## PRAGTGAL WI i ?  iss <br> MARCH 1970



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## AISO:

METAL LOCATOR
FET's AND THEIR USES




The Prfinier Stereo System consists of an all transistor stereo amplifier. Garrard Model 2025 auto/manual record player unit fitted stereo/mono cartridge and mounted in teak finish plinth with perspex cover and two matching teak finish loudspeaker systems. Absolutely complete and supplied ready to plag in and play. The 10 transistor amplifier has an output of 5 watts per channel with inputs for pick up, tape and tuner also tape output socket. Controls: Bass, Treble, Volume, Balance, Selector. Power on/off, stereo/mono switch. Brushed aluminium front panel. Black metal case with teakwood ends: S:ze $12 \times 5 \frac{1}{2} \times 3 \frac{1}{2}$ in. high (Amplifier available separately if required $£ 14.19 .6$. Carr. 7/6.)

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 Operates on 4 Ü 11 batteries

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STEREO


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Total Distortion at 1 KHz at 5 watts, $0.35 \%$, at rated output $1.5 \%$.
Frequency Response: Minus 3 dB points 20 Hz and 40 KHz . Speaker: $3-4$ ohms ( $3-15$ ohms may be used).
Supply voltage: 24 V . DC. at $800 \mathrm{~mA}(6-24 \mathrm{~V}$. may be used)

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Frequency Response - wass control range $\pm 13 \mathrm{~dB}$ at 100 Hz Frequency Response-(with tone controls central) Minus 3 dB points at 20 Hz and 40 KHz . Sigmal to Noise Ratio-better than - 60 dB . Transistors 4 silicon Planar $104^{\prime \prime} \times 4 \frac{1}{2 "}^{\prime \prime} \times 2 \mathrm{t}^{\prime \prime}$. For use with Std. or L.P. records, musical instruments, all makes of pick-ups and mikes. Separate bass and treble lift control. Two inputs with control from gram. and mike. Built and tested,

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For Mullard 510 Amplifier $. . .67 / 11$ $350-0-350 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}, 4 \mathrm{a} .0 .5 \mathrm{~F} .3 \mathrm{v} .3 \mathrm{a} . \quad 39 / 9$ $\begin{array}{lll}350-0-350 \mathrm{v} & 150 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a}, \cdot \\ 350-0-5-6.3 \mathrm{v}, 3 \mathrm{a} . & 47 / 9\end{array}$ $425-0-425 \mathrm{v}, 200 \mathrm{~mA}, 6.3 \mathrm{v}, 4 \mathrm{a} .: \mathrm{c} .2 \mathrm{~L} .5 \mathrm{v}, 3 \mathrm{a}$. 425-0-425v. 200mA. 6.3v. 4a.. 6.3v. 3a.. Sv. $93 / 9$
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Rec. Retail

Plinths, tops and accessories of above available at $10^{\circ} \%$ discount on retail price.

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SHURE 31E
SHURE 32E
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GOLDRING 809
STEREO TAPE DECKS AND RECORDERS AKAI Model 4000D 3-head stereo tape deck AJWA TP 1011 professional stereo 3 head tape deck
SANYO MR910 4 track stereo tape recorde 2 detachable speakers
SANYO MR801 stereo tape deck
REVOX model 1104 4-rrack tape deck
GRUNDIG TK247 de-luxe stereo tape recorder

MONAURAL MAINS TAPE RECORDERS GRUNDIG TK120 continental twin-track
GRUNDIG TK 144 4-track tape recorder
GRUNDIG TK 149 Automatic 4-track tape
PHILIPS 4307 4-track tape recorder
PHILIPS 4308 2-speed 4-track tape recorder
COMPLETE HI-FI SYSTEMS
PHILIPS GF818 Philips autochange player,
integrated $2 \times 4$ watts amplifier, 2 separate RADON 404 SYSTEM G arate $2 \times 8$ watt amplifier. 2 bookshelf type
WINDSOR 1500 Garrard 2025 T/C, integrated $2 \times 4$ watt amplifier, 2 separate speakers. all finished in teak
TOSHIBA SOPHIA Transcription turntable, magnetic cartridge, integrated tuner amplifier, with stereo decoder, fitted hinged perspex top. 2 separate speakers, walnut perspe
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## TOPIC ロF THE MDNTH

## Is the RAE just?

THE object of an examination is to test the ability and proficiency of a candidate in a particular subject. But although the attainment of a pass certificate or diploma endows the holder with appropriate status, there is no doubt that in certain cases this is largely a reflected glory. Due to personal factors such as temperament and academic factors such as choice and phrasing of questions, it is still possible for one candidate to pass and another of greater talent to fail.

When one comes to examinations that are not purely academic, the situation is more complex and can be even more unsatisfactory. Two such examinations that touch our particular field, in which theory and practice intermingle, are the RTEB exam for service engineers and the RAE for aspiring amateur radio operators. Both, in our view, fall short of the ideal mainly because of the complicating factor of practical ability.
One of the commonest and most persistent criticisms of the Radio Amateurs Examination is that the format is heavily weighted in favour of the younger candidate who, because of greater learning ability, is best able to tackle the theoretical nature of the questions. Candidates in older age-groups have often forgotten the magic formulae learned years ago but nevertheless may be perfectly capable of building, operating and maintaining an amateur radio station. (Incidentally, it seems ludicrous that candidates for exams are not allowed to use standard reference sources on the spot-as they are able to do in any later practical application of the type of work involved.)

Of course, it is virtually impossible to arrange oral or practical examinations across the country since the RAE is organised by the City and Guilds of London Institute, not the GPO (to use its old name!). The question paper is set by a Committee including representatives of the RSGB, the GPO and C \& G, and to these bodies we strongly recommend that Part 2 of the RAE be divided into sections of (a) theory and (b) practice, Surely some way could be devised to ensure that future licence holders have been tested in some measure as to their practical ability to run a station, and are not passed purely as egg-heads with good memories.

The validity of the present RAE surely rests on two basic questions: (1) Is the primary object to screen out the incompetent? and (2) Does the present set-up ensure that those who pass can fulfil the requirements and responsibilities of running an amateur transmitting station?
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APRIL ISSUE WILL BE PUBLISHED ON MARCH 6th
PRICE INCREASE

We regret that owing to mounting production costs it has been necessary to increase the price of Practical Wireless to 3s. 6d. as from the April issue.

[^0]
## MEWS... WEWS... NEWS...

## Integrated audio amplifier



A 1 watt audio amplifier integrated circuit that has been designed for use as a single a.f. amplifier or as a semiconductor bed of a tape recorder, is one device in a new range of linear integrated circuits available from UECL, Microelectronics Division.
This audio amplifier, M5101P, is designed for use on a $V_{c o}$ up to 12 volts and with the addition of a fin will dissipate 1.8 watts. Distortion is typically $0.5 \%$ at $45 \%$ circuit efficiency.
The device consists of a preamplifier, driver and power amplifier and has input resistances of 30,000 ohms to both the

pre-amp and driver sections. The circuit consumes only 15 mA under zero signal conditions. The whole device is packaged in plastic dual-in-line and will operate over the temperature range $-10^{\circ}$ to $+125^{\circ} \mathrm{C}$.

This integrated circuit, being d.c. coupled, may also be used
as a servo amplifier.
The M5101P is available exstock at a price of 25 s . 5 d . on a cash with order baisis. Further details of this device may be obtained from Ultra Electronic (Components) Limited, 35-37 Park Royal Road, London, N.W.10. Tel: 01-965 5744.

## Hear it at Graham's

One comparative newcomer to the $\mathrm{Hi}-\mathrm{Fi}$ scene is GRAHAMS HI-FI CENTRE at 86-88 Pentonville Road, N. 1 (837 4412). They have set up instantaneous comparison facilities.

Grahams have provided a comprehensive $\mathrm{Hi}-\mathrm{Fi}$ auditorium which offers customers the opportunity of viewing a wide spectrum of the market. Their policy is first to ascertain the budget level of each customer and to stick to that as closely as possible. "Subject," they say, "to a discreet observation of the customer's reaction to the sound of equipment at his stated price level; if we feel that he is likely to "outgrow' his set-up, to feel dissatisfied with it after a little while, then we explain that we would rather not make a sale at that time. If his ear is so acute, better that he should get the right advice and not buy, than buy the wrong thing. In practice, most people return for equipment that will give them lasting pleasure, perhaps buying it in stages."

Grahams' agencies include Akai, Armstrong, Arena, Bang \& Olufsen, Bryan, Dual Dyna-
tron, Ferguson, Grundig, Rotel, Sony, Tandberg and Vandermolen, in addition to dealing in the normal range of high-quality equipment including Uher, Leak, Quad, Rogers, Thorens, Revox and Goldring.

'Playback' is the title of a 16 -page mini-magazine available free of charge from stockists of Scotch magnetic tape.

The issue now available from electrical and hi-fi shops includes features on actor David Hemmings and his use of a tape recorder both on and off the film
set; tape recording in schools; and 'how-to-do-it' articles on recorder care and recording the spoken word. There is also some helpful advice on using a tape recorder to make your party go with a swing.
'Playback' is published quarterly by the 3M Company, manufacturer of Scotch magnetic tapes and cassettes.

## Anglian rally

The date has been fixed for the above venture, 20th and 21st June, 1970, at the Suffolk Show Ground, Ipswich. Due to the success of the first one, it has been decided to hold a convention on Saturday afternoon, and a social and dance that evening. Sunday the Rally itself will take place. No guest speakers have as yet been appointed.

Another feature is that three awards will be made. (1) Any electronics equipment for ${ }^{\circ}$ groups up to 15 years; (2) Any electronic equipment for groups up to 19 years; (3) Any electronic equipment for any individual any age. For details, send a s.a.e. to D.W.N.Thomas, G8BVE, 9 Burlington Road, Ipswich, Suffolk.

## Eddystone light shines on...

.two new receivers. They are the EC10 Mk. 2 and the EB35 Mk. 2. The EC10 Mk. 2 is a re-styled replacement for the earlier model EC10 incorporating a number of additional features, including an integral carrier level meter, fine tuning control and desensitising facilities. Coverage is 550 kHz to 30 MHz and a low-level output is provided for tape recording. Other features include: Solid state design, $1 \%$ calibration accuracy, standby switch, size of $12 \frac{1}{2} \times 6 \frac{3}{8} \times 8 i n$. and there is a guaranteed 10 years availability of spares. Price is $£ 69$ 10s.

The EB35 Mk. 2 is a fully transistorised a.m./f.m. broadcast receiver designed for the person who requires something superior to the normal domestic set. It has a high sensitivity and wide frequency range (88$108 \mathrm{MHz}, \quad 8 \cdot 5-22 \mathrm{MHz}, \quad 3 \cdot 5-8 \cdot 5 \mathrm{MHz}$, $1 \cdot 5-3 \cdot 5 \mathrm{MHz}, \quad 550-1500 \mathrm{kHz}$ and $\quad 150$ 350 kHz ). A version is available for stereo multiplex v.h.f. broadcasts.

An internal speaker is fitted and outputs are available for tape recorder and $\mathrm{Hi}-\mathrm{Fi}$ speaker connection. The audio stages can be used independently for microphone, tape or record reproduction. Price is $£ 824 \mathrm{~s} 9 \mathrm{~d}$.

For further information, contact J. H. Roche at Imhofs Lid., 112-116 New Oxford Sireet, London. W.C.l. Tel.: 01-636 7878.


EC10 Mk2



The SGS International Group of semiconductor companies have developed a new process called Planox that enables the oxide layers on the surface of a silicon wafer to be effectively flat so that reliability is greatly enhanced and manufacturing yields improved. Applicable to both bipolar and metal-oxide-silicon devices (M.O.S) the Planox process is of particular importance in the production of M.O.S. integrated circuits where oxide thickness varies greatly and metal interconnection patterns are complex.

In a M.O.S. device the oxide layer grown on the gate regions has to be extremely thin in order to achieve low threshold voltage sensitivity while the oxide layer in the field region has to be thick to avoid spurious M.O.S. effects.

With conventional methods, the thick layer on the field region gives rise to high "steps" of oxide on the chip surface over which the metalization pattern has to be formed. Resultant sharp bends in metallization can lead to weak spots.

The Planox process eliminates this problem by removing sufficient underlying silicon to accomodate the oxide thickness so that the resultant surface is essentially flat. This is made possible by depositing a thin layer of silicon nitride on the silicon wafer. This prevents oxidation and enables selective etching with respect to silicon dioxide. The nitride film is then masked and etched to lay bare the regions where thick oxide is to be grown.

## THE WRONG DATE

In the November 1969 issue of P.W. on page 474, under the heading "Free Radio and More for Television" the date for the licence rise should read 1st April 1971.

## Rally diary notes

APRIL 19: North Midlands Mobile Rally. MAY 10: Ealing and District Amateur Radio Society Mobile Rally. JUNE 21: University College of Swansea Amateur Radio Club Annual Ra:ly, Singleton Park, Swansea. JUNE 28: Longleat Safari Mobile Rally, Longleat House, Nr. Warminster. Organised by the City and Council of Bristol RSGB Group. JULY 5: South Shields Mobile Rally. JULY 12: Worcester and District Amateur Radio Club Rally.

## They've got it taped!

"Tape Recorders: A-Z" is a book which covers every audio tape recorder in the VTR, professional, domestic and $\mathrm{Hi}-\mathrm{Fi}$ fields, currently available on the UK market.

All machines listed carry detailed specs. and most entries carry a photograph. The Domestic and Hi-Fi section contains some 250 entries with prices ranging from $£ 20$ to $£ 300$.

Two sub-sections are included in the Professional, Scientific \& Industrial Audio Tape Recorder section, one part dealing with the upper range in the "studio" class and the other with high-quality machines costing $£ 1,000$ or less.

Car tape players are dealt with as are mixers, headphones, tape and accessories.
Tape Recorders: A-Z costs $£ 1$ (price includes post and packing) and is obtainable from the publishers: A.P.A. Publishing (Catalogues) Lid., 4th. Floor, Quality House, Quality Court, Chancery Lane, London, W.C.2.

## Diode power

Philips Research Laboratories, Eindhoven, Holland announce for their silicon diodes in oscillators of the "Avalanche Transit Time" type, a continuous output of 1.75 W at a frequency of 5 GHz ( 6 cms wavelength). For a wavelength of 3 cms it is 0.5 W at 10 GHz .
The oscillators are used for supplying the microwave power in links operating in the centimetre wave range.

# FET's AND THERR USES T. SNOWBALL 

## PART 1

FIIELD EFFECT TRANSISTORS, or f.e.t.'s for short, are becoming cheaply obtainable in very great variety but unfortunately their characteristics have even wider spreads than usual. In the cheaper varieties of f.e.t. the drain current for zero bias voltage can have a spread of up to $15: 1$, and the bias voltage for cut-off can have a similar spread. Usually the more costly f.e.t.'s of up to $£ 4$ each are no better performers than their cheaper brothers, the cost usually just providing a smaller spread of parameters, and metal instead of plastic encapsulation. A simple checker will quickly give you your particular f.e.t. characteristics and enable you to get the maximum performance from the cheap f.e.t.'s now available. It is possible, of course, to allow for spreads of characteristics when designing but of necessity you will only get the performance of the worst unit.

Only two measurements are required on the normal f.e.t. to give the characteristic shown in Fig. 1. Here the drain current ( $\mathrm{I}_{\mathrm{D}}$ ) is plotted against the gate, source or bias voltage $\left(\mathrm{V}_{\mathrm{GS}}\right)$. The two points of interest on this curve are Inss (The drain current for zero bias) and $\mathbf{V}_{\mathbf{P}}$ (The gate source bias voltage for zero drain current).

Having defined $I_{D s s}$ and $V_{P}$ any other point on the curve is obtained from the equation:

$$
\begin{equation*}
I_{D}=I_{D S S}\left(1-\frac{V_{G S}}{V_{P}}\right)^{2} . \tag{1}
\end{equation*}
$$

This is an equation for a parabola with its vertex at $V_{P}$. The above form is the one to use to work out the drain current for a given value of bias.
Below is the formula to use when working out the bias for a given drain current:

$$
\begin{equation*}
\mathrm{V}_{\mathrm{GS}}=\mathrm{V}_{\mathrm{P}}\left(1-\sqrt{\frac{\mathrm{I}_{\mathrm{D}}}{\mathrm{I}_{\mathrm{DSS}}}}\right) \tag{2}
\end{equation*}
$$

The two points of interest, $I_{D S S}$ and $V_{P}$, are easy to measure in a simple test circuit as in Fig. 2. The checker which forms the subject of this article has the same basic circuit but includes switching for N channel ( +ve drain volts) and $\mathbf{P}$ channel ( - ve drain volts) types. It will also check the newer types such as insulated gate field effect transistors (i.g.f.e.t.) or metal oxide silicon transistors (m.o.s.t.) as they are sometimes called, dual gate f.e.t. and f.e.t.'s with substrate connections. The i.g.f.e.t.'s sometimes need bias voltages with the same sign as the drain supply, and these types are called enhancement types as opposed to the more normal ones which are usually junction f.e.t.'s (j.f.e.t.) called depletion types.
Sometimes $I_{D S s}$ and $V_{p}$ are not given in the manufacturer's data, but only $I_{\text {Dss }}$ and $g_{m o}$, where $g_{m}$ is the transconductance in $\mu$ mhos, or mutual conductance in $\mathrm{mA} / \mathrm{V}$ (i.e., the change in $\mathrm{I}_{\mathrm{D}}$ for a given change in $\mathrm{V}_{\mathrm{GS}}$, the slope of the characteristic at the point of use). Remembering back to school days this is obtained by differentiating equation (1) with respect to $V_{G S}$ :

$$
\begin{equation*}
\frac{\Delta I_{D}}{\Delta V_{G S}}=g_{m}=\frac{2}{V_{P}} \times I_{D S S}\left(1-\frac{V_{G S}}{V_{P}}\right) \tag{3}
\end{equation*}
$$



Fig. 1: Drain current versus Gate Source volts.

