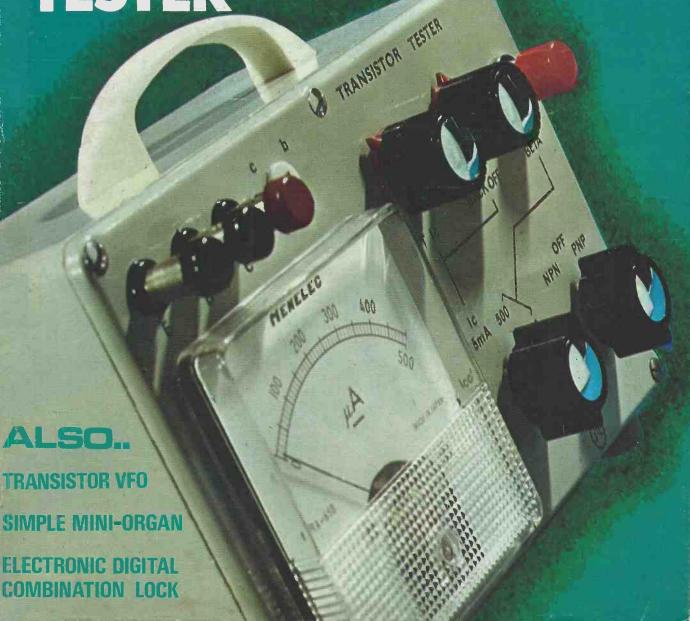
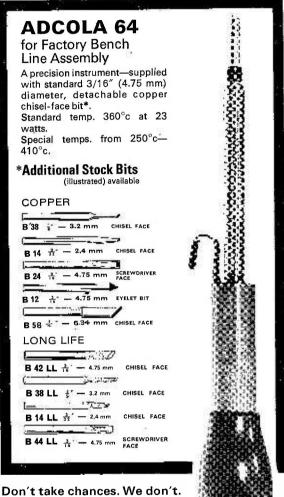
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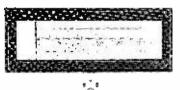
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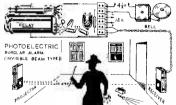
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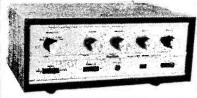
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MODEL 59/6

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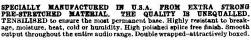
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The new AUDIO DE-VELOPMENT

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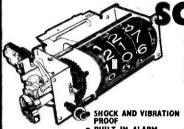
Stereo Magnetic Cartridge. Frequency response: 20-20,000Hz. Output: 5mV. Stylus: Diamond LP. 20-20,000Hz. Output: 5mV. Stylus: Diamond LP. 7 Free Free Replacement stylus type JS-P1 41/- poat free.

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Approx. as Super 30 but single
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Completely replaces batteries supplying 1.5v. and 90v. where A.C. mains 200/250v. 50c/s is available. Complete kit with diagram 59/9 or assembled 69/9.



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Treble 'htt' and 'cut' controls. 3 input sockets for Mike, Gram, Radio or Tapc. Input selector switch. Output for 3-15 ohm spkrs. Max. sensitivity 5 in. Attractive brushed silver finish facia plate 101 × 3 im. and matching knobs. Complete kit or parts with full wiring diagrams and instructions.

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PUSH-PULL ULTRA LINEAR OUTPUT "BUILLT-IN"
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Bass and treble controls. Frequency response ± 3dB
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COVERED IN REXINE/VYNAIR, IDEAL FOR VOCALISTS AND PUBLIC ADDRESS.

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TYPE C482 25/30 WATTS. Pitted four 8in. high flux 8 watt speakers.

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10,000 lines
15 olms. Carr. 7/6

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A powerful high quality all-purpose unit for lead, rhythm, bass guitar, vocalists, gram radio, tape, Peak Output rating.
Loudspeaker unit horizontal or vertical mounting.

\*\*Two extra heavy duty 12in, Loudspeakers.

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Solid state 3 Separately controlled inputs Ind. Bass and Treble Controls. Output for Speaker/s 3-30 ohns. 7;" 200-250 A.C. mains.

Fitted pair of 12" 50 watt high flux

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Peak Output rating.
For fuller details of Phase 29 Gns. Carr. Free 50 and Phase 100 see Mann facturers advert, page 424 or send S. A. E. for leaflets.

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100 Watt Solid State 100 Watt Solid State
4 Separately controlled
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volume Control. Ind.
Bass and Treble Controls. Output for
speaker/s 3-30 ohms.
Protective circuit to
from accidental shorts

I.H.F.M. Output rating 59 Gns.

# RSC 50 Watt L/SPEAKER UNITS RSC GI00 I00 Watt

peak output. Complete with pair of speaker columns and a Bass Unit (Six 12" and Two 15" speakers) 99 gns.

# 28 Gns. FANE ULTRA HIGH POWER LOUDSPEAKERS

All power ratings are R.M.S. continuous. 2 years' guarantee. High flux ceramic magnets. Heavy cast chassis.

'POP' 100 'POP' 60 | 'POP' 50 18" 100 Watt 15" 60 Watt 12" 50 Watt 14,500 gauss 14,000 gauss 10 (4,000 gauss 15 \tau 8/15 \tau 12 ans 8/15 \tau 10 ans 15 \tau 14,500 gauss 2 I gns. 8/15Ω

Dep. £6 and 9 mthly pymnts £2 (Total £24).

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Dual Cone 15O

£5-19-9 than

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 250v.
 60mA.
 6.3v.
 2a
 1

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 60mA.
 6.3v.
 2a
 1

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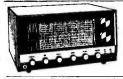
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mA, 0-250 mA. Resistance; 0-6 k, 0-6 Mg (300 ohm and 30K at centre scale). Capacitance: 10t. to .001 mfd. .001 uf to . 1. uf. Decibels: -20 to + 22dB. Size 41 x 32 x 1in. 71/- P. & P.

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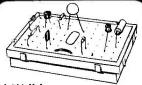
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Complete stereo system £41 plus £2.10. p. & p.

The Viscount F.E.T. Mk I £14.5 plus 7/6 p. & p. High fidelity transistor stereo amplifier employing field effect transistors. With this feature and accompanying guaranteed specifications below, the Viscount F.E.T. was applifier employing field effect transistors. With this vastly surpasses amplifier costing far more.

Specification-Output per channel 10 watts r.m.s. Frequency bandwidth 20 Hz to 20 kHz + 1db at 1 watt. Total distortion at 1 kHz at 9 watts 0.5% Input sensitivities CER. P.U. 100mV into 3 meg ohms. Tuner 100mV into 100K ohms. Tape 100mV into 100K ohms. Overload Factor Better than 26db.

Signal to noise ratio-70db on all inputs (with vol. max). Controls-6 position selector switch (3 pos. stereo and 3 pos. mono). Separate volume controls for left and right channels. Bass ± 14db at 60 Hz. Treble (with D.P.S. on off) ± 12 db at 10 KHz. Tape recording output sockets on each

channel. Size 121in, 6in. 23in, in teak-

finished case, BUILT & TESTED. MkII (MAG P.U.) £15.15 plus 10/- p. & p. Specification same as Mk. 1, but with the following inputs. Mag. P.U. CER. P.U. Tuner. Spec. on Mag. P.U. 3mV at 1 kHz input impedance 47K. Fully equalised to within ±1db RIAA. Signal to noise ratio-65db (vol. max).

# The £29-10-0 Stereo system

The Duetto is a good quality stereo amplifier, attractively styled and finished. It gives superb reproduction previously associated with amplifiers costing far more.

### SPECIFICATION-

R.M.S. power output 3 watts per channel into 10 ohms speakers.

INPUT SENSITIVITY. Suitable for medium or high output crystal cartridges and tuners. Cross-talk better than 30dB at 1Kc/s.

CONTROLS: 4-position selector switch (2 pos. mono and 2 pos stereo) dual ganged volume control.



TONE CONTROL Treble lift and cut Separate on off switch. A preset balance control.

Duetto integrated transistor stereo Amp. Garrard Changer from Cover and teak finish plinth Duo Type I speakers (see opp. page) The above items purchased together

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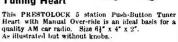
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Similar in design to those on the previous page the 2way speaker system is beautifully finished in polished teak veneer, with matching vynair grille. It is ideal for wall or shelf mounting either upright or horizontolly

Type I SPECIFICATION:-

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Its rugged construction as a sign makes it by far the best value for money. TECHNICAL SPECIFICATIONS

3 electronically mixed channels, with 2 inputs per channel, cnables the use of 6 separate instruments at the same time. The volume controls for each channel leasted directly above the corresponding inputs. are located directly above the corresponding input.

Scokets. SENSITIVITIES AND INPUT IMPEDANCES.
Channels 1 and 2 4mV at 470K. These 2 channels

A inputs) are suitable for microphone or guitars.
Channels 3 and 4 300mV at 1m. Suitable for most high
output instruments (gram, tuner, organ, etc). Input

### THE RELIANT



### SOLID-STATE GENERAL PURPOSE AMPLIFIER

SPECIFICATIONS

Output—10 watts. Output impedance—3 to 4 ohms Inputs—1. -xtal nic 10mV Tone Controls—Treble control range ±12dB at 10KHz.

±12dB at 10KHz.
2. «gram/radio 250mV. Bass control range ±13dB at 100Hz.
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points at 20Hz and 40k Hz. Signal to Noise Ratio—better than
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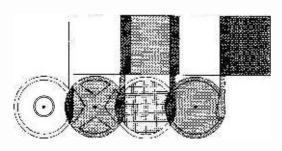
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1/4W	10%	4·7 Ω-10M Ω
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1 W	10%	4-7 Ω-10Μ Ω
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C = carbon	film high stabili	ity low noise
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	Power   1/20W   1/8W   1/4W   1/2W   1/2W	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

Values: E12 denotes series: 10, 12, 15, 18, 22, 27, 33, 39, 47, 56, 68, 82 and their decades. E24 denotes series: as E12 plus 11, 13, 16, 20, 24, 30, 36, 43, 51, 82, 78, 91 and their decades.

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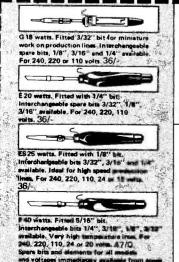
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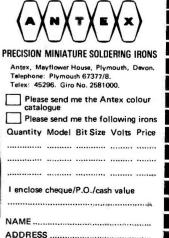
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# RACTICAL

VOL 46 NO 6

Issue 764

OCTOBER 1970

# TOPIC OF THE MONTH

# Women, arise!

WHAT with the establishment of the principles of equal pay and equal rights for women, the unisex concept and other such manifestations of emancipation, perhaps it is about time we did something about this parity of the

genders in this hobby of ours.

For long years, women have been favoured by management to perform those delicate tasks in assembly and inspection etc., so admirably suited to their special temperament and this is increasingly evident in the radio and electronics industries. But after leaving the factory or laboratory they seem to lose interest. They want to wash their hair, go to the pictures or watch the telly, when what they really ought to be doing is getting to grips with F. G. Rayer's latest creation in Practical Wireless!

With their gentle touch and infinite patience, the wiring up of the modern generation of miniature components ought to trouble them not the slightest. And think of the fruitful field for gossip that can be extracted from the tales of constructional triumphs . . . . "she said Radio Australia came booming out the first time she switched on. She hadn't even got the dial on straight. And the colour scheme of

the cabinet!"

We admit that many ladies are involved in amateur radio but most of them take a fairly passive (or resigned!) part in the proceedings, eyeing with varying degrees of distaste the activities of their eccentric menfolk. Before the last war there were just two licensed lady radio amateurs among the ranks of several thousand in this country. The Services, however, took advantage of their usefulness as wireless operators and mechanics and this was the launching pad for many who decided to take up radio as a hobby-and as a hubby, for most of them seem to have been snapped up by male radio enthusiasts who realised they were on to a good thing!

Today the number of licensed ladies is well over 50 strong and still growing. But we could do with more support on the constructional side. We ought to persuade our betters to join us and let them share our pleasures (and agonies). Apart from brightening things up and allowing us more time with the hobby, we'd have another pair of hands to do some of the donkey work. But that is quite

beside the point!

W. N. STEVENS-Editor.

# NOVEMBER ISSUE WILL BE PUBLISHED ON OCTOBER 9

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# NEWS... NEWS... NEWS...

# Radio Bristol

Shown right is the v.h.f. service of Radio Bristol. Frequency is 95.4MHz with horizontal polarisation. Maximum e.r.p. is 5kW with a directional aerial. The inner and outer service area boundaries correspond to average field-strength contours of 60 and 48dB (relative to 1 microvolt per metre) respectively for a receiving aerial height of 30ft above ground level. The field strength at a particular site may differ by 10dB from that indicated.

# R.A.E. Courses

A Radio Amateurs' Examination Course is to be run this winter by Glasgow Corporation Further Education Department at: The Glasgow College of Nautical Studies, 21 Thistle Street, Glasgow, C.5.

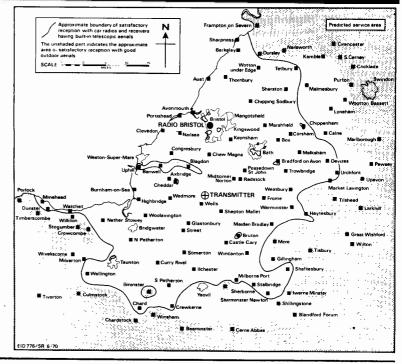
The course will meet at the College on Tuesdays and Thursdays from 7-9.30 p.m., commencing Tuesday, September 15th, 1970. Enrolment will take place at the College at 7 p.m. on the opening evening, and the fee for the course is £3, payable on enrolment. Students under the age of 18 on August 1st, 1970, will not be required to pay a fee.

The syllabus of the course embraces theory, licence conditions, and morse instruction, and no prior knowledge is assumed or required.

There will be a Radio Amateurs' Examination Course on Wednesdays, 6.30-9 p.m., starting September 23rd. Enrolments: Wednesday and Thursday September 9th and 10th, and Wednesday, September 16th, from 6.15-8.15 p.m., Room 8, Acton Technical College, opposite Acton Town Hall, Acton, London, W.3.

Fee: For three terms, £3. Lecturer: W. G. Dyer, M.I.E.E., G3GEH

The Cove Further Education Centre (Hampshire) will be running a R.A.E. Course in mid-September. Further details may be obtained from P. D. Dimmick (Principal), Cove Secondary School, St. John's Road, Farnborough, Hants.



# Mullard puts the brakes on

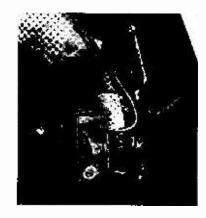


Mullard Ltd. recently announced details of a new car braking system using electronics. The system is designed to prevent a road wheel from locking when the vehicle driver applies too much force to the brake pedal. When a separate anti-lock control is used on each wheel, not only can full steering be available under maximum braking conditions, but shorter stopping distances result. The control circuit monitors wheel speed by means of a toothed mounted on the hub. A magnetic pickup fixed near this wheel supplies a pulse train to the control circuit. Pulse frequency is proportional to wheel speed and so contains all information necessary to deduce deceleration, acceleration and speed. The circuit senses the condition in which a wheel is likely to lock and if

this tendency continues, energises a hydraulic solenoid valve to relieve brake pressure.

Mullard Ltd. state that the whole system represents the result of a research project carried out at their Research Lab. and further development of parts of the system must be undertaken by car and brake manufacturers before the device can be applied to cars during their manufacture.

Pictures show the experimental circuit used for each anti-lock control and the anti-lock actuator inside the wheel.



# NEWS ... NEWS ... NEWS ...

# Bench vice for the radio shack

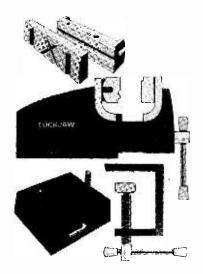
The Lockjaw is a bench vice announced by the Vice & Workholding Co. Ltd. The jaws give a remarkable capacity to grip difficult shapes and delicate objects. With its suction clamp and 'G' clamp, the Lockjaw is a very portable device. It can also be bolted down to a bench, and makes a very useful addition to the wineles 'shack'.

Grooves in the jaws enable a positive hold to be obtained when gripping washers, rods, printed circuits and components. Jawgrips are available with a rubber face for delicate work or silicon metal for harder usage. The silicon metal ones are supplied as standard. One jaw provides a rocking motion so that the face adjusts to work which tapers. If this jawgrip is turned round it is locked into a straight position.

The vice weighs under 4lb and the body is constructed of fine grain silicon alloy metal. It is claimed to hold as strongly as a typical cast-iron type eight times heavier. Jaw width is 4in and overall length closed 8in.

Price of the Lockjaw including silicon metal jaws is 86s. The 'G' clamp base is 30s and the rubberfaced jaws for delicate work 14s a pair. Manufacturers are: Vice and Workholding Co. Ltd., 149a Crayford Road, Crayford, Kent.





# Gravesend. . .

The above Club has now moved from King's Farm Community Centre, Gravesend, to new premises at the Northfleet Recreation Centre, Springhead Road, Northfleet, Kent, and meetings are held on Thursdays from 7.30 p.m. to 10.30 p.m.

They have taken larger premises as they are anxious to extend their membership and any person interested in Radio will be most welcome; there is no age limit.

Anyone interested in joining, should contact Allen J. Moules, after 7 p.m. weekdays at hometel. no. Gravesend 2965.

# I.S.W.C.

The International Short Wave Club will be pleased to send readers a copy of their bulletin International Short Wave Radio, if they would care to make application to them enclosing return postage. The address is: Mr. Arthur E. Bear, 100 Adams Gardens Estate, London, S.E.16.

# Audio 70

The date of the New Northern International High Fidelity Festival, at the Cairn Hotel, Harrogate, is September 18th-20th. Many well-known companies will be exhibiting.

# **Mobile Conference**

One of the first large scale conferences on the subject of mobile radio was held at Brunel University from June 30 to July 2. Organised by the Society of Electronic and Radio Technicians, it comprised eleven contributions from both industry and users. In his concluding address, Mr. J. W. Grandey (Gresham Lion) Chairman of the Conference Organising Committee, said that during his discussions with delegates he had been struck by the interest aroused by the contributions. He felt safe in saying that this Conference had been highly successful from every point of view; not least in bringing together over 120 representatives of all branches of this increasingly important field of electronics. The manufacturing industry was well represented as were the Home Office, Electricity and Gas Boards, Police and British Rail.

Most of the material presented at this Conference was new and had not previously received a public hearing. Many of the delegates were unaware of the work being carried out by various organisations, such as the Home Office, in looking to the future of mobile radio. Mr. E. W. Crompton proposed the adoption of a new system of modulation. double side band suppressed carrier, which appeared to provide two advantages, higher range and narrower bandwidth. Some of the recent work carried out by industry in providing new or better applications of mobile radio were also described. Mr. Welsh and Mr. Carey of Cossor proposed a system of vehicle location using phase measurement which had not previously been publicly described and Mr. N. C. Croft of Storno presented a paper on Automatic Extension Ringing from Vehicles.

One of the pressing problems in this rapidly expanding field is frequency availability. This kept cropping up in discussion and was dealt with at length by Mr. D. B. Balchin of the Ministry of Posts and Telecommunications.

# TRANSIST®R & D‡ODE

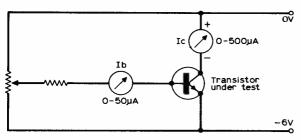
THIS TRANSISTOR AND DIODE TESTER IS THE FIRST OF A SERIES OF ARTICLES DESCRIBING A NEW LINE OF TEST EQUIPMENT. THE VARIOUS INSTRUMENTS, ALL IN MATCHING

CASES, WILL PROVE WORTHY ADDITIONS TO ANY WORKSHOP.

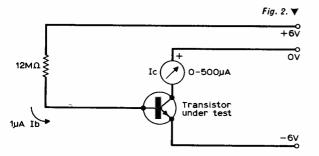
THE Transistor and Diode Tester to be described will rapidly check transistor leakage current and measure current gain (beta), over a range of collector currents, up to 5mA, for both n.p.n. and p.n.p. transistors. It is also suitable for checking semiconductor diode forward conduction and reverse leakage current. The tester is simple to build and contains only passive components.

# Circuit

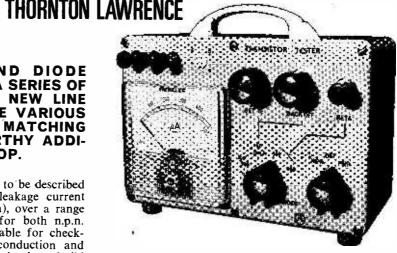
The d.c. beta, or  $h_{\rm FE}$ , of a transistor is the ratio of the collector current to the base current, beta =  $\frac{I_{\rm c}}{I_{\rm b}}$  A simple set-up for measuring beta is shown in Fig. 1 The base bias is adjusted to give a convenient value of Ic and the base current Ib, is read off and the calculation made.



▲ Fig. 1.

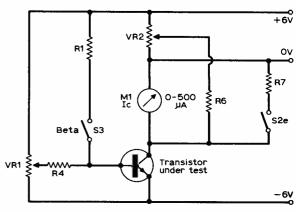


To avoid the necessity of reading Ib from a meter, the base could be fed with a known value of current, say  $1\mu$ A, from a known fixed supply voltage through a known value resistor, as shown in Fig. 2. The Ic, in  $\mu$ A, would then be a measure of the beta, e.g.  $60\mu$ A Ic would indicate a beta of 60.

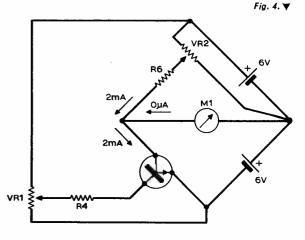


It is often useful to measure beta at different values of Ic, and a basic circuit for doing this is shown in Fig. 3.

In this circuit, R7 is a 5mA shunt for the 500 $\mu$ A meter and with S2e closed, the meter reads 5mA full scale deflection. If, for example, it is desired



▲ Fig. 3.



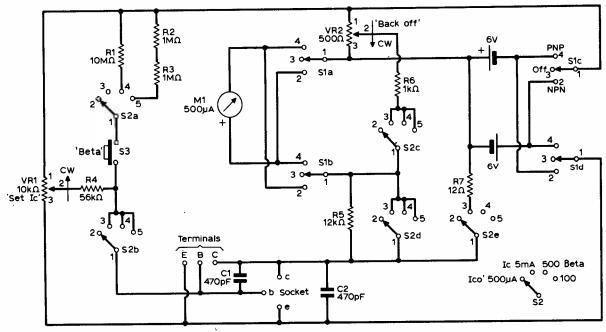


Fig. 5 : Complete circuit of the transistor and diode tester.

to test the transistor at 2mA Ic, VR1 is adjusted to provide sufficient Ib to give an Ic of 2mA, as indicated by M1 (accepting that VR2 and R6 have negligible effect on the accuracy of M1).

The current through M1 is then 'backed-off' by an equal and opposite current, provided by VR2 and R6, until M1 indicates zero. This action may be more easily seen if the circuit is redrawn in the form of a Wheatstone bridge as shown in Fig. 4.

