth
cover and AD76K cartridge. C. As B but with
Shure M55E cartridge. D. McDonald TPD/I
package. E. As D plus Goldring G800 cartridge.
MODEL
A B D E
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HT.70 14-75 22-95 25-50 21-50 23-95
610 13-75 22-95 25-50 21-50 23-95
610 Cartridge with plinth, cover & BSR cartridge
MP.60 TPD2 Styrene base
17-50 21-00
810 transcription model 810 transcription model 810 with BSR plinth and cover

BSR TD8S

8 TRACK STEREO CARTRIDGE PLAYER The TD8S is suitable for use with most modern stereo amplifiers and delivers a

Power requirements: 210/250V AC, 50Hz. Frequency response: 50Hz-10KHz. 4 pole dynamically balanced synchronous motor. Black and woodgrain plastic cabinet. Size: 8½(W) × 3½(H) × 10½ (D) in. List LASKY'S FIICE £17-95 PRICE

AUDIO-TRONIC

JUST **PUBLISHED**

The 1973 edition of Laskys famous "Audio-Tronics Pictorial" is now available. Bigger, brighter and better than ever. Laskys brand new catalogue now contains 48 pages packed with all the latest Hi-Fi and electronics equipment—everything for the layman and enthusiast alike. All the goods shown in the "Audio-Tronics goods shown in the "Audio-Tronics Catalogue" are available from any of our branches or by Mail Order to any address in the U.K. or overseas. Free on request. Just send your name, address and 15p for post and inclusion on our regular mailing

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53in. RT.24 Standard play 900ft. P.V.C.	68p
5∄in. RT.14 Long play 1,200ft. Mylar	75p
5≩in. RT.25 Triple play, 2,400ft	€1-31
7in. RT.22 Standard play, 1,200ft. Acetate	63p
7in. RT.10 Standard play, 1,200ft. Mylar	63p
7in. RT.12 Long play, 1,800ft. Mylar	95p
7in. RT.13 Double play, 2,400ft. Mylar	£1 · 25
7in. RT.11 Long play, 1,800ft. Acetate	75p
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LASKY'S NEW LOW NOISE CASSETTES FROM THE USA

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C120		47p	£2·	29	£4 ·	48	£6.59
Each	cassette	individ	dually	boxed	in	Philips,	type

plastic library. C & P: each 7p, 5—25p, 10—40p, 20—68p.



Special quotes for quantities,

AKAI TAPE RECORDER SCOOP 1

(C & P 75p on all Tape Decks.)

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2 ADM 11/8 mics. Suitable for use on all Akai tape recorders. L £7 50. C & P 15p. List Price £11-90. Lasky's Price

BSR TAPE DECK SCOOP



FANTASTIC VALUE, ONLY Lasky's can offer you a tape deck at such an amazing price. The BSR TD2 tape deck operates by a simple reliable mechanism. Available with ½ track or ½ track mono or stereo heads. Incorporates fast wind and fast rewind, records at 3½ ips, giving up to 3 hrs playing time, takes up to 5½in, spooss, Size 13in, x 8½in, front to rear, 2½in, below plate, 1½in, above plate.

ALSO SUITABLE FOR USE AS A TAPE TRANSPORTER
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Incorporates varicap diodes, printed circuit, coils, squelch circuit I.C. Decoder, etc., supplied completely built and tested and ready to be mounted into any cabinet you choose. It may be used with any High Fidelity Amplifier. Power requirements 25/30V DC. Size 8½* x 1½* x 3½*.

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The clock measures
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(overall from front
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NEW WELLER MINI-SHOP KIT • 600K

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Ideal for handymen, and professionals.

The wide selection of bits helps you grind, sharpen, drill, rout, cut etc. Perfect for delicate work. The complete kit is housed in a strong plastic case.

MODEL 600K 37 piece Kit contains:

Model 600 Power Unit © Accessory Caddy © 8 Grinding/Sharpening Bits © 3 Polishing Wheels Of Accessory Caddy Plastic Case.

4 Cleaning Bits © 8 Abrasive Discs © 3 Abrasive Bands © Expanding Drum © Drill Bit © Mandrell © Chuck Wrench © Dressing Stone © Plastic Polish | Jewellers Rouge © Complete with owners manual Size of power unit only 7½°.

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WIRELESS

VOL 48 NO 8

Issue 790

DECEMBER 1972

Happy Anniversaries

IF you have been orbiting in space, trekking across the Gobi Desert or drifting down the Amazon for the past few months, it is possible that the news of the great event about to be celebrated has not filtered through. Otherwise, you will be aware that this month the BBC notches up the 50th Anniversary of broadcasting in the UK.

Special programmes are being broadcast on radio and television, exhibitions are being mounted by the BBC and others, the Post Office has issued a special set of postage stamps, the IEE is staging a series of lectures. After such a welter of words, pictures and sounds, what is there left to say? Not a lot, really, except for Practical Wireless to add its tribute to all those on the engineering, programme and administrative sides, who over the past 50 years have made a contribution towards what is still (despite its lovable faults) the best broadcasting service in the world.

But while we are indulging in flag-waving, let us not forget the unsung heroes who have also played a part in the development of broadcasting—the component makers, the set makers, the performers, the backroom boys and those overlooked but staunch martvrs, the listeners themselves!

There is yet another group who, collectively, deserve a modest pat on the back—our colleagues, past and present, who presumably through some inherited defect (or sheer masochism) decided to devote their life to the career of technical journalism! In the early days of broadcasting, and even before it, the technical journals generated and sustained the interest in the subject. The famous magazines of the day, such as Popular Wireless, Wireless Magazine and Amateur Wireless have long been but memories, but three of the pioneer publications are still with us—Wireless World, Practical Wireless and Television (which started life as Practical Television as early as 1934).

At the risk of being dubbed chauvinistic, this seems to be the right occasion to mention (with a becoming blush) that during the BBC festive season of celebrating their 50th Anniversary, readers may like to raise a flag or two in recognition of the fact that this year *Practical Wireless* is a contender in the Anniversary Stakes, having now reached its 40th birthday—a period of time during which, like the famous Windmill, we never closed!

W. N. STEVENS-Editor.

NEWS AND COMMENT

Leader	691
NewsNews	692
Practically Wireless by Henry	720
Electronotes by S. Ginsberg	728
MW Column by Charles Molloy	731
On the Short Waves	
by Malcolm Connah and	
Ďavid Gilbson, G3JDG	741
Letters	745

CONSTRUCTIONAL

Amateur Bands Receiver, Part 1	
by F. G. Rayer, G3OGR	694
Loudhailer and Siren	
by A. Lester-Rands	701
Transistors in Transmitter PA Stages	700
by R. Dowling G3NKH	709
Take 20, No. 43, Audio Mixer	744
by Julian Aηderson_	714
The "Music Maker" Electronic Organ	740
by D. Smith	716

Iniversal Bridge	
by Halvor Moorshead	724
Reverberation Unit, Part 2	
by F. C. Judd	729

Nutomatic	Emergency 250V	Suppl	у
by S. Soa			732

OTHER FEATURES

IC of the Month,
Hyreg Power Regulator
by L. A. J. Ireland
Transistor Circuitry for Beginners,
Part 13 by H. W Hellyer and
Michael Hollier
Going Back by Colin Riches and
Arthur Dow

COMPETITION

WIN A HEATHKIT 'SCOPE

THE JANUARY ISSUE WILL BE PUBLISHED ON DECEMBER 1st

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746

721

NEWS...

NEWS...

NEWS...

Bristol '73

The Bristol Group of the R.S.G.B. are now privileged to announce their plans for participation in the 1973 anniversary celebrations of the granting of the Royal Charter to the City and County of Bristol.

One aspect will be the operation of an amateur radio exhibition station on the S.S. *Great Britain*, now being restored in dry dock at Bristol.

The Ministry of Posts and Telecommunications, as the licensing authority, has agreed to the special call sign "GB2GB" for a station to be operated from the vessel and will permit the station to be operated by persons holding current Amateur (Sound) Licences A who visit the vessel during the month of August, 1973.

The general public will hear contacts being made with amateur radio stations, both local and long distance, and information will be available from the operators on the hobby of amateur radio and the role it plays in promoting international understanding.

With the co-operation of the S.S. Great Britain Project, receiving tests already carried out from the vessel have indicated that the site is suitable for reception and therefore transmission is not considered to present any problems.

It is anticipated that the station will make contacts with stations in other Bristols and the cities of Hanover and Bordeaux. Contact will also be attempted with amateur radio stations in the Falkland Islands where the vessel lay in Sparrow Cove for many years.

Specially designed cards depicting the S.S. Great Britain will be sent to amateur radio stations contacting GB2GB and these are being donated by a famous firm of Bristol wine merchants who have also agreed to present cases of sherry as awards in a Bristol Amateur Radio Activity Contest to be held in 1973, details of which will be announced in a few months' time.

As 1973 is also the Diamond Jubilee of the Radio Society of Great Britain, local members are pleased to announce that a convention will be held at a local botel. This is to be on the 26th May, 1973, and details are now being planned.

It is hoped that these events—GB2GB on the S.S. *Great Britain*, and radio contest, and the convention, will make 1973 a memorable year for Bristol and radio amateurs.

Further gen from G. Mather G3GKA, 8 Hills Close, Keynsham, Bristol.

The "Elf"



West Hyde announce the Contil "ELF". Only 6in. x 4in. x 4in., they are offered at five cases for £6 including postage and packing. (£1·25 ea. + 10p p.p.)

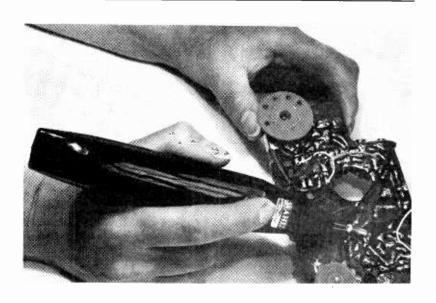
Glass polyester dough moulded in grey or blue, the price includes a chromium plated handle, an aluminium chassis, a protectively coated aluminium front panel and four fitted feet.

Two printed circuit boards can be fitted in the slots provided internally, making the case ideal for the increasing number of applications requiring miniature cases, in step with the firm's well known policy this tough smart little case is available by return of post. West Hyde Developments Ltd., Ryefield Crescent, Northwood Hills, Northwood, Middx.

Portable rechargeable soldering iron

Soldering with the new 8in, long portable, lightweight soldering iron-which is rechargeable and can be used far from a power source-launched by the Van Dusen Aircraft Supplies Company in the UK and Europe. The "Iso-Tip" soldering iron, weighing less than 6 ounces, has been designed to handle, with speed and effievery industrial ciency, domestic soldering requirement. Price of unit and stand is £8.75. Van Dusen Aircraft Supplies Co., Oxford Airport, Kidlington, Oxford.

Picture shows the iron in use.



NEWS...

NEWS...

NEWS...

Pictures on the phone

EMI has entered the facsimile communications market with a document transceiver for sending clear, accurate copies of documents in minutes to anywhere in the world. Known as the EMIfax HF146, this compact, desk-top system transmits and receives any type of document up to A4 size (220 x 305 mm), including invoices, lists, graphs, sketches and handwritten notes, over public or private telephone networks.

A unique cost-saving advantage of the EMIfax machine is that normal office stationery is used for reproducing transmitted copies, eliminating the need for expensive coated papers which create both cost and supply problems. The document transceiver is priced at £900. Leasing and rental facilities are also available.



A quick NIP

NIP Electronics, mentioned in our October News . . . pages have asked us to say that two of the readers who have written to them asking for information on NIP-E-BOARDS omitted to give their full addresses.

If they would please communicate with NIP again, giving their full addresses, they will be pleased to supply the items they require.

The readers are: Mr. A. M. Coppin, 128 Fernside Avenue and Mr. Christopher Jones of Coventry.

NIP Electronics, P.O. Box 11, St. Albans, Hertfordshire.

Texan Reprints

Reprints of the "Texan" 20+20W Stereo Amplifier are now available.

They may be obtained by sending 35p (30p + 5p postage/packing) to Practical Wireless Editorial, Fleetway House, Farringdon Street, London, EC4A 4AD

Paramo Handyvice

Latest addition to the Paramo range of tools is a new design of vice. The vice is manufactured from die cast high strength aluminium alloy, designed to give comparable strength to the standard cast iron product, but with considerable savings in weight.

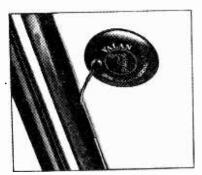
The vice is available in three forms, a 3in. fixed base mechanics vice (HV1), a 3in. swivel base mechanics vice (HV2), a 3in. swivel base mechanics vice with table clamp (HV3).

The vice is finished in hammer blue enamel with chrome plated moving parts. It is supplied with hardened file cut steel jaws and a steel anvil for light metal forming. On the swivel base versions a simple single handed locking lever enables the vices to be swivelled through 360°.

Prices are: HV1, £2·45; HV2, £2·95; HV3 (illustrated), £3·45.— F. Parramore & Sons (1924) Ltd., Caledonian Works, Chapeltown, Sheffield, Yorkshire.



Disc car aerial



A new car radio aerial is being introduced by Valan Electricals to complement their wide range of conventional aerials.

Named the Valan Disc Aerial, it combines the function of an aerial with that of the road tax licence holder or a club card holder, and is fitted on the wind-screen.

It can be fitted in minutes by anyone. The fitting instructions are simple and are on the reverse of the pack. It works equally well in all makes of car and commercial vehicles.

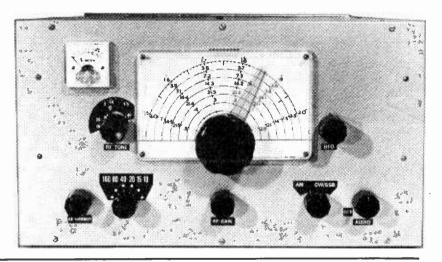
The recommended retail price is £1·20. The Valan Disc Aerial is available from Halfords and leading garage and accessory shops. Valan Electricals, 1034 Yardley Wood Road, Birmingham B14 4BW.

QSL from the BBC

This month there will be an opportunity for listeners to the BBC World Service programme, World Radio Club, to possess one of the BBC's QSL cards verifying reception of the Club's 50th Anniversary Edition.

There are 12,000 members of the Club, spread all over the world. The programme is broadcast on Thursdays at 1330, Fridays at 2345, and Sundays at 0815 GMT in the World Service. Any member who reports accurately on reception of the Anniversary Edition on November 9th, 10th or 12th will be able to receive this QSL.

If you are not a member, write to World Radio Club, BBC, Bush House, London.



1.8-30MHz AM-CW-SSB BANDSWITCHED EASY CALIBRATION

PART 1

use of a crystal controlled oscillator also gives an

HIS receiver possesses high stability coupled with excellent sensitivity, selectivity and adequate bandspread covering the Amateur bands from 10 to 160metres. On all bands, except 80m, the receiver employs double conversion with a crystal controlled first oscillator. It is easy to tune and to hold a.m., c.w. or s.s.b. signals on all bands.

Those who may not be familiar with the method of operation of this type of receiver should find the block diagram of Fig. 1 helpful in conjunction with the description that follows.

CIRCUIT

Referring to Fig. 1 stage (1) is an r.f. amplifier followed by the first mixer (2) both working on all bands except 80m. Each Amateur band, except 80m, employs a crystal (3) chosen so that the output of the mixer (2) falls in the range 3.5 to 4MHz whatever the band in use. This tuning range 3.5 to 4MHz is covered by the tunable r.f./i.f. amplifier (4) and is followed by the second mixer and tunable oscillator (5) forming the tunable i.f. part of the receiver on all bands, except 80m. On 80m signals fall in the range 3.5 to 4MHz and are switched to stage (4).

The output frequency of the second mixer (5) is 455kHz which goes to the crystal filter (6) which is a bandpass filter with 2kHz crystal separation. When using a single filter for a.m., c.w. and s.s.b. this is about the highest degree of selectivity which can be tolerated without excessive cutting of the sidebands of a.m. signals.

Stages (7) and (8) are 455kHz i.f. amplifiers followed by the a.m. diode detector (9), its output going to the a.f. amplifier and output stages (10) and (11) and thence to the speaker. For c.w. and s.s.b. reception the beat frequency oscillator (12) and product detector (13) are switched into circuit. Both tunable oscillators (5) and (12) are fed from a voltage regulated source (14).

As the first i.f. is 3.5 to 4MHz the second channel interference, which can be troublesome on the h.f. bands with a lower i.f., is virtually eliminated. The enormous improvement in overall stability.

F. G.RAYER G30GR

The tuning coverage of each band is a constant 500kHz with fixed 100kHz calibration points which completely eliminates any calibration problems on the h.f. bands. One disadvantage is that because the 10m band is so wide only a small portion of it can be covered but this can be overcome by providing two or more 500kHz sections with very little extra circuitry, as explained later.

CONVERSION FREQUENCIES

As stated the tunable i.f. covers 3.5 to 4MHz and is calibrated at 100kHz intervals. The crystal frequency for the 160m band is 5.5MHz the difference or signal frequency selected by stages (1) and (2) thus extending from 1.5 to 2MHz (5.5.3.5 and 5.5.4). In this case the oscillator frequency is on the high side of the tunable i.f.

Band	Crystal	Calibration MHz					
80	None	3.5	3.6	3.7	3.8	3.9	4.0
160	5.5	2.0	1.9	1.8	1.7	1.6	1.5
40	11	7.5	7.4	7.3	7.2	7 · 1	7.0
20	10.5	14.0	14.1	14.2	14.3	14 · 4	14 · 5
15	17.5	21.0	21 · 1	21.2	21.3	21 · 4	21 · 5
10	24.5	28.0	28 · 1	28 · 2	28.3	28 · 4	28 · 5

For 40m an 11MHz crystal is used giving coverage of 7 to 7.5MHz the crystal again being on the high side. Crystal frequencies for the remaining bands are shown in the accompanying table and it will be noted that they are all below the signal frequency. Calibration points are shown, the direction being reversed on 160 and 40m because these crystals are above the signal frequency.

Since stages (1) and (2) cover 28 to 30MHz three 500kHz segments can be obtained by simply selecting the appropriate crystal with a three way switch, crystals on 25 and 25.5MHz adding bands 28.5 to 29MHz and 29 to 29.5MHz.

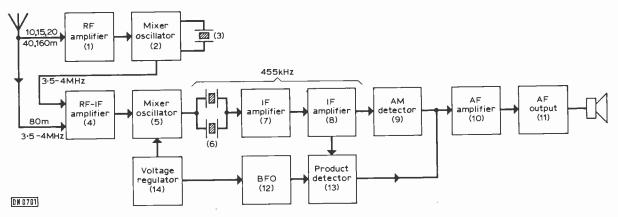


Fig. 1: Block diagram to illustrate the function of each stage in a double conversion communications receiver.

PROGRESSIVE CONSTRUCTION

The constructional work involved is naturally not simple but it can be carried out and tested in sections. This method has much to recommend it as the location of a wiring fault or error is then much easier. The audio stages together with the power supply can be wired and tested with a pick-up or audio oscillator as a signal source. Stages (4) and (5) with one i.f. stage and the a.m. detector can be added thus forming a complete 80m receiver.

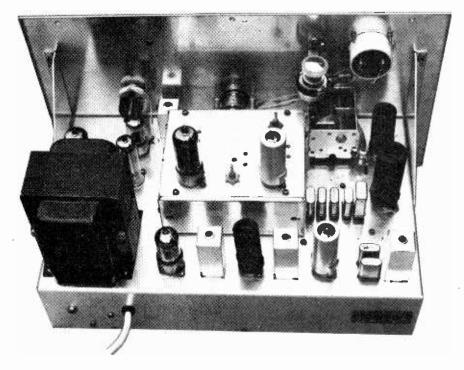
Next the additional i.f. stage and filter together with the b.f.o. and product detector will provide additional selectivity and c.w. and s.s.b. facilities. Stages (1) and (2) should then be wired for one additional band and checked after which the other bands can be added one by one. This general plan will be followed in the articles that follow.

AF/POWER SUPPLY

In Fig. 2D showing this part of the circuit VR1 is the usual audio volume control, followed by a 2-stage amplifier, the output section of the ECL86 providing about 3 watts of audio. An output jack connected to the secondary of the speaker transformer T1 permits the use of phones or an external speaker automatically silencing the phones. This facility can be useful when operating the receiver with a transmitter.

The mains transformer T2 and rectifiers D1 and D2 supply 250V for the triode anode, pentode screen grid and earlier stages of the receiver. The OA2 voltage regulator provides a stabilised 150V supply for the tunable i.f. oscillator and beat frequency oscillator.

If T2 is not as listed, the h.t. voltage may be



Rear view of the completed receiver with the tunable IF amplifier in its own screened box on top of the chassls with the five crystals for the first mixer stage to the right. The two crystals at the bottom right are part of the fixed IF amplifier.

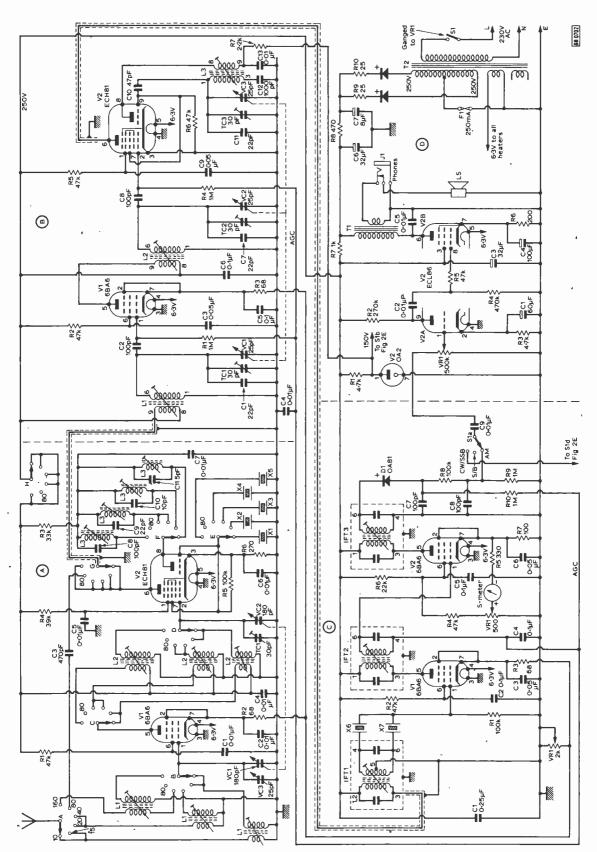


Fig. 24-B-C-D. Complete circuit diagram of the receiver with the exception of the b.f.o.lproduct detector shown on the next page, Fig. 2E.

different. This has little effect on most stages of the receiver, but if it is found that the OA2 is extinguished or nearly so, with the receiver on any band other than 80m and with no aerial connected and the r.f. gain control at maximum gain, then the h.t. is too low. It is then in order to reduce R7 or R8, or both, to obtain about 250V.

Leads to VR1 run against the chassis and need not be screened but R5 should be soldered directly to pin 8 of the ECL86. A 250mA fuse is placed in a holder on the inside of the chassis, and is in the h.t. circuit from T2 to earth.

The heaters require about 3A and are run from the 6.3V 4A winding of T2. If a transformer is fitted which has two 6.3V windings, rated at less than 3A, use one heater winding to supply some heaters and a separate circuit from the other heater winding to the remaining heaters.

The a.f. amplifier and power supply can be checked by connecting a pick-up, audio signal generator or other source of a.f. to the top of VR1. A 3Ω speaker is connected to or plugged into J1.

IF STAGES

Fig. 2C is the circuit of this section of the receiver which operates at 455kHz. IFT1 is an intermediate frequency transformer with a centre-tapped secondary the centre tap being earthed. Balanced output in opposite phase, from pins 4 and 6, go to the two crystals X6 and X7, which have a frequency separation of about 2kHz. This pass-band can readily be modified, as described later. It is, however, a reasonable degree of fixed selectivity for all general amateur band purposes and avoids the need for an adjustable phasing capacitor.

Valves VI and V2 are the two i.f. stages at 455kHz both receiving bias from the a.g.c. line (which also passes to some earlier stages). The manual gain control VR1 adjusts the cathode bias of the first i.f. stage.

Diode D1 provides bias for the a.g.c. line and also operates as the a.m. detector.

Switch S1a is one pole of a 3-way switch, and when in the "AM" position feeds audio via C9 to the volume control.

When Sla is in the "CW/SSB" position, audio signals are fed from the product detector, Fig. 2E. The central position of Sl is for "Standby" when h.t. is removed from several stages.

S-METER

Incoming i.f. signals produce negative bias at diode D1, Fig. 2C, fed through R10 and the secondary of i.f.t.2 to V2 control grid. This moves negative with increased signal strength, the current through R7 and R6 falls, so that the screen of V2 becomes more positive, and the cathode more negative. With no signal, potentiometer VR2 allows the circuit to be balanced so that no voltage is present across the S-Meter. Incoming signals cause the meter reading to rise in proportion to the signal strength. R5 reduces the meter sensitivity to a suitable level.

