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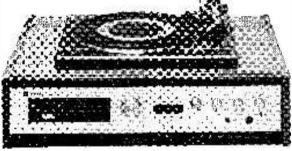
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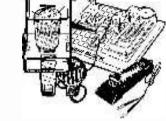
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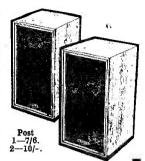
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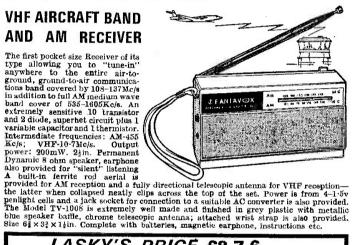


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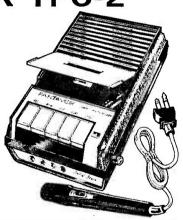
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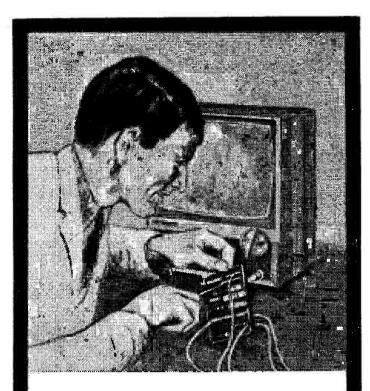
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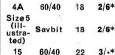
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SETS 1R5, 185, 174, 384, 3V4, DAF91, DF91, DK91, DL92, DL94. Set of 4 for 18/6, DAF96, DF96, DK96, DL96, 4 for 26/6.

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Z4	4/6	12K8GT 7/8	DK91	5/9	EH90	6/3	PCL83	9/-		
A7GT	7/6	129N7GT6/6	DK92	8/3	EL33	8/9	PCL84	7/6	UBF89	
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R5	5/9	20P3 11/9	DL92	5/9	EL84	4/9	PENA4		UCC85	6/
85		20P4 18/6		6/-	EL90	4/6	PFL200	11/9	UCF80	7/
T4	2/9	25L6GT 5/-	DL96	7/-	EL500		PL36	9/9	UCH42	11/
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V4	6/-	30C1 6/6	DY87	5/9	EM81	7/6	PL82	6/6	UCL82	67
U4G	4/6	30C15 13/-	EABC8	0 6/6	EM84		PL83	6/6	UCL83	117
Y3GT		30C17 16/-	EAF42		EM87	7/6	PL84	6/6	UF41	10/
Z4G	7/6	30C18 11/6	EB91	2/3	EY51		PL500		UF80	71
/30L2		30F5 16/-	EBC33	8/-	EY86		PL504	13/6	UF85	6/
AL5	2/3	30FL1 13/9		9/6	EZ40	8/-	PL508	23/6	UF89	6/
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AT6	4/-	30LI 6/6	ECC81	3/9	EZ81		PX25	10/6	UL84	7/
AU6	4/6	30L15 14/-	ECC82	4/9	GZ32	8/0	PY32		UM84	2
BA6	4/6	30L17 15/6	ECC83	7/-	GZ34	8/9 9/9	PY33		UY41	6/
BE6	4/9	30P4 12/-	ECC85	5/-	KT61	8/9	PY81	5/3	UY85	5/
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T 6	3/-	35W4 4/6	ECH81	5/3	PC97	8/6	R20	12/6		7
K7G	2/6				PC900	7/6	U25	13/-	AF115	3/
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V6GT	6/6	B729 12/6	ECL86	8/-	PCC89	10/6	U52	4/6	AF127	3/
X4	4/3	CCH35 13/6	EF37A	6/6	PCC189	11/6	1078	4/8	OC26	5/
X5GT	5/9	CL33 18/6	EF39	4/9	PCF80	6/6	U191	12/6	OC44	2/
B7		CY31 6/9	EF41	10/9	PCF82		U193	8/6		2/
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F1		DAF91 4/8	EF85	5/8	PCR200	19/6	11201	10/6		2/
0F18		DAF96 6/6	EF86	6/3	PCF200 PCF800	13/6	11329	14/6	OC75	2/
)P13		DF33 7/9	EF89	5/3	PCF80	8/0	11801	19/6	OC81	2/
2AT7		DF91 2/9	EF91	2/9	PCF80	9/-	UABC			2/
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NEW! roamer eight mkl WITH VARIABLE TONE CONTROL

7 Tunable Wavebands: Medium Wave 1, Medium Wave 2, Long Wave, SW1, SW2, SW3 and Trawler Band. Built in Ferrite Rod Aerial for Medium and Long Waves. Five section 22in. chrome plated Telescopic aerial for Short Waves can be angled and rotated for maximum performance. Push pull output using 60 mW transistors. Socket for oar aerial. Tape record socket. Selectivity awitch. Switched earpiece socket complete with earpiece for private listening. Eight transistors plus 3 didotes. Famous make 7 lin. x im. Speaker. Air spaced ganged tuning condenser. On/Off switch volume control. Wave change switch and tuning control. Attractive case in rich obestunt shade with gold blocking. Size x x x in. approx. Easy to follow instructions and diagrams make the Roamer Eight a pleasure to build.

Parts Price List and Easy Build Plans 61- (FREE with parts).

Parts Price List and Easy Build Plans 5/- (FREE with parts).



roamer seven mkIV

*

SEVEN FULLY TUNABLE WAYE-BANDS—MWI, MW2, LW, SWI, SW2, SW3 and Trawier Band. Extra Medium waveband provides easier tuning of Radio Luxembours, etc. Built in ferrite rod aerial for Medium and Long Waves. Five Section 22in chrome plated telescopic aerial for Bort Waves—can Sw. listening. Socket for Car-Aerial, Powerful pushpul of the Car-Aeria, Powerful pushpul of the Car-Aeria, Powerful pushpul of the Car-Aeria, Powerful pu

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P.& P. 7/6

NEW!

trans eight SIX WAVEBAND PORTABLE WITH

3in. SPEAKER Attractive case in black with red grille and cream knobs and dial with polished brass in-

with polished brass inserts. Size 9 x 5½ x 2½in.
approx. Tunable on Medium and
Long Waves, three Short Waves and Trawler
Band. Sensitive ferrite rod aerial for M.W. and L.W.
Telescopic aerial for Short Waves. Eight improved type
transistors plus 3 diodes. Push pull output. Ample power to drive
a larger speaker. Parts price list and easy build plans 5/- (FREB
with parts). Earpiece with switched socket for private listening

Total building costs 89'6

pocket five

MEDIUM WAVE, LONG WAVE AND TRAWLER BAND PORTABLE WITH SPEAKER AND EARPIECE

Attractive black and gold case. Size 5½ x 1½ x 3½in. Tunable over both Medium and Long Waves with extended M.W. band for easier tuning of Luxembourg, etc. 7 stages—5 transistors and 2 diodes, supersensitive ferrite rod aerial, fine tone moving 'coil speaker, also Personal Earpiece with switched socket for private listenling. Easy build plans and parts price list 1/6 (FREE with parts).



Total building costs

transona five

MEDIUM WAVE, LONG WAVE AND TRAWLER BAND PORTABLE WITH SPEAKER AND EARPIECE

Attractive case with red speaker grille. Size 6\frac{1}{2} \times 4\frac{1}{3} \times 1\frac{1}{3} \times 1. \times 1. \times 2 \times 2 \times 1. \times 2 \times 1. \times 2 \times 2 \times 1. \times



P. & P.

roamer six

SIX WAVEBAND PORTABLE WITH 3in, SPEAKER

Attractive case with gilt fittings. Size 74 x 54 x 14 in. Tunable on Madium and Long waves, two short waves, Trawler Band Plus an extra M.W. band for easiler tuning of Luxembourg, etc. Sensitive territe rod aerial and telescopic aerial for Short waves. 8 stages—8 transistors and 2 diodes including Micro-Alloy B.F. Transistors etc. (Carrying strap 1/8 extra). Easy build plans and parts price list 2/-. (FREE with parts).



Total building costs P. & P.

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Complete stereo system – 28 gns.

The new Duo general-purpose 2-way speaker system is beautifully finished in polished teak veneer, with matching vynair grille. It is ideal for wall or shelf mounting either upright or horizontally. Type 1 SPECIFICATION:-

Type 1 SPECIFICATION:—
Impedance 10 ohms. It incorporates Goodmans high flux 6" × 4" speaker and 2½" tweeter. Teak finish 12" × 6½" × 5½". 4 guineas each. 7/6d. p. & p. Type 2 as type 1. Size 17½" × 10½" × 6½". Incorporating 10½" × 6½" bass unit and 2½" tweeter. 3 ohms impedance 5½ guineas plus 7/6 p. & p.

Garrard Changers from £7.19.6d. p. & p. 7/6d. Cover and Teak finish Plinth £4.15.0d. 7/6d. p. & p.

The items illustrated can be purchased tagether for 28 gns.

The Duetto is a good quality amplifier, attractively styled and finished. It gives superb reproduction previously associated with amplifiers costing far more.

SPECIFICATION:-

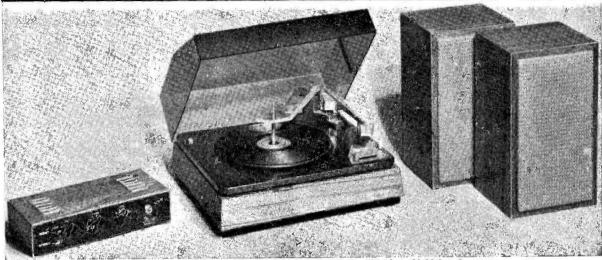
R.M.S. power output: 3 watts per channel into 10 ohms speakers.
INPUT SENSITIVITY: Suitable for medium or high output crystal cartridges and tuners. Cross-talk better than 30dB at 1 Kc/s. CONTROLS: 4-position selector switch (2 pos. mono and 2 pos. stereo)

dual ganged volume control. TONE CONTROL: Treble lift and cut. Separate on/off switch. A preset

balance control.

Duetto Integrated Transistor Stereo Amplifier

9GNS. plus 7/6d.



The above 5 items can be purchased together for £29.10 + £1.10.0 p. & p.

£9 plus 7/6 p. & p.

Controls: Selector switch Tape speed equalisation switch (32 and 71 i.p.s.), Volume, Treble, Bass, 2 position scratch filter and 2 position rumble filter.

Specification: Sensitivities for 10 watt output at 1KHz Into 3 ohms. Tape head: 3mV (at 32i.p.s.). Mag.P.U.: 2mV. Cer.P.U.: 80 mV. Tuner: 100mV. Aux.: 100mV. Tape/Rec. output: Equalisation for each input is correct to within ± 2dB (R.I.A.A.) from 20Hz to 20KHz. Tone control range; Bass ± 13dB at 60Hz. Treble ± 14dB at 15KHz. Total distortion: (for 10 watt output) <1.5%. Signal noise: <-60dB. A.C. mains 200-250v. Built and tested. Size 122in. long, 4in. deep, 2in. high. Teak finished case.

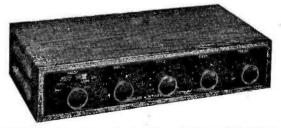




£14.5 plus 7/6 p. & p.

Integrated High Fidelity Transistor Stereo Amplifier. Specification-Output: Integrated High Fidelity Transistor Stereo Amplifier. Specification—Output: 10 watts per channel into 3 to 4 ohms speakers (20 watts monaural). Input: 6 position rotary selector switch (3 pos. mono and 3 pos. stereo), P.U., Tuner, Tape and Tape Rec. out. Sensitivities: All inputs 100mV Into 1:8M ohm. Frequency Response: 40Hz-20KHz ± 26H. Tone Controls: Separate bass and trable controls; treble, 13dB lift and cut (at 15KHz); Bass, 15dB lift and 25dB cut (at 60Hz). Volume Controls: Separate for each channel. A.C. Mains Input: 200-240V. 50-6Dt. Size, 41½" x6" x2" in teak finished case. Built and tested. VISCOUNT MARK II for use with magnetic pick-ups specification as above.

Fully equalised for magnetic pick-ups. Sultable for cartridges with minimum output of 4mV/cm/sec. at 1kc. Input impedance 47k. £15.15 plus 7/6 p. & p.



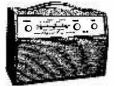


SPECIAL OFFER!

Complete stereo system comprising BALFOUR 4-speed autoplayer with stereo head, 2 Duo speaker systems, size 12in. x 6\frac{2}{2}in. Plinth (less cover) and the DUETTO stereo amplifier. All above items

£20 plus 20/- p. & p.

Also see opposite page



Circuit 2/6 FREE WITH PARTS.

The ELEGANT SEVEN Mk. III (350mW Output)

7 transistor fully tunable M.W.-L.W. superhet portable. Set of parts. Complete with all components, including ready etched and drilled printed circuit board—back printed for foolproof construction.

MAINS POWER PACK KIT: 9/6 extra.

Price £4.9.6 plus 7/6 P. & P.

The DORSET (600mW Output)

7-transistor fully tunable M.W.-L.W. superhet portable—with baby alarm facility. Set of parts. The latest modulised and pre-alignment techniques makes this simple to build. Sizes: $12 \times 8 \times 3$ in.

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MAINS POWER PACK KIT: 9/6 extra





EXTRACTOR FAN

A.C. mains 230/250v. complete with pull switch. Size $6 \times 6 \times 4$ in.

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X101

10W SOLID-STATE HI-FI AMP WITH INTEGRAL PRE-AMP

Specifications: Power Output (into 3 ohms speaker) 10 watts. Sensitivity (for rated output): 1mV into 3K ohms (0·33 microamp). Total Distortion at 1KHz at 5 watts, 0·35%, at rated output 1·5%. Frequency Response: Minus 3dB points 20Hz and 40KHz. Speaker: 3-4 ohms (3-15 ohms may be used). Supply voltage: 24V. D.C. at 800mA (6-24V. may be used).

Price 69/6 plus 2/6 P. & P.



Control assembly: including resistors and capacitors. 1. Volume: PRICE 5/-. 2. Treble: PRICE 5/-. 3. Comprehensive bass and treble: PRICE 10/-. The above 3 items can be purchased for use with the X101.

Power Supplies for the X101: P101 M (for mono) 35/- plus 4/6 p. & p. P101 S (for stereo) 42/6 plus 4/6 p. & p.

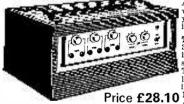
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For 6 volt or 12 volt positive earth systems. Comprising: special high voltage working hermetically sealed silicon transistor mounted in finned heat-sink, high output ignition coil, ballast resistor and hardwear (screws, washers etc.).

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50 WATT AMPLIFIER A.C. Mains 200-250V



An extremely reliable general purpose valve amplifier. Its rugged construction yet space age styling and design makes it by far the best value for money.

it by far the best value for money.

TECHNICAL SPECIFICATIONS
3 electronically mixed channels, with 2 inputs per channel, enables the use of 6 separate instruments at the same time. The volume controls for each channel are located directly above the corresponding input sockets. SENSITIVITIES AND

Price £28.10 INPUT IMPEDANCES. Channels 1 & 2
4mV at 470K. These 2 channels (4 inputs) are suitable for microphone or guitars.

Channels 3 & 4 300mV at 1m. Suitable for most high output instruments (gram, tuner, organ etc.). Input sensitivity relative to 10w output. TONE CONTROLS ARE COMMON

TO ALL INPUTS. Bass Boost 1 12dB at 60 Hz. Bass Gut—13dB at 60 Hz. Treble Boost + 11dB at 15 KHz. Treble Cut—12dB at 15 KHz. With bass and treble controls central—3dB points are 30 Hz and 20 KHz. POWER OUTPUT: For speech and music 50 watts rms. 100 watts peak. For sustained music 45 watts rms. 90 watts peak. For sine wave 38-5 watts rms. Nearly 80 watts peak. Total distortion at rated output 3:29, at 1 KHz. Total distortion at 720 watts 0:15% at 1 KHz. Output to match into 8 or 15 ohms speaker system. NEGATIVE FEEDBACK 20dB at 1 KHz. SIGNAL TO NOISE RATIO 60dB.

MAINS VOLTAGES adjustable from 200-250V. A.C. 50-60 Hz. A protective fuse is located at the rear of unit. Output impedance 3, 8 and 15 ohms.

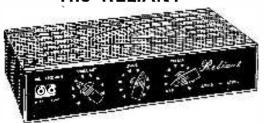
B.S.R. TD-2 TAPE DECK

Takes 5½in. spools, fitted with B.S.R. ½ Track Heads. Size 13½in. long by 8½in. wide. Price £8.19.6 plus 7/6 P. & P.



TERMS C.W.O. All enquiries S.A.E.

The RELIANT



SOLID STATE **GENERAL PURPOSE AMPLIFIER**

SPECIFICATIONS Output—10 watts Inputs—1. -xtal mic 10mV

SPECIFICATIONS
Output—10 watts
Inputs—1. xtal mic 10mV
2. -gram/radio 250mV
Frequency Response—(with tone controls central) Minus 3dB points at 20Hz and 40KHz.
Signal to Noise Ratio—better than —60dB. Transistors—4 silicon Planar type and 3
Germanium type. Mains input—220/250V. A.C. Size of chassis—10½"×4½"×2½". For use with 8td. or L.P. records, musical instruments, all makes of pick-ups and mikes. Separate bass and treble lift control. Two inputs with control from gram. and mike. Built and tested. 8"×6" speaker to suit price 14/6 plus 1/6 p. & p. Crystal mike to suit 12/6 plus 1/6 p. & p.

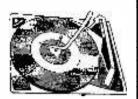
RELIANT Mk. I

As above less teak £5.15 plus 7/6 P. & P. RELIANT Mk. II In teak finished cas £6.16 plus 7/6 P. & P.

RECORD PLAYER SNIP A.C. Mains 240V

The "Princess", 4-speed automatic record changer and player engineered with the utmost precision for beauty, long life, and trouble free service. Will take up to ten records which may be mixed 7' to 10" or 12". Patent stylus brush cleans stylus after each playing and at stylus brush cleans stylus after each playing and at shut off, the pick-up locks itself into its recess, a most useful feature with portable equipment—other features include pick-up height adjustment and stylus pressure adjustment. This truly is a fine instrument which you can purchase this month at only \$5.19.6 complete with cartridge and ready to play. Post and ins. 7/6 extra.

ONLY £5.19.6 plus 7/6 P. & P.



POCKET MULTI-METER

Size $3\frac{7}{8} \times 2\frac{1}{8} \times 1\frac{3}{8}$ in. Meter size $2\frac{1}{8} \times 1\frac{3}{8}$ in. Sensitivity 1,000 O.P.V. on both A.C. and D.C. volts. 0-15, 0-150, 0 1,000 D.C. current 0-150mA. Resistance 0 100k Ω . Complete with test prods, battery and full instructions. 42/6 plus 3/6 P. & P.

FREE GIFT for limited period only. 30 watt Electric Soldering Iron value 15/- to every purchaser of the Pocket Multi-Meter.

STEREO PRE-AMPLIFIER

Inputs—6 position rotary switch (3 position mono, 3 position stereo). Tuner 150mW into 680k. Magnetic pick-up fully equalised and suitable for magnetic cartridges with minimising output of 4mV/cm/sec. Load 47k. Ceramic pickup 150mV into 680k. Sensitivities taken for 200mV output. Controls—separate volume controls for each channel. Twin ganged bass, 12dB lift and 15dB cut at 60c/s. Twin ganged treble, 10dB lift and 15dB cut at 10kc/s. Voltage required 23–30V DC at 5mA. Size 12 $\frac{1}{2}$ x $\frac{3}{2}$ in. In teak finished case, complete with front panel and knobs. Built and tested.

£7.7.0 plus 5/- P. & P.

CYLDON 2 TRANSISTOR U.H.F. TUNER

Price £2.10.0 plus 1/- P. & P.

THREE-IN-ONE HI-FI 10 WATT SPEAKER

A complete Loud Speaker system on one frame, combining three matched ceramic magnet speakers with a low loss crossover network. Peak handling power 10 watts. Impedance 15 ohms. Flux density 11,000 gauss. Resonance 40 60 c/s. Frequency range 50c/s to 20Kc/s. Size 13½ × 8½ 16 × 4½ in. By famous manufacturer.

List price £7

OUR PRICE 74/6 plus 5/- P. & P.

Similar speaker to the above without tweeters in 3 and 15 ohms 44/6 plus 5/- p. & p.

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Push Button Tuning Heart

This PRESTOLOCK 5 station Push-Button Tuner Heart with Manual Over-ride is an ideal basis for a quality AM car radio. Size $6\frac{1}{2}$ " \times 4" \times 2".

25/- plus 3/- P. & P.



QUALITY MAINS TRANSFORMER

Input 250 volts. OUTPUT (All RMS values) 4 windings of 11.5 volts connected in series total 46 volts at 4.5 amps (conservatively rated). The following combinations may be used. 1.23-0-23 volts. 2.46 volts. Both of these above voltages are commonly used in medium to high powered transistor amplifiers, power supplies, etc.

Price 35/- plus 7/6 P. & P.



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REVERBERATION AMPLIFIER. Self-contained transistorised battery operated. An entirely different approach to sound reproduction. Normally sound reproduction from a single source has a flat, one-dimensional effect. With this unit proper sound delay through reverberation, tones are created with a truly third dimension for concert hall originality. Two controls adjust volume and reverberation. Simply plug microphone, guitar, etc. in and the output into your amplifier. Supplied in a beautiful walnut cabinet. 7½×3×4½in. £10.4.0. P.P. & Ins. 6/-



POWER CONTROL-LER. Power at your finger tips. Not merely half wave control but full wave. A single variable control gives zero to full power. Uses latest 15amp 3kW triac and special triggering device Ideal

38W triac and special triggering device. Ideal to all types of lighting. fires, motors, drils, etc. Complete with easy to follow instructions 26.9.6. Ready built 29.4.6 plus 5/8 P.P. & Ins.

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YOX SWITCH. This sound operated switch is ideal from boile TX work, tape recorder switching, etc. Yon speak, it switches. High and medium imp. inputs. AF take off point. Drives your 12 volt relay. In kit form with full instructions, 42/6. Ready built, tested and guaranteed, 62/6 plus 2/6 P.P.

2/6 P.P.
METRONOME UNIT. Variable beat. Listen while you play and keep in time. Easily built, pocket size with personal mini earphone. In kit form 27/6 post paid. Ready built in an attractive black and white polythene case 37/6 post paid.
MORSE OSCILLATOR. PC board, transistors, high stab. components, battery earrier, ear piece. Adjustable tone. Just attach your key. Drives phones or speakers. In kit form 17/6 post paid. Ready built in similar case as above. 25/- post paid. JUST ARRIVED IN STOCK. Texas transistors. Complementary symmetry. Driver, NFN, PNP output. The set of three ONLY 6/6 post paid.

Free lists with every order. For lists only send 1/6 (deductable from first order).



Solve your communication problems with this 4-Station Transistor Intercom system (1 master and 8 Suts), in de-luxe plastic cabinets for desk or wall mounting. Call/telk/listen from Master to Subs and Subs to Master, Ideally suitable for Bueiness, Surgery, Schools, Hospital, Office and Home. Operates on one 9V battery. On/off switch. Volume control. Complete with 3 connecting wires each 68ft. and other accessories. P. & P. 7/8.

MAINS INTERCOM

No batteries—no wires. Just plug in the mains for instant two-way, loud and clear communication. On/off switch and volume control. Price 12 gns. P. & P. 8/5 extra.



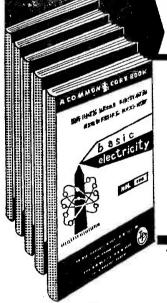


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59/6 Why not boost

with this incredible De-luxe Telephone Amplifier. Take down long telephone messages or converse without holding the handset. A useful office aid. On off switch. Volume Control. Battery 2/6 extra. P. & P. 3/6. Full price refunded if not satisfied in 7 days. WEST LONDON DIRECT SUPPLIES (P/W1) 169 KENSINGTON HIGH STREET, LONDON, W.8.



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RESISTO	RD:						
Code	Power	Tolerance	Range	Values available	1 to 9	10 to 99	100 up
\mathbf{C}	1/20W	5%	$100\Omega - 220 \text{K} \Omega$	E12	16	14	13
C	1/8W	5%	$4.7 \Omega - 1M \Omega$	E24	2.5	2	1.75
C	1/4W	10%	4.7 Ω -10M Ω	E12	2.5	1.75	1.5
C	1/2W	5%	4.7Ω-10M Ω	E24	3	2.25	2
MO	1/2W	2%	$10 \Omega - 1M \Omega$	E24	9	8	7
C	1W	10%	$4.2\Omega - 10M\Omega$	E12	4	3.25	3
ww	1W		0.22Ω -3.3Ω	E12	15d all qu	antities	
ww	3W	5%	$12 \Omega - 10 K \Omega$	E12	15d all qu	antities	
ww	7 W	5%	$12 \Omega - 10 K \Omega$	E12	15d all qu	antities	
Codes:	C = carl	oon film, high sta	bility, low noise.		_		
	MO = met	al oxide, Electros	il TR5, ultra low	noise.			
	WW = wire	wound, Plessey.					
Values:			1.8, 2.2, 2.7, 3.3,	3.9, 4.7, 5.6,	6.8. 8.2 and	their decades.	

Prices are in pence each for each ohmic value and power rating. (Ignore fractions of one penny on total resistor order)

COLVERS 8 WATT WIRE-WOUND POTENTIOMETERS:

 $10\,\Omega,\,15\,\Omega,\,25\,\Omega,\,50\,\Omega,\,100\,\Omega,\,150\,\Omega,\,250\,\Omega,\,500\,\Omega,\,1K\,\Omega,\,1.5K\,\Omega,\,2.5K\,\Omega,\,5K\,\Omega,\,10K\,\Omega,\,15K\,\Omega,\,25K\,\Omega,\,50K\,\Omega.$

CARBON TRACK POTENTIOMETERS: Double wiper ensures minimum noise level. Long plastic spindles.

 Single gang linear: 220 Ω, 470 Ω, 1 K etc. to 2.2M Ω
 2/6

 Single gang log: 4 K 7, 10 K, 22 K, etc. to 2.2M Ω
 2/6

 Dual gang linear: 4 K 7, 10 K, 22 K etc. to 1M Ω
 8/6

 Dual gang log: 4 K 7, 10 K, 22 K etc. to 2M 2Ω
 8/6

FETS n-channel low cost general purpose 2N5163, 25 volt, only 5/- each. Audio/ 5L403A. Only 5/- each. Operates with 18V power supply. Sensitivity 7.1. Texas 2N3819 9/-, Motorola 2N5459 20mv into 20M Ω , 3 watts into 7.5 Ω . PE Nov. 69 Stéreo Amplifier kit less metal work. £11/18/- NET complete.

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Transistors for one channel \$7/9/6 list, with 10% discount only \$6/14/6
Transistors for two channels \$14/19/- list, with 15% discount only \$12/14/Capacitors and/resistors for one channel list \$2.
Printed circuit board free with each transistor set.
Complete unregulated power supply kit \$2/14/6 mono or stereo, subject to discount.
Complete regulated power supply kit \$9/5/- subject to discount. Further details on application.

SINGLATE IC.10 Integrated Circuit Amplifier and Pre-amplifier This remarkable monolithic integrated circuit amplifier and pre-amp now available from stock. The equivalent of 13 transistor/18 resistor circuit plus 3 diodes and the first of its kind ever. It is d.c. coupled and applicable to an unusually wide range of uses as detailed in the manual provided with it. As advertised, post free \$208.NET. post free 59/6 NET.

CARBON SKELETON PRE-SETS. Small, high quality, type PR: Linear only, $100\,\Omega$, $220\,\Omega$, $470\,\Omega$, $1K\,\Omega$, 2K2, 4K7, 10K, 22K, 47K, 100K, 220K, 470K, $1M\Omega$, 2M2, 5M, $10M\,\Omega$ vertical or horizontal mounting, 1/- each.

S-DeCs put an end to "birdsnesting". Components just plug in. Saves valuable time. Use components again and again. S-DeC only 30/6 post free. Compact T-DeC, increased capacity, may be temperature-cycled T-DeC only 51/post free.

CAPACITORS: All new stock

CAFACTORS. At new sock
High ripple current types:
2000μF 25V 7/4; 2000μF 50V 11/4; 5000μF
25V 12/6; 5000μF 50V 21/11; 1000μF 100V
16/3; 2000μF 100V 28/9; 5000μF 70V 36/-;
5000μF 100V 58/3; 1000μF 50V 8/2;
2500μF 64V 15/5; 2500μF 70V 19/6.

Medium elecs.

Medium elecs.

Axial leads: Values (µF/V): 50/50 1/9; 100/25 1/9; 100/50 2/6; 250/50 3/9; 500/25 3/9; 1000/10 3/-; 500/50 4/6; 1000/25 4/6; 1000/25 6/-.

Small elecs.

Axial leads: 5/10, 10/10, 25/10, 50/10 1/- each, 25/25, 47/25, 100/10, 220/10 1/3 each.