With zero reading on M1, S2e is now opened,

# **★** components list

# Resistors:

R4 56kΩ

All ½W 5% carbon

VR1 10k  $\Omega$  potentiometer, wire-wound VR2 500  $\Omega$  potentiometer, wire-wound

## Capacitors:

C1/2 470pF disc ceramic

## Switches:

S1 2 wafers, each 3 pole 4 way, on Maka-Switch shafting unit (Henry's Radio)

S2 1 wafer, 4 pole 3 way, on Maka-Switch shafting unit (Henry's Radio)

S3 Push button (Micro Omron VAQ-40-45 (Henry's Radio)

# Miscellaneous:

M1, Meter, 500μA f.s.d. (Henelec MRA-65B Henry's Radio)

Die-cast box (Eddystone 6357P, Home Radio) Knobs (2-PK, 2-WK, Radiospares)

Terminals (3-Paignton PK 12K Home Radio)
Transistor socket. Handle. Plastic feet. Battery connectors

thus disconnecting the 5mA shunt and returning M1 to  $500\mu$ A f.s.d.

To read beta, S3 is closed and the known current, Ib, provided by R1, causes an increase in Ic which is indicated by M1. As previously mentioned, the value of Ib is chosen so that M1 gives a direct reading of beta.

The backing-off current feed resistor R6, has a slight shunting effect on M1, making the meter read about 550µA f.s.d. The value of R1 is therefore chosen accordingly and the facility of reading beta directly is retained.

The method of testing applies equally to p.n.p. and n.p.n transistors, although provision must be made to reverse the polarity of the supplies, and of course the connections to M1.

The complete circuit of the transistor tester is shown in Fig. 5, and here S1 is the 'PNP-NPN' switch which also has a centre 'off' position.

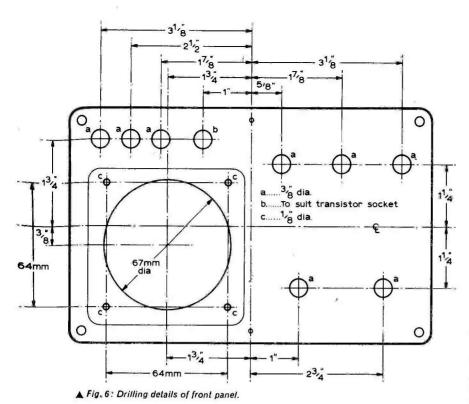
The function switch, S2, switches the meter shunt, R7, the backing-off feed R6, and allows for two ranges of beta 0-500 and 0-100 to be provided by switching two values of Ib through R1 and R2+R3 to the base of the transistor.

Diodes may be checked by connecting between the emitter and collector terminals, when forward and reverse current is indicated. The forward current is limited to  $500\mu A$  by R5.

# Construction

The transistor tester is built in a  $7\frac{1}{4} \times 4\frac{1}{2} \times 3$  in. deep Eddystone die-cast box, type 6357P. The lid of the box forms the front panel and the drillings for this are shown in Fig. 6.

The meter M1, is a Henrys 'Henelec' MRA-65A 500µA moving coil instrument. It should be noted that this meter is a later type to the 65 series illustrated in Henry's catalogue and has slightly different drilling requirements.

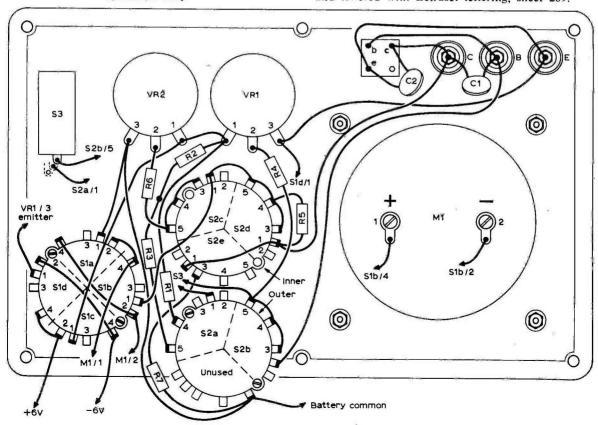


▼ Fig. 7: Wiring diagram of tester. The wafers of switch \$2 have been separated for clarity.

The switches are Radiospares Maka-Switch types and it is important for these to be assembled with the markings on the switch wafer facing the switch mechanism. No spacers are used between the wafers but a 6BA washer is fitted between the front wafer and the switch mechanism. The connections to the switch wafers are shown in Fig. 7.

The tester is powered by two PPI batteries and these fit into the die-cast box as shown in Fig. 8. A strip of polythene or similar material is required between the batteries to prevent an accidental short circuit between the battery connectors. Two 470pF disc ceramic capacitors. and C2, are connected across the transistor socket and terminals to prevent parasitic oscilla-tion of the transistor the transistor under test.

To give a good external appearance, the box is sprayed with one of the popular car enamel aerosols and lettered with Letraset lettering, sheet 209.



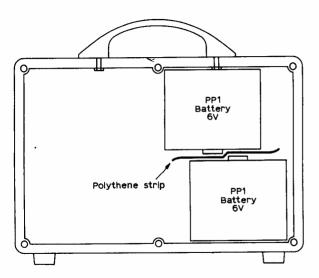


Fig. 8 : Positioning of the two batteries inside the case.

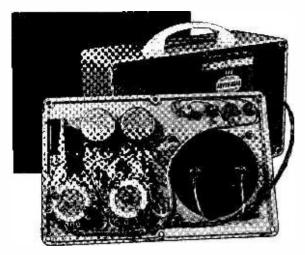
# Operation

1. Before connecting the transistor or diode, check the settings of the controls,

Set Ic fully anti-clockwise
Back off fully clockwise
Function Switch Polarity Switch to 'OFF'

fully anti-clockwise fully clockwise
to 'Ico''
to 'OFF'

- 2. Connect the transistor to the terminals or socket and switch to 'PNP' or 'NPN' as appropriate. The meter now reads 0-500μA of collector leakage current with the base open circuit (Ico'), at a collector voltage of 6 volts. If the meter reads full scale, the transistor is probably faulty and no further tests should be made. (Some very large germanium power transistors may have leakage currents of this order and may not necessarily be faulty. These are outside the capabilities of this tester.)
- 3. Set the function switch to 'Ic.'



Completed tester. Compare with the wiring diagram, Fig. 7.

- 4. Set the 'Set Ic' control for a suitable value of Ic. The meter reads 5mA f.s.d. For small a.f. and r.f. types 1-2mA is suitable, higher currents may be used for higher power types.
- 5. Adjust the back-off control for zero reading of Ic.
- 6. Set the function switch to 'Beta 500' or '100' and if necessary re-zero the meter with the back-off control.
- 7. Press the Beta button for a direct reading of beta.
- 8. Photo-transistors may be checked as normal transistors providing that they are not exposed to light. The sensitivity to light may be checked by setting the tester to Step 3 and alternately exposing and shielding the photo-transistor to and from light. The 'Set Ic' control should be set to minimum (anti-clockwise).
- 9. In the testing of semiconductor diodes, the cathode should be connected to terminal C and the anode to terminal E.
- 10. Set the function switch to Diode.
- 11. Set the polarity switch to 'FOR' for the forward conduction test. The forward current is limited to 500 µA.
- Set the polarity switch to 'REV' for the reverse leakage test. The reverse current, 0-500μA, is measured at 6 volts.
- 13. Switch OFF before returning the controls to the positions given in Step 1.

# Identification

A simple method of identifying p.n.p. or n.p.n. transistors is to insert the unknown type in the socket and temporarily short circuit the E and B terminals with a piece of wire. With the function switch at 'Ico',' turn the polarity switch to 'PNP' and then 'NPN,' the position which produces little or no current reading indicates the transistor type. The short circuit may then be removed and testing carried out in the usual way.

# P.W. BINDERS

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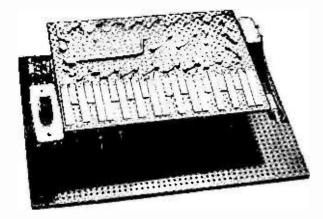
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signal is switched in by S1. The variable resistors VR1-VR25 are used to obtain the different notes.

If a simpler organ is required (without a tremolo), then R1-R7, C1-C4, Tr1 and S1 can be omitted. Similarly a one octave instrument can be built requiring only 13 variable resistors.

# Construction

The organ is built on two pieces of Veroboard—one with copper strips and one without. Before assembling any parts, the holes 'Y' should be drilled to clear 8BA. Beginning with the plain board, a

# P. M. DELANEY



THE small organ to be described in this article can be built in an evening. If it is built as described, then it will give two octaves, one above and one below 'Middle C'. Full constructional details are given, so that even a relative newcomer to electronics should find no difficulty in building this organ.

# Circuit

The organ consists of three sections, the circuit diagram being given in Fig. 1. Tr2 and Tr3 together form an astable multivibrator, tuned by VR1-VR25, R9, C5 and C6. It is sometimes difficult to make a transistorised multivibrator begin to oscillate. However, by the omission of the emitter bias resistor to Tr2, the necessary imbalance is produced.

The output transistor, Tr4, uses a transformer T1 for its load to match the speaker. A tremolo is provided by the low frequency oscillator Tr1, and this

keyboard can be made. Using  $\frac{1}{8}$ th inch 'Cir-kit' strip, a series of copper strips are laid out as shown in Fig. 2. Note that the corners of strips 2 and 24 are cut off slightly.

Next the variable resistors are fitted around the edge of the board, and VR23-25 are placed in the centre. To ease the task of tuning, these are angled back, so that the tags come through the holes indicated. Wires are now connected along the top as shown, and underneath from the wipers to the copper strips.

The wiper of VR1 goes by the wire numbered 1 to the note 1, etc. The notes 18 and 19 are connected on the top of the board. All the wires should be kept short and as close to the board as possible. A length of wire (about  $1\frac{1}{2}$  inches) is attached to the point Z.

The main part of the circuit can then be assembled. Firstly, the copper strips should be broken as indicated in Fig. 4. On the plain side of this board (Fig. 3), the connecting wires to the speaker, switch

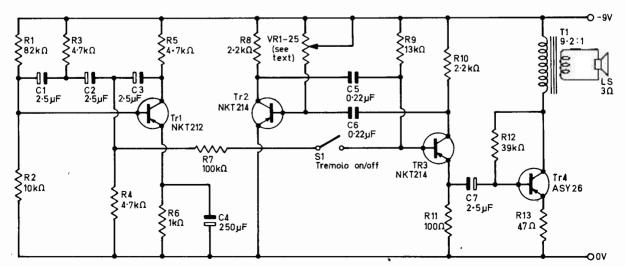


Fig. 1: Circuit of the mini organ. Tr1 provides the tremulo effect, Tr2-3 form the multi-vibrator oscillator and Tr4 the audio amplifier.

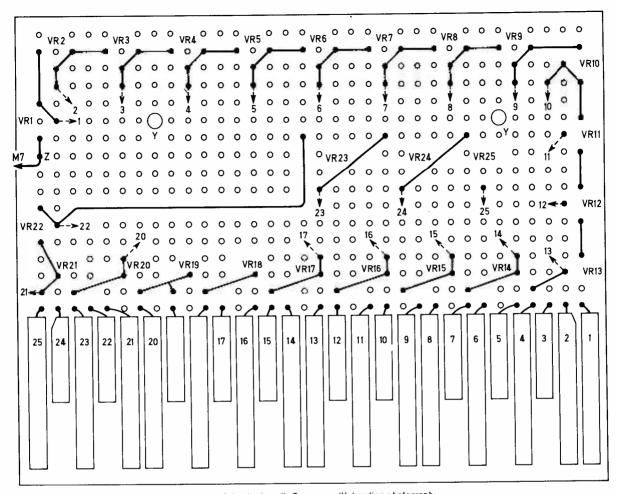


Fig. 2: Layout of the 'keyboard'. Compare with heading photograph.

and battery should be connected, and the wire from the point Z added.

The resistors should be added next, followed by the capacitors (except C4). The switch and the output transformer can then be fixed in place, along with the shorting links. If the transformer specified is used, then the fixing tags should be removed, and the transformer glued to the board, using Araldite (or a similar adhesive).

The four pins to the windings will fit directly onto Veroboard of 0.1 inch matrix—the secondary winding being nearest the edge of the board. Next the transistors can be soldered in. The base diagrams are given in Fig. 5. It is important to get the wires the right way round, and to use a heat shunt between the soldering iron and the transistor can. A pair of pliers held firmly on the wire being soldered will make an excellent heat shunt.

If C4 is not provided with an insulating sleeve



Close-up of some of the pre-set potentiometers which enable the organ to be tuned

around it, then one must be put on the emitter lead of Tr2, which passes underneath. C4 can then be fixed in place. The capacitors C5, C6, and Tr1, Tr2 and Tr3 should be laid against the board.

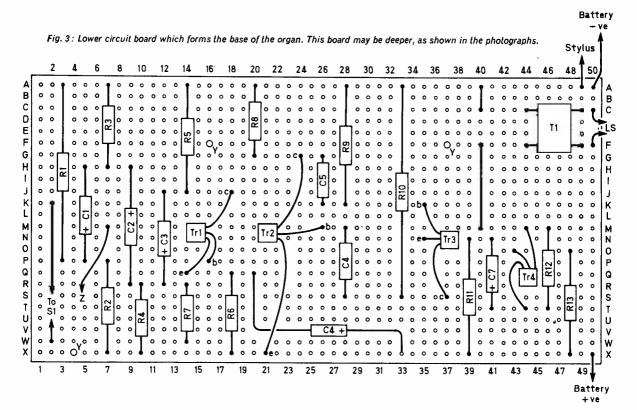
The stylus can be easily made from an old ball-point pen. The ball tip is removed, and the end soldered over—this removes the possibility of any ink coming onto the keys (see Fig. 6). The cut down body (about 4 inches) has a slot cut in one side at the end, and a wire passed through here, and soldered to the back of the metal part of the pen. This is then glued back in the plastic body, the wire pulled out through the slot, and the end cap replaced.

About a foot of wire is then left from the end cap to the point A49 on the Veroboard, to which the free end is fixed. The speaker is connected to the wires provided for it, and the battery leads connected to a suitable battery connector.

# Tuning

Each note is sounded by touching the stylus tip against the corresponding copper strip. The prototype was tuned using the services of a musician and a tuning fork. From the A of the fork, the top C was tuned (using VR1), then the notes 2, 3 and 4 tuned to be of equal intervals in pitch, until note 4 ('A') corresponds exactly to the tuning fork.

The rest of the tuning is completed in a similar



manner—getting equal intervals between successive notes. When completed, notes 1, 13 and 25 should be at octave intervals apart. If an alternative method is required, then the notes can be tuned to be of the same pitch as the corresponding note on a piano. The long strips of copper on the keyboard are equivalent to the white notes on a piano—the short strips to the black notes.

Whichever method is used, once a note has been

set it should be left—the tuning is incremental, so altering one note will affect all the notes below it in the chain. The values of the variable resistors used in the prototype should be used for the range suggested (VR1 and VR14-VR25 are 5k $\Omega$ , VR2-VR13 are 1k $\Omega$ ). Higher values would work of course, but tuning would become difficult. Once tuning is complete, the keyboard and switch should be bolted to the circuit board using 1-inch 8BA bolts.

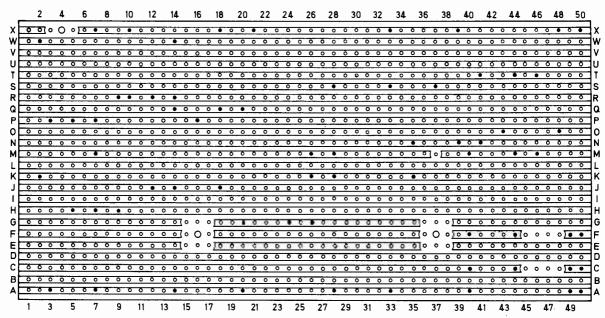


Fig. 4: The copper strips should be cut away as shown above before components are mounted on the lower circuit board.

# \* components list

			<del> </del>						
Resis	tors :								
R1	82k $\Omega$	R8	<b>2·2k</b> Ω						
R2	10k $\Omega$	R9	<b>13k</b> Ω						
R3	4·7kΩ	R10	2·2kΩ						
	4·7kΩ	R11	100 $\Omega$						
R5	4·7kΩ	R12	<b>39k</b> Ω						
R6	1kΩ	R13	47Ω ½W 5%						
R7	100kΩ								
All	resistors &W 5% ur	iless oth	nerwise noted.						
	,,								
VR1	, VR14 to VR25 (13	3 off) 5k	Ω						
	to VR13 (12 off)								
All	subminiature vertic	al skele	ton preset potentio-						
met									
Capa	citors :								
C1		<b>C</b> 5	0·22μF polyester						
C2	2·5μF 6V elec.	C6	0·22μF polyester						
C3	2.5µF 6V elec.	C7	2·5µF 6V elec.						
C4	250µF 6V elec.								
Semi	-conductors:								
	NKT212	Tr3	NKT214						
Tr2	NKT214	Tr4							
Misce	llaneous:		•						
Verd	oboard, 5 x 2½in, 0	.1in ma	trix, copper clad.						
	oboard, 3¾ x 2¾in,								
Cir-l	kit strip, 🖥 in, 5ft. o	card. Sr	nall slide switch.						
Out	out transformer, rat	io 9·2:1 (	(Radio spares T/T4)						
Spe	aker, 3 ohm. Ball	point po	en. 8 BA nuts and						
bolts.									

# Components

Although it is possible to use fixed value resistors in place of VR1-VR25, the tolerances of other parts (C5 and C6 in particular) make variables more satisfactory. The required values of resistance do not equal the standard preferred values anyway, and the extra cost is minimal. Suitable variable resistors are the series PN sold by Messrs Electrovalue.

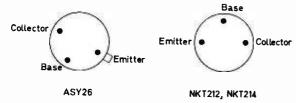


Fig. 5: Base diagrams of transistor connections.

The capacitors may, of course, be substituted by components of higher voltage rating. C1, C2, C3 and C7 could well be from the Mullard C426 series for instance. The speaker is specified only in its impedance (3 ohm), the size being unimportant. Because

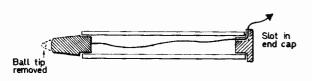
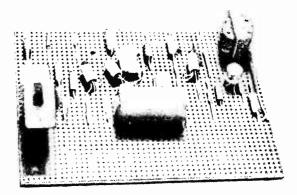


Fig. 6: Stylus made from a ball-pen.

of this no details for a case are given. 0.1 inch Veroboard is specified for ease of assembly, as VR1-VR25 and T1 have tags at multiples of this dimension.

It will be noted from the photographs that the piece of Veroboard used for the circuit board is larger than that specified—however the size specified is sufficient to accommodate all the parts. The total cost for a complete instrument should be under £5, a single octave instrument without tremolo would come to about £3,10.0.



Photograph of lower circuit board. Compare with Fig. 3.

# Alternative Circuits

As stated earlier, the tremolo can be omitted without affecting the rest of the circuit. The pitch of the instrument can be raised by decreasing R9 or C5 and C6. If C5 and C6 are made 0·1/µF, the instrument will play an octave higher than that described. The setting of VR1-VR25 will however be different, so a composite device is not really practicable. It is possible to use a higher impedance speaker (about 80 ohm) without a matching transformer. It will then be necessary to reduce, or possibly even omit R13. If required, a switch can be inserted in the negative battery lead. In use the organ will remain in tune even when the battery voltage falls from 9 volts to 6 volts, and having two octaves will play many simple tunes.

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THE need for a money-making game, for a Scout Coffee Morning, which was a little more sophisticated than the well tried 'Screweye along the bent wire', resulted in this digitally switched combination lock.

# **PRINCIPLE**

The principle of operation is that a code number. 0 to 7, is set up on a 3 pole 8 way rotary switch. The switch is connected in 1-2-4 binary form to a set of three toggle switches, each toggle switch corresponding to one pole of the rotary switch.

For the combination lock to be 'opened', it is necessary to set the three toggle switches (binary 1-2-4) to equal the code number set up on the rotary switch. A correct setting completes the circuit through the switches thus opening the lock. A table of binary—decimal equivalents is shown in Table 1.

If the code number is unknown, the chances of setting the toggle switches to the correct number,

S2	S3 (1)	S4 (2)	S5 (4)
0	0	0	0
2	Ó	1	0
3 4	0	0	1
5 6	1 0	0 1	1
7	1	1	1

TABLE 1

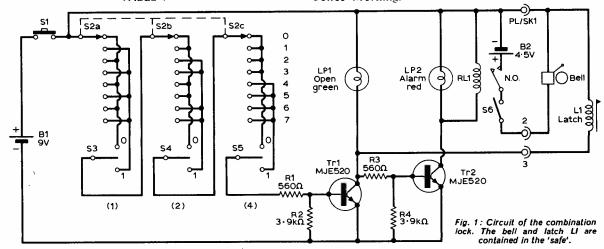
in one try, are 8:1 against. To improve these odds, for the player, it was decided to allow three attempts at any particular combination. The chances of winning are now 8:3 against, but having three attempts psychologically encourages the would-be safe-cracker to feel that the odds could possibly be in his favour.

JOHN STUART

Two indicator lights, red and green, are connected so as to indicate the failure or success of the attempt. However, this display on its own seemed a little tame for the effort involved and it was decided that a more dramatic 'failure' indication and an attractive reward for a successful attempt was required.

To satisfy these requirements, a mock 'safe' was built which had an electrically opening door and a suitably loud bell mounted on top. The general arrangement of the combination lock and safe can be seen in the photograph.

For the commercially minded, small chocolate bars were used as bait and we charged 3d. for three goes. About 35s. profit was made during one Coffee Morning.