Fig. 2: Test circuit for $V_{\mathrm{p}}$ and $I_{\text {Dss }}$


Fig. 3 : Normalised curves for $I_{D}$ and $g_{M}$ versus $V_{G s}$. however, if $\mathrm{V}_{\mathrm{GS}}$ is made zero, then the $\mathrm{g}_{\mathrm{m}}$ at zero bias:

$$
\begin{equation*}
\mathrm{g}_{\mathrm{mo}}=\frac{2 \mathrm{I}_{\mathrm{DSS}}}{\mathrm{~V}_{\mathrm{P}}} \tag{4}
\end{equation*}
$$

So a simple relationship exists between $\mathrm{g}_{\mathrm{mo}}$ and $\mathrm{V}_{\mathbf{P}}$
which means that conversion from one type of specification to the other is simple. If we wish to, we can work in $\mathrm{g}_{\mathrm{m}}$ easily by using equation (4) to get $\mathrm{g}_{\mathrm{mo}}$ from the checker measurements of $I_{\text {Dss }}$ and $V_{P}$.

The mutual conductance at any other value of $I_{D}$ is given by:

$$
\begin{equation*}
\mathrm{g}_{\mathrm{m}}=\mathrm{g}_{\mathrm{mo}} \sqrt{\frac{\mathrm{I}_{\mathrm{D}}}{\frac{\mathrm{I}_{\mathrm{DSS}}}{}}} \tag{5}
\end{equation*}
$$

or at any other value of $\mathrm{V}_{\mathrm{GS}}$ from (3),

$$
\begin{equation*}
\mathrm{g}_{\mathrm{m}}=\mathrm{g}_{\mathrm{mo}}\left(1-\frac{\mathrm{V}_{\mathrm{GS}}}{\mathrm{~V}_{\mathrm{P}}}\right) . \tag{6}
\end{equation*}
$$

A simple graph which will do all the sums in equations (1), (2), (5) and (6) is shown in Fig. 3. This graph is normalised to value one, so as an example, if our measured f.e.t. had an $\mathrm{I}_{\text {Dss }}$ of 5 mA and $\mathrm{V}_{\mathrm{P}}$ of 5 V we must multiply our answers by 5 when read from Fig. 3. Shown dotted is the point where $I_{D}$ is $I_{D S S} / 4=1.25 \mathrm{~mA}$, shown as 0.25 on the graph, so going across horizontally to the $I_{D} / I_{\text {DSs }}$ curve and then reading the intercept vertically below on the $V_{P}$ scale we get the working point to be $0.5 \mathrm{~V}_{\mathrm{P}}$ or 2.5 V bias. Coming back up the vertical line to intercept the $g_{m} / g_{m o}$ curve and reading this off horizontally we get $\mathrm{g}_{\mathrm{m}}=0.5 \mathrm{~g}_{\mathrm{mo}}, \mathrm{g}_{\mathrm{mo}}$ is 2.0 from equation (4), so $g_{m}=1 \mathrm{~mA} / \mathrm{V}$ at $\mathrm{I}_{\mathrm{D}}$ of 1.25 mA and $\mathrm{V}_{\mathrm{GS}}$ of 2.5 V .

## Tester Description

The two gate potentiometers apply voltages of $\pm 15 \mathrm{~V}$ through gate series resistors of $100 \mathrm{k} \Omega$ in order to limit the gate current to a safe value when the f.e.t's are forward biased. These pots are calibrated in 1V steps with the zero voltage point accurately marked.

In the drain circuit of the f.e.t. is a 1 mA meter, which is used unshunted for $\mathrm{V}_{\mathrm{P}}$ measurements and shunted to 20 mA f.s.d. for $\mathrm{I}_{\mathrm{DSs}}$ measurement. The diode D5 across the meter is a high conductance germanium type, which although it does not interfere with the scale calibration, will start to conduct if the current through the meter exceeds 1 mA .

The other diodes D1-D4 are any silicon or germanium junction diodes, their function being to direct the current through the meter in the correct direction irrespective of whether an N or P channel f.e.t. is being tested.
The $0.001 \mu \mathrm{~F}$ capacitors on the four terminals of the f.e.t. are to inhibit oscillation, due to the length of connections, while testing high frequency types.

## Operation

In using the tester, IDSs is found by setting the $V_{G S}$ pot. to zero, and a direct reading of $I_{D S S}$ is obtained on the 20 mA scale of the meter.

In obtaining $\mathrm{V}_{\mathrm{P}}$, which has been specified as the gate source bias for zero $I_{D}$, the procedure is to switch to the $\operatorname{lmA}$ scale and increase the bias until $I_{D}$ has dropped to nearly zero.

The curve gets very flat near $\mathrm{V}_{\mathrm{P}}$ and it is difficult to estimate exactly zero $I_{D}$ so two ways are open. One is to measure $V_{P}$ at 1 per cent of $I_{D S S}$, or the one chosen in this tester, is to measure $V_{P}$ at a fixed low value of $I_{D}, 0.1 \mathrm{~mA}$ is used here and is marked as $\mathrm{V}_{\mathrm{P}}$ on the meter scale.

Having obtained $\mathrm{I}_{\mathrm{Dss}}$ and $\mathrm{V}_{\mathrm{P}}$ the formulae (1), (2), (5) and (6) or graph Fig. 3 will give all the information required to enable the use of the f.e.t. in any circuit.

## Applications

Having tested and measured various f.e.t.'s here are a few ideas on how to use them.

The eusual configurations are grounded source, which corresponds to the grounded emitter transistor case and the source follower which is similar to the emitter follower.

The equations for stage gain in the grounded source case are given for two conditions, with and without source feedback Figs. 5a and 5 b.
In Fig. 5a the gain $A=g_{m} R_{L}$
In Fig. $5 b$ the gain $A=\frac{g_{m} R_{L}}{1+g_{m} R_{S}}$.


Fig. 4: Circuit of the f.e.t. tester.
F.E.T. DATA TABLE



(D)

(E)

(F)

(6)

(a)
Fig. 6: Source follower.

Base connections reference-see data table.
To take a practical case, if we had measured an f.e.t. with $I_{\text {DSS }}=2 \mathrm{~mA}$ and $\mathrm{V}_{\mathrm{P}}=3 \mathrm{~V}$ and wanted to run it from a 9 V supply line at 0.5 mA , from equation (2) the bias needed is:

$$
3\left(1-\sqrt{\frac{0.5}{2}}\right)=1.5 \mathrm{~V}
$$

So the source resistor is $\mathrm{IR}=3 \mathrm{k} \Omega$
If the drain resistor drops 4 V its value is $8 \mathrm{k} \Omega$. The gain from (7) will be $A=g_{\mathrm{m}} \times 8$.

The value of $g_{m}$ can be got from (5) or (6) if we know $g_{\text {mo }}$ which we get from (4).

$$
g_{\mathrm{mo}}=\frac{2 \times 2}{3}=1.3 \mathrm{~mA} / \mathrm{V}
$$

$\therefore$ at $I_{D}=0.5 \mathrm{~mA}$ from (5)

$$
\mathrm{g}_{\mathrm{m}}=1.3 \sqrt{\frac{0.5}{2}}=0.65 \mathrm{~mA} / \mathrm{V}
$$

So gain is $8 \times 0.65=5.2$ Fig. 5a. But for Fig. 5b:

$$
A=\frac{0.65 \times 8}{1+(0.65 \times 3)}=\frac{5.2}{2.95}=1.75
$$

The other characteristics of this configuration are that the input impedance can be very high (equal to the input resistor in fact, which for all normal circuits can be made about $2 \mathrm{M} \Omega$ ) and the output impedance is equal to the drain load.

If the source follower is used as in Fig. 6, the gain is

$$
\begin{equation*}
\frac{g_{\mathrm{m}} \mathrm{R}_{\mathrm{s}}}{1+\mathrm{g}_{\mathrm{m}} \mathrm{R}_{\mathrm{s}}} \tag{9}
\end{equation*}
$$

Fig. 5 (a) Grounded source amplifier, (b) with source feedback.

Output impedance $=\frac{R_{S}}{1+\mathrm{g}_{\mathrm{m}} \mathrm{R}_{\mathrm{S}}}$
which for the f.e.t. considered above at 0.5 mA . $\mathrm{I}_{\mathrm{D}}$ becomes, from (9).

$$
\text { Gain }=\frac{0.65 \times 3}{1+(0.65 \times 3)}=\frac{1.95}{2.95}=0.66
$$

This is thus similar to an emitter follower except perhaps lower gain (higher $g_{m}$ f.e.t.'s improve this), the chief characteristic of this configuration is of course lower input capacitance and lower output impedance to help matching to other circuits.

From (10) the output impedance: $=$

$$
\frac{3 \mathrm{k} \Omega}{1+(0.65 \times 3)}=1 \mathrm{k} \Omega
$$

TO BE CONTINUED

BY D. BOLLEN

In this final part the alignment of the receiver is described and examples of displays are shown.

## ALIGNMENT

For best results circuit alignment should be carried out with a signal generator. Start by ensuring that the medium wave receiver or i.f. strip is working, and is tuned to a frequency of 1.6 MHz . Connect a pair of high impedance headphones, or an audio amplifier and loudspeaker to the detector diode output via Sld (see Fig. 9a). The i.f. transformer cores on the i.f. strip or in the medium wave receiver need not be accurately aligned until later. Temporarily disconnect the three wire links between the diode tuner panel and VC1-VC3, and put S1 in the "listen" position. Connect the converter output lead to the i.f. strip or receiver.

Couple a signal generator to the converter aerial terminal in series with a $470 \Omega$ carbon resistor, and inject a modulated signal at $1 \cdot 67 \mathrm{MHz}$. Fully mesh the vanes of the tuning capacitor VC1-VC3, then adjust the core of T3 to receive the signal. If more than one response is obtained while trimming T3 core, reduce the signal generator output and select the loudest response core position. Next, set the signal generator to 5 MHz , and fully open the tuning capacitor vanes. Adjust trimmer TC3 to receive the signal. Now connect a 2.5 V d.c. meter in place of the headphones or audio amplifier and repeat the above procedures using an unmodulated signal, this time peaking the meter reading by adjustment of T3 and TC3.

Set the signal generator to 1.83 MHz unmodulated and tune in the signal with the tuning capacitor; vanes set approximately $20^{\circ}$ from fully meshed. Adjust T1 and T2 cores for maximum output as indicated by the voltmeter. If necessary, reduce signal generator output if the a.g.c. voltage shown by the meter is near maximum. Set the signal generator to 4.5 MHz and tune in the signal with the tuning capacitor; vanes set approximately $15^{\circ}$ from fully unmeshed. Adjust trimmers TC1 and TC2 for maximum output. If desired, an aerial can now be connected to the converter to check for reception of signals at headphone strength.

## THE DIODE TUNER PANEL

The diode tuner panel is deliberately excluded from the early alignment procedures to avoid confusion and to simplify fault tracing. When the converter is working satisfactorily as an ordinary receiver, in conjunction with its i.f. strip, connect up the diode tuner panel to VC1-VC3, and proceed as follows. After making sure that the tuner diode d.c. bias is operational, set the signal generator to 4.5 MHz unmodulated, fully unmesh the tuning
capacitor, and peak the output meter reading by adjustment of TC3. Now set the signal generator to 4 MHz , tune in the signal with the tuning capacitor, and trim TC1 and TC2 for maximum output. The front end of the panoramic receiver will now be correctly aligned, and all that remains is to obtain a satisfactory response from the following i.f. stages.

Couple the panoramic receiver to an oscilloscope, according to Fig. 9a. Set the signal generator to 3.5 MHz unmodulated, put S 1 in the "sweep" position, VR3 at minimum magnification, and VR4 at maximum resistance, and adjust the tuning capacitor until a narrow response curve is seen at the centre of the display. Adjust VR3 until the curve is similar in width to that shown in Fig. 10a. Normally, the sharpest possible response will be required for DX listening, so trim all i.f. transformer cores, including IFT1 on the converter panel, for a steep-sided, symmetrical response curve. Avoid the flat-topped response normally used for broadcast reception.

To complete the setting up of the panoramic receiver, rotate the signal generator dial so that the curve displayed on the oscilloscope screen is moved across the display. With VR3 set for minimum magnification (full sweep bandwidth), look for any falling off in amplitude at the edges of the screen, particularly on the low frequency, left-hand side. Adjust VR4 to give a sweep of approximately $\pm 250 \mathrm{kHz}$ at the centre frequency of 3.5 MHz , as indicated by the rotation of the signal generator dial. In practice, a perfectly linear response over the full sweep bandwidth is not essential, and some falling off at the edges of the display can be tolerated. If necessary, retrim TC1 and TC2 to correct any tendency for the display to be wedge-shaped in amplitude response, but this correction should not be overdone.

Figure 10 (see overleaf) serves to give some idea of the results obtained with the prototype, but static photographs cannot do real justice to this type of panoramic display, particularly when the timebase speed is slow. Figure 10a shows a plain carrier input signal from a signal generator. A c.w. signal will look like a plain carrier being switched on and off rapidly. In the case of a.m., a modulation ripple is superimposed on the response curve, and when the ripple peaks touch the trace baseline, this corresponds to $100 \%$ modulation. Speech clipping and excessive modulation are readily apparent, as is unintentional frequency modulation, which causes the response curve to shift sideways. As might be expected, an s.s.b. signal lacks a response curve during breaks in modulation, and manifests itself merely as a rising and falling modulation ripple.

Figure 10 b depicts the 80 metre band on a quiet morning in the middle of the week. An amateur a.m. signal occupies the centre of the display, with another station on the left, and a frequency marker curve from a signal generator on the right. In Fig.
—continued on page 872


A SIGNAL GENERATOR INPUT PRODUCING
RECEIVER RESPONSE CURVE



# ABODISHELE speaker 

THE 'bookshelf' size loudspeaker enclosure is the choice of many high fidelity listeners despite its unsuitability for sound reproduction. The function of a speaker enclosure is to contain the sound disturbance emitted from the back of the speaker cone and prevent it interfering destructively with the useful forward sound. The oft-quoted 'ideal' speaker mounting is in a hole in a wall between two large rooms. Here the sound pressures can escape from both sides of the speaker without mutual interference, but this arrangement is rarely practical and factors such as wall thickness have degrading effects.
The wavelength of the lowest audio frequencies required in a good quality system may be as long as 30 ft . (frequencies down to around 30 Hz ). Practical speaker enclosures are considerably smaller than this and therefore sound congestion arises behind the speaker unit at low frequencies. The inescapable result is that the useful sound output at low frequencies is reduced. One trick is to provide a small port in the enclosure through which rear emitted sound can escape. It will of course interfere with the forward sound emission but if the round trip it has taken from the rear of the speaker is at least a quarter of the sound wavelength, serious cancellation will not occur. Thus congestion in the enclosure is reduced and bass interference is not serious down to a frequency determined by the enclosure dimensions; this is the bass reflex cabinet. Such a cabinet needs to be fairly large but gives excellent results. There are many standard designs for these which are generally available from the speaker manafacturers.
The infinite baffle enclosure is a perfectly sealed box. The speaker works against the volume of air sealed behind it, alternately compressing and rarifying it. The efficiency of the speaker is reduced but there is no interference between forward and rearward emission. The cabinet must be strong enough to contain high internal sound pressures without resonating. A large infinite baffle has been described by the author in "Practical Wireless" Oct. 1967 (Economical Speaker Enclosure).

The speaker manufacturers put much research into getting good sound from small enclosures. The usual result is to use an infinite baffle enclosure and concentrate on designing the most efficient bass speaker possible. The springiness of the trapped air raises the resonant frequency of the speaker so this must be low to start with. The bass speakers used in commercial bookshelf enclosures have very low resonant frequencies for their small size. They also have large, powerful magnets and permit large cone excursions for better efficiency. These speakers are

not often available as separate units.
The loudspeaker enclosure to be described is a two way unit i.e.: it contains a 'woofer' speaker for low and midrange frequencies and a tweeter for high frequencies. The speaker units specified are fairly new and have been found to give together excellent


Fig. 1: The circuit of the cross-over network. The capacitor is a non-polarized electrolytic type.
coverage of the audio range. The enclosure is truly 'bookshelf' size as the frontal area is the same as a foolscap sheet ( $13 \mathrm{in} . \times 8 \mathrm{in}$.) and depth is $8+\mathrm{in}$. overall. A series L-C crossover network is used and is shown in Fig. 1. Frequencies above 3 kHz appear across $L$ and are fed to the tweeter. Frequencies


Fig. 2 : The assembled enclosure.