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Brillant new styling and
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Stereo 15 watts per channel
In kit form with complete
amplifier and pre-amplifier
modules and power supply.
Output per channel into 15 Ω 12 watts R.M.S. Price £38/4/- net

25 WATTS PER CHANNEL As above but Output per channel into $15\,\Omega$ 25 watts R.M.S. Price 253/15/- Net Brief specification: Total harmonic distortion 0·1%. Inputs: Magnetic, Ceramic, Tape, Radio Signal to noise ratios: Better than 60dB all inputs. O/load factor 28dB all channels.

ENGLEFIELD CABINET to house either above assemblies (as illustrated) \$6 Net OTHER PEAK SOUND PRODUCTS AS ADVERTISED.

MULLARD Sub-min electrolytic C426 range-Price 1/3 each. Axial leads, Values (μ F/V): 0-84/64: 1/40; 1.6/25; 2.5/16: 2.5/64; 4/10: 4/40; 5/64: 6.4/6.4; 6.4/55; 8/4; 3/40: 10/2.5; 10/16: 10/64; 12.5/25; 16/40; 20/16: 20/64; 25/6.4; 25/25; 32/4: 32/40; 32/64: 40/2.5; 32/4: 32/40; 32/64: 40/2.6; 6.4/25; 80/40; 20/16: 20/64; 50/25; 50/40; 64/4; 64/10: 80/2.5; 80/16; 80/25; 100/6.4; 125/4; 125/16; 150/2.5; 200/6.4; 200/10: 250/4; 320/2.5; 320/6.4; 400/4; 500/2.5.

Wavechange switches: 1P 12W; 2P 6W; 3P 4W; 4P 3W long spindles, 4/9 each.

Slider switches, double pole double throw, 3/- each.

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All power types supplied with free insulating sets

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	ZN 4410	4/9	V 4U5A	7/9

MAIN LINE AMPLIFIER KITS as advertised. Prices Net. Authorised dealer.

COMPONENT DISCOUNTS:

10% on orders for components for £5 or more. 15% on orders for components for £15 or more. (No discount on net items).

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Overseas orders welcome: carriage charged at cost.

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R.S.C. SENSATIONAL HIGH FIDELITY STEREO 'PACKAGE' OFFERS

30 WATT OUTPUT

* Goldring Transcription Turntable on Plinth

* Shure or Goldring Magnetic Pick-up Cartridge

* Super 30 Amplifier in veneered housing

* Pair of Stanway II Loudspeaker Units
Special total price, Four fully wired
units ready to "plug-in", Carr. 30/-.

**TERMS AVAILABLE ALL PACKAGE OFFERS

AUDIOTRINE HIGH FIDELITY LOUDSPEAKERS



Construction. Latest high efficiency ceramic magnets. Treated Cone surround for low fundamental resonance. "D" indicates Tweeter Cone providing extended frequency range up to 15,000 c.p.s. Impedance 3 or 15 ohms. Please state choice. Exceptional performance at low cost. HF100L 5' 10W 57/9 HF120 12' 15W 79/9 HF801D 8' 8W 59/9 HF120D 12' 15W 89/9 HF11D 8' 10W 4 gns. HF126 12' 15W£5.5.0

HIGH FIDELITY LOUDSPEAKER UNITS Cabinets latest style Satin Teak or Afrormosia ve-neer. Acoustically lined or filled woollen damping. Ported where appropriate, credit terms available



DORCHESTER Size 16 x 11 x 9in. Appr. Range 45-15,000 c.p.s. Rating 8-10 watts. Fitted High flux 13 x 8in. Dual **E8.19.9** Cone spkr. Imp. 3 or 15 ohms

STANWAY II Size 20x101x91in. Rating 10 watts. Incorporating Fane 13x8in. speaker with rubber cone surround and 11,000 line magnet. High flux tweeter. Handsome Scandinavian design cabilities smooth realistic sound output.

GLOUCESTER Size 25 x 16 x 10 in. 12 in. High flux 12.000 line speaker. Cross-over unit and Tweeter. Rating 10 watts. Frequency range 12 Gns. 40-20,000 c.p.s. Impedance 15 ohms.

F2 CABINET Size 17" wide

14" deep, 114" high. Cut for TA12, Super 15, Super 30 and other am-plifiers. 'Roll over' transp. plas-tic cover, Satin Teak or Afror-mosia veneer finish **8 Gns.** Inc carr.



MOTOR BOARDS cut for Garrard 12/9

R.S.C. TA6 6 Watt HIGH FIDELITY SOLID STATE AMPLIFIER



STATE AMPLIFIER
200-250v. AC mains operated
Frequency Response 3020,000 c.p.s. —2dB. Harmonic
Distortion 0·3% at 1,000 c.p.s.
Separate Bass and Treble
("ifft' and 'cut' controls. 3 Input sockets for Mike,
Gram, Radio or Tape. Inputselectors witch. Outputfor
3-15 ohm spkrs. Max. sensitivity 5mV. Output rating
I.H.F.M. Fully enclosed enamelled case, 9½ x 22 x 5fin.
Attractive brushed silver finish facia plate 10½ x 3fin.
and matching knobs. Complete kit of parts with full
wiring diagrams and instructions. 7 Gns.
Or factory built with 12 months' guarantee. £8.19.9

Matching as recommended for optimum per-formance. Send for coloured brochure showing other money saving offers.



Package prices apply pro-viding all individual units are purchased from any branch within 3 months. See leaflet.





EXTREMELY ATTRACTIVE PLINTHS finished in Teak or Afrormosia veneer. Transparent plastic "roll over" cover.

RECORD PLAYING UNITS

Money saving units. Mounted on Plinth. Supplied with transparent plastic cover. Ready to plug into Amplifier or Tape recorder.

RP2C Garrard SP25 Mk II
RP2C (with heavy turntable) fitted Goldring CS90
high compliance ceramic
Stereo/Mono cartridge with
diamond stylus.
Inc. Carr.

RP2C Coloring I To Color
RP2C Coloring I To Color

RP3C Goldring Lenco GL68 Transcription unit and CS90 cartridge. 28 Gns. Inc. Carr.

Other types available with Magnetic cartridges and with alternative design plinths.



cut for Garrard 1025, 2025, 3000, AT60, SP25etc

Available 59/9 with trans. plastic cover, Inc. Carr 6 Gns

INTEREST CHARGES

On Credit Sales settled REFUNDED in 3 months.

30 WATT OUTPUT

- * Garrard SP25 Mk II Turntable on Plinth

 * Goldring CS90 Ceramic P.U. Cartridge with
 diamond stylus

 * Super 30 amplifier in veneered housing

 * Pair Stanway II Speaker Units
 Four fully wired units ready to 76 Gns. Carr
 "plug-in" Special total price 76 Gns. 30/-

13 WATT OUTPUT

* Garrard SP25 Mk II 4 sp. player unit on plinth
* Goldring CS90 Ceramic P.U. Cartridge
* TA12 Amplifier in veneered housing
* Pair of Dorchester Loudspeaker
Units. Special total price.

Carr. 25/-

Onits. Special total price. Carr. 25/-Or Dep. £10 and 9 mthly payments £5.11.0 (Total £59.19.0). Transparent plastic cover 3 gns. extra

R-S-C-TA12 13 WATT STEREO AMPLIFIER





AUDIOTRINE HI-FI SPEAKER SYSTEMS

Consisting of matched 12in. 11,000 line 15 watt 15 ohm high quality speaker, cross-over unit and tweeter. Smooth response and extended frequency range ensure surprisingly realistic reproduction. 65.15.0 Cs. 15,000 line Speaker £6.15.0 Carr. 6/6 Carr. 5/9

LINEAR L10 HIGH FIDELITY 10W AMPLIFIER

10 GNS.

with separate Pre-amp. Magnet P.U. matching. To clear HI-FI SPEAKER ENCLOSURES Teak or Afrormosia veneer

finish. Modern design. Acoustically lined.

Prices Inc. carr.

Prices Inc. carr.

JES Size 16 x 11 x 9in. Pressurised. Gives f4.10.0

pleasing results with any 8in. Hi-Fi'speaker.

SES For optimum performance with any 8in. f5.10.0

Hi-Fi'speaker. Size 22 x 15 x 9in. Ported.

SE10 For outstanding results SE12 For excint primnce with 12in Hi-with 10in Hi-Fi'spkr f5.15.0 Fi speaker and Tweeter. f6.15.0

Size 24x15x10in. P'td. f5.15.0 Size 25 x 16 x 10in.

R.S.C. TFM1 SOLID STATE VHF/FM RADIO TUNER



Total cost of parts with detailed wiring diagrams & instructions.

Inc. 14 Gns. 14 Gns.

Carr. Or factory built 16; gns. Or in Teak finished cabinet as illustrated 19; gns. Terms: Deposit \$5 and 9 monthly payments £2. Total £23.



*High-sensitivity * 200-250v. A.C. Mains operation. * Sharp A.M. Rejection. * Drift-free reception. * Sharp A.M. Rejection. * Drift-free reception. * Sharp A.M. Rejection. * Drift-free reception. * Output ample for any amplifier (approx. 500 m.v.). * Simple alignment instructions. * Output available for feeding tuning meter. * Output for feeding stereo Multiplexer. * Tuner head using silicon Planar Transistors. * Designed for standard 80 ohm co-axial input. Visually matching our Super 15 and 30 amplifiers and of the same high standard of performance and reliability. The pre-wired tuning head facilitates speed and simplicity of construction. Printed circuitry. Only high grade transistors and components used. A quality product at considerably less than the cost of comparable units. Stereo version. all parts 20 gns. Inc. carr. Assembled 22; gns. inc. carr.

R.S.C. SUPER 30 MKII HIGH FIDELITY STEREO AMPLIFIER

High Grade Components. Specifications comparable with units costing considerably more.

TRANSISTORS 9 high quality types in each channel.

OUTPUT 10 Watts R.M.S. continuous into 15 Ω (per channel). 15 Watts R.M.S. continuous into 3Ω .

INPUT SENSITIVITIES Mag. P.U. 4 m.V. Ceramic P.U. 35 mV. Tape Amp. 400 mV. Aux. 100 mV. Mic. 5 mV. Tape Head 2-5 mV.

FREQUENCY RESPONSE ±2 dB. 10-TREBLE CONTROL +17 dB to -14 dB

BASS CONTROL +17 dB to -15 dB at 50 c/s.

HUM LEVEL —80 dB.

. Employing Twin Printed Circuits.

200/250v. A.C. mains operation. **HARMONIC DISTORTION** 0.1% at

HARMONIC DISTORTION 0.1% at 10 watts 1.000 c.p.s. CROSS TALK 52 dB at 1,000 c.p.s. CONTROLS 5 Position Input Selector, Bass, Treble, Vol., Bal., Stereof Mono Switch, Tape Monitor Switch, Wains Switch

Mains Switch.

INPUT SOCKETS (1) P.U. (2) Tape

Amp. (3) Radio, (4) Mic. or Tape Head.

(Operation of Input Selector assures

appropriate equalisation).

CHASSIS Strong Steel construction Approx. 12 x 3 x 8in.
FACIA PLATE Attractive design in rigid Perspex. Spun silver matching control knobs as available.
COMPLETE KIT OF PARTS Carr. 15/- 22 Gns. Point to point wiring diagrams and detailed instructions.
Eminently suitable for use with any make of Pick-up or Mic. (Ceramic or Magnetic, Moving Coil, Ribbon or Crystal) currently available. Superb sound output quality can be obtained by use with first-rate ancillary equipment. Unit factory 28 Gns. or Deposit £7.5.0 and 9 monthly payments 56/3 (Total £32.11.3) or in Teak or Afrormosia veneer housing 31 Gns. Carr. 15/-. Terms: Deposit £7.3.6 and 9 monthly payments of 64/- (Total £35.19.6). Send S.A.E. for leafiet.

R.S.C. SUPER 15 HIGH FIDELITY SOLID STATE AMPLIFIER

Approx. as Super 30 but single channel. Complete kit with full constructional details and point to point wiring diagrams.

Carr. 12½ Gns.

or factory built 15½ Gns. Carr. 12/6. Terms: Deposit 4 Gns. and 9 monthly payments 31/1 (Total £18.3.9) or in Teak or Afrormosia ven-eered housing. 19 Gns.

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SHEFFIELD

THE 'YORK' HIGH FIDELITY 3 SPEAKER SYSTEM

★ Moderate size, only 25 x 14 x 10in. Complete Kit

Response 30-20,000 c.p.s. Impedance 15 ohms. 20 Gns.

**Response 30-20,000 c.p.s. Impedance 15 ohms.

**Performance comparable with units costing Carr. 12 considerably more. Consists of (1) 12in. 15 watt Bass unit with cast chassis. Roll rubber cone surround for ultra low resonance, and ceramic magnet. (2) 3-way quarter section series cross-over system. (3) 8 x 5 in. high flux middle range 'speaker. (4) High efficiency tweeter. (5) Woollen acoustic damping material. (6) Teak veneered cabinet. (7) Circuit and full instructions. Terms: Dep. 25.10.6 and 9 monthly payments 39/- (Total £23.1.0).

DEMONSTRATIONS AT ALL BRANCHES



R.S.C. A10 30 WATT ULTRA LINEAR HI-FI



AMPLIFIER Highly sensitive. Push-Pull high output, with Pre-amp. Tone Control Stages. Performance figures of factory built units: Hum level—70dB. Frequency response +3dB30-20.000c/s. Sectionally wound output transformer. All high grade components. Valves EF86, EF86, ECC83, 807, 807, 6734. Separate Bass and Treble Controls. Sensitivity 36 mV. Suitable for high impedance microphones, Crystal or Ceramic P.U's. Designed for Clubs, Schools, Theatres, Dance signed for Clubs, Schools, Theatres, Dance riputs such as Gram and "Mike" can be mixed 200-250v. 50c/s A.C. mains. For 3 and 15 ohm speakers. Complete kit of parts with point- 15 Gns Carr. to-point wiring diagrams and instructions. 12/6 Twin-handled perforated cover 27/6. Supplied factory built with EL34 output valves. 12 months' guarantee for 18 gns. TERMS: Deposit 26.3.0 and 9 monthly payments of 34/- (Total 221.9.0). Send S.A.E. for leaflet.



R.S.C. A11 HIGH FIDELITY 12-14 WATT AMPLIFIER

PUSH-PULL ULTRA LINEAR OUTPUT

"BUILT-IN" TONE CONTROL PRE-AMP.

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TOP SHROUDED DROP-THROUGH TYPE
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350-0-350v. 80mA, 6-3v. 2a. 6-3v. 1a. 28/9
350-0-350v. 80mA, 6-3v. 2a. 0-5-6-3v. 2a. 29/11
250-0-250v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a. 39/9
300-0-300v. 100mA, 6-3v. 4a., 0-5-6-3v. 3a. 39/9
300-0-300v. 130mA, 6-3v. 4a., 0-5-6-3v. 3a. 39/9
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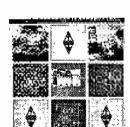
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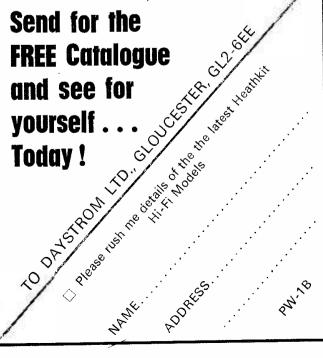
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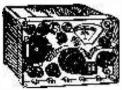
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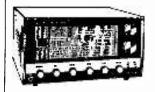
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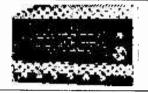
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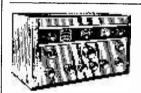
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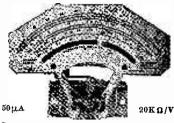
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TE-16A Transistorised Signal Generator. 5 ranges 400kHz-30mHz. An inex-pensive instrument for the pensive institute to the handyman. Operates on 9v battery. Wide easy to read scale. 800kHz modulation. $5\frac{1}{8} \times 5\frac{1}{8} \times 3\frac{1}{8}$ in. Complete with instructions and leads. \$7.19.6, P. & P. 4/-.

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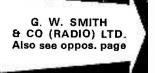
Generator ringing, metal cases. Operates from two 1.5V batteries (not supplied). Excellent condition. £4.10.0 per pair. Carr. 10/-.

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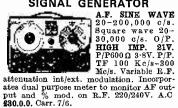
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150 W. \$2, 2.6. P. & P. 3/6.
300 W. \$2,19.6. P. & P. 4/6.
500 W. \$4,10.0. P. & P. 6/6.
1,000 W. \$6,10.0. P. & P. 7/6.
1,500 W. \$7,19.6. P. & P. 8/6.
7,500 W. \$15,10.0. P. & P. 20/-.



ARF-100 COMBINED AF-RD SIGNAL GENERATOR



230.0.0. Carr. 7/6.

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Accurate wide range signal generator covering 120 Kc/s-500 Mc/s on 6 bands. Directly cali-brated Variable R F atbrated variable if r attenuator, audio output. Xtal socket for calibration. 220/240V. A.C. Brand new with instructions. £15. Carr. 7/6. Size $140 \times 215 \times 170$ mm.

PEAK-SOUND PRODUCTS. Full range of Amplifiers, Kits, Speakers in stock

TY75 AUDIO SIGNAL GENERATOR

GENERATUR
Sine Wave 20c/s to 200
kc/s. Square Wave 20c/s
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220/240 volts A.C. Size
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2 pF-2000 mFd 2 ohms 200 meg-ohms. Also checks impedance, turns ratio, insulation, 200/250 V. A.C. Brand New



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It has the fullest capacity for checking on A, B and Ico.
Equally adaptable for checking diodes, etc.
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Resistance for diode
200 Ω-IMΩ. Supplied
complete with instruc-



complete with instruc-tions, battery and lead. £5.19.6. P. & P. 2/6

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Brand new and boxed in original sealed cartons VM. 76 VALVE VOLTMETER. R. F. measurements in excess of 100 Mc/s and D.C. measurements up to 100 V with accuracy of +2% D.C. range 300 MV to 1 KV. A.C. range 300 MV to 300 V RMS. Resistance *02-500 M.C. Price \$72.
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50 Kc/s. sine or square wave. Price \$30. J1B AUDIO SIGNAL GENERATOR. 15 c/s-50 Kc/s. Price £30. TT1S TRANSISTOR TESTER. £37.10.0. Carriage 10/- per item.

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HOSIDEN DHO4S 2-WAY STEREO **HEADSETS**

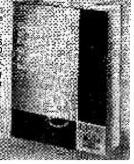


Each headphone contains a $2\frac{1}{2}$ in. woofer and a $\frac{3}{8}$ in. tweeter. Built in individual level controls. 8Ω imp. 25-18.000c/s with cable and stereo plug. £5.19.6. P. & P. 2/6.

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LAFAYETTE LA-224T TRANSISTOR STEREO AMPLIFIER

19 transistors, 8 diodes, IHF music power, 30W at 8Ω. Response 30-20,000 ± 2dB at 1W. Distortion 1% or less. Inputs 3mV and 250mV.

Output 3-16Ω. Separate L and R. volume controls. Treble and bass control. Stereo phone jack.

Brushed aluminium, gold anodised extruded iront panel with complementary metal case. Size 10½ × 3 9/16×7 13/16in. Operation 115/230V. A.C. 298. Carriage 7/6. £28. Carriage 7/6.

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+17dB. £12.10.0. P. & P. 3/6.



MODEL TE-90 50,000 OPV mirror scale overload Protec-tion 0/8/12/60/300/606/1200 v. DC. 0/6/30/120/300/ 1200v. DC. 03/6/60/600mA. DC. 16K/160K/1-6/16meg Q. -20 to +63dB. \$7.10.0. P. & P. 3/-





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MODEL TE-12
20,000 O.P.V. 0/0-6/6/30/120/6
00/1,200/3,000/6,000v. D.C.
0/6/80/120/600/1,200v. A.C.
0/60/LA/6/60/600mA. 0/6K/
600K/6Meg./60 Meg. 0 50pF.
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Stereo multiplex adaptors 99/6.

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NEW SINCLAIR 2000 SYSTEM

35 watt Integrated Amplifier, £29. Carr. 5/-. Self-powered FM Tuner, £25. Carr. 5/-.

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fortable. Lightweight adjustable
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ohm imp. 67/6 Wonderfully com-fortable. Lightohm imp. P. & P. 2/6.

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ATTENUATOR

Variable range 0111dB.Connections,
Unbalanced T and
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10) + (1dB × 10) + 10 + 20 + 30 + 40dB.
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First grade quality American tapes.	Bra	nd
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5in. 900ft. L.P. acetate	. 10)/~
5in. 1,200ft. D.P. mylar	1	5)
5\(\frac{1}{2}\)in. 1,200ft. L.P. acetate	17	ย์เล
5‡in. 1,200ft. L.P. mylar	· 16	R/
52in. 1,800ft. D.P. mylar	. 2	o'le
5%in. 2,400ft. T.P. mylar	∵~;	οία
7in. 1,200ft. std. acetate		9/6
7in. 1,800ft. L.P. acetate		?;-
7in. 1,800ft. L.P. mylar		
7in . 2,400ft . D.P. mylar		
7in. 3,600ft. T.P. mylar	48	> -
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Made by famous British manufacturer to very high standards, heavy duty cast chassis, twin cone construction, smooth extended range, with very low level of distortion.—Response 35–17,500Hz.—impedance 15 ohms—flux, 11,000 gauss.

WALDON 97/6 each plus 6/6 P. & P.

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TRIO Stereo Moving Magnet Cartridge Model AD76K. Diamond Stereo LP Stylus. Frequency response 20-20,000c/s output. 7mV tracking pressure 2 grammes ± 0.5 grm. Fully guaranteed. Price 85/- p/p free.

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*Denotes including Sonotone 9TA-Stereo/ Diamond Cartridge. Elegantly styled plinth and cover to suit the above units. From 5 gns. Please add 10/- p/p each on all above items.

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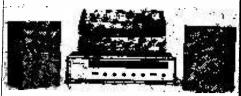
Designed to accept the full range of E.M.I. loudspeakers. Beautifully styled in teak.

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Guitar group 25. 12in. round, heavy duty cone, with solid aluminium chassis, 15 ohms imp. 12,000 gauss. Response 30-10,000c/s. OUR SPECIAL PRICE

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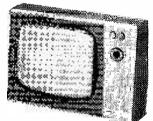
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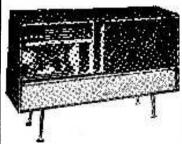
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Speakers 10/-: $3\frac{\pi}{2}$ —25Ω. 4″—10Ω. 7″ × 4″—3Ω. Brand new. P. & P. 2/6 Asstd. Condensers: 10/- for 50. P. & P. 7/6. Asstd. Resistors: 10/for 50. P. & P. 4/6. Asstd. Controls: 10/- for 25. P. & P. 7/6. Transistors: Mullard matched output kit 9 OC81D-2 OC81's, P. & P. FREE. output kit 9/-

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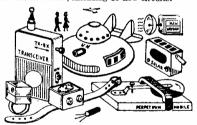
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This is an instant thermostat, simply plug
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Will save its cost in a
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Glass encased, switches operated by external magnet—gold welted contacts. We can now offer

Miniature. lin. long × approximately ½ in. diameter Will make and break up to ½ amp up to 300 volts. Price 2/6 each. 24/- dozen.

Standard 2 in. long × 3/16 in. diameter. This will break currents of up to 1 amp, voltages up to 250 volts. Price 2/e each. 18/- per dozen.

Flat. Flat type, 2 in. long, just over 1/16 in. thick, approximately ½ in. wide. The Standard Type flattened out, so that it can be fitted into a smaller space or a larger quantity may be packed into a square solenoid. Rating 1 amp. 200 volts. Price 6/each, £3 per dozen.

Small ceranic magnets to operate these reed

Small ceramic magnets to operate these reed switches 1/3 each. 12/- dozen.



15 Amp FOOT SWITCH

3 DIGIT COUNTER

For Tape Recorder or other application, re-settable by depressing button. Price 8/6.



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Made by Acos, reference No. 1.D.1001. For measuring vibration, etc., to be used in conjunction with "G" Meter. Regular price £5. Our price 49/6. Brand new and unused.

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Screened 3 Core Flex. Each core 14/0076 Copper PVC insulated and coloured, the 3 cores laid together and metal braided overall. Price \$3.15.

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23/0076 Triple Core P.V.C. covered, circular, normally sold at 1/6 yd. Our price 100 yd. coil \$3.19.6 Post and Insurance 6/6.

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For energising Reed Switches, etc., size approx. 1\(\frac{7}{4} \)in. long by lin. diameter. Hole through Solenoid approx. \(\frac{2}{4} \)in. 8/6 each.

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7 transistor, 2 wave band (medium and long) pocket radio with carrying handle and earplug. These radios use a ferrite slab aerial and a conventional superhet circuit with bullt in moving coil speaker. Completely built up, ready to play. Offe. set than importers price due to bankrupt parchase. A remarkable bargain. 39/6 plus 3/6 post and insurance.



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Beautifully made by famous German Company. PAPST System, 230-240 A.C. Mains operated, size 3½in. × 3½in. × 2½in. × 2½i

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If you hire out equipment such as TV sets by the hour then these slot meters are what you require. We have 3 types, 8d, an hour, 1/- an hour and 1/6 an hour. Brand new Made by the famous Weston Company. Price \$3.19.6, postage and insurance 6/6



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Just what you need for work bench or lab. 4×13 amp sockets in metal box to take standard 13 amp fused plugs. Supplied complete with 6 feet of heavy cable and 13 amp plug. Similar advertised at £5. Our price 39/6, +4/6 P & I.



THIS MONTH'S SNIP 24 HOUR TIME SWITCH

Mains operated. Adjustable Contacts give 2 on/offs per 24 hours. Contacts rated 15 amps, repeating mechanism so ideal for shop window control, or to switch hall lights tanti-burglar precaution) while you are on holiday. Made by the famous Smiths Company. This month only 39/6 with Perspex cover, plus 3/6 postage and insurance, a real snip which should not be missed.



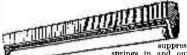
DOUBLE ENDED MAINS MOTOR

On feet with holes for screw-down fixing. To drive models, oven, blower heater, etc. 10/- each, plus 3,6 post and

INSTRUMENT MOTOR WITH GEAR BOX



ATLAS SLIMLINE FLUORESCENTS



A Fluorescent lighting unit made by the famous Atlas company, with super silent polyester filled choke and radio springs in and out and the whole unit beautifully made and finished white enamel. Amazingly call it left on all the time costs only one penny per design.

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5 transistors—highly efficient, made for use with tapehead G4 but equally suitable for microphone or pick up—limited quantity 29/8. Full circuit diag. also shows tape controls 5/-



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15, 30 & 100 WATT HI FI SPEAKERS

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FULL FI 12 INCH LOUDSPEAKER. This is undoubtedly one of the finest loudspeakers that we have ever offered, produced by one of the country's most famous makers. It has a die-cast metal frame and is strongly recommended for Hi-Fi load and Rhythm Guitar and public address.
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Small but very powerful mains motor with 5\(^2_1\)in. blades. Ideal for 5§in. blades. Ideal for cooling equipment or as extractor. Silent but very efficient. 17/6, post 4/6. Mounts from back or front with 4BA



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3/- for first one then
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Easiest way to fault find—traces signal from aerial to speaker—when signal stops you've found the fault. Use it on Radio, TV, amplifier, anything—complete kit comprises two special transistors and all parts including probe tube and crystal earpiece. 29/6—twin stethoset instead of earpiece 11/extra—post and ins. 2/9.



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Designed to operated transistor sets and amplifiers.
Adjustable output 6v., 9v., 12 volts for up to
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0-30pf an old design but on-which has never been betteren. 1/- each. 10/- doz. \$4.0.0 per 100.



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Very powerful 7 r.p.m., operates from standard A.C. mains. 29/6, plus 3/6 P. & P.





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 $\frac{1}{2}$ in. stroke. Size $2\frac{3}{2}$ in. \times 2in. \times $1\frac{3}{2}$ in. 14/6, postage 2/9.

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Run your small transistor radio from the mains—full wave circuit—made the mains—full wave circuit—made up ready to wire into your set and adjustable high or low current.



SPRING COIL LEADS as fitted to telephones, 4 core 2/8 each, 3 core 2/-

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In neat plastic cases, available in several voltages as follows: 4v., 6v., 12v., 24v., 36v., 48v., 60v., 110v., 220v., 380v. Note all below 110v. are fitted with lamps. 110v. and above are neons. Price 3/- each. 30/- dozen.

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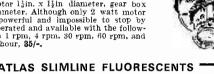
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THE TWENTYLITE & THE FORTYTWIN Fluorescent lighting



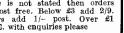
economical. If left on all the time costs only one penny per day (uses \(\frac{1}{2} \) unit). Measures 2ft. long. Is ideal in Kitchen, Bedroom, Hallway, Porch, Loft, etc. Don't miss this amazing offer, 39/6 with tube .Assembled ready to install. 4ft. twin model 59/6. Postage and insurance 6/6 extra.



Will dim incandescent lighting up to 600 watts from full brilliance to out. Fitted on M.K. flush plate, same size and fixing as standard wall switch so may be fitted in place of this, or mount on surface. Price complete in heavy plastic box with control knob £3.19.6.