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6/30L2 12/-	68H7 8/-	25Z6G 8/6	CV6 10/6	ECH35 5/9	TW4/500 6/-	PL302 12/-	U22 7/9	AA120 8/-	CG64H 4/-	OC70 2/8
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6AJ5 8/6	68Q7GT 7/6	30C18 14/-	CY1C 10/6	ECH84 7/6	KT44 20/-	PL508 27/10	U33 29/6	AC113 5/-	GD5 5/6	OC74 2/6
6AJ8 5/9	6887 4/-	30F5 16/-	CY31 7/6	ECL80 7/-	KT63 5/- KT66 17/8	PL509 28/9 PL802 15/-	U35 16/6	AC114 8/- AC127 4/8	GD6 5/6 GD8 4/-	OC75 2/-
6AK5 5/- 6AK6 6/-	6U4GT 12/- 6U7G 10/6	30FL1 13/9 30FL2 15/-	D1 1/8 D41 10/6	ECL82 6/6 ECL83 9/-	KT74 12/6	PL802 15/- PM84 7/9	U37 84/11 U43 7/6	AC128 4/-	GD9 4/-	OC76 8/6 OC78 8/~
6AK8 6/6	6U7G 10/6 6V6G 8/6	30FL12 16/-	D63 5/-	ECL84 12/-	KT76 12/6 KT88 34/-	PX4 28/6	U45 15/6	AC154 5/-	GD10 4/- GD11 4/-	OC78D 8/-
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6AT6 4/- 6AU6 5/-	7A7 12/6 7AN7 6/8	30L17 15/6 30P4 12/-	DD4 10/6 DF33 7/9	EF22 12/6 EF36 8/6	LN309 10/-	PY80 6/-	U76 4/8	AC168 7/6	GET103 4/-	OC82 2/3 OC82D 2/3
6AV6 5/6	7B6 10/9	30P4MR17/6	DF91 2/9	EF37A 7/-	LN319 13/9	PY82 5/8	U107 18/8	AC169 6/6	GET113 4/- GET116 6/6	OC83 4/-
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6BA6 4/6 6BE6 4/9	7C6 6/- 7D6 15/-	30P18 6/6 30P19 12/-	DF97 10/- DH30 15/6	EF40 10/- EF41 10/-	LZ319 6/6	PY301 12/6	U154 5/8	ACY17 8/-	GET119 4/-	OC123 4/6
6BG6G 20/5	7F8 12/6	30PL1 18/9	DH63 6/-	EF42 8/6	M8162 12/6	PY500 21/6	U191 12/6	ACY18 8/8	GET573 7/6 GET587 8/6	OC140 19/-
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6BX6 4/6 6BZ6 6/-	10D1 8/- 10D2 14/7	35Z4GT 4/9	DK96 7/- DL33 6/-	EF94 5/- EF95 5/-	N329 6/6 N339 25/-	R11 19/6 R12 7/6	U403 6/6	AF115 4/8	GEX13 8/6	OC812 8/- OCP71 88/-
6C4 5/-	10F1 15/-	35Z5GT 6/- 42 5/-	DL35 4/9	EF97 10/-	N359 9/6	R16 84/11	U404 7/6	AF117 4/6	GEX35 4/6 GEX36 10/-	ORP12 10/6
6C5GT 6/-	10F9 9/-	43 10/-	DL92 5/9	EF98 10/6	N369 18/9	R17 17/6	U709 4/9 U801 19/6	AF119 8/- AF121 6/-	GEX45 6/6	86M1 5/-
6C6 8/9	10F18 7/-	50B5 7/- 50C5 6/3	DL94 6/8	EF183 6/- EF184 6/-	N379 6/6 N389 12/-	R18 10/- R19 7/6	U4020 7/6	AF124 7/6	GT3 5/-	SM1036A10/
6C9 14/6 6C12 5/9	19FD12 6/9 10L14 7/8	50C5 6/3 50CD6G48/3	DL96 7/- DL810 9/6	EF804 20/5	N709 4/9	R20 11/9	VP13C 7/-	AF126 5/~	M1 2/10 M3 2/10	8T1276 10/- 8X1/6 3/6
6C17 12/6	10LD3 9/-	50L6GT 9/-	DM70 6/-	EFP60 10/-	P61 10/6	RG1-240A	VP23 5/- VP41 7/6	AF139 18/- AF178 18/6	MAT100 7/9	U14706 5/-
6CD6G 23/- 6CH6 7/-	10LD1110/- 10P13 18/-	52KU 14/6 53KU 14/6	DM71 7/6 DY86/87 5/9	EH90 7/6	PABC80 7/8 PC86 10/8	RK34 7/6	VR75 24/-	AF180 9/6	MAT101 8/6	XZ30 5/- Y548 3/6
6CL6 8/6	10P13 18/-	72 6/6	DY8 02 9/6	EL34 10/6	PC88 10/8	SP4 9/-	VR105 6/-	AF181 14/- AF186 11/-	MAT120 7/9 MAT121 8/6	Y728 3/6
6CW4 19/-	10P18 6/6	77 10/6	E80F 24/-	EL37 17/8	PC95 8/8	8P13C 12/6 8P42 12/6	VR150 6/-	AF186 11/- AF239 7/6	OA5 5/6	ZE12V7 1/9
E153 7/6	10PL12 7/-	J 78 4/9	E83F 24/-	EL41 11/-	PC97 8/6	· DI42 12/0	TOIR I			

60W4 18/- 10P18 6/6 77 10/6 E80F 24/- EL37 17/8 PC96 8/8 18P18C 12/6 VR150 6/- AF180 17/6 OA5 5/6 ZEIZV7 1/8 E018 7/6 10PL12 7/- 78 4/9 E83F 24/- EL41 11/- PC97 8/6 8P42 12/8 VT61A 7/- AF239 7/8 OA5 5/6 ZEIZV7 1/8 MATCHED TRANSISTOR SETS 1—0C44 and 2—0C45 8/6; 1—0C81D and 2—0C81 7/6; 1—0C82D and 2—0C82 8/6; Set of three OC83 (GET 118/119) 8/6; LP15 package (AC113, AC154, AC157, AA120) 10/8; Postage 6d. per set. S.T.O. 1 watt Zener diodes. 2.4v: 2.7v: 3.0v: 3.6v: 4.3v: 13v: 15v: 16v: 20v: All 3/8d. each.

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100×400×16mfd/275v 28; 100mfd/100v 5/6; 200mfd/350v 18; 200x/200×100×100mfd/350v 18; 200x/200×200×100mfd/350v 18; 1000mfd/300v 3/6; 20mfd/350v 18; 200x/200×100mfd/350v 18; 200x/200v 3/6; 200x/200×100mfd/350v 3/6; 200x/200v 3/6; 200

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# \* components list

Resistors:

R1 560 Ω R2 3.9k Ω R3 560 Ω R4 3·9 Ω

All 1W 5%

Semi-conductors:

Tr1/2 MJE520 Motorola (L.S.T. Components)

Switches:

S1 Single pole, push-to-make push switch

S2 3 wafers, each 1 pole 8 way, rotary

S3 Single pole, change over, toggle

S4 Single pole, change over, toggle

S5 Single pole, change over, toggle

S6 Single pole, on-off toggle

Miscellaneous:

LP1/2, Lamps 8V 0·2A m.e.s. RL1, Reed operating coil Type 1 with dry reed switch Type 10RSR (Radiospares). L1, Modified P.O. Type 3000 relay, 200 ohm coil. Bell, AC/DC 4·5V. Batterles, 9V PP9, 4·5V 1239 (Ever Ready).

# CIRCUIT OPERATION

The complete circuit is shown in Fig. 1. When the settings of S3, S4 and S5 are such as to equal the setting of S2, (correct combination), continuity exists between the rotor of S2a and the common connection of S5.

In this condition, the closing of S1 (push button) will cause +9 volts to be applied to the collector circuits of Tr1 and Tr2 and to R1.

This results in Tr1 conducting, causing the 'OPEN' lamp, LP1, to light and the latch solenoid, L1, to be energised, thus opening the safe door.

In the event of the setting of S3, S4 and S5 not equalling the setting of S2, (incorrect combination), there will be no continuity through the switch system.

In this condition, the closing of S1 will cause +9 volts to be applied to the collector circuits of Tr1 and Tr2, as before, but Tr1 will now be non-conducting.

This results in TrI collector being at approximately +9 volts, LP1 remaining unlit and L1 de-energised.

The positive voltage at Tr1 end of R3 causes Tr2 to conduct, lighting the 'ALARM' lamp, LP2, energising the reed relay RL1 and thus ringing the alarm bell.

A separate 4.5V battery, is used to drive the alarm bell, as 9V is rather excessive for the type of bell used. Switch S6 is included in the bell circuit so that the bell may be muted if the lamp indication only is required.



The layout of the components is not at all critical. The two transistors are boiled to the chassis to the right of the reed solenoid.

# CONSTRUCTION

The switch system, lamp batteries and other components are housed in a conventional aluminium chassis, size  $10\times6\frac{1}{2}\times2$ in. The layout of components is not critical and the general arrangement can be seen in the photographs.

The rotary switch, S2, does not have any positional markings on the knob, so as not to indicate the combination setting to the contestant and thus increase his chances of opening the safe.

The safe is built from in blockboard and could be scaled up or down to suit individual requirements.

The method of construction is shown in Fig. 2.

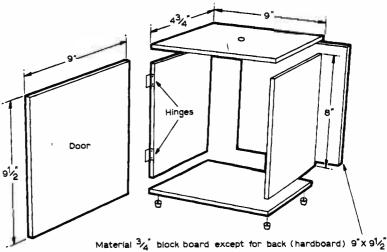
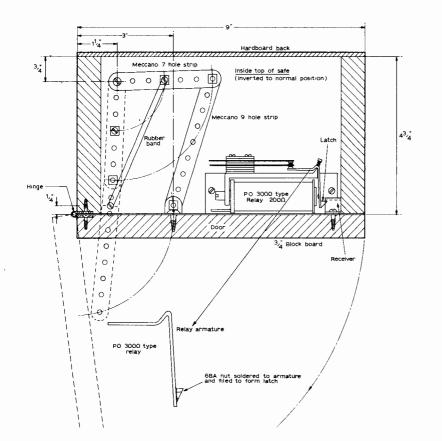


Fig. 2: Constructional details of the 'safe'.



The electrical latch is made from a Post Office type 3000 relay. The relay is modified by soldering a brass latch to the toe of the relay armature as shown in Fig. 3.

The relay is mounted on its side by either soldering the metal bobbin cheek to a brass backing plate or by using a suitable curved clip fitting over the relay bobbin.

The moving part of the latch is formed by a small angle bracket fixed on the side of the door.

The automatic opening mechanism is a crude but effective arrangement using two Meccano strips and a rubber band. The arrangement is shown in Fig. 3. It should be noted that the mechanism is on the underside of the top of the safe and that the drawing and photograph show how it appears when the safe is inverted.

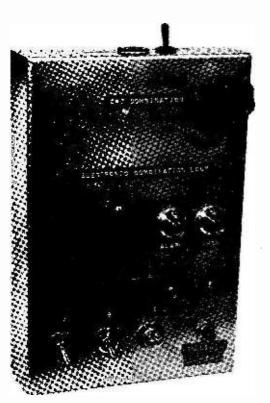
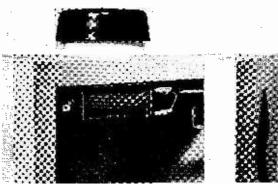


Fig. 3: (top) Details of the latch mechanism and relay modification. (below) photograph of completed control unit.



Close-up view of latch mechanism and door catch.

# **OPERATION**

- 1. Set Combination Switch S2 to any position.
- 2. Set bell switch S6 to 'ON' if bell is required.
- 3. Contestant sets S3, S4 and S5 to his choice.
- 4. Contestant presses S1, (OPEN or ALARM operates).

Note: \$2 must be changed to a new combination after each attempt or set of attempts, to obtain the desired odds.

# COMMENTS

Although the Electronic Digital Combination Lock is used as a game, an extension of the number of digits could form the basis of a commercial combination lock having an easy and rapid change of combination.



Good looks apart the ST.20 offers outstanding performance equal to amplifiers selling at two or three times the

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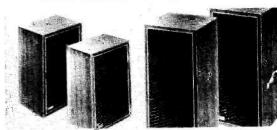
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F. C. Judd "Hi-Fi Sound" August 1970



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#### MONTHLY **NEWS FOR** DX LISTENERS

N the past it has always been thought that the summer months were a time when most enthusiasts had very little time for listening on the bands. The amount of mail that I have received in the last few months has convinced me that this is not so. I sincerely hope that this trend will continue

and reports will continue to pour in.

Because of the large number of reports that I now receive every month I have been forced to be more selective in choosing the material that I use. In the future I would be obliged if all reports gave accurate details of the station heard, such as frequency, time and programme details. Reports which conform to this requirement will stand a much better chance of being published.

When I started writing this column a year ago I said that it would be my policy to try and include as much material as possible from the more exotic stations. This is still my policy and with the large number of reports coming in I can select these more interesting stations. I will, however, continue to mention the more common stations, as I have found that among the beginners to the hobby who read this page there is a real demand for these easier stations.

#### Members Logging and News

Des Walsh of Little Baddow feels that all civilised countries should operate a short-wave service. He is particularly interested in the fact that the Republic of Ireland has no such service. He has tried to get them to start such a service but with no success. He would like all readers who are interested in this problem to write to Radio Telefis Eireann to ask them to start a short-wave service.

Malcolm Cheeseman of Llanberis in Caernarvonshire is using a 20-year-old Pye domestic receiver and a 24 foot vertical aerial and he logged the fol-

lowing stations:

7065 Radio Tirana, Albania at 1840

9625 Radio Israel at 2045 GMT.

11672 Radio Pakistan at 2005

11815 Trans World Radio, Bonaire at 0035

15160 Radio Ankara, Turkey at 2205

15345 Radio Kuwait at 1645

17890 HCJB, Ecuador at 2330

J. Trewick of London Colney has heard some very interesting stations in the last month:

11955 BBC Far Eastern Relay station with ident. at 1658 and at close down at 1815

15165 Radio Damascus, Syria at 1930 in English 15240 ABC Australia with news in Eng. at 2145 15320 ABC Australia at 2155.

R. F. Bruce of Angus in Scotland has an Eddystone 940 receiver and an indoor Joystick which

### THE BROADCAST BANDS

Malcolm Connah

#### Frequencies in kHz • Times in GMT

enabled him to hear:

5050 Radio Tanzania until sign-off at 2000

11735 Radio Morocco, English news at 1715

11955 BBC Far East Relay, ident. at 1815

15020 The Voice of Vietnam in English at 2000 15165 Radio Damascus, Syria, English news at

21690 WIBS, Grenada heard at 2100.

Stephen Wainwright of St. Helens has again used his Skyrover Mark II receiver and 100 foot longwire to good effect:

9625 Radio Trans Europe with test transmissions for the U.K. from 1345 to 1415.

15345 Radio Kuwait in English with news at 1830 Stephen also reports that HCJB are issuing QSL cards without requiring the information stated in this column in the June issue.

Roy Patrick of Derby sent in the following interesting information:

South Africa: Radio RSA broadcasts to the U.K. at 1800-1850 on 21480 and 15250, the former frequency gives the better reception.

Kenya The Voice of Kenya on 4915 is audible with a fairly good signal with a programme in Swahili at 1900.

Terry Gibbs of Swindon heard the following stations:

11800 Italian Broadcasting at 1930 to 2000

17860 ABC Australia at 2130 to 2230

21495 Radio Portugal at 2030 to 2100.

Regular reporter Geoffrey Gilham of London S.E.12 has been on holiday but still managed to send in the following log:

4865 Azores with talk in Portuguese at 2157

4870 Dahomey, vernaculars and music at 2137

4915 Ghana, talk in English at 2156

4940 Kiev. classical music at 1935

5058 Tirana, classical music at 2145.

Mervyn Winters of Co. Antrim used his AR88 and 12 foot whip aerial to hear:

9009 Israel heard at 2115

9560 Amman, Jordan, heard at 1600

11960 All India Radio, Delhi at 2015

15265 Radio Afghanistan at 1800

17855 NHK, Japan heard at 0700.

With apologies to all those reporters whose contributions I have not used I will end with a log from Glen Morgan of Tredegar:

3204 Ibadan in English at 2205

3380 Malawi, dance band music at 2025

4774 Libreville, African music at 2205

6540 Pyongyang in English at 1935.

Please note that by the time this article is published I will have changed my address and all reports should be sent to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex, by the 17th of the month.

T just isn't fair. Every month the contest types come last, so, just to show there's no hidden meaning in it, let's start off by seeing what's happening contest-wise. September 12-13th, WAE DX phone contest; 13th, 3.5MHz field day (go on, have a listen all you h.f. types); October 3-4th, u.h.f./ s.h.f. contest. The 10 metre phone contest on October 10-11th, should prove an interesting one, while for those not too far from London there is a lecture at the Institution of Electrical Engineers on the Trans-Arctic Expedition. You get a cup of tea, too!

P. Newman (Bucks.) reckons we ought to have a page of logs from home-brew equipment only. Start dusting the cobwebs off that old t.r.f. you built and get listening! I agree that there is a greater sense of achievement in bagging some good DX on a homebrew. (You wait until my 600 transistor receiver is finished—Cor, think of the gain.)

M. Bernstein (Lancs.) finds that the mornings are the best time for a listen on 14MHz. S. Ireland, down in Kent, is giving serious thought to building a 144MHz converter "to give Glyn Richards some competition." Steve also claims that the 5B4NZ heard on topband (Amateur Bands, August issue) was flying the Jolly Roger because the only recent licence in that area was 5B4ES. (Well shiver me

dipoles.)

In spite of a patchy period, Steve Ireland (Kent), HRO MX, 67ft. end fed, bagged these on 3.5MHz: CR6IV, CT1MC, CT2AK, OJØDX (Market Reef), PY3BAD, PY5XQ, PY7AF, UW9AF, VEØNEF/G5, VP8FL, VP8KF, ZB2BY, ZS5XA, 6W8DY, 9V1PP. Tuning h.f., a listen on 21MHz brought sigs from: AX9SS, AX9XI AX9AC, (Christmas Island), CT2AK, CX5BV, EA8BQ, EP2SW, HM5PF, HS1ACW, IS1DFO, KG6AAY, CR6CA, FHØVP, HM5PF, H KL7FBK, KP4CH, KR8BY, KR6HB, KV4FZ, KX6HW (Marshall Island), KZ5AM, LU2DAW, LXISD, MP4BFO, MP4MBB, OA8V, OD5BA, OX3LP, OJØDX, PJ9JR, PZ5RK, TA1TR, TU2CW, VP2VI, VP5HZ, VS6DO, ZB2BY, ZC4CB, ZE5JU. ZS6DH, 3V8AL, 5A5TH, 5B4ES, 5H3JL, 5N2AAE, 5V4JS, 5Z4MO, 6W8AL, 7Q7BC, 8P6BQ, 9F3USA, 9G1GD. Perhaps I didn't connect that antenna after

N. Sanderson (Edinburgh), CR45, 200ft. long wire went s.s.b. spotting on 14MHz. Stations observed: AX3XJ, AX2ARZ, AX4HA. AX7GK, AP5HQ, CE3BE, CR6M1, CA8FS, ET3DS, GB3GWC, AXØLD, CR7GJ, CT3SC DU1FH, EA8FS, GC3VJX/ OH5, HC2SO, HK3BCA, HR2HHP JA10WT, K7TGF, K5ARJ. K6ZDP, KA1KSO, KH6OR. KL7EBK, KP4DHV, LU2HC, LX1RC, OX5BL, PJ9HH, PY7ACQ, PZ1BW, OJØDX. SUIMA, Y/AC VOICĂ, VE/IS. TIVM, YAIEXZ, TEIGC VE2BEO, VO1CA W7IM, XE1YM, ZD8DB, ZE1DC TA2AE, VP7NA, VR6TC, W6TSQ, YB2AO, YK1AA, ZD8DB, ZE1DG, ZF1GC, ZS2OF, ZS6IK, 4U1ITU, 4X4QA, 5Z4UK, ZL4CX. 7**Q**7JO, 7X2SMA, 9M2PR, 9Q5MP, 9U5DP, 9Y4US. **R. Dinning** (Ayrshire), HA350, PR3OX, RQ10,

### THE AMATEUR BANDS David Gibson, G3JDG

#### Times in GMT Frequencies in kHz •

380ft. wire at 50ft., has spent a ten-week spell in hospital. It doesn't seem to have affected his skill with a receiver as his 21MHz log shows: CR7GJ, EP2SW, HR1SR/P/HR2, EL2DU, EL1CA. KS6DH, OHONJ, HS1ACW. KR6KB, IRØIJ, VU2IXP, W5YSL/P/DU1, TU2CS, OJØDX, ΥΒΦΒD, ZD9BM, 3V8AL, XW8DS, XW8DM, 5N2ABG, 5Z4GK. 4U1ITU, 5A5TH. 5H3JR. 6W8GE, 6Y5GB, 7P8AB, 9F3USA, 9L1GQ, 9M2VI, 9Q5WF, 9V1PP, 9X5AA.

A. Crooks (Leicester), RA1, PR30, 45ft, end fed, heard CR6IE, on 14MHz, CR6MX and 9G1GT on 28MHz while 21MHz s.s.b. brought: EL2L, HBQLL, PY2HY, PY7GAH, VU2KV, ZD8JK, 4Z4BG, 5N2AAE, 5U4JS, 9J2PV, 9U5DP.

J. Moore (Leicester) claims that topband, eighty and forty were a dead loss this month and bemoans time-base QRM on 160 from local tele's. I reckon that's the transmission of spurious signals, report

them to the GPO!

John's bets on 14MHz s.s.b. were: CR6EV, OX5AP, PY2ELT, UL7JG, VR6TC, ZP5CF. Fifteen produced: CE3OE, CR6LG, JA1TRL, VE3GJU, 4Z4DX, 8P6BQ. The gear is a CR100/2, a.t.u. and 130ft. end fed. Putting a home-brew f.e.t. converter in front and tuning 24.9-26.9MHz gave a.m.-type squeaks on 144MHz from: G2JF, G2BKC, G3VCV, G3DAH, G3TDR, G8VZ, G8CKT/P G3WRD. G3TXB. G8AXŹ, G8BJK. (Surrey), G8BPO, G8BYB, G8CIW, G8CQX, G8CRN, G8CUW, G8DAS, GC2FZC. The same band but s.s.b. raised: G2CIW, G3LQR, G3SOA, G6UW, PAOCML (near The Hague).

A Garex converter feeding a PR30 and CR7OA from an 8-element Yagi is located at Wendover and the controls titivated by N. Richardson. A peep at 144MHz revealed the following stations: G3AOS/P, G3LHO, G3LXP/P, G3PNA, G3PRM/P, G3TQF/P, G3UES/P, G3VPE/P, G6GN, G8BCQA, G8BDJ/P, GW3UCB, GW8ACG/P, G8CGX/P. GW3ITZ.

GW8BEB/P, GW8BHY/P.

V. Koopman (Lancs. but on holiday at Windsor), RA1, Joystick at 15ft., had some success on 7MHz (more success than I did I might warble). Dragged from the dreaded forty (still screaming) were: AX9XI, CR9AK, FP8CS, HS1ABO, JW8MI, KJ6CF, SVØWO, UK3ABA, VQ8CZ, VR6TC (Pitcairn Ísland, VS6DO, W2HCW, YA1SG, 7P8AB, 9N1MM—all on c.w. (splendid, splendid) except W, 7P8 and 9N1.

The same gear on 21MHz raised: CE6DP FO8BW, GM3MNM/MM near Capetown, IRΦXPS, JX8IL (Jan Meyen Island), KM6DQ, LU3AQ, TR8DG, VR2EK (Fiji), VR4EE, VU2BEO, ZD9BN,

9G1GD—all s.s.b.

Please note that the deadline for the month's logs is the 15th of each month, that is, they should reach me by the 15th. If they arrive later, they are too late for the current issue and "out of date" for the following one. So please slaves, letters to 5 Edward Close, St. Albans, Herts., before the 15th—Ta!

## THE COLUMN

S the evenings start to draw in, medium wave stations in North America can be logged as early as midnight. Among the first to be heard are an interesting group in Newfoundland right at the low frequency end of the band. There are three networks. The Canadian Broadcasting Corporation (CBC) operates CBT 540kHz in Grand Falls and CBN 640 St John's with satellites CBNA 600 St Anthony and CBNM 740 Marystown. There are two commercial networks. The Colonial Broadcasting System has key station VOCM 590 in St John's plus CHCM 560 Marystown and CKCM 620 Grand Falls. The Newfoundland Broadcasting Company can be heard on CJCN 680 Grand Falls, CJOX 710 Grand Bank and CJON 930 St John's. All these stations are logged regularly in the UK. Others from the same area include CFCY 630 Charlottetown Prince Edward Island; CFDR 790 Dartmouth Nova Scotia; CJCH 920 Halifax N.S; CHER 950 Sydney N.S; CHNS 960 Halifax; CKBW 1000 Bridgewater N.S. CBA 1070 Moncton New Brunswick; CBD 1110 Saint John N.B; CKCW 1220 Moncton; CKEC 1320 New Glasgow N.S; CKBC 1360 Bathurst N.B. Newfoundland Standard Time is 3½ hours behind G.M.T., the odd half hour being a help to station identification. The remaining Maritime Provinces are on Atlantic Standard Time which is 4 hours back. An unusual catch from this area which counts as a separate DX country, is Radio St Pierre 1375kHz in the French islands of St Pierre et Miquelon which lie to the south of Newfoundland. This station can often be heard when Lille 1376kHz signs off for the night at 2300 hrs G.M.T. The programmes from Radio St Pierre are in French and local time is 3 hours behind G.M.T.