Fig. 3: Mounting and wiring of the speakers on the baffle board.
below 3 kHz appear across C and are fed to the woofer. The crossover network can be made up; a non-polarized electrolytic capacitor must be used for C. Messrs. Wharfedale can supply the two components through a dealer. It is easiest to use the ready made crossover unit specified in the parts list. This, like the speaker units, is part of the Eagle product range and can be supplied by any electrical dealer.

The woofer is a $6 \frac{1}{2}$ in. 11,000 gauss flux density unit that is capable of full range reproduction alone. However its response curve is very jagged above 3 kHz where cone resonances and harsh reproduction occur. We therefore use only the smooth response from 35 Hz to 3 kHz , the excellent lower limit can be achieved with the help of some bass boost at the amplifier.

The tweeter is a 3 in . horn cone type and provides a satisfactory response up to 16 kHz and is only 5 dB down at 20 kHz . The quoted ratings of both woofer and tweeter units is 10 W and response curves are supplied with both units. When the units are mounted in a well lagged enclosure this rating seems quite realistic and this input will give much more volume than will normally be required, thus there is good power capacity to handle strong transients such as percussive sounds. Any good valve or transistor amplifier that will provide at least 5 W into $15 \Omega$ will suffice.

The unusual feature of the loudspeaker enclosure is the rear porting. The cabinet interior is heavily damped and the amount of wadding can be adjusted to vary the effect of the ports. If the ports are blocked by a layer or two of wadding material, the enclosure approximates to an infinite baffle. Alternatively, it is often possible to take advantage of the surroundings by using them to absorb the rear radiation from the ports. By using less wadding and allowing sound to escape from the rear, the effective volume of the enclosure is increased and bass response is improved.

## Construction

The cabinet is built from six pieces of $\frac{1}{8} \mathrm{in}$. plywood and can be stained, painted, varnished or covered as desired. The joints between the top, bottom and sides are mitred at $45^{\circ}$ for good appearance and rigidity. The mitred edges must be cut carefully for a neat fit. Two circular cutouts are required in the baffle board. The two speaker units are screwed to the front of the baffle board for best sound dispersion and avoidance of tunnel effects. Ensure that there is an airtight seal between the two speaker frames and the baffle board. Do not screw down the woofer unit too tightly, or to a warped baffle board, as the pressed steel frame will


Fig. 4: The cutting details and dimensions.


The wadding is adjusted before the top is fixed in place.

(a)

(b)


Fig. 5: Alternative wadding arrangements and poss/ble ways of taking advantage of surroundings. a) Infintte baffle. Wadding blocks rear ports and prevents rear radiation. b) Literal bookshelf mounting using space behind books to absorb rear radlation. c) Use of heavy curtains to absorb rear radlation.


The partially assembled enclosure.
be distorted and the precise cone centering ruined. The front edges of the baffle board must be built up by about $\frac{1}{4} \mathrm{in}$. so that the grill cloth will stretch flat across the speakers. Any convenient material such as scrap wood, polystyrene, foam rubber or cardboard can be glued in strips around the edges of the baffle board to provide this packing.

The crossover unit just fits on the back of the baffle board if the solder tags are bent upward. The unit's metal case serves no purpose and wastes valuable cubic inches; it should be removed by extracting the two fixing rivets. The fibre base carrying the


The rear radiation ports.

## components list

## Mechanical

$\frac{5}{5} \mathrm{in}$. plywood as shown.
12 1in. fixing screws.
$10 \frac{\underset{y}{s} i n . ~ s p e a k e r ~ a n d ~ c r o s s-o v e r ~ m o u n t i n g ~ s c r e w s . ~}{\text { sen }}$
Carpet felt, $\frac{7}{2} \mathrm{in}$. thick-1 square yard. See text.
Rubber feet
Glue.
'Tygan' grille cloth, $15 \mathrm{in} . \times 10 \mathrm{in}$.
Electrical
Eagle FR65 $6 \frac{1}{2} \mathrm{in}$. loudspeaker.
Eagle CT10 tweeter.
Eagle CN216 $16 \Omega$ cross-over.
Connecting wire.
Terminals, if required.
components is then screwed to the baffle board. The speakers are wired to the crossover as shown in Figs. 1 and 3.
The author used $\frac{1}{2}$ in. wool waste carpet felt material obtained from a carpet dealer for wadding. This material is preferable to fibreglass as there is less chance of particles finding their way into the speakers. Plastic foam is useless for this purpose. A layer of wadding is glued to the inside of the top and bottom pieces. The cabinet is now screwed and glued together and inspected for airtightness. Twin core cable can be brought out through one of the ports for connection to the amplifier or any desired form of sockets or terminals used for connections. Leave the top of the cabinet unglued so that the internal wadding can be adjusted. The arrangement of this is mainly experimental. Start with the rear ports completely blocked by two layers of wadding (infinite baffle). Then see if bass response can be improved by readjusting and taking advantage of the surroundings as suggested. Do not stuff too much wadding into the cabinet especially immediately behind the woofer or midrange response will suffer.

Fit rubber feet to the cabinet which can be-stood horizontally or vertically. Two of these enclosures fed from a $10+10 \mathrm{~W}$ stereo amplifier provide the author with excellent stereo listening. The enclosures are used horizontally and are placed 7 ft . apart. There is a slight buzz from the woofer on some sounds but it is only audible a few inches away from the cone and does not detract from the reproduction. It apparently originates in the small 'whizzer' high frequency cone. As the woofer is not used for high frequencies, this additional cone could probably be cut away but the author has not cared to risk it.


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[^1][^2]
# praticially wireless commentary by ILIITII 

IT is not even Spring and already I am being threatened. Vague references to 'How much nicer that room would be for Jane.' Now that she is at college, she wants more space for her books. Colour schemes are being compared, furnishing books pored over, the 'homey' magazines explored. Like a squatting hippy facing the Establishment, Henry is in danger of eviction.

Main weapon in the female armoury is the accusation that my den is untidy.

Women can never understand that a workshop, per se, is untidy. That clutter of cables-all made for special hook-ups, and hung where they are instantly to hand. You never know when the $F$ layer may shift and someone likée Bouvet Island come through weakly, crying out to be recorded, when the only machine switched on is the Humbox Rattler I am repairing for a neighbour. And this uses an odd plug-so I must have a jumper lead ready. Eavesdropping is half the fun of $D X$.

Henry has the added crime of storing piles of papers. Magazines going back to Caxton, torn columns from newspapers (well, she is always borrowing my scissors, apparently to trim the dog. No harm in that? You haven't seen our dog!) My


You haven't seen our dog.
reference books are downstairsin the several bookcases that catch visitors' first glances. I am going to start a campaign for Newnes, Butterworth, Odhams, etc., to bring out special engineers' editions in tattered covers.

My heart went out to Frank Young, guesting a CB article for me in the November 1969 issue of Practical Wireless.
© . . then she wanted our sanctum door left open. Then she began hanging out in there. Then she said the place was untidy. Then, Lord help us, she cleaned it up.'

Note those doom-laden words, she cleaned it up. Henry cannot count the hours he has spent searching for the crimp-ended angle cutters, or an unrepeatable service manual that Her Ladyship has 'put safe.' I found my latest Heathkit catalogue among a pile of colour supplements. Filed there it seems, because it, too, has a pretty cover.

It has some pretty things inside it, also. Have you seen the latest line in test gear? Henry is aching to build himself an oscilloscope. His baby Cossor and old OS-3 are no longer adequate for the tests he has to make, Mr. Michaelis' projects seem much too complicated for the time available, off-the-peg models are beyond my means.

It will do most jobs, except perhaps some of the colour-TV or VTR tests that crop up. In conjunction with the S-3U dualtrace switch and the new IG-18 Sine-Square wave generator, which can supply both waveforms simultaneously, it would form the basis of a newlyplanned workshop. Henry might be tempted to listen to the subversive hints about uprooting.

But have you seen the latest range? Gone the functional look. We are in the space-age now. If I completed those projects, they would end up in the kitchen with

"That's how I left itl"
the Mark VII All-Automatic Stove that FPY described. I wonder if Mr. Perriam would let me order a Heathkit instrument minus its case?

That little subterfuge of an unboxed chassis is the only means whereby Henry has retained the use of his Armstrong tuneramplifier, which performs far better than any of the several radios around the house. All those glowing valves, that surrealistic dial cord, those trailing wires-a deterrent to the tidierupper.

I am reminded of Colin Reid, whose column in the Oct. 6 Daily Mail sparked off a pulse of sympathy. He began with a lovely tale of an actress whose flat was burgled and who led the investigating copper around. He opened the bedroom door and said: 'Whew! They've made a right mess in here, Miss.'

She was wounded. She looked at the drawers pulled open, clothes scattered across the bed, the dressing table a shambles, tights flung across the room, scripts strewn over the floor, and explained:
'No, that's how I left it!'
Colin sympathised, with a quick mental vision of his own den 'where the desk is littered, drawers tilt permanently open and papers, letters and bills are filed on the floor and window ledges for easy reference!'

## AN HEAD for the BSR TD2 A. OLIVER



The TD2 Tape deck used in a home constructed tape recorder.


$$
\begin{aligned}
& \text { With } 1 / 8^{4} \text { drill to partly } \\
& \text { recess screw head } 1 / 32
\end{aligned}
$$



Flg. 1: The constructlonal details for fitting an extra tape head.

ALARGE number of less expensive tape recorders use the TD2 tape deck, extra interest and use can be made by fitting a third head.
To do this, first remove the two push-on operating knobs, then the top-deck cover. (This is fixed by three screws.) The next operation must be done in the order given if the head alignment is to be maintained. Remove the outer fixing screw from the record-replay head base, in its place screw a one-inch length of 6BA brass stud, run a 6BA brass nut down to refix the base. Remove the inner fixing screw on the same head and countersink the hole to take a 6BA screw. The drilling requires only light pressure, the base being made of alloy. Refix the base with a brass countersunk-head screw.

Before altering the erase head, try the tape recorder with a pre-recorded tape to make sure the head alignment is still in order. An easy way to check this is to see that the tape is passing in the same wear groove on the head. A slight adjustment on the screw at one side and the nut at the other side will easily correct any error that is apparent. When satisfied that the playback is correct alter the fixing screws in the erase head base, the 6BA stud on the outside and the countersunk screw on the inside. Test the recorder again to ensure the erase head is in order.

The head to be fitted is the BSR type MN1 55-2R5 which is a half track head, standard fitting to the TD2 deck. When obtained the head is mounted into a base, it is removed from this and fitted with the same screws to a brass strip measuring $2 \frac{1}{8} \mathrm{in}$. $\times$ $\frac{1}{2}$ in. $\times \frac{1}{16}$ in. as shown in Fig. 1. This is now fitted as shown. In the authors case it was found that two washers about 0.008 in . thick were needed to pack the head to give the correct alignment.

All that remains now is the wiring. This must be done quickly with a hot iron, not dwelling too long on the head terminals. Connect a piece of wire between the terminals shown, remove the wires from the original head and solder to the same terminals on the new head. Now connect a piece of twin screened cable on the original head and bring this out to a suitable socket on the tape-deck panel.

A pressure pad was made by glueing a piece of soft felt to a strip of springy-brass, this in turn being glued or soldered to the existing pressure pad strip on the tape-deck as shown in Fig. 1.

The extra head can be used for monitoring whilst recording, repetitive echo can be given to recordings by feeding the outputs from the new head into the mike input of the tape recorder whilst recording an echo effect can be given to pre-recorded tapes by feeding the output of the new head into a suitable amplifier, these effects can be varied by moving the new head nearer to, or further away from the original head.


The serious amateur should never be without this compre－ hensive price list and guide to semico－lductors and electronic components from RCA，IR，SGS， Emihus，Semitron，Keyswitch，Plessey， Morganite，Litesold and others（to－ gether with manufacturers＇application data）which you can buy direct from us at manufacturers＇prices e．g．IN9141／3d． $\square$ IN916 1／11d．$\square$ 2N697 4／5d．$\square$ 2N706 2／3d．$\square$ 2N706A 2／9d．$\square 2 N 929$ 5／8d． $\square 2 N 1613$ 4／8d．$\square 2 N 3011$ 9／1d．$\square 2 N 3053$ 6／2d．$\square$ 2N3055 15／9d．$\square$ 3N140 15／3d．$\square$ BFY50 4／8d．$\square$ BFY51 3／9d．$\square$ BSY27 18／．$\square$ BSY95A 3／3d．$\square$ C407 4／6d．$\square$ CA3012 18／3d．$\square$ СА3014 25／6d．$\square$ СА3020 25／9d． OA200 1／9d．$\square$ OA202 1／11d．

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EDWARD (EDDIE) STARTZ of Radio Nederland's Happy Station programme has been a shortwave personality for nearly twice as long as I have been alive, which makes my task of writing an article on the occasion of his retirement a very difficult one.
I will always remember the first time I heard a shontwave broadoast; that fateful Sunday morning when. more by accident than design, I tuned our old domestic receiver to 6020 and heard Eddie's voice. I say fateful because that Sunday morning made me a shortwave listener for life!
1 am sure that every reader of this column has heard Eddie at some time in the past and on your behalf I send him the very best wishes for his retirement with thanks for the years of enioyment and entertainment that he has given us. Let me conclude by saying that I hope his successor, Tom Meyer, will find as big a place in the hearts of shortwave listeners as Eddie did.
The address of the World DX Club which I gave in the December 1969 issue was incorrect and 1 apologise to Alan Thompson, former-President of WDXC, for any inconvenience this may have caused. The correct address is: 11 Wesley Grove, Portsmouth, PO3 SER.

## Reader's logs and news

John W. Smith, of Anstruther, Fife owns an Eddystone 840 C and a Joystick antenna and a.t.u. which enabled him to hear the Broadcasting Service of the Kingdom of Saudi Arabia at 1900 on 11855 (SINPO 33443) and enjoy their English music programme.

John also contributed a news item which says that Radio Havana, Cuba, is using 17705 for its English language transmissions to Northern Europe from 2110 to 2140.

Bob Loukes, of Richmond, also mentions the Saudi Arabian station adding the information that English is broadcast from 1700 to 2000 and French at 09001100 and $2000-2200$. He heard the broadcast using an Eddystone EC10 with a Joystick and a.t.u.

Richard Royall. of London, E.14, has the following equipment: 20 year old, four-valve domestic superhet. (Pye 19a); a 30 watt p.a. amplifier and a 30 metre sloping wire, despite these difficulties he managed to get: Radio Baghdad on 6095 at 1930 (good signal); Radio Damascus on 9660 at 2030: Radio Ghana on 9545 at 2200 (fair signal); HCJB, Ecuador, on 6050 at 0830 (poor signal); WINB at 1700-1900 on 17820 and 1900-2100 on 11795 and finally, RSA, South Africa on 17745 from 1800 to 1850.

## Times in GMT Frequences in kHz

## THE BROADCAST BANDS Christopher Danpure

Frank Plumb, of Londonderry, contributed several news items: Deutsche Welle transmits in English to North America on 9605, 11795 and 15245 at 1900-1910; Radio Canada transmits to Europe on 17820, 15325 and 11720 at 2115-2152 daily and Radio Nederland (weekdays only) transmits to Europe on 6085 and 6020 from 2000 to 2120.
Many thanks to this month's contributors, I hope to receive many more reports by the 17 th. of the month to 58 Kensington Gardens, Ilford, Essex.

## Africa

Malawi: The 100 kW transmitter of Radio Malawi should start operation in early 1970, until it does the schedule of the station is: 0300 ( 0400 on Sunday) to 2110 ( 2310 on Saturday) on frequencies of 3380 ( 20 kW ) and 5995 ( $10 \mathrm{kW)}$.

## Europe

Andorra: Radio Rupert is a new station which is due to start transmissions in English from Andorra in the early part of 1970 . I understand that the programming will be similar to that used by Radio Luxembourg but do not know whether the station will use mediumwave, shortwave or both.

## Oceania

Australia: Rudio Australia has moved its morning transmission to North America to one hour later, i.e., 1215 on 9580 and 11710. The evening transmission is still at 0100 on 15170, 17775 and 21740.

## South America

Mexico: Radio Mexico (first reported last month) can now be heard on the new frequency of 9535 which you probably recognise as the frequency of SBC, Berne, Switzerland. The Mexican can be heard from 0430 to 0545 whilst Berne is off the air.

Panama: HP5B, Radio Miramar, Apt. 4402, Panama 7, is a new shortwave station. It operates from 1030 to 0330 on a frequency of 6030 .

