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| 1R5 | $5 / 9$ | 20P3 11/9 | DL92 | 5/9 | EL84 4/9 | PENA4 12/6 | UCC85 | 6/9 |
| 185 | $4 / 3$ | 20P4 18/6 | DL94 | 6/- | EL90 4/6 | PFL20011/9 | UCF80 | $7 / 8$ |
| 174 | $2 / 9$ | 25L6GT 5/- | DL9 | 71 | EL500 12/6 | $\begin{array}{ll}\text { PL } 86 & 9 / 9\end{array}$ | UCH42 | 1/6 |
| 384 | $5 / 9$ | 2504GT11/6 | DY | 5/9 | EM80 7/6 | PL81 7/3 | JCH81 | 6/8 |
| 3 V 4 | 61- | $30 \mathrm{Cl} \quad 6 / 6$ | DY87 | 5/9 | EM81 7/6 | PL82 6/6 | UCL | $6 / 9$ |
| 5U4G | 4/6 | $30 \mathrm{Cl5}$ 13/- | EABC8 | 6/6 | EM84 6/6 | PL83 6/6 | UCL | 11/6 |
| 5 Y 3 Gr | 5/9 | $30 \mathrm{Cl7} 16$ /- | EAF42 | 10/- | EM87 7/6 | PL84 6/6 | UF41 | 10/6 |
| 5Z4G | 7/6 | 30 C 18 11/6 | EB91 | $2 / 3$ | EY51 7/6 | PL500 13/- | UF80 | $7 /-$ |
| $6 / 30 \mathrm{~L} 2$ | 12/- | $30 \mathrm{F5}$ 18/- | EBC33 | .81- | EY86 6/6 | PL504 13/6 | UF85 | $6 / 9$ |
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| $6 \mathrm{AQ5}$ | 4/6 | 30FL14 12/- | EBF89 | $6 / 3$ | Ez80 4/6 | PM84 7/6 | UL44 | 201- |
| 6 AT6 | 4/- | $30 \mathrm{LI} \quad 6 / 6$ | ECC81 | $3 / 9$ | EZ81 4/9 | $\begin{array}{ll}\text { PX25 } & 10 / 6\end{array}$ | UL84 | - |
| 6AU6 | 4/6 | 30 L 15 14/- | ECC82 | $4 / 9$ | GZ32 8/9 | PY32 10/- | 84 | 6 |
| A6 | 4/6 | 30 L 17 15/6 | ECC83 | $71-$ | 2334 619 | PY33 10/- | Y4 | 16 |
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| 6 F14 | 91- | 30PL13 15/6 | ECF82 | $5 / 9$ | PC86 10/3 | PY800 7/6 | Transi |  |
| 6 F 23 | 14/3 | 30PL14 15/6 | ECES5 | 6/- | PC88 10/3 | PY801 6/9 | AC107 | 8/6 |
| 6 F 25 | 13/- | 35L6GT 8/6 | ECE42 1 | 12/6 | PC96 8/6 | R19 6/6 | ${ }_{4} \mathbf{C l 2 7}$ | $2 / 6$ |
| 6 6 6 | 3/- | 35W4 4/6 | ECE81 | 5/3 | $\begin{array}{lr}\mathrm{PC} 97 & 8 / 6\end{array}$ | $\begin{array}{ll}\mathrm{R} 20 & 12 / 6\end{array}$ | AD140 | $7 / 6$ |
| 6 K 7 G | $2 / 6$ | 3524GT 5/- | ECR84 | $7 / 6$ | PC900 $7 / 6$ | U25 13/- | AF115 | 1 |
| 6 K 8 G | $2 / 9$ | 6063 12/6 | ECL80 | $6 / 9$ | PCC84 6/6 | U26 12/- | AF116 |  |
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| bV6G | $3 / 3$ | AZ31 9/6 | ECL83 | $8 / 6$ | PCC88 91 - | U49 13/6 | AF125 | A |
| 6V6GT | 6/6 | $\begin{array}{ll}\text { B729 } & 12 / 6\end{array}$ | ECL86 | 81- | PCC89 10/6 | Č2 4/6 | AF12 | 3/6 |
| 6 X 4 | 4/8 | ССН35 13/6 | EF37A | 6/6 | PCC189 11/6 | 078 | 0 O 26 | 5/9 |
| 6X5G | 5/9 | CL33 18/6 | EF39 | $4 / 9$ | PCF80 6/6 | U191 12/6 | OC44 | 3 |
| 7B7 | 7- | CY31 $6 / 9$ | EF41 1 | $10 / 9$ | PCF82 6/6 | U193 8/8 | $0 \mathrm{C45}$ | $2 / 3$ |
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## TRANSISTOR RADIOS TO BUILD YOURSELF

Backed by after sales service

## NEW! roamer eight mkI WITH VARIABLE TONE CONTROL

7 Tunable Wavebands: Medium Wave 1, Medium Wave 2, Long Wave, BW1, BW2, gW3 and Trawler Band. Built in Ferrite Rod Aerial for Medium and Long Waves. Five section 22 in . chrome plated Telescopic aerial for Short Waves can be angled and rotated for maximum per
 sooket. Aelectivity switeh. 3 wifodes. Famous make 7 in . $\mathbf{x} 4 \mathrm{in}$. Speaker. Air spaced ganged tuning condenaer. On/Ofi switch volume control. Wave change switch and tuning control. Attractive case in rich chestnut shade with gold blocking. Size $9 \times 7 \times 4 \ln$. approx. Easy to follow instructcase in and diagrams make the Roamer Eight a pleasure to
ious
build.


Parts Price Lith and Easy Build PJans 5/- (EREE with parts).
P\& P7/6.

## roamer seven mkIV

gEVEN FULLY TUNABLE WAVE-BANDS-MW1, MW2, LW. SWl, SW2, SW3 and Trawler Band. Extra Medium waveband provides easier Built in ferrite rod aerial for Mediom and Long Waves. Five Section 222 in . chrome plated telescopic aerial for short waven-can be angled and rotated for peak S.W. listening. Socket for Car Aerial. Powerful pushpull output. Seven Eramistors and R.F. Transistors. Famous make $7 \times$ sin P.M. speaker. Air spaced ganged tuning condenser. Volume/on/on control, wave change switches and tuning control. Attractive case with carrying handle. Size $9 \times 7 \times$ tin.
approx. Easy to follow instructions and diagrams make the Roamer 7 a pleasure to bulld. Parte price
(FREE wist parts). Personal Earpiece with switched socket tor (FREE With parts), Personal
private listening, $5 /$ - extra.


## Totel building costs $8 . \underbrace{}_{\text {P.\& P. 7/6 }}$

## pocket five

MEDIUM WAVE, LONG WAVE AND TRAWLER BAND PORTABLE WITH SPEAKER AND EARPIECE
Attractive black and gold case. Slize $5 \frac{1}{2} \times 1 \frac{1}{4} \times$ 3 in. Tunable over both Medium and Long Waves With extended M.W. band for easier tuning of diodes, supersensitive ferrite rod aerial, fine tone moving coil speaker, aloo Perbonal Earpiece with switched socket for private Hatening. Easy build plans and parts price ist 1/6 (FREE with parts).


Total building costs
$44^{\prime} 6 \underset{\substack{\text { p.g. } \\ 3,6}}{\substack{\text { p }}}$

## transona five

MEOIUM WAVE, LONG WAVE ano trawler band portable WITH SPEAKER AND EARPIECE

Attractive case with red greaker grille. size $67 \times 4 \ddagger \times 1$ tinc. 7 stage-s transistors and diodes, territe rod aetrial, tuning condenser,
 also Personal Earpiece with switched socket parts price list $1 / 6$ (FREEE with parts).

## NEW!

 trans eight SIX WAVEBAND PORTABLE WITH 3in. SPEAKER Attractive case in black with red grille and cream knobs and dial with polished brass inserts. Size 9 x $5 \frac{1}{4} \times 2 \frac{8}{8} i n$ approx. Tunable on Mediuu and Long Waves, three Short Waves and Trawler Band. Sensitive ferrite rod aerial for M.W. and L. W Telescopic aetial for Short Waves. Eight improved type transistors plus 3 diodes. Push pull output. Ample power to drive a larger speaker. Parts price list and easy build plans 5/- (FREE with parts). Earpiece with switched socket for private listening 5/-extra.Total building costs
P \& P 5/6
89'6

## roamer six

SIX WAVEBAND PORTABLE
WITH 3in. SPEAKER
Attractive case with gilt fittings. Size $7 \mathrm{x} \times 5 \mathrm{x}$ 1 ijn . Tunable on Medrum zad Long waves, two short waves, Trawler Band Plus an ertra M.W. band for easiar tuning of Luzembourg, etc, Sensitive waves. 8 stages- 6 transistora and 2 diodes including Miero-Alloy R.F. Transistors etc. (Cartying strap $1 / 6$ extra). Easy bulld plans and parts price list $2 /$ /. (FREE with parts)


Total building costs


* Callers side entrance Stylo Shoe Shop
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## RADIO EXCHANGECO



# Complete stereo system - 28 gns. 

The new Duo general-purpose 2-way speaker system is beautifully finished in polished teak veneer, with matching vynair grille. It is ideal for wall or shelf mounting either upright or horizontally.
Type 1 SPECIFICATION:-
Impedance 10 ohms. It incorporates Goodmans high flux $6^{N} \times 4^{\prime \prime}$ speaker
 Type 2 as type 1. Size $17 \frac{1}{\prime \prime}^{\prime \prime} \times 10 \frac{3}{2}^{\prime \prime} \times 6 \frac{7}{\prime \prime}^{\prime \prime}$. Incorporating $10 \frac{1}{\prime \prime}^{\prime \prime} \times 6 \frac{1}{*}^{\prime \prime}$ bass unit and $2 t^{\prime \prime}$ tweeter: 3 ohms impedance $5 \frac{1}{f}$ guiness plus $7 / 6$ p. \& p.
Gartara Cfiangers trom E7.19860.p. $8 \mathrm{p} .7 / 6 \mathrm{~d}$.
Cover and Teak finish Plinth E4.15.0d. 7/6d. p. \& p.
The items illustrated can be purchased togecher for 28 gns

The Duetto is a good quality amplifier, attractively styled and finished. It gives suparb reproduction previously associated with amplifiers costing far more.
SPECIFICATION:-
R.M.S. power output: 3 watts per channel into 10 ohms speakers.

INPUT SENSITIVITY: Suitable for medium or high output crystal cartridges and tuners. Cross-talk better than 30 dB at $1 \mathrm{Kc} / \mathrm{s}$.
CONTROLS: 4-position selector switch (2 pos. mono and 2 pos. stereo) dual ganged volume control.
TONE CONTROL: Treble lift and cut. Separate on/off switch. A preset balance control.


The above 5 items can be purchased together for $\mathrm{f} 29.10+$ f1.10.0 p. \& p.

Controls: Selector switch Tape speed equalisation switch ( $3 \frac{3}{2}$ and $7 \frac{1}{2}$ i.p.s.) Volume. Treble. Bass. 2 position scratch filter and 2 position rumble filter.
Specification: Sensitivitles for 10 watt output at 1 KHz into 3 ohms. Tape head:
 Tape/Rec. output: Equalisation for each input is correct to within $\pm 28 \mathrm{~B}$ (R.I.A.A.) from 20 Hz to 20 KHz . Tone control range; Bass $\pm 13 \mathrm{~dB}$ at 60 Hz . Treble $\pm 14 \mathrm{~dB}$ at 15 KHz . Total distortion: (for 10 watt output) $<1.5 \%$. Signal nolss: $<-60 \mathrm{~dB}$. A.C. mains $200-250 \mathrm{v}$. Built and tested. Size $12 \frac{2}{2} \mathrm{in}$. long, $4 \frac{1}{2} \mathrm{in}$. deep, $2 \frac{2}{2} \mathrm{in}$. high. Teak finished case.

. Whe O/iscount
£14.5 plus $7 / 6 \mathrm{p}$. \& p .
Integrated High Fidelity Transistor Stereo Amplifier. Specification-Output: 10 watts per channel into 3 to 4 ohms speakers ( 20 watts monaural). Input: 6 positlon rotary selector switch ( 3 pos. mono and 3 pos. stereo), P.U.. Tuner Tape and Tape Rec, out. Sensitivities: All inputs 100 mV into 1.8 M ohm. Frequency Response: $40 \mathrm{~Hz}-20 \mathrm{KHz} \pm 2 \mathrm{~dB}$. Tone Controls: Separate bass and treble controls; treble, 13 dB 1 ft and cut (at 15 KHz ); Bass, 15 dB lift and 25 dB cut (at 60 Hz ). Volume Controls: Separate for each channel. A.C. Malns input: 200 $240 \mathrm{~V}, 50-60 \mathrm{~Hz}$. Slze, $12 \frac{1}{\prime \prime}^{\prime \prime} \times 6^{\prime \prime} \times 22^{\prime \prime}$ In teak finished case. Built and tested.
VISCOUNT MARK II for use with magnetic pick-ups specification as above. Fully equalised for magnetic pick-ups. Sultable for cartridges with minimum output of $4 \mathrm{mV} / \mathrm{cm} / \mathrm{sec}$. at 1 kc . input impedance 47 k . £ $\mathrm{E} 15.15 \mathrm{plus} 7 / 6 \mathrm{p}, \& \mathrm{pe}$


## SPECIAL OFFER!

Complete stereo system comprising BALFOUR 4-speed autoplayer with head, 2 Duo speaker systems, size 12 in . $\times \frac{6}{4} \mathrm{in}$. $\times \frac{5}{4} \mathrm{i} \mathrm{n}$. Plinth (less cover) and the DUETTO stereo amplifier. All above items
£20 plus 20/-p. \& p.


FREE WITH PARTS

The ELEGANT SEVEN
Mk. III (350mW Output)
7 transistor fully tumable M.W.-L.W. superhet portable. Set of parts. Complete with all components, including ready etched and drilled printed circuit board-back Mrimed for fowiproof construction.

Price $£ 4.9 .6$ plus 7/6 P. \& P.

## The DORSET

( 600 mW Output)
7 -transistor fully tunable M.W.-L.W. superhet portable -with baby alarm facility. set of parts. The latest simple to build. Sizes: $12 \times 8 \times 3$ in.

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MAINS POWER PaCK KIT: 9/6 extra


## EXTRACTOR FAN

A.C. mains $230 / 250 \mathrm{v}$. complete with pull switch Size $6 \times 6 \times 4$ in.
Price 27/6 plus 7/6 P. \& P.

## X101

## 10W SOLID-STATE HI-FI AMP WITH INTEGRAL PRE-AMP

Specifications: $P_{\text {ower }}$ Output (into 3 ohms speaker) 10 watts. Sensitivity (for rated output): 1 mV into 3 K ohms $(0.33$ microamp) Frequency Response: Minus 3 dB points 20 Hz and 40 KHz . Speaker: $3-4$ ohms ( $3-15$ ohms may be used). Supply voltage: 24 V . D.C. at 800 mA ( $6-24 \mathrm{~V}$. may be used).

Price $69 / 6$ plus $2 / 6$ P. $\& P$.
Control assembly: including resistors and capacitors. 1. Volume: PRICE 5/-. 2. Treble


Power Supplies for the X101:
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## CAR TRANSISTOR IGNITION SYSTEM

## by famous manufacturer

For 6 volt or 12 volt positive earth systems. Comprising : special high voltage working hermetically sealed silicon transistor mounted in finned heat-sink, high output ignition coil, ballast resistor and hardwear (screws, washers etc.).

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50 WATT AMPLIFIER A.C. Mains $\mathbf{2 0 0 - 2 5 0 V}$

an extremely reliable general purpose rave amplifier. Its rugged construction yet space age styling and design make far the best value for money.
TECHNICAL SPECIFICATIONS 3 electronically mixed channels, with 2 inputs per chanuel, enables the use of 6 separate instruments at the same time. the volume controls for each channel are located directly above the corresponding input sockets. SENSITIVITIES AND
 plus 20/-p. \& p. 4 mV at 470 K . These 2 channeis ( 4 inputs) are suitable for microphone or guitars Channels $3 \& 4300 \mathrm{mV}$ at 1 m . Suitable for most high output instruments (gram, truner, TO ALL INPUTS. Bass Boost +12 dB at 60 Hz . Bass Cut -13 dB at 60 Hz . Treble Boost TO ALL INPUTS. Bass Boost +12 dB at 60 Hz . Bass Cut -13 dB at 60 Hz . Treble Boost
+11 dB at 15 KHz . Treble Cut - 12 dB at 15 KHz . With bass and treble controls central -3 dB points are 30 Hz and 20 KHz . POWER OUTPUT: For speech and music 50 watts rms. 100 watts peak. For sustained music 45 watts rms. 90 watts peak. For sinc wave $38 \cdot 5$ watts rms. Nearly 80 watts peak. Total distortion at rated output $3.2 \%$ at 1 KHz . Total distortion at 20 watts $0.15 \%$ at 1 KHz . Output to match into 8 or 15 ohms speaker system. NEGATIVE FEEDBACK 20 dB at 1 KHz . SIGNAL TO NOISE RATIO 60dB MAINS VOLTAGES adjustable from $200-250 \mathrm{~V}$. A.C. $50-60 \mathrm{~Hz}$. A protective fuse is located at the rear of unit. Output impedance 3, 8 and 15 ohms.

## B.S.R. TD-2 TAPE DECK

Takes $5_{\frac{1}{2} \text { in. }}^{2}$ spools, fitted with B.S.R. $\frac{1}{2}$ Track Heads. size $13 \frac{1}{4} \mathrm{in}$. long by $8 \frac{8}{4}$ in. wide Price $£ 8.19 .6$ plus $7 / 6 \mathrm{P}$. \& P .


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SOLID STATE
GENERAL
PURPOSE
AMPLIFIER

## 6

PECILICATIONS
Output Impedance-- 3 to 4 ohms Inputs-1. -xtal mic 10 mV Tone Controls-Treble control range $\pm 12 \mathrm{~dB}$ at 10 KHz Frequency Response-(with tone controls central) Minus 3 dB points at 20 Hz and 40 KHz Signal to Noise Ratio-better than -60dB. Transistors- 4 silicon Planar type and 3 Germanium type. Mains input-220/250V. A.C. Size of chassis- $-10 \frac{1^{\prime \prime}}{} \times 43^{\prime \prime \prime} \times 24^{\prime \prime \prime}$. For use with Std. or L.P. records, musical instruments, all makes of pick-ups and mikes. Separate bass and treble lift control. Two inputs with control from gram. and mike. Built and tested. $8^{*} \times 5^{\prime \prime}$ speaker to suit price $14 / 6$ plus $1 / 6$ p. \& p. Crystal mike to suit $12 / 6$ plus $1 / 6$ p. \& p. RELIANTMK.\| IELIANTMK. II
As above less teak case
f5. 15 plus $7 / 6$ P. \& $P$.
In teak finished case
E6.16plus 7/6P. \& P.
RECORD PLAYER SNIP A.C. Mains 240V
The "Princess", 4 -speed automatic record changer and player engineered with the utmost precision for beauty, long life, and trouble free service. Will take up to ten
records which may be mixed $7^{\prime \prime}$ to $10^{\prime \prime}$ or $12^{\prime \prime}$. Patent stylus brush cleans stylus after each playing and at shut off, the pick-up locks itself into its recess, a most useful feature with portable equipment-other features include pick-up height adjustment and stylus pressure adjustment. This truly is a fine instrument which you can purchase this month at only $£ 5.19 .6$ complete with
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## POCKET MULTI-METER

Size $3_{8}^{7} \times 2 \frac{1}{8} \times 1 \frac{3}{3} \mathrm{in}$. Meter size $2 \frac{1}{8} \times 1_{8}^{3} \mathrm{in}$. Sensitivity 1,000 O.P.V. on both A.C. and D.C. volts. $0-15,0-150,0$ 1,000 D.C. current $0-150 \mathrm{~mA}$. Resistance 42/6 plus $3 / 6 \mathrm{P}$. \& P.
FREE GIFT for limited period only. 30 watt Electric Soldering Iron value 15/- to every purchaser of the Pocket Multi-Meter.

## STEREO PRE-AMPLIFIER

Inputs- 6 position rotary switch ( 3 position mono, 3 position stereo). Tuner 150 mW into 680 k . Hagnetic pick-up fully equalised and suitable for magnetic cartridges with minimising output of $4 \mathrm{mV} / \mathrm{cm} / \mathrm{sec}$. Load 47 k . Ceramic pickup 150 mV into 680 k . Sensitivities taken for 200 mV output. Controls-separate volume controls for each channel. Twin ganged bass, 12 dB lift and 15 dB cut at $60 \mathrm{c} / \mathrm{s}$. Twin ganged treble,
10 dB lift and 15 dB cut at $10 \mathrm{kc} / \mathrm{s}$.Voltage required $23-30 \mathrm{~V}$ D at 5 mA . Size $12 \frac{1}{2} \mathrm{x}$ $3_{2}^{1} \times 2 \frac{3}{k} \mathrm{in}$. In teak finished case, complete with front panel and knobs. Built and tested.
£7.7.0 plus 5/- P. \& P.