Chris Stacev of Tunbridge Wells asks what sort of aerial is suitable for DXing on the Long Waves. At this OTH there is a 90ft long-wire at about 20ft above ground level and it performs very well when used with a CR100. Although a long outdoor aerial is an advantage on this band it is not essential. Dick Clark, a lw DXer in Florida USA has converted a standard m.w. loop for long wave use by increasing the number of turns from 7 to 20 and he regularly logs Europeans with it. Buzz from TV receivers may be troublesome with indoor aerials in some QTHs though this will disappear around midnight when the TV closes down. The long waves extend from 151kHz to 433kHz though only the section below 272kHz is in general use in Europe. There are some 50 Asiatics on this band situated in China, Mongolia, Turkey and asiatic USSR, and many can be logged in this country. Look for Ulan Bator 209kHz Mongolia; Tselinograd 227 Khazakistan; Dushanbe 254 Tadjakistan; Harbin 272 China; Ashkhabad 375 Turmenistan. Among semi-DX there is Tiflis 191 Georgia; Azilal 209 Morocco; Orenburg 300 USSR; Oulu 433 Finland.

Charles Molloy

# DON'T MISS THIS! WIN A DECCA (3000 SERIES) SUITE OF HIFT SEPARATES

AUDIO FAIR COMPETITION SPECIAL ENTRY FORM \*ONLY\*

IN THE **NOVEMBER** ISSUE OF

## PRACTICAL WIRELESS

ON SALE · OCTOBER 9TH.

GOING BACK...

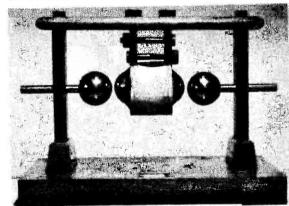
1970 60 50 40 30 20 COLIN RICHES ARTHUR DOW

THE first type of spark transmitting equipment used a simple aerial circuit which included the spark gap. The best type of radiator was found to be an elevated aerial but the spark gap in series with it provided a high resistance and naturally a damping action. Therefore, the discharge began at a high initial voltage which soon died away to zero. After some time, another spark discharge would take place but in the meantime, there was no radiation from the aerial.

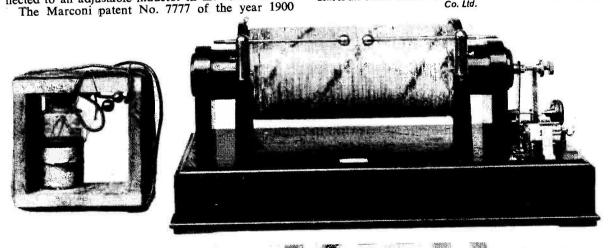
In the circuitry employing aerial coupling, the spark gap was included in a primary circuit; a separate tuned aerial circuit forming the secondary circuit. This latter was low resistance so that any oscillations induced could persist for a relatively long time before they finally died out. Thus for equivalent radiation compared with the plain aerial, the initial voltage would be lower, causing less strain on insulation but the increased radiation performance demanded less initial power. An added advantage was that the radiation covered a narrower waveband.

Marconi's first tuned transmitter (see photograph) was built in the year 1899. It comprised an oscillation transformer in the primary of which was a spark gap and capacitor. The secondary was connected to an adjustable inductor in the aerial circuit.

was based on this design. It covered the later forms of tuned apparatus without which the famous "Atlantic transmission" of 1901 would have been impossible. This patent clearly specifies the tuning of four circuits, i.e. spark gap circuit, transmitter aerial and primary and secondary of the receiving transformer.



Spark gap used by Marconi in his early experiments in the year 1895. Lent to the Science Museum, London, by Marconi Wireless Telegraph Co. Ltd.



Lent to the Science Museum, London, by Marconi Wireless Telepraph
Co. Ltd.

#### Radiograms 1922

"A wireless penny-in-the-slot machine has been invented in America. The invention consists of an automatic apparatus surmounted by a revolving loop aerial, and takes its power from the lighting circuit supply. When the coin is inserted in the slot two valves are switched on, and the music is heard through a large horn at the bottom of the instrument."...

"A racehorse in America has been equipped with a receiver and trained to race by commands from the trainer." . . .

"Suggestions are made in the non-technical Press that by means of piezo-electric crystals London could be lighted by means of its noise. Piezo-electricity is the property possessed by certain crystals whereby they generate electricity when subjected to vibration." . . .

"Experiments in the flying of a pilotless wirelesscontrolled aeroplane will shortly take place in France." . . .

"There are now 350 broadcasting stations in the United States." . . .

"Experiments to determine the feasibility of reception of wireless signals by the sense of taste have recently been carried out. Silver electrodes were used, one of which made contact with the inner part of the upper lip of the operator and the other with the tip of his tongue. Using four-stage amplification, it was found possible to detect signals and to tune in a station by noting when the intensity of the taste sensation was maximum. For messages to be read, the speed must not be greater than ten words a minute."...

"A wireless receiving set has been installed in Buckingham Palace." . . .

"Among the many thousands of people who listenedin to the Prince of Wales's broadcast speech to the
Boy Scouts of the nation were the blind soldiers of
St. Dunstans. Captain Ian Fraser, the blind chairman of St. Dunstans, has been an ardent wireless
experimenter for two years past, and in the course
of a short address following the transmission, he
stated that wireless telephony was opening a new
world for the blind. A blind man's hobbies were
limited, but wireless was one of those which he
could pursue just as well as anyone else. In listeningin, he was at no disadvantage to those who could
see."

"Direct wireless communication between France and New York was established the week before last from the great wireless station at Saint-Assise." . . . August 19, 1922.

"It is rumoured that some enterprising firm has brought out a clothes line which has a stranded copper centre for use in cases where landlords object to aerials." . . .

"Is the doom of the gramophone in sight? A firm is now advertising: 'Why not have your gramophone converted into a high-grade wireless receiving set?' . . ."

#### A Reader Comments

During my early youth I had access to current numbers of the old "Model Engineer" and was fired by the rather brief articles on radio then in its infancy; I was born in 1893. V. W. Delves Broughton had described his own installation which featured all the primitive means available at the time, and when I began work on the railway in 1909 most of my spare time was occupied with my own version of the bits and pieces, improvised from materials to hand; I had not then seen any "real" radio apparatus.

In 1910 I joined the Cadet Unit of the K.R.R's, and was soon learning Army Signalling; by extraordinary good fortune I was picked in 1913 to attend a Radio Course at Marconi House (evenings) and so became acquainted with the real thing. I saw the Fleming valve, its De Forest improvement, and listened on the Marconi Multiple Tuner and Magnetic Detector, which I soon duplicated in my own way at home. The big rotary generators and 10in. spark coils were rather out of my sphere, and the noise and space required were all too obvious. I do wonder if P.W. can come across any others who attended these Cadet Courses?

1914 found me in uniform seriously, putting my earlier signal training to practical use. As Signal Sergeant of my unit we dabbled on the fringe of radio but few infantry units had the opportunity to use it in action. I heard my first Radio speech when visiting Div. H.Q. just after the Armistice.

when visiting Div. H.Q. just after the Armistice.

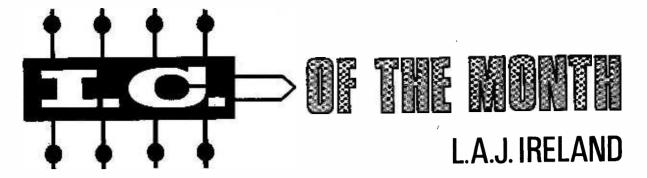
I obtained my first Radio Receiving licence in
November 1919 in the form of a letter from the
G.P.O., and have been a listener ever since.

In North London we formed the North Middlesex Radio Club, which had as the "motto" on the badge: "Listen before sending and so avoid jamming" and our Secretary, Mr. Savage of Winchmore Hill, was a fine enthusiastic character who did great work for us. I moved away to Stevenage in 1922 and found only one radio aerial in the locality, at the hamlet of Todds Green. My own soon went up—I had sold my 30 foot London mast to Arthur Burrows who later became a notable figure in Radio on the organising side; he was the Secretary of the International Organisation.

I had bought No. 1 of *The Wireless World*, and in due course followed with No. 1 of *Practical Wireless* and every other radio paper which appeared and disappeared; I am still faithful to *PW* which has given me much food for thought and had set a fine pattern, if not always "snooty" enough for some.

I am now approaching my 77th birthday, and still dabble, listening over most of the bands, broadcast and otherwise. I was able to do a bit in the Home Guard, and shared the consternation when on official orders we were not able to try out the C.52 sets issued and withdrawn almost at once. Of course I still read Morse, am a sort of unofficial honorary member of the Stevenage Radio Society, who keep the flag flying in this part of the country. But you can imagine I look back and think how very fortunate I was to get that Course of Instruction during 1913/14 at Marconi House when things were still in their infancy.

B. G. ASHMAN, (Stevenage, Herts.).



Number 12 Motorola MFC 4010P/Mullard TAA263 Utility Amplifier

HEN two separate manufacturers in two continents introduce very similar products within a short time, clearly a definite demand has been identified; and even a cursory examination of the circuit diagrams will establish the basic identity of the Motorola MFC4010P (and the Mullard TAA263) mentioned last month.

#### **Application**

The application is also clear, as a small signal utility amplifier or "gain block" for industrial or consumer electronic systems. This function is frequently required, so that an integrated unit which eliminates the chore of designing and assembling discrete transistor units will be very welcome.

# 1-5k 1-5k 7-120 02 3-3k 3-3k 7-120 03 1-5k 7

Fig 1: (a) Circuit of MFC4010P and (b) of the TAA263.

On this point of ubiquity, in the July 1970 Practical Wireless, page 195, C. F. Fletcher describes a hybrid transmitter modulator incorporating a "ring of three" direct coupled audio gain stage identical to the integrated units we deal with this month; the same issue features a reverberation unit with an acoustic delay system requiring small amplifiers in conjunction with the input and output transducers; finally there is an account of a light-operated switch indicating the application of a d.c. amplifier, a function for which this month's circuits are ideal. No doubt other issues of this magazine would contain a similar series of projects in which a small signal gain function is required.

#### **Performance**

The performance of the units extends from d.c. to greater than 1 MHz, a limit which is established by the stray capacitances in the circuit, which degrade gain and introduce phase shifts. However, this still permits the circuit to be described as a wide band unit, i.e., not limited to industrial applications in servomechanisms handling switching or d.c. levels, or to consumer applications in the audio field. It can function, for example, as a fairly effective video amplifier, and indeed, with suitable tuned circuits as an a.m. i.f. amplifier or even as a t.r.f. radio receiver.

One objection may be raised to the circuits as illustrated, Fig. 1. It may be claimed that the base-emitter junction of Tr2 effectively short-circuits

the collector of Tr1, and similarly with Tr3 shunting the output of Tr2. However, it should be remembered that the integrated circuit manufacturing process pre-supposes the use of silicon, and whereas in germanium transistors the 0.2 volts, typical of a baseemitter junction, would indeed bottom the proceeding stage, in silicon this junction establishes a potential of approximately 0.7 volts while the bottoming collector voltage is lower. The designers are quick to exploit this feature of the physics of silicon.

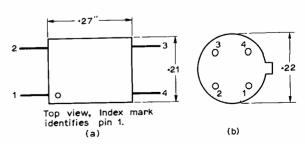
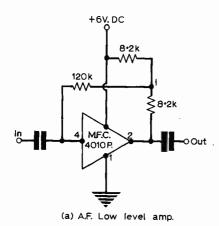
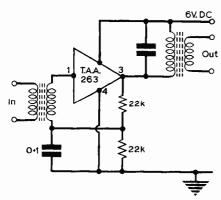


Fig. 2: (a) Connections of MFC4010P and (b) of TAA263.

In a practical application of a "ring of three" direct-coupled transistor amplifier subsystem, the operating conditions are set and stabilised by d.c. feedback, i.e. the base bias of Tr1 is drawn through a suitable resistor network from the output of the block.

Open loop voltage gain for both units is some 70 dB; it is usual to incorporate in the d.c. feedback loop some reactive elements (inductors or capacitors) to determine the amplifier passband and the actual gain realised.





(b) Tuned amplifier (R.F. or I.F.)

Fig. 3 : (a) Circuit as A.F. amplifier. (b) Circuit as R.F. or I.F. amplifier.

The cost of fabrication of a simple i.c. chip is only slightly greater than that of a good discrete transistor, and the yield, or fraction of satisfactory devices, is not much lower. Packaging is a different matter, though, since the typical i.c. requires more manual attention at this stage. Hence the advantage of this month's i.c.'s, in that both are supplied in simplified four terminal packages, requiring only signal input and output, and power leads.

Connection identification is possible by reference to Fig. 2, and the test circuits, Fig. 3, indicate the approach to the incorporation of one of these units

in an actual project.

Constructors may obtain the Mullard units from advertisers in this magazine, while the Motorola i.e. is in stock at the U.K. distributors: Celdis Ltd., 43-45 Milford Road, Reading, Berks.; or Semicomps Ltd., 5 Industrial Estate, Beresford Avenue, Wembley, Middx.



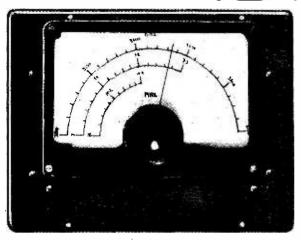
Practical Wireless are invited to submit articles for publication and to compete for the Practical Wireless "Designer's Trophy"

#### RULES.

- Articles submitted for the competition should conform to the general style of material published in Practical Wireless and must describe the operation and construction of a piece of radio, audio or test equipment that has been designed and built by the author.
- 2. Articles should, preferably, be typed using double spacing, leaving wide margins, and on one side only of each sheet. Circuit diagrams and any other drawings should be on separate sheets and numbered to agree with the text. Author's roughs must be clear enough to permit re-drawing. Component lists must also be separate and laid out to the standard PW format.
- Photographs of the equipment are desirable and should be in black and white, sharp and clear. Each photograph should be identified by sticking a piece of paper on the back rather than by writing on the photograph itself.
- Components used in the design must be readily available from retail sources.
- An entry form, properly completed, must accompany each article submitted. There is no limit to the number of articles submitted by any one author.
- 6. Articles must reach the Editor, Practical Wireless. Old Fleetway House, Farringdon Street, London, E.C.4. by the first post on Monday, November 2nd 1970 with the envelope and title sheet clearly marked "Project Autumn". A stamped, self-addressed envelope must accompany each entry.
- 7. All entries submitted will be considered by a panel of judges and the Editor's decision on all matters arising will be final. The Editor will require authors of winning entries to submit the equipment to him immediately on request for final assessment by the panel.
- 8. Employees and staff of Practical Wireless are not eligible for entry to this competition.
- The winner of the competition will receive and retain outright the Practical Wireless "Designer's Trophy 1970". Other prizes will be awarded to the best runners-up. Any article published will be paid for at normal rates.

## PAGE 437

## TRANSISTOR



THIS article describes a relatively simple transistor v.f.o. unit, suitable for use with most amateur transmitters. Its basic merits are an extremely stable, low drift characteristic for large changes in temperature, supply volts, and over long periods of time and almost constant amplitude output over the frequency range together with a cheap and simple construction.

#### Specification

The v.f.o., whose complete specification is given in Table 1, was given most stringent tests, particularly with regard to frequency drift and stability, all frequency measurements being made on a digital frequency meter with a discrimination of  $\pm 1$ Hz. The results of these tests are shown graphically in Table 2. From these curves it can be seen that even under extreme changes in parameters, the frequency drift was always well under 100Hz or better than 0.003%. As the tuning capacitor represents only a small part of the total capacitance, the oscillator only covers the required frequency range, that is 3.5 to 3.8MHz. This means a large open scale and



almost linear divisions in calibration. With a scale radius of  $2\frac{1}{4}$ in. (scale length of about 7in.) each 10kHz occupies approximately  $\frac{1}{4}$ in. Amplitude stability is maintained by an effective control circuit which does not employ a thermister with its attendant time lag. Supply is 24V d.c., though this is not at all critical, while the current drain is less than 50mA.

The complete unit is housed in an  $8in \times 6in \times 6in$  case, co-axial output being taken from the rear. The output impedance is extremely low, thus allowing the unit to drive transmitters having a wide range of input impedance.

#### The Circuit

The complete circuit diagram, together with component list is given in Fig. 1. Basically the circuit comprises a modified Butler oscillator with emitter follower output. Tr1 and Tr2 form the oscillator circuit with Tr3 as an emitter follower output. L1, VC1, VC2 and C1 determine the frequency of oscillation, the output from Tr2 being d.c. coupled to Tr3. This stage provides isolation between the oscil-

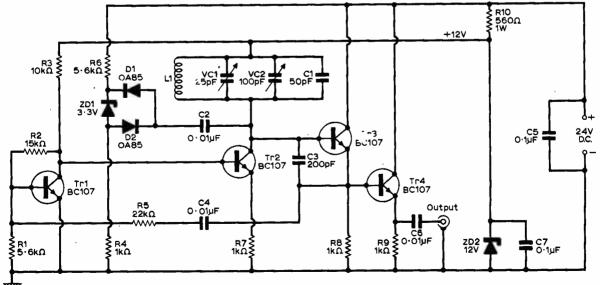
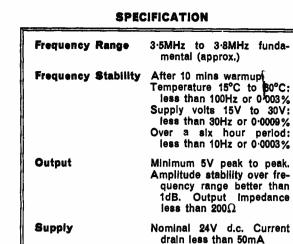
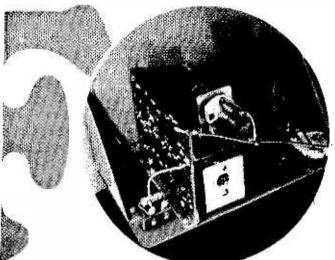


Fig. 1: The complete circuit of the transistor v.f.o. See components list for details of L1.



Dimensions



lator and feedback amplifier Tr1. The output developed across emitter load R8 is applied via the feedback components C4 and R5 to the base of Tr1. The output from this transistor is d.c. coupled back to the base of Tr2. Negative feedback is applied to Tr1 via R2 which, in conjunction with R1, determines the effective level of oscillator feedback.

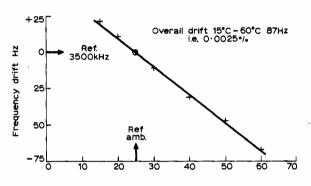
The output stage, Tr4, is also an emitter follower, d.c. coupled from the emitter of Tr3. This stage ensures isolation between the output and oscillator circuit and also provides a low output impedance, C6 providing d.c. blocking to the output terminal. Two levels of supply line are used, 24V and 12V, the 12V being obtained via R10 and ZD2. The output emitter followers are supplied from the higher voltage line, thus ensuring adequate signal swing without clipping and allowing d.c. coupling to be easily achieved.

The amplitude stabilization circuit is formed by components ZD1, D1 and D2. The oscillator output is coupled via blocking capacitor C2 to the diodes D1 and D2. The voltage across the zener diode ZD1 is maintained via the resistor dividers R4 and R6, these being connected across the main d.c. supply. The rectified signal output from diodes D1 and D2 is therefore constantly compared against the fixed zener voltage. Changes in oscillator level are converted to d.c. and simply registering as variations in zener current, the voltage across which is always constant and therefore provides a constant reference for the signal source. Decoupling of the supply lines is provided by C5 and C7.

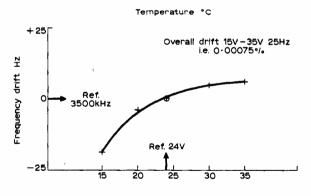
#### Construction

The construction of the v.f.o. is quite straightforward and can best be followed from the photographs shown. All components except the tuning and trimming capacitors, coil and C5, are mounted on a piece of Veroboard 4in. × 3in. The complete Veroboard layout is shown in Fig. 2. This is completed first and then fixed vertically on the chassis by means of a small aluminium bracket.

The chassis is simply an aluminium plate with a small right-angle lip bent along the front edge for fixing to the front panel. Side brackets, with lips bent in for fixing the front panel to chassis are



8in. x 6in. x 6in.



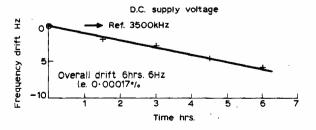


Table 1 (top): gives the specification of the v.f.o. while the graphs in Table 2 demonstrate the stability of the unit with regard to temperature supply voltage and time.

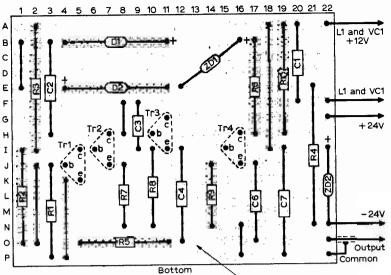
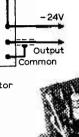


Fig. 2: (left) The component layout on Veroboard.

(Below) The layout of the v.f.o. can be clearly seen from this photograph and the heading illustration.



Looking at copper side of board, matrix. 0.15"

Break in conductor

also used as mechanical rigidity is of major importance for optimum frequency stability. Layout is clearly indicated in the photographs.

Also mounted on the chassis are the tuning capacitor, trimming capacitor and coil. The wiring between these components and the Veroboard is all of 18s.w.g. tinned copper and should be as short and direct as possible, mechanical rigidity again being of first importance. The output co-axial socket is mounted on a small bracket on the rear of the chassis and close to the Veroboard, thus ensuring

#### ★ components list

Resis	tors	:

R6 5.6k Ω 5.6k Ω  $1k\Omega$ R2 15k  $\Omega$ R7  $1k\Omega$ R3 10k  $\Omega$ R8 R4 1kΩ R9 1kΩ

22k Ω R10 560  $\Omega$  1 watt 10%

All resistors ½ watt, 5% except R10

#### Capacitors:

VC1 25pF air-spaced variable, ceramic mounting (Jackson Code JB/804/3·3/25)

VC2 100pF ceramic trimmer

50pF silver mica C1

0.01µF polyester 200pF silver mica

0.01µF polyester

C5 0.1µF polyester

0.01μF polyester

0·1μF polyester

#### Semiconductors:

ZD1 3.3V zener, BZY88-C3V3 Mul-Tr1 BC107 lard

ZD2 12V zener, BZX61-C12 Mullard Tr2 BC107

**BC107** D1 OA85 Mullard Tr3

**BC107** D2 OA85 Mullard Tr4

25 turns, close wound on 1½ in. diameter former, 18 s.w.g. enamelled copper wire

#### Miscellaneous:

Veroboard, 0·15in. matrix, 22 x 16 holes; Transistor heat sinks; Co-ax. socket; Two-way tag strip; Slow motion drive assembly; Chassis 8in. x 6in. x 6in. from H. L. Smith & Co, type W.

short output leads. On the outer side of the Veroboard is the two-way tag strip for the incoming d.c. supply, C5 is connected across these tags, thus decoupling the main supply at its entry point. The negative side of the supply is taken to chassis via the common fixing contact on the tag strip.