Venezuela: Radio Merida is a new station operating as YVTR on the frequency of 9720 with a power of 1 kW . The address for reports is Radio Merida, Avenida Principal, Merida, Venezuela.
Well we are now right in the middle of the winter and the sunspot number has been falling steadily for some months which has led to good reception on the tropical bands. There must be many l.f. specialists who have excellent logs so how about sending them along for us all to have a look at.

73 and good DX until the next time.

## THE AMATEUR BANDS

 David Gibson, G3JDGTHINK of all that lovely DX you missed last year just because you couldn't read c.w. How about making this a New Years resolution? Just imagine, lovely narrow selectivity cutting out all that QRM, and the feverish logging of exotic callsigns to boot.

Another resolution worth thinking about is to listen on eighty and forty before going on to the "easy" DX bands. If you are licenced, how about a serious assault on t.v.i. this year so that you can enjoy your hobby all the time, instead of sneaking out a whiff of r.f. when the telly isn't on?
To all those with nice, shiny, commercial gear, how about a constructional project this year. Aerial enthusiasts might make an antenna impedance bridge, then they can be sure just what impedance the poor old pi-tank is struggling desperately to match. For the more daring, a grid dip oscillator or one of the many transistor variants is an extremely useful item.
If you haven't got a ticket yet, what about a crystal marker. You can find plenty of circuitry for both valve and transistor frequency markers and you can give a far better report if you are able to specify a reasonably accurate frequency.
For the poor but practical, send 9d. to the RSGB and receive your very own countries list. The prefixes change so much these days that it's always worth getting a list at the beginning of each year just to see what all those funny callsigns are which keep popping up on twenty metres.
Many people write in asking what is the best aerial, a question which is impossible to answer. Probably most s.w.l's use a piece of wire, usually as long a piece as they can get out. For those who are in this category an aerial tuner unit (a.t.u.) is highly recommended.

Spies have written in to say that Marion Island is on twenty and another island to listen for is St Brandon Is., also on twenty. If any sleuths hear of anything worth while, please drop me a line but mention the times and, if 'possible, the frequencies when the DX stations are about.

Don't forget that the long cold nights favour DX on the lower frequency bands and eighty is well worth a listen. Remember that some countries can work from 3.5 MHz right up to 4 MHz , so don't stop spinning the dial at $3 \cdot 8$.

Fifteen metres should continue to provide some good DX. Best times to listen, according to the Gibby crystal ball, are 0800 to 1800 . Similar remarks for listening times apply to ten metres.

Trevor Southern (Sussex), reports many G stations on top band: Incidentally, 160 is always worth a listen since there are nearly always a number of local stations on, and many interesting (and sometimes hilarious) discussions take place. Unbelievers of DX on 80 should prepare to weep. Those who only hear G stations and Europeans should reconnect the antenna.
J. Jackson (Leeds), has a TCS 13 receiver and "A length of wire thrown round the loft." Goodies heard roaming the s.s.b. trail on 80 include; CO2DC, CR4BC, EA3OF, EA4JL, HK3NO, HP1JC, HP9FC MM/EA9 (fancy sending that on c.w.), K3UZE,

OE1JPA, OY9LV, VE1ART, VE2LD, VE3CBG, VE8RX, VOIFX, W1FRR, W4OUK, WA4WQB, WB2YY1, 3Z3ATI, 3Z5CK, 3Z7AWA, 3Z9BLF.
James advises that the best times for a listen on eighty are 2400 to early morning. He also heard that the 3 Z prefix for Poland went in January so it looks like we are back to the good old SP's. James says that SM7CRJ is a YL named Britt. further afield Bill logged; VE, VO and 4X4.
W. Waldron (Monmouthshire) sends a log of EU's logged in the 50 kHz from 3750 to 3800 . From further afield Bill logged; VE, VO, and 4X4 plus a

Allan Horne (Middlesex), CR70A, PR30X and 40 ft . indoor wire sends in a list of c.w. stations heard on 40. These include DM, DJ, UA1, UA3, and OK. Come on you superhet types, you can't let a t.r.f. get away with that, or can you?
If you are allergic to RA1 receivers, and PR30 preselectors bring you out in spots then be spotty and get some DX. A. Crooks (Leicester), has both (but not the spots!), and coupled into a 45 fft . end fed logged; CR4BC (Cape Verdi Is.), CT2AS, FG7XT (Guadeloupe), PY7AUT and ZS5KS on ten metres. On fifteen, Andy hooked; EA8GK, HPIRC. HR1KAS, PY1BIM, VE3OSC, VK2AVT, VK4TT, VK7GK, W0JW, ZL4PD, ZS6VE. Twenty raised; CR6FP, KH6BB, OH2AJ/AM on flight from Santa Cruz to Helsinki, PY7BDY, SVICD, VOIFX, ZS5FC, 9Q5EP.
M. Needham (Kent), has a B40 receiver and the antenna is claimed to be a "Piece of wet string" some 70ft. long. (What gauge OM?) According to the receiver, sigs on fifteen arrived from; $\mathrm{F} 5 \mathrm{HN} /$ P/W4, JAIWZV, JA6MVO, KP4DCR, KR6KV, VE3ELP, VE4ZX, VP9MI, 9G1BY.

A quick, but damp, dangle on twenty revealed; VE1AJG, VK2BKM, VK4SD, VK5MS, VK5QX, W8ODV, ZC4AK, ZL1AV, ZL2APT, ZL3SE, ZM2QK. Ten metres proved fruitful with squirts of r.f. from: SV0WA, K8AQS, UA6XA, VE3EWY, W8LBI, ZC4JW, ZE1CX, ZE2JA, ZS60S.
D. Yearman (Renfrewshire), Electroniques front end feeding an HRO and a half size G5RV antenna, reports these sigs on twenty: CN8AD, CT1BT, JA4OI, K1MVT/MM/VR2, K2IXT/M/CT1, KG4AN, MP4TCE, OX2TX, SV0WX, TU2CS, VK2FU, VK3FZ, VK7CW, W4CHH/P4, W4ZDW/MM/VR2, WA4DOU/MM, ZS2PX, ZS6XL, ZL1AV, ZL2AUW. ZL2US, 3V8AL, 5N2AAJ, 5R8DB, 6W8DY.
M. Williams (Lincs.), tells of a European/Canadian net on Friday nights. Time to QRX is 2230BST and frequency around 3.8 MHz . Maurice has a 9R59DE and reports good sigs on ten metres, mostly from American stations plus a 5 and 9 from HP9FC/MM/ operating off the West coast of Africa.
I think that two metres is just a myth. All you can hear is the spotty-faced G8 in the next block at 5 and 5 ! Once you've worked both local stations you're dead. Don't agree? Well, how about proving me wrong with some juicy logs. Get those eight-over-eight mechanical monsters swivelling and see what you can sniff out.

Happenings of the month scribbled down in my diary include: February $7-8$ th., 144 MHz contest; $7-8$ th., ARRL phone contest; $14-15$ th., 1.8 MHz c.w. contest; 21-22nd., ARRL c.w. contest; 23rd., 432 MHz contest; 28-March 1st., French phone contest; 7-8th., March, ARRL phone contest (second part).
Address for logs is 5, Edward Close, St. Albans, Herts. and must arrive bv the 18th. of the month.

## VERSATILE POWER SUPPLY STABILISER

THE circuit, see Fig 1, takes in a "rough" d.c. input Vi of variable d.c. level and high a.c. ripple and converts it to a stable d.c. output. Vo, having low ripple. The rough d.c. input would normally be provided by a conventional power supply unit with choke or capacitor input filter. Basically using only seven components, the circuit described gives an improvement in a.c. ripple and d.c. stability of the order of 500 times, so that with typical values, a final output of $\pm 10$ to 100 millivolts d.c. stability and 1 to 5 millivolts peak to peak a.c. ripple should be attained. The output current can be from milliamps up to several amps and a wide open choice of component types is possible.

## THEORY OF OPERATION

Referring to Fig. 1, current through $\operatorname{Tr} 3$ establishes an "intermediate" voltage, Vx. This value is maintained by the amplifier containing all three transistors and its level is defined by zener diodes $\mathrm{Z1}$ and $\mathrm{Z2}$. In the steady state, the base input voltages of the long-tailed pair Tr 1 and Tr 2 are equal. The voltage at Trl base is zener voltage $\mathrm{Z1}$ (VZ1) and the voltage at Tr 2 base is Vx minus zener voltage Z 2 (VZ2) so that Vx equals VZ1 + VZ2. In this case, provided R2 is appropriately chosen, the collector currents of $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$ are reasonably balanced and the current in $\operatorname{Tr} 3$ base is just sufficient to produce a current from Vi to maintain Vx at its correct value. Now suppose that for some reason Vx rises, the voltage VZ2 remains substantially constant so that Tr 2 base voltage rises, Tr 2 emitter and hence Tr 1 emitter voltage rises. Tr 1 collector current falls since $\operatorname{Trl}$ base voltage is already constant at VZ1. Tr3 base current is thus reduced, its collector current falls, and $V \mathbf{x}$ is allowed to fall back to its original value. The voltage $\mathbf{V x}$ is therefore substantially stabilised with regard to Vi.
Now consider the base of Tr 2 , which is regarded as the circuit output. Provided no transistors are saturated or turned off, Vo must equal (VZ1 $\pm$ difference in Vbe drops of Tr 1 and Tr 2 ). But VZ1 is fairly constant since its current drive is taken via R1 from Vx, already seen to be stable, and changes in (Vbe1-Vbe2) will be small provided the design allows for a fairly low and roughly equal current in these collectors. Thus, the output Vo is highly stable and is almost exactly equal to VZ1. Note that both zeners are driven from stabilised current sources giving very low voltage variation.

## DESIGN NOTES

The circuit of Fig. 1 deliberately gives no component values, these can be chosen to suit many different requirements as outlined below:


Fig. 1: The skeleton circuit of the power supply.
Transistors. As drawn the circuit is negative earth and requires NPN transistors for $\mathrm{Tr} 1, \mathrm{Tr} 2$, with Tr 3 PNP. If an NPN type is desired as the power transistor $\operatorname{Tr} 3$, then Tr 1 and Tr 2 will of course be PNP, the zener polarities should be reversed, and earth will be positive.
Transistors may be silicon or germanium, but Tr 1 and Tr 2 should be of the same type. These last may be a matched pair for highest stability (although not critical), and are low power, but preferably fairly high gain. Their collector voltage rating must exceed Vi.

The power rating of $\operatorname{Tr} 3$ should exceed $(\mathrm{Vi}-\mathrm{Vx}) \times$ (output current + R1 current), although this may be greatly reduced by connecting a suitable resistor in the collector lead.
As suggested below, Trl collector current may be of the order of 1 mA . This must produce at least the full output current through Tr 3 . If the current gain of this transistor is insufficient, it may be increased by connecting a driver transistor Tr4, collector to Vx, base to Trl collector, emitter to $\operatorname{Tr} 3$ base (having disconnected the latter!). Almost 'any transistor types can be used provided the above requirements are met, a few suggestions follow:
Trl and Tr2 PNP 2N3702 or 2N3703
NPN 2N3705 or BC183L or 2N2926 Tr3 NPN 2N3055 (up to 110 watts on good heat sink) or as for Tr1 and Tr2 (up to $\ddagger$ watt)

Zener diodes. Both are low power, Z 1 is chosen equal to desired output voltage Vo. Z 2 is any value. provided not below $\mathrm{Vi}-\mathrm{Vo}-1 \mathrm{~V}$ and not above half Vo (preferably).

Resistor R1. Should give a normal current around 5 mA or as appropriate for chosen Zener Z1.

Resistor R2. The normal output cumrent divided by gain of $\operatorname{Tr} 3$ (and that of $\operatorname{Tr} 4$ if used) gives half the current to be allowed for-this should be of .the order of 1 milliamp. The resistor value can then be'calculated since the voltage is close to Vo.

Low output currents. If output current can be low or zero, a load resistor is needed across the output sufficient to maintain, say, 5 milliamps through $\mathrm{Z} 2+$ extra (say 20 milliamps ) to avoid cutting off the stabiliser loop.

## GENERAL CONSIDERATIONS

1. The circuit is intrinsically safe against indefinite short-circuit output conditions since in this case Tr l and $\operatorname{Tr} 2$ and thus $\operatorname{Tr} 3$ are turned off. Partial overload may be protected against by suitable Tr 3 collector resistor.
2. It is intereseting to note that if all the transistors are initially turned off, then there is no reason for them to turn on. In normal use, these may require a resistor between Vi and Vx to give at least half a volt to turn on Trl. Alternatively, the whole círcuit can be regarded as a bi-stable whose "on" level is the stable output Vo and "off" level zero. For such an application, trigger pulses might be applied to any or all transistor bases. Alternatively, a momentary short circuit of Vo could be allowed to leave the output permanently zero until reset.
3. It will' be clear that Vx (Fig. 1) provides a second stabilised output although not quite so good. If this is used as such, it will have a current capability comparable with Vo, but any ripple imposed on it will be reflected in Vo.

## WATCH OUT FOR THE

## PRACTICAL TELEVISION

## SINGLE-STANDARD 625-LINE TELEVISION RECEIVER

Constructional details commencing in the March issue, on sale February 20th.

## CORRIGENDA

Semiconductor Technology - Two errors occurred in Part 1 of this series, published in the May 1969 issue. First the negative charge on an electron is $48 \times 10^{-10}$ e.s.u. and not $1.6 \times 1^{-12}$ e.s.u. (which is in fact the numerical value of leV expressed in ergs). Secondly regarding the isotopes of hydrogen, deuterium has one and tritium two neutrons: hydrogen itself has none.
Beginners Portable Receiver-January 1970 issue, page 693. Tr6 is incorrectly drawn in both Figs. 1 and 2. For correct operation the emitter and collector connections must be transposed.
I.C. of the Month-February 1970. It has been suggested that the Weyrad RA2W ferrite rod aerial may be used in this design. The long wave winding should be ignored or alternatively removed from the ferrite rod.

## COLUMN



THE new high power station in Calcutta is coming in very well in the afternoons and should provide newcomers to MW DXing with the opportunity to hear their first Asiatic. The new station is on 1130 kHz and has a programme in English daily, between 1530 and 1600 hrs GMT. The writer has logged Calcutta several times recently using a loop aerial. Look for the burble on 1133 kHz and Calcutta will be found on the l.f. side of it. Wait for a minute or two if you do not hear it at first, although the signal is strong it does suffer from fading. Peking on 1000 kHz is another prominent signal when the path is open but in this case the programming is in Chinese.

Last October a DXer resident in Hawaii logged a number of European m.w. stations on two successive nights. The great circle path to Hawaii lies right across the north magnetic pole and it was previously thought that m.w. signals would be absorbed in this region making DX between Hawaii and the UK impossible. A new Alaskan station, KYAK, has now come on the air on 650 kHz , its programming is 'country and western' style and it broadcasts for 20 hours a day with a power of 25 kW . KYAK is the most powerful m.w. station in Alaska and it ought to be audible in the UK. After midnight, on a night when North American DX is really good, would be the time to try for this station. Others that might be heard on 650 kHz are YVLH Venezuala (in Spanish), Godhavn Greenland (sometimes in English) and WSM Nashville Tennessee. WSM is logged occasionally and since its programming too is country and western in the evenings, it is essential that a clear identification be had of the Alaskan to be sure of it. The writer would be glad to hear from any DXer who manages a 'first' from this difficult country.

The band has been quite lively this winter and the following have been logged recently by the writer during the period 2300 hrs to 0100 hrs GMT. On 590 kHz VOCM, St John's, Newfoundland, Tenerife on 620, Canary Islands, YVLH (650) in Spanish, Radio Giradot, Maracay, Venezuala, WNBC (660) in New York City, CBF (690) Montreal (CBC French Network), CJOX (710) Grand Bank Nfld., WJR (760) Detroit, Michigan, Dakar (764) Senegal (in French), Radio Caribbean (840) on the island of St Lucia (in French), WHDH (850) Boston, CJON (930) St John's Nfld., CBM Montreal (940) (English Network), CKBW Bridgewater, Nova Scotia on 1000, WINS (1010) NYC. WBZ, Radio 103, Boston on 1030, CBA (1070) Moncton, N.B., LR 1 (1070) Radio el Mundo, Buenos Aires, Argentina, WBAL (1090) Baltimore, WBT, Charlotte, North Carolina on 1110 , WOWO (1190) Fort Wayne, Indiana, ZBMI (1235) Bermuda (American style programming), PJD2 (1295) St Maartin, Netherlands Antilles, with programmes in English and Dutch, Conakry (1403) Guinea (in French). These are only a selection of what can be heard when conditions are favourable.

## Charles Molloy

# P.W. GUIDE TO Cox Poxicile PART 15 

## Silicon Controlled Rectifier (s.c.r.) or Thyristor

The thyristor or s.c.r. is a four-layer, three-junction structure compounded of alternate p - and n -type semiconductor material and is invariably made from silicon wafers. The circuit symbols commonly used are shown in Fig. 20 and the B.S. preferred symbol is indicated.


