PRACTICAL WIGUST 1971 20p

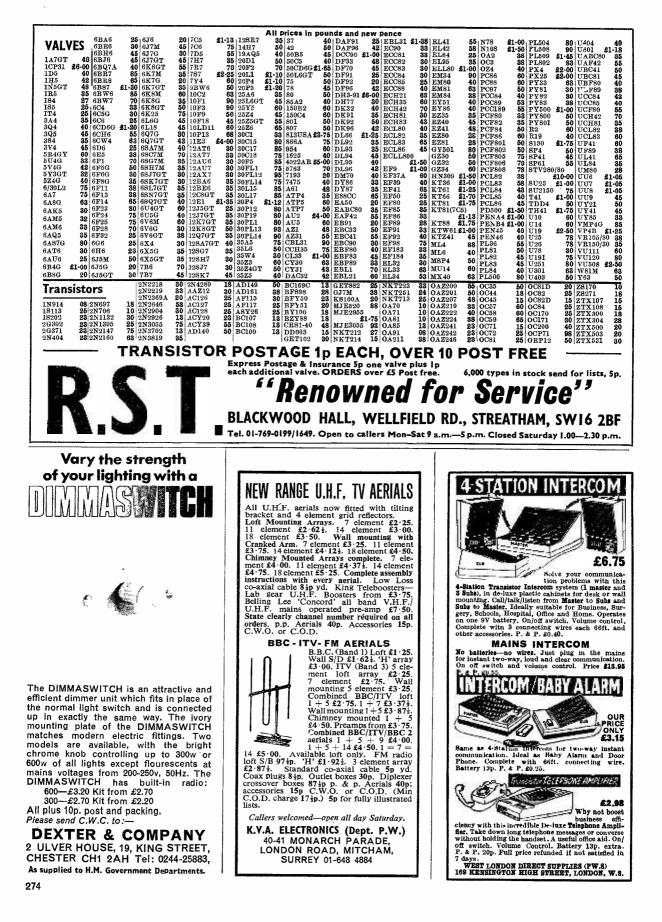
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Total £59.00 Available complete for only £52.00 + £2.50

SPECIFICATION

14 watte per channel into 3 to 4 ohms. Total distortion Available complete for only £49.00 + £2.50 9 10W @ 1kHz oils Advantage into 3 to 4 onms. Jora distortion @ 10W @ 1kHz oils. Advantage into 3 Meg. PU2 4mV @ 1kHz into 47K equalised within ±1dB R1AA. Radio 150mV into 220K. (Sensitivities given at full power.) Tape out facilities; headphone socket, power out 250 mW per channel. Tone controls and the power out 250 mW per channel. Tone controls and filter characteristics. Bass: + 12 dB to - 17 dB @ The characteristics bass + 12 bits -12 bits -12 bits -12 bits -12 bits -12 bits -12 dB (m) 60HZ bass filter: 64B per octave cut, Treble control, treble + 12 dB to -12 dB (m) 12 kHZ, Treble filter: 12 dB per octave. Signal to noise ratio (all controls at max) RT101 - P.U.1. & radio - 65dB, PU 2.2 + 58 dB, RT100 same as RT101 but P.U.2. 450 mV into 3 Meg Concerted to be an experimental formation of the second Cross talk better than -- 35dB on all inputs. Overload characteristics 26dB on all inputs. Size 132"×9"×32"

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As System 1, but with 2 x Duo Type III speakers at pair £32.00+ £3 p&p Available complete for £69 + £4 p&p

SYSTEM

Viscount III Amplifier BT100 £17.00 + 90p p&p 2xDuo Type II speakers, pair £14.00 + £2 p&p Garrard SP25 Mk 411 with CER, diamond pap cartridge, plinth and cover £21.00 + £1 pap

Total £52.00

Dato

SPEAKERS Duo Type-II Size 17" x 10%" x 6%". Drive unit 13" x 8" with parasitic tweeter. Max. power 10 watts, 3 ohms. Teak veneer cabinet, £14 pair + £2 p&p, Duo Type III Sizè 234 "x 114" x 94", Drive unit 131"x84" with H F speaker Max. power 20 watts at 3 ohms. Frequency range 20Hz to 20kHz. Teak veneer cabinet £32 pair + £3 p&p.





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the quality and power you need. Output Power: 45 watts R.M.S. (Sine wave drive). Frequency response: -3dB points 30Hz at 18KHz. Total distortion: less than 2% at rated output. Signal to noise ratio: better than 60dB. Speaker Impedance: 3, 8 or 15 ohms. Bass Control Range: \pm 13dB at 60Hz. Treble Control Range: \pm 12dB at 10 KHz. Inputs: 4 inputs at 5mV into 470K. Each pair of inputs controlled by separate volume control. 2 inputs at 200mV into 470K. To protect the output valves, the incorporated fail safe circuit will enable the amplifier to be used at half power. SPEAKERSI Size 20" \times 20" \times 10" incorporating 12" heavy duty 25 watt high flux, quality loudspeaker with cast frame. Cabinets attractively finished in two tone colour scheme—Black and grey.

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See previous page for address

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Output 10 watts. Output impedance—3 to 4 ohms. Inputs 1. -xtal mic 10mV Tone Controls—Treble control range ± 12dB at 10KHz. 2. -gram/radio 250mV. Bass control range ± 13dB Output 10 watts.

Frequency Response—(with tone controls central) Minus 3dB points at 20Hz and 40KHz. Signal to Noise Ratio—better than -60dB. Transistors—4 silicon Planar type and 3 Germanium type. Mains input—220/250V. A.C. Size of chassis—10§in. x 4§in. x 2§in. For use with Std. or L.P. records, musical instruments, all makes of pick-ups and mikes. Built and tested.



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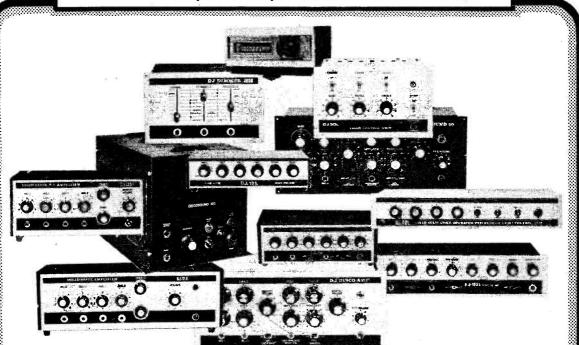
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AF116 25p BFX29 25p £1.00 AF117 25p BFX30 25p TIP34A	Type P.I.V. 1-49 50+ 100+ 500+1000+ 10 Watt Stud Mounting 5%	1000 + 13p 0C/2 Mullard 25p
AF118 62p BFX37 82p £2.00 AF124 25p BFX84 25p TIS43 40p	PL7001 50 20p 18p 17p 16p 14p All voltages $5:1-100V$. 40p each. PL7002 100 20p 18p 18p 17p 15p $25+37p;100+35p$. Any one type. PL7003 200 $22p$ 20n 16p 18p 18p	0C20 97p 100 + 17p 500 + 15p Mullard 100v 1000 + 13p
AF126 17p BFX86 25p TIS61 25p AF127 17p BFX87 25p TIS62 27p	PL/004 400 25p 23p 21p 20p 18p PL/005 600 26p 24p 23p 22p 20p TRIACS	25 + 85p 100 + 80p 500 + 75p 0C83 25p
AF139 30p BFX88 20p ZTX107 15p AF178 47p BFY18 30p ZTX108 15p AF179 65p BFY50 99p ZTX300 12p	PL7007 1000 30p 28p 26p 24p 22p Type Volts rent 1-49 50+ 100+	25 + 20p
AF180 52p BFY51 20p ZTX301 15p AF181 42p BFY52 22p ZTX302 20p	SC35A 100 3 amps 90p 75p 65p FOTTED BRIDGE RECTIFIERS SC35B 200 3 amps 95p 80p 70p (SILICON) SIZE i x i x ins. SC35D 400 3 amps 91:00 35p	25 + 15p 500 + 15p
AF186 40p BFY53 17p ZTX303 20p AF239 40p BFY59 65p ZTX304 25p ASY26 25p BSX20 17p ZTX500 20p	Cur- Type P.I.V. rent 1-49 50+ 100+ 500+ SC40B 200 6 amps £1.20 £1.00 85p	100 + 13p 500 + 11p 1000 + 10p 0C84 25p
ASY27 32p BSX21 20p ZTX501 25p ASY28 25p BSX76 15p ZTX502 25p	1002 100 2 amps 60p 55p 50p 45p 8C40D 400 6 amps 81.25 81.10 21.00 2002 200 2 amps 70p 65p 60p 55p 8C45A 100 10 amps 81.25 81.10 21.00 4002 400 3 amps 80p 75p 70p 65p 8C45A 200 10 amps 81.25 81.10 21.00	0CI 39 Mullard 25p 100 + 17p
ASY29 30p BSY95 15p ZTX503 20p ASY67 47p BSY95A15p ZTX504 40p ASZ21 42p BY100 15p ZTX531 30p	1004 100 4 amps 70p 60p 55p 50p SC45D 400 10 amps ±1.50 ±1.35 ±1.20 2004 200 4 amps 75p 70p 65p 60p SC50A 100 15 amps ±1.65 ±1.50 ±1.35	25 + 20p 500 + 15p 100 + 17p 1000 + 13p
BA116 7p BY126 15p BA164 10p 8Y127 20p DISCOUNTS	5002 600 2 amps 90p 80p 75p 70p SC50D 400 15 amps £2:00 £1:75 £1:60 6004 600 4 amps 80p 80p 75p 70p SC40E 500 6 amps £1:50 £1:25 £1:10	500 + 15p AF239 42p
BAX13 6p BY182 85p 10% 12+ BAX16 7p BY210 40p 15% 25+ BAY31 7p BY211 35p 20% 100+	1006 100 6 amps 75p 70p 65p 60p SC45E 500 10 amps £1.75 £1.50 £1.35 2006 200 6 amps 80p 75p 70n 65n SC50E 500 15 amps £2.25 £2.00 £1.75	OC81 Mullard 25p 25 + 35p 25 + 20p 100 + 30p 100 + 17p 500 + 25p
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N3394 15p 40050 55p BC182 121p BSX20 375p NK12/2 20p I watt 5%, 2p. B24 Series. R53 (S10) \$227f VX3/05 N3402 221p 40251 321p DEC183 121p BSX26 45p NK12/2 20p I watt 5%, 2p. K53 (S10) \$227f VX3/05 Post & Packing 121p per order. Europe 25p. Commonwealth (Air) 65p (MIN.) I watt 10%, 21p. 1W & 1W Mullard Thermistors also Matching charge (audio transistors only) 121p extra per pair. 2 watt 10%, 6p. E12 Beries. stock. Please enquire.	N3063 250 28104 250 N3064 500 28501 3821 N3056 750 28502 352 N3133 300 28503 271 N3135 250 3812 2803 N3135 250 3814 20 N3136 250 3N148 71 N3390 250 3N142 251 N3391 200 3N143 257 N3391 300 3N143 257 N3392 17, 30, 114 251	BC159 200 BFY7 571 BC160 821 BFY89 671 BC167 150 BFW59 851 BC1681 140 BFW59 851 BC1682 150 BFW60 251 BC1682 150 BFW29 81.81 BC1691 140 BPX29 81.81 BC1670 150 BFX39 474 BC1712 150 BSX19 174 BC172 150 BSX20 174	D NKT240 2719 TIS60 2219 D NKT241 2719 TIS61 250 D NKT242 200 TIS62 2719 D NKT243 6219 TIS62 2719 D NKT243 6219 TIF20A 500 D NKT244 1719 TIF20A 600 D NKT245 200 TIF31A 6219 D NKT261 200 TIF3A D NKT264 200 E103A D NKT264 200 E103A	HEAT SINKS 4:8 × 4 × 1 im Finned for Two TO-3 Trans., 4789 × 48 × 2 × 1 im Finned, For One Finned, For One 5247 Fixed. Finned, For TO-18, 1/- Finned. Finned, For TO-18, 1/- Finned. RESISTORS Carbon Film	Log. and Lin., with switch, 3 Wire-wound Pots (3W), 40p. Twin Ganged Stereo Pots, and Lin., 40p. PRESETS (CARBON) 0-1 Watt 6p OR 0-3 Watt 6p OR 0-3 Watt 7ip HORIZON THERMISTORS
Prices subject to alternation without prior instruction	N3394 15p 40050 55 N3402 221p 40251 321 Post & Packing 121p P Matching cha	BC182 $12 \pm p$ BSX21 87 ± 1 BC183 $12 \pm p$ BSX26 45 ± 1 er order. Europe 25 p. Comm ree (audio transistors only) 12 ± 1	p NKT272 20p p NKT274 20p ionwealth (Air) 65p (MIN.) p extra per pair. ior notice.	1 watt 5%, 1p. E24 Scries. 1 watt 5%, 2p. 1 watt 10%, 2p. 2 watt 10%, 6p. E12 Series.	K151 (1k) 1217 Mullard Thermistors also stock. Please enquire.



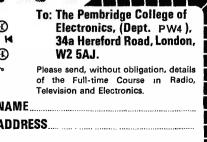
Train for tomorrow's world in Radio and Television at The Pembridge College of Electronics Your first day on Television: 7th September, 1971



This is your opportunity to train as a television and radio engineer on our full-time 2 year College Diploma Course. That is the way to get into a rapidly growing industry with a tremendous demand for skilled technicians. You will be given theoretical and practical instruction on colour television receivers, following a syllabus specially designed to cover the new City and Guilds Radio, Television and Electronic Technicians' Course.

> Minimum entrance requirements are Senior Cambridge or 'O' Level, or equivalent in Mathematics and English.

Complete the coupon below and we will send you the details about training for an exciting, new career.



HEARING AID AMPLIFIERS (Ex behind ear deaf aids) & transistors on tiny PA. board with volume control—whole thing only about haif as big as Oxo cube. £1.75 or with sub-miniature microphone and L.S. attached \$3.50.



CONTROL

DRILL

SPEEDS

MAINS OPERATED SOLENOIDS

Model 772-small but power-ful & pull-approxiste 11⁴ x 11⁴ x 14⁴ 60t. Model 400/1 & pull Size 24⁴ x 2⁴ x 14⁴ 755. Model TT10 11⁴ pull Size x x 24⁴ x 24⁴-8180 Plus 200 post and insurance. BEST QUALITY BRITISH MADE ELECTRICAL PLUGS AT APPROX.

HALF PRICE 15 amp 3 pin 10p each or ten for 90p, 5 amp 3 pin 8p each or ten for 70p, 5 amp 2 pin 5p each or ten Sp each for 45p.

DRILL CONTROLLER NEW IKW MODEL Electronically changes speed from approxi-mately 10 revs. to maximum. Full power at maximum. Full power at all speeds by finger-tip control. Kit includes all parts, case, everything and full instructions. £1.50 plus 13p post and insurance. Made up model also avail-able, £2.55 plus 13p post & p. MAINS MOTOR Precision made. = as

Precision made --- as used in record decks used in record decks and tape recorders— ideal also for extractor fan, blower, heaters, etc. New and perfect. Snip at 50p. Postage 15p for first one then 5p for each one ordered 5p order

NEED A SPECIAL SWITCH?

2.

NEED A SPECIAL SWITCH! Double Lest Contact. Very slight pressure closes both contacts. 6p each. 60p doz. Plastic push-rod suitable for operating, 6p each, 45p doz. MINIAT URE WAFER SWITCHES 2008 2 war 4 pole. 2 war

2 pole, 2 way-4 pole, 2 way-3 pole, 3 way-4 pole, 3 way-2 pole, 4 way-3 pole, 4 way-2 pole 6 way-1 pole, 12 way. All at 18p cach, \$1.80 dozen, your assortment

WATERPROOF HEATING ELEMENT 26 yards length 70W. Self-regulating temperature control. 50p post free.

MICRO SWITCH

MICRO SWITCH 5 amp. changeover contacts, 9p each, 51 doz. 15 amp. on/off 10p each, 10 for 51.36. MAINS OPERATED CONTACTOR 220/240v, 50 cycle solenoid with laminated core so very silent in operation. Closes 4 circuits each rated at 10 amps. Extremely well made by a ferman Electrical Company. Overall size 24 × 2 × 2in. 81 each.

£1 each PAPST MOTORS

PAPST MOTORS Est. 1/40th h.p. Made for 110-120 volt working, but two of these work ideally together off our standard 240 volt mains. A really beautiful motor, extremely quiet running and reversible. **21**:50 each. Postage one 23p, two 330.



EXTRACTOR FAN Cleans the air at the rate of Buitable for kitchens, bath-rooms, etc., its so quiet it car casing with 3¹ fan blades blades, sheet steel casing, pull switch, mains connector, and hardly brackcts, \$2 plus 36p post and ins. MAINS TRANSISTOR POWER PACK EXTRACTOR FAN

PACK

Designed to operate transistor sets and amplifiers. Designed to operate transistor sets and ampliners. Adjustable output 6v., 9v., 12 volts for up to 500mA (class B working). Takes the place of any of the following batteries: PP1, PF3, PF4, PF6, PF7, PF9 and others. Kit comprises: mains transformer rectifier, smoothing and load resistor, condensers and instructions. Real snip at only 83p, plus 13p postage. 24V BUZZER. Mode by CEC in brown heavy bakelite case.

24V BUZZER. Made by G.E.C. in brown heavy bakelite case, these work off AC mains through step down transformer. Price 40p each. 9 PIN PLUG AND SOCKET.

Suitable for connecting multicore flexer to equip-ment. Socket size approx. ^{3"} diameter. Plug size 9/10" diameter with flex entry. 25p pair.

OUT OF SEASON BARGAIN TANGENTIAL HEATERS



TANGENTIAL HEATERS Once again we are able to make a special bargain offer of these very popular heating units. Tangential heaters although brought out a few years ago are still the latest and best type as nothing has yet been made which could be called an improvement on them. The Tan-gential unit is still the only one used in good quality heaters made by Hoover, G.E.C. and all the famous names. The unit comprises quiet running AO induction motor with special bear-switching half and full heat in the case of the 2 k.w. and one third—two thirds and tr" heat in the case of the 2 k.w. and one third—two thirds and tr" heat in the case of the 3 k.w. These heaters are also flited with a safety cutout to cut the heaters should the impeller stop of the air flow be impeded. They are free standing and need only the simplest of cases, even a wooden cabinet is suitable or the plinth of the kitchen cabinet, Lots of customers missed our special Summer offer of these heaters inter years order early. 200/240 2 k.w. model **25**:00.200/240 3 k.w. model **25**:60. Control switch heaters only **25p** or two-heat, cold-blow and off **35p**. Postage and insurance **35p** on heaters.

	STAP	10.4				ится			
Standard size	e 14 wa	fer-s	lver-pl	ated 5-	amp co	ontact,	standa	rd ≩″ :	spindle
2" long-wit	h locki	ng wa	sher ar	id nut.					
No.	2	3	4	5	6	8	9	10	12
of Poles	way	way	way	way	way	way	way	way	way
1 pole	40p	40p	4Óp	40p	40p	40p	40p	40p	40p
2 poles	40p	40p	40p	40p	40p	40p	40p	70p	70p
3 poles	40p	40p	40p	40p	70p	70p	70p	95p	95p
4 poles	400	40p	40p	70p	70p	70p	70p	£1.20	£1 20
5 poles	40p	40p	70p	70p	95p	95p	95p	£1.45	£1.45
6 poles	40p	700	70p	70-0	95p	95p	95p	£1.70	£1 70
7 poles	700	705	70 0	95p	£1.20	£1.20	£1-20	£1.95	£1.95
8 poles	70p	700	70p	95p	£1.20	£1·20	£1-20	£2-20	£2.20
9 poles	70p	70p	95 0	95 [°] D	£1.45	£1.45	£1.45	£2·45	£2·45
10 poles	70p	700	950	£1.20	£1.45	£1·45	£1 45	£2.70	£2 70
11 poles	70p	95p	95p	£1.20	£1 70	£1.70	£1.70	£2-95	£2·95
12 poles	70p	95p	95p	£1.20	£1.70	£1.70	£1.70	£8 20	£3·20
						-	_		

AMPLIFIER MAINS TRANSFORMER

50v 1[±] amp. Upright mounting with fixing brackets and metal shrouds to contain magnetic field, 50 c/s primary, tapped 110v, 117v, 210v, 230v and 250v. 2 secondaries, one 50v 1[±] amp. other 6v 1 amp for pilot light, etc. **£1:95**, postage 300

THIS MONTH'S SNIP BATTERY CONDITION TESTER



BATTERY CONDITION IESIER Made by Mallory but suitable for all batteries made by Ever Ready and others, most of which are zinc carbon types but also mercury manganese-nicad-silver oxide and aikaline batteries may be tested. The tester puts a dummy load on the battery and the meter scale indicates the condition depending upon which section the pointer rests. The section reads "replace" "weak" or "good". The tester is complete in its case, size 34" x 64" x 2" with leads and prods. Price \$1.75 plus 20p postage.

COMPUTER TAPE

2.400 ft. of the best magnetic tape money can buy. Almost unbreakable and on a metal computer spool. Users have claired successful results with video as well as sound recordings 1' wide \$1, \$7 \$80, \$750, \$P\$. & \$P\$. 330 extra. Spare spools 500 each. Nasette to hold spool 500 each. No extra postage if ordered with tape, otherwise 300 extra.

CAPACITOR DISCHARGE IGNITION SYSTEM

Well proved that it helps starting and increases petrol economy. Also increases acceleration but saves contact wear. For details see Practical Wireless June. Gives optional capacitor or standard ignition at the flick of a switch. Price **24:95**

MICROSONIC KEYCHAIN RADIO

7 transistor Keychain Radio in very pretty case, size 21×21×14in.—complete with soft ieather zipped bag. 7 transistor, ferrite rod. Loudspeaker.

Loudspeaker. In transit from the East these sets suffered corrosion as the batteries were left in them but when this corrosion is cleared away they should work-offered without guarantee except that they are new. Frice only **£1.25** less batteries plus **13**9, post f for **£7** post free Pair of rechargeable batteries and charger **85p**.

Special this month are some single, double and treble pole changeover relays. Contacts rated at 15 amps. Operating coil wound for 240V. A.C. Good British

Make, Unused, Size	approx, 17	V T
Open construction		
Single pole	25p each	
Double pole	32p each	
Treble pole	40n each	
TTEDIe Pole	Tob outon	

4 AMP VARIAC CONTROLLERS

With this you can vary the voltage applied to your circuit from zero to full mains without generating undue heat. One obvious application therefore is to dim lighting. Ex equipment but little. used-as good as new offered at approx. half price. £5 plus 75p. post and ins.

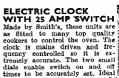
OVEN THERMOMETER WITH ALARM



UVEN THERMOMEIER WITH ALARM Basically this is a thermometer which is calibrated between 500 and 900 deg. C using a sensor on a flerible lead. The second feature, however, is an alarm which can be set anywhere within the temperature range. When the temperature is reached a buzzer sounds. Fresumably the buzzer could be replaced by a relay or contactor to work another device. Limited quantity only of these units, price **33**:50, includes thermometer --scale--sensor and buzzer.

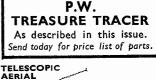
Where Postage is not stated then orders over £5 are post free. Below £5 add 20p. Semi-conductors add 5p post. Over £1 post free, S.A.E. with enquiries please.







tremely accurate. The two small dials enable switch on and off times to be accurately set. Ideal fraction of the regular price-new and unused only \$2, less than the value of the clock alone— post and insurance 14p.





also available same price. Jug heater \$1.50 plus p. & p. 14p.

THYRISTOR LIGHT

DIMMERS Will dim incandescent lighting up to 600 watts from full brilliance to out. Assembled and wired ready to install **\$3**.



12 VOLT 14 AMP POWER PACK

G



REED SWITCHES Class encased, switches operated by external magnet-gold welded contacts. We can now offer strues

Class encased, switches operated by external magnet-gold welded contacts. We can now offer stypes: Minneter, Will make and break up to iA up to 500 volts. Price 139 each. \$1:20 dozn. Standard. 2in long x 3/16in. diameter. This will break currents of up to 1A, voltages up to 250 volts. Price 109 each. \$09 per dozen. Flat. Flat type, 2in. long. Just over 1/16in. thick, approximately jin. wide. The Standard Type flattened out, so that it can be fitted into a smaller square solenoid. Rating 1 ann 200 volts. Price 309 each. £3 per dozen. Small ceramic magnets to operate these reed switches 3p each. 90p per dozen. PULSH RUTTON CHANGE OVER

PUSH BUTTON CHANGE OVER

SWITCHES

SWITCHES This is a Honeywell micro witch mounted on a metal frame with spring loaded plunger to operate. Panel hixing by single ?" hole. single Changeover switch Sig each or ten for \$2:5, 2 changeover switch operated by single Plunger 35p each or ten for \$2:15, 3 change-over switches 45p each or ten for \$2:05.



METER BOX

Designed to take $3\frac{1}{2}$ flush mounting meter. This has a $2\frac{1}{2}$ diameter hole with 3 meter fixing holes. (verall size of box $4^{\circ} \times 4^{\circ} \times 2\frac{1}{2}^{\circ}$ deep, hinged to a metal base $2\frac{1}{2}^{\circ} \times 4\frac{1}{2} \times \frac{2}{2}^{\circ}$ deep. Price **50**9.

PILOT BULBS

6-8 Volts 15 anp tubular MES British made good quality. 1 dozen in a box. 25p per box.

5 AMP CONNECTOR STRIPS This is the normal type of connector strip. 12 connectors with grub screws mounted in a line and moulded in polythene. 15p each \$1.50 perdozen.

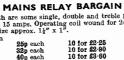
A New Service to Readers. A bulletin bringing news of new lines, special snips and "too few to advertise" lines will be posted to subscribers during first week of each month. The bulletin will be called "Advance Advert News" and the Sub-scription is 60p per year. Subscribers will also receive our completed 1971 catalogue when this is publiched published.