The front panel should be drilled to take the particular type of slow motion drive and dial assembly before being fixed to the chassis and side brackets. The tuning capacitor VC1 is mounted on a bracket of suitable height so as to engage with the slow motion drive shaft. This capacitor should be of the ceramic mounting type as with this circuit both sets of vanes must be isolated from chassis.

Holes should be drilled in the rear of the cabinet to allow for the entry of the co-axial plug and supply leads, these being taken through a grommet. While the size of the cabinet used by the writer is specified, being readily available, any similar type of case or cabinet which is already to hand may be used.

#### Calibration

The ideal instrument for calibrating the v.f.o. is of course a digital frequency meter. As such instruments are seldom available to the average amateur,

-continued on page 477

## Porgan pedal bass unit

#### PART 2

#### A. LESTER-RANDS

THE main note generator is a simple multivibrator, Tr1 and Tr2, Fig. 11, with the base of Tr2 taken to the negative rail via the tuning pre-set potentiometers PR1 to PR13 and VR1/R17 and R18. The pre-sets, PR1 to PR13, are used to tune the multi-vibrator to cover one complete octave in tempered scale from C (65Hz approx) to C (130Hz approx).

The potentiometer VR1 will shift the overall pitch up or down by a full interval (one whole note) so that the unit can be tuned instantly to instruments not tuned exactly to concert pitch. The output from the multi-vibrator provides the fundamental notes for the 8ft. pitch and is taken directly to the tone forming network C23, L1 and C24 which provides the 'flute' voicing. The capacitors C25 and C26, together with the resistors R40 and R43 provide the 'clarinet' voicing.

The output from the multi-vibrator simultaneously drives the divider circuit Tr3 and Tr4 which provides the fundamental notes for the 16 ft. pitch. The output from the divider is taken via the flute voicing

network R14, C10, R15 and C11 and then via S1 and R16 to the buffer amplifier Tr9. The voiced outputs from the 8ft. pitch voicing network are switched via S3 and R45 to Tr9 base. The switches S1 and S3 allow a choice of 8ft. flute (or clarinet with S4 closed) or 16ft. flute (or clarinet with S4) or both i.e., the 8 and 16ft. pitches combined.

The signal output from the buffer amplifier is approximately IV r.m.s. with the output gain control VR2 at maximum.

#### **Drum Brush Circuit**

The drum brush sound is generated when any pedal is depressed either momentarily or continuously. The brush sound begins with a medium degree of attack and decays away in approximately 1 second depending on the setting of the pre-set potentiometer PR14. A four notes per bar pedal bass will therefore produce a four beats per bar brush rhythm. The brush rhythm can be switched on or off as desired.

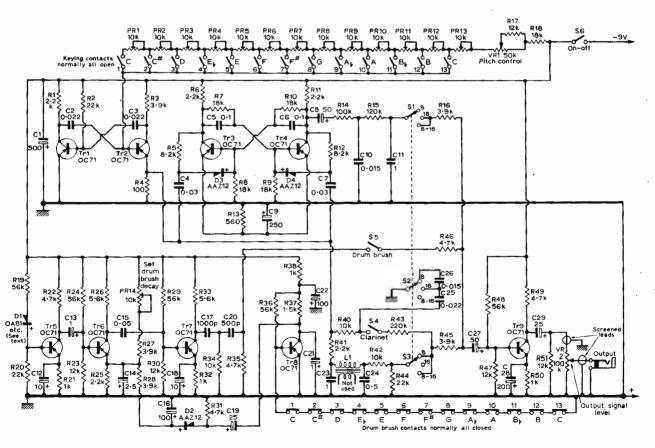


Fig. 11: Complete circuit of the Organ Pedal Bass Unit.

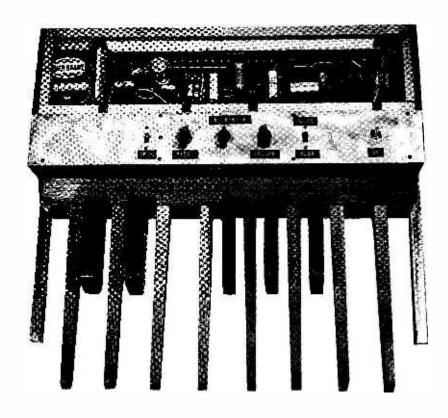
The circuit for the drum brush sound consists of a noise generator (D1, Tr5, Tr6, Tr7) and the attack/decay control circuit (Tr8). The choice of a diode for D1 may require some trial and error as a 'noisy' diode is required i.e., one that generates most noise when current is passed through it.

There should be at least 500mV of white noise from the collector of Tr7 (junction C17 and C20) with Tr6 conducting i.e., with PR14 at maximum resistance. An oscilloscope should display a typical spiky noise signal of about 1V peak to peak.

The function of the attack/delay control is as follows: — With PR14 set to maximum resistance constant noise should appear at the output of the unit. Adjust PR14 until Tr6 is just cut off in which case the continuous noise signal will cease. The function of Tr8 is to provide a positive pulse to

the emitter of Tro when any of the contacts 1 to 13 (drum brush contacts in Fig. 10 Part 1) are opened.

The control transistor Tr8 is normally cut off but conducts rapidly when any of the contacts 1 to 13 are opened. The result is a fairly large pulse at the collector of Tr8 which is rectified by the diode D2 and charges C16. The charge on C16 allows Tr6 to conduct instantly, thus initiating the 'attack' but the charge then dies away slowly via R28 and R25 thus providing the 'decay' of the brush noise. The decay time will be about 1 second with PR14 adjusted so that Tr6 is only just cut off. Decreasing PR14 resistance so that Tr6 is beyond cut off will produce a much shorter decay time to the brush sound.



Top view of the completed unit.

The total current consumption of the whole unit with any pedal depressed and the drum brush circuit switched on should not exceed 25mA. It is therefore quite economical to run the unit from a 9V (PP9) battery. There is no reason why a small mains unit should not be used but the smoothing capacitor should be at least  $5000\mu F$ , to keep hum level to an absolute minimum.

#### Circuit Boards and Panel Controls

The tone generator, divider and voicing networks are assembled on Board A as in Fig. 12. The preset tuning potentiometers PR1 to PR13 should be

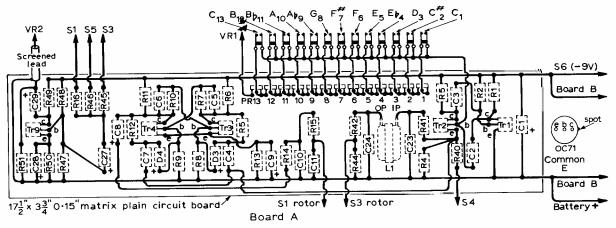


Fig. 12: Layout of circuit Board A for the tone generator, divider and voicing networks.

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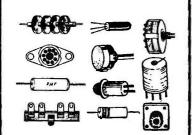
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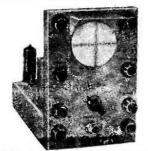
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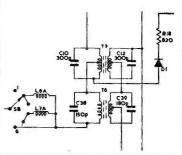
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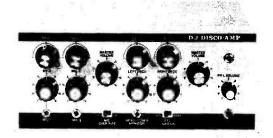
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## DISCOSOUND



#### D.J. DISCO-AMP

Designed specifically for use with discotheques and has many exclusive features not normally found on P.A. amplifiers. The unit will be of use to the professional D.J. as well as in clubs and mobile discotheques.

discotheques. A complete Pre-fade listen (P.F.L.) cueing monitor section is featured with separate input for headphones (either stereo or mono) with an independent volume control for headphone monitoring, and a P.F.L. switch, so that either turntable can be monitored for accurate cueing up of records. A mic over-ride switch is also added which cuts the music volume by half.

Specification: Output power 70 watts R.M.S. ± 1db at 8 ohms. Frequency response: 30-20,000 Hz ± 3db. Harmonic distortion: Less than 1% at full output. Signal/noise ratio: Better than 65db. Inputs: Mic 1 & 2 5 mV at 50 K ohms. Turntable 1 & 2 100mV at 1 meg ohm.

at I meg ohm.

50 ohm or 600 ohm mic inputs may be ordered at extra cost.

Size: Front Panel 16½in × 7in. Cut out 15½in × 6in. Fuses A.C.

1.5 amp (B.S.) mounted on back panel.

PRICE £85.0.0 inc. P & P.



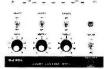
D.J. 102 DISCOTHEQUE MIXER PRE-AMPLIFIER

Consists of a 4 channel mixer each with its own volume control and a complete P.F.L. monitoring system. Also features a mixe cut down switch. For use with amplifiers having tone controls but not having the above facilities. Frequency response 20-20,000 Hz ± 2db. Distortion less than 1%. Signal to noise ratio better than - 65db. Size 10½in × 4in × 4in. Self powered.

PRICE £25.0.0 inc. P & P.

#### DJ 30L PSYCHEDELIC LIGHT **CONTROL UNIT**

3 channel light control unit that handles up to 1,000 watts per channel, Separate middle and controls for full frequency separation. Completely built and tested



PRICE £37.10.0 inc. P & P.



#### DISCOSOUND 40 PRE-AMP

The Discosound 40 offers the same specification as the D.J. Disco Amp without the power output stage. Size  $16 \text{in} \times 7 \text{in} \times 7 \text{in}$ . Self powered and ideal for use with the Discosound 100 Power Amplifier below and one of the outstanding features is that it capable of running ten of these Power Amplifiers (Total 1,000 watts)

PRICE £40.10.0 inc. P & P.

#### **DISCOSOUND 100 POWER** AMPLIFIER

A 100 watts RMS (8 Ohms) High Fidelity power Ampiner which utilises all silicon transistors of modular construction and features full automatic overload protection against short or open circuits. Frequency response: 20-20,000 Hz  $\pm$  2db. The High output is ideally suited for discotheques, groups, clubs, etc., or anywhere where reliability and quality are required. This unit is the companion model for use with our control pre-amp Discosound 40, or model for use with our control pre-amp Discosound 40, or can be used with any other high quality pre-amp control unit. Completely built and tested on steel Chassis.

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#### **DJ 70S** INTEGRATED MIXER-AMPLIFIER



One of the finest units available on the market today, regardless of price. The front end of the unit consists of a four channel mixer with separate inputs and volume controls, plus a separate basis, treble and master volume control. One of the main features of bis remarkable amplifier is its elaborate protection against short and open circuit and we can guarantee that it is virtually indestructable. Allied to this is its very high power output (70 watts R.M.S.) a frequency response (30-20,000 Hz  $\pm$  3db) that is superb, and distortion that is well below 1% even at full output. The unit is suitable for use with discorbeques, groups, P.A., clubs etc., or anywhere that high quality high output is required. Size:  $15\frac{1}{2}$  in  $\times$  5 in  $\times$  6 in.

PRICE £55.0.0 inc. P & P.

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Fig. 13: Details of the layout and wiring of the control panel.

#### \* components list

R1	tors :							
111	2·2k Ω	R14	100k Ω	R2	7 3·9k Ω		R40	10k Ω
R2	<b>22</b> k $\Omega$	R15	120k Ω		3 ·9k Ω			2·2k Ω
R3	3·9k Ω	R16	3.9k Ω		56kΩ			10k Ω
R4	100 Ω	R17	12k Ω		) 12k Ω		R43	
R5	8-2k Ω		18k Ω		4·7kΩ		R44	
R6	2·2k Ω	R19	56k Ω		2 1kΩ			3.9k Ω
R7	1 <b>8</b> k Ω	R20	22k $\Omega$	R3	5·6k Ω			4·7k Ω
R8	18k Ω	R21	1kΩ		10kΩ			12k Ω
R9	18k $\Omega$	R22	4·7k Ω		4·7k Ω		R48	
	18k Ω	R23	1 <b>2</b> k Ω	R3	56kΩ			4·7kΩ
	2·2k Ω	R24	56k Ω	R3	1 ·5k Ω			1kΩ
	8·2k Ω		2·2k Ω	R3	l 1kΩ			12k Ω
R13	560 $\Omega$	R26	5·6k Ω	R39	Not requir	ed		
	itors :			_			. =	
Canac				ntiometer, log.				
C1	500µF (elec)		C11	1μF (paper)		C21	1μF (elec)	•
C2	0.022 <i>u</i> F			10μF (elec)				
-							100000 100	
C3	0·022µF						100µF (ele	
C3 C4	0·022μF 0·03μF		C13	1μF (elec)		C23	1μF (pape	
C3 C4 C5	0·03μF 0·1μF		C13 C14			C23 C24	1μF (pape 0·5μF	
C3 C4 C5 C6	0·03µF		C13 C14 C15	1μF (elec) 2·5μF (elec) 0·05μF		C23 C24 C25	1μF (pape 0·5μF 0·022μF	
C3 C4 C5 C6 C7	0·03μF 0·1μF 0·1μF 0·03μF		C13 C14 C15 C16 C17	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 1000pF (cer)		C23 C24 C25 C26	1μF (pape 0·5μF 0·022μF 0·015μF	er)
C3 C4 C5 C6 C7 C8	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec)		C13 C14 C15 C16 C17	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 1000pF (cer)		C23 C24 C25 C26 C27	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec	er) e)
C3 C4 C5 C6 C7 C8 C9	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec) 250μF (elec)		C13 C14 C15 C16 C17 C18 C19	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 1000pF (cer) 10μF (elec) 25μF (elec)		C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF	c) c)
C3 C4 C5 C6 C7 C8 C9	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec)		C13 C14 C15 C16 C17 C18 C19 C20	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 10υμF (elec) 10μF (elec) 25μF (elec) 500pF (mica)		C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)
C3 C4 C5 C6 C7 C8 C9 C10	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec) 250μF (elec) 0·015μF		C13 C14 C15 C16 C17 C18 C19 C20	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 1000pF (cer) 10μF (elec) 25μF (elec)	ast 12VW	C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)
C3 C4 C5 C6 C7 C8 C9 C10	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec) 250μF (elec) 0·015μF conductors :		C13 C14 C15 C16 C17 C18 C19 C20	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 1000pF (cer) 10μF (elec) 25μF (elec) 500pF (mica) capacitors at le	ast 12VW	C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)
C3 C4 C5 C6 C7 C8 C9 C10 Semi-	0.03µF 0.1µF 0.1µF 0.03µF 50µF (elec) 250µF (elec) 0.015µF conductors :	. D2, 3, 4 A.	C13 C14 C15 C16 C17 C18 C19 C20 All	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 100μF (elec) 10μF (elec) 25μF (elec) 500pF (mica) capacitors at le	ast 12VW	C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)
C3 C4 C5 C6 C7 C8 C9 C10 Semi- Diod Tr1—	0·03µF 0·1µF 0·1µF 0·03µF 50µF (elec) 250µF (elec) 0·015µF conductors : les D1 (see text) -Tr9 OC71	. D2, 3, 4 A	C13 C14 C15 C16 C17 C18 C19 C20 All	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 1000pF (cer) 10μF (elec) 25μF (elec) 500pF (mica) capacitors at le	ast 12VW	C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)
C3 C4 C5 C6 C7 C8 C9 C10 Semi- Diod Tr1—	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec) 250μF (elec) 0·015μF conductors : les D1 (see text) -Tr9 OC71 hes :		C13 C14 C15 C16 C17 C18 C19 C20 All	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 100μF (elec) 10μF (elec) 25μF (elec) 500pF (mica) capacitors at le	ast 12VW	C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)
C3 C4 C5 C6 C7 C8 C9 C10 Semi- Diod Tr1— Switcl	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec) 250μF (elec) 0·015μF conductors : les D1 (see text) -Tr9 OC71 hes : 2, 3 3 pole, 3 w	ay, ganged w	C13 C14 C15 C16 C17 C18 C19 C20 All AZ12 (M.	1μF (elec) 2·5μF (elec) 0·05μF 100μF (elec) 100μF (elec) 10μF (elec) 25μF (elec) 500pF (mica) capacitors at le	ast 12VW	C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)
C3 C4 C5 C6 C7 C8 C9 C10 Semi- Diod Tr1- Switcl S1, 2 S4, 5	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec) 250μF (elec) 0·015μF conductors: les D1 (see text) -Tr9 OC71 hes: 2, 3 3 pole, 3 w 5 Single pol	ay, ganged w e, on-off, slide	C13 C14 C15 C16 C17 C18 C19 C20 All AZ12 (M. (M	1μF (elec) 2·5μF (elec) 0·05μF (elec) 100μF (elec) 10μF (elec) 25μF (elec) 500pF (mica) capacitors at le ullard) ullard)	ast 12VW	C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)
C3 C4 C5 C6 C7 C8 C9 C10 Semi- Diod Tr1— Switcl	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec) 250μF (elec) 0·015μF conductors: les D1 (see text) -Tr9 OC71 hes: 2, 3 3 pole, 3 w 5 Single pol	ay, ganged w	C13 C14 C15 C16 C17 C18 C19 C20 All AZ12 (M. (M	1μF (elec) 2·5μF (elec) 0·05μF (elec) 100μF (elec) 10μF (elec) 25μF (elec) 500pF (mica) capacitors at le ullard) ullard)	ast 12VW	C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)
C3 C4 C5 C6 C7 C8 C9 C10 Semi- Diod Tr1— Switcl S1, 2 S4, 5	0·03μF 0·1μF 0·1μF 0·03μF 50μF (elec) 250μF (elec) 0·015μF conductors: les D1 (see text) -Tr9 OC71 hes: 2, 3 3 pole, 3 w 5 Single pol	ay, ganged w e, on-off, slide	C13 C14 C15 C16 C17 C18 C19 C20 All AZ12 (M. (M	1μF (elec) 2·5μF (elec) 0·05μF (elec) 100μF (elec) 10μF (elec) 25μF (elec) 500pF (mica) capacitors at le ullard) ullard)	ast 12VW	C23 C24 C25 C26 C27 C28	1μF (pape 0·5μF 0·022μF 0·015μF 50μF (elec 200μF (elec	c) c)

mounted at an angle or side by side so that the adjustment slots can be reached with a small screw-driver from the back of the case.

Connection from the tuning pre-sets PR1 to PR14 to their respective contacts are also shown in Fig. 12 together with connections to the panel controls VR1, VR2, S1, S3, S4, S5 etc.

The control panel assembly and wiring is shown in Fig. 13. Note that some components such as R43, C25, C26, R17 and R18 are wired between controls.

Mention has already been made regarding the drum brush circuit and adjustment for long or short decay. The choice is for the user but should the sound level appear too high, then the resistor R46 (4.7K) should be increased until the required balance between drum brush and bass notes is achieved.

Before tuning set the wipers on the pre-sets PRI to PRI3 to midway, set the 'pitch' control VRI also to midway position and then begin tuning with PRI3 which will tune the highest C note. If possible the

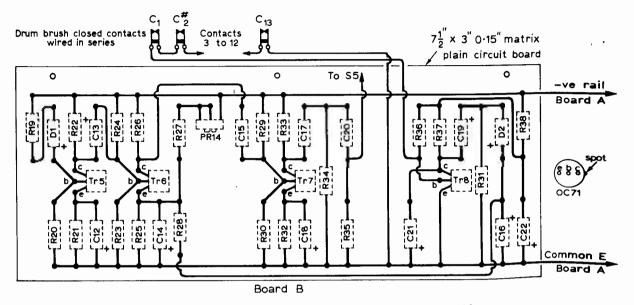


Fig. 14: Circuit Board B containing the noise generator and control amplifier.

The control panel is mounted on the top of the case framework at the front (see Fig. 8 and Fig. 9 Part 1).

The drum brush noise generator and control amplifier is assembled on Board B as shown in Fig. 14. Connections to S5 and the drum brush contacts are also shown.

Board B is mounted toward the rear of the unit on the lower cross members of the case in the position shown in Fig. 8 Part 1. Board A is mounted toward the front of the case as in Fig. 8 Part 1. Board B should be situated to the left of the case (looking from the rear) so as to leave enough space for the battery. The output jack can be mounted on a small aluminium panel as shown in the photograph in Part 1.

#### **Checking and Tuning**

If an oscilloscope is available the waveform from the multi-vibrator Tr1-Tr2 can be checked at the junction of R4 and the collector of Tr2 and from the divider at C8-R14. The function of the drum brush circuit can be checked at C20-R35. The voiced waveforms can of course be checked at the output socket and those for flute should appear nearly sinusoidal. Wth the 'clarinet' switched on a small pulse will be superimposed on the flute waveform and the audible tone will be slightly 'reedy'.

With 8 + 16 pitch the respective waveforms will combine and the 8ft. waveform will appear to sit on top of the 16ft. waveform. Audibly, the 8ft. and/or 16ft. pitch with flute voicing should have a round deep tone.

tuning should be done with the aid of an electronic organ with bass by tuning each note on the pedal unit to zero beat. Failing this, tune with a piano and use the zero beat method for each note. Start with the highest C (PR13) and tune each note going down using 8ft. pitch and flute voicing. The tuning will maintain itself for a long time but should be checked occasionally to ensure perfect pitch.

#### Final Assembly

The covers for the top, back and base can be made from hardboard cut to fit over the framework. Make a cut-out where the battery goes in and a small separate panel to secure the battery in place, Fig. 15. The covers should be screwed on so as to allow quick access to the pedal contacts and circuit

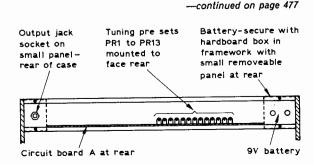
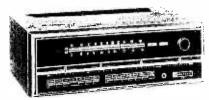
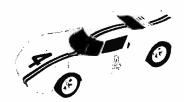


Fig. 15: Arrangement at rear of unit.

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The previous article (Part 1) dealt with the cabinet and main chassis assembly and with the function of the pre-amplifier and tremulant circuitry. The full circuit for the pre-amplifier was included (Fig. 5 Part 1) which should be used in conjunction with the various assembly details given in this article.

The pre-amplifier and tremulant control circuit is divided into three sections each having its own circuit board as in Figs. 6, 7 and 8. Before dealing with these however, it is advisable to construct the small separate assemblies such as the panel tremulant indicator lamp, the l.d.r. mounting, its control lamp and cover, and the mains input socket panel which is fitted at the rear of the cabinet.

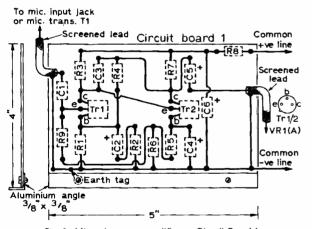


Fig. 6: Microphone pre-amplifier on Circuit Board 1.

With these done and the front panel drilled ready for the controls etc. the circuit boards can be made and wired and the whole amplifier finished off ready for testing.

The panel tremulant lamp unit is simple to make and requires only an m.e.s. batten lampholder mounted on a bracket as in Fig. 9. This is fitted to the chassis with self tapping screws in the position shown Fig. 13, so that the lamp 'looks' through the hole provided as in the front panel layout diagram. A piece of coloured celluloid is glued over the hole, inside the panel, to enhance the appearance.

When the tremulant circuit is operating, this lamp flickers at the tremulant speed and its brilliance varies according to the setting of the tremulant depth control. The l.d.r. is mounted on a small piece of s.r.b.p. attached to a chassis fixing bracket as in Fig. 10. Its control lamp B2 is mounted in a dial light holder (m.e.s.) as shown in the same diagram. The two assemblies are secured to the chassis with self tapping screws so that the lamp is level with the l.d.r. and approximately \$\frac{1}{2}\$ in, in front.

and approximately  $\frac{1}{8}$  in. in front.