If a steady signal is present, from a transmission or a signal generator, all i.f.t. or other adjustments can be directed towards obtaining the best meter reading. This also applies to any external adjustments, such as to an aerial tuner or to the aerial-earth system.

CRYSTAL FILTER

With the i.f.t.'s aligned at 455kHz, crystal X6 was 454kHz and X7 was 456kHz but it is not necessary that X6 and X7 have exactly 2kHz separation. The specified i.f.t.'s are 465kHz types but they tune easily to 455kHz.

If one crystal only is used, and the other replaced by a 15pF variable phasing capacitor, a sharply resonant peak can be obtained together with a rejection notch which can be moved across the i.f. passband. A filter of this type was described in the December 1971 issue of *Practical Wireless* and is excellent for c.w. in particular.

The lead from the mixer pin 6, Fig. 2B, to pin 3 of i.f.t.l is screened right up to the i.f.t., otherwise stray coupling round the filter will degrade results.

If an accurately calibrated signal generator is available, set it midway between the crystal frequencies and inject at pin 1 of V2, Fig. 2C, adjusting the

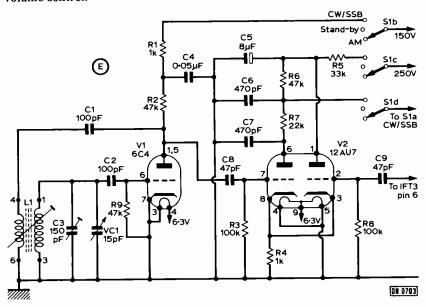


Fig. 2E: Circuit of the b.f.o./ product detector, the addition of this unit to the receiver permitting the reception of c.w. and s.s.b. signals. The frequency of the b.f.o. is variable from the front panel to accommodate upper or lower sideband signals.

1ST. RF, MIXER/OSCILLATOR (FIG. 2A)

Resistors

R1 47kΩ 1W R3 33kΩ 1W R5 100kΩ ½W R6 270Ω ½W R2 68Ω ‡W R4 39kΩ 1W

Capacitors

C1 0.01µF Disc 350VW C7 0.01µF Disc 350VW C2 0.01 µF Disc 350VW C8 100pF SM C3 470pF Mica C9 22pF SM C4 0·01μF Disc 350VW C10 10pF SM 22pF SM C5 0.01µF Disc 350VW C11 5pF SM C6 0.01 µF Disc 350VW TC1 30pF trimmer VC1-2 2 x 180pF (Jackson L2)

25pF midget variable (Jackson C804)

VC3 **Valves**

V1 6BA6

V2 ECH81

Miscellaneous

Valveholders B7G (1) skirted, B9A (1) skirted. Formers (7) see text. Crystals X1-5 Type HC6U (see text) with holders. Bandswitch sections A-H, comprising 4 wafers each 2 pole 6 way. Universal chassis flanged members, 6 x 2in. (1), 5 x 2in. (2) (Home Radio).

TUNABLE IF AMPLIFIER (FIG. 2B)

R1 1MΩ ‡W R4 1MΩ ‡W R7 2·2kΩ 1W R2 47kΩ ½W R5 47kΩ 1W R3 68Ω ±W R6 47kΩ ‡W

Capacitors

C1 22pF SM 100pF SM C8 C2 100pF SM C9 0.05µF 350VW C3 0·05μF 350VW C4 0·01μF 350VW C10 47pF SM C11 22pF SM C5 0.1 µF 350VW C12 - 1000pF SM C6 0·1μF 350VW C7 22pF SM C13 0.01µF 350VW TC1-2-3 30pF trimmer VC1-2-3 3 x 25pF (Jackson 003)

Valves

V1 6BA6

V2 ECH81

Inductors

L1 Blue Range 3 L2 Yellow Range 3 L3 Red Range 3 (All Denco, miniature, valve type)

Miscellaneous

Universal chassis flanged members, 5 x 2in. (2), 4 x 2in. (2), flat plate 5 x 4in. (1) (Home Radio). Cabinet 15 x 9 x 8in. Type W, chassis 13 x 8 x 2½in. Type K, brackets 4 x 4in. Type C (2) (H. L. Smith). Dial and drive, Type DL6 and ball drive Type 4511 (Home Radio). If not available use combined Jackson dial and drive Type 4103/A.

FIXED IF AMPLIFIER (FIG. 2C)

Resistors

R1 100kΩ ‡W R5 330Ω ‡W R9 1MΩ JW R2 47kΩ 1W R6 22kΩ 1W R10 1MΩ ½W R3 68Ω ½W R7 100Ω ‡W VR1 2kΩ linear WW R4 47kΩ 1W R8 100kΩ ½W VR2 500Ω WW pre-

Capacitors

C1 0.25µF 350VW C6 0.05μF C2 0.1µF 350 VW C7 100pF mica C3 0.05µF 350VW C8 100pF mica C4 0.1 µF 350VW C9 0.01µF 350VW C5 0.1µF 350VW

Valves

V1 6BA6

V2 6BA6

Inductors

IFT1 IFT/11/465CT ·IFT3 IFT/11/465 (All Denco) IFT2 IFT/11/465

Miscellaneous

Crystals X6/7 Type HC6U with holders (see text). Valveholders B7G (2) skirted. Diode D1, OA81. Switch S1a-d, 4 pole 3 way wafer switch. S meter, 1mA f.s.d.

AUDIO AMPLIFIER/POWER SUPPLY (FIG. 2D)

Resistors

 $\begin{array}{cccc} \mathsf{R1} & 4 \cdot 7 \mathsf{k} \Omega & 3 \mathsf{W} \\ \mathsf{R2} & 270 \mathsf{k} \Omega & \frac{1}{2} \mathsf{W} \end{array}$ R4 $470k\Omega \pm W$ R7 $1k\Omega \pm 3W$ R5 $47kΩ \frac{1}{2}W$ R8 470Ω 5W R6 $180Ω \frac{1}{2}W$ R9 $25Ω \frac{1}{2}W$ R3 4.7kΩ ½W R10 25Ω ₃W VR1 500kΩ log. pot. with switch, S1

Capacitors

C1 60µF 6VW C5 0.01µF 350VW C2 0·01μF 350VW C6 32µF 450VW C3 32µF 350VW C7 8µF 450VW C4 100µF 15VW

Valves

V1 ECL86

V2 OA2 (150V)

Miscellaneous

Valveholders B7G (1), B9A (1). D1-2 silicon rectiflers 800 p.i.v. 1A. Closed circuit jack. Fuse 250mA and holder. T1, output transformer Type TO46 (Home Radio). T2, mains transformer Parmeko P2931 or similar (Home Radio) see text.

BFO/PRODUCT DETECTOR (FIG. 2E)

Resistors

R1 1kΩ ‡W R4 1kΩ ½W R7 22kΩ ½W R2 47kΩ ½W R5 33kΩ ½W R8 100kΩ ½W R3 100kΩ ‡W R6 47kΩ 1W R9 47kΩ ‡W

Capacitors

C1 100pF SM C6 470pF mica C2 100pF SM C7 470pF mica C3 150pF SM C8 47pF SM C4 0.05µF 350VW C9 47pF SM C5 8µF 350VW VC1 15pF variable

Valves

V1 6C4

V2 12AU7

Miscellaneous

L1, b.f.o. coil (Denco BFO2/465). Valveholders B7G (1), B9A (1).

cores of i.f.t.3 for best output. Repeat with i.f.t.2, with the signal applied at pin 1 of V1 The signal can then be taken to the second mixer grid and i.f.t.1

Assuming no generator is available, tune in any strong, stable signal. It will probably be found that

there are two responses, one is relatively broad and arises from the i.f.t.'s while the other is sharper and may be much weaker if the i.f.t.'s are not tuned near to the crystal frequencies. Tune the signal in at the sharper response position which places it in the continued on page 738

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a 2 dB capture ratio; the phono pre-amplifier uses integrated circuitry and, of course, the world famous Heath 'Black Magic' panel lighting gives a suitably sophisticated finishing touch.

Kit K/AR-1Ž14 AM/FM Stereo Tuner Amplifier £69.80. Carr.: 80p.

The AJ-1214 Tuner (separate) specifications follow that of the AR-1214. The most dramatic are: FM sensitivity, less than $2\mu V$. FM selectivity, 60 dB. Stereo separation, 35 dB minimum. AM sensitivity, less than $100~\mu V$ per metre. AM selectivity, greater than 40 dB.

Like the AR-1214 it features a single-knob flywheel for AM/FM, FM-stereo tuning, push-button mode control and an adjustable ferrite rod antenna for AM reception.

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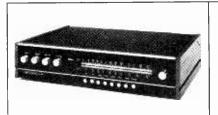
The AA-1214 Stereo Amplifier gives 25 watts per channel. All the

circuitry is on 2-printed circuit boards. A single wiring harness takes care of point-to-point connections. The 15 watts RMS power per channel into 8 ohms is more than enough power to drive most speaker systems. You'll find input jacks for phono, tape and tuner inputs along with a tape monitor socket. Should you also be thinking of 4-channel adaptation, the AA-1214 stereo amplifier is worthy of serious consideration.

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CIRCUIT DIAGRAMS. R1155, B.F.L.N. with values, 50p. R1392, R1475, **30p** ea. CT38 **50p**, Scopes CD518 (CT316), 13a, 1035 Mk. 1 2 & 3, 1049 Mk3 all **50p** ea. Sig Gens TF144G 50p, TF801a 75p. R4187 Rx circ parts list & block diagram £1.

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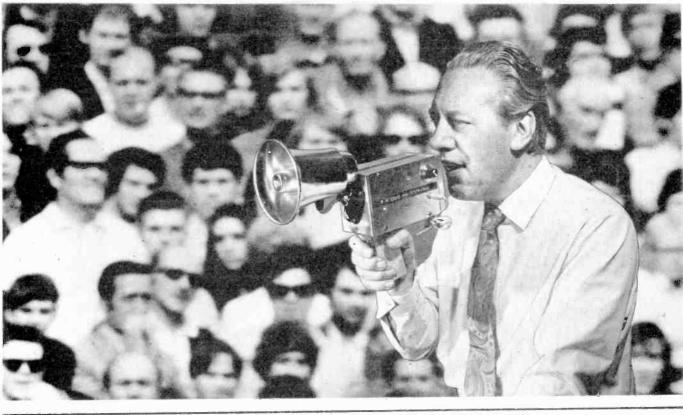
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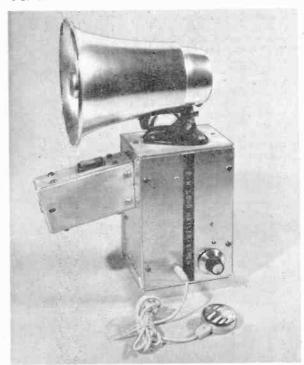
A. LESTER-RANDS

LOUDHAILER is simply a battery powered, portable public address amplifier complete with its own loudspeaker and has a wide variety of uses in or out of doors e.g., making oneself heard to a crowd of people or to a single person at a distance. The addition of a siren (electrically generated) also enables the hailer to be used as a warning device, for example by yachtsmen in foggy weather or simply to attract the attention of people before making an announcement.

The loudhailer with siren described in this article has an output power of 3 to 4 watts on speech and is battery operated by eight 1.5V cells (U11 or equivalent) providing a total of 12V. The siren sound can be produced at about the same power output and is pitched at around 250Hz to achieve maximum carrying range. The loudhailer can be hand held by its pistol grip type handle or can be self standing for use with a detachable microphone (see right). The main hailer on-off button is a rocker type switch mounted on the front of the pistol grip handle. This permits easy intermittent operation when the hailer is hand held but can be used in a continuous 'on' position when the hailer is used self-standing.

The circuit

This is shown in Fig. 1 and consists of a microphone preamplifier Trl, which drives the PC5+ power amplifier via S1 and the volume control VR1. The siren generator Tr2/Tr3 is simply a multivibrator



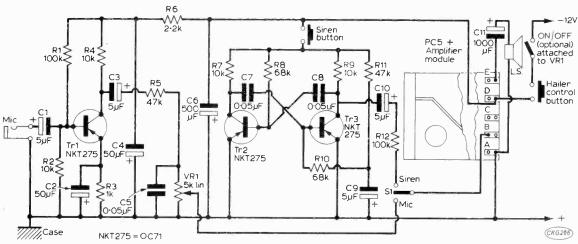
The loudhaider need not be hand held and can be rested as shown with the speaker adjusted to face forwards.

with a charge up circuit (C9/R11) that supplies a slowly increasing potential to the base of Tr3. This introduces a slight rise of pitch as the siren is switched on, resulting in a somewhat distinctive sound. The output of the siren is taken to the PC5+ power amplifier via S1.

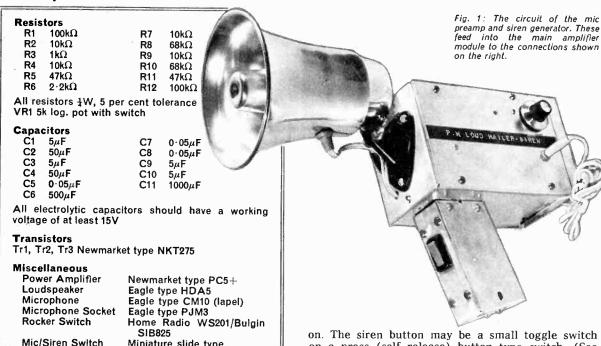
The power amplifier provides some 3 to 4 watts of power output to an 8Ω speaker and is a printed circuit assembly made by Newmarket Transistors. It was chosen because of its small dimensions which, in turn, permitted the use of a case for the hailer of only 6 x 4 x 3ins but yet still large enough to accommodate the microphone preamplifier, the siren generator, the battery cells and the power amplifier itself.

Note that the 12V supply has both an on-off switch and the rocker switch (hailer control button) in series to the negative supply rail to the amplifier. The on-off switch is optional but could be used merely as a safety precaution against the rocker switch being left

Mic. pre-amp



* components list



on. The siren button may be a small toggle switch on a press (self release) button type switch. (See components list regarding suitable rocker switch and self release button switch).

Construction

The 6 x 4 x 3inch case was constructed from Home Radio Universal Chassis parts (see components list). The loudspeaker is an Eagle type PA speaker

Siren Switch

Case

Sundries

Miniature slide type

Home Radio Universal Chas-

sis Parts: CU157(2); CU144

Plain circuit board; Aluminium angle; 16 or 18 s.w.g. aluminium for pistol grip;

Small toggle type

(2); CU146 (2)

Stand-off pillars.

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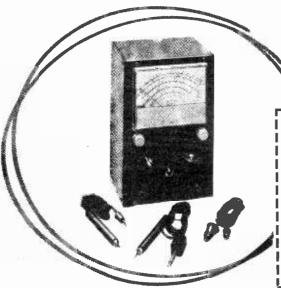
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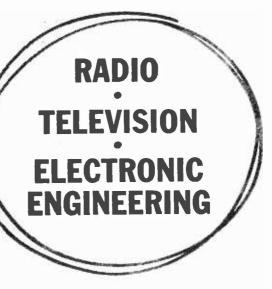
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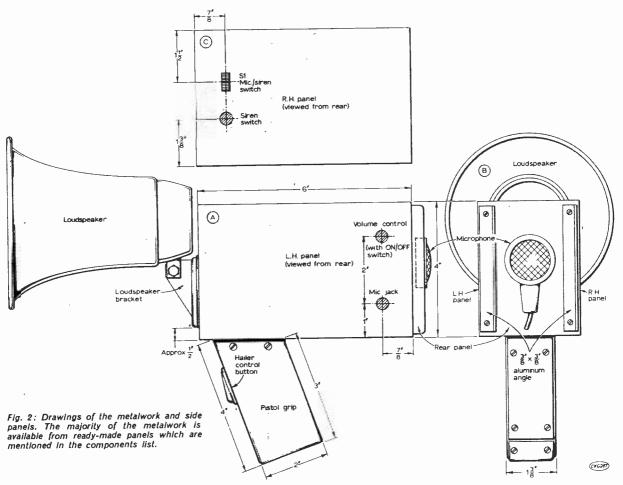
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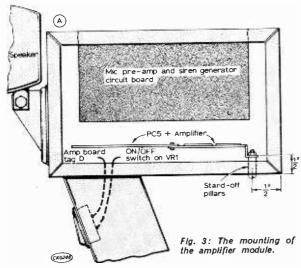
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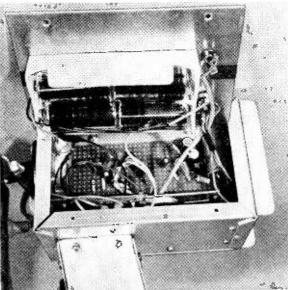
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type HDA5 which is supplied complete with fixing bracket and is mounted on the front end of the case as in Fig. 2a. The rear end of the case is fitted with two aluminium angle pieces as in Fig. 2b which allow the unit to stand evenly when used self-standing. The pistol grip is hollow, being made from aluminium to the dimensions given in Fig. 2a and b and which, in turn, is secured centrally to the underside of the case. The hailer control rocker switch is mounted on the front of the pistol grip as in Fig. 2a.



One of the side panels unscrewed. The components board can be seen clearly while at the extreme bottom is the main amplifler module. One of the battery holders can also be seen; there is another on the other side panel.

The mic/siren switch S1 and the siren control button (or switch) is mounted on the right hand panel of the case (looking from the rear end) whilst the volume control (with integral on-off switch) and

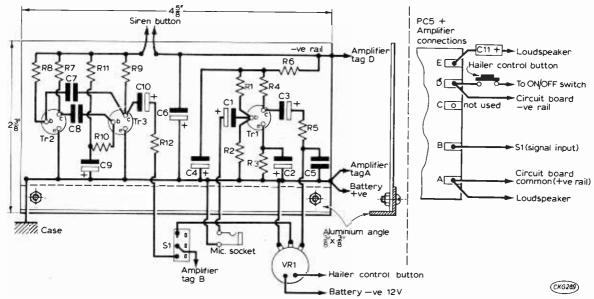
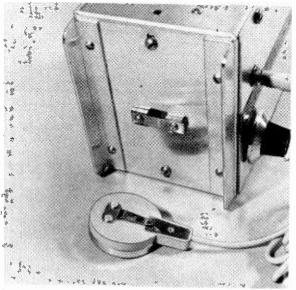


Fig. 4: The component layout and wiring. The connections to the module are shown on the right.



For operation as a loudhailer, the microphone is fitted to the small clip shown.

microphone socket, are mounted on the left hand panel (looking from rear end). The positions of these components are shown in Figs. 2a and 2c. The microphone used for the prototype was an Eagle lapel type CM10 which is fitted with a screened lead and miniature jack plug and also has a small clip on the back. It can therefore, be clipped onto the rear of the hailer as shown in Fig. 2b. The support for the microphone clip is simply a small brass strip about ¹4in. wide bolted onto the rear panel but raised about ¹8in. by spacers. Any small crystal microphone can be used with the loudhailer.

The loudspeaker leads are taken into the case and thence to the amplifier through a hole in the front panel. Before attaching the pistol grip, fit a pair of wires to the rocker switch long enough to go through into the case and thence to a) the on-off switch and b) to tag D on the PC5+ power amplifier.

The position of the microphone preamplifier and siren generator circuit board is shown in Fig. 3. It is mounted slightly off centre within the case to be clear of the battery boxes when they are in situ. The PC5+ amplifier is mounted as shown in Fig. 3 centrally and at the bottom of the case but is raised up on stand-off pillars by about 1_2 in.

The battery boxes (Eagle type BH411) are mounted one on each side panel (see photograph) and in the positions shown so as to be clear of both the circuit board and power amplifier when the panels are fitted. Changing batteries means only removing each side panel.

Layout and wiring of the circuit board containing the microphone preamplifier and the siren generator is shown in Fig. 4. The plain $0\cdot 15$ in. matrix circuit board is mounted on a piece of aluminium angle which, in turn, is secured to the upper panel of the case. Connections to the mic/siren switch S1, the mic socket, the volume control (VR1) and to the power amplifier etc., are all shown in Fig. 4.

Checking out

Current consumption should be about 10 to 12mA with no signals and can be checked with a meter in series with the 12V negative lead from the battery. With the hailer switched to 'mic', adjust the volume control so that no feedback occurs i.e., no howling due to sound from the speaker coming back to the microphone. The supply current should rise to about 100mÅ or a little over on speech peaks. With the switch S1 to 'siren', operate the siren button (or switch). The sound should rise slightly in pitch once it starts but if left on will stay at constant pitch. Intermittent use of the siren button should produce a sound with a slight 'whoop' pitched at about 250Hz (around middle C). The current consumption of the hailer will rise to around 100mA when the siren is operated.

These tests should be made with the side panels open to ensure that operation is satisfactory. Make sure that when the side panels are fitted (with the battery boxes now inside) that no short circuits occur which is quite possible as there is little space between the circuit board and battery containers etc.

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THERE has been no shortage, in recent years, of designs for transistorised transmitters. In the majority of cases, however, the transmitters have been running at inputs of maybe a fraction of a watt. In some cases, modulation appears to have been something of an afterthought. Often, emitter or base modulation has been used in a desperate attempt to obtain the magical 100% modulation—the reason being, one suspects, that the more familiar high-level modulation has not been found to give the desired results.

The purpose of this article is to try to clear away some of the misconceptions surrounding the transistor power amplifier stage, and to outline the way in which amplitude modulation may most effectively be achieved.

THE BASIC CIRCUIT

Fig. 1 shows the basic circuit arrangement for valve and transistor p.a. stages. Superficially, the circuits look very similar, but there are some important differences. First, one must remember that, unlike valves, transistors are current-operated devices. This means that there is no point at all in feeding a huge signal into the base of a p.a. transistor in an attempt to run it at high power. All that one is likely to achieve is the destruction of the transistor as the result of excessive reverse base-emitter potential.

What the base really requires is current, and this can only be achieved if the driver stage can supply adequate power at the correct impedance to match into the p.a. This brings us to the second important difference between valve and transistor p.a.'s. Being current devices, the latter operate at much lower input and output impedances, typically under 20ohms. One must therefore pay careful attention to the problem of matching the transistor accurately to the load it is to feed.

CLASS C OPERATION

In any Class C p.a. stage, we are basically trying to switch the stage into conduction for only a brief portion (typically 140°) of the signal cycle. The resulting burst of current causes the p.a. tank circuit to ring at a frequency determined by the LC of the tuned circuit, the oscillations being fed to the aerial via either a link coupling or some form of pinetwork.

In a valve p.a. it is necessary to provide a negative bias on the grid in order to restrict conduction to the desired 140°, but the situation with transistors is (for once!) much simpler as a transistor will not conduct at all in the absence of an input signal. This immediately provides Class B operation, but there

is a further bonus in that owing to the existence of the base-emitter diode the input signal has to exceed a certain minimum value (approximately 0.6V for silicon transistors) before conduction begins at all. This is ideal, as it means that Class C operation can be achieved with transistors with no special bias arrangements whatsoever. All we need to do is feed a signal with a positive excursion something in excess of 0.6V between base and emitter of the p.a., from a driver stage capable of supplying adequate base current to give the desired mean collector current.

As a guide, a well-designed p.a. stage will provide a power gain of up to 17dB (approximately 15 times). Thus, a 10watt transmitter running at 70% efficiency will require a drive power of at least half a watt.

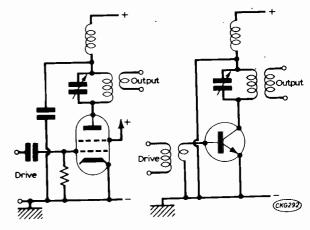


Fig. 1: Circuits Illustrating the similarity in valve and transistor p.a. stages.

MATCHING

With valve transmitters, it has become almost standard practice to use a pi-network to match the p.a. to a 750hm aerial system. The same principles apply to transistor p.a.'s but owing to the lower impedances involved component values can become somewhat inconvenient at the lower frequencies. For this reason, a tapped p.a. tank coil is often used, as a worked example will illustrate.

Assuming a p.a. efficiency of 70%, the approximate p.a. output impedance can be calculated from:

$$R_{pa} = \frac{V_c}{2I_c} \text{ ohms}$$

where V_{o} is the collector voltage and I_{o} is the collector current.

Thus, a p.a. with a collector voltage of 20V and a d.c. input of 0.5A will present an output impedance of

$$\frac{20}{2 \times 0.5} = 20 \text{ohms}$$

The problem is now one of matching the 20ohm p.a. to the 75ohm aerial system. As mentioned earlier, the most suitable technique consists of initially converting the low p.a. impedance to a more convenient value by means of a tapped p.a. coil, and then transforming down to aerial impedance by means of a link coupling. In this way, a reasonable working Q can be obtained with components of a more sensible value than would have been necessary for a pinetwork.

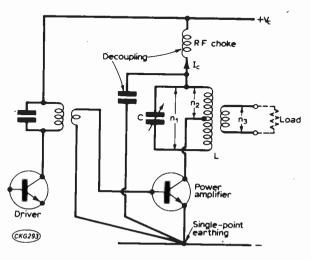


Fig. 2: Typical transistor p.a. stage and the matching problems involved.