Rec. Retail Comet Price Price

STEREO AMPLIFIERS

STEREO AMPLIFIERS		
STEREO AMPLIFIERS ALBA UA 700 ARMSTRONG 521. *DULCI 207 FERROGRAPH F307. FERROGRAPH F307. FERROGRAPH F307. FERROGRAPH F307. EAK Stereo 30 Plus. IEAK Stereo 30 Plus. IEAK Stereo 70. IEAK Stereo 70. IEAK Stereo 70. IEAK Stereo 70. INEAR LT 66 *UINEAR LT 66. *UINEAR LT 66. *UINEAR LT 66. METROSOUND ST20. METROSOUND ST20. METROSOUND ST20. PHILIPS RH 530 PHILIPS RH 530 PHILIPS RH 530 PHILIPS RH 530 PIONEER SA500 PIONEER SA500 PIONEER SA500 PIONEER SA500 PIONEER SA600 PIONEER SA600 PION	$\begin{array}{c} 34 \cdot 58 \\ 56 \cdot 00 \\ 26 \cdot 00 \\ 32 \cdot 00 \\ 62 \cdot 00 \\ 54 \cdot 00 \\ 56 \cdot 50 \\ 69 \cdot 00 \\ 75 \cdot 00 \\ 21 \cdot 00 \\ 36 \cdot 00 \\ 36 \cdot 00 \end{array}$	26 · 00 42 · 50
*DULCI 207	26.00	42.50
DULCI 207M	32-00	17·50 21·95 44·00
GOODMANS Maxamp	62.00	44-00
LEAK Stereo 30 Plus	56 50	43.00
LEAK Stereo 30 Plus, in teak case	62.50	47-95
LEAK Stereo 70, in teak case	75.00	52.00 56.95 17.00 24.95
*LINEAR LT 66	21.00	17.00
METROSOUND ST20	39-50	24.95
PHILIPS RH 591	39.50 79.00 52.00 29.00	29.50 61.50 39.50 23.00
PHILIPS RH 590	52.00	39.50
PIONEER SA500	62.10	41 95
PIONEER SA700	98-00	68·95
PIONEER Reverberation	45 50	95-95 31-95
ROGERS Ravensbourne	59.50	45 · 95 49 · 50
ROGERS Ravensbrook Mk. II	47.50	36 50
ROGERS Ravensbrook (cased)	F0 F0	
Mk. II SINCLAIR 2000 SINCLAIR PROJECT 60/2 X Z30/ PZ5	35.00	41-50 27-00
SINCLAIR PROJECT 60/2 X Z30/		
SINCLAIR PROJECT 60/2 X 750/	23.90	16.20
PZ8/trans.	34-86	23 . 25
SINCLAIR AFU	5-95	4-95
SINCLAIR 3000	45-00	34.95
TELETON SAQ 206 (new release)	29.00	18-50
8 electronically mixed inputs	185-00	139-00
SINCLAIR PROJECT 60/2 X Z30/ PZ5 SINCLAIR PROJECT 60/2 X Z50/ PZ8/trans. SINCLAIR AFU SINCLAIR Neoteric SINCLAIR Neoteric SINCLAIR Noteric SINCLAIR Noteric SINCLAIR 3000 TELETON SAQ 206 (new release) VOLTEX 1000. Stereo Discotheque, 8 electronically mixed inputs Starred items above take ceramic and All others take both ceramic and	cartridge	s only.
All others take both ceramic and ridges.	magneti	ic cart-
TUNERS		
*ARMSTRONG 523 AM/FM	53·76	42.00 33.00
ARMSTRONG M8 Decoder	9.50	8.00
DULCI FMT.7 FM	26.00	22 00 29 25
GOODMANS Stereomax	82-52	49 95
LEAK Stereofetic Chassis	66 - 50	49 95 52 00 59 00
PHILIPS RH 690	47.00	38 00 75 50
PHILIPS RH 691	89.00	75-50
PIONEER TX900 AM/FM	153-69	63 50 123 00 47 95 38 00
ROGERS Ravensbourne chassis	61-89	47-95
ROGERS Ravensbrook (cased)	51 26	41 · 00 31 · 95
TELETON GT 101	45.50	31 · 95 27 · 50
TUNERS *ARMSTRONG 523 AM/FM *ARMSTRONG 524 FM DULCI FMT.7 FM GOODMANS Stereomax. LEAK Stereofetic Chassis LEAK Stereofetic Chassis LEAK Stereofetic Inteak case PHILIPS RH 690 PIONEER TX500 AM/FM PIONEER TX500 AM/FM ROGERS Ravensbrook ROGERS Ravensbrook ROGERS Ravensbrook COGERS Cavensbrook COGERS CAVENS COGERS CAVENS COGERS COGERS CAVENS COGERS C	th MPX	Stereo
Decoder except where sta	rred.	
TUNER/AMPLIFIERS		
AKAI AA 8500 AKAI AA 8500 ARENA 7500 ARENA 2400 ARENA 2700 ARENA 2700 ARMSTRONG 03 Decoder ARMSTRONG 525 ARMSTRONG 525 ARMSTRONG 526 GODMANS Module 80, 35w.	229.00	181-00
AKAI 6600	142.53	112.00
ARENA 2400	90-30	72.00
ARENA 2700	105-00	85-00
ARMSTRONG M8 Decoder	9.50	258.00
ARMSTRONG 525	91.89	74-50
GOODMANS Module 80, 35w.	104.71	84.50
R.M.S.	95.00	72.00
PHILIPS RH 790	139.00	112.00
PIONEER SX770 AM/FM	160.43	126.00
PIONEER 440	194 /4	150·00 89·00
TANDBERG 1171 comp. with	440.00	
*TELETON F2000	51.50	30.50
TELETON 7 AT 20	105-00	77.95
TELETON TESSO	82.50	59.00
TELETON TES 50LA MW/LW/VHE	87·50	63.50
TELETON CR55	120.00	87.00
TELETON GA101	37.50	28-50
Starred Items above take ceramic -	artridaes	s only
All others take both ceramic and	magnetic	c cart-
TUNER/AMPLIFIERS AKAI AA 8500 ARENA 8500 ARENA 8500 ARENA 8500 ARENA 8500 ARENA 1600 ARENA 2000 ARENA 2000 ARENA 1800 ARENA 19000 ARMSTRONG 525 ARMSTRONG 525 GODDMANS Module 80, 35w. R.M.S. MIDLAND 19/542 PHILIPS RH 780 PIONEER SX770 AM/FM PIONEER SX980 AM/FM PIONER SX980 AM/FM<		و المعام الم
All the above Tuners and Tuner/Am MPX Stereo Decoder with the exc strong where decoder is extra as li	primers in option of sted.	Arm-

MPX Stereo Decoder with the exception of Armstrong where decoder is extra as listed.



346.5		· · · • • · · · · · · · · · · · · · · ·
	Rec. Retail	Comet
	Price	Price
PICKUP ARMS		
GOLDRING Lenco 175	12.33	10-50
GOLDRING Lenco L69	9.29	7.00
SME 3009 with S2 Shell	34.47	27.00
GOLDRING Lenco L75 GOLDRING Lenco L69 SME 3009 with S2 Shell SME 3012 with S2 Shell	36.71	30.50
CARTRIDGES		3
GOLDRING 800 GOLDRING 800E GOLDRING 800E *GOLDRING CS90 Stereo *GOLDRING CS91/E GOLDRING G850 EMPIPE 1007E/Y	13-00	6-95
GOLDRING 800E	18.86	10.95
GOLDRING 800 Super E	26.01	19.50
*GOLDRING CS90 Stereo	5·20 7·81	4.25
*GOLDRING CS91/E	7.81	6-25
GOLDRING G850	6.50	5.25
EMPIRE 100ZE/X	63·00 44·50	52:50
EMPIRE 999VE/A	27.60	36·00 22·50
EMPIRE 9991E/A	21.00	17-50
EMPIRE 999E/X	16.50	13.00
EMPIRE 999/X	11.50	9.25
EMPIRE 909E/X	12.85	10.25
EMPIRE 909/X	9.00	7.50
GUDARING BBS0 EMPIRE 1002E/X EMPIRE 9997E/X EMPIRE 9997E/X EMPIRE 9997E/X EMPIRE 9997/X EMPIRE 9997/X EMPIRE 9097/X EMPIRE 9097/X EMPIRE 907/X EMPIRE 907/X EMPIRE 907/X	9.75	8.00
ORBIT Magnetic NM 22	Special Pri	ce 2.90
PICKERING V15 AC2	8.40	7.00
ORTOFON SLIDE	29.65	23.75
EMPIRE 900/X EMPIRE 900/X ORBIT Magnetic NM 22 PICKERING V15 AC2 ORTOFON SL15E ORTOFON SL15E SHURE M3DM SHURE M3DE SHURE M32E SHURE M32-3 SHURE M44-5 SHURE M44-5 SHURE M44-5 SHURE M44-5	7.44	3'25
SHURE M31F	12.05	8.95
SHURE M32E	11.10	8.25
SHURE M32-3	10.20	8.00
SHURE M44-5	11.10	7.95
SHURE M44-7	10.20	8.00
SHURE M-44C	10-20	8.00
SHURE M44E	12.05	8.25
SHURE M44C SHURE M44E SHURE M55E SHURE M75G	12·95	9·50 14·00
SHURE M44E SHURE M55E SHURE M75G SHURE M75G SHURE M75EJ SHURE M75EJ SHURE M75E-95G SHURE M75E SHURE V15-11	17.60	14.00
SHURE M75EJ	19-45	16-00
SHURE M75E-95G	23.15	18.00
SHURE M75E SHURE V15-11	21.30	14-50
SHURE V15-11	21·30 40·76	28.95
SHURE V15-11-7	38.90	29.00
Starred cartridges above are ce	ramic. All oth	ers are
magnetic.		
TUDNTABLES		
TURNTABLES		
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complete with Goldring	G.800 Carte	idae
base and cover, S	pecial Price	0.95
GARRARD SP25, Mk III	fully wired	with
		olete
with base, plinth and cove	er	
CAPPAPD 1015 (pecial Price	21 98
GARRARD 2025 fully wire	d with Sono	tone
9TAHC Cartridge comple	te with base	and
complete with Goldring G8	50 cartridge	hrea
complete with Goldring G8 and cover	25.00	5.95
	the second s	
DUAL 1219 transcription	60-40	50.00
		35.00
GARRARD SP25 Mk III	16.45	11-90
GARRARD SL65 B	21-25	15-90
GARRARD SP25 Mk III GARRARD SL65 B GARRARD SL75 B GARRARD SL95 B	39-20	26.50
GARRARD SL95 B	50.01	35-50
GARRARD 401	38.07	29.50
GARRARD 401	···· 38·07 ···· 33·11	29·50 27·90
GARRARD SL72 B GARRARD 3500, with GKS (38.07 33.11 Cart-	27.90
GARRARD SL72 B GARRARD 3500, with GKS (38.07 33.11 Cart-	27.90
GARRARD \$172 B GARRARD 3500, with GKS (ridge Base and Cover to fit GARR/ SP25, SL55, SL55B and 3500	38.07 33.11 Cart-	27.90
GARRARD SL72 B GARRARD S500, with GKS (ridge Base and Cover to fit GARR) SP25, SL55, SL65B and 3500 CARDA DD crop	38.07 33.11 Cart- ARD Special Prio	27·90 12·90 ce 4·00
GARRARD SL72 B GARRARD SL72 B GARRARD 3500, with GKS (ridge Base and Cover to fit GARR) SP25, SL55, SL65B and 3500 CARDA DD 1000	38.07 33.11 Cart- ARD Special Prio	27 · 90 12 · 90 :e 4 · 00 10 · 97 21 · 50
GARRARD SL72 B GARRARD SL72 B GARRARD 3500, with GKS (ridge Base and Cover to fit GARR) SP25, SL55, SL65B and 3500 CARDA DD 1000	38.07 33.11 Cart- ARD Special Prio	27 · 90 12 · 90 :e 4 · 00 10 · 97 21 · 50
GARRARD SU72 B GARRARD SU72 B Idge and Cover to fit GARR SP25, SL55, SL55B and 3500 GARRARD 40B GARRARD AP 76 GOLDRING GL58 P Mr. II	38.07 33.11 Cart- 17.23 ARD 13.84 13.84 28.88 26.63 35.14	27 · 90 12 · 90 :e 4 · 00 10 · 97 21 · 50 21 · 25 28 · 50
GARRARD SL72 B GARRARD SL72 B GARRARD 3500, with GKS (ridge Base and Cover to fit GARR, SP25, SL55, SL65B and 3500	38.07 33.11 Cart- 17.23 ARD 13.84 13.84 28.88 26.63 35.14	27 · 90 12 · 90 :e 4 · 00 10 · 97 21 · 50 21 · 25

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for G99 GOLDRING G99 GODDMANS 3025. McDONALD MP 60 McDONALD MP 60 Base and Cover for McDONALD Base and Cover for McDONALD PHILIPS 202	11-45	9 - 90	
GOLDRING G99	26.00	22.90	
GOODMANS 3025	37.74	26 90	
MCDONALD 610	20.00	15.75	
Base and Cover for McDONALD	20 00		
MP 60 and 610 Sp	ecial Pri	CB 4-50	
MP 80 and 610		11.00	
PHILIPS GA 146	31.50	25.00	
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GOODMANS Axiom 10	28-31	23.75	
GOODMANS Axiom 201	14-45	10.95	
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ALBA UA662	62 · 97 72 · 50	47 · 95 58 · 95
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H.M.V. 204/5/6	202.85	165-00
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METROSOUND Stereo 1010	82.30	65 .95
PHILIPS GF823	71.00 51.50	55 · 95 41 · 95
PHILIPS GF824	69 · 50 67 · 50	56-95 55-95
PHILIPS GF834	88.00	73-95
PHILIPS 882 (less L/S) PHILIPS GF417	99-00 99-50	78 · 50 82 · 95
TELETON 2S60F, with Stereo Radio	75.00 248.00	55 · 95 175 · 00
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AKAI X330	342-57	265 · 95 243 · 95
AKAI X-3300 AKAI X-330D AKAI X-330D	380.08	279 . 95
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AKAI 1710L AKAI 1720L AKAI CR80 8-track stereo recorder	97-21	77-50 99-95
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deck. FERROGRAPH 704/W 4 track tape	_	
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PHILIPS 4408 4-Track Stereo	139.00	109-00
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/Mains)	45.50	36 - 95
/Mains) TANDBERG 1841 4-track Stereo	40 00	20 23
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Base and Cover for TD 125	15-18	12.50
3500 Specific Specifi	39 . 20	31 25
MOTORBOARDS only	4.95	3.00
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97·95 69·50

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Rec.	Retail Price	Comet Price
GOODMANS AUDIO SUITE,		
Goodmans Maxamp stereo ampli-		
fier, Goodmans stereomax AM/ FM Tuner with decoder. Pair of		
Garrard AP76 turntable in base, complete with cover and Gold- ring G800 Cartridge. Beautifully		
	257.13	169.95
GOLDRING 705P turntable complete	257.13	109.95
GOLDRING 705P turntable complete with G850 Cartridge, Midland		
Tuner/Amp., pair of Metrosound	99·56	69-95
GOODMANS Module 80 Tuner/	00 00	00 00
Amplifler, Goodmans 3025 Turn- table with Goldring G800 Cart-		4
ridge with 2 Goodmans Minister		
Speakers	182.74	139-00
METROSOUND 448 8-track stereo		
play-back unit complete with 2 HFS 10 Speakers	83-56	70-95
GOLDRING 705P turntable complete		
with G850 Cartridge, Teleton 203 Amplifier, pair of Keletron KN500		
Speakers	77.00	49-95
TELETON Stereo 8 track tape Audio		
system complete with speakers	54.75	48 00
GARRARD SP 25, Mk. III mounted in base, plinth and cover with		
COLDRING G900 Carteldan		
Teleton 206 Stereo Amplifier 12 watts RMS, and 2 KELETRON		
NINDUO Speakers, each speaker		
is a 4 speaker system	88.33	58-95
PIONEER PL 12 turntable, Good- mans Maxamp, Shure M55E Cart-		
ridge, 2 Keletron KN 700 speakers		
 (each speaker cabinet contains 4 speakers) 	144.38	105.00
GARRARD AR76 turntable com-		
plete with Goldring G800 Cart-		
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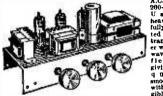
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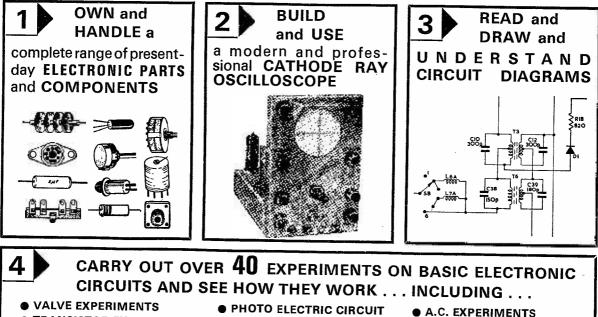
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VOL 47 NO 4

lssue 774

AUGUST 1971

Exhibitions R.I.P.?

THERE are probably more exhibitions today than ever before, but those embracing areas of interest to readers of P.W. appear to have suffered the ravages of economics, indecision and wrong priorities.

RACTICAL

ELF

The pre-war "Radiolympias" were intended for trade and public alike and even the last one in 1939 had lots of interest for the home constructor. Most hobbyists who could get to Olympia, went there. Post-war radio shows carried on the tradition, although with less and less for the amateur enthusiast—the trend was changing.

In the last decade, the unity of the radio industry began to deteriorate as first one, then another, major company broke away from the main exhibition (then at Earls Court) to hold their own private shows. In 1964 there were over ten "splinter" shows in London at exhibition-time and this mass exodus killed the public radio and TV show in this country. The costs of mounting stands in the exhibition halls available, plus the attitude of brushing off the public (the ultimate customers) were contributory factors.

Now, after some years of August trade-only exhibitions scattered all over London, manufacturers this year abandoned the traditional "showtime" period and held their shows during May. An attempt to get the industry together again under one roof failed. Next year, shows will again be held in the Spring. After that one needs a crystal ball. But still there seems to be no hope of anything for the public to see!

On another front, the various audio exhibitions overlap to some extent and are the subject of both praise and criticism. The Audio Fair gave up hotel rooms for the open spaces of Olympia and brought in photographic and then musical instrument interests. There has been talk of radio and TV exhibits. However, even if audio exhibitions do not please everyone, at least the public can get in!

Discounting the more specialised and professional orientated exhibitions, this leaves one more erstwhile important calendar date for the radio amateur—the RSGB Exhibition. We have seen this develop (or disintegrate?) from its unpretentious but delightfully social atmosphere of the Hotel Royal days, through various stages at Seymour Hall and Royal Horticultural Hall. It tried to change its angle, gave itself a pompous (and, we feel, misleading) name, lost its character and died. For this year there is to be no RSGB Exhibition.

A sad story for exhibition-minded radio enthusiasts. The problems will only be solved when we have more modern (and economic) exhibition halls for the larger shows and organisers, societies and manufacturers who are oldfashioned enough to think first of the public, then give them what they want.

W. N. STEVENS-Editor.

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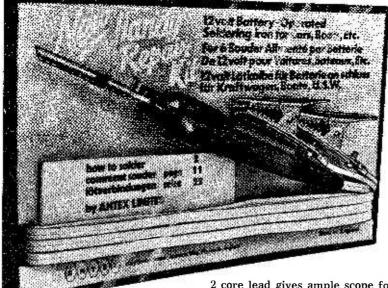
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SEPTEMBER ISSUE WILL BE PUBLISHED ON AUGUST 6th

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12V Iron from Antex



Antex have introduced the 'MES 12' soldering iron for operation from any 12 volt supply such as a car battery or accumulator.

Two large crocodile clips provide direct connection to the battery terminals and 15 feet of

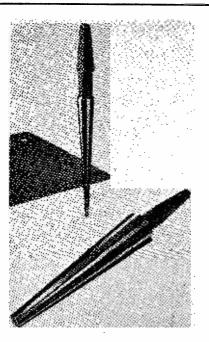
Fudging irons

West Hyde Developments are asking: How often do you fudge a hole? They maintain that their taper reamers are the finest fudging irons available. These West Hyde reamers, due to their many flutes and cutting edges, will open a hole from ${}^{1}_{8}$ in to ${}^{7}_{16}$ in in a few seconds and the hole will be rounder than when drilled. On the many occasions when equipment cannot be put up on a drilling machine due to size and damaging the finish a West Hyde reamer in an ordinary hand brace will solve the problems without vibration and with little effort.

Two sizes are available, ${}^{1}_{8}$ in. to ${}^{1}_{2}$ in (3mm to 12mm) and ${}^{3}_{8}$ in to 1in (9mm to 25mm). Prices are: small size £2.75+10p postage and packing. Large size £3.40+15p postage and packing.

2 core lead gives ample scope for normal operation.

This iron is absolutely ideal for use in conditions where a mains supply is not available. It is supplied in a durable plastic wallet which will 'house' the iron when not in use. Recommended U.K. price is £1.95. Antex Limited, Mayflower House, Plymouth, Devon.



The I.B.C. 1972

One of the leading events in the world broadcasting calendar, the International Broadcasting Convention, will next be held in London from 4-8 September 1972. This will be the fourth IBC.

The Convention, which will be held at Grosvenor House, Park Lane, will comprise technical sessions and a comprehensive exhibition of the latest television and sound broadcasting equipment, both highlighting the future technological options available to broadcasting administrations.

IBC is sponsored by the Electronic Engineering Association, the Institution of Electrical Engineers, the Institute of Electrical and Electronics Engineers, the Institution of Electronic and Radio Engineers, the Royal Television Society and the Society of Motion Picture and Television Engineers.

All enquiries to The Secretariat, International Broadcasting Convention, IEE, Savoy Place, London WC2R 0BL, England.

Cut price stereo

Audio Supplies Limited have a supply of "The Great Musicians" stereo LPs and for $\pounds 1.15p$ (p.p. free) they are offering three records. Each 10in. stereo LP is incorporated in an illustrated 12-page record book which gives an insight into the life of the composer and explains how his life influenced his work.

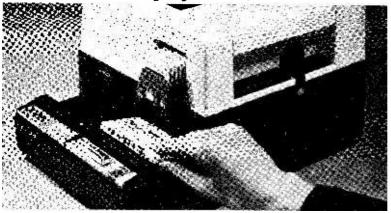
These LPs originally retailed for 13s. 11d. each and there are 55 titles from which to choose by 20 of the world's greatest composers. Audio Supplies Limited, (Dept. P.W.) 50 Stamford Hill, London, N.16. Telep¹one 01-806 3611.

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Zeiss Ikon P500 projector



Basically, the P 500 consists of the Perkeo S 150 projector mounted on top of a Philips cassette tape recorder and loudspeaker to form a single unit. The projector can be used by itself in the normal manner and so can the tape recorder. Individual slides can be inserted in the gate without using the magazine—the importance of this feature will be appreciated by anyone who has done much slide-sorting. The forward and reverse movements of the magazine have also been retained and can be worked either manually (in which case you use a remote control cable instead of the push-buttons that are operated on the standard S 150) or else by means of the tape. To make the magazine move on to the next slide you put a short impulse on the tape; to make it move backwards to the slide shown previously you instead use a long impulse.

The Philips tape recorder is connected to the projector electrically. An extra record/playback head has been fitted to add the highfrequency impulse to the tape which changes the slides; the recorder itself is housed in a drawer which pulls out of the back of the unit. Space is provided to store spare cassettes, the microphone and various cables and accessories.

There are also, in addition to the mains inlet, four sockets. One allows you to connect an external speaker, useful when operating in a large hall. Another a combined input/outlet socket, lets you record from a source such as a microphone, radio, tape recorder, record player or mixer or alternatively to boost the output via an amplifier. A third allows the remote control for the projector to be fitted and the last one is for the cable that lets you put the slide change impulses on the tape.

The recommended price of the P 500 will vary according to the lens fitted, but with the Vario-Talon $f3 \cdot 5$ 70-120mm it is £222.18.6d £222.921₂), including £66.18.6d (£66.921₂) P.T. The price includes the microphone and the impulse device.

IC's on the wall

Mr. J. Evans of the Mullard Press Dept., informs us that a large coloured chart produced by the Mullard Educational Service outlines the manufacturing process of integrated circuits. It measures nearly 30×22 in. and has diagrams showing cut-away views of a silicon chip at different manufacturing stages as resistors, capacitors, diodes and transistors are formed by various diffusion techniques. Captions alongside the diagrams detail what is done to the chip.

The chart is suitable for use in schools, colleges, universities and other training establishments where electronics is taught. Price 25p post free (send cash with order), it can be obtained from the Mullard Educational Service, Mullard Limited, Mullard House, Torrington Place, London WC1E 7HD.

Radio Brighton

From the start of programmes on Saturday, May 29, BBC Radio Brighton transmitted on $95 \cdot 8MHz$ instead of $88 \cdot 1MHz$ and the effective radiated power increased from 75 to 500W.

Lexor's board

Lexor Dis-Boards Limited now announce their brand new 'Mini-Board'. Having pioneered the multi-socket power board business more than ten years ago, Lexor are aware that 75% of users' needs can be met by only one model. This has now been specially designed and set up for quantity production and sells for only $\pounds 3.95$.

Four high-grade 13A ivory sockets are mounted in a slim blue leather-finish case and fed via 5ft. of cable from a readyfitted 13A ivory fused plug. There is the characteristic red safety warning lamp, and the units can be used portable and free-standing or easily fixed permanently to walls, benches, etc. Simple cable extensions of 15ft. or 25ft. are available for the situations where the flex will not reach.

Illustrated brochures carrying full details, prices and sales terms are available from Lexor Dis-Boards Limited 25/31Allesley Old Road, Coventry.



DIRECT GONVERSION RECEIVER for 80 metre SSB/CW r.f.graham

A S anyone who has become interested in the reception of single-sideband and c.w. (Morse) signals knows, the usual type of receiver for a.m. (amplitude modulation) reception is not able to resolve these transmission. When a beat frequency oscillator is present in the receiver, s.s.b. and c.w. can be received and modern communications receivers having a b.f.o. Older communications receivers having a b.f.o. allow reception of s.s.b. but with some difficulty unless the operator is experienced.

REQUIREMENTS

To clarify requirements for s.s.b./c.w. reception, Fig. 1A shows the stages of a typical superhet. (1) is the r.f. amplifier, which amplifies signals at the received frequency. (2) is the mixer, with oscillator (3), which may be separate, or combined in a single frequency-changer. Output from this section is at a fixed intermediate frequency, and passes through the i.f. amplifier (4) to the a.m. and product detector circuits (5). With domestic type receivers, this stage is an a.m. detector only where a.m. signals are demodulated, and passed through the audio amplifier (6) to the speaker (7).

Where the receiver is intended also for s.s.b./c.w. reception, (5) incorporates a product detector and a beat frequency oscillator (8) is also provided.