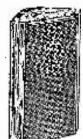


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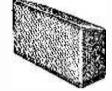


COWDREY FIVE. Specially designed Corner Cabinet; Fitted rubber feet. 203 x 13 x 73in. deep. Finished in natural teak veneers with Vynair front. Fitted 8 x 3in., 7 x 4in. and three 5in. round speakers wired in series to match. 15 ohm impedance (handles 15 watts). £6.6.0, P. & P. 8/6 each.



ADASTRA DOUBLE 5 stereo solid state amplifier housed in handsome cabinet veneered in natural teak. Size 11½ x 6 x 5½ in. 10 Transistors -power output 5 watts peak per channel, 220-240v A.C. Quinut impedance 12 to 15 ohms (our Cowdrey speaker system eminently suitable). Smart blue escutcheon, £14.14.0, P. & P. 10/6.

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ELF. An extension speaker of quality. 9 x 5½ x 3½ in. veneerec in natural teak, with smart gold

and brown Vynair front trimmed

with white. Fitted re-conned

5in. 3 ohm speaker. The baffle is

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CAXTON COLUMN. This is a col-

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watts and will improve the quality of any tape recorder or record player.

Finished in wood grain cloth with

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SPEAKERS: Elac Heavy duty Ceramic Magnets 11,000 line, 10in. round, 10 x 6in. 3 ohm or 15 ohm. 48/6, P. & P. 3/6. 8in. round 15 or 3 ohm, 42/6, P. & P. 3/6. 8in. 3 ohm, 45/-, 15 ohm 48/6, P. & P. 1/6. E.M.i. 3in. tweeter 17/6, P. & P. 1/5. E.M.i. 13½ x 8in. fitted two 21/2 in. tweeters. 15 ohm 77/6, P. & P. 4/6. E.M.I. 131/2 x 8in.

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A superb stereo amplifier offering every facility for the hi-fi enthusiast. Output 10 watts per channel.

10 watts per channel. Frequency response 40-20,000 Hz + 3dB. Inputs for radio, P.U. Ceramic, P.U. Magnetic Tape, Separate bass and treble controls, Volume and Balance controls Mono/Stereo Switch. Also features headphone socket and tape output. Teak case with attractive illuminated front panel. Size 14½ × 9½ × 3½ in. A.C. 200/250V.

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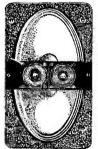
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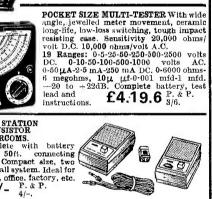


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 Wgt
 1 lb
 7oz
 Price
 28/9
 P&P 4/6

 Wgt
 3 lb
 6oz
 Price
 38/ P&P 6/

 Wgt
 5 lb
 12oz
 Price
 53/10
 P&P 6/

 Wgt
 7 lb
 8oz
 Price
 72/7
 P&P 9/

 Wgt
 11 lb
 13oz
 Price
 95/ P&P 11/

 Wgt
 2lb
 Price
 23/ P&P 6/

 Wgt
 4 lb
 6oz
 Price
 46/2
 P&P 6/

 Wgt
 6 lb
 8oz
 Price
 60/9
 P&P 6/

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 9 lb
 8oz
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WIRELESS

VOL 45 NO 9

Issue 755

JANUARY 1970

TOPIC OF THE MONTH

THE optimists will soon be ringing out 1969 and hopefully heralding what they imagine will be a brighter new year. The pessimists will just groan and say things can't be worse. It's all a matter of viewpoint and temperament, but whatever these are one must first assess the retiring year before speculating on the one to come. We have done this with P.W.

Circulation figures and readers' letters remained at a high level, so we assume that most readers got what they wanted. During 1969 we published 194 articles and features, an average of 16-plus per issue. Of these there were 7 on building amplifiers, 11 on receivers and front ends and 10 on test equipment. This apart from the projects under the Take 20 and IC of the Month banners, and constructional items in other categories.

On the semi-constructional and theoretical front there were series on repairing radio sets, pulse circuits, aerials, magnetic sound recording, semiconductor theory and 12 instalments of P.W. Guide to Components. Other articles ranged a varied field and took in home workshop practice, relays, power supply units, a stereo decoder, printed circuit design, a pedal steel guitar, etc.—and, of course, the regular news and comment features.

If we left anyone out during the year he must surely be a weird misfit! Having modestly patted our own editorial backs it is only just to convey our appreciation for the support from readers in the way of comments, criticisms, suggestions and letters of encouragement. And, of course, for sending along manuscripts for consideration; a high proportion of published material is the work of ordinary readers of P.W. So, to every one of you, from the regular subscribers to those who cadge a copy from a mate at the local club. . . .

Merry Christmas and a Happy New Year

from

W. N. STEVENS

L. E. Howes, G3AYA C. Riches H. Moorshead T. R. Preece, G3TRP

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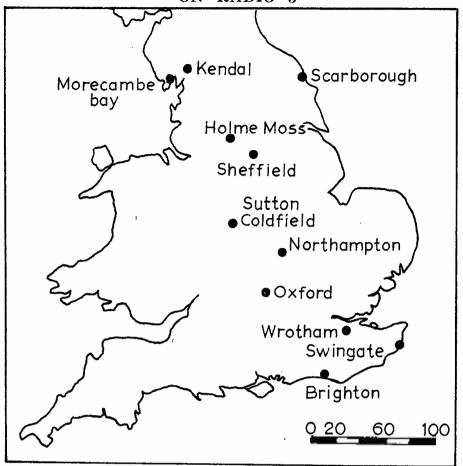
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February issue will be published on January 9th.

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VHF STEREO RADIO TRANSMITTING STATIONS ON RADIO 3



	Frequency		Maximum ERP
Brighton	92·3MHz	South & West	150W (directional aerial)
Holme Moss	91.5MHz	North	120kW`
Kendal	90.9MHz	North	25W (directional aerial)
Morecambe Bay	90·9MHz	North	4kW (directional aerial)
Northampton	91.1MHz	Midland	60W (directional aerial)
Oxford	91 · 7MHz	Midland	22kW (directional aerial)
Scarborough	92·1MHz	North	25W (directional aerial)
Sheffield	92·1MHz	North	60W
Sutton Coldfield	90·5MHz	Midland	120kW
Swingate	92·4MHz	London	7kW (directional aerial)
Wrotham	91.3MHz	London	120kW

THE "ENGLEFIELD" CABINET



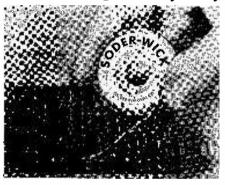
Peak Sound, the CirKit people have announced the "Englefield" cabinet for their amplifier modules. It is in kit form and includes components to complete a stereo amplifier based on the PA.12-15 Power Amp Module, the SCU/400 Stereo Preamp Module and the PS/45K Power Supply Kit. Cost of this kit is £38 4s, for 12W per channel system. Peak Sound, 32 St. Judes Road, Englefield Green, Egham, Surrey.

SWANSEA COLLEGE SOCIETY

The University College of Swansea Amateur Radio Society is once again fully active with activities such as Morse code and R.A.E. tuition for students. Amateurs and listeners are also welcomed to the meetings and details may be obtained from: Rob Wilcox, Room 520, Neuadd Gilbertson, University College of Swansea, Singleton Park, Swansea, SA2 8PS.

North Leeds Radio Club The North Leeds Radio Club has recently been formed. Will anyone wishing to join or visit this club please contact the Secretary, G. Brown, 2 Fearnville Close, Dib Lane, Leeds 8, Yorkshire.

Desoldering the dry way

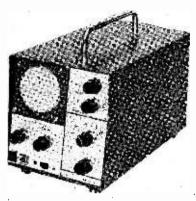


Southern Watch & Clock Supplies Ltd. are UK selling agents for "Soder Wick"—a dry wick method of desoldering. As can be seen in the illustration, it is supplied in reel form and is used by direct contact with the joint together with a soldering iron for heating purposes.

Soder Wick draws the solder up into itself quickly and no excessive heat is required and the desoldered joint is left solder-free, pure and non-corrosive. Prices range from 18 to 20s. but for readers who would like to try it out there is a special offer, open until 31st December whereby they can get a sample for 16s. Further particulars may be obtained from: Southern Watch & Clock Supplies Ltd., Industrial Tools Division, 48/56 High Street, Orpington, Kent, BR6 0JH

NEWS ... NEWS ... NEWS ...

SCOPE FOR SCHOOLS



A new oscilloscope, type EA 0699-1 has been announced by Mitre Electronic Products. It is intended mainly for use as a basic class oscilloscope in schools, and features a $2\frac{3}{4}$ in. diameter tube with green medium persistence trace and the Y bandwidth is d.c. to 100 kHz. There is less than 100 mV/cm Y sensitivity at maximum gain with full Y shift and automatically synchronised timebase range is 100 mS/cm to $10 \mu \text{S/cm}$ (approx.). X input with full X shift when timebase is off is 1 V/cm.

The oscilloscope is housed in an all-metal case measuring $6\frac{1}{4} \times 6\frac{1}{4} \times 10\frac{1}{4}$ in. Weight is 8 lb., supply voltage, 200-250V 50-60Hz and power consumption 25W. It is fully guaranteed and price is £24 10s. (1 off) with a discount for schools. A data sheet is available. Mitre Electronic Products, 22 Powis Terrace, London, W11.

LOW VOLTAGE AND ISOLATING TRANSFORMERS

Gardners Transformers Ltd., have introduced a range of open-style (Avon series) and enclosed style (Twynham series) Low Voltage and Isolating Transformers for input voltages of 100-125V and 200-250V. This applies for sizes from 24V/A to 1kV/A with a wide variation of output voltages. Further details in brochure GT.17 obtainable from: Gardners Transformers Limited, Christchurch, Hampshire.

Better Things are Electric

A new 16-page illustrated booklet in full colour designed to help people choose the right electrical fitting—plug, switch or socket—for every room in their home, is now available. Called "Better Things are Electric—with MK", it has been produced by MK Electric Ltd. It is available free on request from most electrical retailers or electricity showrooms, or direct from MK Electric Ltd., Edmonton, London, N9.

SPLICER FOR CASSETTE TAPES

Bib Division of Multicore Solders Ltd., announce the introduction of the Bib Model 24 \(\frac{1}{8}\) in cassette tape splicing and editing kit. It comes in a plastic wallet together with a plastic handled razor blade, Tape marker, reel of splicing tape on dispenser and a device for withdrawing tape from the cassette. The price is 29s.

The kit has been specially designed for use in jointing tape from C60, C90 or C120 cassettes and is particularly useful as it enables music from pre-recorded cassettes to be joined so that the playing time of a single cassette is extended.

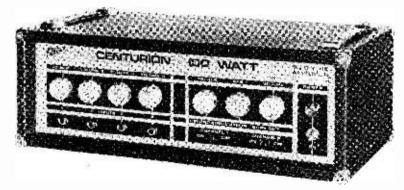
It's 5 new pence



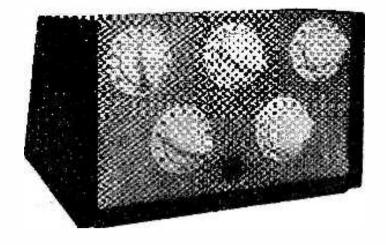
Multicore Ltd. announce an adjustment to their well-known 6d. solder pack. It now costs twice the price but you get double the amount of solder (enough for 100 average joints). It has been given the reference "2D" and packages are marked 1s. or 5p. Multicore Solders Ltd., Hemel Hempstead, Herts.

Don't forget the Practical Wireless filmshow

100 WATTS FROM ADASTRA



Adastra Electronics Ltd. announce their "Centurion" 100W amplifier which has a suggested list price of £99 and features a hand-assembled 25-transistor 6-diode printed circuit construction. The four individually gain controlled inputs have a sensitivity range from 1mV to 20V. A feature of this amplifier is that its design allows its output (100W at 40; 140W peak) to be open- or short-circuited without ill effect. The amplifier is housed in a black leathercloth cabinet with carrying handles and matching silver/black control panel. Adastra Electronics Ltd., 167 Finchley Road, London. N.W.3. Tel. 01-624 8164/5.



A MICROPHONE MIXER UNIT

NE of the main requirements for a microphone mixer is that of low noise level. Many of the cheaper commercial mixers fall down on this feature; although passable when used with low-output power amplifiers, noise levels become noticeable and disturbing at higher powers such as with large p.a. amplifiers. It is true that the ratio between the signal and the noise level will be the same irrespective of the power of the amplifier, but there are moments of silence especially with speech reproduction when there is no signal to mask the noise and it is then that high level noise is especially unpleasant.

Înexpensive commercial mixers were found unacceptable on this score whereas the better ones were unacceptable because of price. Hence the unit here described was designed and built. Other features required were a degree of amplification as well as mixing, a self-contained arrangement that could be operated at some distance from the main amplifier, and an input for tape or gram which

V. CAPEL

could not be overloaded by too high an input signal resulting from use and operation by unskilled hands.

Circuit

One of the reasons why the cheaper commercial mixers fail to achieve a good signal-to-noise ratio is because the input sockets are connected directly to the gain controls. The output from these is combined and fed to the base circuit of the first stage. An advantage of this arrangement is that only one transistor is needed for all inputs which saves cost. However it also means that the noise generated in it is fed uncontrolled into the following stages. Turning down a control only reduces the input signal thereby decreasing the signal-to-noise ratio.

In the circuit adopted for the mixer, each input has its own transistor which is followed by the gain control. When this control is turned down therefore, the noise from the input transistor decreases as well as the signal. The input stage is always the most significant as respects noise, because it is amplified

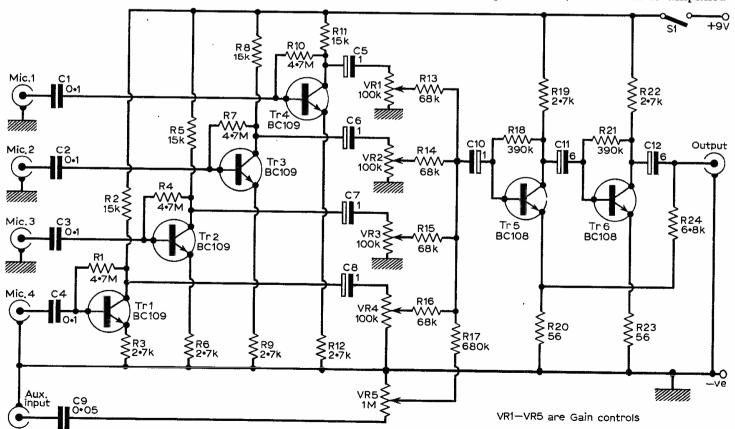


Fig. 1: The circuit of the five channel mixer. Four inputs are provided for microphones with an additional one for high level.

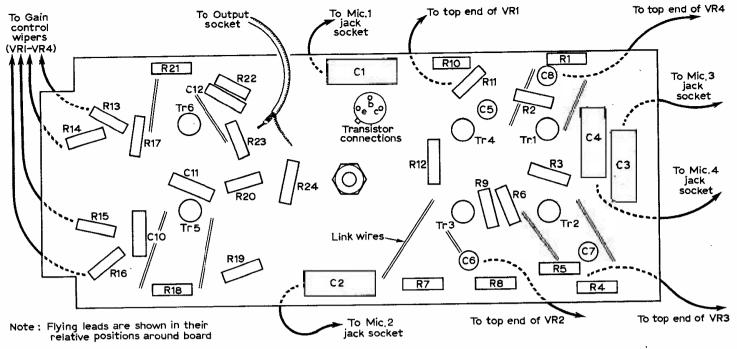


Fig. 2: The components are arranged as shown above on a Radiospares standard printed circuit.

*

components list

Resistors: R1 $4.7 M\Omega$ R13 $68 k\Omega$ R2 $15 k\Omega$ R14 $68 k\Omega$ R3 $2.7 k\Omega$ R15 $68 k\Omega$ R4 $4.7 M\Omega$ R16 $68 k\Omega$ R5 $15 k\Omega$ R17 $680 k\Omega$ R6 $2.7 k\Omega$ R18 $390 k\Omega$ R7 $4.7 M\Omega$ R19 $2.7 k\Omega$ R8 $15 k\Omega$ R20 56Ω R9 $2.7 k\Omega$ R21 $390 k\Omega$ R10 $4.7 M\Omega$ R22 $2.7 k\Omega$ R11 $15 k\Omega$ R23 56Ω R12 $2.7 k\Omega$ R24 $6.8 k\Omega$ All $10\%, \frac{1}{8}$ or $\frac{1}{4}$ watt miniature types. VR1, VR2, VR3 and VR4 $100 k\Omega$ log. potentiometers VR5 $1 M\Omega$ log. pot. Capacitors: C1 0.1μ F C7 1μ F 12V C2 0.1μ F C9 0.05μ F C4 0.1μ F C10 1μ F 12V C5 1μ F 12V C12 6μ F 12V					
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R12 $2 \cdot 7k\Omega$ R24 $6 \cdot 8k\Omega$ All 10% , $\frac{1}{8}$ or $\frac{1}{4}$ watt miniature types. VR1, VR2, VR3 and VR4 $100k\Omega$ log. potentiometers VR5 $1M\Omega$ log. pot. Capacitors: C1 $0 \cdot 1\mu$ F C7 1μ F 12V C2 $0 \cdot 1\mu$ F C8 1μ F 12V C3 $0 \cdot 1\mu$ F C9 $0 \cdot 05\mu$ F C4 $0 \cdot 1\mu$ F C10 1μ F 12V C5 1μ F 12V C11 6μ F 12V C6 1μ F 12V C12 6μ F 12V C6 1μ F 12V C12 6μ F 12V C6 1μ F 12V C12 6μ F 12V C9 T7 BC109 Tr4 BC109 Tr5 BC108 Tr3 BC109 Tr6 BC108 (Plastic encapsulated versions of the BC108 and BC109 are now very common, have identical characteristics and are cheaper. Their numbers are BC168	R11	$-15 \mathrm{k}\Omega$	R23	56Ω	
VR1, VR2, VR3 and VR4 100kΩ log. potentiometers VR5 1MΩ log. pot.	R12	2.7 k Ω	R24	6·8kΩ	
VR5 1MΩ log. pot. Capacitors: C1 $0.1\mu F$ C7 $1\mu F$ 12V C2 $0.1\mu F$ C8 $1\mu F$ 12V C3 $0.1\mu F$ C9 $0.05\mu F$ C4 $0.1\mu F$ C10 $1\mu F$ 12V C5 $1\mu F$ 12V C6 $1\mu F$ 12V C11 $6\mu F$ 12V C6 $1\mu F$ 12V C12 $6\mu F$ 12V Semiconductors: Tr1 BC109 Tr4 BC109 Tr2 BC109 Tr5 BC108 Tr3 BC109 Tr6 BC108 (Plastic encapsulated versions of the BC108 and BC109 are now very common, have identical characteristics and are cheaper. Their numbers are BC168	All 1	0%, 訁 or 钅 watt	miniat	ure types.	
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C3 $0.1 \mu F$ C9 $0.05 \mu F$ C4 $0.1 \mu F$ C10 $1 \mu F$ 12V C5 $1 \mu F$ 12V C11 $6 \mu F$ 12V C6 $1 \mu F$ 12V C12 $6 \mu F$ 12V Semiconductors: Tr1 BC109 Tr4 BC109 Tr2 BC109 Tr5 BC108 Tr3 BC109 Tr6 BC108 (Plastic encapsulated versions of the BC108 and BC109 are now very common, have identical characteristics and are cheaper. Their numbers are BC168	C2		C8	1μF 12V	
C6 1μF 12V C12 6μF 12V Semiconductors: Tr1 BC109 Tr4 BC109 Tr2 BC109 Tr5 BC108 Tr3 BC109 Tr6 BC108 (Plastic encapsulated versions of the BC108 and BC109 are now very common, have identical characteristics and are cheaper. Their numbers are BC168	C 3	0·1μF	C 9	0·05μF	
C6 1μF 12V C12 6μF 12V Semiconductors: Tr1 BC109 Tr4 BC109 Tr2 BC109 Tr5 BC108 Tr3 BC109 Tr6 BC108 (Plastic encapsulated versions of the BC108 and BC109 are now very common, have identical characteristics and are cheaper. Their numbers are BC168	C4	0·1 <i>μ</i> F	C10	1μF 12V	
C6 1μF 12V C12 6μF 12V Semiconductors: Tr1 BC109 Tr4 BC109 Tr2 BC109 Tr5 BC108 Tr3 BC109 Tr6 BC108 (Plastic encapsulated versions of the BC108 and BC109 are now very common, have identical characteristics and are cheaper. Their numbers are BC168	C5	1μF 12V	C11	6μF 12V	
Semiconductors: Tr1 BC109 Tr4 BC109 Tr2 BC109 Tr5 BC108 Tr3 BC109 Tr6 BC108 (Plastic encapsulated versions of the BC108 and BC109 are now very common, have identical characteristics and are cheaper. Their numbers are BC168	C6	1μF 12V	C12	6μF 12V	
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for the BC108 and BC169 for the BC109.)	for the BC108 and BC169 for the BC109.)				
Miscellaneous:					
Six jack sockets; pointer knobs; Radiospares printed			ointer kı	nobs: Radiospares printed	

panel; SW1 toggle on-off switch; battery; battery

clips; screened lead etc.

by all the stages that follow, whereas the succeeding stages have less amplification following them.

Obviously, low-noise transistors should be used, so the Mullard silicon planar epitaxial transistors BC109 and BC108 were chosen. These are n-p-n types so battery polarity will be negative to earth. Constructors used to working with the more familiar p-n-p varieties will need to check polarity of the electrolytic capacitors.

Current biasing of the first stages is employed by returning the single high-value base resistor to the collector. A measure of negative feedback results, and further feedback is achieved by leaving the emitter resistor unbypassed. If desired, a greater or lesser number of inputs can be provided as required. Three were really all that were necessary, but an extra one was fitted in case it should be required in the future. It is easier to add one when first constructing, than later! Extra inputs will not add to the noise level providing the controls of those not being used are turned back to zero.

Although all controls are taken to a common input of the next stage each one will have only marginal effect on the settings of the others due to the isolating resistor in series with the wiper of each control.

The auxiliary input is fed into the same point. In this case it is best to feed the input directly to its gain control, because if applied first to an amplifying stage as is the case with the microphone inputs, this stage could be overloaded by a high level signal such as the output of a tape recorder. Here, the control will reduce the signal to an acceptable level. Impedance of this input is kept as high as possible so that crystal or ceramic pick-ups can be used, hence the higher value of the control and isolating resistor.

At first, direct coupling was considered between the second and third stages as this would avoid reactance in the coupling and provide d.c. stabilisation by a d.c. feedback loop. However, as the second stage must be "above" the first as regards d.c. voltage in directly coupled stages, this in effect halves the battery voltage to each. Where a line voltage of around 20 volts is available as is common with most mains-powered transistor equipment, this is quite satisfactory, but things are different when the supply is only 9 volts and reducing as the battery voltage falls. Silicon transistors are less prone to thermal and other vagaries of germanium transistors, so it was deemed best to dispense with the d.c. stabilisation.

To further reduce noise levels, a negative feedback loop was included right from the output socket back to the emitter of the second stage.

Construction

With any construction, one of the first things to consider is the case, as this will determine the way the components are assembled. The case chosen for the prototype started life as a Channel TV tuner unit. There are probably many of these around in dealers' junk rooms, but if one cannot be obtained, a similar construction can easily be made.

A Radiospares transistor printed panel was used for the building of the circuit. These are not obtainable direct from the firm as they deal only with the trade, but almost any dealer could get one within a few days even if he did not have one in stock. There are positions for eight transistors on these boards, and the base, emitter and collector connections are all marked. A centre strip of print running down the middle of the board can be used for earth, and two conductors on either side, for the battery positive rail. Along both edges of the board are triangular multiple connections.

The most straightforward way of wiring is to connect a wire link from the transistor print connection to the nearest multiple, and then wire the associated components from there. It may be necessary to link two adjacent multiples where several connections are needed to the one point. Flying leads were fitted so that connections could be made to the controls and jack sockets.

Performance

The gain of the microphone channels is 35dB, which enables the mixer to be used with power amplifiers having low input sensitivity. High impedance microphones should be used, either crystals or moving-coil and ribbon instruments with built-in transformers. Medium impedance microphones of 600 or 200 ohms will work satisfactorily, there being sufficient gain for these, although the signal-to-noise ratio is decreased. When used with high impedance instruments, the noise level, even with a large p.a. in a hall, is unobtrusive at normal levels.

The gain of the auxiliary input is unity, there being no amplification required here, only the facility of mixing. A fairly high input impedance is presented so that crystal or ceramic pick-ups can be used with no loss of bass.

Overall frequency response is flat between 20Hz and 10kHz, and there is a gradual drop at the upper end to -3dB at 25kHz. Battery consumption is about 6mA so a PP6 battery should give long service.

When using this or any other mixer, always keep the controls that are not in use to the minimum position. Those that are being used should be set at an advanced level and the control on the power amplifier kept to a low position, as this will give a better signal-to-noise ratio than the reverse.

COLUMN

OUTH AMERICAN medium wave stations are often audible after midnight during the winter. Propagation is good over the long sea path from UK enabling the DXer to hear stations quite considerable distances away. Even when conditions are poor the Argentinian stations LR3 (950) Radio Belgrano and LR1 (1070) Radio el Mundo, can often be heard, sometimes they are the only DX on the band. South Americans are usually at their best when the North American path is poor. Brazilians most frequently logged are PRA3 (860) with the slogan Radio Mundial, PRF4 (940) Radio Jornal, PRE8 (980) Radio Nacional, PRE3 (1180) Radio Globo; all are situated in Rio de Janeiro. Brazilian stations are easy to recognise as the language is Portuguese instead of the more usual Spanish from that continent. A number of Venezuelan stations can be heard, the more prominent being YVRS (1020) Radio Marguarita and YVQJ (1080) in Barcelona. Further to the west are the Colombian stations HJDK (750) La Voz de Antioquia and HJBI (840) Ondas del Caribe in Santa Marta. The Surinam station PZX7 (725) in Paramaribo is frequently a strong signal though interference from the German station on 728 can be troublesome. PZX7 identifies itself as "SRS" which are the initials of the Dutch organisation which owns the station. Announcements are in Dutch, English and Hindi and the station will QSL. More difficult South American countries are Peru with OAX4A (854) Radio Nacional and OAX4U (1010) Radio America, both stations in Lima; Uruguay with CX16 (850) Radio Carve in Montevideo; Chile with CB106 (1060) Radio Mineria and CB118 (1180) Radio Portales, both in

During the late evening while waiting for the DX paths to open, readers may care to try some semi-DX from Europe. The Portuguese National Radio operates a number of high power MW transmitters and two of these—on 755 and 1161—have programmes in English at 2245 hrs GMT. Commercial stations to look for include Radio Coub Portugues with CSB9 (782) in Miramar and CSB2 (1034) in Lisbon; Radio Renascena CSB3 (1286) in Lisbon; Emissora Norte Reunidas CSB5 (1578) Oporto; Emissora Associados de Lisboa CSB4 (1594) Lisbon. The commercial stations run on well into the night and all will QSL. Sud Radio in nearby Andorra on 818 has been heard recently with programmes in English at 2130 hrs and this station too will QSL. Three stations from the far north of Europe that often appear in the late evening are Murmansk (656) in Arctic USSR; Godhavn (650) in Greenland and Hofn

(665) in Iceland.

Santiago.

Ramadan ends on 11th December, so have a look for some of the rare Middle East countries mentioned last month while there is still time. Saudi Arabia has been heard on 705 recently at 2100 hrs GMT with a programme in English. The new All India Radio megawatt station in Calcutta is reported to be on 1130kHz though it has not been heard yet by the writer.

CHARLES MOLLOY

EXHIBITIONS RICHARD COLLINS reports...

This year Practical Wireless was represented at two exhibitions. The first one was the 1969 International Radio Engineering and Communications Exhibition (the RSGB Exhibition) held at the Royal Horticultural New Hall, Westminster, S.W.1 from 1st to 4th October.

The second exhibition was the 1969 International Audio Fair held at Olympia from 17th to 23rd October. Below are photographs taken during the two exhibitions.



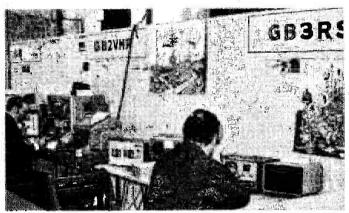
The opening address was made by Mr. R. J. Halsey, C.M.G., F.C.G.I., D.I.C., B.Sc.(Eng.), F.I.L., Director of Cable & Wireless Ltd. He is seen here welcoming visitors to the Exhibition.



Mr. J. W. Swinnerton. T.D., B.Sc.(Econ.), G2YS, President of the Radio Society of Great Britain presents the Exhibition Organisers' Plaque to George Jessop, G6JP, for his 2m Transistorised Transmitter/Receiver.



A group of enthusiasts gathered round the PRACTICAL WIRELESS stand, while staff member, Trevor Preece, G3TRP, explained the workings of the P.W. Pedal Steel Guitar.



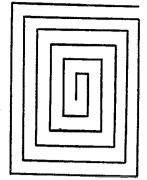
The Exhibition transmitting stations which were operating on all Amateur Bands between 1-8 and 144MHz. The equipment was provided and manned by the Crawley group of the RSGB.



