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H1-Fi solid state me-amplifier and control unit incorporating treble, bsas, volume and balance controls. Bwitched input for p.u. (magnetic and ceramic), mike and radio. Will also accept tape head. Operates from $9 \mathrm{~V}-12 \mathrm{~V}$ battery ( 20 V max. $7-5 \mathrm{~mA})$. Frequencr response $25 \mathrm{~Hz}-30 \mathrm{kHz} \pm 1 \mathrm{~dB}$. Principaily designed for use with Z 12 Amplifier but full Invtructions ate supplied to enable it to be used with any ampliffer. Size $\left.\left.8 \frac{1}{}^{\prime \prime} \times 2\right\}^{\prime \prime} \times 2\right\}^{*}$ overall plus knobs. Brusbed and polinhed aluminium front and guaranteed, with full insttuctions.

UNR-30 4-BAND COMMUNICATION RECEIVER
Covering $550 \mathrm{Kcg}-30 \mathrm{Mc} / \mathrm{s}$. Incorporates BFO. Built in speaker and phone jack. Metal cabinet. Operatio instructions. Carr. $7 / 6$.

13 gns.
TRIO JR. 310 New Amateur Band 10-80
Metre Receiver in slock. 877.10 .0 .


LAFAYETTE SOLID STATE HA600 RECEIVER
5 BAND AM/CW/G8B AMATEUR AND SHORT WA VE $150 \mathrm{Kc} / \mathrm{A}-400 \mathrm{Kc} / \mathrm{s}$ and $5 \overline{50} \mathrm{Kc} / \mathrm{o}-30 \mathrm{Me} / \mathrm{s}$ FE T front end 2 mechanical flters of Huge dial Product detector © Variahle BFO Noive limitar 8 nieter 24in Bandapread 230V. A.C./12V. D.C. neg. earit operation RF
 S.A.E. for full detaily.

AFAYETTE RA-800 SOLID STATE
AMATEUR COMNOHICATION RECEIVER
Six bands $3 \cdot 5-4,7-7 \cdot 3,14-14 \cdot 35,21-21 \cdot 45,38-29-7,60-54 \mathrm{Mc} / \mathrm{A}$. Dual conversion on all bands. $2 \times 455 \mathrm{Ke} / \mathrm{s}$ nechanical flters. FET tront end, product detector, variable BFO, $100 \mathrm{Kc} / \mathrm{s}$ crystal callibrator. 's' Meter. Huge allde rule dial. Operation 230 V AC or 12 V n. Size $15 \times 94 \times 81$ in. Complete with instruction manual. 857.10 .0 Carr. Paid. $100 \mathrm{ke} / \mathrm{s}$ ersntal 39,6 estra.

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## RECEIVER MODEL 9R-59DE

4 band recelver covering $500 \mathrm{Kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$ continuous and electrical bandspread on $10,15,20$, 40 and 80 metres. 8 valve plus 7 dlode circuit, $4 / 8$ ohm out put and phoue jack. BSB-CW ANL clial 1 IF 4F5 Kc/a Auter Sep. bandspread Variable RF and AF gain controls, $115 / 250 \mathrm{~V}$. A.C. Mains. Beautifully derigned. Bize: $7 \times 15 \times$
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TRIO JR. 500SE 10-80 Metre
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RECEIVERS AR88D
Latest release by ministry BrAND NEW in original casea. $110-250 \mathrm{v}$. A.C. uperation. Frequency in 6 Bands. $535 \mathrm{Kc} / \mathrm{A}-35 \mathrm{Mc} \mathrm{Mc} / \mathrm{sc}$ continuous. Output irnpedance $2 \cdot \bar{u}-600$ ohriss. Ineorporating crystal titter, noise limiter, variable BFO, variable selectivity, ete.
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TELETON CR-10T AM/FM STEREO TUNER AMPLIFIER
 A new model from Teleton. 31 sohid state derices. $4+4$ watt output. Inputs for ceramic/crystal cartridge.
Frequency
range
AM
$540-1600 \mathrm{KHz}$ $\underset{\text { FM }}{\substack{\text { Frequency } \\ 88-108 M H z \\ \text { range } \\ \text { AM } \\ \text { Autornatic } \\ 540-1600 \mathrm{KHz} \\ \text { FM }}}$ $\mathrm{FH}_{\mathrm{M}}{ }^{88-108 \mathrm{MHz} \text {. Autornatic } \mathrm{FM}}$ Stereo reception. Stereo indicator Tone and $R \& L$ volame controls. AFU switch. Stereo headphone socket.


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## First grade quality ${ }_{1}^{2 \frac{1}{2}} \mathrm{in}$. \&quare fronts.

| . $500-0-500 \mu \mathrm{~A} 27 / 6$ | 50ma .....27/6 | 150v. D.C. . 27 |
| :---: | :---: | :---: |
| 1 mA ......27/6 | 100mA ....27/6 | 300 V . D.C. . 27 |
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| $750 \mathrm{~mA} \ldots . . .27 /{ }^{\circ}$ | 3V. D.C. -. $27 / 8$ | 150V. A.C. . 27 |
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Excellent condition. 89/6. Carr. 7/6
TE-40 HIGH SENSITIVITY
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Accurate wide range signal generator cover
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TEAK PLINTHS \& PERBPEX COVER

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## STEREO AMPLIFIER

 A fine new Hi.Fl Amplifter at low cost. $12 \cdot 6$ taputs for Mag or Cer Cartridge, Tuner and Auxiliary. Output 4-1日R. Features Hesdphone Socket, Tape output. Protected output stage. Fintsh simulated walnut vinyl clad metal case with black and brushed anodised £24

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$0 / 10 / 50 / 250 / 1.000$ V.A.C. $0 / 50$ $\mu A / 250 \mathrm{MA} .0 / 60 \mathrm{k} / 6$
-20 meg.
$\mathrm{P}_{\mathrm{to}}$ \& $+6 / 2 / 6$.


MODELPT-34 1.000 OPV. $010 / 50$ /200/500/1,000v AC and D.C. $0 / 1 / 100 /$


$\begin{array}{cc}\text { TE-900 } & 90,000 \Omega / V O L T \\ \text { GIANT } & \text { HULTMMETER }\end{array}$ GIANT MULTIMETER mirror casle and overload
protection. 6 in , full view meter. 2 colour ncale. of
$2.5 / 10 / 2 \overline{0} 0 / 1,000 / 5.000$ $2.5 / 10 / 250 / 1,000 / 5.000$
v. A.C. $0 / 25 / 12.5 / 10 / 50 /$ A.C. $0 / 25 / 12.5 / 10 / 50 /$
$250 / 1.000 / 5,000 \mathrm{v}$ D.C $250 / 1.000 / 5,000 \mathrm{v}$ D.C.
$0 / 50 \mu \mathrm{~A} / 110 / 100 / 500 \mathrm{~mA}$ 10 anp. D.C. $02 \mathrm{~K} / 200 \mathrm{~K}$ / 20 MEG. OHM. E16. P. \& P. 51-.

LAFEYETTE 57 Range Super 50 k / $/$ volt Malti-
 -1000 V. A.C. volts 1.5 V
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D. current $25 \mu \mathrm{~A}-10$ amp. Ohins $0-$ 10 meg $\Omega \mathrm{AB}-20$ to +81 dR. Overload protection. ع12.10.0. Carr. 3/t.
MODEL TE- $300,80,000$ O.P.V.
Mirror scale. overlogd proter-Mirror
tion $0 / 6 / 6 / 3 / 15 / 60 / 300 / 1,200 \mathrm{~V}$ d.c. $0 / 6 / 30 / 120 / 600 / 1,200 \mathrm{I}$. A.C. $0 / 30 \mu A / 6 \mathrm{~mA} / 60 \mathrm{~mA}$
$300 \mathrm{~mA} / 600 \mathrm{~mA} \quad 0 / 8 \mathrm{~K} / 80 \mathrm{~K}$ $800 \mathrm{~K} / 8 \mathrm{meg} .-20$ to +63 db.
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MODEL TE-10A. $20 \mathrm{k} \Omega \mathrm{Volt}$ 5/25/60/250/500/2,500v. D.C. 10/50/100/500/1,000 $0 / 50 \mu \mathrm{~A} / 2.5 \mathrm{~mA} / 250 \mathrm{~mA}$ $0 / 6 \mathrm{~K} / 6 \mathrm{meg}$. ohm. - 20 to 10.0 , $100 \mathrm{mFd} .0 .100-0.1 \mathrm{mFd}$.

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Aesistance 12 ohm to 120 ma
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Postage
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 RESISTANCEATTENUATOR
U11dB. Connections,


Vmbalanced $T$ and
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5in. 600ft. atd. plantic . . . . . . . . . . . . . . . . . $8 / 8 / 8$
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$\mathrm{H15} 30$ Top Kat Silicon Rectifiers $750 \mathrm{~mA} .10 /=$
Mixed volts.

$$
\text { B86 } 50 \begin{aligned}
& \text { Sil. Diodes sub. min. IN914 and IN916 } \mid 0 / m \\
& \text { types. }
\end{aligned}
$$

H168 $\begin{aligned} & \text { Experimenters' Pak of Integrated } \\ & \text { circuits. Data supplied. }\end{aligned}$
B88 $50 \begin{aligned} & \text { Sil. Trans. NPN, PNP, equivalent to } \\ & \text { OC200/1, } 2 N 706 A, \\ & \text { BSY } 95 A, ~ e t c . ~\end{aligned}$,
10
B60 107 Watt Zener Diodes. Mixed voltages. $10 /=$
H20 $20 \begin{aligned} & \text { BY126/7 type Silicon Rectifiers } 1 \mathrm{amp} \| 0 /= \\ & \text { plastic. Up to } 1,000 \text { volts. }\end{aligned}$
NEW TESTED \& GUARANTEED PAKS
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| $\left.\mathrm{H} 84 \quad \begin{array}{l}\text { BY127 Silicon Recs. } \\ \text { Plastic. Replaces the BY100 P.I.V. } 1 \text { amp. } 10 /=\end{array}\right)$ |
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B935 GETI13 Trans. equiv. to ACY17 to $|0|=$

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 2500 v．b．C．（ iurrent $0-50 \mathrm{uA}, 0-250 \mathrm{IIA}$ ． Revistauce 0－g0K $0-6$ Meg ohm．Deci－ bels－ 20 to +24 dP Size of meter 418 $34 \times \mathrm{in}$ ．Complete with leather cas TI－TESTER
20.000 p．p．v．DC voltage 5－25－50－250－500－2．5 $\mathrm{K}(20,000$ ohmar per volt $)$ ． AC voltage： $10-50-100-$ obme per volt）．DC： Gurrent： $0-50$ uA， $0-2.5$ $\mathrm{mA}, 0-250 \mathrm{~mA}$ ．Resistance： （ 300 ohm and 30 K at Copacitance：10t to al centre nerie）． Copacitance：10t．Do Decibels：－ 10 to $+\cdots$ inf ．Nize $4+\times 3 \frac{1}{2} \times$ lin． $71 / \mathrm{m}$ ．\＆P．

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fantastic stereo amplifter thade exelu－ sively for Lind－Air and representin cols－ miderabie advance in moin state stereu amplliers．Inputs and proviaion for fiern panel with bask treble balance and volume controls atmo on／ofl and stereo／mono nwileh．Output 5W per channel music power．Frequeney response $40-20,000 \mathrm{~Hz} 8-16$ shri apraker matching．Size 16！＂$\times 14^{\prime \prime} \times 4^{\prime \prime}$ ．


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$2025 \mathrm{~T} / \mathrm{C}$ with stereo cartridge ． 28.18 e
9TA ECD 日tereo cartridge ．．．．．．． 110.19 ． L65B II ．．．．．．．．．．．．．．．．．．．．．． 10.18 .6 Base and cover for above

## ${ }_{\text {AL72B }}$

3L75R
SL95B
Base and co．．．．．．．．．．．．．．．． 88．19．0 ．\＆P．Decks 12／A．Bese \＆Cover $10 /-$ Deck／Base／Cover $17 / 6$ ．
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This superb stereo system is a real price break through. It comprises the VISCOUNT F.E.T. Mk I amplifier on which full details are given below, the famous Garrard SP 25 Mk II (including teak veneer base and transparent cover) with diamond cartridge or 2025 TC and the very successful DUO type 2 speakers. Measuring $17 \frac{1}{5}$ in $\times 10$ in $\times 6 \frac{3}{4}$ in, the Duo type 2 speakers are beautifully finished in teak veneer with matching vynair grifls. They incorporate a $10 \frac{1}{3}$ in $\times 6 \frac{1}{4}$ in drive urit and high frequency speaker, both of which are of 3 ohms impedance. The Duo speaker system is also available separately at $£ 6.6 .0$ each, plus $15 /-\mathrm{p}$. \& p.

Complete stereo system $£ 41$ plus 82.10 . p. \& p.

High fidelity transistor stereo amplifier employing field effect transistors. With this feature and accompanying guaranteed specifications below, the Viscount F.E.T. vastly surpasses amplifiers costing far more.

Specification-Output per channel 10 watts r.m.s. Frequency bandwidth 20 Hz to 20 $\mathrm{kHz}+1 \mathrm{db}$ at 1 watt. Total distortion at 1 kHz at 9 watts $0.5 \%$ Input sensitivities CER. P.U. 100 mV into 3 meg ohms. Tuner 100 mV into 100 K ohms. Tape 100 mV into 100 K ohms. Overioad Factor Better than 26 db .

Signal to noise ratio-70db on all inputs (with vol. max). Controls- 6 position selector switch ( 3 pos. stereo and 3 pos. mono). Separate volume controls for left and right channels. Bass $\pm 14 \mathrm{db}$ at 60 Hz . Treble (with D.P.S. on off) $\pm 12 \mathrm{db}$ at 10 KHz . Tape recording output sockets on each channel. Size $12 \downarrow \mathrm{in}$. 6 in. $2 \underset{3}{2} \mathrm{in}$. in teak-
finished case. BUILT \& TESTED. Mkll (MAG P.U.) $£ 15.15$ plus $10 /-\mathrm{p} . \& \mathrm{p}$. Specification same as Mk. 1, but with the following inputs. Mag: P.U. CER. P.U. Tuner. Spec. on Mag. P.U. 3 mV at 1 kHz input impedance 47 K . Fully equalised to within $\pm 1 \mathrm{db}$ RIAA. Signal to noise ratio65 db (vol. max).

## The f29-10-0 Stereo system

The Duetto is a good quality stereo amplitier, attractively styled and finished. It gives superb reproduction previously associated with amplifiers costing far more.

## SPECIFICATION-

R.M.S. power output 3 watts per channel into 10 ohms speakers.
INPUT SENSITIVITY. Suitable for medlum or high output crystal cartridges and tuners. Cross-taik better than 30 dB at $1 \mathrm{Kc} / \mathrm{s}$.
CONTROLS: 4-position selector swltch (2 pos. mono and 2 pos stereo) dual ganged volume control.


TONE CONTROL Treble lift and cut Separate on off switch. A preset balance control.

Duetto integrated transistor stereo Amp. Garrard Changer from
Cover and teak finish plinth
Duo Type I speakers (aze opp, page) The above items purchased together

ع8.16.0 + $7 / 6$ p\&p.
ع7.16.6 + 7/6 p\&p.
EA.15.0 + $7 / 6$ pap.
ea. s. $4.0+7 / 6 \mathrm{pAp}$.

## CAR TRANSISTOR IGNITION SYSTEM

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For 6 volt or 12 volt positive earth systeme, Comprising: apecial high voltage working bermetically realed silicon transistor mounted in finned beat-sink, higb output ignition coil, ballast resistor and hariwear (screws, washers, ete.).

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## THE DUO SPEAKER SYSTEM

Similar in design to those on the previous page the 2 . way speaker system is beautifully finished in polished teak veneer, with matching vynair grille. It is ideal for wall or sbelf mounting either upright or horizon. taily.

Type 1 SPBCIFICATION:
Impedance 3,8 or 10 ohros (please state requirement). It incorporates Goodmans high flux 6 in $\times 4$ in speaker and $2 \frac{1}{2}$ in speaker. Teak finish $12 \mathrm{in} \times 6 \underline{q} \mathrm{in} \times 5 \mathrm{in}$. 4 guineas each. $7 / 6 \mathrm{p}$. \& p .

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An extrumely reliable general purpnae valve anuplifier. Its rugged conntruction yet upace age atyling and deajgn maker it by far the lient value for money. TECHNICAL SPECIFICATIONS
3 electronically mixed channels, with is inputa per channel. cnables the use of 6 separate instruments at are same time. The volume controls for each chamel pockete. gENSITIVITIES AND INPUT IMPEDANCES Channels 1 and 24 mV at 470 K . These 2 channels (4 inpuls) are enitable for microphone or cuitars. Channels 3 and 4300 mV at 1 m . Sultatile for most high coutput instruments (gram, tuner, organ, etc). Input


## EXTRACTOR FAN

A.C. mains $230 / 259 \mathrm{y}$. complete with pull switch. Size: $6 \times 6 \times 4 \mathrm{in}$.
Price 27/6 plus 7/6 P. \& P.