Fig. 20: Thyristor symbols.
The basic structure is illustrated in Fig. 21(a) with the structure split to show the two transistor equivalent structures in Fig. 21(b). The stable operating conditions of the thyristor are best understood by referring to the equivalent circuit of Fig. 21(c). With the polarities indicated the thyristor has two stable modes of operation. If the potential is applied whilst the gate electrode is shorted to the cathode then no conduction takes place as transistor Tr 1 is off. The maximum voltage that can be withstood by the thyristor in this mode is known as the peak forward voltage (p.f.v.) and if this is exceeded voltage breakdown occurs.


Thyristor structure Equivalent structure Equivalent circuit
Fig. 21: Basic thyristor structure and the equivalent circuit.
The second stable state with the polarities shown occurs when a positive voltage is applied to the gate. In this mode the thyristor conducts heavily to a saturation potential since Tr 1 is made to conduct and its collector current provides the base current for $\operatorname{Tr} 2$ which in turn conducts and supplies base current for Tr1. It can be seen therefore that if the gate is shorted to cathode after conduction has taken place this will not affect the conduction of the device. It should be noted that the saturation potential is $\mathrm{V}_{\mathrm{be} 2}+\mathrm{V}_{\mathrm{ce}}(\mathrm{sat})^{1}$ and has a value of 0.8 V to 1.5 V .

When a reverse voltage is applied to the thyristor it
behaves as a reverse biased diode and blocks current flow providing the maximum peak reverse voltage (p.r.v. or p.i.v.) is not exceeded. The three conditions of operation are therefore forward on or off and reverse off, and it should be noted that either a positive-going pulse or d.c. voltage can be used to trigger the device into the conducting state.

The basic parameters defined by manufacturers are shown in Table 3, together with typical values. From a knowledge of the basic operation discussed above the parameters are self-explanatory. One parameter often neglected is the minimum holding current and this is the current required to maintain saturated conduction. This value is utilised in the operation of thyristors as relaxation oscillators when the device goes out of conduction

Table 3: Typical thyristor parameters and range of values

| Parameter | Symbol | Typical values |
| :---: | :---: | :---: |
| Max. peak reverse voltage | $\begin{aligned} & \text { pi.v. } \\ & \text { p.r.v. } \end{aligned}$ | 50-1,000V |
| Max. peak forward voltage | p.f.v. | 50-1,000V |
| Max. average forward current | If(av) | 1-100A |
| Min. holding current | ih | 1-100mA |
| Turn on time | ${ }^{t}$ on | approx. $3 \mu \mathrm{sec}$ approx 12 |

Table 4: Variation in price and encapsulation with thyristor ratings

| Maximum <br> average <br> forward <br> current <br> If (av) | Maximum <br> reverse <br> voltage <br> p.i.v. | Encapsulation | Price <br> from |
| :---: | :---: | :---: | :---: |
| 1 | 50 | Wire ended plastic | 5 s. |
| 1 | 800 | or metal | 15 s. |
| 6 | 50 | Stud mounting | 15 s. |
| 6 | 800 | (4BA) | 50 s. |
| 30 | 50 | Stud mounting | $£ 2$ |
| 30 | 800 | (OBA $\frac{1}{4}$ UNF) | $£ 15$ |
| 60 | 50 | Stud mounting |  |
| 60 | 800 | (OBA $\frac{1}{4}$ UNF) | $£ 8$ |
|  |  | flexible termina- |  |
|  |  | tions |  |
|  |  |  |  |
|  |  |  |  |



Fig. 22: Thyristor construction.
after discharging a capacitor and the current falls below the minimum holding current.

Thyristors are used in power switching applications such as phase control of heating and motor circuits as well as general a.c. applications. In pure d.c. circuits thyristors require commutation circuits to provide energy in order to switch off and either capacitors or inductors can be used. Thyristors are also widely used in fuse blowing crowbar circuits where the enormous power gain is fully utilised.

The basic construction is very similar to the power rectifier where the junctions are formed by successive diffusions as described in an earlier part of this series. The construction has the advantage of high forward current values but as with rectifiers the disadvantage of slow turn on and turn off times. Thyristor operation at frequencies above 20 kHz results in switching power losses. A typical thyristor construction is illustrated in Fig. 22 and this is obtained by successive diffusions. Planar construction techniques are now employed to enable thyristor operation at high frequencies but as yet these devices are considerably more expensive than the conventional diffused construction. As with power rectifiers transient breakdown is limited by edge chamfering and such devices are known as avalanche thyristors.

Since thyristors are essentially power devices they are encapsulated in high heat dissipation metal cases. Low current ( $\sim 1 \mathrm{~A}$ ) devices are available in TO-5 cans but above 1A stud mounting encapsulations are used. Plastic encapsulations are also used and a selection of encapsulations is shown in Fig. 23.


Fig. 23: Thyristor encapsulations.
Thyristor prices vary enormously and generally follow that of power rectifiers in that prices rise with increase in forward current ratings and with maximum blocking voltages. Typical costs are illustrated in Table 4 and in common with other semiconductor devices plastic encapsulations have resulted in price reductions.

## Triac

Triacs are four-layer semiconductor devices which are a development of the thyristor. Essentially they operate as two thyristors in anti-parallel as shown in the equivalent circuit of Fig. 24(b) and the symbol is shown in Fig. 24(a).
Triacs are used for a.c. switching purposes and were
developed to replace the thyristor-diode bridge arrangements used previously to allow conduction in both directions. The triac is switched into the conducting state by either positive or negative voltages between gate and anode 1 and can conduct in a saturated mode in either direction. Switch off takes place when the current is zero. When the gate-anode 1 electrodes are shorted no conduction can take place, provided the maximum blocking voltage is not exceeded. Unlike the thyristor however the triac will not sustain damage if the voltage is exceeded since it merely reverts to the saturated mode, but naturally a breakdown at the wrong time could have serious consequences on the following circuitry.

Fig. 24: (a) Triac circuit symbol and (b) thyristor equivalent circuit.
Fig. 25 (right): Diac circuit symbol.

(a)

(b)

Triacs are available in standard thyristor encapsulations and are available at current ratings in excess of 40A. High voltage ratings are not at present available and the maximum peak voltages available of 500 V allow operation up to 250 V r.m.s. but not three-phase ( 440 V r.m.s.) switching. Prices are remarkably low and triacs are available from 7s. 6 d. for 240 V r.m.s. 2 A or $£ 2$ for $240 \mathrm{~V}, 15 \mathrm{~A}(3.6 \mathrm{~kW})$ types.

## Diac

Diacs are bidirectional breakdown diodes which conduct only when a specified breakdown voltage is exceeded. They are used primarily as trigger sources for triacs and otherwise have limited applications. They are available in normal diode encapsulations and cost approximately 5 s. to $£ 1$. The symbol for the diac is shown in Fig. 25 and since it is a bidirectional device it is non-polarised.

## Light Emission Diodes

Visible light or infra-red radiation is emitted from semiconductor junctions by the recombination of electrons and holes in the junction. Many semiconductor materials produce useful radiation at suitably constructed diode junctions but at present gallium arsenide (infra-red) and gallium phosphide (visible light) are the most commonly available. Because the light output is directly related to the current they are used as light modulating devices for film marking and in transmission systems where electrical-light-electrical-conversion efficiences of $70 \%$ are possible together with operating frequencies up to 1 GHz . Another application for these devices is as indicator lamps with extremely long life times and high efficiency and reliability though at present cost precludes this use.

Fig. 26: Gallium arsenide light emission diode using mesa construction.


The basic construction is illustrated in Fig. 26 and consists of a diode junction bonded to a metal header for heat dissipation purposes. The light is emitted from the junction through a transparent cover which is either
glass or plastic and often preformed as a lens to give the required optical characteristics.

At present these devices are expensive and are available from $£ 2$ to $£ 25$ which has prevented their use as alternatives to normal indicator lamps. However much research is continuing and with the demand for increased reliability and low power dissipation it is quite likely that they will supersede standard low voltage indicator lamps. Another application is in solid state viewing tubes to replace c.r.t.s and an experimental version based on diode arrays is in current use. Widespread use still depends on improved technology and perhaps with planar techniques the necessary improvement will result.

## Light Operated Devices

Since photon or light bombardment of p-n junctions causes current to flow most devices are available in light activated varieties. These devices, including photodiodes phototransistors, light activated s.c.r.s and triacs, were discussed in a previous part of this series, together with other light operated devices.

## The Future

It is extremely difficult to foretell future trends with semiconductor devices. The more important devices discussed in this article will become widely used and understood and a further miscellany of devices introduced. F.E.T.s are particularly likely to become popular due to the simplicity of design, whilst photoemissive diodes can be expected to have a major impact as the technology of manufacture improves.

Thyristors and triacs will increase in popularity and it is very likely that multiple encapsulations performing the functions of power controllers, switches and contactors will become generally available. It is to be hoped in all these improvements that standardisation of symbols, terminations and designations be carried out at the earliest point of mass production.

## TO BE CONTINUED

## PRACTICAL TELEVISION in the MARCH issue

## * BUILD THIS 625-LINE RECEIVER

Now that all programmes are available in most areas on 625 lines is the time to consider building a single-standard set for optimum u.h.f. performance. Our design features a 20 in . c.r.t., double-wound mains transformer, effective black-level clamping, and uses surplus components wherever possible to keep costs down.
$\star$ SIMPLE UHF SLOT AERIAL
And with all-programme u.h.f. you'll want an effective u.h.f. aerial. This simple design is for indoor use.

## $\star$ FAULT-FINDING PITFALLS

TV fault diagnosis poses many problems for the unwary. Vivian Capel provides a detailed account of the types of difficulties that can mislead and how to avoid them.

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 Printics
## TRANSISTOR MINIGENERATOR

Describes the construction of an almost pocket size r.f. signal generator covering $180 \mathrm{kHz}-2 \cdot 8 \mathrm{MHz}$ on fundamentals and to 30 MHz on harmonics. An audio oscillator is included for modulation of the r.f. signal or for external use for audio circuit checking. The complete Minigenerator measures $5 \times 6 \times 2$ in.

## FET AUDIO PREAMPLIFIER

The matching of ceramic and crystal pickups to transistorised amplifiers often presents problems. The autputs of these transducers must be fed into a high impedance load in order to achieve a satisfactory frequency response and signal to noise ratio. This design using a field effect transistor offers an ideal solution to the problem.

## PORTABLE RADIOACTIVITY DETECTOR

The high voltage required to operate geiger tubes in portable equipment is usually obtained from high tension batteries. This article describes a method for operating one of these tubes from a $7 \frac{1}{2}$ volt battery thus eliminating the need for large and cumbersome power supplies. The pulses produced by radioactive particles are heard as clicks from a loudspeaker or headphone.

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All in the April issue of Practical Wireless-on sale 6th March-price 3s 6d.

#  <br>  

IHIS receiver employs twelve transistors and four semiconductor diodes in all, but can be built in simpler form to begin, extra stages being added later. Proceeding in this way has several advantages. A useful, working receiver is obtained as soon as possible, then additional features can be provided in due course. It can also be helpful to check that portion of the receiver already wired, before fitting further stages. Excellent reception is in fact possible over all frequencies with the basic circuit having only six transistors and two diodes.

Coverage is for medium waves and three short wave bands, or about 550 kHz to 30 MHz in all. The receiver is self-contained with battery. It is capable of long distance reception with the tele-
scopic aerial, though range is naturally greater with a conventional external aerial.

## Block Diagram

The simplified block diagram in Fig. 1 will make stages clear, and also clarify which may be omitted during early or intermediate construction.

Tr l is the r.f. amplifier, a panel trimmer allowing peaking of this circuit with any aerial. Tr 2 is the mixer, Zener stabilised by diode D1. Tr3 and Tr4 are intermediate frequency amplifiers, with doubletuned transformers. VRI allows manual control of r.f. and i.f. gain, which is often useful. Diode D2 furnishes automatic volume control bias, and also detection for a.m. only, if required.

Tr5 is the $S$-meter amplifier, working a small meter of the ready calibrated type. $\operatorname{Tr} 6$ and $\operatorname{Tr} 7$ function in the common-emitter product detector circuit, with $\operatorname{Tr} 8$ as beat frequency oscillator. This permits reception of a.m., s.s.b. and c.w., a "function switch" controlling this part of the receiver, and also a.v.c.

VR2 is the audio gain control, followed by audio amplifier $\operatorname{Tr} 9$, driveı $\operatorname{Tr} 10$, and push-pull pair Tr11 and Tr12, which will give


Rear view of the receiver
plenty of loudspeaker volume. Phones may be used when wanted. Diodes D3 and D4 function as audio limiters, considerably reducing interference of static and similar type and avoiding sudden bursts of uncomfortable volume with phones.

In the completed receiver, Tr 1 and Tr 2 are under the metal chassis, with bandswitch, coils, etc. Tr3, Tr4 and $\operatorname{Tr} 5$ occupy a paxolin panel, forming the i.f. and meter amplifier section.
$\operatorname{Tr} 6, \operatorname{Tr} 7$ and the b.f.o. $\operatorname{Tr} 8$ are wired on a separate panel, and a.m. reception over all bands may be had even if this part of the receiver is wholly omitted, so it can be constructed later.
The audio section, $\operatorname{Tr} 9, \operatorname{Tr} 10$ and $\operatorname{Tr} 11 / 12$ occupy another insulated panel. These various panels are attached to the chassis and grounded to it.

To take advantage of the step-by-step method of wiring, sections are tested as completed. This enormously simplifies the process of locating any fault.

## /ERAGE <br> F. G. RAYER G30GR

The following is probably as good a way to proceed as any, especially for a beginner, though there is naturally no reason why the whole circuit should not be used from the beginning by the more experienced constructor.
(1) Wire mixer $\operatorname{Tr} 2$, i.f. amplifiers $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$, and diode D2, with coils for one band. Feed phones from D2. This will give many transmissions at good phone volume, and allow initial alignment of the i.f. amplifier.
(2) Build the a.f. amplifier, $\operatorname{Tr} 9, \operatorname{Tr} 10, \operatorname{Tr} 11 / 12$. Those signals previously heard with phones should now give excellent speaker strength. If a little simplification is wanted, $\operatorname{Tr} 9$ can be temporarily omitted.
(3) Add the r.f amplifier Trl, with aerial coil for the single band chosen, and check working.

(4) Wire $\operatorname{Tr} 5$ and the S-meter The i.f. panel is so placed and arranged that Tr5 can be wired without removing the panel.
(5) Wire the sets of coils for the other three ranges to the wavechange switch, festing and roughly aligning each range as it is added. This will avoid errors in switch wiring, which could be troublesome to locate.
(6) Wire the product detector and b.f.o. panel, insert and wire it. This is also the time to add the a.m./a.v.c./c.w./s.s.b. switch, and minor extras such as p.u. input, tape output, phone jack, diode limiter, etc.


Fig. 2: R.F., mixer, l.f. and meter ampl/fier stages. See text p.870 for values of padder condenser P. Note: S6 should be shown as ganged to 58.

## Coils and Coverage

The bands are approximately as follows:
S.W.1. $30-11 \mathrm{MHz}$. $10-27$ metres.
S.W.2. $14-5 \mathrm{MHz}$. $21-60$ metres.
S.W.3. $5-1 \cdot 6 \mathrm{MHz}$. $60-190$ metres.
M.W. $1400-550 \mathrm{kHz}$. $210-550$ metres.

If a pre-set trimmer were used with each coil, there would be twelve in all. The number of trimmers is reduced to five by having a single trimmer common to all oscillator coils, and an individual trimmer for each mixer input coil. Then the aerial circuit is adjusted with a panel-mounted capacitor, so giving maximum efficiency with any aerial.

There is clearly no reason why a separate trimmer should not be used for each oscillator coil, if preferred. There will then be eight trimmers, plus the panel capacitor.

## Circuit Details

Notes on the various stages should prove useful at various periods during construction. Almost no changes to existing circuitry are needed when adding other stages, but there are a few points which must not be overlooked.
Figure 2 shows the r.f., mixer, two i.f., and meter amplifier stages. Band changing is accomplished by using a switch having three wafers, each three-pole four-way. Figure 2 shows coils for one band only. In the aerial section, S 1 switches the aerial, S 2 Tr 1 base, and S3 the tuning capacitor VC1.

The central wafer on the spindle has S 4 for Tr 1 collector, S5 for Tr2 base, and S6 for VC2. The
rear wafer uses S7 and S8 for collector and emitter switching of Tr 2 , and S 9 for the tuned windings of the oscillator coils.

Tag $P$ of the oscillator coils is different for each range, as is the value for the related capacitor $P$. For S.W. 1 (highest frequency band) connect pin 6 to chassis, as no padder is required. With range S.W.2, the padder $P$ is $3,000 \mathrm{pF}$, from pin 4 to chassis. For S.W.3, the capacitor is $1,200 \mathrm{pF}$, from tag 3 to chassis. With the m.w. range, the padder is 350 pF , and connected from tag 2 to chassis.
To avoid difficulty in wiring here, it is wise to check that the receiver works correctly on one band, before adding the coils for other bands.
The receiver can be tested without Tr1 and associated circuitry by taking'S4 to the aerial, and temporarily connecting 8 to chassis, instead of C 3. Results should be good.

