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DECEMBEP 1969

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Power supply kit $£ 4.10 .0$ mono or stereo, net
Cabinet kit $£ 2.12 .6$ net. Metalwork available separately from other sources, details on request.

30 WATT (designed by Dr. A. R. Bailey). Published May 1968 W.W., modified November 1968 W.W.

Full kit for main amplifier $£ 9.9 .6$ (less power supply). Transistors only for main amplifier £7.9.6. PC board supplied free with above kit. Heat sinks for output transistors $8 / 6$ extra.
Power supply kit, unregulat --amper 1969 circuit £4.14.0: Regulated version, 60V 1.6 A characteristic: does not nee
3.10.0. T only: 0-25-45-50V 2A 58/. $8 \times 8$ watt Stereo only.
50 mV in to $1 \mathrm{M} \Omega$, output into
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| B9 | NKT163/164 PNP Germ. TO-5 equivalent to $0 \mathrm{C} 44,0 \mathrm{O} 45$. |
| 8924 | NPN. Bil Trans. AO6 $=$ BGX 20 , $2 \mathrm{~N} 2369500 \mathrm{MHz}, 260 \mathrm{~mW}$. |
| ${ }^{\text {B93 } 5}$ | GET113 Trans. equiv. to ACY17 10/- to ACY21 PNP Germ. |
| 6 |  |
| ${ }^{396} 5$ | $\begin{array}{llll}\text { 2N3136 PNP E11. Trans. TO-18, } \\ \text { EFE } & 100 / 300 & \text { I.c. } & 600 \mathrm{~mA} .\end{array}$ |

B98 10 XBII2 and XB102 equiv. to $10 /-$ NKT271, etc.
B99 $200 \begin{gathered}\text { Capacitors, } \\ \text { silver mica, etc. Poot and pack- }\end{gathered} 10 /-$ silver mica, etc.
ing, thim Pak $2 / 6$.

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50 volt
12 volt
12 volt
12 volt
12 volt
10 volt
6 volt

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$\begin{array}{cc}50 \mu \mathrm{~F} & 10 \text { vol } \\ 100 \mu \mathrm{~F} & 12 \text { volt } \\ 100 \mu \mathrm{~F} & 26 \text { volt } \\ 200 \mu \mathrm{~F} & 10 \text { volt }\end{array}$
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BAmp Size $4 \times 3 \times 3$ in. $\begin{array}{rrr}\text { MTT70 } & 6 \mathrm{Amp} & \text { Slize } 4 \times 3 \times 3 \mathrm{in} . \\ \text { MT72 } & 10 \mathrm{Amp} & \text { Size } 31 \times 4 \frac{1}{2} \times 4 \mathrm{in} .\end{array}$ MT72 10 Amp Size $31 \times 4 \frac{1}{2} \times 4 \mathrm{in}$. MT115 20 Amp Size $49 \times 4!\times 4 \mathrm{in}$.

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Controls: Selector switch Tape speed equalisation switch ( $3 \frac{3}{2}$ and $7 \frac{1}{2}$ i.p.s.) Volume. Treble. Bass. 2 position scratch fliter and 2 position rumble filter.

Specification: Sensltivltles for 10 watt output at 1 KHz into 3 ohms. Tape head: 3 mV (at 3 II. p.s.). Mag.P.U.: 2 mV . Cer.P.U.: 80 mV . Tuner: 100 mV . Aux. : 100 mV . Tape/Rec. output: Equalisation for each input Is correct to within $\pm \mathbf{2 d B}$ (R.I.A.A.) from 20 Hz to 20 KHz . Tone control range: Bass $\pm 13 \mathrm{~dB}$ at 60 Hz . Treble $\pm 14 \mathrm{~dB}$ at 15KHz. Total distortion; (for 10 watt output) $<1.5 \%$. Signal noise: $<-60 \mathrm{~dB}$. A.C. mains $200-250 \mathrm{v}$. Built and tested. Size $12 \frac{1}{2} \mathrm{i}$. long, $4 \frac{1}{4} \mathrm{in}$. deep, $2 \frac{3}{4} \mathrm{in}$. high. Teak finished case.


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60 Hz ). Volume Controls: Separate for each channel. A.C. Malns Input: 20060 Hz ). Volume Controls: Separate for each channel. A.C. Malns Input:
$240 \mathrm{~V} .50-60 \mathrm{~Hz}$. Size, $12 \frac{1}{2}^{\prime \prime} \times 6^{* \prime} \times 2 \frac{2}{7}^{\prime \prime}$ in teak finlshed case. Bulit and tested.
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 A new portable cridge oftering exaccuracy at low cost. Ranges: $R$ $\begin{array}{ll}1 \Omega-11 \cdot 1 & \operatorname{meg} \Omega \\ 6 & \text { Ranges } \\ \pm 1 \%\end{array}$ HENRYG 6 Ranges $-2 \%$. C. 10 pF Ranges $+2 \%$. TURNS $\stackrel{ \pm}{\text { RATIO } 1: 1 / 1000-}$ $1: 11100$. 6 Ranges $\pm 1 \%$. Bridge voltage at $1,000 \mathrm{cps}$. Operated from 9 volta. $100 \mu A$. Meter indication. Attractive 2 tone metal case. Size $71 \times 5 \times 2 \mathrm{in}$. \&80. P. \& P. $5 /-$.

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Covering $550 \mathrm{Kc} / \mathrm{s}-30 \mathrm{Mc} / \mathrm{s}$. Incorporates BFO. Built in apeaker and phone jack. Metal cabinet. Operation 220 240V. A.C. Supplied brand new, guaranteed with
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LAFAYETTE SOLID STATE HAGOO RECEIVER 5 BAND AM/OW/BSB AMATEUR AND SHORT WAFE $150 \mathrm{Kc} / \mathrm{s}-400 \mathrm{Kc} / \mathrm{s}$ and $550 \mathrm{Kc} / \mathrm{s}-80 \mathrm{Hc} / \mathrm{s}$ FE T front end 2 mechanical filters Huge dial Product detector Variable BFO Noise limiter 8 meter Zain Bandspread 280V. A.C./1eV. D.C, neg. earth oparawa RF gain control, 8ize $15 \mathrm{in}, \times 8 \frac{1}{2} \mathrm{in}, \times 8$ in. Weight 18 lba EXCEPTIONAL VALUE. \&45. Cerr. 10/8. A.E. for tull details


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First grade quality Moving Coil panel meters. Type MR 38P $21 / 3 \mathrm{in}$. aquare fronts.
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3V. D.C.....27/6
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A.C. VOLTMETER

10 meg. input 10 ranges: $\cdot 01 / \cdot 003 / \cdot 1 / \cdot 3 / 1 / 8 / 10 / 30 /$ $100 / 300 \mathrm{~V}$. +60 dB Decibels +50 dB . supplied new complete with brand and instructions. OperaCarr. $5 /$-.

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 Frequency $0-20 \mathrm{Kc} / \mathrm{s}$. on 2 ranges. Output$500 \Omega$ or $5 \mathrm{~s} \Omega$. Operation $200 / 250 \mathrm{~V}$. A.C.Supplied in perfect order. 818.10 .0 . Carr. $10 \%$

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Each headphone contains a 2 in. wooter and ait in ${ }^{\text {sin. individual }}$ Buit in individual $25-18,000 \mathrm{c} / \mathrm{s}$ with cable and кtereo plug. \$5.19.6. and
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FULL CURRENT RANGE OFFERED BRAND NEW AND GUARANTEED AT YANTASTIC savivas 1025 Mono 87.10 .0 - 81.55 \&11.18.6 1025 Stereo 8715.0 A70 MK 11 212.10.0 1025 Stere 0 27.16.0 ATB0 M K LI E18. 5.0 2025 Stereo $\mathbf{2 7 . 1 9 . 6 \text { *2165 }}$ \&14.14.0 $\begin{array}{lll}\text { 2026T/C } & & \text { AP75 } \\ \text { Mono/Stered } & \text { 48.17.6 } & \text { 401 } \\ \text { 217.17. } & \text { g28. } 7.6\end{array}$ 3000 Stereo 99.18 .6 S108 Carriage/ingurance $7 / 6$ extra any model. WB4
 Bases 28.19.6. Perspex covers 83.10 .0 . *Special offer base and cover avallable for these models at 84.15 .0 . Carr. $5 /$-. Full range of Garrard accessories available


ANSISTOR STEREO AMPLIFIER 19 transistors, 8 diodes, IHF music power, 30 W at $8 \Omega$. Response $30-20.000 \pm 2 \mathrm{~dB}$ at 1 W . DisOutput. 3-10 $\Omega$. Separate $L$ and $R$. volume con trols. Treble and bass control. Eteren phone jack. Brushed alumininm. gold anodised extruded front panel with complementary metal case. Bize 10 a $x$ $39 / 16 \times 713 / 16 \mathrm{in}$. Operation $115 / 230 \mathrm{~V}$. A.C. 208. Carriage $5 / 6$.

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MODEL AS-100D. 100K


MODEL TE-90 50,000 OPV mirror seale overload protection 0/3/12/60/300/600/1200 $\nabla$ DC. $0 / 6 / 30 / 120 / 300 /$
$1200 \mathrm{v} .1 \mathrm{DC} . ~$
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MODEL TE-70. 30,000 OPV, $0 / 3 / 15 / 60 / 300 / 600$ 71200 F BC. $0 / 6 / 30 / 120 \mathrm{j}$ 3/30/300mA. 0/18K $\mathrm{K} / 1 \cdot \mathrm{BM} / 16 \mathrm{Meg}$. $\Omega$.



MODEL PT-34. 1,000 OPV. $0 / 10 / 50$ 1250/500/1,000v AC
and DC. $0 / 1 / 100 /$ 500 m A DC. 0/100K
@. $39 / 6$. P. \& P. $1 / 6$.


TE-800 20,000』/VOLT GLANT MULTLMETER mirror scale and overload protection. 6 in . Pull view meter. al colour scile, of $2 \cdot 5 / 10 / 250 / 1,000 / 5,000$
v AC.
$0 / 25 /[2 \cdot 5 /$ $10 / 50 / 250 / 1,000 / 5,000 \mathrm{v}$. D.C. $0 / 50 \mu \mathrm{~A} / 110 / 100$ $1500 \mathrm{maf} / 10 \mathrm{amp}$. D.C $02 \mathrm{~K} / 200 \mathrm{~K} / 20 \mathrm{MEG}$ OHM.E15. P.\& P. $8 /$

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$221 B$
$19 \cdot 0,100 \mathrm{mFd} .0 \cdot 100-0 \cdot[\mathrm{mFd}$.


LAFEYETTE 57 Range Super 50kn/volt Maltimetor. D.C. Volts 14 mV -1000V. D.C. volis current $25 \mu \mathrm{~A}-10 \mathrm{amp}$. Ohms 0 10 meg $\Omega \mathrm{dB}-20 \mathrm{t} 0+81$ 212.10.0. Carr. $3 / 6$.

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 TRANEISTOK HIGH QUALITY TUNER, AIZE ONLY $6 \times 4 \times 24 \mathrm{~m}$. 1.F. 8 tagon . Double taned discriminator. Ample output to feed mont amplitiers. Operates on 9 Vbattery.Coverage 88 108Mc/s Heady bullt ready for use. Fantaatic value for money. 28.7.6. P. \& P. 2/B Stereo multiplex adaptore $99 / 8$

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NEW SINCLAIR 2000 SYSTEM 35 watt Integrated Amplifier, 389. Carr. $5 /-$ Beli-powered FM Tuner, \&25. Carr. $5 /$

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 Wortable. weight adjuatable vinyl headband. 6it. cable und tereo Jaek plug.
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Unbalanced $T$ and
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CCx3 \& $5 / 6$ \& ELS4 \& $10 / 6$ <br>
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AF1 \begin{tabular}{cc|c}
ACD140 \& $13 /-$ \& <br>
AF117 \& $5 /-$ \& <br>
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AF117 \& $5 /-$ \& C <br>
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\end{tabular} CRS

CRS

CRS \begin{tabular}{lr|r}
AF124 \& $7 / 6$ \& CR <br>
AF127 \& $5 /-$ \&

 

AF127 \& S／－ <br>
AF139 \& $10 /$ \& CR <br>
AF178 \& $12 / 6$ \&

 

AF178 \& $10 / 6$ \& CR <br>
AFY19 $22 / 6$ \& <br>
ASY26 \& $5 / 6$ \&

 

AFY19 $22 / 6$ \& <br>
ASY26 \& $5 / 6$ \& CR <br>
ASY28 \& $5 / 6$ \&

 

ASY28 \& $5 / 6$ \& <br>
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 $\begin{array}{ll}\text { BFY51 } & 5 /- \\ \text { BFY52 } & 4 / 6 \\ \text { BEY2 } & 5 /\end{array}$ $10)^{-}$ MPF104 MPF105 Z Range 

6 K 6 GT \& $8 /-$ \& 12 BE 6 \& 6 <br>
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6 K 7
6 K 7 C $\begin{array}{ll}6 \mathrm{~K} 7 \mathrm{G} & 2 /- \\ 6 \mathrm{~K} 7 \mathrm{GT} & 4 / 9 \\ 6 \mathrm{~K} 8 \mathrm{G} & 4 /- \\ 6 \mathrm{~K} 8 \mathrm{GT} & 7 / 3\end{array}$ 6 K
6 K 8
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£7.19.6 (Carr. 7/6)
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Still ranks as one of the best designs ever. 5 valves, 10 watts, o/p for 3 and 15 ohms.
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£10.10.0 (Carr. 7/6)
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£13. 0.0 (Carr. 7/6)
Basic, with passive control system
£12.10.0 (Carr. 7/6)
Built . . . $£ 15.15 .0$ (Carr. 7/6)
2 Valve Pre-Amp
5 input switching plus auxiliary tone controls, etc.
Kit
£6.19.6 (Carr. 5/6)
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Basic 5-10 Amp and 2 Valve PreAmp
Built and tested $\mathbf{£ 2 1 . 1 0 . 0 ~ ( C a r r . ~ 1 0 / - ) ~}$
$10+10$ Stereo Amplifier
A highly efficient and dependable stereo unit with the best of Mullard and T.R.S. features. $0 / \mathrm{p}$ transformers tapped for 3 and 15 ohms. Can accept ceramic or crystal P.U. direct otherwise pre-amp is necessary.
Kit
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$2+2$ Valve Stereo Pre-Amp
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## T.R.S. 4 + 4 Stereo Amp

Transistor amplifier based on Mullard modules and produced to provide good quality and appearance at low cost. $4+4$ watts output. For $8-15$ ohms speakers. Input switching, etc. Bass and treble controls. Simple module assembly. Amp and pre-amp with front panel and knobs.
Kit
£7.19.6 (Carr. 3/6)
Teak sided cabinet
£1.17.6 (Carr. 2/6)
24V. Power pack f2. 5.0 (Carr. 2/6)
Complete kit inc. DIN plugs and sockets £12.10.0 (Carr. 7/6)
T.R.S. Transistor F.M. Tuner

Assemblies from modules obtainable separately. Features interstation suppression, A.F.C., etc.
Modules and chassis, scale and tuning
drive come to . . £15.15.0 (Carr. 7/6)

Mainspowerunit f2. 5.0 (Carr. 3/-) Cabinet to match " $4+4$ "
f1.17.6 (Carr. 2/6)
Multiplex decoder for stereo
£10.10.0 (Carr. 2/6)
T.R.S. 6 Valve AM/FM Tuner

With power supply, valves, large illuminated station-named scale. Push button on-off and wave change, "magic eye" indicator. Tunes Med. waves and F.M. Diode output for tape.

Kit with power unit
£12.10.0 (Carr. 7/6)
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T.R.S. 12 watt- 15 ohm amplifier as specified in Practical Wireless.
12-12 Stereo amplifier, built $£ 5.19 .6$ Kit, complete
£4.11.0
Sinclair $\mathbf{Z . 3 0 - N e w ~ p o w e r ~ a m p l i f i e r , ~}$
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Pre-amp/tone control .. £9.19.6
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fier and pre-amp.
f2. 9.6
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Kit .. 49 49/6
Built * . . . 59/6

[^0]5-pin piugs, 3/-i 5-pin sockets, 1/6: 3-pin plugs, 3-; 3-pin sockets, $1 / 6$.

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$1 \frac{1}{\mathrm{E}}$ in. dia. Long Spindes. Famous make. All values 5000 ohms-2 Megohms. Guaranteed 12 months.
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Full Range 10 ohms-10 Megohms. (Midget type, modern ratings). $\mathbf{1 0 \%} \frac{1}{4} w$, iw, 4d. ; $\frac{1}{4} w, 6 d$ $20 \%$ 1w, 8d. $2 \mathrm{w}, 1 /-5 \% \mathrm{HI}$ Stab (Cracked Carbon) all pref. values.
10 ohms-1 Meg. $\frac{1}{2} w, 6 d$. $\frac{1}{2} w, 6 d$.
ditto $\quad 1.2 \mathrm{Meg},-10 \mathrm{Meg}$
$10 \%$ iw, 5d.; $\frac{1}{2} w$, ed.
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 TYPESStand. values 25 ohms-10000 ohms
$5 \mathrm{w}, 1 / 6 ; 10 \mathrm{w}, 1 / 9 ; 15 \mathrm{w}, 2 / 3$
SPECIAL VALUES 15K-35K ohms, 5w, 2/6
PRE-SET WIRE WOUND POTS
Slotted Knurled Knob, T.V. Type.
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10t $\frac{1}{2}$ in. die-cast t/table, cueing device and counterbalance. Less cartridge.
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ceramic magnets．freated con low fundamental reso nance．＂$D$＂indicates Tweeter Cone providing extended frequency range providing extended frequency range ohms．Please state cholce．Excep tional performance at low cost
tional performance at low cost
Prices include $\begin{array}{llllllll}\text { HF510L } & 5^{\prime \prime} & 10 W & 57 / 9 & H F 120 & 12^{\prime} & 15 W & 79 / 8 \\ H F R 01 D & 8^{\prime \prime} & 8 W & 59 / 9 & H F 120 D & 1^{*} & 15 W & 89 / 9\end{array}$ HF801D $8^{\prime \prime} 8 \mathrm{8W} 59 / 9$ HF120D 19＊15W 89／8 HF102D $10^{\prime \prime}$ 10W 4 gns．H1～HF126D 12＇ $15 W$ 25．15．0 HIGH FIDELITY LOUDSPEAKER UNITS Cabinets latest style Satin Teak or Airormosia ve neer．Acoustically lined or filled woollen damping Ported where appropriate，credit terms available
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Cone spkr，Imp． 3 or 15 ohms STANWAY II Size 20x10 $\begin{array}{r}\text { C99in．Rating }\end{array}$ 10 watts．Incorporating Fane $13 x 8 i n$ speaker with rubber cone surround and 11，000 line magnet．High flux tweeter Handsome Scandinavian design cabi－ net，Range $35-20,000$ c．p．s．Imp． 15 ohms． 16 Gis．
Gives smooth realistic sound output． GLOUCESTER Size $25 \times 16 \times 10 \mathrm{in}$ ． 12 in ．High flux 12，000 line speaker．Cross－over unit and Tweeter Rating 10 watts．Frequency range $12 \frac{1}{2}$ Gins．
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E2 CABINET Size $17^{*}$ wide $14 t^{*}$ deep， $114^{*}$ high．Cut for TA12
Super 15 Super 30 and other am－ Super 15，Super 30 and other am－
pliffers．＇Roll over＇transp．plas－ pliflers．＇Roll over＇transp．plas－ mosia veneer finish 8 Gits． Inc carr． MOTOR BOARDS cut for Garrard
Turntables and many other units．Price12／9

R．S．C．TA6 6 Watt HIGH FIDELITY SOLID STATE AMPLIFIER
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Red 20,000 c．p．s． 2 dB ．Harmonic Distortion $0.3 \%$ at 1,000 c．p．s．
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30 WATT OUTPUT
＊Garrard SP25 Mk II Turntable on Plinth
＊Goldring Csgo Ceramic P．U．Cartridee with
diamond stylus
ed housing
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Money saving units．Mounted on Pransparent plastic cover Ready to plug into Amplifter or Tape recorder．
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Other types available with Magnetic cartriages and

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FULLY TRANSISTORISED，SOLID STATE CONSTRUCTION HIGH FLDELITY OUTPUT OF 6.5 WATTS PER CHANNEL Designed for optimum performance P．U．cartridge，Radio tuner，Tape re－ corder．＇Mike＇etc．$\star 3$ separate switched input sockets on each chan－ nel $t$ Separate Bass and Treble con－ Speaker Outputch for mono use $\star$ $200-250 \mathrm{v}$ A．C．mains $\star$ Frequency
Response 30－20，000 c．p．s．－2dB＊Harmonic Distortion $0.3 \%$ c．p．s．Hum and Noise－70dB $\rightarrow$ Sensitic Distortion $0.3 \%$ at 1000 100 mV （4） 2 m V．Outputrating I．H．F．M．大 Handsome brushed silver finish Facia and Knobs．Complete kit of parts with foll brushed silver wiring diagrams \＆Instructions．Factory built with $12 \quad 1 / \frac{1}{2} 7 / 9$ mth gntee 16 GNS or Deposit E5．2．6 and 9 mthly -2 GNS． pymts $31 / 6$（Total \＆19．6．0）Or in Teak or Afrormosia veneer hous

