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COMMUNICATION RECEIVERS TRIO
MODEL 9R-59DE Brief spec.: 4 band receiver covering s50 Kc/s
ho $30 \mathrm{Mc} / \mathrm{continuous}$
and electrical band spread and electrical band spread
on $10,15,20,40$ and 80 metres. 8 yalve plue 7 dinue circuit. $4 / 8$ ohm Special features: gsB BFO - 8 meter - Sep
 frequency $455 \mathrm{Ke} / \mathrm{s}$ - Aldin output $1-5 \mathrm{~W}$ - Variable RF and AF gain controls. For use on $115 / 250 \mathrm{~V}$ A.C. Mains. Beautifully deqigued control layout finished in light grey with
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Lasky's Price $£ 36.15 .0$ Carriage and Packing 12/6
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Brief spec.: Covers all the amsteur bands in 7 separate ranges between 3.5 and $29.7 \mathrm{Mc} / \mathrm{s}$. Circuit uses 7 valves, 2 transistors and 5 diodes plus 8 crystala; output 8 and 500 ohm and 500 ohm phone jack. Special features: Cryatal controlled oscillator Sariable BFO
YFO AVC ANL $\$$ meter SSB-CW Stand-by switch VFO AVC ANL \& meter S8B-CW - Stand-by switch - Apecial double gear thal drive with direct reating down to 1 kHz Remote cont rol gocket ior connection to at transmiter. Audio output watt in dare ong Calinet size $7 \times 13 \times 10 \mathrm{in}$. Weight 18 ibs . Fully guaranteed, complete with instruction manual and service data.
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Type KR-65 $3 \frac{3}{3} \times 3 \mathrm{in}$
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100 mA
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put available for feeding tuning meter． put available for feeding tuning meter．toutput
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$250-0-250 \mathrm{v} .100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v} .2 \mathrm{a}, 6.3 \mathrm{v} .1 \mathrm{a}$.
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$$
\begin{aligned}
& 350-0 \cdot 350 \mathrm{v}, 100 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}, 4 \mathrm{a}, 0-5 \cdot 6 \cdot 3 \mathrm{v}, 3 \mathrm{a} . \\
& 350-0-350 \mathrm{v}, 150 \mathrm{~mA}, 6 \cdot 3 \mathrm{v}, 4 \mathrm{a}, 0-5-6 \cdot 3 \mathrm{v} .3 \mathrm{a} .
\end{aligned}
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Decibels -40 to $1 \cdot 2 \mathrm{Mc} / \mathrm{s}$. Decibels - 40 to
+50 dB . Supplied brand tow complete with leads and instructions. Opera. tion 230V. A'.C. 217.10.0. Carr. $5 /$



| 2-WAY RADIOS |  |
| :---: | :---: |
| Super qualit | Brand new |
| and guaranteed. |  |
| 3 transistor | 26.15 .0 pr . |
| 4 transistor | ¢6.19.6 pr. |
| 5 transistor | 87.19 .8 p |
| 6 trausistor | £8.12.6 |
| 6 transiator De Luxe |  |
|  | \$12.10.0 |
| 10 transistor | 222.10.0 |
| sistor 500 | 281.10 .0 |
|  |  |
|  |  | These carnot be operated in U.K.

NOMBREX TRANSISTORISED TEST EQUIPMENT All Post Paid with Bettery


Model 22. Power Supply 0-15V DC 814.10 .0 Model 30 Aulio Generator. $\$ 18.10 .0$ \begin{tabular}{lr}

Model 31. R.F. Signal Generator. \& | \&12.10.0 |  |
| :--- | :--- |
|  |  |
| 10.100 |  | <br>

\hline
\end{tabular}

 Model 33. Inductance Bridge. Model 66. Luductance Bridge Model 61. Power Supply.

## COSSOR DOUBLE BEAM OSCILLOSCOPES

£20.0.0
\&18.0.0 ع6.10.0

EVERSHED VIGNOLES SERIES II 500 VOLT MEGGERS. lerfect condition \&\&1. CT. 58 SIGNAL GENERATORS. 8-9-15-5 and $20-300 \mathrm{Mc} / \mathrm{s}$. Output $1 \mu \mathrm{~L}-100 \mathrm{mV}$ Mains
operated. Perfect condition less charts. 212.10.0. Carr. 15/

WS. 88 TRANS/RECEIVERS. A and B sets available. Complete with valves. $39 / 6$ each.

NO. 10 MICROPHONE AND HEADSET. Moving coil Accessory for 19 set. Cnused.

