# PRAGTICAL WRELESS <br> AUGUST 1969 <br> <br> \section*{30} 

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met ministry by Airmec. ${ }_{20-80}{ }^{\text {Frequen }}$ $\mathrm{CW} / \mathrm{FM}$ /s. AM orates precision dial, level meter, precision atteniato $1 \mu$ 110m. Operation from 12 Folt D.C. or $0 / 110 / 200 / 250$ Yolt A.C. Size
$12 \times 8 \frac{1}{2} \times 9$ in. Supplied in brand new dition complete with all connectors fully tested. $\$ 45$. Carr. $20 /$ -

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UNR-30 4-BAND COMMUNICATION RECEIVER
Covering $550 \mathrm{Ke} / \mathrm{s}-30 \mathrm{Mc} / \mathrm{s}$. Incorporates BFO. Built in speaker and phone jack. Metal cabinet. Operation 2200 instructions. $\quad$ Carr. $7 / 613 \mathrm{gns}$.


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4 band receiver covering $5 \overline{50} \mathrm{Kc} / \mathrm{s}$ to $30 \mathrm{Mc} / \mathrm{s}$. 40 and 80 metres. 8 valve plus 7 diode circnit. $4 / 8$ ohm output and phone jack. SSB-CW - ANL - Variable BFO S meter Sep bandspread Viariable RF and AF gain controts. 15 $15 / 250 \mathrm{~V}$. A.C. Mains. Beautifully designed, Size: $7 \times 15 \times$ 10n. With instruction manual and service dath. 442.10 .0 , calriage paid. TRIO commuN-
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TRIO JR-500SE 10-80 METRE AMATEUR COMMUNICATION RECEIVER IN STOCK £69.10.0. Carr. paid. SPECIAL BONUS OFFERI TRIO SP5D Matching Speaker Mate and TRIO HS4 Communication Headphones Normal Value f10.7.0., FREE OF CHARGE with every JR.500SE purchased.

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LAFAYETTE LA-224T TRANSISTOR STEREO AMPLIFIER


19 transistors, 8 diodes, IHF music power, 30 W 19 transistors, 8 diodes, IHF music power, 30 W
at 88. Reppons $30-20,000 \pm 2 \mathrm{~dB}$ at 1 W . Dis at $8 \Omega$. Response $30-20,000 \pm 2 \mathrm{~dB}$ at 1 W . Dis
tortion $1 \%$ or less. Inputs 3 mV and 250 mV , tortion 1\% or less. Inputs 3m . Separate L and R . volume con trols. Treble and bass control. Stereo phone jack Brushed aluminium, gold anodised extruded front panel with complementary metal case. Size $10.2 \times$
$39 / 16 \times 713 / 16 \mathrm{in}$. Operation $115 / 230 \mathrm{~V}$. A .

MARCONI TEST EQUIPMENT EX.MILITARY RECONDITIONEDD TF. 144 G STANDARD SIGNAL GENERATORS, 85 Ke/s TOR $0.5 \mathrm{Mc} / \mathrm{s} \& 45 \mathrm{Carr}$. $30 /-$. TF. 195 M BEAT FRE TOR O- 5 Mols \& 45 Carr. $30 /-$ TF. 195 M BEAT FREQ20 Carr. 30/-. TF, 142E Distortion Factor Meter, e20 Carr. 20/-. All above offered in excellent condi-
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, 000 V D.C. $0 / 3 / 10 / 50$ 50/500/1,000V A.C. $0 /$ $10 / 100 \mu A / 10 / 100 /$ $500 \mathrm{~mA} / 2 \cdot 5 / 10 \mathrm{~A}$. $\mathrm{K} / 10 \mathrm{~K} / 100 \mathrm{~K} / 10 \mathrm{M} /$
$10 \mathrm{M} \Omega .-10$ to $49 \cdot 4 \mathrm{~dB}$
$818.18 .0 . \mathrm{P}, \& \mathrm{P} .5 / \mathrm{m}$


MODEL TE-80 50,000 O.P.V. mirror scale overload protec D.C. 0/6/30/120/300/1200v. D.C. $\quad 03 / 6 / 60 / 600 \mathrm{~mA}$. D.C $16 \mathrm{~K} / 160 \mathrm{~K} / 1 \cdot 6 / 16 \mathrm{meg} \Omega . \quad-20$
to $+63 \mathrm{~dB} . \mathrm{c}^{2} .10 .0$ P. \& P. $3 /-\mathrm{C}$

MODEL TE-70, 30,000 O.P.V. $0 / 3 / 15 / 60 / 300 / 600$ $60011,200 \mathrm{~V}$. A.C. $0 / 30 \mu \mathrm{~A}$ $3 / 30 / 300 \mathrm{~mA} .0 / 16 \mathrm{~K} / 160 \mathrm{~K}$ $1 \cdot 6 \mathrm{M} / 16 \mathrm{Meg} . \Omega$
$\mathbf{5 5 . 1 0 . 0 . \mathrm { P } . \& \mathrm { P } . 3 / -}$.


TE-900 20,000 $6 / V O L T$ GIANT MULTMETER
mirror scale End overload protection. 6 in. full view $2 \cdot 5 / 10 / 250 / 1,000 / 5,000$ v. AC. $0 / 25 / 12 \cdot 5 /$ $10 / 50 / 250 / 1,000 / \overline{5}, 000 \mathrm{v}$. D.C.O/50 LA/110/100. $1500 \mathrm{~mA} / 10 \mathrm{amp}$. D.C ${ }^{+}$ $02 \mathrm{~K} / 200 \mathrm{~K} / 20$
OHM. $£ 15 . \mathrm{P}$ \& $\&$ P. $5 /-$ OHM. \&15. P. \& P. 5/

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$10 \mathrm{meg} \Omega \mathrm{dB}-20$ to +81 $10 \mathrm{meg} \Omega \mathrm{dB}-20$ to +81
dB . Overload protection. \$12.10.0. Garr. $3 / 6$.


MODEL TE-12 20,000 O.P.V. $0 / 0 \cdot 6 / 6 / 30 / 120 /$ $600 / 1,200 / 3,000 / 6,000 \mathrm{v}$
$0 / 6 / 30 / 120 / 600 / 1,200 \mathrm{v}$ $0 / 6 / 30 / 120 / 600 / 1,200$
$0 / 60 \mathrm{uA} / 6 / 60 / 600 \mathrm{~mA}$ $600 \mathrm{~K} / 6 \mathrm{Meg} / 60 \mathrm{Meg} . \Omega 50 \mathrm{FF}$ $0 \cdot 2 \mathrm{mFd}$. $\mathbf{2 5} .19 .8$. P. \& P. $3 / 6$.

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cost economy oscillosost economy oscilloscope for everyday use.
Y amp. Bandwidth
Bap-1 $\begin{array}{llll}2 & \text { CPS-1 } & \mathrm{mHza} \\ \mathrm{imp} & 2 & \text { Input } \\ \mathrm{man} & 25 & \mathrm{pF}\end{array}$
 tube. $115 \times 180 \times$
230 mm.
Weight
glb. $220 / 240 \mathrm{~V}$. a.c. Supplied brak. £22.10.0. Carr. 10/-.

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Generator ringing, metal cases. Operates from two $1 \cdot 5 \mathrm{~V}$ batteries (not supplied). Excellent condition. 84.10.0 per pair. Carr. 10/-.

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Carr. $5 /-$.


AUTO TRANSFORMERS
$0 / 115 / 230 \mathrm{~V}$. Step up or step down. Fully shrouded.
150 W.


TE22 SINE SQUARE WAVE AUDIO GENERATORS
 Sine: $20 \mathrm{c} / \mathrm{s}$ to
$200 \mathrm{Ke} / \mathrm{s}$ on 4
bands. Square: bands
$20 \mathrm{c} / \mathrm{s}$ to $30 \mathrm{Kc} / \mathrm{s}$ $20 \mathrm{c} / \mathrm{s}$ to
Output imped ance 5,000 ohms $200 / 250 \mathrm{~V}$. A.C supplied brand new and guaran tion manual and leads, £16.10.0. Carr. $7 / 6$

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Variable range 0
111dB. Connections


Unbalanced $T$ and
Bridge T. Impedance $600 \Omega$ range $(0.1 \mathrm{~dB} \times$ $10)+(1 \mathrm{~dB} \times 10)+10+20+30+40 \mathrm{~dB}$ Frequency: d.c. to 200 kHz ( -3 dB ). Accur acy: 0.05 dB . + Tndication $\mathrm{dB} \times 0.01$.
Maximum input less than $4 W$
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Heary duty light
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condenser discharge principle operating on electro mechani cal relay. (As inset) Housed in strong rate between 60-120 Der minute. Maxi mum load 6 amps. size $2-11 / 16 \mathrm{in}$. dia. $x$ 4in. cost. 6/6 each P. P. 2/6. (3 for 17/6 P. P. 4/6)

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 $500 \mathrm{Kc} / \mathrm{s}$. Incorporates ${ }_{2}$ R.F. and 3 I.F. stages, band-pass filter, noise limiter, crystal controlled B.e.'.O., calibrator. O/F output, ete. Built-in speaker,
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COMMUNICATION RECEIVER 11 valve high grade communication receiver sudtable for tropical use. $1 \cdot 20 \mathrm{Mc} / \mathrm{s}$ on 4 bands. AM/CW/FM operation. Incorporates pre-
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$12 \mathrm{v} . \quad \mathrm{D} . \mathrm{C}$. internal power supply.
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$2 \mathrm{pF}-2000 \mathrm{mFi}$
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MEDIUM WAVE, LONG WAVE
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Attractive black and gold case. Size $5 \frac{1}{x} 11 \times$ $s_{1} \mathrm{in}$. Tunable over both Medium and Long Waves with extended M.W. band for easier tuning oo 7 stages- 5 transistors and 2 diodes, supersensitive lerrite rod aerial, fine tone moving coll speaker, also Personal Earpiece with switched socket for private Histening. Easy build plans and parts price ist $1 / 6$ (FREE with parts).

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WITH 3in. SPEAKER
Attractive case size $7 \frac{1}{2} \times 5 \frac{1}{3} \times 1$ in. with gitb attings. The ideal radio for home or outdoors. Covers Medium and Long Waves and Trawler Band. Speclal circuit incorporating 2 R.F. Stages, push pull output, ferrite rod aerial, 7 transiators speaker) and all first grade components. Easy build plans and parts price list $2 /$ - (FRES with parts). (Personal Earplece with switched socket for private listening $5 /-$ extra.)

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\end{gathered} \begin{aligned}
& \text { Fith switched socket }
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TWO WAVEBAND PORTABLE
8 stages- 6 trankistors and 2 diodes. Covers Medium and Long Waves. Top Covers Medium qud Long Waves. Top
quality
3 fin. Lotadspeaker for quality qutput and also with Personal Earpiece with switched socket for private listen ing. Two R.F. sfages for extra boost High "Q". Ferrite Rod Aerial. Push pu . output. Handsome pocket size case with gilt fittings. Size $6 \frac{1}{1} \times 4 \times 2$ in. Kasy build with parts) pal

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$\star$ Moderate size，only $25 \times 14 \times 10$ in．Complete Rit $19 \frac{1}{2}$ Gns． ＊Performance comparable with units costing $\qquad$ Carr． $12 / 6$ considerably more．Consists of（1）121n． 15 watt Bass unit with cast chassis，Roll rubber cone surround for ultra low resonance， and coramic magnet．（2）3－way quarter section series cross－over system．（3） $8 \times 5 i n$ ．htgh flux middle range＇speaker．（4）High efficiency tweeter．（5）Measured weight of woollen acoustic damping material．（6）Teak veneered oabinet．（7）Circuit and full instructions．Terms：Dep．f5．10．6 and9 monthly payments
$39 /$（Total 223.1 .0 ）．
DENGTRATIONS AT ATL BRANCHES．

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1014 WATT UKTRA LINEAR PEAK PUSH－PULL OUG ＇MIKE＇GRAM，RADIO OR TAPE．（7）Valves ECC83，（2 c．p．s．Bum Level： 60 as down．Sensitivity： 30 millipolts

 Gass and Treble controls．Output transformers are high quality section－ ally wound．Outputs for 3 and 15 ohms speakers．Complete set of parts，point－ 15 Gins．to－point wiring diagrams and instructions．Or factory assem－

R．S．C．A10 30 WATT ULTRA LINEAR HI－FI AMPLIFIER 音ighly sensitive Push－Pull Tone Control Stages．Performance figures of factory builtiunits：Hum level－70dB．Frequency response $13 \mathrm{dB3} 30-20,000 \mathrm{c}$／f．Sectionaly wound out－

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Twin－handed perforated cover 27／6．Supplied factory bulit with ELS4


R．S．C．A11 HIGH FIDELITY 12－14 WATT AMPLIFIER
 RUSH－PULL ULTRA LIEAR OUTPUT Two input sockets with associated controls TYo input socket with，＂and gram，etc otc． allowing mixing of＂品ike＂＂and gram，etc，otc． Hith sensitivity 5 valves－ECCB3（2），ELS4（2） E ．
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 An exception ally powerfuI
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gram， radio，tape． ＊．Two extra heavy duty 2in，Loudspeakers． ＊Four Jack inputs and two Volume Controls for simultaneous use of up to four pick－ups or＂mikes＂ 52 Gins．Carr，301－or and 9 monthily payments of 5．11．8．（Total $57 \frac{1}{2}$ gns．）． Send S．A．G．for leafiet． Gi00 100 watt peak output with Pr．speaker columas and a Rass Unit（Six 12＂ and Two 15 SDKr：）．e日t gn CONVERSION UNITS Type BMI An all－dry minator Size $51 \times 41 \times x$
2 in．approx． 2 in．approx． Completely replaces bat teries supplying 1.5 V ．and 900 F ． $50 \mathrm{c} / \mathrm{s}$ is available． Complete kit with diagram Complete kit with diagram
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F．W． RECTIFIERS（Bridged） All 6／12v．D．C．output．Max． A．C．input 18v．1a．4／3． 2a． $6 / 11$.
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$425-0.425 \mathrm{v} .200 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{~s}, 6 \cdot 3 \mathrm{v} .3 \mathrm{a}$, ， 5 v .3 a. $425-0.425 \mathrm{v} .200 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{~s} ., 6 \cdot 3 \mathrm{v} .3 \mathrm{a} ., 5 \mathrm{v}$.
$450-0-450 \mathrm{v}, 250 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .4 \mathrm{a} ., \mathrm{c} . \mathrm{t} ., 5 \mathrm{v} .3 \mathrm{~m}_{\text {．}}$ TOP SEROUDED DROP－THEOUGH TYPE $550-0-250 \mathrm{v} .70 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a}, 0$
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BUDGET HI-FI STEREO SYSTEMS GARRARD 3500 Turntable. Amplifier 8 watts per channel. VHF Tuner and pair of matched speakers beautifully finished

£65 00

Also available without radio $£ 5400$ VAN DER MOLEN stereo system with Garrard SP25 mounted in teak case and perspex. cover. Fitted with Sonotone cartridge and integrated stereo amplifier (12 watts RMS). Complete with 2

Special price $£ 5200$
LL NOVA with VHF Radio. Garrard 2025TC Autochanger with cueing device. 10 watts RMS amplifier and 2 matched

Rec. price $£ 729$ 6. Comet price $£ 59196$ WINDSOR 1500 S Solid Teak plinth with Garrard 2025TC unit, solid state amplifier, 10 watts RMS and 2 speaker units with $9 \times 5$ ellipticals, complete with tweeter domes housed in solid teak cabinets of

Rec. price $£ 57150$. Comet price $£ 49196$ Also available with Garrard SP25 turntable. Rec. price $£ 61190$. Comet price $£ 5200$ PHILIPS STELLA ST 8008 with Philips Autochange turntable. Integrated transistorised stereo amplifier and 2 separate speakers. All in attractive teak cabinets. Rec. price £51 190 . Comet price $£ 4400$

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| Rec. Retai/ Price | Comet Price |
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| £20 156 | £17 16 |
| £30 12 | £26 5 |
| ${ }^{2} 880$ | ¢6 19 |
| £20 05 | £16 19 |
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| £40 20 | £32 49 |
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| £43 100 | £35 19 |
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| £16 60 | £13 18 |
| £20 130 | £17 90 |
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| s aiso available at dis- |  |
| £15 64 | E11 10 |
| 42381 | ¢18 19 |
| £13 1011 | ¢11 12 |
| £17 194 | £15 |

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| Rec. Retail Price | Comet Price |
| :---: | :---: |
| £34 411 | £29 10 |
| 211 41 | ¢9 10 |
| ¢11 1810 | £10 110 |
| c22 72 | 5171911 |
| 5155 | 122815 |
| £4618 8 | E38 |
| 26349 | ¢55 |
| 528 1617 | £25 7 |
| £32 17 | ${ }_{5}^{2} 2818$ |
| 838 17 | £33 19 |
| 245181 | £40 7 | Bases, plinths and covers stocked to sult all the above turntables.

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AKAI X-150D deck 4 track AKAI X-300 2 track. AKAI X-300 4 track. AKAI X-360 4 track. AKAI X-360D deck 4 track AKAl 17404 track w/o acc. AKAl 18004 track. AKA1 1800SD 4 track AKAI 3000D deck 4 track. AKAI X-V 4 track AKAI M-9 4 track wio acc. FIDELITY HF Playmaster 2 track
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TRUVOX R52 3 speed $\quad$ 2track

| $£ 130$ | 2 | 4 | £109 | 0 |
| :--- | :--- | :--- | :--- | :--- | :--- | $\begin{array}{lll}\text { £130 } & 2 & 4 \\ \text { £263 } & 0 & 0\end{array}$ - 0 E220 0 | $£ 263$ | 0 | 0 | £220 | 0 |
| :--- | :--- | :--- | :--- | :--- | | $£ 339$ | 0 | 0 | $E 284$ | 0 | 0 |
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| :--- | :--- | :--- | :--- | :--- | :--- | $£ 158 \quad 0 \quad 0 \quad$ £133 00 £196 0 0 $\begin{array}{llllll} & 899 & 10 & 0 & £ 83 & 0\end{array}$ | $£ 180$ | 0 | 0 | $£ 154$ | 0 | 0 |
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| $£ 198$ | 0 | 0 | $£ 158$ | 0 | 0 |


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£ 35 & 5 & 3 & £ 24 & 18 & 6 \\
£ 96 & 12 & 0 & £ 81 & 0 & 0 \\
£ 85 & 10 & 3 & £ 62 & 0 & 0 \\
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| £ 22 | 2 | 0 | c52 | 2 | 0 |
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PICKUP ARMS
GOLDRING Lenco L75 GOLDRJNG Lenco G65 SME 3009 with $\mathbf{S 2}$ shell SME 3012 with S2 shell

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> $8713 \quad 6 \quad 86 \quad 10$
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\title{

a complete stereo system for only 28 gns! <br>  styled and finished. It gives superb reproduction previously associated with amplifiers costing far more.
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Tone Control: Treble lift and cut. Separate on/off switch.
A preset balance control.



The new Duo general purpose
2-way speaker system is beautifully finished in polished teak veneer, with matching vynair grille. It is ideal for wall or shelf mounting either upright or horizontally.
Specification: Impedance 10 ohms. It incorporates Goodmans high flux $6^{\prime \prime} \times 4$ " speaker and $2 \frac{21^{\prime \prime}}{}$ tweeter. Teak finish. $12^{\prime \prime} \times 6 \frac{3}{4} \times 5 \frac{3}{4}{ }^{\prime \prime}, 4$ gns each, $p$ \& $p 7 / 6$

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p\& $\mathrm{p}^{7 / 6}$
Cover and Teak finish Plinth £4.15.0 p \& p 7/6


$$
8 \frac{1}{2} \text { Gns. }+7 / 6 \mathrm{p} \text { \& } \mathrm{p}
$$

Controls: Selector switch Tape speed equalisation switch ( $3 \frac{3}{2}$ and $7 \frac{1}{2}$ i.p.s.). Volume. Treble. Bass. 2 position scratch filter and 2 position rumble filter.
Specification: Sensitivities for 10 watt output at 1 KHz . Tape head: 3 mV (at $3 \frac{3}{4} \mathrm{i} . \mathrm{p} . \mathrm{s}$.). Mag. P.U.: 2 mV . Cer. P.U.: 80 mV , Radio: 100 mV . Aux.: 100 mV . Tape/Rec. output: 100 mV . Equalisation for each input is correct to within $\pm 2 \mathrm{~dB}$ (R.I.A.A.) from 20 Hz to 20 KHz . Tone control range: Bass $\pm 13 \mathrm{~dB}$ at 60 Hz . Treble $\pm 14 \mathrm{~dB}$ at 15 KHz . Total distortion: (for 10 watt output) $<1.5 \%$. Signal noise : $<-60 \mathrm{c}$ B. A.C. mains $200-250 \mathrm{v}$. Bull and Tested, Size 12年in. long, $4 \frac{1}{2} \mathrm{ir}$. deep, $2 \frac{2}{4} \mathrm{in}$ high. Teak finished case.