## ing 18 Gns．Dep． 2.10 .6 and 9 mLht

Consisting of matched 12 in ．11，000 line 15 watt 15 ohm high quality speaker，cross－over unit and tweeter Smooth response and extended frequency range en sure surprisingly realistic reproduction．E5．15． Or Senior 15 watt inc．HF 126
15,000 line Speaker \＆6．15．0 Carr．6／6
LINEAR L10 HIGH FIDELITY 10W ARPLIFIER 10ans．
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finish．Modern design．Acoustically lined．
Prices Inc．car
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SE8 For optimum performance with any
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## R．8．C．TFM1 SOLID STATE VHF／FM RADIO TUNER

R．8．C．
Total cost of parts
with detailed wiring with detailed wiring diagram tions．
Inc． Inc．
Or fact 4 Gns． 16t gns．Ory built finshed cabinet as illustrated $19 \pm$ gns． Terms：Deposit 25 and 9 monthly pay－
ments 22 ．Total 223 ．


充 High－sensitivity $\star$ 200－250v．A．C．Mains opera－ tion．太 Sharp A．M．Rejection． $\begin{aligned} & \text { D Drift－free recep－} \\ & \text { tion．}\end{aligned}$ Output ample for any amplifier（approx tion．＊Output ample for any amplifier（approx put available for feeding tuning meter．＊Outpu por avaiable for feeding inming meter．Tuner head
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High Grade Components．
Specifications comparable with units costing considerably more．
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OUTPUT 10 Watts R．M．S continuous into $15 \Omega$（per chann
INPUT SENSITIVITIES Mag．P．U． 4 m．V．Ceramic P．U． 35 mV ．Tape Amp Head 2.5 mV ． FREQUENCY RESPONSE $\pm 2 \mathrm{~dB}$ ． 10 $20,000 \mathrm{c} . \mathrm{p} . \mathrm{s}$
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SUPER 15

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 An exce Aly powertu hlfh quatity all-purpose unit for lead,
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$17 / 11$
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$350-0-350 \mathrm{v}, 100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}, 4 \mathrm{a}, 0 \cdot 5-\mathrm{b} \cdot 3 \mathrm{v}, 3 \mathrm{~h}$
 $445 \cdot 0.425 \mathrm{v} .200 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a}$., c.t., 5 v .3 a $425-0.425 \mathrm{v}, 200 \mathrm{mAA} .6 \cdot 3 \mathrm{v} .4 \mathrm{~s} . .6 \cdot 3 \mathrm{v} .3 \mathrm{a} . .6 \mathrm{v}$. TOP 8 IFROUDED DROP-THROUGE TYPE $250 \cdot 16-25 \mathrm{nv}$. $70 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .28 .0 .5-6 \cdot 3 \mathrm{v}, 2 \mathrm{a}$. $250-0-250 \mathrm{v}, 100 \mathrm{~mA}, f \cdot 3 \mathrm{v} .3 \cdot 6 \mathrm{~B}$ $250-0-350 \mathrm{v} .100 \mathrm{~mA},+3 \cdot 3 \mathrm{v} .2 \mathrm{~s}, 6 \cdot 3 \mathrm{v} .1$ $350 \cdot 0.350 \mathrm{v} .80 \mathrm{~mA}, B \cdot 3 \mathrm{v} .2 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{v} .2 \mathrm{a}$ $250-0-250 \mathrm{v} .100 \mathrm{~mA}, 5 \cdot 3 \mathrm{v} .4 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{v}$. 3a $300-0-300 \mathrm{v} .100 \mathrm{~mA}, ~ f \cdot 3 \mathrm{r} .4 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{v}, 3 \mathrm{a}$.
$300-0-300 \mathrm{v}, 130 \mathrm{~mA}, 8 \cdot 3 \mathrm{v}, 4 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{~F}$
 $350-0-350 \mathrm{v} .100 \mathrm{~mA} .6 \cdot 3 \mathrm{v}$ Ampliner
 FILAMENT or TRANEIETOR POWER PACK TYPE $6 \cdot 3 \mathrm{v} .1 \cdot 5 \mathrm{a} .8 / 9 ; 6 \cdot 3 \mathrm{v}, 2 \mathrm{~b}, 9 / 9 ; 6 \cdot 3 \mathrm{v} .3 \mathrm{a}$. $18 / 9 ; 6-3 \mathrm{v}$.
 -8.
CKARGER TRANSFORMERS 0-9-15v 1\%a. 18/9; 2/a. 19/11; 3a.21/11; 5a.25/11; 6a. 89/9; 8a.36/9. AUTO (Step UP/atep DOWN) TRAN8FORYERB $0-110 / 120 \mathrm{v}, 300-230-250 \mathrm{v}$. $\quad .50-80$ watts $19 / \mathrm{g}$
150 wats, $33 / 6 ; 250$ watts $49 / 9 ; 500$ watts $105 /$ OUTPUT TRANSFORMERS
Standard Pentode $5.000 \Omega$ or $7.000 \Omega$ t $03 \Omega$ Prosh-Pull 8 watte FI.R4 to 30 or 15 to 3 Push-Pull 10 watta $6 \mathrm{~V}^{\prime} 9 \mathrm{ECL} \mathrm{H} 6$ to 3.5 .8 or or 150 14/9 Push-Pull Ultra to 3 urear for Mullard 510 etc $\quad 23 / 9$ Push-Pull 15.18 watts, sectionslly wound 6L.f, KT66, ctc., for 3 or 150
Push-Pull 20 watt high quality bectinnaity
wound EL. 34 . $6 \mathrm{LG}, \mathrm{K}$ T66 etc. to 3 or $15 \Omega$.. SMOOTHING OHOKR8
$150 \mathrm{~mA}, 7-10 \mathrm{~F}, 250 \Omega$ 12/9: $100 \mathrm{~mA}, 10 \mathrm{H}, 200 \Omega 10 / 8$; $80 \mathrm{~mA}, 10 \mathrm{H}, 350 \Omega 8 / 8 ; 60 \mathrm{~mA}, 10 \mathrm{H}, 400 \Omega 4 / 11$.
$24 / 9$
$39 / 9$
$47 / 11$
$39 / 9$
$47 / 9$ $89 / 9$
$93 / 9$ 9219
$23 / 8$
$27 / 8$ $28 / 9$
$29 / 11$ $39 / 8$ 46/9 9

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## TOPIC OF THE MONTH

## Regarding Rallies

NOW that the season's spate of mobile rallies is over, it seems in retrospect that there is a large scope for improvement. While admitting that some rallies are parochial and others organised on a grander scale, thus providing a desirable degree of difference, it seems to us that more cohesion would not come amiss.

A central organising body would overcome many of the current defects. Such a body would provide maximum publicity, select the most suitable dates, avoid clashing of events, maintain a better standard and ensure that the calendar contained everything from small local events to large National Mobile Rallies. Events could be arranged to take place in the right part of the country at the right time.

We would like to see more co-operation between clubs in a particular area who could get together as a group and put on a really impressive show, not just a village fête in the back-of-beyond. We would like to see adequate signposting: G3JDG once described the signposts for the Harlow rally as "sweetpapers hidden in hedges", and even this was perhaps too charitable. An organising body could take care of these things and perhaps arrange for commercial organisations to sponsor certain events; for example, if one of the motoring organisations (RAC or AA) is convinced of a large turn-out, its support in signposting can be relied on.

And the tightening up of rally programmes would ensure that they were planned with a bit more imagination. At the moment too much is left to chance and it seems to have escaped many clubs that a rally is partly a family affair. All too often the YLs, XYLs and sprigs sit in cars, bored stiff, waiting for the time to go home. We want more efforts like the Woburn Abbey rally where there is plenty to amuse the family as well as the enthusiast. We would like to see more rallies coupled with open days of suitable establishmentsthe Services, industry and broadcasting. As for a central co-ordinating body, our national society is the natural choice, so how about it RSGB ?
W. N. STEVENS—Editor.

## NEWS AND COMMENT

Leader ..... 573
News and Comment ..... 574
MW Column by C. Molloy ..... 581
Letters to the Editor ..... 582
On the Short Waves by Malcolm Connah and David Gibson, G3JDG ..... 585,586
Practically Wireless by Henry ..... 599
CONSTRUCTIONAL
A Stereo Decoder by F. C. Judd ..... 576
Pedal Steel Guitar, Part 2 by F. C. Judd ..... 589
Miniature Audio Amplifier by T. Bölstad ..... 594
Injectrace by Hal Moorshead ..... 596
I.C. of the Month, Short Wave Converter by L. A. J. Ireland ..... 600
Low Cost Valve Amplifier by R. J. Winfrow ..... 602
Take 20, Intercom by Julian Anderson ..... 604
Audio Noise Limiter by $M$. Wallis ..... 613
L.C. Measurements by W. D. Watkins ..... 621
OTHER FEATURES
Experimenters' Corner, Designing Class A Transistor Output Stages by C. R. Boggis, M.A.P.A.E. ..... 606
Basic Semiconductor Technology. Part 7 by M. F. Docker, M.Sc. ..... 609
P.W. Guide to Components, Part 12 by M. K. Titman, B.Sc. ..... 617
JANUARY ISSUE WILL BE PUBLISHED
ON DECEMBER 5th

[^1]
# news And comment 

## THE THIRD HAND



We are informed by the Coventry Movement Co. Ltd. that they are the manufacturers of the "Multi-Mini" universal vice and stand. This is an ideal device for holding a printed circuit board or components when soldering is taking place. In fact it acts as the "third hand" that many of us wish we had when we are constructing. Price of the Multi-Mini Universal Vice and Stand is 67 s . 6d. There is also a model called the Multi-Mini Twin which is basically the same but has an extra set of jaws. Price of this model is $£ 518 \mathrm{~s}$. It should be possible to obtain both these units at tool stores but should difficulty be experienced, the manufacturers will be pleased to supply direct for a P.P. charge of 3 s . extra on each model. The Coventry Movement Co. Lid., Burnsall Road, Coventry. Tel: OC03 74364.

## LIGHTING UNITS



The DJ.10L ( $£ 19$ 10s.) and the DJ.30L (£37 10s.) are light control units. Both units feature dual input sockets for front or rear connections, plus an override switch so that the lights may be left permanently on. Cabinets are made for panel mounting.

DJ.10L makes lights flash on and off with the music; DJ.30L is however a more sophisticated unit with three channels which enable bass, middle and treble frequencies from the amplifier to be operated individually as required. The maximum.wattage that each channel will take is $1,000 \mathrm{~W}$ in the "flashing
lights" position or 600 W in the "lights on" position with all three channels working simultaneously. D. J. Electronics (Hackney) Ltd., 170 Albion Road, London, N. 16.

## APAE moves Exhibition to

 LondonIt has been found necessary to find a suitable venue to house more exhibitors in larger stands and easier access for visitors from home and abroad for the Assoc. of Public Address Engineers' Exhibition.

The exhibition will be known as "Sound '70 International" and will take place at Camden Town Hall, opposite St. Pancras Station in Euston Road, London N.W. 1 from 10th-12th March, 1970, 10 a.m.- 5.30 p.m. daily. As in other years stress will be made on the educational theme as well as being a selling and viewing exhibition. Various lectures will take place during the show. The sponsor is the Association of Public Address Engineers.

## "SEMICONDUCTOR DEVICES"

The third booklet in the series of "minibooks" published by the Mullard Educational Service is entitled Semiconductor Devices. It is intended as an introduction to the subject which, being treated non-mathematically, should be easily understood by anyone with a basic knowledge of electronics.
The booklet starts with a description of germanium and silicon and shows how they can be made into n - or p-type material by the addition of minute amounts of other elements. Explanations are given of the action of the $p-n$ junction in a diode and the $\mathrm{p}-\mathrm{n}-\mathrm{p}$ or $\mathrm{n}-\mathrm{p}-\mathrm{n}$ arrangement in a transistor. The currentamplifying property of a transistor is explained and several basic transistor circuits are included.

The booklet then describes briefly how various transistors are constructed and has a section on transistor characteristics. In the final section other solid-state devices, such as phototransistors, thyristors, thermistors, f.e.t.s., and Gunn' "diodes", are outlined. The booklet ends with a short description of integrated circuits.

Semiconductor Devices should be of interest to all students. and apprentices as well as lecturers and teachers of electronics in schools, technical colleges and other training establishments. Priced at 5 s. (including packing and postage), it can be obtained from the Mullard Educational Service, Mullard House, Torrington Place, London, W.C.I. Cash should accompany orders.

## RAILWAYMEN'S RADIO CLUB

I am a licensed Radio Amateur working for the railway at the town of Eastleigh which is 7 miles north of Southampton. I am trying to form a radio club of railwaymen but they are very hard to contact because of shifts etc.

If railwaymen in the Basingstoke, Fareham, Eastleigh, Southampton and Bournemouth areas would contact me, we may well be able to get a club going. R. Mannion, G3XFD, 23. Marston Road, Thornhill, Southampton, Hants. Tel: West End $385 /$.

# nEWS ADD comment... 

## BBC SCHOLARSHIP

The Engineering Division maintains six research scholars at United Kingdom universities, and is awarding one scholarship this year. The scholarships are intended to provide the opportunity for selected honours graduates to work for a higher degree, the subject chosen for post-graduate study being within those fields of physics or engineering which have an application to radio or television broadcasting.

Mr. P. A. Ratliff graduated with first-class honours in electronic engineering from the University of Birmingham in June this year. He has been awarded a three-year BBC Research Scholarship to undertake research in the Department of Electronic and Electrical Engineering, University of Birmingham, under Professor D. G. Tucker, D.Sc., F.I.E.E. The subject of Mr. Ratliff's study is "an aerial system designed to combat multipath fading in VHF mobile communications, using existing AM receivers", and his supervisor will be Professor E. D. R. Shearman, B.Sc., F.I.E.E.

IC Breadboards from SDC

S.D.C. Products (Electronics) Ltd. now have in their range of modular solderless breadboarding systems, two new DeCs specifically designed to accommodate integrated circuits as well as modern shortlead discrete components and to have an increased contact capa-bility- 208 contact points per DeC -as compared with the original S-DeC which is of more limited capacity.

The new $\mu$-DeCs, primarily for integrated circuits, can accommodate two 16-lead DIL stations or four 10-lead TO5 stations. The new T-DeCs, primarily for discrete components, can also accommodate one DIL station or two TO5 stations. S.D.C. Products (Electronics) Ltd., 34 Arkwright, Astmoor Industrial Estate, Runcorn, Cheshire.

## MAGNETIC TAPE ON CINE FILM



Supersound Electronic Products announce their new powered film striper. This is a machine that puts a piece of magnetic tape 0.0315 in . (standard-8 film) or 0.026 in . (super-8) down the side of the film so that a sounditrack can be recorded. The new striper incorporates a footage counter and a power rewind which enables the film to be quickly rewound after it has been striped with tape. Models are available for super/standard-8 (dual gauge), 16 mm ., and 9.5 mm . The 8 mm . version (see picture) has a total film capacity of 800 ft . and the price for a kit which consists: Striping machine, 800ft. of Superstripe magnetic tape, loz. bottle of adhesive, loz. bottle of film cleaner and full operating instructions, is $£ 40$.
Less sophisticated models are available for $£ 1210 \mathrm{~s}$, and $£ 1311 \mathrm{~s}$. For further details, contact: Supersound Electronic Products. $1 / 4$ Mount Pleasant Road, Hastings, Sussex. Tel. Hastings 5647.

## SPRAY-ON POWER

Gould Ionics, an American company, have developed a "spray-on" battery. It can be sprayed on to a printed circuit board in thicknesses down to one-thousandth of an inch. It is also possible to recharge it!

It is formed by first spraying on a silver-carbon electrolyte anode, then a rubidium-silver-iodine electrolyte. After this a specially developed iodine-free cathode is fitted.

A 3-cell 1.5 V battery, threehundredths of an inch thick has been sprayed on to a camera flash tube, illustrating one usage.

The absence of iodine in the cathode is important as it is the diffusion of iodine that shortens the life of other batteries. Current is at the moment limited to $200 \mu \mathrm{~A}$ per square centimetre.

Another future application is where a new battery can be selectively sprayed on different portions of a circuit board providing miniaturised isolated power supplies.

## IC FM TUNER KIT



We now show a photograph of the IC FM Tuner kit mentioned first in News and Comment October 1969 issue. The kit sells at $£ 9$ 19 s . 6d. plus 5 s . complete with drilled and tinned printed circuit board, fully illustrated booklet and all necessary components.

## GOLDRING SERVICE AND SPARES

The service and spares department of the Goldring Manufacturing Co. (Great Britain) Ltd., 486-488 High Road, Leytonstone, London, E.ll now has a new telephone number 01-539-4208.

TEREOPHONIC f.m. transmissions are at present available to listeners in the UK service areas of the BBC transmitters located at Wrotham, Sutton Coldfield, Holme Moss and Swingate and certain of their relay stations. In order to hear these programmes "stereophonically" a v.h.f./f.m. receiver with a special "decoder" is necessary as the BBC use the "pilot tone" stereo transmission system commonly employed by many European. American, Canadian and Japanese broadcasters. In this system the left- and right-hand channels are "encoded" at the transmitter by a multiplexing process and transmitted on a common frequency. The signals for the respective channels are "decoded", after detection at the receiver. The system is compatible, which means that receivers without a decoder will receive and produce a "monophonic" version of the stereo transmission. An adapted receiver, i.e., one with a decoder will automatically receive and produce a monophonic output from a monophonic transmission and/or a stereophonic output from a stereophonic transmission.

Monophonic transmission of stereo (left- and right-hand channels) involves only adding the signals of the two channels which can be transmitted and

# a stereo decoder F.C.JUDD 

received in the normal way. For stereo reception however, additional information is necessary in order to separate the left- and right-hand channels. In the system employed by the BBC (the Zenith-G.E. system) the additional information consists of a difference signal-left minus right-which is transmitted as the upper and lower sidebands of a 38 kHz sub-carrier. The sub-carrier itself is totally suppressed. To ensure synchronisation between the receiver "decoder" and the transmitter "encoder", a low level synchronising signal of 19 kHz , the pilot tone, is also transmitted.

## Circuit for a decoder

The circuit described in this article can be used with almost any f.m. tuner with a transistor or valve diseriminator. The circuit is due to Mullard Limited (Central Technical Services) and the writer is indebted to both Mullard Limited and the BBC for permission to quote from their respective publications.

In the decoder circuit shown in Fig. 1 the pilot tone is extracted from the multiplex input by means of a 19 kHz tuned circuit ( $\mathrm{L} 1 / \mathrm{C} 2$ ) immediately fol-



## The author's completed decoder.

lowing the discriminator output. The pilot tone is then amplified by Tr 1 and applied to the base of Tr 2 which is biased to operate in class B condition, i.e., only the positive half-cycles of the pilot tone are amplified. The distorted waveform resulting from this form of amplification is rich in second harmonic content ( 38 kHz ) which is extracted by means of a tuned circuit ( $2 / 2 / \mathrm{C} 6$ ) in the collector of Tr 2 . Note that the peak-to-peak amplitude of the 38 kHz signal between the collector end of the coil and the tapping (pin 4) is limited to approximately twice the supply voltage. Hence its amplitude is constant once a certain input level has been exceeded.

The centre tapped secondary (L3) applies antiphase switching signals to the emitters of $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$ whilst the complete multiplex information is applied
to the bases. With this arrangement, synchronous detection to obtain the difference signal, together with matrixing of the sum and difference signals occurs, and the now separated left- and right-hand signals appear respectively at the collectors of Tr3 and Tr4. However, with a simple decoder operating as described, only a limited separation is obtained. The circuit of Fig. 1 contains additional arrangements to improve separation which is done by introducing a controlled amount of crosstalk into the two outputs and in antiphase to the inherent crosstalk.

Although conventional de-emphasis occurs in the collector circuits of $\operatorname{Tr} 3$ and Tr 4 this is insufficient to remove the 38 kHz waveform from the output. Any strong residual 38 kHz signals could produce distortion in a following audio amplifier or produce spurious whistles on a tape recording by beating with the bias oscillator in the tape recorder. Parallel-T filters are therefore included to reduce the 38 kHz signal at the decoder outputs to a more or less negligible amount.
In the absence of a 38 kHz switching waveform, i.e., during monophonic transmissions, the switching transistors $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$ are biased to operate in class A and any signal applied to their bases is reproduced at their collectors. The circuit is therefore compatible and requires no switching from stereo to mono operation.