## CYLDON 2 TRANSISTOR U.H.F. TUNER <br> Brand new. Complete with circuit diagram. <br> Price $£ 2.10 .0$ plus 1/- P. \& $P$

## THREE-IN-ONE HI-FI 10 WATT SPEAKER

A complete Loud Speaker system on one frame, combining three matched ceramic magnet speakers with a low loss crossover network. Peak handing power 10 watts. Impedance 15 ohms. Frux density 11,000 gauss. Resonance $4060 \mathrm{c} / \mathrm{s}$. Frequency range $50 \mathrm{c} / \mathrm{s}$ to $20 \mathrm{Kc} / \mathrm{s}$. Size $13 \frac{1}{2} \times 8^{1} / 16 \times 4 \frac{1}{2} \mathrm{in}$. By famous manufacturer.

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\text { List price } £ 7 \text { OUR PRICE } 74 / 6 \text { plus } 5 /-P \text {. \& P. }
$$ similar speaker to the above without tweeters in 3 and 15 nhms $44 / 6$ plos $5 /-\mathrm{p} . \& \mathrm{p}$.

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Push Button Tuning Heart
This PRESTOLOCK 5 station Push-Button Tuner Heart with Manual Over-ride is an ideal basis for a quality AM car radio. Size $6 \frac{1}{2}{ }^{\prime \prime} \times 4^{\prime \prime} \times 2^{\prime}$.

25/- plus 3/- P. \& P.

## QUALITY MAINS TRANSFORMER

Input 250 volts. OUTPUT (All RMS values) 4 windings of 11.5 wits connected in series total 46 volts at 4.5 anips (con1. $23-0-23$ volts. 2.46 volts.

Both of these above voltages are commonly used in medium to high powered transistor amplifiers, power supplies, etc. Price $35 /-$ plus $7 / 6$ P. \& $P$.

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No batteries-no wires. Just plug in the mains for lnstant two-way, loud and clear communication On/otl switch and volume control. Price 12 gna


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| C | 1/20w | 5\% | $100 \Omega-320 \mathrm{~K} \Omega$ | E12 | 16 | 14 | 13 |
| C | 1/8W | 5\% | $4.7 \Omega-1 \mathrm{M} \Omega$ | E24 | 2.5 | 2 | 1.75 |
| C | 1/4W | 10\% | $4.70-10 \mathrm{M} \Omega$ | E12 | 2.5 | 1.75 | 1.5 |
| C | 1/2W | 5\% | $4.78-10 \mathrm{M} \Omega$ | E24 | 3 | 2.25 | 2 |
| MO | 1/2W | 2\% | 100-1M ${ }^{\text {d }}$ | E24 | 9 | 8 | 7 |
| C | 1w | 10\% | 4.2 $2-10 \mathrm{M} \Omega$ | E12 | 4 | 3.25 | 3 |
| WW | 1W | $10 \%+1 / 20 \Omega$ | $0.22 \Omega-3.3 \Omega$ | E12 | 15d all | ities |  |
| Ww | 3W | 5\% | 12s-10K $\Omega$ | E12 | 15d all | ities |  |
| WW | 7 W | 5\% | $12 \Omega-10 \mathrm{~K} \Omega$ | E12 | 15 d all | ities |  |
| Codes: | $\begin{array}{r} c= \\ M 0= \\ W W= \end{array}$ | film, high sta xide, Electrosil ound, Plessey. | ility, low noise. 1 TR5, altra low | oise. |  |  |  |
| Values: <br> Prices | E12 deno E24 deno n pence ea | es: $1,1.2,1.5$, es: as E12 plu ach ohmic valu | $1.8,2.2,2.7,3.3$ <br> 1.1, 1.3, 1.6. 2, <br> and power ratin | 3.9, 4.7, 5. <br> 4, 3, 3.6, <br> (Ignore fr | 8, 8.2 a 5.1, 6.2 ons of | ir decad <br> .1 and $t$ <br> ny on tot | ecades. istor ord |

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25 WATTS PER CHANNEL As above but Output per channel into 25 WATTS PER CHANNEL As above but O
$15 \Omega 25$ watts R.M.S. Price $\mathbf{5 5 3} / 15 /-$ Net
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$40 / 2.5: 50 / 6.4 ; 50 / 25 ; 50 / 40 ; 64 / 4 ; 6410 ;$ 80/2.5; 80/16; $80 / 25 ; 100 / 6.4 ; 125 / 4 ; 125 / 10$ $125 / 16 ; 160 / 2.5 ; 200 / 6.4 ; 200 / 10 ; 250 / 4 ; 320$ $2.5 ; 320 / 6.4 ; 400 / 4 ; 500 / 2.5$.

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Carr. 12 * Performance comparable with units costing it with considerably more. Consists of (1) $12 i n$. 15 watt Bass unit with and ceramic magnet. (2) 3-way quarter section series cross-over system. (3) 8 x 5 in . high flux middle range 'speaker. (4) High effiency tweeter. (5) Woolien acoustic damping material. (6) Dep.£5.10.6 and 9 monthly payments $39 /-(T o t a l ~ £ 23.1 .0$ ).
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vity 36 mV . Suitable for high impedance vity 36 mv. Suitable for high impedance microphones, Crystal or Ceramic P. S' De-
signed for Club, Schools, Theatres, Dance
etc. For use with Electronic Orean, Guitar, Halls or Outdoor Functions, etc. For use with Electronic Organ, Guitar, String Bass, etc. Gram, Radio or tape. Reservel vols so that two separate Tuner. Two inputs with associated volume controns "Mike" can be mixed. $200-250 \mathrm{v}$. $50 \mathrm{c} / \mathrm{s}$ A.C. mains. For 3 and 15 ohm speakers. Complete kit of parts with point- 15 Gins Carr. Twin-handled perforated cover $27 / 6$. Supplied factory built with EL34 output valves. 12 months' guarantee for 18 gns. TERMS: Deposit £6.3.0 and
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 PUSE-PULL ULTRA LINEAR OUTPUT Two input sockets with associated controls Two input sockets with associated controls allowing mixing of "mike" and gram, etc, etc. HZgh sensitivity 5 valves-ECC83 wound output transformer. IND. BASS AND TREBLE CONTROLS. Frequency response $\pm 3$ dB $30-20,000 \mathrm{c/s}$. Hum level - 60 dB . SENSITIVITY 40 millivolts. "mikes". For Musical Instruments such as String Bass, Electronic Guitars etc. Size approx. $12 \times 9 \times 7 \mathrm{in}$. For AC mains $200-250 \mathrm{v}$. $50 \mathrm{cps} \quad \mathbf{9} \frac{1}{2}$ Gins.
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 An exception-
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unit for unit for lead, rhythm, bass guitar, vooal-
ists, gram, ists, gram,
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6a. 15/9.
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FULLY GUARANTEED. Interleaved and Impreg-
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250v.
$50 \mathrm{c} / \mathrm{s}$. MIDGET CLAMPED TYPE $2 \frac{5}{8} \times 25 \times 21 \mathrm{in}$, $250 \mathrm{v} ., 60 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a}$.
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$17 / 11$
$18 / 11$
FULLY SHROUDED UPRIGHT MOUNTING $250-0-250 \mathrm{v} .60 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a} ., 0-5-6 \cdot 3 \mathrm{v} .2 \mathrm{a}$. $250-0 \cdot 250 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$
$300-0-300 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., 0-5-6 \cdot 3 \mathrm{v} 3 \mathrm{a}$ $300-0-300 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., 0-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$.
$300-0.300 \mathrm{v}$.
$130 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 a .$, c.t., $6 \cdot 3 \mathrm{v} .1$ For Mullard 510 Amplifier

| $350-0-350 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., 0-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$ |
| :--- |
| $350-0-550 \mathrm{v}$ |
| $150 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}, 4 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{v}, 3 \mathrm{a}$ | $350-0-350 \mathrm{v} .150 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., 0-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$

$425-0-425 \mathrm{v} .200 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}, 4 \mathrm{a} ., \mathrm{c} . \mathrm{t}, 5 \mathrm{v} .3 \mathrm{a}$. $425-0-425 \mathrm{v} .200 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a}$, , c.t., 5 v .3 a.
$425-0-425 \mathrm{v} .200 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., 6 \cdot 3 \mathrm{v} .3 \mathrm{a} ., 5 \mathrm{v} .3$ $425-0-425 \mathrm{v} .200 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} .6 \cdot 3 \mathrm{v} .3 \mathrm{a} ., 5 \mathrm{v} .3$
$450-0-450 \mathrm{v} .250 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a}$, c.t., 5 v .3 a. TOP SHROUDED DROP-THROUGH TYPE $250-0-250 \mathrm{v} .70 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a} . .0-5-6 \cdot 3 \mathrm{v}$. 2 a . $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .3 \cdot 5 \mathrm{a} . \mathrm{c} \cdot \mathrm{F} \cdot$ $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a}, 6 \cdot 3 \mathrm{v} .1 \mathrm{a}$.
$350-0-350 \mathrm{v} .80 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a} ., 0-5 \cdot 6 \cdot 3 \mathrm{v} .2 \mathrm{a}$ $350-0-350 \mathrm{v} .80 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a} ., 0-5-6 \cdot 3 \mathrm{v} .2 \mathrm{a}$.
$250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., 0-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$. $300-0-300 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., 0-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$ $300-0-300 \mathrm{v}$. $130 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., 0-5-6 \cdot 3 \mathrm{v}$. 1 a Suitable for Mullard 510 Amplifier $350-0-350 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a}$.
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$6 \mathrm{a} .22 / 9 ; 12 \mathrm{v} .1 \mathrm{a} .9 / 11 ; 12 \mathrm{v} .3 \mathrm{a}$. or $24 \mathrm{v} .1 .5 \mathrm{a} .23 / 9$; $0-9-18 \mathrm{v}$. $1 \frac{1}{a} \mathrm{a} .19 / 11$; 0-12-25-42v. $2 \mathrm{a} .31 / 9$.
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Standard Pentode 5,000 $\Omega$ or $7,000 \Omega$ to $3 \Omega$
Push-Pull 8 watts EL 84 to $3 \Omega$ or $15 \Omega$ Push-Pull 8 watts EL 84 to $3 \Omega$ or $15 \Omega$ Push-Pull 10 watts 6V6 ECL86 to 3, 5, 8 O. 150 14/9 $10 \cdot 12$ watts $24 / 9$ $\begin{array}{lll}\text { Push-Pull Ultra Linear for Mullard 510, etc. } & 39 / 9\end{array}$ Push-Pull 15-18 watts, sectionally wound 6L6, Push-Pull 20 watt high quality sectionaily wound EL34, 6L6, KT66 etc. to 3 or $15 \Omega$ SMOOTHING CHOKES $150 \mathrm{~mA}, 7-10 \mathrm{H}, 250 \Omega 12 / 9 ; 100 \mathrm{~mA}, 10 \mathrm{H}, 200 \Omega 10 / 8 ;$
$80 \mathrm{~mA}, 10 \mathrm{H}, 350 \Omega 8 / 9 ; 60 \mathrm{~mA} 10 \mathrm{H}$

[^1]FANE POP 30c LOUDSPEAKERS 12in. $8-15 \Omega 25$ watts R.M.S. $\quad \mathbf{f 5 . 1 9 . 9}$

BSC
R.S.C. COLUMN SPEAKERS

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HI-FI GEMTRES LTD.

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In Teak or Afrommosia veneered Cabinets
$\mathrm{L} 1313^{\prime \prime} \times 8^{\prime \prime} 10 \mathrm{Watt}$


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All power ratings are R.M.S. continuous. 2 years' guarantee. High

POWER PACK KIT Consisting of Malns transformer. Metal
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MINI-8 HI-FI Loudspeaker Units Special Offer Teak or Arrormosia veneered cabinet
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Wgt I lb 7oz Price 23/9 PsP 4/6 $\begin{array}{llll}\text { Wgt } 5 \mathrm{lb} 1202 & \text { Price } 58 / 10 & \text { P\&P 6/- } \\ \text { Wgt } \\ 7 \mathrm{lb} & 8 \mathrm{oz} & \text { Price } 72 / 7 & \text { P\&P }\end{array}$ 30 VOLT RANGE


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 MT3 $\left.\begin{array}{lllllllll}102\end{array}\right)$

## BATTERY CHARGER TYPES



 $\begin{array}{lll}\text { MT47 } & 3 \text { Amp } & \text { Slize } 4 \times 3 \times 3 \text { inn. } \\ \text { MT5 } & 4 \text { Amp } & \text { Size } 4 \times 28 \times 3+\text { in }\end{array}$ $\begin{array}{lll}\text { MTS } & 4 \text { Amp } & \text { Size } 4 \times 21 \times 3 t i n . \\ \text { MT78 } & 0 \text { Amp } & \text { Slze } 4 \times 3 \text {. } \times 3 \text {. } \\ \text { Min. }\end{array}$
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## A Merry Christmas to all our readers!



TOPIC OF THE MONTH

THE optimists will soon be ringing out 1969 and hopefully heralding what they imagine will be a brighter new year. The pessimists will just groan and say things can't be worse. It's all a matter of viewpoint and temperament, but whatever these are one must first assess the retiring year before speculating on the one to come. We have done this with P.W.

Circulation figures and readers' letters remained at a high level, so we assume that most readers got what they wanted. During 1969 we published 194 articles and features, an average of 16 -plus per issue. Of these there were 7 on building amplifiers, 11 on receivers and front ends and 10 on test equipment. This apart from the projects under the Take 20 and IC of the Month banners, and constructional items in other categories.

On the semi-constructional and theoretical front there were series on repairing radio sets, pulse circuits, aerials, magnetic sound recording, semiconductor theory and 12 instalments of P.W. Guide to Components. Other articles ranged a varied field and took in home workshop practice, relays, power supply units, a stereo decoder, printed circuit design, a pedal steel guitar, etc.-and, of course, the regular news and comment features.

If we left anyone out during the year he must surely be a weird misfit! Having modestly patted our own editorial backs it is only just to convey our appreciation for the support from readers in the way of comments, criticisms, suggestions and letters of encouragement. And, of course, for sending along manuscripts for consideration; a high proportion of published material is the work of ordinary readers of P.W. So, to every one of you, from the regular subscribers to those who cadge a copy from a mate at the local club. . . .

## Alerxy Christmas 

 from W. N. STEVENSL. E. Howes, G3AYA<br>C. Riches<br>H. Moorshead T. R. Preece, G3TRP

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February issue will be published on January 9th.

[^2]VHF STEREO RADIO TRANSMITTING STATIONS ON RADIO 3



Peak Sound, the CirKit people have announced the "Englefield" cabinet for their amplifier modules. It is in kit form and includes components to complete a stereo amplifier based on the PA.12-15 Power Amp Module, the SCU/400 Stereo Preamp Module and the PS/45K Power Supply Kit. Cost of this kit is $£ 384 \mathrm{~s}$. for 12 W per channel system. Peak Sound, 32 St. Judes Road, Englefield Green, Egham, Surrey.

## SWANSEA COLLEGE SOCIETY

The University College of Swansea Amateur Radio Society is once again fully active with activities such as Morse code and R.A.E. tuition for students. Amateurs and listeners are also welcomed to the meetings and details may be obtained from: Rob Wilcox, Room 520, Neuadd Gilbertson, University College of Swansea, Singleton Park, Swansea, SA2 8PS.

## North Leeds Radio Club

 The North Leeds Radio Club has recently been formed. Will anyone wishing to join or visit this club please contact the Secretary, G. Brown, 2 Fearnville Close, Dib Lane, Leeds 8, Yorkshire.Desoldering the dry way


Southern Watch \& Clock Supplies Ltd. are UK selling agents for "Soder Wick"-a dry wick method of desoldering. As can be seen in the illustration, it is supplied in reel form and is used by direct contact with the joint together with a soldering iron for heating purposes.

Soder Wick draws the solder up into itself quickly and no excessive heat is required and the desoldered joint is left solderfree, pure and non-corrosive. Prices range from 18 to 20s. but for readers who would like to try it out there is a special offer, open until 31st December whereby they can get a sample for 16 s . Further particulars may be obtained from: Southern Watch \& Clock Supplies Ltd., Industrial Tools Division, 48/56 High Street, Orpington, Kent, BR6 0JH

## WEWS... NEWS... NEWS...

## SCOPE FOR SCHOOLS



A new oscilloscope, type EA 0699-1 has been announced by Mitre Electronic Products. It is intended mainly for use as a basic class oscilloscope in schools, and features a $2 \frac{3}{4}$ in. diameter tube with green medium persistence trace and the Y bandwidth is d.c. to 100 kHz . There is less than $100 \mathrm{mV} / \mathrm{cm} \mathrm{Y}$ sensitivity at maximum gain with full $Y$ shift and automatically synchronised timebase range is $100 \mathrm{mS} / \mathrm{cm}$ to $10 \mu \mathrm{~S} / \mathrm{cm}$ (approx.). X input with full X shift when timebase is off is $1 \mathrm{~V} / \mathrm{cm}$.
The oscilloscope is housed in an all-metal case measuring $6 \frac{1}{4} \times 6 \frac{1}{4}$ $\times 10 \frac{1}{4} \mathrm{in}$. Weight is 8 lb ., supply voltage, $200-250 \mathrm{~V} \quad 50-60 \mathrm{~Hz}$ and power consumption 25 W . It is fully guaranteed and price is. $£ 24$ 10s. ( 1 off) with a discount for schools. A data sheet is available. Mitre Electronic Products, 22 Powis Terrace, London, WII.

## LOW VOLTAGE AND ISOLATING TRANSFORMERS

Gardners Transformers Ltd., have introduced a range of open-style (Avon series) and enclosed style (Twynham series) Low Voltage and Isolating Transformers for input voltages of $100-125 \mathrm{~V}$ and $200-250 \mathrm{~V}$. This applies for sizes from $24 \mathrm{~V} / \mathrm{A}$ to $1 \mathrm{kV} / \mathrm{A}$ with a wide variation of output voltages. Further details in brochure GT. 17 obtainable from: Gardners Transformers Limited, Christchurch, Hampshire.

## Better Things are Electric

A new 16-page illustrated booklet in full colour designed to help people choose the right electrical fitting-plug, switch or socketfor every room in their home, is now available. Called "Better Things are Electric-with MK", it has been produced by MK Electric Ltd. It is available free on request from most electrical retailers or electricity showrooms, or direct from MK Electric Ltd., Edmonton, London, N9.

## SPLICER FOR CASSETTE TAPES

Bib Division of Multicore Solders Ltd., announce the introduction of the Bib Model $24 \frac{1}{8} \mathrm{in}$. cassette tape splicing and editing kit. It comes in a plastic wallet together with a plastic handled razor blade, Tape marker, reel of splicing tape on dispenser and a device for withdrawing tape from the cassette. The price is 29 s .

The kit has been specially designed for use in jointing tape from C60, C90 or C120 cassettes and is particularly useful as it enables music from pre-recorded cassettes to be joined so that the playing time of a single cassette is extended.

## It's 5 new pence



Multicore Ltd. announce an adjustment to their well-known 6 d. solder pack. It now costs twice the price but you get double the amount of solder (enough for 100 average joints). It has been given the reference " 2 D " and packages are marked 1s. or 5 p . Multicore Solders Ltd., Hemel Hempstead, Herts.

## Don't forget the Practical Wireless filmshow

## 100 WATTS FROM ADASTRA



Adastra Electronics Ltd. announce their "Centurion" 100W amplifier which has a suggested list price of $£ 99$ and features a hand-assembled 25 -transistor 6 -diode printed circuit construction. The four individually gain controlled inputs have a sensitivity range from 1 mV to 20 V . A feature of this amplifier is that its design allows its output (100W at $4 \Omega$; 140 W peak) to be open- or short-circuited without ill effect. The amplifier is housed in a black leathercloth cabinet with carrying handles and matching silver/black control panel. Adastra Electronics Ltd., 167 Finchley Road, London. N.W.3. Tel. 01-624 8164/5.


0NE of the main requirements for a microphone mixer is that of low noise level. Many of the cheaper commercial mixers fall down on this feature; although passable when used with lowoutput power amplifiers, noise levels become noticeable and disturbing at higher powers such as with large p.a. amplifiers. It is true that the ratio between the signal and the noise level will be the same irrespective of the power of the amplifier, but there are moments of silence especially with speech reproduction when there is no signal to mask the noise and it is then that high level noise is especially unpleasant.

Inexpensive commercial mixers were found unacceptable on this score whereas the better ones were unacceptable because of price. Hence the unit here described was designed and built. Other features required were a degree of amplification as well as mixing, a self-contained arrangement that could be operated at some distance from the main amplifier, and an input for tape or gram which

## V. CAPEL

could not be overloaded by too high an input signal resulting from use and operation by unskilled hands.

## Circuit

One of the reasons why the cheaper commercial mixers fail to achieve a good signal-to-noise ratio is because the input sockets are connected directly to the gain controls. The output from these is combined and fed to the base circuit of the first stage. An advantage of this arrangement is that only one transistor is needed for all inputs which saves cost. However it also means that the noise generated in it is fed uncontrolled into the following stages. Turning down a control only reduces the input signal thereby decreasing the signal-to-noise ratio.
In the circuit adopted for the mixer, each input has its own transistor which is followed by the gain control. When this control is turned down therefore, the noise from the input transistor decreases as well as the signal. The input stage is always the most significant as respects noise, because it is amplified


Fig. 1: The circuit of the five channel mixer. Four inputs are provided for microphones with an additional one for high level.


Fig. 2: The components are arranged as shown above on a Radiospares standard printed circuit.