Tr 1 and $\operatorname{Tr} 2$ operate on a stabilised 5.6 V line, from D1. D1, i.f.t.1, and the other items shown are on the i.f. panel.

Tr 3 and $\operatorname{Tr} 4$ are the i.f. amplifiers, operating on the supply Y obtained from the audio amplifier. VR1 controls emitter bias of Tr1, Tr3 and Tr4, and its main use is to reduce the strength of powerful signals, which may overload some stages. It must also be used when the a.v.c. is out of action.

S10 is one pole of the "function" switch. Two positions give a.v.c. from D2, while two substitute R17, eliminating a.v.c. This is primarily of use with some s.s.b. and c.w. signals. The receiver may initially be operated without S10, by connecting R12 to D2. The six positions of the switch are (1) Receiver off, (2) A.M. reception with a.v.c., (3) A.M. reception


Fig. 3: Product detector, b.f.o., a.f. and output stages. The 5.6 volt stabilised line is taken to the junction of D1/R9 (Fig. 2).

## $\star$ sectional components list

Coils:
Aerial (T1): "Blue". Mixer (T2): "Yellow".
Oscillator (T3): "Red". Denco miniature tran-
sistor type.
S.W.1: Range 5. S.W.2: Range 4. S.W. 3: Range 3.
M.W: Range 2.

VC1/VC2/VE3 Jackson E3 three-gang or similar.
VC4 Jackson C804, 50pF.
Eddystone C898 drive.
R.F. Stage:

| Tr1 | OC170 | R4 | $1 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: |
| R1 | $10 \mathrm{k} \Omega$ | C1 | $0.01 \mu \mathrm{~F} 150 \mathrm{~V}$ |
| R2 | $2 \cdot 7 \mathrm{k} \Omega$ | C2 | $0.05 \mu \mathrm{~F} 150 \mathrm{~V}$ |
| R3 | $1 \mathrm{k} \Omega$ | C3 | $0.01 \mu \mathrm{~F} 150 \mathrm{~V}$ |
| Mixer Stage: |  |  |  |
| Tr2 | OC170 | R8 | $1 \mathrm{k} \Omega$ |
| R5 | $10 \mathrm{k} \Omega$ | C4 | $0 \cdot 02 \mu \mathrm{~F} 150 \mathrm{~V}$ |
| R6 | $2 \cdot 7 \mathrm{k} \Omega$ | C5 | $0.01 \mu \mathrm{~F} 150 \mathrm{~V}$ |
| R7 | $1 \mathrm{k} \Omega$ | C6 | $0.01 \mu \mathrm{~F} 150 \mathrm{~V}$ |

Padders: 350pF, 1,200pF, 3,000pF
TC1 to TC4, each 60 pF miniature compression trimmer.
TC5 30 pF beehive trimmer.
I.F. Amplifier:

D1 5.6 V 1 watt Zener, Z1104
D2 OA81
Tr3 AF117
Tr4 AF117
I.F.T. 1 DencoI.F.T. 18/465
I.F.T. 2 Denco I.F.T. 18/465.
I.F.T. 3 Denco I.F.T. 14.

VR1 miniature 1 watt wire-wound, $2 \mathrm{k} \Omega$ (Home Radio VR25)
$\begin{array}{llll}\text { R9 } & 150 \Omega & R 14 & 4.7 \mathrm{k} \Omega \\ \text { R10 } & 68 \mathrm{k} \Omega & R 15 & 1 \mathrm{k} \Omega \\ \text { R11 } & 680 \Omega & R 16 & 5.6 \mathrm{k} \Omega\end{array}$
R11 $680 \Omega$ R16 $5 \cdot 6 \mathrm{k} \Omega$
R12 $8 \cdot 2 \mathrm{k} \Omega$ R17 $5 \cdot 6 \mathrm{k} \Omega$
R13 22k $\Omega$
C7 $\quad 0.5 \mu \mathrm{~F} 150 \mathrm{~V} \quad \mathrm{C} 11 \quad 0.04 \mu \mathrm{~F} 150 \mathrm{~V}$
C8 $\quad 10 \mu \mathrm{~F} 6 \mathrm{~V}$
C9 $\quad 0.04 \mu \mathrm{~F} 150 \mathrm{~V} \quad \mathrm{C} 13 \quad 0.01 \mu \mathrm{~F} 150 \mathrm{~V}$ C10 $0.04 \mu \mathrm{~F} 150 \mathrm{~V}$ C14 100 pF silver mica
Cx $\quad 0.25 \mu \mathrm{~F} 150 \mathrm{~V}$ required for "A.M. only" circuit.

Meter Amplifier:
Tr5 OC81
$\begin{array}{llll}\text { R18 } & 68 \mathrm{k} \Omega & \text { R20 } & 4 \cdot 7 \mathrm{k} \Omega \\ \text { R19 } & 10 \mathrm{k} \Omega & \text { R21 } & 470 \Omega\end{array}$
R19 10k $\Omega$ R21 470
VR3 Pre-set or panel linear $5 \mathrm{k} \Omega$ wire-wound 1 W .
1 省in. sq. 1 mA S-meter.

Product Detector and B.F.O.:

| Tr6 | OC45 | Tr8 | 0 C 45 |
| :---: | :---: | :---: | :---: |
| Tr7 | 0 C 45 |  |  |
| R22 | $22 \mathrm{k} \Omega$ | R27 | $2 \cdot 2 \mathrm{k} \Omega$ |
| R23 | $2 \cdot 2 \mathrm{k} \Omega$ | R28 | $1 \mathrm{k} \Omega$ |
| R24 | $4.7 \mathrm{k} \Omega$ | R29 | $22 \mathrm{k} \Omega$ |
| R25 | $470 \Omega$ | R30 | $4 \cdot 7 \mathrm{k}$ / |
| R26 | 22k $\Omega$ |  |  |
| C15 | $0 \cdot 02 \mu \mathrm{~F}$ |  |  |
| C16 | $0 \cdot 25 \mu$ |  |  |
| C17 | $0.02 \mu \mathrm{~F}$ |  |  |
| C18 | 18pF |  |  |
| C19 | $0.01 \mu \mathrm{~F}$ |  |  |
| C20 | $0.01 \mu$ |  |  |
| VC5 | 15pF |  |  |

A.F. Section:

| VR2 | small $5 \mathrm{k} \Omega$ log. pot. |  |  |
| :--- | :--- | :--- | :--- |
| R31 | $2 \cdot 2 \mathrm{k} \Omega$ | R 38 | $150 \Omega$ |
| R32 | $120 \mathrm{k} \Omega$ | R 39 | $680 \Omega$ |
| R33 | $47 \mathrm{k} \Omega$ | R 40 | $10 \mathrm{k} \Omega 5 \%$ |
| R34 | $12 \mathrm{k} \Omega$ | R 41 | $10 \mathrm{k} \Omega 5 \%$ |
| R35 | $8 \cdot 2 \mathrm{k} \Omega$ | R 42 | $82 \Omega 5 \%$ |
| R36 | $82 \mathrm{k} \Omega$ | $\mathrm{R} \Omega 3$ | $4 \cdot 7 \Omega$ |
| R37 | $22 \mathrm{k} \Omega$ |  |  |
| C21 | $2 \mu \mathrm{~F} 6 \mathrm{~V}$ | C 24 | $8 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C 22 | $100 \mu \mathrm{~F} 12 \mathrm{~V}$ | C 25 | $100 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C 23 | $2 \mu \mathrm{~F} 6 \mathrm{~V}$ | C 26 | $100 \mu \mathrm{~F} 12 \mathrm{~V}$ |

Tr9 OC71
Tr10 OC81D
Tr11/12 Matched pair OC81/NKT251/ AC128 or similar OC81 types.
T5 Osmor QXD1
T6 Osmor QX02
Limiter:
Two GD9 diodes.
R44 $5 \cdot 6 \Omega$
On-off switch S14
C27 $0.02 \mu \mathrm{~F} 150 \mathrm{~V}$.
Miscellaneous:
$12 \times 7 \times 7 \mathrm{in}$. Type W cabinet, H. L. Smith \& Co, 289 Edgware Road, W.2. $10 \frac{1}{2} \times 6 \frac{1}{2} \times 2 \mathrm{in}$. Type I chassis (three-sided plus flanges), H. L. Smith \& Co, 289 Edgware Road, W.2. WS27A (Home Radio) switch assembly with three WS29 threepole four-way wafers, studding and spacers (see text). WS27 switch assembly, with two WS29 two-pole six-way wafers, studding and spacers. $1 \frac{1}{2} \times 2 \frac{1}{2}$ in. 16 s.w.g. heatsink, knobs, sockets, tags, 6BA bolts, etc. (Home Radia).
without a.v.c., (4) C.W./S.S.B. reception without a.v.c., (5) C.W./S.S.B. reception with a.v.c., (6) A.F. amplifier only in use.
When the product detector and b.f.o. panel is not ready, Cx from D2 is taken to the audio gain control, giving a.m. reception only. For general broadcast s.w. listening, the product detector may be permanently omitted. When it is employed, it is of a type which furnishes a.m. detection with no b.f.o. injection to the emitter pair.

As mentioned, $\operatorname{Tr} 5$ and the $S$-meter may be omitted until some later date. When in use, increased
bias from D2 moves Tr5 base positive, reducing current through R20. The collector voltage of Tr 5 thus moves negative, due to reduced voltage drop in R20. This operates the meter. With the aerial removed, VR3 is adjusted until the meter reads zero. Readings then rise with signal strength.
This is a lively S -meter circuit, operating with a.v.c. on or off, and not upset by b.f.o. injection. With a steady signal, from a signal generator or BBC transmitter (with extremely short aerial) the S-meter can be used to aid alignment. All trimmers and cores, including those of the i.f.t.s, are peaked
for the best $S$-meter reading.
In normal use, the meter shows any improvement in signal, strength, as from changes to aerial or earth, adjustments of an aerial tuner, peaking VC4, or the relative strengths or improvement to amateur signals, etc.

## Band Notes

In order to reduce damping on m.w., a $1 \mathrm{k} \Omega$ resistor is placed between S2 and tag 5 of the coil for this range only. To avoid squegging, a 100 ohm resistor is wired between $\mathbf{S 7}$ and tag 9 of the oscillator coil for this band.
For a similar reason, a 470 ohm resistor is placed between S7 and tag 9 on the S.W.I and S.W. 2 (higher frequency) ranges.

The need for these resistors depends somewhat on the actual transistor Tr 2 , and also on the run of wiring. If excessive oscillation, shown by hissing and whistles, does not arise on a band, no resistor is required. When resistors are fitted, they are best of the lowest value which will prevent this trouble, and values such as those mentioned give no apparent reduction in sensitivity.

## Product Detector and BFO

This is built in a panel holding all components except the pitch control VC5, Fig. 3. This item is connected to the metal chassis, and to 3 on the b.f.o. coil.

When this panel is made, Cx in Fig. 2 is not required. D2 now provides a.v.c. only, and signals go from C14 Fig. 2, to Tr6 Fig. 3. Tr6/7 act in such a way as to provide a.m. reception when no input is available from the b.f.o., Tr8. With the b.f.o. in use, mixing gives reception of s.s.b. or c.w. signals. The function switch wafer SII brings the $5 \cdot 6 \mathrm{~V}$ stabilised supply to Tr 8 , in s.s.b./c.w. positions. In each case audio passes from C16 to the audio amplifier.
This circuit was found particularly easy to adjust for s.s.b., and though VC5 must be correctly adjusted, it is of small value, so not critical to operate. VC5 and Tr8 are completely out of use for a.m. reception, in the usual manner. About 7 V is available at $Y$, which also supplies the i.f. amplifier.

It is often convenient to have an audio amplifier. The last section of the function switch breaks the circuit from C16 to VR2, in the 6th position. A rear socket strip gives input across VR2, so the a.f. section can be used as an audio amplifier. The same socket provides tape output, VR2 being turned to zero, or adjusted to monitor signals.

## Function Switching

The operations described are carried out by a four-pole six-way rotary switch. This gives one control, for all modes of use. But there is no reason why separate switches should not be fitted, if preferred.

If VR2 has a switch, this can be wired for "on-off" in the usual manner. A small rotary or slide singlepole two-way switch can substitute for S10, Fig. 2, for a.v.c. on, a.v.c. off. A further on-off switch may replace S11, so that the b.f.o. can be off for a.m., and on for s.s.b./c.w.

## AF Section

This is also shown in Fig. 3. A lead runs from C16 to VR2, via S13, mounted on the panel. VR2 is earthed to the chassis, and its slider tag wired to the audio panel input point.

Tr9 is the first audio amplifier, $\operatorname{Tr} 10$ the driver, and $\operatorname{Tr} 11 / 12$ the output pair, with individual feedback. This is a very straightforward type of circuit, with the direct current operating conditions of each stage separate from other stages.

If necessary, the first stage $\operatorname{Tr} 9$ can be tested by placing phones across R37, while $\operatorname{Tr} 10$ can be checked with phones across the primary of the driver transformer T5.

The exact value of R 42 considerably influences results. If Tr11/12 draw almost no current with no signal, and reproduction is distorted, R42 may be slightly increased in value. But if $\operatorname{Tr} 11 / 12$ draw much more than 4 mA to 5 mA or so, with no signal, R42 should be reduced in value. This depends somewhat on the actual transistors and R40 and R41. The values given should usually be suitable.
Output from the secondary of T6 is taken to a 5 in . or other reasonably large $2-3$ ohm permanent magnet moving coil speaker, which should occupy a cabinet.

For headphone listening, we may use a jack with contacts which open when the plug is inserted, these contacts being in series with one speaker connection. The loudspeaker is then silenced when the phones are plugged in. Alternatively, T6 secondary may go to a jack outlet, so that-speaker or phones can be plugged in, as wanted.

## Audio Limiter

This is optional, and formed by D3 and D4, Fig. 3, with C27 and R44. With S14 open, results are normal. With S14 closed, the diodes place R44 across T5, to limit output. VR2 should not be so far advanced that all signals are constantly limited, but only those of excess level, such as static crashes, or the sudden bursts of volume sometimes uncomfortable when tuning with phones. Actual results can be modified by changing the value of R44.

## TO BE CONTINUED

## A PANORAMIC RECEIVER

-continued from page 849
loc an unidentified carrier is beating with a amateur a.m. signal in the centre of the display, and when this is magnified by adjustment of VR3 (see Fig. 10d) the thickening of the trace between the two peaks is visible to the eye as a heterodyne waveform. Figure 10e demonstrates the effect of splatter resulting from a grossly overmodulated signal...Finally, Fig. IOf was recorded late in the afternoon and shows a marked increase in the number of stations and amount of noise. At the centre of the display are two s.s.b. signals side by side.
An interesting feature of the panoramic receiver display, is that it distinguishes between noise derived from the mains and other sources. If the oscilloscope timebase is not locked to a sub-multiple of the mains frequency, mains noise is seen as "clumps" of spiky waveforms drifting across the display. Other noise just causes a thickening of the trace baseline, as seen in Fig. 10f.

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The two photographs are of a v.h.f. portable comprising the Practical Wireless V.h.F. Tuner (Feb.-March 1968) and basic amplifier (November 1967).
I have used this as a portable for several months now and it even works well in the car. Good reception can be obtained within 40 miles of the transmitter.
The units could have been installed in a smaller enclosure, but it was felt that to do justice to the output a large as possible speaker should be employed.

I have spent many enjoyable hours assembling these units and many more enjoying the results. C. W. Britnell (Norwich, NOR 76).

## Electric fires

G3TWZ's letter ("P.W.", December 1969) re TO3 "electric fires" reminds me of a true story that I heard about a year ago.

A certain American TV manufacturer was happily producing TV receivers with a power transistor in the line output position. The supply started to dry up so an equivalent (???) from another maker was tried and hence LOPT
electric fires. No matter who made these transistors they all did the same. The only solution was a different circuit design for each transistor manufacturer!
If G3TWZ gets the full spec on these transistors and reads it carefully he will see what I mean -they were the same types and the difference only shows up when the circuit uses the characteristics to the full. It seems that the moral is to use the same type and make that the original circuitdesigner specified.-A. M. Levett (Sussex).

## The early days

Reading a letter in the November copy of Practical Wireless, from F. Towndraw (Newquay, Cornwall), made me think of my early days in Radio. I still have my first licence issued in October 1923. This was the first licence one could obtain, otherwise than a transmission one for a homebuilt broadcast receiver, cost was 15 s . to cover anytime, before that date one had used one without licence, after that, cost was to be 10 s . My first set was also a crystal one built in June 1923. At that time one could obtain very few ready-made components, a pair of phones and crystal was about all. Coils had to be hand wound on cardboard formers, studs and switches could be bought. The hours I spent building this set and all taped out at every 10 turns to studs for tuning. Then the great moment trying to get 2 LO 30 miles away in London. "NO luck, dead silence." Laying awake at 2.30 a.m., realised mistake I had made in wiring, got up and put right and waited until 2 LO started up again and wonder of wonders, after making nearly everything stats, I got 2 LO on phones.
In High Wycombe at that time there were 3 of us in town, the dealers and 2 home-built receivers. How much I owed to Mr. Millner the dealer of West Wycombe Road for his help at that time. From this I went on to make a unit-built valve set again hand wound coils, 400 turns of double silk-covered 20 -gauge wire in one coil on a former $6 \times 3$ in. of cardboard. No light
needed in room with this set's four bright valves on top of set.