The general arrangement is shown in Fig. 2. To establish a starting point in our calculations, we begin by assuming a convenient value for the tuning capacitor C. The value of L is then given in the normal way by:

$$L(\mu H) = \frac{25,000}{f^2 \times C}$$

where f is frequency (MHz) and C is tuning capacitance (pF).

We next decide on the required operating Q. As with valve p.a.'s, this is usually somewhere between 5 and 15 as a compromise between harmonic suppression and tuned circuit loss. Now, Q is given by:

$$Q = \frac{\pi \times f \times C \times R}{500,000}$$

where R is the effective shunt resistance across the tuned circuit. From this, we can obtain an expression for R:

$$R = \frac{500,000 \times Q}{\pi \times f \times C} \text{ohms}$$

Thus, in order to obtain the required operating conditions, the p.a. output resistance must be transformed to look like this shunt resistance R.

Example: Suppose our p.a. is to work at 2MHz and we choose C=500pF as a convenient value for the tuning capacitance. Hence,

$$L(\mu H) = \frac{25,000}{22 \times 500} = 12.5 \mu H$$

If we now choose an operating Q of 10, the effective shunt resistance R will need to be:

$$\frac{500,000 \times Q}{\pi \times f \times C} = \frac{500,000 \times 10}{\pi \times 2 \times 500} = 1,590$$
ohms

It is now necessary to determine the turns ratio for the tapped p.a. coil. This is given by:

$$\frac{n_1}{n_2} = \sqrt{\frac{R}{R_{pa}}}$$

Thus if in our example 30 turns were required to give the required inductance of $12 \cdot 5\mu H$, n_2 could be obtained from:

$$\frac{30}{n^2} = \sqrt{\frac{1590}{20}}$$

from which $n_2 = Approx. 3^{1}$ 2 turns.

The number of turns required for the aerial link coupling can now be calculated in a similar manner from:

$$\frac{n_1}{n_3} = \sqrt{\frac{R}{R_{ae}}}$$

For a 75ohm aerial system, the above example would therefore require a value for n_3 given by:

$$\frac{30}{n_3} = \sqrt{\frac{1590}{75}}$$

from which n₃ = Approx, 6¹₂ turns.

It is vital that the p.a. stage be adequately decoupled. This can be accomplished by means of an r.f. choke and decoupling capacitor as shown. The impedance of the choke should be no more than ten to fifteen times the p.a. output impedance, to discourage low frequency parasitics.

MODULATION

Undoubtedly the best way to modulate a transistor transmitter is by collector modulation of the p.a. and driver stages. The audio power required will be equal to half the p.a. input power; that is, 5watts for a 10watt p.a.

'Efficiency' modulation systems modulating emitter or base of the p.a. with only a few milliwatts of audio can give satisfactory results if carefully set up, but even at their best will never have the 'talk-power' of a high-level modulated system. This is a matter of fundamental fact, not of design.

MODULATOR MATCHING

In order to effectively modulate any p.a., it is essential that it be correctly matched to the modulator. The calculations are very simple. A transistor p.a. with a collector voltage of V_{o} volts and a collector current of I_{o} amperes will present a

load to the modulator of $\frac{V_c}{I_c}$ ohms. If we call this

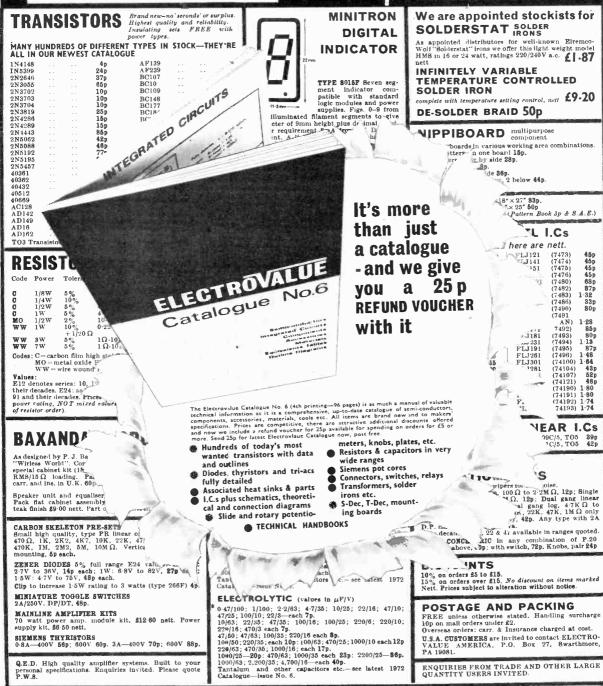
load impedance R_p it can be correctly matched to a modulator of output impedance R_m by means of a modulation transformer with a turns ratio:

$$\frac{N_1}{N_2} = \sqrt{\frac{R_p}{R_m}}$$

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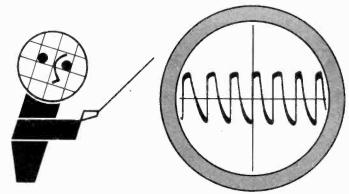
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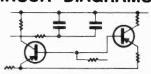
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Example:—Suppose we wish to modulate a p.a. having a collector voltage of 20volts and a collector current of 0.5 amperes by means of a modulator with an output impedance of 1000ohms. From the formula, the modulator load R_p will be

$$\frac{20}{0.5} = 40 \text{ ohms}$$

To match this to a modulator output impedance of 1000ohms, we shall require a modulation transformer with a turns ratio:

$$\frac{N_1}{N_2} = \sqrt{\frac{40}{1000}} = \frac{1}{5}$$

i.e. a step-up ratio of 1:5 between the p.a. and the modulator. The general arrangement is shown in Fig. 3.

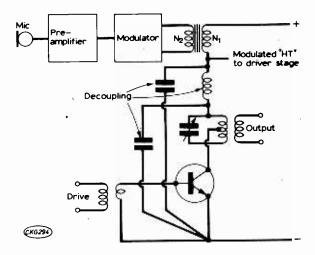


Fig. 3: Circuit showing how the use of formulae given in the text can ensure correct matching between the p.a. and the modulator.

It is not possible, because of internal feedback, to fully modulate a transistor transmitter by means of collector modulation of the p.a. alone. For this reason, it has become established practice for the driver stage also to be collector modulated to a depth best determined by practical tests.

CHOICE OF TRANSISTORS

This article would not be complete without a brief survey of suitable p.a. transistors' available for amateur use at'a reasonable cost.

When selecting a type of transistor to meet a particular requirement, there are a number of important parameters to bear in mind.

The first of these is transition frequency f_T . This is the frequency at which the forward current gain in common emitter mode h_{FE} (also known as β) has dropped to unity. But more important, it is also the gain-bandwidth product for the transistor: a transistor with an f_T of 200MHz will have a gain of 100 at 2MHz and 50 at 4MHz.

From this one might conclude that one should aim for as high an f_T as possible, but in practice this can result in excessive low-frequency gain and consequent instability. It is therefore best to select a transistor with an f_T no more than ten to fifteen times higher than the proposed operating frequency.

Another important transistor parameter is its total dissipation $P_{\rm tot}$. A Class C p.a. stage is generally no more than 70 per cent efficient, the remaining 30 per cent of input power is wasted as heat which must be adequately dissipated by the transistor and its heat sink if the device is to remain within the temperature limits stipulated by the manufacturer.

Finally, it tends to be expensive to pay too little attention to the manufacturer's 'absolute maximum' voltage and current ratings (the writer speaks from rueful experience!). A p.a. fed from a 12volt supply will have a peak r.f. voltage on its collector of up to 24volts on c.w. and up to 48volts on a.m. A valve p.a. will withstand a fair degree of overload without complaining, but the risk is not worth taking with transistors. It is therefore good sense to choose a transistor with a collector-emitter voltage rating at least three times the proposed supply voltage for c.w. and at least six times the proposed supply voltage for a.m.

A list of readily available transistors suitable for amateur p.a. use is given in the accompanying table.

P _{tot} (W)		f _T (MHz)	V _{CBM} (V)	V _{CEM} (V)	I _{CM} (A)
3	2N1893	50	120	· 80	0.5
	2N1613	60	75	30	0.5
	2N1711	70	75	30	0.5
4	2N4030	100	60	-60	1.0
	2N4031	100	80	80	1.0
	2N4032	150	—60	-60	1.0
	2N4033	150	-80	80	1.0
5	2N3053	100	60	40	0.7
	BSY81	100	40	18	1.0
	BSY83	100	80	35	1.0
	BSY85	110	120	64	1.0
1	BSY84	120	80	35	1.0
	BSY82	120	40	18	1.0
	BSY86	130	120	64	1.0
1	2N3866	700	55	30	0.4
11.5	BD106A	100	36	36	2.5
	BD106B	100	36	36	2.5
ĺ	BD106C	100	64	64	2.5
	BD106D	100	64	64	2.5
15	BD124	60	70	45	4.0
45	BD123	85	90	60	5∙0
	BD121	95	60	35	5.0

CONCLUSIONS

The writer concludes with a few recommendations which are the outcome of considerable experimentation and not a few traumatic experiences.

DO... bring up the voltage and drive to a transistor p.a. gradually to avoid any possible overloads.

DO ... use single point earthing.

DO... keep leads short. There are high circulating currents in a transistor p.a. and stray inductance from over-long leads can ruin performance.

DO NOT... over-drive a transistor p.a. with voltage.

DO NOT... forget to decouple the stage properly.

DO NOT... run the p.a. even slightly off-tune or
without a proper load.

TAKE 2®

JULIAN ANDERSON

A series of simple transistor projects, each using less than twenty components and costing less than one pound to build.

HERE are several occasions when audio signals have to be mixed; public address systems frequently have several sources such as a microphone, tape recorder and record player and of course pop groups need an audio mixing facility to bring all the sources together before feeding the main amplifier. Some audio mixers are very complex and sophisticated in that they will handle signals varying from the tiny output from a tape head to more than half a volt produced by a crystal pickup and, as well as providing a mixing system, they equalise the inputs. It is more common however that the signals needing to be added together are of roughly the same level and to mix these is fairly simple as can be seen from the circuit in Fig. 1.

This circuit has facilities for three inputs, two medium level and one high level. One important feature of a mixer is that the level of each of the sources can be controlled individually and so a potentiometer is needed for each. If we simply connected the sliders of the pots together there would be considerable interaction between them. For instance, if one of the pots was set at minimum the slider would be at virtually chassis potential and thus the wanted signals would also be shorted. This interaction can be reduced to negligible proportions by inserting a resistor in series with each slider before taking them all to a common point; in our circuit these are represented by R2, R3 and R4.

The adding of the signals in this way does, however, cut down the level considerably, so much so that the combined signals need amplifying to recover the level and so Trl is necessary. In fact this not only recovers the gain but amplifies the signal by about 20 times.

The high level input is that marked in Fig. 1 as A and this will handle signals of more than 1V without causing distortion. The signal available across VR1 is only one seventh that of the input using the $68k\Omega$ resistor shown but the value of R1 can be altered to suit the particular requirements. Inputs B and C do not have any initial attenuation and will handle signals up to about 150mV without trouble. For this input the output is nearly 3V which is more than sufficient and in most cases will be far too much; few amplifiers need more than 600mV. Working backwards, we shall then find that this amplifier stage will give 600mV out for inputs of 30mV. There is no minimum level at which it will work and signals of lmV could be mixed, though of course the output would then be only about 20mV.

Three inputs have been shown but the final number is up to the constructor. Only two may be required, in which case one can be left out but several more can be added simply by duplicating Input A or or one of the others.

No separate power supply is shown as the mixer will usually be powered from the main amplifier

No. 43 AUDIO MIXER

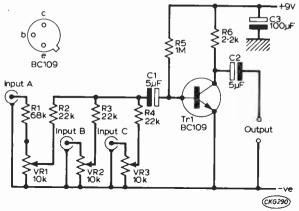


Fig. 1: Circuit of the audio mixer providing for three inputs.

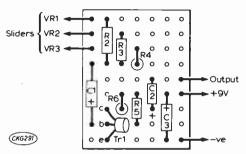


Fig. 2: A suggested component layout; no breaks in the conductor strips are necessary.

★ components list

R1	68kΩ 5%, ½W	1p
R2	22kΩ 5%, 1W	1p
R3	22kΩ 5%, ¼W	1;
R4	22kΩ 5% 1W	15
R5	1MΩ, 5%, ½W	16
R6	2·2kΩ 5%, 1W	10
VR1	10kΩ log. pot.	12
VR2	10kΩ log. pot.	120
VR3		
U.S. C. W.S.	10kΩ log. pot.	12p
C1	5μF, 12V min.	5p
C2	5μF, 12V min.	. 5p
C3	100μF, 12V min.	6p
Tr1	BC109	12p
		-
		70p
	A STATE OF THE PARTY OF THE PAR	

but it will work from a 9V battery and, since the current drain is tiny, a PP3 type may be used.

The components may be built in any convenient form but for those using Veroboard a layout diagram is shown in Fig. 2; no breaks are necessary in the conductor strips.

INNEXTMONTH'S

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Five years ago W. Cameron described his "Low Cost Hi-Fi" system in P.W.—and a rip-roaring success it was tool Now the same author describes the Mk II. The amplifler uses conventional wiring (for those who hate p.c. boards) and has an output very conservatively rated at 10W per channel. All the usual facilities are provided including inputs for magnetic and ceramic pickups, radio and tape, all with the correct equalisation, of course.



Short Wave Converter

Do you sometimes wish that you could receive short wave stations on your domestic radio instead of being confined to the medium and long wavebands? This simple three transistor unit will convert that radio into an efficient receiver for the short wave bands, capable of world-wide reception. Full information is given for the construction and alignment of the converter.

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A highly accurate, easy-to-use unit giving a linear readout. At the low end 1pF corresponds to half a scale division, yet the circuit will measure up to $10\mu F.$

Convenient to use? Just connect a capacitor, select the right scale and press the button.

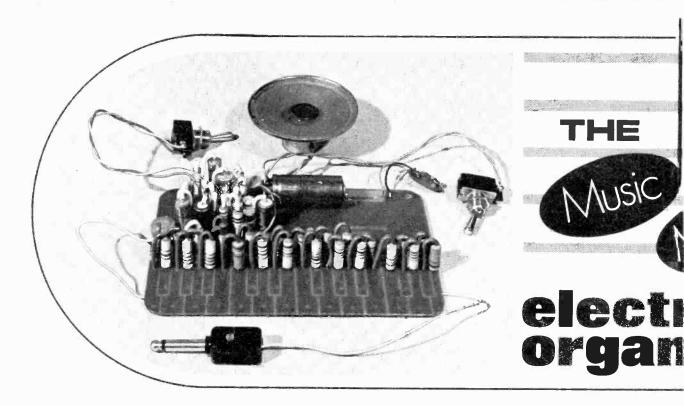
Complex? A couple of i.c.'s and a handful of other components... even using a large scale meter the cost is only about £6.

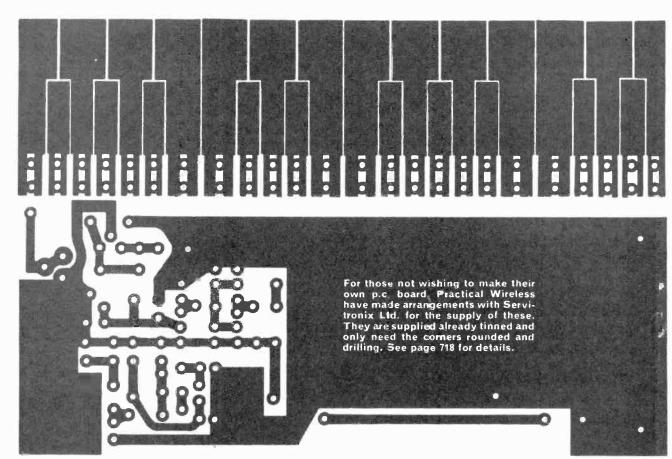




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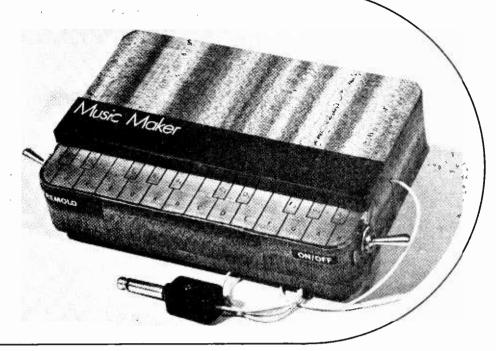




Full size pattern of the p.c. board layout. This drawing may be cut out for those wishing to make their own boards; as this page backs onto details of next month's features, your copy will not be spoift.



ronic D.SMITH



HE Music Maker electronic organ was originally conceived as a toy for the author's young daughter but, after the rigours of field trials of the kind that young children seem to be so well endowed to inflict, it was realised that the organ was more than just a toy.

It turned out to be a very robust and reliable musical instrument, very simple to construct and economic in both manufacture and battery consumption

The complete instrument is housed in a plastic sandwich box, measuring 6^{7}_{8} in. x 4^{5}_{8} in. x 1^{5}_{8} in. of the type offered for sale in most large chain stores for just a few pence. For those who are unable to obtain this, special arrangements have been made for the supply of this; see overleaf.

The organ is monophonic and played with a probe on a printed circuit keyboard laid out in conventional manner. The keyboard covers two full octaves, centred around middle C, including sharps and flats and gives sufficient notation to play almost any tune.

The notes, although not exactly the correct frequencies are close enough to pass the scrutiny of all but the trained musical ear. The accuracy of the notes was checked on a frequency meter and errors of no more than 10Hz were found in the worst case.

The organ may be built without the tremolo circuit, if even greater simplicity is desired, but it is a very worthwhile addition.

circuit description

The circuit diagram is shown in Fig. 1. The notes are generated by a relaxation oscillator Tr1 which is a unijunction transistor. The frequency of the notes is determined by C1 and R7 to R30. Tr2 is a simple audio amplifier feeding the output pair Tr3 and Tr4.

* components list

Resist	ors		
R1	100Ω	R20	1 · 5kΩ
R2	15kΩ	R21	1.5 k Ω
R3	1kΩ	R22	1 · 5kΩ
R4	1 · 5kΩ	R23	$1.3k\Omega$
R5	10kΩ	R24	1 · 2kΩ
R6	10kΩ	R25	$1.2k\Omega$
R7	3kΩ	R26	1 · 1kΩ
R8	3kΩ	R27	1-1kΩ
R9	2·7kΩ	R28	1kΩ
R10	2·7kΩ	R29	910Ω
R11	2·7kΩ	R30	$10k\Omega$
R12	2 · 7kΩ	R31	8·2kΩ
R13	2kΩ	R32	6 · 8kΩ
R14	2kΩ	R33	4 · 7kΩ
R15	2kΩ	R34	1kΩ
R16	2kΩ	R35	82k Ω
R17	2kΩ	R36	10k Ω
R18	1 ·8kΩ	R37	4 · 7kΩ
R19	1 · 8kΩ		

All resistors $\frac{1}{2}$ or $\frac{1}{8}W$, 5 per cent types. See note below on the supply of component packs. VR1 5k Ω lin. skeleton preset pot.

Canacitore

sapat	apacitois						
C1	0·05μF	C6	100μF 12V min.				
C2	0·22μF	C7	250μF 12V min.				
C3	5μF 12V min.	- C8	2·5μF 12V min.				
C4	25μF 12V min.	C9	2·5μF 12V min.				
C5	100μF 12V min.	C10	2·5μF 12V min.				
	•		•				

C8-C10 may be 2·2μF

Semiconductors

Tr1	2N2646 or UT46	Tr4	A C127
Tr2	OC71	Tr5	AC128

Tr3 AC128 Miscellaneous

Case: Plastic lunch box, see overleaf; LS1 30-80 Ω loudspeaker, miniature type, preferably 3in. but $2\frac{1}{2}$ in. or $2\frac{1}{2}$ in. will suffice. SW1, SW2; On-off toggle switches; Probe, see text; PP3 battery.

The output stage has not been designed for quality but cross-over distortion is not important. The prime consideration here is low battery consumption. The quiescent current is only a few milliamps, giving long battery life.

The circuit diagram for the tremolo oscillator is shown enclosed on the circuit diagram. It consists of a simple oscillator working on the principle that a 180° phase change occurs through the feedback capacitors C8 to C10, applying positive feedback from the collector to the base of Tr5, thus forming a low frequency oscillator.

The output of the tremolo circuit is mixed with the output of the note generator at the base of Tr2 when the switch SW2 is made.

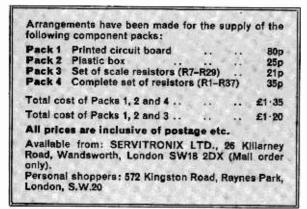
The output power is quite sufficient to allow the organ to be heard in an average sized room and no volume control was considered necessary.

circuit board construction

The printed circuit board is shown full-size on page 716. (For those not wishing to make their own boards, arrangements have been made for the supply of these.) Firstly, the board is cut to size and the corners shaped to fit the case. After checking that the board will fit the case easily, it is then etched and drilled. The components are then soldered in, starting from R1, C1 and Tr1 and progressively through each component shown on the circuit diagram as far as the loudspeaker.

Many small transistor speakers have a 6BA tapped hole in the permanent magnet keep at the back of the cone. The speaker may be fixed to the printed circuit board by a 6BA bolt, screwed into this hole. If the speaker does not have this hole, the magnet

special facilities for practical wireless readers



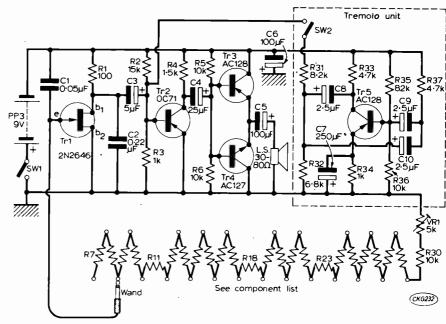


Fig. 1: The complete circuit of the Music Maker. The tremolo section, which is optional, is shown inside the dotted box. See the components list for the values of the note resistors.

can be glued to the board.

At this stage the circuit may be tested by injecting an audio frequency signal at C4 (to prove the output stage) and C3 (to prove the audio amp.). If everything is satisfactory, the audio signal will be heard clearly from the speaker.

The relaxation oscillator may be tested by temporarily connecting a $15k\Omega$ resistor from the 'e' of Tr1 to the positive rail and a note should be heard from the speaker. The keyboard components R7 to R30 and VR1 may then be fitted and the scales tried.

It should be mentioned at this stage that the values of some of the resistors R7 to R29 are not normal 10 per cent preferred values, but are 5 per cent or better types and the closer one adheres to the values stated, the closer the notes will be to the desired frequency. Since some of these values fall in the less common E24 series, special arrangements have been made to supply a kit of the scale resistors.

It was found, on the prototype, that the keyboard

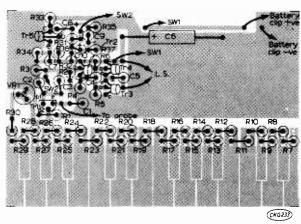
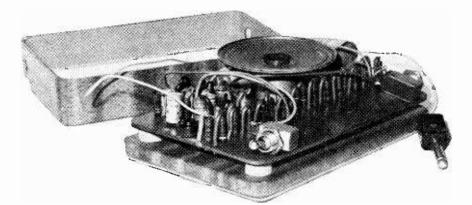


Fig. 2: The component layout on the p.c. board. This is viewed from the components side.



A view of the completed prototype.

must be polished with metal polish before playing because once the surface becomes tarnished the notes change, due to the increased resistance of the copper oxide coating. Several alternatives are possible, either the keyboard may be silver plated or, if the constructor is a soldering expert, the keyboard may be tinned. The ready-made p.c. board which is available is already tinned.

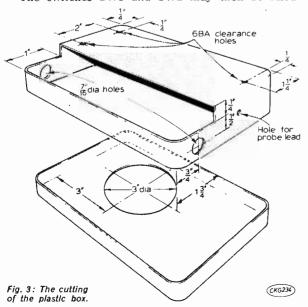
case construction

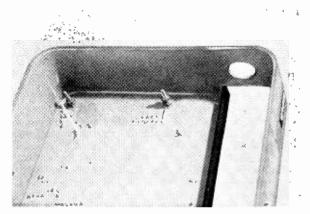
Next the case is cut as shown in Fig. 3. The best method of cutting the case is with the tip of a hot soldering iron, keeping well within the actual line of cut to allow for the shrinking effect as the plastic melts. After cutting, the edges should be cleaned up with a sharp penknife and finally sandpapered to a clean edge.

It is recommended that the speaker hole be cut first so that the constructor may get some practice before attempting the more difficult keyboard slot.

The printed circuit board fixing bolts are put through the case next, and held by means of nuts inside. The speaker hole can be covered with cloth fret and the case may be covered with Vinyl or similar decorative covering. The printed circuit board is then placed inside and fitted on the mounting screws.

The switches SW1 and SW2 may then be fixed





Inside of the case showing the hole for one of the switches and the mounting screws for the p.c. board.



The case used for the prototype—the black escutcheon can be made from cardboard covered with black, self-adhesive plastic.

and the probe lead passed through the hole in the case and the probe connected. The author used a telephone jack plug for the probe, but it may be made from a variety of items.