## Indicator lamp

Stereo transmissions are directly indicated by means of a lamp which lights when the 19 kHz pilot tone is present in the transmission. The signal for driving the stereo indicator lamp is actually taken from the 38 kHz output at the junction of R 7 and L2 in the collector circuit of Tr2. This signal allows Tr5 to conduct and pass sufficient current $(20$ to 30 mA$)$ to light the lamp in its collector circuit. Note that the h.t. voltage required to operate the stereo indicator lamp is 24 V assuming the use of a 24 V 20 mA lamp as originally specified for the Mullard circuit. The decoder itself requires an h.t. rail of only 12 to 14 V and could be run from this potential if the indicator circuit and its lamp is omitted. The indicator light is however a valuable asset to reception and to the alignment of the decoder and is therefore best retained.


Fig. 2: Assembly board and support rails.


Fig. 3a: (above left) Output socket assembly.
Fig. 3b: (above) Input socket assembly.

Fig. 4: (left) Input socket panel.

## Construction

The entire decoder (except the power supply) could no doubt be accommodated as a much smaller assembly board than that shown in Fig. 2. The use of a fairly large board makes layout a little easier and in fact by extending the length of the board the small 24 V power supply might also be included as well. No details for a box of any kind have been given as constructors may wish to mount the unit in some existing form of cabinet perhaps containing the f.m. tuner and amplifier So long as the input and output leads are screened there should
be little trouble with hum pick-up but precautions should be taken by keeping the unit away from leads carrying mains voltages and from large mains transformers.

As shown in Fig. 2 the s.r.b.p. perforated assembly board is mounted on $\frac{1}{2} \times \frac{1}{2}$ inch aluminium angie which gives support to the board and could be used for mounting purposes. Attached to one end of the board as in Fig. 3a is the output socket panel, also mounted on $\frac{1}{2} \times \frac{1}{2}$ inch aluminium angle as in Fig. 3b. The input socket panel (Fig. 4) is mounted directly on one side of the main assembly as shown in Fig. 2.

The component layout for use with Mullard decoder coils type WF2949 (19kHz-L1) and WF2951 $(38 \mathrm{kHz}-\mathrm{L} 2 / 3)$ is shown in Fig. 5. Note that the pin connections are as seen when looking at the base of the coils (through the board) and as also shown in Fig. 6. The reference as to orientation on the board itself is the earthing tag pin 8 . Note that these coils cannot be obtained direct from Mullard Limited, but are available from Gurneys Radio Limited, 91 The Broadway, Southall, Middlesex. Those who decide to use the alternative coils by Henry's Radio Limited, 303 Edgware Road, London, W.2, should use the layout and wiring shown in Fig. 7 and then continue as in Fig. 5. The Henry's decoder coils which are known by frequency, i.e., 19 kHz and 38 kHz respectively, are identical to the other coils in characteristics but the pin connections are as shown in Fig. 6. If these coils are used the reference for orientation is the earthing tag on the metal clamp.

## Power supply

A circuit for a suitable 24 V power supply is shown in Fig. 8 and a schematic for assembly in Fig. 9. As previously mentioned the power supply could be assembled on an extension of the main component board or separately on a small chassis of its own.

When assembly has been completed preliminary tests should be made. Check the h.t. current at the point marked $X$ in the circuit Fig. 1. This should be approximately 2.5 mA if the h.t. is 12 to 14 V and in this case no alteration to the value of R 24


Fig. 5: Wiring and layout of decoder (Mullard Coils).
( $4 \cdot 7 \mathrm{k} \Omega$ ) should be necessary. If an audio generator capable of providing a sine-wave output of approximately 50 mV at 19 kHz is available, a preliminary tuning check on L1 and L2/3 can be carried out. Couple the generator to the input of the decoder and on tuning the coils with the integral tuning slugs, it should be possible to light the stereo indicator lamp. If an r.m.s. reading valve or transistor voltmeter is available further checks can be made as follows. With approximately 50 mV of 19 kHz signal at the input of the decoder the r.m.s. voltage of the 38 kHz signal between the junction of R 7 and L2 and earth should be around 4V. The signal at either side of L3 to earth should be approximately 400 mV . If an oscilloscope is available examination of the waveforms at the input and at the junction of R7 and L2 should show whether or not the 38 kHz signal is being developed.

## components list

## Resistors:

| R1 | 22k $\Omega$ | R10 $1 \mathrm{k} \Omega$ | R19 1.8k $\Omega$ |
| :---: | :---: | :---: | :---: |
| R2 | $10 \mathrm{k} \Omega$ | R11 1k $\Omega$ | R20 18k $\Omega$ |
| R3 | $10 \mathrm{k} \Omega$ | R12 $56 \mathrm{k} \Omega$ | R21 18k $\Omega$ |
| R4 | $10 \mathrm{k} \Omega$ | R13 100k $\Omega$ | R22 150k $\Omega$ |
| R5 | 220ת | R14 12k $\Omega$ | R23 150ks |
| R6 | $4.7 \mathrm{k} \Omega$ | R15 12k $\Omega$ | R24 4.7k $\Omega$ |
| R7 | 100ת | R16 1.8k $\Omega$ | R25 15k |
| R8 | $3.9 \mathrm{k} \Omega$ | R17 1.8k $\Omega$ |  |
| R9 | $1 \mathrm{k} \Omega$ | R18 1.8k $\Omega$ |  |

Potentiometer: VR1 $1 \mathrm{k} \Omega$
Capacitors:

| C1 | $0.01 \mu \mathrm{~F}$ | C12 | $0 \cdot 005 \mu \mathrm{~F}$ |
| :---: | :---: | :---: | :---: |
| C2 | 470pF (s.m.) | C13 | $0.002 \mu \mathrm{~F}$ |
| C3 | $0.1 \mu \mathrm{~F}$ | C14 | $0.002 \mu \mathrm{~F}$ |
| C4 | $0.01 \mu \mathrm{~F}$ | C15 | $0.002 \mu \mathrm{~F}$ |
| C5 | $10 \mu \mathrm{~F}$ Elec. 25 V | C16 | $0 \cdot 002 \mu \mathrm{~F}$ |
| C6 | 470pF (s.m.) | C17 | 220pF (s.m.) |
| C7 | $10 \mu \mathrm{~F}$ Elec. 25 V | C18 | 220pF (s.m.) |
| C8 | $0.005 \mu \mathrm{~F}$ | C19 | $0 \cdot 1 \mu \mathrm{~F}$ |
| C9 | $0.005 \mu \mathrm{~F}$ | C20 | $0 \cdot 1 \mu \mathrm{~F}$ |
| C10 | $10 \mu \mathrm{~F}$ Elec. 25 V | C21 | $0.01 \mu \mathrm{~F}$ |
| C11 | ${ }^{2} 0.005 \mu \mathrm{~F}$ |  |  |
| Transistors:Tr1 |  | DiodeD1 |  |
|  |  | Mullard OA91 |
| Tr2 | Mullard BC108 |  |  |  |
| Tr3 |  |  |  |
| Tr4 |  |  |  |
| Tr5 | Mullard BC107 |  |  |

## Coils:

L1 19kHz—Henry's Radio or MullardWF2949Gurneys Radio
L2 38 kHz -Henry's Radio or Mullard WF2951Gurneys Radio

## Miscellaneous:

Indicator lamp 24V $20 / 30 \mathrm{~mA}$; 3 single phono sockets; perforated s.r.b.p. assembly board; $\frac{1}{2} \times \frac{1}{2}$ aluminium angle etc.

## Power supply:

Transformer T1 (Henry's Radio CT1) Pri 230V with tapped secondary for 15 to 18 V .
Rectifier MR1 Contact cooled type 1 H3
Capacitor C1 Elec. $2500 \mu \mathrm{~F} 30 \mathrm{~V}$ working


Fig. 6: Outlines and connections of available coils.


Fig. 7: Coil wiring for Henry's Radio decoder coils.

## Coupling to an F.M. tuner

## output

The input impedance of the decoder is approximately $15 \mathrm{k} \Omega$ and it may be fed directly from a transistor discriminator capable of providing a loaded output with a peak-to-peak amplitude of approximately 750 mV . The decoder may also be fed from a valve discriminator in which case the output will probably have to be attenuated by a series resistor and shunt capacitor. This arrangement not only provides the correct input level at all multiplex frequencies but also reduces the discriminator loading to an acceptable value. The series resistor may be between $3.3 \mathrm{k} \Omega$ and $33 \mathrm{k} \Omega$ and the capacitor around 300 pF . As an example, a resistor of $15 \mathrm{k} \Omega$ shunted by 300 pF was found just about right when the decoder was operated from a Heathkit (valve) f.m. tuner.

The actual point of signal take off from the tuner


Fig. 8: Circuit of the power supply.


Fig. 9: Power supply assembly details.
is best made directly at the output from the discriminator circuit, i.e., before the de-emphasis network which should be disconnected. The circuit of Fig. 10 is the discriminator of a Heathkit tuner used for subjective testing of the decoder and is typical of those employed in f.m. tuners using valves. The circuit of Fig. 11 shows the discriminator of a transistorised tuner and again is typical of those at present in use.

## Alignment of the decoder

For initial alignment any stereo transmission can be used and the procedure is as follows. Connect a potentiometer of at least $50 \mathrm{k} \Omega$ across the discriminator output and connect the decoder input to the slider of the potentiometer which should now be set to maximum value. Tune the receiver to a stereo broadcast (Radio 3) and carefully and slowly adjust the 19 kHz and 38 kHz coil slugs for maximum brightness of the stereo indicator lamp. (The preliminary test with an audio- signal generator mentioned earlier should have produced the same result, i.e., maximum brilliance of the indicator lamp.) Next adjust the potentiometer until the lamp just glows and then re-set the coil slugs again to produce maximum brightness. Repeat this procedure until any further adjustment of the slugs produces no further increase in brightness. The two coils are now reasonably well aligned. should the slugs fail to tune the coils sharply at approximately their mid-position of travel it may be necessary to alter the value of C2 and/or C6, as the case may be, to 390 pF .

When this alignment procedure has been completed disconnect the potentiometer, re-connect the decoder to the discriminator output and adjust the pre-set control VR1 ( $1 \mathrm{k} \Omega$ ) to its mid-position, i.e., slider halfway round. The decoder should now give a reasonable degree of separation but should now be finally aligned with the help of the BBC test tone
transmissions which are transmitted every Wednesday and Saturday at 11.30 p.m. ( 2330 hrs.) on Radio 3 v.h.f./f.m. Full details of the various tests can be obtained free by writing to the BBC Engineering Information Department, Broadcasting House, London, W1A 1AA. Ask for: Information Sheet No. 1605(2) May 1969 Stereophonic Broadcasting, Test Tone Transmission.

The test tone transmissions will facilitate identification of the left- and right-hand channels which should be done with the decoder output connected to the stereo amplifier. Now, when the left-hand channel only is being transmitted disconnect the left-hand amplifier channel and adjust the 38 kHz tuning slug very slowly anti-clockwise (as viewed from the top of the coil) until the output from the right-hand loudspeaker is at minimum. Anti-clockwise rotation of the slug is necessary because a false minimum will be obtained with clockwise rotation.

Next re-connect the left-hand amplifier channel and when the right-hand channel only is being transmitted disconnect the right-hand amplifier channel and adjust the preset (VR1) to produce minimum output from the left-hand loudspeaker. Reconnect the right-hand amplifier for normal stereo and note that the stereo indicator light will have been on as during any stereo transmission. It does not glow during monophonic transmission.


Fig. 10: Typical discriminator output (valved tuners).


Fig. 11: Typical discriminator output (transistorised tuners).

## Performance

The decoder, exactly as per the circuit in Fig. I. was tested with both valve and transistor f.m. tuners. It was aligned as described above on BBC transmissions and by means of special laboratory stereo test equipment. The performance was quite in accordance with the Mullard specification. Channel separation is around 30 dB and the decoder has a good signal-to-noise performance. It is worth noting however, that as the signal-to-noise ratio of a stereo broadcast is slightly lower than that of a monophonic broadcast a good f.m. aerial should be used to maintain the best reception signal-to-noise level. The average audio signal output per channel is around 400 to 500 mV and should be more than sufficient for the "tuner" input on stereo amplifiers. The impedance of the amplifier inputs should preferably be not less than $50 \mathrm{k} \Omega$.

The following BBC Engineering Information Sheets may also be of interest to those contemplating stereo broadcast reception: Information Sheet 1603 (6) April, 1969-Stereophonic Broadcasting. Information Sheet IIO2(4) May, 1969-VHF Radio Receiving Aerials. Stereo $Q$ and $A$-This leaflet deals generally with stereo broadcast reception and can be obtained, as the other leaflets, free of charge from the BBC Engineering Information Department at the address previously given.

## PRACTICAL TELEVISION in the DECEMBER issue

## * LINEAR TIMEBASES

Generating a linear scanning waveform is not simple. The basic waveform produced by the charge or discharge of a capacitor is exponential. A number of intriguing circuits have been devised at various times to overcome this basic deficiency and in the December issue we shall start to examine timebase circuits such as the bootstrap. Miller, transitron, phantastron and sanatron.

## $\star$ TEST EQUIPMENT LIMITATIONS

A meter never lies-but do you know how to interpret readings correctly? The basic limitations of commonly used test equipment are explained to enable you to avoid the pitfalls caused by misunderstood readings.

## $\star$ TV FILTERING CIRCUITS

Filters are found throughout television circuits, in the power supplies, i.f. sections, a.g.c. feeds and so on. This aspect of television receiver circuitry is highlighted with explanations of how filters act and the different types used, including those found in the chrominance sections of colour receivers.
$\star$ SERVICING THE THORN 1400 CHASSIS The Thorn/BRC 1400 chassis has been used in a very large number of models from 1967 to the present time. L. Lawry-Johns takes a look at this chassis and the common faults associated with it.

## PLUS ALL THE REGULAR FEATURES on sale

NOVEMBER 21st

CONDITIONS on the medium waves have been good throughout the summer in spite of occasional fadeouts. Johannesburg 1286 was logged on the 22nd June by Glyn Morgan of Tredegar. A good effort Glyn, not many of us have heard this one. Latin American reception was excellent in June and July. Brazilians such as PRA3 860, PRF4 940, PRE8 980 all in Rio de Janeiro and PRB9 1000, PRG9 1100 in Sao Paulo were particularly prominent just before sunrise. Reception of the West Coast of the United States came on 1st September at 0431 hrs. GMT when the writer logged KOMO 1000 in Seattle. The following morning KFBK 1530 Sacramento, California was heard as a background to WCKY by a DXer in Cumberland.

Ramadan starts on 11th November this year. During this four week period many radio stations in the Arab world remain on the air all night, providing the DXer with the opportunity to log countries that otherwise would rarely be heirrd. Among the more prominent signals are Morocco on 593 and 837 (Ouijda), 611 (Sebaa Aioun), 935 (Agadir), 1115 and 1232 (Tangier); Algeria with 529 (Constantine), 548 (Oran), 890 and 980 (Algiers): Tunisia on 629 and 962 (Tunis): Egypt with 557 and 773 (Cairo), 620 (Batra). More difficult countries are Libya 674 (Benghazi), 1052 (Tripoli): Saudi Arabia 588 and 647 (Riyadh), 602 and 723 (Jeddah); Jordan 800 (Amman); Syria 566, 665 and 785 (Damascus). 746 (Aleppo): Lebanon 836 (Beirut): Iraq 760 and 908 (Baghdad); Kuwait 1345; Iran 777 (Zahadan), 1390 (Ahwaz). The late evening onwards is the time to look for these stations.

It is now generally agreed that the sunspot maximum has been passed, so we can look forward to a steady improvement on the medium waves possibly with some DX from the Far East. There are two periods of the day for FE reception in the UK. The first is in the afternoon in winter, an hour or so before sunset. Stations to look for include the Voice of America stations in Okinawa on 1178 kHz and in the Philippines on 920 (Malolos) and 1140 (Poro). The programmes from these stations are mainly in Far East languages but station identification is usually in English on the hour and half-hour. Okinawa can be heard behind Horby Sweden when conditions are good, sometimes with news in English. The second period occurs after midnight when All India Radio is often heard on 1070 kHz (Rajkot). Others to look for are Jullender 710, Lucknow 910, Delhi 1020, Bikanar 1330. A.I.R. Rajkot has a news bulletin in English at 0110 hrs. GMT which helps with identification. Do not be misled if you hear Indian music on 760 kHz , it will be from ZFY in Guyana. There is a large Indian population in this South American country and Radio Demerara carries special programmes for them.

The new BBC relay station in Masirah Island has been heard on 1410 kHZ with sign off at 2115 hrs . GMT. This station is a replacement for Perim Island which was part of the Aden Protectorate. Masirah relays the BBC World Service.

CHARLES MOLLOY

## Useful Tips

Having read the article in the October issue of Practical Wireless, "Printed Circuit Design", I would like to point out two labour-saving tips.

First of all, having established the final design this can indeed be transferred to the copper laminate board by means of carbon paper, but I have found from practical experience that Sellotape masking can be omitted. Provided one has a fairly steady hand the outline of the design can be painted with a small paint brush using nail varnish. After etching, nail varnish remover can be used. Secondly, I am doubtful whether the best solution to feedback path problems really is a link wire. For v.h.f. work, for instance, the mechanical nature (and capacitative effect) of such a dodge could result in instability. Better to puzzle the link out in the design and remember the copper laminate path need only be, say, $\frac{1}{8}$ in. wide. This is probably narrow enough to pass between two adjacent paths.-D. M. Aldridge (Co. Durham).

## When is a dB not a dB ?

Mr. Mitchell made some valid points, "Ex-Meter" October Practical Wireless, but the actual situation is even worse. The idea of using an S scale for signal reports, stands or falls on using a standard number of dB's per $S$ point. This is not done in practice. "Home-brew" apart, manufacturers use various ratios for their meter calibration, some use 3 dB per point, others use 6 dB 's per point, while the "cheap" receivers use almost anything. In such circumstances, $S$ reports can be meaningless for any real useful purpose. For example, a station requires a report on an aerial's efficiency, two other stations reply. One says " S 9 here O.M.", the second says "S6 here". O.K. so far, but! the first station's meter is calibrated at 3 dB per point, while the second is 6 dB per point. So we have the position where the " $S 9$ " is actually 27 dB . while the "S6" is 36 dB . What a hopeless situation and of harm to the experimenting station's
efforts. However, a meter can be of great help when used purely as a "comparative indicator" during experiments. If the meter is set to mid-scale (whatever type of calibration is used) on the signal any change in level can be observed and reported as a percentage of the original reading. A much more helpful report than "slavish" S reports. Decremental modulation and comparison between the side-bands on a.m. is observable, plus other effects, using a meter. So if one wishes to be of help, do use a meter, but allow for its drawbacks in practice. the average $S$ meter is only useful for comparative reports and nothing more.-M. J. Shepherd (Essex).

## Beware!!

Regular readers of your magazine will certainly be wary of purchasing semiconductors "on the cheap" if good results are expected, but there would appear to be no guarantee of quality even when full prices are paid to some well-known suppliers. On several occasions I have dismissed the odd "dud" when only a couple of shillings has been involved, but I have recently come unstuck to the tune of nearly $£ 3$ and am fast losing confidence in ordering semiconductors by post. In this instance, the semiconductors involved were some fairly expensive power transistors for use in a well-known Hi -fi audio amplifier circuit. They have a trade-mark with which I was not familiar, and were found to have most undesirable characteristics in use. Each transistor, for instance, had a very high value of $I_{\text {ceo }}$ of the order of hundreds of milliamps with only low $\mathrm{V}_{\mathrm{ce}}$, so what with the live open-circuit the core-temperature rose to very high values. On replacing these transistors with others bearing a well-known trade-mark, the circuit functioned perfectly. The supplier disclaimed liability, stating that as far as he was concerned, the transistors were "to spec." Which spec., though? I have therefore paid out nearly $£ 3$ for some TO3, can electric firesif this had been all that I
required I could have searched for a hefty valve from the junkbox!

Manufacturers and distributors naturally cannot supply small quantities to the constructor, and the local shop cannot be expected to stock every obscure semiconductor, but how can the constructor obtain semiconductors through the post with confidence? The only answer would seem to be to persuade reputable suppliers to advertise the manufacturer's name against each semiconductor, as is indeed already done by some suppliers, so that the constructor knows exactly what device he can expect to receive.-D. J. Farman, G3TWZ (Middlesex).
[I agree with you that the subject you mention could be aired.

With regard to particular cases, $I$ would like you to understand that should you have this sort of trouble with the advertisers of Practical Wireless we are always ready to take up the matter on behalf of a reader, providing that we have full details fairly quickly. In this way, we have been able to obtain satisfaction in a number of instances where a reader has had a poor deal from the advertisers. Perhaps you would bear this in mind for the future,-Editor]

## PSST! WANNA BUY PRACTICALWIRELESS ?

We received a letter recently from F. Laverty, BRS 23419, enclosing a cutting from his local paper the Luton, Beds. Saturday Telegraph. It read: "The scene: One of those little shops that sell lots of girlie magazines, in a Luton side-street. It's fairly filled with goggle-eyed males.