Then on to kit sets obtainable to make up yourself. The old "Cossor Melody Maker set," I made one up for myself and quite a few for other people, with the excitement of hearing people speaking overseas. Now at 73 years old I have a modern 7 -valve receiver, a domestic 4-band f.m. short-, medium- and long-wave can listen all over the world on an internal aerial, and with a long wire outside and earth, well you know what can be done.

This has always been a hobby for me not my job, as I was in the furniture trade and still enjoy picking up an old set perhaps at a jumble sale and getting it to work again. An old lady has just given me a very old Marconi set, just medium band, only portable mains line cord with a pancake frame aerial inside back. This is now working very well again great fun working out.
I do not know how long 1 have taken your Practical Wireless, a great number of years, so I wish you continued success with same.-F. W. Wells (Easthourne).

## Please leave us be Ladies

I agree most wholeheartedly with F. G. Sadler, G3UZ in his article on page 775 of the February 1970 issue of Practical Wireless. It is one of the World's hardest problems trying to convince a wife or mother that the box or pile of valuable priceless equipment lying in a corner of the bedroom or lounge is not a load of blooming old junk, as many of them will term our equipment.

If us chaps were to go around tidying up heaps of knitting, recipes and piles of Woman's Owns, we would soon get a rocket.

So come on wives and mums, let's call a truce. You leave all our equipment, components and service manuals where we put them, or we will gang up on you and start shifting all the piles of ladies' magazines and carefully laid out dress patterns when we feel like having a little tidying up session!-R. Smith (Southgate).

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| B82 $10 \begin{aligned} & \text { OC45., OC81D } \\ & \text { Trans Mullard lass and } \\ & \end{aligned}$ | B81 10Reed Switches, mixed types, $10 /=$ <br> large and small. |
| B83 200 Trans. Makers rejects. NPN/10/- | B89 $2 \quad$5SP5 <br> Light Res. $400 \Omega$ <br> Light <br> Sensitive Cells. $10 / \mathrm{M} \Omega$ |
| 100 to OA200, OA202. $10 /$ - | B91 $8 \quad$NKT163/164 PNP Germ. TO-5 10// <br> equivalent to OC44, OC45. |
| 150 glass type. 10/= | B92 $4 \quad$NPN, Sil. Trans. AO6 BSX20 <br> 2N2369 <br> $500 \mathrm{MHz}, 360 \mathrm{~mW}$. |
| B86 $50 \begin{aligned} & \text { Sil. Diodes sub. min. IN914 and 10/= } \\ & \text { IN916 types. }\end{aligned}$ | B93 $5 \quad$GET113 Trans. equiv. to ACY17 10/- <br> to ACY21 PNP Germ. |
| B87 100 Germ. PNP Trans. equiv. to $10 /=$ |  |
| B88 50Sil. Trans. NPN, PNP, equivalent <br> to $0 C 200 / 1,2 N 706 A, ~ B S Y 95 A, ~ e t c . ~$ | B 9810 XB 112 <br> $\mathrm{AC126}$ <br> $\mathrm{AC1}$ <br> $\mathrm{OC} 71 / 2$, NK271, etc. |
| $6010 \begin{aligned} & 7 \text { Watt } \\ & \text { voltages. }\end{aligned}$ | B99 $200 \begin{gathered}\text { Capacitors, } \\ \text { silver mica, ecte. Post and }\end{gathered}$ ing, this Pak 2/6. |
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THE General Electric (U.S.A.) type PA246 integrated power amplifier has finally become freely available on this side of the Atlantic, and is certainly deserving of our attention this month. With a five watt rated output, it is the culmination of a development process which began with the PA222 described in "Practical Wireless" as long ago as August 1968. That device introduced the idea of mounting the monolithic "chip" of silicon carrying the integrated components on a metal tab; when soldered to an area of a printed circuit board this provides a path of low thermal resistance to a

Characteristics of the G.E. series of audio power i.c.'s.

|  | PA 222 | PA 234 | PA 237 | PA 246 |
| :---: | :---: | :---: | :---: | :---: |
| Supply Voltage | 18-24 | $9-25$ | $9-27$ | $12-34$ |
| Audio Output .. (r.m.s.) | 1 Watt | 1 Watt | 2 Watts | 5 Watts |
| Frequency Response | $55 \mathrm{~Hz}-15 \mathrm{kHz}$ | $30 \mathrm{~Hz}-100 \mathrm{kHz}$ | $30 \mathrm{~Hz}-100 \mathrm{kHz}$ | $30 \mathrm{~Hz}-100 \mathrm{kHz}$ |
| Input signal .. | 52 mV | 600 mV | 8 mV | 12 mV |
| Input impedance | $55 \mathrm{k} \Omega$ | $100 \mathrm{k} \Omega$ | $40 \mathrm{k} \Omega$ | $40 \mathrm{k} \Omega$ |
| Load impedance | $22 \Omega$ | $22 \Omega$ | 16ת | $16 \Omega$ |
| Output impedance | $1 \Omega$ | $2 \Omega$ | $0.85 \Omega$ | $0 \cdot 6 \Omega$ |
| Heat Sink Area .. Device Noise | $\begin{aligned} & 1 \mathrm{sq} . \mathrm{in} . \\ & -65 \mathrm{~dB} \end{aligned}$ | $\begin{gathered} 1 \mathrm{sq} . \mathrm{in} . \\ -80 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 2 \mathrm{sq} \cdot \mathrm{in} . \\ -75 \mathrm{~dB} \end{gathered}$ | $\begin{gathered} 6 \mathrm{sq} . \mathrm{in} . \\ -70 \mathrm{~dB} \end{gathered}$ |

heat sink, with the result that a one watt device dissipation figure could be achieved. The disadvamtage of the number of external discrete component required was next overcome with the PA234, again a one watt unit, while a variation in the driver stage on the chip enabled the PA237 to dissipate two watts. Finally, with an improved heat sinking method, the PA237 chip was uprated to a higher operating voltage and dissipation, with the PA246 designation. The table gives the characteristics of this family of devices, and the development sequence outlined above can be followed.

The PA246 package is a specially designed variant of the familizr 14-lead dual-in-line epoxy i.c. format, with the addition of two wide heat transfer tabs, and staggered leads for greater convenience in the design of printed circuit boards. As with the PA237, only eight of the leads are actually in place, though the manufacturer's literature refers to them by the numbering convention for a full 14-lead package. Further, only six of these leads are actually functional connections to the chip. Figure 2 shows
continued on page 894


FIg. 1: Equlvalent clrcults of General Electric (U.S.A.) audlo power Integrated clrcults.

## by M.F.DOCKER, M.Sc.

LAST month the type of logic integrated circuits which are available were described. The average amateur will not find many applications for these devices in his workshop although they serve very well for use in counting circuits, voltage level detector circuits, automatic morse senders and so on. However the integrated circuit industry can still serve this customer with its products-with linear circuits.

## Operational Amplifiers

Perhaps the most widely used type of linear integrated circuit is the operational amplifier. Available at well under one pound this circuit has uncountable applications in the home laboratory. With a few external resistors and capacitors they can be used to produce high stability d.c. amplifiers using resistive feedback elements. Bandwidths approaching 10 MHz can readily be reached. Using capacitive feedback the circuit can be used to produce an integrator, or with resistive feedback and capacitive input a differentiator is obtained. These three arrangements are shown in Fig. 1. In order to achieve stable operation over a wide bandwidth it is necessary to utilise suitable frequency compensation. Details of this simple procedure, requiring only resistors and capacitors, are obtainable from the device manufac-turer-usually free of charge.


Fig. 1: Operational ampilifer applications
Other uses of the operational amplifier are as active filters, using suitable resistor and capacitor arrangements in the feedback networks. Either bandstop or bandpass filters with very high $Q$ values can be obtained without the necessity for the large inductors required with the usual low-frequency filter. Using a diode as the feedback element it is possible to produce a logarithmic amplifier in which the output bears a logarithmic relation to the input voltage. Summing and differencing amplifiers can also be made, using only resistors and operational amplifiers. These have numerous applications in many enthusiasts' experiments.

Also available in integrated circuit form are audio amplifiers. A one-watt amplifier is currently avail-

able at under two pounds and a preamplifier utilising a MOST is available at less than ten shillings. The integrated circuits in this field enable remarkable miniaturisation. A one-watt amplifier in a space of less than one-tenth of a cubic inch is quite an achievement, especially as the reliability is also high.

## Other Circuits

Numerous other circuits are now becoming available including i.f. amplifiers with built in a.v.c. circuits; combinations of transistors with external connections to suit the user; video amplifiers for use in television equipment; d.c. voltage comparators; and one firm is even making an integrated car radio with all the active elements, including a three-watt output stage, on one chip. The list of circuits which are available grows week by week and not only is the list of available circuits rising but also their prices are falling, some being only one-third of what they were two years ago.- Several manufacturers of integrated circuits are now offering customer design services to the users of integrated circuits: in this way the number of integrated circuits which are available can be expected to grow and both the amateur and the professional engineer can hope to benefit from this development!

## Thin Film Circuits

Another field of integration which has been in existence for some years is that of the thin film circhit. These circuits consist of microminiature arrangements of resistive, conductive and dielectric films on inert substrates. Using these films it is possible to make resistors, capacitors and inductors. Unfortunately there are no reliable active devices available yet which can be made in thin film form. This means that discrete semiconductor devices have to be attached to the thin film circuit after it has been completely processed. The steps in making a thin film circuit are similar to those used in making a silicon integrated circuit, but instead of diffusion of impurity atoms into the substrate an evaporation of metal or dielectric material on to a glass or mica substrate is carried out.

Resistors are produced by depositing a long, thin filament of metal on to the glass. Metals commonly used are nichrome, well known as the metal used in electrical heating elements, and tantalum. They are deposited on to the substrate by heating them strongly so that metal from their surface evaporates and after passing through a suitable mask lands on the substrate. With thin film resistors a much larger range of values can be obtained than can be obtained with monolithic resistors, and also the parasitic capacitances are smaller.

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Fig. 2: Examples of a resistor, capacitor and inductor in thin film form.
Thin film capacitors can be produced by first depositing a layer of metal as one electrode, then a layer of alumina or tantalum oxide to act as a dielectric insulating layer, and finally a top electrode of metal. Inductors can also be produced by thin film techniques although values of inductance greater than one microhenry are difficult to produce. They are made by depositing spirals of metal on to the substrate, connections veing made to each end of the spiral. Figure 2 shows an arrangement of thin film resistors, capacitors and inductors on a suitable substrate.

## Mounting Discrete Components

The active devices required in most circuits are obtained in thin film technology by using discrete semiconductor diodes and transistors as mentioned previously. However there are various methods of mounting them on to the substrate. Either they are attached as complete devices, although this is very rare, or they are supplied to the film manufacturer in an unencapsulated form. Three such forms are shown in Fig. 3: these are the flip chip, tag chip and leadless inverted device (LID). They are soldered into place after all the passive components have been deposited on to the substrate. Finally the circuit is encapsulated.


Fig. 3: Three types of device construction for use with thin film circuits.

## Thick Film Circuits

A variation on the thin film circuit is the thick film circuit. The essential difference between the two types is not so much in the thickness but in the method of manufacture of the circuit. Thin films are deposited by evaporation of metal whilst thick films are screen printed on to the substrate using special inks which form conductive layers after they have been baked. The advantage of this system is one of cost as using this technique it is possible to mass produce the film circuits. However they have disadvantages in that the accuracy of the components is several times worse with thick film circuits than it is with the thin film equivalents. This is because of the diffusion of ink which takes place during printing and baking and because of the variation in the quality of ink between different circuits. Nevertheless the thick film circuit has sufficient economic advantage to ensure that it will be here for some time to come.

## Advantages and Disadvantages

What are the relative advantages and disadvantages of film and silicon integrated circuits? Firstly silicon integrated circuits are considerably cheaper to make in large quantities than film circuits. They are capable of more variety since virtually all components can either be produced on the semiconductor chip or else they can be simulated by the use of other components as in the active filter described previously. Secondly film circuits have far better isolation properties, alleviating the need for special techniques to be applied. Their cost is comparable with the cost of discrete components and it is possible to provide more variety of resistors and capacitors.

## Hybrid ICs

A third form of integrated circuit is the "hybrid integrated circuit" or "chip circuit." These are formed by producing all the components in discrete semiconductor form and connecting them with fine wires. This provides the isolation of the film circuit with the ease of production of the semiconductor device. Another advantage of the chip system is that small quantity orders can be met at much lower cost. Several manufacturers are now producing complete film circuits with functions similar to those of silicon integrated circuits but with better properties as regards temperature stability, isolation and specification tolerances.

## Conclusion

In this series of articles I have tried to show the enormous range of semiconductor devices which are now available to the circuit designer and to the amateur. Although space has been somewhat limited I have tried to point out the essential mechanisms in the manufacture and operation of the devices and a little of their relative advantages. Only occasionally have I been able to give any specific applications but I trust readers will find this information elsewhere and hope that having read this and other more fully explained texts on these devices they will be able to design their own circuits knowing the limitations imposed on them by the devices themselves.

# VOX CONTROL UNIT 

IT is perbaps not too well known that a simple but effective Vox control unit can be incorporated into almost any transmitter using only a handful of components. Apart from the zener diode, most constructors will probably have the components in their junk boxes.

Basically the Vox unit consists of only four items: a $470 \mathrm{k} \Omega$ log. potentiometer, a fairly sensitive relay, a capacitor of about $50 \mu \mathrm{~F}$ (its actual value will depend on the desired drop-out period) and a zener diode. The actual zener used in the prototype is a type MZ27 and the circuit is based around this one. Operation is as follows: VR1 is advanced until the relay just closes and is then backed off very slightly until it opens. A short space of time must be allowed for the delay in drop-out caused by the holding action of C , this delay being necessary to prevent the relay from following the peaks of speech which occur when the transmitter is modulated.

Conduction of the zener is brought about by these modulation peaks adding to the d.c. level exceeding the zener voltage and so actuating the relay. When the basic circuit was applied to the authors transmitter it was found that the audio voltage required to operate the Vox unit detracted overmuch from the voltage required to drive the following audio stage. Since it was not possible to 'tap-off' the requisite feed from a further stage the circuit shown in Fig. 1 was evolved. It will be seen in this particular case a double triode was used, one half being used as a voltage amplifier for the microphone whilst the second half is used


Fig. 1: The circuit of the Vox Control Unit.
solely for the operation of the Vox circuit; in this case the circuit solved this problem and it worked perfectly.
The relay can be a G.P.O. ' 3000 ' type with an operating current of between $5-10 \mathrm{~mA}$ although one of the popular plug-in types manufactured by Omron, Siemens or Keyswitch would be suitable.

# Practical Wireless and Practical Television Filmshow 

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This article describes the theory of metal detection and gives realistic assessment of the performance expected. A practical circuit and constructional details are also given.

BEFORE even explaining the function of this project it is important to place home constructed metal detectors in perspective. They are great fun and within their limitations very useful but they are not practical for any but the most rudimentary form of treasure hunting. Using the techniques described here, and another technique described later, a maximum of about 18 in . is the greatest detection range under ideal conditions and this is reduced to about 1 in . under difficult ones.

The author has seen great claims made for the type of circuit used here but this has never been borne out in practice. Certainly there are metal detectors made which are very much better than the one shown but they cost hundreds of pounds and require great skill and experience to operate. The cost of the project here is unlikely to exceed 50s. including the headphones.

However even with the limitations mentioned, the finished project has considerable uses. Tracing house wiring is the most practical but it can also provide endless hours of fun and is easily adapted to a variety of games for fête side-shows etc.

## METAL DETECTION THEORY

There are two common ways in which metal detectors work. The less common and more difficult type (from the point of view of construction) is to have an audio oscillator which relies on the feedback to maintain oscillation being connected through two coils at right-angles to each other. The gain of the oscillator is set so that oscillation is not quite achieved. When the coils are moved into the proximity of an object-especially a metal one -the coupling between the coils is increased causing oscillation to start.

The second more common type makes use of two oscillators, one of which is at a fixed frequency. The second oscillator is tuned near the frequency of first but its inductance takes the form of a search coil. When this comes into the proximity of some material which increases its inductance the frequency alters and beats with the reference oscillator, producing a beat note in the form of an audible tone whose frequency (but not intensity) varies with the inductance of the search coil.