When s.s.b. signals are received, the b.f.o. supplies an unmodulated r.f. input, which replaces the "carrier", suppressed in s.s.b. transmission. This local carrier and the s.s.b. from the i.f. amplifier (4) are combined in such a way as to give an audio output, which passes to the audio amplifier and speaker.

For c.w. reception, the output of the b.f.o. (8) heterodynes with the c.w. coming through the i.f. amplifier (4) to give an audio tone, is amplified and fed to the speaker (7).

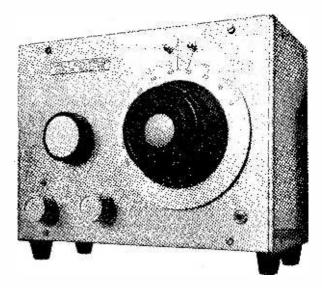


Fig. 1B is a direct conversion receiver and its much greater simplicity is obvious. (1) is the r.f. amplifier, tuned to the required signal in the usual way and fed to a product detector (2) which also receives input from the variable frequency oscillator (3) which covers the band upon which reception is wanted the circuit being so designed that an audio output is obtained directly from the product detector (2), which is amplified by stage (4) and routed to the speaker.

When receiving s.s.b. only those s.s.b. frequencies which combine with the v.f.o. frequency to give an audio output are heard. Thus the selectivity of the receiver does not depend upon the r.f. amplifier or product detector signal frequency circuits but upon the selectivity of the audio stages.

Thus apparent selectivity is achieved because unwanted signals are combined with the v.f.o. in stage (2) to give outputs which are not in the audio range of stage (4). To receive c.w. the v.f.o. is tuned to one side of the c.w. carrier to give an audio output from the product detector. This particular circuit is not really suitable for the reception of a.m. signals which require the local carrier to be phase-locked to the a.m. carrier.

The receiver described here will be found to give a very lively performance. As it is assumed that anyone just becoming interested in the reception of amateur s.s.b. and c.w. may not have much in the way of calibration or test equipment, the v.f.o. is designed to use three 1 per cent tolerance capacitors and a coil with adjustable core, so that it is only necessary to set the core to give 80m band coverage. The radio frequency circuits are peaked for best reception.

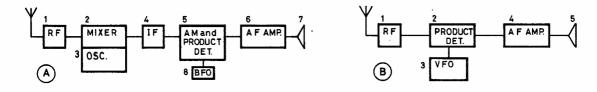
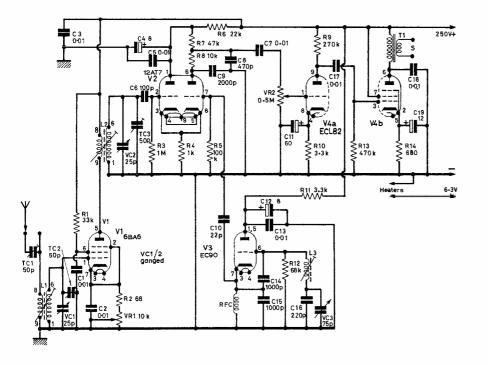


Fig. 1A shows the arrangement of the standard superhet while Fig. 1B illustrates the reduced number of stages required for a direct conversion receiver.



◀ Fig. 2. The complete circuit of the Direct Conversion Receiver. The main tuning dial (shown in the heading photograph) drives the v.f.o. tuning capacitor VC3.

▼ Fig. 3. Layout of the major components on top of the chassis with important dimensions shown.

CIRCUIT

Fig. 2 is the complete circuit. V1 (6BA6) is the r.f. amplifier, with gain control VR1. L1 and L2 are tuned by VC1/2, which is a small ganged capacitor for the r.f. tuning control.

V2 (12AT7) is the product detector, the wanted signal is present at one control grid and injection from the v.f.o. at the other grid. Audio output from the second anode passes to the 2-stage audio amplifier, VR2 being the volume control.

V3 (EC90) is the v.f.o. covering 3.5-3.8MHz, with a little to spare. VC3 is operated through a balldrive and although tuning is quite critical it is eased

by the narrow band covered by VC3. Coverage is determined by L3 and the three capacitors C14, C15 and C16, so it is only necessary to adjust the core of L3. Because of the large value of these capacitors changes in capacitance around V3 have little effect on its frequency.

C5 and C13 are r.f. by-pass capacitors with C4 and C12 in parallel with them to avoid hum from the h.t. supply and reduce audio feedback effects. The receiver is intended for use with a supply of about 220-250V at 40-50mA with the heaters drawing 1.53A at 6.3V.

134 1%ⁿ (О) м. с and ECL82 (0) V 2 V 1 6846 т1 Can Top 6 Speake Ø Ø VC3 ٧C C Aerial tune VFO Tune

CONSTRUCTION

The chassis, Fig. 3, is an $8 \times 4in$. "universal chassis" flanged member. This allows a complete case to be assembled by using two further $8 \times 4in$. members, top and bottom, with two $6 \times 4in$. members for the sides. The panel is $8 \times 6in$. and the surface of the chassis is 2in. above the bottom edge of the panel. Cut away the four corners "X" so that the $6 \times 4in$. sides fit round the chassis, allowing the box to be screwed together.

Flanges on the members listed are ready punched, and can be secured together with 4BA bolts and nuts while the receiver panel is secured to the top, bottom and side flanges with self-tapping screws. The case back should be of perforated metal, or have rows of ventilation holes.

VC1/2 is bolted to the panel, TC2 being soldered to a tag and VC1 as shown. The aerial coil L1 must be screened with the aluminium can supplied. The can lid is secured to the chassis by the fixing bush of L1. Leads for TC1 and VC1 pass out near the chassis. The lead from pin 6 passes through the chassis to tag 1 of V1. The normal adjusting screw of L1 cannot be reached because of VR1. So the core is removed, a shallow saw-cut is made across the end and it is replaced. Drill a hole in the screeening can for this purpose and cut off about one-third of the screwed portion of the can, so that when it is tightly fitted it does not cut into the leads to TC1 and VC1.

TC1 is mounted on a strip of insulating material. A1 and A2 are optional aerial connections.

VC3 is fitted so that its spindle projects ${}^{9}_{16}$ in. The ball drive is lined up so that it rotates freely and its lug is held with a long bolt with extra nuts. The lead MC from VC3 in Fig. 3 runs to a tag bolted to the chassis near L3.

The primary (P) connections of T1 run through to pins 6 and 7 of V4. Secondary leads (S) go to a small panel jack, for speaker or headphones.

Inductors. With the "Range 3" coils listed, Blue for L1 and Yellow for L2, adjustment of the cores and TC2 and TC3 gives easy coverage of 80m and VC1/2 need not be exactly 25pF.

L3 is 30 turns of 26 s.w.g. enamelled wire, closewound on a ${}^{1}_{2}$ in. diameter former with adjustable core. The winding is put near that end of the former furthest from the metal chassis and turns secured with Bostik 1.

Wiring. Wiring and components are shown in Fig. 4. The heater, grid and anode leads are run close to the chassis. Trimmer TC3 has one tag bolted to the chassis, so that it can be adjusted from the rear.

All connections should be reasonably short and direct, and run as shown. VFO wiring, especially to L3, C16 and VC3, is of stout wire, kept as short as possible.

Tag strips are used to support various small components. A 3-cored cable or coloured single flex

★ components list

Resistors :				
	De 10k0			
R1 33kΩ1W R2 68Ω	R8 10kΩ			
	R9 270kΩ			
R3 1MΩ R4 1kΩ	R10 3·3 kΩ			
	R11 3·3kΩ 1W			
R5 100kΩ	R12 68kΩ			
R6 22kΩ	R13 470kΩ			
R7 47kΩ	R14 680 Ω			
All 1 W 10% except as i	ndicated.			
VR1 10kΩ potentiome	ter, wire wound.			
VR2 500kΩ potentiom	eter, log.			
A				
Capacitors :				
C1 0.01 µF 350V disc	C11 60µF 6V			
C2 0.01 µF 350V disc	C12 8µF 350V			
C3 0.01µF 350V disc	C13 0.01 µF 350 V disc			
C4 8μF 350V	C14 1000pF 1% SM			
C1 0·01μF 350V disc C2 0·01μF 350V disc C3 0·01μF 350V disc C4 8μF 350V C5 0·01μF 350V disc C6 100pF SM C7 0·01μF 350V	C15 1000pF 1% SM			
C6 100pF SM	C16 220pF 1% SM			
C7 0·01μF 350∨ C8 470pF	C17 0.01µF 350V			
	C18 0·01µF 350V			
C9 2000pF	C19 12µF 50V			
C10 22pF SM				
VC1 2 x 25pF gang. (J VC3 75pF variable. (Ja	ackson Type 02).			
VC3 75pF variable. (Ja	ickson Type C804).			
TC1, 2, 3 50pF pre-set	trimmers.			
Valves :				
V1 6BA6 (EF93)	V3 EC90			
V2 12AT7	V4 ECL82			
Chassis and Case :				
2 off 6 x 4in. sides, Ty 2 off 8 x 4in. sides, Ty	pe CU41B			
2 off 8 x 4in, sides, ly	pe CU56A			
1 off 8 x 6in. plate, Typ	be CU178			
4 off Case feet, Type Z	146			
(all from Home Radi	0)			
Miscellaneous :				
L1 Denco 'Blue' Range (3 (valve type).			
L2 Denco 'Yellow' Range 3 (valve type).				
L3, see text.				
Ball drive, (Jackson 4489)/C) RFC, 2·5mH.			
2 off B7G skirted valveh				
2 off B9A skirted valveh				
Knobs, tag-strips, outpu				
11, output transformer a	about 60:1 to carry 40mA.			

twisted together, is employed for h.t. positive, 6.3V, and common return connections—red may be used

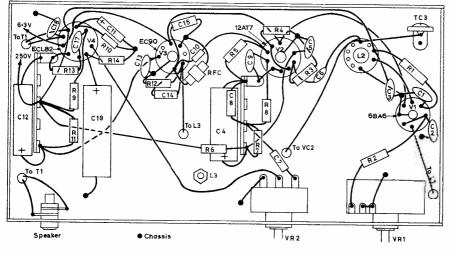


Fig. 4. Wiring guide for components underneath the chassis. Wiring around the v.f.o. valve V3 should be kept as short as possible to improve stability.

continued on page 314

I T is apparent that there is a good deal of interest in small transmitters for the low frequency bands. There are several reasons for this. Such equipment can be constructed at small cost, with easily obtained components, and only a modest power pack is needed to reach the maximum allowed power input of 10 watts in the case of the 160m band. Many newly licensed amateurs start with such equipment, and when using this power on the low frequency bands the chances of interference to TV are minimal.

The transmitter described here is primarily for 160m working, but will be found to be a very practical piece of equipment on 80m also, coverage of this second band being easily arranged. In addition, an end-fed aerial is often used for 160m, which will also generally perform well on 80m. The 80m band also offers greatly improved range over 160m and contacts during daylight, so it is well worth having.



CIRCUIT

In Fig. 1, V1 (6C4) is the variable frequency oscillator, followed by V2 (6AM6) which is a buffer/ doubler. V3 (6BW6) is the power amplifier, and runs at about 10 watts input, anode current being shown by the meter. This is a straightforward arrangement which gives good results with a minimum of difficulty.

VCl tunes the v.f.o. from 1.75-2.0MHz and, for the 160m band, the 1.8-2.0MHz sector is used, transmitter output being on the same frequency as the v.f.o. For 80m, the v.f.o. is tuned over the range 1.75-1.9MHz, and V2 acts as doubler, so that the output frequency is from 3.5-3.8MHz. V6 provides a regulated supply for the v.f.o.

L2 and L3 are broadly resonant coils for 160m and 80m. When first testing the equipment, grid current in the p.a. stage can be checked by clipping a test-meter across R8. L4 is the pi-network tank coil, tapped for 80m.

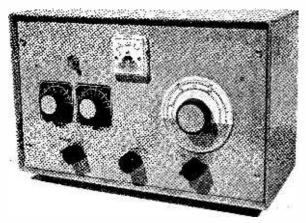
The audio section has V4 (12AX7) as a high gain amplifier, followed by V5 (6BW6) which choke modulates V3. This arrangement has been found to give good modulation and quality when using a crystal microphone and it requires relatively few components.

With any set of transmitting/receiving equipment the problem arises of providing "Transmit" and "Receive" change-over facilities. A relay is often used to switch the aerial from receiver to transmitter, to switch on the transmitter and to mute the receiver or speaker.

No external items of this kind are necessary with this transmitter, as the required switching is incorporated. This gives complete change-over from "Receive" to "Transmit" with single switch control.

The switch has four poles, section SI switching the aerial to the tank coil L4 at T (Transmit), but transferring the aerial to the receiver at R (Receive). Section S2 short-circuits the aerial feed to the receiver during transmission, to minimise r.f. leaking through to the receiver. S3 is in series with one speaker lead, and so silences the speaker during transmission.

The transmitter power circuit is controlled by S4, which applies h.t. to all stages on transmit. S5 is a separate two-way switch, which allows h.t. to be put on V1 and V2 only. This allows the v.f.o. to be tuned to any wanted frequency, and be "netted"



with the receiver, either to answer a CQ, or to begin transmission on a selected channel.

The aerial, or matching device, if used, is plugged into the aerial co-axial socket. A co-axial lead of convenient length is made up, and plugged into the "Rx" outlet of the transmitter. This lead runs to the aerial and earth terminals of the receiver. Communications type receivers normally have a separate speaker, one lead of which is cut, and extended if necessary, so that plugs can be inserted into the "Mute" transmitter sockets.

The two switches on the transmitter then give complete control, for tuning the v.f.o. netting on a signal, and changing from reception to transmission.

CONSTRUCTION

VFO

By using a ready-made inductor and accurate capacitor values, experiments to obtain suitable band coverage are avoided. It is only necessary to adjust the core of L1, and trimmer TC1, to set the band so that VC1 tunes 1.75-2.0MHz, with a little to spare at each end of the dial.

The v.f.o. is assembled in a box $3 \times 2 \times 2in$, which screens it completely and also helps isolate components from sources of heat. This box is readily

made from "universal chassis" strips. One strip is $7 \times 2in$, with flanges which are cut 2in. from each end, so that the strip can be bent into an open U-form 2in. high and 3in. wide, with flanges all round. An accurate bend is most easily obtained by holding the strip on a block of wood.

The second strip is $3 \times 4in$. and also has flanges. It is cut through centrally to obtain two pieces $3 \times 2in$. One of these is bolted to the front of the box as in Fig. 2 and carries VC1. After wiring is complete and the box is fixed to the chassis the second $3 \times 2in$. flanged piece is secured with self-tapping screws to close the back.

The v.f.o. is completely wired as in Fig. 2 before it is mounted. Trimmer TC1 is fixed just clear of the box top with a bracket or by bolts with spacers. A small hole is drilled in the box to permit adjustment of TC1. All connections are direct and rigid and points MC are joined with wire and also to tags bolted to the chassis.

The tag-strip in Fig. 2 is secured inside the box and supports the r.f. choke, C2, and C3. Coloured leads identify the wires which pass through the chassis—brown for h.t. (150V), blue for 6.3V, and yellow for the lead from C5.

The box is fixed to the chassis by bolts through the flanges which turn inwards (omitted in Fig. 2, for clarity) and through the front and back plates. It is placed so that the ball drive can be arranged as in Fig. 3.

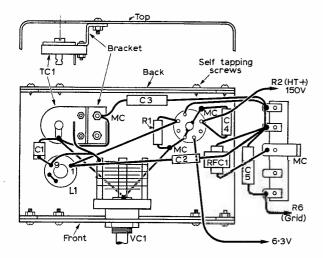


Fig. 2: Constructional details of the VFO assembly.

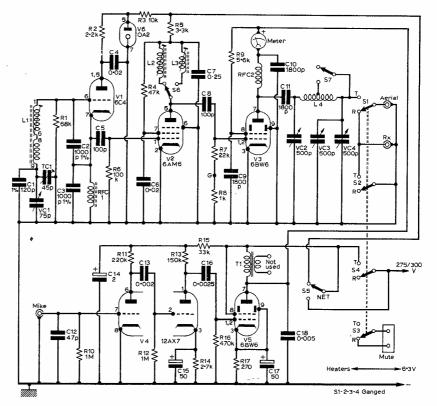


Fig. 1 : Complete circuit of the QRP transmitter.

Top of Chassis

Fig. 3 shows the position of the major components. Capacitor VC2 is of a type fixed to the chassis with small feet. Capacitor VC3/4 has three holes in the front plate and is bolted to a small bracket to bring the spindle level with that of VC2. These spindles pass through $\frac{1}{2}$ in. clearance holes.

Panel and chassis are fixed together by the switches and panel brackets. The lower edge of the panel must project about $\frac{1}{2}$ in. beyond the chassis, to clear the mounting flange of the case.

Buffer Stage

Components are placed around V2 as in Fig. 4, with grid and anode circuits separated and heater leads close against the chassis. The MC connection to the central spigot of the valveholder passes across the holder, as shown.

The coupling winding provided on L2 and L3 is not required, and must be completely removed. The outer end of the larger winding of L3 is then unsoldered from its pin and 28 turns removed. The end of the wire is cleaned and re-soldered to the pin.

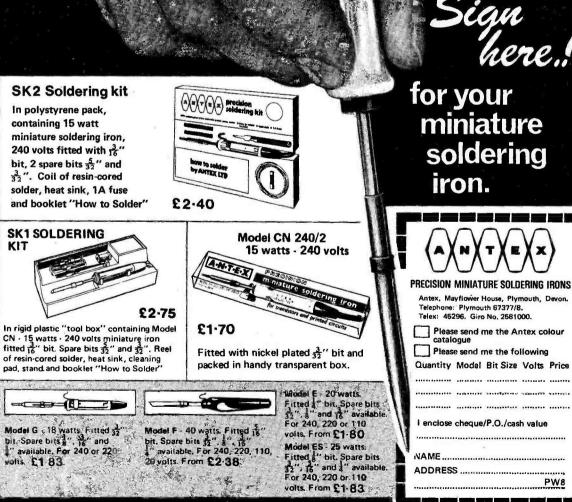
PA Stage

Grid circuit components are under the chassis, and are placed around V3 approximately as in Fig. 4. A hole is drilled in the chassis adjacent to the anode, pin 7, a lead passing directly through to the r.f.c. Anode circuit items are above the chassis.

C10 is anchored to a tag strip (Fig. 3) which also supports r.f.c.2, the top of the choke being held by C11. The 1800pF 1kV disc ceramic capacitors used in these positions are easily obtainable, but 2000pF

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E182CU EF92 370 FCF802 480 C	OAZ207 47p OC84 25p 2N1306 25n 40669 \$145p BFY52 23p RD938 32p 6517GT 32p 307 11	70p 9006 15p 92p C.R. Tubes
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ECC81 30p EL42 53p PCL83 65p EBF80 42p EL84 23p PCL84 42p 10	00V06-404 JIBC41 470 JIV85 300 304 370 64K5 300 6BA6 250 6V6GT 380 30PL1	70p 5FP7 £1.32p
EBF83 42p EL85 40p PCL85 42p	\$5.25p UBF80 35p VR105/30 35 384 35p 6AK8 32p 6BE6 30p 6X4 27p 30PL13	92p 88D £9.00p 85p 88J £9.00p
	B19 375 110035 405 7759 41-655 5B254W 49.90 6A L5W 400 6BJ6 455 6X5GT 829 35L6GT	50p 86L £9.00p
ECC82 28p EL95 85p PL36 58p S	STV280/40 UCF80 55p Z801U 215 0p 5B/255M 6AM6 30p 6BQ7A 35p 6Y6G 60p 35W4	30p Photo Tubes 45p CMG25
ECC83 30p EL500 85p PL81 50p ECC84 20p EM31 25p PL82 40p 8	STV280/80 110441 85n 2900T 75n 5B4GV 60n 6AQ5 35p 6BW6 80p 6Z4 82p 42	45p £2.75p
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ECC86 50p EM84 35p PL84 35p 5 ECC88 37p EM87 55p PL500 73p	1121 12 75 00 00153 00 113 050 574G 40 6AS7G 800 6C6 255 7C6 40p \$1	-60p £17-50p
ECC189 52p EY51 40p PL504 75p	1226 75b UF80 36b 185 24b 5Y3GT 35b 6AT6 80b 6CH6 55b 7H7 32p 50EH5	60p Special Vivs 40p CV1031
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ECF801 62p EZ41 42p PY82 27p 1 ECF802 62p EZ80 25p PY83 35p	UABC80 35p UU5 55p 3A4 80p 6AC7 15p 6B7 40p 6F23 75p 12AT6 80p 80 UABC2 55p UV5 55p 3A4 80p 6AC7 15p 6B7 40p 6F23 75p 12AT6 80p 80 UABC2 55p UV41 45p 3D6 15p 6AB6 50p 6BK7 40p 6F33 21 50 12AT7 80p 803 23	25p JP9/7D
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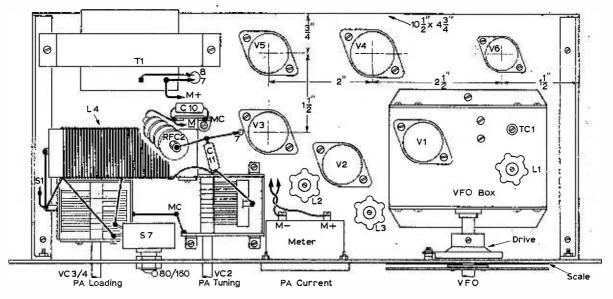


Fig. 3: Plan view of chassis showing disposition of major components.

mica capacitors of 750V rating could be used instead.

The p.a. coil has 63 turns of 22 s.w.g. enamelled wire, close-wound on a lin. diameter paxolin tube about 2³/₄in long. During winding, a loop is made at 33 turns for the switch S7 connection. This leaves 30 turns in circuit from VC2 to the switch.

The coil is mounted by bolting a lin. long strip of paxolin to it and attaching this to the frame of VC2 with a second bolt. The coil is well clear of metal parts and the cabinet top.

Audio Section

Grid leads and components should be against the chassis especially connections to pin 7 of V4 otherwise there is some danger of instability or picking up of hum or r.f.

No gain control was included because it was found that speaking normally with a hand-held crystal

Fig. 4: The wiring underneath the chassis.

microphone gave just about the required audio level. Gain can be reduced by removing C15 or by substituting a 1 megohm potentiometer for R12 connecting the slider to pin 2 of V4. It should be mounted on the back runner near V4 or be connected with screened leads.

The modulation choke T1 is the primary of a mains pentode type speaker matching transformer and should be able to carry 70-80mA, and of low d.c. resistance, to avoid excessive voltage drop.

A test of the a.f. section can be made by connecting a speaker to the secondary of the transformer. The speaker must be well clear of the microphone, to avoid audio feedback. Speech should be reproduced at ample volume with good quality. Causes of distortion could be low emission valves, wrong resistor values, or slight leakage in C13 or C16 upsetting the bias of the following stage.

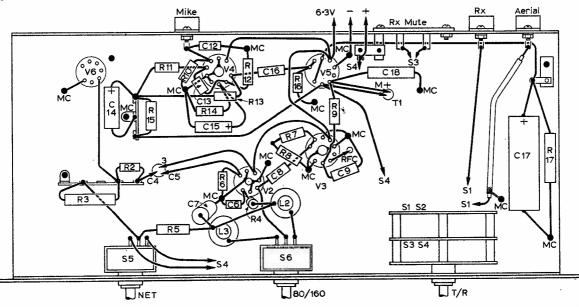
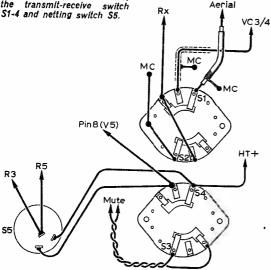


Fig. 5: An "exploded" view of the transmit-receive switch



Switching

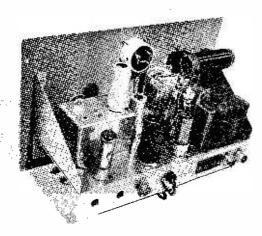
Fig. 5 shows switch connections. A co-axial lead is used for the aerial, taken to chassis at the socket, and at VC3/4. S5 is switched to the "Tune" position only when adjusting the v.f.o. frequency, and so S4 normally switches on all transmitter h.t. circuits.

VFO Dial

A pointer, cursor or disc of transparent material such as perspex can be mounted on the flange of the ball drive by two short 8BA screws. A disc with a line marked on it was used. A piece of thin card of larger diameter than needed was temporarily fixed to the panel, and calibration marks made around the edge of the disc. The card was removed, markings transferred to scales of suitable diameter, and the card cut down to size and cemented in place, finally checking that the calibration was still correct.

CW

V3 can be keyed by disconnecting pin 3 from the chassis, connecting a 5000pF capacitor directly from this tag to chassis and wiring a lead from pin 3 to a jack, normally closed to complete the circuit.



This places the key between cathode and chassis when the plug is in. It is also necessary to take T1 out of circuit, which can be done by fitting a two-way switch to the back runner, so that on c.w. h.t. reaches the r.f. section only. The lamp load mentioned later for a.m. tests is not suitable on c.w. Connect a 470 ohm resistor in series with a 5000pF capacitor across the key jack.

VFO CALIBRATION

Calibration is most easily done with a 100kHz crystal marker used in conjunction with a communications type receiver. First adjust the core of L1, and trimmer TCI, for suitable coverage. As TCl is increased in value, the range of frequencies covered by VCl will be reduced. TCl and Ll also allow the band edges to be adjusted. It is best to arrange that almost the whole swing of VC1 is needed to tune from 1.75-2.0MHz, but to avoid the extreme positions.