Enter a chap who walks up and murmurs something to the proprietor.

The proprietor draws himself up to his full height and says firmly-and loudly-'We don't sell THAT sort of book here, sir!'

Exit rather abashed gent, while the other customers look at each other wondering what exotic sins they might be missing.

The magazine he asked for? Practical Wireless."


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SAVE POSTAL COSTS. CASH AND CARRY CALLERS WELCOME!

[^2]THE beginner to the hobby of short wave listening is possibly not aware of all the interesting and useful information that he can obtain to help him to progress in the hobby. The information which follows is intended to help him gain experience but should also prove useful to the experienced DXer.

Radio Nederland has a DX Information Service which publishes many data sheets and offers courses on practically every aspect of the hobby. Although the service is free of charge I usually include an IRC and/or a reception report to promote friendly relations with the station. For further information write to: DX Information Service, c/o Radio Nederland, P.O. Box 222, Hilversum, Holland.

The World Radio-Television Handbook Co. Ltd. of Sundvej 6, 2900 Hellerup, Denmark publishes several books which are of interest to the SWL. The first of these is the World Radio-Television Handbook (WRTH), this indispensable volume contains full details of every radio and television station in the world. Each entry gives details of the equipment used by the station, a full programme schedule and the address to which reports should be sent. Everyone with an interest in short wave radio should own a copy of this book.

The same company also publishes How to Listen to the World which, like WRTH, appears yearly. The recently published 1969/70 edition contains a wealth of information for both the beginner and the experienced listener. The following selection of chapter titles should give some indication of the scope of this excellent little book: Physics of the Ionosphere; Interference; Fading; How to Measure Frequencies and Calibrate Receivers; The Crystal Calibrator; How to report to Stations; Tape Recording of Reports; Listening to: Asia and the Pacific, The Far East, Africa, Latin America; Languages in International Radio; Sunspot Information and many other interesting chapters. The book is written by an international team of well-known DXers who each write on their own specialised topics.

Another way of obtaining information and gaining experience in the hobby is by joining one of the established DX clubs. The monthly magazines produced by these clubs will keep you informed on the latest news and enable you to compare your results with those of other SWLs. Most clubs also offer certificates in recognition of various achievements and organise regular competitions for their members. Two of the best-known British based clubs are: The International Short Wave League (ISWL), 60 White Street, Derby, DE3 1 HA , and The World DX Club (WDXC), 16 Ena Avenue, Neath, Glamorgan, Wales.

## PROPAGATION FORECAST

The predicted smoothed sunspot number for the month of November is 93 (Switzerland Calling) which

# THE BROADCAST BANDS 

 Malcolm Connahleads me to make these predictions of the most suitable megahertz bands for the month: Europe 4 MHz ; North America $11-25 \mathrm{MHz}$; South America $15-25 \mathrm{MHz}$; Africa 9.17 MHz ; Asia 9 and 11 MHz and Oceania 9 and 11 MHz .

## AFRICA

United Arab Republic: The European Service of Radio Cairo has dropped the two usual frequencies of 9475 and 12005 and is now using 9740. The times of the broadcasts are unaltered, German can be heard at 2030 and English at 2145.

## ASIA

Ceylon: The Commercial Service of Radio Ceylon, which broadcasts in English, has replaced 15230 with 15120 for all its broadcasts. The Home Service now starts fifteen minutes earlier at 0100 on 5020 .

Vietnam: A schedule just received from the Voice of Vietnam in Hanoi gives these details of the English programmes broadcast by the station. Frequencies used are given as $7380,7416,9840,10224$ and 15018. The times of the broadcasts are $0500,1000,1300,1530,2000$ and 2300, 0830 (except Sundays).

## EUROPE

Albania: Radio Tirana has introduced the following English programmes: 0030 on 49 m . and $41 \mathrm{~m} . ; 0100$ on 42 m . and 31 m .; 0230 and 0330 on 49 m . and 41 m .; 1100 on 31 m . and 25 m .; 0630, 1630, 1830, 2030 and 2200 on 42 m . and 31 m . No details of exact frequencies have yet been given but the usual frequencies for this station are: 5950, 6200, 7070, 7300, 9370, 9500, 11840 and 11870.

Armenia: A schedule received from Yerevan gives the news that they have forsaken their usual frequencies of $6155,7185,7200$ and 9540 and are using unspecified frequencies in the 16 and 19 metre bands for the broadcasts to Europe.

Norway: The latest schedule received from Radio Norway gives the following details of programmes in English:
Sundays 0800-0830 on 15345, 21655, 21730, 25730, 25900 ; 1200-1230 on 7240, 17825, 21655, 25730, 25900; $1400-1430$ on $17825,21655,21730,25730,25900$; 1600 1630 on 17825, 21655, 21730, 25730, 25900; 1800-1830 on 15345, 21655, 21730, 25730, 25900; 2000-2030 on 15345, 21670, 21655, 21730, 25730; 2200-2230 on 15345, 17795, 17825, 21655.
Mondays 0000-0030 on $11735,11850,15345 ; 0200-0230$ on 11735, 11850, 11860; 0400-0430 on 9550, 9645, 15345.

Well, that's the lot for another month except to remind you to send in your reports and suggestions. 73's and good DX until next time.

## THE AMATEUR BANDS David Gibson, G3JDG

0NCE again your scribe, one Hippie Gibson, is putting quill to parchment to keep you all fully informed about everything which hasn't happened during the month. For the first time in many moons, the postbag has had that sparse, undernourished appearance. O.K., so the "Let's all hate Gibbie" month is over, now how about some logs, just to show there's no hard feeling?
There should be no great shortage of DX to listen in to on the h.f. end this month as things are considerably better than the summer. This applies particularly to 20 metres which is almost a 24 -hour band these days and carries most of the DX signals.

Down a few kHz on 15, the DX has been quite good with best times to listen from 0600 to 1800 . By the time you read this it will in all probability have moved on, so try 0730-1900 or perhaps a little later.

Ten metres should provide something from Oceana, probably some good sigs from VK, although this will be at a price of poor reception from Canada.

Again, as king winter approaches and G3JDG gets his comms out of pawn, the l.f. bands should improve. Don't neglect 40 metres, there's some very good DX about, it just needs a little patience.

Eighty and topband will be improving fast. This could be a good time to have a crack at listening for topband nets. See how many "local" nets you can log and how far they are from you. Mobile stations on topband seem to become quite rare birds during the colder months and many would doubtless appreciate a decent report on their sigs. A good report though, not just the "heard you five and seven, please QSL" type.

Speaking of the winter months, now is the time to think about some constructional projects to keep you all out of mischief during the dark evenings. An a.t.u. (aerial tuner unit) is well worth while. You could look back through all those back issues of P.W. and find something of interest, perhaps a preamp or an outboard " S " meter? A grid dip oscillator is an invaluable asset to any s.w.l. or amateur, and circuitry for this has appeared in the magazine from time to time.

For those who are interested purely in logging callsigns and getting a long, long list of countries heard, a good time to listen is during contests. During most contests, the callsign is just about all you get anyway. The VK/ZL Oceana DX contest was a good example. There's nearly always two dates for this type of contest, one for c.w. and one for phone, so you can take your pick. It's nearly always easier to bag the goodies on c.w. so if you can't read Morse, how about learning this winter, then you'll be ready for next year? Incidentally, most radio clubs run Morse sessions and there's always slow c.w. signals on topband put out by RSGB members on a rota basis just for the beginner who wants to learn c.w.

In reply to the many queries about callsigns. You can obtain a list of all the different countries and their callsigns from the RSGB, 35 Doughty Street, London, W.C.1. Just send a 9d. stamp or P.O.

An item of interest to constructors is the TAD 100. This is an IC (integrated circuit) which has the
frequency changer, i.f., detector, and audio all on the one chip. Your scribe is trying to get further details and I'll pass on the gen when it arrives. Incidentally, speaking of ICs, an American company has achieved a packing density of 240,000 components to the square inch on a single chip. Admittedly this is only in the laboratory, but it makes you think doesn't it? Perhaps the time will come when you will send the specifications for your ideal receiver to a manufacturer with a ten bob postal order, and receive per return a one-inch slice with it all on, you'll just have to find a dial!

Passing on to the mail this month. Jim Baker (Liverpool) writes to say that there's a new ZL on 80 metres. The callsign is ZL4NM or NH (sri OM ur wrtg nt gud) and he lurks on 3.8 kHz plus or minus a few kHz using s.s.b. with an FT100. His name is Pat, and he's a Liverpudlian (licensed readers call "CQ Whack") and he's looking for contacts in the UK. S.W.Ls who want a card should send their own card, together with an s.a.e., to Jim Baker at 86 Max Road, Liverpool, Lancs., L14 4BJ. See if you can hear the ZL first!

Stephen Randall is very nearly 14 years old and has managed to wrap his digits around a Trio 9R59 DE . The antenna is a 110 ft . long wire, and 20 produced-CT1WB, DK1CQ, HV3SJ, JX1OM, LA8TM, UL7SG, VK3AXQ, VK3MO, VP8RCF. W4YNX. Stephen lives in Hendon, London.

Normally I don't print lists of G calls heard unless short skip conditions are proving interesting. But when you get up to 2 metres, $G$ calls are not too easy to come by over long distances.
J. Simons (Dudley, Worcs.), has an 8 over 8 antenna, (cor, think of the size of one of those on 20), feeding a homebrew preamp and converter. This supplies the AR88 as a tuneable i.f. from 2426 MHz . On 2, John raised-GI5ALP, EI7AF, EI5BH, G18AYZ/P, GM3TGL/P (at Kirkcudbright), G3KDG (Devon), G3GJY/P, G8BGR/P, G8APV/P, G3TAB/P, G3PXF/P (Westmorland), G3WSC/P, G2JF, GD3VXK, GW3NWR/P, GW3UCB/P, GW3ILO, GW3NUE/P.

Philip Batt (Littleborough, Lancs.), has a PCR3. The antenna is 22 ft . bare copper wire on two masts at 15 ft ., with a 58 ft . down lead. Twenty metres pro-duced-CE3FZ, CR6QX, CT1BD, G2MJ, HB $\varnothing$ XBX, HP1XAJ, HRIKS, K6MHO, K6AFT. K6SA, OA6S, TIIECE, TI2CEF, UG6AW, VK2ATT, VK3AM, VK4CK, VK7CR, VK9FW.
Fifteen proved fruitful for Philip too-CE1EF, EA8EG, F $\varnothing \mathrm{QR} / \mathrm{M}, \mathrm{HB} \varnothing \mathrm{AA}, \mathrm{ISIDMN}, \mathrm{HL2IX}$ (Korea), JA1BAC, JA2GQF, JA3JMC, JA4SNM, JA5DRJ, JA7GHM, JA8DEI, JH1GJF, KZ4VA, KP4DCR, KR6EX, LU1DAB, MP4BHL, OD5BCV, OH $\varnothing A S, ~ O X 2 B B A, ~ P Y 6 T P, ~ T F 3 S B, ~ V K 2 R V$, VS6AD, VS9MB, W6MSM, YV3KT, ZE3RK, 3V8AA, 4X4AM, 9H1BH, 9M2DQ, 9G1GB.

A few contests and happenings in November which are worth a listen. 3rd November, 2 metre s.s.b. contest; 8th-9th, 40 metre phone contest; 15 th16th, topband contest, go on, have a listen; 29th30th, CQ world-wide DX contest but it's c.w. only. Start those Morse classes now and you can listen next year!

There are two early ones in December. These are 6th-7th December, CHC international DX contest (c.w.): and 7th, 4 metre contest (c.w.).

All logs to the home QTH please before the 18th of the month. 5 Edward Close, St. Albans Herts.


The serious amateur should never be without this comprehensive price list and guide to semiconductors and electronic components from RCA, IR, SGS, Emihus,Semitron, Keyswitch,Plessey, Morganite, Litesold and others (together with manufacturers' application data) which you can buy direct from us atmanufacturers' prices e.g. IN914 1/3d. $\square$ IN916 1/11d. $\square 2 N 697$ 4/5d. $\square$ 2N706 2/3d. $\square 2 N 706 A$ 2/9d. $\square 2 N 929$ 5/8d. $\square 2 N 1613$ 4/8d. $\square 2 N 3011$ 9/1d. $\square 2 N 3053$ 6/2d. $\square$ 2N3055 15/9d. $\square$ 3N140 15/3d. BFY50 4/8d. $\square$ BFY5l 3/9d. $\square$ BSY27 18/- $\square$ BSY95A 3/3d. $\square$ C407 4/6d. $\square$ CA3012 18/3d. CA3014 25;6d. CA3020 25/9d. $\square$ OA200 1/9d. $\square$ OA202 1 11d.

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A$S$ mentioned in part 1 the production and assembly of the special roller bridge and pedal mechanism calls for fairly accurate work although apart from the usual metal working tools, the writer used only an electric bench drill. Before embarking on the bridge and pedal mechanism however, all the woodwork, i.e., the making of the console and the guitar body should be completed. The tuning pegs do not have to be made of course and these can be purchased from Cyril Proctor, 180 Town Street, Leeds, Yorks. These are known as single geared pegs and cost $£ 2$ for a set of eight but make sure that 4 left-hand and 4 right-hand pegs are ordered. The same firm can also supply the plastic fret board which should be ordered as follows: 25in. scale- 24 frets for 8 string guitar and the price is 25 s . The special 8 string H.G. magnetic pick-up type 2 A with adjustable poles is also available from Cyril Proctor and costs $£ 45$ s.

The raw materials required for the bridge and pedal mechanism are tin. thick brass for the lever rollers etc., $1 / 16 \mathrm{in}$. thick mild steel, 3/16in. and

(A): The Roller Bridge.
$\frac{1}{8} \mathrm{in}$. diameter mild steel rod, $\frac{1}{4} \mathrm{in}$. diameter silver steel rod and $\frac{3}{4} \mathrm{in}$. and $\frac{1}{2} \mathrm{in}$. square section mild steel tube which is for the tie across the bottom of the console between the left- and right-hand sides and the pedals. This tie-bar also serves as a stop for the foot pedals (see Fig. 6 part 1). The remainder of the materials are the 2BA Allen head screws and the compression springs for the lever roller stops and sundry 4 and 6BA screws and nuts as indicated in the various diagrams.

## The Roller Bridge

This consists of a square U-shaped framework which is screwed on to the tail of the guitar body as shown in Fig. 7A (part 1) and in the photograph in this article. It carries the diameter spindle on which the circular rollers and lever rollers are mounted together with the spacers. Six "stop" screws have been provided so that lever rollers can be used for strings other than those indicated for the E6th tuning as given in part 1. Strings which run over the circular rollers are secured to the bridge frame at the rear. Strings controlled by the pedals are anchored directly to the lever rollers.

Details for making the bridge frame are given in Figs. 9A, B, C, D and E. Note the small caps which are used to retain the roller spindle in the frame. The six 2BA Allen screws, each lin. long act as the rear stops for the lever rollers. The compression springs should be about $\frac{3}{8}$ to $\frac{1}{2} \mathrm{in}$. long and are fitted to prevent the screws turning of their own accord. Although only two stop screws are used for the tuning given in part 1 it is worth fitting all six so that either of the strings 7 to 2 could be used with the pedals if required. Before drilling and tapping the holes for these screws secure the $\frac{1}{4} \mathrm{in}$. thick brass block to the rear plate of the bridge frame. The tapped holes go right through this as per Figs. 9D and 9E.
The spindle for the rollers and lever rollers is tin. diameter silver steel cut to fit exactly within the frame but flush with the outer surfaces. The spindle is held in by means of the retaining caps as per Fig. 9E. Next come the plain circular rollers which can be made from sin. diameter brass rod and cut, drilled and grooved as in Fig. 10B. The


Fig. 9 (above): (A) Side of frame-two required. (B), (C) Tail plate assembly. (D) Holes for the 2BA Allen screws drilled and tapped after brass block is fitted as in (C). (E) Final assembly of the roller bridge frame. Note retaining caps for roller spindle.
Fig. 10 (below): Details of rollers and assembly of rollers and lever rollers in the bridge frame.
Fig. 11 (right): Dimensions for the lever rollers.


spacers are cut from $\frac{3}{8}$ in. diameter brass tube with a $\frac{1}{4} \mathrm{in}$. diameter inner bore. Details for these and the two end spacers are given in Fig. 10C.

Next come the lever rollers and although only two are required for a two pedal system it is worth making and fitting four as shown for possible future use with an alternative tuning. These are made from $\frac{1}{4}$ in. thick brass as shown in Fig. 11. Note that they are grooved around the circular portion of the top to hold the strings in place. The action of these lever rollers and the method of securing the string to the lever is shown in Fig 12. The stop screws are set so as to allow only sufficient movement of the lever roller to tension or de-tension the string by an amount required to raise or lower its pitch according to the tuning required. The adjustment available with the stop screws should allow the lever enough movement to raise or lower the string pitch by
more than a whole tone. The final adjustment of the stops is of course made in conjunction with the movement of the pedal rods and the pedals.

Readers may by now be wondering why such a complicated mechanism is necessary merely to raise or lower the pitch of a guitar string by a semitone or so. Why not for instance, use a conventional bridge and simply apply pressure to the strings


Fig. 12: Lever roller action. Note method of anchoring guitar string.
between the bridge and the tailpiece? This has been tried and rejected for the simple reason that strings continually tensioned and de-tensioned across the edge of a bridge very quickly break. The method described in these articles is basically the same as that developed for commercially-made instruments now on the market and overcomes this problem.
Next comes the making and fitting of the forward stop screw assembly shown in Fig. 13A and which must be fitted underneath the tail end of the guitar as in Fig. 13B and before the roller bridge is fitted. This consists of a piece of $\frac{3}{4} \mathrm{in}$. aluminium angle to which is bolted the $\frac{1}{4}$ in. thick brass block that carries the stop screws. A piece of $\frac{1}{2} \times \frac{1}{2}$ in. aluminium angle is fitted across the top of the tail end of the guitar above the stop screw assembly as in Fig. 13B


Fig. 13: Details of the forward stop bar fitted beneath the tail end of the guitar body.
and which is also shown in Fig. 7A part 1 and marked " $Z$ ". Additional guidance as to the function of the forward stop screw assembly is shown in Fig. 14. It will be seen that the lever rollers come forward to meet the lower stop screws and in the opposite direction to meet the higher rear stop screws. The overall movement of the lever rollers should not be more that one-eighth to three-sixteenths of an inch for a pitch change of a semitone up or down.

## The Pedal Mechanism

Schematic diagrams showing the whole mechanism between the lever rollers and the pedals are given in Figs. 2 and 3 of part 1. The mechanism is a system of rods and levers which is shown in greater detail in Fig. 15. The lever assembly is situated underneath the top of the console a little to the left of midway between the two sides. This assembly consists of a mild steel plate on which are mounted


Fig. 14: Position of forward stop bar relative to the bridge frame and lever rollers.
the levers and spindles as shown in Fig. 16A. However, let us return to Fig. 15 for a moment. This shows the de-tensioning system which operates as follows. The $\frac{1}{8} \mathrm{in}$. diameter rod attached to the roller lever is also bolted to the lever marked " $A$ " and a large tension spring is connected between this and the left-hand side of the cabinet via a piece of steel wire (piano wire). The large spring holds the lever roller against the forward stop screw as shown in the diagram, the tension of the spring being. sufficient to overcome the normal tuning tension of the guitar string. When the pedal is pressed, lever " $B$ " actuates lever " $A$ " via the connecting spindle which now moves to the right. This allows the lever roller to move over to the rear stop thus reducing the pitch to which the guitar string is tuned. The other pedal produces the reverse of this action, i.e., when the lever " $D$ " is actuated by the pedal then lever "C" moves to the left and pulls its lever roller toward a forward stop screw thus raising the pitch to which the string is tuned. A side view of the lever assembly is shown in Fig. 17. Note that the levers A, B, C and D as in Figs. 16A and 17 must be bolted directly to the spindles so that no slipping occurs.

