# PRACTICAL WRE L E <br> AUGUST 1971 20p 

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 for Factory Bench Line Assembly A precision instrument-supplied with standard $3 / 16^{\prime \prime}(4.75 \mathrm{~mm})$ diameter, detachable copper chisel-face bit*.Standard temp. $360^{\circ} \mathrm{c}$ at 23 watts.
Special temps. from $250^{\circ} \mathrm{C}$ $410^{\circ} \mathrm{c}$.

## *Additional Stock Bits

(illustrated) available

## COPPER

$\xrightarrow{\text { B } 38}$
B38, - $\mathbf{3 . 2} \mathrm{mm}$ chisel face
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B 44 LL $\frac{3}{16 *}$ - 4.75 mm SCREWDRIVER

Don't take chances. We don't. All our ADCOLA Soldering Instruments are of impeccable quality. You can depend on ADCOLA day after day. That's why they're so popular. You get consistent good service. . . reliability . . . from our famous thermally controlled ADCOLA Element and the tough steel construction of this ideal production tool.


## *

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 can effectively make the 'mono' facility redundant on a stereo amplifier. mono source to reallstically simulate the stereo effect with music. For amplifiers with a tape-monitor facility, connection to the tape socket will allow operation from any selected mono source. Alternatively the unit may be connected in series with most programme sources. We provide a lead and 6 month guarantee. Send s.a.e. for further detalls stating amplifier.
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some ampliflers." some amplifiers." ... there is of material the effect of this simulator is pleasing, ne ver ludicrous and may well be judged worthwhile." Hi-Fi News \& Record Review (New Products section).
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BRAND SEW FULLY TRANSISTORISED PRINTED CREDUIT METAL DETEECTOR MODULE. Reody bsilt and tested-just plug in a PP3 battery and 'phones and it's working. Put it in a aase,
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TREASURE LOCATOR TRANSISTORISED
NOW IT'S HERE AT LAST, after experimenting for four and a half months with a multitude of difierent circuits and carrying out actual field tests with prototypes, our design team have come
up with this real winner. This fully portable transistorized metal ip with this real wimer. This fully portable transistorized metad locator detects and tracks down buried metal objects-it signals
exact location with loud audible sound (no phones used)-uses xact location with loud audibe sound no phones used)-usea
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## 28 watts, r.m.s. 40 Hz to $40 \mathrm{kHz} \div 3 \mathrm{~dB}$

There are two stereo amplifiers - the RT100 forceramiccartridges, the RI101 for magnetic Both incorporate FETS (FIELD EFFECT TRANSISTORS), just like top -priced units FETs give you more of the signal you wantiand almost none of the background hiss vou don't. Both units have ajack socket to plug in headphones and thefe's a separate output for tape recorder F Filters Xan unusual feature in this price rapge) and tone controls give a wide range of bass and treble adjustment which compensate fot input deficiencies and domestic acoustic conditions.


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## SYSTEM 2

As System : but with $2 \times$ Dulo Type II! Available complete for $\mathbf{E 6 9} \& \mathbb{E} \mathrm{p}$ \&p

Viscount III Amplifier RE100 $£ 17.00+90 \mathrm{p}$ p\&p $2 \times$ Duo trpall speakers, pair $\mathrm{I} 14.00+$ E2 p\&p arrard SF 25 Mkwil with CER diamond Total $\overline{55200}$
14 watts per channelinto 3 to 4 ohms. Total distortion a A. 1 A A Radio 150 mV into 220 K (Sensitivities given at full power,) Tape out facilities; headphone socket, filter characteristics Bass. 112 dB to -77 dB CHZ Bass filter: 6dB perioctave cut Trebie contro B $\max$ ) RT101-P.U. $1 . \&$ radio - $85 \mathrm{~dB} . \mathrm{P} \cup 2-5 B d B$ RT100 same as RT101 but P $\mathrm{U} 2 \mathbf{2 5 0} \mathrm{mV}$ into . 3 Meg Cross talk better than -35 dB on allininuts Overioad choracteristics 26 dB on all inputs Size $13 \mathrm{~F} \times \mathrm{P} \times 3 \mathrm{~F}$

# SOUND 50 

## 50 WATT AMPLIFIER \& SPEAKER SYSTEM


(350m W Output)
7 transistor fully-tunable M.W.-L.W. superhet portable. Set of parts. Complete with all components, including ready etched and drilled printed circuit board-back printed for foolproof construction. MAINS POWER PACK KIT : 75p extra.
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7-transistor fully tunable M.W.-L.W. superhet portable. Set of parts. The Jatest modulised and pre-alignment techniques make this simple to build. Sizes: $12 \times 8 \times 3 \mathrm{in}$.

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in simulated teak case $\mathbf{£ 7 . 2 5}$ plus P. \& P. 50p
SPECIFICATIONS
Output 10 watts. Output impedance- 3 to 4 ohms. Inputs 1. -xtal mic 10 mV Tone Controls-Treble control range $\pm$ 12 dB at 10 KHz . 2. -gram/radio 250 mV . Bass control range $\pm 13 \mathrm{~dB}$ at 100 Hz .
Frequency Response-(with tone controls central) Minus 3dB points at 20 Hz and 40 KHz . Signal to Noise Ratio-better than -60 dB . Transistors-4 silicon Planar type and 3 Germanium type. Mains input- $220 / 250$ V. A.C. Size of chassis- $10 \frac{3}{4} \mathrm{in}$. $x 4 \frac{3}{2} \mathrm{in}$. x 2 i in . For use input-220/250V. A.C. Size of chassis-104in. X all makes of pick-ups and mikes. Built and tested.

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Beautifully designed to blend with the interiors of all cars. Permeability tuning and long wave loading coils ensure excellent tracking, sensitivity and selectivity on both wave bands. R.F. sensitivity at 1 MHz is better than 8 micro volts. Power output into 3 ohm speaker is 3 watts. Pre-aligned I.F. module and tuner together with comprehensive instructions guarantees success first time. 12 volts negative or positive earth. Size 7 in $\times 2$ in $\times 4 \frac{1}{2}$ in deep.

See previous page for address


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MODEL MPR 30055 BAND MODEL MPR 30166 BAND


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| 1R5 | . 28 | 25U4GT | -57 | 96 | . 38 | EL500 | . 62 | PCL82 | -36 | UABC80 | .38 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 185 | -22 | 30 Cl | . 30 | DY86 | . 28 | EM80 | . 61 | PCL83 | -69 | UAF42 | .51 |
| 1T4 | -16 | 30 Cl 5 | -63 | DY87 | . 28 | EM81. | . 41 | PCL84 | . 87 | UBC41 | $5^{2}$ |
| 3 S 4 | -28 | $30 \mathrm{C17}$ | . 80 | DY802 | 40 | EM84 | . 33 | PCL85 | . 45 | UBF80 | $\cdot 34$ |
| 3V4 | - 37 | 30 Cl 8 | . 67 | EABC80 | . 32 | EM87 | .37 | POL86 | -41 | UBF88 | . 38 |
| 5U4G | -26 | $30 \mathrm{F5}$ | $\cdot 76$ | EAF42 | . 50 | EY51 | -38 | PCL88 | -72 | UCC84 | . 35 |
| 5V4G | . 37 | 30 FL 1 | -63 | EB41 | . 40 | HY86 | -32 | FCL800 | $\cdot 77$ | UC085 | . 36 |
| 5 Y 39T | . 30 | 30 FL 12 | .72 | EB91 | . 11 | EZ40 | . 43 | PENA4 | . 42 | UCF80 | -36 |
| 524G | $\cdot 37$ | 30 FL 14 | .72 | EBC33 | - 40 | EZ41 | -43 | PEN36C | C $\cdot 70$ | UCH43 | -62 |
| 6/30L2 | -58 | 3011 | -32 | EBC41 | -54 | EZ80 | - 23 | PFL200 | . 58 | UCH81 | . 32 |
| 6AL5 | -11 | 30 L 15 | -62 | EBC90 | . 22 | EZ81 | -24 | PL36 | . 49 | UCL82 | . 35 |
| 6AM6 | -13 | 30 Ll 7 | $\cdot 73$ | EBF80 | . 38 | GZ30 | . 37 | PL81 | . 48 | UCL83 | . 55 |
| $6 \mathrm{AQ5}$ | -26 | 30 P 4 | -65 | EBF89 | - 31 | GZ32 | . 48 | PL81A | . 51 | UF41 | . 56 |
| 6AT6 | -22 | 30 P 12 | $\cdot 77$ | ECC81 | -18 | GZ34 | . 50 | PL82 | .38 | UF89 | . 38 |
| 6AU6 | -22 | 30P19 | -65 | ECC82 | . 33 | KT41 | $\cdot 77$ | PL83 | . 35 | UL41 | -60 |
| 6BA6 | -22 | 30 PL 1 | -63 | ECC83 | .35 | KT61 | -55 | PL84 | . 33 | UL44 | . 00 |
| 6BE6 | . 23 | 30 PL 13 | . 85 | ECC85 | . 28 | KT66 | .83 | PL500 | . 65 | UL84 | . 35 |
| 6BJ6 | -42 | $30 \mathrm{PL14}$ | . 70 | ECC804 | . 60 | LN319 | . 68 | PL504 | . 67 | UM84 | . 22 |
| 6BW7 | . 60 | $30 \mathrm{PL15}$ | . 90 | ECF80 | . 30 | LN329 | . 72 | PM84 | . 37 | UY41 | . 41 |
| 6CD6G | -10 | 35L6GT | . 45 | ECF82 | .30 | LN339 | -63 | PX25 \& | 81.17 | UY85 | . 28 |
| 6 Fl 4 | $\cdot 45$ | 35 W 4 | -28 | ECH 35 | -30 | N78 | -87 | PY32 | . 55 | VP4B | .77 |
| 6 F 23 | $\cdot 71$ | 3584GT | -25 | ECH 42 | . 68 | P61 | . 50 | PY33 | . 55 | 277 | . 22 |
| 6 F 25 | . 62 | 807 | . 45 | ECH81 | . 29 | PABC80 | $\cdot 35$ | PY81 | . 27 | Transi | I |
| 6K7G | . 12 | 6063 | -62 | ECH83 | . 41 | PC86 | - 51 | PY82 | -27 | AC107 | . 17 |
| 6K8G | -17 | AC/VP | . 77 | ECH84 | .37 | PC88 | . 51 | PY83 | . 28 | AC127 | . 18 |
| 6Q7G | -28 | B349 | -65 | ECL80 | .35 | PC96 | - 42 | PY88 | $\cdot 35$ | AD140 | . 37 |
| 6SL7GT | -27 | B729 | . 62 | ECL82 | . 33 | PC97 | $\cdot 40$ | PY800 | . 37 | AF115 | . 20 |
| 6SN7GT | . 30 | CCH35 | . 67 | ECL86 | . 40 | PC900 | - 37 | PY801. | $\cdot 37$ | AF'116 | . 20 |
| 6V6G | -23 | CL33 | . 92 | EF39 | . 23 | PCC84 | . 32 | R19 | -32 | AF117 | . 20 |
| 6 V 6 GT | -32 | CY31 | $\cdot 38$ | EF41 | .60 | PCC85 | $\cdot 30$ | R20 | -65 | AF118 | - 48 |
| $6 \times 4$ | -23 | DAF91 | . 22 | EF80 | -24 | PCC88 | . 45 | U25 | . 68 | AF125 | . 17 |
| 6X5GT | . 28 | DAF96 | -38 | EF85 | . 31 | PCC89 | . 47 | U26 | . 65 | AF127 | .17 |
| $10 \mathrm{P13}$ | . 60 | DF33 | . 38 | EF86 | . 31 | PCC189 | -51 | U47 | . 68 | OC26 | .25 |
| 12AH8 22 | 2.25 | DF91 | . 18 | WF89 | -27 | PCC805 | . 65 | U49 | . 65 | OC44 | . 12 |
| 12AT7 | . 18 | DF96 | .36 | EF91 | . 13 | PCF80 | . 30 | U50 | . 39 | OC45 | . 12 |
| 12AU6 | . 23 | DH77 | . 22 | EF183 | -29 | PCF82 | -32 | U52 | .31 | OC71 | . 12 |
| 12AU7 | . 23 | DK32 | .37 | EF184 | . 32 | PCF86 | . 47 | U78 | -24 | OC72 | . 12 |
| 12AX7 | . 28 | DK91 | . 28 | EH90 | .42 | PCF'800 | . 67 | U191 | . 62 | OC75 | . 12 |
| 19BGGG | . 87 | DK92 | . 42 | ELS3 | . 55 | PCF801 | . 88 | 0193 | . 42 | OC81 | .12 |
| 20 F 2 | . 67 | DK96 | .38 | EL34 | . 49 | PCF802 | . 45 | U251 | . 72 | OC81b | .12 |
| 20 P 3 | . 85 | DL35 | -35 | EL41 | . 55 | PCF805 | .67 | U301 | . 52 | $0 \mathrm{C82}$ | . 12 |
| 20P4 | . 92 | DL92 | . 28 | EL84 | . 24 | PCF806 | . 80 | O329 | $\cdot 72$ | OC82 | . 12 |
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Primarias 200-250v. $50 \mathrm{c} / \mathrm{s}$. Screened MIDGET CLAMPED TYPE $2 \frac{5}{2} \times 2 \frac{3}{8} \times 24 \mathrm{in}$. $250 \mathrm{v} ., 60 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a}$
$250-9-250 \mathrm{v}, 60 \mathrm{~mA} 6.3 \mathrm{v} 2 \mathrm{a}$
FULLY SHROUDED UPRIGHT MOUNTMNG $250-0-250 \mathrm{v} .60 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a}, 0-5-6.3 \mathrm{v} .2 \mathrm{a}$. $£ 1.25$ $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a} ., 0-6-6.3 \mathrm{v}$. 3 a . 81.99 $300-0-300 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}, 0-5-6.3 \mathrm{v} .3 \mathrm{a}$
$300-0-300 \mathrm{v} .130 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}$, c.t., 6.3 v .1 a. For Mullard 510 Amplifier
 $350-0-350 \mathrm{v}$. $150 \mathrm{~mA}, 6.3 \mathrm{v}$. $4 \mathrm{a},, 0-5 \cdot 6.3 \mathrm{v}$. 3 a . 52.40 $425-0-425 \mathrm{v} .200 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}$., c.t., 5v. 3a. 84.49 425-0-425v. $200 \mathrm{~mA}, 6.3 \mathrm{v}$. $4 \mathrm{a} ., 6.3 \mathrm{v}$. $3 \mathrm{a} ., 5 \mathrm{v}$
3 a
$450-0-450 \mathrm{v} .250 \mathrm{~mA}, 6.3 \mathrm{w} .4 \mathrm{a} .$, c.t., $5 v .3 \mathrm{a}$
то
TOP SHROUDED DROP-THRO' TYPE $250-0.250 \mathrm{v} .70 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a}, 0-10$
$250-0-250 \mathrm{v} .100 \mathrm{~mA} .6 .3 \mathrm{v} .3 .5 \mathrm{a}$
$250-0-250 \mathrm{v} .100 \mathrm{~mA} .6 .3 \mathrm{v}$. 3.5 亿.
$250-0.050 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a} ., 6.3 \mathrm{v}, \mathrm{ja}$. $350-0-35.0 \mathrm{v} .80 \mathrm{~mA}, 6.3 \mathrm{v} .2 \mathrm{a}, 0-5-6.3 \mathrm{v} .2 \mathrm{a}$.
$250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a}$
$0-5-63 \mathrm{v}$ $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a} ., 0-5-6.3 \mathrm{v} .3 \mathrm{a}$
$300-0-300 \mathrm{v} .100 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a} .$,
$0-5-6.3 \mathrm{v} .3 \mathrm{a}$ $300-0-300 \mathrm{v}, 130 \mathrm{~mA}, 6.3 \mathrm{v} .4 \mathrm{a} ., 0-5-6.3 \mathrm{v} .1 \mathrm{a}$



HILAEAT OT TRANSISTOR POWER PACK 6 jpes $6.3 \mathrm{v}, 1.5 \mathrm{ta}$. 45 p ; 6.3v. 2a. 49 p ; 6.3v. 3a. 69p; 6.3v. 6a. 21.15; 12v. 1a. s0p; 12v. 3a. or 24v. 1.5 a \$1.20;0.9-18v. 12а. 99p; 0-12-25-42v. 2a. 21. 60 CHARGER TRANSFORMERS 0-9-15v. 11a. 95p;
 AUTO (Step UP/step DOWH) TRANSFORMERS
$0-110 / 120 \mathrm{v}$ 200-230-250\% $50-80$ watts 980.
 OUTPUE TRANEFORMERS
Standard Pentode $5,000 \Omega$ or $7,000 \Omega$ to $8 \Omega \quad 45 p$
Push-Pull 8 patts EL84 to $3 \Omega$ or $15 \Omega$.. Push-Pull 8 watts EL84 to $3 \Omega$ or $15 \Omega$.
Pugh-Pull 10 watts 6 V6, FCL 86 to $3,5,8$.

Push-Pull EL84 to 3 or 15 § $10-12$ watts... El. 20 Push-Pull Ulitra Linear for Mulard 510 , etc. Push-Pull 15-18 watte, sectionally wound
$6 \mathrm{~L} 6, \mathrm{KT66}$, etc, for 3 or $15 \Omega \ldots . .$. 6L6, KT66, etc., for 3 or $15 \Omega$ $\$ 1.80$ Ptash-Pull 20 watt high quality sectionally
wound EL34, $6 \mathrm{~L} 6, \mathrm{KT66}$ etc. to 3 or $15 \Omega$
E 2.99 Wound EL34, 6 L6, KT66 etc. to 3 or $15 \Omega$. 22.98
8MOOTHIHG OHOKES $150 \mathrm{~mA}, 7-10 \mathrm{H}$. 250


$350 \Omega 45 p ; 60 \mathrm{~mA}, 10 \mathrm{H}, 400 \Omega 20 \mathrm{~S}$.
SELCNIUM RECTIFIRRS F- W. (Bridged)
All 6/12v. D.C. output. Max. A.C. input $18 v$
1a. 25 p .2 a .85 p .3 a .50 p .4 a . 65 p .6 a .80 p .


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## BC. 221 MAINS POWER UNITS

200/250v I/P O/P plus 135v at 20 Ma from electronic voltage stabiliser also 6.3v A.C. for heaters. Uses 4 valves made to fit in battery compartment of unit with small control box with swt and fuses. Supplied new with circ and mains lead. Price $\mathbf{5 8} \cdot 00$ plus 60p carr.

## STATIC INVERTORS $115 \mathrm{~V} 400 \mathrm{C} / \mathrm{S}$ I PHASE

These all-transistor units provide a sine wave $O / P$ from a D.C. I/P of 23 to 28v D.C. at approx. 9 amps for an O/P of 180 VA . Use 44 transistors all silicoñ except O/P switching. Overall size $9 \times 10 \times 3^{\prime \prime}$. These units are fitted overload protection and have stabilised O/P. Made by A.C. Cossor to a very high specification. Supplied new unused with connecting data.

Price $\mathbf{5 1 2 . 0 0}$ plus 50p carr.

## RX/IND APN-9

This is a swt tuned Rx with CRT Ind unit, the Rx covers $1 / 8$ to 2 $\mathrm{Mc} / \mathrm{s}$ in 4 channels. The Ind section uses CRT type 3BP1 $3^{\prime \prime}$ green screen and 34 octal type valves 6SN7, 6SL.7, 6SK7, 6SJ7, $6 \mathrm{H} 6,6 \mathrm{Y} 6,5 \mathrm{Z3}, 2 \mathrm{Z} 2$, VR105, 6N7, 6SA7, there is also a high grade 100 Kc xtal, the CRT is fitted Mu Metal shield, all contained in case size $20 \times 12 \times 8^{\prime \prime}$ black crackle finish. These units are for $115 \mathrm{v} 400 \mathrm{c} / \mathrm{s}$ supply, the tube is well suited to scope use or modiflcation to $1.6 \mathrm{Mc} / \mathrm{s}$ Pan Adap. Supplied with circ. Available new with magnifier and visor at £8 plus 75p carr.

## HEAVY DUTY MAINS TRANS

Pria. 200/220/240v 50c/s Sec $500-0-500$ at 400 Ma or can be connected to give 1 Kv at 200 Ma . Varnish finish tag connections, size overall $5 \frac{1}{2} \times 5 \frac{1}{2} \times 4 t$. Supplled in new cond.

Price $\mathrm{E} 2.25^{25}$ plus 40 p post.

## OSCILLOSCOPES VARIOUS

Hartley type 13a with probe leads etc. Good condition. Price £22.00. Solarton CD513 used condition less graticule D.C. to $10 \mathrm{Mc} / \mathrm{s}$ blue phosphor tube $£ 18$. Solartron CD513.2 D.C. to $10 \mathrm{Mc} / \mathrm{s}$ green phosphor tube. Good condition. Price $£ 35$. USM-25 (OS-4) $115 \mathrm{v} 50 \mathrm{c} / \mathrm{s}$ I/P high grade pulse and time measuring scope response to $11 \mathrm{Mc} / \mathrm{s}$. Good condition. Can be used as general purpose scope with probes, etc. Price $£ 18$ all scope plus £1 carr. All units tested supplied with circuit diagrams.

## MISC. ITEMS

Solartron Stabilised O/P P.U. 200/250v I/P, O/Ps H.T. 250 or 300 v at $200 \mathrm{Ma}, 6.3$ at 4 a twice, 6.3 at 1a. Price 54.50 . Delay unit with 230v to $6.31 \cdot 7$ a and 6.3 .3a trans, 6CH6, EF91, EB91, ECC82 valves, $2 \times$ tog. swts, $2 p 11 \mathrm{w}$ yax swt etc. Price £1.50. Trig Stab Unit with $2 \times 0 C 45$ and $2 \times 0 C 41$ transis. delay units, $6 \times$ wander plugs, pots. etc. in case $11 \times 6 \frac{1}{2} \times 5^{\prime \prime}$. New £1-50. Variacs $115 \mathrm{v} 400 \mathrm{c} / \mathrm{s}$ can be used on 40 v AC 50c/s to give 0 to $40 \mathrm{v} O / \mathrm{P}$ at $5 \mathrm{amps} £ 1 \cdot 75$. Meters 0 to $1 \mathrm{Ma} 3 \frac{1}{2}^{\prime \prime}$ scaled 0 to 1 E1-50. 1~0-1 Ma $3 \frac{1}{2} " s$ scaled 1-0-1 玉1.50. 500 Ua scaled 0 to $52 \frac{1}{2}^{\prime \prime}$ OSD £1. Transformers 230 Pria. Sec 235-0235 at $80 \mathrm{Ma} 6.3 \mathrm{3a} 6.3$ 1a, 5 v 2 a . Price $£ 150$. Also Sec $250-0-250$ at $60 \mathrm{Ma} 5 \mathrm{v} 2 \mathrm{a}, 6 \cdot 32 \mathrm{a}$ soiled. £1.00. Table Cabinets size $19^{\prime \prime} \times 12^{\prime \prime} \times 10^{\prime \prime}$ with front panel and some parts $£ 1 \cdot 50$. American 73 Radio Mag, new back issues 8 for $\mathbf{E l} 1 \cdot 45$. Silicon Diodes INi614 200 P.I.V. 5a ea. 4 for 50p. INI206 600 P.I.V. 12a ea. 4 for $\mathbf{E 1} \cdot \mathbf{2 5}$. Choke L.V. $\cdot 25 \mathrm{H}$ at 1 amp. Price 65p.

All above prices include post or carr. All goods ex equipment unless stated otherwise. S.A.E. with enquiry


57 HAIN ROAD, SHEFFIELD S9 5HL

 can be mixed．Fitted renowned Philips plug－in pick－up With styins LP Stereo／EP and 78．Sonsitivity 100 mV ． Frequeacy rasponse $80 \mathrm{cps}-16 \mathrm{Kc} / \mathrm{s}$ ．Lightweight stylns preamure 3－6 gramames，Board size required $14 \times 121 \mathrm{in}$ ． Above 4in．Below 2tin．

## PHILLPS PORTABLE PLAYER CABINET

 sive $18 \times 10 t \times$ rin．Cut for above ceck．Amplifer space $14 \times 5 \times 34 \mathrm{in}$ ．Satin ehuminiusu front grille．Reslly gmart appearance．Blsck／White or Green／Gres． Cbrome fittings．
## BSR C． 109 SUPERSLIM STEREO AND MONO CHANGER

Plays 18＂， $10^{*}$ or $7^{7 \prime}$ records． Arto of manual．A high relisbility with 18 months grarantoe．AC 800／2507． Elice $18 \frac{1}{4} \times 11$ in
Above motor board sizin． below motor boara bing．
with STEEEO and
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GABRARD PLAXRRS with Sonotone 9TA Cartridges Gtereo Diamond sud Mono Sapphire．8P25 Mik II 815 model 8500 Stereo and Mono Autochanger 814 ．Post 25p． REGORD PLAYER PORXARLE CABINET Bpace for amplifter and antochsnger．Post 85p－3． 85 ROS DE－LUXE 8 WATT AMPLIFLER．Resdy made with 2uttage triode pentode vilve， 8 writz ontpat．Tons gnd volume controls Isolated maing traniformer，znobs londspeaker ralves EOL88，EZ 880
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All standerd fixing complete with stylus．
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| IF．P50／200 $470 \mathrm{La} / \mathrm{s} .88 \mathrm{p}$ | Printed Circuit，PCAI | rd I．F．P50／3cc．．．．．．88p 7．B．Toning Gang P51／1 or P51／2 ．．．．．．．88p（Weyrad Bookht


． 8 ．．． 55 p
VOLUME CONTROLS 80 omm Coax 4p．yd． Long spindlez．Hidget Size BRIFISM AERIALFTE 40 yd． $51-40 ; 60$ yd． 82.
 WIRE－WOUND 3－WART POTF．WTRE－WOUNDB－WATH Small type with small knob．STANDARD SIZE POTg．



PIW\＆ 86 per packet 179．FACE CUTVTRES 88 p ．
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BLAMK ALUMIMIUM CZABSIS． 18 g．w．g． $2 \frac{1}{2 i n}$ siden． $6 \times 4 \mathrm{jn}$ ． $4 \mathrm{pp} ; 8 \times 6 \mathrm{in} .50 \mathrm{p} ; 10 \times 7 \mathrm{in} .70 \mathrm{p} ; 14 \times 9 \mathrm{gin} .80 \mathrm{p}:$ $16 \times 6 \mathrm{in} .90 \mathrm{p} ; 12 \times 8 \mathrm{n} .50 \mathrm{p}$ ．
ALDMIIIUM PANGLS 18 s．w．g． $6 \times 4 \mathrm{in} .8 \mathrm{p} ; 8 \times 6 \mathrm{in} .15 \mathrm{p}:$
$10 \times 7 \mathrm{n} .17 \mathrm{p} ; 12 \times 8 \mathrm{in} .23 \mathrm{p} ; 14 \times 9 \mathrm{in} .27 \mathrm{p} ; 12 \times 12 \mathrm{in} .32 \mathrm{p}$. 1 inch DIAMrmep WATE－CEAMGE SWMCRE 25 p 1p．2－way，or 2 p．6－way or 3 p．4－way 25p each． 1 p．12－way
 2 p .6 －way，${ }^{3} \mathrm{p} .4$－way，$\frac{4}{} \mathrm{p}$ ． 5 －way． 6 p ． 2 －way， 1 waiez 60 p ，


ALL PURPOSE HEADPHONES E．R．HEADPEONES 200 ohms Super Sensitive． LOW RESIRTANCE HEADPHONES 3.5 ohms ＇THE INSTANT＇
BULK TAPE
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 $50 / 50 \mathrm{~V}$ ．． $10 \mathrm{p} |$| $32+82 / 850 \mathrm{~V}$ | 25 p | $100+50+50 / 860 \mathrm{~V} 4 \mathrm{p}$ |
| :--- | :--- | :--- | SUB－MIN．ELECTROLTMICS．1，2，4，5，8，16，25，80，50，100， $200 \mathrm{mF} 15 \mathrm{~V} 10 \mathrm{p} ; 500,1000 \mathrm{mF} 12 \mathrm{~V}$ 18p； 2000 mF 25 F 96 p CREAMIC 10F to $0.01 \mathrm{mF}, 4 \mathrm{p}$ ．Silver Fiies 24 to 5000 pF ， 4 p PAPER 350V－0．1 4p， $0.513 \mathrm{p} ; 1 \mathrm{mF} 15 \mathrm{p} ; 2 \mathrm{mF} 150 \mathrm{~V}$ $500 \mathrm{~V}-0.001$ to $0.054 \mathrm{~m} ; 0.159 ; 0.258 \mathrm{p} ; 0.4725 \mathrm{p}$.