## SPECIFICATIONS

Ontput-10 watts. Output imperlance--3 to 4 whins Inputs-1. -xtal nic 10 mV Tone Controls-Treble control range $\pm$-gram aradio $250 \mathrm{~m} \mathbf{V}$

Bass control range $\pm 13 \mathrm{~dB}$ at 100 Hz , Frequency Response (with tole controlk ceniral) Minus $3, \mathbf{i} \mathbf{B}$ points at 20 Hz and 40 K Hz . Bignal to Noise Ratin-better than
 Mains input- $290 / 250$. A.C. size of chasyis- 101 in $\times 4$ zin $x$ 2 2in. For use with Stil. or L.P. records, nusical instrumenth, all makes of pict-ups and mikes. Reparate bases and treble lift control. Two inpuls with control tron gram. and bithe. Built and tested.
RELIANT Mk. I
As above less teak case
$\mathbf{£ 6 . 1 0}$ plus 7/6 P. \& P.
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In teak finixhed caur £7.5 plus 7/6 P. \& P.
sensitivity relative to 10 w utpul. TONE CONTROLS ARE COMmON 20 ALL Cut- -13 dB at 60 Hz . Treble Boost +11 dB at 15 KHz . Treble Cut puints are 30 Hz and 20 KHz . POWER OUTPUT: For Rpeech ant punsic 50 watts rms. 100 watts peak. For sustaineil nuxic 40 music 50 watts rms. 100 watts peak. For bustaine
watis inus. 90 watts peak. For sine wave 3 . 5 wat in rnin. Nearly 80 watts peak. Total distortion at rated output $3.2 \%$ at $1 \mathrm{KH} \%$. Total distortion at 20 watts $\mathbf{0 . 1 5} \%$ at 1 KHz . Outpnt to match into 8 or 15 ohms spea ker aystem. NEGATIVE FEEDBACK 20 dB




This PReBTOLOCK 5 station Puab-Button Tuner Heart wfh Manual Over-ride is an ideal basis for a quality AM car radio. Size $6 \frac{1}{2}^{*} \times 4^{*} \times 2^{*}$.
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amps (eomervatively rated). The folluwhy combinations may be uned. l.23.0-23 volts 2.41 volta.

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| ${ }_{\substack{23 \\ \text { 2x3724 }}}$ | ${ }^{39}$ |  |  | ${ }_{\substack{\text { ciliz } \\ \text { BCl2 }}}$ | 年 | erx | 边 | Tx53 |  |

## RESISTORS

| Code | Power | Tolerance | Range |
| :---: | :---: | :---: | :---: |
| c | 1／20w | 5\％ | \＄2 $\Omega$－220K $\Omega$ |
| ¢ | 1／8w | 5\％ | $4.78-330 \mathrm{~K} \Omega$ |
| c | 1／4W | 10\％ | $4.7 \Omega$－10M $\Omega$ |
| c | 1／2W | 5\％ | $4 \cdot 7 \Omega-10 \mathrm{M} \Omega$ |
| C | 1W | 10\％ | $4.7 \Omega-10 \mathrm{M} \Omega$ |
| Mo | 1／2W | 2\％ | $10 \Omega-1 \mathrm{M} \Omega$ |
| WW | 1W | $10 \% \pm 1 / 20 \Omega$ | $0 \cdot 2 \Omega-3.9 \Omega$ |
| Ww | 3 W |  | $12 \Omega-10 \mathrm{~K} \Omega$ |
| ww | 7 W | 5\％ | $12 \Omega-10 \mathrm{~K} \Omega$ |

Codes：$\quad \mathrm{C}=$ carbon fum high stability low noiar Mo＝metal oxide Flectrosil TRS ultra．low noise

Falues：
E12 denntes peries： $10,12,15,18,22,27,33,39,47,56$ ， $68,8 \%$ and their tecader．
E24 denotes series：as E12 plus 11，13，16，20，24，30，36， 43， $51,62,75,91$ and their decades．

## INTEGRATED CIRCUIT <br> \section*{AMPLIFIERS}

SINCLAIR IC10 complete with instruction book giving amplifier circuit details and range of applicationgs $59 / 6$ nett．
PLessey slana Now only $42 / 6$ nett $3 W$ into $7.5 \Omega$ for 18 V supply．Application data sent wilh iwo more．

WAVECHANGE SWITCHES LONG SPINDLES
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s－DeC＇s put an end to＂birdenesting＂．Components just plug in．Saves valuable time．Use compouents again and
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| Values | 1 to 9 | 10 to 99 | 100 up |
| :---: | :---: | :---: | :---: |
| available |  | （see noto below） |  |
| E12 | 18. | 16 | 15 |
| E：24 | 2.5 | 2 | 1.75 |
| E12 | $\pm .5$ |  | ${ }^{1.75}$ |
| E24 | 3 | 2\％ | $2 \cdot 25$ |
| E12 | 6 | $\stackrel{1}{5}$ | 4.5 |
| $\mathbf{E 2 4}$ | 9 | 8 |  |
| E12 |  | $15 \mathrm{dall} q$ quatities |  |
| E12 |  | 15 dall quantities |  |
| E12 |  | 18d all quantities |  |
| Prices are in pence each for same ohmic value and power rating，NOT mixed values．（Ignors fractions of $1 d$ ．on total restator order） |  |  |  |

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$250 \mathrm{~V} 20 \%$ ： $0.01 ; 0.022 ; 0.033,0.047$ 8d ea． $0.068: 0.1$ gd en．； $0.1511 \mathrm{~d}, 0.221 /-, 10 \%: 0.331 / 5,0.471 / 8,0.68$ MULLARD SUB－MIN ELECTROLYTIC C426 range axial héad

1／3 each
Values（ $\mu \mathrm{F} / \mathrm{V}$ ）$: \mathbf{0 . 6 4 / 6 4 ; 1 / 4 0 : 1 . 6 / 2 5 ; 2 . 5 / 1 6 ; 2 . 5 / 6 4 ; 4 / 1 0 ;}$ $4 / 40: 5 / 64 ; 6 \cdot 4 / 8 \cdot 4 ; 8 \cdot 4 / 25 ; 8 / 4 ; 8 / 40 ; 10 / 2 \cdot 5 ; 10 / 16 ; 10 / 64$ ； 129／5／45；16／40；40／16：200／64：25／6．4；25／25；32／4：93／10： $32 / 40 ; 32 / 64 ; 40 / 16: 40 / 2 \cdot 5 ; 50 / 6 \cdot 4 ; 50 / 25 ; 50 / 40 ; 64 / 4$ ； 64／10：80／2．5： $80 / 76$ ：80／25：100／6－4：125／4：125／10； 125／16；160／2．5；200／6•4；200／10；250／4；320／2．5；3 $30 / 6 \cdot 4$ ； 400／4：500／2．5．

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High ripple purrent types：1000／25 5／6；1000／50 8／2； 1000／100 16／8；2000／25 7／4；2000／50 11／4：2000／50 11／4； $5000 / 50$ ع1／11； $5000 / 100588 / 8: 10000 / 15$ 17／－： $10000 / 25$ 24／8；10000／50 44／－； $10000 / 70$ 61／－．

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## TOPIC OF THE MONTH

## Women, arise!

WHAT with the establishment of the principles of equal pay and equal rights for women, the unisex concept and other such manifestations of emancipation, perhaps it is about time we did something about this parity of the genders in this hobby of ours.
For long years, women have been favoured by management to perform those delicate tasks in assembly and inspection etc., so admirably suited to their special temperament and this is increasingly evident in the radio and electronics industries. But after leaving the factory or laboratory they seem to lose interest. They want to wash their hair, go to the pictures or watch the telly, when what they really ought to be doing is getting to grips with F. G. Rayer's latest creation in Practical Wireless!

With their gentle touch and infinite patience, the wiring. up of the modern generation of miniature components ought to trouble them not the slightest. And think of the fruitful field for gossip that can be extracted from the tales of constructional triumphs . . . . "she said Radio Australia came booming out the first time she switched on. She hadn't even got the dial on straight. And the colour scheme of the cabinet!"
We admit that many ladies are involved in amateur radio but most of them take a fairly passive (or resigned!) part in the proceedings, eyeing with varying degrees of distaste the activities of their eccentric menfolk. Before the last war there were just two licensed lady radio amateurs among the ranks of several thousand in this country. The Services, however, took advantage of their usefulness as wireless operators and mechanics and this was the launching pad for many who decided to take up radio as a hobby-and as a hubby, for most of them seem to have been snapped up by male radio enthusiasts who realised they were on to a good thing!

Today the number of licensed ladies is well over 50 strong and still growing. But we could do with more support on the constructional side. We ought to persuade our betters to join us and let them share our pleasures (and agonies). Apart from brightening things up and allowing us more time with the hobby, we'd have another pair of hands to do some of the donkey work. But that is quite beside the point!
W. N. STEVENS-Editor.

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# NOVEMBER ISSUE WILL BE PUBLISHED ON OCTOBER 9 

## NEWS... NEWS... NEWS...

## Radio Bristol

Shown right is the v.h.f. service of Radio Bristol. Frequency is $95 \cdot 4 \mathrm{MHz}$ with horizontal polarisation. Maximum e.r.p. is 5 kW with a directional aerial. The inner and outer service area boundaries correspond to average field-strength contours of 60 and 48 dB (relative to 1 microvolt per metre) respectively for a receiving aerial height of 30 ft above ground level. The field strength at a particular site may differ by 10 dB from that indicated.

## R.R.E. Courses

A Radio Amateurs' Examination Course is to be run this winter by Glasgow Corporation Further Education Department at: The Glasgow College of Nautical Studies, 21 Thistle Street, Glasgow, C. 5 .
The course will meet at the College on Tuesdays and Thursdays from 7-9.30 p.m., commencing Tuesday, September 15th, 1970. Enrolment will take place at the College at 7 p.m. on the opening evening, and the fee for the course is $£ 3$, payable on enrolment. Students under the age of 18 on August 1st, 1970, will not be required to pay a fee.

The syllabus of the course embraces theory, licence conditions, and morse instruction, and no prior knowledge is assumed or required.
There will be a Radio Amateurs’ Examination Course on Wednesdays, $6.30-9$ p.m., starting September 23rd. Enrolments: Wednesday and Thursday September 9th and 10th, and Wednesday, September 16th, from 6.15-8.15 p.m., Room 8, Acton Technical College, opposite Acton Town Hall, Acton, London, W. 3.
Fee: For three terms, f3. Lecturer: W. G. Dyer, M.I.E.E., G3GEH.
The Cove Further Education Centre (Hampshire) will be running a R.A.E. Course in midSeptember. Further details may be obtained from P. D. Dimmick (Principal), Cove Secondary School, St. John's Road, Farnborough, Hants.


## Mullard puts the brakes on



Mullard Ltd. recently announced details of a new car braking system using electronics. The system is designed to prevent a road wheel from locking when the vehicle driver applies too much force to the brake pedal. When a separate anti-lock control is used on each wheel, not only can full steering be available under maximum braking conditions, but shorter stopping distances result. The control circuit monitors wheel speed by means of a toothed wheel mounted on the hub. A magnetic pickup fixed near this wheel supplies a pulse train to the control circuit. Pulse frequency is proportional to wheel speed and so contains all information necessary to deduce deceleration, acceleration and speed. The circuit senses the condition in which a wheel is likely to lock and if
this tendency continues, energises a hydraulic solenoid valve to relieve brake pressure.

Mullard Ltd. state that the whole system represents the result of a research project carried out at their Research Lab. and further development of parts of the system must be undertaken by car and brake manufacturers before the device can be applied to cars during their manufacture.

Pictures show the experimental circuit used for each anti-lock control and the anti-lock actuator inside the wheel.


## NEWS... WEWS... NEWS...

Bench vice for the radio shack
The Lockjaw is a bench vice announced by the Vice \& Workholding Co. Ltd. The jaws give a remarkable capacity to grip difficult shapes and delicate objects. With its suction clamp and ' $G$ ' clamp, the Lockjaw is a very portable device. It can also be bolted down to a bench, and makes a very useful addition to the wireless 'shack'.

Grooves in the jaws enable a positive hold to be obtained when gripping washers, rods, printed circuits and components. Jawgrips are available with a rubber face for delicate work or silicon metal for harder usage. The silicon metal ones are supplied as standard. One jaw provides a rocking motion so that the face adjusts to work which tapers. If this jawgrip is turned round it is locked into a straight position.
The vice weighs under 4 lb and the body is constructed of fine grain silicon alloy metal. It is claimed to hold as strongly as a typical cast-iron type eight times heavier. Jaw width is 4in and overall length closed 8 in.
Price of the Lockjaw including silicon metal jaws is 86 s . The ' G ' clamp base is 30 s and the rubberfaced jaws for delicate work 14 s a pair. Manufacturers are: Vice and Workholding Co. Ltd., 149a Crayford Road, Crayford, Kent.

## Gravesend. . .

The above Club has now moved from King's Farm Community Centre, Gravesend, to new premises at the Northfleet Recreation Centre, Springhead Road, Northfleet, Kent, and meetings are held on Thursdays from 7.30 p.m. to 10.30 p.m.

They have taken larger premises as they are anxious to extend their membership and any person interested in Radio will be most welcome; there is no age limit.

Anyone interested in joining, should contact Allen J. Moules, after 7 p.m. weekdays at hometel. no. Gravesend 2965.


## I.S.W.C.

The International Short Wave Club will be pleased to send readers a copy of their bulletin International Short Wave Radio, if they would care to make application to them enclosing return postage. The address is: Mr. Arthur E. Bear, 100 Adams Gardens Estate, London, S.E.16.

## Audio 70

The date of the New Northern International High Fidelity Festival, at the Cairn Hotel, Harrogate, is September 18th20th. Many well-known companies will be exhibiting.

## Mobile Conference

One of the first large scale conferences on the subject of mobile radio was held at Brunel University from June 30 to July 2. Organised by the Society of Electronic and Radio Technicians, it comprised eleven contributions from both industry and users. In his concluding address, Mr. J. W. Grandey (Gresham Lion) Chairman of the Conference Organising Committee, said that during his discussions with delegates he had been struck by the interest aroused by the contributions. He felt safe in saying that this Conference had been highly successful from every point of view; not least in bringing together over 120 representatives of all branches of this increasingly important field of electronics. The manufacturing industry was well represented as were the Home Office, Electricity and Gas Boards, Police and British Rail.

Most of the material presented at this Conference was new and had not previously received a public hearing. Many of the delegates were unaware of the work being carried out by various organisations, such as the Home Office, in looking to the future of mobile radio. Mr. E. W. Crompton proposed the adoption of a new system of modulation, double side band suppressed carrier, which appeared to provide two advantages, higher range and narrower bandwidth. Some of the recent work carried out by industry in providing new or better applications of mobile radio were also described. Mr. Welsh and Mr. Carey of Cossor proposed a system of vehicle location using phase measurement which had not previously been publicly described and Mr. N. C. Croft of Storno presented a paper on Automatic Extension Ringing from Vehicles.

One of the pressing problems in this rapidly expanding field is frequency availability. This kept cropping up in discussion and was dealt with at length by Mr. D. B. Balchin of the Ministry of Posts and Telecommunications.

# TRANSIST 9 R \& D $\ddagger$ ODE 



THE Transistor and Diode Tester to be described will rapidly check transistor leakage current and measure current gain (beta), over a range of collector currents, up to 5 mA , for both n.p.n. and p.n.p. transistors. It is also suitable for checking semiconductor diode forward conduction and reverse leakage current. The tester is simple to build and contains only passive components.

## Circuit

The d.c. beta, or $h_{\text {Fe }}$, of a transistor is the ratio of the collector current to the base current, beta $=\frac{\mathrm{lc}}{\mathrm{jb}} \mathrm{A}$ simple set-up for measuring beta is shown in Fig. 1 The base bias is adjusted to give a convenient value of Ic and the base current Ib, is read off and the calculation made.


AFig. 1.

Fig. 2. 7


To avoid the necessity of reading Ib from a meter, the base could be fed with a known value of current, say $1 \mu \mathrm{~A}$, from a known fixed supply voltage through a known value resistor, as shown in Fig. 2. The Ic, in $\mu \mathrm{A}$, would then be a measure of the beta, e.g. $60 \mu \mathrm{~A}$ Ic would indicate a beta of 60 .


It is often useful to measure beta at different values of Ic, and a basic circuit for doing this is shown in Fig. 3.

In this circuit, R7 is a 5 mA shunt for the $500 \mu \mathrm{~A}$ meter and with S2e closed, the meter reads 5 mA full scale deflection. If, for example, it is desired


A Fig. 3.

Fig. 4. 7



Fig. 5 : Complete circuit of the transistor and diode tester.
to test the transistor at 2 mA Ic, VRI is adjusted to provide sufficient Ib to give an Ic of 2 mA , as indicated by MI (accepting that VR2 and R6 have negligible effect on the accuracy of MI).

The current through M1 is then 'backed-off' by an equal and opposite current, provided by VR2 and R6, until M1 indicates zero. This action may be more easily seen if the circuit is redrawn in the form of a Wheatstone bridge as shown in Fig. 4.

With zero reading on M1, S2e is now opened,

## components list

## Resistors

| R1 | $10 \mathrm{M} \Omega$ | R5 | $12 \mathrm{k} \Omega$ |
| :--- | :--- | ---: | :--- |
| R2 | $1 \mathrm{M} \Omega$ | R | $1 \mathrm{k} \Omega$ |
| R3 | $1 \mathrm{M} \Omega$ | R7 | $12 \Omega$ |
| R4 | $56 \mathrm{k} \Omega$ |  |  |

VR1 10k $\Omega$ potentiometer, wire-wound
VR2 $500 \Omega$ potentiometer, wire-wound

## Capacitors:

C1/2 470pF disc ceramic

## Switches:

S1 2 wafers, each 3 pole 4 way, on Maka-Switch shafting unit (Henry's Radio)
S2 1 wafer, 4 pole 3 way, on Maka-Switch shafting unit (Henry's Radio)
S3 Push button (Micro Omron VAQ-40-45 (Henry's Radio)

## Miscellaneous:

M1, Meter, $500 \mu$ A f.s.d. (Henelec MRA-65B Henry's Radio)
Die-cast box (Eddystone 6357P, Home Radio)
Knobs (2-PK, 2-WK, Radiospares)
Terminals (3-Paignton PK 12K Home Radio)
Transistor socket. Handle. Plastic feet. Battery connectors
thus disconnecting the 5 mA shunt and returning M1 to $500 \mu \mathrm{~A}$ f.s.d.

To read beta, S3 is closed and the known current, Ib, provided by R1, causes an increase in Ic which is indicated by MI. As previously mentioned, the value of Ib is chosen so that M1 gives a direct reading of beta.