## The Foot Pedals

The dimensions for the pedals and pedal bearings are given in Figs. 18A, B, C and D. The pedal bar is made from $\frac{1}{2}$ in. square mild steel tube which is


Fig. 15 (above): The action of the lever roller and pedal coupling mechanism situated beneath the top of the consol. Arrows show movement of rods when pedal 1 is pressed. Text explains mechanism.
Fig. 16 (below): Coupling mechanism between lever rollers and pedals.

attached to its bearing (Fig. 18B) by a $\frac{1}{4} \mathrm{in}$. diameter spindle. The spindle is cut so that about one-sixteenth of an inch projects either side. The ends are lightly hammered to prevent the spindle coming out. Make sure that the pedal has free movement but as little side play as possible. The control rod from the lever assembly is attached to the' pedal as shown in Fig. 18C and D. Note the use of a felt washer above the pedal bar and the $\frac{3}{8}$ in. sleeve below. The size of the foot plate and the length of the pedal bar can be adjusted a little for comfort in playing, otherwise the dimensions given should be used. The foot plate need only be about $1 \frac{1}{2} \mathrm{in}$. wide and 3 in . long. Two pedals and bearings are of course required and they should be mounted directly below and in line with the levers to which they are attached. No measurements have been given for this as the positioning is best done experimentally. However, for correct up and down movement of the pedals the bearing spindle should be at a point about 2 in . above the bottom of the lower backboard. The pedals should slope gently to the tie-bar.

## Connecting Rods

Finally comes the connecting rods between the lever rollers on the guitar bridge assembly and the pedal levers under the console top and between these and the foot pedals. The rods from the lever rollers may be made from $\frac{1}{8}$ in. diameter mild steel and those to the pedals of $3 / 16 \mathrm{in}$. diameter. The overall length of each rod is best determined experimentally but for guidance here are the lengths of the rods as on the writer's prototype pedal guitar. The de-tensioning rod between its lever roller and lever "A" (as in Fig. 15) is approximately 16in. long. The rods to pedals from levers " B " and " D " (as in Fig. 15) are both approximately 27 in . long. The "flats" at each end of the rods are produced by heating and hammering and the holes through these flats as in Fig. 19 should provide more than ample adjustment when the mechanism is finally aligned.


Fig. 17: Side view of mechanism shown in Fig. 9A.

As pointed out previously a pedal guitar using the basic control mechanism as described in these articles could of course be built to accommodate more pedals, alternative tuning with 8 or 12 strings or even with twin necks. The roller bridge system is however, the only satisfactory method of tensioning and de-tensioning guitar strings by means of foot pedals.


Fig. 18: Dimensions and assembly of foot pedals.


Fig. 19: Coupling rods. (A), to lever rollers. (B), to pedals.
The final part of this article, next month, will deal with the alignment of the pedal mechanism, the circuit for the tone control preamplifier and a pedal volume control.

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One of the main requirements of a microphone mixer is that of low noise level. This unit has been designed especially with this in view. Other features include a degree of amplification as well as mixing, a self contained arrangement that could be operated at some distance from the main amplifier. Inputs are included for tape and pickup.

## bEGINNER'S PORTABLE RECEIVER

Almost all radio constructors have memories of unsuccessful first attempts. Beginners are faced with a wide selection of designs and often make the mistake of choosing one that is too advanced for their nascent capabilities or alternatively, one whose extreme simplicity leads to a disappointing performance. This radio is a straight forward six transistor superhet on conventional lines. Construction is simplified by the use of Veroboard.

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THE amplifier described in this article is a very simple unit, which is very easy to build. It is thus well suited for the beginner, but it may also be of interest to the more experienced constructor as it may be used for a variety of purposes. It consists of three inexpensive transistors and a handful of other small components and can be built for under $£ 1$.

Audio amplifiers of this type are usually operating in class $B$ push pull, since class $B$ output stages require very little quiescent current (i.e. under no signal conditions), and since their efficiency is near $80 \%$ under signal conditions. However, such an output stage requires matched transistors, which are relatively critical on the biasing circuit, and the beginner may find it difficult to construct a class $B$ push pull output stage with a minimum of harmonic distortion. Class B stages also require a reasonably constant voltage supply, so that the voltage will stay constant when the current in the stage increases with increasing output signal.
The output stage of this particular amplifier operates in class A, which means that the current through the output transistor is constant, whether there is a signal output or not. If a battery is used, this is of course not very economical, but if one uses a mains supply, the constant current drain is not a serious drawback, even if the amplifier is left on for several days. Its power consumption is so small that its existence will not be detected in the electricity bill! However, the maximum efficiency of a class $A$ output stage is only $50 \%$, compared to the $80 \%$ for the class B push pull stage, but when one considers the low initial cost of a single class $A$ output stage, its distortionless output, and its non-critical construction, it is well worth using this type of output in a small amplifier.

## THE CIRCUIT

The schematic diagram of the basic amplifier is shown in Fig. 1. The amplifier is designed around three inexpensive silicon transistors, which may be obtained very cheaply indeed from advertisers in this magazine, and it will give a low distortion output power of approximately $80-100 \mathrm{~mW}$. The current drain is approximately 40 to 50 mA from a 6 V supply. The frequency response is from $200 \mathrm{c} / \mathrm{s}$ to above the audible frequency spectrum, but its lower limit may be improved by increasing the values of Cl and C 3 .

As the transistors used have negligible leakage
currents, very simple biasing techniques have been employed. Trl has the input signal applied to its base, via C1, and it is biased by means of a single resistor, R1, giving both d.c. and a.c. feedback. Tr1 acts as a common emitter voltage amplifier and the signal voltage developing across its collector load R2 is coupled via C 3 to Tr 2 . Tr 2 acts as a common collector (also known as an emitter follower) amplifier, and its bias is derived from the two resistors R 3 and R5. It will thus have a high input impedance so


Fig. 1: The circuit of the transistor amplifier

## * components list

## Resistors

| R1 | $18 \mathrm{k} \Omega$ | R4 | $560 \Omega$ |
| :---: | :---: | :---: | :---: |
| R2 | $1 \cdot 2 \mathrm{k} \Omega$ | R5 | $22 \mathrm{k} \Omega$ |
| R3 | $8 \cdot 2 \mathrm{k} \Omega$ |  |  |

All $\frac{1}{4}$-watt miniature types, $10 \%$ tolerance.

## Capacitors:

| C1 | $5 \mu \mathrm{~F} 6 \mathrm{~V}-$ see text C 3 |
| :--- | :--- |
| C 2 | $100 \mu \mathrm{~F} 15 \mathrm{~V}$ |

Transistors:
Tr1 BC 108 or equivalent
Tr2 BC 108 or equivalent
Tr3 2N696

## Miscellaneous:

Output transformer, 9:1 ratio (Radiospares T/T4, available from retail suppliers): Veroboard $2 \frac{1}{6} \times 1 \frac{1}{2}$ in., $0 \cdot 15 \mathrm{in}$. matrix; $3 \Omega$ loudspeaker.
as not to decrease the effective a.c. load of the first stage, and a low output impedance to match the input impedance of Tr 3 , which is of the order of $40 \Omega$. As in all emitter followers, the voltage gain is approximately unity.

The output stage consists of a 2 N 696 , which is a medium power transistor. It is directly coupled to the emitter of the previous stage, thus avoiding a coupling capacitor, and at the same time provides the bias for the base. A small output transformer acts as the collector load of Tr 3 , matching the output to a $3 \Omega$ speaker. The feedback resistor is connected to the collector of the output stage, and thus both negative a.c. and d.c. feedback are applied. The d.c: feedback stabilises the d.c. conditions of the output stage, and the a.c. feedback improves the quality.

The output transformer has a turns ratio of approximately $9: 1$ to achieve the best possible matching, and the Radiospares T/T4 is suitable for this purpose. The output quality is remarkably good, considering the simplicity of the circuit, and the power delivered to the speaker is quite sufficient for most purposes.


Fig. 2: The component layout on the Veroboard.

## CONSTRUCTION

The amplifier is built on a small piece of Veroboard, of $2 \frac{1}{8} \times 1 \frac{1}{2}$ in., as shown in Fig. 2 and the photograph. The connecting pins of the transformer must be bent slightly to fit it into the board, otherwise there is nothing special about the Veroboard construction. All components are mounted vertically, which allows the amplifier to be a very compact unit. A hole is drilled in each corner for fixing the board into a box etc.
No heatsink is required for Tr3, even if its temperature rises slightly above room temperature. The power dissipation of the output transistor is held at a level well below the permissible amount, and besides, silicon transistors may be operated at higher junction temperatures than germanium ones.

## APPLICATION

It should not be difficult to find uses for this little device. It can be used for a gramophone amplifier (the larger the speaker, the better the output quality) or incorporated in a small receiver system, since its sensitivity is of the order of 1 mV for full output. However, it was originally designed for home communication purposes.

Figure 3 shows a simple baby alarm system, using the amplifier together with a medium impedance dynamic microphone ( $1-3 \mathrm{k} \Omega$ ), and a logarithmir


Fig. 3: Connecting the amplifier as a baby alarm.
potentiometer connected as a volume control across the input. The output is taken to a $3 \Omega$ loudspeaker. In this and the following examples, the mains power supply shown in Fig. 4 is highly recommended, as it would be much more economical to use than conventional dry batteries. It consists of a standard 6.3 V heater transformer and a conventional full wave rectifying bridge. The output voltage is dropped slightly across the $10 \Omega$ resistor and then smoothed in the large electrolytic capacitor. The $10 \mathrm{k} \Omega$ resistor connected across the output simply acts as a bleeder, so that a higher voltage will not build up across the storage capacitor when no load is connected to the supply. The maximum current drain is approximately 50 mA .


Fig. 4: A mains power supply for the amplifier.
As an alternative to the baby alarm just described, the circuit in Fig. 5 can be used. Here, the microphone has been replaced by a small speaker with a matching transformer, to match the low impedance of the speaker to that of the amplifier input. Since the input


Fig. 5: Using a small speaker as a microphone.
impedance of the amplifier is around $1.2 \mathrm{k} \Omega$, a transformer with turns ratio of $1: 20$ is needed (e.g. Repanco type TT52). By arranging a simple switching system, as shown in Fig. 6, the baby alarm is


Fig. 6: Schematic of the amplifier used as an intercom.

# INJECTRACE 

TWO of the most useful pieces of test gear, for both the serviceman and the amateur constructor are a signal source and a signal tracer. The project described here combines both these functions in an inside jacket pocket sized case, $7 \times 1 \times \frac{5}{8}$ in. It generates a very wide band signal from about 1 kHz to over 200 MHz in the inject mode, heaving out a pretty powerful signal. In the trace mode it will detect a.f. and r.f. up to very high frequencies and is sensitive enough to hear local stations when connected to a short length of wire. Switching between the two functions is automatic; in the normal mode it acts as an injector producing a 1 kHz squarewave but as soon as the earpiece is plugged in it becomes a tracer, the earphone itself acting as the switch.

The Injectrace is built into a Wisdom toothbrush case which is strongly built and exactly the right size. Including toothbrush this costs 2 s . 6 d . (3s. 6 d . for bristle!) -not a bad price for a custom size case (never mind the toothbrush). Standard components are used throughout and the metalwork requires only metal cutters, a few drills and a pair of pliers.

## The Circuit

Most readers will be familiar with the straightforward amplifier circuit, that is, R-C coupled. When the earphone is plugged in it is connected to the collector of Tr2 via C3 (see Fig. 1). The connection feeding back to the base of Trl is broken while the earphone is connected.


Fig. 1: The Injectrace signal injector and tracer. Functions are changed merely by plugging in the earphone.

When the earphone is removed C3 connects to the base of Tr 1 forming a multivibrator working at about 1 kHz fundamental. However this waveform takes the shape of a square and as we know

## HAL MOORSHEAD


this is full of harmonics. Due to biasing conditions etc. (the reasons will be described later) the rise time is fairly slow but the cut-off is very sharp. In fact the unit will radiate frequencies well into TV Band III (about 200 MHz ) but above this the transistor is approaching cut-off.

In its trace mode the deliberate distortion enables the Injectrace to detect r.f. signals. There is always detection in an amplifier which is non-linear; although this distorts a.f. signals we will generally be trying to trace a signal rather than judge for quality.

The very high gain of the transistors used and the high frequency response built in can lead to problems. If a crystal earpiece is used this will not damp the output and stray capacitance can cause the circuit to oscillate. Although this will not generally matter (you can still hear your input and the frequency will normally be outside the audio range) this can be overcome by using a $250 \Omega$ earpiece which mismatches the output and consequently reduces the gain. The commoner $8 \Omega$ earpieces will do but the sensitivity is considerably reduced.

## Construction

Having a circuit as described is of little use unless it is housed in a robust container of convenient size. A lot of thought was put into the general constriction and other layouts were tried but the one shown here is the best from several points of view. All the components are fixed to a $\frac{1}{2}$ in. strip of $16 \mathrm{~s} . \mathrm{w} . \mathrm{g}$. aluminium bent as shown. The problem of battery housing and rigid construction are overcome using this method. About the only battery


Fig. 2: The aluminium "chassis".


Fig. 3: Layout of the major components, which also shows how the strip is bent.
suitable is the Ever Ready B154 which is not fitted with clip battery terminals but with "domes" for pressure contact. -

One of these domes, the negative, presses against the aluminium chassis strip while the other presses against the female connection of a PP3 battery clip. Plastic covered clips of this type are widelyavailable and by cutting off the male section, spreading the contacts of the female connector and feeding the wire through a small hole drilled in the chassis, a good spring contact will be made.

The miniature push-button switch and the earphone socket are mounted on the end plate. Care should be taken as there is precious little room and also because of this a 2.5 mm . socket should be used for the earphone.

The active components are mounted on a small piece of 0.1 in . matrix Veroboard $9 \times 5$ holes, the centre hole being drilled out for mounting. The mounting screw for the Veroboard is countersunk


Fig. 4: The circuit panel, showing where components are mounted.
through the chassis and an insulating washer should be fitted to space the underside of the component board away from the chassis. The chassis itself is the negative connection and contact is made to the board by fitting a solder tag underneath the securing nut with a wire from the tag to the negative strip on the board.

The probe itself is connected to the front panel and this of course is insulated from the chassis

using a plastic washer of the type used for mounting power transistors.

To increase the versatility of the Injectrace it was required that three different probes should be used and to facilitate this the probes are plugged in. One probe should be straightforward as illustrated, another fitted with a $0.01 \mu \mathrm{~F} 500 \mathrm{~V}$ capacitor for valved or other high voltage equipment and another probe fitted with a $5.6 \mathrm{M} \Omega$ resistor for use with high level inputs that would otherwise overload the amplifier in the trace mode. These probes are all soldered to banana plugs which fit into a socket fitted to the front of the unit.

Because of the large diameter of the screws on

## components list

## Resistors:

| R1 | $2 \cdot 2 \mathrm{M} \Omega \frac{1}{4}$ watt |
| :--- | :--- |
| R2 | $10 \mathrm{k} \Omega \frac{1}{8}$ watt |
| R3 | $2 \cdot 2 \mathrm{M} \Omega \frac{1}{4}$ watt |
| All $10 \%$ tolerance. |  |

R4 $10 \mathrm{k} \Omega \frac{1}{8}$ watt
R5 $5 \cdot 6 \mathrm{M} \Omega 1$ watt
(for attenuating probe)
All 10\% tolerance.

## Capacitors:

| C1 | $0.002 \mu \mathrm{~F}$ Mylar Film | C4 0.01500 V |
| :--- | :--- | :--- |
| C2 | $0.001 \mu \mathrm{~F}$ Mylar Film | Silvered Mica |
| C3 | $0.001 \mu \mathrm{~F}$ Mylar Film | (for high voltage probe) |

Semiconductors:
Tr1 2N2926G

## Tr2 2N2926G

## Miscellaneous:

B154 15V battery; 0.1 in. matrix Veroboard, $9 \times 5$ holes; 2.5 mm . earphone socket; $250 \Omega$ earphone with 2.5 mm . jack; miniature push-button switch; plastic toothbrush case-see text; socket; three banana plugs; aluminium strip; PP3 battery connector; small crocodile clip; nuts and bolts, etc.
such plugs there is a problem in insulating them from the chassis and to overcome this a 6BA nut was soldered to the base of the socket which in turn fitted on to the insulated 6BA screw on the front of the Injectrace.

The earthing connection is taken from a solder tag fitted underneath the probe, the illustrations show this clearly. A small crocodile clip makes the best type of connection and about 9in. of wire should be about right.

Once the wiring-up of the unit has been completed it should be slipped into the case and holes marked and drilled in the back to line up with the push-button switch and the earphone socket.

The chassis is held into the case by leaving the nut of the push-button switch off while the chassis is being fitted and screwing it on when it protrudes through the back of the case.

One point must be made regarding the switch. These are Japanese imports and are widely available in two forms, both suitable, however the plastic part through which the contacts protrude is very soft and will very easily melt and shift the contacts making the switch useless unless great care is taken when soldering.

## Uses

Once built the Injectrace will prove invaluable and it should not be too long before isolating a

fault in a piece of equipment becomes second nature.
Take for example a transistor superhet radioand there must be few of us who haven't been called upon to fix one.

First eliminate the two commonest faults-flat or low battery and dirty earphone switch. These are by far the easiest things to check and account for a huge proportion of faults. If both these points are O.K. all the rest can be done with the Injectrace.

Inject at the slider of the volume control; if the signal is heard the fault will lie in the r.f./i.f. section. If not, it will probably lie in the amplifier. Working either forwards or backwards through the circuit injecting or tracing will be very simple and the fault will be easily found.

## BLUEPRINT SERVICE

We would like to draw readers' attention to the fact that the BLUEPRINT SERVICE has been discontinued and therefore no further BLUEPRINTS are available.

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## MINIATURE AUDIO AMPLIFIER



Fig. 7: Connections for use as a telephone amplifier.
converted into a two-way intercom system. If one uses this system, a separate calling system could be built using buzzers and push buttons.

Finally, the circuit of a telephone amplifier is given in Fig. 7. A telephone recording adaptor (which is readily obtained from advertisers in this magazine, e.g. Henry's Radio) is connected via the volume control to the input of the amplifier. It connects the telephone inductively to the amplifier so that a telephone conversation may be heard by a third person. The adaptor is fitted with a rubber sucker which is pressed on to the telephone in a position so as to give maximum volume.

This simple amplifier has been a satisfactory (and inexpensive) solution to the author's home communication problem. The devices which were built gave very good results; they had sensitivity enough to pick up weak sounds and voices from sources situated several yards away from the microphone/ speaker, and the output volumes were in excess of most commercial intercom. systems.

# practically wireless commenatav by HEMRI 

FOLLOWING our Editor's September comments. I could have entitled this piece "Third time lucky". Allow me to repeat-for the benefit of those in whose minds the successive editorials do not burn-the gist of the message.
"During the heyday of the valve era, designers, constructors, equipment makers and service engineers were plagued with the vast proliferation of valve types complete listing became well-nigh impossible due to sheer numbers. With the advent of transistors it seemed that a new era of rationalisation was dawning . . . it was inconceivable that the same mistakes would be made

## BUT

"There must be tens of thousands of types in the catalogues . . . there has been little attempt to rationalise the type numbering system. At this stage of the game it is too late to remedy matters."

His nibs went on to say that we were on the threshold of another major opportunity for industry to work together. But our Editor must have felt the vain optimism of his hopes, for he warned that unless industry could prevent itself-lemming fashion-from making the same mistakes the third time, a situation even more chaotic would result. ". . . we are all set to be overwhelmed by an avalanche of IC devices within


Disembarked from their Trojan horses.
the next few years." The small boy's dream, buried 'neath a mountain of chips!

The chip invasion is with us. The recent torrodero laughingly called a Radio Show slipped a number of IC devices into its offerings, and such was the obsession of reporters suffering from incipient chomatomania that the infiltrators disembarked from their coloured Trojan horses and are entering our lives unseen.

Readers of our sister journal, Practical Television, are already being brainwashed. A series of articles by E. J. Hoare entitled Chips with Everything, which got itself front-page billing, no less, sets out to describe the design, development and application of integrated circuits in detail. It is thoroughly recommended reading.

Trouble with the IC label always seems to me the use some equipment makers put that hardworked word integrated to. In grammar as atrocious as my last sentence they pad out their advertising with "integrated for utmost efficiency" items. These reveal themselves to be no more than the familiar units packed into one case.

At this year's Radio Shows we saw a $9 \times 5 \times 3$ in. stereo radio with separate dinky loudspeakers. Rather like matching matchboxes -and not an IC in sight, as far as we could gather. Presumably this trend to miniaturisation will bypass the ultimate status symbol, the super-gram. Yet we may find a large central box with dummy dial and turntable, and the IC hiding behind the aerial plug.

On the grounds of reliability, chips have more flavour. But we remember being told just this when transistors came to town. IC design demands a multiterminal connection to a printed circuit panel with a few discreet components scattered around. Capacitors cannot be formed to any size because of sheer physical limitations, and resistors that


Too many eggs in one basket.
must dissipate some power are also doomed to the fringes. The result will probably be a few more expensive breakdowns, where a ninepenny component will require replacement of the whole panel willy-nilly. There is a disadvantage, as Mr. Hoare has said, of having too many eggs in one basket.

One of the present limitations to the IC is the physical size. Power dissipation is limited to about a quarter-watt. About 20 volts for the "high tension" line is the modern extreme and the feedback problems at high frequency make high-gain circuits an untenable proposition.