$1,000 \mathrm{~V}-0.001,0.0022,0.0047,0.01,0.02,8 p ; 0.047,0.1,14 \mathrm{p}$. STIYES MICA．Close tolerance $1 \% 2.2-500 \mathrm{pF} 8 \mathrm{p} ; 500-2.200$
 TWIN GANG．＂ 0 － 0 ＂＂ $208 \mathrm{pF}+176 \mathrm{pF}$ ，65p；Slow motion drive $365+365$ with $25+25 \mathrm{pF}$ ， 51 p 500 pF slow motion，standard 45；amsil 8－gang 500 p S $51-10 . g E O R T$ FAYE，Single 25 pF 55 D GEROME TBLESCOPIC AERIAL，SWivel base，28in．20p． TURIEG．Eold dielectric． 100 pH ； $500 \mathrm{pF}, 35 \mathrm{p}$ e8ch． 150 pF $8 \mathrm{p} ; 250 \mathrm{pF}, 18 \mathrm{p} ; 600 \mathrm{pF} ; 750 \mathrm{pF} 10 \mathrm{p} ; 1000 \mathrm{pF} 10 \mathrm{p}$ ． 10 mF
 85mA 48p．SIEICOX BY 21830 p ；BY100 80p；BY127 30 p FEON PANGL IMDICATORS 2507 AC／DC Hed Ot Amber 20 p ． REASISTORS．$\frac{1}{2}$ W．，$\frac{1}{\frac{1}{2}}$ W．， $20 \% 1 \mathrm{p} ; 2$ w． $5 p$ ．
 Dito $5 \%$ Preferrad raites io ohms to 10 meg．， 4 ip． FIRE－WOUHD RESISTORS 5 Watt， 10 watt， 15 Fstt
10 ohmit to $100 \mathrm{~K}, 10 \mathrm{~g}$ each； 2 f watt， 1 ohm to 82 hms 10 p
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Complete：s die，a punch，an Allen acrew and key




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 GENERAL PURPOSE LOW VOLLAGE at 2 amg．8，4，5，6，8，9，10，12，15．18． 24 and 00 ontpats
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 FULL WATE BRTDGE CHARGER REGTIEIRRS： 6 or 12 v outputs， $14 \mathrm{amp} .40 \mathrm{p} ; 2 \mathrm{smp}$ ． $55 \mathrm{p} ; 4 \mathrm{smp} 85 \mathrm{p}$

E．M I． $13 \frac{1}{2} \times 8 \mathrm{in}$ ． LOUDSPEAKERS With flaxed tweeter come and ceramic $\left.\begin{array}{l}\text { magnet．} 10 \text { watts．} \\ \text { Bass res．} 45.60 \mathrm{cps} .\end{array}\right\} 25$ Flux 10，000 gauss． Post 15p State 3 or 8 or 15 ohm Alio with twin tweeters 44 and crousover， 10 watt． 44
State 8 or 8 or 16 ohm．Fost $15 p$
As illostrated） As illustrated）


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Triple speaker system combining on ready cut bsfale． $\frac{1}{2}$ in．chiphoard $15 \mathrm{in} . \times 8$ in．Sepsrate Bass．Middle and Treble loudspaakers and crossover condenser．The heavy dufy 5 in ．Bass Woofer unit has a low resonance
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 TEAK BL－FI BPEAKER CABLIETE．FInted wood front For izin．round Loudspesizer For $18 \times 8 \mathrm{in}$ ．Loudspeaker For $10 \times 6$ bin．round Loudspesirar ．．．．．．．．体．Post 85號
THISELAC CONE TWEETERISOFTHEVERY
LATEST DESIGN AND GIYES A HIGHER LATEST DESIGN AND GIYES A HIGHER
STANDARD OF PERFORMANCE THAN PERFORMANCE THAN
MORE EXENSIVE UNTTS． The moving coll diaphragn gives a good ratiation pattern to the highar fraquanoies
and s smooth sxtension of total response from 1,000 cis to 18,000 cDE，Size $8 \frac{1}{5} \times$ $34 \times$ 2in．depp．Reting 10 watts． 8 ohm or 15 ohm modela． 41.90 post 10 p

TWO－WAY XOVER NETWORK 3000 c／s． With varisble tweeter attenuator givint acenaste high／low irequancy balance．monatioa on panel 5ila．X im． input torminalas Suitable for 8. to 8 ohm imp． 4.90 por 10

GOODMANS HEAVY DITY IBİ．WOOFER 10w．Large caramic megnet． $80-12,000 \mathrm{eps}$ ．Ideal P．A．，f C Horn Tweeters 2－18lic／s， 10 W 8 ohm of 15 ohm $81 \cdot 50$
 SPRCLAL OFFERI 80 ohm，Rin．dis．； 35 ohm ． 8 in ．EAOH $250 \mathrm{hm}, 3 \mathrm{in}$, tia．； $6 \times 4 \mathrm{in} . ; 8 \times 8 \mathrm{in}$.
$15 \mathrm{ohm} 8 \mathrm{in} . \mathrm{dia} ; 7 \times 4 \mathrm{in} . ; 8 \times 5 \mathrm{in}$. 3 ohm， 2 in， 8 in ，5in． $5 \times 3 \mathrm{Bin} .7 \times 4 \mathrm{in}$. LOUDSPEAKERS P．M． 3 OEMS． $6 \times 1 \mathrm{Kin}$, \＄1．10； $8 \times$ Gin． 81.85 ； $8 \times 21 \mathrm{in}, 90 \mathrm{p} ; 8 \mathrm{in} .61 .75: 10 \times 6$ in． 81.90. 5 in ．FOOFBR 8 wette max． $20-10,000 \mathrm{cps} .8 \mathrm{ar} 15 \mathrm{ohm} .21-80$ ． ELAAC 8 in．Do Luxe Geramic 8 ohm or 150 hm zigi 00 ． RICEARD ALLAK TWIN CONE LOUDSPEAKRRS． 8 or 8 or 15 ohm models fin． $95{ }^{\circ}$ wach．Post 15 pm ．
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100 WATI ALL PURPOSE POWER AMPLIFIER



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£7．50
BARGAIM 3 WATTY AMPLIFTER． 4 Transistor $\mathbf{~} 3.50$ Push－Full Ready built，with volume control． 8 y

COAXIAL PLEG 6p．PANEL SOCKETS 6p．LINE 18p． OUTLET BOXES，SURFAOS OR FLUSH E5p． BALANCED THIN FEEEDERS 57 FA． 80 ohms or 800 ohms． JAOK SOCKEH Sta．open－circalt 14\％，closed circuit 23 p Chrome Lead Socket 45p．Phono Plugs 5p．Phond 8ocket 5p．
JACK PLUGS Stu．Chrome 15p；8．5mm Chrome 14p．DIn JACK PLUGS Std．Chrome 15p； 8 5mm Chrome 14p．DLi Sockin 18p；5－pin 85 p ．Dhi PLUGS 8－pin 18p； 5 －pin 85 p ． 3－pin 18p；5－pin 85p．Dif PLUGS 8－pin 18p；5－pin
VALVE HOLDERS，5p；CERAMIC 8p；CANS 5p．


E．M．I．TAPE MOTORS
120 v ．or 240 v. AC． 1,200 r．p．m． 4 pole 185 mA ． 8 pindle $0.187 \times 0.75 \mathrm{in}$ ．
Size $3 \frac{1}{4} \times 8 \frac{1}{2} \times 2 \frac{1}{2}$ in．（illustrated）． $\mathcal{P} 1.25$
BALFOUR GRAM MOTOTORS
120 v or 240 v, A．C． 1,200 r．p．m． 4 pole
 $2 \frac{1}{2} \times 2 \frac{2}{4} \times 1 \frac{1}{8} \mathrm{in}$.
POSt 15 p
CALLERS WELCOME CUSTOMERS FREE CAR PARK． 337 WHITEHORSE ROAD，CROYDON Open 9－6 p．m．（Wednesdays 9－1 p．m．，Saturdays 9－5 p．m．）



##  <br> Range of sollo state A.c. MAANs AMpllfiers <br> Employing only

high grade components and transistors.


## LT55 6 WATT AMPLIFIER

A HIGH FIDELITY UNIT PRO. VIDING EXCELLENT RESULTS AT MODEST OUTPUT LEVELS.

## Recommended 211

Size $9 i \times 24 \times 54 \mathrm{in}$. Approx Size $9 \lambda \times 2 \pi \times 5$ in. Approx.
Controls (5) Volume, Bass Controls (5) Volume, Bass Treble, Mains S
Selector Switch.

Sensitivity 5 mv (max)
Frequency Response $\mathbf{3 0 - 2 0 , 0 0 0} \mathrm{cps}-2 \mathrm{~dB}$ Frequency Response $30-20,000 \mathrm{cps}-2 \mathrm{CB}$
Harmonic Distortion $0.5 \%$ at $1,000 \mathrm{cps}$ Harmonic Distortion $0.50^{\circ}$ at $1,000 \mathrm{cps}$
Output Rating I.H.F.M. ${ }^{\circ}$ Watt Output Rating 1.H. "M. 6 Watt Radio Tuner/Tape Recorder. Suitable for speakers $3-15$ ohms

## LT66 12 WATT STEREO AMPLIFIER

A TWIN CHANNEL VERSION OF THE LTS5 PROVIDING UP TO 6 WATTS I.H.F.M. HIGH FIDELITY OUTPUT ON EACH CHANNEL
Switched Input Facilities
Switched Input Facilities
Socket (1) Tape or crystal PU
Socket (1) Tape or crystal PU
(2) Radio Tuner (3) Ceramic PU
(2) Radio Tuner (3) Ceramic PU


Size $12 \times 3 \frac{1}{2} \times 6$ in. Approx.
Controls (6) Volume, Bass, Treble, Balance, Mains Switch, Input Selector Switch, Stereo/Mono Switch.
Facia Plate Rigid Perspex with black/silver background and matching black edged knobs with silver finish centres.

[^0]LINEAR PRODUCTS LTD, Electron Works, Armley, Leeds


## BAKER I2in. REGENT

An inexpensive unit for the beginner in high fidelity and for general purposes. May Amplifier or Television with an
Maximum Power 15 watts
Bass Resonance $45 \mathrm{c.P}$.s. Flux Density 12, 000 gauss Voice Coil impedance

3 or 8 or 15 ohm models Useful response Nett weight 45-13,000 c.p.s. POST Nott weight $516 s$. FREE GUITAR MODEL "GROUP 25" $\mathbf{~} \mathbf{2 5}$
Latest cotalogue 5p with enclosure plans.

## Baker Reproducers Ltd




Post \& Packing $12 \frac{1}{4}$ p per order. Europe 25p. Commonwealth (Air) 65p (MIN.)

|  | TTL. LOGIC I.C. NEW PRICES |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\underset{24}{1-}$ | $\frac{25}{98}$ | $\begin{gathered} 100- \\ 498 \end{gathered}$ |  |  | $\begin{aligned} & \text { 25- } \\ & \hline 99 \end{aligned}$ | $\begin{gathered} 100- \\ 499 \\ 850 \end{gathered}$ |
| SN7400 | 25 p | ${ }^{20} \mathrm{p}$ | 18p | SN7470 |  |  |  |
| SN7401 | 250 | 20 p | 189 | SN742 | $\cdots \quad 40 \mathrm{P}$ | ${ }_{40 \mathrm{p}}$ | ${ }_{850}$ |
| SN7402 | -259 | 20p | 18p | SN7473 | $\begin{array}{ll}. . \\ . & 450\end{array}$ | - $\begin{aligned} & \text { 40p } \\ & 40 \mathrm{p}\end{aligned}$ | 859 |
| SN7404 | 25p | 20 p | 18 D | SN7475. | \$1.00 | 90p | 80 D |
| SN7405 | 25D | 200 | 180 | SN7476 | 45 D | 400 | 850 |
| SN7406 | 80 p | $75 p$ | 70 D | SN7482. | 81.30 | ${ }^{21} 120$ | 81.10 |
| SN7407 | 25 p | 20p | 18p | SN7483 | 21.00 | -90p | 80 p 400 |
| SN7408 | 25p | ${ }^{20 p}$ | 18 D | SN7486 | $\cdots \quad 81.00$ | - ${ }^{45 p}$ | ${ }_{809}^{409}$ |
| 8N7409 SN7410 | ${ }_{250}$ | 20p | 18p | ${ }_{\text {SN7 }}$ | $\because \quad 81.50$ | 81.40 | 21.80 |
| SN7411 | 259 | 20 p | 18 y | 8N7493 | 81.00 | -90p | ${ }^{80 \mathrm{p}}$ |
| SN7413 | 50p | 45p | 40 p | SN7494 | E1.50 | 81.40 | 21.30 |
| SN74118. | 21 | 90 p | 80 p | SN7495 | 81.00 | - 900 | 80 p |
| 8N7420 | 25 y | ${ }^{20 \mathrm{p}}$ | ${ }_{18 \mathrm{p}}^{18}$ | SN7496 | E1.00 | - 90 p |  |
| gN7430 | 250 | ${ }_{20 p}^{20 p}$ | 18p | SN74107 | 7. ${ }^{450 \mathrm{p}}$ | p ${ }^{40 \mathrm{p}}$ | ${ }_{80 \mathrm{p}}^{30}$ |
| gN7440 | ( $\begin{array}{r}\text { 250 } \\ \hline 81.00\end{array}$ | ${ }_{90 \mathrm{p}}^{20 \mathrm{p}}$ | 180 $80 p$ | SN74121. | .. 81.10 | E1.00 | ${ }_{80 \mathrm{p}}^{80}$ |
| GN742 | . 21.00 | ${ }_{90 \mathrm{p}}$ | 80 p | SN74153 | 3 21.90 | - 81.70 | 81.50 |
| sN7445 | 22.50 | 58.30 | 82.10 | SN74154 | 4 E280 | ( 81.45 | 21.80 |
| SN7446 | E1.25 | 21.10 | 81.00 | SN7460/ |  |  |  |
| SN7447 | 81.10 61.00 | 81.00 800 | 90 p 80 p | SN74161 | 1121.80 <br> 2.60 | - 81.50 | 28.40 |
| SN7450 | 250 | 20p | 18 p | SN74164 | - 22.20 | ${ }^{81}$ | 81.80 |
| SN7451 | 25 p | 20 p | 188 | 9N74165 | - 52.25 | 551.95 <br> 8.95 | E1.80 |
| 8N7453 | ${ }^{258}$ | 20 p | 18p | 8N74192 | - $\begin{aligned} & \text { 22.25 } \\ & \text { 82.25 }\end{aligned}$ | ( $\begin{aligned} & \text { 21.95 } \\ & \text { 81.95 }\end{aligned}$ | 81.80 |
| SN7454 | 25p | ${ }_{20 \mathrm{p}}^{20 \mathrm{p}}$ | $18 p$ $18 p$ | SN74193 |  |  |  |
| SILICON RECTIFIERS |  |  |  |  |  |  |  |
| PIV | 50 | 100 | 200 | 00600 | 800 | 1000 | 200 |
| 1 A | ${ }^{10 p}$ | 12¢p |  | 17pp | 198 |  |  |
| 3 A | 15p |  |  | 3 | ${ }_{85 \mathrm{p}}$ |  |  |
| ${ }_{10 \mathrm{~A}}^{64}$ | - | 527p | ${ }^{2727 p}$ | 5 p 7\% ${ }^{\text {a }}$ | ${ }^{3651 p}$ | 971p | 81.25 |
| 17A |  | 578 | ${ }^{62} \mathbf{4} \mathrm{p}$ | $7 \mathrm{pp}{ }^{90 \mathrm{p}}$ | ${ }^{9715}$ | 81.20 | 81.57 $\ddagger$ |
| 35A |  |  |  | $1.00 \quad 81.25$ |  |  |  |
| 1 amp and 3 amp are plastic encapsulat |  |  |  |  |  |  |  |
| DIODES \& RECTIFIERS |  |  |  |  |  |  |  |
| IN34A | 10 p | AA119 | 10 p | BAX16 | 121 p | BYZ13 | $\underset{22 p p}{25 p}$ |
| IN914 | 072p | ${ }_{\text {AA129 }}$ | ${ }_{100}^{101}$ | BAY18 | 17\% ${ }^{\text {\% }}$ | FST3/4 <br> OA5 | $\begin{aligned} & 221 p \\ & 172 p \end{aligned}$ |
| IN916 | 07sp | AAZ13 | ${ }_{12+\mathrm{p}}^{10 \mathrm{p}}$ | BAY31 | ${ }_{85 \mathrm{p}}$ | $\mathrm{OAS}_{\text {Ofio }}$ | 22\% |
| ${ }_{\text {IN440 }}$ | ${ }^{20 p}$ | AAZ17 | 12 \%p | BY100 | 17p | OA9 | 10 p |
| 18113 | 155 | BA100 | 15p | BY103 | $28.4 p$ | OA47 | ${ }^{077}{ }^{07 p}$ |
| IS120 | 15p | BA102 | 2278 | ${ }_{\text {BY1 }}$ | ${ }^{475 p}$ | OA70 | ${ }^{0700}$ |
| 18121 | 17 p | BA110 |  | BYY ${ }^{\text {B }} 126$ | ${ }_{15 p}$ | OA79 | 08p |
| IS130 | ${ }_{12 ¢}$ | BA141 | 82tp | BY127 | 171p | OA81 | 07 D |
| Is132 | ${ }^{15 p}$ | BA142 | 82 bD | BY164 | 57\% ${ }^{\text {d }}$ | OA85 | 078 |
| 15920 | 077p | BA144 | 12 p | BYX10 | ${ }_{350}^{298}$ | OA90 | 07ip |
| 18922 18923 | 07tp | ${ }^{\text {BA145 }}$ | ${ }_{120 \mathrm{p}}$ | BYZZ1 | ${ }^{325 p}$ | 0 A 95 | 0710 |
| 18940 | 071p | BAX13 | 121p | BYZ12 | 30p | $\begin{aligned} & \text { OA200 } \\ & 0 A 202 \end{aligned}$ | $\begin{aligned} & 10 \mathrm{p} \\ & 10 \mathrm{p} \end{aligned}$ |
| TRIACS |  |  |  | BRIDGE RECTIFIERS |  |  |  |
| SC35D | 21.12t | SC51D | ¢1.95 | A. PIV |  | A. PIV |  |
| Sc36D | 21.00 | 40430 | ${ }^{97515}$ | 1100 | 47tp | $\begin{array}{r}4 \\ 4 \\ 4 \\ 4 \\ \hline\end{array}$ | ${ }^{60 p}$ |
| SC40D | 21.50 81.20 | 40486 40.528 | ${ }_{70 \text { 92p }}^{950}$ | 1.4140 | 52ıp | 4 4 400 | ${ }_{950}$ |
| ${ }_{\text {SC41D }}$ | 81.20 | 40528 40430 | 81.20 | $\begin{array}{ll}2 & 50 \\ 2 & \end{array}$ | 50p | $5{ }^{5} 500$ | 62tp |
| SC46D | 81.422 | 40432 | ${ }^{21} .87{ }^{17}$ | 2200 | 70p | 6 <br> 4 <br> 4 | 871p |
| SC50D | 82.05 | 40512 | 51.45 | 2400 | 80p | 4400 | 81-22: |

THYRISTORS
ORS 300

 Also 12 amp . 100 PIV 75
2N3525 at 21.12łD
VEROBOARD

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## CAPACITORS

$A$ large and comprehensive range available: Electrolytic,
Polyester,
Ceramic,
PolyPolyester, Ceramic, Poly-
atyrene, Silver Mica, Tantalum, Trimmers, Tuners Trimmers, Tuners. Examples:
$2,000 \mathrm{mF} 25 \mathrm{~V}, 42 \mathrm{p}$ Most $\begin{array}{ll}2,500 \mathrm{mF} \\ 3,000 \mathrm{mF} & 25 \mathrm{~V}, 67 \mathrm{~g}, 52 \mathrm{p} \\ \text { Mullard } \\ \text { Electrolytics }\end{array}$ $5,000 \mathrm{mF} 50 \mathrm{~V}, 97 \mathrm{p}$ it stock
WIRE-WOUND EESISTORS 2.5 watt $5 \%$ (up to 270 ohms only). $7 \frac{1}{2} p$
5 watts $5 \%$ (up to $8.2 \mathrm{k} \Omega$ oniy), 10 p 10 watt $5 \%$ (up to $25 \mathrm{k} \Omega$ only),
$12 t \mathrm{p}$
POTENTIOMETERS
Carbon:
Log. and Lin., lesg switch, 16p. Log. and Lin., with switch,
Wire-wound Pots (3W), 40 p . Twin Ganged Stereo Pots, Log. and Jin., 40p.
PRESETS (CARBON)
0.1 Watt 6p VERTICAL
$\begin{array}{llc}0.2 & \text { Watt } & \text { 6p } \\ 0.3 & \text { Watt } & \text { OR } \\ \text { 75P } & \text { HORIZONTAL }\end{array}$
THERMISTORS
K53 (STC) $61 \cdot 2 \%$ VA370587ty K151 (1k) 124 p
Mullard Thermistors also in
stock. Please enquire.


 AKG K50 Dynamic Stereo headphones Complete with spare ear muffs.
 Avallable only from us at this price. Due to entire purchase of manufacturer's remaining stock this antastic offer is open only while stocks last. * High-fidelity reproduction due to broad frequency response $(20-20,000 \mathrm{~Hz}$ * Substantially increased stereo effect * Headphones fit the head gently and do not shift *Earpieces fit ears snugly (Cardanic suspension) * Tone quality superior to conventional loudspeakers. * Only expensive studio loudspeakers can match the reproduction quality of the K50. A Music can be reproduced at concert hall volume (1), preserving the lower bass notes and brilliant treble tones without causing any strain to the listener


GARRARD SP25 mk III £12.50 $\begin{gathered}\text { Plust } \\ \text { carriage }\end{gathered}$ Normal price $\mathbf{£ 1 5 . 5 7}$ Wired with mains cable and 5tt. twin screpned stereo cable, 5 pin din plug. 53p extra. AP75 Complete with base and cover $£ 25$ plus 75p carriage,
PLINTH AND COVER SUHT. ABLE FOR GARRARD RANGE
+5.25 plus 50p p. \& p.
Replacement Stereo
DIAMOND STYLI 8TA $9 T A$ 9TAHC
GP91 ST4 ST9 EVRS GC8
 others an request $+13 p$ p. 2 p. Countdown SPEAKER Tedh Cabinet \&12 insurance

A speaker of outstanding speciflcations and technical merit, Solld teak cablnet size: $14^{\prime \prime} \times 10^{\circ} \times 6$ Origlnally designed for use with our Countdown stereo budget bystem but now available separately.


EMI 20w matched loudspeaker set 3-50 Frequency range:
Normal price $£ 13$ EMI 10w matched
loudspeaker set 450
Our price $£ 3.75$ plus 25p. p. $6 \rho$. $131^{\prime \prime} \times 8 \frac{1}{2}^{\prime \prime}$ elliptical loudspeaker and independent high frequency units with associated crossover network. Fre quency range 55 to
13000 Hz . The cone of the basy unit has a surround designed for high travel giving freedom from distortion when operated at low frequencies. Also 150 KIT loW 22.50 p/L



## J. J. FRANCIS

(WOOD GREEN) LTD 123 ALEXANDRA ROAD, HORNSEY, LONDON, N. 8.

## Train for tomorrow's world in Radio and Television at The Pembridge College of Electronics Your first day on Television: 7th September, 1971

## HEARING AID AMPLIFIERS

(Ex behind ear deaf aids) 2 transistors on tiny P.C. board with volume control-whole thing only about half as big as Oxo cube. \&1-75 or with
sub-miniature microphone and I.S. attached 88.50.

## MAINS OPERATED SOLENOIDS <br> SOLENOIDS

Model ry2-small hut power-


 plus 20 p post and insurance.
BEST QUALITY BRITISH MADE ELECTRICAL PLUGS AT APPROX. HALF PRICE
15 amp 3 pin 10 p each or ten for $90 \mathrm{p}, 5 \mathrm{amp} 3$ pin 8 p each or ten for $70 \mathrm{p}, 5 \mathrm{amp} 2 \mathrm{pin} 5 \mathrm{p}$ each or ten for 45 p.

## DRILL

 NEW IKW MODEL slectronically changes
speed from approximately 10 revs. to maximum. Full power at
all speeds by finger-tin all speeds by finger-tip
control. Kit includes all parts, case, everything and full instructions, $£ 1 \cdot 50$ plus
13 p post and insurance. able, $82 \cdot 25$ plus 13 p post availMAINS MOTOR

used in record decks and tape recordersdeal also for extractor fan, blower, heaters, etc. New and perfect. Snip at 50 p . Postage 15 p for first one then
5 p for each one ordered. each
NEED A SPECIAL SWITCH? Double Leat Contact. Very slight pressure closes er cach, bop doz. Plastic push5p each, 45
MINIATURE
WAFER SW WAFER SWITCHES


2 pole, 2 way- 4 pole, 2 way-
3 pole, 3 way- 4 pole, 3 way- 2
pole, 4 way- 3 pole, 4 way- 2 pole 6 way- 3 pole, 12 way. All at 18 p cach, $81-80$ dozen, your assortment

## WATERPROOF HEATING 26 yards length 70 W . Self-regulating temperature control. 50 p post free.

MICRO SWITCH
5 amp. changeover contacts, 9 p each, 81 doz. 15 amp . on/of
MAINS OPERATED CONTACTOR $220 / 240 \mathrm{v}$. 50 cycle solenoid Wilent in operation. Closes 4
silen circuits each rated at 10 amps. Extrenely well made by a German Flectrical Company.
Overall size $2 \frac{1}{2} \times 2 \times 2 i n$ Overall size $2 \frac{1}{2} \times 2$
m1 each.
PAPST MOTORS PAPST MOTORS for 110-120 volt working,
but two of these work ideally together off our standard 240 volt mains. A really beautiful motor, extremely quiet running and reversible $\mathrm{E1.50}$
each. Postage one 23 p ,
 nos


EXTRACTOR FAN Cleans the air at the rate of 10,000 cubic ft. per hour.
Suitable for kitchens, bathSuitable for kitchene,
rooms, factories, changing rooms, ete., it-s so quiet it can hardly be heard. Compact, 5! casing with $5 \frac{1}{2}^{\prime \prime}$ fan blades. Kit comprises motor, fan blades, sheet steel casing, pull switch, mains connector, and
fixing brackets, 22 plus 36 p fixing brackets, 22 plus 36 p

## MAINS TRANSISTOR POWER

 PACKDesigned to operate transistor sets and amplifiers. Adjustable output 6 v ., 9 v ., 12 volts for up to 500 mA (class B working). Takes the place of any of the following batteries: PP1, PP3, PP4, PP6, transformer rectifier, smoothing and load resistor, condensers and instructions. Real snip at only 88 condensers and instruct

## 24V BUZ BUERR.

Made by G.E.C. in brown heary bakelite case. these work off AC mains through step down transformer. Price 40p each.
Suitable for connecting multicore flexer to equip ment. Socket size approx. $\frac{7}{2}^{\prime \prime}$ diameter. Plug size $9 / 10^{\circ}$ diameter with flex entry. 25 p pair.