The backing-off current feed resistor R6, has a slight shunting effect on M1, making the meter read about $550 \mu \mathrm{~A}$ f.s.d. The value of R1 is therefore chosen accordingly and the facility of reading beta directly is retained.
The method of testing applies equally to p.n.p. and n.p.n transistors, although provision must be made to reverse the polarity of the supplies, and of course the connections to M1.
The complete circuit of the transistor tester is shown in Fig. 5, and here S1 is the 'PNP-NPN' switch which also has a centre 'off' position.
The function switch, $\mathbf{S} 2$, switches the meter shunt, R7, the backing-off feed R6, and allows for two ranges of beta $0-500$ and $0-100$ to be provided by switching two values of Ib through R1 and R2+ R3 to the base of the transistor.

Diodes may be checked by connecting between the emitter and collector terminals, when forward and reverse current is indicated. The forward current is limited to $500 \mu \mathrm{~A}$ by R 5 .

## Construction

The transistor tester is built in a $7 \frac{1}{4} \times 4 \frac{1}{2} \times 3 \mathrm{in}$. deep Eddystone die-cast box, type 6357P. The lid of the box forms the front panel and the drillings for this are shown in Fig. 6.

The meter M1, is a Henrys 'Henelec' MRA-65A $500 \mu \mathrm{~A}$ moving coil instrument. It should be noted that this meter is a later type to the 65 series illustrated in Henry's catalogue and has slightly different drilling requirements.


A Fig, 6: Drilling details of front panel.

T Fig. 7: Wiring diagram of tester. The wafers of switch S2 have been separated for clarity.

The switches are Radiospares Maka-Switch types and it is important for these to be assembled with the markings on the switch wafer facing the switch mechanism. No spacers are used between the wafers but a 6 BA washer is fitted between the front wafer and the switch mechanism. The connections to the switch wafers are shown in Fig. 7.

The tester is powered by two PPI batteries and these fit into the die-cast box as shown in Fig. 8. A strip of polythene or similar material is required between the batteries to prevent an accidental short circuit between the battery connectors. Two 470 pF disc ceramic capacitors, Cl and C2, are connected across the transistor socket and terminals to prevent parasitic oscillation of the transistor under test.
To give a good external appearance, the box is sprayed with one of the popular car enamel aerosols and lettered with Letraset lettering, sheet 209.



Fig. 8 : Positioning of the two batteries inside the case.

## Operation

1. Before connecting the transistor or diode, check the settings of the controls,

Set Ic
Back off
Function Switch Polarity Switch
fully anti-clockwise fully clockwise to 'Ico"' to 'OFF'
2. Connect the transistor to the terminals or socket and switch to 'PNP' or 'NPN' as appropriate. The meter now reads $0-500 \mu \mathrm{~A}$ of collector leakage current with the base open circuit (Ico'), at a collector voltage of 6 volts. If the meter reads full scale, the transistor is probably faulty and no further tests should be made. (Some very large germanium power transistors may have leakage currents of this order and may not necessarily be faulty. These are outside the capabilities of this tester.)
3. Set the function switch to 'Ic.'


Completed tester. Compare with the wiring diagram, Fig. 7.
4. Set the 'Set Ic' control for a suitable value of Ic. The meter reads 5 mA f.s.d. For small a.f. and r.f. types $1-2 \mathrm{~mA}$ is suitable, higher currents may be used for higher power types.
5. Adjust the back-off control for zero reading of Ic.
6. Set the function switch to 'Beta 500 ' or ' 100 ' and if necessary re-zero the meter with the back-off control.
7. Press the Beta button for a direct reading of beta.
8. Photo-transistors may be checked as normal transistors providing that they are not exposed to light. The sensitivity to light may be checked by setting the tester to Step 3 and alternately exposing and shielding the photo-transistor to and from light. The 'Set Ic' control should be set to minimum (anti-clockwise).
9. In the testing of semiconductor diodes, the cathode should be connected to terminal $C$ and the anode to terminal E .
10. Set the function switch to Diode.
11. Set the polarity switch to 'FOR' for the forward conduction test. The forward current is limited to $500 \mu \mathrm{~A}$.
12. Set the polarity switch to 'REV' for the reverse leakage test. The reverse current, $0-500 \mu \mathrm{~A}$, is measured at 6 volts.
13. Switch OFF before returning the controls to the positions given in Step 1.

## Identification

A simple method of identifying p.n.p. or n.p.n. transistors is to insert the unknown type in the socket and temporarily short circuit the E and B terminals with a piece of wire. With the function switch at 'Ico',' turn the polarity switch to 'PNP' and then 'NPN,' the position which produces little or no current reading indicates the transistor type. The short circuit may then be removed and testing carried out in the usual way.

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OCTOBER 20th-24th (10 a.m.-9 p.m. each day)
The PRACTICAL WIRELESS stand will feature many constructional items.


THE small organ to be described in this article can be built in an evening. If it is built as described, then it will give two octaves, one above and one below 'Middle C'. Full constructional details are given, so that even a relative newcomer to electronics should find no difficulty in building this organ.

## Circuit

The organ consists of three sections, the circuit diagram being given in Fig. 1. Tr2 and $\operatorname{Tr} 3$ together form an astable multivibrator, tuned by VR1-VR25, R9, C5 and C6. It is sometimes difficult to make a transistorised multivibrator begin to oscillate. However, by the omission of the emitter bias resistor to Tr 2 , the necessary imbalance is produced.

The output transistor, Tr4, uses a transformer T1 for its load to match the speaker. A tremolo is provided by the low frequency oscillator TrI , and this
keyboard can be made. Using $\frac{1}{8}$ th inch 'Cir-kit' strip, a series of copper strips are laid out as shown in Fig. 2. Note that the corners of strips 2 and 24 are cut off slightly.

Next the variable resistors are fitted around the edge of the board, and VR23-25 are placed in the centre. To ease the task of tuning, these are angled back, so that the tags come through the holes indicated. Wires are now connected along the top as shown, and underneath from the wipers to the copper strips.

The wiper of VR1 goes by the wire numbered 1 to the note 1 , etc. The notes 18 and 19 are connected on the top of the board. All the wires should be kept short and as close to the board as possible. A length of wire (about $1 \frac{1}{2}$ inches) is attached to the point $Z$.

The main part of the circuit can then be assembled. Firstly, the copper strips should be broken as indicated in Fig. 4. On the plain side of this board (Fig. 3), the connecting wires to the speaker, switch


Fig. 1 : Circuit of the mini organ. Tr1 provides the tremulo effect, Tr2-3 form the multi-vibrator oscillator and Tr 4 the audio amplifier.


Fig. 2: Layout of the 'keyboard'. Compare with heading photograph.
and battery should be connected, and the wire from the point Z added.

The resistors should be added next, followed by the capacitors (except C4). The switch and the output transformer can then be fixed in place, along with the shorting links. If the transformer specified is used, then the fixing tags should be removed, and the transformer glued to the board, using Araldite (or a similar adhesive).
The four pins to the windings will fit directly onto Veroboard of 0.1 inch matrix-the secondary winding being nearest the edge of the board. Next the transistors can be soldered in. The base diagrams are given in Fig. 5. It is important to get the wires the right way round, and to use a heat shunt between the soldering iron and the transistor can. A pair of pliers held firmly on the wire being soldered will make an excellent heat shunt.
If C4 is not provided with an insulating sleeve


Close-up of some of the pre-set potentiometers which enable the organ to be tuned
around it, then one must be put on the emitter lead of Tr 2 , which passes underneath. C4 can then be fixed in place. The capacitors C5, C6, and TrI, Tr2 and Tr 3 should be laid against the board.
The stylus can be easily made from an old ballpoint pen. The ball tip is removed, and the end soldered over-this removes the possibility of any ink coming onto the keys (see Fig. 6). The cut down body (about 4 inches) has a slot cut in one side at the end, and a wire passed through here, and soldered to the back of the metal part of the pen. This is then glued back in the plastic body, the wire pulled out through the slot, and the end cap replaced.

About a foot of wire is then left from the end cap to the point A49 on the Veroboard, to which the free end is fixed. The speaker is connected to the wires provided for it, and the battery leads connected to a suitable battery connector.

## Tuning

Each note is sounded by touching the stylus tip against the corresponding copper strip. The prototype was tuned using the services of a musician and a tuning fork. From the A of the fork, the top C was tuned (using VR1), then the notes 2, 3 and 4 tuned to be of equal intervals in pitch, until note 4 ("A") corresponds exactly to the tuning fork.

The rest of the tuning is completed in a similar

Fig. 3: Lower circuit board which forms the base of the organ. This board may be deeper, as shown in the photographs.

manner--getting equal intervals between successive notes. When completed, notes 1, 13 and 25 should be at octave intervals apart. If an alternative method is required, then the notes can be tuned to be of the same pitch as the corresponding note on a piano. The long strips of copper on the keyboard are equivalent to the white notes on a piano-the short strips to the black notes.

Whichever method is used, once a note has been
set it should be left-the tuning is incremental, so altering one note will affect all the notes below it in the chain. The values of the variable resistors used in the prototype should be used for the range suggested (VR1 and VR14-VR25 are $5 \mathrm{k} \Omega$, VR2VR13 are $1 \mathrm{k} \Omega$ ). Higher values would work of course, but tuning would become difficult. Once tuning is complete, the keyboard and switch should be bolted to the circuit board using 1 -inch 8 BA bolts.


Fig. 4 : The copper strips should be cut away as shown above before components are mounted on the lower circuit board.

## components list

| Resistors : |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | 82k $\Omega$ | R8 | 2.2k $\Omega$ |
| R2 | $10 \mathrm{k} \Omega$ | R9 | $13 \mathrm{k} \Omega$ |
| R3 | 4.7k $\Omega$ | R10 | $2 \cdot 2 \mathrm{k} \Omega$ |
| R4 | $4.7 \mathrm{k} \Omega$ | R11 | $100 \Omega$ |
| R5 | $4.7 \mathrm{k} \Omega$ | R12 | 39k $\Omega$ |
| R6 | 1 k / | R13 | 47 $\frac{1}{2} \mathrm{~W} 5 \%$ |
| R7 | 100k $\Omega$ |  |  |

All resistors $\frac{1}{8}$ W 5\% unless otherwise noted.
VR1, VR14 to VR25 (13 off) $5 \mathrm{k} \Omega$
VR2 to VR13 (12 off) $1 \mathrm{k} \Omega$
All subminiature vertical skeleton preset potentiameters

## Capacitors:

| C1 | $2.5 \mu \mathrm{~F} 6 \mathrm{~V}$ elec. | C5 | $0.22 \mu \mathrm{~F}$ polyester |
| :--- | :--- | :--- | :--- |
| C2 | $2.5 \mu \mathrm{~F} 6 \mathrm{~V}$ elec. | C | $0.22 \mu \mathrm{~F}$ polyester |
| C3 | $2.5 \mu \mathrm{~F} 6 \mathrm{~V}$ elec. | C 7 | $2.5 \mu \mathrm{~F} 6 \mathrm{~V}$ elec. |

## Semi-conductors:

| Tr1 | NKT212 | Tr3 | NKT214 |
| :--- | :--- | :--- | :--- |
| Tr2 | NKT214 | Tr4 | ASY26 |

## Miscellaneous:

Veroboard, $5 \times 2 \frac{1}{2} \mathrm{in}, 0.1$ in matrix, copper clad. Veroboard, $3 \frac{3}{4} \times 2 \frac{3}{4} \mathrm{in}$, 0.1 in matrix, plain board. Cir-kit strip, $\frac{1}{8} \mathrm{in}$, 5 ft . card. Small slide switch. Output transformer, ratio 9-2:1 (Radio spares T/T4) Speaker, 3 ohm. Ball point pen. 8 BA nuts and bolts.

## Components

Although it is possible to use fixed value resistors in place of VR1-VR25, the tolerances of other parts (C5 and C6 in particular) make variables more satisfactory. The required values of resistance do not equal the standard preferred values anyway, and the extra cost is minimal. Suitable variable resistors are the series PN sold by Messrs Electrovalue.


Fig. 5 : Base diagrams of transistor connections.
The capacitors may, of course, be substituted by components of higher voltage rating. C1, C2, C3 and C7 could well be from the Mullard C426 series for instance. The speaker is specified only in its impedance ( 3 ohm ), the size being unimportant. Because


Fig. 6: Stylus made from a ball-pen.
of this no details for a case are given. $0 \cdot 1$ inch Veroboard is specified for ease of assembly, as VRI-VR25 and T1 have tags at multiples of this dimension.

It will be noted from the photographs that the piece of Veroboard used for the circuit board is larger than that specified-however the size specified is sufficient to accommodate all the parts. The total cost for a complete instrument should be under $£ 5$. a single octave instrument without tremolo would come to about $£ 3.10 .0$.


Photograph of lower circuit board. Compare with Fig. 3.

## Alternative Circuits

As stated earlier, the tremolo can be omitted without affecting the rest of the circuit. The pitch of the instrument can be raised by decreasing R9 or C5 and C6. If C5 and C6 are made $0 \cdot 1 \mu \mathrm{~F}$, the instrument wilh play an octave higher than that described. The setting of VR1-VR25 will however be different, so a composite device is not really practicable. It is possible to use a higher impedance speaker (about 80 ohm) without a matching transformer. It will then be necessary to reduce, or possibly even omit R13. If required, a switch can be inserted in the negative battery lead. In use the organ will remain in tune even when the battery voltage falls from 9 volts to 6 volts, and having two octaves will play many simple tunes.


## ELECTRONIC DIGITAL COMBINATION ILCK

THE need for a money-making game, for a Scout Coffee Morning, which was a little more sophisticated than the well tried 'Screweye along the bent wire', resulted in this digitally switched combination lock.

## PRINCIPLE

The principle of operation is that a code number. 0 to 7 , is set up on a 3 pole 8 way rotary switch. The switch is connected in 1-2-4 binary form to a set of three toggle switches, each toggle switch corresponding to one pole of the rotary switch.

For the combination lock to be "opened", it is necessary to set the three toggle switches (binary $1-2-4)$ to equal the code number set up on the rotary switch. A correct setting completes the circuit through the switches thus opening the lock. A table of binary-decimal equivalents is shown in Table 1.

If the code number is unknown, the chances of setting the toggle switches to the correct number,

| $S 2$ | $S 3$ <br> $(1)$ | $S 4$ <br> $(2)$ | $S 5$ <br> $(4)$ |
| :---: | :---: | :---: | :---: |
| 0 | 0 | 0 | 0 |
| 1 | 1 | 0 | 0 |
| 2 | 0 | 1 | 0 |
| 3 | 1 | 1 | 0 |
| 4 | 0 | 0 | 1 |
| 5 | 1 | 0 | 1 |
| 6 | 0 | 1 | 1 |
| 7 | 1 | 1 | 1 |

TABLE 1
in one try, are 8:1 against. To improve these odds, for the player, it was decided to allow three attempts at any particular combination. The chances of winning are now 8:3 against, but having three attempts psychologically encourages the would-be safecracker to feel that the odds could possibly be in his favour.

Two indicator lights, red and green, are connected so as to indicate the failure or success of the attempt. However, this display on its own seemed a little tame for the effort involved and it was decided that a more dramatic 'failure" indication and an attractive reward for a successful attempt was required.

To satisfy these requirements, a mock 'safe' was built which had an electrically opening door and a suitably loud bell mounted on top. The general arrangement of the combination lock and safe can be seen in the photograph.

For the commercially minded, small chocolate bars were used as bait and we charged 3d. for three goes. About 35 s. profit was made during one Coffee Morning.


Fig. 1: Circuit of the combination lock. The bell and latch $L I$ are contained in the 'safe'.

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[^4]
## components list

## Resistors:

| R1 | $560 \Omega$ |  | R3 |
| :--- | :--- | ---: | :--- |
| R2 | $360 \Omega$ |  |  |
|  | $3.9 \mathrm{k} \Omega$ | All $\frac{1}{2} W \mathrm{~F} ~ 5 \%$ | $3.9 \Omega$ |

Semi-conductors:
Tri/2 MJE520 Motorola (L.S.T. Components)

## Switches:

S1 Single pole, push-to-make push switch
S2 3 wafers, each 1 pole 8 way, rotary
S3 Single pole, change over, togole
S4 Single pole, change over, toggle
S5 Single pole, change over, toggle
S6 Single pole, on-off toggle

## Miscellaneous:

LP1/2, Lamps 8 V 0.2 A m.e.s. RL1, Reed operating coil Type 1 with dry reed switch Type 10RSR (Radiospares). L1, Modified P.O. Type 3000 relay, 200 ohm coil. Bell, AC/DC 4.5V. Batteries, 9V PP9, 4.5V 1289 (Ever Ready).

## CIRCUIT OPERATION

The complete circuit is shown in Fig. 1. When the settings of S3, S4 and S5 are such as to equal the setting of $\mathbf{S} 2$, (correct combination), continuity exists between the rotor of S2a and the common connection of S 5 .
In this condition, the closing of S1 (push button) will cause +9 volts to be applied to the collector circuits of $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$ and to R1.

This results in Tr 1 conducting, causing the 'OPEN' lamp, LP1, to light and the latch solenoid, L1, to be energised, thus opening the safe door.

In the event of the setting of S3, S4 and S5 not equalling the setting of $\mathbf{S} 2$, (incorrect combination), there will be no continuity through the switch system.

In this condition, the closing of S1 will cause +9 volts to be applied to the collector circuits of Tr 1 and $\operatorname{Tr} 2$, as before, but $\operatorname{Tr} 1$ will now be non-conducting.

This results in TrI collector being at approximately +9 volts, LP1 remaining unlit and L1 de-energised.

The positive voltage at Tr1 end of R3 causes Tr2 to conduct, lighting the 'ALARM' lamp, LP2, energising the reed relay RL1 and thus ringing the alarm bell.