Re W/iscount

## 131 ${ }^{1}$ Gns. $+7 / 6 \mathbf{p}$ \& p

Integrated High Fidelity Transistor Stereo Amplifier Specification-Output: 10 watts per channel into 3 to 4 ohms speakers ( 20 watts monaural). Input: 6 position rotary selector switch ( 3 pos. mono and 3 pos. stereo), P.U., Tuner, Tape and Tape Rec. Out. Sensitivities: All inputs 100 mV into 1.8 M ohm. Frequency Response: 40 Hz $20 \mathrm{KHz} \pm 2 \mathrm{~dB}$. Tone Controls; Separate bass and treble controls; treble, 13 dB lift and cut (at 15 KHz ); Bass, 15 dB lift and 25 dB cut (at 60 Hz ). Volume Controls: Separate for each channel. AC Mains Input: 200-240V. $50-60 \mathrm{~Hz}$. Size, $12 \frac{1}{\frac{1}{2}^{\prime \prime}} \times 6^{\prime \prime} \times 2 \frac{3^{\prime \prime}}{4}$ in teak finished case. Built and tested

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10W SOLID-STATE HI-FI AMP WITH INTEGRAL PRE-AMP

Syecifleations: Power Output (into 3 ohms speaker) 10 watts. Sensitivity (for rated output): 1 mV into 3 K ohms ( $0 \cdot 38$ microamp). Total Distortion at 1 KHz . at 5 watis $0 \cdot 35 \%$, at rated
output $1.5 \%$. Frequeney Response: Minus 3dB points 20 Hz and 40KEz. Speaker: 3-4 ohms (3-15 ohms may be used). Supply voltage: 24 V d.c. at 800 mA ( $6-24 \mathrm{~V}$ may be used).
Control assembly: including resistors and capacitors.

1. Volume: PBICE 5/-
2. Comprehensive bass and treble: PRICE 10/-.

The above 3 items can be purchased for use with the X101.


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50 WATT AMPLIFIER A.C. MAINS 200-250V


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An extremely rehable general purpose aive amplifier. Its rugged construction yet space age styling and design make value for money TEOHNICAL SPEOLEICATIONS
4 electronically mixed channela, with inputs per channel, enables the use of 8 separate instruments at the same time The volume controls for each channe are located directly above the corres ponding imput sockets. SENiSITIVITIE 2 AmV HipadANOES. Channels I 24 mV at 470 K . These 2 channeis ( uitars. Channels 3 \& 4200 mV at 1 m . Sultable for most high output instruments (gram umer organ etc.). Input sensitivity relative to 10 w output. TONE CONTROLS ARE Treble Boost +11dB at $15 \mathrm{KHz} / \mathrm{s}$. Treble Cut -12 dB at 15 KHz/s. With bass and treble Treble Eoost controls central -3dB points are $30 \mathrm{Kz} / \mathrm{s}$ and $20 \mathrm{KHz} / \mathrm{s}$. POWER OUTPDT. For speech and music 60 watts rms. 100 watts peak. For sustained music 45 watts rms, 90 wratts peak. For sinc wave 38.5 watts rms. Nearly 80 watts peak. Total distortion at rated output $3 \cdot 2 \%$ at $1 \mathrm{KHz} / \mathrm{s}$. Total distortion at 20 watts $0 \cdot 15 \%$ at $1 \mathrm{KHz} / \mathrm{s}$. Oratput to match into 8 or 15 ohms speaker system. NEGATIVE FFiED BACK 20 dB at $1 \mathrm{KEz} / \mathrm{s}$. SIGNAL TO NOISE
 tective fuse is located at the rear of unit. Output impedance 3,8 and 15 ohms.

##  THE RELIANT SOLID STATE GENERAL PURPOSE AMPLIFIER

## SpECHICATIONS

Output Impedance- 3 to 4 ohms Inputs-1.-xtal mic 10 mV Tone Controls-Treble control range t 12 dB at 10 KH 2 . gramiradio 250 mV Bass control range +13 dB st 100 H 2 Frequency Response-(with tone controls centra Minus 3aB points are 20 H 2 and 40 KHz signal to Noise Ratio-better than - 60 dB . Transistors-4 silicon Planar type and Germanium type. Mains input- $-220-250 \mathrm{~V}$. A.C. Size of chassis $-10 \sum^{2} \times 4 y \times 2 \xi$ A.C. Mains, $200-250 \mathrm{~V}$. For use with Std. or L.P. records, musical instruments, all makes of plek-ups and mikes, Separate bass and treble lift control. Two inputs with control for gram and mike. Built and tested. $8^{* \prime} \times 5^{*}$ speaker to suit price $14 / 8$ plus $1 / 6 \mathrm{P}$. \& P. Crystal mike to suit 12/6 plus 1/6 P. \& P.
Reliant MK. I. $5 \frac{1}{2}$ gns. plus 7/6 p. \& p.
As above less teak case.
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In teak fnished case.

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Brand new. Complete with circuit diagram.
£2.10.0 plus $1 /-\mathrm{p} . \& \mathrm{p}$.

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This tape deck takes $5 \frac{3}{4} \mathrm{in}$. spools complete with two-track heads. Size 13 in. long by 8 各in. wide. $\mathbf{2 8 . 1 9 . 6 \text { plus } 7 / 6 \text { p. \& p. }}$

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Size $3 \frac{7}{8} \times 2 \frac{1}{3} \times 1 \frac{3}{3}$ in. Meter size $2 \frac{1}{5} \times 1$ in. Sensitivity 1000 O.P.V. on both A.C. and D.C. volts. $0-15,0-150,0-1000$ D.C. current -100 mA . Resistance $0-100 k \Omega$. Complete With Fest prods, Gathery and inion Soidering Trom value 15/- to every purchaser of the Pocket Multi-Meter Multi-Meter.


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| $3^{\prime \prime}$ | L.P. | 240 ft . | $5 / 6$ | 5 " | T.P. | 1800 ft . | 27/ |
| $5{ }^{\text {P/ }}$ | L.P. | 1200 ft . | 13/- | $5{ }^{\text {² }}$ | T.P. | 2400 ft . | 34/ |
| $7^{\prime \prime}$ | L.P. | 1800 ft . | 20/- | $7{ }^{\prime \prime}$ | T.P. | 3600 ft . | 4 |
| 594* | D.P. | 1800 ft . | 20/- | 4 " | T.P. | 900 ft . | 16/6 | P. \& P. on each $1 / 6$.



## MOTEK

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A.C. mains, 240 volts, listed at $\ddagger 21.0 .0$.
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## TOPIC OF THE MONTH

## First things first

THERE is currently a good deal of talk about the shape of broadcasting, and the general concensus of opinion is that radio broadcasting in the UK finds itself in some need of reorganisation. Most of the discussion, however, seems to be centred around the constitutional basis of broadcasting and what services are required. This is rather putting the cart before the horse.

The most important aspects-which must be sorted out before considering the question of programmesrevolve around engineering problems. In a recent speech, the BBC Director-General, Mr. Charles Curran, elaborated on this theme. En passant, he said ". . . the long term future for radio in this country-and by long term I mean the next ten years-lies principally with v.h.f." Medium wave broadcasting will continue, he went on, but only in face of growing interference, until there is a new frequency allocation conference. But, as he pointed out, at such a conference we will do well to hold on to what we have and consequently there must be a greater exploitation of v.h.f.

Mr. Curran made three major points. First, local broadcasting on medium wave is unlikely to be a viable proposition ten years hence. Secondly, it would not be right to use the present international common frequencies for a very limited number of local stations in some areas and rely on v.h.f. in all other areas. Thirdly, it would not be right to redistribute some of the present national and regional channels for local station use; this would inevitably lead to the invasion of these frequencies by continental broadcasters

Some sources have suggested invoking Article 8 of the Copenhagen agreement (which allows the use of a frequency allocated to another country provided there is no serious interference with that country's service). This, however, would be tacit admission that the Copenhagen allocations were inadequate (whereas they are generally favourable to the UK), provoking a new frequency allocation conference from which we would certainly emerge worse off.

Obviously, v.h.f. must play a key role in any revised broadcasting shake-up and it has been suggested that v.h.f. coverage be made obligatory on all receivers made. In the USA, u.h.f. TV only got off the ground after legislation to ensure that all receivers had u.h.f. coverage.

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[^0]
B. H. Morris \& Co. (Radio) Ltd., the sole UK distributors for "Trio", "Teac", "Sonics", and "Audio Development" announce some new items of equipment in their range. Amongst the range are the items illustrated above. The speakers are type AS-57 bookshelf models. Power handling capacity is 10 W music power. Voice coil impedance is $8 \Omega$. Frequency response is $70-18,000 \mathrm{~Hz}$. Enclosure dimensions are $5 \frac{7}{8} \times 15 \frac{3}{4} \times 8 \frac{1}{4}$ in. deep. Speaker compliment is a $5 \times 7 \mathrm{in}$. elliptical. Price is $£ 15$ per pair.

The pickup cartridge illustrated at the top left is the "Trio" Supreme 20 photoelectric model. It uses a lamp and screen attached to the cantilever to which is fitted the stylus and photoelectric diodes and a preamp. The movement of the screen controls the amount of light passing through it to the diodes. Therefore stylus movement on the record varies the amount of light through the screen to the diodes thus modulating the current from the cartridge. Retail price is $£ 644$ s. 1d. plus $£ 1315$ s. 11 d. p.t.

An inexpensive magnetic cartridge in the B. H. Morris range is the $A D 76 \mathrm{~K}$ with a sensitivity of 5 mV at 1 kHz and frequency response of $20-20,000 \mathrm{~Hz}$ priced at 90 s.

Full information of the complete range of equipment may be obtained by contacting B. H. Morris \& Co. (Radio) Ltd., 84-88 Nelson Street, London, E.1. TeI.: 01-790 4824.

## RADIO AND TELEVISION COURSES

The London Borough of Brent Stonebridge Evening Institute, Brentfield Road, London, N.W. 10 announce their 1969/70 Radio and TV Course. It commences on 22nd and 24th September, Mondays and Wednesdays $7.0-9.0 \mathrm{p} . \mathrm{m}$. The fees are 50 s . for one or two evenings weekly for session which ends 22nd May, 1970. The course covers some theory and practical work and is mainly intended for amateurs. Cheques and P.O.s should be made payable to "The Brent Borough Treasurer" and students may enrol now by post to : 44 Worcester Crescent, Mill Hill, London, N.W.7.

## RADIO CONTROL FANS

The London Radio Controlled Models Society is holding a meeting on 10 th July at $7.30 \mathrm{p} . \mathrm{m}$. Venue is "The Two Chairmen", Dartmouth Street, London, S.W.1. Further details may be obtained from the Secretary, H. C. Farley, 24 Dacre Crescent, Kimpton, Hitchin, Herts.

## VERY CONVENTIONAL

 Every year the Radio Society of Great Britain sponsors a convention for v.h.f.-minded radio amateurs and enthusiasts. It is usually held at the "Winning Post Hotel" near Twickenham in Middlesex, which is an ideal venue with a large car park that was completely filled at the latest convention on 26th April. Things started at $11 \mathrm{a} . \mathrm{m}$, with an exhibition of home-constructed and commercial equipment: there was very little on show, but the quality of workmanship of the private exhibits was superb, especially a little s.s.b. transceiver for 144 MHz which won D. Dall, G5AHK, the V.H.F. Committee Cup. In the afternoon, two lecture sessions ran in parallel; one was started off by Jack Hum, G5UM, who talked on how to start on v.h.f. with the minimum of trouble and expense and this was followed up with lectures on the technique of listening on v.h.f., the design and construction of 70 and 144 MHz converters and general principles of the design of v.h.f. transistor transmitters. Slightly longer lectures in the other room were led by Arnold Mynett, G3HBW, who talked on v.h.f. s.s.b. phasing transceivers, followed up by G3MED discussing a spurious-free v.h.f. receiver, and in a very similar vein how to measure spurious radiation down to -90 dB by G3FZL. Among the guests who sat down to an excellent dinner in the evening were Colonel I. St. Q. Severin of the cabinet office, and Dr. J. A. Saxton, director of the Radio and Space Research Station.
## NEWS FROM THE CLUBS

GB3SUA will be operational 11 th-13th July on 80,20 , 15 , and 10 m bands using s.s.b./a.m./c.w. modes. Run by Stratford upon Avon ARC to celebrate the 700th anniversary of the Guild of the Holy Cross which was the first recorded form of local government in the town. A special OSL card will be issued via the RSGB Bureau. Further details from M. J. W. Webb, G3OOQ, 14 Townsend Road, Tiddington, Stratford upon Avon.

Pudsey and District Radio Club will be running their first Mobile Rally-the White Rose Mobile Rally-on 27th July. The OTH is Allerton Girls High School, Leeds, Yorkshire. Talk-in stations will be on 160 and 2 m . There will also be a.m. and s.s.b. demonstration stations. Other attractions are: raffle prizes, easy car parking, refreshments, amusements for wives and kids and the whole rally is under cover. Further details: R. Short, G3YEE, 10 Tyersal Grove, Bradford 4, Yorks.

## NORTHERN RADIO SOCIETIES' ASSOCIATION

 CONVENTION \& EXHIBITIONThis event was held at Belle Vue, Manchester on 27th. April, several hundred visitors attending. Mr. John Graham, G3TR, Immediate Past President of the RSGB presented the G8AYD Trophy for the best stand put on by a radio club belonging to the Association. The award was made jointly to the Manchester and District Amateur Radio Society and the South Manchester Radio Club. These two clubs put on show stands that gave a complete picture of the hobby from the very beginning.

Another stand of particular interest was that of the Wirral ARS on which were shown their group constructional projects, their latest being a 160 m s.s.b. Rx/Tx

# news And comment... 

EDDYSTONE'S NEW 10-BAND BABY


A new solid state receiver-the EC958-covering a range of 30 MHz to 10 kHz has been announced by Eddystone Radio-a member of GEC-Marconi Electronics. For best possible accuracy in frequency setting an optical projection method of displaying the frequency scale is used. This gives an effective length of 50 in . for each display scale. Silicon transistors are used throughout and microcircuits and f.e.t.s have been employed where advantageous.

Reception facilities are c.w., m.c.w., a.m., (d.s.b.) and s.s.b. in A3A, A3H and A3J modesupper or lower sideband. F.S.K. (F1) facilities are available when optional module (type LP. 3058) is fitted. Keying speeds up to 200 bauds with shifts of $85-850 \mathrm{~Hz}$ can be accommodated.

Further details may be obtained from Eddystone Radio Ltd., Eddystone Works, Alvechurch Road, Birmingham 31.

## COMARK MULTIMETER

The Comark Multimeter 1231 is the latest addition to the new 1000 Series. The overall accuracy is $\pm 2 \%$ of f.s.d. for d.c. measurements and $\pm 3 \%$ of f.s.d.for a.c. measurements over a bandwidth from 10 Hz to $100 \mathrm{kHz}(3 \mathrm{~Hz}$ to 250 kHz for -3 dB ). Voltage sensitivity is from 1 mV f.s.d. to 300 V in 12 ranges with an input resistance of $1 \mathrm{M} \Omega / \mathrm{V}$ at d.c. the maximum current sensitivity is $1 \mu A$ f.s.d. with a meter volt drop of less than 12 mV . Resistance is measured to an accuracy of $\pm 5 \%$ of reading from $1 \Omega$ to $100 \mathrm{M} \Omega$. The UK list price is $£ 50$.

## NEW PREMISES FOR HOME RADIO

Home Radio have moved from their original shop in London Road, Mitcham, to the top floor of an office block 400 yards away at 240 London Road. They now have 2,400 square feet of extra space, from which to run their mail order business.

## A.S.E.E. CHANGE

"The Association of Supervisory and Executive Engineers" -that is the new name for the Association of Supervision Electrical Engineers. Membership is now no longer restricted to electrical engineers.

## ON 'PHONE?

Amateurs in the United States, because of changes in the Bell System telephone regulations can now legitimately operate "phone patches" connecting overseas stations to telephone subscribers.

## THE MULLARD MEETINGS

At Southampton on 5th May, the 1969/70 season of Mullard meetings for the radio and television trade opened. This year's talk is devoted almost entirely to integrated circuitry and between now and 1970 it will be given at 76 centres in the UK.

The talk deals in a general way with the development of integrated circuits, analyses their advantages and emphasises the radical changes in thinking of design. It then studies the applications of integrated circuits to colour TV receivers. I.C. manufacture is then covered and the talk finishes with a glimpse into the future and what it is likely to hold so far as I.C. applications are concerned.

The programme for July is: 9th: Dolphin Hotel, Swansea; 10th: Park Hotel, Cardiff.

All meetings start at 7.45 p.m. and any readers wishing to attend should apply for tickets to lan Nicholson, Films and Lectures Organisation, Mullard Ltd., Torrington Place, London, W.C.1.

## NEW FROM MARCONIPHONE



Five new models from Marconiphone include two small portable receivers, two radiograms and a record player. The two portables are similar-the 4166 having v.h.f./m.w./l.w. coverage and the 4169 covering l.w./m.w./s.w. Both have push-button waveband selection and an output of 300 mW . Prices are: 4166 (£14 15s.) and 4169 ( $£ 11$ 10s.). The photograph shows model 4169.


WITH a receiver covering long, medium and short waves, it is of advantage to use an internal ferrite rod aerial for long and medium wave reception, and a telescopic or other external aerial for short waves. The circuit used here is of this type, and gives reception of hundreds of short wave transmissions, in addition to medium and long wave coverage. Bands actually tuned are approximately $14-6 \mathrm{MHz}$ s.w. $(21-50 \mathrm{~m}), 1,500-575 \mathrm{kHz}$ m.w. ( $200-$ 530 m ) and $260-160 \mathrm{kHz}$ 1.w. ( $1,150-1,900 \mathrm{~m}$ ).

Some simplification is possible by using a common oscillator coil for m.w. and I.w., and the way in which bandswitching operates can be checked with the aid of Fig. 1.

For s.w. reception, S1 earths C, tag 1 of L1, L3 and L4 being shorted out. L1 is tuned by VC1. S4 shorts

A, $\operatorname{tag} 7$, to earth, so that only the base winding of L1 is in use. S3 places VC2 across L2, for oscillator tuning, and S2 switches Tr1 collector to the collector winding of L2.

For m.w. reception, S1 leaves L3 in circuit, S4 introducing the base coupling winding. S 3 provides oscillator tuning of L5, with the series m.w. padder C 4 while S 2 brings into use the collector winding of L5.

L 5 is also used for l.w. reception, with the extra capacitor C5 to obtain suitable frequency coverage. The l.w. section of the ferrite rod, L4, is also in use.
L1 and L2 are individual s.w. aerial and oscillator coils. L3 and L4 are m.w. and l.w. sections of a dualwave ferrite rod aerial. By using a series circuit as shown, no switching of $\operatorname{Trl}$ emitter is required.


Fig: 1. The Transet theoretical circuit. The aerial, oscillator and i.f. stages-

The telescopic aerial is coupled through T1, and also operates on m.w. and l.w., if extended, though it is normally not required on these bands.

T4 is the s.w. oscillator trimmer, T2 the m.w./l.w. trimmer, and T3 allows adjustment of 1.w. oscillator coverage. To give maximum efficiency on all frequencies, a small manually operated panel trimmer VC3 is used in the aerial circuit. This avoids loss of results due to poor trimming, and also compensates for changes caused by extending the aerial, or using an external aerial. VC3 is simply rotated for best results, and only need be adjusted occasionally.

## IF AMPLIFIER

I.F.T. 1 and i.f.t. 2 are both double tuned, the diode i.f.t. being single tuned. This results in high gain and selectivity, with enough sensitivity for good reception of many transmissions. The i.f. is 465 kHz .

## AUDIO AMPLIFIER

Tr 4 is the first a.f. stage, followed by Tr 5 as driver. Tr6/7 are the output pair, with feedback and base bias via R21 and R22. This type of circuit has the advantage that suitable transistors are readily available, and the operating conditions of each stage are independent of other stages. This avoids difficulties sometimes arising in directly-coupled and similar circuits. There is plenty of amplification and enough power output for loudspeaker reception of most signals, with good tonal quality.
The volume control VR1, ganged capacitor $\mathrm{VC1} / 2$, trimmer VC3, and switch are fixed to a $7 \times$ 3in. flanged aluminium plate, also used as a positive
line or earth return. Other parts are fitted to a paxolin circuit board $7 \times 2 \frac{3}{\frac{3}{9}} \mathrm{in}$., which is bolted to the flanged plate.

## CONSTRUCTION

Figure 2 is a top view of the paxolin board. VC3 is directly under $\mathrm{VC1} / 2$, and the fixed plates tag of VC3 is connected to the underneath tag of VC1. VR1 fits on the aluminium plate to the left of VC1/2, and the four-pole three-way switch occupies a similar position to the right.

The paxolin board was prepared by scribing lines at $\frac{1}{4} \mathrm{in}$. intervals with a sharply pointed tool, then drilling $\frac{3}{67} \mathrm{in}$. holes for all leads. L1 and L2 need $\frac{1}{4} \mathrm{in}$. holes. The board is also drilled to clear the pins of L5, i.f.t.1, i.f.t.2, i.f.t.3, and the fixing feet of T2. Drilling positions for the i.f. transformers and L 5 can be marked by pressing paper against the pins, holding this on the paxolin, and marking through with a sharply pointed tool. A central hole to allow core adjustment is needed under each i.f.t. Two bolts secure the paxolin to the flange, and tags were put under the nuts to provide the MC points.

A slow-motion action is essential with $\mathrm{VC} 1 / 2$, and is provided by concentric spindles in the component listed. A ball drive could be fitted to the ordinary type of capacitor, a little extra space then being needed between the aluminium plate and the inside of the cabinet front. The tuning capacitor also had trimmers fitted. The trimmer for VCl is fully unscrewed, then ignored. The other trimmer is TC2, Fig. 1. A capacitor without trimmers is equally suitable, and TC2 would then be a separate trimmer, connected from frame to VC2. A $100-470$ ohms resistor may be needed between 9. L2. and S2. if the circuit is trimmed for maximum s.w. coverage.

-and above, the detector, first a.f., driver and output stages.