5TANGENTHAL HEATERS
Once again we are able to make a speeial bargain offer of these very popular heating units. Tangential heaters aithough brought out a few years ago are still the latest and best type as called an improvement on them. The Tangential unit is still the only one used in good quality heaters made by Hoover, G.E.C. and all the famous names. Tne unit comprises quiet running AC induction rntor with special bear ings, the tangential impeller and a 2 section heater element which allows Witehing half and in heal in the case of whe These heaters are also fitted with a matety curont to cor the heaters should the impeller stop or the air Fith a saiety cutout to cut the heaters should the impeller stop or the air flow be impeded. They are free standing and need only the simplest of cases, even a wooden cabinet is suitable or the phinth of the kita
cabinet. Lots of customers missed our special Summer offer of these heaters cabinet. Lots of customers missed our special summer offer of these heaters 83.50. Control switch heaters only $25 p$ or two-heat, cold-blow and off $\mathbf{3 5 p}$. Postage and insurance 33p on heaters

## STANDARD WAFER SWITCHES

Standard size $1 \frac{1}{4}$ wafer - silver-plated 5 -amp contact, standard $z^{\prime \prime}$ spindle $2^{\prime \prime}$ long-with locking washer and nut.

|  | 2 | 3 | 4 | 5 | 6 | 8 | 9 | 10 | 12 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| of Poles | way | way | way | way | way | way | way | way | way |
| 1 pole | 40p | 40p | 40p | 40p | 40p | 40p | 40p | 40p | 40p |
| 2 poles | 40p | 40 p | 40p | 40p | 40 p | 40p | 40p | 70 p | 70p |
| 3 poles | 40 p | 40 D | 40p | 40p | 70 p | $70 p$ | 70 p | 95p | 950 |
| 4 poles | 40 p | 401 | 40p | 70 p | 70p | 709 | 70 D | \$1.20 | ¢1. 20 |
| 5 poles | 40 p | 40p | 70p | 70 p | 85 p | 95p | 95 p | £1.45 | £1.45 |
| 6 poles | 40p | 70 p | 70 p | 70 p | 95p | 95p | 951 | E1.70 | ¢1.70 |
| 7 poles | 70 p | 70 p | 70p | 85 p | 21-20 | £1.20 | \$1-20 | $\pm 1.85$ | £1.95 |
| 8 poles | 70 p | 70 p | 70 p | 85p | £1.20 | 11.20 | £1.20 | £2.20 | 28-20 |
| 9 poles | 70 p | 70 p | 95 p | 95p | 21-45 | \&1-45 | £1-45 | 82.45 | ¢2. 45 |
| 10 poles | 70 p | 70 p | 95 p | \$1.20 | \$1.45 | £1.45 | 21.45 | 22.70 | 22.70 |
| 11 poles | 70 p | 95p | 95p | 41.20 | £1.70 | £1.70 | 21.70 | ¢2.95 | 28.95 |
| 12 poles | 701 | 95p | 95p | \&1-20 | 81.70 | E1.70 | 81.70 | \$8.20 | 23-20 |

## AMPLIFIER MAINS TRANSFORMER

$50 \mathrm{r} 1 \frac{1}{2} \mathrm{amp}$. Upright mounting with fixing brackets and metal shrouds to contail magnetic field, $50 \mathrm{e} / \mathrm{s}$ primary, tapped $110 \mathrm{v}, 117 \mathrm{v}, 210 \mathrm{v}, 230 \mathrm{v}$ and 250 v . 2 secondaries, one $50 \mathrm{v} 1 \frac{1}{2}$ amp. 30 p .


## THIS MONTH'S SNIP

## BATTERY CONDITION TESTER

Made by Mallory but suitable for all batteries made by Ever Ready and others, most of which are zinc carbon and alkaline batteries may be tested. The tester puts a dummy load on the battery and ine meter scale indicate the condition depending upon which section the pointer
 and prods. Price \&l 75 plus 20 p postage.

## COMPUTER TAPE

2,400 ft. of the best magnetic tape money can buy. Almost umbreakable and on a metal computer spool. Users have clairced successful results Fith video as wel! as sound
 Spare spools 50 p each. Cassette to hold spool 50 p each. Na
extra postage if ordered with tape, otherwise 30 p extra
CAPACITOR DISCHARGE IGNITION SYSTEM
Well proved that it helps starting and increases petrol economr. Also increases acceleration but saves contact wear, for details sec Praction Wives optional capacitor or standard Lgnition at the flick of a sutch. Price £4.95 MICROSONIC KEYCHAIN RADIO 7 transistor Keychain Radio in very pretty
case, size $2 \frac{3}{2} \times 2 \frac{1}{2} \times 1 \frac{1}{4}$ in.-complete with soft case, size $2 \frac{3}{4} \times 2 \frac{1}{2} \times 1$ in. $-c o m p l e t e ~ w i t h ~$
leather zipped bag. 7 transistor, ferrite rod. Loudspeaker.
n transit from the East these sets suffered corrosion as the batteries were left in them but when this corrosion is cleared away they except that they are new. Price only $21 \cdot 25$ less batteries plus 13p. post 6 for $£ 7$ post free

## MAINS RELAY BARGAIN

Special this month are some single, double and treble pole changeover relays.
Contacts rated at 15 amps. Operating coil wound for 240 V . A.C. Good 3 ritish Make. Unused. Size approx. $1 \frac{1}{2}^{\prime \prime} \times 1^{\prime \prime}$.
Open construction
Single pole
$\begin{array}{ll}25 p \text { each } & 10 \text { for } \mathbf{~ £ 2 . 2 5 ~} \\ 32 \mathrm{p} \text { each } & 16 \text { for } \mathbf{~} 2.90\end{array}$
$\begin{array}{lll}\text { Double pole } & 32 \mathrm{p} \text { each } & 10 \text { fot } £ 2.90 \\ \text { Treble pole } & 40 \mathrm{p} \text { each } & 10 \text { for } £ 3.60\end{array}$

## 4 AMP VARIAC CONTROLLERS

With this you can vary the voltage applied to your circuit from zero to full mains without generating undue heat. One obvious application therefore is to dim lightiag. Ex equipment but little used-as good as new offered at approx. halif price. $\mathbf{2 5}$ plus
75 p . post and ins

## OVEN THERMOMETER WITH ALARM

Basically this is a thermometer which is calibrated between 500 and 900 deg. C using a sensor on a flexible lead. The second feature, however, is an alarm which can be set anywhere within the temperature range. Presumably the buzzer corld be replaced by a relay or contactor to work another device. Limited quantity only of these units, price $\$ 3 \cdot 50$, includes thermometer -scale-sensor and buzzer.

ELECTRIC CLOCK
WITH 25 AMP SWITCH Made by Smith's, these units are as fitted to many top quality cookers to control the ovea. The quency controlled so it is ex quency controlled so it is ex dials enable switch on and of lials enable switch on and olf wersist for switching on tape recorders. Offered at only a fraction of the regular price-new and unused only $£ 2$, less than the value of the clock alonepost and insurance 14p.

## P.W. <br> TREASURE TRACER <br> As described in this issue. Send today for price list of parts.

TELESCOPIC
AERIAL Tor portable, car radio
transmitter. Chrome pla ted-six sections, extends from 7 t to 47 in . Tole in bottom for 6BA
w, 38 p . KNUCKLED MODEL FOR F.M. 50 p .

QUICK CUPPA
Mini Immersion Eeater 350 w . $200 / 240 \mathrm{v}$. Boils full cup in about. two minutes. Use any socket or for tea, baby's food, etc. $£ 1-25$, post and insurance $14 \mathrm{p}, 12 \mathrm{v}$. car model also available same price


## THYRISTOR LIGHT

## DIMMERS

Will dim incandescent lighting up to 600 watts from full brilliance to out. Assemble


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[^1]

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LEAK Stereofetic Chassis
LEAK Stereofetic in teak case
PHILIPS RH 690
PIONEER TX 500 ÄM/FM̈
PIONEER TX900 AM/FN
ROGERS Ravensbourne chassis ROGRS Ravensbrook
ROGERS Ravensbrook (cased)
TELETON GT 101
53.7
$\begin{array}{ll}53.76 & \mathbf{4 2} \cdot 0 \\ 41.89 & 33.00 \\ 9.50 & 8.00\end{array}$
00
ORBIT Magnetic N̈M $22 . . .$. ORTOFON SLI5E ORTOFON $2 \times 1$
SHURE M3DM. SHURE M31E SHURE M32E
SHURE M32-3 SHURE M44-5 SHURE M44-7 SHURE M44E
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SHURE M75E
SHURE V15-11
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| GOODMANS Twin Axiom | 10.23 | 8.25 |
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| D <br>  | 5.00 | 4.00 |
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| ARENA MR15 | 145 | 15 |
| ALBA |  |  |
| ALBA UA662 | 62.97 |  |
| DECCA Sound 603 | 72.50 | \$88-95 |
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[^2]
## Exhibitions R.I.P.?

THERE are probably more exhibitions today than ever before, but those embracing areas of interest to readers of P.W. appear to have suffered the ravages of economics, indecision and wrong priorities.

The pre-war "Radiolympias" were intended for trade and public alike and even the last one in 1939 had lots of interest for the home constructor. Most hobbyists who could get to Olympia, went there. Post-war radio shows carried on the tradition, although with less and less for the amateur enthusiast-the trend was changing.

In the last decade, the unity of the radio industry began to deteriorate as first one, then another, major company broke away from the main exhibition (then at Earls Court) to hold their own private shows. In 1964 there were over ten "splinter" shows in London at exhibition-time and this mass exodus killed the public radio and TV show in this country. The costs of mounting stands in the exhibition halls available, plus the attitude of brushing off the public (the ultimate customers) were contributory factors.

Now, after some years of August trade-only exhibitions scattered all over London, manufacturers this year abandoned the traditional "showtime" period and held their shows during May. An attempt to get the industry together again under one roof failed. Next year, shows will again be held in the Spring. After that one needs a crystal ball. But still there seems to be no hope of anything for the public to see!

On another front, the various audio exhibitions overlap to some extent and are the subject of both praise and criticism. The Audio Fair gave up hotel rooms for the open spaces of Olympia and brought in photographic and then musical instrument interests. There has been talk of radio and TV exhibits. However, even if audio exhibitions do not please everyone, at least the public can get in!

Discounting the more specialised and professional orientated exhibitions, this leaves one more erstwhile important calendar date for the radio amateur-the RSGB Exhibition. We have seen this develop (or disintegrate?) from its unpretentious but delightfully social atmosphere of the Hotel Royal days, through various stages at Seymour Hall and Royal Horticultural Hall. It tried to change its angle, gave itself a pompous (and, we feel, misleading) name, lost its character and died. For this year there is to be no RSGB Exhibition.
A sad story for exhibition-minded radio enthusiasts. The problems will only be solved when we have more modern (and economic) exhibition halls for the larger shows and organisers, societies and manufacturers who are oldfashioned enough to think first of the public, then give them what they want.
W. N. STEVENS-Editor.

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SEPTEMBER ISSUE WILL BE PUBLISHED ON AUGUST 6th

[^3]
## News... NEWS... NEWS...

## 12V Iron from Antex

 normal operation.

This iron is absolutely ideal for use in conditions where a mains supply is not available. It is supplied in a durable plastic wallet which will 'house' the iron when not in use. Recommended U.K. price is $£ 1 \cdot 95$. Antex Limited, Mayflower House, Plymouth, Devon.

## Fudging irons

West Hyde Developments are asking: How often do you fudge a hole? They maintain that their taper reamers are the finest fudging irons available. These West Hyde reamers, due to their many flutes and cutting edges, will open a hole from $1_{g}$ in to $\frac{7}{16}$ in in a few seconds and the hole will be rounder than when drilled. On the many occasions when equipment cannot be put up on a drilling machine due to size and damaging the finish a West Hyde reamer in an ordinary hand brace will solve the problems without vibration and with little effort.

Two sizes are available, ${ }_{8}$ in. to ${ }^{1}{ }_{2}$ in ( 3 mm to 12 mm ) and $3_{8}$ in to lin ( 9 mm to 25 mm ). Prices are: small size $£ 2 \cdot 75+10$ p postage and packing. Large size $£ 3 \cdot 40+$ 15 p postage and packing.


## The I.B.C. 1972

One of the leading events in the world broadcasting calendar, the International Broadcasting Convention, will next be held in London from 4-8 September 1972. This will be the fourth IBC.

The Convention, which will be held at Grosvenor House, Park Lane, will comprise technical sessions and a comprehensive exhibition of the latest television and sound broadcasting equipment, both highlighting the future technological options available to broadcasting administrations.

IBC is sponsored by the Electronic Engineering Association, the Institution of Electrical Engineers, the Institute of Electrical and Electronics Engineers, the Institution of Electronic and Radio Engineers, the Royal Television Society and the Society of Motion Picture and Television Engineers.

All enquiries to The Secretariat, International Broadcasting Convention, IEE, Savoy Place, London WC2R 0BL, England.

## Cul price stereo

Audio Supplies Limited have a supply of "The Great Musicians" stereo LPs and for $£ 1 \cdot 15$ p (p.p. free) they are offering three records. Each 10 in . stereo LP is incorporated in an illustrated 12 page record book which gives an insight into the life of the composer and explains how his life influenced his work.

These LPs originally retailed for 13 s . 11d. each and there are 55 titles from which to choose by 20 of the world's greatest composers. Audio Supplies Limited, (Dept. P.W.) 50 Stamford Hill, London, N.16. Telep ${ }^{\text {nonene }} 01-806$ 3611.

## Mobile rally diary

July 11 Worcester, Upton on Severn.
Aug 8 Woburn Abbey.
Aug 15 Derby.
Aug 22 Swindon, Wroughton Aerodrome.
Aug 29 Stratford-on-Avon.

# NEWS... NEWS... <br> NEWS... 

## Zeiss Ikon P500 projector



Basically, the P 500 consists of the Perkeo S 150 projector mounted on top of a Philips cassette tape recorder and loudspeaker to form a single unit. The projector can be used by itself in the normal manner and so can the tape recorder. Individual slides can be inserted in the gate without using the magazine-the importance of this feature will be appreciated by anyone who has done much slide-sorting. The forward and reverse movements of the magazine have also been retained and can be worked either manually (in which case you use a remote control cable instead of the push-buttons that are operated on the standard S 150) or else by means of the tape. To make the magazine move on to the next slide you put a short impulse on the tape; to make it move backwards to the slide shown previously you instead use a long impulse.

The Philips tape recorder is connected to the projector electrically. An extra record/playback head has been fitted to add the highfrequency impulse to the tape which changes the slides; the recorder itself is housed in a drawer which pulls out of the back of the unit. Space is provided to store spare cassettes, the microphone and various cables and accessories.

There are also, in addition to the mains inlet, four sockets. One allows you to connect an external speaker, useful when operating in a large hall. Another a combined input/outlet socket, lets you record from a source such as a microphone, radio, tape recorder, record player or mixer or alternatively to boost the output via an amplifier. A third allows the remote control for the projector to be fitted and the last one is for the cable that lets you put the slide change impulses on the tape.

The recommended price of the P 500 will vary according to the lens fitted, but with the Vario-Talon $\mathrm{f} 3 \cdot 570-120 \mathrm{~mm}$ it is $£ 222.18 .6 \mathrm{~d}$ $£ 222 \cdot 92^{1}{ }_{2}$ ), including $£ 66.18 .6 \mathrm{~d}\left(£ 66 \cdot 92^{1}{ }_{2}\right)$ P.T. The price includes the microphone and the impulse device.

## IC's on the wall

Mr. J. Evans of the Mullard Press Dept., informs us that a large coloured chart produced by the Mullard Educational Service outlines the manufacturing process of integrated circuits. It measures nearly $30 \times 22 \mathrm{in}$. and has diagrams showing cut-away views of a silicon chip at different manufacturing stages as resistors, capacitors, diodes and transistors are formed
by various diffusion techniques. Captions alongside the diagrams detail what is done to the chip.

The chart is suitable for use in schools, colleges, universities and other training establishments where electronics is taught. Price 25 p post free (send cash with order), it can be obtained from the Mullard Educational Service, Mullard Limited, Mullard House, Torrington Place, London WC1E $7 H D$.

## Radio Brighton

From the start of programmes on Saturday, May 29, BBC Radio Brighton transmitted on 95.8 MHz instead of $88 \cdot 1 \mathrm{MHz}$ and the effective radiated power increased from 75 to 500 W .

## Lexor's board

Lexor Dis-Boards Limited now announce their brand new 'MiniBoard'. Having pioneered the multi-socket power board business more than ten years ago, Lexor are aware that $75 \%$ of users' needs can be met by only one model. This has now been specially designed and set up for quantity production and sells for only $£ 3.95$.
Four high-grade 13A ivory sockets are mounted in a slim blue leather-finish case and fed via 5 ft . of cable from a readyfitted 13 A ivory fused plug. There is the characteristic red safety warning lamp, and the units can be used portable and free-standing or easily fixed permanently to walls, benches, etc. Simple cable extensions of 15 ft . or 25 ft . are available for the situations where the flex will not reach.

Illustrated brochures carrying full details, prices and sales terms are available from Lexor DisBoards Limited 25/31Allesley Old Road, Coventry.


#  for80metre SSBCW R.F.GRAHAM 

A$S$ anyone who has become interested in the reception of single-sideband and c.w. (Morse) signals knows, the usual type of receiver for a.m. (amplitude modulation) reception is not able to resolve these transmission. When a beat frequency oscillator is present in the receiver, s.s.b. and c.w. can be received and modern communications receivers have a b.f.o. Older communications receivers having a b.f.o. allow reception of s.s.b. but with some difficulty unless the operator is experienced.

## REQUIREMENTS

To clarify requirements for s.s.b./c.w. reception, Fig. 1 A shows the stages of a typical superhet. (1) is the r.f. amplifier, which amplifies signals at the received frequency. (2) is the mixer, with oscillator (3), which may be separate, or combined in a single frequency-changer. Output from this section is at a fixed intermediate frequency, and passes through the i.f. amplifier (4) to the a.m. and product detector circuits (5). With domestic type receivers, this stage is an a.m. detector only where a.m. signals are demodulated, and passed through the audio amplifier (6) to the speaker (7).

Where the receiver is intended also for s.s.b./c.w. reception, (5) incorporates a product detector and a beat frequency oscillator ( 8 ) is also provided.

When s.s.b. signals are received, the b.f.o. supplies an unmodulated r.f. input, which replaces the "carrier", suppressed in s.s.b. transmission. This local carrier and the s.s.b. from the i.f. amplifier (4) are combined in such a way as to give an audio output, which passes to the audio amplifier and speaker.

For c.w. reception, the output of the b.f.o. (8) heterodynes with the c.w. coming through the i.f. amplifier (4) to give an audio tone, is amplified and fed to the speaker (7).


Fig. 1B is a direct conversion receiver and its much greater simplicity is obvious. (1) is the r.f. amplifier, tuned to the required signal in the usual way and fed to a product detector (2) which also receives input from the variable frequency oscillator (3) which covers the band upon which reception is wanted the circuit being so designed that an audio output is obtained directly from the product detector (2), which is amplified by stage (4) and routed to the speaker.

When receiving s.s.b. only those s.s.b. frequencies which combine with the v.f.o. frequency to give an audio output are heard. Thus the selectivity of the receiver does not depend upon the r.f. amplifier or product detector signal frequency circuits but upon the selectivity of the audio stages.

Thus apparent selectivity is achieved because unwanted signals are combined with the v.f.o. in stage (2) to give outputs which are not in the audio range of stage (4). To receive c.w. the v.f.o. is tuned to one side of the c.w. carrier to give an audio output from the product detector. This particular circuit is not really suitable for the reception of a.m. signals which require the local carrier to be phase-locked to the a.m. carrier.

The receiver described here will be found to give a very lively performance. As it is assumed that anyone just becoming interested in the reception of amateur s.s.b. and c.w. may not have much in the way of calibration or test equipment, the v.f.o. is designed to use three 1 per cent tolerance capacitors and a coil with adjustable core, so that it is only necessary to set the core to give 80 m band coverage. The radio frequency circuits are peaked for best reception.


Fig. 1A shows the arrangement of the standard superhet while Fig. 1 B illustrates the reduced number of stages required for a direct conversion receiver.


Fig. 2. The complete circuit of the Direct Conversion Receiver. The main tuning dial (shown in the heading photograph) drives the v.f.o. tuning capacitor VC3.

Fig. 3. Layout of the major components on top of the chassis with important dimensions shown.

## CIRCUIT

Fig. 2 is the complete circuit. V1 (6BA6) is the r.f. amplifier, with gain control VR1. L1 and L2 are tuned by VC1/2, which is a small ganged capacitor for the r.f. tuning control.

V2 (12AT7) is the product detector, the wanted signal is present at one control grid and injection from the v.f.o. at the other grid. Audio output from the second anode passes to the 2 -stage audio amplifier, VR2 being the volume control.

V3 (EC90) is the v.f.o. covering $3 \cdot 5-3 \cdot 8 \mathrm{MHz}$, with a little to spare. VC3 is operated through a balldrive and although tuning is quite critical it is eased by the narrow band covered by VC3. Coverage is determined by L3 and the three capacitors C14, C15 and C16, so it is only necessary to adjust the core of L3. Because of the large value of these capacitors changes in capacitance around V3 have little effect on its frequency.

C5 and C13 are r.f. by-pass capacitors with C4 and C12 in parallel with them to avoid hum from the h.t. supply and reduce audio feedback effects. The receiver is intended for use with a supply of about $220-250 \mathrm{~V}$ at $40-50 \mathrm{~mA}$ with the heaters drawing 1.53 A at $6 \cdot 3 \mathrm{~V}$.


## CONSTRUCTION

The chassis, Fig. 3, is an $8 \times 4$ in. "universal chassis" flanged member. This allows a complete case to be assembled by using two further $8 \times 4 \mathrm{in}$. members, top and bottom, with two $6 \times 4 \mathrm{in}$. members for the sides. The panel is $8 \times 6 \mathrm{in}$. and the surface of the chassis is 2 in . above the bottom edge of the panel. Cut away the four corners " X " so that the $6 \times 4 \mathrm{in}$. sides fit round the chassis, allowing the box to be screwed together.

Flanges on the members listed are ready punched, and can be secured together with 4BA bolts and nuts while the receiver panel is secured to the top, bottom and side flanges with self-tapping screws. The case back should be of perforated metal, or have rows of ventilation holes.

VC1/2 is bolted to the panel, TC2 being soldered to a tag and VC1 as shown. The aerial coil L1 must be screened with the aluminium can supplied. The can lid is secured to the chassis by the fixing bush of L1. Leads for TCl and VCl pass out near the chassis. The lead from pin 6 passes through the chassis to tag 1 of V1. The normal adjusting screw of L1 cannot be reached because of VR1. So the core is removed, a shallow saw-cut is made across the end and it is replaced. Drill a hole in the screening can for this purpose and cut off about one-third of the screwed portion of the can, so that when it is tightly fitted it does not cut into the leads to TC1 and VCl.

TCl is mounted on a strip of insulating material. A1 and A2 are optional aerial connections.

VC3 is fitted so that its spindle projects ${ }^{9} 16 \mathrm{in}$. The ball drive is lined up so that it rotates freely and its lug is held with a long bolt with extra nuts. The lead MC from VC3 in Fig. 3 runs to a tag bolted to the chassis near L3.
The primary (P) connections of T1 run through to pins 6 and 7 of V4. Secondary leads (S) go to a small panel jack, for speaker or headphones.
Inductors. With the "Range 3" coils listed, Blue for L1 and Yellow for L2, adjustment of the cores and TC2 and TC3 gives easy coverage of 80 m and $\mathrm{VCl} / 2$ need not be exactly 25 pF .

L3 is 30 turns of 26 s.w.g. enamelled wire, closewound on a ${ }^{1} 2 \mathrm{in}$. diameter former with adjustable core. The winding is put near that end of the former furthest from the metal chassis and turns secured with Bostik 1.
Wiring. Wiring and components are shown in Fig. 4. The heater, grid and anode leads are run close to the chassis. Trimmer TC3 has one tag bolted to the chassis, so that it can be adjusted from the rear.

All connections should be reasonably short and direct, and run as shown. VFO wiring, especially to L3, C16 and VC3, is of stout wire, kept as short as possible.

Tag strips are used to support various small components. A 3-cored cable or coloured single flex

## components list

|  |  |  |
| :--- | :--- | :--- |
| Resistors: |  |  |
| R1 $33 \mathrm{k} \Omega 1 \mathrm{~W}$ | R8 | $10 \mathrm{k} \Omega$ |
| R2 $68 \Omega$ | R9 $270 \mathrm{k} \Omega$ |  |
| R3 $1 \mathrm{M} \Omega$ | R10 $3 \cdot 3 \mathrm{k} \Omega$ |  |
| R4 $1 \mathrm{k} \Omega$ | R11 $3 \cdot 3 \mathrm{k} \Omega 1 \mathrm{~W}$ |  |
| R5 $100 \mathrm{k} \Omega$ | R12 $68 \mathrm{k} \Omega$ |  |
| R6 $22 \mathrm{k} \Omega$ | R13 $470 \mathrm{k} \Omega$ |  |
| R7 $47 \mathrm{k} \Omega$ | R14 $680 \Omega$ |  |

All $1 W$ except as indic $680 \Omega$
VR1 $10 \mathrm{k} \Omega$ potentiometer, wire wound.
VR2 $500 \mathrm{k} \Omega$ potentiometer, log.
Capacitors :

| C1 | $0.01 \mu \mathrm{~F} 350 \mathrm{~V}$ disc | C11 | $60 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| :---: | :---: | :---: | :---: |
| C2 | $0.01 \mu \mathrm{~F} 350 \mathrm{~V}$ disc | C12 | $8 \mu \mathrm{~F} 350 \mathrm{~V}$ |
| C3 | $0.01 \mu \mathrm{~F} 350 \mathrm{~V}$ disc | C13 | $0.01 \mu \mathrm{~F} 350 \mathrm{~V}$ disc |
| C4 | $8 \mu \mathrm{~F} 350 \mathrm{~V}$ | C14 | 1000pF 1\% SM |
| C5 | $0.01 \mu \mathrm{~F} 350 \mathrm{~V}$ dise | C15 | 1000pF 1\% SM |
| C6 | 100 pF SM | C16 | $220 \mathrm{pF} 1 \%$ SM |
| C7 | $0.01 \mu \mathrm{~F} 350 \mathrm{~V}$ | C17 | 0.01 F F 350 V |
| C8 | 470pF | C18 | $0.01 \mu \mathrm{~F} 350 \mathrm{~V}$ |
| C9 | 2000pF | C19 | $12 \mu \mathrm{~F} 50 \mathrm{~V}$ |
| C10 | 22pF SM |  |  |
| VC1 | $2 \times 25 p F$ gang. (Jackson Type 02). 75pF variable. (Jackson Type C804). |  |  |
| VC3 |  |  |  |
| TC1, | 2, 3 50pF pre-s | m |  |

Valves:

| V1 | 6BA6 (EF93) | V3 | EC90 |
| :--- | :--- | :--- | :--- |
| V2 | 12AT7 | V4 | ECL82 |

Chassis and Case :
2 off $6 \times 4 \mathrm{in}$. sides, Type CU41B
2 off $8 \times 4 \mathrm{in}$. sides, Type CU56A
1 off $8 \times 6 \mathrm{in}$. plate, Type CU178
4 off Case feet, Type Z146
(all from Home Radio)

## Miscellaneous :

L1 Denco 'Blue' Range 3 (valve type).
L2 Denco 'Yellow' Range 3 (valve type).
L3, see text.
Ball drive, (Jackson 4489/C) RFC, 2.5 mH .
2 off B7G skirted valveholders and screens.
2 off B9A skirted valveholders and 1 screen.
Knobs, tag-strips, output jack socket.
T1, output transformer about $60: 1$ to carry 40 mA .
twisted together, is employed for h.t. positive, $6 \cdot 3 \mathrm{~V}$, and common return connections-red may be used


Fig. 4. Wiring guide for components underneath the chassis. Wiring around the v.f.o. valve $V 3$ should be kept as short as possibie to improve stability.