## components list

Resistors:

| R1 | $4 \cdot 7 \mathrm{M} \Omega$ | R13 | $68 \mathrm{k} \Omega$ |
| :---: | :---: | :---: | :---: |
| R2 | $15 \mathrm{k} \Omega$ | R14 | $68 \mathrm{k} \Omega$ |
| R3 | $2 \cdot 7 \mathrm{k} \Omega$ | R15 | $68 \mathrm{k} \Omega$ |
| R4 | $4.7 \mathrm{M} \Omega$ | R16 | $68 \mathrm{k} \Omega$ |
| R5 | $15 \mathrm{k} \Omega$ | R17 | $680 \mathrm{k} \Omega$ |
| R6 | $2 \cdot 7 \mathrm{k} \Omega$ | R18 | $390 \mathrm{k} \Omega$ |
| R7 | $4.7 \mathrm{M} \Omega$ | R19 | $2 \cdot 7 \mathrm{k} \Omega$ |
| R8 | $15 \mathrm{k} \Omega$ | R20 | 56ת |
| R9 | $2 \cdot 7 \mathrm{k} \Omega$ | R21 | $390 \mathrm{k} \Omega$ |
| R10 | $4 \cdot 7 \mathrm{M} \Omega$ | R22 | $2.7 \mathrm{k} \Omega$ |
| R11 | $15 \mathrm{k} \Omega$ | R23 | $56 \Omega$ |
| R12 | $2 \cdot 7 \mathrm{k} \Omega$ | R24 | $6.8 \mathrm{k} \Omega$ |

All $10 \%, \frac{1}{8}$ or $\frac{1}{4}$ watt miniature types.
VR1, VR2, VR3 and VR4 $100 \mathrm{k} \Omega$ log. potentiometers
VR5 $1 \mathrm{M} \Omega$ log. pot.

## Capacitors:

| C 1 | $0 \cdot 1 \mu \mathrm{~F}$ | C 7 | $1 \mu \mathrm{~F} 12 \mathrm{~V}$ |
| :--- | :--- | :--- | :--- |
| C 2 | $0 \cdot 1 \mu \mathrm{~F}$ | C 8 | $1 \mu \mathrm{~F} 12 \mathrm{~V}$ |
| C 3 | $0 \cdot 1 \mu \mathrm{~F}$ | C 9 | $0 \cdot 05 \mu \mathrm{~F}$ |
| C 4 | $0 \cdot 1 \mu \mathrm{~F}$ | C 10 | $1 \mu \mathrm{~F} 12 \mathrm{~V}$ |
| C 5 | $1 \mu \mathrm{~F} 12 \mathrm{~V}$ | C 11 | $6 \mu \mathrm{~F} 12 \mathrm{~V}$ |
| C 6 | $1 \mu \mathrm{~F} 12 \mathrm{~V}$ | C 12 | $6 \mu \mathrm{~F} 12 \mathrm{~V}$ |

## Semiconductors:

| Tr1 | BC109 | Tr4 | BC109 |
| :--- | :--- | :--- | :--- |
| Tr2 | BC109 | Tr5 | BC108 |
| Tr3 | BC109 | Tr6 | BC108 |

(Plastic encapsulated versions of the BC108 and BC109 are now very common, have identical characteristics and are cheaper. Their numbers are BC168 for the BC108 and BC169 for the BC109.)

## Miscellaneous:

Six jack sockets; pointer knobs; Radiospares printed panel; SW1 toggle on-off switch; battery; battery clips; screened lead etc.
by all the stages that follow, whereas the succeeding stages have less amplification following them.

Obviously, low-noise transistors should be used, so the Mullard silicon planar epitaxial transistors $\mathrm{BC109}$ and $\mathrm{BC108}$ were chosen. These are n-p-n types so battery polarity will be negative to earth. Constructors used to working with the more familiar $p-n-p$ varieties will need to check polarity of the electrolytic capacitors.

Current biasing of the first stages is employed by returning the single high-value base resistor to the collector. A measure of negative feedback results, and further feedback is achieved by leaving the emitter resistor unbypassed. If desired, a greater or lesser number of inputs can be provided as required. Three were really all that were necessary, but an extra one was fitted in case it should be required in the future. It is easier to add one when first constructing, than later! Extra inputs will not add to the noise level providing the controls of those not being used are turned back to zero.

Although all controls are taken to a common input of the next stage each one will have only marginal effect on the settings of the others due to the isolating resistor in series with the wiper of each control.

The auxiliary input is fed into the same point. In this case it is best to feed the input directly to its gain control, because if applied first to an amplifying stage as is the case with the microphone inputs, this stage could be overloaded by a high level signal such as the output of a tape recorder. Here, the control will reduce the signal to an acceptable level. Impedance of this input is kept as high as possible so that crystal or ceramic pick-ups can be used, hence the higher value of the control and isolating resistor.

At first, direct coupling was considered between the second and third stages as this would avoid reactance in the coupling and provide d.c. stabilisation by a d.c. feedback loop. However, as the second stage must be "above" the first as regards d.c. voltage in directly coupled stages, this in effect halves the battery voltage to each. Where a line voltage
of around 20 volts is available as is common with most mains-powered transistor equipment, this is quite satisfactory, but things are different when the supply is only 9 volts and reducing as the battery voltage falls. Silicon transistors are less prone to thermal and other vagaries of germanium transistors, so it was deemed best to dispense with the d.c. stabilisation.

To further reduce noise levels, a negative feedback loop was included right from the output socket back to the emitter of the second stage.

## Construction

With any construction, one of the first things to consider is the case, as this will determine the way the components are assembled. The case chosen for the prototype started life as a Channel TV tuner unit. There are probably many of these around in dealers' junk rooms, but if one cannot be obtained, a similar construction can easily be made.

A Radiospares transistor printed panel was used for the building of the circuit. These are not obtainable direct from the firm as they deal only with the trade, but almost any dealer could get one within a few days even if he did not have one in stock. There are positions for eight transistors on these boards, and the base, emitter and collector connections are all marked. A centre strip of print running down the middle of the board can be used for earth, and two conductors on either side, for the battery positive rail. Along both edges of the board are triangular multiple connections.

The most straightforward way of wiring is to connect a wire link from the transistor print connection to the nearest multiple, and then wire the associated components from there. It may be necessary to link two adjacent multiples where several connections are needed to the one point. Flyingleads were fitted so that connections could be made to the controls and jack sockets.

## Performance

The gain of the microphone channels is 35 dB , which enables the mixer to be used with power amplifiers having low input sensitivity. High impedance microphones should be used, either crystals or moving-coil and ribbon instruments with built-in transformers. Medium impedance microphones of 600 or 200 ohms will work satisfactorily, there being sufficient gain for these, although the signal-to-noise ratio is decreased. When used with high impedance instruments, the noise level, even with a large p.a. in a hall, is unobtrusive at normal levels.

The gain of the auxiliary input is unity, there being no amplification required here, only the facility of mixing. A fairly high input impedance is presented so that crystal or ceramic pick-ups can be used with no loss of bass.

Overall frequency response is flat between 20 Hz and 10 kHz , and there is a gradual drop at the upper end to -3 dB at 25 kHz . Battery consumption is about 6 mA so a PP6 battery should give long service.

When using this or any other mixer, always keep the controls tha: are not in use to the minimum position. Those that are being used should be set at an advanced level and the control on the power amplifier kept to a low position, as this will give a better signal-to-noise ratio than the reverse.

## COLUMN



SOUTH AMERICAN medium wave stations are often audible after midnight during the winter. Propagation is good over the long sea path from UK enabling the DXer to hear stations quite considerable distances away. Even when conditions are poor the Argentinian stations LR3 (950) Radio Belgrano and LR1 (1070) Radio el Mundo, can often be heard, sometimes they are the only DX on the band. South Americans are usually at their best when the North American path is poor. Brazilians most frequently logged are PRA3 (860) with the slogan Radio Mundial, PRF4 (940) Radio Jornal, PRE8 (980) Radio Nacional, PRE3 (1180) Radio Globo; all are situated in Rio de Janeiro. Brazilian stations are easy to recognise as the language is Portuguese instead of the more usual Spanish from that continent. A number of Venezuelan stations can be heard, the more prominent being YVRS (1020) Radio Marguarita and YVQJ (1080) in Barcelona. Further to the west are the Colombian stations HJDK (750) La Voz de Antioquia and HJBI (840) Ondas del Caribe in Santa Marta. The Surinam station PZX7 (725) in Paramaribo is frequently a strong signal though interference from the German station on 728 can be troublesome. PZX7 identifies itself as "SRS" which are the initials of the Dutch organisation which owns the station. Announcements are in Dutch, English and Hindi and the station will QSL. More difficult South American countries are Peru with OAX4A (854) Radio Nacional and OAX4U (1010) Radio America, both stations in Lima; Uruguay with CX16 (850) Radio Carve in Montevideo; Chile with CB106 (1060) Radio Mineria and CB118 (1180) Radio Portales, both in Santiago.

During the late evening while waiting for the DX paths to open, readers may care to try some semiDX from Europe. The Portuguese National Radio operates a number of high power MW transmitters and two of these - on 755 and 1161-have programmes in English at 2245 hrs GMT. Commercial stations to look for include Radio Coub Portugues with CSB9 (782) in Miramar and CSB2 (1034) in Lisbon; Radio Renascena CSB3 (1286) in Lisbon; Emissora Norte Reunidas CSB5 (1578) Oporto; Emissora Associados de Lisboa CSB4 (1594) Lisbon. The commercial stations run on well into the night and all will QSL. Sud Radio in nearby Andorra on 818 has been heard recently with programmes in English at 2130 hrs and this station too will QSL. Three stations from the far north of Europe that often appear in the late evening are Murmansk (656) in Arctic USSR; Godhavn (650) in Greenland and Hofn (665) in Iceland.

Ramadan ends on 11th December, so have a look for some of the rare Middle East countries mentioned last month while there is still time. Saudi Arabia has been heard on 705 recently at 2100 hrs GMT with a programme in English. The new All India Radio megawatt station in Calcutta is reported to be on 1130 kHz though it has not been heard yet by the writer.

CHARLES MOLLOY

# PW wat the Exhlimilins RICHARD COLLINS reports... <br> This year Practical Wireless was represented at two 

 exhibitions. The first one was the 1969 International Radio Engineering and Communications Exhibition (the RSGB Exhibition) held at the Royal Horticultural New Hall, Westminster, S.W. 1 from 1st to 4th October.The second exhibition was the 1969 International Audio Fair held at Olympia from 17th to 23rd October. Below are photographs taken during the two exhibitions.


The opening address was made by Mr. R. J. Halsey, C.M.G., F.C.G.I., D.I.C., B.Sc.(Eng.), F.I.L., Director of Cable \& Wireless Ltd. He ìs seen here welcoming visitors to the Exhibition.


Mr.J. W. Swinnerton. T.D., B.Sc.(Econ.), G2YS, President of the Radio Society of Great Britain presents the Exhibition Organisers' Plaque to George Jessop, G6JP, for his $2 m$ Transistorised Transmitter/Receiver.


A group of enthusiasts gathered round the PRACTICAL WIRELESS stand, while staff member, Trevor Preece, G3TRP, explained the workings of the P.W. Pedal Steel Guitar.


The Exhibition transmitting stations which were operating on all Amateur Bands between 1.8 and 144 MHz . The equipment was provided and manned by the Crawley group of the RSGB.


Diana and Audrey looking after the magazine sales section of the P.W. and P.E. stand at the Audio Fair. PART EIGHT SEMICONDUCTOR

## by M.F.DOCKER, M.Sc.

IN this article several new devices will be discussed and the final two articles in the series will deal with the techniques of producing integrated circuits, both monolithic and hybrid thick and thin film types.

## Thyristors

The first device, the thyristor, could well have been described in the section dealing with diodes as it is often found in two lead form. However its construction is radically different from that of a diode and the same device can be easily converted during manufacture to form a triode or tetrode thyristor. The thyristor can be defined as a four layer p-n-p-n device as seen in Fig. 1(a) and relies on regeneration in the structure to produce a switching action.

With the polarities shown in this Fig. 1(a) junctions A and C are both forward biased whilst junction B is reverse biased. Consequently only a very small current, the saturation current of the material, will be able to flow across junction B. However, when the potential difference between the input terminals is increased sufficiently it is found that the current through the device suddenly increases as shown in the voltage-current curve of Fig. 2. This behaviour can be explained by considering the device as composed of a pair of complementary transistors, Tr1 and Tr 2 , in Fig. 1(c). From Fig. 1 (b) Tr 1 is seen to be a p-n-p transistor and Tr2 a complementary n-p-n transistor. If the alphas of the two transistors are $\alpha 1$ and $\alpha 2$ respectively and if the saturation collector current of each device is Isat1 and Isat2 respectively then it is readily seen that:

$$
\mathrm{I}=\alpha 2 \mathrm{I}+\text { Isat } 2
$$

and $\mathrm{I} 2=\alpha 1 \mathrm{I}+\mathrm{Isat} 1$ also, since the current across junction $\mathbf{B}$ must be equal to I :

$$
\mathrm{I}=\mathrm{I} 1+\mathrm{I} 2
$$

or $\quad \mathrm{I}=\alpha 1 \mathrm{I}+\alpha 2 \mathrm{I}+\mathrm{Isat}$
where Isat $=$ Isat $1+$ Isat 2 .


Fig. 1: Basic thyristor representation (a) together with two derived equivalents ( $b$ ) and ( $c$ ).

This equation can be reduced to the form:

$$
\mathrm{I}=\mathrm{Isat} /(1-(\alpha 1+\alpha 2))
$$

and this relates the current through the thyristor to the leakage current and the current gains of the equivalent transistors. Now in a previous article it was shown that the alpha of a transistor depends on the amount of recombination which occurs in the base region, so that for a high alpha the base has to be narrow." But the thyristor is intended for high voltage applications, so to avoid punch through the individual regions all have to be wide. This gives the device a low alpha.


Fig. 2: Characteristic curve of the voltage across a thyristor and the current through it.

Because of this the term $(1-(\alpha 1+\alpha 2))$ above is fairly large and $I$ is not much larger than the leakage current. If in some way recombination can be reduced the alphas will grow and I becomes large. This is done by temporarily filling the impurity centres in the base so that a larger current will flow, carriers then becoming available to diffuse across to the collector junction B , normal transistor action then taking place. After this regenerative feedback holds the device on until the voltage across the terminals is reduced to zero.
There are various ways of filling the trapping centres and one of these, used in this diode form, is to increase the voltage across the device until the leakage current across junction $B$ goes into an avalanche condition. This results in a large current flowing across the junction into the two base regions. The carriers constituting this current fill the impurity centres and enable the transistor alphas to become larger, this in turn resulting in an increase in the current through the device so that the thyristor is then turned on. When this happens all the junctions are in effect forward biased and the voltage across the thyristor falls to a fraction of a volt. The voltage at which the avalanche starts to take place is called the forward breakover voltage Vbo and is quoted in manufacturers' literature.
When a reverse voltage is applied to the thyristor junctions A and C are reverse biased and junction B is forward biased. However the previously described


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[^3]action does not occur in this case as the circuit is non-regenerative being in fact simply two diodes in series. The result is that when the reverse voltage does become sufficient to cause avalanching to take place the voltage across the device is maintained and a high power dissipation takes place in the thyristor. The variation of current with voltage across a thyristor is shown in Fig. 2. In most devices the peak reverse capability is made somewhat greater than the forward breakover voltage so that the device can be used as triggerable switch.

The rate of change of voltage across the thyristor can also be used to produce switching. This relies on the injection of charge into the depletion layer as its width changes. In this way it is possible to switch the thyristor by putting a pulse on to the terminals, of amplitude less than the breakover voltage.

## Silicon controlled rectifier

A third method of triggering involves the injection of a pulse of current directly into one of the base regions. This produces an increase in the alpha of the equivalent transistor and the regenerative feedback of the circuit causes the current through the thyristor to rise quickly. Devices using this method are called silicon controlled rectifiers (s.c.r.s.). The size of the pulse required to trigger the thyristor depends on which of the two bases the pulse is injected into. The lower p-type base is the more sensitive and devices in which this base is connected as trigger are called conventional s.c.r.s Connection to the upper n-type layer of Fig. 1(a) results in a socalled complementary s.c.r.

## Silicon controlled switch and light activated s.c.r.

The silicon controlled switch is a thyristor with connections to both the base regions so that in consequence it is a four terminal device. Current pulses can be injected into either one or both of the bases to produce switching. Another method commonly used to trigger the thyristor is the use of light induced carriers in the base regions. This is used in the light activated silicon controlled rectifier (1.a.s.c.r.) and in the phototran. These are used in many optoelectrical control systems.

## Switch off

A point to be noticed in the operation of the thyristor is that once it is switched on it cannot easily be switched off until the voltage across its terminals has been reduced to a very low value. Even then sufficient time has to be given for the charge carriers which are stored in the base region during the forward conducting state of the thyristor. This time is typically several microseconds: if the voltage is reapplied before expiration of this time the thyristor will switch on again immediately.

## Types and uses

The construction of a typical alloy-diffused thyristor is shown in Fig. 3(a). The p-type regions are produced by diffusion of acceptor atoms from the gaseous state and the cathode region is produced by alloying suitable impurities into one surface. Leads are then attached as shown. Planar thyristors are also produced as shown in Fig. 3(b), usually several

(a)

(b)

Fig. 3: Two forms of thyristor.
devices being made on one wafer which is then cut up into dices to give the individual thyristors.

The thyristor is often used to control a.c. supplies. However in this application they have the disadvantage that they only switch into their forward conducting state in one direction. In order to permit full wave control of power supplies it is possible either to use two thyristors or to use a device called a triac. This is a multiple layer device which is equivalent to two s.c.r.s so arranged that they switch on alterna-


Fig. 4: Triac thyristor construction.
tive half-cycles of the mains. The structure of this device is shown in Fig. 4 and its voltage against current characteristic is given in Fig. 5.

A small s.c.r. with an avalanche diode between the anode and gate electrodes is also available. This can be used as a low current switch and is given the name silicon unilateral switch, or s.u.s. A bilateral version of this device is also available and is used to trigger high power triacs as it provides the alter-


Fig. 5: Characteristic curve showing the variation in current flowing through a triac as the voltage across it is changed.
nately positive and negative pulses required for biphasic operation of the triac.

There are numerous other thyristors available including the diac which is similar to the s.b.s. and is also used to switch the triac. The quadrac, which is a three terminal device containing both a diac and triac and can be used in phase control of biphasic power supplies, is another thyristor which has only recently become available.

## Unijunction transistor

Another device exhibiting a negative resistance effect is the unijunction transistor. This is similar in construction to the f.e.t. but its gate electrode is called the emitter and is much smaller than that of the f.e.t. It is normally operated in forward bias and the structure of a typical bar type u.j.t. is shown in Fig. 6 together with its circuit representation. It con-


Fig. 6: Unijunction transistor construction and circuit symbol.
sists of a silicon bar with two ohmic connections made to each end, called the base terminals, and an aluminium emitter which is alloyed to the base to form a p -n junction. If a current is made to flow through the base the potential at the emitter will be Ve. As long as the voltage applied to the emitter is less than this the junction will be reverse biased and no current will flow. However if the applied voltage is increased beyond Ve the junction will go into a forward conducting state and holes will be injected into the base region. In order to maintain neutrality electrons will be released in the base region between the emitter and base one, which results in the resistance of the region falling. This then causes the potential drop across the bar in this region to fall with a consequent increase in the forward bias applied to the junction and the number of injected holes rises yet again. Obviously this is a regenerative effect and causes the emitter current to rise sharply.

A curve showing the variation of emitter voltage as the emitter current changes is shown in Fig. 7, where the curves for different voltages between bases are indicated. The most significant point of this is that when the emitter voltage reaches Ve the


Fig. 7: Variation of emitter voltage with current as the base-tobase voltage in a unijunction transistor is changed.
emitter current suddenly increases and whilst this is happening the voltage across the emitter falls. This is the opposite behaviour to that shown by a resistor and is consequently called a negative resistance effect. This enables the unijunction transistor to be used in many oscillators, staircase waveform generators and dividers and circuits where a negative resistance effect is required.

## Spacistor

Two other devices which are occasionally met but which do not yet seem to have reached the world of the amateur are the spacistor and the tetrode transistor. A brief explanation of these devices is worthwhile.

The spacistor is a single junction amplifier. Basically it is a p-n junction with a large reverse bias so that it has a wide depletion region. Current carriers are injected into this depletion region from a metal contact and are swept across the depletion region by the electric field. Because of the high field it is possible to have quite short transit times and thus to have a high cut off frequency. Another


Fig. 8: Basic spacistor construction.
type of spacistor employs a fourth electrode called a modulator which affects the gain of the device. It also increases the input and output impedances of the spacistor by increasing the isolation of the injector from the output current. A diagram of the simple spacistor is shown in Fig. 8.

## Tetrode transistor

The tetrode transistor is similar to the ordinary transistor except that it has two base contacts. Because of this it is possible to produce a field across the base so that effectively only a small portion of the emitter-base contact is forward biased. This reduces the active width of the base so that its resistance is reduced and also the transition capacitance is reduced. These assets make the tetrode especially useful in high frequency applications including high speed switching circuits. Figure 9


Fig. 9: Construction of a tetrode transistor and its circiuit connections.
shows the schematic cross-section of a tetrode transistor including a representation of the current flow pattern. The reduction in the base width is clearly seen from this figure and results in a decreased base resistance because of the lessened distance the base current has to travel before recombination.