Finally the battery is fitted and the probe is held on middle C. VR1 should then be adjusted until the note corresponds to the correct sound; the rest of the notes should then be correct. If R7 to R29 are replaced by skeleton presets, then all the notes will have to be tuned individually, starting with the highest one because the tuning of the higher notes will upset the ones below it.

practically wireless commentary by HE

HENRY

"Psychological Pservice"

AVE you ever suffered from mice in your bottom drawer, moths in the cambric and half the local pigeon population perching on your aerial?

You have my sympathy. You can even have my telephone number if you require a quick consultancy service in getting rid of birdies on the f.m. band, rumbles on your autochanger or the depredations of the dreaded alum-worm in your electrolytics.

Some things never age. And Henry is convinced by recent experiences that the problems and vicissitudes of servicing will never change, whatever the 'tomorrow men' may predict about modules, and multi-chips, or 'potent ethos determinants'. I do not need to invent these terms. The foregoing is a quote from Jonothan Benthall's review of Science and Technology in Art Today, by Brian Porter.

'I remember the intense castigation I received when, as a humble field engineer, I dared to contribute to print the criticism of the first ever 'module-type' television receiver. The several printed circuit boards, according to the maker, would be supplied as immediate replacement spares, and no on-the-spot servicing would be needed.

Henry predicted that engineers would soon circumvent the system



Mice In your bottom drawer.

by their innate curiosity. They would find that certain components caused common faults and find it as easy to change these as nip back to the workshop for a new PC board. Which, in the event, is precisely as happened. In no time at all, the prevalence of common faults had caused a shortage of those printed circuit panels where the troubles most often took effect. And most of the problems we had with that particular set and its immediate successors were not with the printed circuit boards at all, but externals like volume controls.

Henry cannot share Mr. Benthall's regard of computer technology as art, but begins to see what he means when he describes the relevance of error factors. So much art is accidental: so much science is an inspired leap of one step after a determined plod up five hundred. So many of the radio receivers we have seen come off the production lines-computer controlled?-bear the marks of artistic error. Servicing them calls for some of the inspiration of the artist.

The psychology of service comes into it when you have to tackle those strange innovations under the critical gaze of the owner. A discreet tap with the hammer is not to be recommended, and a fierce tug in unstrategic places can result in two separate halves with a mass of disconnected wires. Instead, one holds it wisely to one's ear, give a twiddle to any visible knobs, shakes it gently, frowns and declares: 'Rather tricky I'm afraid. This is a bench job.'

Depending on his previous experience and the snobbery of modern tech-owning, the reception by the owner of this advice will either be a glow of self-importance or the suspicion of price-rigging. Trouble is, these contretemps are inevitable. No service engineer can keep up with



A fierce tug in strategic places . . .

all the models, nor even all the advances in general trends of technology. And as for the horror of having to order spares—this is where the psychology of service really sorts the professional from the chap round the corner who dabbles in wireless—and who will probably, eventually, do a much better job.

Here, again, the computer has taken over. The philosophy of the pro is to replace C195 with part number XV5600071008 as recommended in the service manual. He is not concerned that C195 is a 1KpF ceramic, available from umpteen makers and a dozen surplus factors under a multitude of names. Superset Ltd., say item XYZ, so that is what he orders, and the receiver sits on the shelf while the part is airlifted from Japan.

But computers are almost human. In fact, take a quote from Benthall's last few lines in the computer section of his book:

'So far, the constraints of working with the computer so dominate anything done with it that they actually appear to oppose the advances of the artist. It is as if the computer were some creature of great sexual attractiveness 'whose actual anatomy remains elusive, fraid and unexplored.' Henry felt that way when they invented tights. But that's another story . . .!

FREE COMPETITION

Organised by Practical Wireless and Heath (Gloucester) Ltd.

In this free competition you have two opportunities of winning a Heathkit 3in. portable oscilloscope kit! Our exciting competition will be repeated in the January issue of Practical Wireless, so save this month's coupon until next month's appears and post your two different attempts in the same envelope.

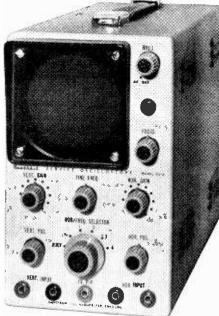
The Heathkit General Purpose Oscilloscope Kit K/OS-2 is a dependable, well-rated design, ideal for the hobby constructor. The small size and light weight make it ideal for the 'shack' while the wide range of facilities make it extremely versatile.

The low price of £29 50 for the kit plus 80p postage and packing (when ordered direct from the Gloucester factory) is an added attraction and of course, coming from Heathkit, the instructions for both assembly and operation are clear and precise, leaving nothing to chance. Even if you already own a 'scope, the OS-2 makes an excellent portable, back-up unit. Just consider the specification: Y Bandwidth from 2Hz to 3MHz; Time base 20Hz-200kHz Automatic sync; P.C. board construction; small size, 12in x 7\frac{2}{3}in x 5in; Switched ext/int Y plate connections; Sensitivity 250mV peak-to-peak per cm.

HOW TO ENTER:

Listed below are eight important features of the Heathkit OS-2 oscilloscope. All you have to do is place them in what you consider to be their order of importance to the average Practical Wireless reader. For example, if you think Portability is most important of all, write D in the box marked 1st on your entry coupon. The key letter of your second choice goes into the box marked 2nd, and so on for all eight. Complete the coupon, all in ink or ball-point pen, with your full name and address, then post in a sealed envelope to: PRACTICAL WIRELESS 'SCOPE COMPETITION, 16 GARRICK STREET, LONDON WC2E 9PR to arrive not later than Wednesday, February 14th, 1973, the closing date. REMEMBER: The competition will be repeated next month, so you can keep the first coupon until then, if you wish, and send both attempts together.

Scopes to be Won!



RULES

There is no entry fee, but each attempt must be fully completed in ink on the proper printed coupon cut from Practical Wireless, and bear the entrant's own full name and address.

Every accepted entry will be examined and the prizes, as described, will be awarded to the ten entrants who, in the opinion of an expert panel of judges, and in any one attempt, have shown the most skill and judgment in listing the eight features in order of importance.

In the event of a tie or ties for any of the prizes, a further eliminating test will be conducted by post between the tying competitors to determine such winners.

Any entry which does not comply with the printed instructions or is received after the closing date will be disqualified, as will any received mutilated or illegible, incomplete, bearing alterations, or with more than one key letter in each space. No responsibility will be accepted for entries lost or delayed in the post or otherwise.

The judges' decision, and that of the Editor of Practical Wireless in all other matters affecting the competition, is final and legally binding. No correspondence can be entered into.

The competition is open to all readers in Great Britain, Northern Ireland, and the Channel Isles except employees (and their families) of IPC Magazines, the printers of Practical Wireless, and Heath (Gloucester) Ltd., all of whom are ineligible.

The winners will be notified, and the result announced in the earliest possible issue of this magazine.

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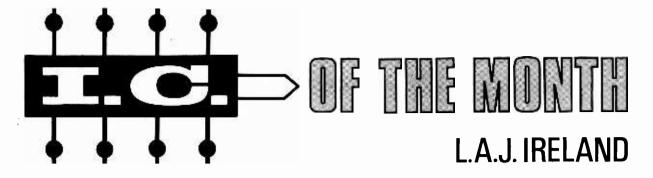
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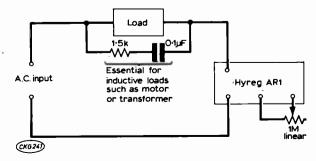
Westinghouse Hyreg AR1 Power Regulator

N general, anyone whose interest in electronics begins with radio and communications is inclined L to think primarily in those terms, maybe extended a little to cover audio and data processing. All else tends to be dismissed as electrical engineering. It is similar with integrated circuits. Application to radio, TV and computers is just about the limit. It comes as something of a surprise, then, to be dealing with an integrated circuit—even if it is a thick film hybrid—designed for power control at ratings of up to 2.5 kW., and operating off the mains. That, however, happens to be our topic for this month, the Hyreg type AR1 power regulator, manufactured by Westinghouse and available from Best Electronics (Slough) Ltd., of Michaelmas House, Salt Hill, Bath Road, Slough, Bucks.

Applications

Applications may be domestic—to regulate an electric heater or keep a kettle just on the boil; to dim the lights for an evening at home or for the local hall when films are on, or a show is presented; to set the speed of an electric drill; anywhere, in fact, where it would be an advantage to control a high powered device with the same convenience as the volume of a radio. It will by now be clear that silicon controlled rectifiers are involved, or to be more precise, a triac, consisting of two s.c.r.'s with a common gate for triggering conduction, and capable of use on a.c. circuits.

It will be remembered by those who have followed this column for a long time that the application of triacs was discussed once before, when the very useful G.E.(USA.) range of triggering circuits was



A potentiometer is all that is required for full power control.

featured. In the present case, however, the triac itself, together with the triggering components, is incorporated in the hybrid assembly. All these items are then bonded to a ceramic substrate of high thermal conductivity and electrical resistivity. The assembly is potted in epoxy, with the ceramic in good thermal contact with a metal base plate.

In use, only three external components are required, and if the load is purely resistive, such as tungsten lighting or a kettle or bar-type electric heater, this can be reduced to one, a variable resistor, as shown. The unit is mounted on a heat sink with thermal contact established with the metal base plate of the regulator. Due to the properties of the ceramic, however, this plate and the attached heat sink are fully insulated and protected.

It is suggested, however, that the variable resistor should be of the type with a plastic operating spindle, or a solid plastic knob used, for safety in the case of component failure, or accidental reversal of the connections to the mains. The fraction of the power dissipated in the load compared with that drawn directly from the mains is linearly dependent on the setting of the variable resistor. For zero resistance, the power delivered to the load is 100% dropping to zero when the resistance rises to some $800 \mathrm{k}\Omega$. It is clear, therefore, that if the application is for lighting, for example, a $1 \mathrm{M}\Omega$ linear variable resistance will control the illumination, from total darkness to full power.

One cautionary note must be sounded, however, about devices employing small a.c. motors. Most such motors, including those generally used to drive cooling fans, are of the induction or squirrel cage type. Such synchronous motors operate at a single speed or not at all. It follows therefore that it is impossible to regulate the speed of such motors with a triac device. Rather, at a particular point such a motor simply stops; and as the operating temperature of the motor, or of other components, if it is driving a fan, will then rapidly rise, damage may result. If it is intended to use this device in a system incorporatting an electric motor, first check that the motor is of the type using brushes, i.e. non-synchronous. If used with a fan heater, for example, ensure that the fan receives the full mains voltage at all times, while the regulator controls only the power dissipated in the heating element.

The AR1/250-10 (250V r.m.s. 10A r.m.s.) costs £5.87 inc. p/p with present delivery of 6 to 8 weeks.

HAVE you ever wanted to find out the value of an unmarked capacitor or wondered which was the primary and secondary of a transformer?

The value of a resistor can often be found easily by using a multimeter but how many of us possess one which can accurately measure 1Ω or, at the other extreme, $2M\Omega$? Capacitors are less easy to measure and an a.c. source is usually required and, the world being the way it is, capacitors tend to have their values erased more easily than most components. Inductors present another problem;

UNIVERSAL BRIDGE HALVOR MOORSHEAD

granted that this facility is rarely required for most of us but when you have to know, what do you do?

The Wheatstone Bridge is the answer; it will rapidly give answers to all the above. In the circuit used here, the values of the components can be read directly off the scale.

THE THEORY

Look at the circuit arrangement in Fig. 1. An audio note (at any reasonable level and frequency, it doesn't affect the operation) is applied across the network made up from VR1, Ca and Cb with headphones connected between the slider of VR1 and the common junction of the capacitors.

Assume that Ca and Cb are of the same value; they will then each have the same reactance at the audio frequency and therefore the signal level between E and F will be half that between E and D.

If the slider of VR1 is at its central position, then the resistance A-B will equal that between B-C and half the applied voltage will appear at the slider. Thus the signal level at B and F are the same: what will be heard in the phones? Nothing of course; since there is no voltage difference across them, no current can flow and so they remain silent. In this state, the Bridge, for that is what this network is called, is in balance and the null position has been achieved.

If the slider of VR1 is at any other position there will be a voltage difference and an audio note will be heard in the phones.

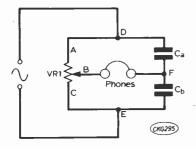


Fig. 1: The Wheatstone Bridge which forms the basis of this project.

A full explanation of the theory is given in the text.



Now if Cb is one tenth the value of Ca, its reactance will be ten times greater and we shall only get a null when the resistance B-C is ten times greater than A-B. If we make Ca a standard, we shall obviously be able to find out the value of Cb as long as we know the relationship between the two parts of the track of VR1.

We have dealt with capacitors but the same applies to resistors and inductors with only one difference. The reactance of both of these is directly proportional to their values—in other words the higher their value, the more resistance they exhibit. With capacitors the reverse is true, the higher the value, the lower the reactance and so two scales are needed for the pot, one a mirror image of the other.

THE CIRCUIT

To operate the bridge we require an audio source, a set of standards and also something to detect the null. Headphones are pretty good but they have to be quite sensitive to detect the setting of VR1 which corresponds to the maximum null and so an amplifier is used. In addition to feeding headphones, a cheap meter is also used which will give a visual rather than an audible indication.

The complete circuit is shown in Fig. 2. The audio frequency generator to drive the bridge is represented by Tr1 and the associated components. This is a phase-shift oscillator which provides a pretty good sine wave. R1 and R2 provide the base bias while C2, C3 and C4 together with R3 and R4 take part of the signal from the collector and invert it by 180°, converting it from a negative to a positive feedback and thus sustaining oscillation. As we have already mentioned, the actual frequency of operation is not important but the values given operate at about 700Hz. This frequency can be altered slightly by modifying the value of R4 but only by plus or minus 50 per cent $(4.7k\Omega)$ to $15k\Omega$). A transformer is included in the collector of Tr1; this is a transistor output transformer type LT700 which is widely available. This has a tap on the primary but this is not required for our purposes. The metal case of the transformer should be connected to the negative line. The secondary of T1 drives the bridge and it will be seen that this part of the circuit is isolated

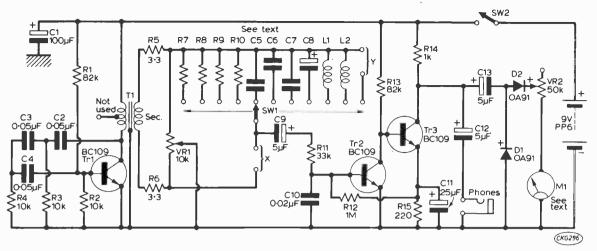


Fig. 2: Complete circuit of the Universal Bridge; the accuracy of the finished unit will depend on the tolerance of the standards and the care taken in calibration.

TEST VOLTAGES

	Emitter	Base	Collector
Tri	ov	0·5V	7-5V
Tr2	0٧	0-25V	1-2V
Tr3	17	1-2V	3-4V
Tr3	14	1-2V	3-4V

Note: Measured on Avo 8 (20,000 ohms per volt) on 10V range, battery voltage on load reading 8.5V. The above voltages should only be regarded as a guide.

from the audio oscillator. Two low value resistors are shown wired in series with the secondary; these do not really affect the circuit but prevent a complete short-circuit of the secondary if very low value resistance components need to be compared. If the secondary is short-circuited, the oscillator may cease to function.

The bridge potentiometer is represented by VR1 which has its slider taken to the negative line. This pot should be a high quality component and should of course have a linear track. A wire-wound component is to be preferred although not essential (the prototype shown uses a standard carbon track pot).

The standard components in the bridge circuit are represented by R7-R10, C5-C8 and L1, L2; these are selected by SW1. SW1 is also able to select an external pair of terminals (marked Y) for matching purposes.

The component to be measured on the bridge is connected across the terminals marked X.

The audio signal, indicating an imbalance in the bridge, will appear between chassis and the junction of the standard and unknown component and a d.c. blocking capacitor C9 takes this output to the amplifier. R11 is included to minimise the loading that the amplifier presents to the bridge. C10 bypasses any high frequencies to chassis and is necessary to prevent r.f. pickup since the amplifier has a very high gain.

The amplifier stage is made up from Tr2 and Tr3 with their associated components and is a fairly conventional arrangement. The use of BC109 transistors ensures considerable amplification of the input. The bias for Tr2 base is provided from the emitter of Tr3; this helps to stabilise the circuit and also takes up any variation in the parameters of the

* components list

1					
Resistors	•				
R1 82ks)	R9	100kΩ		
R2 10ks		R10			
R3 10ks		R11			
R4 10ks			1ΜΩ		
R5 3·30		R13			
			1kΩ		
R6 3·3Ω R7 10Ω	•	R15			
R8 1kΩ		1110	22000		
	114/ 5		-		
			ot R7-R10, see text		
	Ω lin. pot. see t Ω lin. pot. carbo		o le		
V K2 50K	12 IIII. pot. carpt	ח נדמי	CK		
Capacitors					
	F 12V min.	C8	10μF 12V—see text		
	μF ceramic	C9			
	μF ceramic	C10			
	μF ceramic	C11			
	see text	C12			
		C13			
、C7 0·01	μF see text		•		
Semicondu					
Tr1 BC10		D1			
Tr2 BC10		D2	OA91		
Tr3 BC10	09		•		
Miscellane					
T1 Transi	stor output tran	storm	er, Eagle type LT700		
	le, 12-way rotar				
SW2 On-off, miniature toggle switch					
M1 Recording level meter—see text					
Jack socket; 4 off R.S. Components (Radiospares);					
Slim Insulated Terminals, 4mm or similar; Vero- board, 0 15in. matrix, 12 x 16 holes; PP6 battery;					
Battery clip; Case: 'Elf' type, available from West					
Hyde. Developments Ltd., Ryefield Crescent,					
Northwood, Middx., HA6 1NN. Price: £1.25 plus					
10p postage. L1, CH4/A 10mH choke, L2 100μH					
choke, wire ends, available from Repanco Ltd.,					
203-265 Foleshill Road, Coventry, the price of each					
	uding postage.		, p.,,		

transistors.

The amplified audio signal appears at the collector of Tr3 and is connected via Cl2 to the headphone socket. Any type of phones can be connected to this

point—even the low 8Ω types that are now common; the effect on the meter part of the circuit is marginal. The output is also connected to the meter circuit through C13 which rectifies the a.f. and applies it to the meter. D1 provides the d.c bias necessary for correct operation of D2. Since the variation of signal strength applied to this circuit is far more than any meter could sensibly handle, a sensitivity control is fitted. This is simply a variable resistor in series with the meter M1.

When the audio signal is at minimum, the meter will be showing the minimum reading and since we are not interested in calibration, only in noting the minimum deflection, a very simple and inexpensive meter may be used here. The most suitable type is a recording level meter; these come in a variety of shapes and sizes but most have a sensitivity of about $200\mu A$ and cost between 50p and £1. Suitable types are listed in the catalogues of the large mail order component suppliers.

The current drain of the prototype was measured at about 10mA and a PP3 or PP6 type battery may be used; the low consumption should ensure a long battery life.

SW2 is a separate on-off switch and C1 decouples the positive line. The table shows the transistor voltages measured on the prototype; these may be of help if difficulty is experienced in getting the circuit to operate.

CONSTRUCTION

The circuit can, of course, be built into any type of case but the one chosen for the prototype is a very convenient size and looks very attractive. The main body of the case is made from thick plastic and the front panel from aluminium with mounting screws provided. An internal chassis is also provided but this is not required for our purposes. Bearing in mind the attractive appearance of the case the price, £1·25, is not expensive; details of the supplier are given in the components list. All the components are fitted to the front panel and the drilling and cutting of this is shown in Fig. 3. The front panel is supplied

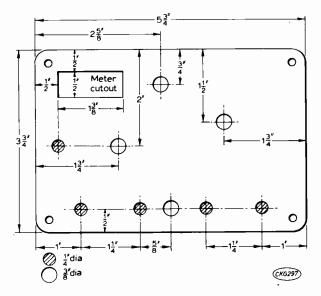


Fig. 3: The front panel, which is supplied with the case, should be drilled and cut as shown.

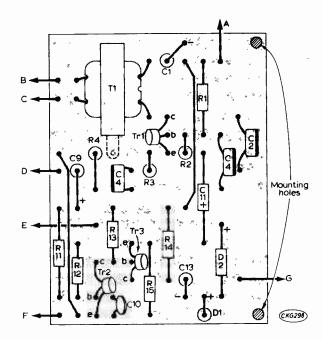
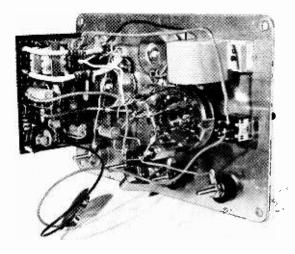


Fig. 4: The majority of the components are mounted on a small piece of Veroboard as shown. Certain of the conductor strips' should be broken.

with a protective plastic sheet and this is best left on while the marking is done to prevent scratching but it should be removed before the actual drilling starts. The meter cut out is shown for the type used in the prototype but other types may vary and so this dimension may have to be worked out separately. The holes are of two diameters, 3 _Bin and 1 ₄in. Two holes are not shown on this diagram: these are for the component board mounting bracket. These are best sited to suit the type of bracket used; they will lie to the right of the VR1 hole.

The majority of the components are fitted to a piece of Veroboard with a 0·15in. matrix. The layout for this is shown in Fig. 4. Three chassis and two positive lines are used, these are connected by link



All the components are mounted on the front panel. The wiring, especially around VR1, should be short and straight.

wires as shown. The transformer T1 is fitted with two tabs which are rather larger than the holes in the board, but by slightly enlarging these with a drill the tabs may be pushed through the board and on one side bent over and soldered to the adjacent strip. The upper tag should be soldered to the upper strip. It is important that both sides are soldered to the correct strip as the upper strip must be at chassis potential for the connection for C1. Take-off pins are connected at various points, these are marked A-G and correspond with similar letters in Fig. 5.

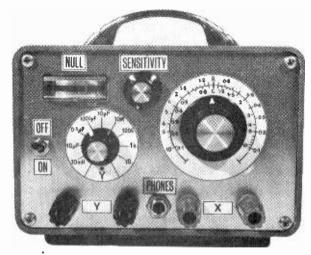
Several breaks are necessary in the copper conductor strip but these are clearly shown in the diagram.

Figure 5 shows the remaining wiring. The component board should be fitted to an aluminium angle bracket which in turn should be fitted to the front panel. A solder tag can be fitted under one of these mounting screws to act as the main chassis connection.

The standard components are wired directly to the switch SW1 and a common wire connects one side of these together; the photograph should make this clear.

To minimise the capacity of the wiring, all connections from and to SW1 and VR1 should be as short as possible and good stout wire should be used; it may look less attractive but will improve the performance of the unit.

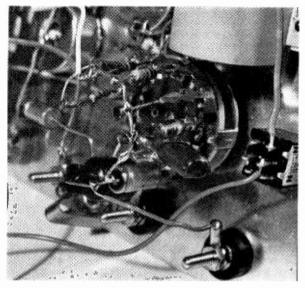
The only component not on the front panel is the battery. This fits into the main body of the case and should be held in some form of clip to prevent it moving around.



Using the recommended case, and taking care over the labelling of the controls, the finished unit can look quite professional.

CHOICE OF STANDARDS

The accuracy of the unit depends on two factors: the quality of the standards and the care taken in calibration. One per cent resistors are available although they are hard to find. Two per cent types are not all that expensive and should be quite adequate; Home Radio list these in their catalogue at 5p each. One per cent capacitors are available from a number of suppliers including Electrovalue Ltd., though C9, $10\mu F$, costs a small fortune in this tolerance. However, it is highly unlikely that high accuracy is needed on this range.



Close-up of the reference components showing how these are wired directly to the switch.

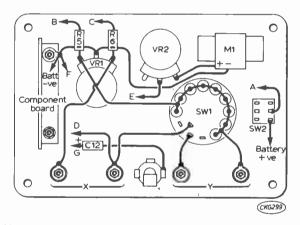


Fig. 5: Wiring of the controls. The letters match up with those on the main component board.

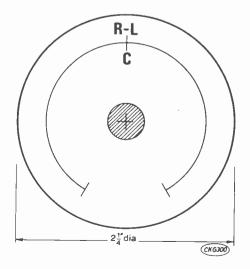


Fig. 6: This scale may be cut out and calibrated as described in the text.

The inductors chosen for the circuit are a matter of choice. The author only included two in the prototype, a 10mH and a 100μ H. Arrangements have been made with Repanco Ltd., for the supply of these 5 per cent tolerance inductors, details are given in the components list. This will allow measurement within reasonable accuracy of inductors lying within the range 1mH to 10μ H. Lower inductances can be measured but the accuracy below this must be suspect because of strays in the circuit.

The matter of standards must be left up to the reader. Many people may be content using 5 per cent components throughout and certainly little

usefulness will be lost.