IT is apparent that there is a good deal of interest in small transmitters for the low frequency bands. There are several reasons for this. Such equipment can be constructed at small cost, with easily obtained components, and only a modest power pack is needed to reach the maximum allowed power input of 10 watts in the case of the 160 m band. Many newly licensed amateurs start with such equipment, and when using this power on the low frequency bands the chances of interference to TV are minimal.

The transmitter described here is primarily for 160 m working, but will be found to be a very practical piece of equipment on 80 m also, coverage of this second band being easily arranged. In addition, an end-fed aerial is often used for 160 m , which will also generally perform well on 80 m . The 80 m band also offers greatly improved range over 160 m and contacts during daylight, so it is well worth having.

## IRP TRANSMITTER for the LF BANDS F.G.RAYER G3OGR

## CIRCUIT

In Fig. l, V1 (6C4) is the variable frequency oscillator, followed by V2 (6AM6) which is a buffer/ doubler. V3 (6BW6) is the power amplifier, and runs at about 10 watts input, anode current being shown by the meter. This is a straightforward arrangement which gives good results with a minimum of difficulty.

VCl tunes the v.f.o. from $1 \cdot 75-2 \cdot 0 \mathrm{MHz}$ and, for the 160 m band, the $1 \cdot 8-2 \cdot 0 \mathrm{MHz}$ sector is used, transmitter output being on the same frequency as the v.f.o. For 80 m , the v.f.o. is tuned over the range $1 \cdot 75-1 \cdot 9 \mathrm{MHz}$, and V 2 acts as doubler, so that the output frequency is from $3 \cdot 5 \cdot 3 \cdot 8 \mathrm{MHz}$. V6 provides a regulated supply for the v.f.o.

L2 and L3 are broadly resonant coils for 160 m and 80 m . When first testing the equipment, grid current in the p.a. stage can be checked by clipping a test-meter across R8. L4 is the pi-network tank coil, tapped for 80 m .
The audio section has V4 (12AX7) as a high gain amplifier, followed by V5 (6BW6) which choke modulates V3. This arrangement has been found to give good modulation and quality when using a crystal microphone and it requires relatively few components.

With any set of transmitting/receiving equipment the problem arises of providing "Transmit" and "Receive" change-over facilities. A relay is often used to switch the aerial from receiver to transmitter,
to switch on the transmitter and to mute the receiver or speaker.

No external items of this kind are necessary with this transmitter, as the required switching is incorporated. This gives complete change-over from "Receive" to "Transmit" with single switch control.

The switch has four poles, section Sl switching the aerial to the tank coil L4 at T (Transmit), but transferring the aerial to the receiver at $R$ (Receive). Section S2 short-circuits the aerial feed to the receiver during transmission, to minimise r.f. leaking through to the receiver. S 3 is in series with one speaker lead, and so silences the speaker during transmission.

The transmitter power circuit is controlled by S4, which applies h.t. to all stages on transmit. S5 is a separate two-way switch, which allows h.t. to be put on V1 and V2 only. This allows the v.f.o. to be tuned to any wanted frequency, and be "netted"

with the receiver, either to answer a CQ, or to begin transmission on a selected channel.

The aerial, or matching device, if used, is plugged into the aerial co-axial socket. A co-axial lead of convenient length is made up, and plugged into the "Rx" outlet of the transmitter. This lead runs to the aerial and earth terminals of the receiver. Communications type receivers normally have a separate speaker, one lead of which is cut, and extended if necessary, so that plugs can be inserted into the "Mute" transmitter sockets.

The two switches on the transmitter then give complete control, for tuning the v.f.o. netting on a signal, and changing from reception to transmission.

## CONSTRUCTION

## VFO

By using a ready-made inductor and accurate capacitor values, experiments to obtain suitable band coverage are avoided. It is only necessary to adjust the core of L , and trimmer TCl , to set the band so that VCl tunes $1 \cdot 75-2 \cdot 0 \mathrm{MHz}$, with a little to spare at each end of the dial.

The v.f.o. is assembled in a box $3 \times 2 \times 2 \mathrm{in}$. which screens it completely and also helps isolate components from sources of heat. This box is readily
made from "universal chassis" strips. One strip is $7 \times 2$ in., with flanges which are cut 2in. from each end, so that the strip can be bent into an open U-form 2in. high and 3in. wide, with flanges all round. An accurate bend is most easily obtained by holding the strip on a block of wood.
The second strip is $3 \times 4 \mathrm{in}$. and also has flanges. It is cut through centrally to obtain two pieces $3 \times 2 \mathrm{in}$. One of these is bolted to the front of the box as in Fig. 2 and carries VC1. After wiring is complete and the box is fixed to the chassis the second $3 \times 2$ in. flanged piece is secured with self-tapping screws to close the back.

The v.f.o. is completely wired as in Fig. 2 before it is mounted. Trimmer TC1 is fixed just clear of the box top with a bracket or by bolts with spacers. A small hole is drilled in the box to permit adjustment of TCl. All connections are direct and rigid and points MC are joined with wire and also to tags bolted to the chassis.

The tag-strip in Fig. 2 is secured inside the box and supports the r.f. choke, C2, and C3. Coloured leads identify the wires which pass through the chassis-brown for h.t. ( 150 V ), blue for $6 \cdot 3 \mathrm{~V}$, and yellow for the lead from C5.

The box is fixed to the chassis by bolts through the flanges which turn inwards (omitted in Fig. 2, for clarity) and through the front and back plates. It is placed so that the ball drive can be arranged as in Fig. 3.


Fig. 2 : Constructional details of the VFO assembly.


Fig. 1 : Complete circuit of the QRP transmitter.

## Top of Chassis

Fig. 3 shows the position of the major components. Capacitor VC2 is of a type fixed to the chassis with small feet. Capacitor VC3/4 has three holes in the front plate and is bolted to a small bracket to bring the spindle level with that of VC2. These spindles pass through $\frac{1}{2} \mathrm{in}$. clearance holes.

Panel and chassis are fixed together by the switches and panel brackets. The lower edge of the panel must project about $\frac{1}{2} \mathrm{in}$. beyond the chassis, to clear the mounting flange of the case.

## Buffer Stage

Components are placed around V2 as in Fig. 4, with grid and anode circuits separated and heater leads close against the chassis. The MC connection to the central spigot of the valveholder passes across the holder, as shown.
The coupling winding provided on L2 and L3 is not required, and must be completely removed. The outer end of the larger winding of L3 is then unsoldered from its pin and 28 turns removed. The end of the wire is cleaned and re-soldered to the pin.

## PA Stage

Grid circuit components are under the chassis, and are placed around V3 approximately as in Fig. 4. A hole is drilled in the chassis adjacent to the anode, pin 7 , a lead passing directly through to the r.f.c. Anode circuit items are above the chassis.
C10 is anchored to a tag strip (Fig. 3) which also supports r.f.c.2, the top of the choke being held by C11. The 1800 pF 1 kV disc ceramic capacitors used in these positions are easily obtainable, but 2000 pF
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Fig. 3: Plan view of chassis showing disposition of major components.
mica capacitors of 750 V rating could be used instead.
The p.a. coil has 63 turns of 22 s.w.g. enamelled wire, close-wound on a lin. diameter paxolin tube about $2 \frac{3}{4}$ in long, During winding, a loop is made at 33 turns for the switch 57 connection. This leaves 30 turns in circuit from VC2 to the switch.

The coil is mounted by bolting a lin. long strip of paxolin to it and attaching this to the frame of VC2 with a second bolt. The coil is well clear of metal parts and the cabinet top.

## Audio Section

Grid leads and components should be against the chassis especially connections to pin 7 of V4 otherwise there is some danger of instability or picking up of hum or r.f.

No gain control was included because it was found that speaking normally with a hand-held crystal
microphone gave just about the required audio level. Gain can be reduced by removing C15 or by substituting a 1 megohm potentiometer for R12 connecting the slider to pin 2 of V4. It should be mounted on the back runner near V4 or be connected with screened leads.
The modulation choke T1 is the primary of a mains pentode type speaker matching transformer and should be able to carry $70-80 \mathrm{~mA}$, and of low d.c. resistance, to avoid excessive voltage drop.
A test of the a.f. section can be made by connecting a speaker to the secondary of the transformer. The speaker must be well clear of the microphone, to avoid audio feedback. Speech should be reproduced at ample volume with good quality. Causes of distortion could be low emission valves, wrong resistor values, or slight leakage in C13 or C16 upsetting the bias of the following stage.

Fig. 4: The wiring underneath the chassis.


Fig. 5: An "exploded" view of the transmit-receive switch S1-4 and netting switch S5.


## Switching

Fig. 5 shows switch connections. A co-axial lead is used for the aerial, taken to chassis at the socket, and at VC3/4. S5 is switched to the "Tune" position only when adjusting the v.f.o. frequency, and so S4 normally switches on all transmitter h.t. circuits.

## VFO Dial

A pointer, cursor or disc of transparent material such as perspex can be mounted on the flange of the ball drive by two short 8BA screws. A disc with a line marked on it was used. A piece of thin card of larger diameter than needed was temporarily fixed to the panel, and calibration marks made around the edge of the disc. The card was removed, markings transferred to scales of suitable diameter, and the card cut down to size and cemented in place, finally checking that the calibration was still correct.

CW
V3 can be keyed by disconnecting pin 3 from the chassis, connecting a 5000 pF capacitor directly from this tag to chassis and wiring a lead from pin 3 to a jack, normally closed to complete the circuit.


This places the key between cathode and chassis when the plug is in. It is also necessary to take Tl out of circuit, which can be done by fitting a two-way switch to the back runner, so that on c.w. h.t. reaches the r.f. section only. The lamp load mentioned later for a.m. tests is not suitable on c.w. Connect a 470 ohm resistor in series with a 5000 pF capacitor across the key jack.

## VFO CALIBRATION

Calibration is most easily done with a 100 kHz crystal marker used in conjunction with a communications type receiver. First adjust the core of L1, and trimmer TCl, for suitable coverage. As TCI is increased in value, the range of frequencies covered by VCI will be reduced. TCI and LI also allow the band edges to be adjusted. It is best to arrange that almost the whole swing of VC1 is needed to tune from $1 \cdot 75-2 \cdot 0 \mathrm{MHz}$, but to avoid the extreme positions.

## components list

## Resistors:

| R1 | $68 \mathrm{k} \Omega$ | R10 | $1 \mathrm{M} \Omega$ |
| :---: | :---: | :---: | :---: |
| R2 | 2.2k $\Omega$ | R11 | $220 \mathrm{k} \Omega$ |
| R3 | $10 \mathrm{k} \Omega$ 3W | R12 | $1 \mathrm{M} \Omega$ |
| R4 | $47 \mathrm{k} \Omega$ | R13 | $150 \mathrm{k} \Omega$ |
| R5 | $3 \cdot 3 \mathrm{k} \Omega 1 \mathrm{~W}$ | R14 | $2 \cdot 7 \mathrm{k} \Omega$ |
| R6 | $100 \mathrm{k} \Omega$ | R15 | $33 \mathrm{k} \Omega 1 \mathrm{~W}$ |
| R7 | 22k $\Omega$ | R16 | $470 \mathrm{k} \Omega$ |
| R8 | $1 \mathrm{k} \Omega$ | R17 | $270 \Omega 2 \mathrm{~W}$ |
| R9 | $5 \cdot 6 \mathrm{k} \Omega 2 \mathrm{~W}$ |  |  |

All $\frac{1}{2} W 10 \%$ unless indicated otherwise.

## Capacitors:

| C1 | 120pF SM 1\% | C10 | 1800pF 1kV |
| :---: | :---: | :---: | :---: |
| C2 | 1000pF SM 1\% | C11 | 1800pF 1kV |
| C3 | 1000pF SM 1\% | C12 | 47pF SM |
| C4 | $0.02 \mu \mathrm{~F} 350 \mathrm{~V}$ | C13 | $0.002 \mu \mathrm{~F} 350 \mathrm{~V}$ |
| C5 | 100 pF SM | C14 | $2 \mu \mathrm{~F} 350 \mathrm{~V}$ |
| C6 | $0.02 \mu \mathrm{~F} 350 \mathrm{~V}$ | C15 | $50 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C7 | $0 \cdot 25 \mu \mathrm{~F} 350 \mathrm{~V}$ | C16 | $0.0025 \mu \mathrm{~F} \mathrm{350V}$ |
| C8 | 100pF SM | C17 | $50 \mu \mathrm{~F} 50 \mathrm{~V}$ |
| C9 | 1800pF 1kV | C18 | $0.005 \mu \mathrm{~F} 1 \mathrm{kV}$ |
| TC1 | 45pF trimmer, | amic |  |
| VC1 | 75 pF miniature |  |  |
| VC2 | 500pF variabl |  |  |
|  | $4500+500 \mathrm{pF}$ | d | able, air. |

## Valves:

| V1 | 6C4 (EC90) | V4 | 12AX7 (ECC83) |
| :--- | :--- | :--- | :--- |
| V2 | 6AM6 (EF91) | V5 | $6 B W 6$ |
| V3 | 6BW6 | V6 | OA2 |

Inductors:
L1 "Yellow", Range 3 (Denco)
L3 "Red", Range 2 (Denco)
L2 "Blue", Range 2 (Denco)
L4 See text
RFC1 2.5 mH miniature iron-cored choke
RFC2 2.5 mH 60 mA sectionalised choke

## Miscellaneous:

Valveholders, B7G with skirt (3) B9A with skirt (3). B7G screens (2) B9A screens (1). Co-axial sockets (3). Switches, 4 pole 2 way rotary (1) 1 pole 2 way rotary (1) on/off toggle (1). Miniature meter, 50 mA f.s.d. T1, see text. Flanged ball drive. Knobs etc. Cabinet No. BX5 with chassis $10 \frac{1}{2} \times 4 \frac{3}{4} \times 1 \frac{1}{2} \mathrm{in}$. (Home Radio). VFO box made from flanged chassis strips CU136 and CU144 (Home Radio).

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With S5 at the "Tune" position and a lead from the receiver lying near the transmitter, tune the receiver to 3.5 MHz using the crystal marker, tune VCl to zero beat, and mark the scale for 3.5 MHz repeating for $3 \cdot 6,3 \cdot 7$ and $3 \cdot 8 \mathrm{MHz}$. Also mark $3 \cdot 6$ as $1.8,3.7$ as 1.85 , and 3.8 as 1.9 MHz . Continue with the $3 \cdot 9$ and $4 \cdot 0 \mathrm{MHz}$ marker pips, but marking the v.f.o. for 1.95 and 2.0 MHz only. If the extreme settings of VCl have been avoided the 10 kHz points can be filled in linearly between the 100 kHz points.

A 10 mA or multi-range meter is connected from "G" Fig. 1 to chassis, the latter being positive. The v.f.o. is set to $1.9 \mathrm{MHz}, \mathrm{S} 6$ to 160 m , and the core of L2 is adjusted for maximum grid current, which should be around 3 mA . Then adjust the v.f.o. to about $3 \cdot 7 \mathrm{MHz}$, switch to 80 m adjusting L 3 core for maximum grid current which will be around 2 mA .

## TESTING

It is simplest and best to test the whole equipment by feeding the transmitter output into an artificial aerial load. This can be a 15 watt or 25 watt 240 V or similar household lamp. Clip it across VC3/4 and chassis, or fit a holder, lead and co-axial plug so that it may always be employed for tests.
P.A. tuning procedure is that generally employed with a pi-network. Check that S 7 is closed for 80 m , or open for 160 m , to match the position of S6. Fully close VC3/4 and also VC2 (to prevent the possibility of doubling in the p.a.). Switch to "Transmit" and open VC2 to obtain a dip in anode current, as shown by the panel meter. Current will be low but loading is increased by opening VC3/4, meanwhile adjusting VC2 for minimum current. As this is done, the minimum current rises, and the 15 watt lamp should light with fair brilliance when the input reaches about 10 W .

The d.c. input to V3 anode is anode volts $\times$ anode current, thus 33 mA at 300 V will be 9.9 watts. A supply voltage of less than 275 V is not recommended.

If the transmitter is loaded into the lamp, and a receiver is tuned to the signal, speech should sound clear and well modulated. The receiver should have its aerial disconnected and r.f. gain turned well back, or overloading may cause distortion.

## POWER SUPPLY

Fig. 6 is the circuit of a suitable power supply. The mains transformer actually used was a Parmeko P.2931, 250/0/250V 150mA, with SE-05 rectifiers D1 and D2, and Parmeko P. 3141120 mA choke. This provided 280 V with a load of 120 mA . BY 100 rectifiers would also be suitable. The voltage obtained when using semi-conductor rectifiers is somewhat higher than with a valve rectifier. Many transformers have winding for valve rectifiers so a 5 U 4 G is a suitable rectifier for a 5 V 3A winding, or an EZ81 for a 6.3 V 1 A winding.

## AERIALS

The simplest possible aerial is an end-fed wire. Some lengths will offer such a load impedance that the transmitter can be worked directly into the aerial, on one or both bands. Other lengths present load impedances which are outside those which can be matched by the transmitter, and then proper tuning or loading will be impossible. One of the


Fig. 6: Suggested power supply for the QRP transmitter.
matching circuits in Fig. 7 can then be used.
Fig. 7(a) is the simplest. Ll may be similar to the tank coil, or be a surplus tapped inductor, or may consist of a number of turns, found by trial and error, on a former lin. to 3in. in diameter.
Fig. 7(b) is similar but has a capacitor VCl added, of about 250 pF , which allows more accurate adjustment and has fewer tappings on L2.
Fig. 7(c) is series tuning often used for quarterwave aerials on l.f. bands. VC2 can be 500 pF and again L3 resembles the tank coil. The tapping makes L3 into an auto-transformer and may be set about 10 turns from earth for 160 m , or 4 or 5 turns from earth for 80 m . For the latter band only L3 may have fewer turns.
Fig. 7(d) is parallel tuning suitable for a half-wave aerial on 80 m . L4 is about 30 turns on a lin. diameter former, with a 250 pF capacitor for VC3 and L5 is about 4 turns of insulated wire over the earthed end of L 4 .


Fig. 7: Four circuits enabling a/most any aerial to be matched to the transmitter.

A typical aerial of 126 ft in length would be about a quarter-wave on 160 m , and a half-wave on 80 m , so Fig. 7(c) would be required for 160 m , and Fig. 7(d) for 80 m working. However, it is generally easier to make up a tuner with one of the circuits in Fig. 7 or a similar circuit and to experiment with tappings until the transmitter can be satisfactorily loaded by the aerial. Even very short wires (under 10ft.) may be used with these circuits but range is much reduced.

L.A.J.IRELAND

Number 22

## G.E. PA264-265 Voltage Regulators

MANY constructors will have come across the difficulty of having to operate 6 volt portable transistorised equipment from a 12 volt car battery. In such equipment current drain will usually be dependent upon the audio output so as to conserve the life of the battery and as a result the conventional voltage dropper resistor will not suffice. An alternative approach is to use some form of voltage regulator and lately the G.E. Company have released a monolithic i.c. capable of fulfilling just this function. With a 5 watt power dissipation capability, the i.c. eliminates the need of both a high power pass transistor and its associated drive components and with a half dozen or so discrete components needed to complete the unit, it makes an ideal compact in-line device.

## Background

Readers familiar with the present series of articles will remember the precision voltage regulator type LM100 reviewed in the June 1970 issue of P.W. This was a rather sophisticated low-power i.c. in which a built-in reference voltage was compared to a fraction of the output voltage to achieve accurate stabilisation. One of its big draw-backs however was the need for an external power transistor if an output current in excess of 12 mA were to be drawn and towards the end of the article attention was drawn to the G.E. unit, type PA264, which would overcome these difficulties but which at the time was only in the development stage of production.

## Operation

Basically the PA264 functions as follows. By referring to Fig. 1 it can be seen that Tr 1 and Tr 2 form a differential comparator whose inputs are controlled by an external zener and a sample of the output voltage. $\operatorname{Tr} 2$ in turn directly controls the Darlington pair Tr4 and Tr5. Any tendency in the output voltage to decrease will be counteracted by a drop in voltage at the base of $\operatorname{Tr} 2$ which in turn will tend to increase the current through Tr 4 and Tr 5 . The reverse situation occurs if the output voltage tends to increase and so the unit is self-compensating.

The output voltage may be varied in two ways, by potting down the reference voltage applied at pin 14 or by varying the feedback voltage at pin 13.

However there are practical limitations to these methods in that the voltages set at pins 14 and 13 should be kept within the limits $1 \cdot 5 \cdot 3 \cdot 5$ volts for optimum performance. Values of components specified in Fig. 1 are for a 6 volt output but it should be remembered that any output above 3 volts may be obtained with suitable choice of components. The maximum voltage rating of the PA264 is 25 V and of the PA265 37 V and this in fact is the only difference in their electrical characteristics.

## Packaging

The units are housed in a rather unusual epoxy package with eight staggered leads in addition to


Fig. 1. Circuit of the PA264 with additional components required to provide $6 v$ from 12 v supply.

THE opening of local radio stations on the v.h.f. band and the continual plugging by the BBC of the better quality obtainable with frequencymodulation is increasing the public interest in this area of broadcast reception.

Unfortunately, the claims that reception is inter-ference-free is far from true, and as a result users and engineers may face some tricky problems. While interference from foreign stations, the bane of medium-wave listening, is absent, there are other forms to take its place.

For those living on or near main roads, car ignition interference is probably the most troublesome. This is especially so if the road is on a hill, when not only is the interference generated by a car in low gear much worse, but it also takes longer to pass.

All new vehicles are now suppressed, and have been for the last few years, indeed it has been noticeable that ignition interference has been thinning out, as the older vehicles become fewer in comparison with the new ones. However, there are still sufficient passing on any main road in a given time to cause a number of serious interruptions to any particular programme.

While the irate listener may feel like taking drastic action against the offenders, the solution in this case cannot be applied to the source, and in any case would be illegal! Usually, part of the trouble lies with the aerial. The majority of chimney stacks are already so festooned with Band I and III television aerials plus probably u.h.f. as well, that there just isn't room for a Band II radio aerial. Often, in areas not too remote from the transmitter, quite good signal strength can be obtained with the internal aerial wire running around the back of the cabinet, or at least with one along the picture rail. So the idea of having anything more elaborate seems pointless and money-wasting.

However, although the signal may be strong enough to give reasonable fade-free reception, it is when a splash of interference comes along that the inadequacy becomes all too apparent. The signal-tonoise ratio is just not good enough.

If the chimney looks as' though it just will not stand any more, the answer may be in the loft. A good loft aerial is much less expensive than an outdoor one as it does not have to be weather-proof, or need chimney lashings. It will give a much stronger signal, and being elevated well above the road will be out of the worse area of ignition interference.

The directional properties of the aerial will also help as any radiation from directions other than the transmitter will be reduced. If the transmitter direction is away from the road, mount the aerial on that side of the loft as this will put the bulk of the house between the aerial and the road, and so afford a degree of shielding. This really should reduce ignition interference to the level of background noise, if not entirely eliminate it.


Loft aerial positioned on side of house furthest from the main road,
House affords measure of screening from ignition interference.
House affords measure of screening from ignition interference.

The other form of interference can be more troublesome to deal with. There seems in most of our major cities a proliferation of private radio-telephone installations as used by police, ambulance, taxis and other services. These operate on a number of frequency bands, three of them in the v.h.f. range, $70-85 \mathrm{MHz} ., 103-140 \mathrm{MHz}$. and $168-175 \mathrm{MHz}$. There is also one in the u.h.f. region. The broadcast v.h.f. frequencies of Radio 1, 2, 3, and the local stations lie within the range $88-96 \mathrm{MHz}$. or right in between the two lowest radio-telephone bands, and so are vulnerable to interference from them.

## Spurious Signals

To see how this interference can occur, we will review the ways by which spurious signals can be received with a superheterodyne receiver. First, there is breakthrough of signals at the i.f. frequency, which in the case of most f.m. receivers is $10 \cdot 7 \mathrm{MHz}$. The local oscillator has no effect on these, so they would be heard irrespective of the setting of the tuning dial, and in fact, this factor serves to identify them. There are no authorised transmissions at this
frequency, so this class of interference should not be encountered unless it was due to a short-wave transmitter operating illegally.

Another form of interference is the well-known image or second-channel type. There are two frequencies that will produce a response in a superheterodyne receiver, one is the sum of the local oscillator frequency and the i.f., and the other is the difference between them. If, as is common practice, the oscillator is running higher than the programme signal, it is operating on the difference, and another signal which is the sum will produce interference.

We can use an example to illustrate: If the wanted signal is at 90 MHz , the oscillator is running at $90+10 \cdot 7=100 \cdot 7 \mathrm{MHz}$. An unwanted signal will produce the i.f. frequency at the output of the mixer if it is higher than the oscillator by the frequency of the i.f., or $100 \cdot 7+10 \cdot 7=111 \cdot 4 \mathrm{MHz}$. As can be seen, this is within the middle band used by radiotelephone services. Second-channel interference then, arises from signals twice the frequency of the i.f. away from the wanted signal; higher if the oscillator is running high, and lower if it is low. For normal v.h.f. sets the interfering signal would be $21 \cdot 4 \mathrm{MHz}$ higher than the broadcast frequency.

Similar, is the i.f. harmonic interference. This is the sum of the local oscillator and half the i.f., and also their difference. Such a signal will produce an output at the mixer anode of half the i.f. frequency, and it is the second harmonic of this which will be passed by the i.f. circuits.

Using our above example, the local oscillator frequency is again $100 \cdot 7 \mathrm{MHz}$, and the interfering frequencies will be $100 \cdot 7+5 \cdot 35=106 \cdot 05 \mathrm{MHz}$ and $100 \cdot 7-5 \cdot 35=95 \cdot 35 \mathrm{MHz}$. In relation to our wanted signal of 90 MHz , the frequencies are plus half and $1^{1}{ }_{2}$ times the i.f. Harmonics are not usually as strong as the fundamental, so interference from this cause is not so likely to give trouble unless the unwanted signal is very strong.

A further type is the beat interference. This occurs from a signal that is spaced from the wanted signal, either above or below, by the i.f. frequency, and is caused by the two signals beating together to form a resultant at the i.f. frequency. Actually, the interfering signal performs the same function as the local oscillator, only of course it carries its own modulation which is passed on through the i.f. stages and detector along with that of the wanted signal. If the interfering signal is strong enough, the set would continue to work with the local oscillator stopped, and this fact could be used to help identify this form of interference. Thus for a wanted signal of 90 MHz , beat interference would be caused by signals at $79 \cdot 3 \mathrm{MHz}$ and $100 \cdot 7 \mathrm{MHz}$.

Finally there is the interference caused by oscillator harmonics. All oscillators produce harmonics, and the second-harmonic of $100 \cdot 7$ which you remember is our local oscillator frequency for receiving a signal at 90 MHz , is $201 \cdot 4$. Signals spaced above and below this by the i.f., i.e. $201 \cdot 4-10 \cdot 7=$ $150 \cdot 7$, and $201 \cdot 4+10 \cdot 7=212 \cdot 1 \mathrm{MHz}$, would therefore be passed into the i.f. circuits.