The l.d.r. cover is shown in Fig. 11 and this is simply fitted over the l.d.r. and its lamp and secured to the chassis with self tapping screws. This cover keeps any external light off the l.d.r. and is useful when the amplifier is being tested out of the cabinet,

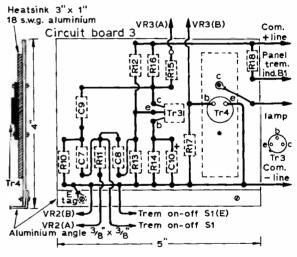


Fig. 8: Phase shift oscillator and LDR control amplifier, Circuit Board 3.

where light could reach the l.d.r. and alter its operating range.

The remaining small assembly is the 3-pin mains input socket which requires only a panel as in Fig. 12. This assembly is fitted at the back of the cabinet as can be seen in the photographs.

#### **Pre-amplifier Circuit Boards**

These are numbered 1, 2 and 3 and are located on the main chassis as in Fig. 13. Boards I and 3 are 5 x 4in. plain s.r.b.p. with 0-1in. matrix and Board 2 is 5 x 7in. of the same material. Each board is mounted on  $\frac{3}{8}$  x  $\frac{3}{8}$ in. aluminium angle which secures the board to the chassis (self tapping screws).

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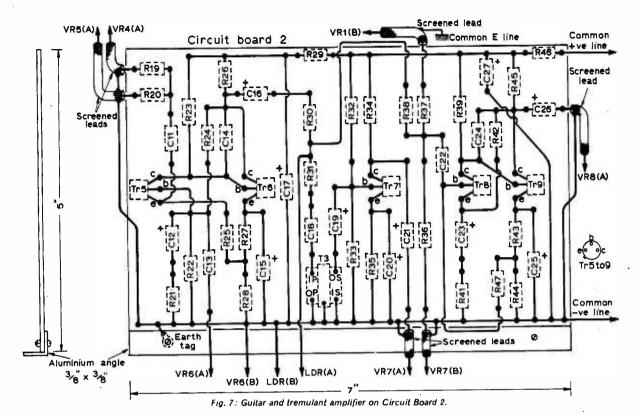
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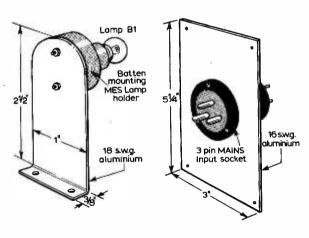
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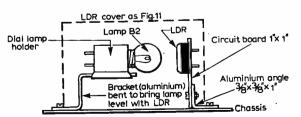
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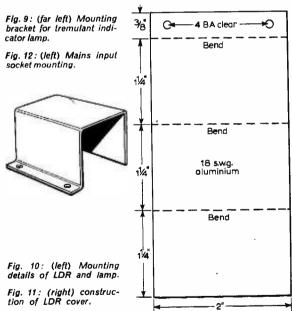






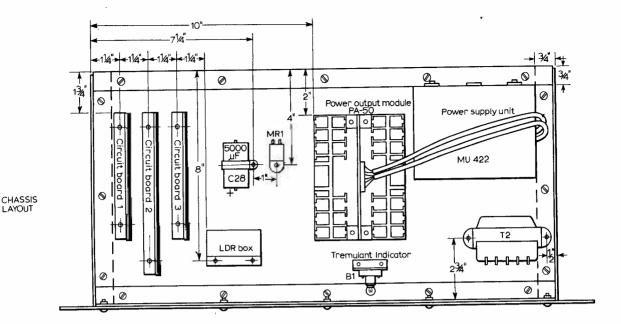
Board I contains the microphone pre-amplifier Tr1 and Tr2 and it is most important that the screened leads are earthed to the common earth line as shown.

Board 3 contains the tremulant phase shift oscillator Tr3 and the l.d.r. control amplifier Tr4. Note that the earth returns from VR2 and the tremulant



on-off switch must be made as shown, to the common earth line on the circuit board, and to nowhere else. The l.d.r. control amplifier Tr4 must be fitted with a small heatsink as shown in Fig. 8.

The guitar and tremulant amplifier board (Board 2) has several screened lead connections and again it is important that these are earthed, as shown, to the common earth line on the board, as must the earth return from the l.d.r. (l.d.r-B).



FRONT PANEL LAYOUT

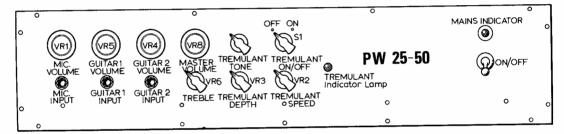


Fig. 13: Layout of panel controls and main components on top of chassis.

The coupling transformer T3 is bolted directly to the circuit board and is a type CP6713/2. It has the IP-OP and IS-OS connections clearly marked on it and these must be connected as in the diagram.

#### Pre-amplifier Power Supply

It is not convenient to take the supply voltage for the pre-amplifiers from the output module power supply as this is a sealed unit. Transformer T2, the rectifier MR1 and smoothing capacitor C28 form the pre-amplifier power supply and are wired as shown in Fig. 14.

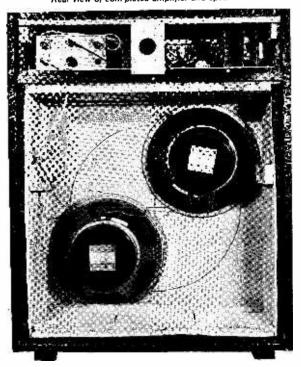
The reason for locating T2 at the far end of the chassis is to prevent the tremulant amplifier transformer T3 from picking up mains hum by mutual coupling. The mains transformer T2 has three secondary tappings but only the 17V tap is used.

#### **Chassis and Panel Layout**

The positions of the circuit boards, the pre-amplifier power supply components, the power module and the module power supply are given in Fig. 13. It is most important to adhere to this layout to prevent hum loops around the chassis.

Points for the fixing holes of the power output module and its power supply have not been included as prototype units were used by the writer for the original amplifier. Fixing holes are however, provided

Rear view of com pleted amplifier and speakers.



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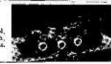
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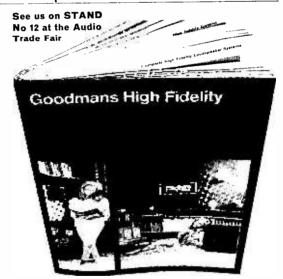
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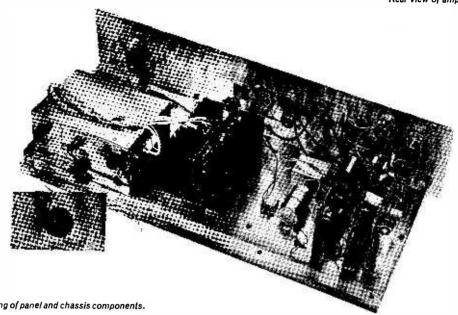
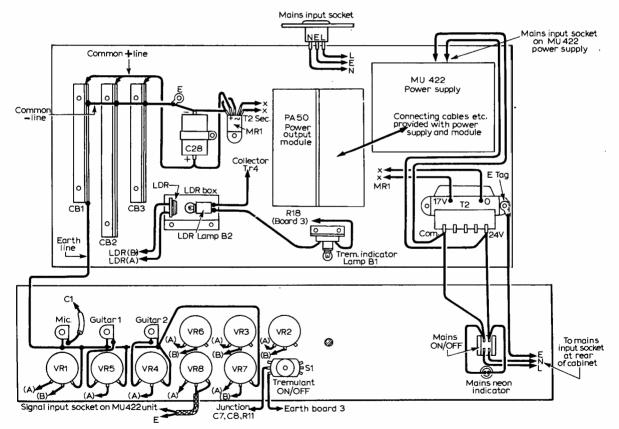


Fig. 14: (below) Wiring of panel and chassis components.



on both and the two units have only to be mounted in the position shown.

Make sure they are firmly bolted to the chassis using all the fixing holes provided.

These units complete with interconnecting cables and plugs and the only external connections necessary are those of the mains input, the loudspeaker(s) and signal lead from the master volume control VR8.

It is most important that the earthed side of VR8 is taken to earth only via the screening braid to the earth pin of the power unit input signal DIN socket as shown in Fig. 15B. It should be explained that although the signal input socket for the power module is located on the MU422 power supply unit it is carried through to the power module by the screened interconnecting cables.

Point to point wiring of the various controls, the pre-amplifier power supply and the mains input connections are given in Fig. 14. Note the earth connections for the signal input jacks and controls VR1, VR4, VR5 and VR7 which finally go to the common earth line on circuit Board 1. The mains supply circuits are shown separately in Fig. 16.

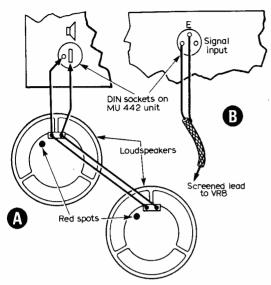


Fig. 15: Connections for speakers and signal input lead.

#### Loudspeakers

The terminals of the Goodmans type 12P loud-speakers specified for the PW25-50 amplifier are marked with regard to phasing. Connect them in parallel as shown with the 'red spot' terminals on the same line. Do not under any circumstances earth either of the loudspeaker connections or the loudspeaker frames. Connect only to the DIN loud-speaker socket on the left hand side of the MU422 unit as shown in Fig. 15A.

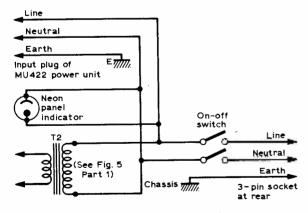


Fig. 16: Mains input wiring details.

The third and final article will deal with optional extras—the foot control tremulant, the wah-wah control and with testing the amplifier for correct performance.

#### TO BE CONTINUED

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# WIRELESS

#### P.W. 25/25 HI-FI STEREO AMPLIFIER

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### SHORT-WAVE TRANSISTOR PREAMPLIFIER

This article describes the construction of a unit which can be used in conjunction with almost all types of short wave receivers to improve their performance. It will prove of particular value, with many of the older models or "ex govt" receivers whose sensitivity is not always what one would wish.

Basically the unit is a two stage r.f. transistor amplifier with switched broad-band pre-tuned circuits to give a good measure of r.f. signal gain.

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The Codar CR.70A is an excellent general coverage communica-The Coudi Cr. 10A is an excellent general coverage communications receiver for the keen short wave listener. Very reasonably tions receiver for the keen short wave listeller. Very reasonably priced at just £22,10.0 the CR.70A is outstanding value for money. priced at just \$22,100 the CR.IDA is outstanding value for money. In four stable ranges, the receiver covers from 540 metres medium m rour stable ranges, the receiver covers from 340 metres medium wave, right through the shipping and coastguard frequencies all wave, right infough the shipping and coasiguate frequencies and the short wave and international amateur bands up to and including the metro.

The CR.70A has a high 'Q' aeriel input stage using exclusive CODAR COIL air space inductor. Double tuned, iron cored I.F. transformers produce high selectivity. Ready to plug into 200-250 years 40 mains the CP 70A peods only very action of the transformers produce high selectivity. Ready to plug into 200-250 volt AC mains, the CR.70A needs only your aerial and a 2-3 ohm loudspeaker. The cabinet measures only 13" x 5\frac{2"}{x} x 7\frac{2"}{x} and the control panel is finished in black and white with chrome trim knobs.

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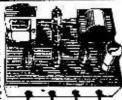
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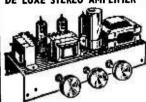
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# practically wireless HENRY commentary by

## The "Ah-Ha" Syndrome

NCE I could rattle away quite happily at these monthly pieces, secure in the knowledge that the boys at the P.W. Office would do no more than rip the sense from context with their surgical blue pencils. At least, I consoled myself, they hadn't to correct the spelling.

Now, I am not so sure. What you see here, Joe, may be the polished version of what my palsied typewriter has stuttered onto the page. All because those indefatigable watchdogs of the public weal, the Consumers' Association, once told me it was not "Good Value for Money."

According to Which—and not even a current one, but an oldie Mrs. Henry recovered from a wardrobe drawer—this honest old machine, now stuttering out its resentment after years of faithful service, is far from being a Best Buy.

Lately, shame on them, the watchdogs of Which have cast their blight on things hi-fi. Their prime choice of loudspeakers, for example, completely shunned my precious DM1s and my gramophone deck, the result of many hours overtime (not only earning but choosing), gained nary the breath of a mention.



One in forty explodes

Knowing the fierce independence cherished by some reviewers, and guessing at a similar trait in others, Henry is inclined to regard the Consumers' Association as well-meaning but misguided. Unfortunately, the sort of public who write letters of sympathy to Annie Walker or believe that Waggoner's Walk exists, are inclined to take the Which verdict as the word of the Law.

The C.A. may say that drafts of reports are subject to verification and revision, and that it is often these drafts that receive instant publicity, but how often, we may ask, is refutation made? Recently, for example, Which came out quite strongly about the high breakdown rate of colour television receivers. According to their survey, one in 17 sets gives off smoke and one in 40 explodes!

Explodes, mind you, not merely dissolves into an indeterminate mix of dun and indigo, or curses visual blue streaks at its user, but '... expands violently with loud report under influence of suddenly developed internal energy.'\*

Along with the technical secretary of the British Radio Equipment Manufacturers' Association, this cynical onlooker is inclined to think that the *Which* findings were unrepresentative and 'out of line with makers' reports on breakdowns'.

This gent, the appropriately named Mr. Donald Doo, claimed that when the first draft of the Which report was submitted to him the paragraph on smoking and exploding colour television sets was conspicuous by its absence.

'We would have challenged it straight away,' he claimed. 'We have had no reports from any of our members of problems like this.'

I'll bet they haven't. Not since the early days of colour television at least. Those of us who have



The permutations from knob-twiddling. . .

slogged at a bench are well aware that teething troubles were experienced; are even ready to admit that, despite the brochures and advertisements, modern television receivers can and do break down.

Stop and think—the average colour television receiver has four times as much in it as the monochrome equivalent. There are between twice and three times as many controls for the installer to set up. The permutations of error from quite simple knob-twiddling are disproportionately large. Signal variations at the site—ghosting, changes in level, interference, etc.—which would be tolerated in black and white become very pronounced when a chromatic scene is being viewed.

Yet how many of the 400,000 colour TV installations are totally unsatisfactory? A higher proportion than black and white—of course. But do we really believe, as Which implies, that 10,000 sets have 'exploded' since installation?

After all, if you read this article and feel the same way about the pontifical pronouncements of Which as I do, you don't say: 'Ah-Ha, I agree with the writer.'

Oh no, you say: 'Ah-Ha, Henry agrees with me.'

I hope.

\*My dictionary definition.

# NOTES ON THE PW UNIT-BUILT GENERAL COVERAGE RECEIVER

ETAILS of this 12-transistor 4-waveband receiver were published in the March and April 1970 issues of "Practical Wireless."

These brief notes should be of assistance to anyone

considering constructing the receiver.

The completed circuit shows 4 diodes and 12 transistors, with 4-band coverage, and it is apparent that quite a number of constructors feel that the wiring of the whole receiver is rather complicated. The whole circuit is not unusually complex for this type of equipment. However, it should not be overlooked that the receiver can be constructed in simpler form, and added to from time to time, and is, in fact, the manner in which the original receiver was made.

This is an important point, because it does mean that a relatively simple, straightforward superhet is initially built and wired which can be tested and used in this way. When this is found to perform correctly, other features can be added the receiver being tested each time an addition is made. Should a wiring error or other fault be present, this greatly reduces the number of circuits to be investigated.

A few further details on this stage by stage method of building the receiver should prove useful.

#### STAGE BY STAGE ASSEMBLY

The initial circuit is wired for one waveband only which will avoid errors in wiring the many switch contacts, and sets of coils. The SW1 range coils, for 30-11MHz, are very near the switch wafers, and tend to hinder the wiring of coils, so it is probably best to wire the SW2 range coils first, for 14-5MHz.

By omitting the r.f. stage, there are only two coils, those for the mixer and oscillator circuits. The bandswitch is set to its second position, and these two coils are wired in. Should the receiver fail to operate because of a switch or coil wiring error, only these few connections need be checked.

When the receiver is working correctly on the SW2 range, add the pair of coils for the SW3 range, and test to see that proper results are obtained. Then add the m.w. range, and test again. Finally, the

SW1 range coils are wired in.

When the r.f. stage has been added, wire in the SW2 aerial coil, and test the receiver. Should a fault be present, only the few new items introduced need be checked. Then add the other aerial coils, one at a time, testing the receiver after each addition.

This is much better than wiring in the twelve coils, for four bands with r.f. stage, then finding some obscure fault exists in coil or bandswitch connections.

As described, the receiver is easily wired as a 6-transistor superhet, for one band. It will then have Tr2 (mixer), Tr3 and Tr4 (i.f. amplifiers), Tr10 (driver) and the output stage Tr11/Tr12. Only the a.m. diode and a.g.c. rectifier D2 need be connected. This means that Tr1 (r.f. amplifier), Tr5 (meter amplifier), Tr6 and Tr7 (product detector) with b.f.o. Tr8, and a.f. amplifier Tr9, are not needed, neither is the multi-way function switch, nor diodes D1, D3 and D4. The circuit, in this simplified form, is capable of excellent reception and volume.

The additional features can be added in any order preferred. Probably the r.f. amplifier, Tr1, will be found most useful. After this, Tr9, for additional

audio gain, may be included.

Adding Tr6, Tr7 and Tr8, will then allow c.w. and s.s.b. to be resolved, as the use of the diode D2 allows reception only of a.m. signals.

Remember to test the receiver after each addition. Then if a fault or error has been introduced, it must be in the part of the circuit last added. By proceeding in this way there will be no need to check the whole receiver, but only some relatively small part of it.

#### **AUDIO TRANSFORMERS**

The driver and output transformers listed are no longer made. Fortunately many transformers suitable exist for OC81D driver and 2xOC81 and similar output transistors. The Weyrad LFDT4 driver and OPT1 output transformers will be found suitable. Connecting data for the LFDT4 appear in Fig. 1, connections for the OPT1 remaining unchanged.

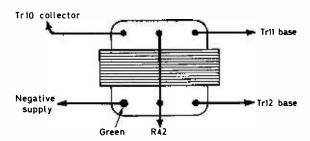


Fig. 1: Connections to alternative audio driver transformer

As is usual with this type of circuit, operation of the output pair is critically dependent upon the relative values of R42 and R40/R41. If there is distortion, R42 should be increased slightly to about 100 ohms.

Any ordinary 2 or 30hm speaker is suitable, preferably a reasonably large unit, in a cabinet.

#### **AERIALS**

Long-range reception is possible with the telescopic aerial, especially on the h.f. ranges. However, for the best possible results with weak signals, some form of external aerial should be added. This can be of any type normally employed with a communications receiver such as a random length external wire, or an end-connected wire with tuner, or a dipole or tuned doublet, etc. Any of these aerials can be expected to give an improvement in the signal strength of several S-points.

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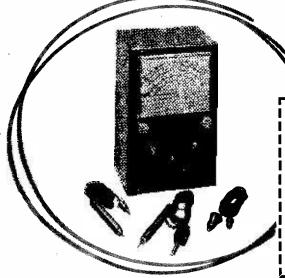
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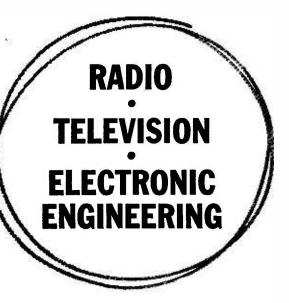
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maint Transformer Type 8.0. 30:03 Chassis mounting type, size approximately 3 × 2½ × 3in., 2 secondaries one 330 voit at 60 mA and other 6.3 voits 1.5 amp. Earth screen between primary and secondaries. This will power a 5 watt amplifier (circuit available 2/6). Matching OPT. 5 56734 described below. Price 18/6 plus 4/8 post. Mains Transformer Type No. 58695

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OPT. r. 1. 56787

OPT. r. 1. 86787 Upright mounting, size approximately  $3\frac{1}{2} \times 2 \times 2$ ln. Matching impedance 60 ohms to 15 ohms. 5 watts output using transistor type AD140 (Circuit diagram available price 2/6). Price 8/6 each, no extra for postage if ordered with maina transformer type 56786. OPT. ref. 585004

Upright mounting, size approximately 2 × 2½ × 2in. Primary impedance 60 ohm, secondary impedance 3 ohm, otherwise this is as 56787. OPT. ref. 56784

Chassis mounting, size approximately  $2\frac{1}{2} \times 2 \times 1\frac{1}{2}$ in. Primary 500 ohm centre tapped. Ratio 27/1.5 watts output using twin ELL80 or similar. Price 12/6. No extra for postage if ordered with

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a good communications receiver with either internal or external 100kHz marker of known accuracy are the basic alternatives. If an existing v.f.o. of known accuracy is obtainable, this can make things much easier.

Having connected the necessary d.c. supply to the v.f.o., set the trimmer capacitor to about mid-point and the tuning capacitor to maximum value (vanes fully meshed). Loosely couple the output to the receiver aerial input and allow to warm up for 10 to 15 minutes. Next search around 3.5MHz on the receiver dial, the b.f.o. being switched in first. When the beat note is heard, note the frequency on the receiver dial. If no beat note can be found, check that the v.f.o. output is present using an oscilloscope or valve-voltmeter.

With the beat frequency noted, set the receiver dial accurately to 3.5MHz using the 100kHz marker to ensure accuracy. Now adjust the trimming capacitor in the v.f.o. until the beat note is obtained on exactly 3.5MHz. If the original beat frequency was high, VC2 should be increased and if it was low, decreased. The setting of VC2 should be carried out with care, the trimming tool being removed after each adjustment as a small hand capacity effect is almost unavoidable. With this frequency correctly set on zero beat, the v.f.o. dial can be marked at this point. No further trimming should now be required.

The receiver dial is next set to 3.6MHz, again using the crystal marker, and the v.f.o. tuning capacitor slowly adjusted until the beat note is again heard. Having set VC1 for exactly zero beat, mark the appropriate point on the scale. This procedure is repeated for 3.7 and 3.8MHz. The upper limit of 3.8MHz will vary slightly between different units due to differences in stray capacitance.

The mid-points of 50kHz steps and 10kHz subdivisions can only be accurately marked if the receiver dial has suitable calibration points or if an existing v.f.o. is available. As the scale divisions are almost linear, however, reasonably accurate subdivisions can be obtained geometrically. When the main scale is fully calibrated, the harmonic calibrations for the other bands (7MHz, 14MHz, etc.) can be completed on the lower scales of the v.f.o. dial.

#### **CORRIGENDA**

FREQUENCY METER—MAY 1970 Under the heading "Construction" the sentence "Note the breaks in the copper strip at holes D9, D15 and E4" should read "at holes C14, D3 and D9."

SUMS AND CIRCUITS—JUNE 1970

The voltage and current waveforms shown in Fig. 3.3 and 3.4b should be interchanged

192 reading -1+0·3010=\overline{0}\text{-1}04010 192 readi -0.6990.

TEN OR FIFTEEN METRE CONVERTER-JUNE 1970 Figure 1 and the components list should show R3, R8 and R10 as  $1k\Omega$  and not  $10k\Omega$ .