A separate 4.5 V battery, is used to drive the alarm bell, as 9 V is rather excessive for the type of bell used. Switch S6 is included in the bell circuit so that the bell may be muted if the lamp indication only is required.


Flg. 2 : Construclional detalls of the 'safe'.


The electrical latch is made from a Post Office type 3000 relay. The relay is modified by soldering a brass latch to the toe of the relay armature as shown in Fig. 3.

The relay is mounted on its side by either soldering the metal bobbin cheek to a brass backing plate or by using a suitable curved clip fitting over the relay bobbin.

The moving part of the latch is formed by a small angle bracket fixed on the side of the door.

The automatic opening mechanism is a crude but effective arrangement using two Meccano strips and a rubber band. The arrangement is shown in Fig. 3. It should be noted that the mechanism is on the underside of the top of the safe and that the drawing and photograph show how it appears when the safe is inverted.


Fig. 3: (top) Details of the latch mechanism and relay modification. (below) photograph of completed control unit.

## OPERATION

1. Set Combination Switch $\mathbf{S} 2$ to any position.
2. Set bell switch S 6 to 'ON' if bell is required.
3. Contestant sets S3, S4 and S5 to his choice.
4. Contestant presses S1, (OPEN or ALARM operates).
Note: S2 must be changed to a new combination after each attempt or set of attempts, to obtain the desired odds.

## COMMENTS

Although the Electronic Digital Combination Lock is used as a game, an extension of the number of digits could form the basis of a commercial combination lock having an easy and rapid change of combination.


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## READERS RADIO

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IN the past it has always been thought that the summer months were a time when most enthusiasts had very little time for listening on the bands. The amount of mail that I have received in the last few months has convinced me that this is not so. I sincerely hope that this trend will continue and reports will continue to pour in.

Because of the large number of reports that I now receive every month I have been forced to be more selective in choosing the material that I use. In the future I would be obliged if all reports gave accurate details of the station heard, such as frequency, time and programme details. Reports which conform to this requirement will stand a much better chance of being published.
When I started writing this column a year ago I said that it would be my policy to try and include as much material as possible from the more exotic stations. This is still my policy and with the large number of reports coming in I can select these more interesting stations. I will, however, continue to mention the more common stations, as I have found that among the beginners to the hobby who read this page there is a real demand for these easier stations.

## Members Logging and News

Des Walsh of Little Baddow feels that all civilised countries should operate a short-wave service. He is particularly interested in the fact that the Republic of Ireland has no such service. He has tried to get them to start such a service but with no success. He would like all readers who are interested in this problem to write to Radio Telefis Eireann to ask them to start a short-wave service.

Malcolm Cheeseman of Llanberis in Caernarvonshire is using a 20 -year-old Pye domestic receiver and a 24 foot vertical aerial and he logged the following stations:

7065 Radio Tirana, Albania at 1840
9625 Radio Israel at 2045 GMT.
11672 Radio Pakistan at 2005
11815 Trans World Radio, Bonaire at 0035
15160 Radio Ankara, Turkey at 2205
15345 Radio Kuwait at 1645
17890 HCJB, Ecuador at 2330
J. Trewick of London Colney has heard some very interesting stations in the last month:

11955 BBC Far Eastern Relay station with ident. at 1658 and at close down at 1815
15165 Radio Damascus, Syria at 1930 in English
15240 ABC Australia with news in Eng. at 2145
15320 ABC Australia at 2155.
R. F. Bruce of Angus in Scotland has an Eddystone 940 receiver and an indoor Joystick which

# THE BROADCAST BANDS 

Frequencies in kkz • Times in GMT
enabled him to hear:
5050 Radio Tanzania until sign-off at 2000
11735 Radio Morocco, English news at 1715
11955 BBC Far East Relay, ident. at 1815
15020 The Voice of Vietnam in English at 2000
15165 Radio Damascus, Syria, English news at 1930
21690 WIBS, Grenada heard at 2100.
Stephen Wainwright of St. Helens has again used his Skyrover Mark II receiver and 100 foot longwire to good effect:

9625 Radio Trans Europe with test transmissions for the U.K. from 1345 to 1415.
15345 Radio Kuwait in English with news at 1830
Stephen also reports that HCJB are issuing QSL cards without requiring the information stated in this column in the June issue.

Roy Patrick of Derby sent in the following interesting information:
South Africa: Radio RSA broadcasts to the U.K. at 1800-1850 on 21480 and 15250, the former frequency gives the better reception.
Kenya The Voice of Kenya on 4915 is audible with a fairly good signal with a programme in Swahili at 1900 .

Terry Gibbs of Swindon heard the following stations:

11800 Italian Broadcasting at 1930 to 2000
17860 ABC Australia at 2130 to 2230
21495 Radio Portugal at 2030 to 2100.
Regular reporter Geoffrey Gilham of London S.E. 12 has been on holiday but still managed to send in the following log:

4865 Azores with talk in Portuguese at 2157
4870 Dahomey, vernaculars and music at 2137
4915 Ghana, talk in English at 2156
4940 Kiev, classical music at 1935
5058 Tirana, classical music at 2145.
Mervyn Winters of Co. Antrim used his AR88 and 12 foot whip aerial to hear:

9009 Israel heard at 2115
9560 Amman, Jordan, heard at 1600
11960 All India Radio, Delhi at 2015
15265 Radio Afghanistan at 1800
17855 NHK, Japan heard at 0700.
With apologies to all those reporters whose contributions I have not used I will end with a log from Glen Morgan of Tredegar:

## 3204 Ibadan in English at 2205

3380 Malawi, dance band music at 2025
4774 Libreville, African music at 2205
6540 Pyongyang in English at 1935.
Please note that by the time this article is published I will have changed my address and all reports should be sent to me at 5 Ranelagh Gardens, Cranbrook, Ilford, Essex, by the 17th of the month.



T just isn＇t fair．Every month the contest types come last，so，just to show there＇s no hidden meaning in it，let＇s start off by seeing what＇s happening contest－wise．September 12－13th，WAE DX phone contest；13th， 3.5 MHz field day（go on， have a listen all you h．f．types）；October 3－4th，u．h．f．／ s．h．f．contest．The 10 metre phone contest on October $10-11$ th，should prove an interesting one， while for those not too far from London there is a lecture at the Institution of Electrical Engineers on the Trans－Arctic Expedition．You get a cup of tea，too！

P．Newman（Bucks．）reckons we ought to have a page of logs from home－brew equipment only Start dusting the cobwebs off that old t．r．f．you built and get listening！I agree that there is a greater sense of achievement in bagging some good DX on a homebrew．（You wait until my 600 transistor receiver is finished－Cor，think of the gain．）
M．Bernstein（Lancs．）finds that the mornings are the best time for a listen on 14 MHz ．S．Ireland， down in Kent，is giving serious thought to building a 144 MHz converter＂to give Glyn Richards some competition．＂Steve also claims that the 5B4NZ heard on topband（Amateur Bands，August issue） was flying the Jolly Roger because the only recent licence in that area was 5B4ES．（Well shiver me dipoles．）
In spite of a patchy period，Steve Ireland（Kent）， HRO MX， 67 ft ．end fed，bagged these on $3 \cdot 5 \mathrm{MHz}$ ： CR6IV，CT1MC，CT2AK，OJDDX（Market Reef）， PY3BAD，PY5XQ，PY7AF，UW9AF，VE 0 NEF／G5， VP8FL，VP8KF，ZB2BY，ZS5XA，6W8DY，9V1PP． Tuning h．f．，a listen on 21 MHz brought sigs from： AX9AC，AX9SS，AX9XI（Christmas Island）， CR6CA，CT2AK，CX5BV，EA8BQ，EP2SW， FHØVP，HM5PF，HS1ACW，IS1DFO，KG6AAY， KL7FBK，KP4CH，KR6HB，KR8BY，KV4FZ， KX6HW（Marshall Island），KZ5AM，LU2DAW， LX1SD，MP4BFO，MP4MBB，OA8V，OD5BA， OX3LP，OJ $\emptyset \mathrm{DX}$, PJ9JR，PZ5RK，TA1TR，TU2CW， VP2VI，VP5HZ，VS6DO，ZB2BY，ZC4CB，ZE5JU， ZS6DH，3V8AL，5A5TH，5B4ES，5H3JL，5N2AAE， 5V4JS，5Z4MO，6W8AL，7Q7BC，8P6BQ，9F3USA， 9G1GD．Perhaps I didn＇t connect that antenna after all．

N．Sanderson（Edinburgh），CR45，200ft．long wire went s．s．b．spotting on 14 MHz ．Stations observed： AP5HQ，AX2ARZ，AX3XI，AX4HA，AX7GK， AXøLD，CE3BE，CR6MT，CR7GJ，CT3SC， DUIFH，EA8FS，ET3DS，GB3GWC，GC3VJX／ OH5，HC2SO，HK3BCA，HR2HHP，JA1OWT， K5ARJ，K6ZDP，K7TGF，KA1KSO，KH6OR， KL7EBK，KP4DHV，LU2HC，LX1RC，OJゆDX， OX5BL，PJ9HH，PY7ACQ，PZ1BW，SU1MA， TA2AE，VE2BEO，VOICA，VP7NA，VR6TC， W6TSQ，W7IM，XE1YM，YA1EXZ，YB2AO， YK1AA，ZD8DB，ZE1DG，ZF1GC，ZL4CX， ZS20F，ZS6IK，4U1ITU，4X4QA，5Z4UK，7Q7JO， 7X2SMA，9M2PR，9Q5MP，9U5DP，9Y4US．

R．Dinning（Ayrshire），HA350，PR3OX，RQ1O，

# THE AMATEUR BANDS David Gilson，G3JOG 

## Frequencies in kllz－Times in GMI

380 ft ．wire at 50 ft ．，has spent a ten－week spell in hospital．It doesn＇t seem to have affected his skill with a receiver as his $21 \mathrm{MHz} \log$ shows：CR7GJ， EL1CA，EL2DU，EP2SW，HR1SR／P／HR2， HS1ACW，LR $\phi \mathrm{IJ}, \mathrm{KR} 6 \mathrm{~KB}, \mathrm{KS} 6 \mathrm{DH}, \mathrm{OH} \phi \mathrm{NJ}$ ， OJゆDX，TU2CS，VU2IXP，W5YSL／P／DU1， XW8DM，XW8DS，YBфBD，ZD9BM，3V8AL， 4U1ITU， 5 A5TH， $5 \mathrm{H} 3 \mathrm{JR}, 5 \mathrm{~N} 2 \mathrm{ABG}$ ， $5 Z 4 \mathrm{GK}$ ， 6W8GE，6Y5GB，7P8AB，9F3USA，9L1GQ，9M2VI， 9Q5WF，9V1PP，9X5AA．

A．Crooks（Leicester），RA1，PR30， 45 ft ．end fed， heard CR6IE，on 14 MHz ，CR6MX and 9G1GT on 28 MHz while 21 MHz s．s．b．brought：EL2L，HBゆLL， PY2HY，PY7GAH，VU2KV，ZD8JK，ZS6AD， 4Z4BG，5N2AAE，5U4JS，9J2PV，9U5DP．

J．Moore（Leicester）claims that topband，eighty and forty were a dead loss this month and bemoans time－base QRM on 160 from local tele＇s．I reckon that＇s the transmission of spurious signals，report them to the GPO！

John＇s bets on 14 MHz s．s．b．were：CR6EV， OX5AP，PY2ELT，UL7JG，VR6TC，ZP5CF．Fifteen metres produced：CE3OE，CR6LG，JAITRL， VE3GJU，4Z4DX，8P6BQ．The gear is a CR100／2， a．t．u．and 130 ft ．end fed．Putting a home－brew f．e．t． converter in front and tuning $24 \cdot 9-26 \cdot 9 \mathrm{MHz}$ gave a．m．－type squeaks on 144MHz from：G2JF，G2BKC， G3DAH，G3TDR，G3TXB，G3VCV，G3WRD， G8VZ，G8CKT／P（Surrey），G8AXZ，G8BJK， G8BPO，G8BYB，G8CIW，G8CQX，G8CRN， G8CUW，G8DAS，GC2FZC．The same band but s．s．b．raised：G2CIW，G3LQR，G3SOA，G6UW， PA ${ }^{\circ} \mathrm{CML}$（near The Hague）．
A Garex converter feeding a PR30 and CR7OA from an 8－element Yagi is located at Wendover and the controls titivated by N．Richardson．A peep at 144 MHz revealed the following stations：G3AOS／P， G3LHO，G3LXP／P，G3PNA，G3PRM／P，G3TQF／P， G3UES／P，G3VPE／P，G6GN，G8BCQA，G8BDJ／P， G8CGX／P，GW3ITZ，GW3UCB，GW8ACG／P， GW8BEB／P，GW8BHY／P．

V．Koopman（Lancs．but on holiday at Windsor）， RA1，Joystick at 15 ft ．，had some success on 7 MHz （more success than I did I might warble）．Dragged from the dreaded forty（still screaming）were： AX9XI，CR9AK，FP8CS，HS1ABO，JW8MI， KJ6CF，SV $\phi$ WO，UK3ABA，VQ8CZ，VR6TC（Pit－ cairn Island，VS6DO，W2HCW，YA1SG，7P8AB， 9N1MM－all on c．w．（splendid，splendid）except W， 7 P 8 and 9N1．

The same gear on 21 MHz raised：CE6DP， FO8BW，GM3MNM／MM near Capetown，IR $\phi$ XPS， JX8IL（Jan Meyen Island），KM6DQ，LU3AQ， TR8DG，VR2EK（Fiji），VR4EE，VU2BEO，ZD9BN， 9G1GD－all s．s．b．

Please note that the deadline for the month＇s logs is the 15 th of each month，that is，they should reach me by the 15 th．If they arrive later，they，are too late for the current issue and＂out of date＂for the following one．So please slaves，letters to 5 Edward Close，St．Albans，Herts．，before the 15th－Ta！

## THE <br> MW <br> COLUMN



AS the evenings start to draw in, medium wave stations in North America can be logged as early as midnight. Among the first to be heard are an interesting group in Newfoundland right at the low frequency end of the band. There are three networks. The Canadian Broadcasting Corporation (CBC) operates CBT 540 kHz in Grand Falls and CBN 640 St John's with satellites CBNA 600 St Anthony and CBNM 740 Marystown. There are two commercial networks. The Colonial Broadcasting System has key station VOCM 590 in St John's plus CHCM 560 Marystown and CKCM 620 Grand Falls. The Newfoundland Broadcasting Company can be heard on CJCN 680 Grand Falls, CJOX 710 Grand Bank and CJON 930 St John's. All these stations are logged regularly in the UK. Others from the same area include CFCY 630 Charlottetown Prince Edward Island; OFDR 790 Dartmouth Nova Scotia; CJCH 920 Halifax N.S; CHER 950 Sydney N.S; CHNS 960 Halifax; CKBW 1000 Bridgewater N.S; CBA 1070 Moncton New Brunswick; CBD 1110 Saint John N.B; CKCW 1220 Moncton; CKEC 1320 New Glasgow N.S; CKBC 1360 Bathurst N.B. Newfoundland Standard Time is $3 \frac{1}{2}$ hours behind G.M.T. the odd half hour being a help to station identification. The remaining Mari-
time Provinces are on Atlantic Standard Time which is 4 hours back. An unusual catch from this area which counts as a separate DX country, is Radio St Pierre 1375 kHz in the French islands of St Pierre et Miquelon which lie to the south of Newfoundland. This station can often be heard when Lille 1376 kHz signs off for the night at 2300 hrs G.M.T. The programmes from Radio St Pierre are in French and local time is 3 hours behind G.M.T.

Chris Stacey of Tunbridge Wells asks what sort of aerial is suitable for DXing on the Long Waves. At this QTH there is a 90 ft long-wire at about 20 ft above ground level and it performs very well when used with a CR100. Although a long outdoor aerial is an advantage on this band it is not essential. Dick Clark, a lw DXer in Florida USA has converted a standard m.w. loop for long wave use by increasing the number of turns from 7 to 20 and he regularly logs Europeans with it. Buzz from TV receivers may be troublesome with indoor aerials in some QTHs though this will disappear around midnight when the TV closes down. The long waves extend from 151 kHz to 433 kHz though only the section below 272 kHz is in general use in Europe. There are some 50 Asiatics on this band situated in China, Mongolia, Turkey and asiatic USSR, and many can be logged in this country. Look for Ulan Bator 209 kHz Mongolia; Tselinograd 227 Khazakistan; Dushanbe 254 Tadjakistan; Harbin 272 China; Ashkhabad 375 Turmenistan. Among semi-DX there is Tiflis 191 Georgia; Azilal 209 Morocco; Orenburg 300 USSR; Oulu 433 Finland.

Charles Molloy



THE first type of spark transmitting equipment used a simple aerial circuit which included the spark gap. The best type of radiator was found to be an elevated aerial but the spark gap in series with it provided a high resistance and naturally a damping action. Therefore, the discharge began at a high initial voltage which soon died away to zero. After some time, another spark discharge would take place but in the meantime, there was no radiation from the aerial.
In the circuitry employing aerial coupling, the spark gap was included in a primary circuit; a separate tuned aerial circuit forming the secondary circuit. This latter was low resistance so that any oscillations induced could persist for a relatively long time before they finally died out. Thus for equivalent radiation compared with the plain aerial, the initial voltage would be lower, causing less strain on insulation but the increased radiation performance demanded less initial power. An added advantage was that the radiation covered a narrower waveband.

Marconi's first tuned transmitter (see photograph) was built in the year 1899. It comprised an oscillation transformer in the primary of which was a spark gap and capacitor. The secondary was connected to an adjustable inductor in the aerial circuit.

The Marconi patent No. 7777 of the year 1900
was based on this design. It covered the later forms of tuned apparatus without which the famous "Atlantic transmission" of 1901 would have been impossible. This patent clearly specifies the tuning of four circuits, i.e. spark gap circuit, transmitter aerial and primary and secondary of the receiving transformer.