Diana and Audrey looking after the magazine sales section of the P.W. and P.E. stand at the Audio Fair.

A C I PART EIGHT

DADIU SEMICONDUCTOR TIPHNINEY



by M.F. DOCKER, M.Sc.

In this article several new devices will be discussed and the final two articles in the series will deal with the techniques of producing integrated circuits, both monolithic and hybrid thick and thin film types.

Thyristors

The first device, the thyristor, could well have been described in the section dealing with diodes as it is often found in two lead form. However its construction is radically different from that of a diode and the same device can be easily converted during manufacture to form a triode or tetrode thyristor. The thyristor can be defined as a four layer p-n-p-n device as seen in Fig. 1(a) and relies on regeneration in the structure to produce a switching action.

With the polarities shown in this Fig. 1(a) junctions A and C are both forward biased whilst junction B is reverse biased. Consequently only a very small current, the saturation current of the material, will be able to flow across junction B. However, when the potential difference between the input terminals is increased sufficiently it is found that the current through the device suddenly increases as shown in the voltage-current curve of Fig. 2. This behaviour can be explained by considering the device as composed of a pair of complementary transistors, Tr1 and Tr2, in Fig. 1(c). From Fig. 1 (b) Tr1 is seen to be a p-n-p transistor and Tr2 a complementary n-p-n transistor. If the alphas of the two transistors are $\alpha 1$ and $\alpha 2$ respectively and if the saturation collector current of each device is Isat1 and Isat2 respectively then it is readily seen that:

 $I1 = \alpha 2I + Isat2$ and $I2 = \alpha 1I + Isat1$ also, since the current across junction B must be equal to I:

or
$$I=I1+I2$$

 $I=\alpha II+\alpha 2I+Isat$
where $Isat=Isat1+Isat2$.

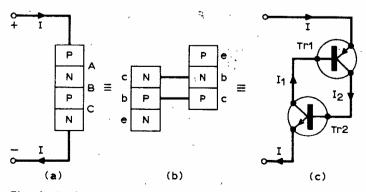


Fig. 1: Basic thyristor representation (a) together with two derived equivalents (b) and (c).

This equation can be reduced to the form: $I = Isat/(1 - (\alpha 1 + \alpha 2))$

and this relates the current through the thyristor to the leakage current and the current gains of the equivalent transistors. Now in a previous article it was shown that the alpha of a transistor depends on the amount of recombination which occurs in the base region, so that for a high alpha the base has to be narrow.* But the thyristor is intended for high voltage applications, so to avoid punch through the individual regions all have to be wide. This gives the device a low alpha.

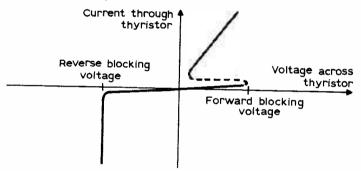


Fig. 2: Characteristic curve of the voltage across a thyristor and the current through it.

Because of this the term $(1-(\alpha 1+\alpha 2))$ above is fairly large and I is not much larger than the leakage current. If in some way recombination can be reduced the alphas will grow and I becomes large. This is done by temporarily filling the impurity centres in the base so that a larger current will flow, carriers then becoming available to diffuse across to the collector junction B, normal transistor action then taking place. After this regenerative feedback holds the device on until the voltage across the terminals is reduced to zero.

There are various ways of filling the trapping centres and one of these, used in this diode form, is to increase the voltage across the device until the leakage current across junction B goes into an avalanche condition. This results in a large current flowing across the junction into the two base regions. The carriers constituting this current fill the impurity centres and enable the transistor alphas to become larger, this in turn resulting in an increase in the current through the device so that the thyristor is then turned on. When this happens all the junctions are in effect forward biased and the voltage across the thyristor falls to a fraction of a volt. The voltage at which the avalanche starts to take place is called the forward breakover voltage Vbo and is quoted in manufacturers' literature.

When a reverse voltage is applied to the thyristor junctions A and C are reverse biased and junction B is forward biased. However the previously described





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action does not occur in this case as the circuit is non-regenerative being in fact simply two diodes in series. The result is that when the reverse voltage does become sufficient to cause avalanching to take place the voltage across the device is maintained and a high power dissipation takes place in the thyristor. The variation of current with voltage across a thyristor is shown in Fig. 2. In most devices the peak reverse capability is made somewhat greater than the forward breakover voltage so that the device can be used as triggerable switch.

The rate of change of voltage across the thyristor can also be used to produce switching. This relies on the injection of charge into the depletion layer as its width changes. In this way it is possible to switch the thyristor by putting a pulse on to the terminals, of amplitude less than the breakover voltage.

Silicon controlled rectifier

A third method of triggering involves the injection of a pulse of current directly into one of the base regions. This produces an increase in the alpha of the equivalent transistor and the regenerative feedback of the circuit causes the current through the thyristor to rise quickly. Devices using this method are called silicon controlled rectifiers (s.c.r.s.). The size of the pulse required to trigger the thyristor depends on which of the two bases the pulse is injected into. The lower p-type base is the more sensitive and devices in which this base is connected as trigger are called conventional s.c.r.s Connection to the upper n-type layer of Fig. 1(a) results in a so-called complementary s.c.r.

Silicon controlled switch and light activated s.c.r.

The silicon controlled switch is a thyristor with connections to both the base regions so that in consequence it is a four terminal device. Current pulses can be injected into either one or both of the bases to produce switching. Another method commonly used to trigger the thyristor is the use of light induced carriers in the base regions. This is used in the light activated silicon controlled rectifier (l.a.s.c.r.) and in the phototran. These are used in many opto-electrical control systems.

Switch off

A point to be noticed in the operation of the thyristor is that once it is switched on it cannot easily be switched off until the voltage across its terminals has been reduced to a very low value. Even then sufficient time has to be given for the charge carriers which are stored in the base region during the forward conducting state of the thyristor. This time is typically several microseconds: if the voltage is reapplied before expiration of this time the thyristor will switch on again immediately.

Types and uses

The construction of a typical alloy-diffused thyristor is shown in Fig. 3(a). The p-type regions are produced by diffusion of acceptor atoms from the gaseous state and the cathode region is produced by alloying suitable impurities into one surface. Leads are then attached as shown Planar thyristors are also produced as shown in Fig. 3(b), usually several

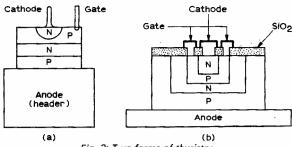


Fig. 3: Two forms of thyristor.

devices being made on one wafer which is then cut up into dices to give the individual thyristors.

The thyristor is often used to control a.c. supplies. However in this application they have the disadvantage that they only switch into their forward conducting state in one direction. In order to permit full wave control of power supplies it is possible either to use two thyristors or to use a device called a triac. This is a multiple layer device which is equivalent to two s.c.r.s so arranged that they switch on alterna-

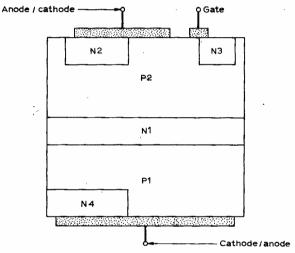


Fig. 4: Triac thyristor construction.

tive half-cycles of the mains. The structure of this device is shown in Fig. 4 and its voltage against current characteristic is given in Fig. 5.

A small s.c.r. with an avalanche diode between the anode and gate electrodes is also available. This can be used as a low current switch and is given the name silicon unilateral switch, or s.u.s. A bilateral version of this device is also available and is used to trigger high power triacs as it provides the alter-

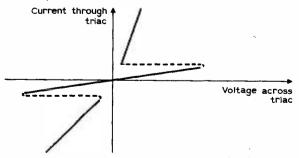


Fig. 5: Characteristic curve showing the variation in current flowing through a triac as the voltage across it is changed.

nately positive and negative pulses required for biphasic operation of the triac.

There are numerous other thyristors available including the diac which is similar to the s.b.s. and is also used to switch the triac. The quadrac, which is a three terminal device containing both a diac and triac and can be used in phase control of biphasic power supplies, is another thyristor which has only recently become available.

Unijunction transistor

Another device exhibiting a negative resistance effect is the unijunction transistor. This is similar in construction to the f.e.t. but its gate electrode is called the emitter and is much smaller than that of the f.e.t. It is normally operated in forward bias and the structure of a typical bar type u.j.t. is shown in Fig. 6 together with its circuit representation. It con-

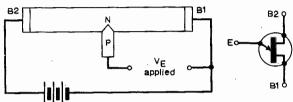


Fig. 6: Unijunction transistor construction and circuit symbol.

sists of a silicon bar with two ohmic connections made to each end, called the base terminals, and an aluminium emitter which is alloyed to the base to form a p-n junction. If a current is made to flow through the base the potential at the emitter will be Ve. As long as the voltage applied to the emitter is less than this the junction will be reverse biased and no current will flow. However if the applied voltage is increased beyond Ve the junction will go into a forward conducting state and holes will be injected into the base region. In order to maintain neutrality electrons will be released in the base region between the emitter and base one, which results in the resistance of the region falling. This then causes the potential drop across the bar in this region to fall with a consequent increase in the forward bias applied to the junction and the number of injected holes rises yet again. Obviously this is a regenerative effect and causes the emitter current to rise sharply.

A curve showing the variation of emitter voltage as the emitter current changes is shown in Fig. 7, where the curves for different voltages between bases are indicated. The most significant point of this is that when the emitter voltage reaches Ve the

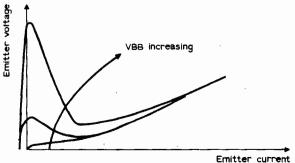


Fig. 7: Variation of emitter voltage with current as the base-tobase voltage in a unijunction transistor is changed.

emitter current suddenly increases and whilst this is happening the voltage across the emitter falls. This is the opposite behaviour to that shown by a resistor and is consequently called a negative resistance effect. This enables the unijunction transistor to be used in many oscillators, staircase waveform generators and dividers and circuits where a negative resistance effect is required.

Spacistor

Two other devices which are occasionally met but which do not yet seem to have reached the world of the amateur are the spacistor and the tetrode transistor. A brief explanation of these devices is worthwhile.

The spacistor is a single junction amplifier. Basically it is a p-n junction with a large reverse bias so that it has a wide depletion region. Current carriers are injected into this depletion region from a metal contact and are swept across the depletion region by the electric field. Because of the high field it is possible to have quite short transit times and thus to have a high cut off frequency. Another

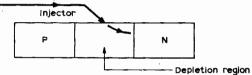


Fig. 8: Basic spacistor construction.

type of spacistor employs a fourth electrode called a modulator which affects the gain of the device. It also increases the input and output impedances of the spacistor by increasing the isolation of the injector from the output current. A diagram of the simple spacistor is shown in Fig. 8.

Tetrode transistor

The tetrode transistor is similar to the ordinary transistor except that it has two base contacts. Because of this it is possible to produce a field across the base so that effectively only a small portion of the emitter-base contact is forward biased. This reduces the active width of the base so that its resistance is reduced and also the transition capacitance is reduced. These assets make the tetrode especially useful in high frequency applications including high speed switching circuits. Figure 9

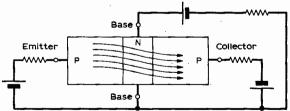
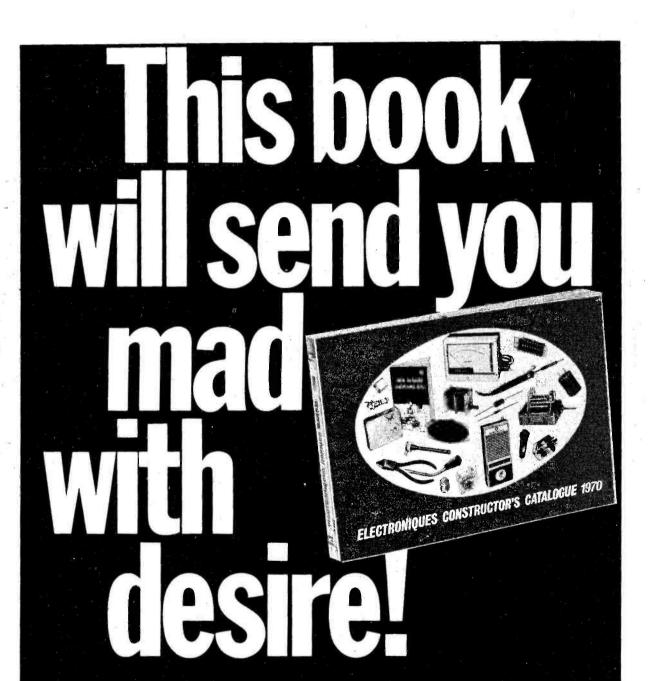


Fig. 9: Construction of a tetrode transistor and its circuit connections.

shows the schematic cross-section of a tetrode transistor including a representation of the current flow pattern. The reduction in the base width is clearly seen from this figure and results in a decreased base resistance because of the lessened distance the base current has to travel before recombination.

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PEDAL STEEL GUITAR Part 3 F.C.JUDD

THE conclusion of Part 2 dealt with the last stage of assembly which was the linkage of the pedals to the roller levers by means of the "connecting" rods. The photograph on this page shows the actual connection of the horizontal rods to the roller levers. Adjustment of the pedal movement and linkage depends on the tuning adopted for the instrument but for the example given in Part 1 (an E6th tuning), string 2 will be tuned sharp and string 4 will be tuned flat when their respective pedals are depressed. The accuracy of the raising or lowering of pitch depends entirely on the accuracy of adjustment to the roller lever stop screws and the downward movement of the pedals. Adjustment should be such that when the pedal is depressed the string is re-tuned just as the pedal touches the stop rail beneath it and as the roller lever comes into contact with its own stop screw. The actual downward movement of the pedal for a semitone change of pitch should not be more than half an inch i.e., the pedals should normally rest about $\frac{1}{2}$ inch or even less above the stop rail as shown in the photograph.

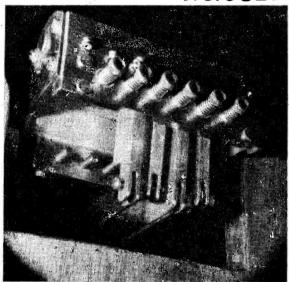
When preliminary adjustment of the pedal mechanism has been completed the engraved fretboard can be fitted. This may be glued to the guitar body with Evostik or Bostik. The strings can now be tuned to pitch and the accuracy of tuning checked over the full length of the fretboard i.e., at all fret positions. Providing the distance between the "nut" and the 12th fret and between the 12th fret and the centre line of the roller bridge are exactly equal (see diagrams in Part 1) the tuning should be accur-

ate at all fret positions.

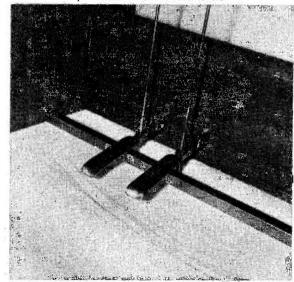
The Preamplifier

The final stages of construction are concerned with the preamplifier, its power supply and the optional foot pedal volume control (swell pedal). The preamplifier might also be considered as optional for there is no reason why the guitar pick-up should not be directly connected to a suitable amplifier already equipped with tone controls and volume control and having an input sensitivity of 50 to 100mV.

However, there is a purpose for the built-in preamplifier in that it makes up for gain loss incurred by the foot-operated volume control and more important, it has a treble lift and cut control that will enable the player to obtain that very sharp brilliant tone favoured by players of the pedal steel guitar. In



How the flat ends of the connecting rods are secured by 4BA screws to the roller levers.



Linkage to foot pedals. Adjustment is made by the 2BA nuts beneath the pedals, i.e., the pedals can be raised or lowered on the ends of the vertical connecting rods.

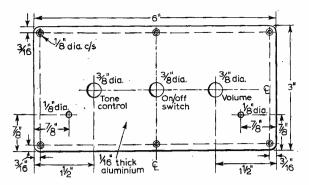


Fig. 20: The preamplifier panel. Details for drilling, etc.

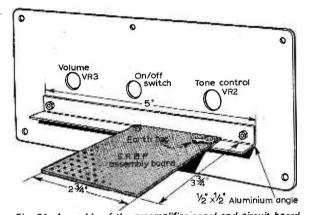


Fig. 21: Assembly of the preamplifier panel and circuit board. fact the preamplifier may be of interest to plectrum guitarists.

The whole preamplifier is assembled on its own panel and if constructed to the dimensions given in Figs. 20 and 21 will fit into the slot provided on the top of the guitar consol (see Part 1). The circuit is shown in Fig. 22 and employs two Mullard BC109 transistors with a negative feedback tone control system that provides approximately 15dB treble lift

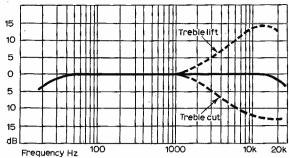


Fig. 23: Frequency response of the preamplifier.

and 12dB treble cut as shown by the response curves in Fig. 23.

The overall gain of the preamplifier can be varied a little by means of the pre-set control VR1 $(4.7k\Omega)$. For normal operation this control should be set to about midway position. At its maximum resistance the overall gain of the amplifier will be decreased. At its minimum resistance the gain of the amplifier will be increased but the amount of treble lift will

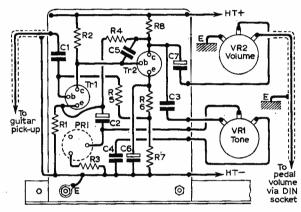


Fig. 24: Pictorial wiring diagram and layout for the preamplifier.

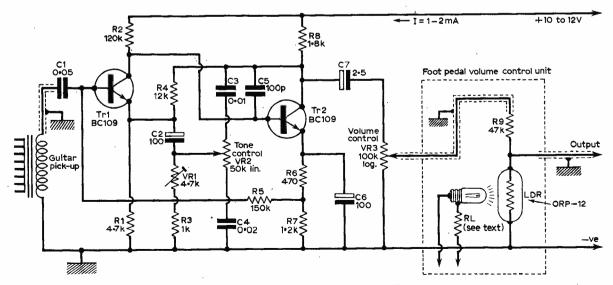


Fig. 22: Circuit diagram of the preamplifier.

be reduced. The average signal output from the preamplifier is about 200mV with VR1 set midway. With the foot pedal volume control in circuit the output is reduced to about 100 to 150mV. If the pedal volume control is not used, the output can be taken from the slider of VR3 and will be around 200mV. The preamplifier, with or without the pedal volume control, can be connected to any amplifier having an input impedance of $10k\Omega$ or greater and an input sensitivity of 100 to 200mV. As already mentioned a higher or lower signal output can be obtained by adjusting the pre-set VR1. A pictorial wiring diagram for the preamplifier is given in Fig. 24.

Details for the power supply are given in Figs. 25A and B. If constructed as shown it can be mounted up inside the console as can be seen in the photograph. It may be necessary to orientate or reposition either the whole assembly or the mains transformer itself to prevent hum being induced into the guitar pick-up.

The Foot Pedal Volume Control

Assuming the pedal volume control is to be used, then the pre-amplifier output can be fed to it via a 3-pin DIN socket mounted at the side of the console (see Part 1). This socket also carries the 12V d.c. (from the power supply) to light the control lamp in the pedal volume control. Wiring connections for the socket are shown in Fig. 26. The signal lead must be screened and the overall length of the cables between the two DIN plugs (A and B) should be at least 2 feet.

The pedal volume control employs a light discriminating resistor (ORP12) which becomes part of

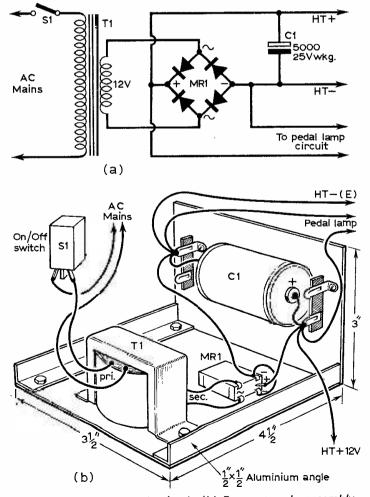
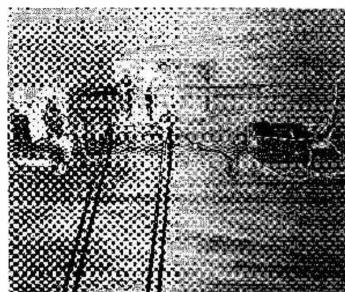


Fig. 25: (a) Power supply circuit. (b) Power supply assembly.



The position of the power supply (left) and the pre (right). Note also the relative position of the pedal rod linkage mechanism (centre) and the pre-tension spring just to the left of it.

an attenuating network formed by itself and R9. When the pedal is depressed in the backward direction, light from the control lamp decreases the resistance of the LDR and reduces the signal level. The light must not be too bright hence the need for some series resistance (RL). The author used a 6.3V 0.15A bulb with a series resistor of approximately 60 ohms. Lamps up to 12V at 60 to 100mA

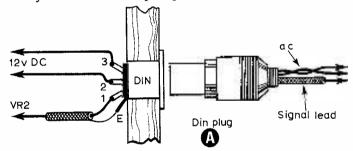
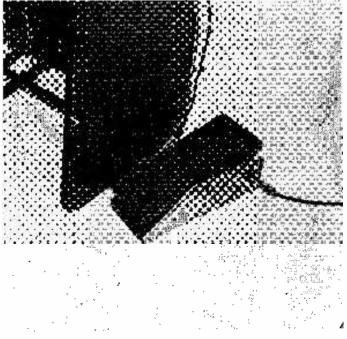


Fig. 26: Connections to the 3-pin DIN socket at the side of the console



The completed foot pedal volume control.

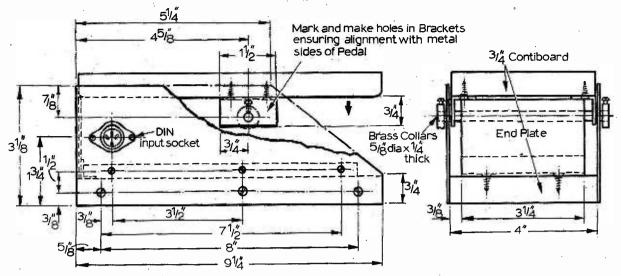


Fig. 27: Details of the foot pedal volume control.

can be used but should be dimmed a little with series resistance of appropriate wattage. A pre-set wire-wound resistor of about 50 ohms and 2W rating would be suitable.

An ordinary geared potentiometer pedal volume control could of course be used. The only real advantage of the LDR system is noiseless operation and the fact that it does not wear out as would a carbon track potentiometer. The photograph shows the completed pedal volume control and the diagrams in Figs. 27, 28, 29, and 30 give details for construction. The base of the control and the foot pedal were cut from \$\frac{1}{4}\text{in}\$. Contiboard left over from making the console. The two sides were made from \$\frac{1}{15}\text{in}\$. thick Dural. The pedal itself is hinged to the body on a \$\frac{1}{4}\text{in}\$. diameter spindle held fast by collars at each end and has an overall movement from level to a backward slant, of about 30°.

The control lamp and the LDR are both mounted in small wood blocks as shown in Figs. 30 and 31. It is best to solder the leads for the lamp directly to it and secure the lamp in the block with a spot of adhesive. The two blocks must be only just far enough apart to allow the aperture plate to move freely between them. The wiring for the 3-pin DIN socket, the output jack socket and the LDR and lamp are shown in Fig. 31. Providing the LDR is recessed in its mounting as shown in the diagrams it will not be affected by light coming from outside. Note that the end plate as shown in Fig. 29 serves as a forward stop for the pedal.

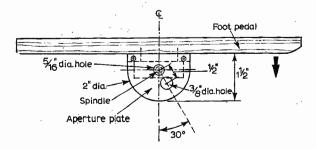
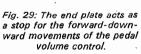
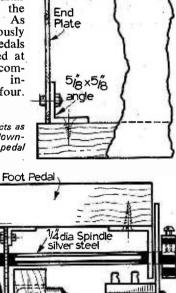


Fig. 28. The foot pedal of the volume control and the LDR aperture plate.

The complete and finished instrument, exactly as described in this series of articles, gave a very pleasant but brilliant tone quality with a good sostenuto (sustaining of sound) typical of the pedal steel guitar and its forerunner the Hawaiian guitar. pointed out previously the number of pedals need not be confined at two only-some commercial single-neck inhave struments four.



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Output .

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seetext

Fig. 30: The LDR and its lamp are mounted so as to be in line with the ½in. diam. spindle and the centre line of the aperture plate.

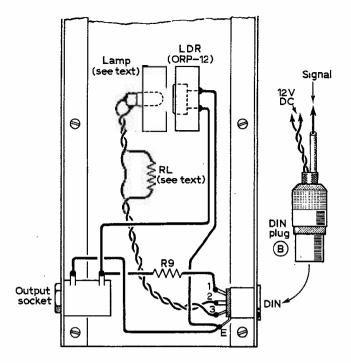


Fig. 31: Wiring for the pedal volume control, its input and output sockets and the 3-pin DIN connecting plug.

However, by making and fitting four roller levers as suggested, the two pedals can be changed over to other strings should alternative tuning combinations be required.

On reading through the first two articles again the writer has discovered one or two points that might not have been clear. First the unused roller levers. These should be locked at midway position (hanging vertically) by means of the locking screws. The strings can be anchored to them directly or to the holes in the tailpiece.

Before adjusting the movement of the pedals and linkage, set the roller levers concerned by means of their stop screws, so that they too hang vertically. The roller that is used to tension its string should now have its forward stop screw adjusted so that the lever can move forward i.e., toward the pick-up. The roller lever that is used to de-tension its string should have the rear (tailpiece) stop screw adjusted so that the lever can move toward the tailpiece. The basic tuning should of course be done with the pedals in their off or neutral position.

Finally a note on suitable strings. Those used for the tuning prescribed in Part 1 which is based on the chord of E6 were selected from the wide range of "Rotosound" strings for guitars of all kinds. These were as follows:

8	7	6	5	4	3	2	1
Aþ	В	D	E	Ab	В	C#	\mathbf{E}
0.038"	1	0.028"	- 1	0.020"	1	0.016"	
Covered		Covered	.	Plain		Plain	_
0	03	5" O	024	•	0.018		0.014″
Co	ove	red 1	Plaiı	n :	Plair	1	Plain

Heavy gauge covered strings could be used for 8, 7 and 6 with a resultant rounder and stronger tone. Some experiment with string gauges is well worthwhile and a list giving all the different gauges of strings and a chart showing the different types recommended for guitars i.e., pedal steel, Hawaiian and plectrum can be obtained by writing to Rotosound—James How Industries Limited (Music Division), 20 Upland Road, Bexley Heath, Kent.

NEXT MONTH IN

WIRELESS

THE MICROTEST

Few people build multi-range testmeters nowadays because Japanese ready-built meters are freely available at very competitive prices. There does, however, remain one distinct advantage in "rolling one's own", and this is the high degree of accuracy to which a meter can be calibrated. It is quite easy to do, and is fully described in this article on the Microtest 24-range a.c./d.c. multimeter using a 50µA movement.

THE TWO-FIFTY TRANSMITTER

Radio Amateurs who are keen on turning their attention to 2-metres will find G3TYJ's Two-Fifty transmitter very appropriate. It is a relatively simple crystal controlled 4-valve 40watt input design which can be used as it stands for c.w., or connected to any normal modulator for phone. A circuit is also provided to assist those who prefer to use the simpler clamp-tube modulation. Full coil-winding details are given, along with sufficient constructional information to enable anyone who has a transmitting licence to build this transmitter without difficulty.

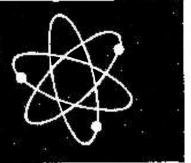
REPAIRING LOUDSPEAKERS

Loudspeaker cones are very fragile, and the slightest tear can seriously impair reproduction quality. Having a speaker reconed professionally can be very expensive, however, and so this article explains how to carry out this task oneself, replacing the original paper cone with a combination of paper, expanded polystyrene, polyure-thane foam and aluminium foil, the mixtures depending on which frequency range the loudspeaker is intended to cover. The complete cost of repairing one of the author's 12in. loudspeakers came to about 14s.

PLUS OTHER CONSTRUCTIONAL PROJECTS AND REGULAR FEATURES

Do not miss your copy of the February issue of Practical Wireless—on sale 9th January price 3/-

EXPERIMENTERS CORNER



DESIGNING CLASS "A" TRANSISTOR AMPLIFIERS

C. R. BOGGIS, M.A.P.A.E.

DESIGNING basic transistor amplifier stages can be made very simple by following a few "rules of thumb", so enabling the experimenter with but a modicum of theoretical knowledge to tailor established circuits to his own needs. This article, which can be read in conjunction with last month's "Experimenters Corner", describes how to work out the component values for germanium or silicon amplifiers and couple them to other stages without upsetting their operation.

Germanium Amplifiers

If a single amplifier stage as shown in Fig. 1 is designed as follows it will be able to function over the temperature range of 20 to 50° Centigrade. In the worked example, a general-purpose small signal transistor is used (Mullard type OC71, or similar).

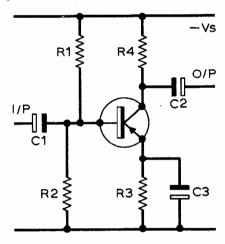


Fig. 1: A straightforward amplifier stage suitable for a germanium transistor.