## WIRING

This can be carried out with 22 s.w.g. or similar tinned copper wire, with insulated sleeving where necessary. In most places the wire ends of the resistors and capacitors are long enough to reach the various connecting points.

The diode D1, and electrolytic capacitors, must be fitted with the polarity shown. C6 lies under C2 and C16 is underneath C15.
Figure 3 shows all connections under the paxolin board.

L5 and the i.f.t.s have small tags which earth the screening cans. These are connected as in Fig. 3. The core of T2 is also earthed.
A red flexible lead from the switch of VR1 is fitted with a positive battery clip. Battery negative is the centre-tap of the primary of T2, Fig. 3. Twin flexible leads from $\mathbf{T} 2$ secondary will go to the loudspeaker.

## TRANSISTORS

It is probably as well to leave these until most other wiring has been done. $\operatorname{Tr} 1$ is behind the fourpole switch, allowing short leads from collector to $\mathbf{S 2}$, and emitter to tag 5 of L2. The base lead goes to C1, R1, R2.
$\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ can have $\frac{1}{2} \mathrm{in}$. lengths of coloured sleeving on emitter, base and collector leads, for insulation, and to identify them. These wires should not be unnecessarily long.

The remaining transistors can conveniently have about $\frac{3}{4} \mathrm{in}$. of lead above the circuit board. Many alternatives will operate satisfactorily in this type of audio amplifier. A poor transistor should on no account be used for Tr 4, as noise generated in this stage is considerably amplified. As the listed transistors are readily available, it is recommended they be used if transistors are to be purchased. But this does not mean that equivalents already to hand could not be fitted. Some might need different base or emitter resistor values.

## FERRITE ROD

This may be 6 in . or 7 in ., of the usual type for m.w./l.w. ferrite aerials. A bracket is bolted to the paxolin board, Fig. 2. This supports a vertical strip of paxolin 3 in . high and $\frac{5}{8} \mathrm{in}$. wide. A strip of flexible insulating material passes round the ferrite rod, and is bolted to the paxolin strip.

When connecting the ferrite rod windings, note that the m.w. tuned section is from points C to D , Fig. 1. The m.w. base coupling winding is from A to B. The l.w. tuned section L4 is from D to earth line. Should a rod with separate base winding be used, instead of a tapping on L4, this winding is connected between the m.w. winding at $B$, and earth line. Should tuning difficulties arise on l.w., this might be caused by L4 being in the reversed phase to L3, and this can be corrected by reversing connections. to L4. Windings intended for 208 pF tuning capacitance and OC44 type transistors are usually satisfactory provided the base coupling is reduced by removing a few turns. Four turns should suffice for m.w. base coupling. L.W. coupling need not be changed unless instability arises.
components list

## Resistors:

| R1 | $10 \mathrm{k} \Omega$ | R12 | 47k |
| :---: | :---: | :---: | :---: |
| R2 | 2.7k $\Omega$ | R13 | .12k $\Omega$ |
| R3 | $150 \Omega$ | R14 | 8-2k $\Omega$ |
| R4 | $1 \mathrm{k} \Omega$ | R15 | $470 \Omega$ |
| R5 | $68 \mathrm{k} \Omega$ | R16 | $82 \mathrm{k} \Omega$ |
| R6 | $8 \cdot 2 \mathrm{k} \Omega$ | R17 | $22 \mathrm{k} \Omega$ |
| R7 | $680 \Omega$ | R18 | $680 \Omega$ |
| R8 | $22 \mathrm{k} \Omega$ | R19 | $4 \cdot 7 \Omega$ |
| R9 | $4 \cdot 7 \mathrm{k} \Omega$ | R20 | 82, 5\% |
| R10 | $1 \mathrm{k} \Omega$ | R21 | 10k』 5\% |
| R11 | $120 \mathrm{k} \Omega$ | R22 | 10k $\Omega 5 \%$ |

VR1 $5 \mathrm{k} \Omega$ log. pot. with switch
All $10 \% \frac{1}{4}$ watt except where stated
Capacitors:

| C1 | $0.01 \mu \mathrm{~F}$ |
| :---: | :---: |
| C2 | $0.5 \mu \mathrm{~F}$ |
| C3 | $0 \cdot 01 \mu \mathrm{~F}$ |
| C4 | 200pF 2\% silver mica |
| C5 | 175pF 2\% silver mica |
| C6 | $10 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C7 | $0.04 \mu \mathrm{~F}$ |
| C8 | $0 \cdot 02 \mu \mathrm{~F}$ |
| C9 | $0.02 \mu \mathrm{~F}$ |
| C10 | $0.01 \mu \mathrm{~F}$ |
| C11 | $2 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C12 | $100 \mu \mathrm{~F} 12 \mathrm{~V}$ |
| C13 | $8 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C14 | $2 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C15 | $100 \mu \mathrm{~F} 6 \mathrm{~V}$ |
| C16 | $100 \mu \mathrm{~F} 12 \mathrm{~V}$ |
| $\mathrm{VC1} /$ | VC2 Jackson 00 208/176pF slow motion |
| VC3 | 25pF or 30pF miniature air-spaced variable |
| TC1 | 30pF pre-set |
| TC2 | 30 pF pre-set |
| TC3 | 60pF pre-set |
| TC4 | 30pF pre-set |

Inductors:
L1 s.w. aerial coil, Denco transistor range 4 Blue
L2 S.w. oscillator coil, Denco transistor range 4 Red
L3/L4 l.w./m.w. ferrite rod aerial
L5 I.w./m.w. oscillator coil, Weyrad P50/1AC
IFT1 Denco IFT18/465
IFT2 Denco IFT18/465
IFT3 Denco IFT14
T1 Osmor QXD1
T2 Osmor $0 \times 02$

## Semiconductors:

Tr1 OC170
Tr2 AF117
Tr3 AF117
Tr4 OC71
Tr5 OC81D
$\left.\begin{array}{ll}\text { Tr6 } & \text { OC81 } \\ \text { Tr7 } & \text { OC81 }\end{array}\right\}$ Matched pair
D1 OA81

## Miscellaneous:

2/3 ohm $3 \frac{1}{2} \mathrm{in}$. or similar speaker; four-pole threeway rotary switch; $7 \times 3 \mathrm{in}$. flanged plate (Home Radio); $7 \times 2 \frac{3}{4}$ in. paxolin sheet; four knobs; $6 \frac{1}{2} /$ $35 i n$. telescopic aerial.

Note that the receiver can be tested on s.w. with the ferrite rod omitted, and on m.w. with L4 omitted. This may help localise wiring faults, if any arise.

## BANDSWITCH

The position of this allows short leads from 1, L1, to S 1 and earthed return to $\mathrm{VC} 1 / 2$, from 1, L 2 to S 3 and VC2, and from 4, L 2 to $\mathrm{VCl} / 2$.

C4 and C5 are mounted vertically on the paxolin board, to reach the switch tags. There should be no difficulty if tags and connections are correctly identified.

When first testing the receiver, a meter may be
included in one battery lead. Current should be around 9 mA to 12 mA with no signal or at low volume. If it is excessive, switch off at onde and look for an error in wiring or other fault. During normal listening, current peaks will be about 20 mA to 40 mA , according to volume.

## IF AMPLIFIER

This is most readily aligned with a signal generator, set to give a modulated signal at 465 kHz . Adjustments can then be for maximum battery continued on page 262


Fig. 2: View of components on the upper side of the paxolin board.


Fig. 3: Wiring on the underside of the paxolin component board.

# THECULT OFTHE JAMES HOSSACK <br>  

THE modern meaning of the word "cult", like that of others such as "juvenile", etc., has become debased by common usage in association with a more sinister partner (e.g. "juvenile delinquent'), and one imagines the adherents of a cult as supporting it with a sort of fanatical, and frequently misplaced, semi-religious fervour. It is useful to remember that the word itself shares a common origin with "cultivate", which basically means to "make good use of", and this is precisely what possession of a junk-box (or perhaps one ought to use the more elegant term "spares box") implies to those readers who have come, to a greater or lesser degree, to rely on one as providing a valuable addition to the resources available for pursuing their favourite hobby.

To many experimenters, who may have been introduced to radio construction via the influence of a big brother, the junk-box comes, in a sense, readymade. In other words, virtually a family heirloom. Other less fortunate (or more affluent) members of the radio fraternity commence operations by purchasing everything the hard way, down to the smallest nut, bolt, or resistor. Gradually, however, even those who pursue their hobby in a very modest way will acquire, over the years, a small stock of components which, while perhaps not quite as good as new, will serve them adequately for all normal constructional purposes. There is no doubt that a junk box of this type has much to recommend it.
There is, however, a more positive approach to this subject which was pursued some time ago by the writer, and which has paid handsome dividends in terms of component acquisition at bargain prices, and, what may be even more important to those residing in rural areas, complete and immediate availability of components "off the shelf" as and when these are required.
The plan is quite simply the purchase, or similar legitimate acquisition, of unwanted electronic gear, followed by a careful, painstaking, and thorough dismantling of all the usable components therein. Sources of such components are many and varied. Some dealers, for example, will gladly dispose of old TV equipment for a nominal sum. On the other hand, constructors are frequently presented with the opportunity of procuring quite complex pieces of electronic gear which have ceased to function, or merely become obsolete, on the understanding that these are removed from the premises forthwith and "broken up"-hardly a euphemistic term for the extremely delicate dismantling operation to which they will be subsequently subjected on arrival back at the "shack".

A word of warning should, perhaps, be given here
about all equipment containing c.r.t.s of any description. In general, these are not worth salvaging, but it is imperative, before commencing operations on any chassis, that they be carefully removed and placed on one side for subsequent disposal via the refuse collection.

Do not succumb to the temptation to break a c.r.t. in order to facilitate its subsequent disposal, since the danger of flying glass from the resultant explosion (more correctly, implosion, since the tube collapses inwards) can be a very real one. The same advice applies to large glass valves, with the additional consideration that they may, in fact, prove worth preserving with a view to possible future use as transmitting tubes.
Having discussed how to collect, we now come to the question of what to collect. The answer would appear to be, whatever can be easily removed from a discarded chassis, but one or two points must be borne in mind, and it will be advantageous to consider the dismantled items in turn.

## Transistors

While examples of discarded gear containing transistors are, of course, comparatively limited at the present time, there are excellent opportunities for procuring, very cheaply, surplus computer panels and such like which often consist of masses of identical transistors embedded in a printed circuit matrix. These transistors are frequently mounted in such a position that by "unwinding" the transistor, so to speak, the wires can be cut off close to the board, leaving 1 inch or more of connecting lead. A snag with most boards of this type is that no details are generally available regarding the components, but, frequently, a meter check, or insertion of one transistor into a simple amplifying circuit (a.f. or r.f.) will be sufficient to identify the type satisfactorily. A number of excellent transistor testers, suitable for determining beta, leakage current, and other characteristics of unknown transistors, have been described in past issues of PW.

## Valves

The position as regards reclaimed valves is less satisfactory, particularly when one remembers that, after a few years' hard wear, the average rectifier or power output valve has completed perhaps twothirds of its useful life, although its characteristics may still be entirely satisfactory for use in experi-

TABLE 1

| Valve | Description | Heater |  | Anode Volts | Screen Volts | Maximum <br> Rectified Current | Peak Inverse <br> Volts (Rect.) | Base Connections |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Voltage | Current |  |  |  |  |  |
| 807 | Power Tetrode | $6 \cdot 3$ | 0.9A | 500 | 200 | - | - | A |
| 6 L 6 | a.f. Power Tetrode | $6 \cdot 3$ | 0.9 A | 350 | 250 | - | - | B |
| 6F6 6 | a.f. Power Pentode | $6 \cdot 3$ | 0.7 A 0.45 A | 250 | 250 | - | - | B |
| $6 \times 6$ $6 \times 5$ | Rectifier | $6 \cdot 3$ | 0.7 A 0.6 A | 325 | - | 70 mA | 750 | C |
| 83 V | Rectifier | 5 | 2 A | 575 | - | 175 mA | 1100 | D |
| 5 R 4 | Rectifier | 5 | 2 A | 750 | - | 250 mA | 2800 | E |
| $5 \vee 4$ | Roctifier | 5 | 2 A | 375 350 | - | 175 mA | 1100 | F |
| $5 \nvdash 4$ | Rectifier | 5 | 2A | 350 | - | 125 mA | 1100 |  |

TABLE 2

| Valve Type | Description | Heater Volts* | Pin Connections (B9A bases) |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| PCC 85 | v.h.f. double triode | $9 \cdot 0$ | $\mathrm{a}^{\prime \prime}$ | $\mathrm{g}^{\prime \prime}$ | ${ }^{\prime \prime}$ | , | h | $\mathrm{a}^{\prime}$ | $\mathrm{g}^{\prime}$ | $\mathrm{k}^{\prime}$ | s |
| PCF 80 | Triode-pentode mixer | $9 \cdot 0$ | $\mathrm{a}_{\mathrm{t}}$ | $\mathrm{g}_{1}$ | $\mathrm{g}_{2}$ | h | h | $\mathrm{a}_{\mathrm{p}}$ | $\mathrm{k}_{\mathrm{p}}$ | $\mathrm{k}_{\mathrm{t}}$ | $\mathrm{g}_{\mathrm{t}}$ |
| PCF 82 | Triode-pentode mixer | $9 \cdot 5$ |  |  |  |  |  |  |  |  |  |
| PCL 82 | Triode output-pentode | 16 | $\mathrm{g}_{\mathrm{t}}$ | k | $\mathrm{g}_{1}$ | h | h | $a_{p}$ | $\mathrm{g}_{2}$ | $\mathrm{k}_{\mathrm{t}}$ | $\mathrm{at}_{\mathrm{t}}$ |
| PCL 83 | Triode output-pentode | $12 \cdot 6$ | $\mathrm{a}_{\mathrm{t}}$ | $\mathrm{g}_{\mathrm{t}}$ | $\mathrm{k}_{\mathrm{t}}$ | h | h | $\mathrm{a}_{1}$ | $\mathrm{k}_{\mathrm{p}}$ | $\mathrm{g}_{2}$ | $\mathrm{g}_{1}$ |
| PCL 84 | Triode video output-pentode | 15 | $\mathrm{g}_{\mathrm{t}}$ | $\mathrm{a}_{\mathrm{t}}$ | $\mathrm{k}_{\mathrm{t}}$ | h | h | $\mathrm{ap}_{\mathrm{p}}$ | $\mathrm{k}_{\mathrm{p}}$ | $\mathrm{g}_{1}$ | $\mathrm{g}_{2}$ |
| PCL 85 | Triode output-pentode | 18 | $\mathrm{a}_{\mathrm{t}}$ | $\mathrm{gt}^{\text {t }}$ | $\mathrm{k}_{\mathrm{t}}$ | h | h | $\mathrm{a}_{\mathrm{p}}$ | $\mathrm{g}_{2}$ | $\mathrm{k}_{\mathrm{p}}$ | $\mathrm{g}_{1}$ |
| PCL 86 | Triode output-pentode | $13 \cdot 3$ | $\mathrm{g}_{\mathrm{t}}$ | $\mathrm{k}_{\mathrm{t}}$ | $\mathrm{g}_{2}$ | h | h | $\mathrm{a}_{\mathrm{p}}$ | $\mathrm{k}_{\mathrm{p}}$ | $\mathrm{g}_{1}$ | $\mathrm{a}_{\mathrm{t}}$ |
| PL 82 | Output pentode | $16 \cdot 5$ |  | $\mathrm{g}_{1}$ | k | h | h |  | a | - | $\mathrm{g}_{2}$ |
| PY 82 | Rectifier (half-wave) | 19 | - |  | k | h | h | - | - | - | a |

*Heater current is 0.3 A in all cases.


Fig. 1: Valve base connections A-F are for Table 1. All valves in Table 2 have 9 pin bases (B9A.).
mental hook-ups, or as test replacements for the diagnosis of circuit faults. Unless one is an ardent collector of vintage components (see, for example, The Radio Collector by P. N. Wood in the June 1966 issue of PW), it is probably wisest to consign all valves of the pre-octal-base era to the dustbin before they have the opportunity to ruin a perfectly good circuit. The same may be said to apply to most octal-base specimens, with the exception of a few such as 6L6, 6X5, 807, and some others; also, power rectifiers of the 5 volt series, such as $5 \mathrm{Z4}$, may come in useful, provided they are known to be in good condition. Characteristics and base connections for some of these are given in Table 1. Miniature battery valves based on B7A may prove of some
interest to the radio control enthusiast. B9G television valves are sometimes designed to operate from a standard 6 volt heater supply; more often they are designed to run from a higher voltage, and can be neatly pressed into experimental service by adapting a suitable transformer (see next section).

## Transformers

Unlike valves, these seldom deteriorate with age, and, in fact, probably represent the most valuable components in any chassis, from the reclamation point of view. A good mains transformer can cost anything from $£ 2$ upwards, so that the initial price of an old chassis is repaid several-fold if it happens to contain a mains transformer likely to be suitable to one's requirements. Television line and field transformers are unlikely to be of great use unless one is especially interested in audio oscillators, but the output transformer should certainly be salvaged, particularly if it is one of the multi-tapped variety.

Table 2 shows the heater voltages and general applications of some popular television valves, and it is frequently possible to utilise two or even more heater windings, connected in a suitable manner to obtain the required power for circuits using such valves, as described earlier. Sometimes, other lowvoltage windings can be interconnected to provide between 12 and 20 volts at a few amps., a useful
feature for those interested in building their own transistor power supplies.
I.F. transformers were, generally designed for $465 \mathrm{kc} / \mathrm{s}$ operation, and are therefore worth preserving unless they happen to incorporate the old-style compression trimmers, which were notoriously unreliable. Television i.f.t.s are usually somewhere in the $20-30 \mathrm{Mc} / \mathrm{s}$ region, and as such can prove of interest to potential constructors of amateur v.h.f. equipment. In this context, old f.m. mixers or TV turret tuners can sometimes be dismantled as complete units, and are very easily adapted for 70 or $144 \mathrm{Mc} / \mathrm{s}$ amateur band operation.

## Coils

Unless these are of fairly modern design, the trouble of removing them is scarcely justified, although, if a complete unit with wavechange switch can be salvaged intact, it may well come in handy at a later date. Old wafer switches, by themselves, are seldom of much value, since they will almost certainly be badly worn.

## Potentiometers

These have the merit of being amenable to direct assessment with a simple test meter. They will usually fall into two classes-good and bad-the worn track of the latter showing up immediately the control is turned backwards and forwards a few times. Keep the good ones carefully, since a wide selection of values on the experimenter's shelf is a very decided asset at all stages of construction. (The writer has a circuit in operation at present with about a dozen variable resistors-most of which will finally be replaced by fixed values once the optimum circuit constants have been determined.

## Variable Capacitors

Check these, also, with a meter, to locate faulty insulation, rubbing vanes, etc. Do not, in this case, be in too much of a hurry to dispose of ancient types. Many of the best transmitters use tank coils which are tuned by components once gracing the panel of a 1930 battery two-valver, whose designers appeared to imagine that the presence of 120 volts across the vanes rendered a spacing of less than $\frac{1}{8}$ in. completely unacceptable. Needless to say, you will be unlikely to recover any components small enough to incorporate in that projected transistor portable, although occasionally, old valve-operated car radios can be found which were provided with astonishingly small, neat, and efficient tuning mechanisms and capacitors, which are well worth saving for future use.

## Switches

Test routine is the same as for potentiometers. Subject the switch to a continuity test and also an insulation test to earth, especially if it is likely to be used for mains switching. Into this category we can
include relays, which may be found on some old television sets, or more probably on surplus or exW.D. equipment of more recent vintage. Do not neglect the possibility of using these on, for example, radio control equipment, or for similar purposesthe experimental potentialities of a sensitive relay coupled with a photo-cell or photo-sensitive transistor are endless.

## Metal Rectifiers

These can provide useful accessories, together with heavy duty resistors, for receiver and even transmitter power supplies, although, with the advent of silicon rectifiers at very reasonable prices, their potential usefulness is likely to be less than it might otherwise be.

## Resistors and Capacitors

These should be cut off as near the terminals as possible (not unsoldered), but unless at least 1 inch wire ends remain after this operation, they are unlikely to be worth keeping. There is undoubtedly a point where thrift ends and parsimoniousness begins, and it may be that we are in danger of reaching that point now. The fact remains that, with the low cost and high reliability of new components of this sort, it may prove false economy to store what may turn out to be less than $95 \%$ perfect material-remember that a good junk-box must never live up to its name!

## Other Components

Finally, an example of one component which it is usually wise to hang on to, and, in contrast, one which is almost never worth storing. The former is the loudspeaker, especially if it is the small elliptical type popular in most TV receivers. These actually improve with age, since the cone suspension becomes less stiff with use, and the undesirable bass resonance can therefore drop, sometimes by as much as an octave. The component to avoid is the highvoltage electrolytic capacitor. Even when these test satisfactorily, their subsequent failure rate, when incorporated into constructional projects, can be alarmingly high, and they are best consigned to the dustbin forthwith-new ones, besides being considerably smaller than their older counterparts, are surprisingly cheap nowadays, and represent extremely good value for money.

In conclusion, a word about storage. Even the smallest "shack" can accommodate a reasonably wide range of components, provided these are stored in a methodical manner. Shelves are a necessity, as are stout wooden boxes for all heavier pieces of equipment such as transformers, etc. The best guide here is commonsense, the point being that the "junkbox" must never consist of a single large container into which material is deposited haphazardly. Far better a series of small, neatly labelled boxes, even if these do take up a little more space. Sensibly handled, the cult of the junk-box, besides reducing costs, can add considerably to the pleasure of all aspects of radio construction.