★ components list

Resistor	s:			
R1	68kΩ	R10	1MΩ	2
R2	2·2kΩ	R11	220k	
R3	10kΩ 3W	R12		
R4	47kΩ	R13	150k	Ω
R5	3·3kΩ 1W		2.7ks	
R6	100kΩ		33 kΩ	
	22 kΩ		470k	Ω
R8	1kΩ	R17	270 Ω	2 2W
R9	5•6kΩ 2W			
All	≟W 10% un le	ess ind	dicate	d otherwise.
Capacito				
C1	120pF SM 1	%	C10	1800pF 1kV
C2	1000pF SM	1%	C11	
C3	1000pF SM	1%	C12	
C4	0.02µF 350V	-	C13	
C5			C14	2µF 350V
<u>C6</u>	0.02µF 350V		C15	50µF 6∨
C7			C16	0.0025µF 350∨
C8	100pF SM		C17	
C9	1800pF 1kV		C18	0.005µF 1kV
	1 45pF trimm	er, cer	amic.	
	1 75pF miniat	ture, a	ir.	
	2 500pF varia	ble, ai	r.	
	8-4 500+500p	r gan	gea v	ariable, air.
Valves:	_			
	6C4 (EC90)		V4	12AX7 (ECC83)
	6AM6 (EF91))	V5	6BW6
V3	6BW6		V6	OA2
Inductors				
L1	"Yellow", Ra	nge 3	(Den	ico)
L3	"Red", Rang	e 2 (C)enco	}
L2	"Blue", Rang	je 2 ([Denco))
L4	See text			
RFC	1 2.5mH mir	niature	iron-	-cored choke
RFC	2 2·5mH 60n	nÅ se	ctiona	alised choke
Miscellan	eous:			()
		G with	skirt	(3) B9A with skirt
(3). I	B7G screens	(2) B9/	A scr	eens (1), Co-axial
sock	ets (3). Switc	hes. 4	pole	2 way rotary (1) 1
pole	2 way rotary	'(1) c	on/off	togale (1) Mini-
ature	e meter, 50mA	\ f.s.d.	T1.	see text. Flanged
ball	drive. Knobs	etc. C	Cabine	et No. BX5 with
chas	sis 10월 x 4월	x 1÷	in. (F	Home Radio), VFO
box	made from fl	anged	chas	ssis strips CU136
and	CU144 (Home	e Rad	io).	

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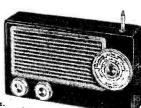
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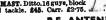
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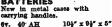
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With S5 at the "Tune" position and a lead from the receiver lying near the transmitter, tune the receiver to 3.5MHz using the crystal marker, tune VC1 to zero beat, and mark the scale for 3.5MHz repeating for 3.6, 3.7 and 3.8MHz. Also mark 3.6as 1.8, 3.7 as 1.85, and 3.8 as 1.9MHz. Continue with the 3.9 and 4.0MHz marker pips, but marking the v.f.o. for 1.95 and 2.0MHz only. If the extreme settings of VC1 have been avoided the 10kHz points can be filled in linearly between the 100kHz points.

A 10mA or multi-range meter is connected from "G" Fig. 1 to chassis, the latter being positive. The v.f.o. is set to 1.9MHz, S6 to 160m, and the core of L2 is adjusted for maximum grid current, which should be around 3mA. Then adjust the v.f.o. to about 3.7 MHz, switch to 80m adjusting L3 core for maximum grid current which will be around 2mA.

TESTING

It is simplest and best to test the whole equipment by feeding the transmitter output into an artificial aerial load. This can be a 15 watt or 25 watt 240V or similar household lamp. Clip it across VC3/4 and chassis, or fit a holder, lead and co-axial plug so that it may always be employed for tests.

P.A. tuning procedure is that generally employed with a pi-network. Check that S7 is closed for 80m, or open for 160m, to match the position of S6. Fully close VC3/4 and also VC2 (to prevent the possibility of doubling in the p.a.). Switch to "Transmit" and open VC2 to obtain a dip in anode current, as shown by the panel meter. Current will be low but loading is increased by opening VC3/4, meanwhile adjusting VC2 for minimum current. As this is done, the minimum current rises, and the 15 watt lamp should light with fair brilliance when the input reaches about 10W.

The d.c. input to V3 anode is anode volts \times anode current, thus 33mA at 300V will be 9.9 watts. A supply voltage of less than 275V is not recommended.

If the transmitter is loaded into the lamp, and a receiver is tuned to the signal, speech should sound clear and well modulated. The receiver should have its aerial disconnected and r.f. gain turned well back, or overloading may cause distortion.

POWER SUPPLY

Fig. 6 is the circuit of a suitable power supply. The mains transformer actually used was a Parmeko P.2931, 250/0/250V 150mA, with SE-05 rectifiers D1 and D2, and Parmeko P.3141 120mA choke. This provided 280V with a load of 120mA. BY100 rectifiers would also be suitable. The voltage obtained when using semi-conductor rectifiers is somewhat higher than with a valve rectifier. Many transformers have winding for valve rectifiers so a 5U4G is a suitable rectifier for a 5V 3A winding, or an EZ81 for a 6.3V 1A winding.

AERIALS

The simplest possible aerial is an end-fed wire. Some lengths will offer such a load impedance that the transmitter can be worked directly into the aerial, on one or both bands. Other lengths present load impedances which are outside those which can be matched by the transmitter, and then propertuning or loading will be impossible. One of the

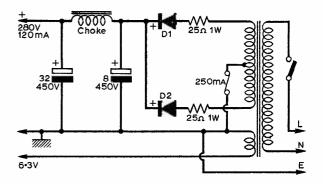


Fig. 6: Suggested power supply for the QRP transmitter.

matching circuits in Fig. 7 can then be used.

Fig. 7(a) is the simplest. L1 may be similar to the tank coil, or be a surplus tapped inductor, or may consist of a number of turns, found by trial and error, on a former lin. to 3in. in diameter.

Fig. 7(b) is similar but has a capacitor VCl added, of about 250pF, which allows more accurate adjustment and has fewer tappings on L2.

Fig. 7(c) is series tuning often used for quarterwave aerials on l.f. bands. VC2 can be 500pF and again L3 resembles the tank coil. The tapping makes L3 into an auto-transformer and may be set about 10 turns from earth for 160m, or 4 or 5 turns from earth for 80m. For the latter band only L3 may have fewer turns.

Fig. 7(d) is parallel tuning suitable for a half-wave aerial on 80m. L4 is about 30 turns on a lin. diameter former, with a 250pF capacitor for VC3 and L5 is about 4 turns of insulated wire over the earthed end of L4.

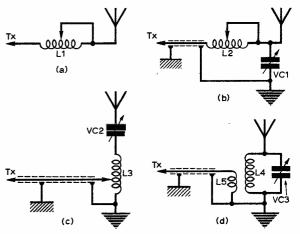
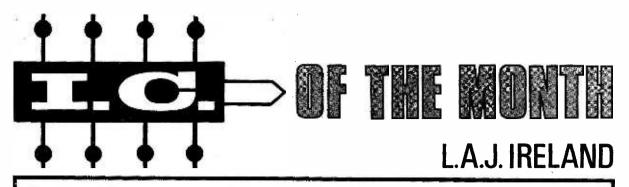


Fig. 7: Four circuits enabling almost any aerial to be matched to the transmitter.

A typical aerial of 126ft in length would be about a quarter-wave on 160m, and a half-wave on 80m, so Fig. 7(c) would be required for 160m, and Fig. 7(d) for 80m working. However, it is generally easier to make up a tuner with one of the circuits in Fig. 7 or a similar circuit and to experiment with tappings until the transmitter can be satisfactorily loaded by the aerial. Even very short wires (under 10ft.) may be used with these circuits but range is much reduced.



Number 22

G.E. PA264-265 Voltage Regulators

ANY constructors will have come across the difficulty of having to operate 6 volt portable transistorised equipment from a 12 volt car battery. In such equipment current drain will usually be dependent upon the audio output so as to conserve the life of the battery and as a result the conventional voltage dropper resistor will not suffice. An alternative approach is to use some form of voltage regulator and lately the G.E. Company have released a monolithic i.c. capable of fulfilling just this function. With a 5 watt power dissipation capability, the i.c. eliminates the need of both a high power pass transistor and its associated drive components and with a half dozen or so discrete components needed to complete the unit, it makes an ideal compact in-line device.

Background

Readers familiar with the present series of articles will remember the precision voltage regulator type LM100 reviewed in the June 1970 issue of P.W. This was a rather sophisticated low-power i.c. in which a built-in reference voltage was compared to a fraction of the output voltage to achieve accurate stabilisation. One of its big draw-backs however was the need for an external power transistor if an output current in excess of 12mA were to be drawn and towards the end of the article attention was drawn to the G.E. unit, type PA264, which would overcome these difficulties but which at the time was only in the development stage of production.

Operation

Basically the PA264 functions as follows. By referring to Fig. 1 it can be seen that Tr1 and Tr2 form a differential comparator whose inputs are controlled by an external zener and a sample of the output voltage. Tr2 in turn directly controls the Darlington pair Tr4 and Tr5. Any tendency in the output voltage to decrease will be counteracted by a drop in voltage at the base of Tr2 which in turn will tend to increase the current through Tr4 and Tr5. The reverse situation occurs if the output voltage tends to increase and so the unit is self-compensating.

The output voltage may be varied in two ways, by potting down the reference voltage applied at pin 14 or by varying the feedback voltage at pin 13. However there are practical limitations to these methods in that the voltages set at pins 14 and 13 should be kept within the limits 1.5-3.5 volts for optimum performance. Values of components specified in Fig. 1 are for a 6 volt output but it should be remembered that any output above 3 volts may be obtained with suitable choice of components. The maximum voltage rating of the PA264 is 25V and of the PA265 '37V and this in fact is the only difference in their electrical characteristics.

Packaging

The units are housed in a rather unusual epoxy package with eight staggered leads in addition to

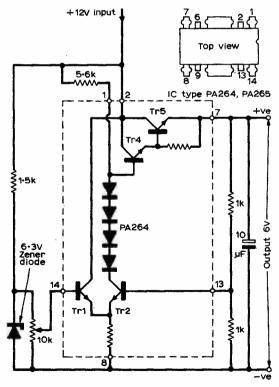


Fig. 1. Circuit of the PA264 with additional components required to provide 6v from 12v supply.

continued on page 322



THE opening of local radio stations on the v.h.f. band and the continual plugging by the BBC of the better quality obtainable with frequencymodulation is increasing the public interest in this area of broadcast reception.

Unfortunately, the claims that reception is interference-free is far from true, and as a result users and engineers may face some tricky problems. While interference from foreign stations, the bane of medium-wave listening, is absent, there are other forms to take its place.

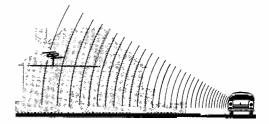
For those living on or near main roads, car ignition interference is probably the most troublesome. This is especially so if the road is on a hill, when not only is the interference generated by a car in low gear much worse, but it also takes longer to pass.

All new vehicles are now suppressed, and have been for the last few years, indeed it has been noticeable that ignition interference has been thinning out, as the older vehicles become fewer in comparison with the new ones. However, there are still sufficient passing on any main road in a given time to cause a number of serious interruptions to any particular programme.

While the irate listener may feel like taking drastic action against the offenders, the solution in this case cannot be applied to the source, and in any case would be illegal! Usually, part of the trouble lies with the aerial. The majority of chimney stacks are already so festooned with Band I and III television aerials plus probably u.h.f. as well, that there just isn't room for a Band II radio aerial. Often, in areas not too remote from the transmitter, quite good signal strength can be obtained with the internal aerial wire running around the back of the cabinet, or at least with one along the picture rail. So the idea of having anything more elaborate seems pointless and money-wasting.

However, although the signal may be strong enough to give reasonable fade-free reception, it is when a splash of interference comes along that the inadequacy becomes all too apparent. The signal-tonoise ratio is just not good enough.

If the chimney looks as' though it just will not stand any more, the answer may be in the loft. A good loft aerial is much less expensive than an outdoor one as it does not have to be weather-proof, or need chimney lashings. It will give a much stronger signal, and being elevated well above the road will be out of the worse area of ignition interference. The directional properties of the aerial will also help as any radiation from directions other than the transmitter will be reduced. If the transmitter direction is away from the road, mount the aerial on that side of the loft as this will put the bulk of the house between the aerial and the road, and so afford a degree of shielding. This really should reduce ignition interference to the level of background noise, if not entirely eliminate it.



Loft aerial positioned on side of house furthest from the main road. House affords measure of screening from ignition interference.

The other form of interference can be more troublesome to deal with. There seems in most of our major cities a proliferation of private radio-telephone installations as used by police, ambulance, taxis and other services. These operate on a number of frequency bands, three of them in the v.h.f. range, 70-85MHz., 103-140MHz. and 168-175MHz. There is also one in the u.h.f. region. The broadcast v.h.f. frequencies of Radio 1, 2, 3, and the local stations lie within the range 88-96MHz. or right in between the two lowest radio-telephone bands, and so are vulnerable to interference from them.

Spurious Signals

To see how this interference can occur, we will review the ways by which spurious signals can be received with a superheterodyne receiver. First, there is breakthrough of signals at the *i.f. frequency*, which in the case of most f.m. receivers is 10.7MHz. The local oscillator has no effect on these, so they would be heard irrespective of the setting of the tuning dial, and in fact, this factor serves to identify them. There are no authorised transmissions at this frequency, so this class of interference should not be encountered unless it was due to a short-wave transmitter operating illegally.

Another form of interference is the well-known image or second-channel type. There are two frequencies that will produce a response in a superheterodyne receiver, one is the sum of the local oscillator frequency and the i.f., and the other is the difference between them. If, as is common practice, the oscillator is running higher than the programme signal, it is operating on the difference, and another signal which is the sum will produce interference.

We can use an example to illustrate: If the wanted signal is at 90MHz, the oscillator is running at 90+10.7=100.7MHz. An unwanted signal will produce the i.f. frequency at the output of the mixer if it is higher than the oscillator by the frequency of the i.f., or 100.7+10.7=111.4MHz. As can be seen, this is within the middle band used by radiotelephone services. Second-channel interference then, arises from signals twice the frequency of the i.f. away from the wanted signal; higher if the oscillator is running high, and lower if it is low. For normal v.h.f. sets the interfering signal would be 21.4MHz higher than the broadcast frequency.

Similar, is the *i.f.* harmonic interference. This is the sum of the local oscillator and half the *i.f.*, and also their difference. Such a signal will produce an output at the mixer anode of half the *i.f.* frequency, and it is the second harmonic of this which will be passed by the *i.f.* circuits.

Using our above example, the local oscillator frequency is again 100.7MHz, and the interfering frequencies will be 100.7+5.35=106.05MHz and 100.7-5.35=95.35MHz. In relation to our wanted signal of 90MHz, the frequencies are plus half and 1^{1}_{2} times the i.f. Harmonics are not usually as strong as the fundamental, so interference from this cause is not so likely to give trouble unless the unwanted signal is very strong.

A further type is the *beat interference*. This occurs from a signal that is spaced from the wanted signal, either above or below, by the i.f. frequency, and is caused by the two signals beating together to form a resultant at the i.f. frequency. Actually, the interfering signal performs the same function as the local oscillator, only of course it carries its own modulation which is passed on through the i.f. stages and detector along with that of the wanted signal. If the interfering signal is strong enough, the set would continue to work with the local oscillator stopped, and this fact could be used to help identify this form of interference. Thus for a wanted signal of 90MHz, beat interference would be caused by signals at $79 \cdot 3MHz$ and $100 \cdot 7MHz$.

Finally there is the interference caused by oscillator harmonics. All oscillators produce harmonics, and the second-harmonic of $100 \cdot 7$ which you remember is our local oscillator frequency for receiving a signal at 90MHz, is $201 \cdot 4$. Signals spaced above and below this by the i.f., i.e. $201 \cdot 4-10 \cdot 7=190 \cdot 7$, and $201 \cdot 4+10 \cdot 7=212 \cdot 1$ MHz, would therefore be passed into the i.f. circuits.

These frequencies are in the commercial television band and above the highest radio-telephone range. The third-harmonic of the oscillator would bring it even higher. Frequencies so remote from the wanted ones should be greatly attenuated by the tuning in the r.f. circuits and the tuned aerial, so should not present any problems. If though it is found that commercial t.v. signals are breaking through, this is the probable cause.

Summing up then, interfering signals can be spaced from the wanted one by twice (second channel); 1^{1}_{2} times (i.f. harmonic); once (beat interference); and half (i.f. harmonic) times the i.f. frequency, on the high side; and one (beat interference) times on the low side. So there are at least five possible frequencies that will interfere with each and every broadcast station. As there are four BBC programmes in most areas, this gives us some 20 possible interfering frequencies. The situation is aggravated by the fact that f.m. receivers are not sharply tuned as are a.m. sets. It is of course necessary to maintain a wide pass-band because of the nature of the f.m. signal. Broadcast deviations are up to 75kHz either side of the carrier frequency, so receiver circuits must extend well beyond these limits.

This means that interfering frequencies do not have to be spot on the values calculated, and if only near them, interference can result. With the previously noted increase in radio-telephone users, it can be seen that the possibility of interference with broadcast programmes is high, and is steadily increasing.

Radio-telephones

The question is, what can be done? Mobile units are not so much a nuisance, as they operate at low power, and usually cause interference only when they are fairly close to the receiver. The chance of a mobile operating at a frequency which could cause interference, coming sufficiently close to a working f.m. receiver tuned to a vulnerable frequency, is not very great, and the odd occasion when it may occur could hardly constitute a major nuisance.

It is the base stations that are the real menace. These are operating more or less continually, and are relatively high powered. Should one of these be within a few miles and operating on a critical frequency, then constant jamming will result.

The first step is to try to identify the offender. This is not too difficult as a number of his messages are being unwillingly intercepted. The class of business can be quickly deduced, and a local knowledge of the businesses of that type large enough to operate radio telephones, will help to narrow things down. One clue is whether the interference is present in the evenings or at week-ends. If it is, then a business that offers service outside normal hours will be the obvious culprit.

After eventually identifying the source, one can try swinging the aerial away from the direction of the transmitter while not losing too much of the broadcast signal. A local road map will help to obtain the precise directions involved. Do not swing too far away from the BBC station though, as the received signal may then be reflected and suffer phase-distortion, which is similar to ghosting on a television picture.

The next step is to find out the exact frequency of the transmitter. Once the owner has been identified, this should present no problem; if the reason for requiring the information is explained, he will no doubt be willing to co-operate. He may not know the frequency, perhaps being non-technical, but this should be shown on the transmitting licence or other paperwork connected with the system. The relationship between the frequency and that of the broadcast signal with which it is interfering can then be seen and the type of interference identified.

If it has not proved possible to discover the source of the interfering transmission, it may be possible to deduce the type of interference from the clues given above, and so arrive at the possible frequency. For example, stopping the local oscillator (without shorting-out the input signal) will determine whether the interference is due to a beat-signal. If this is found to be the case, the frequency will be spaced either above or below the wanted signal by an amount equal to the i.f. So if receiving a station on 90MHz, the interference will be either $79 \cdot 3$ or $100 \cdot 7$ MHz. As the latter does not fall within the band used for radio telephones, then it is fairly certain that $79 \cdot 3$ MHz or thereabouts is the offending frequency.

Co-axial Stubs

Having discovered the interfering frequency, the next thing is to suppress it (electrically of course). One method of doing this which is often recommended is the parallel stub of co-axial cable. Co-ax exhibits the properties of inductance and capacitance and so will form a resonant tuned circuit. With a velocity factor of unity, the length of the stub should be a quarter of the wavelength of the signal it is desired to eliminate. It should then be connected in parallel with the aerial-feeder near to the aerial socket on the receiver, the free end being left opencircuited.

In theory then, it is a straightforward matter to calculate the length and connect up. Not so in practice. First of all, the velocity factor of the co-ax is not unity, but varies from one sample to another. Typical values are 0.67 for the solid dielectric type, and 0.85 for the semi-air spaced variety. This must be multiplied by the quarter-wavelength to arrive at the actual length, so an exact calculation with any sample of co-ax is not easy.

There is a further complication; much depends on the characteristics of the aerial input circuit, whether it is inductive of capacitive. At a frequency higher than resonance, a tuned cricuit appears capacitive, whereas at a lower frequency it is inductive, the two balance out only at the resonant frequency. The receiver aerial circuits will be tuned to the wanted frequency, so at an interfering frequency, the circuit will appear either inductive or capacitive depending on whether the frequency is higher or lower than the wanted one, and the degree of inductance or capacitance will depend on the spacing of the frequencies and the Q of the circuit.

It can be seen then, that cutting a stub to the exact size is very much a matter of chance. The recommended method of tuning the stub is to cut it longer than the estimated length and cut off sections about 1_2 inch at a time until the minimum level of interfering signal is attained. To do this as with most tuning procedures, it is necessary to go through the resonant point to ensure that the peak (or trough in this case) has been reached, and then tune back. Obviously it is not possible to stick back on the last few sections that have been chopped off, so the thing to do is carefully note how much has been removed since the signals started to increase, and then measure up a new stub made from the same type of co-ax.

Severe interference was being experienced on the author's own set-up which consisted of a separate f.m. tuner feeding the hi-fi system. The trouble was with the reception of Radio 3 from the Wenvoe transmitter which uses the frequency of 96.8MHz. Programmes were completely blotted out when the interference occurred, not only during the day but up to late at night and also at weekends. It was impossible to enjoy a concert, and tests with other f.m. receivers in the neighbourhood confirmed that they too likewise suffered. Their owners either put up with it, switched to a.m., or just didn't listen to Radio 3.

It was obvious from the messages received that the source was a television repair shop controlling its service vans. The fact that a number of vans were apparently in communication indicated a business of some size, and also the evening and weekend operation narrowed down the field among the local firms. A few phone calls to the short-list of suspects revealed that it was the local Rediffusion workshop. The chief engineer was co-operative and apologetic, offering to check the frequency of the transmitter and that it was duly suppressing its harmonics, but of course the frequency was assigned by the Post Office Telecommunications Department, and there was nothing he could do about that.

He was able to state the frequency which was $85 \cdot 725$ MHz. It then became obvious that this was a case of beat interference, as the frequency is $10 \cdot 7$ MHz away from $96 \cdot 425$ MHz, which is just $0 \cdot 375$ MHz off the Radio 3 centre frequency. It was an obvious boob by the Post Office in assigning so critical a frequency to a powerful base station. Admittedly, frequencies are scarce and the demand is great, but troublesome frequencies such as these could easily be assigned to mobiles.

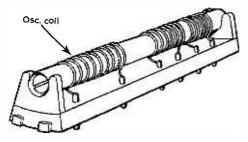
An interference form was obtained from the Post Office, and all the details as to source of interference, frequency and type were included and duly sent off. However, nothing more was ever heard, and as the interference continued it appears that nothing was done by way of re-allocating the frequency.

Series Wavetrap

It was therefore decided to tackle the problem without G.P.O. assistance. First of all, stubs were tried, but the difficulties previously described foiled success with these. Unfortunately, the Rediffusion base was in exactly the same direction from the aerial as the Wenvoe transmitter, so no rejection could be obtained by swinging the aerial. Nonetheless it was tried, and although the f.m. signal dropped, the interference decreased more so, so some improvement in signal interference ratio was obtained.

Finally the possibility of a series resonant wavetrap in the aerial feeder was considered. A coil resonating with its self-capacity and tuned with a brass slug was needed to enable a quick and convenient adjustment frequency adjustment to be made. The problem was, how to make one with any degree of accuracy that would not need lengthy experiments with the intermittent signal source similar to a stub.

Looking around the workshop for some readymade component which might fill the bill, attention turned to some old coil biscuits from scrapped television tuners. A channel 2 oscillator biscuit was found among them. The BBC station on channel 2 operates at $48 \cdot 25$ MHz (sound). The sound i.f. for the set concerned, and which is now common for most modern t.v. receivers, is $38 \cdot 15$ MHz. This means that the frequency of the oscillator coil was $86 \cdot 4$ MHz. As the Rediffusion frequency was $85 \cdot 725$ MHz., this was near enough to be within the tuning range of the coil.



Appearance of typical coil biscuit. Oscillator coil is usually the largest and contains a tuning slug.

Accordingly it was connected in series with the aerial feeder, and the interference was completely eliminated, without the need even to tune the coil.

Most t.v. workshops have old tuners knocking around, so a call at the local radio dealers could well produce a coil suitable for the purpose, should similar interference be experienced. The chart shows the frequencies of the main BBC band I television channels, and assuming a $38 \cdot 15$ MHz sound i.f., the actual tuning range of an oscillator-coil biscuit. It will be noted that channels 3 and 4 coils will tune to frequencies within the v.h.f. radio band, so will be no use as wavetraps for radiotelephone frequencies as these are all outside this band. Channel 5 is just at the start of the medium radiotelephone band, and could easily tune to some of its lower frequencies.

TELEVISION CHANNEL	SOUND FREQUENCY	OSCILLATOR COIL FREQUENCY
1	41.5MHz	79·65MHz
2	48·25MHz	86·40MHz
3	53·25MHz	91·40MHz
4	58·25MHz	96·4MHz
5	63·25MHz	101·4MHz

Remember, too, that the range of the coil can be extended by the fitting of a different type of tuning slug. A brass slug will decrease the inductance, hence increase the frequency, while an irondust slug will increase inductance and decrease the frequency. If the range is still outside the interfering frequency, a couple of turns taken off the coil will push it higher, or a small capacitor of a few pF. will bring it lower, if wired in parallel. The biscuit may have two or three coils on the same former, the oscillator is the one nearest the open end and which has the tuning slug. The other coils are coupling coils and should be ignored.

Direct Conversion Receiver continued from page 300

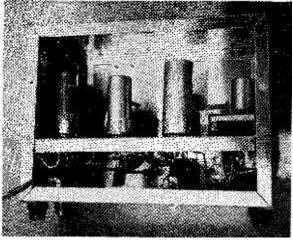
for h.t. positive, black for chassis and some other colour for the 6.3V heater supply.

ALIGNMENT

Set TC2 and TC3 about half closed and tune in any signal, with VC3 nearly open, and adjust TC2 and VC1/2 for best volume. Find a signal with VC3 nearly fully closed and peak VC1/2 for best results, then rotate the core of L1 for maximum volume.

If necessary, the core of L3 is rotated to obtain suitable band coverage with VC3. The coverage of VC3 can be checked by placing the aerial lead of a calibrated receiver near L3 and listening for the carrier produced by V3.

At all times the r.f. gain control VC1/2 is adjusted as needed for best reception even though VR1 may have to be turned back with strong signals. The cores of L1 and L2 are adjusted around 3.5MHz and the trimmers TC2 and TC3 are set near 3.8MHz. TC2 may also need re-adjustment after changing the aerial. These circuits are merely peaked up for



Rear view of the finished receiver.

best volume and are not too critical. The extent of rotation of this control needed to tune from $3\cdot 8-3\cdot 5MHz$ can be increased by screwing down TC2 and TC3 and unscrewing the cores of L1 and L2 to compensate.