First the supply voltage is chosen. Here we select 9 volts, this being readily available from standard batteries. We then decide on a value of collector current. For a very small input and low noise this should be around 100-200 microamperes, but for large inputs the current could be anything up to about 100 milliamps. As a general rule a current of 1mA is desirable, and it is around this figure that the stage designed here is evolved.

Having decided on the collector current, the first rule may be applied. This states that the emitter resistor should drop approximately 1 volt. Therefore in our example, R3 will be equal to $\frac{1 \text{ volt}}{1\text{mA}}$, since the emitter current can be considered equal to the collector current for this purpose, which suggests a resistor value of 1000 ohms.

The next rule states that for good stability, the collector voltage should be equal to half of the result of subtracting the emitter voltage from the supply voltage.

Here the collector voltage should be $\frac{9-1 \text{ volts}}{2}$ or 4 volts.

With a collector current of 1mA, R4 should be $\frac{4 \text{ volts}}{1\text{mA}} = 4000 \text{ ohms}$, the nearest preferred value being $3.9\text{k}\Omega$.

Using yet another rule of thumb, R2 should be 10 times R3, which yields a value of $10 \times 1 k\Omega$, or $10 k\Omega$ in this case.

The base voltage is determined by the $V_{\rm be}$ for the transistor plus the emitter voltage. For a germanium transistor, $V_{\rm be}=0.2$ volts approx., so the base voltage required is 1.2 volts. The current through R1 is the same as the current through R2, since the base current, being very small, can be ignored. This current equals $\frac{1.2 \text{ volts}}{10 \text{k} \Omega}$, which is 120 microamps. Thus R1 should drop 9-1.2 or 7.8 volts at 120 microamps. R1 therefore equals $\frac{7.8 \text{ volts}}{120 \mu \text{A}}$, which is $65 \text{k} \Omega$ (use a $62 \text{k} \Omega$ preferred value).

The values of C1 and C2 hardly need calculating. Suffice to say that their reactance should be negligible at the lowest frequency to be amplified. An ideal value for each is $10\mu F$. The working voltage is determined by the collector voltage of the stage and the base voltage in the following stage—usually a 6 volt capacitor will be suitable. Note the polarity of these two capacitors.

C3 should also be chosen such that its reactance is small at the lowest frequency. Here a value of $50\mu F$ will be ample, but again, note the polarity.

Silicon Amplifiers

Using silicon transistors it is possible to obtain adequate temperature stability with a simplified circuit as shown in Fig. 2. The design procedure is even simpler

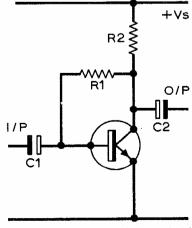
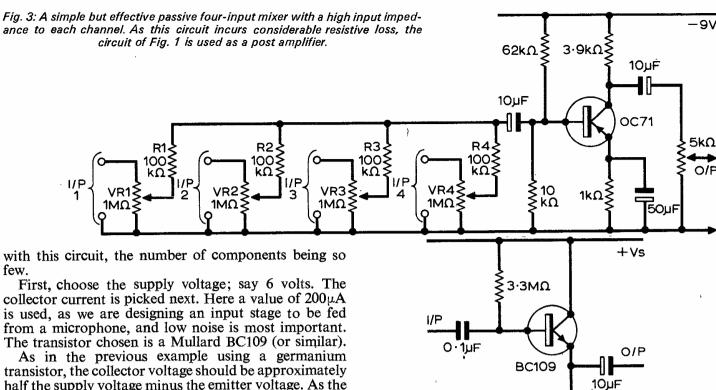


Fig. 2: A simple amplifier particularly suitable for a silicon transistor.



half the supply voltage minus the emitter voltage. As the emitter voltage is zero, the collector voltage should be

3V. R2 will therefore be equal to $\frac{3 \text{ volts}}{200\mu\text{A}}$

R1 is arranged to drop the collector voltage down to the level required for the base of the transistor. The base voltage needed here is equal to the $V_{\rm be}$ for the transistor, which is about 0.4 volts for silicon.

The base current required is calculated from the collector current divided by $h_{\rm fe}$ or beta for the transistor at that collector current. For the BC109, h_{fe} at I_{c} = 200 µA is typically 300, so the required base current is 200 µA which is 0.6μA. R1 is therefore equal to 300,

, which is $4M\Omega$. Allowing for somewhat lower h_{fe} values that may occur in production spreads R1 should be chosen as $2.7-3.3M\Omega$.

Using the Circuitry

3-0.4 volts

The circuit designed in Fig. 1 could be utilised in many ways. It could be used to amplify the signal from the detector of a tuner up to sufficient level to drive an earphone, in which case R4 should be replaced by a headset with a d.c. resistance of 4000 ohms. Alternatively, R4 may be left in circuit and driver and output stages added to drive a loudspeaker.

Another application could be as an audio mixer for several inputs, and the circuit in Fig. 3 shows such an arrangement. Resistors R1-R4 are included to reduce interaction between each of the mixer volume controls. The volume control at the output is the master volume control, and is effective over all inputs. By inverting the supply rail polarity, the circuit in Fig. 2 could be substituted for the OC71 amplifier stage.

High Input Impedance

Where a high input impedance is required such as for amplification of a gramophone pick-up output, an emitter follower can be used in front of the circuit in Fig. 2. This additional amplifier is shown in Fig. 4, and this will give an input impedance of approximately $2M\Omega$. This is because the input impedance of the Fig. 4: An emitter-follower which exhibits a very high input impedance and a low output impedance. Its voltage gain is fractionally less than 1.

15kΩ

transistor is almost equal to the beta or $h_{\rm fe}$ times $R_{\rm e}$. Input $Z=300 \times 15 \text{k} \Omega=4.5 \text{M} \Omega$. This is shunted by R1, which is $3.3M\Omega$, so the input

 $\frac{3\cdot3\times4\cdot5}{3\cdot3+4\cdot5}M\Omega=2M\Omega.$ impedance=

PRACTICAL GIFT FOR A PRACTICAL MAN

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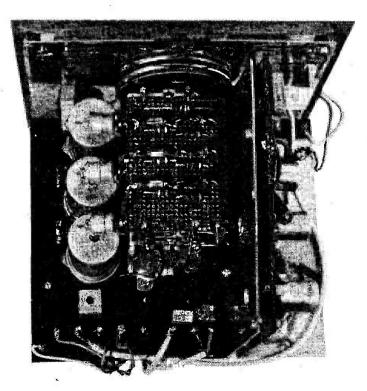
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A PANORAMIC RE



D.BOLLEN PART 1



PANORAMIC receiver provides a visual display of a band of frequencies when coupled to an oscilloscope, and this can be a useful aid to the serious short-wave listener or radio amateur. Signals appear on the oscilloscope screen as a series of resonance curves, of differing amplitude and character, spaced along the X-axis as though on a tuning scale. All signals are resolved visually without switching, whether they be a.m., c.w., s.s.b. or f.m., and the operator soon learns to distinguish between them. A quick assessment of general conditions on the band can be made without having to break off an existing contact on the main "shack" receiver. Thus, the need for searching by means of frequent manual retuning is largely eliminated.

Before semiconductors came on the scene, automatic "sweep" tuning of a receiver could only be accomplished by complicated arrangements of motor-driven tuning capacitors or reactance valve circuits, but now simple circuits based on the capacitance variation of semiconductor diodes when reversed biased are used.

The equipment described here employs ordinary, readily available components, and is designed for simple construction and low cost, to cover bands of frequencies up to 500kHz wide lying between 1.7MHz and 4.5MHz, which includes 160 and 80m.

HOW IT WORKS

Figure 1 gives the block diagram of the panoramic receiver. A conventional two transistor converter, involving three "gang" tuned circuits, is coupled to a 1.6MHz i.f. strip. An alternative arrangement is with the converter feeding a medium wave receiver which is tuned to 1.6MHz, thus achieving a double-superhet configuration. A voltage taken from the oscilloscope timebase simultaneously varies the capacitance of three diodes, each placed across one of the tuned circuits in the converter. At the same time, an output voltage is derived from the final i.f. detector diode for display on the oscilloscope Y-axis. If a continuous unmodulated carrier is received, the oscilloscope will show the overall response curve of the panoramic receiver, in the form of a single peak situated somewhere along the X-axis. Two plain carriers at different frequencies will appear side by side. The effects of modulation will be discussed later.

In practical terms, the small change of diode capacitance, compared with the main tuner capacitance swing, is quite sufficient to offer a useful "sweep". If an attempt is made to get a really wide panoramic bandwidth then signals will be too cramped on the display for easy recognition, and

CEIVER for 160 to 80 MINIETRES

"tracking" problems will arise. Under typical operating conditions, "sweep" bandwidths of less than 50kHz will offer an informative display, but the bandwidth obtained with the prototype receiver is continuously variable between zero and 500kHz on 80 metres, and zero to 100kHz on Top Band, which is sufficient for most requirements.

Although intended primarily as an accompaniment to an existing communications receiver, the panoramic receiver can be used on its own. Switching is included to stop the "sweep" and allow normal reception of an a.m. signal, either with headphones or via an amplifier and loudspeaker, as shown in Fig. 1.

The prototype receiver made use of a mixer and 465kHz i.f. strip taken from an old transistor portable radio. After careful peaking of the 465kHz i.f. transformers—made easy by the panoramic receiver display of its own response curve—excellent reception of signals was obtained, including s.s.b. when a b.f.o. was added.

Although, at first sight, the panoramic receiver would seem to involve quite a lot of constructional work, it will only be necessary to build a straightforward two transistor converter, plus a "sweep" tuner circuit panel consisting of a small collection of components, if a medium wave receiver and an inexpensive oscilloscope are already to hand. Even greater simplification results when the "sweep" tuner is fitted to an existing receiver.

DIODE CAPACITANCE

Virtually all semiconductor rectifier diodes exhibit junction capacitance, due to the depletion layer when reversed biased, and this capacitance varies with reverse voltage. Varactor diodes are specially manufactured to exploit depletion layer capacitance and to offer a good performance at very high frequencies. It is not generally realised, however, that ordinary silicon power rectifiers, as used for h.t. supplies, can also be employed as voltage controlled capacitors in circuits working at several MHz. The graph given in Fig. 2 shows the capacitance characteristics of four types of silicon rectifier. It can be seen that the characteristic of each diode is non-linear, and that maximum capacitance depends on the particular diode type. In nearly all cases, a capacitance variation amounting to some 50% of maximum junction

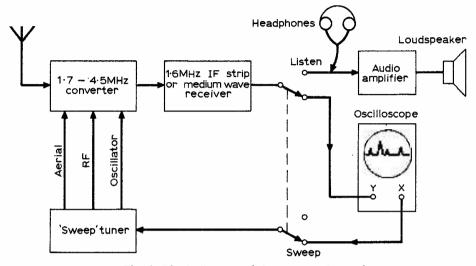


Fig. 1: Block diagram of the panoramic receiver.

capacitance is obtained when a reverse voltage of 10V is applied.

A single diode "sweep" tuner circuit serves to demonstrate how a rectifier diode can be linked to the tuned stage in a radio receiver (see Fig. 3). The tuned circuit, consisting of an r.f. inductor L1, a trimmer capacitor TC1 and a variable capacitor VC1, is coupled in parallel with the variable capacitance diode D1 via d.c. blocking capacitor C1. A re-

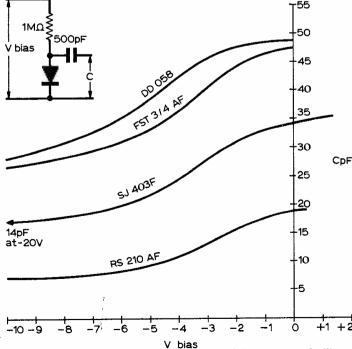


Fig. 2: The capacitance characteristics of four types of silicon diode.

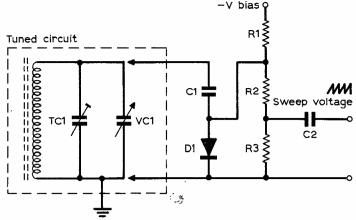


Fig. 3: A single diode "sweep" tuner.

verse voltage is applied to the diode by the potential divider formed by R1, R2 and R3. R1 and R2 have values of more than 1M ohm, to minimise loading of the tuned circuit. Approximately half the bias voltage will appear at the junction of R1 and R2, and the sawtooth timebase voltage, which is fed to R3 via C2, will cause the reverse voltage across the diode to "sweep" in sympathy with the oscilloscope X deflection, between zero and full bias conditions. It is important to avoid driving the diode into conduction by the application of too large a timebase voltage. Although no damage will result, a forward bias across the diode will lower the "Q' of the tuned circuit, and cause loss of gain. An interesting feature of the Fig. 3 circuit is that a small alteration of d.c. bias across the diode will change its capacitance, therefore, bandspread tuning can be accomplished easily merely by placing a variable resistor in series with R1.

The governing factor in the choice of a diode for receiver tuning is its zero bias capacitance. If the diode has a large capacitance it will seriously restrict the high frequency coverage of the receiver. On the other hand, if the diode has a small capacitance, the "sweep" bandwidth of the panoramic receiver will be correspondingly narrow. As a general rule, a zero

bias capacitance of about 10% of the maximum tuned circuit capacitance will be about right.

In the case of the 1.7MHz-4.5MHz converter used for the panoramic receiver, maximum tuned circuit capacitance is in the region of 330pF, calling for a diode capacitance of 33pF. Varactor diodes listed by well-known suppliers fall outside the required capacitance value, being either too large or too small, but a wide choice of rectifier diodes exists. The A.E.I. type SJ 403F was found to be ideal, having a zero bias capacitance typically of 34pF, falling to some 14pF with a reverse voltage of 20V, see Fig. 2. If difficulty is experienced in obtaining the SJ 403F, there is no reason why other types should not be tried. A diode can be checked for zero bias capacitance value by connecting it, in series with a fixed mica capacitor of about 500pF, across the terminals of a capacitance bridge. The aim should be to find three diodes, preferably of the same type, which have a nearly identical capacitance value falling close to 33pF. In practice, anything from, say, 25pF to 40pF can be deemed usable in the panoramic receiver.

The converter circuit of Fig. 4 is designed around Denco transistor tuning coils and n-p-n silicon transistors. Coils T1, T2, and T3 are intended for use with a 310pF+310pF+310pF tuning capacitor and 30pF trimmers. Padder capacitor C7 in Fig. 4 serves to give correct tracking between oscillator and other stages.

Denco 3T coils normally cover the range 1.7MHz to 5MHz, but the addition of extra diode tuner capacitance to the tuned circuits in the converter will lower the upper frequency limit to 4.5MHz, without otherwise affecting performance.

In Fig. 4, the aerial coil T1 is tuned by VC1. A signal is amplified by r.f. stage Tr1 and is then passed to the secondary winding of T2. T2 is tuned by VC2. Self-mixing oscillator Tr2 converts the signal to 1.6MHz, and the oscillator coil T3 is tuned by VC3. I.f. transformer IFT1 provides the correct matching impedance to the base of a following tran-

components list

Resisto	ors:	Transistors:	Capacitors:
R1	18kΩ	TR1 \ 2N2926 (orange	C1 0.05µF
R2	6·8kΩ	TR2 spot)	C2 0·01µF
R3	2·7kΩ	Diodes:	C3 0.05, E
R4	18kΩ	D1)	C4 0.033 µF polyester 250V
R5	6·8kΩ	D2 >SJ403F (see text)	C5 0·01 μF
R6	2·7kΩ	D3	C6 0·01μF
R7	1kΩ	Switch:	C7 340pF polystyrene 125V ±2½%
R8	470Ω	S1 Four-pole three-	C8 0·1 μF polyester 250V
R9)	way rotary	C9 470pF)
R10		Coils and transformers:	C10 470pF \Rightarrow polystyrene 125V $\pm 2\frac{1}{2}\%$
R11	2·2MΩ	T1 Blue	C11 470pF
R12	2.210122	T2 Yellow ≻Denco 3T	C12 0·1 µF polyester 500V
R13		T3 White	VC1/VC2/VC3 Jackson type E3 310pF+ 310pF+
R14	J	FT1 Denco IFT 16/1·6	310pF
R15	560 k Ω		TC1
VR1	1kΩ carbon lir	near pot.	TC2 >30pF Philips concentric airspaced.
VR2	25kΩ carbon l	inear pot.	TC3
VR3	100k Ω carbon	ı linear pot.	Miscellaneous:
VR4	$1M\Omega$ miniatur	e skeleton pre-set.	Jackson SL16 scale drive assembly. Bias battery
All fix	ced resistors ½W	/, 10%.	type B122. S.r.b.p. sheet 7in. \times 5 $\frac{7}{8}$ in., turret tags,
			0.1 in. matrix Veroboard or plain drilled s.r.b.p.
			21 × 30 holes, matrix pins, 18s.w.g. aluminium
			plate 7 in. \times 2½ in.

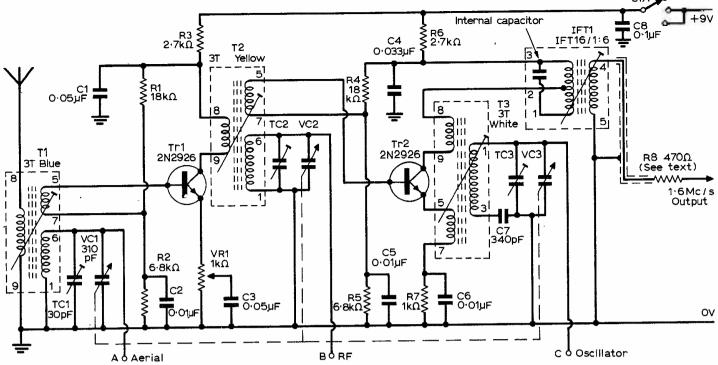


Fig. 4: The 1.7 to 4.5MHz front-end. This is a simple tuner designed around Denco coils.

sistor stage in a 1.6MHz i.f. strip, or a mixer in a medium wave receiver. Methods of coupling the converter to following stages will be outlined later.

To prevent instability, the r.f. stage in Fig. 4 is decoupled by R3 and C1, and the mixer by R6 and C4. C8 decouples the +9V supply line. VR1 is included to allow adjustment of r.f. gain, so that an optimum signal-to-noise performance may be achieved. The purpose of resistor R8 will be explained later.

THREE-GANG diode tuner

In the diode tuner circuit of Fig. 5, d.c. bias for the diodes is conveniently supplied by a small, longlife 22.5V battery. Diode and bias polarities are so arranged that a left to right timebase sweep will give high frequency signals on the right-hand side of the display. VR2 and R15 form a potential divider, and VR2 acts as a bandspread control, giving deviations of the order of $\pm 15 \text{kHz}$ at 3.4MHz, and just a few kHz at 1.9MHz. Short-term frequency stability of the diode tuner, when switched to "listen" is sufficiently good to allow s.s.b. signals to be easily resolved with the aid of a b.f.o.

Each diode in Fig. 5 has its own potential divider, formed by the 2·2M ohm bias resistors R9-R14, but the dividers are connected to earth via a common resistor, formed by the track of potentiometer VR3. Thus, while each diode is individually d.c. biased, and is isolated from other diodes by the high value of divider resistors, a sweep voltage injected into VR3 will swing all three diodes simultaneously. Capacitors C9-C11 couple the diodes to the tuned circuits in the converter.

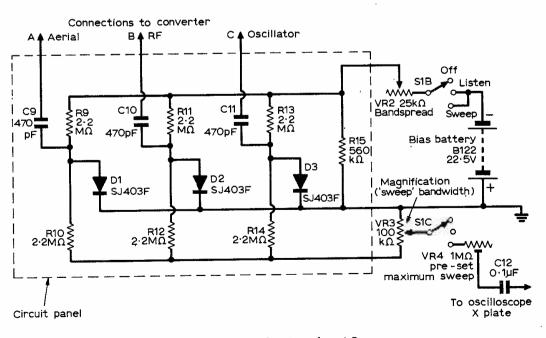


Fig. 5: The "three gang" diode sweep tuner, Sections A and B swing the r.f. tuned circuits T1 and T2 in Fig. 4, and section C sweeps the oscillator T3.

The oscilloscope timebase sweep voltage is fed to the diode tuner via C12 and VR4. VR4 serves to pre-set the maximum sawtooth peak voltage when VR3 is set for minimum magnification (maximum sweep bandwidth), and will cater for typical oscilloscope X-plate voltages of 100V-400V. As the slider of VR3 is moved towards the earth rail, a signal peak at the centre of the display will be expanded, i.e., magnified, until it fills the screen; this facility is useful for a close examination of adjacent signal heterodyne interference, as well as various transmitter modulation defects.

Part 2 next month:
Construction, alignment and use.



MONTHLY NEWS FOR DX LISTENERS

To is my intention to devote as much space as possible to news and logs sent in by readers of this column. Several logs were received this month and they have been included in this article.

If you have any news or loggings which you think would be of interest to your fellow-readers you should send them to PRACTICAL WIRELESS by the 14th of each month or to my home address: 58 Kensington Gardens, Ilford, Essex, by the 17th. It would be helpful if you could enclose a list of the equipment you use as this helps people to make a comparison between your logs and their own results.

Readers' Logs

John W. Smith, of Anstruther, in Fife, sent in the following items from his log:

11,770: Radio Nigeria in English from 1900 to 1930.

15,080: Radio Euzkadi, clandestine, in the late evening.

15,155: Radio Dif. de Sao Paulo at 2320.

He also reports that *Radio Denmark* transmits its European Service from 1030 to 1115 (Saturday-Sunday) instead of 1015-1100. The frequency is still 9,520 and the "DX Window" programme will be broadcast at 1045 on Sundays.

Mr. H. Wood, of Manchester, sent in these news items:

Canada: The new autumn schedule of the CBC is 0715-0745 on 9,625 and 5,990, 1217-1313 on 15,325 and 2115-2152 on 11,720, 15,325 and 17,820. All times and frequencies refer to the European Service.

Netherland Antilles: The Radio Nederland transmitter at Bonaire is now using the frequency of 9,715 from 0800 to 0920 and from 0500 to 0620.

Roy Patrick, of Derby, sent in these interesting items.

Andorra: The English Service of Radio Andorra is from 0100 to 0200 on Saturday mornings (according to my information, Roy, it is from 0000-0100 GMT). Roy also lists the shortwave outlet as being inactive.

Canada: CHNX has been logged by Roy on 6,130 around 0100 with a fair signal.

According to Radio Canada the plan to replace the 50kW transmitters with ones of 250kW has been dropped. (This is due to the Government's recent austerity economy measures.—MC.)

Luxembourg: The shortwave outlet of Radio Luxembourg on 6,090 will increase its power to 500kW early next year.

S. Arabia: Roy has heard an English newscast from this country at 1700 on 11,855 but has not been able to hear it since.

Africa

Biafra: The Voice of Biafra continues to broadcast on 6,144 from 0455 to 0200 whilst Radio Biafra

Times Frequencies in GMT

THE BROADCAST BANDS

Malcolm Connah

uses 7,307 from 0430 to 2230. The two stations do not use parallel programming.

Asia

Cyprus: The Cyprus Broadcasting Corporation has resumed its shortwave transmissions. The station broadcasts at 1900-2105 Monday to Saturday on 15,260 and at 0900-1600 on Sundays on 17,875. The Corporation is very interested in receiving reports from listeners.

Korea: Radio Pyongyang has a new frequency of 9,613 for its English transmissions at 1900-2000 which are beamed to Europe, Africa, the Near and Middle East.

Europe

Andorra: The English Service of Radio Andorra on 701 and 5,995 is now scheduled for 0000-0100 on Saturday mornings but there is no sign as yet of the shortwave outlet.

Austria: Radio Austria's DX programme is broadcast every second Sunday at 1915 on 6,135, 9,610, 11,925 and 15,210.

Belgium: The English programme "Belgium Speaking" is broadcast at 2205-2215 on 9,550, 9,660 and 11,715 and at 0050-0100 on 6,125, 9,660 and 11,715; 9,660 is a new frequency for this broadcast.

Germany: One of my German colleagues informs me that Europe's most powerful shortwave transmitter will be built at Mindelheim, West Germany. The transmitter will beam programmes to all parts of the world during the Olympic Games at Munich. Six hundred announcers will inform sports fans all over the world about the Games in twenty-eight languages.

Great Britain: The Sunday broadcast of the BBC's "World Radio Club" programme is now broadcast at 0815 instead of 0930.

Sweden: Due to interference problems *Radio Sweden* is altering the frequency of its broadcasts to Eastern North America from 9,710 to 5,990. This change concerns the English, Swedish and Spanish programmes broadcast between 0000 and 0230.

South America

Colombia: Emisora Atlantico, Barranquilla (HJAG) which is listed as inactive in the World Radio-TV Handbook is now operating on 4,905 until sign-off at 0500 with a power of 10kW.

Ecuador: HCJB, The Voice of the Andes, uses two new frequencies of 15,415 and 17,780 for its programmes from 1845 to 2030.

Nicaragua: Radio Nacional de Nicaragua can be heard in Europe after 0100 on the new frequency of 11,875.

73's and good DX until next time.

THE AMATEUR BANDS David Gibson, G3JDG

VERY good month for the DX hounds, but not too satisfying for those who only listened on 120 metres. This band, although, perhaps, the main DX band for many, has put on its winter overcoat of fading and is usually rather dead in the evenings

The l.f. bands are beginning to come into their own and there has had been a noticeable improvement.

especially on 40 and 80.

Topband has helped to inspire its followers by allowing a few American c.w. signals across the pond and this is very heartening for topband transatlantic enthusiasts. Listen early mornings down the

I.f. end for these sigs.

Honours this month go to 10 metres which played host to a very large number of signals throughout the month. Twice when your scribe's ears flapped over the 28-29.7MHz segment, four of the continents could be heard during the same session. It's quite surprising how many a.m. signals are loose on this band as compared to, say, 14MHz where sideband mostly dominates. The majority of the 10 metre signals were romping through at \$9 too, so don't forget to keep an eye on this band whenever you switch

Two sharp-eyed correspondents have drawn my attention to the G3RPE/P F2FO/P contact made on 10,000MHz. Alas, my "red spot" transistors don't function up that far, but congrats to both operators on a very fine achievement! Who knows, now that the amateurs have shown that it's possible, the professionals may decide to have a go.

Just to be different, let's take a look at the happenings for the month when all good Christmas puds are stirred. Four main events down in my diary are: 6th-7th December, 80 metre c.w. contests; 6-7th, CHC International c.w. contest; 7th, 4 metre c.w. contest; 13th-14th, CHC international s.s.b. contest.

Don't forget that on Christmas morning there will be a large number of "local" club nets on the go. Topband is a favourite for these and some are quite witty. Certainly they all provide good festive r.f. entertainment. G3JDG promises to erect a reasonable antenna for topband on that morning and rude remarks concerning signal strength and mod. from over 25 miles would be appreciated.

So, where's it all been happening? Well, Charles Morgan (Northumberland), had great success on topband. Between 0430 and 0630 he logged K1PBW (599), KV4FZ (579), VP9GJ (459), W1BB/1 (599), W2EQS (359), W2IU (499). Figures in brackets are standard RST reports and all signals were c.w. Frequencies to listen from band edge to 1,805kHz.

If you are still unconvinced that the l.f. end of the spectrum is worth a listen, how about the log from R. Bagwell (Surrey). He runs a Trio 9R59DE with a PR30 pre-selector, an RQ10 and a switched attenuator fed by an a.t.u. which in turn squints down a 70ft. long wire. Eighty metres revealed—CN8AW, HV3SJ, JW1CI, JW3KJ, VE1IE, PY7ASQ, PY7GV, TF5TP, VO1CW, VU1AX, 3V8NC, 3Z3BLG (new prefix for Poland) 5A2TR, all on s.s.b.

Philip Lawson (Derby), has an Ekco domestic receiver and sends in a long log bearing evidence of high Eu activity on 80 with the majority of stations at S8-9, so there's plenty of stations on the band.

John Moore (Leicester), hasn't done too well on topband mainly due to high noise level with similar remarks for 80, although he did log XE1KB at 0615 and says that W's are beginning to show on 75 metres around this time.

Higher up on good old 20 the stalwarts managed to pull in some good DX sigs even with the band closing in the evenings.

Trevor Rumble (Wilts.), has an HA700 plus PR3OX and a 100ft. long wire. Twenty s.s.b. between 0720 and 0755 produced some good openings to Australia and stations logged included—VK2ID, VK3MO, VK3RZ, VK3ŬJ, VK5AX VK7PR and ZL4BX at 5 and 9 plus 10dB. VK5AX, VK6FB,

Fifteen metres was the band for Stephen Randall (London), whose 9R59DE and 110ft. long wire produced r.f. music from s.s.b. types like—CR6LVC CT1BF, CX2SA, EA3RF, EP2CB, JA2JAW, JA9AGP, JH1ODO, KP4AST, KZ5IT, LA7XM, TZ5CJT, VE3OSC, VU1FA, VK2ZQ, VK7AZ, VP2ME, WA9NSR/P1, YV4UA, 4X4FQ, 4Z4HF, 5A2AAF.