IN Part 2 the processes involved in the production of pure semiconducting materials were described． This leaves the device manufacturer in possession of his basic raw material，a uniformly doped slice of germanium or silicon．With this he can produce an enormous range of devices，from simple diode recti－ fiers to complex integrated circuits．This month the principles involved in the theory and manufacture of the diode will be discussed．

In Part 1 it was shown that the energy states in a semiconductor are arranged in bands separated by a certain band gap．At a temperature of $-273^{\circ} \mathrm{C}$ ，or absolute zero as it is called，electrons in all atoms are in the valence band and none are in the con－ duction band．In this case it may be said that there is a one hundred per cent certainty of a level in the valence band being filled but a zero probability of a level in the conduction band being filled．Con－ sequently a curve like the one in Fig．1（a）can be drawn．At higher temperatures electrons are excited into higher energy states so that the probability of an electron being in the conduction band is in－ creased，as shown at（b）in the same figure for a temperature of $27^{\circ} \mathrm{C}$ ．

## The Fermi level

As can be seen，both curves go through the same energy level at the point where there is a fifty per cent probability of this level being filled．This energy level is called the Fermi level and in the case of intrinsic（i．e．undoped）semiconductor material it is as shown midway between the valence and con－ duction bands．

The curves are symmetrical about the Fermi level


Fig．1：Probability of occupancy of energy levels at different temperatures．
as can be seen．This is because the probability of occupancy of conduction band levels increases as the probability of occupancy of the valence band levels decreases．In practical terms this means that electrons which reach the conduction levels have come from the valence band since the number of electrons in the material is constant．


ーーーーーーーーーーーーーーーー－－Fermi level at very high temperatures

Fig．2：Movement of Fermi level with temperature in doped semiconductor material．

With doped semiconductors however the Fermi level moves as the temperature is raised．With n－type material at absolute zero all the donor states are filled so that these behave like the valence band and the Fermi level lies between the donor level（see Fig．2）and the conduction band．At higher tempera－ ures however these states become vacant as elec－ trons move to the conduction band and the Fermi level moves towards the level it has in intrinsic material．An analogous situation exists in p－type material．Here at low temperatures the Fermi level lies between the valence and acceptor levels．

The rate at which the Fermi level moves down－ wards depends on the doping level and on the host material．In typical combinations of these the Fermi level lies at room temperature just below the donor level or just above the acceptor level．

## The p－n junction

If a piece of $p$－type material and a piece of n－type material could be brought together it could be shown that their Fermi levels would coincide，as shown in Fig．3（a）．Initial contact would not show this correspondence，as the Fermi level of the n－type material would be higher than that of the p－type material．However when contact is established on the atomic scale electrons diffuse from the material of n－type which has a high concentration of excess electrons to the p－type material which has a deficit


Fig. 3: (a) Energy levels and carrier flow in an unbiased diode. (b) Conditions at the p-n junction with forward bias applied. (c) Conditions with reverse bias applied to the diode.
of electrons. These electrons set up an electric field, the n-type side having a more positive potential than the p-type side. This is because the region to the right of the junction in the diagram then contains ionised donor atoms whilst the region to the left of the junction contains ionised acceptor atoms, with positive and negative charges respectively.

This field opposes the diffusion of electrons, itself giving rise to a drift of electrons in the opposite direction to the diffusion. Eventually an equilibrium is set up when the number of electrons diffusing from the n-type is equal to the number returning from the p -type material by the drift process. When this situation is established it is found that the Fermi levels at each side of the junction are equal (as shown in Fig. 3(a)). At the same time that the motion of electrons is under consideration it is also necessary to consider the diffusion and drift of holes in the opposite directions.

## Depletion region

The positive donor ions and the negative acceptor ions are fixed in the crystal lattice and consequently in the region of the junction there is a deficiency of mobile current carriers and the term "depletion layer" is usually applied to the region. The ionised atoms compose a space charge which extends mostly into the region with lowest impurity, that is into the region of higher resistivity. Some consequences of this will be seen later when the punch-through effect in transistors is discussed.

Although there is an electric field across the junction this cannot be measured with a voltmeter because of effects which occur at the metal-semiconductor junctions. If it were possible to make this measurement the system would constitute a form of perpetual motion machine which unfortunately is not feasible.

## Forward bias

Consider now what happens when a voltage source $s$ connected across the junction with the positive erminal attached to the p-type material and the regative terminal attached to the n -type material. The Fermi levels will be displaced by a potential
proportional to the voltage applied, as shown in Fig. 3(b). In this situation electrons from the $n$-type material have a much smaller potential hill to climb and consequently a much larger current will flow due to diffusion. However the thermally generated electrons from the other side will still produce the same drift current since their number depends on the temperature alone and they are all collected by the drift field. A current will flow through the p-n junction diode when it is connected in this forward direction. This current consists of electrons and holes although only the electrons have been considered here.

## Reverse bias

If the voltage is connected in the opposite direction the potential hill against which electrons from the n-type region have to flow is increased as shown in Fig. 3(c). This results in a reduction of the diffusion current. Again the current due to thermally generated electrons from the p-side remains constant. Consequently when a reverse bias is applied to the system in this way only a small current flows, this time in the opposite direction to the current flow with forward bias. When a large reverse bias is applied this current approximates that due to thermally generated electrons alone and is independent of the bias. This is called the saturation current of the diode.

## Diode characteristics

A typical voltage-current curve for a silicon and a germanium junction diode is shown in Fig. 4. It can be seen that the reverse saturation current $I_{\text {sat }}$ is several times larger for germanium than for silicon; this is a consequence of the larger band gap of silicon. The offset voltage $V_{\text {os }}$ is the value of forward bias for which the forward current is greater than some small threshold.
The current through the diode can be shown to be given by the equation:

$$
I=I_{\mathrm{sat}}\left(e^{a V \mathrm{app}}-1\right)
$$

where $a$ is a constant which increases with temperature, $V_{\text {app }}$ is the voltage applied to the diode and $e=2.7$. This exponential increase explains the appearance of the offset voltage, and the larger value of

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[^1]

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Fig. 4: Typical current/voltage characteristic curves for silicon and germanium junctlon diodes.
$I_{\text {sat }}$ for germanium explains why it has a lower offset voltage.

At high reverse bias voltages breakdown of the junction occurs. There are two main effects responsible for the breakdown. First the process called avalanche multiplication, which is caused by thermally generated electrons being accelerated across the depletion layer. During their passage they collide with unionised atoms and liberate more electrons by ionising these atoms. This process is repeated by the greater number of electrons now existing and results in a large current flowing across the junction. A voltage of more than 6 V is required to produce the avalanche breakdown effect. At lower, voltages another effect can produce breakdown of the junction; this is the zener effect which is caused by the strong field across the junction. Because of its narrow width a voltage of 6 V can lead to a large potential gradient which is what the breakdown relies upon.

## The manufacture of diodes

In Part 2 the production of a crystal of semiconducting material with a uniform impurity concentration was described. Because of the different segregation coefficients of different dopents various quantities of dope have to be added to the melt from which the crystal is being grown. To obtain the same doping concentration with different dopents appropriate amounts are required. If equivalent amounts of n - and p -type dopents are added it is possible to produce compensation, with acceptors and donors balancing exactly, giving no net doping.

This can be utilised in preparing a p-n junction during crystal growth. If n-type dope is added to the melt from which the crystal is being grown then the first part of crystal to be grown would be n-type. Now if sufficient p-type material is added to the melt the $n$-type dopent will be over-compensated so that the next part of the crystal to be grown will be p-type. By doing this it is possible to produce a p-n junction.

The segregation coefficient for different dopents changes as the rate at which the crystal is grown from the melt is changed. For antimony in germanium the segregation factor increases quickly with growth rate but with gallium it changes more slowly. If correct amounts of these dopents are added to the melt it is found that a rapid growth rate results in
antimony doped n-type material but a slow growth rate leads to gallium p-type doping. So variation of the growth rate can also be used to produce successive n - and p -type regions giving a chain of junctions. These are subsequently sliced to give discs of perhaps 1 in . diameter which are made into hundreds of diodes.

## Diffused junction diodes

It has been described how impurity atoms will diffuse rapidly into the body of a semiconductor at a high temperature. This fact is utilised in one type of diffused junction diode. A coating of a p-type impurity is applied to one surface of a slice of n-type material. This is subsequently heated to $800-900^{\circ} \mathrm{C}$ for a defined time whilst the impurity diffuses into the slice. A p-n junction will be formed across the plane reached by the impurity.

The process of heating results in a decrease in the lifetime of the minority carriers and consequently to an increase in the forward resistance of the diode, making it less suitable for high current applications. However it also results in a decrease in the diffusion capacity which improves the switching characteristics. A gradient of impurity ions is obtained across the junction in this type of device so that the field strength across the junction is reduced and consequently the reverse breakdown voltage is increased. Because of this it is also possible to employ a high impurity concentration with consequent low series resistance whilst still maintaining a high reverse breakdown voltage.

## Alloy diodes

Alloying is very frequently used in the manufacture of diodes. A small piece of a suitable impurity such as indium is placed on an n-type germanium slice and heated to about $500^{\circ} \mathrm{C}$. The indium melts and dissolves the surrounding germanium. As the slice is slowly cooled the mixture of indium and germanium recrystallises to give a strongly p-type region. An abrupt junction is formed at the boundary region, without any built-in impurity gradient.

## Epitaxial planar diodes

Epitaxial planar diffused junction diodes are becoming available as integrated circuit techniques develop. However their method of manufacture will be described together with those of integrated circuits in a later article.

## Diode connections

Leads are connected to both sides of the diode to give non-rectifying or ohmic connections so that the diode can conveniently be coupled to an external circuit. The diode is then sealed in a glass or metal case in order to avoid atmospheric contamination occurring.

In the following Part the other types of diode which are available will be described and their individual merits discussed.

TO BE CONTINUED

# practically wireless commenarvathenni 

IF you have ever paused to wonder why your ten-transistor portable spends more time going back to the workshop than receiving Radio One; if your brand-new amplifier develops an angry hum; if I-Cs disintegrate in your hand, don't worry-it is probably the Peter Principle at work.

Not so different really from some of the extensions to Henry's Law (inanimate objects subsection), the Peter Principle quests further afield and takes in cybernetics. It is the study of human incompetence.
Dr. Laurence Peter is a Canadian, a university professor, once a prison instructor and a school psychologist. He has collaborated with Raymond Hull, a British writer now living in Canada, to produce a wildly satirical book based on the theory: for every job there is a man somewhere who cannot do it. Sooner or later they will coincide.

In a large organisation, such as the Superset factory where your transistor radio was born, a man who shows promise at his job can expect to be offered promotion. He moves up the ladder each time he proves a success until he reaches the level where his capabilities are blocked by the demands of his new task. And there he sticks.
First of all, he was sorting out the components in the Superset stores. Then, when he had learned the colour codes and

. . . ears in the back of their heads
other fundamentals, they shifted him up to the production line. Not content with merely soldering bits into chassis, he went to night school and learned a few formulae, so they moved him to the test department.

Now the test department in the average radio factory (or, at least, those few Henry has worked in) consists of the lancejacks who carry out spot alignment, with instruments set up for them-"You just twiddle this screw till that needle reaches this line, see?"-then the corporals who do alignment and other adjustment checks, then the final test bods, who have to have ears in the back of their heads, and finally the elite warrant officer class who undertake the trouble-shooting.

There are several lines of progress. With his acquired know-how, he may just be capable of entering the planning or design department; in a mundane capacity, making up breadboard lash-ups as instructed.

In time, his breadboard efficiency is noticed and he is given a few minor modifications to do. Being wise in factory ways by now, he keeps his eyes open, follows the trend and doesn't quite make a hash of it. But we all know how late his mods are, don't we? The set we bought is very different from the model Superset market now. It is a corollary to Henry's Fourth Law that our receiver will be the Mark One with the knobs that split, the volume control that rasps, the on/off switch that flips but does not flop, the noisy transistors, the printed circuit without that link that bridges the draughtsman's error . .
Nobody notices our friend is beginning to flag. He marries the Sales Manager's daughter and becomes a fully-fiedged designer. He is the chap that was responsible for the amplifier whose output valves cooked a hole in the

. . . whose output valves cooked a hole in the cabinet
cabinet. But that was so long after production, and the design was remarkably cheap to make, so he was once more a success and now leads a subsection team.

There he sticks-and why? Because he has reached the limit of his capability. New techniques have overtaken him, his mental gate is closed to F.E.T.s, he can't even pronounce quasi-complementary and to him Darlington is just a place where the trains start from.

But the reason he eventually gets the sack-in accordance with the Peter Principle-is not his incompetence. Just the opposite, in fact. In a desperate attempt to redeem his good name he designs a tuner about which the reviewers rave. It has all the station-seeking attributes one could wish for and Superset spend a mint on advertising it before the prototype is completely unwrapped.

Our friend has made his name. He glows with pride as the first ten roll off the line-then sinks into oblivion, for the gold-plated I-C on which he based his i.f. strip can only be made in midtransvaria and the Customs and Fxcise won't release any more from bond. So the Superset tuner is modified out of all recognition, becomes uneconomic and, like its designer, is dropped.

Henry's Third Law tells us that you and I, Joe, will always get the modified type!

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MT112 0．5 Amp Size $37 \times 2^{7} /_{10} \times \quad$ Wgt 11 lb 4of Price 17／4 P\＆P $3 / 9$
MT79．I Amp Size $2 \frac{3}{2} \times 2 \frac{1}{2} \times 2$ 青in．Wgt 2lb Price 23／－P\＆P6／－


MT89 10 Amp Size $5 \frac{1}{2} \times 4 \times 4 \frac{4}{5} \mathrm{in}$ ．Wgt 121 lb 20 z Price 103／6 P\＆P11／－

## LOW VOLTAGE 50 VOLT RANGE

## Primary 200－050v SECONDARY TAPPED 19－25－33－40－50V



 MT119 10 Amp Size $6 \frac{1}{2} \times 4 \frac{1}{2} \times 6 \frac{1}{2}$ in．Wgt $19 \mathrm{lb} 120 z$ Prime 185／－P\＆P 15／6

## LOW VOLTAGE 60 VOLT RANGE

Primary 200／250v．Secondary Tapped 24－30－40－48－60
MT124 0.5 Amp Stae $34 \times 2 \mathrm{a} \times 2 \mathrm{jin}$ ．Wgt 2 lb 402 Price $24 /-\mathrm{P} \& \mathrm{P} 6 /-$
 MTI22 10 Amp gize $6 \frac{1}{2} \times 5 \times 6$ inim．Wgt 23 lb 202 Price 152／－Corr $11 /$

## MAIMS H．T．RANCE Size PriceP\＆P

MT1AT $250-0-250 v$ 80MA $6.3 \mathrm{v} 3-5 A .3 / 6 \cdot 3 \mathrm{v} 1 \mathrm{~A} \quad 3 \frac{1}{2} \times 3 \times 3 \mathrm{in}$ ． $88 /-\quad 6 /-$
 MT110 $250-0-250 \mathrm{~V} 120 \mathrm{MA} \quad 6 \cdot 3 \mathrm{~V} \quad 3 \cdot 5 \mathrm{~A} \quad 5 / 6 \cdot 3 \mathrm{~V} 1 \mathrm{~A} 4 \times 4 \times 31 \mathrm{in}$ ． $44 / 9 \quad 6 /$





## BATTERY CHARGER TYPES

| M77 | 1 Amp | Sfze $2 \frac{7}{} \times 21 \times 2$ 者in． | Wgt | 1 lb 60 z | Price | 15／－ | P\＆P 4／6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MT45 | 1.5 Amp |  | Wgt | 11b 902 | Price | 21／9 | P\＆P 4／6 |
| MT46 | 2 Amp |  | Wgt | 2 lb 402 | Price | 25／4 | P\＆P $6 /-$ |
| MT47 | 3 Amp | Stize $4 \times 3 \times 3$ itin． | Wgt | 8 lb 8 cz | Price | 28／4 | P\＆P60 |
| MT5 | 4 Amp | Eize $4 \times 2{ }^{2} \times 3$ in． | Wgt | $8 \mathrm{lb} \mathrm{110z}$ | Prlce | 381－ | $\mathbf{P} \& \mathrm{P}^{6 /-}$ |
| MT78 | 5 Amp |  | Wgt | 5 nb 403 | Price | 421－ | P\＆P6／－ |
| MT86 | 6 Amp | Slze $4 \times 3 \frac{1}{2} \times 8$ 2in． | Wgt | $515120 z$ | Price | 481－ | P\＆P6／－ |
| MT48 | 7 Amp | Size $4 \times 4 \times 3$ gin | Wgt | 6 lb | Price | 86／7 | P\＆P91－ |
| MT146 | 8 Amp | Size 3 \％$\times 4 \times 4 \mathrm{in}$ ． | Wgt | 6 Ib 40 z | Price | 751－ | P\＆P9／－ |
| MT49 | 9 Amp | Size $4 \times 3 \times 4 \times 4 \mathrm{in}$ ． | Wgt | $71 \mathrm{~b} 80 z$ | Price | 991－ | P\＆P9／－ |
| MT147 | 10 Amp |  | Wgt | 91 b 30 z | Price | 105／－ | P\＆P 9／－ |
| MT50 | 12.5 Am | Size $51 \times 4 \frac{1}{4} \times 4 \frac{3}{4}$ in | Wgt | $1116140 z$ | Price 1 | 125／－ | P\＆P 11／－ |
| Amper | ges are | th nominal |  | e reetifl |  |  |  |

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 P25 less cart，with base P．\＄P．Decks $12 / 6$ ，Cover $4 / 6$ ，Base 4／6 MINIATURE SOLDERING IRON

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## JOHNSON'S (RADIO)

St. Martin's Gate, Worcester

IT'S all very confusing really. The propagation Confuciuses say: "When sun is spotty, l.f. bands grotty." True as this may theoretically be, it becomes rather difficult to explain the $W$ stations on c.w. regularly heard happily squeaking away on 1.8 MHz . The PY stations on 3.5 MHz , not to mention the African stations, all seem to indicate that theory and practice do go together-but you need quite an imagination at times to believe it.

John Moore (Leicester) says that LGSLG is near Magnor in Norway. He also tells that this month he logged a station at every hour of the day and night except 0400 hrs GMT. Never mind John, I never have any luck at 0400 , probably 'cos I'm fast asleep in bed!

Various scribes have written in with titbits of info. One tells of rumours that OY stations are hoping to be on 1.8 MHz soon. Foreign parts to tune for when switching on are Tokelau Island (listen for ZM7) and Manahiki (ZK1).

Barry Weston (Poole) informs that Chatham Island is going strong, but this is rather a sore point with me since my Chatham Is. signals were almost certainly emanating from the spotty faced s.w.l. of 12 moons who, I feel sure, is "at it" with a transistor rig about 800 yards from my long wire.

Twenty metres offers an easy way to log half the world in one go. Best times for VK/ZL have been the wee small hours till breakfast time. The JA stations seem to arrive later around lunch time. Twenty's stablemate, 21 MHz , is good from breakfast until midnight and peaks very well at times. Ten metres comes and goes, but early mornings to tea time usually produce some good sigs with DX sneaking through and peaking to 5 and 9 plus. Late night listening has produced noises like frying eggs in the cans and has been no good at all.

Nobody listens on 70 MHz and 144 MHz , or if they do, they keep jolly quiet about it. As soon as you've read this sentence, stand up and shout "Listen on 4 and 2 metres", and then go and do it. Don't forget to let me know what you hear-when I'm sure it's safe, I'll have a listen too. Incidentally, for those who think these are just cross-town bands, the recent SM7/ZL1 2-metre contact would take a bit of explaining.

## MULTIBAND LOGS

Most s.w.l.s listen on more than one band, although usually they have a favourite. Because of space considerations I usually put in one-band reports only and select the best one from the log. But, this month, I'm setting down all the logs for a change (Ooh! Isn't he bold).
A. Hall (Kent) lists among his possessions one modified Eddystone 888 A plus a.t.u., a 110 ft . long wire, and a multiband folded, loaded dipole. On $1.8 \mathrm{MHz}-\mathrm{GI}$ and $\mathrm{GM} ; 3.5 \mathrm{MHz}-\mathrm{CT} 2 \mathrm{AT}, \mathrm{EP} 2 \mathrm{BQ}$, GI, GM, GW3XTA, running 6 watts, HB9ABM, HB9ALG, I1AHO, K1CTA, MP4TAF, OH, ON, OZ, OY4OV, OY6NRA (club station), PAø, PY7ASQ, PY7GV, SK, SM, UA3KAA, UP2TB, VO1FG, VO1FX, W2BL, W4BFA, YO5TI, YU2HPE, ZB2BS, 5 A1TN: $7 \mathrm{MHz}-\mathrm{GB} 2 \mathrm{SM}, \mathrm{I} 1 \mathrm{LAI}$, MP4TAF, YV4IQ, YU3TGI, W4PHE, WA1FKS, WA3FWJ, WA5ORK. All on s.s.b. except the last four W stations.
W. Harper (Staffs) describes 40 metres as ". audible fog". The gear comprises an 840 C , Joystick plus Joymatch at 36 ft . with a 66 ft . feeder. Forty s.s.b. -CT1GD, CT2AK, EA3HF, EP2BQ, HC4ME, HB9UD, HI2HH, K4RUG, MP4TAF, OZ5VT, PY8VA, SK5AA, SL3ZV, UF6CR, UV9KAG, W2EWT, W3IGK, W4QR, W5GTP, W5OVR, WA2GLH, WA3PSJ, WA4VWX; 20 s.s.b.-EA1CRP, F2UX, FP8CS, KP4AST, HV3SJ, KV4DL, KR6AF, KZ5NF, OA4JRT, OZ8QX, PI1GHK, PY8MG, SVøDD, TI4JM/P7, UM8IKZ, VE2DC, VE3CRP, VE6AFJ, VK1RD, VK2BSM, VK2DY, VK3TG, VK4UC, VK5MS, VK7AZ, W7SFA, YV4VA, ZC4MA, ZL4BX, ZL4LD, 4S7AS, 9G1YJ, 9E3USA, 9V1PB.