Spark gap used by Marconi in his early experiments in the year 1895. Lent to the Science Museum, London, by Marconi Wireless Telegraph Co. Ltd.


## Khadiograms 1922

"A wireless penny-in-the-slot machine has been invented in America. The invention consists of an automatic apparatus surmounted by a revolving loop aerial, and takes its power from the lighting circuit supply. When the coin is inserted in the slot two valves are switched on, and the music is heard through a large horn at the bottom of the instrument." .
"A racehorse in America has been equipped with a receiver and trained to race by commands from the trainer.".
"Suggestions are made in the non-technical Press that by means of piezo-electric crystals London could be lighted by means of its noise. Piezo-electricity is the property possessed by certain crystals whereby they generate electricity when subjected to vibration."
"Experiments in the flying of a pilotless wirelesscontrolled aeroplane will shortly take place in France."
"There are now 350 broadcasting stations in the United States."
"Experiments to determine the feasibility of reception of wireless signals by the sense of taste have recently been carried out. Silver electrodes were used, one of which made contact with the inner part of the upper lip of the operator and the other with the tip of his tonguc. Using four-stage amplification, it was found possible to detect signals and to tune in a station by noting when the intensity of the taste sensation was maximum. For messages to be read, the speed must not be greater than ten words a minute."
"A wireless receiving set has been installed in Buckingham Palace.".
"Among the many thousands of people who listenedin to the Prince of Wales's broadcast speech to the Boy Scouts of the nation were the blind soldiers of St. Dunstans. Captain Ian Fraser, the blind chairman of St. Dunstans, has been an ardent wireless experimenter for two years past, and in the course of a short address following the transmission, he stated that wireless telephony was opening a new world for the blind. A blind man's hobbies were limited, but wireless was one of those which he could pursue just as well as anyone else. In listeningin, he was at no disadvantage to those who could see."
"Direct wireless communication between France and New York was established the week before last from the great wireless station at Saint-Assise."
August 19, 1922.
"It is rumoured that some enterprising firm has brought out a clothes line which has a stranded copper centre for use in cases where landlords object to aerials."
"Is the doom of the gramophone in sight? A firm is now advertising: 'Why not have your gramophone converted into a high-grade wireless receiving set?'. . ."

## A Kirader Eomments

During my early youth I had access to current numbers of the old "Model Engineer" andl was fired by the rather brief articles on radio then in its infancy; I was born in 1893. V. W. Delves Broughton had described his own installation which featured all the primitive means available at the time, and when I began work on the railway in 1909 most of my spare time was occupied with my own version of the bits and pieces, improvised from materials to hand; I had not then seen any "real" radio apparatus.

In 1910 I joined the Cadet Unit of the K.R.R's, and was soon learning Army Signalling; by extraordinary good fortune I was picked in 1913; to attend a Radio Course at Marconi House (evenings) and so became acquainted with the real thing. I saw the Fleming valve, its De Forest improvement, and listened on the Marconi Multiple Tuner and Magnetic Detector, which I soon duplicated in my own way at home. The big rotary generators and 10in. spark coils were rather out of my sphere, and the noise and space required were all too obvious. I do wonder if P.W. can come across any others who attended these Cadet Courses?

1914 found me in uniform seriously, putting my earlier signal training to practical use. As Signal Sergeant of my unit we dabbled on the fringe of radio but few infantry units had the opportunity to use it in action. I heard my first Radio speech when visiting Div. H.Q. just after the Armistice.

I obtained my, first Radio Receiving licence in November 1919 in the form of a letter from the G.P.O., and have been a listener ever since.

In North London we formed the North Middlesex Radio Club, which had as the "motto" on the badge: "Listen before sending and so avoid jamming" and our Secretary, Mr. Savage of Winchmore Hill, was a fine enthusiastic character who did great work for us. I moved away to Stevenage in 1922 and found only one radio aerial in the locality, at the hamlet of Todds Green. My own soon went up-I had sold my 30 foot London mast to Arthur Burrows who later became a notable figure in Radio on the organising side; he was the Secretary of the International Organisation.

I had bought No. 1 of The Wireless World, and in due course followed with No. 1 of Practical Wireless and every other radio paper which appeared and disappeared; I am still faithful to $P W$ which has given me much food for thought and had set a fine pattern, if not always "snooty" enough for some.

I am now approaching my 77th birthday, and still dabble, listening over most of the bands, broadcast and otherwise. I was able to do a bit in the Home Guard, and shared the consternation when on official orders we were not able to try out the C. 52 sets issued and withdrawn almost at once. Of course I still read Morse, am a sort of unofficial honorary member of the Stevenage Radio Society, who keep the flag flying in this part of the country. But you can imagine I look back and think how very fortunate I was to get that Course of Instruction during 1913/14 at Marconi House when things were still in their infancy.
B. G. ASHMAN, (Stevenage, Herts.).


Number 12 Motorola MFC 4010P/Mullard TAA263 Utility Amplifier

WHEN two separate manufacturers in two continents introduce very similar products within a short time, clearly a definite demand has been identified; and even a cursory examination of the circuit diagrams will establish the basic identity of the Motorola MFC4010P (and the Mullard TAA263) mentioned last month.

## Application

The application is also clear, as a small signal utility amplifier or "gain block" for industrial or consumer electronic systems. This function is frequently required, so that an integrated unit which eliminates the chore of designing and assembling discrete transistor units will be very welcome.


Fig 1 : (a) Circuit of MFC4010P and (b) of the TAA263.

## Performance

The performance of the units extends from d.c. to greater than 1 MHz , a limit which is established by the stray capacitances in the circuit, which degrade gain and introduce phase shifts. However, this still permits the circuit to be described as a wide band unit, i.e., not limited to industrial applications in servomechanisms handling switching or d.c. levels, or to consumer applications in the audio field. It can function, for example, as a fairly effective video amplifier, and indeed, with suitable tuned circuits as an a.m. i.f. amplifier or even as a t.r.f. radio receiver.

One objection may be raised to the circuits as illustrated, Fig. 1. It may be claimed that the baseemitter junction of $\operatorname{Tr} 2$ effectively short-circuits the collector of Tr 1 , and similarly with Tr 3 shunting the output of Tr 2 . However, it should be remembered that the integrated circuit manufacturing process pre-supposes the use of silicon, and whereas in germanium transistors the 0.2 volts, typical of a baseemitter junction, would indeed bottom the proceeding stage, in silicon this junction establishes a potential of approximately 0.7 volts while the bottoming collector voltage is lower. The designers are quick to exploit this feature of the physics of silicon.

On this point of ubiquity, in the July 1970 Practical Wireless, page 195, C. F. Fletcher describes a hybrid transmitter modulator incorporating a "ring of three" direct coupled audio gain stage identical to the integrated units we deal with this month; the same issue features a reverberation unit with an acoustic delay system requiring small amplifiers in conjunction with the input and output transducers; finally there is an account of a light-operated switch indicating the application of a d.c. amplifier, a function for which this month's circuits are ideal. No doubt other issues of this magazine would contain a similar series of projects in which a small signal gain function is required.


Fig. 2 : (a) Connections of MFC4010P and (b) of TAA263.

In a practical application of a "ring of three" direct-coupled transistor amplifier subsystem, the operating conditions are set and stabilised by d.c. feedback, i.e. the base bias of Tr 1 is drawn through a suitable resistor network from the output of the block.

Open loop voltage gain for both units is some 70 dB ; it is usual to incorporate in the d.c. feedback loop some reactive elements (inductors or capacitors) to determine the amplifier passband and the actual gain realised.

(a) A.F. Low level amp.

(b) Tuned amplifier (R.F. or I.F.)

Fig. 3 : (a) Circuit as A.F. amplifier.
(b) Circuit as R.F. or I.F. amplifier.

The cost of fabrication of a simple i.c. chip is only slightly greater than that of a good discrete transistor, and the yield, or fraction of satisfactory devices, is not much lower. Packaging is a different matter, though, since the typical i.c. requires more manual attention at this stage. Hence the advantage of this month's i.c.'s, in that both are supplied in simplified four terminal packages, requiring only signal input and output, and power leads.

Connection identification is possible by reference to Fig. 2, and the test circuits, Fig. 3, indicate the approach to the incorporation of one of these units in an actual project.
Constructors may obtain the Mullard units from advertisers in this magazine, while the Motorola i.c. is in stock at the U.K. distributors: Celdis Ltd., 43-45 Milford Road, Reading, Berks.; or Semicomps Ltd., 5 Industrial Estate, Beresford Avenue, Wembley, Middx.

## RULES.

1. Articles submitted for the competition should conform to the general style of material published in Practical Wireless and must describe the operation and construction of a piece of radio, audio or test equipment that has been designed and built by the author.
2. Articles should, preferably, be typed using double spacing, leaving wide margins, and on one side only of each sheet. Circuit diagrams and any other drawings should be on separate sheets and numbered to agree with the text. Author's roughs must be clear enough to permit re-drawing. Component lists must also be separate and laid out to the standard PW format.
3. Photographs of the equipment are desirable and should be in black and white, sharp and clear. Each photograph should be identified by sticking a piece of paper on the back rather than by writing on the photograph itself.
4. Components used in the design must be readlly available from retail sources.
5. An entry form, properly completed, must accompany each article submitted. There is no limit to the number of articles submitted by any one author.
6. Articles must reach the Editor, Practical Wireless, Old Fleetway House, Farringdon Street, London, E.C.4. by the first post on Monday, November 2nd 1970 with the envelope and title sheet clearly marked "Project Autumn". A stamped, self-addressed envelope must accompany each entry.
7. All entries submitted will be considered by a panel of judges and the Editor's decision on all matters arising will be final. The Editor will require authors of winning entries to submit the equipment to him immediately on request for final assessment by the panel.
8. Employees and staff of Practical Wireless are not eligible for entry to this competition.
9. The winner of the competition will receive and retain outright the Practical Wireless "Designer's Trophy 1970". Other prizes will be awarded to the best run-ners-up. Any article published will be paid for at normal rates.

ENTRY FORM
PAGE 437

## TRANSISTDR



THIS article describes a relatively simple transistor v.f.o. unit, suitable for use with most amațeur transmitters. Its basic merits are an extremely stable, low drift characteristic for large changes in temperature, supply volts, and over long periods of time and almost constant amplitude output over the frequency range together with a cheap and simple construction.

## Speciflcation

The v.f.o., whose complete specification is given in Table 1, was given most stringent tests, particularly with regard to frequency drift and stability, all frequency measurements being made on a digital frequency meter with a discrimination of $\pm 1 \mathrm{~Hz}$. The results of these tests are shown graphically in Table 2. From these curves it can be seen that even under extreme changes in parameters, the frequency drift was always well under 100 Hz or better than $0.003 \%$. As the tuning capacitor represents only a small part of the total capacitance, the oscillator only covers the required frequency range, that is 3.5 to 3.8 MHz . This means a large open scale and

almost linear divisions in calibration. With a scale radius of $2{ }_{4}^{4} \mathrm{in}$. (scale length of about 7 in .) each 10 kHz occupies approximately 4 in . Amplitude stability is maintained by an effective control circuit which does not employ a thermister with its attendant time lag. Supply is 24 V d.c., though this is not at all critical, while the current drain is less than 50 mA .

The complete unit is housed in an $\sin \times 6$ in $\times 6$ in case, co-axial output being taken from the rear. The output impedance is extremely low, thus allowing the unit to drive transmitters having a wide range of input impedance.

## The Circuit

The complete circuit diagram, together with component list is given in Fig. 1. Basically the circuit comprises a modified Butler oscillator with emitter follower output. $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$ form the oscillator circuit with $\operatorname{Tr} 3$ as an emitter follower output. L1, VC1, VC2 and C1 determine the frequency of oscillation, the output from Tr 2 being d.c. coupled to Tr3. This stage provides isolation between the oscil-


## SPECIFICATION

| Frequency Range | 3.5 MHz to 3.8 MHz fundamental (approx.) |
| :---: | :---: |
| Frequency 8tablity | After 10 mins warmup Temperature $15^{\circ} \mathrm{C}$ to $80^{\circ} \mathrm{C}$ : less than 100 Hz or $0003 \%$ Supply volts 15 V to 30 V : less than 30 Hz or $0.0009 \%$ Over a six hour period: less than 10 Hz or $0.0003 \%$ |
| Output | Minimum 5V peak to peak. Amplitude stabllity over frequency range better than 1dB. Output Impedance less than $200 \Omega$ |
| Supply | Nominal 24V d.c. Current draln less than 50 mA |
| Dimensions | $8 \mathrm{in} \times \mathrm{x}$ in. $\times 6 \mathrm{in}$. |

lator and feedback amplifier Trl. The output developed across emitter load R8 is applied via the feedback components C4 and R5 to the base of Tr1. The output from this transistor is d.c. coupled back to the base of Tr2. Negative feedback is applied to Tr 1 via $\mathbf{R 2}$ which, in conjunction with R1, determines the effective level of oscillator feedback.

The output stage, $\operatorname{Tr} 4$, is also an emitter follower, d.c. coupled from the emitter of Tr3. This stage ensures isolation between the output and oscillator circuit and also provides a low output impedance, C6 providing d.c. blocking to the output terminal. Two levels of supply line are used, 24 V and 12 V , the 12 V being obtained via R10 and ZD2. The output emitter followers are supplied from the higher voltage line, thus ensuring adequate signal swing without clipping and allowing d.c. coupling to be easily achieved.
The amplitude stabilization circuit is formed by components ZD1, D1 and D2. The oscillator output is coupled via blocking capacitor C2 to the diodes D1 and D2. The voltage across the zener diode ZD 1 is maintained via the resistor dividers R4 and R6, these being connected across the main d.c. supply. The rectified signal output from diodes D1 and D2 is therefore constantly compared against the fixed zener voltage. Changes in oscillator level are converted to d.c. and simply registering as variations in zener current, the voltage across which is always constant and therefore provides a constant reference for the signal source. Decoupling of the supply lines is provided by C5 and C7.

## Construction

The construction of the v.f.o. is quite straightforward and can best be followed from the photographs shown. All components except the tuning and trimming capacitors, coil and C5, are mounted on a piece of Veroboard $4 \mathrm{in} . \times 3 \mathrm{in}$. The complete Veroboard layout is shown in Fig. 2. This is completed first and then fixed vertically on the chassis by means of a small aluminium bracket.

The chassis is simply an aluminium plate with a small right-angle lip bent along the front edge for fixing to the front panel. Side brackets, with lips bent in for fixing the front panel to chassis are

D.C. supply voltage


Table 1 (fop): glves the spec/fication of the v.f.o. while the graphs in Table 2 demonstrate the stabllity of the unit with regard to temperature supply voltage and time.

Looking at copper side of board, matrix. 0.15
also used as mechanical rigidity is of major importance for optimum frequency stability. Layout is clearly indicated in the photographs.

Also mounted on the chassis are the tuning capacitor, trimming capacitor and coil. The wiring between these components and the Veroboard is all of 18 s.w.g. tinned copper and should be as short and direct as possible, mechanical rigidity again being of first importance. The output co-axial socket is mounted on a small bracket on the rear of the chassis and close to the Veroboard, thus ensuring

## $\star$ components list

## Resistors:

| R1 | $5 \cdot 6 \mathrm{k} \Omega$ | R6 |
| :--- | :--- | :--- |
| R2 | $15 \mathrm{k} \Omega$ | $\mathrm{k} \Omega$ |
| R3 | $10 \mathrm{k} \Omega$ | R7 $1 \mathrm{k} \Omega$ |
| R4 $1 \mathrm{k} \Omega$ | R8 $1 \mathrm{k} \Omega$ |  |
| R5 | $22 \mathrm{k} \Omega$ | R9 $1 \mathrm{k} \Omega$ |
| All resistors | $\frac{1}{2}$ watt, | R10 $560 \Omega 1$ watt $10 \%$ |

## Capacitors:

VC1 25 pF air-spaced variable, ceramic mounting (Jackson Code JB/804/3-3/25)
VC2 100 pF ceramic trimmer
C1 $\quad \mathbf{5 0 p F}$ silver mica
C2 $\quad 0.01 \mu \mathrm{~F}$ polyester
C3 200 pF silver mica
C4 $0.01 \mu \mathrm{~F}$ polyester
C5 $\quad 0.1 \mu \mathrm{~F}$ polyester
C6 $\quad 0.01 \mu \mathrm{~F}$ polyester
$\mathrm{C} 7 \quad 0.1 \mu \mathrm{~F}$ polyester

## Semiconductors:

Tr1 BC107 ZD1 3.3V zener, BZY88-C3V3 Mullard
Tr2 BC107 ZD2 12V zener, BZX61-C12 Mullard
Tr3 BC107 D1 OA85 Mullard
Tr4 BC107 D2 OA85 Mullard
Coil:
25 turns, close wound on $1 \frac{1}{2} \mathrm{in}$. diameter former, 18 s.w.g. enamelled copper wire

## Miscellaneous:

Veroboard, 0.15in. matrix, $22 \times 16$ holes; Transistor heat sinks; Co-ax. socket; Two-way tag strip; Slow motion drive assembly; Chassis 8in. x 6in. x 6 in . from H. L. Smith \& Co, type W.

Fig. 2: (left) The component layout on Veroboard.
(Below) The layout of the v.f.o. can be clearly seen from this photograph and the heading illustration.
short output leads. On the outer side of the Veroboard is the two-way tag strip for the incoming d.c. supply, C5 is connected across these tags, thus decoupling the main supply at its entry point. The negative side of the supply is taken to chassis via the common fixing contact on the tag strip.

The front panel should be drilled to take the particular type of slow motion drive and dial assembly before being fixed to the chassis and side brackets. The tuning capacitor VCl is mounted on a bracket of suitable height so as to engage with the slow motion drive shaft. This capacitor should be of the ceramic mounting type as with this circuit both sets of vanes must be isolated from chassis.