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THE conclusion of Part 2 dealt with the last stage of assembly which was the linkage of the pedals to the roller levers by means of the "connecting" rods. The photograph on this page shows the actual connection of the horizontal rods to the roller levers. Adjustment of the pedal movement and linkage depends on the tuning adopted for the instrument but for the example given in Part 1 (an E6th tuning), string 2 will be tuned sharp and string 4 will be tuned flat when their respective pedals are depressed. The accuracy of the raising or lowering of pitch depends entirely on the accuracy of adjustment to the roller lever stop screws and the downward movement of the pedals. Adjustment should be such that when the pedal is depressed the string is re-tuned just as the pedal touches the stop rail beneath it and as the roller lever comes into contact with its own stop screw. The actual downward movement of the pedal for a semitone change of pitch should not be more than half an inch i.e., the pedals should normally rest about $\frac{1}{2}$ inch or even less above the stop rail as shown in the photograph.

When preliminary adjustment of the pedal mechanism has been completed the engraved fretboard can be fitted. This may be glued to the guitar body with Evostik or Bostik. The strings can now be tuned to pitch and the accuracy of tuning checked over the full length of the fretboard i.e., at all fret positions. Providing the distance between the "nut" and the 12 th fret and between the 12 th fret and the centre line of the roller bridge are exactly equal (see diagrams in Part 1) the tuning should be accurate at all fret positions.

## The Preamplifier

The final stages of construction are concerned with the preamplifier, its power supply and the optional foot pedal volume control (swell pedal). The preamplifier might also be considered as optional for there is no reason why the guitar pick-up should not be directly connected to a suitable amplifier already equipped with tone controls and volume control and having an input sensitivity of 50 to 100 mV .

However, there is a purpose for the built-in preamplifier in that it makes up for gain loss incurred by the foot-operated volume control and more important, it has a treble lift and cut control that will enable the player to obtain that very sharp brilliant tone favoured by players of the pedal steel guitar. In


How the flat ends of the connecting rods are secured by $4 B A$ screws to the roller levers.


Linkage to foot pedals. Adjustment is made by the 2BA nuts beneath the pedals, i.e., the pedals can be raised or lowered on the ends of the vertical connecting rods.


Fig. 20: The preamplifier panel. Details for drilling, etc.


Fig. 21: Assembly of the preamplifier panel and circuit board.
fact the preamplifier may be of interest to plectrum guitarists.

The whole preamplifier is assembled on its own panel and if constructed to the dimensions given in Figs. 20 and 21 will fit into the slot provided on the top of the guitar consol (see Part 1). The circuit is shown in Fig. 22 and employs two Mullard BC109 transistors with a negative feedback tone control system that provides approximately 15 dB treble lift


Fig. 23: Frequency response of the preamplifier.
and 12 dB treble cut as shown by the response curves in Fig. 23.
The overall gain of the preamplifier can be varied a little by means of the pre-set control VR1 $(4 \cdot 7 \mathrm{k} \Omega)$. For normal operation this control should be set to about midway position. At its maximum resistance the overall gain of the amplifier will be decreased. At its minimum resistance the gain of the amplifier will be increased but the amount of treble lift will


Fig. 24. Pictorial wiring diagram and layout for the preamplifier.


Fig. 22: Circuit diagram of the preamplifier.
be reduced. The average signal output from the preamplifier is about 200 mV with VR1 set midway. With the foot pedal volume control in circuit the output is reduced to about 100 to 150 mV . If the pedal volume control is not used, the output can be taken from the slider of VR3 and will be around 200 mV . The preamplifier, with or without the pedal volume control, can be connected to any amplifier having an input impedance of $10 \mathrm{k} \Omega$ or greater and an input sensitivity of 100 to 200 mV . As already mentioned a higher or lower signal output can be obtained by adjusting the pre-set VR1. A pictorial wiring diagram for the preamplifier is given in Fig. 24.

Details for the power supply are given in Figs. 25 A and B. If constructed as shown it can be mounted up inside the console as can be seen in the photograph. It may be necessary to orientate or reposition either the whole assembly or the mains transformer itself to prevent hum being induced into the guitar pick-up.

## The Foot Pedal Volume Control

Assuming the pedal volume control is to be used, then the pre-amplifier output can be fed to it via a 3-pin DIN socket mounted at the side of the console (see Part 1). This socket also carries the 12 V d.c. (from the power supply) to light the control lamp in the pedal volume control. Wiring connections for the socket are shown in Fig. 26. The signal lead must be screened and the overall length of the cables between the two DIN plugs (A and B) should be at least 2 feet.

The pedal volume control employs a light discriminating resistor (ORP12) which becomes part of


Fig. 25: (a) Power supply circuit. (b) Power supply assembly.


The position of the power supply (left) and the pre-amp (right). Note also the relative position of the pedal rod linkage mechanism (centre) and the pre-tension spring just to the left of it.
an attenuating network formed by itself and R9. When the pedal is depressed in the backward direction, light from the control lamp decreases the resistance of the LDR and reduces the signal level. The light must not be too bright hence the need for some series resistance (RL). The author used a 6.3 V 0.15 A bulb with a series resistor of approximately 60 ohms. Lamps up to 12 V at 60 to 100 mA


Fig. 26: Connections to the 3-pin $D I N$ socket at the side of the console.


The completed foot pedal volume control.


Fig. 27: Details of the foot pedal volume control.
can be used but should be dimmed a little with series resistance of appropriate wattage. A pre-set wirewound resistor of about 50 ohms and 2 W rating would be suitable.

An ordinary geared potentiometer pedal volume control could of course be used. The only real advantage of the LDR system is noiseless operation and the fact that it does not wear out as would a carbon track potentiometer. The photograph shows the completed pedal volume control and the diagrams in Figs. 27, 28, 29, and 30 give details for construction. The base of the control and the foot pedal were cut from $\frac{3}{4} \mathrm{in}$. Contiboard left over from making the console. The two sides were made from $\frac{1}{16}$ in. thick Dural. The pedal itself is hinged to the body on a $\frac{1}{4}$ in. diameter spindle held fast by collars at each end and has an overall movement from level to a backward slant, of about $30^{\circ}$.

The control lamp and the LDR are both mounted in small wood blocks as shown in Figs. 30 and 31. It is best to solder the leads for the lamp directly to it and secure the lamp in the block with a spot of adhesive. The two blocks must be only just far enough apart to allow the aperture plate to move freely between them. The wiring for the 3-pin DIN socket, the output jack socket and the LDR and lamp are shown in Fig. 31. Providing the LDR is recessed in its mounting as shown in the diagrams it will not be affected by light coming from outside. Note that the end plate as shown in Fig. 29 serves as a forward stop for the pedal.


Fig. 28. The foot pedal of the volume control and the LDR aperture plate.

The complete and finished instrument, exactly as described in this series of articles, gave a very pleasant but brilliant tone quality with a good sostenuto (sustaining of sound) typical of the pedal steel guitar and its forerunner the Hawaiian guitar. As pointed out previously the number of pedals need not be confined at two only-some commercial single-neck instruments have four.

Fig. 29: The end plate acts as a stop for the forward-downward movements of the pedal volume control.


Fig. 30: The LDR and its lamp are mounted so as to be in line with the $\frac{1}{4}$ in. diam. spindle and the centre line of the aperture plate.


Fig. 31: Wiring for the pedal volume control, its input and output sockets and the 3-pin DIN connecting plug.

However, by making and fitting four roller levers as suggested, the two pedals can be changed over to other strings should alternative tuning combinations be required.

On reading through the first two articles again the writer has discovered one or two points that might not have been clear. First the unused roller levers. These should be locked at midway position (hanging vertically) by means of the locking screws. The strings can be anchored to them directly or to the holes in the tailpiece.

Before adjusting the movement of the pedals and linkage, set the roller levers concerned by means of their stop screws, so that they too hang vertically. The roller that is used to tension its string should now have its forward stop screw adjusted so that the lever can move forward i.e., toward the pick-up. The roller lever that is used to de-tension its string should have the rear (tailpiece) stop sorew adjusted so that the lever can move toward the tailpiece. The basic tuning should of course be done with the pedals in their off or neutral position.

Finally a note on suitable strings. Those used for the tuning prescribed in Part 1 which is based on the chord of E6 were selected from the wide range of "Rotosound" strings for guitars of all kinds. These were as follows:

| 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ab | B | D | E | Ab | B | C\# | E |
| $0.038^{\prime \prime}$ Covered |  | $0.028^{\prime \prime}$ Covered |  | $\begin{gathered} 0.020^{\prime \prime} \\ \text { Plain } \end{gathered}$ |  | $\begin{gathered} 0.016^{\prime \prime} \\ \text { Plain } \end{gathered}$ | $1$ |
|  |  |  |  |  |  |  |  |
|  | 0.036 |  | Plain ${ }^{\prime \prime}$ |  | ${ }_{\text {Plain }}^{0.018}$ |  | 0.014" |

Heavy gauge covered strings could be used for 8,7 and 6 with a resultant rounder and stronger tone. Some experiment with string gauges is well worthwhile and a list giving all the different gauges of strings and a chart showing the different types recommended for guitars i.e., pedal steel, Hawaiian and plectrum can be obtained by writing to Roto-sound-James How Industries Limited (Music Division), 20 Upland Road, Bexley Heath, Kent.

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Few people build multi-range testmeters nowadays because Japanese ready-built meters are freely available at very competitive prices. There does, however, remain one distinct advantage in "rolling one's own", and this is the high degree of accuracy to which a meter can be calibrated. It is quite easy to do, and is fully described in this article on the Microtest 24 -range a.c./d.c. multimeter using a $50 \mu \mathrm{~A}$ movement.

## THE TWO-FIFTY TRANSMITTER

Radio Amateurs who are keen on turning their attention to 2-metres will find G3TYJ's Two-Fifty transmitter very appropriate. It is a relatively simple crystal controlled 4 -valve 40watt input design which can be used as it stands for c.w., or connected to any normal modulator for phone. A circuit is also provided to assist those who prefer to use the simpler clamp-tube modulation. Full coil-winding details are given, along with sufficient constructional information to enable anyone who has a transmitting licence to build this transmitter without difficulty.

## REPAIRING LOUDSPEAKERS

Loudspeaker cones are very fragile, and the slightest tear can seriously impair reproduction quality. Having a speaker reconed professionally can be very expensive, however, and so this article explains how to carry out this task oneself, replacing the original paper cone with a combination of paper, expanded polystyrene, polyurethane foam and aluminium foil, the mixtures depending on which frequency range the loudspeaker is intended to cover. The complete cost of repairing one of the author's 12 in . loudspeakers came to about 14s.

## PLUS OTHER CONSTRUCTIONAL PROJECTS AND REGULAR FEATURES

Do not miss your copy of the February issue of Practical Wire-less-on sale 9th January price 3/-

## EXPERIMENTERS CORNER

DESIGNING CLASS "A"' TRANSISTOR AMPLIFIERS

C. R. BOGGIS, M.A.P.A.E.

DESIGNING basic transistor amplifier stages can be made very simple by following a few "rules of thumb", so enabling the experimenter with but a modicum of theoretical knowledge to tailor established circuits to his own needs. This article, which can be read in conjunction with last month's "Experimenters Corner", describes how to work out the component values for germanium or silicon amplifiers and couple them to other stages without upsetting their operation.

## Germanium Amplifiers

If a single amplifier stage as shown in Fig. 1 is designed as follows it will be able to function over the temperature range of 20 to $50^{\circ}$ Centigrade. In the worked example, a general-purpose small signal transistor is used (Mullard type OC71, or similar).


Fig. 1: A straightforward amplifier stage suitable for a germanium transistor.
First the supply voltage is chosen. Here we select 9 volts, this being readily available from standard batteries. We then decide on a value of collector current. For a very small input and low noise this should be around 100-200 microamperes, but for large inputs the current could be anything up to about 100 milliamps. As a general rule a current of 1 mA is desirable, and it is around this figure that the stage designed here is evolved.

Having decided on the collector current, the first rule may be applied. This states that the emitter resistor should drop approximately 1 volt. Therefore in our example, R3 will be equal to $\frac{1 \mathrm{volt}}{1 \mathrm{~mA}}$, since the emitter current can be considered equal to the collector current for this purpose, which suggests a resistor value of 1000 ohms.
The next rule states that for good stability, the collector voltage should be equal to half of the result of subtracting the emitter voltage from the supply voltage.

Here the collector voltage should be $\frac{9-1 \text { volts }}{2}$ or 4 volts.

With a collector current of $1 \mathrm{~mA}, \mathrm{R} 4$ should be $\frac{4 \text { volts }}{1 \mathrm{~mA}}=4000$ ohms, the nearest preferred value being $3.9 \mathrm{k} \Omega$.

Using yet another rule of thumb, R2 should be 10 times R3, which yields a value of $10 \times 1 \mathrm{k} \Omega$, or $10 \mathrm{k} \Omega$ in this case.

The base voltage is determined by the $V_{\mathrm{be}}$ for the transistor plus the emitter voltage. For a germanium transistor, $V_{\mathrm{be}}=0.2$ volts approx., so the base voltage required is 1.2 volts. The current through R1 is the same as the current through R2, since the base current, being very small, can be ignored. This current equals $\frac{1 \cdot 2 \text { volts }}{10 \mathrm{k} \Omega}$, which is 120 microamps. Thus R1 should drop $9-1.2$ or 7.8 volts at 120 microamps. R1 therefore equals $\frac{7.8 \text { volts }}{120 \mu \mathrm{~A}}$, which is $65 \mathrm{k} \Omega$ (use a $62 \mathrm{k} \Omega$ preferred value).
The values of C 1 and C 2 hardly need calculating. Suffice to say that their reactance should be negligible at the lowest frequency to be amplified. An ideal value for each is $10 \mu \mathrm{~F}$. The working voltage is determined by the collector voltage of the stage and the base voltage in the following stage-usually a 6 volt capacitor will be suitable. Note the polarity of these two capacitors.

C3 should also be chosen such that its reactance is small at the lowest frequency. Here a value of $50 \mu \mathrm{~F}$ will be ample, but again, note the polarity.

## Silicon Amplifiers

Using silicon transistors it is possible to obtain adequate temperature stability with a simplified circuit as shown in Fig. 2. The design procedure is even simpler


Fig. 2: A simple amplifier particularly suitable for a silicon transistor.

few. the level required for the base of the transistor. The base voltage needed here is equal to the $V_{b e}$ for the transistor, which is about 0.4 volts for silicon.

The base current required is calculated from the collector current divided by $h_{\mathrm{fe}}$ or beta for the transistor at that collector current. For the BC109, $h_{\mathrm{fe}}$ at $I_{\mathrm{c}}=$ $200 \mu \mathrm{~A}$ is typically 300 , so the required base current is $\frac{200 \mu \mathrm{~A}}{300}$, which is $0.6 \mu \mathrm{~A}$. R1 is therefore equal to $\frac{3-0.4 \text { volts }}{0.6 \mu \mathrm{~A}}$, which is $4 \mathrm{M} \Omega$. Allowing for somewhat lower $h_{\mathrm{fe}}$ values that may occur in production spreads R1 should be chosen as $2 \cdot 7 \cdot 3 \cdot 3 \mathrm{M} \Omega$.

## Using the Circuitry

The circuit designed in Fig. 1 could be utilised in many ways. It could be used to amplify the signal from the detector of a tuner up to sufficient level to drive an earphone, in which case R4 should be replaced by a headset with a d.c. resistance of 4000 ohms. Alternatively, R4 may be left in circuit and driver and output stages added to drive a loudspeaker.

Another application could be as an audio mixer for several inputs, and the circuit in Fig. 3 shows such an arrangement. Resistors R1-R4 are included to reduce interaction between each of the mixer volume controls. The volume control at the output is the master volume control, and is effective over all inputs. By inverting the supply rail polarity, the circuit in Fig. 2 could be substituted for the OC71 amplifier stage.

## High Input Impedance

Where a high input impedance is required such as for amplification of a gramophone pick-up output, an emitter follower can be used in front of the circuit in Fig. 2. This additional amplifier is shown in Fig. 4, and this will give an input impedance of approximately $2 \mathrm{M} \Omega$. This is because the input impedance of the

Fig. 4: An emitter-follower which exhibits a very high input impedance and a low output impedance. Its voltage gain is fractionally less than 1.
transistor is almost equal to the beta or $h_{\mathrm{fe}}$ times $R \mathrm{e}$. Input $Z=300 \times 15 \mathrm{k} \Omega=4 \cdot 5 \mathrm{M} \Omega$.
This is shunted by R 1 , which is $3 \cdot 3 \mathrm{M} \Omega$, so the input impedance $=\frac{3 \cdot 3 \times 4.5}{3 \cdot 3+4.5} \mathrm{M} \Omega=2 \mathrm{M} \Omega$.

## PRACTICAL GIFT FOR A PRACTICAL MAN

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## A PANORAMIC RE $\Omega N M \_$_man



## D.BOLLEN PART 1



APANORAMIC receiver provides a visual display of a band of frequencies when coupled to an oscilloscope, and this can be a useful aid to the serious short-wave listener or radio amateur. Signals appear on the oscilloscope screen as a series of resonance curves, of differing amplitude and character, spaced along the X -axis as though on a tuning scale. All signals are resolved visually without switching, whether they be a.m., c.w., s.s.b. or f.m., and the operator soon learns to distinguish between them. A quick assessment of general conditions on the band can be made without having to break off an existing contact on the main "shack" receiver. Thus, the need for searching by means of frequent manual retuning is largely eliminated.

Before semiconductors came on the scene, automatic "sweep" tuning of a receiver could only be accomplished by complicated arrangements of motor-driven tuning capacitors or reactance valve circuits, but now simple circuits based on the capacitance variation of semiconductor diodes when reversed biased are used.
The equipment described here employs ordinary, readily available components, and is designed for simple construction and low cost, to cover bands of frequencies up to 500 kHz wide lying between 1.7 MHz and 4.5 MHz , which includes 160 and 80 m .

## HOW IT WORKS

Figure 1 gives the block diagram of the panoramic receiver. A conventional two transistor converter, involving three "gang" tuned circuits, is coupled to a 1.6 MHz i.f. strip. An alternative arrangement is with the converter feeding a medium wave receiver which is tuned to 1.6 MHz , thus achieving a doublesuperhet configuration. A voltage taken from the oscilloscope timebase simultaneously varies the capacitance of three diodes, each placed across one of the tuned circuits in the converter. At the same time, an output voltage is derived from the final i.f. detector diode for display on the oscilloscope Y-axis. If a continuous unmodulated carrier is received, the oscilloscope will show the overall response curve of the panoramic receiver, in the form of a single peak situated somewhere along the X -axis. Two plain carriers at different frequencies will appear side by side. The effects of modulation will be discussed later.

In practical terms, the small change of diode capacitance, compared with the main tuner capacitance swing, is quite sufficient to offer a useful "sweep". If an attempt is made to get a really wide panoramic bandwidth then signals will be too cramped on the display for easy recognition, and

# CEIVER for  

"tracking" problems will arise. Under typical operating conditions, "sweep" bandwidths of less than 50 kHz will offer an informative display, but the bandwidth obtained with the prototype receiver is continuously variable between zero and 500 kHz on 80 metres, and zeno to 100 kHz on Top Band, which is sufficient for most requirements.

Although intended primarily as an accompaniment to an existing communications receiver, the panoramic receiver can be used on its own. Switching is included to stop the "sweep" and allow normal reception of an a.m. signal, either with headphones or via an amplifier and loudspeaker, as shown in Fig. 1.

The prototype receiver made use of a mixer and 465 kHz i.f. strip taken from an old transistor portable radio. After careful peaking of the 465 kHz i.f. transformers-made easy by the panoramic receiver display of its own response curve -excellent reception of signals was obtained, including s.s.b. when a b.f.o. was added.

Although, at first sight, the panoramic receiver would seem to involve quite a lot of constructional work, it will only be necessary to build a straightforward two transistor converter, plus a "sweep" tuner circuit panel consisting of a small collection of components, if a medium wave receiver and an inexpensive oscilloscope are already to hand. Even greater simplification results when the "sweep" tuner is fitted to an existing receiver.

## DIODE CAPACITANCE

Virtually all semiconductor rectifier diodes exhibit junction capacitance, due to the depletion layer when reversed biased, and this capacitance varies with reverse voltage. Varactor diodes are specially manufactured to exploit depletion layer capacitance and to offer a good performance at very high frequencies. It is not generally realised, however, that ordinary silicon power rectifiers, as used for h.t. supplies, can also be employed as voltage controlled capacitors in circuits working at several MHz. The graph given in Fig. 2 shows the capacitance characteristics of four types of silicon rectifier. It can be seen that the characteristic of each diode is non-linear, and that maximum capacitance depends on the particular diode type. In nearly all cases, a capacitance variation amounting to some $50 \%$ of maximum junction


Fig. 1: Block diagram of the panoramic receiver.
capacitance is obtained when a reverse voltage of 10 V is applied.

A single diode "sweep" tuner circuit serves to demonstrate how a rectifier diode can be linked to the tuned stage in a radio receiver (see Fig. 3). The tuned circuit, consisting of an r.f. inductor L1, a trimmer capacitor TC1 and a variable capacitor $\mathrm{VC1}$, is coupled in parallel with the variable capacitance diode D1 via d.c. blocking capacitor C1. A re-


Fig. 2: The capacitance characteristics of four types of silicon diode.