CALIBRATION

A blank calibration scale is shown in Fig. 6. This can be cut out and stuck onto the front panel, the null position is already marked. For calibration a source of close tolerance components is required and the remarks made above apply. However, as we are only interested in one set of markings, this can be done using the cheapest components-resistors. The best range on which to calibrate is probably the 1kΩ one and a set of resistors with their values ranging between 100Ω and $10k\Omega$ will be needed. Points can be obtained by interpolation if only a few components are used. Alternatively, if a highly accurate test meter is available (one with an individually calibrated scale) a variable resistor can be adjusted on this and then used for the calibration. There are several ways of approaching this problem and the above points are only a guide. However, once calibrated, the scale will hold good for all values of resistance, capacitance and inductance as long as the standards are accurate.

For matching two components the internal standards are not used. The two components are fitted to X and Y and their similarity compared, if they are the same the null will appear at the 1:1 setting right at the top.

MAXWELL

by G8DSH



"I think it needs a plug change and its valves ground in!"



OMETIME back, comment was made in this column about miniature lasers. Some will have wondered about the applications of these devices while others, perhaps, even doubted the existence of such midget marvels.

It will be of interest, therefore, that small lasers are available in this country from a company in Edgware. These are colourfully described as "Hip Pocket He-Ne Lasers". Ratings of one, three and 10mW are available and the power supply allows operation from 230V a.c. or 12V d.c. Dare our imagination picture a man from Mars reaching for the "sky" on the commands of a Space Sheriff on whose hip hangs a 45MW laser? Jesse James would turn in his grave!

Before anyone ridicules the laser as just a novelty, they should consider the latest application by the Dutch electronics giant Philips. The Eindhoven laboratories use one in their latest system of video recording.

The reflection from a minute spot of light generated by a miniature laser is used to obtain a signal from a video LP. A 45 minute colour television programme can be recorded on a normal LP sized disc. This amounts to something like recording 50,000 separate frames or individual pictures.

Since there is no direct physical contact with the pick-up head, wear is almost non existent. However, one sees scratches as a problem and, more importantly, dust and/or dirt in the groove will throw up as noise in the system.

New electronic products flood the market every week. From amongst the current list is an interesting new IC. It is believed to be the first IC timer commercially available. Designated the 555 its applications include a timer which will cover intervals from fractions of a second to one hour, frequency divider, frequency modulator and missing pulse detector.

Another interesting newcomer is the range of epoxy-coated inductors. This IR-4 Series extends from $0.015\mu H$ to $240\mu H$ which is a very useful coverage. The devices are small, wire-ended and colour coded. The smaller ones in the range might be mistaken for resistors by the unwary. Selfresonant frequencies go from 5.9MHz to 525MHz. Weight is only 0.65 grammes maximum and size of the largest is 0.45in. by 0.2in. with an overall length of almost 3in. (including the length of the wire end leads). Looks as though it won't be long before nobody bothers to wind coils. Old timers in radio wil be saddened and doubtless harbour fond nostalgic memories of winding 100 turns of 24s.w.g. on a cardboard toilet roll former in order to receive 2LO.

Reverberation Unit



F.C.JUDD

PART TWO

ONNECTIONS to each of the panel mounted components are given in Fig. 11. Note that the slider control connections are numbered as follows—1 is the earth connection, 2 is the slider and 3 is the signal input. They must be wired this way to obtain the logarithmic performance of the potentiometer.

The layout and wiring of the circuit board is shown in Fig. 12. Note also that the leads coupling the spring line unit to the circuit board have to be screened and connected to the unit itself by means of phono plugs.

Construction of the power supply is shown in Fig. 13 in which details are also given regarding the size of the chassis etc. The capacitor C13 and the bridge rectifier BR1 are mounted on a small piece of circuit board elevated from the chassis on stand-off pillars.

Checking out and Performance

The overall performance of the finished reverb unit is given in the specification table given last month.

The supply rail current at the negative 18V point (see circuit) should be approximately 15mA with no

signal and with the reverb control off. The no-signal current of the reverb driver amplifier only should, if possible, be checked by connecting a meter in series with the negative supply rail at the starred point shown in Fig. 2. The pre-set PR1 should be adjusted until the standing current is about 10mA. Otherwise set PR1 to mid position.

With signals, and with the reverb control VR3 at max, the current to the driver amplifier should rise to not more than 100mA on speech peaks. A higher current indicates overload.

The Overload Meter

The overload meter will read only with reverb on and on strong signals may show full scale deflection. This is well beyond the point of overload at which distortion from the reverb amplifier circuit will be high. The meter used in the prototype is an Eagle type MR2P with a $50\mu A$ movement and calibrated 0-10. For the prototype reverb unit the figures on the meter scale were erased leaving only the scale itself. The overload point is marked (in red ink) at what was division 8 as shown in Fig. 14. In normal use the input signal should always be adjusted so that with full reverb the overload meter never quite reads to the overload mark.

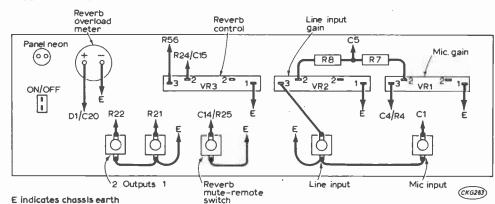


Fig. 11: The wiring of the front panel components.

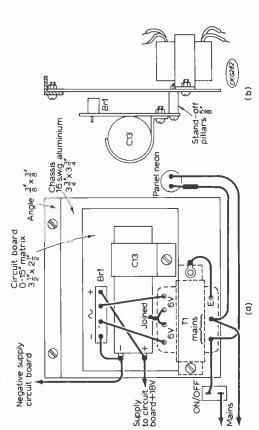
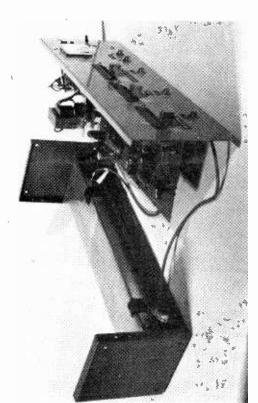
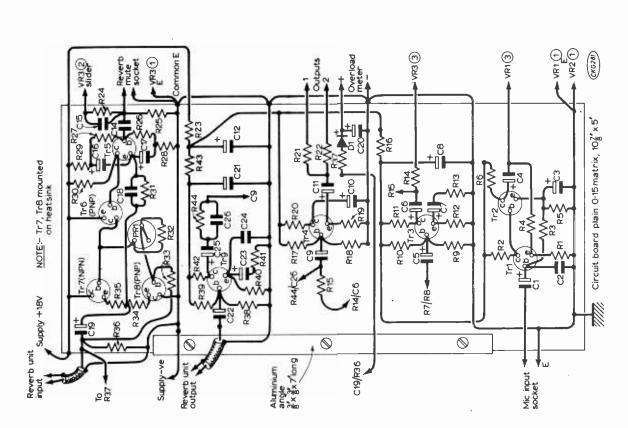


Fig. 12 (left): The wiring of the main com- Fig. 13 (above): The wiring and construction of ponent board. The siting of this can be seen the power supply on its own small sub-chassis. from the photograph below.



A view of the prototype. The main component board and power supply sub-chassis can be seen behind the front panel and fixed to it.



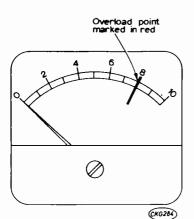


Fig. 14: The overload meter can be marked as shown. The plastic cover can easily be removed to do this.

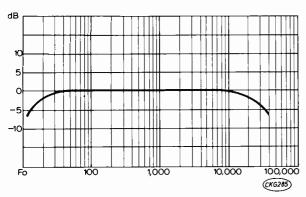


Fig. 15: The overall frequency response of the reverb unit from either input but with no reverb included.

Frequency Response

The overall frequency response for through signals (i.e., with reverb 'Off'), is shown in Fig. 15. The frequency responses of the spring line driver amplifier and its output amplifier can be checked against the responses shown in Figs. 3 and 4 respectively. For checking the response of the line driver amplifier. connect an audio signal generator at the junction of R14 and VR3 and set VR3 at maximum. Input signal should be not greater than about 20mV. Check the response at the output with an audio voltmeter between C19/R36 and chassis and with the line unit disconnected. Check the response of the spring line output amplifier Tr9 with an audio signal generator connected to C22 and with line unit output plug connected. Input signal should not be greater than about 5mV. Check the response with an audio voltmeter connected between C9/R15 and chassis.

Reverb Mute

The socket marked "Reverb Mute" (external remote switch) as in Fig. 2, is optional but can be used for remote control by means of a switch on the end of a screened lead. When the switch is closed signals feeding the reverb driver amplifier are short circuited to chassis.

CHARLES MOLLOY



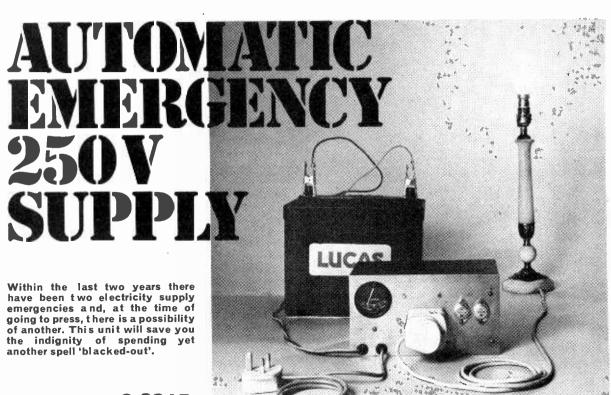
EOFFREY DRIVER who lives in Woodham, Surrey has been active on the medium waves and he reports reception of Tenerife, Canary Islands on 620kHz after 2300hrs; Radio Andorra 701kHz in both French and Spanish from 2030hrs until midnight; Radio Portugal 755kHz in English at 2300hrs with "DX Magazine" on the last Monday of the month; Algiers 890kHz in English at 0300hrs; Bissau, Portuguese Guinea with a good signal on 1070kHz after midnight.

During the winter months North American medium wave stations are often heard in the U.K. before midnight and sometimes they are audible as early as 2300hrs. This is the hour when a number of Europeans close down for the night leaving a few spaces for the DX to be heard. North Americans operate on channels spaced 10kHz apart and all of them are allocated identifying call letters which they use frequently. Listen on 710kHz at 2305hrs after Cairo 2 signs-off, for CJOX which is located in Grand Bank, Newfoundland. This is a commercially owned station and it carries the "CJON Radio Service" programme. On 1070kHz, Paris closes down at 2300hrs leaving the frequency clear for CBA, a 50kW outlet of the Canadian Broadcasting Corporation situated in Moncton, New Brunswick. CBA relays the CBC Radio Network and it identifies locally on the hour and the half hour. Propagation is variable on the North American path but when conditions are favourable CJOX and CBA should be heard by 2330hrs. Others to listen for between 2330hrs and midnight, are WHDH Boston on 850kHz; CJON St John's, Newfoundland on 930kHz; CBM Montreal on 940kHz; CHER Sydney, Nova Scotia 950kHz; WINS New York City on 1010kHz; WNEW 1130kHz also in NYC; CKEC 1320kHz in New Glasgow, Nova Scotia.

A list of North American loggings made in the UK since 1962 and covering nearly 400 different stations, is currently being distributed by the Medium Wave Circle to its members. This club, which is now in its 19th year, deals exclusively with DXing on the medium waves. Its bulletin "Medium Wave News" appears 8 times a year and contains up-to-date information about the medium waves, loggings of DX, a verification section and articles on MW DXing. Further information about the MWC is obtainable from Ken Brownless, 7 The Avenue, Clifton, York YO3 6AS.

S. N. Gaythorpe of Cranbrook, Kent asks if it is possible to hear Bermuda on the medium waves. Bermuda has 3 medium wave stations; ZFBI on 960kHz; ZBM1 on 1230kHz and ZBM2 on 1340kHz and all have been heard in the UK. There is no short wave broadcasting in Bermuda and consequently this is a "medium waves only." DX country. Try on 1230kHz after midnight for ZBM1, and log this rare DX country.

Please send logs and information about the medium waves to the author at 132 Segars Lane, Southport PR8 3JG.



S.SOAR

HE unit described here was developed during the power crisis of February 1972 and was primarily intended as a standby emergency lighting unit, although since the restoration of normal power the device has had considerable use, both as a battery charger and as a portable power supply in garage and caravan. The power output is sufficient to operate a small electric drill or an inspection lamp.

Specification As a Charger As an Inverter

	As a Ginarger	70 411 111 1111 1111		
Input	240V mains	12V battery		
Output	12V, 12A d.c. to battery	240V, 50Hz square wave, up to 150W		

Circuit Description

The unit has two modes of operation, with a 12V accumulator and 240V mains connected, the unit is a charger capable of delivering up to 12A, this charge rate falls to approximately 1.5A with the battery fully charged. An auxiliary socket on the unit provides a 240V mains output.

In the event of the mains supply being interrupted, the unit automatically switches over and power is taken from the battery and by inverter action is delivered to the auxiliary socket at 240V thus maintaining the supply. When the mains supply is restored, the unit again switches automatically to its charging condi-

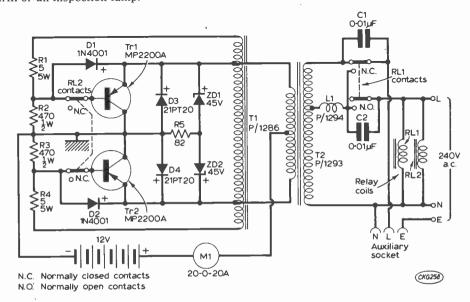


Fig. 1: The complete circuit on the combined charger/inverter. This will give up to 150W at 240V, 50Hz. See text for a description of the operation.

tion and the battery is restored to its fully charged state.

Since the inverter output is a square wave, it is not ideally suitable as a supply for equipment such as a television receiver, however, satisfactory performance has been achieved with slightly reduced picture size and tolerable interference on sound.

As a Charger

With the mains supply connected, relays RL1 and RL2 are energised, transistor bases are isolated and mains supply is connected directly to the auxiliary socket and to the output transformer secondary via choke L1. Rectifiers D3 and D4 supply full wave rectified current to charge the battery. Ballast choke L1 limits the charging current to a safe maximum of around 12A with a flat battery, this charge rate decreasing as the battery potential rises.

As an Inverter

With the mains supply interrupted, the relays deenergise, the transistor bases are connected and the output socket is connected directly to the secondary of the output transformer. The unit now operates as an inverter.

Referring to Fig. 1, assume Tr1 to be conducting, then transformer action (T1) holds Tr2 off (+ve on base) and Tr1 on (-ve on base) magnetic flux in the transformer core (T1) increases uniformly and current is substantially constant. However, as the flux density in the core approaches saturation, current increases rapidly in an attempt to maintain the rate of flux increase constant. Base drive on Tr1 is limited by R1 and the gain of the transistor falls with increased collector current, these two factors result in Tr1 coming out of its saturated state and collector current can increase no further, flux cannot increase

* components list

Resis	tors					
R1	5Ω	5W	F	24	5Ω	5W
R2	470Ω	1W	1	₹5	82Ω	1W
R3	470Ω	⅓W				
	conduc					
Tr1	MP22	00A	D3		100\ . 21P	/ p.i.v. rectifier
Tr2	MP22	00A	D4	20A		/ p.i.v. rectifier
D1 D2	1N400 1N400		ZD1 ZD2	45 V	1W	zener, e.g. 1S3045 zener, e.g. 1S3045
availa) Derby	ole froi	n Qu	ıarndo	n El	ectro	ZD1 and ZD2 are nics, Slack Lane,
Trans RL1	former					v a.c. coil
						V a.c. coil
T1	Driver	tran	sforme	er typ	e P/	1286
T2	Outpu	t trar	sform	er ty	pe P/	1293
L1	Ballas	t Cho	ke typ	e P/	1294	
68 Dal	2 and e Stree £6 65 p	et, Ma	anches	ter;	a con	n Magtor Limited, nplete kit of these
Misce	llaneo	us *				
C1, C2	2, 0-01µ	F 600				r with centre zero, suitable).

and base drive falls causing a further reduction in collector current. Falling flux causes Tr2 to become biased on and the collector current increases rapidly and Tr2 is switched hard on, this completes one cycle.

Frequency of operation is determined by the time taken for the transformer core to saturate, suitable choice of core and windings results in an operating frequency of approximately 50Hz.

The transistors are protected against reverse bias by diodes D1 and D2, and ZD1 and ZD2 clip voltage switching transients to a safe level.

Construction

Since the power transistors are connected in common collector, these devices should be fixed directly to the chassis, 16 s.w.g. aluminium was used on the prototype. Transformers, relay and choke are also bolted directly to the chassis, and if rectifiers with anode studs are used, these can also be fixed directly to chassis. Other components should be mounted on insulated tag strips. It is advisable to have all low voltage components on one side of the output transformer (i.e. primary winding side) and all mains voltage components on the other side (i.e. secondary side).

TELEVISION

DECEMBER ISSUE

EHT SYSTEMS FOR TV SETS

A lot of confusion seems to be present about the nature of the e.h.t. pulse, the stabilisation of the e.h.t. voltage and the different characteristics of half-wave and multiplier systems. This month we are taking a close look at this department, for both monochrome and colour set use.

UHF PREAMPLIFIER

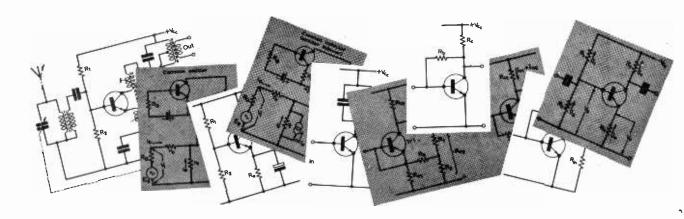
Full constructional details of a simple u.h.f. aerial preamplifier which has given excellent results for both fringe area and DX use. Several prototypes have been tried out and the stability is so good that they can be cascaded.

SERVICING THE PYE 368 CHASSIS

The chassis to be dealt with in the regular servicing feature is the Pye group 368 hybrid dual-standard chassis used in many Pye, Ekco, Ferranti and Invicta models.

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TRANSISTOR CIRCUITRY for beginners PART 13 H.W. HELLYER & MICHAEL HOLLIER

Minimum noise

We have already stated that our principal aim is as good a signal swing as we can afford provided that we do not thereby increase the noise in the circuit. With any transistor type, some noise is generated, but this can be aggravated tremendously by collector currents and also by the source resistance seen by the transistor—and, as might be expected, the optimum conditions alter with frequency.

A digression here, for colleague Mike feels strongly on this subject, having been too often caught with unsuitable replacements. Transistors with the same code number but made by different firms can have widely odd noise performances, as we have found when using them for laboratory equipment.

To find the optimum operating conditions under which our chosen transistor is to be used, we must turn to the graphs of noise figures quoted by the maker. These indicate a typical noise level expected at a selected collector current, with a selected source resistance 'seen' by the transistor base. But the quotes are at one single frequency. In practice we find conditions vary widely-a whole family of curves is really needed for optimum choice-and is seldom available, even from our old friends Mullard, who kindly acknowledged our quotes while pointing out an omission, in a letter from L. W. Owers in the October issue of PW. Very few firms, including Mullard, give figures that allow us to optimise for the whole audio band-in fact, they seem to think the world ceases revolving below 100Hz, giving data at 1kHz and 10kHz, generally. More noise is generated at low frequencies than high, and the higher the operating current, the higher the noise

We have decided upon a collector current of 80 microamps for Tr1 and the graphs, such as are available, would indicate that a source resistance of between 5 and $20k\Omega$ would be best for low noise. We shall aim at the lower figure.

The base of Tr1 will 'see' the resistance formed by the virtual earth (see Fig. 62) shunted by the series input resistor plus whatever the impedance may be of the device that is feeding the circuit. The inset of Fig. 64 should give us some idea.

The virtual earth resistance can be calculated

from
$$R_v = \frac{R_b}{G_o}$$
 so R_b becomes $500k\Omega$, or, in prac-

tice, a $470 \mathrm{k}\Omega$, 5% component. The voltage across this resistor is the Tr2 emitter voltage less the base voltage of Tr1, or $9.303\mathrm{V}$ and the current through this resistor will be around 19.8 microamps (remember we are ignoring the very small Ib1).

The current through R2 will, of course, be the same. So we come to a preferred value of $39k\Omega$. I shall not insult you with the details of the workings after 11 plodding articles of preparation . . .

We now have a working circuit with a low input resistance of around $5k\Omega$. And we insert R3 into the base 'feed' circuit of Tr1. This does two things: first, it raises the input resistance—that is, the resistance the source will 'see'; second, it gives us some control of the gain of this circuit. Remember, closed loop gain is equal to R_b dividend by R, which is, in this particular configuration, R1+R3. To get a theoretical gain of 20, for example, R3 would have to be $23.5k\Omega$ (preferred value, $22k\Omega$).

$$G_c = \frac{R1}{R3} = \frac{470k\Omega}{22k\Omega} = 21.3613$$

Coupling

As for that input and output coupling. We found, in practice, great care had to be taken. In fact, we built the circuit and had some very strange figures before remembering that the feedback was both a.c. and d.c. conscious. So the input capacitor serves a double function; that of blocking the d.c. from previous stages (and to previous stages) and coupling the signal to the stage which we are designing.

Now the problem is that it must be of a sufficiently large value to present a short-circuit, or as near this as may be, to the frequencies over which our amplifier has to work. In the practical case, something like 200μ F is in order. One reason that