So, if we want to avoid overcooking our chips, we shall have to be content with small-signal, low-frequency circuits, such as i.f. stages, TV sync separators, a.g.c. and a.f.c. amplifiers and discriminators.

Power stages are taboo-as yet. (We need the saving phase because, remember? it was not so long ago that the line output stage of a television receiver simply had to be a valve. Nowadays a couple of BU105 transistors handle the power for a colour TV line output section with no more than a gentle blush.)
No, we shan't be saying "Goodbye Mr. Chips" for a long, long time, lemming-like proliferation notwithstanding.


The CA3028 used as a S.W. Converter

INTEGRATED circuits have by now fairly well established themselves in many branches of Lamateur electronics. The cost of these devices is continually decreasing and in some cases use of an i.c. can work out to be cheaper than its discrete counterparts. Moreover due to their compactness and ruggedness they lend themselves especially for use in equipment where reliability is important


Fig. 1: The integrated circuit under review this month is the CA3028 manufactured by R.C.A. The theoretical circuit, containing three transistor elements, is shown alongside.


Fig. 2: The CA3028 can be used as a combined r.f. amplifier, mixer and oscillator in a receiver front-end. This particular circuit is for a short-wave tuner to go ahead of a medium-wave receiver.
since they are not easily damaged. This article describes the use of an R.C.A. CA3028 i.c. in a 1.6 MHz short wave converter.

Figure 1 shows the theoretical circuit of the CA3028. As can be seen from the diagram a great number of access points to the unit are available and this makes it particularly useful. The designers intended the unit to be used in either the cascode or differential mode but in the present design each transistor will be used to perform a different function thereby utilising all the advantages afforded by the i.c.


Fig. 3: The printed-circuit layout for Fig. 2, seen from the copper side.

The complete circuit diagram of the converter is shown in Fig. 2. The r.f. signal from the tuned circuit is fed to the base of Trl operating as an r.f. amplifier. in the common emitter mode. Tr2 oscillates at a frequency determined by L2 and VC2 with regeneration provided by the coupling winding from the base of Tr 3 , which in addition provides the

## components list

Resistors:
R1 $2 \cdot 2 \mathrm{k} \Omega$ R2 $1 \mathrm{k} \Omega$
Both $10 \%, \frac{1}{4}$ watt miniature

## Capacitors:

| C1 | $0.01 \mu \mathrm{~F}$ | C3 | $0.01 \mu \mathrm{~F}$ |
| :--- | :--- | :--- | :--- |
| C2 | $0.01 \mu \mathrm{~F}$ | C | 960 pF |
| VC1 $/ 2$ | 365 pF variable |  |  |
| TC1, TC2 | 5-30pF Beehive trimmers |  |  |

## Coils:

IFT $1 \cdot 6 \mathrm{MHz}$, Denco type IFT.16/1.6
L1 Aerial coil, Denco type 4T Blue
L2 Oscillator coil, Denco type 4T White

## Miscellaneous:

Integrated circuit, R.C.A. CA3028; printed circuit board, coax sockets, battery, etc.
proper biasing conditions for Tr 3 . The amplified r.f. aerial signal appearing at the collector of Tr 1 is mixed with the oscillator signal appearing at the emitter of $\operatorname{Tr} 2$ and the resultant 1.6 MHz i.f. signal is extracted at the collector of Tr3. From here it is fed to the aerial socket of a medium wave receiver tuned to a vacant spot on the high frequency end of the band around 1.6 MHz .
The printed circuit layout pattern is shown in Fig. 3. This pattern should be painted on a sheet of copper laminate board and etched in the usual way in a solution of ferric chloride. The etched board should be thoroughly cleaned and all traces of paint removed. Drilling should be done from the copper side of the board to prevent peeling of the copper, noting that larger holes are required for the mounting of the B9A valve holders and the trimmer capacitors. The pins of the valve holders are numbered in a clockwise direction with a larger gap between pins 1 and 9 . This helps to identify the pins on the coils.

The prototype used Denco range 4 coils covering the $20-60$ metre band. Any other range may be utilised by inserting the proper coils and associated padders. It should be noted that all component leads must be kept as short as possible to prevent instability. Both the aerial and oscillator coils should be mounted in their shielding cans with solder tags bolted to them to provide suitable earth connections.
A small aluminium chassis together with a few $\frac{1}{4} \mathrm{in}$. standoff spacers were used to mount the printed circuit board, with the coax sockets, on-off switch and tuning control mounted on a front panel bolted to it. The drilling details for these panels are given in Fig. 4.

The unit is now ready for testing and calibrating. The tuning on the medium wave receiver should be set to a vacant spot near 1.6 MHz . Next tune-in a station on the converter at the low frequency end of the band and adjust the cores of the aerial and oscillator coils for maximum volume. A small adjustment to the core of the i.f.t. may also be required. After this tune-in a station at the high frequency end of the band and adjust the trimmers for maximum volume. Repeat this procedure until the tracking is correct. The easiest method of calibration, if one has not access to a signal generator, is


Fig. 4: A small chassis and panel suitable for the i.c. tuner.
to obtain a few spot frequencies on the band and calibrate it accordingly. Many stations regularly give their operating frequencies. For the newcomer to short wave listening this will prove to be an ideal project since with so few components involved in its construction results are virtually guaranteed.

## PRACTICAL WIRELESS and PRACTICAL TELEVISION FILM SHOW

## Caxton Hall, Caxton Street London S.W.1. Friday, March 6th, 1970 at 7.30 p.m.

Come and spend an interesting evening (free tea and sandwiches), which will include a colour film entitled SOMETHING BIG IN MICROCIRCUITS. Ian Nicholson of Mullard Ltd., will be the principal speaker. W. N. Stevens, Editor, Practical Wireless and Practical Television will be in the chair.

# Low cost valve amplifier <br> <br> R. J. WINFROW 

 <br> <br> R. J. WINFROW}

WITH the current trend towards complicated transistor Hi-Fi amplifiers and preamplifiers, it is often forgotten that very good quality can be obtained from fairly simple, low cost valve amplifiers. The amplifier described here is a two valve one giving very acceptable quality at a cost of under $£ 6$.

## The Circuit

The input is fed directly to the tone and volume control stage and although this is a passive network, gives wide control over the tone. The output from this is fed to the first valve, EF86, which is a high


Fig. 2: The wiring of the tone control panel.
 former is fed to the cathode of this stage which makes use of extra gain by improving the overall quality.

The output of the first stage is fed to the triode section of the ECL86 which further amplifies the signal and applies this to the grid of the output section in the same valve which applies the signal to the output transformer in the anode circuit.

The only component that is critical with regard to quality is the output transformer, the difference between a good one and a small cheap one is tremendous. Any good transformer having a primary impedance of about $8 \mathrm{k} \Omega$ will do.
Because of the high gain of the EF86, care should be exercised in the layout of the components. The main sources of noise in an amplifier are the components associated with this valve and if good noise figures are wanted R3, R4, R5 and R6 should be high stability types. The unscreened lead to the grid of the first valve should be kept as short as possible.
All the main components are mounted on a chassis

[^3]

Fig. 3: The under chassis wiring.

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THERE are on the market several types of intercom costing upwards of $£ 210$ s., and there is no doubt that many readers could find a use for one, but doubt whether even this expenditure would be justified. The unit described here comes within our 20 s . limit and this expenditure may make it a viable proposition. It can easily be used as a baby alarm-it is certainly sensitive enough-merely by switching one of the units on permanently.

Most of the commercially available units are arranged so that first a signal button is pressed and the unit is then switched on and the volume level set. Also nearly all of them can be used for "spying", that is, switching on by the master activates the slave microphone so that the master can eavesdrop.

The unit described here is not fitted with a buzzer as calling over the unit is usually enough to draw the attention of the distant party. It cannot be used for eavesdropping (an undesirable, "Big Brother" type feature) and thus its installation can cause no offence. Since no volume control is fitted (this is really unnecessary for this type of equipment) only one control is made by either end to activate the unit.

## The Circuit

The basis of the intercom is a simple amplifier which boosts the "microphone" output to feed a speaker. To make the project simpler and cheaper we use balanced armature earpieces which, by being switched, serve both functions as microphone and


# No. 8 INTERCOM 



The two intercom stations.
loudspeaker. These balanced armature earpieces are really marvellous pieces of design. They are extremely sensitive, have a perfect impedance for transformerless transistor work and are very cheap -mine cost me 2 s ., unfortunately from a retailer who doesn't do mail order. After the Take 20 Electronic Organ I had a number of letters asking where to obtain these and I understand that they are no longer made and are in short supply. However, some are still available from various retailers, but this will not help those who can't obtain them. Eighty-ohm loudspeakers can be used in their place and these, even if a little more expensive and taking us over the 20 s. limit, are available.
The amplifier is slightly unusual and is an alternative to the one described in Take 20 No. 1 as a very simple Lo-Fi (I imagine that's the opposite of $\mathrm{Hi}-\mathrm{Fi}$ !) sensitive a.f. amplifier. It uses a p-n-p and an n-p-n transistor and is R-C coupled. The switching is straightforward; two batteries are used, one each in the master and slave section. This is done purely to enable a three-wire rather than a four-wire connector to be used.
In the normal position (as shown in Fig. 1) no current is drawn and the switch on the master is set to receive calls from the slave. The only thing the slave has to do is apply battery voltage to the master by making SW2.
When the master makes a call the output from the amplifier is fed to the slave loudspeaker, its own loudspeaker is switched to the input, becoming the microphone. and the slave's microphone becomes the loudspeaker switched to the output of the amplifier. The master unit will, of course, override the slave.


Fig. 2: Component layout and wiring details

## * components list



## Construction

Both the sections are built on Paxolin panels about $4 \frac{1}{2} \times 2 \frac{1}{2} \mathrm{in}$. and all the components, including the battery, are mounted on this; the layout is by no means critical and the drawing is self-explanatory (see Fig. 2).

Although it may be better if press button switches were used, these are not readily available and are rather dear compared with the rotary switches used here. Also, using rotary switches enables either of these units to be switched on permanently for use as a baby alarm.

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T|HE purpose of this article is to show that it is possible to design an output stage operating in the class "A" mode, with very little involved mathematics. The design procedure is based on several "rules of thumb" and the assumption that the losses are negligible.

A power amplifier designed by this method will prove to be a viable proposition, and gives the added satisfaction of being able to say "I designed and built it myself". For simplicity of design the input to the amplifier is transformer coupled, see Fig. 1.

First we decide on the output power required and the supply voltage that is available. We then choose a transistor capable of meeting the specification. In this example, the required power is 2 watts and the power supply is to be a fully-charged car battery, the voltage of which will be about 14.5 volts.

A transistor which will more than "fit the bill" is type OC35, which is, incidentally, readily available on the surplus market. Ignoring any losses, the power required ( $P_{0}$ ) is equal to the peak collector current ( $I_{\mathrm{c}}$ ) times the peak collector voltage ( $V_{\mathrm{c}}$ ), each divided by the square root of 2 to obtain r.m.s. values.

The peak collector current can be determined thus:

$$
P_{\mathrm{o}}=\frac{V_{\mathrm{c}}}{\sqrt{2}} \times \frac{I_{\mathrm{c}}}{\sqrt{2}} \quad \therefore I_{\mathrm{c}}=P_{\mathrm{o}}(\sqrt{2}) \times \frac{\sqrt{2}}{V_{\mathrm{c}}}
$$

Substituting our requirements this becomes:

$$
=2 \sqrt{2} \times \frac{\sqrt{2}}{14 \cdot 5}=278 \mathrm{~mA}, \text { or approx. } 300 \mathrm{~mA}
$$

In class " $A$ ", the d.c. collector current and the peak collector current are similar, and can be considered equal. Thus the collector voltage and current are 14.5 volts and 0.3 amps respectively. The voltage drop across $\mathrm{R}_{\mathrm{e}}$ is usually around 0.6 volts in power output stages. This value is calculated from: $\mathrm{R}_{\mathrm{e}}=\frac{V}{I_{\mathrm{e}}}$ where $V$ equals 0.6 volts, and $I_{\mathrm{e}}$ is considered equal to $I_{\mathrm{c}}$, which is equal to 0.3 amps . Thus here $\mathrm{R}_{\mathrm{e}}=2$ ohms.

The voltage from base to earth is equal to the base-toemitter voltage ( $V_{\mathrm{be}}$ ) of the transistor (normally 0.6 volts in silicon, 0.4 volts in germanium transistors) plus the voltage drop across $\mathrm{R}_{\mathrm{e}}$, in this case 0.6 V . The voltage across R2 is therefore 1 V . By "rule of thumb" R2 is made equal to $\mathrm{R}_{\mathrm{e}}$ times 10 , or 20 ohms (use preferred value 22 ohms). Thus the current through R2 is equal to the voltage across R2 divided by R2, which equals in this example 45 mA .
The current through R1 can be considered equal, since the base current is very small in comparison with the bleed current through resistors R1 and R2.

Thus R1 $=\frac{14 \cdot 5-1}{45 \mathrm{~mA}}=320 \mathrm{ohms}$ (use 330 ohms ). (The


Fig. 1: The circuit referred to in the text.
voltage drop across Tl can be ignored, the d.c. resistance being very small.)

The output transformer requirements are calculated from the a.c. voltages and currents in the circuit. The peak collector voltage swing that can be utilised before "clipping" occurs is approximately $90 \%$ of the supply voltage, or 13 volts in this example.

The peak collector current swing available is, as previously stated, 300 mA . The collector load should thus be 13 volts divided by 300 mA or approx. 43 ohms in this case. The transformer should match this impedance to the actual load impedance used. A 3 ohm loudspeaker is to be the load here, thus the impedance ratio should be $43: 3$ ohms or the turns/voltage ratio should be $\sqrt{(43: 3)}$ or $3 \cdot 8: 1$.

The total input power that is required to drive the stage to full output is the voltage needed across T1 secondary times the current. This current is equal to the base current required. This is determined from the transistor characteristics, being the value of peak collector current divided by the $\beta$ value for the transistor at that current. Here, $\beta$ is equal to the range 25-75 for an OC35. Choosing the mean, 50 , and from previously calculated collector current 300 mA , drive signal required is 0.3 A divided by 50 , which equals 6 mA peak, or 4.2 mA r.m.s.

The peak input a.c. voltage is nearly equal to the sum of the base-emitter voltage, plus the voltage across $\mathbf{R}_{\mathrm{e}}$, plus the peak a.c. voltage across $\mathrm{R} 2(6 \mathrm{~mA} \times 22 \mathrm{ohms})$.

Thus, in this case, the drive voltage required is equal to 1.132 V peak $(0.4 \mathrm{~V}+0.6 \mathrm{~V}+0.132 \mathrm{~V})$ or 0.8 volts r.m.s. The total a.c. power required is thus 0.8 volts times 4.2 mA , or 3.4 mW . The input impedance is 0.8 volts divided by 4.2 mA , that is about 200 ohms. T1 should be designed to match this impedance to the optimum load for the preceding stage. This can be designed along the same lines as the power amplifier discussed in this article.


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$1,0007-0.001,0.0022,0.0047,0.01,0.02,1 / 6 ; 0.047,0.1,2 / 6$. 8ILVER MICA. Close tolerance $1 \%$. 6 -500p F $1 /-$; $580-2,200 \mathrm{pF}$ $2 /-; 2,700-5,600 \mathrm{pF} 8 / 6 ; 6.800 \mathrm{pF} 0.01$, midd $6 /-$ each. THIN GANG. 0 208pF $+176 \mathrm{pF}, 10 / 6 ; 385 \mathrm{pF}$, miniature $10 / 8 ; 500 \mathrm{pF}$ standard with trimmers, $18 / 6 ; 500 \mathrm{pF}$ midget less trimmert, 7/8;500pR slow motion, randard $9 /-$ small 8 -gang 500p $19 / 6$. Single "0" $865 \mathrm{pF} 7 / 6$. Twin 10/6. SHORT WAVE. $8 \mathrm{jngle} 10 \mathrm{pF}, 25 \mathrm{pF}, 60 \mathrm{pF}, 75 \mathrm{pF}$, 100 pF $100 \mathrm{pF}, 200 \mathrm{nz}, 10 / 6$ oach.
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IN the last two parts the operation of the minority carrier transistor was explained. These devices depend on the injection of carriers into a base region across which they diffuse towards the collector. They can thus be thought of as charge controlled devices. Shockley and his colleagues discovered these devices in 1948. They had been trying to make an amplifying device, though of a different type to that they found. Theit idea had been to find a device whose conductivity was altered by changing the voltage applied to a separate electrode. They were looking in fact for a field controlled device which would not depend on the injection of minority carriers for its operation but rather on the regulation of the current carried by the majority carriers by a field in the device. It would thus be a majority carrier device and because the current would be carried by only one type of carrier it would be "unipolar".
However because of the rather poor specimens of semiconducting material which were then available Shockley had very little success. It was not until 1958 that the first field effect transistor was produced, by a French firm under the name Technetron. This was not a commercial device and it was not until 1962 that an American firm produced the first commercial f.e.t., priced at about 50s.
The first f.e.t. devices were junction field effect transistors, or j.u.f.e.ts. Later a superior device became available, the metal oxide field effect transistor or m.o.s.t. This latter device has an insulated gate electrode and is sometimes called an insulated gate field effect transistor or in short an i.g.f.e.t.

## Junction Field Effect Transistors

Before describing the method of operation of the junction field effect transistor it is perhaps best to describe its construction. The simplest geometrical arrangement is that shown in Fig. 1. It consists of an n-type slice of silicon into which a heavily doped p-type layer is diffused to form the gate of the transistor. Contacts are provided at either end of the slice by $n^{+}$diffusion, giving ohmic contacts which are called the source and drain terminals. Practical devices are constructed by a double diffusion process. A p-type substrate is used and an n-type channel region diffused into it. A second diffusion of p-type material then forms the gate region. Such a structure is shown in Fig. 2.

Returning to the simple structure shown in Fig. 1 it will be seen that if the gate electrode is made negative with respect to the source the junction will be reverse biased. Consequently a depletion layer will extend into the n-type silicon. If at the same time a voltage is applied between the source and drain electrodes a current will flow through the channel of n-type silicon. By definition the source terminal is that from which
the current carriers originate and the drain terminal is the one to which they go.

## Junction f.e.t. Characteristics

In this example the source is the negative terminal and the drain is positive, thus there is a potential drop between these electrodes. Near the source the reverse bias across the junction will be essentially the same as the gate to source voltage, Vgs, but nearer the drain the reverse bias is greater because of the voltage drop across the drain to source channel region. The result of this is that the channel available for conduction is reduced in


Fig. 1: Basic junction field effect transistor and its equivalent circuit and biasing.

Fig. 2 (below): Practical junction f.e.t. structure.

width so that the resistance between the source and drain electrodes is increased as the drain current increases. Eventually, the channel is reduced to such a width that further increase in the drain to source voltage produces no increase in the drain current. Of course the channel is never completely closed as this would lead to zero drain current, with a resultant fall in the potential drop between the drain and source and a widening of the channel once more. The voltage at the gate which produces an essentially constant drain current is called the pinch off voltage, Vp . This depends very much on the construction of the device and at present most of the commercially available field effect transistors have a large spread in their pinch off voltages.


Fig. 3: Curves showing variation in drain current with drain voltage for different gate voltages.

From the characteristic curve shown in Fig. 3 it is seen that at high drain to source voltages the drain current suddenly increases. This is because of our old friend the avalanche effect. The large voltage is in effect in series with the reverse voltage across the gate junction and produces avalanching in this region. This effect sets a limit to the maximum voltage that can be applied to the f.e.t. either directly to the gate or via the drain supply.

It is possible to make both n - and p -channel junction field effect devices. The n-channel device gives a decreased drain current if the gate is made negative whilst p-channel device gives a decreased drain current if the gate is made positive.

## Insulated Gate Field Effect Transistors

A later addition to the range of the majority carrier devices was the insulated gate field effect transistor. Although the input resistance of the gate electrode of the junction f.e.t. is high, often being of the order of $100 \mathrm{M} \Omega$, that of the i.g.f.e.t. is often up to $10^{14} \Omega$ or $100 \mathrm{MM} \Omega$. This is of course of immense value in high input impedance instruments used in laboratories and for circuits requiring low loading of previous stages.

The insulated gate field effect transistor, or metal oxide silicon transistor as it is more usually called, is made by diffusing into a p-type substrate two heavily doped $\mathrm{n}^{+}$regions which act as source and train electrodes, being separated by perhaps 1 mil. A layer of silicon oxide is then grown over the top of the device and two holes are etched in this to enable metal contacts to be attached to the source and drain. A further layer of metal is attached to the oxide over the region between the source and drain as seen in Fig. 4: this becomes the gate terminal of the complete device.


Fig. 4: Structure of an enhancement-mode insulated gate field effect transistor.