Fig. 3: A single diode "sweep" tuner.
verse voltage is applied to the diode by the potential divider formed by R1, R2 and R3. R1 and R2 have values of more than 1 M ohm, to minimise loading of the tuned circuit. Approximately half the bias voltage will appear at the junction of R1 and R2, and the sawtooth timebase voltage, which is fed to R3 via C2, will cause the reverse voltage across the diode to "sweep" in sympathy with the oscilloscope X deflection, between zero and full bias conditions. It is important to avoid driving the diode into conduction by the application of too large a timebase voltage. Although no damage will result, a forward bias across the diode will lower the " Q " of the tuned circuit, and cause loss of gain. An interesting feature of the Fig. 3 circuit is that a small alteration of d.c. bias across the diode will change its capacitance, therefore, bandspread tuning can be accomplished easily merely by placing a variable resistor in series with R1.

The governing factor in the choice of a diode for receiver tuning is its zero bias capacitance. If the diode has a large capacitance it will seriously restrict the high frequency coverage of the receiver. On the other hand, if the diode has a small capacitance, the "sweep" bandwidth of the panoramic receiver will be correspondingly narrow. As a general rule, a zero
bias capacitance of about $10 \%$ of the maximum tuned circuit capacitance will be about right.

In the case of the $1.7 \mathrm{MHz}-4.5 \mathrm{MHz}$ converter used for the panoramic receiver, maximum tuned circuit capacitance is in the region of 330 pF , calling for a diode capacitance of 33 pF . Varactor diodes listed by well-known suppliers fall outside the required capacitance value, being either too large or too small, but a wide choice of rectifier diodes exists. The A.E.I. type SJ 403F was found to be ideal, having a zero bias capacitance typically of 34 pF , falling to some 14 pF with a reverse voltage of 20 V , see Fig. 2. If difficulty is experienced in obtaining the SJ 403 F , there is no reason why other types should not be tried. A diode can be checked for zero bias capacitance value by connecting it, in series with a fixed mica capacitor of about 500 pF , across the terminals of a capacitance bridge. The aim should be to find three diodes, preferably of the same type, which have a nearly identical capacitance value falling close to 33 pF . In practice, anything from, say, 25 pF to 40 pF can be deemed usable in the panoramic receiver.

The converter circuit of Fig. 4 is designed around Denco transistor tuning coils and n-p-n silicon transistors. Coils T1, T2, and T3 are intended for use with a $310 \mathrm{pF}+310 \mathrm{pF}+310 \mathrm{pF}$ tuning capacitor and 30 pF trimmers. Padder capacitor C 7 in Fig. 4 serves to give correct tracking between oscillator and other stages.

Denco 3 T coils normally cover the range 1.7 MHz to 5 MHz , but the addition of extra diode tuner capacitance to the tuned circuits in the converter will lower the upper frequency limit to 4.5 MHz , without otherwise affecting performance.

In Fig. 4, the aerial coil T1 is tuned by VC1. A signal is amplified by r.f. stage $\operatorname{Tr} 1$ and is then passed to the secondary winding of T2. T2 is tuned by VC2. Self-mixing oscillator $\operatorname{Tr} 2$ converts the signal to 1.6 MHz , and the oscillator coil T3 is tuned by VC3. I.f. transformer IFT1 provides the correct matching impedance to the base of a following tran-

## components list

| Resistors: |  | Transistors: |  |
| :---: | :---: | :---: | :---: |
| R1 | $18 \mathrm{k} \Omega$ | TR1 | 2N2926 (orange |
| R2 | $6.8 \mathrm{k} \Omega$ | TR2 $\}$ | $\int$ spot) |
| R3 | $2.7 \mathrm{k} \Omega$ | Diodes: |  |
| R4 | $18 \mathrm{k} \Omega$ | D1 | SJ403F (see text) |
| R5 | $6.8 \mathrm{k} \Omega$ | D2 |  |
| R6 | $2.7 \mathrm{k} \Omega$ | D3 |  |
| R7 | $1 \mathrm{k} \Omega$ | Switch: |  |
| R8 | $470 \Omega$ | S1 | Four-pole three- |
| R9 | 7 |  | way rotary |
| R10 |  | Coils an | d transformers: |
| R11 |  |  | Blue |
| R12 | 2.2M 2 | T2 | Yellow $\}$ Denco 3T |
| R13 |  | T3 | White |
| R14 | f | IFT1 | Denco IFT 16/1-6 |
| R15 | $560 \mathrm{k} \Omega$ |  |  |
| VR1 | $1 \mathrm{k} \Omega$ carbo | r pot. |  |
| VR2 | $25 \mathrm{k} \Omega$ carb | ar pot. |  |
| VR3 | $100 \mathrm{k} \Omega$ car | near pot. |  |
| VR4 | $1 \mathrm{M} \Omega$ minia | keleton pr | --set. |
| All fix | ed resistors | 0\%. |  |

Capacitors:


## Miscellaneous:

Jackson SL16 scale drive assembly. Bias battery type B122. S.r.b.p. sheet 7in. $\times 5 \frac{7}{8}$ in., turret tags, 0.1 in . matrix Veroboard or plain drilled s.r.b.p. $21 \times 30$ holes, matrix pins, 18 s.w.g. aluminium plate $7 \mathrm{in} . \times 2 \frac{1}{2} \mathrm{in}$.


Fig. 4: The 1.7 to 4.5 MHz front-end. This is a simple tuner designed around Denco coils.
sistor stage in a 1.6 MHz i.f. strip, or a mixer in a medium wave receiver. Methods of coupling the converter to following stages will be outlined later.

To prevent instability, the r.f. stage in Fig. 4 is decoupled by R3 and C1, and the mixer by R6 and C4. C8 decouples the +9 V supply line. VR1 is included to allow adjustment of r.f. gain, so that an optimum signal-to-noise performance may be achieved. The purpose of resistor R8 will be explained later.

## THREE-GANG diode tuner

In the diode tuner circuit of Fig. 5, d.c. bias for the diodes is conveniently supplied by a small, longlife 22.5 V battery. Diode and bias polarities are so arranged that a left to right timebase sweep will give high frequency signals on the right-hand side of the
display. VR2 and R15 form a potential divider, and VR2 acts as a bandspread control, giving deviations of the order of $\pm 15 \mathrm{kHz}$ at 3.4 MHz , and just a few kHz at 1.9 MHz . Short-term frequency stability of the diode tuner, when switched to "listen" is sufficiently good to allow s.s.b. signals to be easily resolved with the aid of a b.f.o.

Each diode in Fig. 5 has its own potential divider, formed by the $2 \cdot 2 \mathrm{M}$ ohm bias resistors R $9-$ R14, but the dividers are connected to earth via a common resistor, formed by the track of potentiometer VR3. Thus, while each diode is individually d.c. biased, and is isolated from other diodes by the high value of divider resistors, a sweep voltage injected into VR3 will swing all three diodes simultaneously. Capacitors C9-C11 couple the diodes to the tuned circuits in the converter.


Fig. 5: The "three gang" diode sweep tuner, Sections $A$ and $B$ swing the r.f. tuned circuits $T 1$ and $T 2$ in Fig. 4, and section $C$ sweeps the oscillator $T 3$.

The oscilloscope timebase sweep voltage is fed to the diode tuner via C12 and VR4. VR4 serves to pre-set the maximum sawtooth peak voltage when VR3 is set for minimum magnification (maximum sweep bandwidth), and will cater for typical oscilloscope X-plate voltages of $100 \mathrm{~V}-400 \mathrm{~V}$. As the slider of VR3 is moved towards the earth rail, a signal peak at the centre of the display will be expanded, i.e., magnified, until it fills the screen; this facility is useful for a close examination of adjacent signal heterodyne interference, as well as various transmitter modulation defects.

## Part 2 next month:

Construction, alignment and use.


IT is my intention to devote as much space as possible to news and logs sent in by readers of this column. Several logs were received this month and they have been included in this article.

If you have any news or loggings which you think would be of interest to your fellow-readers you should send them to Practical Wireless by the 14th of each month or to my home address: 58 Kensington Gardens, Ilford, Essex, by the 17th. It would be helpful if you could enclose a list of the equipment you use as this helps people to make a comparison between your logs and their own results.

## Readers' Logs

John W. Smith, of Anstruther, in Fife, sent in the following items from his log:

11,770: Radio Nigeria in English from 1900 to 1930.

15,080: Radio Euzkadi, clandestine, in the late evening.

15,155: Radio Dif. de Sao Paulo at 2320.
He also reports that Radio Denmark transmits its European Service from 1030 to 1115 (SaturdaySunday) instead of 1015-1100. The frequency is still 9,520 and the "DX Window" programme will be broadcast at 1045 on Sundays.

Mr. H. Wood, of Manchester, sent in these news items:

Canada: The new autumn schedule of the CBC is 0715-0745 on 9,625 and 5,990, 1217-1313 on 15,325 and 2115-2152 on 11,720, 15,325 and 17,820. All times and frequencies refer to the European Service.

Netherland Antilles: The Radio Nederland transmitter at Bonaire is now using the frequency of 9,715 from 0800 to 0920 and from 0500 to 0620.

Roy Patrick, of Derby, sent in these interesting items:

Andorra: The English Service of Radio Andorra is from 0100 to 0200 on Saturday mornings (according to my information, Roy, it is from 0000-0100 GMT). Roy also lists the shortwave outlet as being inactive.

Canada: CHNX has been logged by Roy on 6,130 around 0100 with a fair signal.

According to Radio Canada the plan to replace the 50 kW transmitters with ones of 250 kW has been dropped. (This is due to the Government's recent austerity economy measures.-MC.)
Luxembourg: The shortwave outlet of Radio Luxembourg on 6,090 will increase its power to 500 kW early next year.
S. Arabia: Roy has heard an English newscast from this country at 1700 on 11,855 but has not been able to hear it since.

## Africa

Biafra: The Voice of Biafra continues to broadcast on 6,144 from 0455 to 0200 whilst Radio Biafra

## THE BROADCAST BANDS Malcolm Connah

uses 7,307 from 0430 to 2230 . The two stations do not use parallel programming.

## Asia

Cyprus: The Cyprus Broadcasting Corporation has resumed its shortwave transmissions. The station broadcasts at 1900-2105 Monday to Saturday on 15,260 and at $0900-1600$ on Sundays on 17,875 . The Corporation is very interested in receiving reports from listeners.
Korea: Radio Pyongyang has a new frequency of 9,613 for its English transmissions at 1900-2000 which are beamed to Europe, Africa, the Near and Middle East.

## Europe

Andorra: The English Service of Radio Andorra on 701 and 5,995 is now scheduled for $0000-0100$ on Saturday mornings but there is no sign as yet of the shortwave outlet.

Austria: Radio Austria's DX programme is broadcast every second Sunday at 1915 on $6,135,9,610$, 11,925 and 15,210.
Belgium: The English programme "Belgium Speaking" is broadcast at $2205-2215$ on $9,550,9,660$ and 11,715 and at $0050-0100$ on $6,125,9,660$ and 11,$715 ; 9,660$ is a new frequency for this broadcast.
Germany: One of my German colleagues informs me that Europe's most powerful shortwave transmitter will be built at Mindelheim, West Germany. The transmitter will beam programmes to all parts of the world during the Olympic Games at Munich. Six hundred announcers will inform sports fans all over the world about the Games in twenty-eight languages.

Great Britain: The Sunday broadcast of the BBC's "World Radio Club" programme is now broadcast at 0815 instead of 0930 .
Sweden: Due to interference problems Radio Sweden is altering the frequency of its broadcasts to Eastern North America from 9,710 to 5,990. This change concerns the English, Swedish and Spanish programmes broadcast between 0000 and 0230 .

## South America

Colombia: Emisora Atlantico, Barranquilla (HJAG) which is listed as inactive in the World Radio-TV Handbook is now operating on 4,905 until sign-off at 0500 with a power of 10 kW .

Ecuador: HCJB, The Voice of the Andes, uses two new frequencies of 15,415 and 17,780 for its programmes from 1845 to 2030.

Nicaragua: Radio Nacional de Nicaragua can be heard in Europe after 0100 on the new frequency of 11,875 .

73's and good DX until next time.

## THE AMATEUR BANDS David Gihson, G3JDG

AVERY good month for the DX hounds, but not too satisfying for those who only listened on 20 metres. This band, although, perhaps, the main DX band for many, has put on its winter overcoat of fading and is usually rather dead in the evenings.
The l.f. bands are beginning to come into their own and there has had been a noticeable improvement, especially on 40 and 80 .

Topband has helped to inspire its followers by allowing a few American c.w. signals across the pond and this is very heartening for topband transatlantic enthusiasts. Listen early mornings down the l.f. end for these sigs.

Honours this month go to 10 metres which played host to a very large number of signals throughout the month. Twice when your scribe's ears flapped over the $28-29 \cdot 7 \mathrm{MHz}$ segment, four of the continents could be heard during the same session. It's quite surprising how many a.m. signals are loose on this band as compared to, say, 14 MHz where sideband mostly dominates. The majority of the 10 metre signals were romping through at S 9 too, so don't forget to keep an eye on this band whenever you switch on.

Two sharp-eyed correspondents have drawn my attention to the G3RPE/P F2FO/P contact made on $10,000 \mathrm{MHz}$. Alas, my "red spot" transistors don't function up that far, but congrats to both operators on a very fine achievement! Who knows, now that the amateurs have shown that it's possible, the professionals may decide to have a go.

Just to be different, let's take a look at the happenings for the month when all good Christmas puds are stirred. Four main events down in my diary are: 6th-7th December, 80 metre c.w. contests; 6-7th, CHC International c.w. contest; 7th, 4 metre c.w. contest; 13th-14th, CHC international s.s.b. contest.

Don't forget that on Christmas morning there will be a large number of "local" club nets on the go. Topband is a favourite for these and some are quite witty. Certainly they all provide good festive r.f. entertainment. G3JDG promises to erect a reasonable antenna for topband on that morning and rude remarks concerning signal strength and mod. from over 25 miles would be appreciated.

So, where's it all been happening? Well, Charles Morgan (Northumberland), had great success on topband. Between 0430 and 0630 he logged K1PBW (599), KV4FZ (579), VP9GJ (459), W1BB/1 (599), W2EQS (359), W2IU (499). Figures in brackets are standard RST reports and all signals were c.w. Frequencies to listen from band edge to $1,805 \mathrm{kHz}$.

If you are still unconvinced that the l.f. end of the spectrum is worth a listen, how about the $\log$ from R. Bagwell (Surrey). He runs a Trio 9R59DE with a PR30 pre-selector, an RQ10 and a switched attenuator fed by an a.t.u. which in turn squints down a 70ft. long wire. Eighty metres revealed-CN8AW, HV3SJ, JW1CI, JW3KJ, VE1IE, PY7ASQ, PY7GV, TF5TP, VO1CW, VU1AX, 3V8NC, 3Z3BLG (new prefix for Poland) 5A2TR, all on s.s.b.

Philip Lawson (Derby), has an Ekco domestic receiver and sends in a long log bearing evidence of high Eu activity on 80 with the majority of stations at $S 8-9$, so there's plenty of stations on the band.

John Moore (Leicester), hasn't done too well on topband mainly due to high noise level with similar remarks for 80 , although he did $\log$ XE1KB at 0615 and says that W's are beginning to show on 75 metres around this time.

Higher up on good old 20 the stalwarts managed to pull in some good DX sigs even with the band closing in the evenings.

Trevor Rumble (Wilts.), has an HA700 plus PR3OX and a 100 ft . long wire. Twenty s.s.b. between 0720 and 0755 produced some good openings to Australia and stations logged included-VK2ID, VK3MO, VK3RZ, VK3UJ, VK5AX, VK6FB, VK7PR and ZL4BX at 5 and 9 plus 10dB.

Fifteen metres was the band for Stephen Randall (London), whose 9R59DE and 110ft. long wire produced r.f. music from s.s.b. types like-CR6LVC, CT1BF, CX2SA, EA3RF, EP2CB, JA2JAW, JA9AGP, JH1ODO, KP4AST, KZ5IT, LA7XM, TZ5CJT, VE3OSC, VU1FA, VK2ZQ, VK7AZ, VP2ME, WA9NSR/P1, YV4U'A, 4X4FQ, 4Z4HF, 5A2AAF.

Glyn Richards (Isle of Wight), is still the only 2 metre fan who writes in. What about it, all you v.h.f. types? Glyn runs a JXK converter into a Mohican receiver used as an i.f. strip. Although his antenna is only 6 ft . of wire, still the signals come in on 2. Examples include-G3CLW (Paignton) and G3MCS (Aylesbury), F5NS (near Normandy) and G3GZI (Redruth), the latter station being some 120 miles away.

On to the top of the pops for this month, the one and only- 10 metres. John Moore (see earlier) logged these on s.s.b.-CR6AG, CR6GM, CR6LF, CR7LX, DU1FH, ET3USA, HK4DF, K8YBU, K $\varnothing$ SFU, KP4DGX, LU3DD, LU4BH, MP4BHC, MP4BHR, OD5BA, OD5BZ, PY2DVH, UA9TT, VE2DHF/P/YV1, VE3CI/W4, VE3ABS, VP5AA (Caicos Is.), VP8KD, VP8KL. VQ8CV (Mauritius), VS6DR, VU2DK, VU2XX, VU2BEO, W2CRW, W4IQS, WA5SDT, WA8SWV, WøIMC, XW8AL, YV4UA, YV5CIL, ZC4AK, ZE1BP, ZE1JE, ZE3JJ, ZE6JN, ZS2GP, ZS4AA, 4X4UF, 4X4YP, 5H3KJ, 5H3LV, 5N2AAF, 8P6CX, 9J2DT, '9J2VX.

Nicholas Richardson (Bucks), has a CR7OA and PR30. Together with a 40 ft . long wire at 18 ft . they produced-CT1OF, K8ASM, KV4AD, OD5RZ, PY1MT, PY3GS, UA3NUE, VE2AIH, VE3WY, YV5BX, ZE1CE, 5B4EZ all on s.s.b.

On a.m., Nicholas managed-CE2JA, CR7FM, LU5XE, SV1CX, UA3AFA, UA6OJ, UA6ARA, UB5FAQ, WB4KJF, ZE1BR, 9H1BG which is pretty good going.

Ian Wadman (Berks) reckons that the JGD earholes should be alert on 10 metres on Sunday afternoons. Ian sends news of great activity around this part of the day. Ian logged CR7EZ, K4BG, OD5BZ, UW4II, ZE1JE, 4X4GB, 5N2AAF. All these with a CR70A and 70ft. long wire.

That's it for this year! Vy Mx OM's es benu in 1970. Address for logs is 5 Edward Close, St. Albans, Herts, and the deadline is that they must reach me by the 18th of the month.


ANY definition of electronics today would have to include among its applications not only computation and communications, but also control circuits. More and more mechanical and even electromechanical control systems are being replaced by all-electronic methods, and this month we shall see the initial contribution of integrated circuits to this process. The key device in the development of electronic control circuits is, of course, the silicon controlled rectifier (S.C.R.) in which the device operates as a diode only when a pulse is applied to a gate electrode. Following this event, the device conducts only as long as the voltage applied to it retains its proper polarity. In a.c. circuits, therefore, a separate pulse is required to initiate conduction in each cycle.

For full wave operation, two S.C.R.s are required, though these may take the form of a single bidirectional silicon controlled switch or TRIAC. To maintain conduction in a TRIAC 100 pulses per second are required, one to initiate conduction in each positive and negative-going half-cycle of the waveform. If these pulses are applied simultaneously with the beginning of each half-cycle of an a.c. waveform, the device behaves as a short-circuit, and current flows in exactly the same way as if the device were absent from the circuit.
If, however, the pulse is delayed relative to the start of the half-cycle, no current will flow in the interval, and the total power delivered to the load will be reduced by an amount dependent on the extent of the delay. Obviously, then, if a control system delays or eliminates pulses from the gate circuit of an S.C.R. or TRIAC, the output power is dependent on the control system. And this is where our I.C.s come in.

Many situations requiring power control can be sensed or measured electronically, for example temperature by a thermistor, illumination by a photoconductor, or even pressure by a strain gauge. Control is then exercised by relating transducer output to timing pulses in a TRIAC gate, limiting the power supplied to a heater, lamp, or pump. Two suitable I.C.s for the job are the General Electric types PA424 and PA436.

First the PA424. This unit is described as a zero voltage switch, and acts as a combined threshold detector and pulse generator. The signal from the transducer is compared with a preset internal voltage using the differential amplifier $\operatorname{Tr} 1$ and $\operatorname{Tr} 2$. If the threshold is not exceeded, pulses are generated and applied to the TRIAC; otherwise pulses are inhi-


Fig. 1: Circuit of the PA424 'zero voltage switch'. The device is supplied in a 14-lead dual in-line plastic package.


Fig. 2: Application circuit for the PA424. RT is the thermistor and Rc the temperature control preset.
bited and the TRIAC will not conduct. This circuit, then, acts as a go/no go control; to some extent this is a limitation, in that the circuit controlled is either fully on or shut off.

In practice this is only a slight problem, since in heating systems, for example, the sensitivity of a thermistor/PA424 combination is such that the temperature is held to within a fraction of a degree of the chosen value by the automatic succession of periods off and at full power. Further, as all the pulses occur at the instant of crossover between positive and negative-going half-cycle of the waveform. (hence the name "zero voltage switch") there is no question of repetitive switching of appreciable currents, a factor which can produce r.f. interference in some power control circuits.

One obvious advantage of the PA424 is that it serves as its own d.c. power supply; the application


Fig. 3: Application circuit for the PA436, phase control trigger circuit.