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2N456A	0.75	2N3417	0·21 1·25	3N154 3N159	0·74 1·00	ASY27 ASY28	0.86 0.88	BCY59	0·18 0·19	BFX87 BFX88	0·25 0·20
2N457A 2N491	0.80 8.25	2N3570 2N3571	1.12	3N187 3N200	1·80 2·07	ASY29 ASY50	0.80 0.20	BCY66 BCY67	0.58 0.82	BFX89 BFY10	0·45 0·35
2N584 2N591	0·26 0·84	2N3572 2N3702	0-97 0-10	3N201	1.05	ABY55	0.85	BCY70	0·15 0·20	BFY11 BFY17	0·45 0·90
2N696 2N697	0·15 0·15	2N3703 2N3704	0·10 0·10	40050	0.78	ABZ21 AU103	0.55 1.25	BCY71 BCY72	0.13	BFY18	0.25
2N698 2N699	0.25 0.29	2N3705 2N3706	0·10 0·90	40050 40251	0.81	BC107 BC108	0·10 0·10	BCY87 BCY88	8·47 2·40	BFY19 BFY20	0.25 0.50
2N706 2N706A	0·10 0·12	2N3707 2N3708	0·10 0·70	40309 40310	0.88	BC109 BC113	0·12 0·10	BCY89 BCZ10	0·80 0·27	BFY29 BFY37	0·40 0·20
2N708	0.18	2N3709	0.90	40313 40316	0.92 0.50	BC114 BC115	0·12 0·15	BCZ11 BD115	0·40 0·75	BFY41 BFY43	0·48 0·62
2N709 2N711	0.88 0.80	2N3710 2N3711	0.80	40318 40322	0.92	BC116 BC116A	0·15 0·18	BD116 BD121	0·75 0·85	BFY50 BFY51	0·16 0·16
2N718 2N718A	0·21 0·30	2N3712 2N3713	0.95 1.08	40360 40361	0·46 0·48	BC117	0.20	BD123	0.80	VFY52 BFY53	0·16 0·15
2N720 2N721	0.50 0.55	2N3714 2N3715	1·15 1·28	40362	0.44	BC118 BC119	0·11 0·27	BD124 BD130	0.50	BFY56	0.84
2N914 2N916	0·15 0·17	2N3716 2N3773	1.80 2.85	43063 40389	0.88 0.46	BC121 BC123	0.20 0.25	BD131 BD132	0·75 0·75 0·38	BFY64 BFY75	0·41 0·40
2N918	0.80	2N3774	8-33 4-19	40394 40395	0.56 0.50	BC125 BC126	0·15 0·20	BD135 BD136	0·38 0·44	BFY76 BFY77 BFY78	0·22 0·24
2N919 2N929	0·20 0·14	2N3775 2N3776	5.95	4040 6 40407	0·44 0·88	BC132 BC134	0.80 0.11	BD137 BD138	0·47 0·55	BFY78 BFY90	0·86 0·55
2N9.0 2N1090	0·14 0·28	2N3777 2N3778	4·84 2·25	40408 40409	0·50 0·52	BC135 .	0·11 0·15	BD139 BD140	0·62 0·73	BRY39 B8X19	0·80 0·13
2N1091 2N1131	0-24 0-20	2N8779 2N3780	8·15 4·50	40410 40411	0.58 2.00	BC136 BC137	0-15	BDY10	1.25	B8X20 B8X21	0·14 0·20
2N1132 2N1184	0.20 1.27	2N3781 2N3782	8·67 8·37	40414	3.55	BC138 BC140	0·20 0·30	BDY11 BDY17	1.50 1.50	B8X26	0.34
2N1302	0·16 0·16	2N3789 2N3790	1.76 1.90	40438 40467 A	1·44 0·69	BC141 BC142	0·84 0·18	BDY18 BDY19	1·75 1·97	B8X27 B8X28	0·84 0·25
2N1303 2N1304	0.20	2N3791	2 06	40468A 40600	0.44	BC143 BC144	0·21 0·24	BDY20 BDY38	0-92 0-65	B8X29 B8X30	0·47 0·68
2N1305 2N1306	0.20 0.22	2N3792 2N3794	2·20 0·10	40601 40602	0.67 0.46	BC145 BC147	0·21 0·10	BDY60	0-90 0-85	B8X59 B8X60	0·78 0·54
2N1307 2N1308	0·22 0·25	2N3819 2N3820	0·26 0·47	40603 40604	0.58 0.56	BC148	0.09	BDY61 BDY62	0·75 0·28	BSX61 BSX76	0·42 0·15
2N1309 2N1483	0.25 0.90	2N3923 2N3824	0.50 0.75	40636 40673	1·10 0·56	BC149 BC153	0·10 0·10	BF115 BF117	0·48 0·58	BSX77 ASX78	0.20 0.25
2N1507 2N1613	0·24 0·20	2N3826 2N3854	0.28 0.16	AC107	0·85 0·16	BC154 BC157	0·11 0·09	BF119 BF121	0.25	B8W70	0.28
2N1631 2N1637	0.85	2N3854A 2N3855	0·16 0·16	AC113 AC115	0.16	BC158 BC159	0·10 0·10	BF123 BF125	0·27 0·25	BSY24 BSY25	0·20 0·15
2N1638	0.27	2N3855A	0.16	AC117 AC121	0.20 0.18	BC160 BC167B	0·87 0·11	BF127 BF152	0·27 0·20	BSY26 BSY27	0·20 0·15
2N1671 2N1701	1·00 1·10	2N3856 2N3856A	0·16 0·16	AC126 AC127	0·20 0·20	BC168B BC168C	0·10 0·10	BF153 BF154	0·29 0·16	BSY28 BS138	0·15 0·15
2N1702 2N1711	2·15 0·17	2N3858 2N3858A	0·16 0·16	AC128 AC141K	0.20	BC169B	0.11	BF158 BF159	0·15 0·27	BSY39 BSY51	0·15 0·25
2N1893 2N2102	0·84 0·80	2N8859 2N3859A	0·16 0·16	AC142K AC151V	0·25 0·14	BC169C BC170	0·11 0·11	BF160	0.28	BSY52	0.25
2N2147 2N2148	0·70 0·60	2N3860 2N3866	0·16 0·70	AC152V	0.17	BC171 BC172	0·18 0·11	BF161 BF163	0·85 0·20	BSY53 BSY54	0·25 0·80
2N2192	0.40	2N3877 2N3877A	0.25 0.26	AC153 AC153K	0·22 0·25	BC182 BC182L	0·10 0·10	BF166 BF167	0·85 0·18	B8Y56 B8Y65	0·79 0·15
2N2192A 2N2193	0.40	2N3878	1.22	AC154 AC176	0·20 0·18	BC183 BC183L	0.09	BF173 BF177	0·19 0·25	BSY78 BSY79	0·40 0·40
2N2193A 2N2194	0.27	2N3879 2N3900	0.20	AC176K AC187K	0.20 0.20	BC184 BC184L	0·11 0·11	BF178 BF179	0·25 0·80	BSY790 BSY95A	0.45
2N2194A 2N2195	0·80 0·87	2N3900A 2N3901	0.32	AC188K ACY17	0.25	BC186	0.25	BF180 BF181	0·85 0·82	BU104 BU105	1·42 2·25
2N2195A 2N2218A	0.18	2N3903 2N3904	0.20	ACY18 ACY19	0·15 0·20	BC187 BC204	0·25 0·11	BF182	0.30	C111	0.58
2N2219 2N2219	0.20	2N3905 2N3906	0·21 0·20	ACY20	0.20	BC205 BC206	0·10 0·11	BF183 BF184	0·40 0·17	C407 C424	0·18 0·15
2N2220	0.20	2N 4036	0.40 0.35	ACY21	0·18 0·13	BC207 BC268	0·10 0·09	BF185 BF194	0·17 0·14	C425 C426	0·86 0·25
2N2221 2N2221	0.22	2N4037 2N4058	0.12	ACY28 ACY30	0·18 0·42	BC209 BC211	0·10 0·80	BF195 BF196	0·15 0·15	C428 C444	0·25 0·26
2N2222 2N2222		2N3059 2N4060	0·90 0·11	ACY39 ACY40	0·55 0·17	BC212K	0.10	BF197	0·15 0·15	D40N3 GET111	0.82 0.45
2N2368 2N2369	0·11 0·12	2N4061 2N4062	0·11 0·11	ACY41 ACY44	0·15 0·23	BC212L BC214L	0·12 0·14	BF198 BF199	0.18	GET113	0.20
2N2369 A 2N2646	0·15 0·41	2N4302 2N4303	0·25 0·82	AD136V	0.94	BC236 BC237	0·16 0·08	BF200 BF224J	0·85 0·14	GET114 GLT115	0.50
2N2647 2N2711	1.20 0.12	2N4913 2N4914	0.80 0.87	AD140 AD140	0.50 0.55	BC238 BC239	0.08	BF225J BF257	0·19 0·22	GET119 GET120	0·85 0·25
2N2712	0.12	2N4915	0.95 0.11	AD142 AD143	0.50 0.45	BC251 BC252	0.20 0.18	BF238 BF244	0·22 0·16	GET535	0.20
2N2713 2N2714	0·17 0·17	2N4916 2N4917	0.17	AD149V AD149V	0.66 1.26	BC253 BC257	0·28 0·08	BF245 BF246	0.88 0.48	GET536 GET538	0·20 0·20
2N2904 2N2904		2N4918 2N4919	0-50 0-58	AD150 AD161	0·68 0·87	BC258 BC259	0.08 0.11	BF247	0.49	GET873	0.12
2N2905 2N2905	0.26	2N4920 2N4921	0-80 0-50	AD162 AD161 \	0.87 PR	BC261	0.20	BF254 BF255	0·14 0·15	GET880 GET883	0·80 0·20
2N2906	0.18	2N4922 2N4923	0.55 0.60	AD162 \(\)	0.69	BC262 BC263	0·18 0·23	BF257	0.41	GET 887	0.20
2N2906A 2N2907	0.18	2N4926 2N4927	0.90 1.00	ADZ11 ADZ12	1.50	BC300 BC501	0·42 0·84	BF258 BF259	0·46 0·48	GET890 GET895	0·22 0·25
2N2907A 2N2913	0-25 0-75	2N4928	1.80	AF106 AF109R	0.27 0.40	BC302	0.27	BF261 BF264	0·28 1·45	MA8001 MA8002	0·16 0·47
2N2923	0.12	2N4929 2N4930	2·28 2·25	AF114 AF115	0·25 0·24	BC303 BC304	0.50 0.48	BF270	0.25	MA8003	0.47
Post & F	acking	13p per o	rder.	Europe 25 ktra per p	p. Cor	nmonwea	lth (Ai	r) 65p (M	IN.) N	fatching o	harge otice
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	1-24	25+	1	-24	25 +		1-24	25 +
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BN7401	0.20	0.18	SN7430	0.20	0.18	BN7470	0.80	0.26
8N7402	0.20	0.18	BN7432	0.48	0.42	BN7472	0.80	0.25
BN7403	0.20	0.18	8N7433	0.71	0.62	8N7473	0.40	0.84
BN7404	0.20	0.18	8N7437	0.52	0.45	BN 7474	0.40	0.84
BN7405	0.20	0.18	BN7438	0.52	0.45	8N7475	0.45	0.85
8N7406	0.80	0.24	BN7439	0.52	0.45	8N7476	0.44	0.89
BN7407	0.56	0.48	BN7440	0.20	0.18	BN7480	0.75	0.70
BN7408	0.20	0.18	8N7441AN	0.75	0.72	SN7481	1.25	1.07
BN7409	0.20	0.18	8N7442	0.79	0.68	8N7482	0.87	0.61
BN7410	0.20	0.18	BN7443	1.04	0.88	BN 7483	1.00	0.82
8N7411	0.22	0.20	BN7444	1.04	0.88	BN7484	0.95	0.85
BN7412	0.42	0.86	8N7445	1.85	1.70	BN 7485	2.50	8.80
BN7413	0.80	0.27	BN7446	2.00	1.60	BN7486	0.45	0.40
BN7416	0.45	0.40	8N7447	1.80	1.20	BN7488	12.40	11.80
8N7417	0.45	0.40	8N7448	1.04		BN7489	4.97	
BN7420	0.20	0.18	BN7449		e to be	BN7490	0.80	
8N7421	0.22	0.20	annour	nced s	hortly	BN 7491	1.20	
8N7422	0.48	0.42	BN 7450	0.20		BN7492	0.75	
BN7423	0.52	0.45	BN7451	0.20	0.18	8N7493	0.75	
BN7425	0.48	0.42	BN7452	0.20		BN7494	0.84	
8N7426	0.82	0.28	BN7453	0.20	0.18	8N7495	0.80	
8N7427	0.48	0.42	8N7454	0.20	0.18	8N7496	1,00	0.80
	_							

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Arial lead Sp. each Values: (\(\mu \text{F/V}\); 6-64/64; 1/40; 1-6/25; 2-5/16; 2-2/63; 4-7/16; 4-7/25; 6-4/64; 6-4/25; 10/16; 10/25; 10/64; 12-5/25; 16/40; 20/16; 20/64; 25/6-4; 25/25; 23/10; 32/40; 40/16; 50/6-4; 50/25; 50/40; 64/10; 80/16; 80/25; 100/6-4; 125/10; 125/16; 200/10.

	S	ILIC	NC	RECT	IFIE	RS		
PIV	50	100	200	400	600	800	1000	1200
1.4	8p	9p	10p	11p	12p	15p	20p	
3.A	15p	17p	20p	22 ł p	25p	27p	80p	85 p
6A	_	_	25p	80p	32 ł p	85p	_	_
10A	30p	85p	40p	47p	56p	66p	759	_
15A	86p	45p	48p	55p	65p	75p_	87p	
35.A	70p	80p	90p	21 00	£1·40	£1·70	#2-75	_
1 amp and 3	amp s	re plastic	encar	sulation.				

	DIODE	S &	RECTIF	IERS		
IN34A 10p IN914 7p IN916 7p IN4007 20p I844 7p I8113 15p I8120 12p I8121 14p I8130 8p I8131 10p I8132 12p I8320 7p	AA119 AA129 AAZ13 AAZ15 AAZ17 BA100 BA102 BA110 BA114 BA114 BA142 BA144	7p 15p 12p 12p 10p 15p 25p 25p 15p 7p 17p 17p 12p	RECTIF BAX16 BAY18 BAY31 BAY38 BY100 BY102 BY122 BY124 BY126 BY127 BY164 BYX10	1249 1749 79 859 159 229 4749 159 179 579 229	F8T3/4 OA5 OA10 OA9 OA47 OA70 OA72 OA79 OA81 OA82 OA90 OA91	2219 17p 20p 10p 8p 7p 10p 7p 10p 7p 7p
IS922 Sp IS923 12p IS940 Sp	BA144 BA145 BA154 BAX13	17p 17p 12p 5p	BYZ11 BYZ12 BYZ13	32p 30p 25p	OA200 OA202 TIV807	7p 10p 50p

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	Matrix	Matrix
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21 × 5in	25p	25p
31 × 31in	25p	25p
34 × 5in	80p	29 p
5 × 17in (Plain)	82p	_
Vero Pins (Bag o	1 36) 20p	

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CAPACITORS							
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0.068, 0				4p each			
0.15, 0.2	22, 0⋅3	3		5p each			
0.47				99			
0.68				11p			
1μF				14p			
1 6µF				21p			
$2.2\mu F$				25p			

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care is needed here is again to reduce that bother—noise. If we make short-circuit and open-circuit input tests while measuring the residual noise at the output, we find there are some amazingly variant readings. A practical tip, for those who get fun from building their own hook-ups, is to load the circuit, at the actual input point, with the input impedance you want the circuit to 'see'. You may be surprised at the difference from abstract theory which your eventual readings reveal!

Measurement

We have talked glibly about open-loop gain, $G_{\rm o}$, but given no clues as to its measurement. This is no easy task—you see, if you disconnect the feedback to measure open-loop gain the first transistor bias goes adrift, and the measurements mean nothing.

We must take into account the a.c. feedback as well as the d.c., and here there is a gag which is worth recounting. A network can be made up temporarily, and inserted in place of the feedback resistor, which maintains the essential d.c. conditions, but effectively ties the a.c. feedback down to chassis. Fig. 65(a) shows a simple, three resistor

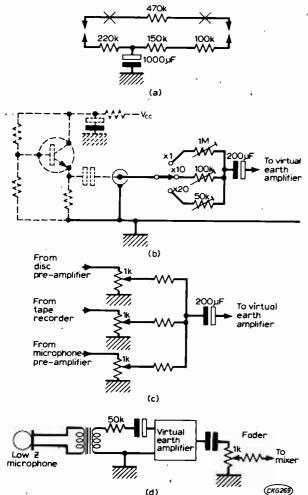


Fig. 65. (a) Substituting the feedback resistor with a decoupled network enables the gain to be measured more accurately. (b) Input for a variable gain pre-amplifier. An emitter follower, shown dotted, may be needed to effect matching. (c) Mixing facilities. (d) Microphone pre-amplifier.

and one-capacitor network, chosen so that the resistive values are approximately as R1 in Fig 64, but the large electrolytic capacitor acts as a complete shunt to any a.c. in which we might be interested. As Mike says, this may be of academic interest, but is worth a mention.

Of greater than academic interest is the capacitor shown dotted across the feedback resistor in Fig. 64. It has been said too often—which does not stop me from saying it again—that the wider one opens the window, the more the dirt blows in. Being interpreted, the wider our bandwidth, the more likelihood is there of our little amplifier getting upset by extraneous influences, like Aunty switching on the vacuum cleaner.

Without joining the argument that can set the hi-fi world by its ears; one group of contenders arguing for an almost infinite bandwidth and the inclusion of filters, the other for a 'tailored bandwidth', we can say here that the ease of making our frequency response roll off in a controlled manner at the top end appeals to us. Without that capacitor, our frequency response of the built amplifier (made up in a Norman Rose AB9 box with co-axial terminations, for complete screening) was within +0-3dB at 78kHz and at 150kHz, we were still only $8\cdot 2dB$ down.

At the bottom end, incidentally, we were -0.1dB at 40Hz and -0.8dB at 15Hz, which is negligible. Shunting the feedback resistor with 22pF gave us -3dB points at 20kHz and -6dB points (complying with DIN 45 500, in case anyone wanted to argue!) at 31kHz. Under these conditions, the broadband residual noise was 0.13mV with an open-circuited input, 990 microvolts with a short-circuited input. As clipping took us to slightly over 6 volts (for a 410mV input), our signal-to-noise ratio, unweighted, could be said to be $20 \log 10^{-6}.0.0001$, taking a figure of 0.1mV as a typical residual noise measurement. A rather impressive (who said impossible?) 95.5dB.

Effective input noise is the output noise with input short-circuited divided by the gain. Our measured gain at a typical 10mV input was only 14·7, not as much as we had expected, but accounted for most likely by component spreads and the second transistor, which happened to be an odd type we had handy. You can always select with great care for precision, as we said earlier, but it is great fun to 'suck it and see'. So in the practical instance, we can say our effective input noise is 68 microvolts. This now becomes the limiting factor for any use to which we are going to put such a device. I think you will agree that in the present case the limitation is hardly exclusive.

Application

A few of the possible applications were hinted at previously. Without wasting any more space on design data, take a look at the three sub-circuits of Fig. 65 (b), (c) and (d). First we see a way of altering the input resistor, precisely, by presets, so that we get a variable gain pre-amplifier, as might be useful for an oscilloscope. The problem here may be an alteration of input impedance, and it is a good idea to precede the virtual earth pre-amplifier with an emitter follower stage, which gives, you will remember, a reasonably high input impedance and a low output impedance (providing the necessary low source our device wants to 'see'.)

Let's suppose we want to use the virtual earth pre-amplifier as an input stage for a mixer, where there are several odd sources that may be used separately or simultaneously, and where the action of one must not interfere with that of another. As any amateur disc-jockey will tell you, a very practical problem. In Fig. 65(c) we get the inputs from the sources taken to low value potentiometers and from there we can feed up to three R3 resistors to the virtual earth point, this time using our coupling capacitor to follow the resistors, for effective isolation. By juggling resistor values, with a little experiment, we can again get our levels somewhere the same, and use a master gain control later in the circuit, where its operation at a higher signal level will not introduce unwanted noise, etc.

Of course, there is always the microphone preamplifier, as in (d), where we want a bit more gain prior to a mixer stage. The transformer is a low/ high or medium/high type and is best mounted in the overall screened box that houses the virtual earth amplifier.

Power supply

Finally, this month, having again not kept my promise to lead us on to tone controls, although a careful perusal of the foregoing will have seen the trend our thoughts are taking, we have a brief look at the proposed power supply for this and other projects. This was knocked up easily in an hour and needs no particular layout finesse, nor screening. It uses any convenient transformer that can give between 24 and 33 volts—not really safe to exceed 33.6V—and the rectifiers are easily obtained types with minimum requirements of peak-inverse voltage

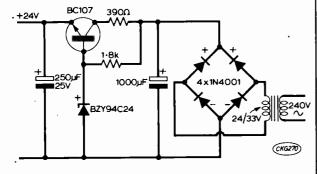


Fig. 66. A practical power supply, suitable for use with the circuits described.

50V and handling capacity 200mA. We used a REC 60 because it happened to be there, but four 1N4001's would have done. The particular requirement is the zener diode, which must be a 24 volt type, such as shown, and components can be halfwatt types, with the biggest problem the mounting of the two large capacitors. Note that this zener operates in the reverse to the breakdown mode, i.e., it is set to regulate, with cathode to positive. This 24 volt output, with the $2k\Omega$ resistor (or $2\cdot 2k\Omega$, if you have no $2k\Omega$ version available) drops to the needed 20 volts for our amplifier.

TO BE CONTINUED

AMATEUR BANDS RECEIVER

-continued from page 698

crystal pass-band. Adjustment of any of the i.f.t. cores should then bring about a great increase in signal strength as they are shifted into the crystal pass-band. The i.f.t.'s are all finally peaked in this way, signal strength being reduced by VR1 as necessary.

When the i.f. amplifier is aligned in this way, a very steep sided response should be obtained. If X6 and X7 are removed and a 100pF capacitor plugged into one holder, general selectivity will still be very good, but there should be a very noticeable reduction in sharpness of tuning and noise will increase due to the broader pass-band.

MODIFICATIONS

As the idea of construction in stages is to obtain fully working circuits as quickly and easily as possible, the i.f. section can be simplified initially then modified to the full circuit.

The S-Meter circuit can be omitted completely at first and fitted later.

IFT1 and V1, Fig. 2C may be omitted and mixer pin 6 taken to pin 3 on i.f.t.2 or V1 and i.f.t.2 may be omitted and the crystals or secondary of i.f.t.1 may be temporarily connected to pin 1 of V2.

When the tunable first i.f. section is constructed, the receiver can be employed for the 3.5-4MHz band only. The receiver cannot be used on other bands until the crystal controlled first conversion section is completed.

With some valves i.f. instability occurred with VR1 at maximum gain. This was cured by placing a $2 \cdot 2k\Omega$ resistor between pin 2 of i.f.t.1 and h.t., with a $0 \cdot 25\mu F$ capacitor from pin 2 to chassis.

TUNABLE FIRST IF AMPLIFIER

This has two stages, Fig. 2B, and is constructed in a screened box to minimise pick-up of unwanted signals. Coverage is 3.5MHz to 4MHz, with a little to spare at the extreme positions of the 3-gang capacitor VC1, VC2 and VC3.

V1 operates as an r.f. amplifier on the 3.5.3.8MHz band and as first i.f. on the other ranges. The gain of this stage is also controlled by VR1. AGC bias is applied to both stages via R1 and R4 (it is not good practice to apply a.g.c. to a frequency changer of this type—Ed).

The oscillator section of the mixer-oscillator V2 is run from the 150V stabilised h.t. supply. Input to L1 is via a screened lead and a similar screened lead runs from V2 to the 455kHz i.f. amplifier.

The box is $5\times4\times2in$. deep, with the valves on top and all other parts, including VC1/2/3, inside. This box is made from a $5\times4in$. flat plate, to which are bolted two $4\times2in$. and two $5\times2in$. "universal chassis" flanged members. It is easier to leave the sides and back off the box until wiring is completed.

TO BE CONTINUED

Next month we shall cover the construction and alignment of the tunable IF amplifier and give full information on the BFO/Product Detector and RF/1st Mixer stages to enable the receiver to be completed.

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ACY17	0.20	OC201	0 - 25
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AF186	0 - 20	2N1304-5	0 - 17
AF139	0 · 30	2N I 306-7	0 - 20
BC154	0 · 20	2N 308-9	0 - 22
BC107	0 - 10	2N3819FET	0 - 40
BC108	0.10	2N4416FET	0.35
BC109	0.10	2N3823EFET	0 · 30
BC 148	0 - 10	Power Transi	
BC169	0 - 12	OC20	0 - 40
BF194	0 - 15	OC23	0 · 25
BF274	0 - 20	OC25	0 25
BFY50	0.15	OC26	0.25
B\$Y25	0-13	OC28	0.30
BSY26	0.13	OC35	0 - 25
BSY27	0.13	OC36	0 - 37
B\$Y28	0 - 13	AD149	0.35
BSY29	0 · 13	AUY10	0.75
BSY95A	0.10	25034	0 · 25
OC41	0 - 15	2N3055	0 - 40
QC44	0.13	Diodes	
OC45	0.10	AAY42	0 10
QC71	0 10	OA95	0.07
OC72	01.0	QA79	0.07
OC81	0 · 13	18AO	0 · 07
OCSID	0.13	OA95	0 - 07
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Hex. Inverter	BMC936	12p	Hp	I Op
Hex. Inverter	BMC937	12p	Hp	10p
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Hex. Inverter	BMC941	120	iib	100
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Clocked Flip Flop	BMC945	20p	180	16p
Quad Inverter	BMC946	Hp	100	9p
Clocked Flip Flop	BMC948	20p	18p	I ép
Quad Inverter	BMC949	120	Hp	l Op
Pulsed Trig. Binary	BMC950	20p	186	l ép
Monostable Multivib.	BMC951	25p	23p	2 lp
Dual J/K Flip Flop	BMC953		180	16p
Dual J/K Flip Flop	BMC955	20p		
	BMC956		18p	l ép
Dual J/K Flip Flop	8MC958	20p	18p	16 p
Quad. 2-input Power		12p	llp	10p
2/4-input Gate	BMC961	12p	Hp	10p
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HI-FI STOCKISTS

MONTHLY NEWS FOR DX LISTENERS

A LTHOUGH a great deal of pleasure can be obtained from simply listening to Broadcast stations many listeners take the hobby a step further and collect QSL cards from all over the world.

A QSL card is a verification from the station that the listener did, in fact, hear their broadcast. QSL cards are issued as a reply to reception reports from the listener after the details have been checked

against the station log.

The majority of stations are very glad to receive reports from listeners as a well prepared report tells the station how well its transmissions are getting through. The subject for this month is the preparation of reception reports which are helpful to the station.

The first essential of a good reception report is the name and address of the reporter, without this the station does not know where the reception occurred and is unable to send a reply. The technical information should be given in the following manner:—

RECEPTION REPORT

I received your broadcast on (date), on a frequency ofkHz, and listened to it from to hours G.M.T.

The receiver used was a (TRF/Superhet etc.) with (Number) Valves/Transistors, made by model number

The aerial was an interior/exterior one, metres high and metres long of the type.

I hope that this report is of use to your Engineers and trust that you will be able to verify that my report is correct. If so, will you please send me your QSL card, or verification letter, in reply to this report. I enclose an International Reply Coupon to cover your postage costs.

I hope that I shall have the pleasure of hearing your station in the future and look forward to sending you further reports on your transmission.

Yours sincerely,

......

The SINPO code mentioned in the above specimen report may be new to some readers so I will give details of this method of assessing reception.

The "P" in the SINPO code stands for Propagation but is probably easier to understand if we refer to it as Fading.

THE BROADCAST BANDS

Malcolm Connah

Frequencies in kHz • Times in GMT

Rating	1	2	3	4	5
S	Barely	Poor	Fair	Good	Excellent
	Audible				
Ī	Extreme S	evere	Moderate	Slight	Nil
N	**	,,	,,	,,	,,
P	**	"	,,,	,,	**
0	Unusable	Poor	Fair	Good	Excellent

Reception of BBC Radio One on 247 metres in the medium wave band can usually be rated as 55555 but the transmissions are sometimes affected by slight interference which reduces the rating to 54554. Radio Luxembourg on 208 metres is usually subject to severe fading and slight interference giving a rating of 54522.

The overall Merit figure is a very subjective rating and takes into account the other four figures, it would however be unusual to have an overall merit figure which is greater than the lowest of the other four. To use the above example some listeners would rate Radio Luxembourg as 54523, others would take the average of the first four figures as the "O" rating. In this case Luxembourg would rate 54524, which is incorrect since reception with severe fading cannot be classed as good.