These frequencies are in the commercial television band and above the highest radio-telephone range. The third-harmonic of the oscillator would bring it even higher. Frequencies so remote from the wanted ones should be greatly attenuated by the tuning in the r.f. circuits and the tuned aerial, so should not present any problems. If though it is found that
commercial t.v. signals are breaking through, this is the probable cause.

Summing up then, interfering signals can be spaced from the wanted one by twice (second channel); $1^{1_{2}}$ times (i.f. harmonic); once (beat interference); and half (i.f. harmonic) times the i.f. frequency, on the high side; and one (beat interference) times on the low side. So there are at least five possible frequencies that will interfere with each and every broadcast station. As there are four BBC programmes in most areas, this gives us some 20 possible interfering frequencies. The situation is aggravated by the fact that f.m. receivers are not sharply tuned as are a.m. sets. It is of course necessary to maintain a wide pass-band because of the nature of the f.m. signal. Broadcast deviations are up to 75 kHz either side of the carrier frequency, so receiver circuits must extend well beyond these limits.

This means that interfering frequencies do not have to be spot on the values calculated, and if only near them, interference can result. With the previously noted increase in radio-telephone users, it can be seen that the possibility of interference with broadcast programmes is high, and is steadily increasing.

## Radio-telephones

The question is, what can be done? Mobile units are not so much a nuisance, as they operate at low power, and usually cause interference only when they are fairly close to the receiver. The chance of a mobile operating at a frequency which could cause interference, coming sufficiently close to a working f.m. receiver tuned to a vulnerable frequency, is not very great, and the odd occasion when it may occur could hardly constitute a major nuisance.

It is the base stations that are the real menace. These are operating more or less continually, and are relatively high powered. Should one of these be within a few miles and operating on a critical frequency, then constant jamming will result.

The first step is to try to identify the offender. This is not too difficult as a number of his messages are being unwillingly intercepted. The class of business can be quickly deduced, and a local knowledge of the businesses of that type large enough to operate radio telephones, will help to narrow things down. One clue is whether the interference is present in the evenings or at week-ends. If it is, then a business that offers service outside normal hours will be the obvious culprit.

After eventually identifying the source, one can try swinging the aerial away from the direction of the transmitter while not losing too much of the broadcast signal. A local road map will help to obtain the precise directions involved. Do not swing too far away from the BBC station though, as the received signal may then be reflected and suffer phase-distortion, which is similar to ghosting on a television picture.

The next step is to find out the exact frequency of the transmitter. Once the owner has been identified, this should present no problem; if the reason for requiring the information is explained, he will no doubt be willing to co-operate. He may not know the frequency, perhaps being non-technical, but this should be shown on the transmitting licence or other paperwork connected with the system. The relation-
ship between the frequency and that of the broadcast signal with which it is interfering can then be seen and the type of interference identified.
If it has not proved possible to discover the source of the interfering transmission, it may be possible to deduce the type of interference from the clues given above, and so arrive at the possible frequency. For example, stopping the local oscillator (without shorting-out the input signal) will determine whether the interference is due to a beat-signal. If this is found to be the case, the frequency will be spaced either above or below the wanted signal by an amount equal to the i.f. So if receiving a station on 90 MHz , the interference will be either $79 \cdot 3$ or $100 \cdot 7 \mathrm{MHz}$. As the latter does not fall within the band used for radio telephones, then it is fairly certain that $79 \cdot 3 \mathrm{MHz}$ or thereabouts is the offending frequency.

## Co-axial Stubs

Having discovered the interfering frequency, the next thing is to suppress it (electrically of course). One method of doing this which is often recommended is the parallel stub of co-axial cable. Co-ax exhibits the properties of inductance and capacitance and so will form a resonant tuned circuit. With a velocity factor of unity, the length of the stub should be a quarter of the wavelength of the signal it is desired to eliminate. It should then be connected in parallel with the aerial-feeder near to the aerial socket on the receiver, the free end being left opencircuited.
In theory then, it is a straightforward matter to calculate the length and connect up. Not so in practice. First of all, the velocity factor of the co-ax is not unity, but varies from one sample to another. Typical values are 0.67 for the solid dielectric type, and 0.85 for the semi-air spaced variety. This must be multiplied by the quarter-wavelength to arrive at the actual length, so an exact calculation with any sample of co-ax is not easy.
There is a further complication; much depends on the characteristics of the aerial input circuit, whether it is inductive of capacitive. At a frequency higher than resonance, a tuned cricuit appears capacitive, whereas at a lower frequency it is inductive, the two balance out only at the resonant frequency. The receiver aerial circuits will be tuned to the wanted frequency, so at an interfering frequency, the circuit will appear either inductive or capacitive depending on whether the frequency is higher or lower than the wanted one, and the degree of inductance or capacitance will depend on the spacing of the frequencies and the Q of the circuit.
It can be seen then, that cutting a stub to the exact size is very much a matter of chance. The recommended method of tuning the stub is to cut it longer than the estimated length and cut off sections about $1_{2}$ inch at a time until the minimum level of interfering signal is attained. To do this as with most tuning procedures, it is necessary to go through the resonant point to ensure that the peak (or trough in this case) has been reached, and then tune back. Obviously it is not possible to stick back on the last few sections that have been chopped off, so the thing to do is carefully note how much has been removed since the signals started to increase, and then measure up a new stub made from the same type of co-ax.

Severe interference was being experienced on the author's own set-up which consisted of a separate f.m. tuner feeding the hi-fi system. The trouble was with the reception of Radio 3 from the Wenvoe transmitter which uses the frequency of $96 \cdot 8 \mathrm{MHz}$. Programmes were completely blotted out when the interference occurred, not only during the day but up to late at night and also at weekends. It was impossible to enjoy a concert, and tests with other f.m. receivers in the neighbourhood confirmed that they too likewise suffered. Their owners either put up with it, switched to a.m., or just didn't listen to Radio 3.

It was obvious from the messages received that the source was a television repair shop controlling its service vans. The fact that a number of vans were apparently in communication indicated a business of some size, and also the evening and weekend operation narrowed down the field among the local firms. A few phone calls to the short-list of suspects revealed that it was the local Rediffusion workshop. The chief engineer was co-operative and apologetic, offering to check the frequency of the transmitter and that it was duly suppressing its harmonics, but of course the frequency was assigned by the Post Office Telecommunications Department, and there was nothing he could do about that.

He was able to state the frequency which was $85 \cdot 725 \mathrm{MHz}$. It then became obvious that this was a case of beat interference, as the frequency is 10.7 MHz away from 96.425 MHz , which is just $0 \cdot 375 \mathrm{MHz}$ off the Radio 3 centre frequency. It was an obvious boob by the Post Office in assigning so critical a frequency to a powerful base station. Admittedly, frequencies are scarce and the demand is great, but troublesome frequencies such as these could easily be assigned to mobiles.

An interference form was obtained from the Post Office, and all the details as to source of interference, frequency and type were included and duly sent off. However, nothing more was ever heard, and as the interference continued it appears that nothing was done by way of re-allocating the frequency.

## Series Wavetrap

It was therefore decided to tackle the problem without G.P.O. assistance. First of all, stubs were tried, but the difficulties previously described foiled success with these. Unfortunately, the Rediffusion base was in exactly the same direction from the aerial as the Wenvoe transmitter, so no rejection could be obtained by swinging the aerial. Nonetheless it was tried, and although the f.m. signal dropped, the interference decreased more so, so some improvement in signal interference ratio was obtained.

Finally the possibility of a series resonant wavetrap in the aerial feeder was considered. A coil resonating with its self-capacity and tuned with a brass slug was needed to enable a quick and convenient adjustment frequency adjustment to be made. The problem was, how to make one with any degree of accuracy that would not need lengthy experiments with the intermittent signal source similar to a stub.

Looking around the workshop for some readymade component which might fill the bill, attention turned to some old coil biscuits from scrapped television tuners. A channel 2 oscillator biscuit was
found among them. The BBC station on channel 2 operates at $48 \cdot 25 \mathrm{MHz}$ (sound). The sound i.f. for the set concerned, and which is now common for most modern t.v. receivers, is $38 \cdot 15 \mathrm{MHz}$. This means that the frequency of the oscillator coil was 86.4 MHz . As the Rediffusion frequency was $85 \cdot 725 \mathrm{MHz}$., this was near enough to be within the tuning range of the coil.


Appearance of typical coil biscuit. Oscillator coil is usually the largest and contains a tuning slug.

Accordingly it was connected in series with the aerial feeder, and the interference was completely eliminated, without the need even to tune the coil.
Most t.v. workshops have old tuners knocking around, so a call at the local radio dealers could well produce a coil suitable for the purpose, should similar interference be experienced. The chart shows the frequencies of the main BBC band I television channels, and assuming a $38 \cdot 15 \mathrm{MHz}$ sound i.f., the actual tuning range of an oscillator-coil biscuit. It will be noted that channels 3 and 4 coils will tune to frequencies within the v.h.f. radio band, so will be no use as wavetraps for radiotelephone frequencies as these are all outside this band. Channel 5 is just at the start of the medium radiotelephone band, and could easily tune to some of its lower frequencies.

| TELEVISION <br> CHANNEL | SOUND <br> FREQUENCY | OSCILLATOR <br> CRIL <br> CREQUENCY |
| :---: | :---: | :---: |
| 1 | 41.5 MHz | 79.65 MHz |
| 2 | 48.25 MHz | 86.40 MHz |
| 3 | 53.25 MHz | 91.40 MHz |
| 4 | 58.25 MHz | 96.4 MHz |
| 5 | 63.25 MHz | 101.4 MHz |

Remember, too, that the range of the coil can be extended by the fitting of a different type of tuning slug. A brass slug will decrease the inductance, hence increase the frequency, while an irondust slug will increase inductance and decrease the frequency. If the range is still outside the interfering frequency, a couple of turns taken off the coil will push it higher, or a small capacitor of a few pF . will bring it lower, if wired in parallel. The biscuit may have two or three coils on the same former, the oscillator is the one nearest the open end and which has the tuning slug. The other coils are coupling coils and should be ignored.

## Direct Conversion Receiver continued from page 300

for h.t. positive, black for chassis and some other colour for the 6.3 V heater supply.

## ALIGNMENT

Set TC2 and TC3 about half closed and tune in any signal, with VC3 nearly open, and adjust TC2 and $\mathrm{VCl} / 2$ for best volume. Find a signal with VC3 nearly fully closed and peak VC1/2 for best results, then rotate the core of Ll for maximum volume.
If necessary, the core of L3 is rotated to obtain suitable band coverage with VC3. The coverage of VC3 can be checked by placing the aerial lead of a calibrated receiver near L3 and listening for the carrier produced by V3.

At all times the r.f. gain control $\mathrm{VCl} / 2$ is adjusted as needed for best reception even though VRi may have to be turned back with strong signals. The cores of L 1 and L 2 are adjusted around $3 \cdot 5 \mathrm{MHz}$ and the trimmers TC2 and TC3 are set near 3.8 MHz . TC2 may also need re-adjustment after changing the aerial. These circuits are merely peaked up for


Rear view of the finished receiver.
best volume and are not too critical. The extent of rotation of this control needed to tune from 3.8 $3 \cdot 5 \mathrm{MHz}$ can be increased by screwing down TC2 and TC3 and unscrewing the cores of L1 and L2 to compensate.
Power Supply. Any supply giving about the outputs mentioned should be satisfactory. If a power pack has to be made, one with full-wave rectification is most suitable. This may employ a $250 / 0 / 250 \mathrm{~V} 60 \mathrm{~mA}$, $6.3 \mathrm{~V}(1.5 \mathrm{~A}$ or 2 A$)$ transformer, with smoothing by means of two $16 \mu \mathrm{~F} 350 \mathrm{~V}$ capacitors and a 60 mA choke.
Speaker and Phones. A reasonably large $2 / 3$ ohm speaker is most suitable with a cabinet or baffle.

When phones are plugged in, the mis-match can generally be disregarded. Inexpensive surplus 600 ohm phones will be found to work well. It would be possible to use an external matching transformer for high impedance phones or to feed them through reliable isolating capacitors from V4 anode. Aerials. Numerous transmissions were received with a short indoor aerial but changing to an outdoor wire tuned as for transmission purposes naturally gave a great increase in range and volume. In practice, any end-connected wire can be taken to A1 or A2 while the A2 connection is most suitable for short aerials.

## * iN NEXTMONTH'S <br> 



DIGITAL FREQUENGY GOUNTER/TIMER


Yesterday's dreams have a habit of becoming today's realities in the field of electronics. Five years ago direct readout frequency meters cost so much that many companies flinched at the price but today inexpensive integrated circuits have brought these into the bracket for the home constructor.
Just imagine. Pop in any frequency (below 20 MHz ) and there you are-it's displayed before your eyes to the nearest cycle! The Digital Frequency Counter/Timer makes use of four digit neon numeral tube displays and uses the widely available " 74 " series of TTL i.c.'s.
Certainly this is a complex project-theoretically-but it's the i.c.'s that do the work, not you, and thi's project could be tackled by anyone who can wield a soldering iron

## AlSO: <br> THE <br> 'HARMONIC SIX' RECEIVER



## THE HARMONICSIX RECERER

This is a six transistor superhet covering all the popular short wave bands and designed to power eithe ta loudspeaker or headphones. The unusual feature is that there is no ascillator switching-instead the 2 nd harmonic on the oscil? lator is used.
Standard parts are used throughout and this together with the fact that it's designed by one of our top gutbor makes this a first class project.

## MINI-AMPLIFIER

Although measuring only $2^{\prime \prime} x^{\prime \prime} 1^{\prime \prime} \times{ }^{1 /}$; this ampifief osing four silicon transistors has an output of 250 mW into a 256 loudspeaker. A multitude of uses can be found for thes project which can be built for a total cost of no more than eita

ALL IN THE SEPTEMBER ISSUE ON SALE AUGUST 6th


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WE thought very carefully before calling this article the PW Treasure Tracer. Certainly this sounds better than "metal locator" but could we justify the title? We think we can, especially after our test. We found nothing of great value but judging by the results we could have, that is, if there had been any there. Even if valuables are not found, certainly a whole lot of extremely interesting items will be and the history of an area of ground will yield up its secrets. However, your chances of finding coins are very good-about $150,000,000$ coins are lost every year and a high proportion of these must be lost in areas where they can be found using a device of this type.
Not many months ago a hoard of Anglo-Saxon coins was found, using a metal locator, these were later auctioned for $£ 9,000$. It shows what can be done.
Metal locators work on a variety of principles and the author has experimented with a number of different circuits. Nearly all rely on the fact that metal objects distort magnetic fields. Complex designs have appeared from time to time making use of various effects-each claiming to be an improvement over others-but the author's experience has not borne out these claims. The principal used herethe Beat Frequency Type-is possibly the oldest and certainly the simplest. It needs only one wound coil, unlike many other circuits, and the sensitivity and results are excellent. We are deliberately not overstating our claims and the only figures for range etc. are those proved by our tests.
The Treasure Tracer comprises two low power r.f. oscillators working at about 130 kHz . One of the oscillators is screened inside the chassis and the frequency can be altered over a fairly wide range to match it close to the other. The second oscillator uses a frequency determined by the inductance of a winding which is used as the search coil.

In the absence of any material which will affect the inductarce of this search coil, the oscillator is at one frequency. However when this coil is moved near some metal object, the inductance is altered slightly and the frequency of oscillation is changed. If the oscillators are set closely together an audio beat note is produced (equal to the difference in frequency) which may be amplified to feed a loudspeaker.
Finding a small copper cllp (ttem 16).
The grass guard made from Perspex can be seen fitted under the coll framework.


Searching along were cart fitting: places should ge


Let us assume that the search oscillator is working at 130.0 kHz . The reference oscillator is adjusted to say 130.2 kHz . The two signals are mixed together producing notes of $130 \cdot 2-130 \cdot 0=200 \mathrm{~Hz}$. There is also another frequency produced, the sum of the two, $260 \cdot 2 \mathrm{kHz}$, but this can be ignored.

The presence of a metal object near the search coil will increase the inductance causing the frequency of the search coil oscillator to fall to say $129 \cdot 8 \mathrm{kHz}$. The beat note will now be $130 \cdot 2-129 \cdot 8=400 \mathrm{~Hz}$ so the raising of frequency of the beat note will thus indicate the presence of a metal object near the coil.
From this theory the Treasure Tracer was built, using a frequency below 150 kHz to conform to regulations. Initial tests in the lab showed that the prototype was working reasonably well and that a definite beat note was obtained-but how would it work in practice?

## THE TESTS

The first test was arranged at the PW offices. A couple of dozen telephone directories were piled two high (making for a thickness of at least two inches) and coins ranging from $\mathrm{I}_{2}$ p to 50 p were hidden under certain piles. All coins were found immediately, but there was an extra reading-this turned out to be the wiring under the floor!
These tests in themselves were interesting and we were slightly encouraged but how would the metal locator (for we were still calling it that at this stage) fare in a field test? Only one way to find outarrange one.

One Monday in late May Eric Dowdeswell (PW Editorial), Peter Metalli (Art Editor), Jack Wood (Photographer) and the author set out for Canvey Island in South Essex to put it to the test.

The weather was fantastic and the beach was far from empty and under the puzzled eyes of day trippers we began our search, panning up and down the beach, just above the water line.

Our hearts fell. For several minutes the whistle remained unaltered. Up and down we panned and gradually we began to think that the journey was wasted. Then suddenly the note changed frequencya very definite, strong reading. As we dug Jack Wood
photographed us and the picture is that used on the cover. A quick dig produced a rusty hinge about three inches under the sand. We must have been unlucky to start with for after our first "find" we got readings every few yards. The items we found on this short stretch of beach and at other locations tried on the test are shown overleaf.

One thing cursed the search-silver paper. We found it everywhere and it accounted for over 75 per cent of all readings. We couldn't ignore these of course, for until we dug we didn't know what was causing the note to change frequency. The silver paper was from ice cream wrappings, cigarettes and sweets and even pieces so small that they were only found after extensive sifting, gave strong readings.

We altered our technique because of the sensitivity of the Treasure Tracer to small objects. As soon as we obtained a reading we carefully located the exact position before we began to dig-this could be done within an inch or two. As we dug we put the sand in two piles and checked at intervals with the Treasure Tracer that there was still a reading in the original position. If we had found nothing and the reading had disappeared we checked the two piles of sand. Invariably the metal was found in one of these. Even quite careful digging did not stop us missing several items the first time around.

Our deepest find was at 9 in . The strength of the reading confused us at first-it was too strong and over a fairly wide area. The "treasure" turned out to be an aerosol can for retouching cars, a beer can of similar size was found at 4 in with less trouble. The reading at 9 in . was strong and it would be fair to assume that if the can had been deeper it would still have been found.

We were very successful near the sea wall where people were sunning themselves but due to the numbers already there we could only try a few yards of this but it was here that we found our only coinwhich turned out to be a 1966 penny, badly corroded. We had expected to find more money and because of our failure to do so we arranged a test. One person buried coins of various sizes in a marked off area and we tried to locate them. These tests were successful and convinced us that we could unfailingly find all coins at depths up to four or five inches and larger coins at even more.
 s (ltems 1 and 26) but such ?nerally be more fruitful.


Money! Right against the sea wall we found our only coin-a 1966 penny, badly corroded.


The one that got awayl The tide came in so fast that before we had time to dig out the "find" the water put an end to it.


1 Cart fitting (?). Found on the old farm road at $2^{\prime \prime}$ down.
2 Boiler clinker (?). Gave strong reading: $1^{\prime \prime}$ down.
3 Sheet metal handfe, badty rusted. Found in author's garden at $2 \frac{1^{*}}{}{ }^{*}$.
4 Iron Hinge. Our first find, $3^{\prime \prime}$ under the sand.
5. Nail found under the beach, $\frac{4}{2}$ down.

6 Coppel gasket ring (?). Found under the beach at " 6 ".
7. Shrapnef Author's garden at 2,

8 Sharp metal spike. On the beach at $3^{\prime \prime}$.
9. Screw eye (from clothes Dine?) Author's garden, $2^{\prime \prime}$ down.
10 Small piece of torn metal. Beach at $3^{\prime \prime}$.
11. Copper tube (squashed). Author's garden, $2^{\prime \prime}$ down.
12 . Piece of unidentified fron. Beach at $1 \frac{1}{2}$.
13 File badiy rusted. Garden at $2 \frac{1}{2}$ "
14 Plant label (?). Zinc, garden at 4"
15 Shrapnel, Garden at $1^{\text {", }}$
16 Copper clip. Beach, fourid at $3 \%$
17 Shrapnel gun metal, beach at 4".
18 Screw-on bottletop, beach; 1"down.
19 Shrapnel. Author's garden at $3^{\prime \prime}$.
20 1966 penny. Beach at $3^{*}$.
21 Encrusted iron fitting. Under the beach at $1 \frac{1}{2}$ ".
22 Thin coppef tube (squashed). Beach at $2^{\prime \prime}$.
23 Copper tube "(squashed). Author's garden, at 2".
24 Piece of cast iron. Beach at $3^{\prime \prime}$
25 Nail with small piece of wood attached. Beach at $1^{\prime \prime}$.
26 . Cart fitting. Old farm koad at 4".
27 Galvanised washer. Author's garden at $3 \frac{1}{2}$. Looked just Jike a coin until cleaned up.
28 and 29 (not shown) Aerosol ean and beer can: At 9" and 4".

As we progressed experience enabled us to locate more accurately and our ears became more and more sensitive to changes in the note.

Just one word of caution. The beach will provide finds of all types but be careful near the water's edge. The spray landing on the search coil sent it haywire and searching became almost impossible. Later tests carried out in the light rain proved fruitless for the same reason. Not only does the impact of the spray or raindrop change the note but water trapped in the turns alters the inductance of the coil. As the water evaporates the pitch of the note changes-the effect lasts several minutes during which searching is impossible.
The second part of the test was made on the outskirts of a nearby castle. Not unreasonably the custodians would not let us search in the grounds but recommended trying outside, pointing the way to the original approach roads. A number of items were found, though none of any great age.
The final test was conducted in the author's garden in north-east London. Surprisingly most of the items were found at the same depth under the lawn. When a reading was obtained a circle of turf about 6in. in diameter was cut out, the item was found and the
earth replaced, laying the turf back in position; in this way no damage was done to lawn.

The house was built in 1913 and the lawn is probably original. The objects found were probably from the building process, spread out before turfing -though the file was probably lost by some workman long ago.
Some pieces of shrapnel were found. This is not really surprising for at the height of the London Blitz the fire from the anti-aircraft guns was so heavy that shrapnel apparently came down almost like "hail stones," according to a neighbour. Most of the shrapnel was cleared up but quite a lot would have buried itself in the ground.
A grass guard was developed from experience, this can be seen in the photographs. It is a piece of Perspex, $6 \times 6 \mathrm{in}$. fixed to the bottom of the search coil framework to stop blades of grass from touching the coil and so cause the beat note to change.

A total of four hours test searching was carried out to produce the finds shown. In that short period we became very much better at identifying signals and in the end knew exactly where to dig and even how deep we could expect to find the metal object.

## HOW TO BUILD THE P.W. TREASURE TRACER

The circuit of Treasure Tracer comprises three distinct sections: the search coil oscillator, the reference oscillator and the audio amplifier.
The search coil oscillator is made around L1 which is wound on a wooden framework shown in Fig. 1. This is made up from two 6in. lengths of hardwood batten with a section of $1 \times{ }_{4}$ in., though this section is not critical. These should be made into a cross by half-lapping as shown and small $\mathbf{V}$ shaped grooves cut into the ends. This framework must be rigid and if poor joints are made, these should be firmly glued.

The handle is made up from wood of the same cross section as the coil framework and about 4 ft .


Fig. 1 : The construction of the search coil wooden framework.
in length, though this will depend upon the height of the user. The base of this should be cut at $45^{\circ}$ and screwed firmly to the coil former. A normal type screw can be used; it will alter the inductance of the coil but as it is a constant it does not affect operation.

A small three way stand off tag strip should be mounted a few inches from the bottom to provide a firm anchorage for the coil wires. A thin enamelled copper wire should be used; the gauge is not too critical and 32 to 38 s.w.g. will do. If the wire has to be specially bought, 36 s.w.g. (as used in the prototype) would be a good choice. The start of the wire should be soldered to one of the outside terminal tags and 48 turns should be wound in the upper grooves, ending by fixing to the centre terminal tag.
The second part of L 1 is wound in the lower


The search coil. Note the terminal tag at the lop left and the taping of the wires.
grooves, again 48 turns, anchoring at the centre and other outer terminal. Both coils should be wound in the same direction and the centre terminal used only as a convenient centre tap which is needed for the circuit.

All windings should be tight, including the leadups to the terminal tag. Once completed the windings should be taped together at several points to hold them firmly.

It should be emphasised that the successful operation of the Treasure Tracer depends largely on the care taken in the construction of this search coil and loose windings will make operation very difficult and unreliable.

L1 is connected into the collector circuit of $\operatorname{Tr} 1$ as shown in the circuit diagram in Fig. 2. C2, shown as a 500 pF capacitor, is connected across the coil and this combination will resonate at about 130 kHz . The value of C2 and C4 (in the reference oscillator circuit) should be of the same type and reasonably close in value; miniature 5 per cent polystyrene types are very good here and inexpensive. It doesn't
matter too much what their values are as long as they are the same, but to stay within the regulation frequency band they should be over 390 pF .

The components in the search coil oscillator are connected to form a Hartley oscillator, working at the frequency mentioned. R1 provides the base bias for Tr 1 and Cl provides the feedback signal to maintain oscillation.

A low value resistor, $R 3$, is connected in the emitter and this is shared by $\operatorname{Tr} 2$ which forms the reference oscillator.

L2 is a standard Denco LW aerial coil which is fitted with the three windings necessary. The main one (between points 1 and 6) is tuned by C4. Another of the windings is arranged to feed back to the base forming a blocking oscillator; this also carries the base bias to $\operatorname{Tr} 2$.

The shared emitter resistor R3 means that there is a mixing action in $\operatorname{Tr} 2$ and a degree of the search coil oscillator signal is mixed with that of the reference oscillator to make the beat note.

It is necessary to tune one of the oscillators to

Fig. 2 : The complete circuit for the P.W. Treasure Tracer.

## components list

| Resistors |  |  |
| :--- | :--- | :--- |
| R1 | $330 \mathrm{k} \Omega$ | R5 |
| R2 | $4.7 \mathrm{k} \Omega$ | R6 |
| R3 | $22 \mathrm{k} \Omega$ |  |
| R4 | $27 \Omega$ | $R 7$ |
| R4 | $390 \mathrm{k} \Omega$ | All $120 \Omega$ |


| Capacitors |  |  |
| :---: | :---: | :---: |
| C1 47pF | C5 | 1000pF |
| C2 $500 \mathrm{pF} \dagger$ | C6 | $0.01 \mu \mathrm{~F}$ |
| C3 $0.1 \mu \mathrm{~F}$ | C7 | $100 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C4 500pFt | C8 | $100 \mu \mathrm{~F} 25 \mathrm{~V}$ |
| $\dagger$ see text |  |  |
| Semiconductors |  | - |
| Tr1 2N2926 | Tr3 | 2N2926 |
| Tr2 2N2926 | D1 | OA91 |
| Tr3 2N2926 |  |  |

## Miscellaneous

L1-see text and drawings
L2 Denco LW aerial coil, Type 1T
LS 75-80 miniature loudspeaker
JK1 3.5 mm jack socket with cut-out switch
SW1 On-Off slide switch
B1 PP3, 9V battery
Chassis $6 \frac{3}{8} \times 2 \frac{3}{4} \times 1 \frac{7}{9} \mathrm{in}$., (H. L. Smith Ltd. 287/9
Edgware Road, London W.2.) 60p inc. postage.
bring it close to that of the other and here the reference oscillator can be tuned over a wide range by altering the position of the ferrite dust core. The coil should be mounted as shown in Fig. 3 with a small knob fixed to the brass thread attached to the dust core.