Holes should be drilled in the rear of the cabinet to allow for the entry of the co-axial plug and supply leads, these being taken through a grommet. While the size of the cabinet used by the writer is specified, being readily available, any similar type of case or cabinet which is already to hand may be used.

## Calibration

The ideal instrument for calibrating the v.f.o. is of course a digital frequency meter. As such instruments are seldom available to the average amateur, -continued on page 477

## A. LESTER-RANDS

THE main note generator is a simple multivibrator, Trl and Tr 2 , Fig. 11, with the base of Tr 2 taken to the negative rail via the tuning pre-set potentiometers PRI to PR13 and VR1/R17 and R18. The pre-sets, PRI to PR13, are used to tune the multi-vibrator to cover one complete octave in tempered scale from C ( 65 Hz approx) to $\mathrm{C}(130 \mathrm{~Hz}$ approx).
The potentiometer VRI will shift the overall pitch up or down by a full interval (one whole note) so that the unit can be tuned instantly to instruments not tuned exactly to concert pitch. The output from the multi-vibrator provides the fundamental notes for the 8 ft . pitch and is taken directly to the tone forming network C23, L1 and C24 which provides the 'flute' voicing. The capacitors C25 and C26, together with the resistors R40 and R43 provide the 'clarinet' voicing.
The output from the multi-vibrator simultaneously drives the divider circuit Tr3 and Tr4 which provides the fundamental notes for the 16 ft . pitch. The output from the divider is taken via the flute voicing
network R14, C10, R15 and C11 and then via S1 and R16 to the buffer amplifier Tr 9 . The voiced outputs from the 8 ft . pitch voicing network are switched via S 3 and R 45 to Tr 9 base. The switches S 1 and S 3 allow a choice of 8 ft . flute (or clarinet with S4 closed) or 16 ft . flute (or clarinet with S 4 ) or both i.e., the 8 and 16 ft . pitches combined.

The signal output from the buffer amplifier is approximately IV r.m.s. with the output gain control VR2 at maximum.

## Drum Brush Circuit

The drum brush sound is generated when any pedal is depressed either momentarily or continuously. The brush sound begins with a medium degree of attack and decays away in approximately I second depending on the setting of the pre-set potentiometer PR 14. A four notes per bar pedal bass will therefore produce a four beats per bar brush rhythm. The brush rhythm can be switched on or off as desired.


Fig. 11 : Complete circuit of the Organ Pedal Bass Unit.

The circuit for the drum brush sound consists of a noise generator (D1, Tr5, Tr6, Tr7) and the attack/decay control circuit (Tr8). The choice of a diode for Dl may require some trial and error as a 'noisy' diode is required i.e., one that generates most noise when current is passed through it.

There should be at least 500 mV of white noise from the collector of Tr 7 (junction C17 and C20) with Tr6 conducting i.e., with PR14 at maximum resistance. An oscilloscope should display a typical spiky noise signal of about IV peak to peak.
The function of the attack/delay control is as follows:- With PR14 set to maximum resistance constant noise should appear at the output of the unit. Adjust PR14 until Tr6 is just cut off in which case the continuous noise signal will cease. The function of Tr 8 is to provide a positive pulse to the emitter of Tr6 when any of the contacts 1 to 13 (drum brush contacts in Fig. 10 Part 1) are opened.

The control transistor Tr8 is normally cut off but conducts rapidly when any of the contacts 1 to 13 are opened. The result is a fairly large pulse at the collector of Tr8 which is rectified by the diode D2 and charges C16. The charge on C16 allows Tr6 to conduct instantly, thus initiating the 'attack' but the charge then dies away slowly via R28 and R25 thus providing the 'decay' of the brush noise. The decay time will be about 1 second with PR14 adjusted so that Tr6 is only just cut off. Decreasing PR14 resistance so that Tr6 is beyond cut off will produce a much shorter decay time to the brush sound.


The total current consumption of the whole unit with any pedal depressed and the drum brush circuit switched on should not exceed 25 mA . It is therefore quite economical to run the unit from a 9V (PP9) battery. There is no reason why a small mains unit should not be used but the smoothing capacitor should be at least $5000 \mu \mathrm{~F}$. to keep hum level to an absolute minimum.

## Circuit Boards and Panel Controls

The tone generator, divider and voicing networks are assembled on Board A as in Fig. 12. The preset tuning potentiometers PR1 to PR13 should be


Fig. 12: Layout of circuit Board A for the tone generator, divider and voicing networks.


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50 ohm or 600 ohm mic inputs may be ordered at extra cost Size: Front Panel $16 \frac{1}{\mathrm{in}} \times 7 \mathrm{in}$. Cut out $15 \frac{1}{2} \mathrm{in} \times 6 \mathrm{in}$. Fuses A.C. 1.5 amp (B.S.) mounted on back panel.

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Control panel -18 s.w.g. aluminium $21^{1} 2^{\prime \prime} \times 2 \frac{7}{8} 8^{11}$


Fig. 13 : Details of the layout and wiring of the control panel.

## components list

## Resistors :

| Resistors : |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| R1 | 2.2k $\Omega$ | R14 | 100k $\Omega$ |  | R27 | 3-9k $\Omega$ | R40 | 10k $\Omega$ |
| R2 | 22k $\Omega$ | R15 | 120k $\Omega$ |  | R28 | 3.9k $\Omega$ | R41 | $2 \cdot 2 \mathrm{k} \Omega$ |
| R3 | 3.9k $\Omega$ | R16 | 3.9k $\Omega$ | * | R29 | 56k $\Omega$ | R42 | 10k $\Omega$ |
| R4 | $100 \Omega$ | R17 | 12k $\Omega$ |  | R30 | 12k $\Omega$ | R43 | 220k $\Omega$ |
| R5 | 8-2k $\Omega$ | R18 | 18k $\Omega$ |  | R31 | 4-7k $\Omega$ | R44 | 22k $\Omega$ |
| R6 | 2.2k $\Omega$ | R19 | 56k $\Omega$ |  | R32 | $1 \mathrm{k} \Omega$ | R45 | $3 \cdot 9 \mathrm{k} \Omega$ |
| R7 | 18k $\Omega$ | R20 | 22k $\Omega$ |  | R33 | 5.6k $\Omega$ | R46 | $4 \cdot 7 \mathrm{k} \Omega$ |
| R8 | 18k $\Omega$ | R21 | 1k $\Omega$ |  | R34 | 10k $\Omega$ | R47 | $12 \mathrm{k} \Omega$ |
| R9 | 18k $\Omega$ | R22 | 4-7k $\Omega$ |  | R35 | $4 \cdot 7 \mathrm{k} \Omega$ | R48 | 56k $\Omega$ |
| R10 | 18k $\Omega$ | R23 | 12k $\Omega$ |  | R36 | 56k $\Omega$ | R49 | $4 \cdot 7 \mathrm{k} \Omega$ |
| R11 | $2 \cdot 2 \mathrm{k} \Omega$ | R24 | 56k $\Omega$ |  | R37 | $1 \cdot 5 \mathrm{k} \Omega$ | R50 | $1 \mathrm{k} \Omega$ |
| R12 | $8 \cdot 2 \mathrm{k} \Omega$ | R25 | $2 \cdot 2 k \Omega$ |  | R38 | $1 \mathrm{k} \Omega$ | R51 | 12k $\Omega$ |
| R13 | $560 \Omega$ | R26 | 5-6k $\Omega$ |  | R39 | Not required |  |  |

All resistors $\frac{1}{4}$ W $10 \%$
PR1-14 10k $\Omega$ pre-set potentiometer. (Sub-miniature carbon skeleton type.)
VR1 $50 \mathrm{k} \Omega$ carbon potentiometer, linear.
VR2 $100 \mathrm{k} \Omega$ carbon potentiometer, log.

## Capacitors :

| C1 | $500 \mu \mathrm{~F}$ (elec) |
| :--- | :--- |
| C2 | $0.022 \mu \mathrm{~F}$ |
| C3 | $0.022 \mu \mathrm{~F}$ |
| C4 | $0.03 \mu \mathrm{~F}$ |
| C5 | $0.1 \mu \mathrm{~F}$ |
| C6 | $0.1 \mu \mathrm{~F}$ |
| C7 | $0.03 \mu \mathrm{~F}$ |
| C8 | $50 \mu \mathrm{~F}$ (elec) |
| C9 | $250 \mu \mathrm{~F}$ (elec) |
| C10 | $0.015 \mu \mathrm{~F}$ |


| C11 | $1 \mu \mathrm{~F}$ (paper) | C21 | $1 \mu \mathrm{~F}$ (elec) |
| :---: | :---: | :---: | :---: |
| C12 | $10 \mu \mathrm{~F}$ (elec) | C22 | $100 \mu \mathrm{~F}$ (elec) |
| C13 | $1 \mu \mathrm{~F}$ (elec) | C23 | $1 \mu \mathrm{~F}$ (paper) |
| C14 | $2 \cdot 5 \mu \mathrm{~F}$ (elec) | C24 | $0.5 \mu \mathrm{~F}$ |
| C15 | $0.05 \mu \mathrm{~F}$ | C25 | $0.022 \mu \mathrm{~F}$ |
| C16 | $100 \mu \mathrm{~F}$ (elec) | C26 | $0.015 \mu \mathrm{~F}$ |
| C17 | 1000 pF (cer) | C27 | $50 \mu \mathrm{~F}$ (elec) |
| C18 | $10 \mu \mathrm{~F}$ (elec) | C28 | $200 \mu \mathrm{~F}$ (elec) |
| C19 | $25 \mu \mathrm{~F}$ (elec) | C29 | $25 \mu \mathrm{~F}$ (elec) |
| C20 | 500 pF (mica) |  |  |
|  | capacitors at least 12 VW |  |  |

Semi-conductors :

Tri-Tr9
Switches:
S1, 2, 3 pole, 3 way, ganged wafer type.
S4, 5 Single pole, on-off, slide type.
S6 Single pole, on-off, toggle or slide type.

## Miscellaneous :

Aluminium panel $21 \frac{1}{2} \times 2 \frac{2}{6}$ in. 18 s. w.g. Inductor L1 (Type CP6713/2, Henrys Radio Ltd). Output Socket.
Control knobs (3). Veroboard (2) $17 \frac{1}{2} \times 3 \frac{3}{4} \mathrm{in}$. and $7 \frac{1}{2} \times 3$ in. both plain, 0.15 in . matrix.
mounted at an angle or side by side so that the adjustment slots can be reached with a small screwdriver from the back of the case.
Connection from the tuning pre-sets PR1 to PR14 to their respective contacts are also shown in Fig. 12 together with connections to the panel controls VR1, VR2, S1, S3, S4, S5 etc.
The control panel assembly and wiring is shown in Fig. 13. Note that some components such as R43, $\mathrm{C} 25, \mathrm{C} 26, \mathrm{R} 17$ and R18 are wired between controls.

Mention has already been made regarding the drum brush circuit and adjustment for long or short decay. The choice is for the user but should the sound level appear too high, then the resistor R46 ( 4.7 K ) should be increased until the required balance between drum brush and bass notes is achieved.

Before tuning set the wipers on the pre-sets PRI to PR13 to midway, set the 'pitch' control VR1 also to midway position and then begin tuning with PR13 which will tune the highest C note. If possible the


Fig. 14 : Circuit Board B containing the noise generator and control amplifier.

The control panel is mounted on the top of the case framework at the front (see Fig. 8 and Fig. 9 Part I).

The drum brush noise generator and control amplifier is assembled on Board B as shown in Fig. 14. Connections to S 5 and the drum brush contacts are also shown.

Board B is mounted toward the rear of the unit on the lower cross members of the case in the position shown in Fig. 8 Part 1. Board A is mounted toward the front of the case as in Fig. 8 Part 1. Board B should be situated to the left of the case (looking from the rear) so as to leave enough space for the battery. The output jack can be mounted on a small aluminium panel as shown in the photograph in Part 1.

## Checking and Tuning

If an oscilloscope is available the waveform from the multi-vibrator $\operatorname{Tr} 1-\operatorname{Tr} 2$ can be checked at the junction of R4 and the collector of Tr2 and from the divider at C8-R14. The function of the drum brush circuit can be checked at C20-R 35 . The voiced waveforms can of course be checked at the output socket and those for flute should appear nearly sinusoidal. Wth the 'clarinet' switched on a small pulse will be superimposed on the flute waveform and the audible tone will be slightly 'reedy'.

With $8+16$ pitch the respective waveforms will combine and the 8 ft . waveform will appear to sit on top of the 16 ft . waveform. Audibly, the 8 ft . and/or 16 ft . pitch with flute voicing should have a round deep tone.
tuning should be done with the aid of an electronic organ with bass by tuning each note on the pedal unit to zero beat. Failing this, tune with a piano and use the zero beat method for each note. Start with the highest C (PR13) and tune each note going down using 8 ft . pitch and flute voicing. The tuning will maintain itself for a long time but should be checked occasionally to ensure perfect pitch.

## Final Assembly

The covers for the top, back and base can be made from hardboard cut to fit over the framework. Make a cut-out where the battery goes in and a small separate panel to secure the battery in place, Fig. 15. The covers should be screwed on so as to allow quick access to the pedal contacts and circuit
-continued on page 477


Fig. 15 : Arrangement at rear of unit.

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The previous article (Part 1) dealt with the cabinet and main: chassis assembly and with the function of the pre-amplifier and tremulant circuitry. The full circuit for the pre-amplifier was included (Fig. 5 Part 1) which should be used in conjunction with the various assembly details given in this article.

The pre-amplifier and tremulant control circuit is divided into three sections each having its own circuit board as in Figs. 6, 7 and 8. Before dealing with these however, it is advisable to construct the small separate assemblies such as the panel tremulant indicator lamp, the 1.d.r. mounting, its control lamp and cover, and the mains input socket panel which is fitted at the rear of the cabinet.


Fig. 6: Microphone pre-amplifier on Circuit Board 1.
With these done and the front panel drilled ready for the controls etc. the circuit boards can be made and wired and the whole amplifier finished off ready for testing.

The panel tremulant lamp unit is simple to make and requires only an m.e.s. batten lampholder mounted on a bracket as in Fig. 9. This is fitted to the chassis with self tapping screws in the position shown Fig. 13, so that the lamp 'looks' through the hole provided as in the front panel layout diagram. A piece of coloured celluloid is glued over the hole. inside the panel, to enhance the appearance.

When the tremulant circuit is operating, this lamp flickers at the tremulant speed and its brilliance varies according to the setting of the tremulant depth control.

The 1.d.r. is mounted on a small piece of s.r.b.p. attached to a chassis fixing bracket as in Fig. 10. Its control lamp B2 is mounted in a dial light holder (m.e.s.) as shown in the same diagram. The two assemblies are secured to the chassis with self tapping screws so that the lamp is level with the l.d.r. and approximately $\frac{1}{8}$ in. in front.

The l.d.r. cover is shown in Fig. 11 and this is simply fitted over the l.d.r. and its lamp and secured to the chassis with self tapping screws. This cover keeps any external light off the 1.d.r. and is useful when the amplifier is being tested out of the cabinet,


Fig. 8 : Phase shift oscillator and LDR control amplifier, Círcuit Board 3.
where light could reach the l.d.r. and alter its operating range.

The remaining small assembly is the 3 -pin mains input socket which requires only a panel as in Fig. 12. This assembly is fitted at the back of the cabinet as can be seen in the photographs.

## Pre-amplifier Circuit Boards

These are numbered 1, 2 and 3 and are located on the main chassis as in Fig. 13. Boards 1 and 3 are $5 \times 4 \mathrm{in}$. plain s.r.b.p. with $0 \cdot 1 \mathrm{in}$. matrix and Board 2 is $5 \times 7 \mathrm{in}$. of the same material. Each board is mounted on $\frac{3}{8} \mathrm{X} \frac{3}{8} \mathrm{in}$. aluminium angle which secures the board to the chassis (self tapping screws).

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| :--- | :--- | :--- | :--- | :--- |
| DL92 | $6 / 6$ | EF41 | $12 / 6$ | PCE800 |

 \begin{tabular}{ll|ll|ll|l|}
DL96 \& $7 / 9$ \& EF80 \& $6 /-$ \& PCF80 \& $6 / 6$ \& OA200 <br>
DM70 \& $6 /-$ \& EF83 \& O/7 \& PCF82 \& $6 / 9$ \& OA20 2

 

\hline DM70 \& $6 /-$ \& EF883 \& $9 / 7$ \& PCF82 \& $6 / 9$ \& OA2 202 <br>
DM71 \& EF85 \& $6 / 8$ \& PCF84 \& O/8 \& OA210
\end{tabular}$0 /-101$

## $2 / 6.0029$

7/6.8FR 17/6 AF139 $10 /$ CRS3/80 1 $1 /{ }^{-18 P 2}$\begin{tabular}{r|ll}
$7 / 6$ \& $3 N 139$ \& 80 <br>
$10 /-$ \& $3 N 140$ \& 10



\hline $0 A 211$ \& $9 / 6$ \& $0 C 78$ <br>
OAZ200 \& $11 /-$ \& $0 C 76$
\end{tabular}

| $Y 86$ | EF88 |
| :--- | :--- | :--- | :--- |
| EF89 |  |



 E88CC $/ 01$  | $0 A Z 207$ | $9 / 6$ | $0 C 82$ |
| :--- | :--- | :--- |

 | EBC8S | $8 /-$ | EL84 | $10 / 6$ | PCH200 |
| :--- | :--- | :--- | :--- | :--- |
|  | EL4 | $11 / 6$ | PCL81 |  |

EBF8 ..... 