The limitations of this type of detector are governed by the fact that any material can vary the inductance although metals have a very much


The prototype of the metal locator.
greater effect than others. A large stone, however, will produce a similar effect to a small nail and it will be quickly appreciated that searching for materials in anything but a few inches of earth is frustrated by many other effects.
The frequencies of the oscillators are not too critical but must lie between about 100 kHz and 1 MHz . Below 100 kHz it is hard to detect the change in note since a $0.5 \%$ increase in inductance for instance will alter the frequency by only a few Hertz. Above 1 MHz almost anything will change the inductance enough to send the beat note way out of audio range since a $0.5 \%$ change will have a considerable effect.
The reference frequency chosen was approximately 450 kHz , or in other words the commonest i.f. frequency; this has several advantages. First, an i.f. transformer can be used to produce the reference frequency, secondly the secondary of the transformer can be used as the take-off point for the audio amplifier thus providing a good impedance match and thirdly this frequency enables a standard radio set to be used instead of two of the stages shown. The metal detector circuit shown is self-contained but a simpler version will be described later.

## THE CIRCUIT

L1 is the search coil and is connected into a Hartley oscillator with a 250 pF trimmer as the tuning capacitor, C 1 as the feedback capacitor and R1 acting as the base bias resistor. The tuning capacitor is necessary since the frequency has to be tuned very closely to that of the reference oscillator and it can take account of strays that increase the inductance; In this way the background can be compensated for. The frequency must of course be set at the beginning of each search.


Fig. 1: The complete circult of the metal locator. Note that C2 Is not a physical component as it is stray capacilance; It is drawn here to
slmplify the explanatlon.

The i.f. transformer, $\operatorname{Tr} 2, \mathrm{C} 3$ and R2 are also connected to form a Hartley oscillator, the secondary of the i.f. transformer (in which the beat note is developed) couples to the simple amplifier comprising Tr 3 with associated bias resistors etc. The output is fed to the volume control. Head-phones-preferably good ones with an impedance of $2000 \Omega$-are plugged into the jack to monitor the beat note.

The coupling capacitor which connects the output of Tr 1 to the base of Tr 2 needs some explanation. This coupling has to be very, very small otherwise. one oscillator would trigger the other, clamping the two together. C2 was found unnecessary in practice and the loose coupling relied purely on strays.

## CONSTRUCTION

All the components, apart from the search coil, are fitted into a plastic soap box and are fixed to its lid. The majority of the components are fixed to a small piece of Veroboard, 0.15 in . matrix type, $6 \times 12$ holes; the actual layout is however uncritical.
The 250 pF capacitor is of the postage stamp compressor type. To make use of this it is necessary to remove the screw used for compressing the vanes and replace this with a screw of the same thread but one inch long; this will enable the knob to be fitted.
The search coil consists of twelve turns of enamelled copper wire, centre tapped, wound around a 3 in . square plastic box. The gauge of the wire is not very important-about 28 s.w.g. is right. The size of the box is not very important as a considerable amount of latitude is allowed for in tuning to bring it to the correct frequency. If a larger sized box is available fewer turns are needed, with a smaller one more turns. A plastic box is not essential and if difficult to obtain a 3 in . square of wood about lin. thick will do as an alternative. The windings around the former-whether it be plastic or wood-should be neat and tight and when finished should be covered with adhesive plastic tape or insulating tape.
The wires then run up a length of non-metallic tube which is connected at an angle of about $45^{\circ}$ to the soap box which is clamped to the other end. If a plastic tube is not available then wooden doweling of $\frac{1}{2}$ in. diameter will be a good substitute.

If the wires are run up through the tube a small amount of glue should be run down it to stop the wires flapping about; if doweling is used then the


Fig. 2: The component layout inside the soap box.


An Interior view of the prototype.
wires should be firmly taped to the side.
It is very important that the wires associated with the search coil are really firmly held for the detector makes use of the change in inductance and these are in the order of fractions of a per cent and loose wires or turns can easily cause this much when flapping about.

Continued on page 894

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## EALING \& DISTRICT AMATEUR RADIO SOCIETY G3UUP

ALOT of water has flowed under the proverbial bridge since the Ealing and District Amateur Radio Society was formed over four yeats ago in September 1965. After pestering the life out of the local Council to help provide club rooms for eight very enthusiastic Hams, we obtained our present QTH. This is quite unique and a "Palace" when one thinks of some of the very poor conditions in which some Clubs have to operate!

One room, about the size of an average living room is the actual shack in which are housed the stores, benches, tools and equipment. A larger room about twice the size of the shack adjoins and is used for lectures, filmshows, etc. These rooms are the only ones upstairs in the building, which looks something like a sports pavilion with a flat roof which is a radio Amateur's delight for putting up an antenna farm for which there are no restrictions.

The Society started off with the usual Top Band rig with 132 ft . end-fed wire which produced very fair results. Now most of the members are mobile on 4 m . with a couple on 2 and 160 m .

Whilst some of the SWL's have obtained their licences with the help of the Society, we have had two weddings amongst our celebrations, G3SGS and G3UDV. G3UDV married the daughter of G3TXB.

One side-line of the Society is putting on exhibition stations, three regulars being the Chiswick Town Exhibition for Adult Education, the Ealing Arts Council Hobbies Exhibition and the Brentford


The top picture shows the main tent at the RSGB Amateur Radio Mobile Rally 1969 held at Woburn Abbey.
The photograph above shows the Ealing and District Amateur Radic Soclety stand which was situated in the main tent. Here members sell donated components and gear to ald the Society funds.
The picture to the left shows the Society station with Bern., G3KLK (/eft) and Bill, G3SGT, on the mic


No, it's not the Ealing and District Amateur Radio Football Club with three reserves, it's a few of the members that we persuaded to say "cheese" when we went along to the Society QTH.

Evening Institute for the RAE and budding Hams.
The latest activity is attending mobile rallies around the London area and selling small components to raise funds for the Society which are still very healthy after buying a much-needed 230 V 1 kW petrol generator for our many field days.
We are a small Society but members are really keen. Over the four years membership has grown and more equipment has been acquired-much of this has been donated by members. With it, grew the Society's funds which started at $£ 8$--each founder-member donating $£ 1$ to get the Group under way. It would be grossly unfair to mention any names of dedicated members, because there have been so many that have made this Society the success that it is.

After the Ealing and District Amateur Radio Society was in full swing, with lectures and filmshows on anything from radio to old-time car racing, we began to think about weekend activities.

The Society went out on mad weekends (not dirty ones) everyone taking with them all types of equipment from the home QTH to operate /P. The Devil's Punch Bowl in Surrey was the first target which operated on $160,80,40$ and 2 m . with the YL's and XYL's cooking bangers and bacon and brewing the tea.

Many v.h.f. contests were and still are entered for, with excellent results. We have one prize award for
the first-ever recorded 13 cm . contact at v.h.f. NFD by G3THQ.
There are about thirty members at Ealing who are active from the Society on 2,4 and 160 m . under the call sign G3UUP.

This year, the Society will be holding a Mobile Rally at the Hanwell Community Association on May 10th.

It is thought that this will be the first time a rally has been held in London. The Automobile Association will do the signposting and will have their own exhibition caravan at the site. The Rally address will be: Hanwell Community Association, Westcott Crescent, Hanwell, London, W.7.

Meetings of the Ealing and District Amateur Radio Society are held every Tuesday evening at the Community Centre, 71a Northcroft Road, London, W. 13.

Further details about the Society and the Mobile Rally may be obtained by sending a s.a.e. to the Secretary, Bill Teale, G3SGT, 16 Whitestile Road, Brentford, Middlesex.
note to radio club secretaries If you would like to see your Club featured in Practical Wireless, drop a line to Colin R. Riches, IPC Magazines Ltd., Fleetway House, Farringdon Street, London, E.C.4.

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## RADIO EXCHANGE CO



A series of simple transistor projects, each using less than twenty components and costing less than twenty shillings to build.

THE multivibrator is one of the most widely used forms of oscillator and can be used for a variety of purposes. It is also one of the simplest forms and in this particular circuit we are making it operate small 0.75 W bulbs, flashing these at a frequency of about 1 Hz , the lights flashing alternately.

## THE MULTIVIBRATOR

The multivibrator works as follows: one of the transistors, when a voltage is applied to the circuit, will pass slightly more current than the other; for the sake of explanation we will assume that this is Tr1 but of course it doesn't matter which. Since it is passing more current its collector voltage will drop. This change will be fed to the base of $\operatorname{Tr} 2$ causing it to pass less current and so its collector voltage will rise. This action will cause $\operatorname{Tr} 1$ to be further switched on and this will go on until Tr1 is completely switched on and Tr 2 completely off. C 1 then charges up through R2 until the base of Tr 2 becomes positive enough to conduct, switching it on and in turn switching off Tr 1 -and so on.

As will be seen from the above, values of the resistors and capacitors affect the switching rate and by altering these it is an easy matter to choose your own flashing interval. To increase the rate decrease the values of R1, R2, C1 or C2 and to reduce the rate increase any of the values.

If we choose values so that the switching rate falls within the audio range and substitute resistors of $330 \Omega$ for the bulbs we could tap off the note from either collector via a capacitor. However in the form shown we are using the changing currents through the transistors to switch the bulbs on and off.

If only one flashing bulb is required a $330 \Omega$ resistor can substitute for the other bulb. The current consumption is fairly low using the specified bulbs-between 30 and 40 mA and most layer batteries will provide this.

As for uses it is up to you, but flashing lights make the ideal warning device. If used as such one of the bulbs may be replaced by an $80 \Omega$ loudspeaker or a lower impedance type with matching transformer to provide audible plops as well as having one flashing light.

## CONSTRUCTION

A suitable Veroboard layout is shown in Fig. 2 but of course the construction is uncritical; in the one shown none of the copper strips need be broken.
Make sure you use the specified bulbs as most types are unsuitable; these are a Radiospares product available from most component stockists and although they are rated at 14 V they give a very bright emission from only 9 V .

## No. 11 NOVELTY LIGHT FLASHER



Fig. 1: The circuit of the light flasher.


Fig. 2 : The component layout on a small piece of Veroboard.

## components list

| R1, R2 | 10k $\Omega \ddagger$ watt, $10 \%$ | 6d. |
| :---: | :---: | :---: |
| C1, C2 | $80 \mu \mathrm{~F} \mathrm{12V}$ | 3 s . 0d. |
| Tr1, Tr2 | 2N2926G | 5s. 0d. |
| LP1, LP2 | Radiospares 'Lilliput' bulbs, 14V, 0.75 W | 5s. Od. |
| Veroboard, Battery, Battery clips, etc. |  | 5s. Od. |
|  |  | 18s. 6d. |

Next month's Take 20 describes a simple lie detector which makes use of a multimeter. The circuit also is suitable for the measurement of very high resistance.

## Metal Locator - Continued from page 886

The length of the connecting tube or dowel is uncritical and will depend on usage, but in the prototype 12 in . was found to be a convenient length.

## USE WITH A TRANSISTOR RADIO

The circuit can be simplified by using a transistor superhet having an i.f. of between 450 and 470 kHz , if this is used the second and third stages are unnecessary (that is the reference oscillator and the audio amplifier). Since the circuit works on approximately the i.f. frequency it is only necessary to make the search oscillator work and beat with the i.f. in the receiver by placing it close to it. It is necessary to tune into a station and listen to the heterodyne produced.

## INITIAL SETTING UP

A transistor radio is all that is necessary for setting up. Place the radio near the soap box with it tuned to a station and adjust the core on the i.f. transformer until a beat note is heard. Then move

## components list

| Resistors |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | 1.5M $\Omega$ | R3 | 1M $\Omega$ |
| R2 | 1M $\Omega$ | R4 | $56 \mathrm{k} \Omega$ |
| All resistors $\frac{1}{4}$ watt $10 \%$ types. |  |  |  |
| VR1 $250 \mathrm{k} \Omega \log$ with switch. |  |  |  |
| Capacitors |  |  |  |
|  | 20pF | C4 | $0.1 \mu \mathrm{~F}$ |
|  | See text | C5 | $0.1 \mu \mathrm{~F}$ |
|  | 20 pF |  | 250pF trimme |
| Semiconductors |  |  |  |
| Tr1, Tr2 and Tr3 2N2926G |  |  |  |
| Miscellaneous |  |  |  |
| L1, search coil, see text: IFT1, 465kHz i.f. transformer; J1, headphone jack socket; Veroboard |  |  |  |

the radio near the search coil and adjust VC1 until a beat note is also heard. When the phones are plugged in and VCl is slightly adjusted the note will be heard in the phones.

The metal detector will now work as soon as the search coil is moved towards a metal object. It takes a little bit of getting used to before the necessary skills are acquired, but with practice operation is simple.

Just one small practical point in conclusion. Your ears are much more sensitive to a frequency change around 200 Hz than below or above and it is best to set the beat note in that region before starting the search. If the two oscillators are exactly together no change will be heard until the audible range is reached and this is probably about 80 Hz in the case of normal headphones.
I.C. of the Month - Continued from page 877


Fig. 2: Practical circult for the PA246 with 5 watts audio output. Alternatively, the PA237 may be used but the audio output will be 2 watts. Capacitor C3 is an electrolytic-the plus side should be taken to the junction of R3 and the loudspeaker.

## components list

| Resistors: |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | $680 \mathrm{k} \Omega$ | R5 | 82k $\Omega$ |
| R2 | $75 \mathrm{k} \Omega$ | R6 | $6.8 \mathrm{k} \Omega$ fo |
| R3 | 18 k ת |  | 0 for ma |
| R4 | 330 k ת | R7 | $22 \Omega$ |
| Capacitors : |  |  |  |
| C1 | $0.33 \mu \mathrm{~F}$ | C4 | $4 \mu \mathrm{~F} \quad 2$ |
| C2 | $0.001 \mu \mathrm{~F}$ |  | $0.05 \mu \mathrm{~F}$ |
| C3 | $500 \mu \mathrm{~F}$ |  |  |
| Miscellaneous: |  |  |  |
| Loudspeaker, any $15 \Omega$ impedance type. I.C. PA246 (PA237); General Electric Co. (U.S.A.) |  |  |  |

a suitable amplifier circuit for use with the PA246; it should be preceeded by a conventional tone control and volume control circuit. The experienced constructor will find no difficulty in laying out a suitable printed circuit, or assembling a prototype on Veroboard with separate copper heat sinks.

## BLUEPRINT SERVICE

We would like to draw readers' attention to the fact that the BLUEPRINT SERVICE has been discontinued and therefore no further BLUEPRINTS are available.

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The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output of 5 watts R.M.S. ( 10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 Zener diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.
The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of such components as tone and volume controls and a battery or mains powe supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c.' coupled throughout) etc. The photographic masks required as part of the process of producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. This enables us to cover every IC-10 with the Sinclair guarantee of reliability.

## - SPECIFICATIONS

Output 10 Watts peak, 5 Watts R.M.S. continuous.

Frequency response
5 Hz to $100 \mathrm{KHz}^{2} 9 \mathrm{~dB}$. Total harmonic distortion Less than $1 \%$ at full output. Load impedance Load impedance gain $110 \mathrm{~dB}(100,000,000,000$ times) total. Supply voltage 8 to 18 volts. Size Sensitivity Input impedance

## CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class A8 output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, miaking battery operation eminently satisfactory.

## APPLICATIONS

Each IC. 10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

## SINCLAIR


2.30

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Hi-fi amplifisr; car radio amplifier; record player amplifier fed directly from pick-up; intercom; electronic music and instruments; P.A.; laboratory work, etc. Full details for these and many other applications are given in the manual supplied with the $\mathbf{Z . 3 0}$.


## SPECIFICATIONS

Power output: 15 watts R.M.S. into 8 ohms using a 35 volt supply; 20 watts R.M.S. in to 3 ohms using a 30 volt supply.

Output: Class AB
Frequency response: 30 to $300,000 \mathrm{~Hz}$ 1 dB .
Distortion : 0.02\% total harmonic distortion at full output into 8 ohms and at all lower output levels.
Signal-to-noise ratio: better than 70 dB unweighted.
Input sensitivity: 250 mV into 100 Kohms. Damping factor: >500.
Loudspeaker impedances: 3 to 15 ohms.
Power requirements: From 8 to 35V. d.c. (The $Z .30$ will operate ideally from batteries if required).
Size: $3 \frac{1}{2} \times 2 \frac{1}{4} \times \frac{1}{2}$ inches.

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The Stereo-60 may also be used with 2 IC-10's or any other high performance amplifiers.

## SPECIFICATIONS

- Input sensitivities-Radio-up to 3 mV Magnetic Pickup - 3 mV ; correct to R.I.A.A. curve $\pm 1 \mathrm{~dB} ; 20$ to $25,000 \mathrm{~Hz}$. Ceramic Pickup-up to 3 mV : Auxiliary -up to 3 mV .
- Output-250mV
- Signal-to-noise ratio-better than 70 dB .
- Channel matching-within 1 dB .
- Tone Controls-TREBLE +15 to -15 dB at 10 kHz . BASS +15 to
-15 dB at 100 Hz .
- Power consumption 5 mA.
- Front panel-brushed aluminium with black knobs and controls.
- Size $8 \frac{1}{4} \times 1 \frac{1}{2} \times 4$ ins.


## PZ. 5 POWER SUPPLY UNIT

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Q.16 Loudspeaker and Micromatic on next page.


## SINCLAIR 0.16

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[^5]
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