The take-off point of the coil comes from the third winding of L2 (between pins 8 and 9). This is d.c. blocked by C5, detected by D1, smoothed by C6 and applied to the base of $\operatorname{Tr} 3$.

The signal here will be the beat note or an audio
 frequency represented by the difference in frequency of the two signals.

The base bias for $\operatorname{Tr} 3$ is provided by R 5 with $\mathbf{R} 6$ acting as the collector load.
Tr4 further amplifies this audio signal and applies it to the $80 \Omega$ loudspeaker in the collector. R7 and C7 are included to raise the emitter voltage of $\operatorname{Tr} 4$ and to limit the quiescent current. The impedance of the


Fig. 3 : The p/n numbering and mounting of $L 2$.
loudspeaker can lie between $35 \Omega$ and $80 \Omega$ and various miniature types with impedances in this range are available. If difficulty is experienced in obtaining one of these, the loudspeaker can be replaced by a transistor output transformer (such as the Eagle LT 700) feeding a lower impedance loudspeaker.

There is a tendency for the two r.f. signals to lock together if they are within a few Hertz of each other. This is not too serious bat the inclusion of R2, which drops the supply to Trl, reduces this tendency. Theoretically the junction of R1 and R2 should be decoupled to the negative line using a $0 \cdot 1 \mu \mathrm{~F}$ capacitor; this however made no difference in the prototype but may be included if $\operatorname{Tr} 1$ fails to oscillate.
Note that the chassis is connected to the positive rail rather than the more conventional negative line. This enables simple fitting of the jack socket, JK1, one connection of which has to touch the chassis.

## CONSTRUCTION

The majority of the components are mounted on a small piece of $0 \cdot 15 \mathrm{in}$. matrix Veroboard, 16 holes by 13 holes and this is shown in Fig. 4.
The chassis used in the prototype, and highly recommended, is available from H. L. Smith Ltd. (see components list) and the bottom of this is drilled as shown in Fig. 5. The three holes in a triangle are fitted with lin., 4BA screws and the component board is mounted on these, spaced off by means of nuts.
The loudspeaker can be glued in place and the wiring between the Veroboard and the other components is shown in Fig. 6.

The recommended chassis comes with a lipped lid which is screwed to the wooden handle as shown in Fig. 7. A hole ${ }^{1}{ }^{1} \mathrm{in}$. in diameter is fitted with a rubber grommet to take the wires leading to the search coil L1. Stiff wire should be used to run between the chassis and the terminal tag and this should be firmly taped to the handie as shown in the photographs. A small loop is left before entering the chassis to enable it to be opened.


An internal view of the completed prototype.


Fig. 4 The component layout on Veroboard.


Fig. 5: The drilling of the bottom of the chassis.


Fig. 6 : The wiring between the component board and the other components.


## TESTING

Once all wiring is done a visual check should be made to ensure all is well and this being so, the Treasure Tracer can be switched on.

If all is correct the tuning of L2 will produce two positions where a strong beat note can be heard.

A number of weak signals may be heard at other settings. These are probably caused by radio signals on those frequencies but they are very low compared to the main signals.

The beat note should be set at the lowest stable audio note-probably between 50 Hz and 200 Hz . When a metal object is brought near L1 the note will either go up or down, depending on whether the search coil oscillator is working higher or lower than the reference oscillator.

By experience it was found that is was better to arrange for the note to go down in frequency when a metal object was approached but this is up to the user-a rising note may be preferred.

Certain objects-especially brass-go against the general trend and operate in reverse-causing the note to rise when iron and aluminium cause it to fall.

No volume control is fitted as the output from the loudspeaker is fairly low-about 75 mW , though this proved sufficient and was not found too low even by the sea shore. Headphones or earpieces with impedances between $50 \Omega$ and $4000 \Omega$ all work when plugged into the socket-this automatically cuts the loudspeaker out if wired as shown.

The current consumption is not too high-it should certainly be under 20 mA and several hours of searching are possible using the PP3 battery specified.

Before carrying out your first search, eliminate as much movement of the leadup wires as possible by taping them, as even a mild breeze will cause a change in note otherwise.

In testing it will be found that nearly all large objects cause some change in frequency-even laying the coil on the ground- but these changes will be minute compared to that caused by even a small piece of metal.

Do not expect to become an expert in a few minutes. The use of a device of this type needs a degree of skill and it took all of us several hours before we became reasonable at it. Now, after the test, we have used the detector to find a whole mass of new material, including more coins, but this was outside the testing period and the finds were not witnessed so we are not including later items in the list.

Well, where do you search? Note that there are very heavy penalties for $u$ sing such a device in areas scheduled as being of historical interest and there have been prosecutions for this. However there is no need to search in such places and paths or

[^4]roads that have been in use for centuries are a good place to start; river banks will also prove fruitful.

An excellent small book "A Fortune Under Your Feet" by E. Fletcher elaborates on this and is recommended reading for those encouraged by early results.

If you find something of interest, let us know. We are offering $\mathbf{f} 2$ for the most interesting letter we receive dealing with objects found. It doesn't have to be valuable, just as long as it is interesting.

## I.C. of the Month-continued from page 310

two heatsink tabs. If the i.c.'s are to be used to their full 5 watt rating some form of additional heatsinking is needed. This may take the form of directly soldering about two square inches of copper to each tab or alternatively to equivalent area of printed circuit board foil. At any rate, in most applications the full output ratings will not be approached so that the above precautions are necessary only for worst case operating conditions.


View of I.C. showing unusual heatsink tabs and staggered leads.
To find out the maximum output currents that the units can deliver all one has to do is to determine the product of the voltage drop across terminals 2 and 7 of the i.c. and the current drawn, making sure that the answer does not exceed 5 watts.

"He says never mind the beads-have you got any back numbers of Practical Wireless ?"

## SERVISG 

## H. W. HELLYER

## PART 4

## NOW THAT GORDON KING HAS COVERED THE BASICS OF FAULT-FINDING CO-AUTHOR 'MAC' HELLYER DISCUSSES THE PROBLEMS OF RECEIVER ALIGNMENT WITH PARTICULAR REFERENCE TO THE TEST EQUIPMENT NEEDED FOR THIS TASK.

ENOUGH has been said by Gordon King in the earlier parts of this series to absolve me from a tedious description of the make-up of superhet circuitry. In this section, we shall now be able to concentrate wholly upon alignment of the a.m. and the f.m. receiver.

A little theory must creep in since the most practical of readers should still be blessed with some natural curiosity. We need to know why we are twiddling that screw, that slug, that bit of wire, and not just be content to follow a mechanical sequence of instructions.

Servicing consists very largely of using one's native wit to interpret or augment the information given by manufacturers. In many cases, handling a piece of equipment that may be obsolete or, even if new, backed by the most meagre data, one has to fall back on one's knowledge of basic principles and experience of designers' whims to solve some very tricky problems.

Our intention here is to provide a few short-cuts toward those neat solutions. So general principles have to be the order of the day. There will always be exceptions in design, so long as there are exceptions in men. Bravo! say I-there is no more hideous prospect than the "People's Set", which can be
serviced by numbers, or, more likely if the doubleentry cost-watchers have their way, thrown away when it goes wrong! We all saw what could happen, on page 1030 of the April issue of PW. ("The Committee Supet-FET".)

## AM ALIGNMENT

Gordon King has said, already, that a.m. receivers are still stuck with capacitive tuning, although the f.m. receiver, and, particularly, the combination a.m./f.m. set, may have tuning gangs plus variable inductors plus potentiometer plus fixed tuning all wrapped up in one package.
If alignment has to be carried out, begin by sorting out the a.m. section, identifying the stages (see Part 2) and then making up your mind what kind of circuit you are about to tackle. This is assuming that you are not able to get the manufacturer's detailed information, always supposing he has got around to preparing it for publication!

The tuning I have spoken about is the 'front-end' tuning, where the frequency of an oscillator beats with that of the incoming signal to provide a steady intermediate frequency, the i.f. So, before we can tackle the front end, we must make sure the several


Fig. 1: The skeleton circuit of the tuned sectlon of typical a.m. receiver. The fixed tuned Transfilter, now becoming quite common, helps to reduce the amount of re-alignment required.
parts of the i.f. circuitry are doing their job. But before we can do this, it is necessary to check the audio section and the detector.
Let me refresh your memory with Fig. 1. Here we have a skeleton circuit of an a.m. receiver, showing the tuned circuits with which we are concerned here, the detector and a hint of the audio section that will follow. It is obvious that a signal injected at a post-detector stage must be at audio frequencies. In the old days, it was easy enough. A finger tapped on the appropriate valve grid, or on the 'hot' end of the volume control would produce a healthy 'buzz'. Mains pickup and the high impedance of the input circuits made this possible. With a battery-operated piece of equipment or the low-impedance circuitry of semiconductor devices, the 'disturbance test' type of operation is not so effective. It can, in fact, be positively dangerous.

## SIGNAL INJECTION

The answer is to inject a signal of known characteristic (even if unknown precise amplitude), simply to verify that the following stages are working. We are not interested so much, at this point, in their exact efficiency, their lack of distortion, their overall output. For the following tests we need some method of indicating variations of output, either at the final part of the receiver-the feed to the loud-speakers-or at some earlier audio stage, where the readings may be more convenient.
It must be stressed again that when signal injection methods are employed, we are not expected to measure the output accurately. As Gordon King has explained, the quality of one piece of test equipment is determined by (a) the standards to which one must test the circuit, (b) the quality of associated gear and (c) the standard of testing we wish to apply.
Signal injectors are the easiest of all test instruments to make and apply, and there have been numerous suggested circuits in PW. We shall sktp lightly past the subject, pausing only to remark that if you are thinking of alignment, it can be argued that you will be using a signal generator. There are very few of these that do not incorporate an audio output facility. There is your post-detector tester, ready made.

The 400 Hz or 1 kHz note we hear from the loudspeaker is suitable for rough tests and basic alignment in an emergency. It is certainly no more than a guide for precise circuit adjustment of the modern set. Visual alignment checking is needed so a meter, or some other visual indicating device, will have to be used. So this is where the ordinary multimeter can be pressed into service.

With valved equipment, nothing is easier than a low a.c. voltage-reading meter (say from $0-5 \mathrm{~V}$ a.c.) across the loudspeaker or a dummy load. The dummy load, it should be said, has not been outdated by transformerless output transistorised receivers. For test and measurement purposes, the output circuit should always be correctly loaded.

Figs. 2(a) and (b) show alternative ways of indicating audio output, for both valved and transistorised equipment. We include these notes on valved equipment simply because the accent here is on servicing and it is in the nature of things that servicing will be required more often on older equipment. Measurement of anode current in an output


Fig. 2: Measuring output, (a) across dummy load or shunting speaker, (b) across speaker of transformerless stage, (c) current indication in series with anode load, (d) in series with cathode or voltage across bias resistor.
stage of valved equipment, either in the anode or cathode lead, is an alternative, where a low voltage d.c. meter, or a $0-100 \mathrm{~mA}$ d.c. meter is available, Fig. 2(c) (d).

## MEASURING OUTPUT

Breaking into the output stages of a transistorised amplifier for such alternative readings is neither easy nor desirable. Because of the low impedances of emitter circuits, voltage variations are too small to be of any great value, and should, in any case, be stabilised.
But let's do things properly. Let us consider the output power that we should get, and make arrangements to measure that. There are two things to consider here: audio power measurement and indication of standard audio output. They are not the same. As Gordon King will be showing later in greater detail, measurement of audio power is not a simple process, and interpretation of results must be made with great care.
Briefly, the expected outputs from general apparatus would be: (a) small transistorised radios, 500 mW to 1 watt (b) larger radios, 1 watt to 3 watts (c) tape recorders and record players, $2-6$ watts (d) small amplifiers, up to 10 W (e) larger amplifiers, 10 watts upwards.
Standard outputs are related to the sensitivity of the apparatus. For example, a radio may be quoted as having a sensitivity of $25 \mu \mathrm{~V}$ for m.w. reception, $40 \mu \mathrm{~V}$ for l.w. reception and $1 \mu \mathrm{~V}$ for both s.w. and v.h.f. reception. Alone, these figures mean nothing. They must be related to the standard audio output and to other factors such as signal-to-noise ratio. In the case of these quoted figures, the audio output
would be 50 mW for a $\mathrm{s} / \mathrm{n}$ ratio of 6 dB , relative to the 0 dB figure of $1 \mu \mathrm{~V}$.
This gives us a clue to the statement 'decibels below 1 volt' which may sometimes be used. 'Decibels below 1 milliwatt' is another alternative and 'field strength' yet another. The last term is employed to assess sensitivity when loop or ferrite rod aerials are used.
For now, we do not need to worry too much about all this. Practical service work very often consists of bringing up to scratch the circuits that may be only a little out of alignment. If components in tuned circuits have been replaced or if maladjustment has occurred, then the procedure is to check the alignment throughout and to make the small alterations found to be needed.

## VISUAL DISPLAY

The oscilloscope is invaluable here, saving hours of careful tabulation and giving both the facility of viewing the result of the input signal and of measuring it. A secondary facility, often overlooked, but quite important, is the ability we have, when viewing a trace, of determining how much output is signal and how much noise and distortion-common causes of faulty results when only a meter is used.

We shall later look more closely at this matter of noise and distortion assessment. For now, a brief note on the practical alignment of a typical receiver, using a standard signal generator and a measuring device, augmented by an oscilloscope. Response curves are the usual method of measurement and, very often, a manufacturer will give no more than the

(a)

(c)

(b)

(d)
expected curves in his service manual, referenced to some level and bandwidth. It is as well to be clear at this point, therefore, what we mean by response curves, reference levels and bandwidth.

Fig. 3 shows a selection of the graphs one would produce by plotting the output from the receiver (vertical axis) against the frequency at which the signal was applied (horizontal axis). It is possible to produce these curves from careful and detailed measurements but it is much simpler to feed to the receiver a signal which varies regularly across the bandwidth, locking this to the timebase of the oscilloscope and displaying the output from the detector of the receiver. Such an input signal is obtained from a sweep generator, or 'wobbulator' (see page 1038 PW April 1971):

The response characteristic of a superhet receiver is mainly that of its i.f. circuits, for the r.f. circuits are not so sharply tuned. Quite often, response testing and alignment concentrates on the i.f. circuits, leaving the r.f. section of the receiver to be aligned on one or two spot frequencies and checking the padding and trimming of the oscillator.
The acceptance band of a receiver has to take in the sidebands of the transmission for full handling of the higher frequency components of the modulation, but if it extends too far beyond this, the signal-tonoise ratio will suffer. A perfect response character-istic-an impossible one-is shown in Fig. 3 (a). All the frequencies within the passband are received with the same sensitivity; those outside the passband having no effect. In practice, the response curve may be more as (b), where the 'usable' bandwidth is that between the -3 dB points. This is where output power falls by 3 dB or half its maximum value.

Note, however, that the response curve may be neither as flat as (a), nor as gently peaked as (b). In fact, it may be double-humped, as in (d). One important point here is that the reference point, relative to the -3 dB level, is the centre frequency of the passband, and not the peak of the humps.
Merely to state the frequency limits at which a curve is 3 dB down is not enough. This tells us what the gain of the receiver is, but not the extent of the rejection of unwanted frequencies. Always plot beyond the -3 dB points, as shown in the accompanying curves.

Making response measurements of the a.m. receiver with a low audio frequency modulating signal (example: $30 \%$ modulation at 400 Hz ), we feed the signal generator to the mixer input, as shown in Fig. 4. It is essential that the impedance from which the signal is derived is as low as possible. In the mixer input, the tuned circuits will not be at the intermediate frequency, so the low impedance is needed. Hence the two resistors, Ra and Rb, where

Fig. 3: (above) Response curves, carrier frequency $f$ with $+f$ and $-f$ representing bandwidth limits. (a) ldeal curve, (b) peaked response, with bandwidth indicated at $-3 d B$ (c) flat tuning to give desired response, same peak level and bandwidth as (b) but quite different response. (d) double-hump tuning as approach to flat top response of (a)


Fig. 4. (right) Instrument set-up for measuring i.f. response. Note attenuator resistors $R a$ and $R b$, and isolating capacitor C1.
a reduction of the generator output impedance from the usual 50 or 75 ohms to as little as 10 ohms can be effected. The values are easily worked out: for a generator of 50 ohms output, to present a 10 ohm (very nearly) load to the mixer input, we need to make Ra around 40 ohms (nearest preferred value 39 ohms) and Rb 10 ohms. The choice of values gives a $10: 1$ voltage ratio also, just in case you want to work out sensitivity figures.

The value of Cl should be such as to make its reactance at the test frequencies no greater than 50 ohms. At an i.f. of $470 \mathrm{kHz}, \mathrm{Cl}$ would thus be around $0.01 \mu \mathrm{~F}$. Its inclusion is to prevent the d.c. bias conditions being upset.

Disabling the a.g.c. is the next consideration although the method of disconnecting the a.g.c. line and putting a fixed bias in its place may not be so simple with modern sets. Sometimes the manufacturer will indicate a method of killing the a.g.c. action. The need to do so is evident from an understanding of a.g.c. action, which has already been described.

If we feed to a receiver aerial input a signal varying between say a microvolt and a volt, we may find that at around $5-10 \mu \mathrm{~V}$ input, a $2: 1$ increase-in input produces very nearly a $2: 1$ increase in output. But after about $100 \mu \mathrm{~V}$ input, the curve relating output to input flattens drastically, and it needs a good deal more 'in' to produce just a little more 'out'. The a.g.c. curve, in other words has a definite 'threshold value' with two fairly linear slopes, above and below that threshold. In fact, a.g.c. "quality" is often defined in terms of the mean slope of the curve above the threshold.

Assuming first that the a.g.c. is prevented from working, our tests would comprise first setting the generator to the reference frequency, with its output adjusted so that at full receiver gain the rated full output is obtained. The generator output is then attenuated to produce the 'standard' output, 50 mW . The receiver's gain control can be used to set the output indicator to a convenient value and then left strictly alone.

The generator is swung over the required frequency band and output plotted relative to the reference. The bandwidth is the frequency difference between the 3dB 'down' points.

If the a.g.c. cannot be 'killed', there are alternative ways of going about the checking. We can tackle the problem 'backwards', measuring for a constant output for a 3 dB increase of input, with the attenuator of the signal generator set to increase the test input by 3 dB , then the two limiting frequencies where the


Close-up of amif.m. tuner showing part of a.m. ferrite rod aerial at left and drive cord and pointer.
monitor reading is returned to the reference level define the bandwidth.

Another way of testing bandwidth without having to 'kill' the a.g.c. is to keep the carrier frequency of the generator constant and to vary the bandwidth. This cannot be done with the normal signal generator, as modulation frequency and depth are often fixed. But where a c.w. only output is obtainable and a separate audio generator is available to apply a varying input, then the r.f. generator can be set up to the central frequency and the modulation varied in frequency, without any change in depth, and a note made of the points at which the output reading (across the detector load, for utmost accuracy) is 0.707 of the reference level. These limits are the bandwidth, i.e., bandwidth is twice modulation frequency.

## CW TESTS

It is not so easy to align higher quality receivers. The sides of the response curve can appear deceptively steep, because of the relative phase shift of the sidebands. The way to overcome this possibility of error is to use a c.w. (unmodulated) input and to read off the d.c. voltage at the detector.

One snag: there may be some standing d.c. voltage. It can be allowed for and carefully taken into


Before attempting alignment it is essential that drums, cords, springs and attachments are in order. Always check traverse of pointer before making adjusiments.
account by subtracting it from final readings. The use of a d.c. valve voltmeter or similar instrument allows us to back off the settings to obtain a new zero.

Working on s.s.b. receivers can be a good deal easier. Better-class communications receivers work also in the single-sideband mode and these can be aligned by using the beat between the input signal and the internally generated carrier, with a.g.c. switched off-which is usually possible with these sets.

## PRACTICAL POINTS

Procedures must differ between makes and models. Some general rules follow:-
(1) Allow sufficient warming up time before making tests. On valved equipment, fifteen minutes for both receiver and test gear should be regarded as the minimum. Despite all the advertising, transistorised equipment does not 'warm up' to operating conditions 'in the twinkling of an eye'. One very famous hi-fi amplifier I recently tested took seven-and-a-half minutes for the current in the output stages to settle to a steady reading, and that is not exceptional.
(2) Check mechanical points. Dials and cursors, pointers and drums should be run from end to end of their travel and limits noted. Where datum points are provided by makers, these should also be checked before alignment commences. In general, maximum frequency (minimum wavelength) should be indicated when the capacitor plates of the usual ganged capacitor are fully unmeshed.
(3) Make any necessary adjustments to counteract backlash, so that a setting of the cursor or pointer accurately reflects the setting of the tuned circuits.
(4) Check before operations that the required trimming tools that are available. It is simply asking for trouble to use worn grub-screw drivers where hexagon-holed slugs are used, or when core slots are only suitable for miniature plastic tools. Some time ago $P W$ presented a set of plastic trimming tools to readers. Mine are still in use, augmented from time to time by filed plastic knitting needles and crochet hooks.
(5) Cores of inductors, despite all our efforts and care, may jam. The only recourse then is to drill or chip them out, taking great care not to damage the former wall or the iriductor. Resetting of new cores may need either a rubber band inserted in the core or the use of a non-hardening adhesive. There are core-locking compounds that provide an adequate fixing but still allow some adjustment.
(6) Finally-before starting, make sure that test gear is isolated and that there are no false return loops. Connect the neutral side of a.c./d.c. equipment to chassis if you have no isolating transformer and provide capacitive isolation, as previously described.

## GENERAL PROCEDURES

Consider a combination a.m./f.m. receiver, as shown in skeleton form in Fig. 5. Crystal filters are used widely and we can expect to find this trend growing. No alignment is normally required except
for the last stage, which will be peaked up to the intermediate frequency. A little care is needed here and some 'swing' about the nominal frequency may be necessary. A good idea is to peak the last i.f. to the input from a weak signal after the rest of the alignment has been done, bringing it into tune only temporarily at first.

Where tuned circuits are used throughout, inject a signal at the frequency changer that will produce a 50 mW output. across the appropriate load. As power in watts is the voltage squared divided by the resistance, we can work out the required reading. (For 3 ohms this will be 0.387 V , for 8 ohms, 0.633 volts and so on.)

A meter that has a full-scale deflection of around 2.5 V a.c. is required. Exact readings are not important at this stage as our aim is to maintain the output at the same level while bringing the circuits into tune, turning down the input as the gain increases. For this, the volume control will be turned to maximum, and if there are tone controls fitted, the treble control will be adjusted for the least top-cut.

Tuned circuits should be adjusted for peak output, starting at the rearmost and working toward the mixer. After initial peaking, go back over these adjustments. With some sets, there may be a tendency for one tuned circuit to 'pull' another, and readjustment should be made until no further improvement can be gained.

Where the response curve is humped, two peaks will be found as the signal generator is swung over the passband. In this case, the middle position should be used. Tune for the slight dip between the peaks.

## IF REJECTION

Before readjusting the signal generator, remove it from the mixer input and apply the signal, still at intermediate frequency, to the aerial input, then tune any i.f. rejection circuit to give the minimum output. It is always wise to make this test early on, then rechecking after mixer alignment. For this test, increase the i.f. output from the generator and switch the receiver to the medium-wave band (where breakthrough could be bothersome), turning the tuning gang till the vanes are fully meshed, i.e. the low frequency end of the band.

Another rejection circuit that will be found nowadays is the 19 kHz pilot tone filter. This is also tuned for minimum output with a strong 19 kHz tone injected.

Alignment of the broadcast band is conveniently done at this point. Set the generator to around $600 \mathrm{kHz}(500 \mathrm{~m})$ and the pointer of the set to the same


Fig. 5. Block diagram of combined a.m.l f.m. receiver, wilh switching omitted, as a guide to following the alignment procedures described in the text.
frequency, after checking that it traverses the scale correctly, and reaches any datum points marked by the manufacturer with the correct scale indication.

Adjust the padder and/or the oscillator coil (if this is adjustable) and obtain maximum output. Then readjust to the other end of the band, setting the trimmer. Best procedure is to carry out these operations for the mixer first, then peak up the aerial circuits and return to the mixer for readjustment, then again to the aerial to make sure the circuits remain in tune. Adjustments of this nature take time and demand patience. Maybe this is why realignment of receivers can be a costly job! It is never good enough to make a perfunctory gesture of 'twiddling the cores'. The long wave adjustments can then be done.


Fig. 6 Instrument set-up for checking i.f. response of fim. receiver,
Do not attempt them in reverse order, as settings of the medium wave tuning can affect the long wave band. Similarly, where there are several short wave bands, first adjust the highest frequency band.

Long wave adjustment often consists of adjustment of one trimmer in the mixer circuits and one in the aerial circuits. There is rarely any need to check tracking over the band as carefully as one would with medium wave tuning, there being few stations available.

Short wave adjustment often requires slight movement of coil turns and care has to be taken with the dressing of leads. Tuning is considerably simplified by the omission of padders in the short-wave section of most receivers. Instead, we find coil adjustments, or core settings being made at the low frequency end of each band and trimming used at the high frequency end.

## FM ALIGNMENT

Most adjustments to f.m. tuned circuits are carried out nowadays with the aid of a wobbulator and oscilloscope. Here, we find the output displayed, the signal swept over the response band and variable capacitors and coil cores adjusted to obtain the correct response curve. Addition of an a.m. marker generator aids the set-up, and the inter-connection of these instruments is shown in Fig. 6.

Because the average serviceman is unlikely to possess a wobbulator, we shall concentrate here on the adjustment of f.m. circuits using only an ordinary signal generator and a high-resistance meter. A more tedious job, but practically as efficient.

First requirement is a d.c. voltmeter, capable of reading around 10 volts, with a $20,000 \mathrm{ohms} /$ volt sensitivity at least. This is connected across the d.c. load of the ratio detector, the aim here being to keep the reading to a set level, determined by circuit characteristics, by turning down the generator input as the circuits are brought into line.

With the generator tuned to the f.m. intermediate frequency $(10.7 \mathrm{MHz})$, and with the modulation switched off, the signal is injected at the mixer and

the i.f. circuits aligned for maximum output. The correct procedure, again, is to start at the rearmost and work forward, but even more care is needed and constant rechecking is necessary.

If a ratio detector is used, the next step is to note the output reading from this 'peaked-up' process, transfer the meter to the a.f. output capacitor and note that the reading is now exactly one-half of what it was before. The ratio detector winding is adjusted to achieve this.

After this, repeat the steps until no further improvement can be gained. It is important to ensure that later steps do not impair earlier results; hence this need for repeated operations.

The ratio detector is finally balanced. The coil that gave its 'half-volts' reading earlier is now readjusted for a minimum reading. The mean of these two is calculated: i.e., halfway between the maximum and minimum voltages that can be obtained by adjusting the coil of the ratio detector. This is the setting for correct alignment.

## END OF PART FOUR

NEXT MONTH 'MAC' HELLYER WILL DISCUSS HOW FM STEREO SIGNALS ARE GENERATED AND TRANSMITTED. THEN FOLLOWS DETAILS OF TYPICAL STEREO DECODERS AND THEIR ALIGNMENT.