Stephen Cole (Monmouthshire) has a trio JR60. An indoor wire (man that's living) raised these on 28 MHz - CX4IX, FG7XT, KV4AD, PZ1DA, VP8KL, VS6AL, YA1AR, ZS1YX, 7Q7WW, 9N1MM, 9X5AA; $7 \mathrm{MHz}-\mathrm{CO} 2 \mathrm{DC}$, K2RTH, MP4TAF, PY7EC, W8UM, YV1BI, ZC4HS, 5A2TR, 9H1BA.

## TWENTY METRES

R. Dinning (Ayrshire), HA350 Mk2, PR30X and RQ10, 380ft. long, long wire, logged this lot on 14 MHz s.s.b.-CT2AK, CT3AW, DU1ZAG, ET3USA, HR1DB, HV3SJ, JA3GZN, KX6FA, HL9UU, LG5LG, PZ1DD, SU1MA, TI2AP, VK2XG, VK3XI, VK6ID, WA4DUC/HS, XE1DE, ZL1KM, ZL1NB, VP2LA, VP9FE, VR6AL, VU2OLK, 3AØCU, 3V8AC, 5N2AAX, 6Y5DB, 8P6AF, 9E3USA, 9K2AM, 9Q5HS, 9Y4LP.
J. Moore (Leics.), CR100/2, 60ft. end fed, had two weeks off from school. Homework on 20 s.s.b. gets him ten out of ten for logging-CE3FH, CE6CA, CP1GN, CX6CG, DU1FH, F9UC/FC, HK5BDS, HS3RT, JA4AS, K7BCX, KR6KN, LG5LG, M1B, OA4OS, OY6NRA, PJ2CC, PJ7JC, SV $\varnothing W N$, TA1MGP, TA3RF, TF2WLT, TI2MEF, UA9KDL, UF6CR, VE3EQI, VE5BV, VE6XJ, VE7PV, VK2EK VK5MO, VP7NH, VQ8CPR, VR6TC, W2FHO/W7, W5HE, WA4PUC/P/HS, WA6BMG, WB6MOS, W7AEK, XE1IX, XW8AX, YS1O, YS2RAR, YV2HQ/P/3, ZL4BX, 4S7PB, 4Z4HF, 5R8AN, 8P6CV, 9Q5IA.

## HAPPENINGS

If you are thinking of having a rest in July, don't bother. It's quite a busy month for the keen types who can stand the pace. July 5th-6th, topband contest; 5th-6th, 2 metre contest; 6th, South Shields mobile rally; 12 th -13 th, high power field day; 13 th, Worcester mobile rally; $20 \mathrm{th}, 70 \mathrm{cms}$, contest; 27th, Cornish mobile rally.

Please remember that logs must reach me by the 20th of the month, otherwise they miss out no matter how good they are. Those in alphabetical order are always at the top of the list, while those with no mention of which band or mode etc., are right at the bottom.

Warning well in advance. A letter from G3FSN says listen for GB3WRA from the annual Wycombe Show, all bands 160-4 metres on Saturday, September 6th.

# TAKE 2중 

## A series of simple transistor projects, each using less than twenty components and costing less than twenty shillings to build. This month's project is described more fully than usual and should prove popular with both our musical and unmusical readers.



The Take 20 prototype of the electronic organ.

PERHAPS we are cheating a bit this month as, although we are still within our 20s. limit we are using more than 20 components. As an excuse 1 offer that if only a single octave version is required we remain strictly within our category.

In building it I had a problem, apart from unsuccessfully attempting to vamp a guitar and successfully reproducing the drone of Lancaster bombers by depressing one note of a foot-pumped organ, I have never played a musical instrument. On seeking advice I learnt that about 15 notes including sharps and flats were necessary to play the simplest tunes and this our project achieves.

Last month a metronome was described and it was while playing about with this that the idea was born. If, instead of using a $30 \mu \mathrm{~F}$ capacitor a $0.1 \mu \mathrm{~F}$ was substituted, a high note is reached, varying with the setting of the potentiometer. A version based on this circuit however has disadvantages; stability was hard to achieve and the resistance scale followed no known law, probably due to the leakage etc. of the transistors.

## THE CIRCUIT

A unijunction transistor 2 N 2646 was used instead with very much better results and one is used in the final circuit. However, the volume from the

The working of the unijunction has been described recently in an article in Practical Wireless (Nov. and Dec. 1968) and there is no point in duplicating this information-all that need be said is that the unijunction has two bases and one emitter, but no collector. The amplifier section is completely standard and needs no explanation.

The actual frequency depends on the value of the resistance selected between the positive rail and the emitter of the unijunction; the combination of the resistance and the $0.1 \mu \mathrm{~F}$ capacitor determines the note.

## THE OUTPUT

Either an $80 \Omega$ impedance loudspeaker or a balanced armature earpiece may be used: funnily enough in this circuit the latter was not only louder but produced a more pleasant note (this doesn't apply of course to normal audio). This is probably due to the waveform which takes the shape of a spike when displayed on an oscilloscope.

Although the volume is more than adequate, the battery drain is only about 15 mA from a 9 V battery. If one wants to use an external amplifier the takeoff points are across R16, $100 \Omega$, but the input impedance of any such amplifier should be fairly



Fig. 2: The layout of the components on the Veroboard. The balanced armature earpiece is held by two short screws.
high otherwise a damping effect takes place on the oscillator.

Difficulty may be experienced in obtaining the correct value resistors as some, such as the 620 , $750 \Omega, 910 \Omega$ and $1 \cdot 1 \mathrm{k} \Omega$ are not preferred values. One way is to select these values from a batch of $20 \%$ tolerance resistors but arrangements have been made with Electrovalue Ltd. of Egham to supply a pack of R1 to R15 to the specification inclusive for 3s. 4 d . including postage.

## CONSTRUCTION

All the components are mounted on a piece of Veroboard $5 \frac{1}{2} \times 2 \frac{1}{2}$ ins, one end of this forming the "keyboard", the other holding the battery, the loudspeaker and the main components. The actual keys are made by using short lengths of Cir-Kit adhesive copper strip bent over the end of the board to bring the "keys" to the top. To differentiate between the ordinary notes and the semitones the latter strips were cut shorter than the others.

The layout is completely uncritical and many constructors may wish to build the unit into a small cabinet. Figure 2 shows the suggested layout.

## PLAYING THE ORGAN

The actual notes are played using a probe (one from an old testmeter was used by the author) to select the correct notes.

VR1 is a $2 \mathrm{k} \Omega$ trimmer pot. which will tune the instrument to another such as a piano. A volume control is fitted and unfortunately, because of the simplicity of the circuit, this very slightly affects the note, but no problem will be experienced if the volume is set before tuning up. Extra octaves can be added by placing a carefully matched capacitor either in series or in parallel with Cl .

The range of the basic keyboard can be extended by adding further resistors to the chain (these will have to be chosen by experiment). The tone of the instrument can be altered by removing or changing

## $\star$ components list

## Resistors:

R1, R2 1-2k $\Omega$ 5
R3, R4 1-1k $\Omega$ 5\%
R5, R6 $1 \mathrm{k} \Omega 5 \%$
R7, R8 $910 \Omega 5 \%$
R9, R10 820 25
R11 750 ${ }^{5} 5$
VR1 $2 k \Omega$ lin. preset
R12, R13 680 $5 \%$
R14 620』 5\%
R15 10k $\Omega$ 5
R16 100』 10\%
R17 27k $\Omega$ 10\%
All $\frac{1}{3}$ or $\frac{1}{4}$ watt miniature
VR2 $5 k \Omega \log$ with switch
Capacitors:
C1 $0.1 \mu \mathrm{~F} 12 \mathrm{~V}$
C3 $0.04 \mu \mathrm{~F}$ (optional)
C2 $2 \mu \mathrm{~F} 12 \mathrm{~V}$

## Miscellaneous:

Tr1 2 N 2646 or equiv. Tr2 0 C 81 or equivalent Veroboard, 0.15 in . matrix $5 \frac{1}{2} \times 2 \frac{1}{2}$ in.; Balanced armature earpiece or $80 \Omega$ loudspeaker; 9 V battery; Cir-Kit strip; test probe; heatsink.
the value of C 3 , also extra volume will be achieved, but with it removed the notes are harsh and unpleasant-at least to my unmusical ears.

An attractive point that this circuit has because of the use of a unijunction is that the note emitted is virtually independent of battery voltage; the prototype was stable even when the battery was reading only 4.5 V .

Next month our project is a transistor tester designed to sort out the good, fair and dud transistors sold in the surplus 10s. packs for leakage and gain in both $\mathrm{p}-\mathrm{n}-\mathrm{p}$ and $\mathrm{n}-\mathrm{p}-\mathrm{n}$ types. In addition it checks its own battery, measures other battery voltages under load, measures resistance between $500 \Omega$ and about $50 \mathrm{k} \Omega$, acts as an electrolytic capacitor check and checks continuity; in fact it should prove an extremely useful addition to your testgear. For this a moving coil meter with a movement of 3 mA or better is needed (details of adapting any meter with a greater sensitivity are given). Meters with a 3 mA movement are advertised in this issue for 9 s . 6 d . and these should be ideal.


When the distant receiver is lifted, switch A changes over to complete the speech circuit. Replacing the receivers causes both switches to revert to normal, and the keys or buttons to cancel. Only the battery at the local end is used for a call, and the person on the extension need not operate any of the keys or buttons to receive an incoming call.

The circuit in Fig. 1 is that for the key units shown in the photograph. For the button units, the ring switches (complete depression of the selector button) will need to be paralleled together and coupled between $X$ and $Y$ in Fig. 1.

## Wiring of the key units

After removing the outer casing it can be seen that the unit consists of:
(i) The main frame carrying a $G$ block with some 12-20 terminals and two buzzers.
(ii) A front panel carrying the key switches.
(iii) An intermediate portion containing a miscellany of transformers, condensers etc.
The simplicity of the circuit makes the capacitors and transformer unnecessary and these are best removed, also remove the multicore cable and receiver. Next, trace the wires from the key switch contacts to the $G$ block and disconnect all others. It is best to adopt a logical approach to the rewiring of the $G$ block so that faults may be remedied easily at a later date if necessary. The receiver will have four wires connected to it. Strap the Blue and Green on the G block and connect the Red and White to

## Basic system

Any number of the basic units may be connected together (see Fig. 1) depending upon the availability of the switches. Lifting the receiver causes the restswitch, A, to change over to the receiver contact. A selector key or button is then operated to select the desired station. Pressing the ring key now provides a path between the local battery and the buzzer at the distant end via the appropriate loop wire and the common return wire.


Fig. 1: Circuit of basic system showing three units.


Fig. 2: Wiring diagram for key units.
make/release to break" button in any convenient position. In the units used one of the pilot indicator lamps was removed to facilitate insertion of such a switch.
The ring button is wired to the small G-block within the telephone instrument itself. Whilst in some cases there may be room within the instrument to house a battery, some of the later models do not permit this and the battery must be located in the junction box.
There are nominally four types of extension which the author has incorporated in his system although the variation within these types makes the list almost endless.

## Incoming calls only

This extension utilises any of the ordinary GPO type phones with or without a dial. The circuit is arranged so that a call incoming,
the unit. The sidetone produced by coupling the transmitter and receiver in series is not too distracting.

The receiver rest switch consists of three leaves each side of a rubber roller which causes the three leaves to short together-the upper set when the receiver is lifted and the lower set when the receiver is "on". In order to make a single-pole change-over switch from this arrangement it will be necessary to common one leaf from each of the sets (see Fig. 2).

## Button units

Several types of these units are available but all the later ones incorporate basically the same type of switching facility. Some may have junction boxes containing up to three relays which are not required. The author has found that the variation between these units involves the "receiver rest" switch. In the simpler kind the switch consists of one or two change-over contacts which are actuated when the receiver is lifted. Later versions have a spring set containing two change-over contacts. These change over when the receiver is lifted for an incoming call but revert to normal when a "station select" key is depressed. The wiring diagram in Fig. 1 must therefore be modified to allow for this.

When a caller wishes to contact a button unit of this type 4.5 V is applied across the outgoing loop wire and the common return wire. Switch A changes over when the receiver is lifted and conversation may proceed. Should an outgoing call be made from a button unit of this type, the receiver is lifted which results in the switch A changing over and a "station select" key is operated. This switch will cause the switch A to revert to normal by a mechanical arrangement so that ringing and speaking can proceed in the usual way.
None of the button units the author has come across has a spring return "ring button' as such and rather than modify one of the existing buttons it is considered preferable to install a separate "press to


Fig. 3: Typical arrangement of button selectors.
say, to a large room may be answered at the main unit or at the extension on the other side of the room (but not both), it is not possible to make an outgoing call from the extension. The circuit is shown in Fig. 4.

The "works" of the telephone used will vary but are best removed as only the receiver rest switch is required.


Fig. 4: Circuit for incoming calls only type extension.


Fig. 5: Wiring for a "parented" extension.

## Parented extension

This extension which can be "parented", meaning directly connected to and dependent upon, on to any of the standard units enables the extension to call that unit by using a dial telephone or an auxiliary key switch mounted near the telephone. The circuit for this is shown in Fig. 5.
If a dial phone is used, the method of operation is to lift the receiver and dial 0 . Ten rapid pulses of 4.5 V will be sent over the line to operate the buzzer at the parent main unit. When wiring up the dial, strap $F$ and D and connect $E$ and $C$ to contacts 1 and 2 in the diagram. The receiver rest switch will be connected so that the bell is in circuit when the receiver is "on". Any number of these extensions may be parented on to one main unit.

## TO BE CONTINUED

## THE TRANSET

## continued from page 245

current (best volume) but signals should be kept down so that continuous current is not over 25 mA or so.

If no generator is available, tune in a signal on any band, even if this requires an external aerial. Then adjust the five i.f.t. cores for best volume.

Should no signals be obtained, it is not wise to make large adjustments to the i.f.t. cores at random, as the fault may be elsewhere. It is possible for wrong alignment alone to prevent signals passing through the i.f. amplifier. Should there be no fault except unnecessary disturbance of the cores, the best solution is to inject 465 kHz at 5 of i.f.t. 2 , and adjust i.f.t.3. Then inject at 2 of i.f.t.2, and adjust the secondary of i.f.t.2. Follow by injecting at 5 of i.f.t.1, and adjust both cores of i.f.t.2. Then inject at Tr 1 base and adjust i.f.t.1.

When all the i.f.t. cores are peaked, using a reduced signal input or weak signal, they are left untouched during subsequent trimming.

## SW range

Unscrew the trimmer across VC1, and set TC2 about half-closed. With VC1/2 nearly fully open, adjust T4 until the trimmer VC3 can be peaked for best results, and is well open when this is done.
Tune towards the l.f. end of this band, meanwhile adjusting the core of L1 for best results, and to minimise the need for any readjustment of VC3. Actual band coverage depends also on the cores of L1 and L2, which should be locked with 6BA nuts.

If T 2 is adjusted for m.w. trimming, T 4 may need resetting. This is unavoidable with T2 incorporated in $\mathrm{VC1} / 2$, but would not arise if T 2 is separate and connected for L5 only.

## MW range

Adjust the core of L5 for suitable frequency coverage, and slide L3 on the rod for best volume at the 1.f. end of the band. At the h.f. end, VC3 should peak up for best volume near the fully open position. If VC3 needs to be completely open, screw TC2 down slightly. Check the position of L3 on the rod, so that much adjustment of VC3 is not required when tuning over the band.

## LW range

Adjust TC3 for a suitable tuning point for 200 kHz , or near the l.f. end of the band. Move L4 on the rod, for best volume, and least need to readjust VC3 when tuning over the band.
It should be found that normal m.w. and l.w. tuning can be obtained with no need to adjust VC3, but that it is almost impossible to find alignment which does not result in some improvement, at some frequencies, by means of VC3. This is quite usual.
On the extreme h.f. end of the s.w. band, adjustments to VC3 tend to become sharp, and to pull tuning slightly. This cannot be avoided here, and is not important.
The trimmer TC1 can be set to about one-third of maximum capacitance, for the telescopic aerial. For a long aerial, such as an outdoor wire, it should be reduced. The telescopic aerial is normally sufficient. Alignment should allow VC3 to be peaked up for best volume with the aerial extended, or closed, on m.w. and l.w.

## Cabinet

This is about 7in $\times 8 \mathrm{in}$. inside dimensions, and $3 \frac{1}{2}$ in. deep. It was made from $\frac{3}{16}$ in. plywood, glued at all joints. It is glass-papered, well dusted, then covered with self-adhesive material of any preferred colour.

The telescopic rod bracket is fixed with two bolts through the side of the case. T1 is soldered to a short, stiff lead from VC1, and the second tag of T1 has a lead which is taken to one bolt holding the aerial. The receiver is used with a PP9 or similar 9 volt supply.

#  <br> PART 8 <br> <br> M.K.TITMAN, B.Sc.(Eng) 

 <br> <br> M.K.TITMAN, B.Sc.(Eng)}

Most meters are retailed for specific requirements and consequently have series resistors or shunts incorporated to give the required voltage or current range required, with the scale suitably engraved. The accuracy of most meters is between $\pm 1 \%$ and $\pm 2 \%$ of full-scale deflection. It must be remembered that this figure does not account for reading errors which may be between $\pm 1 \%$ and $\pm 5 \%$ depending on the type of scale and engraving. Generally a meter is only as accurate as the smallest division on the scale. Another point worth noting is that accuracy is based on full-scale deflection (f.s.d.) and thus a reading at $1 / 10$ of full scale has a percentage accuracy of $\pm 10 \%$, i.e. measuring with a $10 \AA 1 \%$ f.s.d. meter, a 1A reading can be within the actual limits of 0.9 to 1.1 A and this excludes further errors due to reading inaccuracies.

Meters are available at a wide variety of prices which rise with quality and also figure of merit. Thus $1-10 \mathrm{~mA}$ ( $1000-100 \Omega / \mathrm{V}$ ) meters can be obtained at from 10s. to £ 3 depending on mirror scale and size whilst $20-100 \mu \mathrm{~A}$ ( $50,000-10,000 \Omega / \mathrm{V}$ ) meters cost from $£ 1$ to $£ 10$. Precision series resistors are available from 1s. to 10 s . depending on value and tolerance whilst meter shunts are available from 5 s . to $£ 1$.

## Loudspeakers

Loudspeakers are devices which convert electrical energy into acoustical energy by utilising electromagnetic forces to provide physical movements. A very considerable amount of work has been carried out into the improvement of loudspeakers with the result that there are many different varieties and configurations. Since the permanent magnet, moving-coil or electrodynamic loudspeaker is by far the most widely used, only this type will be considered here.

The basic features of a moving-coil loudspeaker are


Fig. 1: Basic features of a moving-coil loudspeaker.
illustrated in Fig. 1 and the circuit symbol shown in Fig. 2(a). The electrical audio output is fed to a voice coil suspended by means of a cone in a magnetic field generated by the permanent magnet. The electromagnetic field interacts with the permanent magnetic field to produce a movement of the coil and cone.

(a) Loudspeaker

(b) Headphone

(c) Microphone

Fig. 2: Circuit symbols for acoustic transducers.
Ideally the acoustical power output should be identical to the electrical signal fed to the voice coil but unfortunately this cannot occur except over a very limited frequency range. The deficiency is due to the mechanical construction of the speaker as a whole. If the cone is large then the mass and inertia of the cone damp out the higher frequencies whilst a small cone results in a loss of low frequency tones due to the compliance (inverse of stiffness). The coil mounting and cone stiffness characteristics lead to a bass resonant frequency which varies from $20-30 \mathrm{~Hz}$ for large cone speakers to $200-300 \mathrm{~Hz}$ for smaller stiffer cones. Below this frequency damping forces reduce the acoustical output.

Large cone speakers however suffer at high frequencies due to the mass of the cone and phasing of the sound waves which can be more than 180 deg . out of phase between the coil and periphery of the cone. For this reason corrugations are introduced to reduce the effective cone area at high frequencies. Alternatively changes in cone thickness can be used to increase efficiency at high frequencies. In all cases the transient response is increased by increasing the permanent magnetic field in order to damp out oscillatory tendencies.

Essentially therefore loudspeaker design is a compromise between large size and cone stiffness (compliance) together with voice coil mountings and permanent magnetic strength. To give wide frequency coverage the most popular means is to use two speakers in parallel, together with a crossover network, or a double cone speaker. The double cone speaker has a small cone attached directly to the voice coil whilst the large cone is flexibly coupled. At low frequencies the large cone gives the required output, whilst at high frequencies the flexible coupling ceases to operate and the small cone alone produces the acoustical output.

For efficient operation loudspeakers must be operated on baffles which eliminate the out-of-phase sound component from the rear of the speaker. Loudspeaker enclosures are many and varied since over-all efficiency, particularly the bass response, can be increased by
suitably mixing low frequency components from the rear of the speaker such that addition is caused by the phase relationship.

We have seen how loudspeaker performance depends largely on mechanical considerations; let us now look at parameters and prices of speakers. The standard voice coil impedances are $3 \Omega, 8 \Omega$, and $15 \Omega$ with some $35 \Omega-$ $75 \Omega$ speakers available for transistor circuits. Standard sizes vary from $2 \frac{1}{2} \mathrm{in}$., having a bass resonance of 400 Hz , to 14 in ., having bass resonances of $20-50 \mathrm{~Hz}$. Low cost units have flux densities of 5,000 to 8,000 gauss (G) whilst wide frequency range speakers have flux densities of 10,000 to $14,000 \mathrm{G}$ and employ both single and double cone construction.