The first log this month comes from Michael Berry of Dewsbury in Yorkshire who used his Eddystone EB35 receiver and 20 foot horizontal wire in

the loft to hear:

3227 ELWA, Liberia, vernacular at 2010.

4890 R. Diff. Venezuela, Spanish at 0100. 11795 ETLF, Ethiopia in Malagache at 0330.

15105 R. Rural, Brazil, Portuguese at 2125.

15155 R. Diff. de Sao Paulo, Portuguese, 2235.

15170 ELWA, Liberia in French at 2000. 15445 R. Nacional be Brazilia, English at 2130.

Nigel Knowlman of Cullompton in Devon has sent in another log using his Lafayette HA-600A with an inverted 'L' antenna to hear:

11720 Radio Tashkent, USSR, at 1405.

11815 TWR, Bonaire noted at 0040.

11850 Radio Vilnius, USSR at 2245.,

15185 WINB, USA in English at 2215. 15195 R. Ankara, Turkey in English at 2200.

17855 NHK, Japan, news in English at 0705.

17920 Radio Cairo in English at 1415.

A. P. Turner of Eastbourne, Sussex has a Peto-Scott H-25, 5-valve domestic superhet receiver and a 65 foot long wire which enabled him to hear:

6040 *VOA* with news at 1917.

7100 R. Tirana, Albania in English at 2223.

7245 R. Austria, news in English at 0907.

11805 R. Pakistan in English at 1830.

15245 RSA, South Africa in English at 1608.

17810 R. Kuwait, news in English at 1738.

Reports should arrive by the 15th. of the month and be addressed to me at 59 Windrush, Highworth, Swindon, Wiltshire. Please note the new address.



THE AMATEUR BANDS David Gibson, G3JDG

Frequencies in kHz Times in GMT

OUBTLESS many will not be pursuing the noble art of Amateur Radio on November 5 but will usefully employ the time to honour (?) Guy Fawkes for his near miss. However, that does leave another twenty nine days in which to

make up for lost time.

One thought is the topband transatlantics. Quite a few signals have been received, not merely from across the pond but from other countries/continents also. A session around 0600 hours might be worth a try although most 160 metre stalwarts are just as liable to be putting out a slow CQ in c.w. in the evenings too. Many d.x. stations are trying their hands at topband using s.s.b. and this band should make an interesting playground for the more seriously minded s.w.l. during the long winter evenings ahead.

Intruders in the Amateur bands are pests who have no moral or legal right to be there. The R.S.G.B. keep an intruder watch and this relies heavily upon reports received. Any s.w.l. with reasonable equipment is welcome to assist, but reports must be accurate. If you have a single conversion superhet, for example, you must ensure that it is not an image signal you are hearing which is, in fact, outside the band.

It's funny callsign time again. Queries flood in about those using a letter followed by two numbers. Not a postal code for Hong Kong, just a new prefix time-again! Bangladesh is apparently active and the call sign here begins S21 (sounds like the washroom in a Government building). Just in case you think I've picked out an odd one, how about C21 for Nauru. Don't be fooled though, the latter have also been known to use a C29 prefix too.

Paul Genner (Liverpool) writes in with news of activity from Vietnam which must surely be a rare one for anyone to bag. Callsign is XV5AC and no band given but 20 and/or 15 would be a safe bet. Paul also mentions that anyone wanting to add Willis Island to their list should look out for VK9ZB who will set sail in December from Willis. Quick, while

there is yet time.

John Tirrall (Bognor) tells the amazing tale of a W7 reported to be putting up a 40 (forty) element beam for 28MHz and will feed the brute on generous helpings of r.f.-a kilowatt no less. Those who hear nothing on ten metres could make it a red letter day. (Perhaps a red aerial day with all that power

coming in).

Talking of ten metres, with the decline of the sunspot activity count this band is perhaps one of the most interesting. Readers might consider erecting a simple ground plane antenna especially for this band. The elements are only just over 8 feet in length and even a vertical dipole might be dangled down the side of the house. Feed in the centre with 75Ω coax as for a horizontal dipole and your in business. Watch that your receiver isn't one which is to be nurtured on 300Ω feed though or you'll have a mismatch.

Times to listen are always a dangerous thing to predict with any degree of dogma since some bright soul always hears half the world at the very opposite times to those you have predicted. However, according to the JDG crystal ball, afternoons and evenings appear favourite for 21 and 14MHz which are still the most popular listening bands if logs received are any indication. Hopefully, adventurous s.w.ls will venture forth into regions such as 3.5MHz and 7MHz during the coming months as conditions

Alan Smith (Nelson), JR310, a.t.u. and 60ft. end fed is one who braved 3.5MHz to get s.s.b. scalps from; HK1NR, KZ5JF, K3JH, PY1HA, SP9FMA. VEIARH, VEIIE, VEIXI, VOIBT, VOICV, WIPSK, W3MFW, XEIIIJ, YN1FI, ZL2BT, ZM4PG, 6Y5AR.

Up on 21MHz Alan bagged; CR6QA, CR7LE, CR8BF, DU1BOB, DU2EL, EP2JW, ET3USA, FP8DH, HS4AGN, HS4AGZ, JA1HIV, JA2DX, JA3BLC, HS4AGN, HS4AGZ, JAMMA, JA8QX, JA9EFQ, JA6FBQ, JA7MFA, JA8QX, JA9EFQ, JA0GRR, KA6MH, KH6KHD, KP4DDO, LU1ACO, CVICP TJ1DF, VE1AM, VE3AUM, VE3AUM SV0WW, SV1GP, TJ1DF, VE1AM, VE3AUM, VS6AD, W8EX, W9ADW, XV5AC, ZS1J, ZS2MI, ZS3AK, ZS4LW, ZS5OE, ZS6OF, 4S7AB, 4S7PB, 4Z4EF, 4Z4LK, 5B4KP, 5N2ESH, 6W8YL, 6V5GB.

Paul Russell (High Wycombe), went to West Norfolk for a holiday. With him went a Sentinal converter, UR-1A receiver as a tuneable i.f. (4-6MHz) and a 5-element yagi which posed transport problems on the way there, especially on the London Underground. Rewards for these sterling efforts included 144MHz signals from; F5VA, F6AGV, F6NM, G2AKQ, G3BN, G3CZA, G3DAH, G3OXV, G3PMH/P, G3POI, G3SRT/A, G3TTV, G3UJK. G3XIX, G3ZYC, G4ARD/P, G8DYK, G3WW, GW4ABR/P, P0HVA, PA0VJ, PA0VZL.

William Fereday (Aston-on-Trent) uses an R107 and bent 50ft long wire (Oh-bold). Twenty metre tweets from; JA1QZY, JA2PJC, VK3AHI, VK3RZ, VK5FH, W6BMP, W6BT, YN3NPF, 9V1QT.

Roger Dixon (Skipton), PR30, CX203 receiver and 100ft, long wire end fed sent in a log for ten metres (bless you). Stations bagged include; CE3AGU, LU4DCO, TU2DO and 9J2KY. Who says there's nothing up there?

Glyn Fisher (Oakham) landed a number of EU stations on 7MHz. Among these were signals of the s.s.b. type from VK2AVA, VK5PB and VK7GK. Gear is a Westminster radiogram and a 50ft. endfed.

Well worth a listen is the 1.8MHz contest on November 11-12. There is also a Czechoslovakian contest on the 12th. The Czech stations are often in evidence on topband but if you want to log stations from further afield, try the CQ WW d.x. c.w. contest on November 25-26.

Logs, in alphabetical order please to arrive by the 15th of the month to 12 Cross Way, Harpenden, Herts.



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AD14	40p	BC154	20p	ME0404	14p	OC201	25 u	2N3055	49p	IN4002	4
AD150	44 p	BC168	10p	ME4401	10p	OC25	25=	2N3702	12p	IN4003	5
A DIGI	-	BC169	11p	ME4102	12p	OC28	30	2N3703	12p	IN4004	7
AD162 M	/P55p	BC182L	8p	ME6002	14p	OC29	36	2N3704	12p	OA 90	6
AF114	15p	BC183L	8p	ME6101	14p	OC35	25=	2N3705	12p	OA91	- 6
AF115	15p	BC184L	8p	ME6102	15p	OC36	86=	2N3706	10p	OA200	10
AF116	15p	BC212L	8p	MP8111	32p	TIP29A	48=	2N3707	10p	OA202	8
AF117	15p	BC214L	8p	MP8511	84p	TIP30A	56 m	2N3708	9p	1844	10
			_	MP8513	45p	TIP31A	58 m	2N3709	10p	IN4149	4
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(Closed Wednesday)

In the post

As a purchaser, in a small way of components advertised in P.W. I have sometimes been amazed at the varying rates of postage charged for parcels to N.Z. I therefore wrote to the Post Office, London to find out the reason.

I enclose copies of my letter

and the reply.

I am sure that the advertisers are trying to act in our best interests. It is no advantage to them to pay out extra postage, but it's our money they're using!—C. J. NewChristie (Whangarei. Zealand).

LETTER TO GPO:

I should be grateful for your advice in the following problem.

I am a hobbyist meddler in things electronic and from time to time I make purchases of equip-

ment from England.

Postage on parcels varies so much—for example: (1) Six hearing-aid inserts (1 oz.) Liversedge, 5p. (2) One integrated circuit (1 oz.) Sevenoaks, 6112p. (3) Resistance wire (7 ozs.) Croydon, 712p. (4) Loudspeakers (3 lb.) Liversedge, £1.23. (5) Five tape cassettes from London, 75p.

All these goods have been mail"-not marked "surface

registered.

I don't object to waiting a couple of months for goods sent sea-mail but I must confess to being mystified by the postages quoted.

Can you advise the most economical rate in general terms for the sort of equipment I am

buying please?

REPLY FROM POST OFFICE:

We were interested to see the rates that were charged on the packets you have been receiving. Items 1 and 2, the hearing aids and integrated circuit, weighing one ounce each, should have been sent by the Letter Post at the Commonwealth Rate of 2 new pence (3p from 1 July 1971). There was no service operating in March 1971, surface or air, by which the charges you mention of 5p and 6112p could have been correctly made for these items. Although they were sent a long time ago, if you still have their

wrappings we will gladly investigate how the charges were raised. Item 3 was sent by the Small Packet service, and although you have not given us a date for the packet, the charge of 1s 6d was almost certainly correct. Item 4, the radio speakers weighing 3 lb would have been sent by the Surface Parcel Post Service for £1 · 15p.

The most economical service available for the sort of goods you have been receiving, including the tape cassettes, is undoubtedly the Small Packet service. This provides a cheap rate for lightweight goods (up to 2 lbs in the case of New Zealand). Small packets must be packed so that they can be easily examined without breaking any seal, and should not contain any letters personal correspondence. although an invoice is permissible. The words 'Small Packet' should be marked on the top left hand corner. In this service a packet of cassettes weighing, say, 14 oz can be sent for 15p.

I enclose various leaflets showing our current charges and a photocopy of the Small Packet regulations taken from the current edition of the Post Office Guide. I am sure you will find the Small Packet service meets your

Radio fags



I enclose the photo of a packet which once held ESS-O-ESS cigarettes as I thought you might like to reproduce it in your maga-

Whereas countless cigarette brand designs are based on ideas to do with the sea there must be few that have anything to do with radio. The only item apart from this that I know of is Wireless Mixture tobacco.

I do not know when the packet was introduced but this brand was on sale in 1939 at 3d for 6, also 12 for 6d and 3 for 112d. It was to disappear during the next ten years as it is not included in the 1949 retail price lists. Gallaher Ltd. are now the proprietors of Cope's brands.

One of my achievements is getting something into the Guinness Book of Records concerning wireless. I sent them an obituary from a newspaper called "the forgotten inventor." This resulted in the inclusion of details of the world's first advertised broadcast by Sir Aubrey Fessenden.-W. Humphries (Suffolk).

She saw the light

One day a dear old lady came into our shop and asked if we could sell her a light bulb for her "loo". Upon asking what wattage she wanted she replied that she had not any idea. I then asked her to bring her old bulb into the shop so that I might try to read the wattage. At this suggestion she stepped back in surprise and flatly refused to do this. When asked the reason for her attitude she replied, "Young man, if I take the old bulb out without putting a new one in straight away, all the electricity will fall out of the socket and I'll have a big bill to pay next quarter".

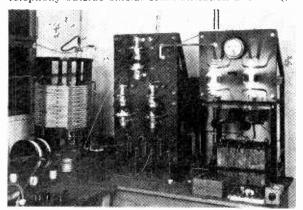
It took me several minutes to explain to her that this was not the case and she went away with a new 25W bulb in her bag which we gave her as a prize for being our 'customer of the month'.--C. Scott, (Edinburgh).

We are glad to hear that the lady went away a happy customer. If any readers have amusing stories like this, we'll be glad to consider them for our "Letters" pages—Editor.

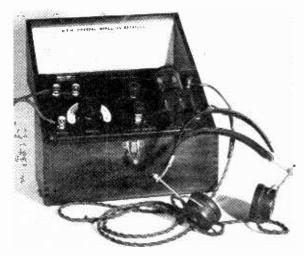
GOING BACK... 1970 60 50 40 30 20 COLIN RICHES ARTHUR DOW

in an ex-army hut near Chelmsford in Essex, when on 14th February 1922 a group of Marconi engineers began a series of regular experimental transmissions. Every Tuesday evening from a rigged-up transmitter, call sign 2MT Writtle, or more affectionately to its listeners, Two Emma Tock, they transmitted programmes whose original purpose was entirely technical. Shortly afterwards, in May, another transmitter, later to be even better known, was opened up by the company at Marconi House in the Strand in London. This was the famous 2LO station that provided the foundation from which the British Broadcasting Company grew after its formation on 14th November of the same year.

Two Emma Tock provided the first regular broadcast service in this country, and incidentally broadcasting's first audience, an audience which in its enthusiasm for the pioneering programmes, generated the original demand for public service broadcasting. The 2MT transmitter was set up for use in a series of experiments designed to establish the effective range of a wireless telephony transmitter. At the same time a number of radio amateurs were appearing, largely young ex-service men who had learnt about radio during the 1914-18 war, who had put together their own receiving sets, and who wanted transmissions to receive. Earlier experiments with entertainment, as when Dame Nellie Melba and later Lauritz Melchior, the Danish tenor, had broadcast from a makeshift studio in Chelmsford in 1920, had shown that there was a potential for wireless telephony outside official communication and naviga-



The 2MT transmitter at Writtle from which the first regular broadcast transmissions in this country began on Feb. 14th, 1922.



A B.T.H. crystal receiver of 1923 vintage.

tion usage, but the official attitude had been discouraging, and the duty of granting licences for transmitters was the preserve of the Postmaster General. Government was unwilling to consider licences for more than a token number of even technical transmissions.

2MT was finally granted an experimental licence to transmit early in 1922, though the permission was hedged about with many restrictions. But for half an hour on Tuesday evenings, experiments were to be allowed, though even then with three-minute breaks in every ten, to ensure that no interference with "legitimate services" was being perpetrated.

2MT opened regular broadcasts officially on behalf of the amateurs who needed a source against which they could calibrate their receivers, and to begin with its programmes were not very much more interesting than early 1920 transmissions made before the government clamp-down, when W. T. Ditcham read from Bradshaw's railway timetable, but the enthusiasm and gaiety of the young Marconi engineers who ran it very soon turned it into a half-hour's entertainment in its own right. The names of those men read like a roll-call of some of the great names in broadcasting. In charge of the project was Captain P. P. Eckersley, who later went to the new British Broadcasting Company as its first chief engineer. It was his infectious and spontaneous humour which gave 2MT its unique flavour; he was

PICTURES TO BRING BACK MEMORIES . . .



"Marconi House" main entrance from the Strand (taken 1912).



The "Television Toppers" view a 23th screen. The largest at the 1953 Radio Shows



The "Roving Eye", taken in 1954.



Jean Metcalf, compere of "Family Favourites" (1954).



BBC camera used for televising the "Victory Parade", Seen here with Windmill Girls (1946).

not only the first engineer in charge, he was also the first of the true radio entertainers, with a gift for ad-libbing that constantly alarmed those of a less adventurous 'disposition who worked with and around him. Others in the team were Noel Ashbridge, later Sir Noel, who was the BBC's first technical director, till his retirement in 1952, R. T. B. Wynn, a later chief engineer of the BBC and B. N. MacLarty, who became head of the BBC's Design and Installation team before he returned to Marconi's in 1947 as Engineer in Chief.

By contrast, Marconi's 2LO station, granted its licence in May, began a rather staid existence, a happy coincidence for the pioneers of 2MT, as it gave them an opportunity to provide skits and lampoons which were much appreciated by their listeners. 2LO operated on conditions of restricted timing, at first even no music, and low power, beginning with 100 watts, later raised to 1½kW. Its programmes had each to be individually licensed by the PMG, and were limited to private occasions often for charity, at which Marconi engineers installed the receiving apparatus and operated it. Each programme was notified to listeners by postcard by means of a special mailing list kept by The Marconi Company, and most of them consisted of polite light music.

The 2LO station transmitter was designed by Captain H. J. Round, installed by C. S. Franklin and run by A. R. Burrows who eventually became the much-loved Uncle Arthur of the BBC. Among the many papers in the Marconi archives which tell the story of the birth of British Broadcasting, not the least interesting is Arthur Burrows' letter requesting permission to recruit a young man of particular quality to compere the station's programmes, a young man with "technical tendencies grace of manner and an excellent telephone voice." Many of Burrows' requirements were couched in terser terms and it was his organisational skill and foresight that shaped the studio techniques which are still the basis of modern broadcasting.

By this time many wireless societies had been formed and more and more the demand for radio receivers was being felt. In the United States since 1919 "wireless" had become fashionable, but with no constitutional control of the use of wavelengths, chaos reigned in a commercially sponsored free-forall. The British Government, seeking a way from the dilemma posed by popular demand on the one hand and a justifiable reluctance to allow free access to the air on the other, set up the Wireless Sub-Committee of the Imperial Communications Committee in April of 1922. After consideration, their recommendation to set up a single broadcasting company was accepted and in November 1922 the British Broadcasting Company was formed from six commercially interested companies with £100,000 share capital.

The six companies were The Marconi Company, the Metropolitan Vickers Co., the Western Electric Co., the British Thomson-Houston Co., the Radio Communication Co., and the General Electric Co., and on its formation on 14th November a Broadcasting Committee of the founder members took over the responsibility of running 2LO.

2MT Writtle continued to transmit until the following January, when it finally closed down.



Our favourite "dumb blonde"—Sabrina shown during rehearsals for Arthur Askey's "Before Your Very Eyes" show (1955).

We would like to thank the Marconi Company, the BBC, the Science Museum and readers whose help in compiling this article has really been appreciated.



CAR/PORTABLE RADIO. October 1972
Readers experiencing difficulty in obtaining the oscillator coil L3 (Osmor PW/01) can use the Denco coil Type TOC1 using the following connections:—Pin 1 to C3 and R3, Pin 2 to the positive line, Pin 3 to S1b, Pin 4 to IFT1, Pin 5 to Tr1 collector and Pin 6 to Tr1 emitter. (Denco Ltd., 357 Old Road, Clacton-on-Sea, Essex).

INTERCOMM CALLING SYSTEM. October 1972 There is an error regarding the wiring around the secondary of T2. The loudspeaker is connected in series with the wire from pin 5 of SW1 to the positive line; the speaker is not connected directly to the top of the secondary of T2.

DX'ers A.F. PROCESSING UNIT. July 1972 In Fig. 4 a break in the conductor strip should be shown at 30-g.

I.C. AUTO PARKING LIGHT. September 1972
It has been brought to our attention that a single parking light is no longer sufficient; all four parking lights are necessary. This does not of course invalidate the circuit.

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BA 48	15p	BCY21	96p	GET102	39p	T1561	20p
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BAX12 BAW63	12p 36p	BCY71 BCY72	20p	ME0412	15p	2N70B	, 9p 12p
BAW65		BCY89	97p	ME0413	13p	2N753	10p
BAW67	36p 35p	BDII5	75p	ME0462	19p	2N919	45p
BB105	37p	BD124	80p	ME2002	8p	2N920	42p
BBY20	37p	BD131	75p	ME4003	12p	2N 1302	17p
BC107	10p	BDI32	80p	ME4102	10p	2N1304	21p
BC107B	i2p	BDI35	75p	ME4104	-8p	2N1306	24p
BC108	10p	BDI75	44p	ME6002	12p	2N1307	24p
BC108A	10p	BDIBI	90p	ME6101	12p	2N1308	24p
BC108C	15p	BD184	£1.3	ME6102	13p	2N1309	24p
BCI09	12p	BFI21	25p	ME8001	12p	2N3053	20p
BC113	15p	BF123	30p	ME8003	13p	2N3054	50p
BCI16	20թ	BFI25	25p	MEFI04	34p	2N3055	55p
BC117	20p	BF127	30p	MELII	30p	IN914	бр
BCI19	30p	BF153	20p	MP8112	34p	IN916	
BC121	25p	BF154	20p	MPBI13	40p		10p
BC125B	25p	BF160	25p	OA47	10p	IN4148	6р

TERMS. Retail mail order subject to £1.00 minimum order. Cash with order only. Trade and educational establishments M/AC on application (minimum 65). Postage 10p inland, 25p Europe, GUARANTEE. All goods carry full manufacturer's warranty. Special Enquiries etc. Please enclose stamped addressed envelope.

TRANSISTORISED F.M. tuner head with A.M. gang, slow motion drive. 88-108Mcs, with circuit diagram. £2 10p.

B.F.W. 10 Fet. New (unmarked) 5 for £1 00p.

SPECIAL OFFERS of Unmarked Tested Power Transistors. 2N3055 Silicon NPN 30p each 4 for £1. 2N3054 Silicon 20p each 3 for 50p. Plastic 40 Watt NPN 25 Volt 20p each 3 for 50p.

P-C BOARDS (not computer panels).

1 off 6 transistors single wave band 1 off 4 transistor audio

1 off 3 transistor £1 50 the three.

Encapsulated bridge rectifier (itt usd 3 3mdh) 100 PIV 2 amps. 50p each.

Transistor F.M. Stéréo Multiplex Decoder. Size: 51 x 21 x 11. As used in well known British stereo units with circuit. £3 75.

GARRARD SP25 MK. II less Cartridge. £10-50.

10 VOLUME CONTROLS consisting of 2 off each. 100K log. ganged L S—20K log. ganged L/S 470K log. D/P Switch—10K lin. L/S—50K lin. L/S. £1 25.

4 PHONO SOCKETS ON PANEL. 10 panels for £1 25.

12 PLASTIC KNOBS. Chrome and Gold, 3 types—4 off each -spring clip £1 25.

10 COMPUTER PANELS packed with components including one panel with 2 Power Transistors. £1-00.

All items post pald in

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learn how to become a radio-amateur in contact with the whole world. We give skilled preparation for the G.P.O. licence

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NAME -

ADDRESS :.

WB122

BLOCK CAPS please

TAPE HEADS

We are gradually obtaining more information about the Truvox tape heads we have, we are told that these have been wound in a very ingenious way so that winding may be coupled either in parallel or in series depending whether high or low impedance is required. We also have matching erase heads and now offer these in pairs. 1 record and 1 erase head. Price of the 2 track 45p per pair, 4 track 75p per pair. Pair mounted on plate 45p extra.

I R.P.M. MOTOR

Made by the famous Smiths Company. 240v. 50 cycle mains working. Ideal motor to drive clock mechanisms. Price £1 each or 10 for £9.

DRILL CONTROLLER

CONTROLLER
NEW IKW MODEL
Electronically changes
speed from approximately 10 revs. to
maximum. Full power at
all speeds by finger-tip
control. Kit includes all
parts, case, everything and
full instructions. \$1:50 plus
13p post and insurance.
Made up model also available, £2:25 plus 13p post & p.

MAINS OPERATED CONTACTOR

220/240v. 50 cycle solenoid with laminated core so very silent in operation. Closes 4 circuits each rated at 10 amps. Extremely well made by a German Elec-trical Company. Overall size 21 × 2 × 2in. £1.50 each.

CONTROL DRILL

SPEEDS



Uses differential comparator 1.C. with thermister as probe. Designer claims temperature control to within 1/7th of a degree. Complete kit with power pack £5-50

AUTO-ELECTRIC CAR AERIAL with dashboard control switch-fully extendable to 40in or fully retractable. Suitable for 12v positive or negative earth. Supplied complete with fitting instructions and ready wired dashboard switch. 25·75 plus 25p post and insurance.



WATERPROOF HEATING
ELEMERT
26 yards length 70W. Self-regulating
temperature control. 50p post free.

MULTI-SPEED MOTOR

MULTI-SPEED MOTOR
Replacement in many well-known
food mixers. Six speeds are available 500, 850 and 1,100 rp.m. from
either or both of the nylon sockets
(where the beaters of the food
mixer normally go) and 8,000,
12,000 & 15,000 rp.m. (ideal polishing speeds)
from the main drive shaft. This drive shaft is
j. in. diameter and approximately 1 in. long. A
further point about this motor is that being
230/240v. AC-DC series wound its speed may be
further controller. This is a very powerful and useful. controller. This is a very powerful and useful motor size approx. 2 in. dia. × 5 in. long, mains 230/240v. Price 88p plus 23p postage and insurance, 12 or more post free.