Fig. 5: Enhancement-mode insulated gate field effect transistor characteristic curve.

The operation of the m.o.s.t. is explained quite easily by considering the arrangement of Fig. 4. If the gate is made positive with respect to the substrate an electric field will be developed and will induce charges on the surface of the semiconductor. Since the field is directed into the surface negative charges will be induced by the force acting on the atoms in the semiconductor. In this way a layer of negative charge is produced between the source and drain, which results in a decreased source to drain resistance and an increase in the drain current.

## Enhancement Mode Operation

The layer of induced charge is called an inversion layer because the charge carrier is of opposite type to that in the bulk of the semiconductor. This arrangement is called the enhancement type of m.o.s.t. as the conductivity of the channel is enhanced by application of the gate potential. It is characterised by the fact that very little current flows through the channel when there is no field at the gate. A curve showing the relationship between the drain current and the gate voltage of a typical m.o.s.t. of the enhancement type is shown in Fig. 5. It is seen that only a very small current flows through the device until a gate threshold voltage Vgst is reached. This threshold voltage varies from device to device and is the voltage required to produce the inversion charge layer.


Fig. 6: Depletion-mode i.g.f.e.t. construction.

## Depletion Mode Operation

A second type of insulated gate f.e.t. exists, called a depletion type device. This has an n-type layer diffused into the region between the source and drain as can be seen in Fig. 6. Consequently a considerable current flows through the device when there is zero applied gate voltage because of the conductivity of this channel. However if the gate is made negative relative to the
continued on page 622


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# NDTM <br> NOISE Tixice M. WALLIS 



ANYONE who has tried DXing will know that one of the limitations on receiving those prized stations is the background noise, static etc. Frequently one can hear a station below this noise but it cannot be identified for sure because it is swamped by the noise level, and of course increasing the volume doesn't help.

Others may be interested in very old 78r.p.m. records, some of which have a very low modulation level compared with the inevitable scratches; here the audio limiter will work well, although it is primarily designed for radio use, fitting between the phone output socket and the headphones.

Most good communication receivers are fitted with a noise limiter which automatically adjusts itself to limit just above the level of the incoming signal. There is however a strong disadvantage in this system; the limiter will only cut signals above the average and of course the noise itself contributes to that average. Such a limiter, in heavy noise conditions, will limit the peaks of the noise


Fig. 7: The audio noise limiter using transistors biased almost to cut-off for clipping noise.
rather than that of the signal. Simpler non-automatic noise limiters do not suffer from this, but since they cannot be controlled are virtually ineffective on weak signals.

The unit described here not only overcomes these problems but requires no modification to the set; it is a self-powered unit which is fitted between the set and the headphones. It doesn't matter whether the phones' take-off point is immediately after the volume control or across the loudspeaker, it will work equally well on both.

In addition to acting as a limiter in the normal manner it is also extremely effective at reducing the effects of side-band splash caused either by a close adjacent transmission or cross-modulation within the receiver itself. The unit can be adjusted so that the wanted signal is at comfortable listening level and the splash only reaching that level at a maximum. In addition treble cut is incorporated in the circuit making this even less objectionable.

As well as doing all the above it provides audio gain-useful when the audio stages are working flat out and the signal is still too quiet. It has another advantage over more conventional diode type clippers in that it "rounds off" the clipped signal rather than converting it into a sort of square wave which is heard as a nasty "rasping" sound. The same circuit can be used as a speech compressor for transmitters and similar equipment.

## components list

## Resistors:

| R1, 3 | $2 \cdot 2 \mathrm{M} \Omega$ | VR1 | $500 \mathrm{k} \Omega \log$. |
| :--- | :--- | :--- | :--- |
| R2, 5 | $5 \cdot 6 \mathrm{k} \Omega$ | VR2 | $5 \mathrm{k} \Omega \log$. |

R2, $5 \quad 5 \cdot 6 \mathrm{k} \Omega$ VR2 $5 k \Omega \log$.

## The Circuit

The output from the receiver is connected across VR1, a $500 \mathrm{k} \Omega$ potentiometer. Its high value prevents it loading previous stages in certain types of radios, at the same time this value works perfectly well for all inputs. (It may be found that with VR1 at its maximum setting the input impedance of the transistor loads previous stages on certain radios. This will not generally matter as the control will rarely be on maximum but can be overcome by fitting a $47 \mathrm{k} \Omega$ resistor between the input and the top of VR1.)

The signal is fed to the base of Tr 1 via Cl which acts

(C)
(D)
(A) A typical incoming audio signal with noise peaks apparent. (B) A diode type noise limiter will clip the peaks squarely. causing splatter. (c) The first stage of the audio limiter (Fig. 1) will clip and round off the lower peaks. (D) TR2 completes the process by flattening the upper peaks.
as a d.c. blocking capacitor. Tr 1 is biased by R 1 , $2 \cdot 2 \mathrm{M} \Omega$; in small signal conditions this acts as a linear amplifier but with high level signals the positive peaks will bias Tr 1 towards cut-off. Phase inversion takes place in Tr 1 since it is arranged as a common-emitter amplifier and the signal is fed via C2 to the junction of R3 and R4. R3, $2 \cdot 2 \mathrm{M} \Omega$ provides the bias for Tr 2 while


Fig. 2: The rear view chassis layout and component grouping on the Veroboard. The soldering tag connects to F1


The rear view o, the limiter.

R4 attenuates the signal so that the cut-off points will be the same as for $\operatorname{Tr} 1$.

Negative peaks were unaffected by Trl but after inversion they become positive peaks and are limited by Tr 2 . The output from Tr 2 is taken via C3 to the top of VR2 which acts as a straightforward volume control. This is necessary as the level at which it is required to limit is not necessarily the level at which you want to listen.

SW1 in the on position as shown in Fig. 1 provides battery power to the unit and also the headphones to the output of the limiter. In the off position the battery is disconnected and the phones taken directly to the input, making the limiter inoperative. This enables the limiter to be permanently connected and makes for easy comparison between the corrected and uncorrected signal.

## Construction

The prototype was built into a small aluminium case, $4 \times 2 \frac{1}{2} \times 2 \mathrm{in}$., which was supplied with a flanged lid. These small instrument cases are fairly widely available but if difficulty is experienced a small aluminium case can be made up or another type of box (even plastic) used. All the components are mounted on the lid as shown in the photograph. The two transistors and associated components are mounted on a small piece of Veroboard $13 \times 9$ holes.

The centre hole of the board is drilled out to take a 4BA screw and six adjacent holes should have the copper strip removed as shown in Fig. 2. The board itself is mounted behind the two variable resistors on a $1 \frac{1}{2} \mathrm{in}$. screw and held by a couple of 4BA nuts. A solder tag should be fitted under the top nut and a wire from this taken to the positive strip. Apart from the above points construction is perfectly straightforward if Fig. 2 is carefully followed.

## Usage

After checking that all wiring etc. is correct, with the slide switch in the off position, plug the unit into the radio and the phones into the unit. Set the volume of the radio to a comfortable level. Now switch the unit on and adjust VR1 to a level just below a point where rasping is heard and distortion is not noticeable. Above this point the limiter is overloaded and the transistors are completely cut off. Next set VR2 to a comfortable listening level. VR1 and VR2 will have to be set for each signal heard but a considerable improvement will be heard between the unit inserted and out of circuit. A little practice to achieve the best balance between receiver volume, limiting level and output level is needed but after this it should be invaluable for DX listening.


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BOTH germanium and silicon diffused diodes are available but due to the greater operating temperature and low reverse leakage of silicon devices they have virtually eliminated germanium diodes for power rectification. Diffused diodes are capable of passing high currents and can be made to close tolerances to give the required reverse characteristics. They are robust and reliable and therefore ideal for general purpose applications.

A further increase in robustness is obtained in the glass encapsulation by using a technique of inserting molybdenum blocks between the junction and the lead-out wires. These blocks match the glass and metal temperature coefficients and thus remove the requirement for the " S "-shaped connection. Such devices are sometimes referred to as "whiskerless diffused diodes" and despite the construction are obtainable at prices between 2 s . and 5 s . each.

## Avalanche Diodes

The avalanche diode is a development of the diffused construction which considerably reduces failures due to reverse voltage transients. To enhance the avalanche breakdown protection the periphery of the diffused junction is chamfered to a fairly critical angle. The slice is then cleaned and the edge treated with varnish or resin.

The chamfering affects the edge irregularities and properties. During transient switch-off the current flows mainly in the periphery of the junction and as a result this technique enables the diode to withstand greater transients. The avalanche rectifier is therefore particularly suitable for applications in which transients are likely to be encountered-such as high-speed power switching. It must be remembered however that the avalanche diode does not have a higher frequency response than the normal diffused


Fig. 10: Basic rectifier assemblies.
rectifier and is only suitable for power switching below 20 kHz before derating for switching losses is necessary.

A development which does lead to an increased working frequency is the addition of gold to the diffused junction. The gold reduces the recombination time of the charges within the junction on switch-off and considerably reduces the switch-off time. Most fast switching rectifiers operating with up to 50 kHz squarewaves utilise this modified construction.

## Gold-Bonded Diodes

Signal diodes which utilise this addition of gold are referred to as gold-bonded diodes and are available in both silicon and germanium materials. As they are manufactured to give increased frequency of operation germanium is often used and germanium gold-bonded diodes have high frequency characteristics closely approaching those of the point contact diode.

## Planar Epitaxial Diodes

Another form of construction which has resulted in increased switching speeds is the planar epitaxial construction. This method of forming the junction utilises silicon dioxide as a masking layer and a photographic etching technique: it is explained fully in other parts in this series. The encapsulation for signal diodes is usually glass as shown in Fig. 8 but plastic encapsulations are now appearing with a resultant reduction in cost.

Planar diodes are reliable and are used in highspeed switching circuits such as computers. Several power rectifiers are now available with this form of construction which gives increased switching performance, although at the present time they are considerably more expensive than diffused rectifiers.

## Bridges and Assemblies

The general use in industrial and commercial applications of plastic encapsulation has led to the introduction of diode rectifier assemblies encapsulated in plastics. These assemblies are available in various forms of which the bridge rectifier and centre tapped transformer rectifier configurations shown in Fig. 10 are the most popular. Individual rectifiers, signal diodes and zener diodes are all now available in plastic encapsulations at a considerable saving in cost.

Table 4: General comparison of available diodes

| Construction | Material | Typical parameters |  |  | Encapsulation | Cost | Application |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Maximum forward current | Average reverse current | Reverse voltage |  |  |  |
| Point contact | Germanium | 50 mA | 10-500 A | 30-150V | glass | 1s. to 5 s . | V.H.F. signal diode |
| Gold bonded | Germanium | 100 mA | $7-200 \mu \mathrm{~A}$ | 30-150V | glass | 1s. 1d. to 5 s . | V.H.F. signal diode |
| Junction | Germanium Silicon | $\begin{aligned} & 1 \mathrm{~A} \\ & 1 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 1-100 \mu \mathrm{~A} \\ & 0 \cdot 01-1 \mu \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 100-800 \mathrm{~V} \\ & 100-800 \mathrm{~V} \end{aligned}$ | glass, metal $\int$ and plastic | $\begin{aligned} & 3 \mathrm{~s} . \text { to } 10 \mathrm{~s} . \\ & 2 \mathrm{~s} . \text { to } 10 \mathrm{~s} . \end{aligned}$ | $\} \text { general purpose }$ |
| Whiskerless diffused | Silicon | 200 mA | $0.01-1 \mu \mathrm{~A}$ | 50-200V | glass | 2s. to 5s. | High-speed switching |
| Diffusion | Silicon | $>250 \mathrm{~A}$ | $0 \cdot 01-100 \mu \mathrm{~A}$ | 100-1,200V | metal and plastic | see table 1 | General purpose and rectification |
| Planar | Silicon | $\begin{aligned} & 100 \mathrm{~mA} \text { and } \\ & 10 \mathrm{~A} \end{aligned}$ | $0 \cdot 001-1 \mu \mathrm{~A}$ | 25-800V | glass, metal and plastic | 1s. to $f 1$ <br> £2 upward | Signal <br> Power rectification h.f. |
| Avalanche diffused | Silicon | $>50 \mathrm{~A}$ | $0.01-100 \mu \mathrm{~A}$ | 200-1200V | metal and plastic | 10s. upward | Switching and rectification with transients |
| Bridges | Silicon | $>10 \mathrm{~A}$ | $0.01-100 \mu \mathrm{~A}$ | 100-1000V | metal but mainly plastic | 11s. to $£ 20$ | Transformer power rectification |

Figure 11 illustrates two bridge encapsulations primarily intended for use as rectifier bridges. Figure 11 (a) shows a 1.8 A silicon rectifier bridge which can be wired directly to a printed circuit without the necessity of a heatsink. Figure 11(b) shows a 10A silicon rectifier bridge which can be bolted to a heatsink. Both are considerably smaller than general attempts to mount four diodes to give the same performance.

## Conclusion

Table 4 summarises the main methods of construction, their parameters, cost and uses. This should not be regarded as absolute in any parameter or statement but just a typical device range of the


Fig. 11: (a) 1.8A and (b) 10A bridge encapsulations.
particular construction. There are many hundreds of different device types and this article will have served its purpose if the search for a required diode is reduced to a given form of construction.

## TO BE CONTINUED

## LOW COST VALVE AMPLIFIER

## components list

| Resistors: |  |
| :---: | :---: |
| R1 $680 \mathrm{k} \Omega$ | R9 $4.7 \mathrm{k} \Omega$ |
| R2 $68 \mathrm{k} \Omega$ | R10 $220 \mathrm{k} \Omega$ |
| R3 $1 \mathrm{M} \Omega$ high-stab. | R11 10k $\Omega$ |
| R4 150k $\Omega$ high-stab. | R12 $3.3 \mathrm{k} \Omega 1$ watt |
| R5 $2.7 \mathrm{k} \Omega$ high-stab. | R13 820k $\Omega$ |
| R6100 2 high-stab. | R14 180 2 watt |
| R7 150k $\Omega$ | R15 33k $\Omega$ |
| R8 $560 \mathrm{k} \Omega$ | R16 $27 \mathrm{k} \Omega$ |
| All $10 \% \frac{1}{4}$ watt except where stated. |  |
| Capacitors: |  |
| C1 150pF | C8, C9 $8 \mu \mathrm{~F} 350 \mathrm{~V}$ |
| C2 1000pF | C10 $50 \mu \mathrm{~F} 25 \mathrm{~V}$ |
| C3 620pF | C110.1 $\mu \mathrm{F} 150 \mathrm{~V}$ |
| C4 4700pF | $\mathrm{C} 1250 \mu \mathrm{~F} 25 \mathrm{~V}$ |
| C5 $0.05 \mu \mathrm{~F} 150 \mathrm{~V}$ | C13 100pF |
| C6 $100 \mu \mathrm{~F} 25 \mathrm{~V}$ | C14 100pF |
| C7 $0.5 \mu \mathrm{~F} 150 \mathrm{~V}$ | C100p |
| Miscellaneous: |  |
| VR1, VR2, VR3 $2 \mathrm{M} \Omega$ log pots.V1 EF86 |  |
|  |  |
| V2 ECL86 |  |
| Metal chassis, metal panel (see text); Outp transformer (see text); Two B9A valve base Suitable power supply. |  |

about $6 \times 6 \times 2 \frac{1}{2}$ ins., and the controls on a panel $6 \times 2 \frac{1}{2}$. No details are given for a power supply as any capable of giving between 200 V . and 350 V . at 75 mA and 6.3 V . 1.5 A . will do.


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THIS article is intended to help those constructors and experimenters who like myself have been frustrated in attempting to decide which, out of a number of capacitors or inductors, is the one with the required value. A bridge is undoubtedly the quickest, and possibly the best method, but values may be easily determined by another method employing a grid dip oscillator (g.d.o.), a calibrated capacitor and a coil of an arbitrary value.

The method used is simplicity itself. If the coil is connected across the calibrated capacitor, which should be adjusted to somewhere near its maximum capacitance the combination will resonate at some particular frequency which is determined by use of the grid dip oscillator, with as loose a coupling as possible to prevent "pulling" of the oscillator frequency. The unknown capacitor is now connected across the combination in parallel, and the variable capacitor is reduced in value until the combination once again resonates at the same frequency. Now, since the frequencies are the same, and the coil is the same, the total capacitance must also be the same as before. Thus it must be obvious that the variable capacitor has been decreased in value by an amount which is equal to the value of the unknown capacitor. The value of this is, therefore, simply the difference between the two readings on the calibrated capacitor.


Fig. 1: By placing a G.D.O. near the tuned circuit using the calibrated capacitor, unknown capacitors and inductors are quickly measured.

The method used in the determination of inductance is slightly different, inasmuch as it involves a small amount of calculation. The unknown inductor is connected as before, across the calibrated capacitor, and the resonant frequency is determined with the grid dip oscillator. The value is now calculated using the formula:

$$
\mathrm{f}=\frac{1}{2 \pi \sqrt{\mathrm{L.C}} .}
$$

Where $f$ is the measured resonant frequency in Hz , L is the inductance in Henrys, C is the capacitance in Farads.

## CONSTRUCTION AND CALIBRATION

The variable capacitor to be employed should be beyond reproach, in that it should be free from any backlash or play in the bearings. Attention to these details will contribute to the final accuracy and quality of the capacitor. The most useful value to use is in the region of 200 pF , since this will enable small increments of capacitance to be read off with ease. Larger values may be made up by adding good quality capacitors of known value in parallel. Direct calibration may be used where the actual value of capacitance is marked for each division on the scale, or a calibration graph may be drawn where the angle of rotation of the cursor is plotted against capacitance. The latter is the better method, since a good graph will avoid any errors which may be made in drawing in the individual points using direct calibration. Another advantage is that scales and knobs are available already marked in degrees.

Calibration may be carried out, either by the easiest method of borrowing a bridge from an affluent friend, or a simple bridge may be made up for the purpose. The circuit shown in Fig. 2 will serve.

The oscillator is a simple feedback type which has a frequency of about 1 kHz , but if an oscillator is already available with a higher frequency, then it may be used, provided it operates in audible frequency range.
The bridge section uses headphones for detection. The resistors R5 and R6 should be close tolerance high stability types and, for Cx , a number of close tolerance, silvered mica capacitors, with values ranging up to near the maximum value of the capacitor to be calibrated. Where is graph to be drawn, a smaller number of fixed value capacitors will be required, since the number of points needed in order to draw the graph is less than the number required to give individual points for direct calibration.

When the bridge is at balance, the voltage at point $A$, equals the voltage


Fig. 2: The circuit used for accurately calibrating the capacitor, shown as CV above.
at point $B$. Therefore, the potential difference across $C x$ and Cv must be equal. Thus since the values of the resistors are the same with equal potential differences across each, it will follow that the values of capacitors Cx and Cv will be the same. The balance condition for the bridge is, of course, that at which a null point is detected in the phones.

No dimensions in relation to the actual construction are offered, as the types of capacitor available will differ in physical size. The best type to use is one providing a linear relationship between capacitance and angle of rotation.

For the case, plywood or aluminium is suitable, but the terminals should be mounted on a panel of paxolin or synthetic resin-bonded paper in order to minimise losses. For this reason also, it is best not to place the terminals too close together; a separation of about two inches is suitable, whilst bearing in mind the lengths of the wire leads on components which may have to be connected across.

The capacitor terminals should be brought out through the same side of the case as that upon which the capacitor itself is mounted. This will minimise upsetting of the calibration should the case have to be opened for any reason. For ease of dial positioning, a reduction drive should be fitted, which, needless to say, must be free from backlash.

As a final note the constructor will find this simple unit of great value, and apart from the previously mentioned uses, it will be found most useful in a number of other ways which include: frequency comparison, calibration, as a bridge component, etc.

## BASIC SEMICONDUCTOR TECHNOLOGY

## -continued from page 610

source, an induced positive charge appears on the surface of the n-type channel layer and as this is composed of relatively immobile charges the conductivity of the channel is decreased. Because the device relies on the reduction in the number of charge carriers as the gate voltage is increased it is called a depletion m.o.s.t. A maximum value of gate voltage which can be applied to this device is set by the field required to reduce the drain current to a negligible value.


Fig. 7: Curve of drain current against gate voltage for a depletion mode i.g.f.e.t.

This very same device can also be used in the enhancement mode by making the gate positive with respect to the source. In this situation negative charges are induced on the surface of the channel which increase
its conductivity. A curve showing the variation of drain current with the gate voltage is shown in Fig. 7, where the regions of enhancement and depletion operation are shown. In most applications the substrate is connected to the source terminal. However it can also be used as a second gate terminal.