Maximum power depends upon size and construction and is usually $1-2 \mathrm{~W}$ for small low cost speakers and 2-4W for larger (5in.-8in.) low cost units. Wide frequency, high gauss speakers are capable of handling power levels up to 20W although it must be remembered that the maximum power is the value which if exceeded results in physical damage to the coil and cone assembly and consequently bears no relation to the distortion. For example for 7 W power at 30 Hz the cone must move $2 \cdot 3 \mathrm{in}$. for a 5 in . speaker, lin. for an 8 in . speaker or $0 \cdot 6 \mathrm{in}$. for a 10 in . speaker.

Loudspeaker prices vary widely and largely depend upon power capability and frequency response. General purpose speakers are available from 10s. to $£ 2$ depending upon size, whilst high flux, wide frequency response speakers vary from $£ 3$ to $£ 15$. Twin cone and other complex cone and coil construction speakers can be obtained in the price range $£ 3$ to $£ 25$.

## Headphones

Headphones consist of an earpiece behind which is a diaphragm. The earpiece traps a small volume of air and consequently the power requirements to give satisfactory acoustic power levels are very low. Many forms of drive for the diaphragm are utilised, including: direct electromagnetic action on the diaphragm; moving-armature types; moving-coil; crystal; ribbon (for high fidelity reproduction) and inductor. Headphones vary in price in the range 10 s. to $£ 5$ depending on quality and availability. The British Standard symbol is shown in Fig. 2(b).

## Microphones

Microphones are essentially transducers which convert sound pressure waves into electrical energy and the circuit symbol is shown in Fig. 2(c). Many different types of microphone are used and unlike loudspeakers no one type is pre-eminent. Basically microphones can be divided into two categories: those which are pressure operated and velocity operated types. The pressure operated microphones are by far the most common and operate by the displacement of a diaphragm. The velocity operated types have a response to the particle velocity or pressure gradient. The velocity ribbon microphone, which consists of a free ribbon suspended in a magnetic field, has by far the best frequency response characteristics and is widely used in studio hi-fi systems, but is very expensive. The great majority of microphones are of the pressure operated variety.

The common forms of pressure operated microphone are the carbon, crystal, dynamic (or moving-coil), and condenser microphones. All incorporate a diaphragm
which is physically moved and consequently alters the electrical characteristics of the microphone.
Carbon microphones are used in telephone systems and the output is derived from a change in the carbon resistance. Crystal microphones are common for radio and other uses and derive an output through an effective capacitance change. Condenser microphones similarly derive an output from capacitance variations between two plates, one of which is the diaphragm.

Dynamic or moving-coil microphones operate essentially as loudspeakers in reverse and indeed loudspeakers can be used as dynamic microphones. Most portable radio links use this interchangeability to advantage. Moving-coil microphones are widely used for general purpose and domestic applications, particularly in conjunction with semiconductor circuits, where their low impedance properties allow effective matching. Condenser and crystal microphones are high impedance devices and their performance is degraded by long cable lengths or low input impedance circuits.

Moving-coil microphones have essentially 'similar frequency characteristics to loudspeakers and consequently the average domestic microphone has a relatively poor response of from 200 Hz to 6 kHz . They áre however universally available at prices ranging from 15 s. to $£ 5$. High quality, wide frequency versions using special coil mountings and acoustical matching horn and diaphragm assemblies are available at prices from $£ 5$ to $£ 100$ depending largely on quality. Of the other forms of microphone both carbon and crystal types are very cheap-from 7s. 6d. upwards-and easily available whilst condenser types are expensive.

## Moving-coil indicators

Moving-coil indicators are becoming popular as replacements for lamps in situations where extremely low power is required or where a greater reliability is required. Generally however they are not used simply as lamp replacements but for fail safe and enunciator applications.


Fig. 3: Moving-coil indicator.

Basically they consist of a dial face which revolves as shown in Fig. 3 by the action of a moving-coil. The face may show any colour or design but those generally available for use in process control display units have crosses or lines which appear when activated to show the opening of a valve or closing of a switch. Such devices require d.c. levels of $1-10 \mathrm{~mA}$ which is a considerably reduced power requirement than filament bulbs. When used as indicators they are fail safe since any loss of power can result in the display of a line or cross in the fail-safe condition. They are therefore a modern approach to the flag indicators used in switchgear. Prices vary but are generally in the region $£ 1$ to $£ 5$ depending largely upon the design of the legend and quality.

## Solenoids and counters

Electromagnetic counters are basically mechanical ratchet driven counters which are operated by a solenoid. A typical counter is shown in Fig. 4. The driving mechanism is a solenoid which consists of a movable core of magnetic material surrounded by a coil. The


Fig. 4: Electromagnetic counter.
core is generally spring loaded off centre from the coil so that excitation of the coil attracts the core to the centre of the solenoid. This movement is then utilised in the counter to drive a ratchet arm. The counter is essentially a totaliser but can usually be reset either electrically or mechanically. Prices of such devices vary from $£ 3$ to $£ 20$ depending largely upon the number of digits required and the type of reset. Lifetimes of such counters can be very high, up to $10^{3}$ counts, but they are inherently unreliable since they have a definite mechanical lifetime.


Fig. 5: Solenoid force-stroke characteristic.
Solenoids are available in many forms and are used widely for electrical activation of mechanical control circuits. The distance and force associated with the core movement is related to solenoid size, whilst the stroke length against force characteristic follows the inverse square law and is illustrated in Fig. 5. Solenoids designed for specific stroke lengths should always be used only for the design stroke since on every application of power the force-stroke characteristic applies and if the stroke is shortened excessive force levels may damage either the solenoid or the controlled object.

Prices and availability vary widely. For relatively small solenoids giving a force of 2 lb . at $\frac{1}{4} \mathrm{in}$. prices vary from $£ 2$ to $£ 10$ whilst high power solenoids are considerably more expensive. Low power solenoids of the
type used to operate chime door bells are available from 10s. to $£ 4$.

## The future

We have seen how essential electromagnetic devices are to electronic circuits where often they provide the only practical interface between mechanical effects and electrical signals. Thus they are unlikely to be superseded despite many problems of reliability. Reliability can however be increased by improved materials and constructional techniques and it is in this direction that future trends lie. Speakers will be made of better materials to give greater life and frequency response, reed relays will improve in power capability and supersede standard relays, meters will improve in accuracy and clarity although eventually they may be superseded by electronic readouts such as digital tubes. Improvements are the keynote and due to size and unreliability it is likely that large strides may be made in the field of electromagnetic devices.

## TO BE CONTINUED



A handy and simple-to-build item for the constructor. Enables voltages at parts of the chassis difficult to reach to be speedily checked.

## * TRANSISTORS IN TIMEBASES

The timebase sections of the receiver have not so far yielded to the transistor. In this new series the problems of using transistors in this field will be outlined and the present position described, starting with sync separator stages.

## * DX TV PREAMP

DX enthusiasts will find this high-gain preamp of great help. Full details along with a simple noise generator to assist with alignment.

## FAULT FINDING IN LINE OSCILLATOR STAGES

A detailed look at current line generator circuits with details of common faults and their cure.


THIS year's London Electronic Component Show, held at Olympia towards the end of May, was the 21st of its kind and by far the biggest ever staged. Sponsored as usual by the Radio and Electronic Component Manufacturers' Federation, it was international for the first time, with 75 foreign firms represented.

The reasons behind the change-over to an international exhibition were clearly stated by Mr. A. F. Bulgin, chairman of the Exhibition Committee:
"The possibility of national self-sufficiency to provide all the components a country needs is now an unlikely one. The speed of progress and increase in complexity as the electronics industry gets more and more sophisticated means that no one country can provide all its own needs. Even America cannot exist as a "solo" unit: last year they bought more than $£ 14$ million-worth of components from Britain and represented our second biggest market after the European free-trade area countries, whose trade with the UK was $£ 18$ million.
"Today, no one country can expect to be the leader in all techniques-which is another reason why international co-operation is necessary."

Each Component Show seems to be more successful than its predecessors, and this year there were 436 exhibitors.

The show is very much a technical one, and some of the latest developments were not obvious to the casual observer walking round from stand to stand. However, what struck us was the greater emphasis on integrated circuits both for domestic equipment and for items such as computers. Prices of established i.c.s are coming down, while new developments give the promise of simplified circuitry and construction, and eventual reduction in the price of equipment.

## PICK-UP CARTRIDGE

Acos (Cosmocord) showed a new stereo cartridge, the 104 ceramic. This is designed for the latest slim-line pick-up arms and has a weight of only 2 gm with the standard bracket. The tracking weight is 3 gm to 4 gm .
Cosmocord Limited, Eleanor Cross Road, Waltham Cross, Hertfordshire.

## CLEANING FLUIDS

Two types of aerosol cleaning fluid were shown'by Automation Facilities. "Ultraclene" is a universal general cleaner, harmless to most insulating varnishes and lacquers, which rapidly removes oil, and grease. It evaporates quickly and leaves no residue. "AF-Spray" contains ICI's Arklone P, a non-flammable highly penetrating solvent which instantly removes oils, greases, and most contaminants, without harming plastics and surface coatings.
"Ultraclene" costs 30s. for three $160 z$. aerosols, and "AF-Spray" costs 20s. for a single sample aerosol (prices are reduced for larger quantities).
Automation Facilities Limited, Oxford Avenue, Slough, Buckinghamshire.

## ELECTRONIC MULTIMETER EA113

On the Avo stand, an electronic Avometer was revealed. This has a d.c. sensitivity of $1 \mathrm{M} \Omega / \mathrm{V}$, a basic accuracy of $1.25 \%$, and may be operated up to 100 kHz . There is a centre-zero facility, and resistance measurements may be made up to $100 \mathrm{M} \Omega$.
Avo Limited, Avocet House, Dover, Kent.

## TRANSFORMERS

The Belclere Company showed a new range of miniature stabilised power supplies. These units are hermetically sealed and intended for printed-circuit mounting.

The three versions available are the P.S.2009, P.S.2012, and P.S.2020, which have outputs of $9 \mathrm{~V} 40 \mathrm{~mA}, 12 \mathrm{~V}$ 30 mA , and 20 V 15 mA respectively. The overload points in each case are at 5 mA over the rated output, and the output potentials are within $\pm 5 \%$ of nominal. Ripple is less than $500 \mu \mathrm{~V}$ r.m.s.
The Belclere Company Limited, 385-7 Cowley Road, Oxford.

## INSTRUMENTS

The universal meter TVM1070 by B.P.L. is a versatile instrument with f.s.d.s from 100 mV to 300 V d.c. and 100 mV to 300 V a.c. Centre-zero ranges are available on d.c. volts, from $50 \mathrm{mV}-0-50 \mathrm{mV}$ to $150-0-150 \mathrm{~V}$. On d.c., the input resistance is $1 \mathrm{M} \Omega / \mathrm{V}$ up to 10 V , and $10 \mathrm{M} \Omega$ above 10 V , while on a.c., it is $200 \mathrm{k} \Omega$ on ranges up to 30 V , and $2 \mathrm{M} \Omega$ on the 100 V and 300 V ranges.

The meter also measures direct current, the most sensitive range being $1 \mu \mathrm{~A}$ f.s.d., and the least sensitive 100 mA . Centre-zero direct current ranges are also a feature, from $0.5 \mu \mathrm{~A}-0-0.5 \mu \mathrm{~A}$ to $50 \mathrm{~mA}-0-50 \mathrm{~mA}$.

Three resistance ranges are included: $0-10 \mathrm{k} \Omega, 0-1 \mathrm{M} \Omega$, and $0-100 \mathrm{M} \Omega$, with mid-scale values of $150 \Omega, 15 \mathrm{k} \Omega$, and $1.5 \mathrm{M} \Omega$ respectively.

A plug-in r.f. test-probe is supplied with each meter and gives four ranges: $0-1 \mathrm{~V} ; 0-3 \mathrm{~V} ; 0-10 \mathrm{~V}$; and $0-30 \mathrm{~V}$. The frequency range is 100 kHz to 300 MHz for -3 dB points, with an input resistance of $140 \mathrm{k} \Omega$ on each range (shunt capacity, 3 pF ).

## B.P.L. (Instruments) Limited, Radlett, Hertfordshire.

## WIDE-RANGE RECEIVER

A professional receiver, the EC958, was the main feature of the Eddystone stand. This fully transistorised


The AVO Electronic Avometer EA113
 gowertul $7 \times 4$ in. speaker and four transistor one watt power amplifier plus ultia sensitive microphone Uses PP9 battery. Brand new in Makers'
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guarantee. World famous make. only $90 /-$ Post guarantee, World famous make. RA2W Gin. Ferrite Aerial Spare Cores
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 Long spindles. Midget Size BRITISH AMRIALITE




 EDGE CONNECTORS 16 way $5 /-; 24$ way $7 / 6$.
PINS 36 per packet $8 / 4$. FACE CUTXERS $\% / 6$ S.R.B.P. Board 0.15 MATRIX $2 \frac{1}{1} \mathrm{in}$, wide 6 d , per 1 in . $3 \frac{3}{2} \mathrm{in}$. wide 9d. per 1 in ; 5 in, wide $1 /-$ per 1 in . up to 17 in .
S.R.B.P. undrilled 16 in . Board. $10 \times 8 \mathrm{~m}$. $\times 4$ in., $5 / 6 ; 9 \times 7$ in., $6 / 6 ; 11 \times$ 3in., 6/6; $11 \times 7 \mathrm{nin}, 7 / 6$


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 SUB.MIN. ELECTROLYTICS. 1. 2. $4,5,8,16,25,30,50,100$ $50 \mathrm{mF} 15 \mathrm{C} 2 /-500,1000 \mathrm{mF} 12 \mathrm{~V} 3 / 6 ; 2000 \mathrm{mF} 25 \mathrm{~V} 7 /-$ PAPER $350 \mathrm{~V}-0.1 \mathrm{~T} 9 \mathrm{~d} ; 0.52 / 6 ; 1 \mathrm{mF} 3 /-2$
00V-0.001 to 0.05 9d: $0.11 /-0.251 / 8:$ $1,000 \mathrm{~V}-0.001,0.0022,0.0047,0.01,0.02,1 / 6 ; 0.047,0 \cdot 1,2 / 6$ SIL VER MICA. Close toleranoe $1 \% .5-500 \mathrm{pF} 1 /-; 560-2,200 \mathrm{pF}$ /- $2,700-5,600 \mathrm{pF} 3 / 6 ; 6,800 \mathrm{pF}-0 \cdot 01$, mtd $6 /-$ each.
TWIN GANG. "0-0", 208pF $+176 \mathrm{DF}, 10 / 6 ; 365 \mathrm{FF}$, minia ure $10 /-; 500 \mathrm{pF}$ standard with trimmers. $12 / 6: 500 \mathrm{pF}$ midget less trimmers, $7 / 6: 500 \mathrm{pF}$ silow motion, standard $9 /$; SHORT WAVE. Single $10 \mathrm{DFF}, 25 \mathrm{pF}, 50 \mathrm{pF}, 75 \mathrm{pF}, 100 \mathrm{pF}$, $160 \mathrm{pF}, 200 \mathrm{pF}, 10 / 6$ each.
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 50V RECTIFIERS. Selenium $\frac{1}{2}$ wave 100mA $5 /-$;BY10010/CONTACT COOLED $\frac{1}{2}$ wave $60 \mathrm{~mA} 7 / 6 ; 85 \mathrm{~mA} 9 / 6$.
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TT45. Push Pull Drive, 9:1 CT, 6/-. TT46 Output, OX8:1. 6/TT23/4 PAIR 10 watt Amp. Transformers and circuit 45/TRANSISTOR MAINS POWER PACKS. FULL WAVE 9 volt 500 mA Size $4 \frac{1}{2} \times 2 \frac{1}{2} \times 2$ in. Output terminals. $\quad 49 / 6$ Switched.Metal case, crackle finish. On/off switch.
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$250-0-25050 \mathrm{~mA} .6 .3 \mathrm{v} .3 .5 \mathrm{a}$. 6.3v. 1a. or 5 z . 2 a.
$350-0-35080 \mathrm{~mA} .8 .3 \mathrm{v} .3 .5 \mathrm{a} .6 .3 \mathrm{v} .1 \mathrm{a}$. or 5 v .2 a
$300-0-300 \mathrm{v} .120 \mathrm{~mA} .6 .3 \mathrm{r} .4 \mathrm{a} . \mathrm{C} . \mathrm{T} . ; 6.3 \mathrm{v}$. 2 a .
 MIDGET 220v. 45 mA ., 6.8 Bv . 2 a . $8 \frac{3}{4} \times 2 \frac{1}{2} \times 2 \mathrm{in}$

 4, 5, 6, 8. 9. 10. 12.15. 18, 24. and 30v, at 2a. 3 amp..., $1,10,12,16,18,20,2$ AUTO TRANSFORMERS 0 -ils-230v, Input/Output 60w. 18/6; 150w. $30 /-$; 500 ww . $92 / 6 ; 1000 \mathrm{w}$. $195 /-$.
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OUTLET BOXES, SURFACE OR FLUSH 4/6. BALANCED TWIN FEEEDERS 1/- Yard 80 or 300 ohms Jhrome Leä̃ Socket $\% / 6$. Phono Plugs $1 /$-. Phono Socket $1 /$. JACK PLUGS Std. Chrome $3 /-; 3-5 \mathrm{~mm}$ Chrome $2 / 6$. DIN SOGKETS Chassis 3-pin $1 / 6 ; 5$-pin $2 /$ - Lead 3 -pin $3 / 6$ 5 -pin $5 /-$. DIN PLUGS 3 -pin $3 / 6$; 5 -pin $5 /$ -
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W. 12-way, "MA 4.2 -way, or 4 D. -way, $4 / 6$ each.
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 Cone $13 \frac{1}{2} \times 3$ ing. 8 or 15 ohm models, $45 /=$ or with twin tweters, crossover and ceramic magnet, 78/6.
 8in. LOUDSPEAKER ONITS $30 \times 2 \mathrm{ohm} 2 \% / 6,15$ ohm $30 /-$ 8in. De Luxe Ceramic 3 ohm $45 /-; 150 \mathrm{hm} 501-$
8in. LOUDSPEAKER TWLN
8in. LOUDSPEAKER TWIN CONE $30 \mathrm{hm} 35 /$ -
5in. WOOFER. 8 watts max $20-10,000 \mathrm{cps}$. 8 or $15 \mathrm{ohm} 39 / 6$ OUTPUT TRANS. ELS4 etc. 4/6; MKE TRANS. 50:1, $3 / 9$


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Five Valves: ECH81, EF89,
Long, Med., Short, Gram.
12-month guarantee. A.C. 200-250v. Ferrite Aerial 5 watts
 Two pilot Lamps. Four Knobs. Aligned $\mathrm{E}^{11} 1.18 .6$ DE LUXE STEREO GRAM CHASSIS V.H.F., MW, SW $19-50 \mathrm{~m}$. SW $60-180 \mathrm{~m}$. Magic eye, push butons. $\mathbf{f} 22.10$
6 valve plus rect. Size $15 \times 7_{2}^{2} \times 6 \mathrm{in}$, high. 10

## ALL EAGLE PRODUCTS <br> SUPPLIED AT LOWEST PRICES

BARGAIN AM TUNER. Medium Wave.
Transistor Superhet. Ferite aerial, 9 volt 79/6
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trims joins for
DUXE
Titing and
bargain 4 channel transistor mizer. ad musioal highlights and sound effects to recordings musioal highlights and sound effects to recordings.
Will mix Microphone, records, tape and tuner
with separate oontrols into single output. 9 volt. BARGAIN FM TUNGR 88-108 Mc/s Six Transistor. Ready built. Printed Circuit. Calibrated slide dial f6.19.6. BARGAIN 3 WATT AMPLIFlER. 4 Trangistor
Push-Pull Ready built, with volume control. 9 v.

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Supersensitive Transistor Pocket Radio
High Fidelity Speaker Enclosures and Pians
Radio Valve Guide, Books 1, 2, 3, or 4 ea. $5 /$ No. 5 ea
Practical Radio Inside Ont
Shortwave Transistor Reoeivers
Transistor Communication Sets
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Valves, Transistors, Diodes equivalents manial Receive Foreign T. V. by simple modifcations Transistor Circuits Radio Controlled Models

## BRAND NEW QUALITY

 EXTENSION LOUDSPEAKER Handsome plastic cabinet, 20ft. lead and adaptors. For any radio, intercom, tape recorder, etc. 3 to 15 ohms. 30/-Size: $7 \frac{1}{4} \times 5 \frac{1}{4} \times 3$ in.
POST $2 / 6$
unit provides gap-free coverage between 10 kHz and 30 MHz in ten overlapping ranges.

Shown in conjunction with the receiver was the panoramic display unit, EP961, which provides a visual display of all signals which are received in a selected frequency spectrum. The spectrum covered by the display may be up to 10 MHz wide.

Further details of the receiver are given in "News and Comment" on page 241.
Eddystone Radio Limited, Alvechurch Road, Birmingham, 31.

## RECORD-CHANGER

The GC10 automatic record-changer by Garrard was unveiled for its first British showing. This unit has a one-piece control panel offering simultaneous selection of record speed and size for the $12 \mathrm{in} .33 \frac{1}{3} \mathrm{rev} . / \mathrm{min}$. and $7 \mathrm{in} .45 \mathrm{rev} . / \mathrm{min}$. settings, and its facility for playing single records automatically if required.