Choice of which I.C. to use in any particular situation requires some consideration. In heating circuits, for example, it will not be immediately obvious whether the element is conducting at any instant, provided overall thermal regulation is satisfactory. With lighting, we are all aware that the action of the a.c. mains in incandescent lamps provides quite a satisfactory light, and there is no objectionable flickering; however, this can occur under certain conditions with a PA424 controlled lamp, as the I.C. causes "off" periods much longer than the normal a.c. cycle. Similar considerations lead to the selection of the PA436 true proportional controller in a few other specialised situations, but in general the PA424 is advised, for its greater

| APPLICATION DATA, TYPE PA436 |  |  |  |
| ---: | :---: | :--- | :---: |
|  | Minimum | Maximum |  |
| External gain controls $\mathrm{R}_{\mathrm{G}}$ | $7.5 \mathrm{k} \Omega$ | $100 \mathrm{k} \Omega$ |  |
| $\mathrm{C}_{\mathrm{G}}$ | $0.01 \mu \mathrm{~F}$ | $0.1 \mu \mathrm{~F}$ |  |
| $\mathrm{R}_{\mathrm{A}}+\mathrm{R}_{\mathrm{B}}$ | $10 \mathrm{k} \Omega$ | $200 \mathrm{k} \Omega$ |  |
|  |  |  |  |

$\mathrm{R}_{\mathrm{A}}$ and $\mathrm{R}_{\mathrm{B}}$ : external control resistors (one may be a transducer, e.g. thermistor, photocell, resistive vacuum gauge etc.).
For temperature control systems $\mathrm{R}_{\mathrm{A}}$ is a thermistor of resistance about $5 \mathrm{k} \Omega$ at the controlled temperature: $\mathrm{R}_{\mathrm{B}}$ is a preset of $20 \mathrm{k} \Omega$.
The integrated circuits PA424 and PA436 are available from:
Jermyn Industries, Vestry Estate, Sevenoaks, Kent; or Neltronic Ltd., 14 Wellington Park, Belfast BT9 6DJ.
simplicity and economy, not to mention its "cleaner" r.f.i.-free operation. At any rate, control systems will become much more elegant with the elimination of slow bulky relays, with the associated difficulties of burnt contacts and general unreliability.
N.B. Just before going to press we have learnt from the suppliers of the PA436 that problems in manufacture have led to a temporary withdrawal of stocks. Newer versions using the same type number will be available in a few months but these are only capable of handling 150 mA instead of 2 A . Constructors should take careful note of the instructions supplied with this device which may modify certain parts of the above article.

## BLUEPRINT SERVICE

We would like to draw readers' attention to the fact that the BLUEPRINT SERVICE has been discontinued and therefore no further BLUEPRINTS are available.

# beginner's <br>  <br> <br> C.R.BRADLEY 

 <br> <br> C.R.BRADLEY}

ALMOST all radio constructors have memories of unsuccessful first attempts. Beginners are faced with a wide selection of designs and often make the mistake of choosing one that is too advanced for their nascent capabilities, or alternatively, one whose extreme simplicity leads to a disappointing performance. This portable radio design is intended for the beginner and aims to fulfil the following requirements:

1. The circuit must be straightforward and trouble
free. The radio is a six transistor superhet on conventional lines.
2. Performance must be good enough to repay the builder's efforts. In fact, performance of the radio is comparable with commercial portables. Alloy diffused transistors provide high gain in the mixer and i.f. stages, and the audio quality from the transformerless complementary output stage is especially good. No external aerial or earth is required.
3. All components must be immediately obtainable so that there will be no necessity to choose substitutes. To this end a matched kit of miniature coils and tuning capacitor is specified in the parts list. A packaged set of matched semiconductors is used for the audio stage. The remaining components are easily found, everything is available from advertisers in Practical Wireless.
4. Construction must be simple. The circuit is wired on a small piece of Veroboard using a suitable miniature soldering iron. There is a good prospect of the radio working "first try" provided normal precautions are taken in construction, i.e., insulated sleeving used where required to avoid shorts between closely mounted components, and correct identification of transistor, diode and electrolytic capacitor leads.

## The Circuit

The circuit is shown in Fig. 1. The ferrite bar aerial L1 is tuned to the desired station by VCl and


Fig. 1: The mixer/oscillator and i.f. stages, followed by the detector and audio stages. Note that the value of C6 should


the radio frequency signals induced in it are fed to the base of $\operatorname{Tr} 1$. Base bias current for $\operatorname{Tr} 1$ is provided by R1 and R2. C3 couples Tr1 base to a tapping on the oscillator coil L2, and $\operatorname{Tr} 1$ therefore oscillates at a frequency tuned by VC2. The radio frequency is mixed with the oscillation frequency in Tr 1 to produce a difference frequency known as the intermediate frequency. VC1 and VC2 are ganged together to maintain a constant i.f. (about 455 kHz ) as VCl is tuned over the whole tuning range (medium waveband). The importance of this is that subsequent stages can be tuned by their coupling transformers for maximum gain at one frequency only. $\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ amplify the i.f. signal and are coupled by single tuned i.f. transformers i.f.t.1, i.f.t. 2 and i.f.t.3. The AF117 transistor used for $\operatorname{Tr} 1, \operatorname{Tr} 2$ and $\operatorname{Tr} 3$ is an alloy diffused type with a low feedback capacitance ( $2-3 \mathrm{pF}$ ). We can therefore dispense with the neutralisation components normally needed to maintain stability with the OC44/OC45 junction type transistors which have a higher internal capacitance, and have a higher i.f. gain.

The amplified i.f. signal appears at i.f.t. 3 secondary. It is rectified and smoothed by D1 and C9 to isolate (detect) the audio envelope-see waveforms in Fig. 1. A portion of the audio signal is picked off by R5 and fully smoothed by C5 to provide automatic volume control to Tr 2 base. If a strong signal is tuned in, the resulting positive a.v.c. voltage returned to $\operatorname{Tr} 2$ base reduces the transistor's gain and overloading of subsequent stages is avoided. The a.v.c. compensates to some extent for fading signals and the signal variation caused by moving the radio from place to place. When a weak station is received, there is no a.v.c. feedback and all stages work at full gain.

The audio signal is applied across volume control VR1 whose slider feeds audio driver transistor $\operatorname{Tr} 4$. The amplified signal at $\operatorname{Tr} 4$ is direct cóupled to the base of complementary symmetry output pair $\operatorname{Tr} 5 /$ Tr6. The voltage drop across D2 is fairly independent of battery voltage and maintains the small no-


Fig. 3: Lead identification of various components.
signal bias current to $\operatorname{Tr} 5 / \operatorname{Tr} 6$ needed for minimum distortion. $\operatorname{Tr} 6(\mathrm{n}-\mathrm{p}-\mathrm{n})$ and $\operatorname{Tr} 5(\mathrm{p}-\mathrm{n}-\mathrm{p})$ are turned on by positive and negative voltage swings respectively. The transistors drive the loudspeaker in pushpull; each supplies current alternately through C13. This arrangement provides a very low output impedance which permits the circuit to drive the speaker directly without an output transformer. D.C. feedback for stability and a.c. feedback for improved audio quality are provided by R17 and VR2. VR2 is preset to give a no-signal voltage of -5 V at the junction of R14 and R15.

The audio output power is about $\frac{1}{2}$ watt. With a $7 \times 4 \mathrm{in}$. or larger loudspeaker, volume and clarity are more than ample. The radio is best built in a non-miniature cabinet for best audio quality. But the circuit board is small enough to be incorporated in a pocket size radio in which case a 2 in . loudspeaker could be used.


Fig. 2: Veroboard layout viewed from the copper side.

## Construction

The components are wired on a standard piece of Veroboard and the layout is given in Fig. 2. The numbers and letters provide a cross-reference for each hole. The top and bottom copper strips (unlettered) are left unused for possible use in mounting the Veroboard in the cabinet.

First cut the Veroboard strips as shown, preferably with the Vero cutting tool. There are 36 breaks in all. It is advisable to mark (say) the top left-hand corner of the board before starting for identification. Wiring is easier if the positions of the components are sketched on the top of the board with a fibre-tip pen. Identify the three i.f.t.s ("A", "B", "C") and oscillator coil L2 ("O") in the coil kit. Bend up the screening can lugs. With slight persuasion the coil pins will make a neat fit in the Veroboard holes in the positions shown in Fig. 2. Solder them in place. It may be noticed that the lefthand pair of pins on the oscillator coil L2 in Fig. 2 are connected oppositely to the manufacturer's data with the coil kit. The author has decided the data is incorrect as the stage will only oscillate with this way of connection, with the coils sampled at least. However, if the mixer subsequently refuses to oscillate, it is easy to try swapping the connections at 2 L and 1 N to agree with the manufacturer's data. Short pieces of wire are used to earth the screening cans of L2, i.f.t.1, i.f.t. 2 and i.f.t. 3 to holes $8 \mathrm{~L}, 5 \mathrm{~B}, 13 \mathrm{~B}$ and 21 B respectively. Resistors and capacitors are next mounted with the shortest possible lead lengths, mostly upright. Put a piece of plastic sleeving on the lead from the top of each component wherever there is any danger of it touching any adjacent metal. This is particularly likely if bare metal-cased electrolytic capacitors are used. Electrolytic capacitors must be wired the right way round, i.e., positive lead to earth (except C10 and C13). Finally, solder the diodes and transistors to the board, making sure the leads are identified correctly from Fig. 3. Note that the lead identification of D2 can be misleading. Some surplus transistors marked AF117 were tried by the author and worked satisfactorily; however the lead arrangement was non-standard for AF117 (see Fig. 3) and they


Fig. 4: Adding a socket for a low impedance magnetic earpiece.
had no screen lead. The screen lead of the AF117 has little use at the frequencies used here and can be cut short or connected to the nearest earth point as preferred. Leave about $\frac{1}{2}$ inch of sleeved lead on all transistors and diodes and solder as quickly as possible to avoid heat damage.

The cabinet for the author's prototype was a Woolworth's plastic lunch box. The top of the box carries the tuning capacitor, volume control VR1 and


Internal view of the completed receiver.


Fig. 5: Adding a bass/treble tone control.


Fig. 6: Adding a socket for microphone, guitar, record player etc.
the ferrite aerial is taped underneath. The calibrated knob supplied with VC is rather small and a larger disc of plastic glued to it would make tuning easier. The $7 \times 4 \mathrm{in}$. loudspeaker is mounted in the side of the box and the aperture is covered with Tygan speaker fret. The largest 9 volt battery the cabinet
-continued on page 706

# practically Wireess commentary by IENKI 

SIX hundred million people, we are told, watched Neil Armstrong plant his foot in the moondust on 20th July, 1969 -the day that President Nixon, begging a few questions, described as ‘ . . . the greatest since Creation'.

You have had time to simmer down since then; to consider the equally stupendous achievement of discovering that Mars has no little green men paddling along its canals. And perhaps join a disgruntled chorus who were muttering, even as the Eagle took flight, that the $24,000,000,000$ dollars might have been better spent on child welfare, cures for cancer or ear-muffs for under - privileged ocelots.


In answer to these mutterings the science-bent will usually say something about the spin-off. Non-stick aluminium frying pans often find their way into the conversation.
"And it took 300,000 technicians eight years to produce a non-stick pan?" someone is bound to ask.

Well, there is more to it than that. Many of the technical innovations creeping into our lives had their origins in space research.
You need look no farther than
the flip-chips that are occupying our editorial wizards at present. How do you think contributors could continue to dream up ten different ways of constructing an electronic shoehorn * $\dagger$ without integrated circuits to save them from repetitions? Only recently I sat in a high-level quorum who wanted to know how the advent of IC designs would affect serviceability. And had to admit that my own opinion was for a shift in emphasis, no more. I cannot see the spin-off as a threat-yet.
There is, however, a much more human type of spin-off problem. Inspiration was drawn from a very readable book, Don't Launch him, he's mine! by Mary Jane Chambers, who is the wife (or space-widow) of one of the boffins behind the Apollo project.

Randall Chambers is an experimental psychologist whose work on the centrifuge which gave the astronauts their moon-legs has earned him world scientific recognition. Mary Jane describes life with him very amusingly and touches Henry on several risible trigger-points.

First, his "study", which seems as typical as the den of any wireless ham I've met. Looking like "a library recently wrecked by an explosion", it houses "piles of graphs, notes, charts of atmospheric measures and weights and measures and maps of many places, including outer space. There are railway timetables, old telephone books, a sterilizer with an assortment of old surgical instruments . . . an assortment of synthetic hearts, brains, ears, skulls. Overlooking all, a huge model of the human eye, staring balefully at the casual visitors".

More than ever am I reminded of life with the Henrys by Mrs. Chambers' account of the day the children knocked the extractor fan out of the window. There were present: an aeronautical engineer, a project engineer, a mechanical engineer and a

". .s. Staring balefully at the casual visitors."
human factors engineer. "Prodded by several doctors and psychologists, the engineers hesitantly studied the fan, but they made no promises. Each one kept saying: 'I'm not that kind of engineer'".
They finally mended it with the help of a flight-surgeon and a research psychologist. That gives you and me, Joe, a fine excuse for the day the 'fridge breaks down or the washing machine develops a "kerplunk". We are chips specialists, not that kind of engineer.
If only Mrs. Henry, confronted with a scattered square-wave generator on the draining-board -because that is just the right height and the soldering iron lead will reach, and there is a halfdrawn "project" on the only flat surface of the den-would realise, as Mary Jane has done, that a male brain runs anti-clockwise . . .
I hope Mrs. Chambers gets her book serialised in the women's magazines. That would be the best possible spin-off from the space-race. Henry wants to construct a few of these chipflavoured projects, and the ironing-board seems ideal for the purpose. We boffins need encouragement.

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[^5]
## Martians Again!

Whilst not having heard that Marconi claimed to have received signals from Mars as A. Trowbridge of Middlesex says, I was told many years ago that some person who believed in the existence of men on Mars paid the GPO a sum of money to transmit a certain regular pattern of Morse code signals each day either from Daventry or Rugby, on long waves.

I was told that this went on for quite a time but with no response from the Red Planet.

I would imagine that we shall not hear anything from other planets until we are able to probe frequencies such as those involved in thought-transference and in which extra-sensory perception is only on the extreme outer fringe.

When the thought-transference frequencies are discovered, all will be plain sailing.

In answer to the letter from Mr. Richard Ross of Worcester, I think perhaps he is using a plumber's soldering iron and no heatsink!-R. Hall (Penzance, Cornwall).

## The Early Days

I would like to comment on two of the letters in the November issue.

As another "oldie" I also remember the early days of wireless. Around 1917 I made an 8in. dia. coil, tapped every turn to a stud switch for tuning, and. a coherer as detector, with which I could hear Morse from ships. As I could not read Morse a recorder was made to mark it on paper tape.
The gift of a box camera, loaded in the dark with 12 glass plates, took my interest for some years, but when broadcasting started interest in wireless was revived, and a crystal set was made using the large coil.

The purchase of a valve was a big step, there was not much money to spare in those days. Two tins sliding inside each other made an experimental condenser. A real $0.005 \mu \mathrm{~F}$ tuning condenser was the next purchase, and with a few more home-made items mounted on a base-board, and a 3 ft . long wooden rod fitted to the
condenser shaft, it was a thrill to hear Sydney, Australia, for the first time.

A fortunate find at a surplus shop in Strutton Ground was a number of fixed condensers made of copper foil and mica sheets clamped between ebonite plates. These could easily be altered to give other capacities. I still have some of the mica.

Then with the arrival in shops of more components, remember Igranic and Telsen etc? a multivalve receiver was built with elaborate dials and panel of ebonite on an oak case. The loudspeaker was a 6 ft . papier-maché exponential horn which was pretty good. Next, to save the space this took up, I made a stretched doped linen cone 2 ft . square which hung up like a picture. It was some time before an 8in. permanent-magnet speaker could be bought and mounted in a 3 ft . square board as - a "firescreen". That gave beautiful music.

The h.t. battery was made from a lot of little glass pots, copper, zinc and chemicals obtained from a chemist in Charing Cross Road. I was just married then and my wife and I sat for hours packing manganese dioxide in linen bags. The finished battery giving 120 volts was packed in a wooden crate. L.T. was from an accumulator, one in the set and one at the shop being charged. The local electricity station also charged them for you.

Licences at that time were in my father's name as the householder, but I still have one for 1927. On the back are regulations such as "the combined height and length of the aerial shall not exceed 100 feet", "interference is taking place if a... whistle is heard, if this... changes when the wavelength of the receiver is altered the cause is inside the receiver and the reaction must be reduced".

At an early Radio Exhibition I bought "Commander Someone's" aerial device for which marvellous results were claimed. It made no difference in my case so I opened it to find no wonderful new invention, only a coil of wire and a small condenser in a
card tube filled with pitch.
A trick to mystify friends was to wind a certain number of turns of wire around the hand, twist one end to a needle resting on a piece of coal and with headphones hear 2LO. For this you still required a licence!

I have some sub-min diodes in a small tin labelled the "Mighty Atom Crystal", one of the first I bought and mounted in Wood's metal in a brass cup.

No doubt youngsters nowadays get some satisfaction when they put supplied components into holes in a printed-circuit board and it works, but I bet it is not the kind of thrill we got in those early days, and now with cheap i.c's. even less is left to the constructor.

The second item I would refer to is the Hertz, a term which I refuse to use, and no one can make me! The good old "cycle per second" is clear and selfsufficient, whether for electrical or mechanical purposes. Imagine, my watch ticks 5 Hz . And Hz itself could mean Henry $\times$ Impedance.

As to the new mains-lead colours, can anyone explain the reasoning behind the decision to use brown for live. Is it not natural to us to connect the colour red with danger, green with safety and black or grey with neutral? Brown has usually been used for things like valve heater supplies. Anything red made one think before touching. Do "they" contemplate changing all the traffic warning signs to brown? Shall we soon hear it referred to as the "Brown Button"?

I could not agree more with Mr. Harold's last paragraph. Trouble is, except in things like using Hz , we do have to acquiesce. Of course, behind the decimal currency there is a welllaid scheme to put prices up and get even more of our money out of us, as well as using our money to effect the change. I feel that in major decisions such as this, and any others which profoundly affect our way of life, there should be a nation-wide referendum. After all, in most of the things being altered, we WERE first. - E. W. Baigent (High Wycombe, Bucks.).


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T-HE number of devices using semiconductor materials to meet specific-requirements in electronic circuits is increasing rapidly as research and development continues on an unprecedented scale. The devices examined in this part of the series are the most common and easily obtainable of such devices, but because of the diversity and number of items to be discussed only general practical information has been included. Further detailed information can usually be obtained from manufacturers. Let us now examine the usage, construction, limitations, cost and operation of each type.

## Variable Capacitance Diode or Varactor

The variable capacitance diode, varactor or voltage variable capacitor is a device which behaves essentially as a capacitor and circuit symbols are shown in Fig. 1. The capacitance is however capable of variation by means of a d.c. bias voltage. It is therefore particularly useful for automatic frequency control (a.f.c.), frequency modulation, fine tuning and bandwidth regulation. Varactors are also used for frequency multiplication purposes at microwave frequencies.

Varactors are constructed from single p-n junction semiconductor material and are operated in the reverse -non-conducting-direction, the capacitance being the normal diode junction capacitance. They are thus diodes which utilise normal diode construction-such as the alloy, diffusion or planar processes described in a previous part in this series. The junction size and impurity levels are modified to give the required capacitance values and characteristic. A typical capacitance against reverse voltage characteristic is shown in Fig. 2.


Fig. 1a, b (left): Circuit symbols for a diode used as a variable capacitor or varactor.
Fig. 2 (right): Reverse biased diode capacitance characterIstic.

It is worth noting that all semiconductor diodes exhibit a similar characteristic and can therefore be used by the home constructor for applications where variable capacitance diodes are required. However the actual capacitance level differs from diode to diode and for most signal diodes is reduced to a minimum since it is parasitic and determines the upper frequency limit of the diode. Improvisation can nevertheless save time and expense and the home constructor is well advised to try a selection of available diodes for a.f.c. and oscillator tuning applications.

The ideal varactor should have all the characteristics of a capacitor: low leakage, low capacitance tolerance, stability and reliability. The real device closely approaches this ideal except for leakage current which is generally $0 \cdot 1 \mu \mathrm{~A}-10 \mu \mathrm{~A}$ and is generally higher than all but eletrolytic capacitors. Capacitance tolerance varies and is usually $\pm 10 \%$ or $\pm 20 \%$. Stability and reliability are both good as it is a semiconductor device. The main disadvantage is the requirement for a d.c. bias since they are polarised devices; also the Q factors, which are generally $30-40$ for the v.h.f. range low cost units, although Q factors up to 500 can be obtained.


Fig. 3: Varactor encapsulations.
As varactors employ the basic diode structure the encapsulations follow the same pattern. Oscillator trimming and a.f.c. diodes at v.h.f. frequencies, with capacitances of approximately 30 pF at 1 V reverse, usually employ standard glass encapsulations as shown in Fig. 3(a). Microwave varactors which operate at extremely low capacitance values from $0 \cdot 1 \mathrm{pF}$ to 10 pF , with reverse voltages in excess of 50 V , utilise special low capacitance encapsulations such as that illustrated in Fig. 3(b). Microwave varactors-which operate in various bands up to 250 GHz -frequently operate at higher power levels and consequently have metal encapsulations which directly connect to heatsinks to give increased dissipation.

With all semiconductor devices costs are largely determined by the level of demand and the tolerance ratings and yield of the device. Varactors are no exception and glass encapsulated v.h.f. devices with high
demand levels and low Q factors (10-40) are available from 7s. to 30 s . whilst devices with higher $Q$ factors and tuning ranges can cost from $£ 2$ to $£ 5$. Microwave varactors, particularly power devices, are correspondingly more expensive and cost from $£ 3$ to $£ 20$ for low power and from $£ 15$ upwards for high power types.