Power Supply. Any supply giving about the outputs mentioned should be satisfactory. If a power pack has to be made, one with full-wave rectification is most suitable. This may employ a 250/0/250V 60mA, $6\cdot 3V$ ($1\cdot 5A$ or 2A) transformer, with smoothing by means of two 16μ F 350V capacitors and a 60mA choke.

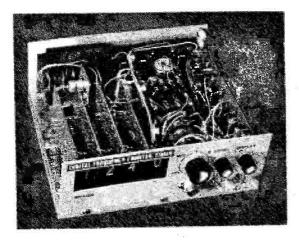
Speaker and Phones. A reasonably large 2/3 ohm speaker is most suitable with a cabinet or baffle.

When phones are plugged in, the mis-match can generally be disregarded. Inexpensive surplus 600 ohm phones will be found to work well. It would be possible to use an external matching transformer for high impedance phones or to feed them through reliable isolating capacitors from V4 anode.

Aerials. Numerous transmissions were received with a short indoor aerial but changing to an outdoor wire tuned as for transmission purposes naturally gave a great increase in range and volume. In practice, any end-connected wire can be taken to A1 or A2 while the A2 connection is most suitable for short aerials.

IN NEXT MONTH'S WIRELESS

DIGITAL FREQUENCY COUNTER/TIMER



HARMONIC SIX'

ALSO:

THE



Yesterday's dreams have a habit of becoming today's realities in the field of electronics. Five years ago direct readout frequency meters cost so much that many companies flinched at the price but today inexpensive integrated circuits have brought these into the bracket for the home constructor.

Just imagine. Pop in any frequency (below 20MHz) and there you are—it's displayed before your eyes to the nearest cycle! The Digital Frequency Counter/Timer makes use of four digit neon numeral tube displays and uses the widely available "74" series of TTL i.c.'s.

Certainly this is a complex project—theoretically—but it's the i.c.'s that do the work, not you, and this project could be tackled by anyone who can wield a soldering iron.

THE HARMONIC SIX RECEIVER

This is a six transistor superhet covering all the popular short wave bands and designed to power either a loudspeakep or headphones. The unusual feature is that there is no oscillator switching—instead the 2nd harmonic of the oscillator is used.

Standard parts are used throughout and this together with the fact that it's designed by one of our top authors, makes this a first class project.

MINI-AMPLIFIER

Although measuring only $2'' \times 1'' \times 1''$, this amplifier, using four silicon transistors has an output of 250mW into a 250 loudspeaker. A multitude of uses can be found for this project which can be built for a total cost of no more than, $\mathcal{E}_{1,2}$

ALL IN THE SEPTEMBER ISSUE ON SALE AUGUST 6th

HARMONICESIX



W E thought very carefully before calling this article the PW Treasure Tracer. Certainly this sounds better than "metal locator" but could we justify the title? We think we can, especially after our test. We found nothing of great value but judging by the results we could have, that is, if there had been any there. Even if valuables are not found, certainly a whole lot of extremely interesting items will be and the history of an area of ground will yield up its secrets. However, your chances of finding coins are very good—about 150,000,000 coins are lost every year and a high proportion of these must be lost in areas where they can be found using a device of this type.

Not many months ago a hoard of Anglo-Saxon coins was found, using a metal locator, these were later auctioned for £9,000. It shows what can be done.

Metal locators work on a variety of principles and the author has experimented with a number of different circuits. Nearly all rely on the fact that metal objects distort magnetic fields. Complex designs have appeared from time to time making use of various effects—each claiming to be an improvement over others—but the author's experience has not borne out these claims. The principal used here the Beat Frequency Type—is possibly the oldest and certainly the simplest. It needs only one wound coil, unlike many other circuits, and the sensitivity and results are excellent. We are deliberately not overstating our claims and the only figures for range etc. are those proved by our tests.

The Treasure Tracer comprises two low power r.f. oscillators working at about 130 kHz. One of the oscillators is screened inside the chassis and the frequency can be altered over a fairly wide range to match it close to the other. The second oscillator uses a frequency determined by the inductance of a winding which is used as the search coil.

In the absence of any material which will affect the inductance of this search coil, the oscillator is at one frequency. However when this coil is moved near some metal object, the inductance is altered slightly and the frequency of oscillation is changed. If the oscillators are set closely together an audio beat note is produced (equal to the difference in frequency) which may be amplified to feed a loudspeaker.

Finding a small copper clip (Item 16). The grass guard made from Perspex can be seen fitted under the coil framework.

Searching along were cart fitting places should ge



Let us assume that the search oscillator is working at 130.0kHz. The reference oscillator is adjusted to say 130.2kHz. The two signals are mixed together producing notes of $130 \cdot 2 - 130 \cdot 0 = 200$ Hz. There is also another frequency produced, the sum of the two, $260 \cdot 2 \text{kHz}$, but this can be ignored.

The presence of a metal object near the search coil will increase the inductance causing the frequency of the search coil oscillator to fall to say 129.8kHz. The beat note will now be $130 \cdot 2 - 129 \cdot 8 = 400$ Hz so the raising of frequency of the beat note will thus indicate the presence of a metal object near the coil.

From this theory the Treasure Tracer was built, using a frequency below 150kHz to conform to regulations. Initial tests in the lab showed that the prototype was working reasonably well and that a definite beat note was obtained-but how would it work in practice?

THE TESTS

The first test was arranged at the PW offices. A couple of dozen telephone directories were piled two high (making for a thickness of at least two inches) and coins ranging from ${}^{1}_{2}p$ to 50p were hidden under certain piles. All coins were found immediately, but there was an extra reading-this turned out to be the wiring under the floor!

These tests in themselves were interesting and we were slightly encouraged but how would the metal locator (for we were still calling it that at this stage) fare in a field test? Only one way to find outarrange one.

One Monday in late May Eric Dowdeswell (PW Editorial), Peter Metalli (Art Editor), Jack Wood (Photographer) and the author set out for Canvey Island in South Essex to put it to the test.

The weather was fantastic and the beach was far from empty and under the puzzled eyes of day trippers we began our search, panning up and down the beach, just above the water line.

Our hearts fell. For several minutes the whistle remained unaltered. Up and down we panned and gradually we began to think that the journey was wasted. Then suddenly the note changed frequencya very definite, strong reading. As we dug Jack Wood

an old track. All we found here s (Items 1 and 26) but such enerally be more fruitful.

Money! Right against the sea wall we

photographed us and the picture is that used on the cover. A quick dig produced a rusty hinge about three inches under the sand. We must have been unlucky to start with for after our first "find" we got readings every few yards. The items we found on this short stretch of beach and at other locations tried on the test are shown overleaf.

One thing cursed the search-silver paper. We found it everywhere and it accounted for over 75 per cent of all readings. We couldn't ignore these of course, for until we dug we didn't know what was causing the note to change frequency. The silver paper was from ice cream wrappings, cigarettes and sweets and even pieces so small that they were only found after extensive sifting, gave strong readings.

We altered our technique because of the sensitivity of the Treasure Tracer to small objects. As soon as we obtained a reading we carefully located the exact position before we began to dig---this could be done within an inch or two. As we dug we put the sand in two piles and checked at intervals with the Treasure Tracer that there was still a reading in the original position. If we had found nothing and the reading had disappeared we checked the two piles of sand. Invariably the metal was found in one of these. Even quite careful digging did not stop us missing several items the first time around.

Our deepest find was at 9in. The strength of the reading confused us at first-it was too strong and over a fairly wide area. The "treasure" turned out to be an aerosol can for retouching cars, a beer can of similar size was found at 4in with less trouble. The reading at 9in. was strong and it would be fair to assume that if the can had been deeper it would still have been found.

We were very successful near the sea wall where people were sunning themselves but due to the numbers already there we could only try a few yards of this but it was here that we found our only coinwhich turned out to be a 1966 penny, badly corroded. We had expected to find more money and because of our failure to do so we arranged a test. One person buried coins of various sizes in a marked off area and we tried to locate them. These tests were successful and convinced us that we could unfailingly find all coins at depths up to four or five inches and larger coins at even more.

> The one that got away! The tide came in so fast that before we had time to dig out the "find" the water put an end to it.



found our only coin-a 1966 penny, badly corroded.







3

11

22

6

16

23

26

13

- Cart fitting (?). Found on the old farm road at 2″ down.
- 2 Boiler clinker (?).⁵ Gave strong reading: 1" down.
- 3 Sheet metal handle, badly rusted. Found in author's garden at $2\frac{1}{2}$.
- 4 Iron Hinge. Our first find, 3" under the sand.
- 5_ Nail found under the beach, ¹/₂ down.
- 6 Copper gasket ring (?). Found under the beach at 6".
- 7 Shrapnel: Author's garden at 2"
- 8 Sharp metal spike. On the beach at 3".
- 9 Screw eye (from clothes line ?). Author's garden, 2" down.
- 10 Small piece of torn metal. Beach at 3".
- 11 Copper tube (squashed). Author's garden, 2″ down.
- 12 Piece of unidentified iron. Beach at $1\frac{1}{2}^{\prime\prime}$.
- **13** File badly rusted. Garden at $2\frac{1}{2}$ ",
- 14 Plant label (?). Zinc, garden at 4"
- 15 Shrapnel. Garden at 1",
- 16 Copper clip. Beach, found at 3%
- 17 Shrapnel, gun metal, beach at 4".
- 18 Screw-on bottle top, beach, 1" down.
- 19 Shrapnel. Author's garden at 3".
- 20 1966 penny. Beach at 3".
- **21** Encrusted iron fitting. Under the beach at $1\frac{1}{2}^{"}$.
- 22 Thin copper tube (squashed). Beach at 2".
- 23 Copper tube (squashed). Author's garden at 2".
- 24 Piece of cast iron. Beach at 3".
- 25 Nail with small piece of wood attached. Beach at 1".
- 26 Cart fitting. Old farm road at 4".
- 27 Galvanised washer. Author's garden at 3½". Looked just Jike a coin until cleaned up.
- 28 and 29 (not shown) Aerosol can and beer can. At 9" and 4".

14

20

24

As we progressed experience enabled us to locate more accurately and our ears became more and more sensitive to changes in the note.

Just one word of caution. The beach will provide finds of all types but be careful near the water's edge. The spray landing on the search coil sent it haywire and searching became almost impossible. Later tests carried out in the light rain proved fruitless for the same reason. Not only does the impact of the spray or raindrop change the note but water trapped in the turns alters the inductance of the coil. As the water evaporates the pitch of the note changes—the effect lasts several minutes during which searching is impossible.

The second part of the test was made on the outskirts of a nearby castle. Not unreasonably the custodians would not let us search in the grounds but recommended trying outside, pointing the way to the original approach roads. A number of items were found, though none of any great age.

The final test was conducted in the author's garden in north-east London. Surprisingly most of the items were found at the same depth under the lawn. When a reading was obtained a circle of turf about 6in. in diameter was cut out, the item was found and the earth replaced, laying the turf back in position; in this way no damage was done to lawn.

The house was built in 1913 and the lawn is probably original. The objects found were probably from the building process, spread out before turfing —though the file was probably lost by some workman long ago.

Some pieces of shrapnel were found. This is not really surprising for at the height of the London Blitz the fire from the anti-aircraft guns was so heavy that shrapnel apparently came down almost like "hail stones," according to a neighbour. Most of the shrapnel was cleared up but quite a lot would have buried itself in the ground.

A grass guard was developed from experience, this can be seen in the photographs. It is a piece of Perspex, $6 \times 6in$. fixed to the bottom of the search coil framework to stop blades of grass from touching the coil and so cause the beat note to change.

A total of four hours test searching was carried out to produce the finds shown. In that short period we became very much better at identifying signals and in the end knew exactly where to dig and even how deep we could expect to find the metal object.

HOW TO BUILD THE P.W. TREASURE TRACER

The circuit of Treasure Tracer comprises three distinct sections: the search coil oscillator, the reference oscillator and the audio amplifier.

The search coil oscillator is made around L1 which is wound on a wooden framework shown in Fig. 1. This is made up from two 6in. lengths of hardwood batten with a section of $1 \times {}^{3}_{4}$ in., though this section is not critical. These should be made into a cross by half-lapping as shown and small V shaped grooves cut into the ends. This framework must be rigid and if poor joints are made, these should be firmly glued.

The handle is made up from wood of the same cross section as the coil framework and about 4ft.

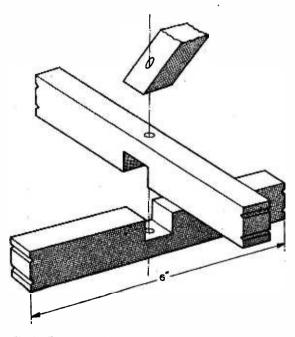
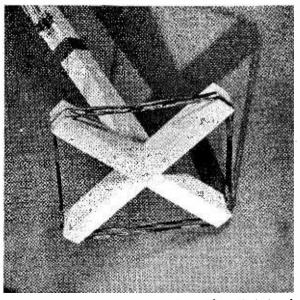


Fig. 1 : The construction of the search coil wooden framework.

in length, though this will depend upon the height of the user. The base of this should be cut at 45° and screwed firmly to the coil former. A normal type screw can be used; it will alter the inductance of the coil but as it is a constant it does not affect operation.

A small three way stand off tag strip should be mounted a few inches from the bottom to provide a firm anchorage for the coil wires. A thin enamelled copper wire should be used; the gauge is not too critical and 32 to 38 s.w.g. will do. If the wire has to be specially bought, 36 s.w.g. (as used in the prototype) would be a good choice. The start of the wire should be soldered to one of the outside terminal tags and 48 turns should be wound in the upper grooves, ending by fixing to the centre terminal tag.

The second part of L1 is wound in the lower



The search coil. Note the terminal tag at the top left and the taping of the wires.

grooves, again 48 turns, anchoring at the centre and other outer terminal. Both coils should be wound in the same direction and the centre terminal used only as a convenient centre tap which is needed for the circuit.

All windings should be tight, including the leadups to the terminal tag. Once completed the windings should be taped together at several points to hold them firmly.

It should be emphasised that the successful operation of the Treasure Tracer depends largely on the care taken in the construction of this search coil and loose windings will make operation very difficult and unreliable.

L1 is connected into the collector circuit of Tr1 as shown in the circuit diagram in Fig. 2. C2, shown as a 500pF capacitor, is connected across the coil and this combination will resonate at about 130kHz. The value of C2 and C4 (in the reference oscillator circuit) should be of the same type and reasonably close in value; miniature 5 per cent polystyrene types are very good here and inexpensive. It doesn't matter too much what their values are as long as they are the same, but to stay within the regulation frequency band they should be over 390pF.

The components in the search coil oscillator are connected to form a Hartley oscillator, working at the frequency mentioned. R1 provides the base bias for Tr1 and C1 provides the feedback signal to maintain oscillation.

A low value resistor, R3, is connected in the emitter and this is shared by Tr2 which forms the reference oscillator.

L2 is a standard Denco LW aerial coil which is fitted with the three windings necessary. The main one (between points 1 and 6) is tuned by C4. Another of the windings is arranged to feed back to the base forming a blocking oscillator; this also carries the base bias to Tr2.

The shared emitter resistor R3 means that there is a mixing action in Tr2 and a degree of the search coil oscillator signal is mixed with that of the reference oscillator to make the beat note.

It is necessary to tune one of the oscillators to

bring it close to that of the other and here the reference oscillator can be tuned over a wide range by altering the position of the ferrite dust core. The coil should be mounted as shown in Fig. 3 with a small knob fixed to the brass thread attached to the dust core.

The take-off point of the coil comes from the third winding of L2 (between pins 8 and 9). This is d.c. blocked by C5, detected by D1, smoothed by C6 and applied to the base of Tr3.

The signal here will be the beat note or an audio

Fig. 2 : The complete circuit for the P.W. Treasure Tracer.

★ components list Resistors $330k\Omega$ R5 820kΩ R1 R2 $4.7k\Omega$ 22kQ R6 **R**3 27Ω **R7** 120Ω $390k\Omega$ R4 All &W, 5% types. Capacitors **C**1 47pF C5 1000pF C2 500pF† C6 0.01µF **C**3 0.1µF C7 100µF 6V 500pF† 100µF 25V C4 C8 † see text Semiconductors Tr1 2N2926 Tr3 2N2926 Tr2 2N2926 D1 OA91 Tr3 2N2926 Miscellaneous L1-see text and drawings Denco LW aerial coil, Type 1T L2 LS 75-80Ω miniature loudspeaker JK1 3-5mm jack socket with cut-out switch SW1 On-Off slide switch PP3, 9V battery **B1** Chassis 63 x 23 x 13in., (H. L. Smith Ltd. 287/9 Edgware Road, London W.2.) 60p inc. postage.

frequency represented by the difference in frequency of the two signals.

The base bias for Tr3 is provided by R5 with R6 acting as the collector load.

Tr4 further amplifies this audio signal and applies it to the 80Ω loudspeaker in the collector. R7 and C7 are included to raise the emitter voltage of Tr4 and to limit the quiescent current. The impedance of the

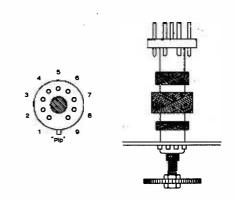
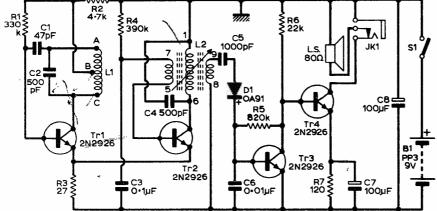


Fig. 3 : The pin numbering and mounting of L2.



loudspeaker can lie between 35Ω and 80Ω and various miniature types with impedances in this range are available. If difficulty is experienced in obtaining one of these, the loudspeaker can be replaced by a transistor output transformer (such as the Eagle LT 700) feeding a lower impedance loudspeaker.

There is a tendency for the two r.f. signals to lock together if they are within a few Hertz of each other. This is not too serious but the inclusion of R2, which drops the supply to Tr1, reduces this tendency. Theoretically the junction of R1 and R2 should be decoupled to the negative line using a 0.1μ F capacitor; this however made no difference in the prototype but may be included if Tr1 fails to oscillate.

Note that the chassis is connected to the positive rail rather than the more conventional negative line. This enables simple fitting of the jack socket, JK1, one connection of which has to touch the chassis.

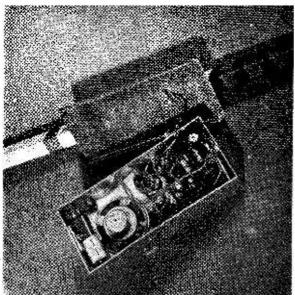
CONSTRUCTION

The majority of the components are mounted on a small piece of 0.15in. matrix Veroboard, 16 holes by 13 holes and this is shown in Fig. 4.

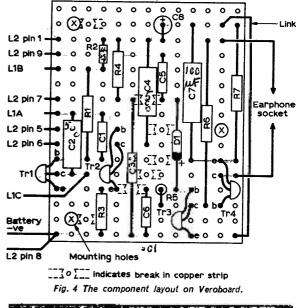
The chassis used in the prototype, and highly recommended, is available from H. L. Smith Ltd. (see components list) and the bottom of this is drilled as shown in Fig. 5. The three holes in a triangle are fitted with lin., 4BA screws and the component board is mounted on these, spaced off by means of nuts.

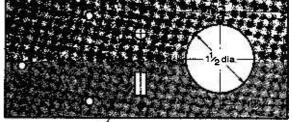
The loudspeaker can be glued in place and the wiring between the Veroboard and the other components is shown in Fig. 6.

The recommended chassis comes with a lipped lid which is screwed to the wooden handle as shown in Fig. 7. A hole ${}^{1}_{4}$ in. in diameter is fitted with a rubber grommet to take the wires leading to the search coil L1. Stiff wire should be used to run between the chassis and the terminal tag and this should be firmly taped to the handle as shown in the photographs. A small loop is left before entering the chassis to enable it to be opened.



An internal view of the completed prototype.





Cutout to suit switch Fig. 5 : The drilling of the bottom of the chassis.

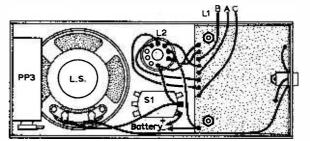
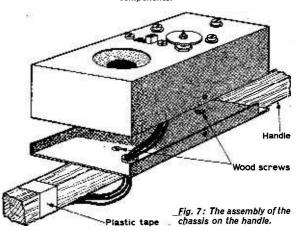


Fig. 6 : The wiring between the component board and the other components.



TESTING

Once all wiring is done a visual check should be made to ensure all is well and this being so, the Treasure Tracer can be switched on.

If all is correct the tuning of L2 will produce two positions where a strong beat note can be heard.

A number of weak signals may be heard at other settings. These are probably caused by radio signals on those frequencies but they are very low compared to the main signals.

The beat note should be set at the lowest stable audio note---probably between 50Hz and 200Hz. When a metal object is brought near L1 the note will either go up or down, depending on whether the search coil oscillator is working higher or lower than the reference oscillator.

By experience it was found that is was better to arrange for the note to go *down* in frequency when a metal object was approached but this is up to the user—a rising note may be preferred.

Certain objects—especially brass—go against the general trend and operate in reverse—causing the note to rise when iron and aluminium cause it to fall.

No volume control is fitted as the output from the loudspeaker is fairly low—about 75mW, though this proved sufficient and was not found too low even by the sea shore. Headphones or earpieces with impedances between 50Ω and 4000Ω all work when plugged into the socket—this automatically cuts the loudspeaker out if wired as shown.

The current consumption is not too high—it should certainly be under 20mA and several hours of searching are possible using the PP3 battery specified.

Before carrying out your first search, eliminate as much movement of the leadup wires as possible by taping them, as even a mild breeze will cause a change in note otherwise.

In testing it will be found that nearly all large objects cause some change in frequency—even laying the coil on the ground— but these changes will be minute compared to that caused by even a small piece of metal.

Do not expect to become an expert in a few minutes. The use of a device of this type needs a degree of skill and it took all of us several hours before we became reasonable at it. Now, after the test, we have used the detector to find a whole mass of new material, including more coins, but this was outside the testing period and the finds were not witnessed so we are not including later items in the list.

Well, where do you search? Note that there are very heavy penalties for using such a device in areas scheduled as being of historical interest and there have been prosecutions for this. However there is no need to search in such places and paths or

To conform with the Wireless Telegraphy Act (1949) a licence is required to use the Treasure Tracer described here.

Under Section 1(1) (Pipe Finder Licence) the band 16 to 150kHz can be used for equipment of this type.

A licence for five years costs 75p and can be applied for on a form obtainable from the Ministry of Posts and Telecommunications, Waterloo Bridge House, Waterloo Road, London S.E.1. roads that have been in use for centuries are a good place to start; river banks will also prove fruitful.

An excellent small book "A Fortune Under Your Feet" by E. Fletcher elaborates on this and is recommended reading for those encouraged by early results.

If you find something of interest, let us know. We are offering £2 for the most interesting letter we receive dealing with objects found. It doesn't have to be valuable, just as long as it is interesting.

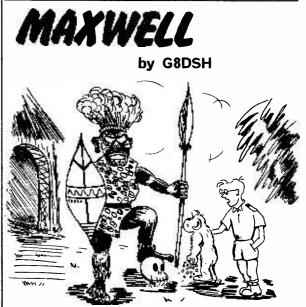
I.C. of the Month—continued from page 310

two heatsink tabs. If the i.c.'s are to be used to their full 5 watt rating some form of additional heatsinking is needed. This may take the form of directly soldering about two square inches of copper to each tab or alternatively to equivalent area of printed circuit board foil. At any rate, in most applications the full output ratings will not be approached so that the above precautions are necessary only for worst case operating conditions.



View of I.C. showing unusual heatsink tabs and staggered leads.

To find out the maximum output currents that the units can deliver all one has to do is to determine the product of the voltage drop across terminals 2 and 7 of the i.c. and the current drawn, making sure that the answer does not exceed 5 watts.



"He says never mind the beads—have you got any back numbers of Practical Wireless ?"



NOW THAT GORDON KING HAS COVERED THE BASICS OF FAULT-FINDING CO-AUTHOR 'MAC' HELLYER DISCUSSES THE PROBLEMS OF RECEIVER ALIGNMENT WITH PARTICULAR REFERENCE TO THE TEST EQUIPMENT NEEDED FOR THIS TASK.

E NOUGH has been said by Gordon King in the earlier parts of this series to absolve me from a tedious description of the make-up of superhet circuitry. In this section, we shall now be able to concentrate wholly upon alignment of the a.m. and the f.m. receiver.

A little theory must creep in since the most practical of readers should still be blessed with some natural curiosity. We need to know why we are twiddling that screw, that slug, that bit of wire, and not just be content to follow a mechanical sequence of instructions.

Servicing consists very largely of using one's native wit to interpret or augment the information given by manufacturers. In many cases, handling a piece of equipment that may be obsolete or, even if new, backed by the most meagre data, one has to fall back on one's knowledge of basic principles and experience of designers' whims to solve some very tricky problems.

Our intention here is to provide a few short-cuts toward those neat solutions. So general principles have to be the order of the day. There will always be exceptions in design, so long as there are exceptions in men. Bravo! say I—there is no more hideous prospect than the "People's Set", which can be serviced by numbers, or, more likely if the doubleentry cost-watchers have their way, thrown away when it goes wrong! We all saw what could happen, on page 1030 of the April issue of PW. ("The Committee Supet-FET".)

AM ALIGNMENT

Gordon King has said, already, that a.m. receivers are still stuck with capacitive tuning, although the f.m. receiver, and, particularly, the combination a.m./f.m. set, may have tuning gangs plus variable inductors plus potentiometer plus fixed tuning all wrapped up in one package.

If alignment has to be carried out, begin by sorting out the a.m. section, identifying the stages (see Part 2) and then making up your mind what kind of circuit you are about to tackle. This is assuming that you are not able to get the manufacturer's detailed information, always supposing he has got around to preparing it for publication!

The tuning I have spoken about is the 'front-end' tuning, where the frequency of an oscillator beats with that of the incoming signal to provide a steady intermediate frequency, the i.f. So, before we can tackle the front end, we must make sure the several

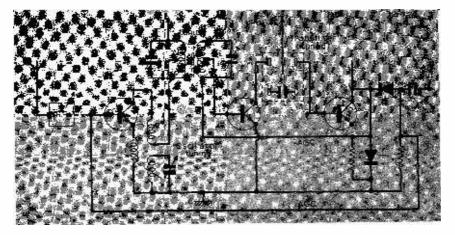


Fig. 1: The skeleton circuit of the tuned section of a typical a.m. receiver. The fixed tuned Transfilter, now becoming quite common, helps to reduce the amount of re-alignment required.

parts of the i.f. circuitry are doing their job. But before we can do this, it is necessary to check the audio section and the detector.