The unit also has a self-engaging pick-up arm retaining clip which operates automatically when the arm returns to rest after playing a single record or the last of a stack. The clip disengages automatically when the "manual" or "automatic" play control is operated.
Garrard Engineering Limited, Newcastle Street, Swindon, Wiltshire.

## TRANSFORMER SAFETY

Transformers incorporating a double-bobbin system were shown by Hinchley Engineering. These designs, to meet international safety standards, feature thermal fuses embedded in the windings to give short-circuit protection, and a secondary bobbin carrying a moulded skirt which completely surrounds the primary mains winding when the assembly is complete.
Hinchley Engineering Company Limited, Pans Lane, Devizes, Wiltshire.

## AUDIO AMPLIFIER

Much of Mullard's display this year concerned itself with the impact of integrated circuits and thyristors on domestic TV, but also shown was experimental 30 W Class D audio amplifier. The unit shown used 30 dB of feedback and had harmonic distortion of only $0.25 \%$. Previously published circuits operated at switching speeds in the 100 kHz to 200 kHz region, but the system shown operated at any desired frequency up to 2 MHz . The high speed enables smaller, cheaper, filters to be used with very low radiation levels, and gives reduced intermodulation distortion.
Mullard Limited, Torrington Place, London, W.C.1.

## RESISTORS

Muirhead were showing what they believe to be the smallest wire-wound resistor offering a range of $1 \mathrm{k} \Omega$ to $100 \mathrm{k} \Omega$ at an accuracy of $0.1 \%$ to $0.5 \%$. Another of the four precision wire-wound resistors announced is mounted in the popular TO-5 transistor can, with standard lead spacing.

All four resistors use a new type of wire which enables temperature coefficients of $\pm 5$ p.p.m. $/{ }^{\circ} \mathrm{C} \quad\left(0^{\circ} \mathrm{C}\right.$ to $100^{\circ} \mathrm{C}$ ) to be achieved as standard.
Muirhead Limited, Beckenham, Kent.

## SCOPE

SE Laboratories revealed their portable oscilloscope SM111, which may be powered from 95 V to 130 V a.c.
and 190 V to 260 V a.c., 45 Hz to 440 Hz , and from an external 24 V d.c. source.

The SM111 uses a rectangular high brightness c.r.t. with built-in graticule. The bandwidth of the two Yamplifiers is from d.c. or 3 Hz to $18 \mathrm{MHz}(-3 \mathrm{~dB})$ at $20 \mathrm{mV} / \mathrm{cm}$, depending on the setting of the d.c./a.c. switch. The timebase speeds are calibrated from $200 \mathrm{~ns} / \mathrm{cm}$ to $1 \mathrm{sec} / \mathrm{cm}$ in 21 ranges. The circuitry features solid-state design, and uses a total of eight plug-in integrated circuits.
SE Laboratories (Engineering) Limited, North Feltham Trading Estate, Feltham, Middlesex.

## VOLTAGE REGULATOR

A TO-5 linear microcircuit by SGS can be used as a series regulator, shunt regulator, switching regulator, floating high voltage regulator, or a regulated current source for both positive and negative supplies. The L123 is believed to be the first linear circuit with an $n$-channel f.e.t. directly on the chip.

SGS (United Kingdom) Limited, Planar House, Walton Street, Aylesbury, Buckinghamshire.

## METERS

A range of meters for back-of-panel mounting was shown by Sifam. The meters are clamped behind the panel without the need for the usual fixing holes, and the panel cut-out is framed by a separate matt-black diecast surround which is also held by the clamp. Three sizes are available with scale lengths of 2.2 in ., 2.75 in ., and 3.75 in.
Sifam Electrical Instrument Company Limited, Woodland Road, Torquay, Devon.


Mullard experimental hi-fi 30W class $D$ audio amplifier.

## DUAL-BEAM OSCILLOSCOPES

Two new products from Telequipment are the D51 and D54 dual-beam oscilloscopes. The D51 is a general purpose scope with a 5 in . flat-faced tube. It is suitable for use by students working on A-level courses, or studying at technical colleges.

The D54 uses solid-state design with f.e.t. input circuitry and features wide timebase range, wide bandwidth, and calibrated deflection amplifiers. The D54 is suitable for a variety of laboratory work.
Telequipment Limited, 313 Chase Road, London, N14.


MAINS MOTOR
Precision made -as and tape recordersideal also for extractor fans, blower, heater, etc. New and perfect. Snip at 9/6. Postage $1 /-$ for each ordered. 12 and over post free.


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MOTOR
Mery powerful 7 r.p.m., operates from standard A.c. mains, 29/6, plus $3 / 6$ P. \& P.


230 VOLT SOLENOID Zin. stroke, Size $24 \mathrm{in}, x$
$2 \mathrm{in} . \times 18 \mathrm{in} .14 / 6$, postage

Famons war-time "cat's eye" used dark. This is an infra-red image converter cell with a silver cacsium screen which lights up (like a cathode ray tabe)
when the electron released by electrons infra-red atrike it. A golden opportunity for some nteresting experiments. $8 / 6$ each, post $2 / 6$. Data

## MAINS TRANSFORMER SNIP

Maktng a power pack for
amplifier or other equipment? These transformers have normal mains primaries ( $230 / 240 \mathrm{v}$ ) and types (1) 12 v .500 mA . at types (1) 12 v .600 mA . a
$8 / 6 ;$ (2) 15 v .500 mA . a


PP3 ELIMINATOR. Play your pockei radio from the mains! save ts. Complete component kit eomprises 4 rectifters-mains dropper resistances, smoothing condenser and instruc
tions, only $6 / 6$ plus $1 /$ post.

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Quadruple tape on 3 in. spool giving f00ft. Of the finest quality by very famous maker. Especiadly Regular price $30 /$ - per spool. Our price ' $7 / 6$ pius $2 / 9$ p, \& p. ог 3 for $22 / 6$ poest paid.


SOIL WARMING ELEMFNT, 30 yards, heavy Pre eovering. 12/6

## BATTERY CHARGER FOR NICADS

This is in plastic case, size $5 \times 4 \times 3$ in. appros. All vired up with 3 core output lead and 3 core mains input lead. Contains mains transifmer with 40 v Also contains fall wave tridge rectifier, neon indicator, wired up with resistors to charge 2 Nicad batteries simultaneously. Churge rates of $50 \mathrm{~mA}: a: 12 \overline{\mathrm{ma}}$ respectively. Batteries up to 30 volts nay be charged. Price $39 / 6$ each, plus $3 / 6$ postage and insurance.

## VARYLITE

Will dim fluorescent or incandescent lighting up to 600 watts from full brilliance to out. Fitted on M.K. fuap plate, same place of this, or mount on surface. Priee complete in heavy plastic box with control knob $£ 3.19 .6$.

## NICAD RECHARGEABLE BATTERIES

3.6 V 500 mA size $1_{6}^{1} \times 1_{6}^{3} \mathrm{in}$. dia. type ref. DKZ 500 really powerful will deliver 1 amp for $\frac{t}{2}$ hour. Regular price $32 / 6$ our are 1 avail able, single cell 1.2 V 6/6. 5 cell 6 V 29/6.

## ELECTRIC CLOCK WITH 20 AMP SWITCH

Made by Smith's these units are as fitted to
The clock is mains driven and frequency con. trolled so it is extremely accurate. The two small dials enable switch on and off times to be accurately set-also on the left is another timer or alarm-this may be set in minutes up to 4 hours. At the end of the period a bell will sound. Ideal for switching on tape recorders. Offered at only a fraction of the regular price-new and unused only $45 /-$ leas than the value of the clock alone-
 post and insurance $2 / 9$

THIS MONTH'S SNIP

## BATTERY OPERATED TAPE DECK

With Capstan control. This unit is extremely well made and measures approx. $6 \times 5 \times 2 \mathrm{in}$. deep. Has three piano key type controls for Record, Playback and Rewind. Motor is a special heavy duty type intended for opera-
tion off $4 / 5$ volts. Supplied complete with 2 tion off $4 / 5$ volts. Supplied complete with 2 spools ready to instail. Record, Replayhead with trausistor, amplifier. Price 59/6. Post and insurance $4 / 6$.

## B $\because-1 \div 1 \div 1$

DISTRIBUTION PANELS
$J$ ust what you need for work benoh or lab. $4 \times$ 13 amp fused plugs. Supplied complete with 6 feet of heavy cable and 13 amp phug. Similar advertised at 45 . Our price $39 / 6$, plus $3 / 6$ post and insurance.


## PROCESS TME CONTROLLER

Made by smiths, motorised and mains driven, enables 15̄ circuit to be started up to 18 hours in advance and to itay on for a period from 15 minutes to 3 hours. Totally enclosed in metal box with glass front and chrome urround. 49/6 plus $4 / 6$ post and ins.

## REED SWITCH

Suitable for dozens of different applications, such as burglar alarms, eonveyor belt switching. These are simply glass encased switches which can be operated by a passing permanent magnet coil. A special buy enables us to offer these at 2/6 each, or 24/- a diozen. Suitable magnets are $1 /-$ each.

## MOVING COIL METER BARGAIN

Panel meters are always being needed and they are jolly costly when you have to buy them in a hurry-so you shonid take advantage of this offer: 2in. moving coil tush mounting meters only $9 / 6$. These are actually R.F. meters and cost about $£ 3$ each but if you don't want them for R.F. then all you have to do is to remove the thermocouple and you will have a $2-3$ ma, meter which you can

## MOTORISED CAM SWITCH

Made by the famous meter company Chamberlain and Hookham, these have a normal mains $200-240 \mathrm{~V}$ motor which Srives a ratchet wechanism so geared to give one ratchet
action per minute on a wheel with 60 teeth thus a complete action per minute on a wheel with 60 teeth thus a complete
revolition of the cam takes place in one hour. The cam revolution of the cam takes place in one hour. The caro
operates 8 switches ( 6 changeover and 2 on/off thus 480 operates 8 switches ( 6 changeover and 2 on/off thus 480
circuit changes per hour are possible). Contacts, rated at 15 amps have been set for certain switch combinations but can, no doubt, be aitered to suit a special job. Also other switch
waiers or uevices can be attached to the shaft which extends approximately one inch. 47/6, p. \& ins. 4/6.

## MAINS TRANSISTOR POWER PACK

Designed to operate transistor sets and amplifiers. Adjustable output $6 \mathrm{v} ., 9 \mathrm{v}$. 12 volts for up to 500 mA (class B working). Takes the place of any of the following batteries: PP1, PP3, PP4, PPG, PP7, PP9, and others. Kit comprises nuains transformer rectifier, smoothing and load resistor, condensers and instructions. Real snip at only $16 / 6$, plus $3 / 6$ postage.

FLEX CABLE BARGAIN
$23 / 0076$ triple core P.V.C. covered, circular, normally sold at $1 / 6 \mathrm{yd}$. Our price $23 / 0076$ triple core P.Y.C. covered, circular, $\mathbf{n}$
100 yd. coil 18.19 .6 . Post and Insurance $6 / 6$.


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INPUT 230/240v. A.C. 50/60- I OUTPUT VARIABLE 0.260 v . BRAND NEW
Keenest prices in the country. All Types (and Spares) from $\frac{1}{2}$ to 50 amp. from stock. SHROUDED TYPE
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50 amps , $£ 92.0 .0$.

PORTABLE TYPE OPEN TYPE (Panel Mounting) amp, £3.10.0. 1 amp, £5.10.0. 2 $\frac{1}{2} \mathrm{amps}$, $\mathbf{5 6 . 1 2 . 6 .}$
PORTABLE TYPE
.5 amp. portable fitted metal case, Voltmeter, lamp, switch, etc. £9.5.0
ió WATT POWER RHEOSTATAT (NEW)
available in the following values
$1 \mathrm{ohm}, 10 \mathrm{a} \cdot ; 5 \mathrm{ohm}, 4 \cdot 7 \mathrm{a}, 10 \mathrm{ohm}, 3 \mathrm{a}, \mathrm{i} 25$ ohm, 2a.; 50 ohm, 1.4 a.; $100 \mathrm{ohm}, 1$ a.; 250 ohm , . 7 a.; 500 ohm, 45 a .; 1,000 ohm, $280 \mathrm{~mA}_{\text {; }}$, 1,500 ohm, $230 \mathrm{~mA} ; \mathbf{2 , 5 0 0}$ ohm, 2 a. Diameter $3 \frac{1}{4} \mathrm{in}$. Shaft length $\frac{7}{8} \mathrm{in} .$, dia. $\frac{15}{64} \mathrm{in}$. All at $27 / 6$ each. P. \& P. $1 / 6$.
50 WATT. $1 / 5 / 10 / 25 / 50 / 100 / 250 / 500 / 1,000 / 1,500 / 2,500 / \mathrm{ohm}, 21 / \mathrm{m}$ P. \& P. 1/6.

25 WATT. 10/25/50/100/250/500/1,000/1,500/2,500 ohm, 14/6. P. \& P. $1 / 6$.

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Avaliable in red, white, yellow, black, blue and green. New 17l/ per doz. 2l-P.-A P. I
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Heavy duty type, approx. 3 lbs , pull. Price 17/6 plus 2/6 P \& $P$
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CONDENSERS $2,500 \mathrm{mfd} .100 \mathrm{v} .12 / 61 / 6$ P. \& P. $4,000 \mathrm{mfd}$, 25v. 10/-1/6 P. \& P. $4,000 \mathrm{mfd}$, 50v. 15/~ 1/6 P. \& P. $10,000 \mathrm{mfd}$. 35 v . 15/~ $1 / 6$ P. \& P.
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Input 185-250 v. A.C. Output 230 v. A.C. Capaclfy 250 watt. Attractive metal case. Fitted red signal lamp. Rubberfeet. Weight 17 lb . Price E11.10.0. P. \& P. $15 /-\frac{1}{L . T}$ TRANSFORMERS
All primaries 220-240 volts
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30, 32, 34, $36 \mathrm{v}_{\mathrm{t}}$ at $5 \mathrm{amps} . . . . . \begin{gathered}\text { Price }\end{gathered}$
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10, 17, 18 v . at 10 amps.
$6,12 \mathrm{v}$. at 20 amps .
17, $18,20 \mathrm{v}$. at 20 amps.
6, 12, 20 v. at 20 amps..
24 v . at 10 amps.
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DOUBLE WOUND VARIABLE L.T. TRANSFORMER Input 230 v. A.C. OUTPUT CONTINUOUSLY VARIABLE $0-36$ v. A.C.
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Kit of parts, including ORP12 Cad- $x_{2}$ mium Sulphide Photocell, Relay, whits Transistor and Circuit, etc., 6-12 ${ }^{2}$ volt D.C. op. price $25 /$ - plus $2 / 6$ P. \& P. ORP 12 including circult,

10/6 each, plus $1 /-\mathrm{P}$. \& P.
A.C. MAINS MODEL Incorporates Mains Transformer. Rectifier and special relay with 3,5 amp mains c/o contacts. Price inc. circuit 47/6 plus 2/6 P. \& P.

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light source with focus lens assembly and ventilate lamp housing, to take MBC bulb. Separate photo cell mounting assembly for ORP 12 or similar cell. Both units are single hole fixing. Price per pair £2.15.0. P. \& P, $3 / 6$.

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3 banks of 11 positions plus
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2 make +2 break (or, 2 c/o.).
15 amp. contacts. $230 / 240 \mathrm{~V}$, A.C. operation. Brand new. Price 22/6 plus $1 / 6$ P. \& P

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3 lbs . (post $5 / \mathrm{m}$ )
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$29 / 6$
$29 /-$


## continued from the July issue

THE meter was an expensive item, and some form of protection circuit was considered mandatory. The meter protection circuit comprises D8 D9 R43 and R44, the modus operandi being somewhat as follows. The diodes on their own do not conduct until a potential difference of 600 to 700 mV exists across them. Being connected in parallel, though oppositely phased, either one or the other will conduct irrespective of the polarity of the voltage impressed across them. This property is only required when connected into the d.c. amplifier, where the terminals can be connected into an incorrect polarity circuit. The meter requires 60 mV for f.s.d., which means a current some 10 to 12 times f.s.d. would pass through the meter before the diodes conducted. This does not represent an adequate safety margin, and so the resistors R43 and R44 were included. This means that the voltage now required for f.s.d. is 250 mV or one-third of the conduction voltage of the diodes, the measure of protection afforded being proportionally greater. The resistors could be further increased to improve the degree of protection, but we are then in danger of incurring scale non-linearity as well as a further loss in the sensitivity of both amplifiers. With the selected components, the meter has only to pass a current $\times 3$ f.s.d. or $150 \mu \mathrm{~A}$ before the diodes conduct.
The purpose of C11 is to "damp" the meter needle against constantly varying outputs, such as an audio signal from the a.c. amp and therefore provide a more easily read "average" voltage.

It also serves to slow the meter needle in its progression over the scale, so that in the event of an overload it comes to rest fairly gently against the end stop.

## Constructional Details

The "active" part of the complete instrument, the a.c. and d.c. amplifiers, are built on a printed circuit board to the dimensions and layout given in Fig. 4.

The passive parts of the instrument are the attenuators, incorporated round S1a-b and $\$ 3 \mathrm{a}-\mathrm{b}$. On the prototype, these consisted of Radiospares Makaswitch shafting assemblies. To ease the problem of connecting the various components associated with the a.c. attenuator, a spare single-pole ten-way wafer was pressed into service, this being suspen-
ded by means of appropriate spaces between the two twelve-way wafers. The wiring of these attenuators is shown in Figs. 5 and 6.
The meter scaling is in the now familiar, almost standard 1-3-10 sequence, the range resistors being chosen to suit. There is, quite clearly, no reason why any other sequence preferred by the individual constructor should not be used, the range resistors being altered as necessary.
The front panel carries the moving coil meter, and the various switches and potentiometers; the wiring of these are straightforward and are therefore not illustrated.

The complete instrument is built into a cabinet of 20 gauge aluminium to the dimensions given in Fig. 7 and held together by self-tapping screws. The cabinet, in turn, is suspended in a " U " bracket of 10 gauge aluminium by means of $\frac{1}{4} \mathrm{in}$. UNF bolts, washers and shakeproof nuts as detailed in Fig. 9.

The front panel is drilled and cut to the dimensions of Fig. 8. The legends for the front panel were drawn on white cartridge paper with red and black ballpoint pens, the red begin used only for the mV sections of the two input attenuators. This was then faced, for protective purposes, by a sheet of $\frac{1}{16}$ in. Perspex.
Construction should not be commenced until all the components are to hand, in order to allow for dimensional differences between the components used in the prototype, and those to be used by the individual constructor. Both circuits are quite stable and there was little difference between the breadboard experimental circuits and the finished article. Other forms of construction are therefore quite suitable, provided some simple precautions are observed. These consist, for the a.c. amplifier, of

## SWITCH FUNCTIONS

$$
\begin{aligned}
& \text { S1 - Range switch - d.c. } \\
& \text { S2 - On/off switch - d.c. } \\
& \text { S3 - Range switch - a.c. } \\
& \text { S4 - On/off switch - a.c. } \\
& \text { S5 - AC/DC selector } \\
& \text { S6 - Norm/rev. switch. }
\end{aligned}
$$



Fig. 4: The printed circuit board for the a.c. and d.c. amplifiers, as etched by the author. The a.c. section is on the left, the d.c. section on the right.


Fig. 5: Wiring and components associated with the d.c. input attenuator.
keeping the input stage and attenuator well screened to obviate the picking-up of hum and other extraneous signals and, for the d.c. meter, of keeping the input terminals and circuitry well isolated from each other to obviate the leakages that exist undetected and unsuspected, in many circuits. The input resistance is very high, and leakage resistances can exist, of magnitudes sufficient to upset the working of the amplifier.
As far as components are concerned, there is only one thing to remember. This is a measuring instru-


Fig. 6: The a.c. attenuator switch. The wafer numbering corresponds with that given in the circuit diagrams.
ment, the yardstick of the future. Therefore only the best components must be used; components of unknown origin, of dubious characteristics, must be ruthlessly discarded. The use of "bakelite" switches for the input attenuators is to be deprecated, as the leakage resistance between adjacent pins and contacts is low enough to adversely affect the working of the d.c. amplifier.

Only the best grade of printed circuit board should be used. When the instrument is fully and satisfactorily operational, the copper side and, if desired the

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component side, should be painted over with one of the special printed circuit board varnishes. This has the effect of insulating the circuits against the dust that invariably seems to collect and that can, in time, affect the working of the circuits.

The semiconductors used have proved to be satisfactory, and whilst it is not unreasonable to suppose that similar semiconductors will work just as well, their use has not been investigated.

It was stated earlier that it is very desirable for the transistors of the d.c. amplifier, $\mathrm{Tr} 1-\mathrm{Tr} 4$, to be in close proximity, even to the extent of being physically bonded together in a common heat sink. This latter condition, quite safe with many transistor encapsulations, is not possible with the 2 N 2484 transistors used, as the TO-18 case is internally connected to the collector lead. If these cases are physically touching, the circuit will not be damaged (provided "opposite" pairs are involved) but will refuse to work.

It is suggested that one circuit at a time be built, and checked for correct functioning before the other is built and checked. Final calibration can best be carried out when the instrument is fully completed and ready for mounting in the cabinet. Thus, the d.c. amplifier can be built and checked to see that VR1 and VR2 can satisfactorily zero the meter. Ideally, they should zero the meter at the mid-point of their travel, thereby denoting component equality. If means are at hand the hfe of Tr 1 and $\operatorname{Tr} 4$ also $\operatorname{Tr} 2$ and $\operatorname{Tr} 3$ should be equal. If zero cannot be obtained by adjustment of VR1 and VR2, the transistors if not accurately matched could be changed about. Alternatively, the values of R11 R12 and R17 R18 or R15 R14 could be altered in value. Once this is achieved, then attention can be directed to the construction of the a.c. meter.