LIGHT OPERATED SWITCH-JULY 1970

The value of R7 both in the circuit and the components list should read  $4.7\Omega$  and not  $4.7k\Omega$ .

AUDIO EXPANDER/COMPRESSOR—AUGUST 1970

In the components list C11 should have read 100pF and not 100pF. The circuit is however correct.

In Fig. 11, the screening of the wire connected to the slider of S1 section C should be connected to the other screen wires and not to the slider of S1 section B.

#### ORGAN PEDAL BASS UNIT—continued from page 460

boards in the event of a faulty contact or circuit failure.

The last stage is to fit aluminium or wooden rails, one on each side of the case, to prevent the unit tipping forward when the pedals are pressed. Full downward pressure on a pedal should bring it to within half inch or so of floor level. Further pressure would tip the unit forward, hence the need for the rails as shown in Fig. 16.

#### Amplifier Requirements

Because of the very low frequency of the pedal bass notes a sizeable loudspeaker in a suitable enclosure is necessary if the true bass fundamentals are to be audible. Small organs like the Philicorda have only small loudspeakers which are not suitable for bass reproduction. For organs of this calibre it is best to build a suitable amplifier with an output of 5 to 10 watts which can be incorporated within the speaker enclosure. The speaker should be 10 to 12in. in diameter.

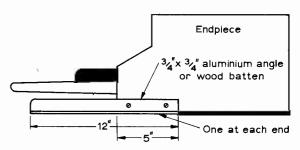


Fig. 16: Fitting of rails to case.

There is no reason why the pedal bass unit described in this article should not be integrated with an amplifier and speaker so designed as to fit beneath small organs like the Philicorda. For portables fed into large power amplifiers with sizeable speakers it should only be necessary to connect the pedal bass unit to a suitable input on the amplifier.

There is of course the question of volume control or 'expression' whilst playing. For small organs where the overall sound output is relatively low it will be sufficient to set the pedal bass sound to an arbitrary level. A pedal type volume control could be used or an extra volume control mechanically coupled to an existing pedal.



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A series of simple transistor projects, each using less than twenty components and costing less than twenty shillings to build.

LTHOUGH we have described two general-purpose amplifiers in this series, tone control facilities have not been incorporated, mainly due to our limitation on cost. The tone control stage described here is a general-purpose one which can be added to most transistor amplifiers in the early stages. The gain, with the controls in their middle settings, is very small as the amplification of the stage is nearly all used as negative feedback to alter the tone. The circuit shown is not very original, in fact it is widely used in commercial amplifiers.

Performance of this type of circuit is excellent;

Performance of this type of circuit is excellent; with reference to 1kHz, frequencies of 100Hz can be boosted or cut by up to 15dB and the same degree of control is available at 15kHz. A low noise transistor, a BC169C, is used so noise introduced by this additional stage is negligible.

#### THE CIRCUIT

For those unfamiliar with this type of circuit, a quick glance will probably lead to rapid bafflement, but basically the design is simplicity itself.

The input is coupled to the d.c. blocking capacitor C1 and is then applied by one path to the base of the transistor through C3 and a part of VR1, a  $100k\Omega$  potentiometer. The actual part of VR1 that it passes through depends on the setting of the control. By another path the signal reaches the transistor via R2 and C5. It will be seen that C5 is paralleled by a part of VR2, again depending on the setting of the control.

These combined signals are applied to Tr1 which has R3, a  $10k\Omega$  resistor acting as the collector load and R4 as the base bias. The output is taken from the collector via C7 to the existing volume control.

Also connected to the collector of Tr1 is C6. Now in a common emitter amplifier (which is what we are using here) there is phase inversion, that is the signal at the collector is out of phase with the signal applied to the base. This anti-phase signal is applied to the other side of VR1 and VR2 via an identical network to the one that fed the original signal to these controls.

It will be seen then that both controls are able to select either very little or a considerable amount of the out-of-phase signal and since these networks are frequency selective we are able to achieve a considerable amount of control over the tone.

Careful scrutiny of the circuit will show that a certain degree of negative feedback is applied to the transistor through R4, the base bias resistor, but this is quite small and anyhow is not frequency selective. Many designs decouple this a.c. feedback by using two resistors in series, their common junction being connected to earth via a high value capacitor, such as  $100\mu$ F; in practice the author has found this to be unnecessary.

## No. 18 ADD-ON TONE CONTROL

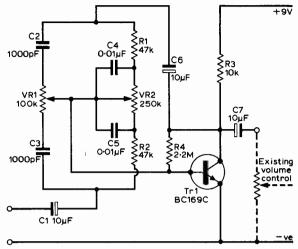


Fig. 1: The circuit of the add-on tone control. VRI is the treble control, VR2 the bass control.

#### ★ components list

#### Resistors: R1 47k Ω R3 10k Ω R2 47k Ω 2.2M Ω All 1 or 1 watt, 5% types VR1 100k $\Omega$ linear pot. Treble control VR2 250k $\Omega$ linear pot. Bass control Capacitors: C1 10µF 12V C5 0.01 uF C6 10µF 12V C2 1,000pF C7 10µF 12V C3 1,000pF 0.01µF Transistor: Tr1 BC169C or BC109

#### FREQUENCY SELECTIVE NETWORKS

There are probably many readers who are unsure what we mean by "frequency selective networks." In practice these are very simple and can be calculated and designed by even the raw beginner. A.C. theory can be very complicated and describing, from first principles, the operation of capacitors would be hard and is anyway unnecessary; just take it as a fact that the impedance of a capacitor is directly proportional to the frequency and the impedance, in ohms, is equal to  $1/(2\pi i\alpha)$  where f is the frequency and C the capacitance in Farads; so that C2 and C3 at 100Hz have a "resistance" of about  $1.6\text{M}\Omega$  and at 10kHz,  $16\text{k}\Omega$ . Similarly C4 and C5 have a "resistance" at the same two frequencies of  $160\text{k}\Omega$  and  $1.6\text{k}\Omega$  respectively. Substituting these "resistance" values instead of the capacitors we are left with a potential divider (but only of course at a particular frequency) and it will be seen that the gain can be changed by the setting of the controls VR1 and VR2.



# **MONOLITHIC INTEGRATED** CIRCUIT HIGH FIDELITY AMPLIFIER AND PRE-AMP



# the world's most advanced high fidelity amplifier

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output of 5 watts R.M.S. (10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 Zener diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.

The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required as part of the process of producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. This enables us to cover every IC-10 with the Sinclair guarantee of reliability.

#### ■ SPECIFICATIONS

Output 10 Watts peak, 5 Watts R.M.S. continuous. 5 Hz to 100 KHz±1dB. Frequency response Less than 1% at full output. Total harmonic distortion Load impedance 3 to 15 ohms. 110dB (100,000,000,000 times) total. Power gain 8 to 18 volts. Supply voltage 1 - 0.4 - 0.2 inches. 25.6 - 10 - 5 mm. 5mV. Size Sensitivity Input impedance Adjustable externally up to 2.5 M ohms.

#### **■ CIRCUIT DESCRIPTION**

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

#### APPLICATIONS

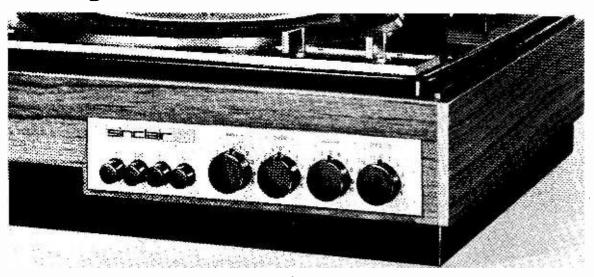
Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

IC.10 with IC.10 manual



SINCLAIR RADIONICS LIMITED 22 NEWMARKET ROAD · CAMBRIDGE Telephone 0223 52731

# **Project 60**



# Laboratory standard modular high fidelity

Sinclair Project 60 comprises a range of modules which connect together simply to form a compact stereo amplifier with really excellent performance. So good, in fact, that only 2 or 3 amplifiers in the world can compare in overall performance and now the constructor has choice of assemblies with either 20 or 40 watts output per channel, with or without filter facilities. The modules are: 1. The Z.30 and Z.50 high gain power amplifiers. 2. The Stereo 60 preamplifier and control unit. 3. The Active Filter Unit. 4. 4 supply units—PZ.5; PZ.6; PZ.7 and PZ.8. In a normal domestic application, there will be no significant difference between PZ.5 or PZ.6 unless loudspeakers of very low efficiency are being used, in which case the PZ.6 will be required. For assemblies using two Z.50's there is the PZ.8 supply unit to ensure maximum performance from these amplifiers. No skill or experience are needed to build your system and the Project 60 manual gives all the instructions you can possibly

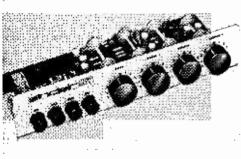
want, clearly and concisely. Perhaps the greatest beauty of the system is that it is not only flexible now but will remain so in the future as new additions are made to the range. A stereo F.M. tuner is next to come. These and all other modules introduced will be compatible with those already available and may be added to your system at any time. And because Sinclair are the largest producers of constructor modules in Europe, Project 60 prices are remarkably low.

	System	The Units to use	In conjunction with	Your Project 60 Units will cost
Α	Car Radio	Z.30	Existing car radio, Sinclair Micromatic	89/6
В	Simple battery powered record player	Z.30	Crystal pick-up, 12 V or more battery supply and volume control	89/6
C	Mains powered record player	Z.30 and PZ.5	Crystal or ceramic P.U. Vol. control etc.	£9.9.0
D	20+20 watts RMS stereo amplifier for most needs	Two Z.30s, Stereo 60 and PZ.5	Crystal, ceramic or magnetic P.U., most dynamic speakers, FM tuner, etc.	£23.18.0
E	20+20 watts RMS stereo amplifier for use with low efficiency (high performance) speakers	Two Z.30s, Stereo 60 and PZ.6	High quality ceramic or mag. P.U., F.M. Tuner, Tape Deck, etc. All dynamic spkrs.	£26.18.0
F		Two Z.50s, Stereo 60 PZ.8 and mains transformer	As for E	£32.17.6
G	Outdoor public address system	Z.50	Microphone, up to 4 P.A. speakers, 12V car battery with or without converter, controls	£5.9.6
Н	Indoor P.A	One Z.50, PZ.8 and mains transformer	and mains Mic., guitar, heavy duty	
J	High pass and low pass filters	AFU	D, E or F as above	£5.19.6
K	Stereo F.M. tuner	To be r	released shortly	

How to assemble and use Project 60 modules to best advantage in the above and other applications will be found in the fully descriptive Project 60 manual included with Project 60 systems. This 48 page manual is available separately, price 2/6d including postage.













#### **GUARANTEE**

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge to service thereafter. No charge for postage by surface mail. Air-mail charged at cost.



#### Z.30 & Z.50 POWER AMPLIFIERS

The Z.30 together with the Z.50 are both of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low 0.02% at full output and all lower outputs. Whether you use the Z.30 or Z.50 power amplifiers in your Project 60 system will depend on personal preference, but they are the same physical size and may be used with other units in the Project 60 range equally well, For operating from mains, for the Z.30 use PZ.5 for most domestic requirements, or PZ.6 if you have very low efficiency loudspeakers. For Z.50, use the PZ.8 described below.

SPECIFICATIONS (Z.50 units are interchangeable with Z.30s in all applications.)

#### **Power Outputs**

Z.30 15 watts R.M.S. into 8 ohms. using 35V: 20 watts R.M.S. into 3 ohms using 30 volts.

Z.50 40 watts R.M.S. into 3 ohms from 40 volts: 30 watts R.M.S. into 8 ohms, using 50 volts.

Frequency response 30 to 300,000 Hz ± 1dB

Distortion 0.02% into 8 ohms

Signal to noise ratio better than 70 dB unweighted

Input sensitivity 250mV into 100 Kohms.

For speakers from 3 to 15 ohms impedance

Size  $3\frac{1}{2} \times 2\frac{1}{4} \times \frac{1}{2}$  ins. (90 x 58 x 13 mm)

Built

89/6 tested and quaranteed

tested and guaranteed

#### STEREO 60 Pre-amp/Control unit

Designed for the Project 60 range but suitable for use with any high quality power amplifier. Silicon epitaxial planar transistors are used throughout, achieving a really high signalto-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

 Input sensitivities — Mag. p.u. -3mV correct to R.I.A.A. curve ± 1dB: 20 to 25,000Hz. Ceramic p.u., Radio and Aux, each up to 3mV.

- Output 250mV.
- Signal-to-noise ratio better than 70dB.
- Channel matching within 1dB.
- Tone controls TREBLE +15 to -15dB at 10kHz: BASS +15 to -15dB at 100Hz.
- Front panel brushed aluminium with black knobs and controls.
- Size 8½ x 1⅓ x 4 ins. (210 x 138 x 102 mm)

Built, tested and guaranteed £9.19.6

#### ACTIVE FILTER UNIT

For use between Stereo 60 unit and two Z.30s or Z.50s, the Active Filter Unit matches the Stereo 60 in styling and is as easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid (12dB/octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The Sinclair A.F.U. is suitable also for use with

any other amplifier system.

Two stages of filtering are incorporated-rumble (high pass) and scratch (low pass). H.F cut-off (-3dB) (low pass). H.F cut-off (-3dB) variable from 28kHz to 5kHz. L.F cutoff (-3dB) variable from 25Hz to 100Hz. Filter slope, both sections 12dB per octave. Distortion at 1kHz (35V supply) 0.02% at rated output.

Built, tested

Built, tested and guaranteed £5.19.6

#### POWER SUPPLY UNITS

Designed specially for use with the Project 60 system of your choice. Illustration shows PZ.5 power supply unit to left and PZ.8 (for use with Z.50s) to the right. Use PZ.5 for normal Z.30 assemblies and PZ.6 where stabilised supply is essential.

PZ-5 30 volts unstablisied £4.19.6

money order

PZ6-35 volts stabilised £7.19.6

PZ-8 45 volts stabilised (less mains transformers £5.19.6 PZ-8 mains transformer £5.19.6

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TRANS	ISTORS	etc.	F	OC26	7/6	OC81	2/6
			i i	OC28	8/6	OC81D	2/6
AC107	3/	OA5	1/6	OC35	8/6	OC82D	2/6
AC126	2/3	OA9	1/8	OC44	2/9	OC140	5
AF115	3/-	OA10	1/6	OC45	2/3	OC169	3/6
AF116	3/-	OA47	1/9	OC70	2/3	*OC170	4
*AF117	4/-	OA81	1/6	OC71	2/3	OC171	2/8
BFY18	4/6	OA85	1/6	OC72	2/3	OC202	4/6
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ELECTROLYTIC CONDENSERS Full details of many types from 6d each in our list (see below).

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MULTIMETER: 20,000 Ω/V D.C., 10,000 Ω/V A.C. 0-5/25/50/500/1K volts D.C.

-10/50/10/50/1K volts A.C.

-0-50/A 2.5mA/250mA D.C.

-0-10/50/10/50/1K volts A.C.

-0-10/50/10/50/1K volts A.C.

-0-50/A 2.5mA/250mA D.C.

-0-10/50/10/50/1K volts A.C.

-0-10/50/10/50/1K volt

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10-section 71-561, ¾ dia. 15/9.

All are strongly plated (P. P. & I. on all above, up to three 1/-)

SWITCHES: Standard toggle, metal, 250V 2A. One hole fixing: SPST 2/3, SPDT 2/9, DPST 3/- DPDT 3/3, Slide type, Sub-nin. DPDT 1/8 each. Small DPDT 3 way, certer "off" 1/9, Reed magnetic on/off 1/9 (up to three, 1/-; 1d each all additional). Rotary Switches etc. in list. Example: 4 pole 3 way 3/9 (1/-)

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7 pin synch. (Equit. 12SR7) 12/6 (1/- each either type). A few specified other types now available (See list).