## ARF-100 COMBINED AF-RF SIGNAL GENERATOR



AF. SINE WAVE 20-200,000 c/a.
8quare wave $20-$

30000 , $\begin{array}{lll}\text { 8quare wave } & 20- \\ 30,000 & \mathrm{c} / \mathrm{s} . & 0 / \mathrm{P}\end{array}$ | 30,000 c/s. O/P |
| :--- |
| HIGH IMP. 21 V |
| $\mathrm{P} / \mathrm{P} 600$ | $\mathrm{F} / \mathrm{P} 600 \Omega 3-8 \mathrm{~V}$ P/P.

$\mathrm{T} \mathbf{F} / 100 \mathrm{~K} / \mathrm{B}-300$ TF $100 \mathrm{Kc} / \mathrm{B}-300$
$\mathrm{Mc} / \mathrm{s}$. Variable R.F. attenuation int/ext, modulation. Incorporates dual purpose meter to monitor AF output and \% mod. on R.F. 220/240V A.C.
e27.10.0. C8rr. $7 / 6$.

TE-20RF SIGNAL GENERATOR


TE22 SINE SQUARE WAVE AUDIO GENERATORS


| First grade quality American tapes. |  |  |  |
| :---: | :---: | :---: | :---: |
| Brand new. Diveount on quantities. <br> 3/6 |  |  |  |
|  |  |  |  |
| 3tin. 600ft . T.P. mylar . . . . . . . . . . . . . . $10 /-$ |  |  |  |
| 5 in. |  |  |  |
| 5 l ( 900ft. L P. acetale . . . . . . . . . . . . . 10/- |  |  |  |
| Sin. 1,2001t. D.P. mylar . . . . . . . . . . . . . 15/- |  |  |  |
| $5 \mathrm{Sin}. \mathrm{1,800ft}. \mathrm{T.P} .\mathrm{mylar} \mathrm{}. \mathrm{}. \mathrm{}. \mathrm{}. \mathrm{}. \mathrm{}. \mathrm{}. \mathrm{}. \mathrm{}. \mathrm{}. \mathrm{}. \mathrm{} 32 /$. |  |  |  |
| $5 \frac{3}{1} \mathrm{in}$. 1 | 1,200ft. L P. acetat |  |  |
| 5isin. 1,200ft. L.P. my |  |  |  |
| 5 gin in 1,800ft. I).P. mylar |  |  |  |
|  |  |  |  |
| $7 \mathrm{in} .1,200 \mathrm{ft}$. std, mcetate ............... $12 / 6$ |  |  |  |
| Tin. 1,800ft. L.P. acetate . . . . . . . . . . . . 15/- |  |  |  |
| 7in. 2,400ft. D.P. mylar . . . . . . . . . . . . . .25/- |  |  |  |
|  |  |  |  |
| $7 \mathrm{in} .3,600 \mathrm{ft}$. T.P. mylar . . . . . . . . . . . . $45 /$ |  |  |  |
| Postage 2/-. Over 23 post paid |  |  |  |
| TAPE CASSETTES <br> C60-60 minutes . . . . . . . . . . . . . . . . . . . . $12 / 6$ |  |  |  |
|  |  |  |  |
| C90- | 90 minutes |  |  |
| Over |  |  |  |
| EVERSHED VIGNOLES SERIES II 500 |  |  |  |
| VOLT MEGGERS. lerfect condition 281. |  |  |  |
| - | -10.- |  |  |
| CT. 58 SIGNAL GENERATORS. 8-9-15-5 and |  |  |  |
| $20-300 \mathrm{Mc} / \mathrm{s}$. Output $1 \mu \mathrm{~V}-100 \mathrm{mV}$. Mains operated. Perfect condition less charts. |  |  |  |
|  |  |  |  |
| 212.10.0. Carr. 15/. |  |  |  |
| WS. 88 TRANS/RECEIVERS. A and B sets available. Complete with valves. $39 / 6$ each. P. \& P. 4/6. Acceasories available . |  |  |  |
|  |  |  |  |
|  |  |  |  |
| No. 10 MICROPHONE AND HEADSET. Moving coil Accessory for 19 set. Lnused. 15/-. P. \& 1'. 4/-. |  |  |  |
|  |  |  |  |
|  |  |  |  |
| DUBILIER NITROGEL CONDENSERS. Brand new. 8 mfd. 800V. 8/6. P. \& P. 2/-; 2 infd. 5,000 V., 42/6. P. \& P. 5/-, |  |  |  |
|  |  |  |  |
|  |  |  |  |
| LUCAS 20/0/20 AMMETERS. Brand new boxed. Suitable car/motorcycle. 12/6. P. \& P. 2/-. |  |  |  |
|  |  |  |  |
|  |  |  |  |

Type 1035. General purpose. A.C. Coupled
Type 1049. L.F. D.C. Cotupled. $£ 35$ each Carr. 301