- OAZ223 to
- OAZ223 to

| $7 / 6$ | OAZ225 |
| :--- | :--- |
| OC16 |  |
| OC22 |  || CCC86 | $7 / 6$ | EM80 | $7 / 6$ |
| :--- | :--- | :--- | :--- |
| COC88 | $7 /-$ | EM84 | $7 /-$ |
| EM8 | $11 /$ |  |  ||  | $7 / 6$ | EM80 | $7 / 6$ |
| :--- | :--- | :--- | ---: |
| ECC88 | $7 /-$ | EM84 | $7 /-$ |
| ECC189 | O/6 | EYBI | $11 /-$ |
| RCF80 | $6 / 6$ | EY81 | $7 /-$ || ECF88 | 15/6 | EY86 |
| :--- | :--- | :--- |
| EY88 |  |  |ECF801 12/6 EY88ECF802 $12 / 8$ EZ41| BCF802 | $12 / 6$ | EZ48 |
| :--- | :--- | :--- | :--- |$\begin{array}{ll}\text { ECH } \\ \text { ECH } & 11 /- \\ 18 & -\end{array}$$\begin{array}{cc}\text { ECH42 } & 18 / 9 \\ \text { ECH81 } & 5 / 9\end{array}$| ECH81 | $5 / 9$ | GZ34 |
| :--- | :--- | :--- |
| KCH83 | $8 / 6$ | KT88 || ECH84 | $8 / 6$ | KT86 |
| :--- | ---: | :--- | :--- |
| ECH2 |  |  |
| ECH200 | $18 / 6$ | N78 || ECH200 $18 / 6$ | N78 |
| :--- | :--- | :--- |
| ECL80 | OA? |7/6 PL504$8 / 6 |$| PX2 |
| :--- |
| PY |$5 / 6$

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$87 / 6$| ECL83 | $10 / 6$ | PABC80 | $7 / 6 \mid$ |
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| EYY80! | $0 / 6$ |  |  |

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$8_{i}$ \& UCF80 <br>
$17 / 6$ \& UCH42 <br>
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$7 /-$ \& Z800U <br>
78 <br>
7 \& Z801U
\end{tabular}$18 \mathrm{O} / 40$

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Fig. 7: Guitar and tremulant amplifier on Circuit Board 2.


Board 1 contains the microphone pre-amplifier Tr 1 and $\operatorname{Tr} 2$ and it is most important that the screened leads are earthed to the common earth line as shown.

Board 3 contains the tremulant phase shift oscillator $\cdot \operatorname{Tr} 3$ and the I.d.r. control amplifier Tr4. Note that the earth returns from VR2 and the tremulant

Flg. 9: (far left) Mounting bracket for tremulant indicator lamp.

Fig. 12: (left) Mains input socket mounting.

on-off switch must be made as shown, to the common earth line on the circuit board, and to nowhere else. The l.d.r. control amplifier $\operatorname{Tr} 4$ must be fitted with a small heatsink as shown in Fig. 8.

The guitar and tremulant amplifier board (Board 2) has several screened lead connections and again it is important that these are earthed, as shown, to the common earth line on the board, as must the earth return from the 1.d.r. (l.d.r-B).


Fig. 13: Layout of panel controls and main components on top of chassis.

The coupling transformer T3 is bolted directly to the circuit board and is a type CP6713/2. It has the IP-OP and IS-OS connections clearly marked on it and these must be connected as in the diagram.

## Pre-amplifier Power Supply

It is not convenient to take the supply voltage for the pre-amplifiers from the output module power supply as this is a sealed unit. Transformer T2, the rectifier MRI and smoothing capacitor C28 form the pre-amplifier power supply and are wired as shown in Fig. 14.

The reason for locating T2 at the far end of the chassis is to prevent the tremulant amplifier transformer T3 from picking up mains hum by mutual coupling. The mains transformer T2 has three secondary tappings but only the 17 V tap is used.

## Chassis and Panel Layout

The positions of the circuit boards, the pre-amplifier power supply components, the power module and the module power supply are given in Fig. 13. It is most important to adhere to this layout to prevent hum loops around the chassis.

Points for the fixing holes of the power output module and its power supply have not been included as prototype units were used by the writer for the original amplifier. Fixing holes are however, provided

Rear view of com pleted amplifier and speakers.


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Fig. 14 : (below) Wiring of panel and chassis components.

on both and the two units have only to be mounted in the position shown.

Make sure they are firmly bolted to the chassis using all the fixing holes provided.

These units complete with interconnecting cables and plugs and the only external connections necessary are those of the mains input, the loudspeaker(s) and signal lead from the master volume control VR8.

It is most important that the earthed side of VR\& is taken to earth only via the screening braid to the earth pin of the power unit input signal DIN sócket as shown in Fig. 15B. It should be explained that although the signal input socket for the power module is located on the MU422 power supply unit it is carried through to the power module by the screened interconnecting cables.

Point to point wiring of the various controls, the pre-amplifier power supply and the mains input connections are given in Fig. 14. Note the earth connections for the signal input jacks and controls VR1, VR4, VR5 and VR7 which finally go to the common earth line on circuit Board 1. The mains supply circuits are shown separately in Fig. 16.


Fig. 15: Connections for speakers and signal input lead.

## Loudspeakers

The terminals of the Goodmans type 12P loudspeakers specified for the PW25-50 amplifier are marked with regard to phasing. Connect them in parallel as shown with the 'red spot' terminals on the same line. Do not under any circumstances earth either of the loudspeaker connections or the loudspeaker frames. Connect only to the DIN loudspeaker socket on the left hand side of the MU422 unit as shown in Fig. 15A.


Fig. 16: Mains input wiring details.

The third and final article will deal with optional extras-the foot control tremulant. the wah-wah control and with testing the amplifier for correct performance.

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gible hum. Talve line up: $-2 \times$ ECL86 Triode Pentorles. $1 \times$ EZ80 as full wave rectifler. Two dual potentionmeters are provided for bass and trebie control, giving bass and treble boost and cut. A dual volume control is used Balance of the left and right hand channels can be ad usted by means of a separate halance at the rear of the cull pals. nately $300 \mathrm{~m} / \mathrm{v}$ for full peak output of 4 watts per charne feedback in a carefully calculated circuit, allows high eedback in a carefuly calculaped eircit, allowa high Supplied complete with knobs, Supplied complete with knobs, chassis size $11^{\prime \prime} \mathrm{w} \times 4$ d. Overail height including valves $5^{\prime \prime}$. Ready built and tested
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Knowing the fierce independence cherished by some reviewers, and guessing at a similar trait in others, Henry is inclined to regard the Consumers' Association as well-meaning but misguided. Unfortunately, the sort of public who write letters of sympathy to Annie Walker or believe that Waggoner's Walk exists, are inclined to take the Which verdict as the word of the Law.

The C.A. may say that drafts $o_{\text {f }}$ reports are subject to verification and revision, and that it is often these drafts that receive instant publicity, but how often, we may ask, is refutation made? Recently, for example, Which came out quite strongly about the high breakdown rate of colour television receivers. According to their survey, one in 17 sets gives off smoke and one in 40 explodes!

Explodes, mind you, not merely dissolves into an indeterminate mix of dun and indigo, or curses visual blue streaks at its user, but ${ }^{\circ}$. . expands violently with loud report under influence of suddenly developed internal energy.'*

Along with the technical secretary of the British Radio Equipment Manufacturers' Association, this cynical onlooker is inclined to think that the Which findings were unrepresentative and 'out of line with makers' reports on breakdowns'.

This gent, the appropriately named Mr. Donald Doo, claimed that when the first draft of the Which report was submitted to him the paragraph on smoking and exploding colour television sets was conspicuous by its absence.
'We would have challenged it straight away,' he claimed. 'We have had no reports from any of our members of problems like this.'

I'll bet they haven't. Not since the early days of colour television at least. Those of us who have


The permutations from knob-twidd/ing. . .
slogged at a bench are well aware that teething troubles were experienced; are even ready to admit that, despite the brochures and advertisements, modern television receivers can and do break down.

Stop and think-the average colour television receiver has four times as much in it as the monochrome equivalent. There are between twice and three times as many controls for the installer to set up. The permutations of error from quite simple knob-twiddling are disproportionately large. Signal variations at the siteghosting, changes in level, interference, etc.-which would be tolerated in black and white become very pronounced when a chromatic scene is being viewed.

Yet how many of the 400,000 colour TV installations are totally unsatisfactory? A higher proportion than black and white-of course. But do we really believe, as Which implies, that 10,000 sets have 'exploded' since installation?

After all, if you read this article and feel the same way about the pontifical pronouncements of Which as 1 do, you don't say: 'Ah-Ha, I agree with the writer.'

Oh no, you say: ‘Ah-Ha, Henry agrees with me.'

I hope.

[^6]
# NOTES ON THE PW UNIT-BUILT GENERAL COVERAGE RECEIVER 

DETAILS of this 12-transistor 4-waveband receiver were published in the March and April 1970 issues of "Practical Wireless." These brief notes should be of assistance to anyone considering constructing the receiver.

The completed circuit shows 4 diodes and 12 transistors, with 4-band coverage, and it is apparent that quite a number of constructors feel that the wiring of the whole receiver is rather complicated. The whole circuit is not unusually complex for this type of equipment. However, it should not be overlooked that the receiver can be constructed in simpler form, and added to from time to time, and is, in fact, the manner in which the original receiver was made.

This is an important point, because it does mean that a relatively simple, straightforward superhet is initially built and wired which can be tested and used in this way. When this is found to perform correctly, other features can be added the receiver being tested each time an addition is made. Should a wiring error or other fault be present, this greatly reduces the number of circuits to be investigated.

A few further details on this stage by stage method of building the receiver should prove useful.

## STAGE BY STAGE ASSEMBLY

The initial circuit is wired for one waveband only which will avoid errors in wiring the many switch contacts, and sets of coils. The SW 1 range coils, for $30-11 \mathrm{MHz}$, are very near the switch wafers, and tend to hinder the wiring of coils, so it is probably best to wire the SW2 range coils first, for $14-5 \mathrm{MHz}$.

By omitting the r.f. stage, there are only two coils, those for the mixer and oscillator circuits. The bandswitch is set to its second position, and these two coils are wired in. Should the receiver fail to operate because of a switch or coil wiring error, only these few connections need be checked.

When the receiver is working correctly on the SW2 range, add the pair of coils for the SW3 range, and test to see that proper results are obtained. Then add the m.w. range, and test again. Finally, the SWl range coils are wired in.

When the r.f. stage has been added, wire in the SW2 aerial coil, and test the receiver. Should a fault be present, only the few new items introduced need be checked. Then add the other aerial coils, one at a time, testing the receiver after each addition.

This is much better than wiring in the twelve coils, for four bands with r.f. stage, then finding some obscure fault exists in coil or bandswitch connections.

As described, the receiver is easily wired as a 6 -transistor superhet, for one band. It will then have $\operatorname{Tr} 2$ (mixer), $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$ (i.f. amplifiers), $\operatorname{Tr} 10$ (driver) and the output stage $\operatorname{Tr} 11 / \operatorname{Tr} 12$. Only the a.m. diode and a.g.c. rectifier D2 need be connected. This means that $\operatorname{Tr} 1$ (r.f. amplifier), $\operatorname{Tr} 5$ (meter amplifier), Tr6 and Tr7 (product detector) with b.f.o. $\operatorname{Tr} 8$, and a.f. amplifier $\operatorname{Tr} 9$, are not needed, neither is the multi-way function switch, nor diodes D1, D3 and D4. The circuit, in this simplified form, is capable of excellent reception and volume.

The additional features can be added in any order preferred. Probably the r.f. amplifier, Trl, will be found most useful. After this, $\operatorname{Tr} 9$, for additional audio gain, may be included.

Adding $\operatorname{Tr} 6, \operatorname{Tr} 7$ and $\operatorname{Tr} 8$, will then allow c.w. and s.s.b. to be resolved, as the use of the diode D2 allows reception only of a.m. signals.

Remember to test the receiver after each addition. Then if a fault or error has been introduced, it must be in the part of the circuit last added. By proceeding in this way there will be no need to check the whole receiver, but only some relatively small part of it .

## AUDIO TRANSFORMERS

The driver and output transformers listed are no longer made. Fortunately many transformers suitable exist for OC81D driver and 2xOC81 and similar output transistors. The Weyrad LFDT4 driver and OPT1 output transformers will be found suitable. Connecting data for the LFDT4 appear in Fig. I, connections for the OPTI remaining unchanged.


Fig. 1: Connections to alternative audio driver transformer

As is usual with this type of circuit, operation of the output pair is critically dependent upon the relative values of $R 42$ and $R 40 / R 41$. If there is distortion, R42 should be increased slightly to about 100 ohms.

Any ordinary 2 or 3 ohm speaker is suitable, preferably a reasonably large unit, in a cabinet.

## AERIALS

Long-range reception is possible with the telescopic aerial, especially on the h.f. ranges. However, for the best possible results with weak signals, some form of external aerial should be added. This can be of any type normally employed with a communications receiver such as a random length external wire, or an end-connected wire with tuner, or a dipole or tuned doublet, etc. Any of these aerials can be expected to give an improvement in the signal strength of several S-points.

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## 

MINIATURE

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a good communications receiver with either internal or external 100 kHz marker of known accuracy are the basic alternatives. If an existing v.f.o. of known accuracy is obtainable, this can make things much easier.
Having connected the necessary d.c. supply to the v.f.o., set the trimmer capacitor to about mid-point and the tuning capacitor to maximum value (vanes fully meshed). Loosely couple the output to the receiver aerial input and allow to warm up for 10 to 15 minutes. Next search around 3.5 MHz on the receiver dial, the b.f.o. being switched in first. When the beat note is heard, note the frequency on the receiver dial. If no beat note can be found, check that the v.f.o. output is present using an oscilloscope or valve-voltmeter.

With the beat frequency noted, set the receiver dial accurately to $3 \cdot 5 \mathrm{MHz}$ using the 100 kHz marker to ensure accuracy. Now adjust the trimming capacitor in the v.f.o. until the beat note is obtained on exactly 3.5 MHz . If the original beat frequency was high, VC2 should be increased and if it was low, decreased. The setting of VC2 should be carried out with care, the trimming tool being removed after each adjustment as a small hand capacity effect is almost unavoidable. With this frequency correctly set on zero beat, the v.f.o. dial can be marked at this point. No further trimming should now be required.
The receiver dial is next set to 3.6 MHz , again using the crystal marker, and the v.f.o. tuning capacitor slowly adjusted until the beat note is again heard. Having set VC1 for exactly zero beat, mark the appropriate point on the scale. This procedure is repeated for 3.7 and 3.8 MHz . The upper limit of 3.8 MHz will vary slightly between different units due to differences in stray capacitance.
The mid-points of 50 kHz steps and 10 kHz subdivisions can only be accurately marked if the receiver dial has suitable calibration points or if an existing v.f.o. is available. As the scale divisions are almost linear, however, reasonably accurate subdivisions can be obtained geometrically. When the main scale is fully calibrated, the harmonic calibrations for the other bands ( $7 \mathrm{MHz}, 14 \mathrm{MHz}$, etc.) can be completed on the lower scales of the v.f.o. dial.

## CORRIGENDA

## FREQUENCY METER-MAY 1970

Under the heading "Construction"' the sentence "Note the breaks in the copper strip at holes D9, D15 and E4" should read "at holes C14, D3 and D9."

## SUMS AND CIRCUITS-JUNE 1970

The voltage and current waveforms shown in Fig. 3.3 and 3.4b should be interchanged

In the July issue of the same article the equation on page 192 reading $-1+0 \cdot 3010=\overline{0} \cdot 6990$ should read $-1+0 \cdot 3010=$ -0.6990 .

TEN OR FIFTEEN METRE CONVERTER-JUNE 1970
Figure 1 and the components list should show R3, R8 and R 10 as $1 \mathrm{k} \Omega$ and not $10 \mathrm{k} \Omega$.

LIGHT OPERATED SWITCH-JULY 1970
The value of R7 both in the circuit and the components list should read $4.7 \Omega$ and not $4.7 \mathrm{k} \Omega$.

## AUDIO EXPANDER/COMPRESSOR-AUGUST 1970

In the components list C11 should have read 100 pF and not $100 \mu \mathrm{~F}$. The circuit is however correct.
In Fig. 11. the screening of the wire connected to the slider of Si section $C$ should be connected to the other screen wires and not to the slider of S 1 section B .
boards in the event of a faulty contact or circuit failure.

The last stage is to fit aluminium or wooden rails, one on each side of the case, to prevent the unit tipping forward when the pedals are pressed. Full downward pressure on a pedal should bring it to within half inch or so of floor level. Further pressure would tip the unit forward, hence the need for the rails as shown in Fig. 16.

## Amplifier Requirements

Because of the very low frequency of the pedal bass notes a sizeable loudspeaker in a suitable enclosure is necessary if the true bass fundamentals are to be audible. Small organs like the Philicorda have only small loudspeakers which are not suitable for bass reproduction. For organs of this calibre it is best to build a suitable amplifier with an output of 5 to 10 watts which can be incorporated within the speaker enclosure. The speaker should be 10 to 12 in . in diameter.


Fig. 16 : Fitting of rails to case.
There is no reason why the pedal bass unit described in this article should not be integrated with an amplifier and speaker so designed as to fit beneath small organs like the Philicorda. For portables fed into large power amplifiers with sizeable speakers it should only be necessary to connect the pedal bass unit to a suitable input on the amplifier.

There is of course the question of volume control or 'expression' whilst playing. For small organs where the overall sound output is relatively low it will be sufficient to set the pedal bass sound to an arbitrary level. A pedal type volume control could be used or an extra volume control mechanically coupled to an existing pedal.



#### Abstract

A series of simple transistor projects, each using less than twenty components and costing less than twenty shillings to build.


ALTHOUGH we have described two generalpurpose amplifiers in this series, tone control facilities have not been incorporated, mainly due to our limitation on cost. The tone control stage described here is a general-purpose one which can be added to most transistor amplifiers in the early stages. The gain, with the controls in their middle settings, is very small as the amplification of the stage is nearly all used as negative feedback to alter the tone. The circuit shown is not very original, in fact it is widely used in commercial amplifiers.