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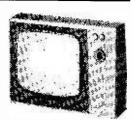
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2N 4U4	4/6	2N3570 2N3572	25/- 17/6	40312 40314	9/6 7/6	BC175 BC182	5/6 4/6	BPX29 BPY10	36/ 29/	NKT10	519 <b>5</b> /~	3A	2/9 3/-		3/3	3/6 4/6	8/9	4/- 6/-	4/6	_
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2N914 2N916	8/6	2N3707	8/-	40362	11/6	BCY39	8/6	BSX76 BSX77	4/6 5/6	NKT802	<b>21</b> / 211	IS010 3/ IS021 4/	- AAZ	13 4/	BA'	Y31 :	1/6 B	YZ12	6/- O	A90 1/6
2N918	8/6 6/~	2N3708 2N3709	2/- 2/-	40370 40406	6/6 11/6	BCY40 BCY42	7/6 8/	BSX78 BSY24	5/6 3/-	NKT802	17/-	IS44 2/-	- AAZ					YZ13 3T3/8		A91 1/6 A95 1/6
2N929 2N930	4/6 5/6	2N3710 2N3711	2/6 2/6	40407 40408	8/- 10/6	BCY43 BCY54	8/-	BSY25	8/		17/6	IS113 3/ IS120 3/						A5 A9	3/6 €	A200 2/- A202 2/-
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2N1090 2N1091	6/6 6/6	2N3823 2N3854	22/6 5/6	40467A 40468A	11/6 7/-	BCY59 BCY60	4/6 19/6	BSY28 BSY29	3/6 3/6	NKT802	17/6	IS130 2/6 IS131 2/6						A47 A70	1/6 1/6	
2N1131 2N1132	5/6 6/6	2N3854A 2N3855	5/6 5/6	40600 AC107	14/6 6/-	BCY70 BCY71	4/- 8/6	BSY32	5/~	NKT802	15	RCA	1	NTEG	RAT	ED C	IRCU	ITS		
2N1302	8/6	2N3855A	8/-	AC126	4/	BCY72	8/6	BSY36 BSY37	5/ 5/	NKT802	17/6	CA3000 3	19/6 C	A3020A	32/	CAS	3036	14/6	CA3050	
2N1303 2N1304	3/6 4/6	2N3856 2N3856A	6/- 1 7/-	AC127 AC128	5/- 4/-	BCZ10 BCZ11	5/6 7/6	BSY38 BSY39	4/6 4/6	OC20	17/6 15/-	CA3007 5	7/6 C	A3021 A3022	32/ 26/		3039 3041	16/9 22/	CA3051	27/~ 2 33/~
2N1305 2N1306	4/8 5/~	2N3858 2N3858A	5/- 6/-	AC154 AC176	4/6 5/	BD116 BD121	22/6 13/-	BSY40 BSY51	6/6	OC22	10/-	CA3011 10 CA3012 1	.4/9 C	A2023 A3026	25/6 20/~	CA:	3042 2043	22/- 27/6	CA3054 CA3054	10/-
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2N1631 2N1632	8/6 8/6	2N3877A	8/-	ACY20	5/	BDY11	37/6	BSY82	10/6	OC29 OC30	15/ 8/	CA3020 25	5/8 C	A3035	24/6	CAS		32/		
2N1637	8/6	2N388A 2N3900	12/6 7/6	ACY21 ACY22	5/- 4/-	BDY17 BDY18	37/6 49/6	BSY95A	11/6 2/6	OC35 OC36	8/ 12/6	Data and app Motorola	plication	sheets 2	}/− per	· type				
2N1638 2N1639	7/6 7/6	2N3900A 2N3901	19/6	ACY28 ACY40	4/- 4/-	BDY19 BDY20	62/6 22/6	BSW41 BSW70	8/6 5/6	OC38 OC41	10/6	MC724P MC780P		17/ 57/			MC79			17/6
2N1711 2N1889	5/- 6/6	2N3903 2N3004	7/-	ACY41	5/-	BDY38	19/6	D16P1	7/8	OC42	4/6 5/-	MC788P		19/	6		MC83 MC13	03P		130/- 57/9
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2N2147 2N2148	14/6 12/6	2N 3906 2N 4058	7/6 3/6	AD149 AD150	11/6 12/6	BDY62 BF115	27/6 5/-	D16P4 GET102	8/- 6/-	OC46 OC70	3/- 3/-	MC792P Fairchild		17/	6 1-	e	7-1			120/
2N2160 2N2193	11/6 9/6	2N4059 2N4060	5/- 5/-	AD161 AD162	7/6 7/6	BF117 BF163	9/6	GET113	4/-	OC71	2/6	L900 Buffer			9,	/9	9		12 + 8/ -	
	10/-	2N4061	4/6	AF106	8/6	BF167	7/6 5/-	GET114 GET118	4/- 4/-	OC72 OC74	2/6 6/6	L914 Dual Ga L923 JK Flip	Flop		9/ 12/		9, 11/		8/ 11/	
2N2217	4/6 5/6	2N4062 2N4244	4/6 9/6	AF114 AF115	5/ 6/	BF173 BF177	6/6 6/6	EET119 GET120	4/- 6/6	OC75 OC76	4/6 4/6	L709 Operatio Quantity Pric	onal Am	plifier	21	-	19/		18/ -	
2N2218 2N2219	6/	2N4255 2N4285	8/6 8/6	AF116 AF117	5/ 5/	BF178 BF179	12/6	GET873 GET880	3/-	OC77	6/	General Electr	ric							
2N2220 2N2221	5/- 5/-	2N4286 2N4287	8/6	AF118	12/6	BF180	14/6 7/-	GET887	6/- 4/-	OC81 OC81D	4/- 4/6	PA230 PA234		Low Lev	vel Am Audio .	iplifier Amplifi	er			22/6 21/6
2N2222	5/-	2N4288	3/6 3/6	AF119 AF124	4/- 4/6	BF181 BF184	6/6 6/6	GET889 GET890	4/6 4/6	OC83 OC84	5/ 5/	PA237 PA246		2 watt A 5 watt A	Ludio .	Amplifi	er			87/6 57/6
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2N2924 2N2925	3/6 3/6	2N5355 2N5356	5/6 6/6	BC116A BC118	·7/6 6/6	BFX92A BFY10	12/6 6/6	NKT125 NKT126	4/6 4/	T1852 T1853	3/6 6/	2½ × 5in 3½ × 3½in	4/3 4/8	4/9 4/9			watt : nly). 1/(		p to 27	0 ohms
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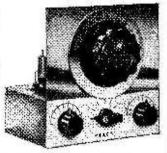
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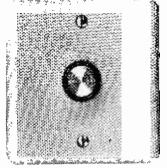
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IR5	5/6	DL35	4/9	EL84	4/9	PL82	5/9
185	4/8	DL92	5/9	EY51	7/-	PL83	6/8
1T4	2/9	DL94	6/6	EY86	6/8	PL84	6/-
384	5/9	DL96	7/8	EZ80	4/8	PL500	12/9
3V4	6/6	DY86	5/8	EZ81	4/6	PL504	13/3
6/30L2	11/6	DY87	5/8	KT61	9/8	PY32	10/-
6AQ5	5/-	EABC80	6/8	KT66	16/6	PY33	10/-
6F25	12/-	EB91	2/-	N78	17/-	PY81	5/-
68N7G		EBC33	7/9	PC86	10/8	PY82	5/-
25L6G7		EBF89	6/-	PC88	10/8	PY83	5/6
30C18	12/9	ECC81	8/6	PC97	7/6	PY88	6/6
30FL1	12/6	ECC82	4/-	PC900	7/-	PY800	7/-
30L15	12/9	ECC83	4/9	PCC84	6/8	PY801	7/-
30P4	11/9	ECC85	5/-	PCC89	9/8	R19	6/8
30P19	11/9	ECH35	5/6	PCC189		U25	12/9
30PL1	12/8	ECH81	5/9	PCF80	5/11	U26	11/6
30PL13	3 14/-	ECL80	7/-	PCF86	8/9	U191	18/-
30PL14	18/6	ECL82	6/8	PCF801		U251	14/-
CCH35	18/-	ECL86	7/6	PCF802		U329	14/-
DAC32	6/9	EF39	4/6	PCF805		UABC	
DAF91	4/8	EF80	4/6	PCF806		UBF89	
DAF96	7/-	EF85	5/9	PCL82	6/9	UCC85	7/8
DF33	7/6	EF86	6/3	PCL83	11/9	UCH81	
DF91	2/9	EF89	4/9	PCL84	7/-	UCL82	6/9
DF96	7/-	EF91	2/6	PCL85	8/6	UF89	6/-
DK32	6/9	EF183	5/6	PCL86	8/-	UL84	6/3
DK91	5/6	EF184	6/-	PFL200	11/6	UY41	7/-
DK92	8/8	EH90	6/-	PL36	9/8	UY85	5/2
DK96	7/8	EL33	9/8	PL81	9/8	Z77	8/9
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1N400	2/- AC126	5/- B8X76 3/- 5/- B8Y27 4/-	Type   12+ UL914 8/6 7/9	25 + 100 + 500 + 7/3 6/9 6/6
1N400			UL914 8/6 7/9	7/3 6/9 6/6 11/- 10/- 9/3
1N400 1N400		5/_ RSV29 5/-	BCI 403 A 42 /6 41 /_	11/- 10/- 9/3 40/- 37/6 35/-
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2G240	49/6 AC176	5/- BBY67 5/-	77	
20301	4/- AC187	6/- BSY95A 3/- 6/- BSY95 3/-	2N3055 15/-	2N3819 7/-
2G302 2G303	4/6 AC188 5/- ACY17	6/- BSY95 3/- 6/- BY100 3/6	Mullard I 15watt	Texas F.E.T.
2G303 2G306	6/- ACY18	4/- BY103 4/6	Silicon Power	25 + 6/-
2G308	6/- ACY19	5/- BY126 3/-	25 + 13/- 100 + 11/-	25 + 6/- 100 + 5/3 500 + 4/9
2G309	6/- ACY20	4/- BY127 4/-	100 + 11/-	300 1: T/7
2G371	4/6 ACY21	4/6 BYZ10 8/-	INADO2 == 4 4 2 /	202444 1074
20374	5/6 ACY22 5/- ACY28	3/6 BYZ11 7/- 3/6 BYZ12 6/-	IN4003 and 42/-	2N2646 10/6
2G381 2G382	5/- ACY28 6/- ACY34	4/- BYZ13 5/-	25 + 1/9	Motorola Unijunction
2G383	5/- ACV36	5/- BYZ15 20/-	100 + 1/6	25 + 8/9
2N404	4/6 ACY39 8/6 ACY40	11/- BYZ16 12/6	500 + 1/3	25 + 8/9 100 + 7/6
2N696	8/6 ACY40	3/- GET102 6/- 10/- GET103 4/6		500 + 6/9
2N697 2N698	8/6 AD140 8/6 AD149	10/- GET103 4/6 10/- MPF102 8/6	AF139 6/-	
2N698 2N706	2/-\AD161	7/8 MPF103 7/-		AF186 8/-
2N706	A 2/6 AD162	7/6 MPF104 7/6	25 + 5/3 $100 + 4/6$	Mullard V.H.F.
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2N920 2N922	5/- AF124 8/6 AF125	6/- OA70 2/- 5/- OA71 2/-	OCI71 6/-	1 amp Plastic 25 + 2/6 100 + 2/3
2N930		4/- OA73 2/-	25 + 5/3 $100 + 4/6$	100 + 2/6
2N113	1 8/_ AF127	4/- OA74 2/-		100 7 2/3
2N113	2 6/6 AF139	6/- OA79 2/- 9/6 OA81 2/-	BY127 4/-	DV713 E/
2N 130 2N 130	3 4/8 AF178 4 5/- AF181	9/6 OA81 2/- 8/6 OA85 2/6	Mullard 1000v	BYZI3 5/- Mullard 6a 200v
2N 130	5 5/- AF186	8/- OA86 4/-		25 + 4/-
2N130	6 5/- AF239	8/IOA90 2/-	25 + 3/3 100 + 3/-	25 + 4/- 100 + 3/6
2N 130	7 5/- AFY19	22/6 OA91 1/6 12/6 OA95 1/6		500 + 3/-
2N130 2N130	8 6/- AFZ11 9 5/- AFZ12	15/- OA200 1/6		
2N16	3 4/6 ASY26	5/- OA202 2/-	15/-	BC107/8/9
2N214	7 15/- ASY27	6/6 OA210 5/-	Muliard	2/6 ea.
2N316	0 12/6 ASY28	5/- OA211 7/6 6/- OAZ225 7/6	Thyristor	1.T.T. Planars 25 + 2/3
2N228 2N264		0/8 0 4 729 98 7/6	500 p.i.v. 6.5a	100 + 2/-
2N204 2N290	4 6/- ASZ21	8/6 OAZ229 9/6 19/6 OAZ231 9/6	500 p.i.v. 6.5a 25 + 12/6 100 + 11/-	500 + 1/9
2N290	5 7/6 AUY10	19/6 OAZ231 9/6		
2N293		19/8 OAZ234 7/6	L UAZUU/UAZUZ	OCP71 19/6
2N299 2N30	1 5/- HAY31	2/- OC16 8/6	2/-	Mullard Photo
2N30	3 5/- BC107	2/6 OC19 7/6	I SHILCON Diodes	25 + 17/3 100 + 14/9
2N30	4 10/- BC108	2/8/OC30 19/0	25 + 1/6 100 + 1/3	25 + 17/3 100 + 14/9 500 + 13/6
2N30		2/6 OC22 9/6 5/- OC23 10/-	500 + 1/1	
2N37	9 2/6 RC116	8/- OC24 10/- 7/6 OC25 7/0	1-	OC28 12/6
2N370	4 8/6 BC118	7/6 OC25 7/6 7/6 OC26 5/-		Mulland Power
2N37		6/- OC28 12/0	Mullard	25 + 11/-
2N37	9 2/6 BC136	7/- 0029 12/0	100 + 4/9	25 + 11/- 100 + 10/- 500 + 8/6
2N37	0 2/6 BC137	R/=\OC35 10/-	500 + 4/3	333   5/5
2N37 2N37		8/- OC36 12/6 5/6 OC41 5/-		OC71 3/-
2N37	11 19/8 BCY31	6/- OC42 6/-	OC45 3/6	Mulland
2N 37	4 2/6 BCY32	10/- 0043 8/-	Mullard 25 + 3/-	25 + 2/3 100 + 2/-
2N38 2N38	9 7/- BCY33 20 17/6 BCY34	4/- OC44 4/- 5/- OC45 8/0	25 + 3/- 100 + 2/6 500 + 2/-	100 + 2/- 500 + 1/9
2N38	3 17/6 BCY38	6/- OC46 5/		300 F 1/2
2N40	8 8/6 BCY39	9/8/OC70 2/		BCY34 5/-
2N40	31 3/-  BCY40	8/6/00/1 0/	OC75 5/-	Mullard
2N42 2N42	86 8/- BOY42 88 8/- BCY43	5/- OC73 6/-	25 ± 4/3	25 + 4/3 $100 + 3/9$
2N42	39 3/6 BCY70	4/- OC74 6/-	100 + 3/6	100 + 3/9 500 + 3/6
2N42	00 8/- BCZ11	7/6 OC75 5/ 8/9 OC76 5/	500 + 3/-	500 + 3/6
2N42 2N42	91 8/- BC147 92 8/- BC148	2/9 OC77 8/		IN4001 2 1/4
40361	11/-BC149	4/-IOC78 5/		IN4001 and 2 1/6
40362		6/- OC81 5/- 8/6 OC81D 4/	25 + 15/9	1 amp 100-200v 25 + 1/4 100 + 1/2 500 + 1/-
25001 28001	10/- BF194 10/6 BF195	3/- OC82 5/	100 + 14/6	100 + 1/2
2800		12/6 OC83 5/	500 + 13/3	500 + 1/-
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2832	7/6 BF181 3 10/- BFX30	7/8/OC200 7/ 8/- OC201 9/	8 800v 3/- 1000v 4/- 6 25 + 2/103/3 6 100 + 2/62/9	500 + 1/9
2832 2832	10/- BFX 85	5/- OC202 12/	8 100 + 2/62/9	1000 + 1/7 any one type
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2870	1 8/6 BFY50	4/8/00/204 8/		05140
2870 2873		4/8 OC206 15/	Mulland	OCI40 7/6 Mullard
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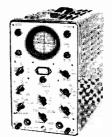
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OA2	0.38	6AR5 0.35	6EJ7 0.35	6Y6G 0.65						0.65			U191 0.75
OA3	0.45	6AR6 0.40	6EW6 0.65	7Y4 0.60	P	- 11a				0.70	EZ41 0.45	PCL800 0.93	
OB2	0.35	6AS5 0.35	6F1 0.70	9BW6 0.50	First Qu	ality F	ully Guar	anteed		0.25	EZ80 0.25	PCL801 0.70	U201 0.35
		6AS7G 0.80	6F5 <b>0.50</b>	10C2 0.50		_	-		EF83	0.55	EZ81 0.28	PD500 1.50	U281 0.40
OB3	0.60			10D1 0.50			<b>B</b> RA		EF85	0.35	GY501 0.80	PF86 0.60	U282 0.40
OC3	0.38	6AT6 0.30	6F6G 0.30							0.30	GZ30 0.40	PF818 0.85	U301 0.40
OD3	0.85	6AU6 0.25	6F11 0,38	10D2 0.40	V775	A PARTIE OF	<b>30</b> 100			0.28	GZ31 0.33	PFL2000.70	U403 0.50
IB3GT	0.38	6AV6 0.30	6F13 <b>0.38</b>	10F1 <b>0.90</b>	32					0.33	GZ32 0.48	PL33 0.85	U404 0.40
IL4	0.20	6AW8A 0.55	6F14 0.65	10F9 0.50		5 I.HI	Maga RRA	ND			GZ33 0.70	PL36 0.55	
IR4	0.35	6BA6 0.25	6F15 0.65	10F18 0.45		-	200	***		0.40			U801 1.00
IR5	0.35	6BE6 0.30	6F18 0.45	10L1 0.45	200				EF95	0.30	HABC80	PL81 0.50	UABC80
		6BF5 0.80	6F23 0.80	10LD11 0.60					EF97	0.65	0.45	PL82 0.45	0,35
I84	0.27	6BF6 0.50	6F24 0.75	10P13 0.55					EF183	0.30	HK90 0.35	PL83 0.45	UAF41 0.50
185	0.25			10P14 1.10		TDAN	IC VA	IVEC	EF184	0.35	KT66 1.70	PL84 0.40	UAF42 0.55
IT4	0.25	6BH6 0.45		12AB5 0.60		INVI	10 17		EF800	1.00	KT88 1.75	PL302 0.80	UBC41 0.50
IU4	0.27	6BJ6 0.45	6F26 0.35						EK90	0.30	N78 1.15	PL504 0.80	UBC81 0.40
IU5	0.50	6BK7A 0.55	6F28 0.60	12AC6 0.40	DETACLED OF	50B5 0.45	CY31 0.35	ECC81 0.33	EL34	0.50	PABC80	PL508 0.90	UBF80 0.40
IV2	0.45	6BL7GTA	6J4 0.50	12AD6 0.40	25Z6GT 0.65		DAF96 0.42	ECC82 0.30	EL36	0.50	0.40	PL801 0.80	UBF89 0.85
IX2B	0.40	0.65	6J5GT 0.30	12AL5 0.45	30A5 0.45	50C5 0.40		ECC83 0.30	EL41	0.55	PC86 0.60	PL802 0.75	UBL1 0.50
2D21	0.35	6BN5 0.43	6J7 <b>0.45</b>	12AQ5 0.48	30AE3 0.40	50CD6G1.65		ECC84 0.30	EL42	0.58	PC88 0.60	PM84 0.50	
3A4	0.35	6BN6 0.40	6K6GT 0.55	12AT6 0.30	30C1 0.30	50L6GT 0.50	DK40 0.55		EL81	0.55	PC97 0.50	PY31 0.30	UBL21 0.60
3B28	2.15	6BQ5 0.25	6K7 0.35	12AT7 0.83	30C15 0.80	83A1 1.50	DK92 0.50	ECC85 0.60			PC900 0.48	PY33 0.63	UC92 0.85
3BP1	2.75	6BR8 0.65	6K8G 0.35	12AU6 0.30	30C17 0.85	85A2 0.40	DK96 0.42	ECC88 0.40	EL83	0.42		PY80 0.85	UCC85 0.40
304	0.40	6BS7 1.30	6K23 0.55	12AU7 0.30	30C18 0.75	90AV 2.50	DL96 0.42	ECC89 0.50	EL84	0.25		PY81 0.80	UCF80 0.58
384	0.35	6BW6 0.85	6K25 0.75	12AV6 0.33	30F5 0.85	90C1 0.60	DY86 0.33	ECC91 0.20	EL85	0.43		PY82 0.30	UCH21 0.60
3V4	0.45	6BW7 0.70	6L6GT 0.45	12AV7 0.50	30FL1 0.70	90CV 1.25	DY87 0.35	ECC189 0.60	EL86	0.40	PCC88 0.55		UCH42 0.70
5R4G)		6BX6 0.25	6L7 0.40	12AX7 0.30	30FL12 0.93	807 <b>0.50</b>	DY802 0.50	ECF80 0.35	EL90	0.35	PCC89 0.50		UCH43 0.78
5U4G	0.33	6BZ6 0.35	6L18 0.45	12AY7 0.70	30FL14 0.75	811A 1.60	E55L 2.75	ECF82 0.35	EL95	0.35	PCC189 0.55	PY88 0.40	UCH81 0.34
5U4GI		6C4 0.33	6LD20 0.40	12BT4A0.55	30L1 0.40	812A 3.50	E88CC 0.65	ECF83 0.75	EL360		PCC805 0.85	PY500 1.00	UCL81 0.60
5V4G	0.42	6C5GT 0.40	6N7GT 0.40	12BA6 0.85	30L15 0.85	813 3.75	E130L 5.00	ECF86 0.65	EL803		PCC806 0.80	PY800 0.50	UCL82 0.34
5 Y 3 G		6CA4 0.28	6P1 0.60	12BA7 0.35	30L17 0.80	866A 0.75	E180F 0.95	ECF8041.50	EL821		PCF80 0.30	PY801 0.50	UCL83 0.60
5Z3	0.50	6CA7 0.50	6P28 0.65	12BE6 0.35	30P12 0.80	5642 0.65	EABC800.35	ECH42 0.70	EL822		PCF82 0.35	PZ30 0.35	UF41 0.6
		6CB6 0.30	6Q7 0.40	12BH7 0.40	30P19 0.80	6080 1.50	EAF42 0.55	ECH81 0.30	ELL80		PCF84 0.50	QQV2·6	UF42 0.6
5Z4G 6/30L2	0.40	6CD6GA	68A7 0.40	12BY7 0.55	30PL1 0.70	6146 1.50	EBC33 0.50	ECH83 0.40	EM34	0.90	PCF86 0.60	2.15	UF43 0.6
		1.15	68G7 0.35	12K5 0.55	30PL13 0.93	6146B 2.50	EBC41 0.55	ECH84 0.45	EM71	0.75	PCF87 0.85	QQV03-10	UF80 0.8
6AB4	0.85	6CG7 0.50	68K7 0.35	12K7GT0.35	30PL14 0.90	6360 1.25	EBC81 0.30	ECL80 0.40	EM80	0.40	PCF801 0.50	1.25	UF85 0.4
6AF4A		6CH6 0.55	68L7GT0.35	12Q7G 0.30	35A3 0.55	6939 2.15	EBF80 0.40	ECL81 0.45	EM91	0.60	PCF802 0.50	QQV03-20A	UF89 0.3
6AG7	0.40		68N7GT0.35	12SR7 0.35	35A5 0.75	7199 0.75	EBF83 0.40	ECL82 0.35	EM84	0.35	PCF805 0.75	5.25	
6AH6	0.50		68Q7 0.40	1487 0.80	35B5 0.65	7360 1.80	EBF89 0.30	ECL83 0.65	EM87	0.55	PCF806 0.70	TT21 2.65	
6AJ8	0.30	6CW4 0.68		20D1 0.45	35C5 0.40	7586 1.25	EC53 0.50	ECL84 0.55	EN91	0.35	PCF808 0.75	TT22 2.80	UL84 0.3
6AK5	0.30	6CY7 0.65			35D5 0.70	7895 1.25	EC86 0.60	ECL85 0.55	EY51	0.40	PCH2000.70	U18/20 0.75	UM84 0.2
6AK6	0.57	6D3 0.45	6T8 0.85		35L6GT 0.50	9002 0.35	EC88 0.60	ECL86 0.40	EY80	0.45	PCL81 0.50	U25 0.75	UY1N 0.5
6AL3	0.43	6DC6 0.75	6U4GT 0.60		35W4 0.30	9003 0.50	EC90 0.33	ECLL800	EY81	0.40	PCL82 0.35	U26 0.75	UY11 0.6
6AL5	0.20	6DK6 0.48	6U8A 0.40	20P4 1.10	35Z3 0.60	AZ1 0.48	EC92 0.35	1.50	EY83	0.55	PCL83 0.65	U31 0.45	UY41 0.4
6AM5	0.32	6DQ6B 0.63	6V6GT 0.88	20P5 1.20	35Z3 0.60 35Z4G 0.30	AZ31 0.55	EC93 0.50	EF37A 0.60	EY86	0.40	PCL84 0.65	U37 1.50	UY82 0.5
6AM6	0.33	6DS4 0.75	6X4 0.80	25C5 0.50		CBL1 0.80	EC8010 2.25	EF39 0.40	EY87	0.43	PCL85 0.40	U52 0.33	UY85 0.8
6AQ5	0.35	6EA8 0.58	6X5GT 0.35	25L6GT 0.45	35Z5GT 0.40	CBL31 0.90	ECC40 0.60	EF40 0.50	EY88	0.43	PCL86 0.45	U76 0.30	Z803U 0.9
6AQ6	0.55	6EH7 0.30	6X8 0.55	25Z4G 0.30	50A5 0.70	· ODDA1 0.80	- MCC-40 0.00	~1.0 0.00	2230				
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Quantity prices quoted on request								
2N404	0.17	28003	1.00	BCY34	0.30			
2N444A	0.25	28034	1.00	BCY72	0.20			
.2N696	0.20	28102	0.40	BCZ11	0.40			
2N697	0.23	28104	0.50	BD121	0.80			
2N698	0.40	28701	0.50	BD123	0.95			
2N705	0.70 0.15	28702	0.50 0,30	BF115	0.20			
2N706	0.15	28746 AC113	0.15	BF167 BF173	$0.25 \\ 0.30$			
2N708	0.20	AC125	0.30	BF181	0.25			
2N753 2N929	0.25 0.30	AC126	0.25	BF184	0.25			
2N930	0.35	AC127	0.20	BF185	0.20			
2N987	0.35	AC128	0.20	BF194	0.20			
2N1131	0.40	AC153	0.25 0.15	BF195	0.15			
2N1132	0.45	AC154	0.15	BF196	0.20			
2N1184	1.25	AC157	0.20	BF197	0.20			
.2N1301	0.40	AC169	0.10 0.25	BFX88	0.25			
2N1302	0.25	AC176 AC187	0.23	BFY17 BFY19	0.40			
2N1304	0.25	AC188	0.30	BFY50	0.25			
2N1305	0.25 0.25	ACY17	0.30	BFY51	0.20			
$2N1306 \\ 2N1307$	0.30	ACY18	0.20	BFY52	0.25			
2N1308	0.40	ACY19	0.25	BSY26	0.25			
2N1309	0.35	ACY20	0.20	BSY27	0.30			
2N1613	0.25	ACY21	0.20	BSY28	0.30			
2N1711	0,30	ACY22	0.15	BSY65	0.20			
2N1756	0.75 0.75	AD140	0.80	BSY95A	0.20			
2N2147	0.75	AD149	0.50 0.35	OC16	0.75			
2N2160	1.25	AD161 AD162	0.35	OC22	0.65 0.60			
2N2217	0.30	AF114	0.25	OC23 OC24	0.60			
2N2218 2N2219	0.40 0.45	AF115	0.30	OC25	0.40			
2N2219 2N2369A	0.45	AF116	0.25	OC26	0.30			
2N2477	0.65	AF117	0.20	OC28	0.60			
2N2646	0.60	AF118	0.45	OC29	0.65			
2N2905	0.50	AF125	0.25	OC30	0.75 0.50			
2N2923	0.15	AF126	0.25	OC35	0.50			
2N2924	0.15	AF127	0.25	OC36	0.60			
2N2926	0.15	AF178	0.40	OC42	0.30 0.20			
2N3053	0.30	AF186 AF239	0.50 0.40	OC44				
2N3055 2N3133	0.75 0.35	AFZ11	0.45	OC45	0.20 0.20			
2N3133	0.50	ASY26	0.25	OC70 OC71	0.25			
2N3391	0.20	ASY27	0.30	OC72	0.25			
2N3391 2N3392	0.25	ASY28	0.30	OC73	0.40			
2N3393	0.15	ASY29	0.30	OC75	0.25			
2N3394	0.15	ASY54	0.25	OC76 OC78	0.25			
2N3395	0.20	ASY74	0.50	OC78_	0.25			
2N3402	0.15	ASY77	0.85	OC78D	0.20			
2N3403	0.15	ASY82	0.20	OC81	0.25			
2N3404	0.35	ASY86	0.20 0.15	OC81D OC83	0.15 0.20			
2N3414	0.20 0.15	BC107 BC108	0.15	OC139	0.35			
2N3415 2N3416	0.15	BC109	0.20	OC140	0.40			
2N3417	0.25	BC113	0.40	OC141	0.60			
2N3702	0.15	BC118	0.80	OC170	0.25			
2N3703	0.15	BC134	0.30	OC171	0.25			
2N3704	0.20	BC147	0.20	OC200	0.30			
2N3707	0.20	BC148	0.15	OC201	0.60			
2N3709	0.15	BC149	0.15	OC202	0.65			
2N3710	0.15	BC152	0.15	OC203	0.40			
2N3819	0.35	BC175	0.25	OC204	0.40			
2N3906	0.80	BCY30	0.85	OC205 OC206	0.70			
28002	1.00	BCY33	0.25	· UC200	0,70			

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D226V	300p.i.v.	300mA	Wire ended	0.15
K D2021	300p.i.v.	1A	Stud mounted	0.20
18113	400p.i.v.	400mA	Wire ended	0.25
DD006	400p.j.v.	500mA	Wire ended	0.25
DD226	400p.i.v.	1 A	Wire ended	0.80
BYZ12	400p.i.v.	6A.	Stud mounted	0.25
DD716	400p.i.v.	35 A	Stud mounted	1.50
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1N649	600p.i.v.	400mA	Wire ended	0.85
18115	600p.i.v.	400mA	Wire ended	0.40
1N2071	600p.i.v.	750mA	Wire ended	0.20
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