Glyn Richards (Isle of Wight), is still the only 2metre fan who writes in. What about it, all you v.h.f. types? Glyn runs a JXK converter into a Mohican receiver used as an i.f. strip. Although his antenna is only 6ft. of wire, still the signals come in on 2. Examples include—G3CLW (Paignton) and G3MCS (Aylesbury), F5NS (near Normandy) and G3GZJ (Redruth), the latter station being some 120 miles

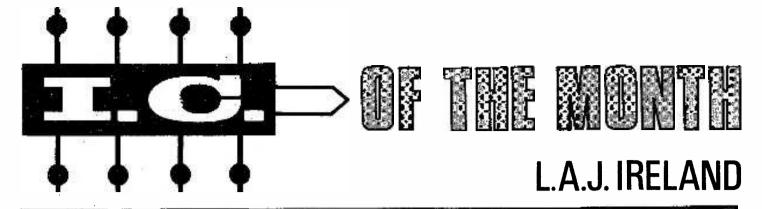
On to the top of the pops for this month, the one and only—10 metres. John Moore (see earlier) logged these on s.s.b.—CR6AG, CR6GM, CR6LF, CR7LX, DU1FH, ET3USA, HK4DF, K8YBU, KØSFU, KP4DGX, LU3DD, LU4BH, MP4BHC, MP4BHR, OD5BA, OD5BZ, PY2DVH, UA9TT, VE2DHF/P/YV1, VE3CI/W4, VE3ABS, VP5AA (Caicos Is.), VP8KD, VP8KL. VQ8CV (Mauritius). VS6DR, VU2DK, VU2XX, VU2BEO, W2CRW, W4IQS, WA5SDT, WA8SWV, WØIMC, XW8AL, YV4UA, YV5CIL, ZC4AK, ZE1BP, ZE1JE, ZE3JJ, ZE6JN, ZS2GP, ZS4AA, 4X4UF, 4X4YP, 5H3KJ, 5H3LV, 5N2AAF, 8P6CX, 9J2DT, 9J2VX.

Nicholas Richardson (Bucks), has a CR7OA and PR30. Together with a 40ft. long wire at 18ft. they produced—CT1OF, K8ASM, KV4AD, OD5RZ, PY1MT, PY3GS, UA3NUE, VE2AIH, VE3WY, YV5BX, ZE1CE, 5B4EZ all on s.s.b.

On a.m., Nicholas managed—CE2JA, CR7FM, LU5XE, SV1CX, UA3AFA, UA6OJ, UA6ARA, UB5FAQ, WB4KJF, ZE1BR, 9H1BG which is pretty good going.

Ian Wadman (Berks) reckons that the JGD earholes should be alert on 10 metres on Sunday afternoons. Ian sends news of great activity around this part of the day. Ian logged CR7EZ, K4BG, OD5BZ, UW4II, ZE1JE, 4X4GB, 5N2AAF. All these with a CR70A and 70ft. long wire.

That's it for this year! Vy Mx OM's es benu in 1970. Address for logs is 5 Edward Close, St. Albans, Herts, and the deadline is that they must reach me by the 18th of the month.



Number 3

The PA424 and PA436, power control circuits

NY definition of electronics today would have to include among its applications not only computation and communications, but also control circuits. More and more mechanical and even electromechanical control systems are being replaced by all-electronic methods, and this month we shall see the initial contribution of integrated circuits to this process. The key device in the development of electronic control circuits is, of course, the silicon controlled rectifier (S.C.R.) in which the device operates as a diode only when a pulse is applied to a gate electrode. Following this event, the device conducts only as long as the voltage applied to it retains its proper polarity. In a.c. circuits, therefore, a separate pulse is required to initiate conduction in each cycle.

For full wave operation, two S.C.R.s are required, though these may take the form of a single bidirectional silicon controlled switch or TRIAC. To maintain conduction in a TRIAC 100 pulses per second are required, one to initiate conduction in each positive and negative-going half-cycle of the waveform. If these pulses are applied simultaneously with the beginning of each half-cycle of an a.c. waveform, the device behaves as a short-circuit, and current flows in exactly the same way as if the device were absent from the circuit.

If, however, the pulse is delayed relative to the start of the half-cycle, no current will flow in the interval, and the total power delivered to the load will be reduced by an amount dependent on the extent of the delay. Obviously, then, if a control system delays or eliminates pulses from the gate circuit of an S.C.R. or TRIAC, the output power is dependent on the control system. And this is where our I.C.s come in.

Many situations requiring power control can be sensed or measured electronically, for example temperature by a thermistor, illumination by a photoconductor, or even pressure by a strain gauge. Control is then exercised by relating transducer output to timing pulses in a TRIAC gate, limiting the power supplied to a heater, lamp, or pump. Two suitable I.C.s for the job are the General Electric types PA424 and PA436.

First the PA424. This unit is described as a zero voltage switch, and acts as a combined threshold detector and pulse generator. The signal from the transducer is compared with a preset internal voltage using the differential amplifier Tr1 and Tr2. If the threshold is not exceeded, pulses are generated and applied to the TRIAC; otherwise pulses are inhi-

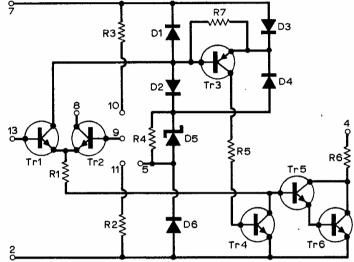


Fig. 1: Circuit of the PA424 'zero voltage switch'. The device is supplied in a 14-lead dual in-line plastic package.

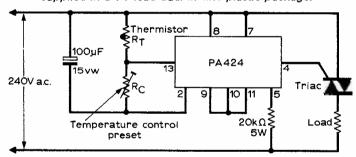


Fig. 2: Application circuit for the PA424. Rt is the thermistor and Rc the temperature control preset.

bited and the TRIAC will not conduct. This circuit, then, acts as a go/no go control; to some extent this is a limitation, in that the circuit controlled is either fully on or shut off.

In practice this is only a slight problem, since in heating systems, for example, the sensitivity of a thermistor/PA424 combination is such that the temperature is held to within a fraction of a degree of the chosen value by the automatic succession of periods off and at full power. Further, as all the pulses occur at the instant of crossover between positive and negative-going half-cycle of the waveform. (hence the name "zero voltage switch") there is no question of repetitive switching of appreciable currents, a factor which can produce r.f. interference in some power control circuits.

One obvious advantage of the PA424 is that it serves as its own d.c. power supply; the application

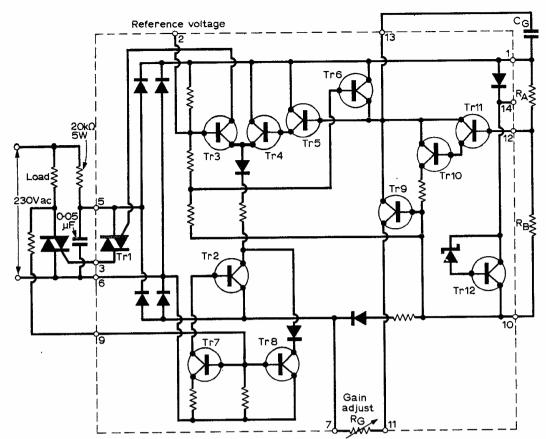


Fig. 3: Application circuit for the PA436, phase control trigger circuit.

diagram shows it in operation directly off the power line without a separate transformer. This is an obvious contribution to economy. In a negative-going half-cycle D1 conducts, charging C1, which supplies d.c. for the remainder of the cycle. As pin 5 approaches zero volts, the output Darlington pair, Tr5 and Tr6 begin to conduct, thereby applying a pulse to the TRIAC gate, unless Trl happens to be conducting. In this case, Tr3 is also conducting, and Tr4 saturates, shunting the base input to Tr5 and inhibiting the pulse. The internal resistors R2 and R3 are available as one arm of a bridge circuit, the other being the thermistor (in heating applications) and a preset potentiometer. The ingenuity of the reader will indicate analogous transducer circuits for the control of other systems, such as those already mentioned.

The other device for our consideration this month is an actual phase controlling trigger circuit. It actually delays the triggering pulses required by the TRIAC to the extent determined by the transducers employed, and in some cases this feature is well worth the slightly higher price. Again, the power for the operation of the circuit comes directly from the mains, and a minimum of external components leads to further convenience and economy. The d.c. from the internal bridge rectifier is regulated by a zener diode and a reference voltage produced at pin 2. As in the PA424 there is a differential amplifier (here Tr3 and Tr4) to compare reference and transducer levels and hence control the pulse output.

One of these is modulated with a time-dependent voltage built-up across the external timing capacitor, and hence the variable delay in pulse generation. The rate of variation of this time-dependent modulation depends on Rg, which therefore acts as a sensitivity control for the system. The actual output pulse is obtained by discharge of the external capacitor C1 through a low current, low voltage TRIAC, Tr1, integrated into the PA436.

APPLICATION DATA, TYPE PA436

Choice of which I.C. to

use in any particular situation requires some consideration. In heating circuits, for example, it will not be immediately obvious whether the element is conducting at any instant,

provided overall thermal regulation is satisfactory. With lighting, we are all aware that the action of

the a.c. mains in incan-

quite a satisfactory light, and there is no objectionable flickering; however, this can occur under certain conditions with a PA424 controlled lamp, as the I.C. causes "off" periods much longer than the normal a.c. cycle. Similar considerations lead to the selection of the PA436 true proportional controller in a few other

specialised situations, but

in general the PA424 is advised, for its greater

lamps provides

descent

 $\begin{array}{ccc} & \textit{Minimum} & \textit{Maximum} \\ \text{External gain controls Rg} & 7 \cdot 5 \text{k} \Omega & 100 \text{k} \Omega \\ \text{Cg} & 0 \cdot 01 \mu \text{F} & 0 \cdot 1 \mu \text{F} \\ \text{RA} + \text{RB} & 10 \text{k} \Omega & 200 \text{k} \Omega \end{array}$

R_A and R_B: external control resistors (one may be a transducer, e.g. thermistor, photocell, resistive vacuum gauge etc.).

For temperature control systems R_A is a thermistor of resistance about $5k\Omega$ at the controlled temperature: R_B is a preset of $20k\Omega$.

The integrated circuits PA424 and PA436 are available from

Jermyn Industries, Vestry Estate, Sevenoaks, Kent; or Neltronic Ltd., 14 Wellington Park, Belfast BT9 6DJ.

simplicity and economy, not to mention its "cleaner" r.f.i.-free operation. At any rate, control systems will become much more elegant with the elimination of slow bulky relays, with the associated difficulties of burnt contacts and general unreliability.

N.B. Just before going to press we have learnt from the suppliers of the PA436 that problems in manufacture have led to a temporary withdrawal of stocks. Newer versions using the same type number will be available in a few months but these are only capable of handling 150mA instead of 2A. Constructors should take careful note of the instructions supplied with this device which may modify certain parts of the above article.

BLUEPRINT SERVICE

We would like to draw readers' attention to the fact that the BLUEPRINT SERVICE has been discontinued and therefore no further BLUEPRINTS are available.

beginner's PORTABLE RECEIVER

C.R. BRADLEY

A LMOST all radio constructors have memories of unsuccessful first attempts. Beginners are faced with a wide selection of designs and often make the mistake of choosing one that is too advanced for their nascent capabilities, or alternatively, one whose extreme simplicity leads to a disappointing performance. This portable radio design is intended for the beginner and aims to fulfil the following requirements:

1. The circuit must be straightforward and trouble

free. The radio is a six transistor superhet on conventional lines.

2. Performance must be good enough to repay the builder's efforts. In fact, performance of the radio is comparable with commercial portables. Alloy diffused transistors provide high gain in the mixer and i.f. stages, and the audio quality from the transformerless complementary output stage is especially good. No external aerial or earth is required.

3. All components must be immediately obtainable so that there will be no necessity to choose substitutes. To this end a matched kit of miniature coils and tuning capacitor is specified in the parts list. A packaged set of matched semiconductors is used for the audio stage. The remaining components are easily found, everything is available from advertisers in Practical Wireless.

4. Construction must be simple. The circuit is wired on a small piece of Veroboard using a suitable miniature soldering iron. There is a good prospect of the radio working "first try" provided normal precautions are taken in construction, i.e., insulated sleeving used where required to avoid shorts between closely mounted components, and correct identification of transistor, diode and electrolytic capacitor leads.

The Circuit

The circuit is shown in Fig. 1. The ferrite bar aerial L1 is tuned to the desired station by VC1 and

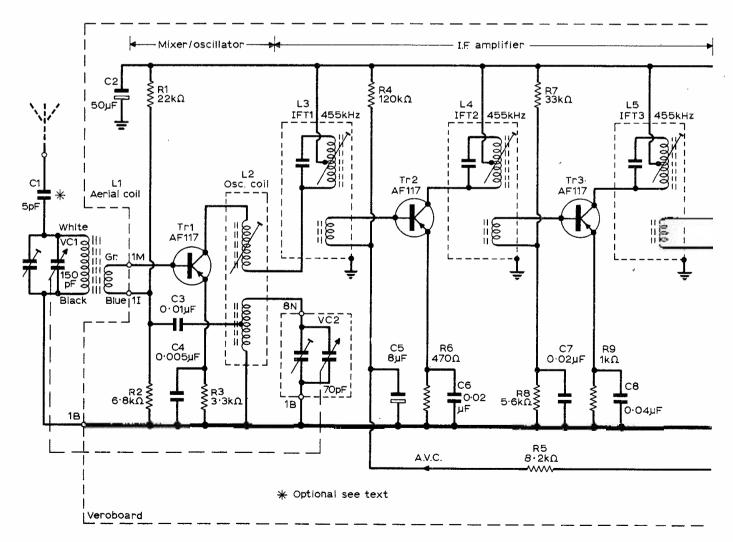
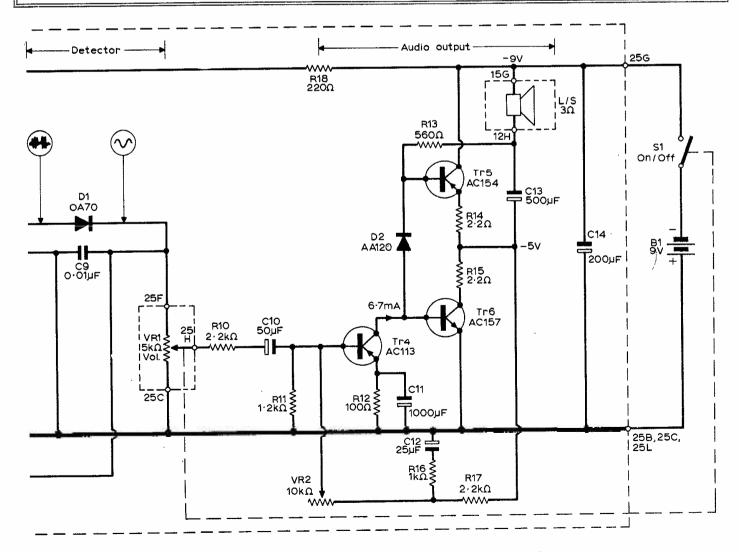


Fig. 1: The mixer/oscillator and i.f. stages, followed by the detector and audio stages. Note that the value of C6 should

components list

	rs: $ 22k\Omega \qquad \qquad \text{R10} 2\cdot 2 \\ 6\cdot 8k\Omega \qquad \qquad \text{R11} 1\cdot 2 \\ 3\cdot 3k\Omega \qquad \qquad \text{R12} 100 \\ 120k\Omega \qquad \qquad \text{R13} 560 \\ 8\cdot 2k\Omega \qquad \qquad \text{R14} 2\cdot 2 \\ 470\Omega \qquad \qquad \text{R15} 2\cdot 2 \\ 33k\Omega \qquad \qquad \text{R16} 1k\Omega \\ 5\cdot 6k\Omega \qquad \qquad \text{R17} 2\cdot 2 \\ 1k\Omega \qquad \qquad \text{R18} 220 \\ 5k\Omega volume control with swith $	Tr5 AC154 Thorn Tr6 AC157 LP15 Tr6 AC157 package D1 Germanium detector diode, e.g.: OA70, OA79,
	sistors ¼W 10% unless indica	Miscellaneous:
Capaci C1 C2 C3 C4 C5 C6 C7 C8 C9 C10	tors: $5pF$ ceramic (optional) $50\mu F$ 10V electrolytic $0.01\mu F$ (10,000pF) ceramic $0.005\mu F$ (5,000pF) ceramic $8\mu F$ 6V electrolytic $0.05\mu F$ (50,000pF) ceramic $0.02\mu F$ (20,000pF) ceramic $0.04\mu F$ (40,000pF) ceramic $0.01\mu F$ (10,000pF) ceramic $50\mu F$ 6V electrolytic $100\mu F$ 6V electrolytic	L5 I.F.T.3 "C"



have been shown as $0.05\mu F$ and C11 as $100\mu F$. The Veroboard circuitry is indicated by the dotted enclosure.

the radio frequency signals induced in it are fed to the base of Tr1. Base bias current for Tr1 is provided by R1 and R2. C3 couples Tr1 base to a tapping on the oscillator coil L2, and Tr1 therefore oscillates at a frequency tuned by VC2. The radio frequency is mixed with the oscillation frequency in Tr1 to produce a difference frequency known as the intermediate frequency. VC1 and VC2 are ganged together to maintain a constant i.f. (about 455kHz) as VC1 is tuned over the whole tuning range (medium waveband). The importance of this is that subsequent stages can be tuned by their coupling transformers for maximum gain at one frequency only. Tr2 and Tr3 amplify the i.f. signal and are coupled by single tuned i.f. transformers i.f.t.1, i.f.t.2 and i.f.t.3. The AF117 transistor used for Tr1, Tr2 and Tr3 is an alloy diffused type with a low feedback capacitance (2-3pF). We can therefore dispense with the neutralisation components normally needed to maintain stability with the OC44/OC45 junction type transistors which have a higher internal capacitance, and have a higher i.f. gain.

The amplified i.f. signal appears at i.f.t.3 secondary. It is rectified and smoothed by D1 and C9 to isolate (detect) the audio envelope—see waveforms in Fig. 1. A portion of the audio signal is picked off by R5 and fully smoothed by C5 to provide automatic volume control to Tr2 base. If a strong signal is tuned in, the resulting positive a.v.c. voltage returned to Tr2 base reduces the transistor's gain and overloading of subsequent stages is avoided. The a.v.c. compensates to some extent for fading signals and the signal variation caused by moving the radio from place to place. When a weak station is received, there is no a.v.c. feedback and all stages work at full gain.

The audio signal is applied across volume control VR1 whose slider feeds audio driver transistor Tr4. The amplified signal at Tr4 is direct coupled to the base of complementary symmetry output pair Tr5/Tr6. The voltage drop across D2 is fairly independent of battery voltage and maintains the small no-

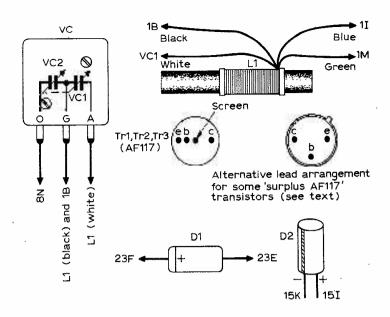


Fig. 3: Lead identification of various components.

signal bias current to Tr5/Tr6 needed for minimum distortion. Tr6 (n-p-n) and Tr5 (p-n-p) are turned on by positive and negative voltage swings respectively. The transistors drive the loudspeaker in pushpull; each supplies current alternately through C13. This arrangement provides a very low output impedance which permits the circuit to drive the speaker directly without an output transformer. D.C. feedback for stability and a.c. feedback for improved audio quality are provided by R17 and VR2. VR2 is preset to give a no-signal voltage of -5V at the junction of R14 and R15.

The audio output power is about $\frac{1}{2}$ watt. With a 7 × 4in. or larger loudspeaker, volume and clarity are more than ample. The radio is best built in a non-miniature cabinet for best audio quality. But the circuit board is small enough to be incorporated in a pocket size radio in which case a 2in. loudspeaker could be used.

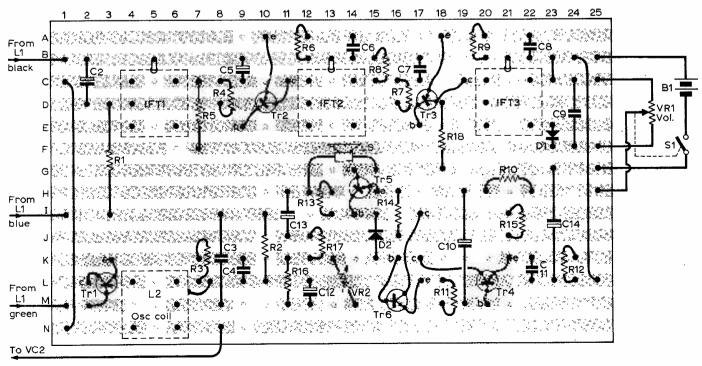


Fig. 2: Veroboard layout viewed from the copper side.

Construction

The components are wired on a standard piece of Veroboard and the layout is given in Fig. 2. The numbers and letters provide a cross-reference for each hole. The top and bottom copper strips (unlettered) are left unused for possible use in mounting the Veroboard in the cabinet.

First cut the Veroboard strips as shown, preferably with the Vero cutting tool. There are 36 breaks in all. It is advisable to mark (say) the top left-hand corner of the board before starting for identification. Wiring is easier if the positions of the components are sketched on the top of the board with a fibre-tip pen. Identify the three i.f.t.s ("A", "B", "C") and oscillator coil L2 ("O") in the coil kit. Bend up the screening can lugs. With slight persuasion the coil pins will make a neat fit in the Veroboard holes in the positions shown in Fig. 2. Solder them in place. It may be noticed that the lefthand pair of pins on the oscillator coil L2 in Fig. 2 are connected oppositely to the manufacturer's data with the coil kit. The author has decided the data is incorrect as the stage will only oscillate with this way of connection, with the coils sampled at least. However, if the mixer subsequently refuses to oscillate, it is easy to try swapping the connections at 2L and 1N to agree with the manufacturer's data. Short pieces of wire are used to earth the screening cans of L2, i.f.t.1, i.f.t.2 and i.f.t.3 to holes 8L, 5B, 13B and 21B respectively. Resistors and capacitors are next mounted with the shortest possible lead lengths, mostly upright. Put a piece of plastic sleeving on the lead from the top of each component wherever there is any danger of it touching any adjacent metal. This is particularly likely if bare metal-cased electrolytic capacitors are used. Electrolytic capacitors must be wired the right way round, i.e., positive lead to earth (except C10 and C13). Finally, solder the diodes and transistors to the board, making sure the leads are identified correctly from Fig. 3. Note that the lead identification of D2 can be misleading. Some surplus transistors marked AF117 were tried by the author and worked satisfactorily; however the lead arrangement was non-standard for AF117 (see Fig. 3) and they

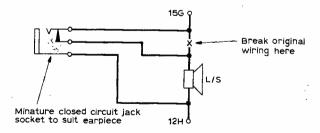
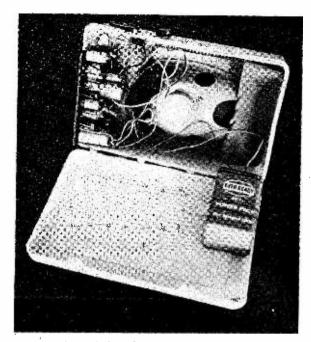


Fig. 4: Adding a socket for a low impedance magnetic earpiece.

had no screen lead. The screen lead of the AF117 has little use at the frequencies used here and can be cut short or connected to the nearest earth point as preferred. Leave about $\frac{1}{2}$ inch of sleeved lead on all transistors and diodes and solder as quickly as possible to avoid heat damage.

The cabinet for the author's prototype was a Woolworth's plastic lunch box. The top of the box carries the tuning capacitor, volume control VR1 and



Internal view of the completed receiver.

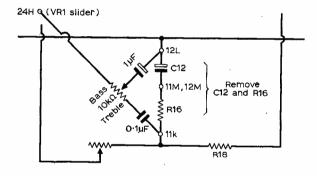


Fig. 5: Adding a bass/treble tone control.

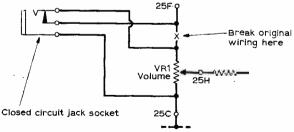


Fig. 6: Adding a socket for microphone, guitar, record player etc.

the ferrite aerial is taped underneath. The calibrated knob supplied with VC is rather small and a larger disc of plastic glued to it would make tuning easier. The 7×4 in. loudspeaker is mounted in the side of the box and the aperture is covered with Tygan speaker fret. The largest 9 volt battery the cabinet

-continued on page 706

practically wireless HENR commentary by

Spin-off

IX hundred million people, we are told, watched Neil Armstrong plant his foot in the moondust on 20th July, 1969—the day that President Nixon, begging a few questions, described as '... the greatest since Creation'.

You have had time to simmer down since then; to consider the equally stupendous achievement of discovering that Mars has no little green men paddling along its canals. And perhaps join a disgruntled chorus who were muttering, even as the Eagle took flight, that the 24,000,000,000 dollars might have been better spent on child welfare, cures for cancer or ear - muffs for under - privileged ocelots.



"... ear-muffs for under-privileged ocelots."

In answer to these mutterings the science-bent will usually say something about the spin-off. Non-stick aluminium frying pans often find their way into the conversation.

"And it took 300,000 technicians eight years to produce a non-stick pan?" someone is bound to ask.

Well, there is more to it than that. Many of the technical innovations creeping into our lives had their origins in space research.

You need look no farther than

the flip-chips that are occupying our editorial wizards at present. How do you think contributors could continue to dream up ten different ways of constructing an electronic shoehorn * † without integrated circuits to save them from repetitions? Only recently I sat in a high-level quorum who wanted to know how the advent of IC designs would affect serviceability. And had to admit that my own opinion was for a shift in emphasis, no more. I cannot see the spin-off as a threat—vet.

emphasis, no more. I cannot see the spin-off as a threat—yet. There is, however, a much more human type of spin-off problem. Inspiration was drawn from a very readable book, Don't Launch him, he's mine! by Mary Jane Chambers, who is the wife (or space-widow) of one of the boffins behind the Apollo project.

Randall Chambers is an experimental psychologist whose work on the centrifuge which gave the astronauts their moon-legs has earned him world scientific recognition. Mary Jane describes life with him very amusingly and touches Henry on several risible trigger-points.

First, his "study", which seems as typical as the den of any wireless ham I've met. Looking like "a library recently wrecked by an explosion", it houses "piles of graphs, notes, charts of atmospheric measures and weights and measures and maps of many places, including outer space. There are railway timetables, old telephone books, a sterilizer with an assortment of old surgical instruments . . . an assortment of synthetic hearts, brains, ears, skulls. Overlooking all, a huge model of the human eye, staring balefully at the casual visitors'

More than ever am I reminded of life with the Henrys by Mrs. Chambers' account of the day the children knocked the extractor fan out of the window. There were present: an aeronautical engineer, a project engineer, a mechanical engineer and a



".... Staring balefully at the casual visitors."

human factors engineer. "Prodded by several doctors and psychologists, the engineers hesitantly studied the fan, but they made no promises. Each one kept saying: 'I'm not that kind of engineer'".

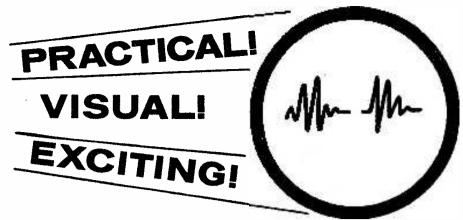
They finally mended it with the help of a flight-surgeon and a research psychologist. That gives you and me, Joe, a fine excuse for the day the 'fridge breaks down or the washing machine develops a "kerplunk". We are chips specialists, not that kind of engineer.

If only Mrs. Henry, confronted with a scattered square-wave generator on the draining-board—because that is just the right height and the soldering iron lead will reach, and there is a half-drawn "project" on the only flat surface of the den—would realise, as Mary Jane has done, that a male brain runs anti-clockwise...

I hope Mrs. Chambers gets her book serialised in the women's magazines. That would be the best possible spin-off from the space-race. Henry wants to construct a few of these chip-flavoured projects, and the ironing-board seems ideal for the purpose. We boffins need encouragement.

* Bootstrapped, of course. † Ouch!! Ed.





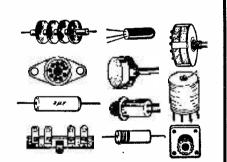
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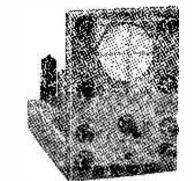
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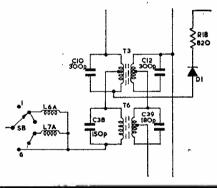
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Martians Again!

Whilst not having heard that Marconi claimed to have received signals from Mars as A. Trowbridge of Middlesex says, I was told many years ago that some person who believed in the existence of men on Mars paid the GPO a sum of money to transmit a certain regular pattern of Morse code signals each day either from Daventry or Rugby, on long waves.

I was told that this went on for quite a time but with no response from the Red Planet.

I would imagine that we shall not hear anything from other planets until we are able to probe frequencies such as those involved in thought-transference and in which extra-sensory perception is only on the extreme outer fringe.

When the thought-transference frequencies are discovered, all

will be plain sailing.

In answer to the letter from Mr. Richard Ross of Worcester, I think perhaps he is using a plumber's soldering iron and no heatsink!—R. Hall (Penzance, Cornwall).