## Tunnel Diode and Backward Diode

Tunnel diodes, like varactors, are two-terminal singlejunction devices, but unlike the varactor their action is active in that they are capable of producing power gains despite the two-terminal configuration. They are used as oscillators, amplifiers and switching devices and can be used up to very high frequencies. Indeed tunnel diodes are used in amplifiers operating at 6 GHz . They are extremely stable components and crystal controlled transmitters and chronometers use tunnel diodes particularly in frequency division circuits-where three tunnel diodes can give an accurate frequency division of 2,000 to 1 . At present the circuit symbol for the tunnel diode has not been standardised and consequently a selection of symbols is shown in Fig. 4, with the B.S. preferred symbol indicated.

(a)

(b)

(C) B.S. pretferred

Fig. 4: Tunnel diode symbols.

A typical tunnel diode characteristic is illustrated in Fig. 5 and this clearly indicates its essentially active mode of operation. The characteristic shows a peak and a valley, and a region between in which the current falls with increase in voltage, indicating a negative resistance and therefore unstable region. Switching action from point A to point B can occur and is used to aid tuned circuits to give gain or oscillations. Following this region the characteristic follows a normal diode characteristic as would be expected from its single p-n junction structure. This curve is shown for comparison.


The mechanism which produces the negative resistance region in the characteristic is called the quantummechanical tunnelling effect, from which the device takes its name. This rather awe-inspiring terminology
tends to overwhelm the potential user but-although the mechanism is mathematically complicated to prove -this should not be a deterrent to the practical engineer. Suffice it to say that the tunnelling effect causes an increase of current at a definite point in the characteristic by sweeping or tunnelling the electrons across the junction, thus producing the characteristic of Fig. 5. The parameters quoted by manufacturers confine themselves to the characteristic and when considered with the characteristic are relatively self-explanatory. Table 1 shows the parameters with a range of values for typical general-purpose tunnel diodes. Microwave diodes up to 40 GHz have negative conductance values of 65-75 mhos $\times 10^{-3}$ and capacitance values of $0.35-5 \mathrm{pF}$.
Backward diodes are tunnel diodes with current values below 0.5 to 1 mA and a consequent negative resistance greater than $1 \mathrm{k} \Omega$. The characteristic is consequently modified and a typical backward diode characteristic is illustrated in Fig. 6. The peak point

current varies from 0.01 to 1 mA with capacitance values of $1-20 \mathrm{pF}$. The characteristic allows the backward diode to be particularly useful as mixer and detector diodes at extremely high frequencies.
Both tunnel and backward diodes, being single p-n junction structures, use normal diode manufacturing techniques. They are manufactured from germanium material with extremely heavily doped, small area junctions. The heavy doping produces the tunnelling effect whilst the small junction area minimises junction capacitance. Due to the extremely high operating frequencies lead inductance is a problem and is reduced to a minimum ( 0.5 nH to 5 nH ) in diodes operating below 2 GHz which use axial or TO-18 packages. Epoxy resin plastic packages are used and have lead inductances of $1-2 \mathrm{nH}$ whilst microminiature pill packages having lead inductances of 0.1 nH are used for microwave diodes. Some typical encapsulations are illustrated in Fig. 7.

Tunnel diode costs vary considerably but increase

Table 1 : General purpose tunnel diode parameters with typical values

| Peak point <br> current <br> Ip | Max. valley <br> point current <br> Iv | Peak <br> voltage <br> Vp | Max. series <br> resistance <br> Rs | Capacitance <br> C | Negative <br> conductance <br> G | Cut off <br> frequency <br> from |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1-25 \mathrm{~mA}$ | $0.5-5 \mathrm{~mA}$ | $50-60 \mathrm{mV}$ | $1-10 \Omega$ | $5-150 \mathrm{pF}$ | $4-200 \mathrm{mhos}$ <br> $\times 10^{-8}$ | $1-4 \mathrm{GHz}$ |

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rapidly in the regions beyond 1 GHz . Average axial and plastic package diodes for use below 1 GHz are available from 15 s. to $£ 4$, with metal encapsulations ranging from 30s. to $£ 7$. Microwave devices are available from $£ 10$ upwards.

## Unijunction Transistor

As its name implies the unijunction transistor is a three-terminal, single-junction device and its symbol is shown in Fig. 8. The circuit operation is however unlike either a transistor or diode, as indeed is the construction.


Fig. 8a, b (left): Unijunction transistor symbols. Fig. 9a, b (right): Unijunction transistor constructions.

The structure consists of a block of resistive semiconductor material with a junction formed at a definite position along the length of the bar. Leads are connected to the ends of the bar and are denoted base 1 and base 2 whilst the connection to the junction is referred to as the emitter. Hence the designation double base diode which was the original term for this device. At present only n -type silicon is used for the bar and the junction is formed by alloying or diffusing a p-type impurity at the required point along the bar. Typical alloy and diffused junction constructions are shown in Fig. 9 and although alloy junction types are the cheapest as well as the most widely used the diffused construction is increasingly popular due to the low leakage currents and faster switching times. Encapsulation is usually in the familiar TO-18 and TO-5 transistor casing although plastic is used increasingly for the cheaper devices. At present terminations are not completely standardised and the manufacturers' data should be consulted.

The circuit operation of the unijunction transistor can be understood by referring to Fig. 10 which shows the essential diagrammatic structure and its equivalent


Fig. 10: Basic unijunction structure.
circuit. If the battery is connected as indicated, a voltage gradient is set up in the high resistivity n-type bar. As a result the position of the junction along the bar determines the positive potential required at the emitter terminal to enable the p-n junction diode to conduct. Thus if the battery is 12 V and the junction is midway between base 1 and base 2 -the potential required to make the diode conduct is $(6 \mathrm{~V}+$ diode drop) $\simeq 6.7 \mathrm{~V}$. This parameter is sometimes quoted in specifying unijunction transistors and is known as the peak point emitter voltage ( Vp ). The resistance ratio which determines this potential on the equivalent circuit is $\left(\frac{R 1}{R 1+R 2}\right)$ and this is known as the intrinsic standoff ratio $(\eta)$. Hence to turn on the unijunction transistor the emitter voltage must satisfy the following equation:

$$
\begin{align*}
\mathrm{V} \text { emitter }=\mathbf{V p} & =\left(\frac{\mathbf{R} 1}{\mathbf{R} 1+\mathrm{R} 2}\right) \mathrm{V}_{\mathrm{B}}+\mathbf{V d} \\
& =\eta \mathbf{V}_{\mathrm{B}}+\mathbf{V d} \tag{1}
\end{align*}
$$

Since the intrinsic standoff ratio $\eta$ determines $V p$ for any supply voltage this is always quoted as a parameter and for any given device has a stated tolerance.

When the diode is made to conduct by this potential Vp then the base 1 resistance $R 1$ reduces rapidly to a low value-thus causing a rapid increase in emitter current and a drop in emitter voltage towards zero volts. This effect is achieved by the electron input through the emitter causing the reduction in resistivity of the base 1 region of the bar structure.

In order to reduce the base 1 region to low resistivity a minimum current into the emitter is required. This parameter is called the peak point current (Ip) and is clearly shown in the unijunction characteristic Fig. 11.

Fig. 11: Unijunction transistor characteristic.


The characteristic also shows the negative resistance region which causes the switching action and the stable saturation region which is achieved after Ip is exceeded. Ip is usually of the order of 0.5 to $100 \mu \mathrm{~A}$ and $\eta$ of the order of 0.5 to 0.85 . The total resistance known as the interbase resistance $R_{\text {вв1 }}$ varies between $4 \mathrm{k} \Omega$ and $12 \mathrm{k} \Omega$. Other parameters supplied by the manufacturer are peak emitter current $(\sim 2 \mathrm{~A})$, power $\left(\mathrm{P}_{\mathrm{D}}\right)$, maximum base to base voltage ( $\mathrm{V}_{\mathrm{B} 2} \mathrm{~V}_{\mathrm{B} 1}, \sim 30-50 \mathrm{~V}$ ) and frequencywhich can be in the megacycle region.

It can be seen from the characteristics that until the diode conducts the impedance is very high ( $1-10 \mathrm{M} \Omega$ ) whilst at switch on it drops rapidly towards zero. When coupled to a charging capacitor it is off until Vp is reached, then rapidly conducts and discharges the capacitor. When the discharge current falls below Ip it switches off and the capacitor can recharge to Vp. Thus it is useful as a relaxation oscillator but can also be used for thyristor triggering, voltage sampling and in protection circuits.

The disadvantages of unijunction transistors are that the ratio $\eta$ varies considerably as it depends on the
positioning of the junction-as a result the turn-on emitter voltage (peak point voltage Vp ) also varies considerably. In addition these parameters are affected by temperature.

Unijunction transistors are available at varying price levels depending on the demand, range of tolerance of $\eta$ and hence $V p$, and frequency response. Cheapest types are plastic encapsulated at 5 s . with high frequency, low leakage devices available at 9 s . to 35 s . At present only p-type emitter devices are available as shown by the symbol which indicates-in the emitter arrow-the direction of current flow. If n-type emitter devices become available they will be expensive initially and as with transistors the reversal of current flow will be indicated on the symbol by a reversal of the emitter arrow.

## TO BE CONTINUED

## PRACTICAL TELEVISION in the JANUARY issue

$\star$ DEVELOPMENTS IN TV RECEIVERS

A detailed account of the changes that have been taking place in TV receivers in recent years, including the introduction of i.c.s and single-standard operation.

## * A CONSTRUCTOR'S 625-LINE RECEIVER

Details of a 17 in . 625 -line receiver built up by a constructor to provide superior performance, including black-level stabilisation.

## *TRANSISTOR LINE DRIVER STAGES

Line output driver stages are unique to fully transistorised receivers and present some tricky design problems. A detailed. look is taken at these problems and the methods of successfully overcoming them.

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[^6]
## BEGINNERS PORTABLE RECEIVER

-continued from page 695
will accommodate should be used. The wires between L1, VC and the board must be short and not liable to flexing or the alignment will be affected. If possible, L1 and VC should be fixed rigidly to the Veroboard to ensure this. The wires connecting the volume control to the board are not so critical.

## Operation

The receiver should work fairly well without any alignment at this stage and the coil cores must not be adjusted indiscriminately if it does not. If there is no sound, the stages can be checked individually as follows. Connect one end of a capacitor (about $0.1 \mu \mathrm{~F}$ ) to battery negative and touch the other end to successive transistor bases, working from the loudspeaker to the aerial. Clicks should be heard in the loudspeaker until the faulty stage is located.

The radio works well without an external aerial but this can be used by adding C1 to the circuit (see Fig. 1). A car aerial can be connected in this way. If the connection of the external aerial upsets the radio tuning unduly or causes overloading, use a smaller value for C .

## Alignment

If the radio is receiving signals, it can be aligned without other equipment if proper care is taken. Tune in a weak station at the centre of the range. Use a plastic screwdriver blade (e.g., a filed down plastic knitting needle or toothbrush handle) to adjust i.f.t.1, i.f.t.2, i.f.t. 3 for the strongest signal. Repeat this adjustment several times, keeping the signal tuned in as well as possible with VC. Find a weak station at the l.f. end of the range. Adjust L2 oscillator core in one direction somewhat and retune the station with VC. If the reception is better, continue adjusting the dust core in the same direction until the best signal is obtained; if the reception is worse, adjust in the opposite direction. After each core adjustment, the same station must be retuned with VC. Retune VC to a weak station at the h.f. end of the range and adjust VC2 trimmer for correct station position. Finally adjust VCl trimmer for maximum signal strength. The process must be repeated until best results are obtained. Alignment is now complete.

A socket for a magnetic earpiece can be connected as shown in Fig. 4. The same socket can be used to operate extension speakers. If the socket is wired as shown, the radio speaker is muted when anything is plugged in.
Figure 5 shows a treble/bass tone control that can be added to the circuit. R16 and C12 are no longer used and should be removed from the board. The tone control reduces the audio gain slightly but provides a useful range of adjustment.

The audio stages can be used as a useful loudspeaker amplifier for microphone, guitar, signal tracing, record playing, etc. by adding a socket as shown in Fig 6.


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0.55 OA5
OA9 $\mathrm{OA9}$
$0 \mathrm{OA47}$ OA47 OA81 OA85
OC23 0 C 23
0 C 25 0 C 25
0 C 26 0C28
 Additional Transistors-AF147 and AF150, 24V. Larger en current 10 mA . gain $70-4 /$ - each. AF149-gann 225-4/6 each Also $8 \mu \mathrm{~F} 350 \mathrm{~V} 1 / 2.25 \mu \mathrm{~F} 20 \mathrm{~V} 1 / 3$ and $50 \mu \mathrm{~F} 50 \mathrm{~V} 1 / 8$. Other electrolytics in current inst Postage, Packing and Insurance all mbove $1 /-u p$ to 11,12 and over charges paid. 2 GANG VAR. CONDEESERR: Mod., air-spaced, ${ }^{\circ} 0005$ ea. sec. $5 /-(1 /-)$. 8 GANG, $7 / 6$ ( $1 /-$ ) SUB-MIN TRANSFORMERS: Output ( $3 \Omega$ for OC72 ete.) 2/6. Driver $2 / 9$ (up to six, I/-) MULTMMETER: $20,000 \Omega / V$ D.C., $10,000 \Omega / V$ A.C. $0-5 / 25 / 50 / 250 / 500 / 1 \mathrm{~K}$ voits D.C

 at $47 / 6$ (2/6) $1000 \Omega / V$ described in free list
SOLDERING IRON. Slim Mod. British High speed. $8 \frac{1}{4}$ in., all parts replaceable, fully guaranteed for professional, radio and generat D.I.Y. use. 19/6 (1/6)
DIAMOND STYLI. Replacements for BSR TC8LP, TC8/S and TC8LP/STEREO COLLARO "O"; RONETTE BF40LP; GARRARD GC2LP and GCSLP; ACOS GP65/67 all at $7 / 6$ each ( $1 /$-). ACOS GP91 ST/LP; BSR ST4 and ST9; BONOTONE 9TA an 9TAHC, PHILIPS AG3306, 30 (3) $18 / 6(1 /-)$. all at 18/6(1/-)

PIGK-UP CARTRIDGES. All fitted Styli and Standard fitings. Mono GP67/2, 18/6 Stereo Compatible-Mono which also plays Stereo records monaurally with min. wear, GP91/SO, 19/6. Latest Stereo GP9B. 24/6. Ceramic Stereo, top quality for expensive
PRS ELIMMNATOR (A.C.) 17/6. (I/6) TWO STATION TRANS. INTER-COM. Excellent baby alarm. Instant, easy fitting with leads, plugs and battery. All you require $52 / 6$ (3/-) TRANSISTORISED AMPLIFLERS. 3 watt, $9 V$ operation, $45 / 6$ ( $1 / 6$ ); $7 \frac{1}{2}$ watt, 6 trans 24V operation, $67 / 6$ (2/6). Extra High Torque MINI-MOTOR, $4 \frac{1}{2}$ to $12 \mathrm{~V}, 14 \times$ zin. $5 /-$ (1/-). 9,000 r.p.m.
SUBSTITUTION BOXES, Capacitance $25 / 6$ (1/6). Resistance $32 / 6$ (1/6). Both full range and SUBSTITUTION BOXES, Cap
complete. Full details in list. TEST PRODS: Flexible, unbreakable 24in. Red and Black leads, thin $4 \frac{1}{4} \mathrm{in}$. prods, $1 \pm i \mathrm{in}$. pluge $4 / 9$ (1/-). Croc. Clips: Plated with screw, or with red/bluck handles, 8 d . exch, $5 /-\mathrm{doz}$. ( $1 /-$ ). RECORDING TAPE: Finest quality British Mylar. STANDARD: 5in. 600ft. $7 / 8_{1}, 5 \frac{3}{3} \mathrm{in}$. $850 \mathrm{ft} .8 / 9,7 \mathrm{in} .1200 \mathrm{ft} .11 / 3$. KONG PLAY $5 \mathrm{in} .900 \mathrm{ft} .10 /-, 5 \neq \mathrm{iz}$. $1200 \mathrm{ft} .11 / 3,7 \mathrm{in}$. 1800 ft . 18/- ( $1 / 3$ reel). Still the finest quality and value obtainable.
MYCROPHONES-CRYSTAL. MIC91, Desk, 16/3; MIC45, curved hand grip 17/6; Stick "60" 20/8; Stick "39" 28/6 (1/6 each type). Cream plastic hand type "/6, or with "strut" stand, 8 witch and 2 leads with $2 \cdot 5$ and $3 \cdot 5$ plugs $12 / 6$ (1/3). Lapel (or hand) with clip $6 / 6$ (1/-). Machined metal tapered stick type with neck cord and adio $50 \mathrm{~K} \Omega$, $3 \pm \times$ zin with stands, 2 i/- (1/0). DYiAuMc, Cream har but fixed on fiexible swan neck to switch-fitted base $42 / 6$ (2/6). Dw128 Uni-directional, $50 \mathrm{~K} / 600 \mathrm{ohms} \mathrm{imp}$, stand adaptor, very high quality 6 x $\times 2 \times 1$ inin, 95.9 .8 ( $5 /-$ ). . GARDIOLD DYNAMIC OMNT-DIN with bullt-in vol. control. switch $50 \mathrm{~K} / 600$ ohms imp. \$5.17.6 (either type $5 /-$ ). Full details in list.
MICROPHONE INSERTS: Diameter $1 \cdot 75 \mathrm{in}$. or 0.9 in . either size $5 / 6$ (I/-
SPEAKERS: 12ib. round, fitted Tweeter. 6 W. 3 or $15 \Omega$ (state which), $87 / 6$ (5/6); or for stereo, 80/-per pair (charges paid); $2 \sin$. $3 \Omega 8 / 6$ (1/-); $6 \times 4$ heavy duty $3 \Omega 14 / 6$ (3/6) or for stereo 34/6 pair charges paid), (1/-). $5 / 8$ (1/-). HEADPHONES: High Res. 20008 ea. replacement speaker, high onms, exiece $18 / 6(1 / 6)$; Stereo $D y n-16 \Omega 68 /-(3 /-)$. EARPIECES with lead and min. jack plug, magnetic 1/9, Crystal $4 / 9$ (up to 3 for $1 /$ on either). State if 2.5 mm . or 3.5 mm . plug required. (Crystal 3.5 mm . only.)
ARRIALS, Car Types: Telescopic, vandal proof, locks retracted, 2 keya and all fittings, $22 / 6$ (2/6) Motor driven, $12 \mathrm{~V}, 5$ section, complete $27.10 .0(5 /-)$.
FOR ALL PORTABLES and F.M. SETSS. 7-gection $\overline{5} \frac{1}{2}-32 i n$., no swivel, screw hole in base, 6/6. 10 -section $6 \frac{1}{\mathrm{~g}}-47 \frac{1}{2} \mathrm{in}$., no swivel, serew hole in base, $12 / 6$. DISAPPEARING 8 section, swivel fixing assembly, $6 \frac{1}{2}-$ and $1 /(1 /-$ all sizes $)$. 4/-, (1/- all sizes).
DPST 3/न. DPDT 3/b. Slide iype. Sub-min. DPDT $1 / 6$ each. Small DPDT 3 way. centre 'off' $1 / 9$. Reed magnetic on/ofi $1 / 8$ (up to three, 1/-: 1d, each all additional). Rotary Switches etc. in list.
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Flexible $8 /$ Super thin for transistor wiring etc. $3 /-$ (1/- all types per 5 coils), PICK-UP Flexible $8 /$-. Super thin for transistor wiring etc. $3 /-(1 /-$ all types per 6 coils). Pick-UP Wost free). TWIN MIKE CABLR: $1 / 3$ yd. SINGLE MIKE CABLE: 7d. yd. Both flexible, screened and sheathed. (Up to 3 yds 8d., each additional yard, 1 ã, extra.)
R.F. INDICATOR, 5-Band, with meter antenna, monitoring crystal earpiece etc., $48 / 6$

RETRACTABLE FLEXIBLE LEADS. Space saving "Curly", many uses in car and home: with phono plug each end, Bft., 4/6; 12it., $7 / 9$. With phono plug one end, phono socket at other, $6 \mathrm{ft} ., 5 /-, 12 \mathrm{ft} ., 8 / 6$ (1/- each all types).
CAR RADIO: Splendid new All-British dash-mounting radio using Mullard transistors and circuit. M. and I. wave. Separate speaker and baffe. Absolutely complete, for + or - chassis. E11.11.0 (6/6). A huge success since introduction
corinnthe slent with all orders or free for s.a.e. details of cable, croc. clips and leads, Continental din plugg for Grundig, Telefunken equipment, etc., dials, plugs and sockets, eqfipment. terminals, tape recorder, special transistors, portable sets, more switches and other components, tools, Veroboard etc., etc. This advertisement cancels all previous ones and lists supplled prior to November 30th.