# Marconi sets the running with a multi-million pound contract for Skynet II. 

by John Chapman

THE first communications satellite system to be designed and built in Europe will be a British venture. Marconi Space and Defence Systems, a member of the GEC-Marconi Electronics group, has won a multi-million pound Ministry of Defence contract to design and build two satellites to gradually take over the expanding military communications traffic currently being carried by "Skynet I," a satellite built by the Americans for exclusive use by the British Armed Forces.
Skynet II will be more powerful than the existing satellite and will be one of the most advanced satellites in orbit in the world.
The first of the new satellites will be launched into a near synchronous orbit over the Indian Ocean in the first half of 1973. By this time the American built Skynet I will be approaching the end of its design life: the second of the new satellites will be used as a standby and launched later in 1973.
The GEC-Marconi group has already played a major role in the provision of ground stations for the Skynet system. Four 21 -foot diameter dish transportable stations have been supplied by Marconi Space and Defence Systems at Stanmore and this part of the company is at an advanced stage in the development of a $3^{1}{ }_{2}$-foot diameter aerial terminal (called SCOT) which can be mounted on a ship to provide the Royal Navy with further links into the Skynet system. Marconi Communications Systems, based at Chelmsford, built the first three earth terminals back in 1966. Two of these 40 -foot diameter ground staions which were used with the satellite system built for the U.S. Government and used successfully by the American Armed Forces have now been modified to form part of the Skynet system.

Outlining the activities of Marconi Space and Defence Systems at Portsmouth, the company's manager Mr. M. Lovell said that their experience in spacecraft electronics has been developed over a period of about seven years in which time they have provided the satellite electronics for every British spacecraft programme to date.

The first of these was Aerial 3 (later called UK3), a satellite launched in May 1967 as part of a scientific programme. Although this satellite had a design life of a year, it was not switched off until 1968 and furthermore, the system was reactivated last September in order to check on the long-term reliability of the electronics equipment in a space environment.

The next important project was the X3 satellite which will be the first technological satellite to be launched in a Black Arrow launch vehicle. In this project Marconi engineers are responsible not only for the onboard electronics but also for satellite assembly, system test and the preparation of the

spacecraft for launch. By contrast with the earlier satellite, X3 features modular electronics systems built to conform with ESRO standards which are suitable for use in a wider range of satellites.
Marconi has also been heavily involved in the UK4 and UK5 satellites. The later satellite is packed with electronic equipment and offers two important advances to the experimenters taking part in the joint NASA/Science Research Council project. Firstly it will be possible to adjust the direction of the spin axis of the spacecraft using a propane attitude control system so that experimenters can scan space for objects of potential interest and then point a second set of experiments along the spin axis at selected sources. Secondly, through the use of the spacecraft's magnetic core stores, it will be possible to collect data around an orbit and to replay this upon command in a format most convenient for the experimenters.

## CONSTRUCTION

The Skynet II satellite is to be built in the form of a cylindrical drum, with solar cells covering the entire curved surface to provide the power for all of the electronics. It will measure approximately 78 inches long with a diameter of 75 inches. Laun' ${ }^{3}$ weight will be about 960 pounds.

An apogee motor contained in the satellite itself, and mounted along the major axis of the cylinder, will be used to transfer Skynet II into its synchronous orbit. It will be spin-stabilised at about 90 revolutions per minute from the time the second stage burning ceases and once placed in synchronous orbit by the solid fuel apogee motor, the communications antenna will be de-spun and controlled to point continuously at the earth.
Attitude control will be achieved by means of hydrazine jets which will be used to adjust the attitude of the satellite, both before the apogee
motor burn, and subsequently for the life of the satellite after it has achieved the required synchronous orbit. Control movements will be provided by a single pair of jets located at the edge of the satellite and thrusting parallel to the axis of the satellite, with another pair of jets mounted in the curved surface of the satellite, and pointing radially out from the centre. These jets when fired will be pulsed to synchronise with the rotation of the satellite so as not to upset the high rate of spin which will eliminate any tendency of the satellite to rock, or even tumble and so interupt communications traffic.
During the initial manoeuvres and the final positioning, control communications will be carried out through an omnidirectional aerial system consisting of an array of cavity-back dipoles operating at S-band. This array is mounted in a single band round the complete circumference of the satellite. Once synchronous orbit has been attained and the satellite has been turned into the correct position with respect to earth, a single horn aerial mounted on the major axis of the satellite-at the opposite end to the rocket motor-will be brought into use to provide the main communications function of the satellite. This aerial whose beam-width is just sufficient to cover the entire visible portion of the earth's surface will be mechanically de-spun and aimed directly towards the centre of the earth.
Much of the technical detail of the electronic packages onboard Skynet II is, of course, classified. Presumably the transmitter/receiver operates in the GHz band using sophisticated multiplexing techniques to cope with the wide variety of traffic it will be called to handle. Also it will have to cope with a variety of powers, since the ground stations with which it will have to work range from tiny ship and shore-based portables with $3 \cdot 5$-foot diameter dish shaped aerials to the large 40 -foot units having outputs measured in kW.

## TECHNOLOGY SATELLITE

Much more information is available on the technology satellite X3 which is in the final stages of preparation for launching shortly. The satellite has been checked in the solar chamber at RAE Farnborough and at the time of writing it is being checked for magnetic inter-reaction at the ESRO European Space Technology Centre in Holland prior to installation on to a Black Arrow launcher.

The Black Arrow ' X ' series of technology satellites is aimed at improving British technology in spacecraft and launch vehicles. All of the satellite systems are designed with future requirements in mind and some of the operational data equipment is duplicated in new experimental form to be proved in space.

Marconi has designed and built the power conditioning system, the telemetry transmitters, telecommand receivers and decoders and the data conditioning systems for the satellite to the relevant NASA and ESRO standards.

Although the power requirements of X 3 is only 10 watts, the power conditioning system has been designed for future spacecraft in the series and is rated to supply up to 30 watts continuously, both in sunlight and eclipse conditions. A 6 ampere-hour nickel-cadmium battery charged by the solar cell array supports the equipment during eclipse periods.

Owing to the limitations of the pulse frequency modulation data system used on previous satellites, channel capacity has been increased through the


This picture shows the assembly of a welded circuit for an r.f. module. (Skynet II).
adoption of a modular pulse code modulation data system. Besides meeting the immediate requirements of the X3 satellite, the system could be expanded easily to cope with more complex data systems of future spacecraft.

The new data handling system uses a small number of standardised logic elements, such as shift registers and multipliers, packaged in all-welded "modules" assembled to form a complete telemetry system. Essential modules are duplicated to enhance system reliability.

The telemetry, tracking and command system makes use of an r.f. package comprising 6 sub-units based on common piece parts. Again the telemetry transmitter is duplicated to increase reliability. Two receivers are used and connected in polarization diversity configuration to minimise the effects of spin modulation of the r.f. signal-induced by the rotation of the satellite.
A completely new command decoder has been developed for X3. This operates on the NASA ToneDigital Command Standards and provides a capacity of up to 70 commands per decoder address. Two of these are fitted to the satellite. For a transmitted command to have any effect on the satellite, the r.f. carrier frequency, the tone frequency, the relative timing and lengths of the tone bursts, and the number of bits per word must all be correct and the decoder must also recognise its allocated address followed by a valid execute code within a defined time period. Reasonably secure!

## TOTAL CAPABILITY

Now that a British company has won its spurs in the space race, Marconi is in an ideal position to open up satellite communications for commercial applications. Already there are suggestions that countries like Canada and several in Africa where the population is spread over wide areas could make use of communications satellites feeding small ground stations such as the SCOT terminal being built for the British Armed Forces.

By the end of the decade radio and television direct from 'stationary' satellites could become a reality. The technology is here already-it seems to be more a matter of getting the economics right.

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# THE BROADCAST BANDS Malcolm Connah 

## Frequencies in kHz - Times in GMT

## NEWS FOR

## DX LISTENERS

THE onset of fine, summery weather has caused the usual drop in the number of reports as DXer's leave their shacks for the great outdoors. Among the stalwarts who remained in their shacks was John Trewick of London Colney who used his Lafayette HE-40 and vertical whip to hear the following:-
9525 RSA, South Africa in English at 2020.
11820 BBC, Ascension, 'The Music Scene' at 2015.
15018 Hanoi, Vietnam with 'Letterbox' at 2000.
15170 ELWA, Liberia in French at 2030.
15185 Helsinki, Finland in English at 1800.
15195 Ankara, Turkey in German at 2100.
15265 Kabul, Afghanistan in English at 1800.
17730 Havana, Cuba with news in English at 2010.
21535 NHK, Japan with 'DX Corner' at 0800.
21535 RSA, South Africa with Folk Songs at 1120.
Howard Stephenson of Newcastle-upon-Tyne has used his Eddystone EC10, Mk. II receiver and Joystick antenna to hear some interesting stations includ-ing:-
3260 R. Niamey, Niger, African music at 2015.
3905 All India Radio in English at 2245.
3915 BBC, Tebrau, Malaysia relay at 2215-
4680 HCWE1, R. Nac. Espejo, Ecuador with LatinAmerican music at 0545.
4680 HCWE1, R. Nac. Espejo, Ecuador with Latin15395 VOA, Tinang, Philippines at 2200.

Ray Warren of Bury St. Edmunds has used his Astrad Auriga receiver and a Koyo 1661 receiver to hear the following:-
6195 Tunis, Tunisia in French at 0840.
6540 Pyongyang, N. Korea in English, 1900.
9489 Radio Tirana, Albania, English, 1830.
9570 R. Nacional, Spain in Spanish at 1540.
15180 Radio Australia, pop music at 0800.
15460 Radio Kuwait, news in English at 1830.
R. J. Downes of Bournemouth does not mention what equipment he uses but he heard:-
6010 R.T. Belgium in Dutch at 1430.
11710 RAE, Argentina in English from 2300 to 2400.
11965 Trans Europe Radio in English, 1345.
15160 Ankara, Turkey in English from 2200.
15185 Nigeria B.C. noted in English at 0715.
Derek J. Hart of Lancaster sent in the following list of stations which he has heard recently:-
6080 Radio Berlin International at 2037.
9505 Radio Tirana, Albania news at 2035.
9625 Israel B.C., news at 2056.
9915 All India Radio, news at 2056.
11672 Radio Pakistan, news at 2045.
15125 Radio Australia to Pacific at 0830.
Nigel Williams of Caewern, Neath, Glamorgan, has a Lafayette receiver and a Joystick antenna with which he heard:-
4990 Radio Kiev, Ukraine, DX programme at 1945. 5015 Windward Islands B.S. to Europe at 2345.

6130 Radio Tirana, Albania in English at 2130.
7306 Polish Pathfinders in English at 1700.
15230 BBC, Ascension relay at 1710.
15250 RSA, South Africa at 1750.
21460 HCJB, Quito, Ecuador, DX programme at 1945.
21595 Radio Canada International at 1850.
C. Gibbs gives no indication of the equipment used but he managed to hear the following at his shack in Camberley:-
6020 Radio Nederland in English at 1515.
6025 Radio Portugal at 2125.
6025 Radio Budapest, Hungary in English at 2130.
7145 Radio Warsaw, Poland in English at 1600.
9535 SBC, Berne, Switzerland at 1115.
9730 Radio Berlin International from 1515.
9735 NHK, Japan in Japanese at 2012.
15325 Radio Canada in French at 2045.
A new reporter from Hessle in East Yorkshire is Ian Jarvis who owns a Lafayette HA-700 receiver and a 50 foot long aerial which enabled him to hear:-
7210 The International Radio Service of the Red Cross from Switzerland at 1200.
7290 Trans World Radio, Monaco at 1645.
9770 Austrian Radio, English for Europe at 2045.
11672 Radio Pakistan in English at 2015.
15130 Radio Australia in English at 0815.
15240 Radio Sweden in English at 2245.
The article in the May issue has prompted a number of queries as to which is the best receiver for the Broadcast Bands DXer. This is a very difficult question to answer but my general advice is to pick one of the following ex-military sets: CR100, AR88, R1155 or an HRO. If you prefer a new receiver the following two sets are good value for money: Lafayette HA-600 or Trio 9R59DE. Both these receivers retail at about $£ 45$, much better sets can be purchased if the money is available of course.

## KJ Catalogue

KJ Enterpises announce their latest Leisuresound Mail Order catalogue. There are 128 pages, containing stereo systems, record players of every variety, tape and cassette recorders, amplifiers, speakers, turntables, microphones, p.a. equipment, all types of recording tape, cassettes, books 8 -track cartridge players, car radios, countless hundreds of accessories of every kind, radios, specialist furniture lines etc. As usual the majority of items are available at substantial discounts and where possible recommended retail prices are listed for direct comparison with KJ. Although this catalogue is automatically distributed to existing KJ customers it is available $F R E E$ on request, to anyone interested. KJ Enterprises, 33 Bridle Path, Watford, Herts.

| Mr |
| :--- |

 OUR chance this month to get a special QSL card. The Irish Radio Transmitters Society are off on a DX-pedition to Dalkey Island which is, according to the map, a small island off the coast of the Republic of Ireland (see if you can find it). Operating dates are 1200 on July 31 to 1200 on August 2. Operation will be Al and A3a on all bands from $3 \cdot 5$ to 30 MHz . Sean Nolan, EI7CD, says that the callsign to listen for is EIODI and the station will QSL all contacts. Station will be operating from petrol generators, according to Sean, so if you intend to have a QSO-don't smoke.
D. Palmer (Glasgow), tells that ZSIMH has been heard operating a DX net several evenings on forty and is rumoured to be in on a similar net on eighty. Another one on forty is LU7ACC who, with the ZS, has been logged around 2145 hrs . Aerial at the Glasgow location is described as a V-beam with arms approximately $170^{\circ}$ which almost merits a dipole rating. Feeding the output to a balanced a.t.u. gives a significant improvement in signal to noise ratio. Receiver is a modified 19 set with a crystal filter which bagged: CP6EL, CT2AK, CX1AA, CX1BBR, JW7UH, LU8AJG, PY2ELZ, PY4BSZ, PY5OF, PY6JM, PY7BBD, VP2MM, ZS1JA all on 7 MHz s.s.b.
S. Chack (Harrogate), comments that stations have been dying out rather earlier on 14 MHz and says that 80 has been very good of late. Surprisingly though, his $\log$ is for 7MHY from which his best were HI3PY and JA6SM.
"The a.t.u. has been made from a cannibalised arystal set", says Stefan Kaye (Witney). Further admissions include a confession to using an AR88 to log these on 80; EA6BN, F6ABP/M, JY9WB, KV4FS, PY7BFN, PY0AD, VO1BT, ZC4IK, ZD7SD, ZS1MH, 4X4NJ, 6W8DY, 9G1DY.
S. Elsdon (Halesowen) warns, "You can be sure of hearing from me again soon", and promptly describes the gear as a CR-70A. Samuel also has a 240 ft . long wire bent in the middle (nasty) and managed VK3IQ and VK3LR on $3 \cdot 5 \mathrm{MHz}$.

John Moore (Leicester) says he's come to the conclusion that people who don't tune the low ends of bands are missing about one-third of the DX. Nonec.w. types please note. John also reminds that Italian prefixes are allocated according to area and range from $I 1$ to 10 . This might not be a bad idea for $G$ stations and would make life on two metres and up a whole lot easier.

John's log shows GM3SVK/A back on from the Shetlands on topband together with OK1FJS. Twenty metres s.s.b. showed: EA8GZ, ET3DS, JA3IXL, JW5NM, LU8DB,PY1CCC, PY2ZAD, PZ1DF, TA3HC, UK9AAQ, VE8RX, VK3ATN, VK6KK, VO1CM, YB3AAY, YB0AAG, 9H1CD, 9Q5BV. Ten metres raised: JA1ZTC, LU9FAN, PY2EWF, UK9HAD, VE2ASZ, VE3BKA, VE3FIQ, W3DQD/YVI.
G. Kent (St. Leonards-on-Sea) uses a B40 receiver and the aerial is "a strand of Woolworth's wire", (sounds a bit of a thin story to me). Although only

# THE AMATEUR BANDS David Gibson, G3JDG 

## Frequencies in kHz - Times in GMT

some 15 ft . long (the aerial not G. Kent) the following were heard on 14 MHz : CT1SG, JA4HM, JH1OTO, JM2HCA, K2OUS, VE3GMT, VE6MC, VK2WC, VK4DY, VK5ED, VK5NB, ZL4BX, ZP2KN, 4X4VB.

Someone's got a favourite band. Don't worry, your address at Satinforth Road, Ilford, Essex, is safe with me. I know you didn't sign the letter and just for that I won't tell anyone that you heard: CR4AJ, CR6EM, CR7F'M, CT2AK, DU6MG, EA6AS, EA9AA, EL7TL, EP2BQ, ET3USA, FC8APT, G3DJK/P/W1, HC1HV, HR3VFJ, IS1PZR, JA1QJE, JA7JLB, JH1JLR, K7ZTM, KC4USP, KG4CS, KP4DCR, LU1CBR, LX1HD, MP4BEU, MP4BJE, OX3DL, PY2BDY, PY8ZZA, SV1AE, SV0WDD, SZ0SU/P, TI3E, TJ1DA, VQ9RK, VU2HLU, VU2REG, VS9MB, VS9MT, W3UBM/MM/1, WA4MOC/P/8R1, WA6DBP/P/4X4, W6DLE,/4X4, W6VLH, W9LGV,, YU2REE/MM (off coast of Cameroons), ZC4CB, ZD9BN, ZL1HA, ZS6ES, ZS6ON, 3B8CZ, 4U1ITU, 4X4IX, 4Z4GV, 4Z4HF, 5H3JR, 5N2AAF, 5N2ABG, 5Z4DV, 6W8BD, 7X2OM, 7X2SX, 8P6AJ, 9E3USA, 9H1R, 9H1V, 9M2BQ, $9 \mathrm{~N} 1 \mathrm{MM}, 9 \mathrm{~V} 1 \mathrm{PX}, 9 \mathrm{X} 5 \mathrm{WJ}$, all on 21 MHz and probably s.s.b. too.
J. Iredale (Llandudno) expresses great delights at his newly-installed JR-500SE receiver (JDG's going all green again). A preliminary peep on 14 MHz revealed: HK3CFM, LU2DEK, LX1BA, MP4BFO (resolves his own sideband?), SV0WW, WA6AUE, 4X4DK, 4Z4HF, 5X5NA.

A Hallicrafters S120 and a 66ft. end-fed located at Ilford allowed Mark Marsden to bag these on 20 s.s.b.: JA20XF, JA7GY, HP9AVQ/MM, KX6DQ, TA6JB, TR8MC, VE6ARC, VK3CR, VK2AB, W3GLY/ VS6, ZS5DJ, 4Z4HF.

Come into my antenna says C. Henderson whose aerial does bear a remarkable resemblance to a spider's web. Receiver is a B40 and the other antenna is a 120 ft . long wire. Goodies on fifteen include: CR4BC, CR71C, HB9TE, HI8FED, KV4AD, OD5AO, PY2AAA, PY5EG, SU1BN, VE3BMB, VS9MT, XW8BP, YA2GNT, YV4YC, YV5BNR, ZC4MU, 4U1ITU, 4X4CW, 5N2AAJ, 9Q5RH, 9Y4RB. Crispin says that 20 metres has been excellent at round 0100 hrs .
S. Wainwright (St. Helen's), 9R-59DE, PR30, 70ft. inverted $L$ at 28 ft ., all s.s.b. on 14 MHz : FG7TD, FM7AA, FM7WW, HZ1TA, JR6JU, KS6CY, PJ8DZ, VR6TC, WA8FPN/P/KS6, ZF1GC.

Happenings for July include: 3-4, topband contest; $3-4$, two metre contest; 3-4, two metre listeners contest; 10-11, Field Day; 11, Worcester Mobile Rally, Upton-on-Severn; 18, 70 cms open contest; $18,70 \mathrm{cms}$ listeners contest; $10-25$ listen for G3EKW/A at the Nottingham Festival '71. Augugst 7-8, WAE c.w. contest.

Logs, in alphabetical order please, to arrive by the 15th of the month to:

12 Gross Way, Harpenden, Herts.

## THE <br> MW COLUMN



OVERCROWDING on the medium waves has encouraged DXers to develop the MW loop aerial. This type of indoor antenna is both tunable and directional. Maximum pick-up is along the plane of the windings and there are two nullsdirections of little or no pick-up-opposite each other at right angles to the windings. These nulls enable DXers to reduce or eliminate interference simply by rotating the loop on its vertical axis so that stations such as Malaga 1007 kHz can be heard with the null on Hilversum or Buenos Aires on 1070 kHz with the null on CBA Moncton N.B. in Canada. Since a loop is an indoor aerial it can be used in locations where it would be impossible to erect an outdoor one. The writer invariably uses a loop in preference to a 90 ft longwire as the overall performance is nearly always better.
R. Garwood of Bournemouth has asked for constructional details. The standard MW loop consists of 7 turns of plastic covered hookup wire wound in the shape of a square of 40 in . side together with a one-turn coupling winding wound parallel and central to the main winding. The windings are supported on a frame made out of two pieces of 1 inch square wood joined at right angles at the centre to form an X. The turns are kept apart by means of four paxolin spacers which have saw cuts ${ }_{4} \mathrm{in}$. apart along one edge to retain the windings. The spacers are fixed to the ends of the arms. The main winding terminates on a 500 pF variable capacitor mounted at the centre of the loop. This is the tuning control. The single coupling winding ends at a small terminal block from which a 5 ft . length of twin feeder (plastic covered lighting flex will do) connects to the receiver dipole input or to the aerial and earth terminals. The loop is fixed to a stand so that it can be rotated on its vertical axis.

To use the loop, tune in a station on the receiver peak-up the signal with the loop tuning control and rotate the loop for optimum reception. As well as reducing co-channel interference, a loop will usually have a better signal-to-noise ratio then a longwire and it will often reduce cross-modulation, splash and occasionally static. Ray Eaton, a retired reader who lives in Brighton has been experimenting with loop aerials on frequencies up to 4 MHz and reports some success.

South Americans are at their best in summer so now is the time to look for the rarer countries. Between 0100hrs GMT and sunrise listen for Radio Cruz del Sur on 1380 and Radio Mineria 1060 kHz ; both are 7,000 miles away in Chile. OAX4U 1010 kHz Radio America is in Lima, Peru. It is normally a strong signal and has been logged already this year by a DXer in Norfolk. ZP4 1330kHz Radio Chaco in Paraguay and CP57 Radio Progresso 1090 kHz in La Paz, Bolivia were heard last year while CP4 1020 kHz also in La Paz is another recent catch from this difficult DX country. Conditions are at their best during the hour before dawn and the band is often alive with Latin Americans at this time.

## CHARLES MOLLOY




IT'S those integrated circuits again. Different types appear on the professional market almost daily. A fairly recent one is of great interest since it could well affect a whole industry. This $16-$ pin dual in-line beast is called the TBA 631 and hidden within the confines of its diminutive carcass is a limiting amplifier, an f.m. coincidence detector, low frequency separator, low frequency preamplifier and self-balancing circuit, driver and audio amplifier. It's immediate application is in television receivers and the trend is that the average black and white receiver will be reduced to five integrated circuits (which should make the do-it-yourself t.v. builder jump for joy). Colour sets will need another two i.c.s.

There is more to it than merely simplifying construction, although from the manufacturing point of view this is extremely important. Servicing becomes an important aspect of many things, especially television receivers. If this trend of reducing a black and white set to five i.c.s continues, then the servicing aspect becomes a comparatively simple matter, since the would-be service man has, at worst, only to work his way round the set simply substituting "good" i.c.s. for each one in the set until the fault is cleared. This in turn implies that initial servicing in the home could be performed by an unskilled person.

It is not possible to fault the idea in terms of initial cost either, since the TAB 631 markets for around $£ 2.80$ for quantities of 1 to 24 . Again, the chip in question will supply 3 watts into a $16 \Omega$ speaker for 10 per cent distortion with a 24 V line. Limiting sensitivity of the unit is less than $100 \mu \mathrm{~V}$ at 6 MHz for the quoted output. The output stage is class B and is capacitively-coupled to the speaker. The r.f. amplification, demodulation and output separator section has it's own power supply terminations and will work at voltages from $4 \cdot 5 \mathrm{~V}$ to 15 V . The quiescent current at 12 V is typically 18 mA and the frequency range of the r.f. stage is between 5 kHz and 60 MHz . Over 60 dB of gain is available from the limiting amplifier alone, while a.m. rejection is given as better than 45 dB . A few resistors and capacitors plus tuned circuits are all that are needed to get this chip perking happily.

While the cathode ray tube and power supply are still required and have not, as yet, been reduced to a chip, experiments in solid state readout devices look promising although many companies have these behind locked doors. With advances like this, the wristwatch television doesn't seem quite such a ludicrous idea after all.


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WELL; we've only just made it this month as far as price limit is concerned but it is worth it, I hope. It is rather an unusual circuit and has not appeared before, as far as I am aware, in any form. The circuit is that of a "Touch Alarm" which does exactly what the title suggests; an alarm sounds off as soon as a metal plate is touched and stays on until the supply voltage is taken away. The metal plate can be all sorts of things, a safe, french windows, door handle, etc., etc., The applications and construction are left up to you but the circuit is not exactly complex and should take no more than a couple of hours to build once the components are assembled.

## THE CIRCUIT

The first transistor, Trl, is coupled in the com-mon-collector mode (also known as the emitterfollower mode) with the base wired to the touch plate. The characteristics of this configuration are very high input impedance and low output impedance and this is the key to the operation.

The input impedance is roughly equal to the gain of the transistor times the emitter load resistor (here $6 \cdot 8 \mathrm{k} \Omega$ ). The BC169C has very high gain figures, up to 900 , but a more common figure would be 400. Therefore on this basis the input impedance is $400 \times 6,800$ which equals nearly $3 \mathrm{M} \Omega$. As soon as anything touches this base it biases the transistor on and the same voltage which has been applied to the base at very high input impedance, appears at the emitter at the same voltage level but at a usable impedance.

Most of you have dabbed a damp figure at the input of an amplifier and heard the resulting sounds, made up from radio signals and hum. Here we are making the best use of these signals and putting them to use. All sorts of "muck" is picked up when the plate is touched and this appears at the emitter as an a.c. voltage. The detector diode rectifies the signals and applies them across the capacitor C1. This charges up so that a positive supply appears at the junction of $D 1, C 1$ and $R 2$. This voltage applies a bias via the resistor to the base of $\operatorname{Tr} 2$ which conducts and in turn applies bias to $\operatorname{Tr} 3$ and a pulse passes through the primary of the output transformer. However C2 is connected in a manner which causes the second two transistors to oscillate.

The beauty about the values and configuration used here is that once the alarm oscillator has started it is self-holding. That is, the pulses through C 2 themselves bias Tr 2 to maintain the cycle necessary for a continually sounding alarm. So it will be seen that R 2 is only necessary to start the alarm which can only be switched off by disconnecting the battery supply. C3, which decouples the supply, is not essential but with a low battery it does help the operation.

## No. 28 <br> TOUCH ALARM



Fig. 1 : The circuit of the touch alarm

## $\star$ components list

|  | BC169 | 11 pt |
| :---: | :---: | :---: |
|  | BC169 | 11p $\dagger$ |
| Tr3 | 2N3702 | 13pt |
| Di | OA91 | 5p $\dagger$ |
| R1 | 6.8k $\Omega, 10 \%, \frac{1}{4} \mathrm{~W}$ | $1 \mathrm{p} \dagger$ |
| R2 | 150kS, $10 \%$, ${ }^{\text {W }}$ W | 1 pt |
| C1 | $25 \mu \mathrm{~F}, 25 \mathrm{~V}$ Mullard | 6pt |
| C2 | $0 \cdot 1 \mu \mathrm{~F}$ Mullard | 4 pt |
| C3 | $50 \mu \mathrm{~F}, 25 \mathrm{~V}$ Mullard | $6 \mathrm{p} \dagger$ |
| SW1 | D.P.S.T. Toggle switch | $5 p^{*}$ |
| T1 | Transistor output transformer, Eagle LT700 | 20p $\ddagger$ |
| LS $6 \times 4 \mathrm{in}, 3 \Omega$ loudspeaker |  | 15p* |
|  |  | $98 p$ |
| $\dagger$ Electrovalue Ltd. |  |  |
| * Padgetts Radio Stores |  |  |
| $\ddagger$ Henrys Radio Ltd. |  |  |
| Prices are those advertised in June 1971 and may have changed. No allowance is made for minimum order costs or for postage and packing; this should be checked before ordering. |  |  |

Current drain is important in all alarm circuits because if it is high, batteries, which are continually left on would rapidly run down. In the quiescent condition current consumption was measured as $1_{\mu} \mathrm{A}$ in the prototype as silicon transistors are used throughout, though when in operation this rises to over 20 mA and a PP9 type battery has to be used.