Let me refresh your memory with Fig. 1. Here we have a skeleton circuit of an a.m. receiver, showing the tuned circuits with which we are concerned here, the detector and a hint of the audio section that will follow. It is obvious that a signal injected at a post-detector stage must be at audio frequencies. In the old days, it was easy enough. A finger tapped on the appropriate valve grid, or on the 'hot' end of the volume control would produce a healthy 'buzz'. Mains pickup and the high impedance of the input circuits made this possible. With a battery-operated piece of equipment or the low-impedance test' type of operation is not so effective. It can, in fact, be positively dangerous.

SIGNAL INJECTION

The answer is to inject a signal of known characteristic (even if unknown precise amplitude), simply to verify that the following stages are working. We are not interested so much, at this point, in their exact efficiency, their lack of distortion, their overall output. For the following tests we need some method of indicating variations of output, either at the final part of the receiver—the feed to the loudspeakers—or at some earlier audio stage, where the readings may be more convenient.

It must be stressed again that when signal injection methods are employed, we are not expected to measure the output accurately. As Gordon King has explained, the quality of one piece of test equipment is determined by (a) the standards to which one must test the circuit, (b) the quality of associated gear and (c) the standard of testing we wish to apply.

Signal injectors are the easiest of all test instruments to make and apply, and there have been numerous suggested circuits in PW. We shall skip lightly past the subject, pausing only to remark that if you are thinking of alignment, it can be argued that you will be using a signal generator. There are very few of these that do not incorporate an audio output facility. There is your post-detector tester, ready made.

The 400Hz or 1kHz note we hear from the loudspeaker is suitable for rough tests and basic alignment in an emergency. It is certainly no more than a guide for precise circuit adjustment of the modern set. Visual alignment checking is needed so a meter, or some other visual indicating device, will have to be used. So this is where the ordinary multimeter can be pressed into service.

With valved equipment, nothing is easier than a low a.c. voltage-reading meter (say from 0-5V a.c.) across the loudspeaker or a dummy load. The dummy load, it should be said, has not been outdated by transformerless output transistorised receivers. For test and measurement purposes, the output circuit should always be correctly loaded.

Figs. 2(a) and (b) show alternative ways of indicating audio output, for both valved and transistorised equipment. We include these notes on valved equipment simply because the accent here is on servicing and it is in the nature of things that servicing will be required more often on older equipment. Measurement of anode current in an output

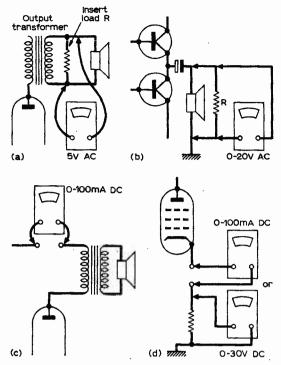


Fig. 2: Measuring output, (a) across dummy load or shunling speaker, (b) across speaker of transformerless stage, (c) current indication in series with anode load, (d) in series with cathode or voltage across blas resistor.

stage of valved equipment, either in the anode or cathode lead, is an alternative, where a low voltage d.c. meter, or a 0-100mA d.c. meter is available, Fig. 2(c) (d).

MEASURING OUTPUT

Breaking into the output stages of a transistorised amplifier for such alternative readings is neither easy nor desirable. Because of the low impedances of emitter circuits, voltage variations are too small to be of any great value, and should, in any case, be stabilised.

But let's do things properly. Let us consider the output power that we should get, and make arrangements to measure that. There are two things to consider here: audio power measurement and indication of standard audio output. They are not the same. As Gordon King will be showing later in greater detail, measurement of audio power is not a simple process, and interpretation of results must be made with great care.

Briefly, the expected outputs from general apparatus would be: (a) small transistorised radios, 500mW to 1 watt (b) larger radios, 1 watt to 3 watts (c) tape recorders and record players, 2-6 watts (d) small amplifiers, up to 10W (e) larger amplifiers, 10 watts upwards.

Standard outputs are related to the sensitivity of the apparatus. For example, a radio may be quoted as having a sensitivity of $25\mu V$ for m.w. reception, $40\mu V$ for l.w. reception and $1\mu V$ for both s.w. and v.h.f. reception. Alone, these figures mean nothing. They must be related to the standard audio output and to other factors such as signal-to-noise ratio. In the case of these quoted figures, the audio output would be 50mW for a s/n ratio of 6dB, relative to the 0dB figure of $1/\nu$ V.

This gives us a clue to the statement 'decibels below l volt' which may sometimes be used. 'Decibels below 1 milliwatt' is another alternative and 'field strength' yet another. The last term is employed to assess sensitivity when loop or ferrite rod aerials are used.

For now, we do not need to worry too much about all this. Practical service work very often consists of bringing up to scratch the circuits that may be only a little out of alignment. If components in tuned circuits have been replaced or if maladjustment has occurred, then the procedure is to check the alignment throughout and to make the small alterations found to be needed.

VISUAL DISPLAY

The oscilloscope is invaluable here, saving hours of careful tabulation and giving both the facility of viewing the result of the input signal and of measuring it. A secondary facility, often overlooked, but quite important, is the ability we have, when viewing a trace, of determining how much output is signal and how much noise and distortion—common causes of faulty results when only a meter is used.

We shall later look more closely at this matter of noise and distortion assessment. For now, a brief note on the practical alignment of a typical receiver, using a standard signal generator and a measuring device, augmented by an oscilloscope. Response curves are the usual method of measurement and, very often, a manufacturer will give no more than the

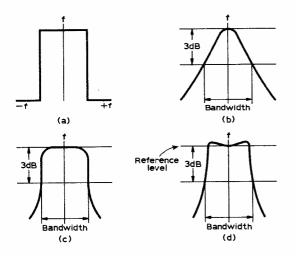


Fig. 3: (above) Response curves, carrier frequency f with +f and -frepresenting bandwidth limits. (a) Ideal curve, (b) peaked response, with bandwidth indicated at -3dB (c) flat tuning to give desired response, same peak level and bandwidth as (b) but quite different response. (d) double-hump tuning as approach to flat top response of (a)

Fig. 4. (right) Instrument set-up for measuring i.f. response. Note attenuator resistors Ra and Rb, and isolating capacitor C1. expected curves in his service manual, referenced to some level and bandwidth. It is as well to be clear at this point, therefore, what we mean by response curves, reference levels and bandwidth.

Fig. 3 shows a selection of the graphs one would produce by plotting the output from the receiver (vertical axis) against the frequency at which the signal was applied (horizontal axis). It is possible to produce these curves from careful and detailed measurements but it is much simpler to feed to the receiver a signal which varies regularly across the bandwidth, locking this to the timebase of the oscilloscope and displaying the output from the detector of the receiver. Such an input signal is obtained from a sweep generator, or 'wobbulator' (see page 1038 PW April 1971).

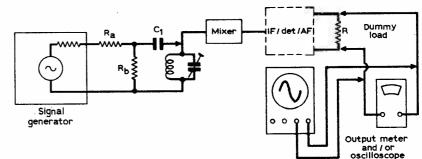
The response characteristic of a superhet receiver is mainly that of its i.f. circuits, for the r.f. circuits are not so sharply tuned. Quite often, response testing and alignment concentrates on the i.f. circuits, leaving the r.f. section of the receiver to be aligned on one or two spot frequencies and checking the padding and trimming of the oscillator.

The acceptance band of a receiver has to take in the sidebands of the transmission for full handling of the higher frequency components of the modulation, but if it extends too far beyond this, the signal-tonoise ratio will suffer. A perfect response characteristic—an impossible one—is shown in Fig. 3 (a). All the frequencies within the passband are received with the same sensitivity; those outside the passband having no effect. In practice, the response curve may be more as (b), where the 'usable' bandwidth is that between the -3dB points. This is where output power falls by 3dB or half its maximum value.

Note, however, that the response curve may be neither as flat as (a), nor as gently peaked as (b). In fact, it may be double-humped, as in (d). One important point here is that the reference point, relative to the -3dB level, is the centre frequency of the passband, and not the peak of the humps.

Merely to state the frequency limits at which a curve is 3dB down is not enough. This tells us what the gain of the receiver is, but not the extent of the rejection of unwanted frequencies. Always plot beyond the -3dB points, as shown in the accompanying curves.

Making response measurements of the a.m. receiver with a low audio frequency modulating signal (example: 30% modulation at 400Hz), we feed the signal generator to the mixer input, as shown in Fig. 4. It is essential that the impedance from which the signal is derived is as low as possible. In the mixer input, the tuned circuits will not be at the intermediate frequency, so the low impedance is needed. Hence the two resistors, Ra and Rb, where



a reduction of the generator output impedance from the usual 50 or 75 ohms to as little as 10 ohms can be effected. The values are easily worked out: for a generator of 50 ohms output, to present a 10 ohm (very nearly) load to the mixer input, we need to make Ra around 40 ohms (nearest preferred value 39 ohms) and Rb 10 ohms. The choice of values gives a 10:1 voltage ratio also, just in case you want to work out sensitivity figures.

The value of Cl should be such as to make its reactance at the test frequencies no greater than 50 ohms. At an i.f. of 470kHz, Cl would thus be around 0.01μ F. Its inclusion is to prevent the d.c. bias conditions being upset.

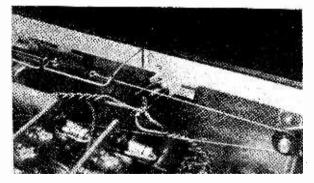
Disabling the a.g.c. is the next consideration although the method of disconnecting the a.g.c. line and putting a fixed bias in its place may not be so simple with modern sets. Sometimes the manufacturer will indicate a method of killing the a.g.c. action. The need to do so is evident from an understanding of a.g.c. action, which has already been described.

If we feed to a receiver aerial input a signal varying between say a microvolt and a volt, we may find that at around 5-10 μ V input, a 2:1 increase in input produces very nearly a 2:1 increase in output. But after about 100 μ V input, the curve relating output to input flattens drastically, and it needs a good deal more 'in' to produce just a little more 'out'. The a.g.c. curve, in other words has a definite 'threshold value' with two fairly linear slopes, above and below that threshold. In fact, a.g.c. "quality" is often defined in terms of the mean slope of the curve above the threshold.

Assuming first that the a.g.c. is prevented from working, our tests would comprise first setting the generator to the reference frequency, with its output adjusted so that at full receiver gain the rated full output is obtained. The generator output is then attenuated to produce the 'standard' output, 50mW. The receiver's gain control can be used to set the output indicator to a convenient value and then left strictly alone.

The generator is swung over the required frequency band and output plotted relative to the reference. The bandwidth is the frequency difference between the 3dB 'down' points.

If the a.g.c. cannot be 'killed', there are alternative ways of going about the checking. We can tackle the problem 'backwards', measuring for a constant output for a 3dB increase of input, with the attenuator of the signal generator set to increase the test input by 3dB, then the two limiting frequencies where the



Close-up of am.if.m. tuner showing part of a.m. ferrite rod aerial at left and drive cord and pointer.

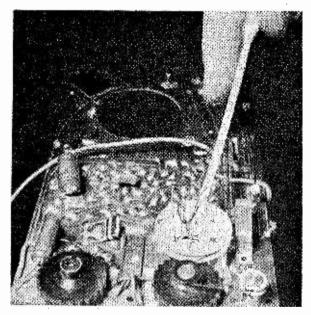
monitor reading is returned to the reference level define the bandwidth.

Another way of testing bandwidth without having to 'kill' the a.g.c. is to keep the carrier frequency of the generator constant and to vary the bandwidth. This cannot be done with the normal signal generator, as modulation frequency and depth are often fixed. But where a c.w. only output is obtainable and a separate audio generator is available to apply a varying input, then the r.f. generator can be set up to the central frequency and the modulation varied in frequency, without any change in depth, and a note made of the points at which the output reading (across the detector load, for utmost accuracy) is 0.707 of the reference level. These limits are the bandwidth, i.e., bandwidth is twice modulation frequency.

CW TESTS

It is not so easy to align higher quality receivers. The sides of the response curve can appear deceptively steep, because of the relative phase shift of the sidebands. The way to overcome this possibility of error is to use a c.w. (unmodulated) input and to read off the d.c. voltage at the detector.

One snag: there may be some standing d.c. voltage. It can be allowed for and carefully taken into



Before attempting alignment it is essential that drums, cords, springs and attachments are in order. Always check traverse of pointer before making adjustments.

account by subtracting it from final readings. The use of a d.c. valve voltmeter or similar instrument allows us to back off the settings to obtain a new zero.

Working on s.s.b. receivers can be a good deal easier. Better-class communications receivers work also in the single-sideband mode and these can be aligned by using the beat between the input signal and the internally generated carrier, with a.g.c. switched off—which is usually possible with these sets.

PRACTICAL POINTS

Procedures must differ between makes and models. Some general rules follow:—

(1) Allow sufficient warming up time before making tests. On valved equipment, fifteen minutes for both receiver and test gear should be regarded as the minimum. Despite all the advertising, transistorised equipment does not 'warm up' to operating conditions 'in the twinkling of an eye'. One very famous hi-fi amplifier I recently tested took seven-and-a-half minutes for the current in the output stages to settle to a steady reading, and that is not exceptional.

(2) Check mechanical points. Dials and cursors, pointers and drums should be run from end to end of their travel and limits noted. Where datum points are provided by makers, these should also be checked before alignment commences. In general, maximum frequency (minimum wavelength) should be indicated when the capacitor plates of the usual ganged capacitor are fully unmeshed.

(3) Make any necessary adjustments to counteract backlash, so that a setting of the cursor or pointer accurately reflects the setting of the tuned circuits.

(4) Check before operations that the required trimming tools that are available. It is simply asking for trouble to use worn grub-screw drivers where hexagon-holed slugs are used, or when core slots are only suitable for miniature plastic tools. Some time ago PW presented a set of plastic trimming tools to readers. Mine are still in use, augmented from time to time by filed plastic knitting needles and crochet hooks.

(5) Cores of inductors, despite all our efforts and care, may jam. The only recourse then is to drill or chip them out, taking great care not to damage the former wall or the inductor. Resetting of new cores may need either a rubber band inserted in the core or the use of a non-hardening adhesive. There are core-locking compounds that provide an adequate fixing but still allow some adjustment.

(6) Finally—before starting, make sure that test gear is isolated and that there are no false return loops. Connect the neutral side of a.c./d.c. equipment to chassis if you have no isolating transformer and provide capacitive isolation, as previously described.

GENERAL PROCEDURES

Consider a combination a.m./f.m. receiver, as shown in skeleton form in Fig. 5: Crystal filters are used widely and we can expect to find this trend growing. No alignment is normally required except for the last stage, which will be peaked up to the intermediate frequency. A little care is needed here and some 'swing' about the nominal frequency may be necessary. A good idea is to peak the last i.f. to the input from a weak signal after the rest of the alignment has been done, bringing it into tune only temporarily at first.

Where tuned circuits are used throughout, inject a signal at the frequency changer that will produce a 50mW output across the appropriate load. As power in watts is the voltage squared divided by the resistance, we can work out the required reading. (For 3 ohms this will be 0.387V, for 8 ohms, 0.633volts and so on.)

A meter that has a full-scale deflection of around 2.5V a.c. is required. Exact readings are not important at this stage as our aim is to maintain the output at the same level while bringing the circuits into tune, turning down the input as the gain increases. For this, the volume control will be turned to maximum, and if there are tone controls fitted, the treble control will be adjusted for the least top-cut.

Tuned circuits should be adjusted for peak output, starting at the rearmost and working toward the mixer. After initial peaking, go back over these adjustments. With some sets, there may be a tendency for one tuned circuit to 'pull' another, and readjustment should be made until no further improvement can be gained.

Where the response curve is humped, two peaks will be found as the signal generator is swung over the passband. In this case, the middle position should be used. Tune for the slight dip between the peaks.

IF REJECTION

Before readjusting the signal generator, remove it from the mixer input and apply the signal, still at intermediate frequency, to the **aerial** input, then tune any i.f. rejection circuit to give the **minimum** output. It is always wise to make this test early on, then rechecking after mixer alignment. For this test, increase the i.f. output from the generator and switch the receiver to the medium-wave band (where breakthrough could be bothersome), turning the tuning gang till the vanes are fully meshed, i.e. the low frequency end of the band.

Another rejection circuit that will be found nowadays is the 19kHz pilot tone filter. This is also tuned for minimum output with a strong 19kHz tone injected.

Alignment of the broadcast band is conveniently done at this point. Set the generator to around 600kHz (500m) and the pointer of the set to the same

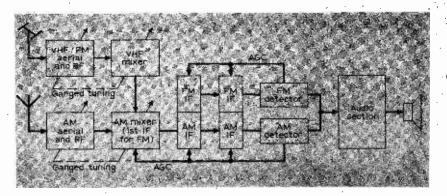


Fig. 5. Block diagram of combined a.m.! f.m. receiver, with switching omitted, as a guide to following the alignment procedures described in the text. frequency, after checking that it traverses the scale correctly, and reaches any datum points marked by the manufacturer with the correct scale indication.

Adjust the padder and/or the oscillator coil (if this is adjustable) and obtain maximum output. Then readjust to the other end of the band, setting the trimmer. Best procedure is to carry out these operations for the mixer first, then peak up the aerial circuits and return to the mixer for readjustment, then again to the aerial to make sure the circuits remain in tune. Adjustments of this nature take time and demand patience. Maybe this is why realignment of receivers can be a costly job! It is never good enough to make a perfunctory gesture of 'twiddling the cores'. The long wave adjustments can then be done.

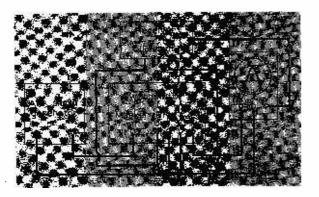


Fig. 6 Instrument set-up for checking i.f. response of f.m. receiver.

Do not attempt them in reverse order, as settings of the medium wave tuning can affect the long wave band. Similarly, where there are several short wave bands, first adjust the highest frequency band.

Long wave adjustment often consists of adjustment of one trimmer in the mixer circuits and one in the aerial circuits. There is rarely any need to check tracking over the band as carefully as one would with medium wave tuning, there being few stations available.

Short wave adjustment often requires slight movement of coil turns and care has to be taken with the dressing of leads. Tuning is considerably simplified by the omission of padders in the short-wave section of most receivers. Instead, we find coil adjustments, or core settings being made at the low frequency end of each band and trimming used at the high frequency end.

FM ALIGNMENT

Most adjustments to f.m. tuned circuits are carried out nowadays with the aid of a wobbulator and oscilloscope. Here, we find the output displayed, the signal swept over the response band and variable capacitors and coil cores adjusted to obtain the correct response curve. Addition of an a.m. marker generator aids the set-up, and the inter-connection of these instruments is shown in Fig. 6.

Because the average serviceman is unlikely to possess a wobbulator, we shall concentrate here on the adjustment of f.m. circuits using only an ordinary signal generator and a high-resistance meter. A more tedious job, but practically as efficient. First requirement is a d.c. voltmeter, capable of reading around 10 volts, with a 20,000 ohms/volt sensitivity at least. This is connected across the d.c. load of the ratio detector, the aim here being to keep the reading to a set level, determined by circuit characteristics, by turning down the generator input as the circuits are brought into line.

With the generator tuned to the f.m. intermediate frequency (10.7 MHz), and with the modulation switched off, the signal is injected at the mixer and



◀ Oscilloscope trace of response curve using wobbulator, with marker pip at top of curve (centre frequency f).

A similar response curve but this time the marker pip is placed at the ---3dB level on one side of the curve.



the i.f. circuits aligned for maximum output. The correct procedure, again, is to start at the rearmost and work forward, but even more care is needed and constant rechecking is necessary.

If a ratio detector is used, the next step is to note the output reading from this 'peaked-up' process, transfer the meter to the a.f. output capacitor and note that the reading is now exactly one-half of what it was before. The ratio detector winding is adjusted to achieve this.

After this, repeat the steps until no further improvement can be gained. It is important to ensure that later steps do not impair earlier results; hence this need for repeated operations.

The ratio detector is finally balanced. The coil that gave its 'half-volts' reading earlier is now readjusted for a minimum reading. The mean of these two is calculated: i.e., halfway between the maximum and minimum voltages that can be obtained by adjusting the coil of the ratio detector. This is the setting for correct alignment.

END OF PART FOUR

NEXT MONTH 'MAC' HELLYER WILL DISCUSS HOW FM STEREO SIGNALS ARE GENERATED AND TRANSMITTED. THEN FOLLOWS DETAILS OF TYPICAL STEREO DECODERS AND THEIR ALIGN-MENT.

the <u>European space race</u>

Marconi sets the running with a multi-million pound contract for Skynet II.

by John Chapman

The first communications satellite system to be designed and built in Europe will be a British venture. Marconi Space and Defence Systems, a member of the GEC-Marconi Electronics group, has won a multi-million pound Ministry of Defence contract to design and build two satellites to gradually take over the expanding military communications traffic currently being carried by "Skynet 1," a satellite built by the Americans for exclusive use by the British Armed Forces.

Skynet II will be more powerful than the existing satellite and will be one of the most advanced satellites in orbit in the world.

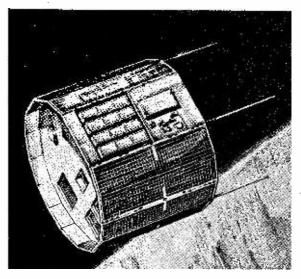
The first of the new satellites will be launched into a near synchronous orbit over the Indian Ocean in the first half of 1973. By this time the American built Skynet I will be approaching the end of its design life: the second of the new satellites will be used as a standby and launched later in 1973.

The GEC-Marconi group has already played a major role in the provision of ground stations for the Skynet system. Four 21-foot diameter dish transportable stations have been supplied by Marconi Space and Defence Systems at Stanmore and this part of the company is at an advanced stage in the development of a 3¹₂-foot diameter aerial terminal (called SCOT) which can be mounted on a ship to provide the Royal Navy with further links into the Skynet system. Marconi Communications Systems, based at Chelmsford, built the first three earth terminals back in 1966. Two of these 40-foot diameter ground stations which were used with the satellite system built for the U.S. Government and used successfully by the American Armed Forces have now been modified to form part of the Skynet system.

Outlining the activities of Marconi Space and Defence Systems at Portsmouth, the company's manager Mr. M. Lovell said that their experience in spacecraft electronics has been developed over a period of about seven years in which time they have provided the satellite electronics for every British spacecraft programme to date.

The first of these was Aerial 3 (later called UK3), a satellite launched in May 1967 as part of a scientific programme. Although this satellite had a design life of a year, it was not switched off until 1968 and furthermore, the system was reactivated last September in order to check on the long-term reliability of the electronics equipment in a space environment.

The next important project was the X3 satellite which will be the first technological satellite to be launched in a Black Arrow launch vehicle. In this project Marconi engineers are responsible not only for the onboard electronics but also for satellite assembly, system test and the preparation of the



spacecraft for launch. By contrast with the earlier satellite, X3 features modular electronics systems built to conform with ESRO standards which are suitable for use in a wider range of satellites.

Marconi has also been heavily involved in the UK4 and UK5 satellites. The later satellite is packed with electronic equipment and offers two important advances to the experimenters taking part in the joint NASA/Science Research Council project. Firstly it will be possible to adjust the direction of the spin axis of the spacecraft using a propane attitude control system so that experimenters can scan space for objects of potential interest and then point a second set of experiments along the spin axis at selected sources. Secondly, through the use of the spacecraft's magnetic core stores, it will be possible to collect data around an orbit and to replay this upon command in a format most convenient for the experimenters.

CONSTRUCTION

The Skynet II satellite is to be built in the form of a cylindrical drum, with solar cells covering the entire curved surface to provide the power for all of the electronics. It will measure approximately 78 inches long with a diameter of 75 inches. Laun'h weight will be about 960 pounds.

An apogee motor contained in the satellite itself, and mounted along the major axis of the cylinder, will be used to transfer Skynet II into its synchronous orbit. It will be spin-stabilised at about 90 revolutions per minute from the time the second stage burning ceases and once placed in synchronous orbit by the solid fuel apogee motor, the communications antenna will be de-spun and controlled to point continuously at the earth.

Attitude control will be achieved by means of hydrazine jets which will be used to adjust the attitude of the satellite, both before the apogee motor burn, and subsequently for the life of the satellite after it has achieved the required synchronous orbit. Control movements will be provided by a single pair of jets located at the edge of the satellite and thrusting parallel to the axis of the satellite, with another pair of jets mounted in the curved surface of the satellite, and pointing radially out from the centre. These jets when fired will be pulsed to synchronise with the rotation of the satellite so as not to upset the high rate of spin which will eliminate any tendency of the satellite to rock, or even tumble and so interupt communications traffic.

During the initial manoeuvres and the final positioning, control communications will be carried out through an omnidirectional aerial system consisting of an array of cavity-back dipoles operating at S-band. This array is mounted in a single band round the complete circumference of the satellite. Once synchronous orbit has been attained and the satellite has been turned into the correct position with respect to earth, a single horn aerial mounted on the major axis of the satellite-at the opposite end to the rocket motor-will be brought into use to provide the main communications function of the satellite. This aerial whose beam-width is just sufficient to cover the entire visible portion of the earth's surface will be mechanically de-spun and aimed directly towards the centre of the earth.

Much of the technical detail of the electronic packages onboard Skynet II is, of course, classified. Presumably the transmitter/receiver operates in the GHz band using sophisticated multiplexing techniques to cope with the wide variety of traffic it will be called to handle. Also it will have to cope with a variety of powers, since the ground stations with which it will have to work range from tiny ship and shore-based portables with 3.5-foot diameter dish shaped aerials to the large 40-foot units having outputs measured in kW.

TECHNOLOGY SATELLITE

Much more information is available on the technology satellite X3 which is in the final stages of preparation for launching shortly. The satellite has been checked in the solar chamber at RAE Farnborough and at the time of writing it is being checked for magnetic inter-reaction at the ESRO European Space Technology Centre in Holland prior to installation on to a Black Arrow launcher.

The Black Arrow 'X' series of technology satellites is aimed at improving British technology in spacecraft and launch vehicles. All of the satellite systems are designed with future requirements in mind and some of the operational data equipment is duplicated in new experimental form to be proved in space.