## Test and Calibration

The a.c. meter can be roughly checked by replacing the secondary attenuator resistors by a $1 \mathrm{k} \Omega$


Fig. 7: Cabinet and " $U$ " bracket dimensions. It is recommended that all metal work is carried out in 20 siw.g. material. The "U"brackethowever, should be in 10 s.w.g. if possible.

Fig. 8: The instrument front panel fabricated in 20 s.w.g. material, preferably aluminium. The cut-out for the meter will depend upon the size of unit used.

A Holes $0.86 \mathrm{~cm}\left(3 / 8^{\prime \prime}\right)$

B Holes to suit switches
C Holes to suit terminals


For owners of a CdS exposure meter, or of a camera incorporating one, a very convenient and accurate way is illustrated in Fig. 10. In this method, an RM13 or similar 1.35 V mercury cell is used. The $330 \Omega$ resistor drops the 0.35 V leaving 1 V across the $1 \mathrm{k} \Omega$ resistor. The d.c. meter is set to 1 V f.s.d. and is connected across the $1 \mathrm{k} \Omega$ resistor and VR3 is set for f.s.d. If close tolerance resistors are used for the other ranges, these will automatically be correct.
The a.c. meter requires the use of an accurate a.f. signal generator having an output constant between some 50 Hz and 10 kHz minimum, higher if possible. The output is fed into the a.c. meter amplifier and VR4 is adjusted to give an appropriate reading on the meter at 50 Hz . In order to set TC1, the frequency is next increased to at least 10 kHz and TCl is adjusted so that the meter reading at 10 kHz is the same as that obtained at 50 Hz . The reading will be higher than the 50 Hz reading if the capacity of TC1 is excessive, lower if the capacity is insufficient. Only when the time constant of TC1 $\times$ R21 is equal to the time constant of R22 $\times \mathrm{C1}$ plus strays will the two readings be equal. In order to ensure accuracy, the higher frequency should be at least 20 times the lower frequency, and the audio generator output must be constant over the frequency range. In order to ensure absolute accuracy, the strays (capacitance) imposed by the enclosure of the circuit within the cabinet must be checked when the front panel is screwed into the cabinet. These usually cause the high frequency response to drop slightly, necessitating an increase in TCl. Accurate setting of TCl will ensure a response extending well into the multiple kilohertz region.

## NEXT MONTH IN P.W.

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10 d .
$8 / 9$

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## HI-Q!

Allowing that Mr. Floyd is entitled to his viewpoint, I feel that the letter in May's P.W. was rather harsh in its sweeping criticism. As one who works almost entirely with f.e.ts and m.o.s f.e.ts and am designing an "All-Band" "PhaseLocked" Receiver, I think my IQ is of an average level; but so far have not been upset by the content of either P.W. or P.E. which I have taken for years.
Of course many articles are "simple" and descriptive, but many are of a reasonably advanced nature as well. This is how it should be in a magazine catering to such a wide gap between newcomers and the more experienced readers. As for being too descriptive, even the advanced reader who often tries a dozen or more projects each month -simple and otherwise-can save time by broadly following the basic layout as illustrated in the articles, instead of starting from the circuit alone.
If articles and projects of an advanced nature are wanted, there are many "specialist" magatinss published which contain them. I personally take 10 radio magazines each month but still find Practical Wireless a good "threebob's worth."-M. J. Shepherd (Essex).

In reply to M. Floyd's letter I would like to say that the so called "spoon-feeding" of readers is quite often just.
I am quite keen on radio but as yet I have not indulged in it enough to fully understand the full principles of it, and I find the description in many articles very useful.
I would suggest that either M. Floyd realises that there are people like me who benefit from "spoonfeeding" or he tries to do better and make a success of it.P. Yates (Staffs.).

In reply to M. Floyd on the subject of articles published in P.W. and P.E. all I can say is that if he does not like the articles which are printed then he does not have to buy the books.

I think myself that most of the articles printed are varied and suit all tastes. After all there are not
many monthly radio magazines on sale so you really have to cater for beginners as well as those who can undertake more ambitious projects.

As to spoon-feeding the readers I agree to a slight degree that there is quite a bit of emphasis on the way projects are constructed, but to those who don't want to build up a project using the construction details they can use the construction details as a guide line and proceed from these - S. R. Cole. (Birmingham).

## Write your own

As a reply to Mr. Floyd's letter, I regard his attitude as one of entire selfishness. I am sure that there are many other people like myself who prefer plodding along to streaking straight to the uttermost limits of radio success, which Mr. Floyd seems to have evidently accomplished.
Although a novice I have had some success in transistors and still prefer Practical Wireless and Practical Electronics in their old and well loved forms. There seems to be plenty to suit all tastes at the moment; and if Mr. Floyd thinks it is not intellectual enough he should consider one of the main purposes of such magazines, which, surely is to encourage more people to join in the hobby. If the magazines were to become more intellectual no raw novice or anyone with just a casual interest would be able to understand a word. I suggest that he either designs his own circuits, or, even writes his own magazine! - R. Heeley (14) (Sheffield).

## Doo wot?

Dere Sur,
I bet that that Mister Floyd of Barks iss two lazi too mak isself a whyless set. Yores trooly, A Barkshire Moron.
[And on that point we must close the correspondence on this subjectEditor.]

## Heat treatment

In the April issue of Practical Wireless, Mr. P. Hamley writes of the heat treatment of silver steel. He says that the easiest way of tempering is to heat away from the cutting edge until the straw colour
reaches this edge. This is very easy with, say, sections over $\frac{8}{8} \mathrm{i}$ in. dia., but on sections of say $\frac{1}{8} \mathrm{in}$. dia. or less, e.g. for small pin punches, the colours will run too fast for the man with little or no experience, to see. I find that if the punchis placed on a steel plate, which is then heated, the conductance between the two is limited, and the tempering colours will easily be seen, as they will run slowly.
This method also applies to larger sections when heating over a coal fire.
This method was shown to me by a very experienced blacksmith during my apprenticeship.-P. G. Howson (Preston, Lancashire).

## Pleasing to the eye

Recently I have been experimenting with various materials from this point of view. Many materials have come to my attention, and these following notes may, I hope, prove useful to others.
Perspex can be shaped somewhat more easily than aluminium, although it is best to drill it at a fairly low speed. Various finishes can be applied, polished, satin, or an effect something like milled metal can be obtained by rubbing in small circles with a very fine emery paper. An added advantage is that it is semi-transparent, and therefore pilot lights, etc. need not be mounted through the material.

Leather cases can be obtained very cheaply from ex-govt. sources and are usually in good condition. Many of these are sufficiently rigid not to need any additional stiffening, although with some a light framework may be advisable to support component boards, etc.
Plywood makes strong rigid boxes, as long as the corners are reinforced, and looks extremely good if sanded and coated with polyurethane, or painted with "hammer" finish paints, providing the surface is sealed with a midgrey undercoat.
Aluminium foil can be stuck on the inside of all these to provide r.f. screening, and in the case of Perspex, also enhances the colour of the material.
Amateur radio has suffered too long from the "Tony Hancock" image, let's make a start on changing it with brighter cases.C. Warwick (Birmingham, 16).

##  puse arruts operartion I. J. KAMPEL  PART 3: THE MONOSTABLE FAMILY

IN the past two articles on the subject of pulse circuits, saturation switching and various forms of multivibrator have been discussed. We shall now discuss the monostable family of circuits, which, although closely related to the multivibrator family, are at the same time distinctly different.

The multivibrator oscillates between its two quasistable states without any external stimuli, whereas the monostable requires external influence to change states. It has one stable state and one quasi-stable state, and with no external stimuli will continue to rest in the stable state. Upon the application of a pulse of the right sense, the circuit will "flip" into its quasi-stable state for a predetermined period of time, to then "flop"' back into its stable state. Hence the monostable is often referred to as the flip-flop.

The input pulse must be long enough for the circuit to switch, but once removed, the circuit will not return to the stable state until the programmed time period has elapsed. Uses of the flip-flop are in pulse shaping-a trigger pulse of any shape will deliver a square-wave output pulse; pulse amplification-a small pulse will give maximum output pulse; and as a delay-if a following circuit is triggered from the rear edge of the output pulse. The flip-flop can be useful also as a buffer trigger stage-where an input pulse in not long enough to trigger a following circuit, the flip-flop will provide the longer pulse for the shorter input pulse. The flip-flop can act as a reset in this mode, where a short trigger must cause a longer reset action, or the flip-fiop may simply be used to provide an indication of long time duration upon application of a rapid triggering pulse.
The multivibrator, or astable circuit, may be made monostable by replacing one of the capacitive couplings be a resistive coupling, and this is shown in Fig. 3.1 if C 2 is ignored for the moment. It will be seen that


Fig. 3.1: Simplest monostable with single supply.
resistor R3 provides base bias for $\operatorname{Tr} 2$ as long as $\operatorname{Tr} 1$ is in the OFF state, since then the top end of this bias resistor will be at line potential, $+V_{\mathrm{cc}}$. In the stable state, however, Tr 1 is on, and since it is driven into saturation, $V_{\mathrm{C}_{1}}=V_{\mathrm{CE}} \mathrm{Sat} \simeq 0 \cdot 1 \mathrm{~V}$. There is thus not enough voltage to allow Tr 2 to switch on and this transistor remains off. R1 programmes sufficient base current in Tr 1 to ensure that this transistor is normally in saturation, and with $V_{\mathrm{B}_{1}} \simeq 0.7 \mathrm{~V}$, the normal $V_{\mathrm{BE}}$, and $V_{\mathrm{C}_{2}}=V_{\mathrm{ec}}$, capacitor Cl charges to line potential ( $-V_{\mathrm{BE}_{1}}$ ).

To switch off Tr1, since this transistor is in saturation, sufficient triggering current must be made available to remove the stored charge in the base region, and the coupling capacitor C3 must be large enough to ensure this, while the trigger pulse must be longer than the switching time. When a negative pulse is applied to Tr1 base, $\operatorname{Tr} 1$ is cut off, its collector rising to line potential, thus turning on Tr 2 as base bias is now provided through resistor $\mathrm{R} 3 . \mathrm{C} 2$ is in fact a speed-up capacitor, and provides additional current during switching to drive Tr 2 hard into saturation, this current reducing after the initial transient until, with C2 charged, only the current provided by R3 flows through Tr2 base, this being $I_{\mathrm{B} 2} \mathrm{sat}(\mathrm{min})$ to reduce power dissipation. The subject of speed-up capacitors was dealt with in Part One of this series.

When $\operatorname{Tr} 2$ switches on, $V_{\mathrm{C}_{2}}$ drops to the level $V_{\mathrm{CESat}}$, i.e., nearly ground potential, and with Cl charged to approximately $V_{\text {ec }}$ volts, $\operatorname{Tr} 1$ base is taken down to - Vec volts. When the input pulse which drove Tr2 base slightly negative is removed, C 1 keeps the base negative. This capacitor charge will gradually decay, however, just as in the case of the multivibrator, and in fact Cl now tries to charge in the reverse polarity up to the line voltage through R1. Eventually, when Trl base has gone from its negative bias to about $+0.7 \mathrm{~V}, \mathrm{Tr} 1$ switches on again, the falling collector potential cuts off the base bias to $\operatorname{Tr} 2$, and the circuit then goes back to its stable state until another trigger pulse disturbs it.

The characteristics of output $B$ in this circuit are similar to those discussed in the case of the multivibrator, and there is the same limitation in line voltage. That is to say a slow rising edge will be seen at output B, and since $\operatorname{Tr} 1$ base is taken to the potential of the line voltage in the negative direction, $V_{\text {ce }}$ should not exceed the maximum reverse bias rating of the emitter-base of the transistor used for Tr 1 . It is pointed out that Tr 2 base will not go to this negative potential without capacitor C 2 , but with C 2 , when Tr 2 is cut off, the speed-up capacitor can cause $\operatorname{Tr} 2$ base to be taken negatively beyond earth potential which, incidentally, also helps the turnoff time. For low frequency operation this enables a saving in components as will be seen later. For the cir-

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cuit as it stands in Fig. 3.1, the line voltage should not exceed the maximum $V_{\text {EB }}$ for the transistors (usually about 5 V for silicon transistors).

The circuit is basically similar for $\mathrm{p}-\mathrm{n}-\mathrm{p}$ transistors, the chief difference being that the reference rail will be of opposite polarity.

The time the flip-flop spends in its quasi-stable state may be determined approximately from $\mathrm{t} \simeq 0 \cdot 7 . \mathrm{C}_{1} \cdot \mathrm{R}_{1}$, and the derivation of this formula was given in Part Two of this series.

Since the speed-up capacitor is small, if an output is taken from A an improved rising edge may be achieved, this output $180^{\circ}$ out of phase with output B.

The chief disadvantage of the circuit of Fig. 3.1 is that in high frequency operation, the stored base charge is not always removed sufficiently rapidly, and the leakage current through $\operatorname{Tr} 2$ collector may be too high if the circuit has to operate in high ambient temperatures. To reduce this current it is necessary to apply negative bias to $\operatorname{Tr} 2$ base. The simplest way this may be achieved is with a negative supply as well as the normal positive supply, the former being only a low voltage supply, usually -1.5 V (for $\mathrm{n}-\mathrm{p}-\mathrm{n}$ circuit, +1.5 V for $\mathrm{p}-\mathrm{n}-\mathrm{p}$ ).

Figure 3.2 shows this, where R4 and R5 act as a potential divider between $V_{\mathrm{CE}_{1}}$ sat and $-V_{\mathrm{bb}}$, and these may be so arranged that Tr2 base is always negatively biased. Operation of this circuit is just as previously described for Fig. 3.1, except that when Trl cuts off, the potential divider of R4 and R5 now sets a new base voltage for Tr 2 of approximately +0.7 V , set between the potentials of $+V_{\mathrm{cc}}$ and $-V_{\mathrm{bb}}$.


If a line voltage larger than the maximum reverse $V_{\mathrm{EB}}$ is to be used, the method previously described with the multivibrator may be employed. By placing diodes in the emitter line of the transistors, as shown in Fig. 3.3, the greater breakdown voltage of the diodes protects the emitter-bases. For low frequency operation it may not be necessary to employ a speed-up capacitor, and if this is done, diode D2 may be omitted since the potential divider formed by R4 and R5 ensures that the base only goes negative by the programmed amount, which should, of course, be less than the maximum reverse rating.

It is frequently not convenient to use two supply lines, and reverse base bias for cut off can be achieved with a single line in a number of ways. By lifting the emitters with diodes the situation is improved, and by lifting them further with say voltage-dependent resistors to just over 1V, potential dividers may be used down to the earth rail.

The voltage-dependent resistor, for those not familiar with it, may be regarded as a low current, low voltage reference diode.


Figure 3.4 shows an alternative method for lifting the emitters enough to allow a potential divider to be used. Resistor R7 is used by both transistors for their current supply, and if the saturation currents of both transistors are made the same, the current through R7 will remain substantially constant throughout the circuit's operation, since either one or the other of the transistors will draw this saturation current. $V_{\mathrm{x}}$ may thus be regarded as constant. Now the sense of the output at A may be wrong for some applications, or perhaps two outputs $180^{\circ}$ apart might be required. In such a situation, a fast rising edge at output B is required, and this should be slightly faster than that at A if the diode coupling resistor method is employed, since C2 must have some effect on output A, however small.


Fig. 3.4: Modified monostable with single supply and both edges fast; for high voltage rail.
For those readers who may not have read the description of how the diode resistor coupling operates in multivibrator circuits, it will be explained again in the case of this monostable. Assume that initially Tr1 is in the ON state, Tr 2 in the OFF state. Now $V_{\mathrm{C}_{1}}=$ $V_{\mathrm{CE}_{1}} \mathrm{sat}+V_{\mathrm{F}}+V \mathrm{x}$, and $V_{\mathrm{B}_{2}} \simeq \frac{V_{\mathrm{C}_{1}} \cdot R_{6}}{R_{5}+} \frac{R_{6}}{R_{6}} V_{\mathrm{B}_{2}}$ is made $-v e$, but less than $-V_{E B}$ max. It might be

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simpler here to consider some specific values, so if $+V_{\mathrm{cc}}=10 \mathrm{~V}$ and in the ON state, $V_{\mathrm{C}_{1}}=2.8 \mathrm{~V}$, with $V_{\mathrm{x}}=2 \mathrm{~V}$, we might make $V_{\mathrm{B} 2}=+1 \mathrm{~V}$, that is to say 1 V less positive than the emitter, or a 1 V reverse-bias on $\operatorname{Tr} 2$ emitter-base, holding $\operatorname{Tr} 2$ hard off. Now a negative input pulse through C 3 of say 2 V amplitude will turn $\operatorname{Tr} 1$ off, $\operatorname{Tr} 1$ collector rising to 10 V , carrying, via the potential divider, $\operatorname{Tr} 2$ base to 2.7 V , thus switching on Tr 2 . Before this switching operation, when Tr 1 base was at about 3.4 V , and diode D2 reverse biased, capacitor Cl will have charged to the potential $10-$ $3 \cdot 4=+6 \cdot 6 \mathrm{~V}$. When Tr 1 collector rises to 10 V bringing on $\mathrm{Tr} 2, \mathrm{Tr} 2$ collector falls to about $+2 \cdot 8 \mathrm{~V}$, thus taking Tr1 base down to $2.8-6.6 \mathrm{~V}=-3.8 \mathrm{~V}$.

C 1 then begins to discharge, and finally charge in the reverse polarity until $V_{\mathrm{B}_{1}}$ reaches about +3.4 V , switching on Tr1 again. Now Tr1 collector bottoms, and Tr 2 collector rises towards the 10 V rail. Without the diode D2, capacitor C1 would normally be connected directly to $\operatorname{Tr} 2$ collector, and initially has a potential of $3.4-2.8=0.6 \mathrm{~V}$ across it, and this voltage would slow the collector up in its rise towards the rail, since the capacitor must charge to the rail potential. Diode D2 acts as a gate, and with the anode at the capacitor potential, when the collector rises towards the +ve rail, the diode goes into reverse bias, blocking off the effect of C 1 to the collector, so allowing the collector to rise rapidly towards the rail, giving the improved rise time desired.
Diodes D1 and D2 serve to protect the transistors in cases where a line voltage higher than in the example taken is used. If the maximum reverse emitter-base bias is -5 V , in the example, it was seen that this was not exceeded. C2 is of course a speed-up capacitor.

The circuit of Fig. 3.5, instead of triggering from the negative edge of the trigger pulse, triggers from the positive edge, and is suitable for narrow pulse width inputs. A positive pulse input is passed by D1 and cuts on Tr 2 , which is normally held off in the stable state by the low potential of $V_{\mathrm{CE}_{1}}$ sat. C 1 will be fully charged, and take $\operatorname{Tr} 1$ base negative as $\operatorname{Tr} 2$ switches on, discharging through R1 until regenerative switching occurs and the circuit flops back to the stable state.


Fig. 3.5: Monostable for narrow trigger pulse.
The circuit of Fig. 3.6 might be triggered from a multivibrator set up as a pulse generator, and be also capable of external triggering. Tr 1 is ON in the stable state, and with only about 0.1 V at Tr 1 collector,

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Fig. 3.6: Pulse generator element.
with voltage to be dropped by both D6 and R6 before Tr 2 may switch on, it is of course in the OFF state. A negative input pulse switches Tr 1 off and causes $\operatorname{Tr} 2$ to go into conduction, however, in this modified circuit, while $\operatorname{Tr} 2$ collector drops fast towards earth potential, it does not go as low as $V_{\text {CE }} s a t$. This is prevented this time by diode D4 coming into forward conduction, the point $V_{\mathrm{x}}$ being held at a little over a volt by a voltage-dependent resistor. $V_{\mathrm{C}_{2}}$ is thus stopped just short of saturation, and in this way the base does not become flooded with minority carriers as it does when saturation occurs. The diode clamp allows the collector to go as low as possible but just prevents saturation. When this transistor is to be switched off, there is not such a large stored base charge to remove, and for high frequency operation, better switching times can be thus achieved.
Apart from this saturation prevention clamp on both transistor collectors the circuit operates in the normal manner with a diode resistor coupling to improve rise times to the optimum. As a matter of interest, if the v.d.r. is replaced by a higher voltage zener diode and diodes D3 and D4 reversed in polarity, they may be used to act as clamps in the reverse direction. In this mode they prevent the collectors rising to the line potential, restricting them to about 0.7 V greater than the zener voltage.
In the circuit of Fig. 3.6 adjustment of VR1 alters the length of the quasi-stable state.
Speed-up capacitors have been used in nearly all of the monostable circuits to be described, and the calculation of the precise value for a speed-up capacitor is quite involved, and is in any case subject to some error in practice. It is quite normal practice to select optimum values by trial and error in a particular circuit, the optimum capacitance being when the cleanest pulse is obtained at the output, i.e., fastest edges. This capacitor will usually be of the order of hundreds or thousands of pFs. As such, it does not present any particular danger in terms of reverse voltages to transistors' emitter-base as it will rapidly discharge on switching, causing only a small spike. Even momentary excess of voltage ratings is not to be recommended, however, for reliable service, particularly if high repetition rates are to be encountered.

In part four of this series, the family of bistable circuits will be discussed, and here it will be seen that the situation is somewhat complicated in the necessity of using a steering circuit for the input pulses. The Schmitt Trigger, complementary trigger, and a triggered ramp generator will also be discussed.


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