Cl can be left out. If this is done the alarm is triggered by the slightest pulse-even by the switching on of fluorescent lights and this is a disadvantage. The inclusion of C2 has a slight delaying action as it takes time to charge up.

In certain locations the level of "muck" may be so high as to trigger the alarm without it being touched. In this case the value of R1 should be reduced to a suitable level which only triggers on touch; this also applies if a large touch plate is used.


## TITANIC DISASTER

We are at present compiling a Going Back article about the Titanic Disaster and the radio messages that were transmitted and received on that tragic day. If any readers have any information or photographs that they think may help us, we would be very glad to hear from them.

MR. WILLIAM COBBETT tells us that he has a Harmsworth's Wireless Encyclopedia which was published in 1923. He says that it contains many interesting features and drawings, etc., the preface being written by Oliver Lodge himself. Mr. Cobbett says that 50 years after the books were first published it is amusing to read a line that states, "It is with great hesitation that we predict the time when each individual will possess his own pocket wireless set."

Perhaps any readers of Practical Wireless requiring information on wireless in the 1920's would like to contact Mr. Cobbett at 15 Copford Road, Billericay, Essex.

By the way, he tells us that anyone wishing to purchase the books will have to wait another 50 years!

Mr. C. R. Gunn of 48 Aldwark Road, Liverpool, L14.0N6 asks if anyone could tell him whether Paris (Eiffel Tower) still transmits the 300 dot second Time Signal that it used to years ago on long wave. Mr. Gunn cannot recall the wavelength of the transmissions but says that it used to be very interesting as with a microphone in the case of the Grandfather clock and a phone earpiece on one ear together with the radio phone on the other ear, the times when the two signals coincided were noted and checked by the time given after the transmission.

Mr. Gunn also asks if there is a publication giving a list of long wave stations transmitting Morse and what are the longest wavelength stations today? So if there are any readers who have any information that may interest Mr. Gunn, please write to him at the above mentioned address.

Basil D. Van Der Syde, F.S.E.R.T., 30 Langdon Road, Parkstone, Poole, Dorset, BH14 9EH asks if anyone can date a pair of headphones he has containing a built-in crystal receiver. There is no makers name and the "cans" are about twice the
normal depth. In the back of one there is a tapped inductance with a 20 -position selector switch for tuning. This earpiece has two terminals marked A and $E$. The other earpiece has a centrally fitted crystal detector, part of which is missing but the cap end contains a piece of "galena" crystal. Also contained within this earpiece is a wind-up aerial of some 20 feet of wire-woven tape about $1_{2} \mathrm{in}$. wide, and two small terminals marked "phones" (extension phones!). There is a Postmaster General approved stamp and the number 4145 printed on it. The crystal detector is integral with the small handle that winds the aerial in and the words "detector" prov. pat, printed below this--Mr. Van Der Syde mentions that when fitted with an 0A70 or similar diode, this set still provides fair MW signals (Charles Molloy please note!)

Many readers, we are sure, will remember our great colleague John Scott-Taggart. He used to bring out one "star" receiver for the home constructor every year in the magazine Popular Wireless. Mr. Van Der Syde says that checking over his collection of these magazines some years back, he was suddenly struck with the fact that the series was brokenthat is that it began with ST100 then went to ST300, 400,500 and so on up to about ST900-in other words no ST200! At first he thought his collection was not complete but this did not appear to be so. This made him wonder if there had ever been a ST200 design and if not, why not?-or if so, had it been withdrawn? He made many enquiries and at last managed to contact JST himself in about 1963. He wrote to him but in his reply, JST was unable positively to give any information about an ST200. He thought that there may have been one and that details may be found in one of his early radio books Practical Wireless Valve Circuits or its sequel More Practical Valve Circuits published by the Radio Press about 1924/25.

Can any readers help to clear up the mystery of the missing ST200? If so, please write to us (because this one has us puzzled) and we will pass your letters on to Mr. Van Der Syde.

Vintage enthusiast S. Ellis, 30 Pynne Close, Stockwood, Bristol 4 writes to ask if we have any information on the receiver used for the "Committee Superfet" article. Unfortunately we don't as this receiver was kindly donated to us by a reader who said that a relative of his had constructed it from a kit in the 20's (we would like to say here that Arthur Dow did not rip the set open and implant an inte-

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grated circuit-it was a clever bit of camera trickery!). Anyway, Mr. Ellis says that in his set there are more wires with nothing at the end of them than there are connecting components. The components appear to be in good condition. There valves are included (PM1A, D210, PM1LF-possibly), the valve-holders are square and the four pins marked F, A, F, G. Stamped on the holders is the word "Benjamin" and "Genuine Bakelite."
There are two variable capacitors made by Ormond Engineering Co. each fitted with a dial similar to the "Committee Superfet". The coil is 7in. long and 4in. in diameter and is stamped "Trade ISOLO Mark" there are three windings of cotton or silk covered wire. Resistors are Dubilier Dumetohm which have the appearance of cartridge fuses, each one clipping into a holder. The capacitors have thumbscrew terminals as does a fully-shrouded transformer inscribed "Hollingwood" with markings for secondary, primary, grid, plpate, h.t. + and +D . Also, one point to note is that there is a bracket attached to the base-board reading "Etherplus."

Once again, the staff of $P . W$. would like to hear more about this, so please droy us a line, and we'll pass the letters on.

Our aerial photograph is enough to make Dave Gibson's hair curl ("what hair?" shouts someone from the back row). What about strapping this one on the top of your wagon, Gibby and working a bit of mobile DX?


Actually it's an early frame aerial used for direction-finding in aircraft. The date is about 1916 and the photograph was lent to the Science Museum by the National Physical Laboratory.

In "Going Back" May 1971, we published a photograph which we captioned "Magnetic Detector". This should have read "Multiple Tuner" and we would like to thank all those readers who were kind enough to point this out.


This year we are sponsoring another Project Autumn competition. The rules have been amended so that the PW "Designer's Trophy" 1971 will be awarded to the author of the best constructional article published in PW issues dated July 71 to March 72 inc.

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8. Employees and staff of PW are not eligible for entry to this competition.

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# practically wireless commentar by IILIIII 

MOTORING correspondents are fond of telling us the tales of woe they experience with their new cars. Doors jam, windscreen wipers fail, handles fall off, and other, more technical failings begin to show after a short spell of use. "The suspension suffered badly

. . . experience with their new cars.
from hugging on anything more than a twenty-degree bend . . ."

They don't know the half of it. The benefits of mass production hit the radio industry long ago, and with all the paraphenalia of printed circuits and peripheral hardware, modern radio and audio equipment has reached its nadir of vulnerability.

Only last week we had a very expensive, very elaborate hi-fi amplifier on the bench, sighing dolefully. It coudn't sing; its protection circuits, which comprised more than half the twisted jungle through which we tried to hack our way, did their work too thoroughly. Every time a signal pushed past the preamps, $\operatorname{Tr} 1$ switched hard on, putting Tr2 "off" and interrupting the bias control of $\operatorname{Tr} 3$ which promptly bottomed. This overcame the zener regulation of $\operatorname{Tr} 4$ which is in the feedback line of . . .

Henry tuned in last week, hoping to brush up his faltering maths, and was greeted with the pontifical statement: "Mathematics is not so much about numbers as about sets."

Sets? Sets of what? Or did the Professor mean wireless sets? It might have been appropriate to our subject if he did, for the ensuing discussion was more
philosophical than enlightening.
Some of the equipment that comes in for service within weeks of being sold must have been assembled under similar conditions. Perhaps, in the Buzzbox factory in Arnold's Wick, SW 19, the wires have got crossed and those overtime earners on Saturday mornings are listening to the cut and thrust of $\mathrm{O}-\mathrm{U}$ discussion.

Well, not so much cut and thrust as snip and shove. Which may account for some of the untightened bearing clamps, twisted drive cords, unsealed iron-dust cores and knobs that fall off. The operator is away in a dream, lapped by the lulling voices. There used to be a saying in a radio factory where Henry once worked: "Lil's in love again."

It was invoked whenever we slaves of the troubleshooting department discovered a "run" of faults.

The inspectors would reject one set in five for "no-go" faults, normally. Then would come a spate of rejections, and we-the only true engineers in the factory, we averred, not excepting the de-signer-ran our delicate diagnostic probiscuses over them.
Hovering at our shoulder, the Production manager waited for the dread words: "R21 wrong value, should be 33 k , not 33 ohms." We laid bets on the number of sets that Lil had allowed through as she dreamed over the new boy. The variables for handicapping were the rate of the conveyor, the alacrity of the Production manager and, top weight for the course, the slowness of the troubleshooter.
In that sort of job, every day was Saturday. Down in Arnold's Wick, SW 19, the Monday set, the rogue receiver, is the speciality of their range. After a week of use it hesitates and splutters.
We bang it. A knob falls off. We shake, and two programmes arrive together. The volume con-
trol adds its crackling obligatto and then the tiny loudspeaker squawks in protest. So we take it in for service.

The knowledgeable salesman shakes his head sadly. 'Perhaps the worst model they made," he pronounces. "You didn't buy it here of course?" His question is more a statement; that isn't the sort of trash they would sell. But they do, eventually, repair it, after weeks of waiting for irreplaceable parts that have to be ferried from Japan in a leaking sampan.

And within another week it splutters and coughs into silence. A little tense, we face the salesman again. Could we see the manager? Not, it seems, without an appointment, but they guarantee their work and condescend to look at it again.

This time, again with a bill to pay, we are told that another vital component has failed. "Quite unforeseeable. The quality of the components used in these-erless expensive receivers . . ." The

work done on their last job, the guaranteed work, could not cover the eventuality of that component's failure.

It would have been better, less expensive, if we had faced up to the truth. Ours was a Saturday set, or a Monday set, or whatever day our Lil habitually assembles errors down in Arnold's Wick, SW 19. Better thrown away.

## new



## Highfidelity Monolithic Integrated Circuit Amplifier

Two years ago Sinclair Radionics announced the World's first monolithic integrated circuit $\mathrm{Hi}-\mathrm{Fi}$ amplifier, the IC.10. Now we are delighted to be ahle to introduce its successor the Super IC.12. This 22 transistor unit has all the virtues of the original $I C .10$ plus the following advantages:

1. Higher power.
2. Fewer external components.
3. Lower quiescent consumption.
4. Compatible with Project 60 modules.
5. Specially designed built-in heat sink. No other heat sink needed.
6. Full output into $3,4,5$ or 8 ohms.
7. Works on any voltage from 6 to 28 voits without adjustment.
8. NEW 22 transistor circuit.

Output power 6 watts RMS continuous (12 watts peak)
Frequency Response 5 Hz to $100 \mathrm{KHz} \pm$ 1 dB .
Total Harmonic Distortion Less than $1 \%$ (Typical $0.1 \%$ ) at all output powers and all frequencies in the audio band.
Load Impedance 3 to 15 ohms.
Power Gain 90dB (1,000,000,000 times) after feedback.
Supply Voltage 6 to 28 volts (Sinclair $\mathrm{PZ}-5$ or PZ-6 power supplies ideal).
Size $22 \times 45 \times 28 \mathrm{~mm}$ including pins and heat sink.
Input Impedance 250 Kohms nominal.
Quiescent current 8 mA at 28 volts.
Price: including FREE printed circuitboard for mounting. $\mathbf{f 2 . 9 8}$ Post free

With the addition of only a very few external resistors and capacitors the Super IC. 12 makes a complete high fidelity audio amplifier suitable for use with pick-up. F.M tuner etc. Alternatively, for more elaborate systems, modules in the Project 60 range such as the Stereo 60 and A.F.U. may be added. The comprehensive manual supplied with each unit gives full circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include car radios, oscillators etc. The very low quiescent consumption makes the Super IC. 12 ideal for battery operation.

## Sinclair Project 60



## the world's most advanced high fidelity modules

Sinclair Project 60 presents high fidelity in such a way that it meets every requirement of performance. design. quality and value and now that the remarkable phase lock loop stereo FM tuner is available. it becomes the most versatile of high fidelity systems. With Project 60, it is possible to start with a
modest mono record reproducer and expand it to a sophisticated stereophonic radio and record reproducing system of fantastically good quality to hold its own with any other equipment, no matter how expensive. Project 60 is a unique high fidelity module system where compactness and ease of assembly are combined with

|  | System | The Units to use | together with | Cost of Units |
| :---: | :---: | :---: | :---: | :---: |
| A | Simple battery record player | 2.30 | Crystal P.U., 12 V battery volume control | $£ 4.48$ |
| 8 | Mains powered record player | 2.30. PZ.5 | Crystal or ceramic P.U. volume control etc. | £9.45 |
| C | $20+20$ W. R.M.S. stereo amplifier for most needs | $\begin{aligned} & 2 \times 2.30 \text { s. Stereo } 60 \text {. } \\ & \text { PZ. } 5 \end{aligned}$ | Crystal. ceramic or mag. P.U., most dynamic speakers. F.M. tuner etc. | £23.90 |
| D | $20+20$ W. R.M.S. stereo amplifier with high performance spkrs. | $\begin{aligned} & 2 \times Z .30 \mathrm{~s}, \text { Stereo } 60, \\ & \text { PZ.6 } \end{aligned}$ | High quality ceramic or magnetic P.U.. F.M. Tuner. Tape Deck. etc. | £26.90 |
| E | $40+40$ W. R.M.S. deluxe stereo amplifier | $2 \times 2.50$ s, Stereo 60 PZ.8, mains trsfrmr | As for 0 | £34.88 |
| F | Outdoor P.A. system | 2.50 | Mic., up to 4 P.A. speakers controls, etc. | £5.48 |
| G | Indoor P.A. | Z.50, PZ.8, mains transformer | Mic., guitar, speakers, etc.. controls | £19.43 |
| H | High pass and low pass filters | A.F.U. | C. Dor E | £5.98 |
| J | Radio | Stereo F. M. Tuner | C. Dor E | £25.00 |

circuitry that is far in advance of any other manufacturer in the world. Thus it is extraordinarily easy to assemble any combination of modules using nothing more complicated than the simplest of tools, and you certainly do not have to be experienced to build with complete confidence. The 48 page manual free with Project 60 equipment makes everything easy and you can house your assembly in an existing cabinet, motor plinth. free standing cabinet or virtually any arrangement you wish. Once you have completed your assembly you will have superlatively good equipment to give you years of service and enjoyment. You will have obtained superb value for money because Project 60 is the best selling modular system in Europe and can therefore be produced at extremely competitive prices and with excellent quality control.
Sinclair Radionics Lid.. London Road. St. Ives, Huntingdonshire PE17 4HJ.
Tel: St. Ives (048 06) 4311


## Sinclair Project 60

## Z.30 \& 2.50 power amplifiers



The $Z .30$ and $Z .50$ are of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low $0.02 \%$ at full output and all lower outputs. Whether you use Z.30 or Z. 50 amplifiers in your Project 60 system will depend on personal preference, but they are the same size and may be used with other units in the Project 60 range equally well.
SPECIFICATIONS (Z50 units are inter-
changeable with 2.30 s in allapplications).

## Power Outputs

Z.30 15 watts R.M.S. into 8 ohms using 35 volts: 20 watts R.M S. is.to 3 ohms using 30 volts.
$\mathbf{Z . 5 0} 40$ watts R.M S. into 3 ohms using 40 volts: 30 watts R.M.S. into $80 h m s$. using 50 volts.
Frequency response: 30 to $300000 \mathrm{~Hz} \pm 1 \mathrm{~dB}$.
Distortion: $0.02 \%$ into 8 ohms .
Signal to noise ratio: better than $70 d B$ unweighted.
Input sensitivity: 250 mV into 100 Kohms .
For speakers from 3 to 15 ohms impedance.
Size $3 \frac{1}{2} \times 2 \frac{1}{4} \times \frac{1}{2} \mathrm{n}$.
2.30

Bult tested and guaranteed with circults and instructionşmanual $£ 4.48$
Z. 50

Built. tested and guaranteed with circuits and instructions manual.
$£ 5.48$

## Power Supply Units



Designed specially for use with the Project 60 system of your choice.
Illustration shows PZ. 5 to left and PZ. 8 (for use with Z.50s) to the right. Use PZ. 5 for normal Z. 30 assemblies and PZ. 6 where a stablised supply is essential.
PZ-5 30 volts' unstabiltsed $\mathbf{£ 4 . 9 8}$
PZ-6 35 volts stabul/sed $£ 7.98$
PZ-8 45 volts stabilised
(less mains transformer) $£ 7.98$
PZ-8 mans transformer $£ 5.98$

## Stereo 60

 pre-amp/control unit

Designed for the Project 60 range but suitable for use with any high quality power amplifier. Again silicon epitaxial planar transistors are used throughout. achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection ts by means of push buttons and accurate equalisation is provided for all the usual inputs.

## SPECIFICATIONS

Input sensitivities: Radio-up to 3 mV . Mag. p.u. 3 mV : correct to R.I.A.A. curve $\pm 1 \mathrm{~dB}: 20$ to 25.000 Hz . Ceramic p.u-up to 3 mV : Aux-up to 3 mV .
Output: 250 mV
Signal-to-noise ratio: better than 70 dB .
Channel matching: within 1 dB
Tone controls: TREBLE +15 to -15 dB at $10 \mathrm{KHz} \cdot$ BASS +15 to -15 dB at 100 Hz .
Front panel: brushed aluminium with black knobs and controls.
Size: $8 \frac{1}{4} \times 1 \frac{1}{2} \times 4 \mathrm{~ms}$.
Built tested
and guaranteed.
£9.98

## Active Filter Unit



For use between Stereo 60 unit and two $Z .30$ s or $\mathrm{Z}$..50 s . and is eas!ly mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are neghgible The A.F.U. is suitable for use with any other amplifier system. Two stages of filtering are incorporatedrumble (high pass) and scratch (low pass). Supply voltage -15 to 35 V . Current - 3 mA . H.F. cut-off ( -3 dB ) varable from 28 k Hz to 5 kHz . L.F cut-off ( -3 dB ) variable from 25 Hz to 100 Hz . Distortion at 1 kHz ( 35 V . supply) $0.02 \%$ at rated output.
Buitt tested
and guaranteed
£5.98

## Stereo FM Tuner



## first in the worid to use the

phase lock loop principle
Before production of this tuner. the phase lock loop principle was used for recerving signals from space craft because of its vastly improved signal to noise ratio over other systems. Now. for the first time. the principle has been applied to an FM tuner with fantastically good results. Other original features include vanicap diode tuning, printed circuit coils, an I.C. in the - specially designed stereo decoder and squelch circuit for sient tuning between stations. Sensitivity is such that good reception becomes possible in difficult areas. Foreign stations can be tuned in sultable conditions and often a few inches of wire are enough for an aerial. In terms of a high fidelity this tuner has a lower level of distortion than any other tuner we know. Stereo broadcasts are received automatically as the tuning control is rotated a pane! indicator lighting up as the stereo signal is tuned in. This tuner can also be used to advantage with any other high fidelity system.

## SPECIFICATIONS:

Number of transistors: 16 plus 20 in I.C.
Tuning range: 87.5 to 108 MHz
Captureratio: 1.5 dB
Sensitivity: $2 \mu V$ for 30 dB quieting: $7 \mu \mathrm{~V}$ for full limiting.
Squelch level: $20 \mu \mathrm{~V}$.
A.F.C. range: $\pm 200 \mathrm{KHz}$

Signal to nolse ratio: $>65 \mathrm{~dB}$
Audio frequency response: $10 \mathrm{~Hz}-15 \mathrm{KHz}$ ( $\pm 1 \mathrm{~dB}$ )
Total harmonic distortion: $0.15 \%$ for $30 \%$ modulation
Stereo decoder operating lèvel: $2 \mu \mathrm{~V}$
Pilot tone suppression: 30dB
Cross talk: 40 dB
1.F. frequency: 10.7 MHz

Output voltage: $2 \times 150 \mathrm{mV}$ R.M.S.
Aerial Impedance: 750 hms
Indicators: Mains on: Stereo on; tuning indicator Operating voltage: $25-30 \mathrm{VDC}$
Size: $3.6 \times 1.6 \times 8.15$ inches: $91.5 \times 40 \times 207 \mathrm{~mm}$


Price: $\mathbf{£ 2 5}$ built and tested. Post free

## Guarantee

If within 3 months of purchasing Protect 60 modules directly from us, you are dissatisfied with them we will refund your money at once. Each module is guaranteed to work pe fectly and should any defect anise in normal use we will service it at once and without any cost to you whatsoevet provided that it is returned to us within 2 years of the purchase date. There will be a small charge for service thereafter No charge for postage by surface mail. Air-mall charged at cost.

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|  |  |  |  |
|  |  |  |  |
|  |  | dWELL TIME UNIT These small units contain the following components: 700 ohmDPDT relay with basc, $1 \mu \mathrm{~F}$ DPDT relay250 v. paper, $0.01 \mu \mathrm{~F}$400 v - paper, $50 \mu \mathrm{~F} 35 \mathrm{v}$. electrolytic, 3 diodes OC200 transiator, a $2 N 2926$trane type transistor onmarked,skeleton pre-set pot, 4 pla din sxeleton pre-getplug $\&$ skt., 4 foot of 4 core plug es All housed in a small neat metal box. Can be made into many timing devices. mate 435 $\qquad$ |  |



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Transistor Radio Cases: 25p each
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\hline Double \& \& \& <br>
Swltched \& $500 \mathrm{~K} \Omega / 500 \mathrm{~K} \Omega$ \& $3 \frac{1}{2}$ " <br>
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\hline Swltched <br>
\hline Double 8 <br>
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Switched
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| AC127 | 0.17 | $\bigcirc \mathrm{OC} 200$ | 0.25 |
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| $0 \subset 73$ | 0.17 | Diodes |  |
| OC81 | 0.13 | AAY42 | 0.10 |
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NPN/PNP Silicon Planar Transistors TO-18 mixed untested similar to 2N706-6A-8, BSY26-7A9-95A and BCY70 etc. $\mathbf{X 4 - 2 5}$ per 500 . $\& 8$ per 1000.
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| $\mathbf{B 6 6}$ | 150 | Germanium Diodes <br> Min. glass type | $\mathbf{5 0 p}$ |
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| NEW | TESTED AND |
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This field effect transistor is the 2N3823 in a plastic encapsulation, coded as 3823 E . It is also an excellent replacement for the 2N3819.
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| :---: | :---: | :---: | :---: |
|  | 20V．D．C．．．${ }^{20 \mathrm{E} 2.971}$ |  |  |
| $50 \mu \mathrm{~A} \ldots \ldots .$. $50-50 \cdot 47$ 583 | ${ }_{\text {300V．}}^{\text {50，}}$ | $50-0-50 \mu \mathrm{~A}$ $100 \mu \mathrm{~A}$ | ${ }_{300 \mathrm{~V}}^{50 \mathrm{~V}}$ ． |
| ${ }_{100} 02 \mathrm{~A} \ldots \ldots . .83 .37$ | $1 \mathrm{amp} . \mathrm{D} . \mathrm{C} .82 .071$ | $100-0-100 \mu \mathrm{~A} 82.875$ | 1 amp ．D |
| $1000-0-100 \mu \mathrm{~A} 29.25$ | ${ }^{5} \mathrm{ampr}$ ．D．C． |  | 5 amp ．D．${ }^{\text {che }}$ |
|  |  |  | ${ }^{300 V}$ VU Meter． |

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| :---: | :---: |
|  | $100 \mathrm{ma} \cdot . .$. |
|  | $1 \mathrm{mmp} . . . .$. ． 22.60 |
|  | $5 \mathrm{amp} . . . .$. ． 28.40 |
|  | 15 amp．．．．．${ }^{\text {¢ } 2 \cdot 60}$ |
|  | $30 \mathrm{mmp} . . .$. ． 8 EE 60 |
|  |  |
|  | 50V．D．C．．． $2 \mathbf{8 . 6 0}$ |
| $30 \mu \mathrm{~A}$ ．．．． 580 | 150V．D．C． 88.60 |
| $50-0-50 \mu \mathrm{~A} \quad 83.10$ | $300 \mathrm{~V} . \mathrm{DC}$. ． $\mathbf{4} \mathbf{6 0}$ |
| $100 \mu \mathrm{~A}$ … 28.10 | 15V．A．C．．． 58 2－60 |
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| 500－0－500 2 A ¢2－60 |  |
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| 5 mA ．．．．． 58.60 | 20 amp A．C．4E2．60 |
| $10 \mathrm{~mA} . .$. ex2－60 | 30 amp ．A．C． 48.60 |


| Type MR．52P．23，${ }^{\text {gin }}$ ．square fronts． |  |
| :---: | :---: |
| 50pA ．．．．． 28.10 | 10 V. D．C．．． 82.00 |
| $50-0-50 \mu \mathrm{~A} \quad 22.60$ | 20V．D．C．．． |
| $100 \mu \mathrm{~A}$ ．．．$£ 28.60$ | 50 V ．D．C．．． 22.00 |
| 100－0－100 12 A ？ 38.37 | 300V．D．C．${ }^{\mathbf{4} 2000}$ |
| $500 \mu \mathrm{~A}$ ．．． 2 Lz | 15V．A．C．． 28.00 |
| $1 \mathrm{~mA} . . . . . .$. | 300 V ．A．C． 82.00 |
| 5 mA ．．．．． $\mathbf{~} 2200$ |  |
|  | VU Meter $.933 \cdot 10$ |
| 50 ma ．．．88． 00 | 1 amp A．C．＊ 28.00 |
| 100mA ．．．．${ }^{\text {S } 2.00}$ | 5 amp A．C．＊${ }^{\text {2 }}$－ 00 |
| 500 mA ．．．． 52.00 | 10 amp ．A．C．$* 28.00$ |
| 1 amp．．．．．$\pm 200$ | 20 amp ．A．C．＊22． 00 |
| 5 amp．．．．． 28.00 | -30 anp．A．C．${ }^{\text {c }} 2000$ |


| Type MR，65P．83in．$\times$ 3tin．Irontg ． |  |
| :---: | :---: |
|  | 10V．D．C．．．${ }^{\text {s2 }}$ ． 10 |
| 50－0－50 4 A 88.75 | 20V．D．C．．． 52.10 |
| $100 \mu \mathrm{~A}$ … 22.75 | 50V．D．C．．．．$\pm 2 \cdot 10$ |
| 100－6－100 $\mathrm{A}^{2} 2680$ | 150V．D．C．．． 22.10 |
| $200 \mu \mathrm{~A}$ ．${ }^{\text {20．}} 8280$ | 300 V ．D．C．棘－10 |
|  | 15V．A．C．．． 2 2．10 |
| 800－0－500 $\mu \mathrm{A}$ E2．10 | 50 V ．A．C．．． 42.10 |
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|  | 500 Y ．A．C．${ }^{\text {ce } 2.10}$ |
|  |  |
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| 5 amp．．．．． $32 \cdot 10$ | $200 \mathrm{~mA} \mathrm{A.C.*SE-} 10$ |
| $10 \mathrm{amp} . . . .$. ． 88.10 | 500 mA A．C．＊22－10 |
| 15 amp．．． 28.10 | 1 amp A．C．＊ $22-10$ |
| $20 \mathrm{amp} . . .8210$ | 5 mmp A．C．＂ |
| 30 amp ．．． 22.10 | 10 mmp ．A．C．＊镍－10 |
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| :--- |
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