Marconi has designed and built the power conditioning system, the telemetry transmitters, telecommand receivers and decoders and the data conditioning systems for the satellite to the relevant NASA and ESRO standards.

Although the power requirements of X3 is only 10 watts, the power conditioning system has been designed for future spacecraft in the series and is rated to supply up to 30 watts continuously, both in sunlight and eclipse conditions. A 6 ampere-hour nickel-cadmium battery charged by the solar cell array supports the equipment during eclipse periods.

Owing to the limitations of the pulse frequency modulation data system used on previous satellites, channel capacity has been increased through the



This picture shows the assembly of a welded circuit for an r.f. module. (Skynet II).

adoption of a modular pulse code modulation data system. Besides meeting the immediate requirements of the X3 satellite, the system could be expanded easily to cope with more complex data systems of future spacecraft.

The new data handling system uses a small number of standardised logic elements, such as shift registers and multipliers, packaged in all-welded "modules" assembled to form a complete telemetry system. Essential modules are duplicated to enhance system reliability.

The telemetry, tracking and command system makes use of an r.f. package comprising 6 sub-units based on common piece parts. Again the telemetry transmitter is duplicated to increase reliability. Two receivers are used and connected in polarization diversity configuration to minimise the effects of spin modulation of the r.f. signal—induced by the rotation of the satellite.

A completely new command decoder has been developed for X3. This operates on the NASA Tone-Digital Command Standards and provides a capacity of up to 70 commands per decoder address. Two of these are fitted to the satellite. For a transmitted command to have any effect on the satellite, the r.f. carrier frequency, the tone frequency, the relative timing and lengths of the tone bursts, and the number of bits per word must all be correct and the decoder must also recognise its allocated address followed by a valid execute code within a defined time period. Reasonably secure!

TOTAL CAPABILITY

Now that a British company has won its spurs in the space race, Marconi is in an ideal position to open up satellite communications for commercial applications. Already there are suggestions that countries like Canada and several in Africa where the population is spread over wide areas could make use of communications satellites feeding small ground stations such as the SCOT terminal being built for the British Armed Forces.

By the end of the decade radio and television direct from 'stationary' satellites could become a reality. The technology is here already—it seems to be more a matter of getting the economics right. EGTRO

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21706	12p	2N3053	27p	AC127	20p	BC157	12p	BFY52	23p
2N930	29p	2N3055	65p	AC128	20p	BC158	11p	BSX 20	16p
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2N1307	86p	2N3709	13p	AD161	83p	BC182L	10p	NKT274	18p
2N1308	36p	2N3710	18p	AD162	36p	BC183L	10p	NKT403	65p
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2N1613	23p	2N3794	15p	AF115	30p	BC212L	16p	OC71	29p
2N1711	26p	2N3819	85p	AF117	28p	BC213L	16p	0C81	25p
2N1893	54p	2N3906	35p	AF124	30p	BC214L	16p	OC83	20p
2N2147	95p	2N4058	18p	AF127	28p	BCY70	19p	ZTX300	17p
2N2218	34p	2N4059	10p	AF139	38p	BCY71	33p	ZTX 301	17 p
2N2218A	43p	2N4060	11p	AF239	36p	BCY72	15p	ZTX302	22p
2N2219	38p	2N4061	11p	ASY26	27p	BF115	23p	ZTX303	22p
2N2219A	58p	2N4062	12p	ASY28	27p	BF167	18p	ZT X 304	27 p
2N2270	62p	2N4124	18p	BC107	12p	BF173	19p	ZTX 500	18p
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2N2483	85p	2N4284	15p	BC109	12p	BF195	15p	ZTX502	25 p 22 p
2N2484	42p	2N4286	15p	BC125	15p	BFX29	81p	ZTX503	
2N2646	54p	2N4289	15p	BC126	22p	BFX84	25p	ZTX 504	52p 27p
2N2904A	42p	2N4291	15p	BC147	10p	BFX85	34p	ZTX530	279
2N2905	44p	2N4292	15p	1		1			

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C.	1/20W	5%	82 Ω-220K Ω	E12	9	8	7
č	1/8W	5%	4·7 Ω-470K Ω	E24	1	0.8	0.7
č	1/4W	10%	4.7 Ω-10Μ Ω	E12	1	0.8	0.7
ď	1/2W	5%	4·7 Ω-10M Ω	E24	1.2	1	0.9
č	110	10%	4·7 Ω-10M Ω	E12	2.5	2	1.8
мо	1/2W	2%	$10 \Omega - 1M \Omega$	E24	4	3.5	3
ww	iw	$10\% \pm 1/20 \Omega$	0-22 Ω-3-9 Ω	E12	7	7	6
ww	3w	5%	12 Ω-10K Ω	E12	7	7	6
ww	7W	5%	12 Ω-10K Ω	E12	9	9	8
Codes:	C = carboa	film high stabil oxide Electrosil		rating, N	re in pence eac 70 T mixed valu resistor order)	h for same ohmic v us. (Ignore fraction)	alue and powers of 1p. on tote

Values: **Yanues:** E12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 69, 82 and their decades. E24 denotes series: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 62, 76, 91 and their decades.

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THE BROADCAST BANDS

Malcolm Connah

MONTHLY NEWS FOR DX LISTENERS

THE onset of fine, summery weather has caused the usual drop in the number of reports as DXer's leave their shacks for the great outdoors. Among the stalwarts who remained in their shacks was John Trewick of London Colney who used his Lafayette HE-40 and vertical whip to hear the following:---

- 9525 RSA, South Africa in English at 2020.
- 11820 BBC, Ascension, 'The Music Scene' at 2015.
- 15018 Hanoi, Vietnam with 'Letterbox' at 2000.
- 15170 ELWA, Liberia in French at 2030.

15185 Helsinki, Finland in English at 1800.

- 15195 Ankara, Turkey in German at 2100.
- 15265 Kabul, Afghanistan in English at 1800.
- 17730 Havana, Cuba with news in English at 2010.
- 21535 NHK, Japan with 'DX Corner' at 0800.

21535 RSA, South Africa with Folk Songs at 1120.

Howard Stephenson of Newcastle-upon-Tyne has used his Eddystone EC10, Mk. II receiver and Joystick antenna to hear some interesting stations including:—

- 3260 R. Niamey, Niger, African music at 2015.
- 3905 All India Radio in English at 2245.
- 3915 BBC, Tebrau, Malaysia relay at 2215.
- 4680 HCWE1, R. Nac. Espejo, Ecuador with Latin-American music at 0545.

4680 HCWE1, R. Nac. Espejo, Ecuador with Latin-15395 VOA, Tinang, Philippines at 2200.

Ray Warren of Bury St. Edmunds has used his Astrad Auriga receiver and a Koyo 1661 receiver to hear the following:----

- 6195 Tunis, Tunisia in French at 0840.
- 6540 Pyongyang, N. Korea in English, 1900.
- 9489 Radio Tirana, Albania, English, 1830.
- 9570 R. Nacional, Spain in Spanish at 1540.
- 15180 Radio Australia, pop music at 0800.
- 15460 Radio Kuwait, news in English at 1830.
- **R. J. Downes** of Bournemouth does not mention what equipment he uses but he heard:—
- $6010 \ R.T.$ Belgium in Dutch at 1430.
- 11710 RAE, Argentina in English from 2300 to 2400.
- 11965 Trans Europe Radio in English, 1345.
- 15160 Ankara, Turkey in English from 2200.
- 15185 Nigeria B.C. noted in English at 0715.
- **Derek J. Hart** of Lancaster sent in the following list of stations which he has heard recently:—
- 6080 Radio Berlin International at 2037.
- 9505 Radio Tirana, Albania news at 2035.
- 9625 Israel B.C., news at 2056.
- 9915 All India Radio, news at 2056.
- 11672 Radio Pakistan, news at 2045.
- 15125 Radio Australia to Pacific at 0830.
- **Nigel Williams** of Caewern, Neath, Glamorgan, has a Lafayette receiver and a Joystick antenna with which he heard:—
- 4990 Radio Kiev, Ukraine, DX programme at 1945. 5015 Windward Islands B.S. to Europe at 2345.

- 6130 Radio Tirana, Albania in English at 2130.
- 7306 Polish Pathfinders in English at 1700.
- 15230 BBC, Ascension relay at 1710.
- 15250 RSA, South Africa at 1750.
- 21460 HCJB, Quito, Écuador, DX programme at 1945. 21595 Radio Canada International at 1850.

C. Gibbs gives no indication of the equipment used but he managed to hear the following at his shack in Camberley:—

- 6020 Radio Nederland in English at 1515.
- 6025 Radio Portugal at 2125.
- 6025 Radio Budapest, Hungary in English at 2130.
- 7145 Radio Warsaw, Poland in English at 1600.
- 9535 SBC, Berne, Switzerland at 1115.
- 9730 Radio Berlin International from 1515.
- 9735 NHK, Japan in Japanese at 2012.
- 15325 Radio Canada in French at 2045.

A new reporter from Hessle in East Yorkshire is **Ian Jarvis** who owns a Lafayette HA-700 receiver and a 50 foot long aerial which enabled him to hear:—

- 7210 The International Radio Service of the Red Cross from Switzerland at 1200.
- 7290 Trans World Radio, Monaco at 1645.
- 9770 Austrian Radio, English for Europe at 2045.
- 11672 Radio Pakistan in English at 2015.
- 15130 Radio Australia in English at 0815.
- 15240 Radio Sweden in English at 2245.

The article in the May issue has prompted a number of queries as to which is the best receiver for the Broadcast Bands DXer. This is a very difficult question to answer but my general advice is to pick one of the following ex-military sets: CR100, AR88, R1155 or an HRO. If you prefer a new receiver the following two sets are good value for money: Lafayette HA-600 or Trio 9R59DE. Both these receivers retail at about £45, much better sets can be purchased if the money is available of course.

KJ Catalogue

KJ Enterpises announce their latest Leisuresound Mail Order catalogue. There are 128 pages, containing stereo systems, record players of every variety, tape and cassette recorders, amplifiers, speakers, turntables, microphones, p.a. equipment, all types of recording tape, cassettes, books 8-track cartridge players, car radios, countless hundreds of accessories of every kind, radios, specialist furniture lines etc. As usual the majority of items are available at substantial discounts and where possible recommended retail prices are listed for direct comparison with KJ. Although this catalogue is automatically distributed to existing KJ customers it is available FREE on request, to anyone interested. KJ Enterprises, 33 Bridle Path, Watford, Herts.



YOUR chance this month to get a special QSL card. The Irish Radio Transmitters Society are off on a DX-pedition to Dalkey Island which is, according to the map, a small island off the coast of the Republic of Ireland (see if you can find it). Operating dates are 1200 on July 31 to 1200 on August 2. Operation will be Al and A3a on all bands from 3.5 to 30MHz. Sean Nolan, EI7CD, says that the callsign to listen for is EI0DI and the station will QSL all contacts. Station will be operating from petrol generators, according to Sean, so if you intend to have a QSO—don't smoke.

D. Palmer (Glasgow), tells that ZS1MH has been heard operating a DX net several evenings on forty and is rumoured to be in on a similar net on eighty. Another one on forty is LU7ACC who, with the ZS, has been logged around 2145hrs. Aerial at the Glasgow location is described as a V-beam with arms approximately 170° which almost merits a dipole rating. Feeding the output to a balanced a.t.u. gives a significant improvement in signal to noise ratio. Receiver is a modified 19 set with a crystal filter which bagged: CP6EL, CT2AK, CX1AA, CX1BBR, JW7UH, LU8AJG, PY2ELZ, PY4BSZ, PY5OF, PY6JM, PY7BBD, VP2MM, ZS1JA all on 7MHz s.s.b.

S. Chack (Harrogate), comments that stations have been dying out rather earlier on 14MHz and says that 80 has been very good of late. Surprisingly though, his log is for 7MHY from which his best were HI3PY and JA6SM.

"The a.t.u. has been made from a cannibalised crystal set", says **Stefan Kaye** (Witney). Further admissions include a confession to using an AR88 to log these on 80; EA6BN, F6ABP/M, JY9WB, KV4FS, PY7BFN, PY0AD, V01BT, ZC4IK, ZD7SD, ZS1MH, 4X4NJ, 6W8DY, 9G1DY.

S. Elsdon (Halesowen) warns, "You can be sure of hearing from me again soon", and promptly describes the gear as a CR-70A. Samuel also has a 240ft. long wire bent in the middle (nasty) and managed VK3IQ and VK3LR on 3.5MHz.

John Moore (Leicester) says he's come to the conclusion that people who don't tune the low ends of bands are missing about one-third of the DX. Nonec.w. types please note. John also reminds that Italian prefixes are allocated according to area and range from 11 to 10. This might not be a bad idea for G stations and would make life on two metres and up a whole lot easier.

John's log shows GM3SVK/A back on from the Shetlands on topband together with OK1FJS. Twenty metres s.s.b. showed: EA8GZ, ET3DS, JA3IXL, JW5NM, LU8DB,PY1CCC, PY2ZAD, PZ1DF, TA3HC, UK9AAQ, VE8RX, VK3ATN, VK6KK, VO1CM, YB3AAY, YB0AAG, 9H1CD, 9Q5BV. Ten metres raised: JA1ZTC, LU9FAN, PY2EWF, UK9HAD, VE2ASZ, VE3BKA, VE3FIQ, W3DQD/YVI.

G. Kent (St. Leonards-on-Sea) uses a B40 receiver and the aerial is "a strand of Woolworth's wire", (sounds a bit of a thin story to me). Although only



Frequencies in kHz • Times in GMT

some 15ft. long (the aerial not G. Kent) the following were heard on 14MHz: CT1SG, JA4HM, JH1OTO, JM2HCA, K2OUS, VE3GMT, VE6MC, VK2WC, VK4DY, VK5ED, VK5NB, ZL4BX, ZP2KN, 4X4VB.

Someone's got a favourite band. Don't worry, your address at Satinforth Road, Ilford, Essex, is safe with me. I know you didn't sign the letter and just for that I won't tell anyone that you heard: CR4AJ, CR6EM, CR7FM, CT2AK, DU6MG, EA6AS, EA9AA, EL7TL, EP2BQ, ET3USA, FC8APT, G3DJK/P/W1, HC1HV, HR3VFJ, IS1PZR, JA1QJE, JA7JLB, JH1JLR, KG4CS, KP4DCR, LU1CBR, KC4USP, K7ZTM, MP4BJE, OX3DL, PY2BDY, LX1HD, MP4BEU, PY8ZZA, SV1AE, SV0WDD, SZ0SU/P, TI3E, TJ1DA, VS9MT, VU2HLU, VU2REG, VS9MB, VQ9RK, W3UBM/MM/1, WA4MOC/P/8R1, WA6DBP/P/4X4, W6DLE,/4X4, W6VLH, W9LGV,, YU2REE/MM (off coast of Cameroons), ZC4CB, ZD9BN, ZL1HA, ZS6ES, ZS6ON, 3B8CZ, 4U1ITU, 4X4IX, 4Z4GV, 4Z4HF, 5H3JR, 5N2AAF, 5N2ABG, 5Z4DV, 6W8BD, 7X20M, 7X2SX, 8P6AJ, 9E3USA, 9H1R, 9H1V, 9M2BQ, 9N1MM, 9V1PX, 9X5WJ, all on 21MHz and probably s.s.b. too.

J. Iredale (Llandudno) expresses great delights at his newly-installed JR-500SE receiver (JDG's going all green again). A preliminary peep on 14MHz revealed: HK3CFM, LU2DEK, LX1BA, MP4BFO (resolves his own sideband?), SV0WW, WA6AUE, 4X4DK, 4Z4HF, 5X5NA.

A Hallicrafters S120 and a 66ft. end-fed located at llford allowed Mark Marsden to bag these on 20 s.s.b.: JA2OXF, JA7GY, HP9AVQ/MM, KX6DQ, TA6JB, TR8MC, VE6ARC, VK3CR, VK2AB, W3GLY/ VS6, ZS5DJ, 4Z4HF.

Come into my antenna says C. Henderson whose aerial does bear a remarkable resemblance to a spider's web. Receiver is a B40 and the other antenna is a 120ft. long wire. Goodies on fifteen include: CR4BC, CR71C, HB9TE, HI8FED, KV4AD, OD5AO, SU1BN, VE3BMB, VS9MT, PY2AAA, PY5EG, XW8BP, YV4YC, YV5BNR, ZC4MU, YA2GNT, 4U1ITU, 4X4CW, 5N2AAJ, 9Q5RH, 9Y4RB. Crispin says that 20 metres has been excellent at round 0100hrs.

S. Wainwright (St. Helen's), 9R-59DE, PR30, 70ft. inverted L at 28ft., all s.s.b. on 14MHz: FG7TD, FM7AA, FM7WW, HZ1TA, JR6JU, KS6CY, PJ8DZ, VR6TC, WA8FPN/P/KS6, ZF1GC.

Happenings for July include: 3-4, topband contest; 3-4, two metre contest; 3-4, two metre listeners contest; 10-11, Field Day; 11, Worcester Mobile Rally, Upton-on-Severn; 18, 70cms open contest; 18, 70cms listeners contest; 10-25 listen for G3EKW/A at the Nottingham Festival '71. Augugst 7-8, WAE c.w. contest.

Logs, in alphabetical order please, to arrive by the 15th of the month to: 12 Gross Way, Harpenden, Herts.

THE COLUMN

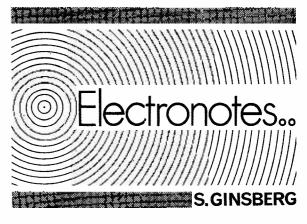
VERCROWDING on the medium waves has encouraged DXers to develop the MW loop aerial. This type of indoor antenna is both tunable and directional. Maximum pick-up is along the plane of the windings and there are two nullsdirections of little or no pick-up-opposite each other at right angles to the windings. These nulls enable DXers to reduce or eliminate interference simply by rotating the loop on its vertical axis so that stations such as Malaga 1007kHz can be heard with the null on Hilversum or Buenos Aires on 1070kHz with the null on CBA Moncton N.B. in Canada. Since a loop is an indoor aerial it can be used in locations where it would be impossible to erect an outdoor one. The writer invariably uses a loop in preference to a 90ft longwire as the overall performance is nearly always better.

R. Garwood of Bournemouth has asked for constructional details. The standard MW loop consists of 7 turns of plastic covered hookup wire wound in the shape of a square of 40in. side together with a one-turn coupling winding wound parallel and central to the main winding. The windings are supported on a frame made out of two pieces of 1 inch square wood joined at right angles at the centre to form an X. The turns are kept apart by means of four paxolin spacers which have saw cuts ¹₄in. apart along one edge to retain the windings. The spacers are fixed to the ends of the arms. The main winding terminates on a 500pF variable capacitor mounted at the centre of the loop. This is the tuning control. The single coupling winding ends at a small terminal block from which a 5ft. length of twin feeder (plastic covered lighting flex will do) connects to the receiver dipole input or to the aerial and earth terminals. The loop is fixed to a stand so that it can be rotated on its vertical axis.

To use the loop, tune in a station on the receiver, peak-up the signal with the loop tuning control and rotate the loop for optimum reception. As well as reducing co-channel interference, a loop will usually have a better signal-to-noise ratio then a longwire and it will often reduce cross-modulation, splash and occasionally static. **Ray Eaton**, a retired reader who lives in Brighton has been experimenting with loop aerials on frequencies up to 4MHz and reports some success.

South Americans are at their best in summer so now is the time to look for the rarer countries. Between 0100hrs GMT and sunrise listen for Radio Cruz del Sur on 1380 and Radio Mineria 1060kHz; both are 7,000 miles away in Chile. OAX4U 1010kHz Radio America is in Lima, Peru. It is normally a strong signal and has been logged already this year by a DXer in Norfolk. ZP4 1330kHz Radio Chaco in Paraguay and CP57 Radio Progresso 1090kHz in La Paz, Bolivia were heard last year while CP4 1020kHz also in La Paz is another recent catch from this difficult DX country. Conditions are at their best during the hour before dawn and the band is often alive with Latin Americans at this time.

CHARLES MOLLOY



T'S those integrated circuits again. Different types appear on the professional market almost daily. A fairly recent one is of great interest since it could well affect a whole industry. This 16pin dual in-line beast is called the TBA 631 and hidden within the confines of its diminutive carcass is a limiting amplifier, an f.m. coincidence detector, low frequency separator, low frequency preamplifier and self-balancing circuit, driver and audio amplifier. It's immediate application is in television receivers and the trend is that the average black and white receiver will be reduced to five integrated circuits (which should make the do-it-yourself t.v. builder jump for joy). Colour sets will need another two i.c.s.

There is more to it than merely simplifying construction, although from the manufacturing point of view this is extremely important. Servicing becomes an important aspect of many things, especially television receivers. If this trend of reducing a black and white set to five i.c.s continues, then the servicing aspect becomes a comparatively simple matter, since the would-be service man has, at worst, only to work his way round the set simply substituting "good" i.c.s. for each one in the set until the fault is cleared. This in turn implies that initial servicing in the home could be performed by an unskilled person.

It is not possible to fault the idea in terms of initial cost either, since the TAB 631 markets for around £2.80 for quantities of 1 to 24. Again, the chip in question will supply 3 watts into a 16Ω speaker for 10 per cent distortion with a 24V line. Limiting sensitivity of the unit is less than 100μ V at 6MHz for the quoted output. The output stage is class B and is capacitively-coupled to the speaker. The r.f. amplification, demodulation and output separator section has it's own power supply terminations and will work at voltages from 4.5V to 15V. The quiescent current at 12V is typically 18mA and the frequency range of the r.f. stage is between 5kHz and 60MHz. Over 60dB of gain is available from the limiting amplifier alone, while a.m. rejection is given as better than 45dB. A few resistors and capacitors plus tuned circuits are all that are needed to get this chip perking happily.

While the cathode ray tube and power supply are still required and have not, as yet, been reduced to a chip, experiments in solid state readout devices look promising although many companies have these behind locked doors. With advances like this, the wristwatch television doesn't seem quite such a ludicrous idea after all. STEPHENS ELECTRONICS, P.O. BOX 26, AYLESBURY, BUCKS. SEND S.A.E. FOR LISTS GUARANTEE Satisfaction or money refunded.

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ELL; we've only just made it this month as far as price limit is concerned but it is worth it, I hope. It is rather an unusual circuit and has not appeared before, as far as I am aware, in any form. The circuit is that of a "Touch Alarm" which does exactly what the title suggests; an alarm sounds off as soon as a metal plate is touched and stays on until the supply voltage is taken away. The metal plate can be all sorts of things, a safe, french windows, door handle, etc., etc., The applications and construction are left up to you but the circuit is not exactly complex and should take no more than a couple of hours to build once the components are assembled.

THE CIRCUIT

The first transistor, Tr1, is coupled in the common-collector mode (also known as the emitterfollower mode) with the base wired to the touch plate. The characteristics of this configuration are very high input impedance and low output impedance and this is the key to the operation.

The input impedance is roughly equal to the gain of the transistor times the emitter load resistor (here $6.8k\Omega$). The BC169C has very high gain figures, up to 900, but a more common figure would be 400. Therefore on this basis the input impedance is 400×6,800 which equals nearly 3MΩ. As soon as anything touches this base it biases the transistor on and the same voltage which has been applied to the base at very high input impedance, appears at the emitter at the same voltage level but at a usable impedance.

Most of you have dabbed a damp figure at the input of an amplifier and heard the resulting sounds, made up from radio signals and hum. Here we are making the best use of these signals and putting them to use. All sorts of "muck" is picked up when the plate is touched and this appears at the emitter as an a.c. voltage. The detector diode rectifies the signals and applies them across the capacitor C1. This charges up so that a positive supply appears at the junction of D1, C1 and R2. This voltage applies a bias via the resistor to the base of Tr2 which conducts and in turn applies bias to Tr3 and a pulse passes through the primary of the output transformer. However C2 is connected in a manner which causes the second two transistors to oscillate.

The beauty about the values and configuration used here is that once the alarm oscillator has started it is self-holding. That is, the pulses through C2 themselves bias Tr2 to maintain the cycle necessary for a continually sounding alarm. So it will be seen that R2 is only necessary to start the alarm which can only be switched off by disconnecting the battery supply. C3, which decouples the supply, is not essential but with a low battery it does help the operation. No. 28 Touch Alarm

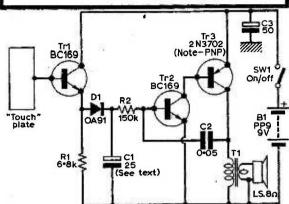


Fig. 1 : The circuit of the touch alarm

★ components list

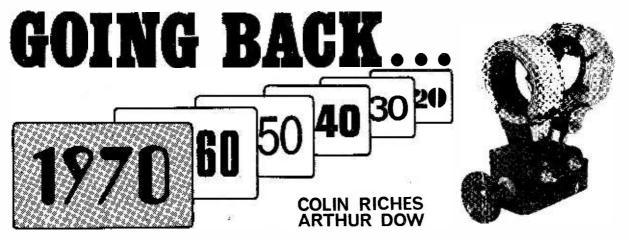
Tr1 Tr2 Tr3	BC169 BC169 2N3702	11p† 11p† 13p†
D1	OA91	5p†
R1 R2	6·8kΩ, 10 <i>%</i> , ∔ W 150kΩ, 10%, ↓ W	1p† 1p†
C1 C2 C3	25μF, 25V Mullard 0·1μF Mullard 50μF, 25V Mullard	6p† 4p† 6p†
SW	1 D.P.S.T. Toggle switch	5p*
T1	Transistor output transformer, Eagle LT700	20p‡
LS 6	x 4in, 3Ω loudspeaker	15p*
		98p
† El	ectrovalue Ltd.	
* P	adgetts Radio Stores	
‡ H	enrys Radio Ltd.	
Pric	on are those advertised in June 1971 and	l may have

Prices are those advertised in June 1971 and may have changed. No allowance is made for minimum order costs or for postage and packing; this should be checked before ordering.

Current drain is important in all alarm circuits because if it is high, batteries, which are continually left on would rapidly run down. In the quiescent condition current consumption was measured as 1μ A in the prototype as silicon transistors are used throughout, though when in operation this rises to over 20mA and a PP9 type battery has to be used.

Cl can be left out. If this is done the alarm is triggered by the slightest pulse—even by the switching on of fluorescent lights and this is a disadvantage. The inclusion of C2 has a slight delaying action as it takes time to charge up.