Performance of this type of circuit is excellent; with reference to 1 kHz , frequencies of 100 Hz can be boosted or cut by up to 15 dB and the same degree of control is available at 15 kHz . A low noise transistor, a BCl 69 C , is used so noise introduced by this additional stage is negligible.

## THE CIRCUIT

For those unfamiliar with this type of circuit, a quick glance will probably lead to rapid bafflement, but basically the design is simplicity itself.

The input is coupled to the d.c. blocking capacitor C1 and is then applied by one path to the base of the transistor through C3 and a part of VR1, a $100 \mathrm{k} \Omega$ potentiometer. The actual part of VR1 that it passes through depends on the setting of the control. By another path the signal reaches the transistor via R 2 and C 5 . It will be seen that C5 is paralleled by a part of VR2, again depending on the setting of the control.

These combined signals are applied to Tr 1 which has R 3 , a $10 \mathrm{k} \Omega$ resistor acting as the collector load and R4 as the base bias. The output is taken from the collector via C 7 to the existing volume control.

Also connected to the collector of $\operatorname{Tr} 1$ is C6. Now in a common emitter amplifier (which is what we are using here) there is phase inversion, that is the signal at the collector is out of phase with the signal applied to the base. This anti-phase signal is applied to the other side of VR1 and VR2 via an identical network to the one that fed the original signal to these controls.

It will be seen then that both controls are able to select either very little or a considerable amount of the out-of-phase signal and since these networks are frequency selective we are able to achieve a considerable amount of control over the tone.

Careful scrutiny of the circuit will show that a certain degree of negative feedback is applied to the transistor through R4, the base bias resistor, but this is quite small and anyhow is not frequency selective. Many designs decouple this a.c. feedback by using two resistors in series, their common junction being connected to earth via a high value capacitor, such as $100 \mu \mathrm{~F}$; in practice the author has found this to be unnecessary.

No. 18

## ADD-ON TONE CONTROL



Fig. 1: The circuit of the add-on tone control. VRI is the treble control, VR2 the bass control.

## components list

## Resistors:

| R1 | $47 \mathrm{k} \Omega$ | R3 |
| :--- | :--- | :--- |
| R2 | $47 \mathrm{k} \Omega$ | R4 $\Omega$ |

R2 $47 \mathrm{k} \Omega$
R4 $2 \cdot 2 \mathrm{M} \Omega$
All $\frac{1}{8}$ or $\frac{1}{4}$ watt, $5 \%$ types
VR1 $100 \mathrm{k} \Omega$ linear pot. Treble control
VR2 $250 \mathrm{k} \Omega$ linear pot. Bass control

## Capacitors:

| C1 | $10 \mu \mathrm{~F} 12 \mathrm{~V}$ | C5 | $0.01 \mu \mathrm{~F}$ |
| :--- | :--- | :--- | :--- |
| C2 | $1,000 \mathrm{pF}$ | C6 | $10 \mu \mathrm{~F}$ |
| 12 V |  |  |  |
| C3 | $1,000 \mathrm{pF}$ | C7 | $10 \mu \mathrm{~F}$ |
| C4 | $0.01 \mu \mathrm{~F}$ |  |  |

Transistor:
Tr1 BC169C or BC109

## FREQUENCY SELECTIVE NETWORKS

There are probably many readers who are unsure what we mean by "frequency selective networks." In practice these are very simple and can be calculated and designed by even the raw beginner. A.C. theory can be very complicated and describing, from first principles, the operation of capacitors would be hard and is anyway unnecessary; just take it as a fact that the impedance of a capacitor is directly proportional to the frequency and the impedance, in ohms, is equal to $1 /\left(2 \pi \pi^{\mathrm{fc}}\right)$ where f is the frequency and C the capacitance in Farads; so that C 2 and C3 at 100 Hz have a "resistance" of about $1 \cdot 6 \mathrm{M} \Omega$ and at $10 \mathrm{kHz}, 16 \mathrm{k} \Omega$. Similarly C 4 and C 5 have a "resistance" at the same two frequencies of $160 \mathrm{k} \Omega$ and $1.6 \mathrm{k} \Omega$ respectively. Substituting these "resistance" values instead of the capacitors we are left with a potential divider (but only of course at a particular frequency) and it will be seen that the gain can be changed by the setting of the controls VR1 and VR2.


## theworld's most advanced high fidelity amplifier

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output of 5 watts R.M.S. ( 10 watts peak). It con. tains 13 transistors (including two power types), 2 diodes, 1 Zener diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.
The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required as part of the process of producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. This enables us to cover every IC-10 with the Sinclair guarantee of reliability.

# MONOLITHIC INTEGRATED CIRCUIT HIGH FIDELITY AMPLIFIER AND PRE-AMP 



## SPECIFICATIONS

Output 10 Watts peak, 5 Watts R.M.S. continuous.

Frequency response
Total harmonic distortion
5 Hz to $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$. Less than $1 \%$ at full output. Load impedance 3 to 15 ohms. Power gain $110 \mathrm{~dB}(100,000,000,000$ times) total. Supply voltage Size
Sensitivity
Input impedance
. $0.4 \cdot 0.2$ nches. $25.6 \cdot 10 \cdot 5 \mathrm{~mm}$.
Adjustable externally up to 2.5 M ohms.

## CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class $A B$ output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

## APPLICATIONS

Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

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# Project 60 



## Laboratory standard modular high fidelity

Sinclair Project 60 comprises a range of modules which connect together simply to form a compact stereo amplifier with really excellent performance. So good, in fact, that only 2 or 3 amplifiers in the world can compare in overall performance and now the constructor has choice of assemblies with either 20 or 40 watts output per channel, with or without filter facilities. The modules are: 1. The $Z .30$ and $Z .50$ high gain power amplifiers. 2. The Stereo 60 preamplifier and control unit. 3. The Active Filter Unit. 4. 4 supply units-PZ.5; PZ.6; PZ.7 and PZ.8. In a normal domestic application, there will be no significant difference between PZ. 5 or PZ. 6 unless loudspeakers of very low efficiency are being used, in which case the PZ. 6 will be required. For assemblies using two $Z .50$ 's there is the PZ.8 supply unit to ensure maximum performance from these amplifiers. No skill or experience are needed to build your system and the Project 60 manual gives all the instructions you can possibly want, clearly and concisely. Perhaps the greatest beauty of the system is that it is not only flexible now but will remain so in the future as new additions are made to the range. A stereo F.M. tuner is next to come. These and all other modules introduced will be compatible with those already available and may be added to your system at any time. And because Sinclair are the largest producers of constructor modules in Europe, Project 60 prices are remarkably low.

How to assemble and use Project 60 modules to best advantage in the above and other applications will be found in the fully descriptive Project 60 manual included with Project 60 systems. This 48 page manual is available separately, price $2 / 6 \mathrm{~d}$ including postage.

|  | System | The Units to use | In conjunction with | Your Project 60 Units will cost |
| :---: | :---: | :---: | :---: | :---: |
| A | Car Radio | 2.30 | Existing car radio, Sinclair Micromatic | 89/6 |
| B | Simple battery powered record player | 2.30 | Crystal pick-up, 12 V or more battery supply and volume control | 89/6 |
| C | Mains powered record player | Z. 30 and PZ. 5 | Crystal or ceramic P.U. Vol. control etc. | £9.9.0 |
| D | $20+20$ watts RMS stereo amplifier for most needs | Two Z.30s, Stereo 60 and PZ. 5 | Crystal, ceramic or magnetic P.U., most dynamic speakers, FM tuner, etc. | £23.18.0 |
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| F | $40+40$ watts RMS deluxe stereo amplifier | Two Z.50s, Stereo $60 \mathrm{PZ}$.8 and mains transformer | As for E | £32.17.6 |
| G | Outdoor public address system | 2.50 | Microphone, up to 4 P.A. speakers, 12 V car battery with or without converter, controls | £5.9.6 |
| H | Indoor P.A | One Z.50, PZ. 8 and mains transformer | Mic., guitar, heavy duty speakers etc., controls | ¢17.8.6 |
| J | High pass and low pass filters | AFU | D, E or F as above | £5.19.6 |
| K | Stereo F.M. tuner | To be released shortly |  |  |

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## GUARANTEE

If within 3 months of purchasing Project 60 modules directly from us, you are dissatisfied with them, we will refund your money at once. Each module is guaranteed to work perfectly and should any defect arise in normal use we will service it at once and without any cost to you whatsoever provided that it is returned to us within 2 years of the purchase date. There will be a small charge to service thereafter. No charge for postage by surface mail. Air-mail charged at cost.

## Z. 30 \& Z. 50 POWER AMPLIFIERS

The $\mathbf{Z . 3 0}$ together with the $\mathbf{Z . 5 0}$ are both of advanced design using silicon epitaxial planar transistors to achieve unsurpassed standards of performance. Total harmonic distortion is an incredibly low $0.02 \%$ at full output and all lower outputs. Whether you use the $\mathbf{Z} .30$ or $\mathbf{Z} .50$ power amplifiers in your Project 60 system will depend on personal preference, but they are the same physical size and may be used with other units in the Project 60 range equally well. For operating from mains, for the $Z .30$ use PZ. 5 for most domestic requirements, or PZ. 6 if you have very low efficiency loudspeakers. For $Z .50$, use the $P Z .8$ described below.

SPECIFICATIONS (Z. 50 units are interchangeable with 2.30 s in all applications.)

## Power Outputs

Z.30 15 watts R.M.S. into 8 ohms, using 35 V : 20 watts R.M.S. into 3 ohms using 30 volts.
Z. 5040 watts R.M.S. into 3 ohms from 40 volts: 30 watts R.M.S. into 8 ohms, using 50 volts.
Frequency response 30 to 300,000 $\mathrm{Hz} \pm 1 \mathrm{~dB}$
Distortion $0.02 \%$ into 80 hms
Signal to noise ratio better than 70 dB unweighted
Input sensitivity 250 mV into 100 Kohms.
For speakers from 3 to 15 ohms impedance
Size $3 \frac{1}{2} \times 2 \frac{1}{4} \times \frac{1}{2}$ ins. $(90 \times 58 \times 13 \mathrm{~mm})$

## STEREO 60 Pre-amp/Control unit

Designed for the Project 60 range but suitable for use with any high quality power amplifier. Silicon epitaxial planar transistors are used throughout, achieving a really high signal-to-noise ratio and excellent tracking between channels. Input selection is by means of push buttons and accurate equalisation is provided for all the usual inputs.

- Input sensitivities - Mag. p.u. 3 mV correct to R.I.A.A. curve $\pm$ 1dB: 20 to $25,000 \mathrm{~Hz}$. Ceramic p.u., Radio and Aux, each up to 3 mV .
- Output - 250 mV .
- Signal-to-noise ratio - better than 70 dB .
- Channel matching - within 1dB.
- Tone controls - TREBLE + 15 to -15 dB at 10 kHz : BASS +15 to
-15 dB at 100 Hz .
- Front panel - brushed aluminium with black knobs and controls.
- Size $8 \frac{1}{4} \times 1 \frac{1}{2} \times 4$ ins.
$(210 \times 138 \times 102 \mathrm{~mm})$
Built, tested
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## ACTIVE FILTER UNIT

For use between Stereo 60 unit and two Z.30s or Z.50s, the Active Filter Unit matches the Stereo 60 in styling and is as easily mounted. It is unique in that the cut-off frequencies are continuously variable, and as attenuation in the rejected band is rapid ( $12 \mathrm{~dB} /$ octave), there is less loss of the wanted signal than has previously been possible. Amplitude and phase distortion are negligible. The Sinclair A.F.U. is suitable also for use with
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Built, tested Built, tested
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## POWER SUPPLY UNITS

Designed specially for use with the Project 60 system of your choice. Illustration shows PZ. 5 power supply unit to left and PZ. 8 (for use with Z.50s) to the right. Use PZ.5 for normal Z.30 assemblies and PZ.6 where stabilised supply is essential.
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Data and application sheets 2／－per type


|  | Sheets $2 / 6$ |
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| $3 \mathrm{~A} \quad$ 6／－7／6 8／－9／－10／6 | range available：Electrolytie， |
| $5 \mathrm{~A}-11 / \mathrm{C}$ 13／－$-15 /-$ | styrene，Silver Mica，Tantalum， |
| $\begin{array}{llllll}7 \mathrm{~A} & - & 11 /-13 /- & -19 / 6 \\ 25 A & 27 / 6 & 80 /-83 /- & - & 37 / 6\end{array}$ | Trimmers，Tuners． |
| $\begin{array}{lllll} \text { 25A } & 27 / 6 & 80 /-83 /- & 37 / 6 \\ \text { Also } & 12 \text {, } & 100 & \text { PIV, } 15 /-: & 600 \end{array}$ | Examples： |
| PIV，35／6：25A， $400 \mathrm{PIV} 37 / 6$ | $2,000 \mathrm{mF} 25 \mathrm{~V}, 8 / 6$ |
| VEROBOARD | 3，000mH2 $25 \mathrm{~V}, 10 / 6$ |
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| $3 \frac{2}{2} \times 17 \mathrm{in} \quad 16 /-\quad 21 / 6$ | 10 watt $5 \%$（up to $25 \mathrm{k} \Omega$ only）， |
| $3{ }^{3} \times 17$ in（plain）$\cdots \quad 11 / 6$ | 2／6 |
| ${ }^{5} \times 17 \mathrm{lin}$（plain） $15 / 6$ | POTENTIOMETERS <br> Carbon： |
| $\text { of 50) } \quad 5 /-$ |  |
| Vero Cutter， $9 /-$ | Log，and Lin．，less switch， 3 ／ Log．and Lin．，with switeh，4／6． Wire－woum．Pots（3W），5／6． |
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| $4 \cdot 8 \times 4 \times$ lin Finned for Two | Twin Ganged Stereo Potk，Log． and Lin．，7／6． |
| TO－3 Trans．， $9 / 6.4 .8 \times 2 \times 1$ in Finned，for One TO－3 Trans． |  |
| 6／6．For SO－1，6d．For TO－5， | PRESETS（CARBON） |
| 1／－Finned．For TO－18，1／－ |  |
| Finned．For T0－18， $1 /-$ Finned． | 0.1 Watt $\quad 1 /-$ |
| RESISTORS | 0.3 Watt $\quad 1 / 6$ |
| Carbon Film |  |
| t watt 5\％，8d． | THERMISTORS |
| \％watt 5\％，［d． | R53（ETC）25／6 |
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| PCC189 | 0.55 |
| PCC805 | 0.85 |
| PCC806 | 0.80 |
| PCF80 | 0.30 |
| PCF82 | 0.85 |
| PCF84 | 0.50 |
| PCF86 | 0.80 |
| PCF87 | 0.85 |
| PCF801 | 0.50 |
| PCF802 | 0.50 |
| PCF805 | 0.75 |
| PCF806 | 0.70 |
| PCF808 | 0.75 |
| PCH2000.70 |  |
| PCL81 | 0.50 |
| PCL82 | 0.35 |
| PCL83 | 0.65 |
| PCL84 | 0.65 |
| PCL85 | 0.40 |
| PCL86 | 0.45 |
|  |  |



[^7]
## SILICON MAINS POWER

 RECTIFIERS| DD000 | 50p.i.s. | 500 mA | Wire ended | 0.15 |
| :---: | :---: | :---: | :---: | :---: |
| KD202 ${ }^{\text {B }}$ | 50 p . i.v. | 1A | Stud mounted | 0.15 |
| KD202A | 50 p .i.c | 3 A | Stud mounted | 0.25 |
| Rs21AF | $100 p$ i.. | 500 mA | Wire ended | 0.50 |
| RS210AF | 100p.i.r. | 750 mA | Wire ended | 0.20 |
| SX631 | 100p.i.v. | 750 mA | Stud mounted | 0.20 |
| K D202G | 100p.i.v. | 1 A | Stud mounted | 0.15 |
| KD202V | 100p.i.v. | 3 A | Stud mounted | 0.25 |
| D242 | 100p.i.v. | 10A | Stud mounted | 0.30 |
| 18121 | 150p.i.v. | 200 mA | Wire ended | 0.20 |
| IN3193 | 200p.i.v. | 750 mA | Wire ended | 0.15 |
| K [202E | 200p.i.v. | 1 A | Stud mounted | 0.20 |
| KD202D | $200 \mathrm{p} . \mathrm{i}$. | 3 A | Stud mounted | 0.30 |
| BYZ13 | 200p.ix. | 6 A | Stud mounted | 0.40 |
| IN645 | 225 p.i.v. | 400 mA | Wire ended | 0.25 |
| D226V | 300p.i.*. | 300 mA | Wire ended | 0.16 |
| K D2021 | 300p.i.v. | 1A | Stud mounted | 0.20 |
| 15113 | 400p.iv. | 400 mA | Wire ended | 0.25 |
| DD006 | 400p.i.r. | 500 mA | Wire ended | 0.25 |
| DD2? 6 | 400 p .i.v. | 1 A | Wire ended | 0.80 |
| RYZIE | 400 p ,i.v. | 6A | Stud mounted | 0.25 |
| DD716 | 400p.iv. | 35A | Stud mounted | 1.50 |
| RS27AF | 600 p .i.v. | 100 mA | Wire ended | 0.20 |
| 1N649 | $600 \mathrm{p} . \mathrm{i} . \mathrm{v}$. | 400 mA | Wire ended | 0.35 |
| IS715 | 600p.i.v. | 400 mA | Wire ended | 0.40 |
| 1N207I | 600 p . s . | 750 mA | Wire ended | 0.20 |
| BY127 | 600p.iv: | 1.4 | Wire ended | 0.15 |
| BY100 | 700p.i.s. | 450 mA | Wire ended | 0.20 |
| DD058 | 800p.i.2. | 500 mA | Wire ended | 0.35 |
| BYZ10 | 800p.i.s. | 6 A | Stud mountes | 0.40 |
| 1N5399 | 1000 p .i, | 1.5A | Wire ended | 0.25 |
| 1N5408 | 1000p.i, | 3A | Wire ended | 0.50 |

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