The Early Days

I would like to comment on two of the letters in the November issue.

As another "oldie" I also remember the early days of wireless. Around 1917 I made an 8in. dia. coil, tapped every turn to a stud switch for tuning, and a coherer as detector, with which I could hear Morse from ships. As I could not read Morse a recorder was made to mark it on paper tape.

The gift of a box camera, loaded in the dark with 12 glass plates, took my interest for some years, but when broadcasting started interest in wireless was revived, and a crystal set was made using the large coil.

The purchase of a valve was a big step, there was not much money to spare in those days. Two tins sliding inside each other made an experimental condenser. A real $0.005\mu F$ tuning condenser was the next purchase, and with a few more home-made items mounted on a base-board, and a 3ft. long wooden rod fitted to the

condenser shaft, it was a thrill to hear Sydney, Australia, for the first time.

A fortunate find at a surplus shop in Strutton Ground was a number of fixed condensers made of copper foil and mica sheets clamped between ebonite plates. These could easily be altered to give other capacities. I still have some of the mica.

Then with the arrival in shops of more components, remember Igranic and Telsen etc? a multivalve receiver was built with elaborate dials and panel of ebonite on an oak case. The loudspeaker was a 6ft. papier-maché exponential horn which pretty good. Next, to save the space this took up, I made a stretched doped linen cone 2ft. square which hung up like a picture. It was some time before an 8in. permanent-magnet speaker could be bought and mounted in a 3ft. square board as a "fire-That gave beautiful screen". music.

The h.t. battery was made from a lot of little glass pots, copper, zinc and chemicals obtained from a chemist in Charing Cross Road. I was just married then and my wife and I sat for hours packing manganese dioxide in linen bags. The finished battery giving 120 volts was packed in a wooden crate. L.T. was from an accumulator, one in the set and one at the shop being charged. The local electricity station also charged them for you.

Licences at that time were in my father's name as the householder, but I still have one for 1927. On the back are regulations such as "the combined height and length of the aerial shall not exceed 100 feet", "interference is taking place if a ... whistle is heard, if this... changes when the wavelength of the receiver is altered the cause is inside the receiver and the reaction must be reduced".

At an early Radio Exhibition I bought "Commander Someone's" aerial device for which marvellous results were claimed. It made no difference in my case so I opened it to find no wonderful new invention, only a coil of wire and a small condenser in a card tube filled with pitch.

A trick to mystify friends was to wind a certain number of turns of wire around the hand, twist one end to a needle resting on a piece of coal and with headphones hear 2LO. For this you still required a licence!

I have some sub-min diodes in a small tin labelled the "Mighty Atom Crystal", one of the first I bought and mounted in Wood's

metal in a brass cup.

No doubt youngsters nowadays get some satisfaction when they put supplied components into holes in a printed-circuit board and it works, but I bet it is not the kind of thrill we got in those early days, and now with cheap i.c's. even less is left to the constructor.

The second item I would refer to is the Hertz, a term which I refuse to use, and no one can make me! The good old "cycle per second" is clear and self-sufficient, whether for electrical or mechanical purposes. Imagine, my watch ticks 5Hz. And Hz itself could mean Henry × Impedance.

As to the new mains-lead colours, can anyone explain the reasoning behind the decision to use brown for live. Is it not natural to us to connect the colour red with danger, green with safety and black or grey with neutral? Brown has usually been used for things like valve heater supplies. Anything red made one think before touching. Do "they" contemplate changing all the traffic warning signs to brown? Shall we soon hear it referred to as the "Brown Button"?

I could not agree more with Mr. Harold's last paragraph. Trouble is, except in things like using Hz, we do have to acquiesce. Of course, behind the decimal currency there is a welllaid scheme to put prices up and get even more of our money out of us, as well as using our money to effect the change. I feel that in major decisions such as this, and any others which profoundly affect our way of life, there should be a nation-wide referendum. After all, in most of the things being altered, we WERE first. — E. W. Baigent (High Wycombe, Bucks.).



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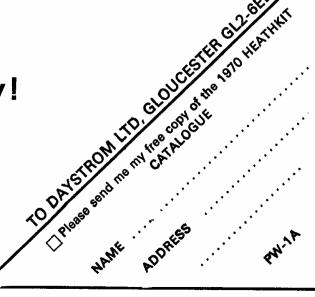
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P.W. GUIDE TO PART 13 M.K.TITMAN, B.Sc. (Eng)

THE number of devices using semiconductor materials to meet specific requirements in electronic circuits is increasing rapidly as research and development continues on an unprecedented scale. The devices examined in this part of the series are the most common and easily obtainable of such devices, but because of the diversity and number of items to be discussed only general practical information has been included. Further detailed information can usually be obtained from manufacturers. Let us now examine the usage, construction, limitations, cost and operation of each type.

Variable Capacitance Diode or Varactor

The variable capacitance diode, varactor or voltage variable capacitor is a device which behaves essentially as a capacitor and circuit symbols are shown in Fig. 1. The capacitance is however capable of variation by means of a d.c. bias voltage. It is therefore particularly useful for automatic frequency control (a.f.c.), frequency modulation, fine tuning and bandwidth regulation. Varactors are also used for frequency multiplication purposes at microwave frequencies.

Varactors are constructed from single p-n junction semiconductor material and are operated in the reverse—non-conducting—direction, the capacitance being the normal diode junction capacitance. They are thus diodes which utilise normal diode construction—such as the alloy, diffusion or planar processes described in a previous part in this series. The junction size and impurity levels are modified to give the required capacitance values and characteristic. A typical capacitance against reverse voltage characteristic is shown in Fig. 2.

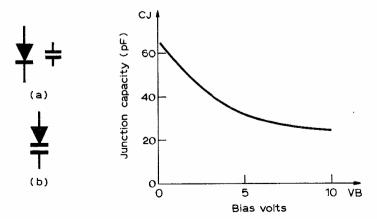


Fig. 1a, b (left): Circuit symbols for a diode used as a variable capacitor or varactor.

Fig. 2 (right): Reverse biased diode capacitance characteristic.

It is worth noting that all semiconductor diodes exhibit a similar characteristic and can therefore be used by the home constructor for applications where variable capacitance diodes are required. However the actual capacitance level differs from diode to diode and for most signal diodes is reduced to a minimum since it is parasitic and determines the upper frequency limit of the diode. Improvisation can nevertheless save time and expense and the home constructor is well advised to try a selection of available diodes for a.f.c. and oscillator tuning applications.

The ideal varactor should have all the characteristics of a capacitor: low leakage, low capacitance tolerance, stability and reliability. The real device closely approaches this ideal except for leakage current which is generally $0.1\mu\text{A}-10\mu\text{A}$ and is generally higher than all but eletrolytic capacitors. Capacitance tolerance varies and is usually $\pm 10\%$ or $\pm 20\%$. Stability and reliability are both good as it is a semiconductor device. The main disadvantage is the requirement for a d.c. bias since they are polarised devices; also the Q factors, which are generally 30-40 for the v.h.f. range low cost units, although Q factors up to 500 can be obtained.

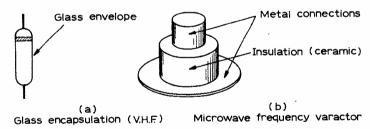


Fig. 3: Varactor encapsulations.

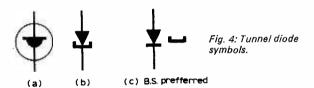
As varactors employ the basic diode structure the encapsulations follow the same pattern. Oscillator trimming and a.f.c. diodes at v.h.f. frequencies, with capacitances of approximately 30pF at 1V reverse, usually employ standard glass encapsulations as shown in Fig. 3(a). Microwave varactors which operate at extremely low capacitance values from 0·1pF to 10pF, with reverse voltages in excess of 50V, utilise special low capacitance encapsulations such as that illustrated in Fig. 3(b). Microwave varactors—which operate in various bands up to 250GHz—frequently operate at higher power levels and consequently have metal encapsulations which directly connect to heatsinks to give increased dissipation.

With all semiconductor devices costs are largely determined by the level of demand and the tolerance ratings and yield of the device. Varactors are no exception and glass encapsulated v.h.f. devices with high

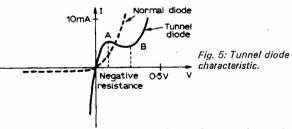
demand levels and low Q factors (10-40) are available from 7s. to 30s. whilst devices with higher Q factors and tuning ranges can cost from £2 to £5. Microwave varactors, particularly power devices, are correspondingly more expensive and cost from £3 to £20 for low power and from £15 upwards for high power types.

Tunnel Diode and Backward Diode

Tunnel diodes, like varactors, are two-terminal single-junction devices, but unlike the varactor their action is active in that they are capable of producing power gains despite the two-terminal configuration. They are used as oscillators, amplifiers and switching devices and can be used up to very high frequencies. Indeed tunnel diodes are used in amplifiers operating at 6GHz. They are extremely stable components and crystal controlled transmitters and chronometers use tunnel diodes particularly in frequency division circuits—where three tunnel diodes can give an accurate frequency division of 2,000 to 1. At present the circuit symbol for the tunnel diode has not been standardised and consequently a selection of symbols is shown in Fig. 4, with the B.S. preferred symbol indicated.



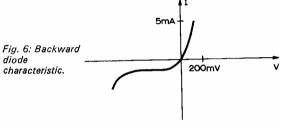
A typical tunnel diode characteristic is illustrated in Fig. 5 and this clearly indicates its essentially active mode of operation. The characteristic shows a peak and a valley, and a region between in which the current falls with increase in voltage, indicating a negative resistance and therefore unstable region. Switching action from point A to point B can occur and is used to aid tuned circuits to give gain or oscillations. Following this region the characteristic follows a normal diode characteristic as would be expected from its single p-n junction structure. This curve is shown for comparison.



The mechanism which produces the negative resistance region in the characteristic is called the quantum-mechanical tunnelling effect, from which the device takes its name. This rather awe-inspiring terminology

tends to overwhelm the potential user but—although the mechanism is mathematically complicated to prove—this should not be a deterrent to the practical engineer. Suffice it to say that the tunnelling effect causes an increase of current at a definite point in the characteristic by sweeping or tunnelling the electrons across the junction, thus producing the characteristic of Fig. 5. The parameters quoted by manufacturers confine themselves to the characteristic and when considered with the characteristic are relatively self-explanatory. Table 1 shows the parameters with a range of values for typical general-purpose tunnel diodes. Microwave diodes up to $40 \, \mathrm{GHz}$ have negative conductance values of $65-75 \, \mathrm{mhos} \times 10^{-3}$ and capacitance values of $0.35-5 \, \mathrm{pF}$.

Backward diodes are tunnel diodes with current values below 0.5 to 1mA and a consequent negative resistance greater than $1k\Omega$. The characteristic is consequently modified and a typical backward diode characteristic is illustrated in Fig. 6. The peak point



current varies from 0.01 to 1mA with capacitance values of 1-20pF. The characteristic allows the backward diode to be particularly useful as mixer and detector diodes at extremely high frequencies.

Both tunnel and backward diodes, being single p-n junction structures, use normal diode manufacturing techniques. They are manufactured from germanium material with extremely heavily doped, small area junctions. The heavy doping produces the tunnelling effect whilst the small junction area minimises junction capacitance. Due to the extremely high operating frequencies lead inductance is a problem and is reduced to a minimum (0.5nH to 5nH) in diodes operating below 2GHz which use axial or TO-18 packages. Epoxy resin plastic packages are used and have lead inductances of 1-2nH whilst microminiature pill packages having lead inductances of 0.1nH are used for microwave diodes. Some typical encapsulations are illustrated in Fig. 7.

Tunnel diode costs vary considerably but increase

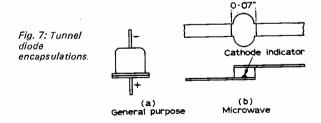
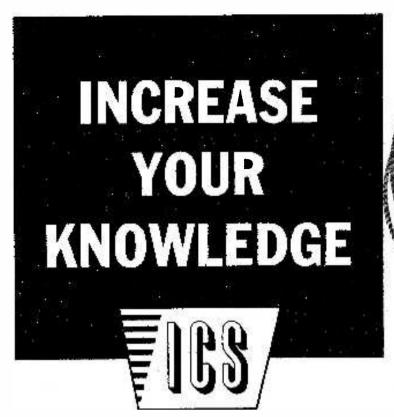


Table 1: General purpose tunnel diode parameters with typical values

Peak point current lp	Max. valley point current lv	P eak voltage Vp	<i>Max. series</i> resistance Rs	Capacitance C	Negative conductance G	Cut off frequency from
1-25mA	0·5-5mA	50-60mV	- 1-10Ω	5-150pF	4-200mhos ×10 ⁻⁸	1-4GHz



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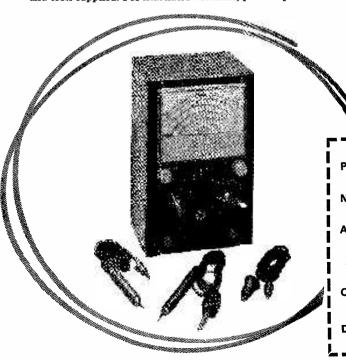
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rapidly in the regions beyond 1GHz. Average axial and plastic package diodes for use below 1GHz are available from 15s. to £4, with metal encapsulations ranging from 30s. to £7. Microwave devices are available from £10 upwards.

Unijunction Transistor

As its name implies the unijunction transistor is a three-terminal, single-junction device and its symbol is shown in Fig. 8. The circuit operation is however unlike either a transistor or diode, as indeed is the construction.

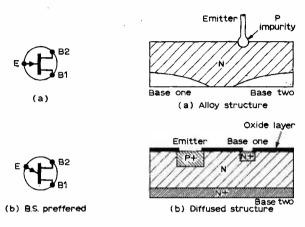


Fig. 8a, b (left): Unijunction transistor symbols. Fig. 9a, b (right): Unijunction transistor constructions.

The structure consists of a block of resistive semiconductor material with a junction formed at a definite position along the length of the bar. Leads are connected to the ends of the bar and are denoted base 1 and base 2 whilst the connection to the junction is referred to as the emitter. Hence the designation double base diode which was the original term for this device. At present only n-type silicon is used for the bar and the junction is formed by alloying or diffusing a p-type impurity at the required point along the bar. Typical alloy and diffused junction constructions are shown in Fig. 9 and although alloy junction types are the cheapest as well as the most widely used the diffused construction is increasingly popular due to the low leakage currents and faster switching times. Encapsulation is usually in the familiar TO-18 and TO-5 transistor casing although plastic is used increasingly for the cheaper devices. At present terminations are not completely standardised and the manufacturers' data should be consulted.

The circuit operation of the unijunction transistor can be understood by referring to Fig. 10 which shows the essential diagrammatic structure and its equivalent

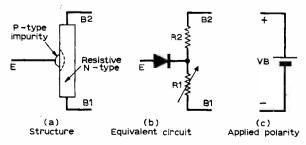


Fig. 10: Basic unijunction structure.

circuit. If the battery is connected as indicated, a voltage gradient is set up in the high resistivity n-type bar. As a result the position of the junction along the bar determines the positive potential required at the emitter terminal to enable the p-n junction diode to conduct. Thus if the battery is 12V and the junction is midway between base 1 and base 2—the potential required to make the diode conduct is (6V + diode drop) = 6.7V. This parameter is sometimes quoted in specifying unijunction transistors and is known as the peak point emitter voltage (Vp). The resistance ratio which determines this potential on the equivalent circuit is $\left(\frac{R1}{R1 + R2}\right)$ and this is known as the intrinsic standoff

ratio (η). Hence to turn on the unijunction transistor the emitter voltage must satisfy the following equation:

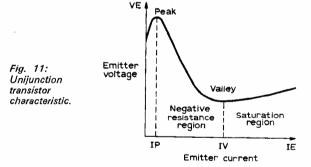
V emitter=
$$Vp = \left(\frac{R1}{R1 + R2}\right)V_B + Vd$$

= $\eta V_B + Vd$ (1)

Since the intrinsic standoff ratio η determines Vp for any supply voltage this is always quoted as a parameter and for any given device has a stated tolerance.

When the diode is made to conduct by this potential Vp then the base 1 resistance R1 reduces rapidly to a low value—thus causing a rapid increase in emitter current and a drop in emitter voltage towards zero volts. This effect is achieved by the electron input through the emitter causing the reduction in resistivity of the base 1 region of the bar structure.

In order to reduce the base 1 region to low resistivity a minimum current into the emitter is required. This parameter is called the peak point current (Ip) and is clearly shown in the unijunction characteristic Fig. 11.



The characteristic also shows the negative resistance region which causes the switching action and the stable saturation region which is achieved after Ip is exceeded. Ip is usually of the order of 0.5 to 100μ A and η of the order of 0.5 to 0.85. The total resistance known as the interbase resistance R_{BBI} varies between $4k\Omega$ and $12k\Omega$. Other parameters supplied by the manufacturer are peak emitter current (\sim 2A), power (P_D), maximum base to base voltage (V_{B2} V_{B1}, \sim 30-50V) and frequency—which can be in the megacycle region.

It can be seen from the characteristics that until the diode conducts the impedance is very high $(1-10M\Omega)$ whilst at switch on it drops rapidly towards zero. When coupled to a charging capacitor it is off until Vp is reached, then rapidly conducts and discharges the capacitor. When the discharge current falls below Ip it switches off and the capacitor can recharge to Vp. Thus it is useful as a relaxation oscillator but can also be used for thyristor triggering, voltage sampling and in protection circuits.

The disadvantages of unijunction transistors are that the ratio η varies considerably as it depends on the

8-

positioning of the junction—as a result the turn-on emitter voltage (peak point voltage Vp) also varies considerably. In addition these parameters are affected by

temperature.

Unijunction transistors are available at varying price levels depending on the demand, range of tolerance of η and hence Vp, and frequency response. Cheapest types are plastic encapsulated at 5s. with high frequency, low leakage devices available at 9s. to 35s. At present only p-type emitter devices are available as shown by the symbol which indicates—in the emitter arrow—the direction of current flow. If n-type emitter devices become available they will be expensive initially and as with transistors the reversal of current flow will be indicated on the symbol by a reversal of the emitter arrow.

TO BE CONTINUED

PRACTICAL TELEVISION in the JANUARY issue

★ DEVELOPMENTS IN TV RECEIVERS

A detailed account of the changes that have been taking place in TV receivers in recent years, including the introduction of i.c.s and single-standard operation.

★ A CONSTRUCTOR'S 625-LINE RECEIVER

Details of a 17in. 625-line receiver built up by a constructor to provide superior performance, including black-level stabilisation.

★TRANSISTOR LINE DRIVER STAGES
Line output driver stages are unique to fully
transistorised receivers and present some tricky
design problems. A detailed look is taken at
these problems and the methods of successfully
overcoming them.

★ SIMPLE GADGETS FOR THE REPAIR SHOP

A number of simple gadgets that can save much time and effort are described in *Workshop Hints*.

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FILM SHOW

Caxton Hall, Caxton Street London S.W.1 Friday, March 6th, 1970 at 7.30 p.m.

Come and spend an interesting evening (free tea and sandwiches), which will include a colour film entitled SOMETHING BIG IN MICRO-CIRCUITS. Ian Nicholson of Mullard Ltd., will be the principal speaker. W. N. Stevens, Editor, Practical Wireless and Practical Television will be in the chair.

BEGINNERS PORTABLE RECEIVER

-continued from page 695

will accommodate should be used. The wires between L1, VC and the board must be short and not liable to flexing or the alignment will be affected. If possible, L1 and VC should be fixed rigidly to the Veroboard to ensure this. The wires connecting the volume control to the board are not so critical.

Operation

The receiver should work fairly well without any alignment at this stage and the coil cores must not be adjusted indiscriminately if it does not. If there is no sound, the stages can be checked individually as follows. Connect one end of a capacitor (about $0.1\mu\mathrm{F}$) to battery negative and touch the other end to successive transistor bases, working from the loudspeaker to the aerial. Clicks should be heard in the loudspeaker until the faulty stage is located.

The radio works well without an external aerial but this can be used by adding C1 to the circuit (see Fig. 1). A car aerial can be connected in this way. If the connection of the external aerial upsets the radio tuning unduly or causes overloading, use a smaller value for C1.

Alignment

If the radio is receiving signals, it can be aligned without other equipment if proper care is taken. Tune in a weak station at the centre of the range. Use a plastic screwdriver blade (e.g., a filed down plastic knitting needle or toothbrush handle) to adjust i.f.t.1, i.f.t.2, i.f.t. 3 for the strongest signal. Repeat this adjustment several times, keeping the signal tuned in as well as possible with VC. Find a weak station at the l.f. end of the range. Adjust L2 oscillator core in one direction somewhat and retune the station with VC. If the reception is better, continue adjusting the dust core in the same direction until the best signal is obtained; if the reception is worse, adjust in the opposite direction. After each core adjustment, the same station must be retuned with VC. Retune VC to a weak station at the h.f. end of the range and adjust VC2 trimmer for correct station position. Finally adjust VC1 trimmer for maximum signal strength. The process must be repeated until best results are obtained. Alignment is now complete.

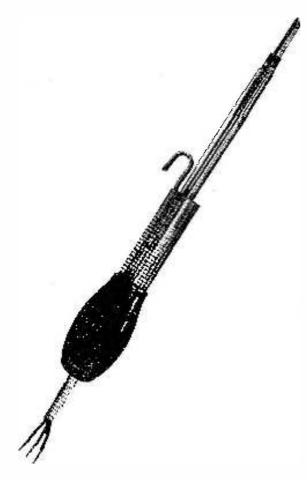
A socket for a magnetic earpiece can be connected as shown in Fig. 4. The same socket can be used to operate extension speakers. If the socket is wired as shown, the radio speaker is muted when anything is plugged in.

Figure 5 shows a treble/bass tone control that can be added to the circuit. R16 and C12 are no longer used and should be removed from the board. The tone control reduces the audio gain slightly but provides a useful range of adjustment.

The audio stages can be used as a useful loudspeaker amplifier for microphone, guitar, signal tracing, record playing, etc. by adding a socket as shown in Fig 6.



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COLLARO "O": RONETTE BF40LE: GARRARD GC2LP and GCSLP: ACOS GP65/67, and at 7/8 each (1)-). ACOS GP91 ST/LP: BBR ST4 and ST9; SONOTONE 9TA and 9TAHC. PHILIPS AG3306, 3060 (3063, 3066, 3301, 3302, 3804) state whether \$\frac{1}{2}\$ in. or \$\frac{1}{2}\$ in. all at 18/6 (1/-). ACOS (396) (3063, 3066, 3301, 3302, 3804) state whether \$\frac{1}{2}\$ in. or \$\frac{1}{2}\$ in. all at 18/6 (1/-). No other types at present, and no 78 rpm available in any type.

PICK-UP CARTRIDGES. All fitted Styll and Standard fittings. Mono GP67/2, 18/6 • Stereo Compatible—Mono which also plays Stereo records uncaurally with min. wear GP91/SO, 19/6. • Datest Stereo GP98, 24/6. • Ceramic Stereo, top quality for expensive outfits, GP94, 38/6 (all 1/-).

PER ELIMINATOR (A.C.) 17/6. (1/6) TWO STATION TRANS. INTER-COM. Excellent baby alarm. Instant, easy fitting with leads, plugs and battery. All you require 52/6 (3/-).

TRANSISTORISED AMPLIFIERS. 3 watt, 90 operation, 45/6 (1/6); 7½ watt, 6 trans. 24V operation, 67/6 (2/6).

EXTH High Torque MINI-MOTOR, 4½ to 12V, 1½ x \(\frac{1}{2}\) in. 5/- (1/-), 9,000 r.p.m.

SUBSTITUTION BOXES, Capacitance 25/6 (1/6), Resistance 32/6 (1/6), Both full range and complete. Full details in list.

TEST PRODS: Flexible, unbreakable 24/n. Red and Black leads, thin 4½m. prods, 1½m. plugg 4/9 (1/-), Croc. Clips: Plated with screw, or with red/batch handles, 6d. each, 5/- doz. (1/-). RECORDING TAPE: Finest quality British Mylar. STANDARD: 5in. 600ft. 7/8, 5\frac{1}{2}\) in. 18/- (1/3) are 18/- (1/3) a

Switches etc. in list.

VIBRATORS: Famous makes only. 12 volt 4 pin non-synch 2/6. 12 volt 7 pin synch 10/6 volt 7 pin synch 10/- (1/- each, all types). No other types available.

MAINS NEON TESTER: Fly leads 2/-. Pocket screwdriver type 3/6. PLUGS: Std. Jack,
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Flexible 3/-. Super thin for transistor wiring etc. 3/- (1/- all types per 6 coils). PICK-UP
WIRE: Twin Super thin Flex, Screened, Sheathed. 1/3 yd. (6d. up to 6 yds. over 6 yds.
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screened and sheathed. (Up to 3 yds 8d., each additional yard, 1d. extra.)

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(1/6). Details in list.

(1/6). Details in list.

RETRACTABLE FLEXIBLE LEADS. Space saving "Curly", many uses in car and home: with phono plug each end, 6ft., 4/6; 12ft., 7/9. With phono plug one end, phono socket at other, 6ft., 5/-, 12ft., 8/6 (1/- each all types).

CAR RADIO: Splendid new All-British dash-mounting radio using Mullard transistors and circuit. M and L. wave. Separate speaker and baffle. Absolutely complete, for + or - chassis. \$11.1.0 (6/6). A huge success since introduction.

CURRENT LIST: Sent with all orders or free for s.s.e. details of cable, croc. clips and leads, Continental din plugs for Grundig, Telefunken equipment, etc., dials, plugs and sockets, panel meters, record player and tape recording accessories. BATTERY CHARGERS: test equipment, terminals, tape recorder, special transistors, portable sets, more switches and other components, tools, Veroboard etc., etc. This advertisement cancels all previous ones and lists supplied prior to November 30th.

FELSTEAD ELECTRONICS

(PW26) LONGLEY LANE, GATLEY, CHEADLE, CHESHIRE, SK8 4EE

TERMS: Cash with order only. No C.O.D. or caller service. Post, packing and insurance charges are shown in brackets after all items, Regret orders under 5/- plus carriage cannot be accepted, and a minimum charge of 1/- is now made. Charges apply to G.B. and Eire only. Overseas air or surface mail extra at cost, plus 3/2 registration or insurance fee. S.A.E. please for all enquiries, otherwise regret cannot be replied to

TAKE 2®

JULIAN ANDERSON

This month's special Christmas project describes a three transistor radio which is highly selective together with a good output level. By careful 'shopping around' among the advertisers the complete radio may be built for under 20s; as usual less than twenty components are used

FEW months ago our project was a one transistor radio which did not require an external aerial and operated a loudspeaker; however this design did have limitations—especially volume which was mentioned in the text. With Christmas just around the corner there must be many readers who would like to take advantage of their interest in electronics and knock up something for the children, and it was with this specifically in mind that this month's project was planned.

First, the radio had to have decent selectivity and volume, and as it is intended primarily for children it had to be able to get Radio Luxembourg well. The circuit had to be reliable and quickly built. (To this end three prototypes were built to ensure the circuit was reliable.) Building of the prototype shown in the

photographs took under three hours including the cabinet. Also the radio had to have a presentable but cheap case.

The Circuit

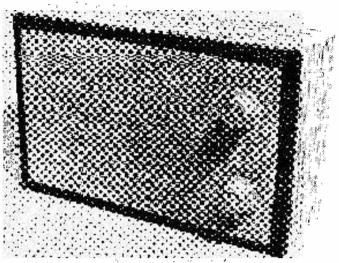
There is nothing particularly unusual about the circuit. The first transistor acts as an r.f. amplifier with VR1 as its collector load. Positive r.f. feedback (regeneration) is taken from the slider of VR1 and connected via VC2 to the top of the aerial coil.

The r.f. signal is fed to the base of Tr2 which is biased in such a way as to detect the r.f. signal, the output is smoothed by C3. The audio output is d.c. connected to Tr3, the output transistor. The emitter resistor is bypassed by C4, the base bias for Tr2 being taken from this circuit via R3, $100 \mathrm{k}\Omega$. The $200 \mu\mathrm{F}$ capacitor, C5, decouples r.f. and a.f. from the positive rail.

Components

Care will have to be taken in the purchase of components to come within our 20s. maximum. Whereas aerial coils can be bought, it is far cheaper and very

No. 9 THREE TRANSISTOR RADIO

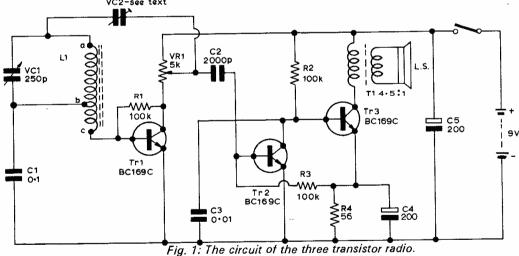


The Take 20 three transistor radio.

simple to wind your own. For this L1 should consist of about 70 turns and L2 of 5 turns on a four to six inch length of $\frac{3}{8}$ in. or $\frac{1}{4}$ in. ferrite rod. VC1 may be any type of tuning capacitor between 200pF and 350pF. For economy the loudspeaker should be a 6 × 4in, size removed from old TV sets.