ISA ELECTRICAL PROGRAMMER



6

Learn in your sleep: Have radio playing and kettle boiling as you awake—switch on lights to ward off intruders you can do if you invest in an electrical programmer. Clock by famous maker with 15 amp. on/off switch. Switch on time can be set anywhere to stay on up to 6 hours. Independent 60 minute memory logger. A beautiful unit. Price £1-95 + 20p p & p or with glass front chrome bezel 75p extra.

0-8 AMMETER 2in. square full vision for flush mounting. Moving iron instrument. Ideal for charger. Price 60p each. 10 for 25-40,

NÚMICATOR TUBES For digital instruments, counters, timers, clocks, etc. Hi-vac XN. 3, Price 21-45 each. 10 for 213.

12 WAY SUB-MINIATURE
MULTI-CORE CABLE
7-0076 copper cores each core P.V.C. insulated and
of different colour. P.V.C. covered overall and
approx. 3/16in. tbick. Price 20p per yard. LIGHT CELL
Almost zero

Almost zero realstant in sun-light increases to 10 K Ohms in dark or dull light, epoxy resin sealed. Size approx. Im. dia, by Jin. thick. Rated at 500 MW, wire ended. 43p with circuit. Also ORP 12 light cell 45p.

BAKELITE INSTRUMENT CASE



MULLARD 4 + 4UNILEX AMPLIFIER



We demonstrate these daily and almost always a sale results; it really is a cracking amplifier. Only Mullard with their know how could have made it possible at this low price. SPEC.: Mains operated. 4 watts music or speech per channel. Double wired power supply eliminates cross talk. Harmonic distortion less than 2%. Frequency response 50hz-16Khz. Input suitable for pick-up tuner or microphone. 6 month guarantee. Only 28.95 + 30p postage and insurance.

THYRISTOR LIGHT DIMMER

For any lamp up to 200w. Mounted on switch plate to fit in place of standard switch. Virtually no radio interferences. Price \$2.95, plus 200 post and insurance.

TANGENTIAL HEATER UNITS

This heater unit is the very latest type, most efficient, and quiet running. Is as fitted in Hoover and blower heaters costing £15 and more. We have a few only. Comprises motor, impeller, 2k W. element and 1k W. element allowing switching 1, 2 and 3k W. and with thermal safety cut-out. Can be fitted into any metal line case or cabinet. Only need control switch. £3:50. 2k W. Model as above except 2 kilowatts £2:50. Don't miss this. Control Switch \$5p. P. & P. 40p

DISTRIBUTION PANELS

Just what you need for work bench or lab. 4×13 amp sockets in metal box to take tandard 13 amp sockets in metal box to take tandard 13 amp fused plugs and on/off switch with neon warning light. Supplied complete with 6 feet of flex cable. Wired up ready to work, 42.25 plus 23p P. & I.

_ THIS MONTH'S SNIP

BATTERY MOTORS A bargain parcel of 7 motors for \$1. Some not as large as a postage stamp and only \$\frac{1}{2}\$ thick, largest is \$1\frac{1}{2}\$ "\text{ li}" \text{ dia. Some work off \$1\frac{1}{2}\$ "\text{ some as high as \$1\frac{1}{2}\$". These motors are used in racing cars, power toys, etc. The largest is so powerful that it will dirive a Mini drill, model lathe, or similar. This is a 4 pole motor, optimum working \$16.5\times\$ but very powerful even as low as \$4\frac{1}{2}\$". Don't miss this wonderful snip.

A 14 4 4

REPEATING TIME SWITCH

1 or 2 on off per 24 hours. Repeats until re-programmedSwitches up to 15 amp. Switching time completely adjustable
through 24 hours. Precision made with 24 hour dlai. Miniature—will fit into 2ins. cube. Mains operated clock but
switch may be isolated for switching battery sets. Ideal
for: shop window lighting, anti-thief devices, central
heating control and many other automatic processes.
Price with instructions £2-50 each plus 20p post and insurance.

STANDARD WAFER SWITCHES

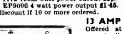
Standard size 11" wafer—silver-plated 5-amp contact standard I" spindle 2" iong-with locking washer and nut.

No. of Poles	2 way	3 way	4 way	5 way	6 way	8 way	9 way	10 way	12 way
1 pole	40p	40p	40p	40p	40p	40p	40p	40p	40p
2 poles	40p	40p	40p	40p	40p	40p	40p	70p	70p
3 poles	40p	40p	40p	40p	70p	70p	70p	95p	95p
4 poles	40p	40p	40p	700	70p	70p	70p	£1.20	£1-20
5 poles	40p	40p	70p	70p	95p	95p	95p	£1·45	£1-45
6 poles	40p	70p	70p	70p	95p		95p	£1.70	£1.70
7 poles	70p	70p	70p	95p	£1.20				
8 poles	70p	70p	70p	95p	£1-20	£1-20			£2-20
9 poles	70p	70p	95p	95p	£1·45				£2-45
10 poles	70p	70p	95p	£1.20	21-45	£1-45			£2-70
11 poles	70p	95p	95p	£1.20					£2-95
12 poles	70p	95p	95p	£1.20	£1.70	\$1.70	\$1.70	£3-20	£3·20

MULLARD AUDIO AMPLIFIERS

All in module form, each ready built complete with heat sinks and connection tags, data sup-

plied.
Model 1153 500m watt power output 75p.
Model 1172 750m watt power output 85p.
Model EP9000 4 watt power output 21-45.
10% discount if 10 or more ordered.





13 AMP TWIN GANG SOCKETS

13 AMP TWIN GANG SOCKETS
Offered at less than wholesale price your
opportunity to replace those dangerous
adaptors—brown bakelike tush mounting—
standard fitting. Unswitched 20p sach, we load
and with neon on/off indicators 40p each. Less
10% ten or more + 20p postage if order under
24-40

50 MICRO AMPMETER

Square, panel mounting type. \$2. INTEGRATED CIRCUIT DIAGRAM

A parcel of integrated circuits made by the famous Plessey Company. A once-in-a-lifetime offer of Micro electronic devices well below cost of manufacture. The parcel contains 5 ICs all new and perfect, first-grade device, definitely not sub-standard or seconds. 4 of the ICs are single silicon chip GP ampliflers. The 6th is a monolithle NPN matched pair. Regular price of parcel well over \$5. Full circuit details of the ICs are included and in addition you will receive a fits of many different IC's available at bargain prices 25p upwards with circuits and technical data of each. Complete parcel only \$1 post paid. DON'T MISS THIS TERRIFIC BARGAIN.

MULLARD I.F. MODULE

This is a fully screened intermediate frequency module for amplification and detection of f.m. signals at 10°AMIz and a.m. signals at 40°AHz. The first stage is used as an i.f. amplifier for f.m. and a self oscillating mixer for a.m. operation, in conjunction with an external oscillator coil. 85p each. 10 for 27.85. 100 for 282.50p. With connection dig.

Where postage is not stated then orders over £5 are post free, Below £5 add 20p, Semiconductors add 5p post. Over £1 post free. S.A.E. with enquiries please.



MINIATURE WAFER SWITCHES

2 pole, 2 way—4 pole, 2 way—3 pole, 3 way—4 pole, 3 way—2 pole, 4 way—2 pole, 4 way—2 pole 6 way—1 pole, 12 way. All at 20p each 21-80 for ten, your assortment.

TOGGLE SWITCH

amp. 250v. with fixing ring 71p each, 75p doz.

ROCKER SWITCH

13 amp self-fixing into an oblong hole. Size approximately 1° × 2° 6p each, 10 for 54p.





Slide Switch. 2-pole changeover panel mounting by two 6 B.A. screws. Size pprox. lin x fin rated 250V lamp. 6p each. 10 for 54p, 100 for 25-10, 500 for £24.

MICRO SWITCH

5A changeover contacts. 9p each. £1 doz. 15 amp Model each or £1.05 doz

NEED A SPECIAL SWITCH?

Double Leaf Contact. Very slight pressure closes both contacts. 6p each, 60p doz. Plastic pushrod suitable for operating 5p each, 45p doz.

PRESSURE SWITCH

PRESSURE SWITCH
Containing a 15 amp. change over
switch operated by a disphragm
which in turn is operated by air
pressure through a small metal
tube. The operating pressure is
adjustable but is set to operate in
approx. 10 in. of water. These are quite low
pressure devices and can in fact he operated
simply by blowing into the inlet tube. Original
use was for waehing machines to turn off water
when tub has reached correct level but no doubt
has many other applications.
\$1.50 each.

SWITCHES ???

We could fill this whole page with all the switches we have so if you can't see the one you want send for our switch list.

TIMED "ON" SWITCHES

TIMED "ON" SWITCHES
Made by Smiths for washing machines, etc.
Centre spindle closes double pole 15 anp switch
directly it is turned. A full 360° turn or only a
part turn winds the clockwork mechanism and
keeps the switch closed until the spindle returns
to the "Off" position. A dial therefore could be
fitted to indicate hours and minutes and the
switch on period could be set quite accurately.
3 models available—90 minutes, 120 minutes and
360 minutes. Price 95p each. Metal clad pointer
knob 15p. Suitable relay to make the switch
"on" instead of "off" 35p.
LEYER SWITCH—RAS H59/4

LEVER SWITCH—Ref. H52/4
Ideal for intercom or similar. Pressing the lever down operates 6 pairs of change-over contacts, pressing the lever up operates 4 pairs of change-over contacts. The switch is spring loaded and normally returns to the off or centre position. Size approximately 1½" long × 2½" deep × ½" thick. 40p each.

thick. 40p each.

5 PUSH BUTTON SWITCHES
Mains, suitable for audio or R.F. Each switch
rated at 250v. 15 amps. 1st (black push button)
closes 2 circuits, 2nd (white push button) operates
one change-over, 3rd (white push button) operates
one change-over, 4rd (white push button) operates
one circuit. Note: all depressed buttons remain
down until cleared by the 5th (red button).
Further note: It is a relatively easy job to alter
the position of the tags thus making the switches
suit your circuit. Fitted with 3 white, 1 red and
1 black button. 30p each or 10 for \$2.70.
PUISH OPERATED MICROSWITCH

PUSH OPERATED MICROSWITCH Change-over contacts, spring return when plunger released. Also fitted with lamp holder to take Lilliput lamp in plunger; fixing is by locknut, through if hole. Price 25p each or 10 for 42-25. 22-POSITION SOLENOID OPERATED

STUD SWITCH

STUD SWITCH
Mains operated, each current pulse to switch
solenoid moves switch arm through one position
on to the next contact stud—current to release
solenoid brings back switch arm to position one.
These are ex-equipment but in good working
order. Any not so would be replaced. Price 50p each.

SNAP ACTION SLIDE SWITCH

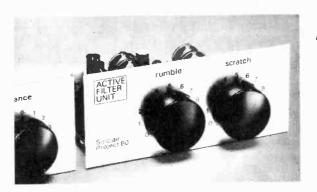
Rated 5a. 240v. Made by Arrow. Type fitted in the handles of electric drills, vacuums, etc. 5p each. 10 for 45p.

NOTE: All items subject to 10% discount on quantities of 10 or more

J. BULL (ELECTRICAL) LTD.

(Dept. P.W.) 7 Park Street, Croydon CRO IYD Callers to: 182/3 Tamworth Road, CROYDON

Sinclair Project 60



Active Filter Unit

(A.F.U.)

Built and tested post free

£5.98

The value of an efficient filtering system cannot be over emphasized in these days of very high quality reproduction since there are so often occasions where its use can mean the difference between comfortable and uncomfortable listening. On the low pass side the Sinclair A.F.U. will effectively reduce hiss from radio or tape, cut out heterodyne whistles on A.M. reception, greatly reduce record surface noise and other imperfections; on the high-pass side it will cut out motor rumble and other spurious low frequency intrusion. The unit is for use between pre-amp (including tape pre-amps) and power amplifiers, and operates in two sections, both stereo. The cut-off frequencies are continuously variable, and since attenuation in the rejection band is rapid (12dB/octave) there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The A.F.U. is as easy to mount as the stereo 60 pre-amp/control unit which it matches in styling, along with the Stereo

SPECIFICATIONS

The A.F.U. employs two Sallen and Key type active filter stages, one rumble (high pass) and one scratch (low pass). The two stages use complementary transistors to minimise distortion.

Supply voltage: 15 to 35 volts. Current

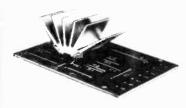
Gain at 1kHz: Filters flat 0.98 (—0.2 dB)

HF cut off: (—3dB) variable from 28 kHz
to 5 kHz at 12 dB/octave.

LF cut off: (—3dB) variable from 25Hz to 100Hz at 12dB/octave.

Distortion: at 1kHz (35 volt supply) 0.02% at rated output

Super IC.12 Integrated circuit high fidelity amplifier



Having introduced Integrated Circuits to hi-ficonstructors with the IC.10, the first time an IC had ever been made available for such purposes, we have followed it with an even more efficient version, the Super IC.12, a most exciting advance over our original unit. This needs very few external resistors and capacitors to make an astonishingly good high fidelity amplifier for use with pick-up, F.M. radio or small P.A. set up, etc. The free 40 page manual supplied, details many other applications which this remarkable IC. make possible. It is the equivalent of a 22 tranker possible. It is the equivalent of a 22 tranker possible.

sistor circuit contained within a 16 lead DIL package, and the finned heat sink is sufficient for all requirements. The Super IC.12 is compatible with Project 60 modules which would be used with the Z.50 and Z.30 amplifiers. Complete with free manual and printed circuit board.

SPECIFICATIONS

Output power: 6 watts RMS continuous (12 watts peak). 6-80. Frequency Response: 5Hz to 100KH2±1dB. Total Harmonic Distortion: Less than 1%. (Typical 0-1%) at all output powers and frequencies in the audio band (28V). Load Impedance: 3 to 15 ohms. Input Impedance: 250 Kohms nominal. Power Gain: 90dB (1,000,000,000 times) after feedback. Supply Voltage: 6 to 28V. Quiescent current: 8mA at 28V. Size: 22×45×28mm including pins and heatsink.

Manual available separately 15p post free.

With FREE printed circuit board and 40 page manual.

£2.98 Post free

Project 605



The easy way to buy and build Project 60

Project 605 is one pack containing: one P25 two Z30's, one Stereo 60 and one Masterlink. This new module contains all the input sockets and output components needed together with all necessary leads cut to length and fitted with neat little clips to plug straight on to the modules. Thus all soldering and hunting for the odd part is eliminated. You will be able to add further Project 60 modules as they become available adapted to the Project 605 method of connecting.

Complete Project 605 pack with comprehensive manual, post free £29.95

Everything you need to assemble a superb 30 watt high fidelity stereo amplifier without having to solder.

Sinclair Radionics Ltd, London Road, St. Ives, Huntingdonshire PE17 4HJ, Tel: St. Ives 64311

the world's most advanced high fidelity modules

PZ.5 30 volts unstabilised £4.98 PZ.6 35 volts stabilised PZ.8 45 volts stabilised (less mains transformer) PZ.8 mains transformer

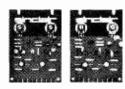
Z.30 & Z.50 power amplifiers

Built, tested and guaranteed with circuits and instructions manual z.30 £4.48 z.50 £5.48

The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to provide unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at 15w (8Ω) and all lower outputs. Whether you use Z 30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and are intended for use principally with other units in the Project 60 range. Their performance and design are such, however, that Z.50s and Z.30 may be used in a far wider range of applications.

SPECIFICATIONS (2.50 units are interchangeable with 2.30s in all applications).—Power Outputs: 2.30 15 watts R M.S. into 8 ohms using 35 volts. 20 watts R M S. into 3 ohms using 30 volts. 2.50 40 watts R M.S. into 3 ohms using 40 volts. Sold volts. 8 watts R M.S. into 8 ohms using 50 volts. Frequency response: 30 to 300,000 Hz: 1dB Distortion: 0.02% into 8 ohms. Signal to noise ratio: better

than 70dB unweighted. Input sensitivity: 250mV into 100 Kohms (for 15w into 8 Ω). For speakers from 3 to 15 ohms impedance Size: 14 x 80 x 57mm.



Stereo 60 Pre-amp/control unit

Designed specifically for use on Project 60 systems, the Stereo 60 is equally suitable for use with any high quality power amplifier. Since silicon epitaxial planar transistors are used throughout, a really high signal-to-noise ratio and excellent tracking between channels is achieved. Input selection is by means of press buttons, with accurate equalisation on all input channels. The Stereo 60 is particularly

SPECIFICATIONS—Input sensitivities: Radio – up to 3mV. Mag. p.u. 3mV correct to R.I.A.A. curve : 1dB 20 to 25,000 Hz. Ceramic p.u. – up to 3mV. Aux.—up to 3mV. Output: 250mV. Signal to noise ratio: better than 70dB. Channel matching: within 1dB. Tone controls: TREBLE+12 to —12dB at 10KHz. BASS + 12 to —12dB at 100Hz Front panel: brushed aluminium with black knobs and controls. Size: 66 x 40 x 207mm.



Ruilt and tested. Post free

Built, tested and quaranteed

£9.98

Project 60 Stereo F.M. Tuner

The phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio. Now, Sinclair have applied the principle to an F.M. tuner with fantastically good results. Other advanced features include varicap diode tuning, printed circuit coils, an LC, in the specially designed stero decoder and switchable squelch circuit for silent tuning between stations In terms of high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with most other high fidelity systems

SPECIFICATIONS—Number of transistors: 16 plus 20 in IC Tuning range: 87.5 to 108MHz. Sensitivity: 7μV for lock-in over full deviation. Squelch level: Typically 20μV. Signal to noise ratio: >65dB. Audio frequency response: 10Hz = 15KHz (: 1dB). Total harmonic distortion: 0.15% for 30% modulation. Stereo decoder operating level: 2μV. Cross talk: 40dB. Output voltage: 2 x 150mV.R.M.S. maximum. Operating voltage: 25–30VDC. Indicators: Stereo don, tuning. Size: 93 x 40 x 207mm.



Power Supply Units

Designed specifically for use with the Project 60 system of your choice. Use PZ.5 for normal Z.30 assemblies and PZ 6 or PZ.8 where a stabilised supply

Typical Project 60 applications

System	The Units to use	together with	Units cost
Simple battery record player	Z.30	Crystal P.U., 12V battery volume control, etc.	£4.48
Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control, etc.	£9.45
12W RMS continuous sine wave stereo amp for average needs	2 x Z.30s, Stereo 60; PZ.5	Crystal, ceramic or mag P.U., F.M Tuner, etc.	£23.90
25W. RMS continuous sine wave stereo amp. using low efficiency (high performance) speakers	2 x Z.30s, Stereo 60; PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner, Tape Deck, etc.	£26.90
80W. (3 ohms) RMS continuous sine wave de luxe stereo amplifier. (60W. RMS into 8 ohms)	2 x Z.50s, Stereo 60; PZ.8, mains transformer	As above	£34.88
Indoor P.A	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43
F.M. Stereo Tuner (£25) & A	F.U. (£5.98) may be	added as required.	





Guarantee

If, within 3 months of purchasing any product direct from Sinclair Radionics Ltd., you are dissatisfied with it, your money will be refunded at once. Many Sinclair appointed Stockists also offer this same guarantee in co-operation with Sinclair Radionics Ltd.

Each Project 60 module is tested before leaving our factory and is guaranteed to work perfectly. Should any defect arise in normal use, we will service it at once and without any charge to you, if it is returned within two years from the date of purchase. Outside this period of guarantee a small charge (typically £1.00) will be made. No charge is made for postage by surface mail. Air Mail is charged at cost.

SINCLAIR RADIONICS, ST IVES, HUNTING	DONSHIRE PE17 4HJ
Please send renclose cash/cheque/money order.	
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Address	PW 12/72

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The T.V. Graveyard of the North, as seen on T.V. Telewrecks. Close to the Motorway, plenty of Free Parking Space. Call in and see us any day 9-6. Closed Sunday. Est. 1935.

Speakers Ex T.V, Sets. 7 x 4", 6 x 4", 8 x $2\frac{1}{2}$ ", all 3 ohm P.M. 25p each. Post on any Speaker 10p.

Complete Untested T.V. Sets with all Valves and Back. BBC1 and ITV. 17" 90° Tube £2. 17" 110° Tube £3. 19" Slim £5. Carriage and Ins. £1.50p.

We are now breaking up many Stimline Sets. Send S.A.E. and please quote Model and Serial Number and part you require.

Reclaimed T.V. Tubes. All with 12 months' Guarantee. AW43/88 £1·50p. AW43/89 £1. Many other Types in Stock. Carriage and Ins. on any Tube £1·50.

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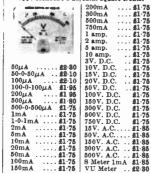
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2N2614 80p 2M4284 2N2646 40p 2N4285	42p AD149 17p AD150 17p AD161 17p AD162	62p BD131 75p GET897 22p O 85p BD132 80p GET898 22p O	C204 40p 600 PI	V 2A 45p 100 PIV 6A 55p	10C2 50p EF39 50p UCC84 49p 10F1 75p EF40 50p UCC85 40p 10P13 60p EF41 65p UCC80 55p 10P14 \$1:10 EF42 70p UCH21 60p
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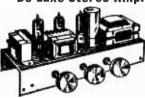
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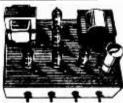
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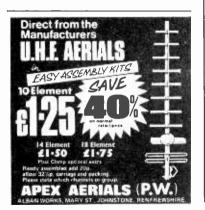
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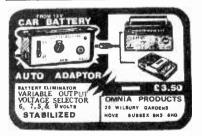
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3A4 0.45	6BS7 1.35	6K7 0.43			90C1 0.75	DY87 0.88	ECF80 0.35	ELL80	0.75	PCC806 0.95	PY500 1.00	UCL81 0.60
8A5 0.75	6BW6 0.90	6K8G 0.45	12AU6 0.45			E88CC 0.70	ECF82 0.85		1.00	PCF80 0.80	PY800 0.47	UCL82 0.85
3BP1 8.50	6BW7 0.90	6K25 0.75	12AU7 0.33	30FL1 0.80		E180F 1.00	ECF8041.65		0.80	PCF82 0.35	PY801 0.50	UCL83 0.85
384 0.40	6BX6 0.25	6L6GT 0.55	12AV6 0.45	30FL12 1.10	807 0.50				0.45	PCF84 0.60	PZ30 0.88	UF9 0.65
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5U4G 0.40	6C5GT 0.55	6LD20 0.50	12AY7 0.75	30L15 0.95	5649 0.70	EAF42 0.60	ECH84 0.45		0.50	PCF801 0.50	QQV03-10	UF42 0.65
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	1.80	6P28 0.65	12BA7 0.50	30P19 0.95	6146B 2.50	EBC81 0.88	ECL82 0.85		0.70	PCF805 0.90	QQV03-20A	
5Z3 0.75		6Q7 0.50	12BE6 0.50	30PL1 0.95	6360 1.25	EBF80 0.40	ECL83 0.70	EN91	0.40	PCF806 0.75	5.25	UF85 0.40
5Z4G 0.45	6CG7 0.60		12BH7 0.50	30PL13 1.10	6939 2.25	EBF83 0.40	ECL84 0.55	EY51	0.40	PCF808 0.90	TT21 8.40	UF89 0.40
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	6DO6B 0.75	6U5G 0.75	20P4 1.10	35Z3 0.75	CBL1 0.90	ECC35 1.00	EF85 0.35		0.28	PCL801 0.95	U78 0.40	W729 0.75
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	2N 3391	0.17	A8Z 18	0.75	OC42	0.20				
	2N3393	0.15	ASZ20	0.25	OC44	0.15				
	2N3394	0.15	A8Z21	0.40	OC45	0.12				
	2N3395	0.20	BC107	0.10	OC70	0.10				
	2N3402	0.15	BC108 BC109	0.10	OC71 OC72	0.12				
	2N3403	0.15	BC113	0.10	OC72	0.12				
	2N3404 2N3414	0.32	BC118	0.20	OC75	0.30				
	2N3415	0.15	BC134	0.20	OC76	0.15				
	2N3417	0.25	BC147	0.10	OC78	0.25				
	2N3702	0.10	BC148	0.10	OC78D	0.20				
	2N3703	0.10	BC149	0.12	OC81	0.20				
	2N 3704	0.12	BC152 BC158	0.15 0.15	OC81D	0.20				
	2N3707	0.12	BC175	0.15	OC83 OC139	0.30				
	2N3709 2N3710	0.10	BC186	0.25	OC140	0.35				
Ĺ	2N3819	0.35	BCY30	0.25	OC141	0.60				
ŀ	2N3906	0.25	BCY31	0.30	OC170	0.25				
	28702	0.50	BCY33	0.25	OC171	0.25				
	28746	0.25	BCY34	0.30	OC200	0.30				
	ACI13	0.15	BCY72	0.15 0.30	OC201	0.60				
ı	AC125	0.80	BCZ10	0.30	OC202 OC203	0.65				
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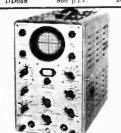
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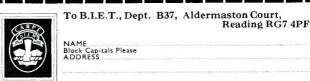
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