## FELSTEAD ELECTRONICS

(PW26) LONGLEY LANE, GATLEY, CHEADLE, CHESHIRE, SK8 4EE
TERMS: Cash with order only. No C.O.D. or caller service. Post, packing and insurance charges are shown in brackets after all ttems, Regret orders under $\overline{\text { a }}$-plus carriage cannot oe accepted, and a minimum charge of $1 /$ - is now made. Charges apply o ins. S.A.E. pleate for all enquiries, otherwise regret cannol be replied to

This month's special Christmas project describes a three transistor radio which is highly selective together with a good output level. By careful 'shopping around' among the advertisers the complete radio may be built for under 20 s ; as usual less than twenty components are used

AFEW months ago our project was a one transistor radio which did not require an external aerial and operated a loudspeaker; however this design did have limitations-especially volume which was mentioned in the text. With Christmas just around the corner there must be many readers who would like to take advantage of their interest in electronics and knock up something for the children, and it was with this specifically in mind that this month's project was planned.

First, the radio had to have decent selectivity and volume, and as it is intended primarily for children it had to be able to get Radio Luxembourg well. The circuit had to be reliable and quickly built. (To this end three prototypes were built to ensure the circuit was reliable.) Building of the prototype shown in the photographs took under three hours including the cabinet. Also the radio had to have a presentable but cheap case.

## The Circuit

There is nothing particularly unusual about the circuit. The first transistor acts as an r.f. amplifier with VR1 as its collector load. Positive r.f. feedback (regeneration) is taken from the slider of VR1 and connected via VC 2 to the top of the aerial coil.

The r.f. signal is fed to the base of Tr2 which is biased in such a way as to detect the r.f. signal, the output is smoothed by C3. The audio output is d.c. connected to $\operatorname{Tr} 3$, the output transistor. The emitter resistor is bypassed by C 4 , the base bias for Tr 2 being taken from this circuit via R3, $100 \mathrm{k} \Omega$. The $200 \mu \mathrm{~F}$ capacitor, C5, decouples r.f. and a.f. from the positive rail.

## Components

Care will have to be taken in the purchase of components to come within our 20 s . maximum. Whereas aerial coils can be bought, it is far cheaper and very

## No. 9 <br> THREE TRANSISTOR RADIO



The Take 20 three transistor radio.
simple to wind your own. For this L1 should consist of about 70 turns and L2 of 5 turns on a four to six inch length of $\frac{3}{8} \mathrm{in}$. or $\frac{1}{4} \mathrm{in}$. ferrite rod. VCl may be any type of tuning capacitor between 200 pF and 350 pF . For economy the loudspeaker should be a $6 \times 4 \mathrm{in}$. size removed from old TV sets.

## Construction

All components apart from the speaker, VR1, VC1 and the battery are mounted on an eleven-way minia-



Fig. 2: The components are mounted on an eleven way tagboard. Compare this with the photograph.
ture tag board as shown in Fig. 2. The ferrite rod is secured to this board by tying one end to the top of the tag board as shown in the photograph.

The cabinet front is made from a piece of hardboard $9 \times 5$ in. to which are fixed the sides made from $2 \frac{1}{2} \times \frac{1}{2}$ in. planed softwood. These sides should be glued and nailed together and nailed with hardboard pins to the side framework. Holes must of course be drilled for the speaker and the two controls. The tag board is held inside the case by making a small bracket, one end of which is bolted to one of the holes in the tag board and the other screwed to the inside of the case ensuring that the ferrite rod is not too close to the speaker magnet.

The cabinet front can be covered with speaker fabric or any reasonably strong material. This should be cut exactly to size and glued. The sides and the back of the cabinet are covered in self-adhesive plastic covering such as Fablon. The junction of the speaker fabric and plastic covering may be hidden by using black plastic tape.

## OUERYCOUPON

This coupon is available until 7th January, 1970 and must accompany all queries in accordance with the rules of our Query Service.

PRACTICAL WIRELESS, JANUARY 1970

## $\star$ components list

## Resistors:

| R1 | $100 \mathrm{k} \Omega$ | R3 | $100 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- |
| R2 | $100 \mathrm{k} \Omega$ | R4 | $56 \Omega$ |

All $\frac{1}{8}$ or $\frac{1}{4}$ watt, $10 \%$ miniature types
VR1 $5 \mathrm{k} \Omega \log$ pot. with switch
Capacitors:

| C1 | $0.1 \mu \mathrm{~F}$ | C4 | $200 \mu \mathrm{~F} 9 \mathrm{~V}$ |
| :--- | :--- | :--- | :--- |
| C2 | 2000 pF | C5 | $200 \mu \mathrm{~F} 12 \mathrm{~V}$ |
| C3 | $0.01 \mu \mathrm{~F}$ |  |  |
| VC1 | 250 pF variable-see text |  |  |
| VC2 |  |  |  |
| Vee text |  |  |  |

## Miscellaneous:

Tr1, Tr2, T3r BC169C; Ferrite rod with windingssee text; T1, transistor output transformer, approx. 4.5:1; Loudspeaker $3 \Omega$; Battery PP7 or equivalent; Eleven-way tag board; Hardboard and softwood for case-see text; Speaker fabric; Self-adhesive plastic covering.


An interior view of the prototype.

## Conclusion

Assuming everything has been wired up correctly the only adjustment is that of VC2 and this, being frequency selective, should be peaked so that the set just fails to break into oscillation on Radio Luxembourg. VC2 consists of two lin. lengths of wire twisted together. Incidentally the gain of the first stage is so high that unless the general layout is carefully followed there is a danger of the set continually oscillating. Because of the fairly high capacitance of Veroboard it is not to be recommended for this particular project.

> Next month's Take 20 article describes a small, cheap, transformerless amplifier. It provides between 750 mW and 1 W into a $3 \Omega$ loudspeaker.

[^7]

MONOLITHIC INTEGRATED CIRCUIT HIGH FIDELITY AMPLIFIER AND PRE-AMP


# theworld's most advanced high fidelity amplifier 

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output of 5 watts R.M.S. ( 10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 zenor diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.

The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of the usual tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required for producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. It also enables us to give a 5 year guarantee on each IC-10 knowing that every unit will work as perfectly as the original and do so for a lifetime.

## SPECIFICATIONS

Output 10 Watts peak, 5 Watts R.M.S. continuous. Frequency response 5 Hz to $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$. Total harmonic distortion Less than $1 \%$ at full output. Load impedance 3 to 15 ohms.
Power gain $110 \mathrm{~dB}(100,000,000,000$ times) total. Supply voltage Size
Sensitivity
Input impedance
$1 \times 0.4 \times 0.2$ inches.
5 mV .
Adjustable externally up to
2.5 M ohms.

## CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class $A B$ output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

## APPLICATIONS

Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

SINCLAIR

IC. 10with IC. 10 with $1 C .10$
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# 2.30 <br> <br> THE WORLD'S LOWEST DISTORTION <br> <br> THE WORLD'S LOWEST DISTORTION HIGH FIDELITY AMPLIFIER. 

 HIGH FIDELITY AMPLIFIER.}

For four years, the Sinclair $Z .12$ dominated the constructor world, being the best selling unit of its kind this side of the Atlantic. Excellent as it was, the new Sinclair $Z .30$ is still better. Half the size of the Z.12, it has more than twice the power, very much greater gain and a level of distortion 50 times lower. This incredible figure results from using over 60 dB of negative feed back with a constant current load to the driver stage obtained by incorporating a two transistor circuit in place of the more usual boot-strapping. 9 silicon epitaxial planar transistors are used to provide enormous power (up to 20 watts RMS continuous sine wave, 40 watts peak). The circuitry of this marvellous amplifier allows it to be operated from any voltage from 8 to 35 to perfection.

At all output levels, distortion is only $0.02 \%$. This puts true laboratory standards into the hands of every user of a Z.30. Two Z.30s and a new Stereo Sixty will make a stereo assembly of such perfection that it could not be bettered in its class no matter how much you spent. But the $Z .30$ has an enormous variety of applications, particularly where quality, precision and reliability are essential. Yet this brilliant new Sinclair design costs not a penny more than its famous predecessor.

## APPLICATIONS

Hi-fi amplifier; car radio amplifier; record player amplifier fed directly from pick-up; intercom; electronic music and instruments; P.A.; laboratory work, etc. Full details for these and many other applications are given in the manual supplied with the $Z .30$.


## SPECIFICATIONS

Power output: 15 watts R.M.S. into 8 ohms using a 35 volt supply: 20 watts R.M.S. into 3 ohms using a 30 volt supply.

Output: Class AB.
Frequency response: 30 to $300,000 \mathrm{~Hz}$ $\pm 1 \mathrm{~dB}$.
Distortion: 0.02\% total harmonic distortion at full output into 8 ohms and at all lower output levels.
Signal-to-noise ratio: better than 70 dB unweighted.
Input sensitivity: 250 mV into 100 Kohms . Damping factor: > 500.

Loudspeaker impedances: 3 to 15 ohms.
Power requirements: From 8 to 35 V . d.c. (The $Z .30$ will operate ideally from batteries if required).
Size: $3 \frac{1}{2} \times 2 \frac{1}{4} \times \frac{1}{2}$ inches.

## Built, tested and guaranteed, with circuits and instructions <br> 89/6 manual




Curves to show bass and treble cut and boost


This attractive and completely new unit is intended for use with two new Z.30 amplifiers to provide the finest possible standards of stereo reproduction. Four press buttons and four rotary controls are used to provide on-off, three input selectors and Volume, Bass cut/boost, Treble cut/boost and Stereo balance. The on-off button also switches the power amplifiers. The front panel in brushed aluminium is flush mounted to the cabinet front, it being necessary only to drill holes to accommodate the controls. Rear adjustable brackets hold the chassis tight to the cabinet. The very latest ganged rotary controls are used to afford compactness and extra long working life free from noise.
The Stereo-60 may also be used with 2 IC-10's or any other high performance amplifiers.

## SPECIFICATIONS

- Inputsensitivities-Radio-upto 3 mV Magnetic Pickup -3 mV ; correct to R.I.A.A. curve $\pm 1 \mathrm{~dB} ; 20$ to $25,000 \mathrm{~Hz}$. Ceramic Pickup-up to 3 mV : Auxiliary -up to 3 mV .
- Output-1 volt.
- Signal-to-noise ratio-better than 70 dB .
- Channel matching-within 1 dB
- Tone Controls-TREBLE +15 to -15 dB at 10 kHz . BASS +15 to -15 dB at 100 Hz .
- Power consumption 5mA.
- Front panel-brushed aluminium with black knobs and controls.
- Size $8 \frac{1}{4} \times 1 \frac{1}{2} \times 4$ ins


## PZ. 5 POWER SUPPLY UNIT

A new heavy duty mains power supply unit designed specially to drive two $\mathrm{Z.30}$ s and a Stereo Sixty. New compact design. For AC Mains, $200-240 \mathrm{~V} / 50 \mathrm{~Hz}$.
£4.19.6

### 0.16 Loudspeaker and Micromatic on next page.



## SINCLAIR 0.16 <br> new elegance in an outstanding loudspeaker

All the superb features which went to make the Sinclair 0.14 have been incorporated in the new 0.16 which gives an exciting new opportunity for you to match your Sinclair equipment with modern decor. Employing the same well proven acoustic system in which materials, processing and styling are used in such a radical and successful departure from conventional design, the new 0.16 presents an entirely new appearance with its attractive teak surround and all-over special cellular foam front chosen as much for its appearance as for its ability to pass all audio frequencies without loss. The 0.16 is compact and slim. Its new styling makes it eminently suitable for shelf mounting, but it is no less versatile than its famous predecessor. Listen to a pair of 0.16 s in stereo and marvel at the standards of quality and clarity they give.


The 0.16 will handle loading up to 14 watts R.M.S. and presents an 8 ohm impedance to the amplifier output. Frequency response extends from 60 to $16,000 \mathrm{~Hz}$ with exceptional smoothness. A specially designed driver system is used in a sealed and contoured pressure chamber to ensure good transient response at all frequencies. Size: $9 \frac{3^{\prime \prime}}{4}$ square $\times 4 \frac{3{ }^{\prime \prime}}{}{ }^{\prime \prime}$ deep from front to back.

## f8.19.6

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The world's most successful miniature radio


SPECIFICATIONS-Size: $1 \frac{13^{\prime \prime}}{}{ }^{\prime \prime} \times 1 \frac{7}{16}{ }^{\prime \prime} \times \frac{1}{2}^{n}$ ( $46 \times 33 \times 13 \mathrm{~mm}$ ). Weight incl. batteries: 1 oz ( 28.35 gm ) approx. Tuning: Medium wave band with bandspread at higher frequency end. Earpiece: Magnetic type. Case: Black plastic with anodized aluminium front panel, spun aluminium dial.

Complete kit incl, earpiece, case,
solder and instructions in fitted
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| For which I enclose cash/cheque/ money order | ................................................. PW. 170 |

Considerably smaller than an ordinary box of matches, this is a multi-stage A.M. receiver meticulously designed to provide remarkable standards of selectivity, power and quality. Powerful A.G.C. is incorporated to counteract fading from distant stations; bandspread at higher frequencies makes reception of Radio 1 easy at all times. Vernier type tuning plus the directional properties of the self-contained special ferrite rod aerial makes station separation much easier than with many larger sets. The plug-in magnetic earpiece which matches exactly with the output provides wonderful standards of reproduction.
Everything including the batteries is contained within the attractively designed case. Whether you build your Micromatic or buy it ready built and tested, you will find it as easy to take with you as your wristwatch, and dependable under the severest listening conditions.

## USE THIS COUPON FOR MICROMATIC AND Q. 16 ORDERS

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# BEIIER Bargains Service FROM TRS 

## BUILD THIS FINE VERSION OF THE PW.12-12 WITH A TRS KIT

T.R.S. have produced their own kIt version of this outstanding combined stereo amp and pre-amp. It conforms precisely to Practical Wireless' excellent circuit but is styled for a flatter, more conventional cablnet which will be avallable shortly. Kit includes two-tone front panel and control knobs, components and transistors.

Inputs-Mag. P.U. (R.I.A.A.) 2.5mV into 68 Kohms; Ceramic P.U. and Radio; Response 20 Hz to $30 \mathrm{KHz} \pm 1 \mathrm{~dB}$. Output-12 watts per channel. R.M.S. Into 15 ohms.

Kit complete, $£ \mathbf{2 4 . 1 0 . 0}$ Kitse aniabible semataiely.


## AMPLIFIERS

Styled and kitted by T.R.S., using quality comT.R.S. service.
MULLARD 5-10. Basic kit (requires pre-amp). Input Sensitivity-40mV; Response $20 \mathrm{~Hz}-15 \mathrm{KHz} \pm 1 \mathrm{~dB}$; Output 10 watts R.M.S. at 3 or 15 ohms. KIT £10.10.0. BUILT £13.0.0 (Carr. either, 7/6).
MULLARD 2 VALVE PRE-AMP. Switching for 5 inputs; bass/treble/ volume controls, etc. Sensitivity at input- 4 mV max. into $80 \mathrm{~K}-1$ Megohm; Response $20-25,000 \mathrm{~Hz} \pm 1 \mathrm{~dB}$. KIT £6.19.6. BUILT $£ 9.10 .0$ (Carr. either $5 / 6$ ). MULLARD 10-10 STEREO AMPLIFIER. Input sensitivity- $\mathbf{2 1 0 \mathrm { mV }}$ per channel; Response $12 \mathrm{~Hz}-35 \mathrm{KHz} \pm 3 \mathrm{~dB}$; 10 watts R.M.S. output per channe into 3 or 15 ohms. KIT £18.10.0. BUILT £22.10.0 (Carr. elther 12/6),
Basic Kit (no panel or controls) £17,0.0. Built £21.0.0. Pre-amp must be used here,
MULLARD $2+2$ STEREO PRE-AMP with same characteristics per channel as mono pre-amp ( + balance). BUILT £13.19.6 (Carr. 7/6).
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£1.17.6 (Carr. 2/6)
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WEYRAD P50—TRANSISTOR COILS RA2W 6in. Ferrite Aerial Spare Cores with car aerial coil ...... 12/6 $\quad$ Driver Trans. LFDT4....... 9d. Osc. P50/1AC ..............5/4 Printed Circuit, PCA1. I.F. P50/2CC $470 \mathrm{kc} / \mathrm{s}$...5/7 $/$ J.B. Tuning Gang 3rd I.F. P50/3CC...........6/-6/ Weyrad Booklet Telescopic Chrome Aerials 6in. extends to 23in. 5/Ferrite Rods Oniy $8 \times{ }^{3}$ in. 4/-

80 ohm Coax 8 $8^{\mathrm{D}}$ yd. Long spindles. Midget Size BRITISH AERIALITE 5 K. ohms to 2 Meg . LOG or AERAXIAL-AIR SPACED
 Edge 5K. S.P. Transistor, $5 /$-. WIRE-WOUND 3-WATT POTS. WIRE-WOUND 3-WATT T.V. Type Knurled Knob.
Values $10 \Omega$ to $\left.30 \mathrm{~K} ., 4 / 6 \begin{array}{l}\text { STANDARD SIZE POTS } \\ \text { LONG SPINDLE }\end{array}\right] / 6$ Carbon 30 K to 2 meg .

$$
\text { VEROBOARD } 0.15 \text { MATRIX }
$$

$2 \frac{1}{2} \times 5 \mathrm{in} .3 / 8$. $2 \frac{1}{2} \times 3 \frac{3}{2} \mathrm{in} .3 / 2 .{ }^{3} 3^{\frac{3}{4}} \times 3 \frac{3}{3} \mathrm{in} .3 / 8.33_{i}^{3} \times 5 \mathrm{in} .5 / 2$
PINS 36 per packet $3 / 4$. FACE CUTTERS $\% / 6$.
S.R.B.P. Board 0.15 MATRIX $2 \frac{1}{2}$ in. wide 8 d . per 1in 3 in. Wide 9 d. per 1 in. ; 5in. wide $1 /-$ per 1 in. (up to $1 \%$ in. $)$ S.R.B.P. undrilled $/ 15$ in Board $10 \times 8$ in. $3 /-$.

 ALUMINIUM PANELS 18 s.w.g. $12 \times 12 \mathrm{in}$, , $6 / 6 ; 14 \times 9 \mathrm{in}$
 Complete: a die, a punch, an Allen screw and key

 WAVE-CHANGE SWITCHES $1 \frac{1}{s}$ in. Diameter.
2 p .2 -way, or 2 p .6 -way, or 3 p . 4 -way $4 / 6$ each.
2 p. 2 -way, or 2 p. 6-way, or 3 p. 4 -way $4 / 6$ each.
1 p. 12 -way, or 4 p. 2-way, or 4 p. 3 -way, $4 / 6$ each
1 inch Diameter Wavechange "MAKITS' 1 p. 1 p. 12 -way, 2 p . 6 -way, 3 p. 4 -way, 4 p. 3 -way, 6 p. 2 -way, 1 waier $12 /$-, 2 wafer $18 /-, 3$ wafer $24 /-, 4$ wafer $30 /-5$ wafer $36 /$.
TOGGLE SWITCHES, sp. 2/6; sp. dt. $3 / 6 ;$ dp. $3 / 6$; dp. dt. 4/6


BARGAIN STEREO/MONO SYSTEM
Attractive Slim PLAYER CABINET with B.S.R. Stereo
Autochanger, 3 valve Stereo Amplifier, two $6 \frac{1}{2}$ in. LOUDAutochanger, 3 valve Stereo Amplifier, two $6 \frac{1}{2}$ in. LOUD-
SPEAKERS. (Only 4 pairs of wires to join). f19,19. 6
Carr. 10/6. S.A.E. for details SPEAKERS. (Only 4 pairs of
Carr. 10/6. S.A.E. for details

| NEW TUBULAR ELECTROLYTICS | CAN TYPES |  |  |
| :--- | :--- | :--- | :--- |
| $2 / 350 \mathrm{~V}$ | $\ldots .2 / 3$ | $100 / 25 \mathrm{~V}$ | $2 /-$ |
| $2 / 600 \mathrm{~V} .$. |  |  |  | $2 / 350$

$4 / 350$
$4 / 350 \mathrm{~V}$
$8 / 450 \mathrm{~V}$
$16 / 450 \mathrm{~V}$
$32 / 450 \mathrm{~V}$
$25 / 25 \mathrm{~V}$
$50 / 50 \mathrm{~V}$
STB N... $2 /-\left\lvert\, \begin{array}{llll}10+32 / 350 \mathrm{~V} & 4 / 6 & 32+32+32 / 350 \mathrm{v} .8 /- \\ 100+50+50 / 350 \mathrm{v} & 9 / 6\end{array}\right.$ SUB-MIN. ELECTROLYTICS. 1, 2, 4, 5, 8, 16, 25, 30, 50, 100 , $250 \mathrm{mF} 15 \mathrm{~V} 2 / \mathrm{F} ; 500,1000 \mathrm{mF} 12 \mathrm{~V} 3 / 6 ; 2000 \mathrm{mF} 25 \mathrm{~V} 7 /-$ CERAMIC. 500 V 1 pF to $0.01 \mathrm{mF}, 9 \mathrm{~d}$.
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${ }_{4}^{\frac{1}{4}} \mathbf{W}$.
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$B$ or 12 v . outputs. $1 \frac{1}{2}$ amp. $8 / 9 ; 2$ amp. $11 / 8 ; 4 \mathrm{amp}$. $17 / 6$.
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AF139
AF139
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BSY28-9
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$\mathrm{OC26-35}$
$\mathrm{OC} 28-29$
OC44-45
OC4
OC71-81
OC72-75
OC72-75
OC81D-82D
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OCP71
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    Come and spend an interesting evening (free tea and sandwiches), which will include a colour film entitled SOMETHING BIG IN. MICROCIRCUITS. Ian Nicholson of Mullard Ltd., will be the principal speaker. W. N. Stévens, Editor, Practical Wireless and Practical Television will be in the chair.

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