Construction

All components apart from the speaker, VR1, VC1 and the battery are mounted on an eleven-way minia-



A vacancy exists on the editorial staff of

PRACTICAL WIRELESS

Required to prepare articles from authors copy through to final printing. Knowledge of modern electronics and editorial procedure essential. Applicants are invited to write to the Managing Editor, Practical Wireless, Tower House, Southampon St., London W.C.2 giving full details.

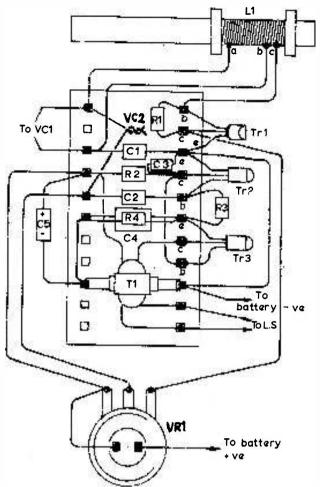


Fig. 2: The components are mounted on an eleven way tagboard. Compare this with the photograph.

ture tag board as shown in Fig. 2. The ferrite rod is secured to this board by tying one end to the top of the tag board as shown in the photograph.

The cabinet front is made from a piece of hardboard 9×5 in. to which are fixed the sides made from $2\frac{1}{2} \times \frac{1}{2}$ in. planed softwood. These sides should be glued and nailed together and nailed with hardboard pins to the side framework. Holes must of course be drilled for the speaker and the two controls. The tag board is held inside the case by making a small bracket, one end of which is bolted to one of the holes in the tag board and the other screwed to the inside of the case ensuring that the ferrite rod is not too close to the speaker magnet.

The cabinet front can be covered with speaker fabric or any reasonably strong material. This should be cut exactly to size and glued. The sides and the back of the cabinet are covered in self-adhesive plastic covering such as Fablon. The junction of the speaker fabric and plastic covering may be hidden by using black plastic tape.

QUERY COUPON

This coupon is available until 7th January, 1970 and must accompany all queries in accordance with the rules of our Query Service.

PRACTICAL WIRELESS, JANUARY 1970

components list

Resistors:

R1 $100 k\Omega$ R3 100k Ω R2 $100k\Omega$ R4 56Ω All $\frac{1}{8}$ or $\frac{1}{4}$ watt, 10% miniature types VR1 5k Ω log pot, with switch

Capacitors:

C1 0·1μF 200μF 9V C4 2,000pF 200μF 12V C2 **C**5

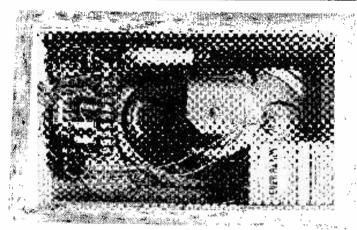
C3 0·01μF

VC1 250pF variable—see text

VC2 see text

Miscellaneous:

Tr1, Tr2, T3r BC169C; Ferrite rod with windingssee text; T1, transistor output transformer, approx. 4.5:1; Loudspeaker 3 Ω ; Battery PP7 or equivalent; Eleven-way tag board; Hardboard and softwood for case—see text; Speaker fabric; Self-adhesive plastic covering.



An interior view of the prototype.

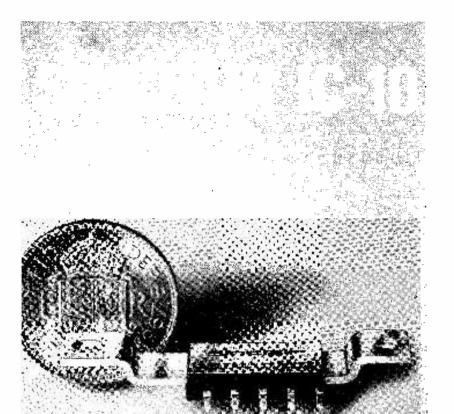
Conclusion

Assuming everything has been wired up correctly the only adjustment is that of VC2 and this, being frequency selective, should be peaked so that the set just fails to break into oscillation on Radio Luxembourg. VC2 consists of two 1in. lengths of wire twisted together. Incidentally the gain of the first stage is so high that unless the general layout is carefully followed there is a danger of the set continually oscillating. Because of the fairly high capacitance of Veroboard it is not to be recommended for this particular project.

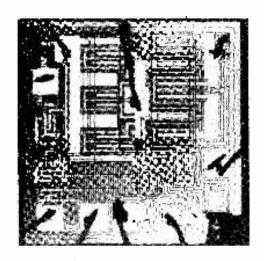
Next month's Take 20 article describes a small, cheap, transformerless amplifier. It provides between 750mW and 1W into a 3Ω loudspeaker.

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MONOLITHIC INTEGRATED CIRCUIT HIGH FIDELITY AMPLIFIER AND PRE-AMP



theworld's most advanced high fidelity amplifier

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output of 5 watts R.M.S. (10 watts peak). It contains 13 transistors (including two power types), 2 diodes, 1 zenor diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.

The IC-10 is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of the usual tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required for producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. It also enables us to give a 5 year guarantee on each IC-10 knowing that every unit will work as perfectly as the original and do so for a lifetime.

SPECIFICATIONS

10 Watts peak, 5 Watts R.M.S. continuous. Frequency response 5 Hz to 100 KHz±1dB. Less than 1% at full output. Total harmonic distortion 3 to 15 ohms. Load impedance 110dB (100,000,000,000 times) total. Power gain Supply voltage 8 to 18 volts. 1 imes 0.4 imes 0.2 inches. Size Sensitivity 5mV. Adjustable externally up to Input impedance 2.5 M ohms.

■ CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier. Class AB output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

APPLICATIONS

Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

SINCLAIR

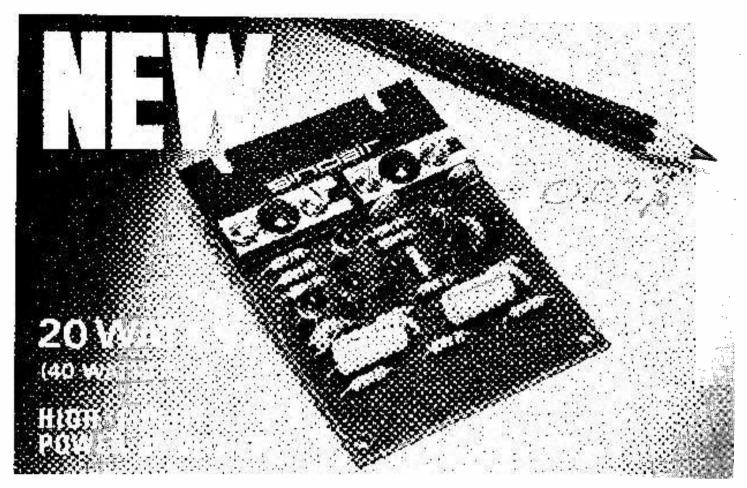
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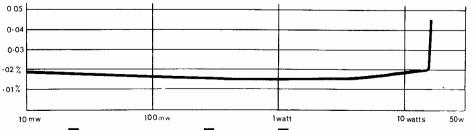
THE WORLD'S LOWEST DISTORTION HIGH FIDELITY AMPLIFIER.

For four years, the Sinclair Z.12 dominated the constructor world, being the best selling unit of its kind this side of the Atlantic. Excellent as it was, the new Sinclair Z.30 is still better. Half the size of the Z.12, it has more than twice the power, very much greater gain and a level of distortion 50 times lower. This incredible figure results from using over 60dB of negative feed back with a constant current load to the driver stage obtained by incorporating a two transistor circuit in place of the more usual boot-strapping. 9 silicon epitaxial planar transistors are used to provide enormous power (up to 20 watts RMS continuous sine wave, 40 watts peak). The circuitry of this marvellous amplifier allows it to be operated from any voltage from 8 to 35 to perfection.

At all output levels, distortion is only 0.02%. This puts true laboratory standards into the hands of every user of a Z.30. Two Z.30s and a new Stereo Sixty will make a stereo assembly of such perfection that it could not be bettered in its class no matter how much you spent. But the Z.30 has an enormous variety of applications, particularly where quality, precision and reliability are essential. Yet this brilliant new Sinclair design costs not a penny more than its famous predecessor.

APPLICATIONS

Hi-fi amplifier; car radio amplifier; record player amplifier fed directly from pick-up; intercom; electronic music and instruments; P.A.; laboratory work, etc. Full details for these and many other applications are given in the manual supplied with the Z.30.



SPECIFICATIONS

Power output: 15 watts R.M.S. into 8 ohms using a 35 volt supply: 20 watts R.M.S. into 3 ohms using a 30 volt supply.

Output: Class AB.

Frequency response: 30 to 300,000Hz

 \pm 1dB.

Distortion: 0.02% total harmonic distortion at full output into 8 ohms and at all lower output levels.

Signal-to-noise ratio: better than 70dB

unweighted.

input sensitivity: 250mV into 100 Kohms.

Damping factor: > 500.

Loudspeaker impedances: 3 to 15 ohms.

Power requirements: From 8 to 35V. d.c. (The Z.30 will operate ideally from bat-

teries if required). Size: $3\frac{1}{2} \times 2\frac{1}{4} \times \frac{1}{2}$ inches.

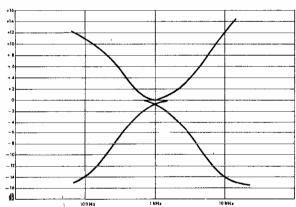
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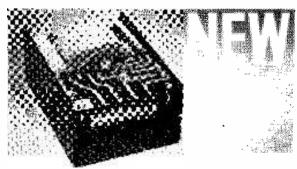




Curves to show bass and treble cut and boost

Ready built, tested and guaranteed with instructions

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This attractive and completely new unit is intended for use with two new Z.30 amplifiers to provide the finest possible standards of stereo reproduction. Four press buttons and four rotary controls are used to provide on-off, three input selectors and Volume, Bass cut/boost, Treble cut/boost and Stereo balance. The on-off button also switches the power amplifiers. The front panel in brushed aluminium is flush mounted to the cabinet front, it being necessary only to drill holes to accommodate the controls. Rear adjustable brackets hold the chassis tight to the cabinet. The very latest ganged rotary controls are used to afford compactness and extra long working life free from noise.

The Stereo-60 may also be used with 2 IC-10's or any other high performance amplifiers.

SPECIFICATIONS

- Input sensitivities—Radio—up to 3mV Magnetic Pickup —3mV; correct to R.I.A.A. curve ± 1dB; 20 to 25,000 Hz. Ceramic Pickup—up to 3mV: Auxiliary—up to 3mV.
- Output—1 volt.
- Signal-to-noise ratio—better than
- Channel matching—within 1dB.
- Tone Controls—TREBLE +15 to —15dB at 10kHz. BASS +15 to —15dB at 100Hz.
- Power consumption 5mA.
- Front panel—brushed aluminium with black knobs and controls.
- Size 8½ x 1½ x 4 ins.

PZ.5 POWER SUPPLY UNIT

A new heavy duty mains power supply unit designed specially to drive two Z.30s and a Stereo Sixty. New compact design. For AC Mains, 200-240V/50Hz. **£4.19.6**

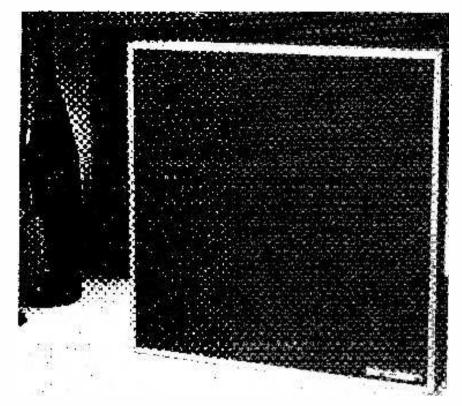
Q.16 Loudspeaker and Micromatic on next page.

To: SINCLAIR RADIONICS LTD., 22 NEWMARKET RD CAMBRIDGE Please send			
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SINCLAIR Q.16

new elegance in an outstanding loudspeaker

All the superb features which went to make the Sinclair Q.14 have been incorporated in the new Q.16 which gives an exciting new opportunity for you to match your Sinclair equipment with modern decor. Employing the same well proven acoustic system in which materials, processing and styling are used in such a radical and successful departure from conventional design, the new Q.16 presents an entirely new appearance with its attractive teak surround and all-over special cellular foam front chosen as much for its appearance as for its ability to pass all audio frequencies without loss. The Q.16 is compact and slim. Its new styling makes it eminently suitable for shelf mounting, but it is no less versatile than its famous predecessor. Listen to a pair of Q.16s in stereo and marvel at the standards of quality and clarity they give.



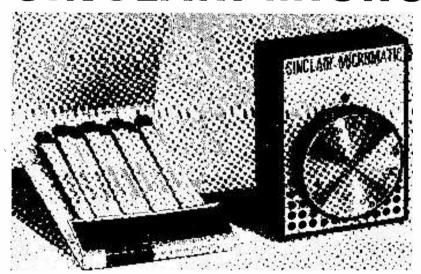
The 0.16 will handle loading up to 14 watts R.M.S. and presents an 8 ohm impedance to the amplifier output. Frequency response extends from 60 to 16,000Hz with exceptional smoothness. A specially designed driver system is used in a sealed and contoured pressure chamber to ensure good transient response at all frequencies. Size: 9¾ square × 4¾ deep from front to back.

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SPECIFICATIONS—Size: $1\frac{13}{16}'' \times 1\frac{7}{16}'' \times \frac{1}{2}''$ (46×33×13mm). Weight incl. batteries: 1 oz. (28-35gm) approx. Tuning: Medium wave band with bandspread at higher frequency end. Earpiece: Magnetic type. Case: Black plastic with anodized aluminium front panel, spun aluminium dial.

Complete kit incl. earpiece, case, solder and instructions in fitted pack. Plus 11d. P.T. surcharge Ready built, tested and guaranteed, with earpiece. 49/6

Plus 1/1d. P.T. surcharge Mallory Mercury Cell RM675 (2 req.) 2/9 each

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Everything including the batteries is contained within the attractively designed case. Whether you build your Micromatic or buy it ready built and tested, you will find it as easy to take with you as your wristwatch, and dependable under the severest listening conditions.

USE THIS COUPON FOR MICROMATIC AND Q.16 ORDERS

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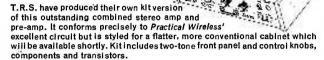
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Inputs—Mag. P.U. (R.I.A.A.) 2.5mV into 68 Kohms; Ceramic P.U. and Radio; Response 20Hz to 30KHz ± 1 dB. Output—12 watts per channel. R.M.S. Into 15 ohms.

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Kit complete, £24.10.0 (Carr. 7/6) Kits available separately. S.A.E. brings list.

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used nere.

MULLARD 2+2 STEREO PRE-AMP with same characteristics per channel as mono pre-amp (+ balance). BUILT £13.19.6 (Carr. 7/6).

T.R.S. 4×4 ECONOMY STEREO. Modular assembly. With cabinet power supply and Din plugs £12.10.0 (Carr. 7/6).

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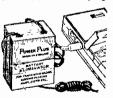
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6A, 23/0076 circular PVC covered as fitted to electric drills and most portable appliances, ideal extension lead. Regular price 1/6 per yard, our price 79/6 for 100 yard coil. Post 6/6.



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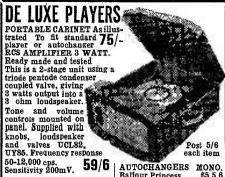
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Long spindles. Midget Size
5 K. ohms to 2 Meg. LOG or AERAXIAL-AIR SPACED
LIN. L/S 3/-. D.P. 1/-6
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BLANK ALUMINIUM. CHASSIS 18 s.w.g. 2½ in. sides,

5.K.B.F. unurineu $^{1}_{16}$ III nouru 10 × 5111. 517. 517. 518. 18 s.w.g. $^{2}_{2}$ in. sides, 7×4 in., 5/6; 9×7 in., 6/6; 11×3 in., 6/6; 11×7 in., 7/6; 13×9 in., 9/6; 14×1 iin., 12/6; 15×14 iin., 15/6 ALUMINIUM FANELS 18 s.w.g. 12×12 in., 6/6; 14×9 in. 5/6; 12×8 in., 4/6; 10×7 in. 3/6; 8×6 in. 2/6; 6×4 in. 1/6.

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ALL PURPOSE HEADPHONES

H.R. HEADPHONES 2000 ohms Super Sensitive ... LOW RESISTANCE HEADPHONES 3-5 ohms DE LUXE PADDED STEREO PHONES 8 ohms ...

THE INSTANT **BULK TAPE** ERASER ANO 42/6 RECORDING HEAD DEMAGNETISER 200/250 v. A.C. Leaflet S.A.E.

BARGAIN STEREO/MONO SYSTEM

Attractive Slim PLAYER CABINET with B.S.R. Stereo Autochanger, 3 valve Stereo Amplifier, two 6½ in. LOUD-SPEAKERS. (Only 4 pairs of wires to join). £19.19.6 Carr. 10/6. S.A.E. for details

NEW TUBULAR ELECTROLYTICS | CAN TYPES 2/350V 2/3 | 100/25V 2/- | 8/600V 9/6 | 16/600V 9/6 | 18/350V 2/3 | 250/25V 2/6 | 16/600V 9/6 | 18/350V 12/3 | 250/25V 2/6 | 16/600V 9/6 | 18/450V 12/3 | 250/25V 2/6 | 16/600V 7/6 | 16/450V 3/9 | 8+16/450V 3/9 | 6+100/350V 11/6 | 25/25V 1/9 | 16+16/450V 3/9 | 6+100/350V 11/6 | 25/25V 1/9 | 16+16/450V 4/3 | 32+32/350V 8/- | 25/350V 1/9 | 16+16/450V 4/3 | 32+32/350V 8/- | 25/350V 1/9 | 16+16/450V 4/3 | 32+32/350V 8/- | 25/350V 1/9 | 16+16/450V 4/3 | 32+32/350V 8/- | 25/350V 1/9 | 16+16/450V 4/3 | 32+32/350V 8/- | 25/350V 1/9 | 16+16/450V 4/3 | 32+32/350V 8/- | 25/350V 1/9 | 100-50-50/1000mF 12V 3/6; 2000mF 25V 7/- | 25RAMIC. 500V 1pF to 0.01mF, 9d. | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 | 25/25 |

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250-0-250 50 mA. 6.3 v. 2 amps, centre tapped
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COAXIAL PLUG 1/3. PANEL SOCKETS 1/3. LINE 2/COUTLET BOXES. SURFACE OR FLUSH 4/6.
BALANCED TWIN FEEDERS 1/- yd. 80 ohms or 300 ohms.
JACK SOCKET Std. open-circuit 2/6, closed circuit 4/6;
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SOCKETS Chassis 3-pin 1/6; 5-pin 2/-. DIN SOCKETS Lead
3-pin 3/6; 5-pin 5/-. DIN PLUGS 3-pin 3/6; 5-pin 5/-.
VALVE HOLDERS, 9d.; CERAMIC 1/-; CANS 1/-.

T.S.L. LOUDSPEAKER **CROSSOVER HLP2**

2-way crossover for 8 or 15 ohm speakers and tweeters. 3 phono input/output sockets.

Made to sell OUR PRICE at 42/- Post 2/6.

Tape Spools 2/6. Tape Splicer 5/-. Leader Tape 4/6. Reuter Tape Heads for Collaro models 2 track 21/- pair. PHOTO-ELECTRIC RELAY SYSTEM, 240v. A.C. Exciter and relay unit with infra red filter. For counting, door signals, alarms, etc. 212 POST FREE.

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10 WATT 55/- CARRIAGE 5/-

Triple speaker system combining on ready cut baffle, in. chipboard 15in. ×8\(\frac{2}{3}\)in. Separate Bass, Middle and Treble loudspeakers and crossover condenser. The heavy duty 5in. Bass Woofer unit has a low resonance cone. The Mid-Range unit is specially designed to add drive to the middle register and the tweeter recreates the top end of the musical spectrum. Total response 20-15,000 cps. Full instructions for 3 or 8 ohm.

TEAK VENEERED BOOKSHELF $16 \times 10 \times 9 \text{in. Modern Scandinavian}$ fluted front design for Mini-Module 94/6 Post 5/-

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30-14,500 c.p.s., Hi-Fi double cone, woofer and tweeter cone together with a ceramic BAKER magnet assembly having a flux density of 14,000 gauss and a total flux of 145,000 Maxwells. Bass resonance 45 c.p.s. Rated 20 watts. Voice coils available 3 or 8 or 15 ohms. Price £8, or Module kit. 30-17,000 c.p.s. with tweeter, crossover, baffle and £10.19.6 instructions. LOUDSPEAKER CABINET WADDING 18in. wide, 2/6ft.

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Horn Tweeters 2-18kc/s, 10W 15 ohm 29/6. Crossover 16/6.

LOUDSPEAKERS P.M. 3 OHMS. 2½in 3in, 4in, 5in, 5 × 2½in.

7 × 4in. 17/6 each; 6½in 22/6; 8 × 5in, 21/-; 8 × 2½in, 21/-;

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E.M.I. Double Cone 13½ × 8in, 3 or 15 ohm 10 watt. 45/-,

DITTO twin tweeters and X/over, 3 or 8 or 15 ohm 10 w. 79/-,

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For 10in. or 12in. dia. Loudspeaker 24.14.6.

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SPECIAL OFFER! 8 ohm, 2½in; 6 × 4in; 30 ohm, 2½in;

15/6 EACH 25 ohm, 6 × 4in; 35 ohm, 3in;

TYPE 15 ohm, 7 × 4in., 8 × 5in.

Sin. LOUDSPEAKER UNITS 3 ohm 27/6; 15 ohm 30/-;

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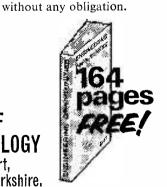
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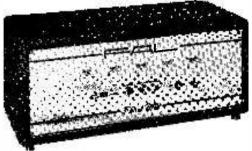
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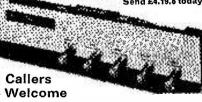
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TRANSISTOR STEREO 8 + 8 MK II

Now using Silicon Transistors in first five stages on each channel resulting in even lower noise level with improved sensitivity. A really first-class Hi-Fi Stereo Amplifier Kit. Uses 14 transistors giving 8 watts push pull output per channel (16W. mono). Integrated pre-amp. with Bass, Treble and Volume controls. Suitable for use with Ceramic or Crystal cartridges. Output stage for any speakers from 3 to 15 ohms. Compact design, all parts supplied including drilled metal work. Cir-Kit board, attractive front panel, knobs, wire. solder, nuts, bolts—no extras to buy. Simple step by step instructions enable any constructor to build an amplifier to be proud of. Brief specification: Freq. response ± 3dB. 20-20,000 c/s. Bass boost approx. to +12dB. Treble cut approx. to -16dB. Negative feedback 18dB over main amp. Power requirements 25V at 6 amp.

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Also available STEREO 10+10. As above but 10 watts per channel. PRICES: AMPLIFIER KIT \$12. POWER PACK KIT \$3.10.0.

Circuit diagram, construction details and parts list (free with kit) 1/6. (S.A.E.).

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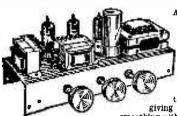
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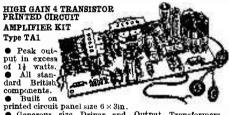
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Generous size Driver and Output Transformers.

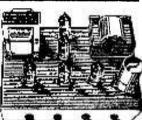
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U23	30 Madt's like MAT Series PNP Transistors	10/-
U24	20 Germanium 1-amp Rectifiers GJM up to 300 PIV	10/-
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U26	30 Fast Switching Silicon Diodes like IN914 Micro-min.	10/-
U28	Experimenters' Assortment of Integrated Circuits, untested. Gates, Flip-Flops, Registers, etc., 8 Assorted Pieces	20/-
U29	10 1-amp SCR's TO-5 can up to 600PIV CRS1/25-600	20/-
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U32	25 Zener diodes 400mW D07 case mixed Volts, 3-18	10/-
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Code Nos. mentioned above are given as a guide to the type of device in the Pak. The devices themselves are normally unmarked

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OA79 OA81-85	1/6
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200	1/9	4/-	4/9	20/-
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800	3/6	7/6	11/-	40/-
1000	5/-	9/3	12/6	50/-
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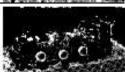
STEREO AMPLIFIER type HV-2 x 3 Watts

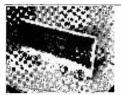
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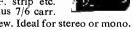
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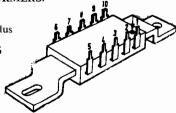
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0·015 0·022		7d. 7d.	5/2 5/3	11/10 12/ -	37/6 37/9	$\begin{array}{cccccccccccccccccccccccccccccccccccc$			
0·033 0·047		8d. 9d.	5/8 6/7	12/7 14/5	42/7 49/-	$\frac{2}{2}$ W 5% $3\frac{1}{d}$. $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{2}$ $\frac{1}{10}$			
0·068 0·1		11d. 11d.	7/8 8/-	16/7 17/2	51/- 57/4	SEMICONDUCTORS Type 1 off 10 off 25 off 100 off Type 1 off 10 off 25 off 100 off			
0·15 0·22		1/2 1/6	10/3 14/3	22/- 28/5	74/- 95/10	AĈ107 3/6 26/3 63/- 232/9 OA5 2/- 15/- 36/- 133/4			
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value (μF) 0·01, 0·015	a paoreano	7d.	5/2	11/3	38/7	AF116 2/6 18/9 45/- 166/3 OC35 6/- 45/- 108/- 399/-			
0·022 0·033, 0·047		7d. 8d.	5/4 5/11	11/9 12/10	41/8 43/9	BC107 3/6 26/3 63/- 232/9 OC45 2/6 18/9 45/- 166/3			
0.068 0.1		9 d. 9 d .	6/7 6/9	14/1 14/9	47/1 51/-	BC108 3/- 22/6 54/- 199/6 OC71 2/- 15/- 36/- 133/4 BC109 3/6 26/3 63/- 232/9 OC72 2/6 18/9 45/- 166/3 BY234 2/9 24/3 52/4 177/- OC75 2/4 17/6 42/- 155/4			
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0·33 0·47		1/5 1/8	12/6 14/8	27/- 31/9	91/8 107/10	BY237 3/6 30/8 65/6 218/9 OC82D 2/4 17/6 42/- 155/4 BY238 3/9 34/4 71/6 227/6 OC139 3/4 25/- 60/- 221/8			
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39, 47, 56, 6	8, 22, 27, 33 8, 82, 100, 1	20,				$3\frac{3}{4} \times 5$ in. $5/6$ $50/ 114/7$ $3\frac{3}{4} \times 5$ in. $5/6$ $48/4$ $111/5$			
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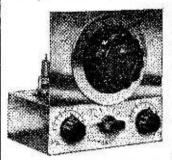
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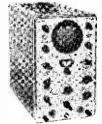
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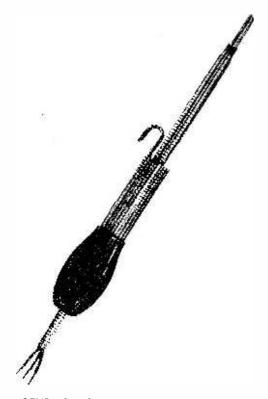
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18021	5/-	2N2923	4/	AD149	11/6	BF117	10/6	MPF103	
18113		2N2924	4/-	AD161	7/6	BF167	5/6	MPF104	
	3/~	2N2925	3/6	AD162	7/8	BF173	7/6	MPF104	
18120	2/6	2N2925 2N2926	010	AF114	5/-	BF173 BF180			
18121	2/6	", Green	3/-	AF114	5/-		7/-	NKT001	3 8/6
18130	2/6	Valler.	v 2/9	AF117		BF181	6/6	NKT216	
18131	2/6	,, Yellow		AF117 AF118	5/-	BF184	7/6	NKT217	
18132	2/6	, Orange	e 2/9		12/6	BF194	5/-	NKT261	4/-
1844	2/-	2N3011	12/6	AF124	4/6	BFX12	4/6	NKT262	
2G301	4/-	2N3053	6/6	AF125	4/6	BFX13	4/6	NKT264	
2G302	4/-	2N3054	12/6	AF126	4/-	BFX29	12/6	NKT271	
2G303	4/-	2N3055	15/-	AF127	3/6	BFX30	9/-	NKT272	
2G371	3/-	2N3702	3/6	AF139	7/6	BFX35	19/6	NKT274	4/-
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2N706A	2/6	2N3708	3/6	ASY27	8/6	BFX87	6/6	NKT613	
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2N1091	6/6	2N3820	23/6	BAX13	2/6	BFY19	4/6	NKT781	
2N1131	6/6	2N4058	5/6			BFY20	12/6	NKT203	
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2N1304	4/6	2N4062	4/6	BC107	3/6	BFY51	4/6	PARTOOT.	
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2N1306	5/-	2N44254 2N4255	8/6	BC109	3/6			NKT801	
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2N1308	6/-	2N4284 2N4285	3/6	BC116	12/6				2/6
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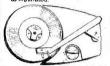
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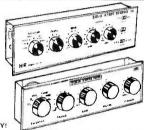
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