In certain locations the level of "muck" may be so high as to trigger the alarm *without* it being touched. In this case the value of R1 should be reduced to a suitable level which only triggers on touch; this also applies if a large touch plate is used.



TITANIC DISASTER

We are at present compiling a Going Back article about the Titanic Disaster and the radio messages that were transmitted and received on that tragic day. If any readers have any information or photographs that they think may help us, we would be very glad to hear from them.

M ^{R.} WILLIAM COBBETT tells us that he has a Harmsworth's Wireless Encyclopedia which was published in 1923. He says that it contains many interesting features and drawings, etc., the preface being written by Oliver Lodge himself. Mr. Cobbett says that 50 years after the books were first published it is amusing to read a line that states, "It is with great hesitation that we predict the time when each individual will possess his own pocket wireless set."

Perhaps any readers of *Practical Wireless* requiring information on wireless in the 1920's would like to contact Mr. Cobbett at 15 Copford Road, Billericay, Essex.

By the way, he tells us that anyone wishing to purchase the books will have to wait another 50 years!

Mr. C. R. Gunn of 48 Aldwark Road, Liverpool, L14.ON6 asks if anyone could tell him whether Paris (Eiffel Tower) still transmits the 300 dot second Time Signal that it used to years ago on long wave. Mr. Gunn cannot recall the wavelength of the transmissions but says that it used to be very interesting as with a microphone in the case of the Grandfather clock and a phone earpiece on one ear together with the radio phone on the other ear, the times when the two signals coincided were noted and checked by the time given after the transmission.

Mr. Gunn also asks if there is a publication giving a list of long wave stations transmitting Morse and what are the longest wavelength stations today? So if there are any readers who have any information that may interest Mr. Gunn, please write to him at the above mentioned address.

Basil D. Van Der Syde, F.S.E.R.T., 30 Langdon Road, Parkstone, Poole, Dorset, BH14 9EH asks if anyone can date a pair of headphones he has containing a built-in crystal receiver. There is no makers name and the "cans" are about twice the normal depth. In the back of one there is a tapped inductance with a 20-position selector switch for tuning. This earpiece has two terminals marked A and E. The other earpiece has a centrally fitted crystal detector, part of which is missing but the cap end contains a piece of "galena" crystal. Also contained within this earpiece is a wind-up aerial of some 20 feet of wire-woven tape about 12in. wide, and two small terminals marked "phones" (extension phones!). There is a Postmaster General approved stamp and the number 4145 printed on it. The crystal detector is integral with the small handle that winds the aerial in and the words "detector" prov. pat. printed below this---Mr. Van Der Syde mentions that when fitted with an 0A70 or similar diode, this set still provides fair MW signals (Charles Molloy please note!)

Many readers, we are sure, will remember our great colleague John Scott-Taggart. He used to bring out one "star" receiver for the home constructor every year in the magazine *Popular Wireless*. Mr. Van Der Syde says that checking over his collection of these magazines some years back, he was suddenly struck with the fact that the series was brokenthat is that it began with ST100 then went to ST300, 400, 500 and so on up to about ST900-in other words no ST200! At first he thought his collection was not complete but this did not appear to be so. This made him wonder if there had ever been a ST200 design and if not, why not?--or if so, had it been withdrawn? He made many enquiries and at last managed to contact JST himself in about 1963. He wrote to him but in his reply, JST was unable positively to give any information about an ST200. He thought that there may have been one and that details may be found in one of his early radio books Practical Wireless Valve Circuits or its sequel More Practical Valve Circuits published by the Radio Press about 1924/25.

Can any readers help to clear up the mystery of the missing ST200? If so, please write to us (because this one has us puzzled) and we will pass your letters on to Mr. Van Der Syde.

Vintage enthusiast S. Ellis, 30 Pynne Close, Stockwood, Bristol 4 writes to ask if we have any information on the receiver used for the "Committee Superfet" article. Unfortunately we don't as this receiver was kindly donated to us by a reader who said that a relative of his had constructed it from a kit in the 20's (we would like to say here that Arthur Dow did not rip the set open and implant an inte-

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BP141=74141 BCD-to-Decimal Decoder/Driver	available at these Exclusive LOW FALDS. 1 coded, brain and new to Manufacturers' Specification packages. BI-PAL Order No. Description BP 00=7400 Quadruple 2-input NaND Gate BP 01=7401 Quadruple 2-input Positive NANI (with open-collector output) BP 02=7402 Quadruple 2-input Positive NANI (with Open-collector Output) BP 04=7404 Hex Inverters in M.D. Gate BP 13=7413 Dual 4-input Schnitt Trigger P 02=7420 Dual 4-input Schnitt Trigger BP 04=7404 Hex Inverters (with Open-collector Output) BP 04=7404 Hex Inverters BP 20=7420 Dual 4-input Schnitt Trigger BP 20=7420 Dual 4-input Schnitt Trigger BP 40=7440 Dual 4-input Positive NAND Gates BP 40=7440 Dual 4-input Positive NAND Bath BP 41=7441 BCD to decimal nize driver BP 50=7450 Custor Segment Decoler/Drive DB 51=7453 Quad 2-input Expandable AND OR NO BP 51=7453 Quad 2-input Expandable AND OR NO BP 51=7453 Quad 2-input Expandable AND OR NO BP 53=7455 Quad 2-input Expandable AND OR NO BP 72=7472 Master clave J-K FID-FID B7 72=7473 Master clave J-K FID-FID B7 74=7474 Dual 0-type FID-FID B7 74=7481 Goht And the money BP 50=7480 Gated FUI Adders. BP 50=7480 Gated FUI Adders. BP 51=7481 Goht Poll Adders. BP 51=7482 Quad 2-input Exclusive QE Gates BP 51=7480 Gated FUI Adders. BP 51=7480 Gated Schult Adders. BP 51=7480 Charled FUI Adders. BP 51=7480 Gated FUI Adders. BP 51=7480 Gated Schult Adders. BP 51=7480 Charled FUI Adders. BP 51=7480 Charled FUI Adders. BP 51=7480 Charled Schult Adders. BP 51=7480 Charled FUI Adders. BP 51=7480 Charled Schult Actor Connters. BP 51=7480 Gated Schult Adders. BP 51=7480 Gated Schult Adders. BP 51=7480 Gated Schult Adders. B	Price and Qir, Pric Dual In-Line Plastic Id & 16 p Price and Qir, Pric 1-24 25-99 100 Gate	A.8 Type No. Case Leads Description Image: Construct of the second
BP191=74191 Binary Counter reversable	BP141=74141 BCD-to-Decimal Decoder/Driver BP145=74145 BCD-to-Decimal Decoder/Drivers BP151=74151 8-bit Data Selectors (with Strobe) BP153=74153 Dual 4-Line-to-Line Data Selector Multiplezers	s/ 	ALL PRICES IN NEW PENCE. Please send all orders direct to our warehouse and despatch department. BI-PAK SEMICONDUCTORS P.O. BOX 6, WARE, HERTS. Postage and Backing add 7p. Overees add extra for Airmail. Minimum order 50p.

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Our design and manufacturing experience and component bulk buying capacity make it possible to offer modules built

printed circuit boards, all modules are fitted with edge connectors to permit easy insertion and removal. They may also be wired in where desired.

> 71Z RANGE. Basic zener stabilised P.U. with floating output. For general use including switching & op. amp. circuits. Size

71Z9	± 9v at 30m A	Price £3·95 }each + £0·25
71Z12	± 12v at 15mA	>each + £0.25
71Z15	\pm 15v at 10mA	J P&P

71ZR RANGE. A more complex circuit than the 71Z Range giving greater stability with changing loads and with reduced ripple content. Output current limiting is included for general protection. An ideal P.U. for electronic instruments and control circuits. Size 4" x 3".

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714. Special power unit suitable for the Audio Signal Generator described in the May issue. Price £4.20 each + £0.25 P & P. Trade enquiries invited.

We are also distributors of the full range of Newmarket Transistors Limited's P.C. Modules HARVEY HALL (Dept. P.W.), BRECKLAND WORKS, EARLS ST., THETFORD, NORFOLK.

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H.A.C.

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Garrard SP25 Mk. III with KS40A cartridge. In good quality teak plinth with perspex dust cover. Complete with all leads ready to use #20. SP25 Mk. III deck only less cartridge £11.87.

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Acos Mic 45 \$1-12; ; Acos Mic 60 99;p ; Planet CM70 £1.50 ; Hand Mike 75p.

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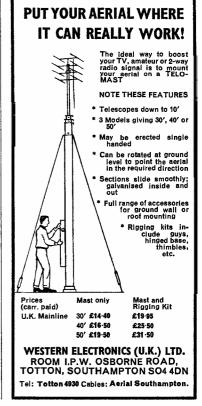
Famous for over 35 years for Short-Wave Equip-ment of quality, "H.A.C." were the Original suppliers of Short-Wave Receiver Kits for the amateur constructor. Over 10,000 satisfied customers-including Technical Colleges, Hos-pitals, Fublic Schools, R.A.F., Army, Hams, etc.

NEW "DX" RECEIVER

Improved one-value model "DX" mark 2. Complete kit—price \$3.80 (post & packing 20p.). Customer writes: "Australia_India and America at loud volume."—"I am 14 years of age and have logged over 130 stations, plus counciles Amateurs from all over the world."

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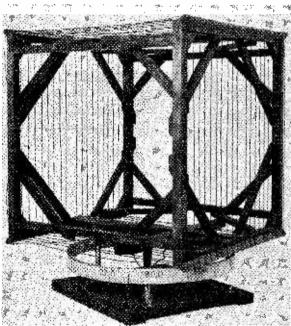


grated circuit-it was a clever bit of camera trickery!). Anyway, Mr. Ellis says that in his set there are more wires with nothing at the end of them than there are connecting components. The components appear to be in good condition. There valves are included (PMIA, D210, PMILF-possibly), the valve-holders are square and the four pins marked F, A, F, G. Stamped on the holders is the word "Benjamin" and "Genuine Bakelite."

There are two variable capacitors made by Ormond Engineering Co. each fitted with a dial similar to the "Committee Superfet". The coil is 7in. long and 4in. in diameter and is stamped "Trade ISOLO Mark" there are three windings of cotton or silk covered wire. Resistors are Dubilier Dumetohm which have the appearance of cartridge fuses, each one clipping into a holder. The capacitors have thumbscrew terminals as does a fully-shrouded transformer "Hollingwood" inscribed with markings for secondary, primary, grid, plpate, h.t.+ and +D. Also, one point to note is that there is a bracket attached to the base-board reading "Etherplus."

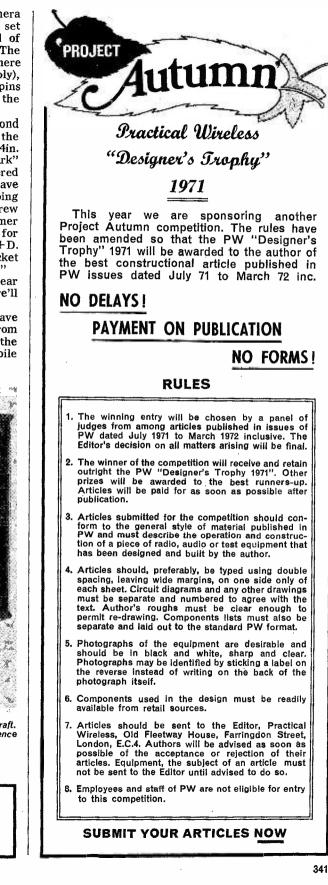
Once again, the staff of P.W. would like to hear more about this, so please drop us a line, and we'll pass the letters on.

Our aerial photograph is enough to make Dave Gibson's hair curl ("what hair?" shouts someone from the back row). What about strapping this one on the top of your wagon, Gibby and working a bit of mobile DX?



Actually it's an early frame aerial used for direction-finding in aircraft. The date is about 1916 and the photograph was lent to the Science Museum by the National Physical Laboratory.

In "Going Back" May 1971, we published a photograph which we captioned "Magnetic Detector". This should have read "Multiple Tuner" and we would like to thank all those readers who were kind enough to point this out.



practically wireless commentary by HENR

MOTORING correspondents are fond of telling us the tales of woe they experience with their new cars. Doors jam, windscreen wipers fail, handles fall off, and other, more technical failings begin to show after a short spell of use. "The suspension suffered badly



... experience with their new cars.

from hugging on anything more than a twenty-degree bend . . ."

They don't know the half of it. The benefits of mass production hit the radio industry long ago, and with all the paraphenalia of printed circuits and peripheral hardware, modern radio and audio equipment has reached its nadir of vulnerability.

Only last week we had a very expensive, very elaborate hi-fi amplifier on the bench, sighing dolefully. It coudn't sing; its protection circuits, which comprised more than half the twisted jungle through which we tried to hack our way, did their work too thoroughly. Every time a signal pushed past the preamps, Trl switched hard on, putting Tr2 "off" and interrupting the bias control of Tr3 which promptly bottomed. This overcame the zener regulation of Tr4 which is in the feedback line of . . .

Henry tuned in last week, hoping to brush up his faltering maths, and was greeted with the pontifical statement: "Mathematics is not so much about numbers as about sets."

Sets? Sets of what? Or did the Professor mean wireless sets? It might have been appropriate to our subject if he did, for the ensuing discussion was more philosophical than enlightening.

Some of the equipment that comes in for service within weeks of being sold must have been assembled under similar conditions. Perhaps, in the Buzzbox factory in Arnold's Wick, SW 19, the wires have got crossed and those overtime earners on Saturday mornings are listening to the cut and thrust of O-U discussion.

Well, not so much cut and thrust as snip and shove. Which may account for some of the untightened bearing clamps, twisted drive cords, unsealed iron-dust cores and knobs that fall off. The operator is away in a dream, lapped by the lulling voices. There used to be a saying in a radio factory where Henry once worked: "Lil's in love again."

It was invoked whenever we slaves of the troubleshooting department discovered a "run" of faults.

The inspectors would reject one set in five for "no-go" faults, normally. Then would come a spate of rejections, and we—the only true engineers in the factory, we averred, not excepting the designer—ran our delicate diagnostic probiscuses over them.

Hovering at our shoulder, the Production manager waited for the dread words: "R21 wrong value, should be 33k, not 33 ohms." We laid bets on the number of sets that Lil had allowed through as she dreamed over the new boy. The variables for handicapping were the rate of the conveyor, the alacrity of the Production manager and, top weight for the course, the slowness of the troubleshooter.

In that sort of job, every day was Saturday. Down in Arnold's Wick, SW 19, the Monday set, the rogue receiver, is the speciality of their range. After a week of use it hesitates and splutters.

We bang it. A knob falls off. We shake, and two programmes arrive together. The volume con-

Lil's in love

trol adds its crackling obligatto and then the tiny loudspeaker squawks in protest. So we take it in for service.

The knowledgeable salesman shakes his head sadly. 'Perhaps the worst model they made," he pronounces. "You didn't buy it here of course?" His question is more a statement; that isn't the sort of trash they would sell. But they do, eventually, repair it, after weeks of waiting for irreplaceable parts that have to be ferried from Japan in a leaking sampan.

And within another week it splutters and coughs into silence. A little tense, we face the salesman again. Could we see the manager? Not, it seems, without an appointment, but they guarantee their work and condescend to look at it again.

This time, again with a bill to pay, we are told that another vital component has failed. "Quite unforeseeable. The quality of the components used in these—er less expensive receivers . . ." The



'Lil's in love again.'

work done on their last job, the guaranteed work, could not cover the eventuality of that component's failure.

It would have been better, less expensive, if we had faced up to the truth. Ours was a Saturday set, or a Monday set, or whatever day our Lil habitually assembles errors down in Arnold's Wick, SW 19. Better thrown away.



High fidelity Monolithic Integrated Circuit Amplifier

Two years ago Sinclair Radionics announced the World's first monolithic integrated circuit Hi-Fi amplifier, the IC.10. Now we are delighted to be able to introduce its successor the Super IC.12. This 22 transistor unit has all the virtues of the original IC.10 plus the following advantages:

- 1. Higher power.
- 2. Fewer external components.
- 3. Lower quiescent consumption.
- 4. Compatible with Project 60 modules.
- 5. Specially designed built-in heat sink. No other heat sink needed.
- 6. Full output into 3, 4, 5 or 8 ohms.
- 7. Works on any voltage from 6 to 28 volts without adjustment.
- 8. NEW 22 transistor circuit.

- Output power 6 watts RMS continuous (12 watts peak).
- Frequency Response 5 Hz to 100KHz \pm 1dB.
- **Total Harmonic Distortion** Less than 1%. (Typical 0.1%) at all output powers and all frequencies in the audio band.
- Load Impedance 3 to 15 ohms. Power Gain 90dB (1,000,000,000 times)
 - after feedback.
- Supply Voltage 6 to 28 volts (Sinclair PZ-5 or PZ-6 power supplies ideal).
- Size 22 x 45 x 28 mm including pins and heat sink.
- Input Impedance 250 Kohms nominal. Quiescent current 8mA at 28 volts.
- Price: including FREE printed circuit board for mounting. **£2.98** Post free

Sinclair Radionics Ltd., London Rd, St. Ives Huntingdonshire PE17 4HJ Telephone St Ives (048 06) 4311 With the addition of only a very few external resistors and capacitors the Super IC.12 makes a complete high fidelity audio amplifier suitable for use with pick-up, F.M. tuner etc. Alternatively, for more elaborate systems, modules in the Project 60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radios, oscillators etc. The very low quiescent consumption makes the Super IC.12 ideal for battery operation.



Sinclair Project 60



the world's most advanced high fidelity modules

Sinclair Project 60 presents high fidelity in such a way that it meets every requirement of performance, design, quality and value and now that the remarkable phase lock loop stereo FM tuner is available, it becomes the most versatile of high fidelity systems. With Project 60, it is possible to start with a

modest mono record reproducer and expand it to a sophisticated stereophonic radio and record reproducing system of fantastically good quality to hold its own with any other equipment, no matter how expensive. Project 60 is a unique high fidelity module system where compactness and ease of assembly are combined with

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A	Simple battery record player	Z.30	Crystal P.U., 12V battery volume control	£4.48
8	Mains powered record player	Z.30, PZ.5	Crystal or ceramic P.U. volume control etc.	£9.45
С	20+20W. R.M.S. stereo amplifier for most needs	2 x Z.30s. Stereo 60, PZ.5	Crystal. ceramic or mag. P.U., most dynamic speakers, F.M. tuner etc.	£23.90
D	20+20 W. R.M.S. stereo amplifier with high performance spkrs.	2 x Z.30s, Stereo 60, PZ.6	High quality ceramic or magnetic P.U., F.M. Tuner. Tape Deck. etc.	£26.90
E	40+40W. R.M.S. de- luxe stereo amplifier	2 x Z.50s, Stereo 60 PZ.8, mains trsfrmr	As for D	£34.88
F	Outdoor P.A. system	Z.50	Mic., up to 4 P.A. speakers controls, etc.	£5.48
G	Indoor P.A.	Z.50, PZ.8, mains transformer	Mic., guitar, speakers, etc., controls	£19.43
Н	High pass and low pass filters	A.F.U.	C, D or E	£5.98
J	Radio	Stereo F. M. Tuner	C, D or E	£25.00

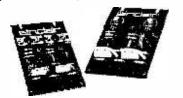
circuitry that is far in advance of any other manufacturer in the world. Thus it is extraordinarily easy to assemble any combination of modules using nothing more complicated than the simplest of tools, and you certainly do not have to be experienced to build with complete confidence. The 48 page manual free with Project 60 equipment makes everything easy and you can house your assembly in an existing cabinet, motor plinth, free standing cabinet or virtually any arrangement you wish. Once you have completed your assembly you will have superlatively good equipment to give you years of service and enjoyment. You will have obtained superb value for money because Project 60 is the best selling modular system in Europe and can therefore be produced at extremely competitive prices and with excellent quality control.

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Sinclair Project 60

Z.30 & Z.50 power amplifiers



The Z.30 and Z.50 are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use Z.30 or Z.50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.

SPECIFICATIONS (Z50 units are inter-changeable with Z.30s in all applications). Power Outputs

Power Outputs Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M.S. into 3 ohms using 30 volts. Z.50 40 watts R.M.S. into 3 ohms using 40 volts: 30 watts R.M.S. into 8 ohms. using 50 volts. Frequency response: 30 to 300 000 Hz ±1dB.

Distortion: 0.02% into 8 ohms.

Signal to noise ratio: better than 70dB unweighted.

Input sensitivity: 250mV into 100 Kohms. For speakers from 3 to 15 ohms impedance. Size 3½ x 2¼ x ½ in.

Z.30 Built tested and guaranteed with circuits and instructions manual **F4 48** £4.48

Z.50

Built. tested and guaranteed with circuits and instructions manual. **F5_48** £5.48

Power Supply Units



Designed specially for use with the Project 60 system of your choice.

Illustration shows PZ.5 to left and PZ.8 (for use with Z.50s) to the right. Use PZ.5 for normal Z.30 assemblies and PZ.6 where a stablised supply is essential.

PZ-5 30 volts' unstabilised £4.98 PZ-635 volts stabilised £7.98 PZ-8 45 volts stabilised (less mains transformer) £7.98 PZ-8 mains transformer £5.98

Guarantee

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each them, we will return your money at once. East module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter No charge for postage by surface mail. Air-mail charged at cost.

Stereo 60 pre-amp/control unit



Designed for the Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

SPECIFICATIONS

Input sensitivities: Radio-up to 3mV. Mag. p.u. 3mV: correct to R.I.A.A. curve ± 1dB:20 to 25.000 Hz. Ceramic p.u.-up to 3mV: Aux-up to 3mV. Output: 250mV

Signal-to-noise ratio: better than 70dB. Channel matching: within 1dB.

Tone controls: TREBLE + 15 to —15dB at 10KHz BASS + 15 to—15dB at 100Hz. Front panel: brushed aluminium with black knobs and controls.

£9.98

Size: 8 # x 1 ½ x 4 ins. Built, tested and guaranteed.

Active Filter Unit



For use between Stereo 60 unit and two Z.30s or Z.50s, and is easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible The A.F.U. is suitable for use with any other amplifier system. Two stages of filtering are incorporated rumble (high pass) and scratch (low pass). Supply voltage - 15 to 35V. Current - 3mA. H.F. cut-off (-3dB) variable from 28k Hz to 5kHz. L.F cut-off (-3dB) variable from 25Hz to 100Hz. Distortion at 1kHz (35V. supply) 0.02% at rated output. Ruult, tested £5.98

and guaranteed



Stereo FM Tuner



first in the world to use the phase lock loop principle

Before production of this tuner, the phase lock loop principle was used for receiving signals from space craft because of its vastly improved signal to noise ratio over other systems. Now, for the first time, the principle has been applied to an FM tuner with fantastically good results. Other original features include varicap diode tuning, printed circuit coils, an I.C. in the specially designed stereo decoder and squelch circuit for silent tuning between stations. Sensitivity is such that good reception be-comes possible in difficult areas. Foreign stations can be tuned in suitable conditions and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated, a panel indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.

SPECIFICATIONS:

Number of transistors: 16 plus 20 in I.C. Tuning range: 87.5 to 108 MHz Capture ratio: 1.5dB Sensitivity: $2\mu V$ for 30dB quieting: $7\mu V$ for full limiting. Squelch level : 20µV A.F.C. range: ±200 KHz Signal to noise ratio : >65dB frequency response: 10Hz-15KHz Audio fi (±1dB) Total harmonic distortion: 0.15% for 30% modulation Stereo decoder operating level: 2µV Pilot tone suppression: 30dB Cross talk: 40dB I.F. frequency: 10.7 MHz Output voltage: 2 x 150mV R.M.S. Aerial Impedance: 75 Ohms Indicators: Mains on: Stereo on: tuning indicator Operating voltage: 25-30 VDC Size: 3.6 x 1.6 x 8.15 inches: 91.5 x 40 x 207 mm Souri - and Steren Oute A G C Amphie Voltage controlle osc. later Price: £25 built and tested. Post free

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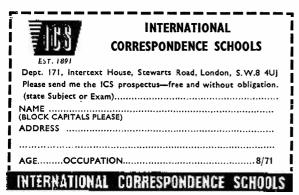
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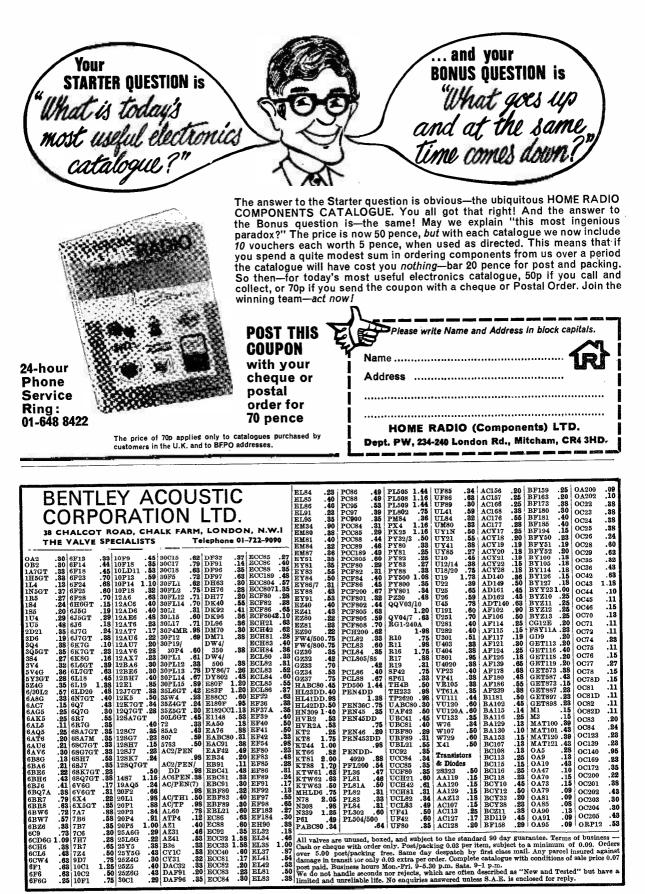
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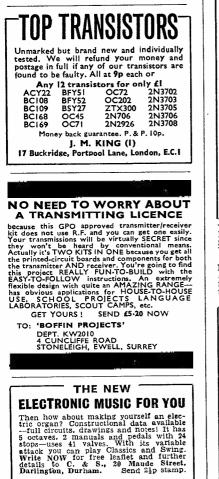
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