Because of the very high input impedance of the m.o.s.t. the gate is capable of storing a very small quantity of charge for a long time. This is useful when it is required to measure the voltage of a small capacitor. However it also means that if the gate is left opencircuited small charges induced on it from external static electricity can build up large voltages which are capable of puncturing the very thin insulating layer between the gate and channel. In order to avoid this it is necessary to keep an external short between the gate and source. This is provided by the manufacturers and should not be removed until the device is wired into the circuit. A second method of avoiding this danger is adopted in some devices. This involves a diode built into the device across the vulnerable leads. The breakdown voltage of the diode is arranged to be less than that of the m.o.s.t. so that irreparable damage is not done to the device if an excessive voltage is applied. However this reduces the input impedance of the device which is not therefore suitable for use in very high impedance circuits.

## Advantages of f.e.t.s.

The main advantages of field effect transistors over conventional bipolar transistors are as follows:
(1) They have in general very high input impedances; in the case of the m.o.s.t. this can reach $10^{14} \Omega$. This makes them very useful for measuring voltages from very high impedance sources in such applications as pH measurement, measurement of very small charges etc.
(2) Except at low frequencies they are much quieter than valves of bipolar transistors. This makes them more suitable for low level amplification where noise is especially important.
(3) Since they do not rely on the diffusion of minority carriers across a potential barrier-as the bipolar transistor does-they are far more stable with respect to temperature than the conventional transistor.
(4) The input signal to the gate terminal is measured in volts rather than the millivolts commonly applied to minority carrier devices. This leads to their use in applications where higher voltages are involved, such as high level logic circuits. They can even be used in valve circuits, forming hybrid arrangements, providing the correct voltages are applied to them.
(5) Lastly but perhaps of most importance there is no offset voltage in their drain current versus drain voltage characteristic so that they are ideally suited for use as analogue switches and in chopper circuits for amplifying small d.c. voltages.

It would appear that these devices are always better than bipolar transistors. However they do have some disadvantages. For example they have a smaller gainbandwidth product than the normal transistor, and as a switch they have a much greater "on" resistance than the bipolar device does, amounting to several hundred ohms.

## TO BE CONTINUED

[^5]

# MONOLITHIC INTEGRATED CIRCUIT HIGH FIDELITY AMPLIFIER AND PRE-AMP 



## the world's most advanced high fidelity amplifier

The Sinclair IC-10 is the world's first monolithic integrated circuit high fidelity power amplifier and pre-amplifier. The circuit itself, a chip of silicon only a twentieth of an inch square by a hundredth of an inch thick, has an output of 5 watts R.M.S. ( 10 watts peak). It contains 13 transistors (including two power types). 2 diodes, 1 zenor diode and 18 resistors, formed simultaneously in the silicon by a series of diffusions. The chip is encapsulated in a solid plastic package which holds the metal heat sink and connecting pins. This exciting device is not only more rugged and reliable than any previous amplifier, it also has considerable performance advantages. The most important are complete freedom from thermal runaway due to the close thermal coupling between the output transistors and the bias diodes and very low level of distortion.
The $1 \mathrm{C}-10$ is primarily intended as a full performance high fidelity power and pre-amplifier, for which application it only requires the addition of the usual tone and volume controls and a battery or mains power supply. However, it is so designed that it may be used simply in many other applications including car radios, electronic organs, servo amplifiers (it is d.c. coupled throughout) etc. The photographic masks required for producing monolithic I.Cs are expensive but once made, the circuits can be produced with complete uniformity and at very low cost. It also enables us to give a 5 year guarantee on each IC-10 knowing that every unit will work as perfectly as the original and do so for a lifetime.

## - SPECIFICATIONS

Output 10 Watts peak, 5 Watts R.M.S. continuous. Frequency response 5 Hz to $100 \mathrm{KHz} \pm 1 \mathrm{~dB}$. Total harmonic distortion Less than $1 \%$ at full output. Load impedance
Power gain 110dB (100,000,000,00

Size
Sensitivity
Input impedance
$1 \times 0.4 \times 0.2$ inches.
Adjustable ext 2.5 M ohms.

## CIRCUIT DESCRIPTION

The first three transistors are used in the pre-amp and the remaining 10 in the power amplifier, Class $A B$ output is used with closely controlled quiescent current which is independent of temperature. Generous negative feedback is used round both sections and the amplifier is completely free from crossover distortion at all supply voltages, making battery operation eminently satisfactory.

## APPLICATIONS

Each IC-10 is sold with a very comprehensive manual giving circuit and wiring diagrams for a large number of applications in addition to high fidelity. These include stabilised power supplies, oscillators, etc. The pre-amp section can be used as an R.F. or I.F. amplifier without any additional transistors.

SINCLAIR

IC. 10 第 $59 / 6$ | 至 | $\square$ | $\square$ | $\square$ | $\square$ |
| :--- | :--- | :--- | :--- | :--- | :--- |



### 2.30

## THE WORLD'S LOWEST DISTORTION HIGH FIDELITY AMPLIFIER.

For four years, the Sinclair $\mathbf{Z . 1 2}$ dominated the constructor world, being the best selling unit of its kind this side of the Atlantic. Excellent as it was, the new Sinclair Z.30 is still better. Half the size of the $\mathbf{Z . 1 2}$, it has more than twice the power, very much greater gain and a level of distortion 50 times lower. This incredible figure results from using over 60 dB of negative feed back with a constant current load to the driver stage obtained by incorporating a two transistor circuit in place of the more usual boot-strapping. 9 silicon epitaxial planar transistors are used to provide enormous power (up to 20 watts RMS continuous sine wave, 40 watts peak). The circuitry of this marvellous amplifier allows it to be operated from any voltage from 8 to 35 to perfection.

At all output levels, distortion is only $0.02 \%$. This puts true laboratory standards into the hands of every user of a $\mathbf{Z . 3 0}$. Two $\mathbf{Z . 3 0 s}$ and a new Stereo Sixty will make a stereo assembly of such perfection that it could not be bettered in its class no matter how much you spent. But the $Z .30$ has an enormous variety of applications, particularly where quality, precision and reliability are essential. Yet this brilliant new Sinclair design costs not a penny more than its famous predecessor.

## APPLICATIONS

$H_{1}$-fi amplifier; car radio amplifier; record player amplifier fed directly from pick-up; intercom: electronic music and instruments; P.A.; laboratory work, etc. Full details for these and many other applications are given in the manual supplied with the $\mathbf{Z . 3 0}$.


Pan



Curves to show bass and treble cut and boost


This attractive and completely new unit is intended for use with two new Z. 30 amplifiers to provide the finest possible standards of stereo reproduction. Four press buttons and four rotary controls are used to provide on-off, three input selectors and Volume. Bass cut/boost, Treble cut/boost and Stereo balance. The on-off button also switches the power amplifiers. The front panel in brushed aluminium is flush mounted to the cabinet front, it being necessary only to drill holes to accommodate the controls. Rear adjustable brackets hold the chassis tight to the cabinet. The very latest ganged rotary controls are used to afford compactness and extra long working life free from noise.
The Stereo-60 may a/so be used with 2 IC-10's or any other high performance amplifiers.

## SPECIFICATIONS

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- Output-1 volt.
- Signal-to-noise ratio-better than 70 dB .
- Channel matching-within 1 dB
- Tone Controls-TREBLE +15 to -15 dB at 10 kHz . BASS +15 to -15 dB at 100 Hz .
- Power consumption 5mA
- Front panel--brushed aluminium with black knobs and controls.
- Size $8 \frac{1}{4} \times 1 \frac{1}{2} \times 4$ ins.


## PZ. 5 POWER SUPPLY UNIT

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Q. 16 Loudspeaker and Micromatic on next page.

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铬.19.8. Post and Insurance 6/6.


ELECTRIC TIME SWITCH
Made by Smiths these are AC mains operated, NOT CLOCKWORK. Ideal for mounting on rack or thelf or can be built into box with 13A socket. 2 completely adjustable time periods per 24 hours, 5 amp changeover periods 59/6, post and ins. $4 / 6$. Additional time contacts 10/-pair.

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Size $26 \mathrm{in} . \times 14 \mathrm{in}$. $\times 9 \frac{1}{2}$ in deep-speaker compart nent each end. Centre portion with hinged lid and romov for amplifler. Two tone (red and grey) rexine covered but loud speaker ends need metal grilles With handle and clips, 22/6. Carriage and packing
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 7 transistor, 2 wave band (medium and long) pocket radio with carrying handle and earplug. These rudios use a ferrite slab aerial and moving coil speaker Completety built up, ready to play. Offered at less than importers price due to bankrupt purchase. A remarkable bargain. 89/6 plus $3 / 6$ post and insurance.

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This Tuner is a preclsion instrument made by the famous "Cyldon" Company for the equally famous Radiomobile Car Radio. It is a medium wave tumer (but set of longwave colls available as an extra if required) with a frequency coverage $1620 \mathrm{Kc} / \mathrm{b}-525 \mathrm{Kc} / \mathrm{s}$ and intended to operate with an I.F. value of $470 \mathrm{Kc} / \mathrm{s}$. Extremely compact (aize only $2 \neq 2 \times$ lins.
thick) with reduction gear for fine tuning. Snip price this thick) with reduction gear for fine tuning. Snip price this month 12/6, with circuit of front end suitable for car radio or

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Just what you need for work bench or lab.
$4 \times 13$ amp sockets in metal box to take standard 13 amp fused plugs. Supplied complete with 6 feet of heavy cable and 13 amp plug. similar advertised at 25 . Our price $39 / 6,+4 / 6 \mathrm{P}$ \& I .

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Will dim incandescent lighting up to 600 watts from full brilliance to out. Fitted on M.K. flush plate, same size and fixing as standard wall switch so may be fitted in place of this, or mount on surface. Price complete in heavy plastic box with control knob 23.19.6.

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14in. length of flexible capillary tubing-control range is $20^{\circ} \mathrm{F}$ to $150^{\circ} \mathrm{F}$ so it is suitable to control range is $20^{\circ}$ F to heating and liquid heating especially when in buckets or portable vessels as the sensor can be raised out and lowered into the vessel. This thermostat could also be used to sound a bell or other alarm when critical temp. \&s reached in stack or heap subject to spontaneous combustion or it liquid is being heated by gas or other means not
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Teddingtom Co., we offer these at $12 / 6$ each. Postage and insurance $2 / 9$.

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FULL F1 12 INOE LOODGPEAKGR. This is undoubtedly one of the finest loudspeakers that we have ever offered, produced by one of the country's most famous makers. It has a die-cast metal frame and is atrongly recommended for Hi-Fi load and Rhythm Guitar and public address. Flux Densitity 11,000 gausg-Total Flux 44,000 MaxwellsPower Handling 15 watts R.M.8. Cone Moulded fibre-Freq response $30-10,000$ c.p.s.-specify 3 or 15 ohms - Mains re
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ing lugs-Baffie hole 11 in . Diam.-Mounting holes 4 , holes ing lugs-Baffie hole 1nin. Diam.-Mounting holes 4, holes 5 inin. A $£ 6$ speaker offered for only 88.9 .6 plus $7 / 6 \mathrm{p}$. \& p . Don't miss this offer. 15 in . 80 watt 87.19 .6 . 18 in . 100 watt 2 p 4.10 .0 .

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Cleans the air
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| 175 | 71 | 6BR8 | 18/6 | 8K7GT | 4/8 | 10 Cl | 18/6 | 26L6GT 7\% | 150 B 2 | $11 / 8$ | DK 52 | $7 / 9$ | ECH21 | 1216 | EM84 | $7 / 6$ |  | 10/6 | SP4 8/- | L84 | 71 |
| 1LD6 | 6/- | 6B87 | 251- | 6K8 | $2 / 8$ | $10 \mathrm{C2}$ | 18/6 | 26 Y 6 6/- | 150 C 4 | $9 / 8$ | DK91 | $8 /$ |  | 11/8 |  |  |  |  |  |  |  |
| 1N5GT | 81 | 6BW6 | 14/6 | 6K8M | $11 / 8$ | 10Fl | 14/8 | 2684 6/3 | 801 | $8 / 6$ | 9K92 | 9 - | ECL |  | RY51 | $7 / 6$ |  |  |  | UU6 |  |
| 1RS | $61-$ | 6BW7 | 18/- | 6K8G | $31-$ | 10F3 | 181- | 2525 8/- | 807 | 9\% | DK | 7/9 | ECH8 | 51 | Y86 | 71 |  | 0/8 | ETV280/80 | UU7 | 81/- |
| 184 | $5 / 8$ | $6 \mathrm{C4}$ | $81-$ | 6K8GT | $71-$ | 10F9 | 10/6 | 2626 8/6 | 8134 |  | DL66 | 85 | ECH83 | 8/6 | EZ35 | $81-$ | PCF84 | $81-$ | 051- | UUB | 81/- |
| 185 | $4 / 8$ | 6C5G | $81-$ | 6K25 | 151- | 10F18 | 81 - | 28D7 9/8 |  | 1801- | DL92 | $8 / 8$ | ECL80 | 5/9 | EZ4 | $8 / 8$ | PCP | 9/- | SU25 19/6 | UU9 | $8 / 8$ |
| 1T4 | $4 / 1$ | 6C6 | $3 / 8$ | 6 Ll | 121- | 10L1 | $81-$ | 30 Cl 8/9 | 813 | ${ }^{751}$ | DL93 | $4 /-$ | ECL82 | $7 / 1$ | 2841 | $9 / 6$ | PCP801 | $9 / 9$ | 6 | UY21 | 16 |
|  |  | 6C8G | $81-$ | 6L60 | $7 / 8$ | 10LD11 | $10 / 6$ |  | 8664 | 151- | DL94 | 6/9 | ECL83 | 10/8 | 12880 | 5/6 | PCF802 | 976 | 17/6 | UY41 | 8 |
|  |  | 60D60 | 241- | 6L18 | $61-$ | 10P13 | 12/6 | $30 \mathrm{Cl7}$ 18/- | 954 | $5 / 8$ | DL95 | 779 | ECL86 | $8 /$ | CZ81 | $5 / 6$ | PCP80 | 15/- | TDD4 $8 / 6$ | UY85 | 816 |
| 886 | 71 - | 6CE6 | $7 / 6$ | 607G | 61- | 11 ES | 701- | 30 Cl 18 15/- | 1625 | 8/6 | DL96 | $7 / 6$ | ECLL8 |  | 0230 | $201-$ | PCP80 | 181- | U10 7/8 | VMP4 | 17/- |
| 384 | 8 | 6CW4 | 12/- | 6Q7GT | $8 / 6$ | 12AT6 | 4/8 | $30 \mathrm{~F} 517-$ | 4022A | $67 /$ | DM 70 | $81-$ |  | 301- | G232 | 10/- | PCP8 | 16 | U14 $\quad 7 / 6$ | VP4 | 85/- |
| $3{ }^{3} 4$ | $6 / 8$ | 6Dd | $8 / 9$ | 68A7M | 71 | 12AT7 | 8/- | 30 FLL 10/- | 5763 | 18/- | DY86 | $8 /-$ | EF9 | 201- | CZ84 |  | PCL8 2 |  | U19 |  |  |
| SR4GY | $10 / 6$ | 6ES | $7 / 6$ | $68 \mathrm{C7}$ | 71 | 12AU6 | $6 / 9$ | 30FLl2 19/- | 7193 | $81-$ | DY87 | 8 - | EF37A | $71-$ | KT36 |  | L |  | 256 $15 / 6$ <br> $15 / 8$  |  |  |
| 5 S 4 O | $5 / 0$ | ${ }_{6}^{6 \mathrm{Fl}}$ | 18 | $68 \mathrm{G7} 7$ |  | 12AU7 |  | 30FL14 16/6 | 74 | 1 |  |  |  |  |  |  | PCL85 | 9/8 | U78 1/6 |  | 8 - |
| 5V4G |  | ${ }^{6 F 6 G}$ | $8 /$ <br> 51 <br> 1 | 68H77 |  | 12BA6 | \% | $\begin{array}{ll}30 \mathrm{LI6} & 17 /- \\ 30 \mathrm{~L} 17 & 17 /-\end{array}$ | A61 ATP4 | $2 / 8$ | EAs0 | 8/6 | HFS50 | 5 | KT81 | 851- | PCL86 | $9 / 8$ | U191 18/9 | VT2 | 151- |
| 6Y9GT | \% | 6F8G | $8 / 6$ | 68K79T | 4/8 | 12BE6 | 6/8 | $\begin{array}{ll}30217 & 17 /- \\ 30 \mathrm{P} 12 & 10 /-\end{array}$ | ATP4 | 121- | EAFP42 | 101- | EF580 | $4 / 8$ | KT81 | 7C5) | PEN | 801- | U251 16/8 | VT81 | $801-$ |
| 6Z4G $8 / 30 \mathrm{~L} 2$ | 717- | 6 FII | $8 / 6$ | 68L7GT | 8/- | 12 CBG | 61 | 30P19 15/- | ATP7 | 8/6 | EB41 | 10/- | EF85 | 7 7- |  | 151- | PENB4 | 20\% | U301 $12 / 8$ | VU111 | 8/9 |
| 647 | 15/- | 6 Fl 3 | 818 | 68N7G | \$/8 | 12E1 | 01- | $30 \mathrm{PL1} 16 /$ - | AU2 | 801- | EBP91 | 8/- | EF86 | $8 / 6$ | KT88 | 301- | PRN45 | 7/- | U403 618 | VU608 |  |
| 8480 | 12/8 |  |  | 6807 844 | 718 | 12J6GT |  | 30PL13 18/6 | AUS | $8 / 9$ | EBC33 | $8 / 6$ | EF89 | 5/8 | KTW6 | $8 / 6$ | PEN4 |  | 4801 28/6 | W81M | 12/6 |
| 6AC7 | 1, | 6F24 | 14/ | 6U5 | 718 | 12K7G | 7/- | 30PL14 15/- | ${ }^{\text {A }} \mathrm{Z} 1$ | 3/ | EBC41 | $9 / 9$ $4 / 9$ | EF92 | 8/9 | KTZ4 | $17 / 8$ | PL81 | 10/9 | UABC80 $/ 8$ | XH1-5 | 51- |
| 6AK5 |  | 6F25 | 151 | 6V6M | 12/- | 12K8GT | $8 /-$ | $\begin{array}{cc}3545 & 11 / 6 \\ 36 L 6 & 9 /-\end{array}$ | AzBLS1 | 16 | EBE80 | $7 / 8$ | EF92 | 151- | ML6 | 176 | PL82 | $8 / 6$ | UAF42 $10 / 6$ | ${ }^{\text {X Pl-5 }}$ | 51- |
| 6AL6 | 1 | 6F29 | 14- | 676G | $4 / 6$ | 1297GT | $81-$ | $\begin{array}{ll}3016 & /- \\ 35 W 4 & 4 / 6\end{array}$ | CCH35 | 161- | EBF83 | 9f- | EF188 | 6/6 | M8P4 | 101- | PL83 | $7 / 6$ | UBC41 $9 / 8$ | X8681- | 10/6 |
| 6AM5 | 4/6 | 6F32 | 219 | 6V6GT | 816 | 128A7 | 81 | $\begin{array}{ll}3528 & 10 / 7\end{array}$ | ${ }_{\text {CL3 }}$ | 801- | EBF89 | 8/6 | EF184 | $7 /-$ | MU14 | $7 / 6$ | PL84 | 71 | UBC81 9/8 | Y68 |  |
| 6AM6 | $8 / 8$ | $6 \mathrm{G6}$ | 216 | 6X4 |  | 12897 |  | 3574 GT 8/6 | ${ }_{\text {CY }}$ | 28/6 | EBL1 | 14- | EL32 | $8 / 6$ | MX40 | 12/6 | PL500 | $14 / 6$ | UBF80 $7 /$ | 3EGl | 65]- |
| 6AB7G | 101- | 6J5 |  | 6XbG |  | 12857 | 819 | 85256 | CY31 | 8/6 | EBL21 | 12/- | EL33 | $12 / 6$ | N78 | 19/- | PX4 | 14/- | BF89 $7 / 8$ | 3FP7 | 801- |
| 6AT6 | 419 | 6 JJGG |  | 7B6 | 11 | 126K7 | $4 / 0$ | $37 \quad 6 / 6$ | DACs2 | 71 | EBL31 | 87/6 | EL34 | 10/8 | N108 | 80/- | PY38 | 1019 | $\begin{array}{ll}\text { UGC84 } & 8 / 8 \\ \text { UCC88 } & 7 / 8\end{array}$ | ECP1 | $501-$ |
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| 6B4G | 201- | 6.J8 | $8 / 6$ | 7C5 | 88/6 | 14H7 | $0 / 8$ | 50B5 6/8 | DaF96 | 7/8 | ECC81 | $8 /$ | EL42 | 1018 | NGT7 | 5.51 | PY82 | 7/9 | UCF80 UCH42 10/6 | ACA1 | $1100 /$. |
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D814V 9．5V D814G 11.0 V
D814D 12.6 V

68V D817B $\begin{array}{rl}82 V & \text { D817V } \\ 100 \mathrm{~V} & \mathrm{D} 817 \mathrm{G}\end{array}$

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