## LELAND MODEL 27 BEAT

 FREQUENCY OSCILLATORS $0-20 \mathrm{Ke} / \mathrm{s}$. Output 5 K or 500 ohms. 200/25 V. A.C. offereci in excellent condition
## GEM PANEL WMETERS

Send S.A.E. for full lista. Other ranges a vailable. Please inolude postage


Type MR.38P. $121 / 82 \mathrm{in}$. square ${ }^{\text {Pronts }}$

| A | . $87 / 6$ | 750 mA |
| :---: | :---: | :---: |
| $50-0-50 \mu \mathrm{~A}$ | .35/- | 1 amp |
| $100 \mu \mathrm{~A}$ | . $35 /-$ | 2 amp |
| 100-0.100 AA | .32/6 |  |
| $200 \mu \mathrm{~A}$ | .32/6 | 10v. D |
| $500 \mu \mathrm{~A}$ | .37/6 | $20 \mathrm{~V} . \mathrm{b}$. |
| 500-0-500 A A | .25j- | 50 v . $\mathrm{D} . \mathrm{C}$ |
| 1 mA | .25]- | 100V. D. |
| ${ }^{1}$-(1)-1mA | .25]- | $150 \mathrm{~V} .10 . \mathrm{C}$ |
| 2114 | .25/- | 300 v .1 ce |
| 5 ma | .251- | $500 \mathrm{~V} . \mathrm{D} . \mathrm{C}$. |
| 10 mA | 251- | 750 V. D.c. |
| 20 mA | 251- | 15v. A.C. |
| 50 ma | .25)- | 50V. A.C. |
| 100 mA | .251- | 150V. A.C. |
| 150 mA | .251- | 300 V. Ac. |
| 200 mA | 251- | 500 V . A. |
|  | .251- | S meter |
|  |  | S |

Type Mr.45P.

## $60-0-50 \mu$

 $100 \mu \mathrm{~A}$ $1000-10-100$ $500 \mu \mathrm{~A}$ $\operatorname{limA}_{\operatorname{mim}}$10 mA
100 mA

100 mA . | 1 aup. $. . . . . . . .27 / 8$ | 10 anp. A.C.". $27 / 6$ | 20 аmp. |
| :--- | :--- | :--- | 30 amp. A.C. $27 / 6$

Type MR.52P. 20/6, square fronts $50-0-60 \mu \mathrm{~L}$
$100 \mu \mathrm{~A} .$.

CLEAR PLASTIC METERS
$5 \mathrm{~mA} \ldots$.
$10 \mathrm{~mA} \ldots$
$50 \mathrm{~mA} \ldots$
100 mA.
500 mA.
1 amp.
5 amp.
$10 \mathrm{~V} . \mathrm{B} . \mathrm{C}$
$20 \mathrm{~V} . \mathrm{D.C}$
$50 \mathrm{~V} . \mathrm{D} . \mathrm{C}$
$.87 / 6$
$.37 / 6$
.376
$.37 / 6$
$.37 / 6$
$.37 / 6$
$.37 / 6$
$.37 / 6$
$.37 / 6$
 $.37 / 6$
$.37 / 6$
$.37 / 6$
$.39 / 6$
$.59 / 6$
$.37 / 6$
$.37 / 6$
$.37 / 6$
$.37 / 6$
$.87 / 6$

Tgpe MR.85P. $41 \mathrm{in} . \times 4$ in. fronts. $50 \mu \mathrm{~A} . .$. $100 \mu \mathrm{~A}$ $100-0 \cdot 10$ $500 \mu \mathrm{~A}$ $500 \mu \mathrm{~A} \cdot \mathrm{b0} 0 \mu \mathrm{~A}$ ${ }_{1-0-1 m A}$ 5 mA . 10 mA
50 mA
100 mA 100 mA . 1 amp.
5 amp.

$50 \mu \mathrm{~A}$
$50.0-50 \mathrm{CA}$ $100 \mu \mathrm{~A}$ $100 \cdot 0-100 \mu \mathrm{~A}$
$500 \mu \mathrm{~A}$


TE-51. NEW 20,000 $/$ / VOLT MULTIMETER with overioad protection and
mirror scale, $0 / 6 / 60 / 120 /$ 1,200v. A.C. 0/3/30/60/3001 $600 / 3,000 \mathrm{v}$. D.C. $0 / 60 \mu \mathrm{~L} / 12$ 300 mA . D.C. $0 / 60 \mathrm{~K} / 6 \mathrm{meg}$ ohm. 85/-, P.\& P. 2/6.


MODEL 250J. 2.000 Q.P.V. $\quad$ O/ $10 / 50 / 500$ 2,500 ₹. D.C. O/10/50/ $\begin{array}{lll}\text { Meg. } \Omega \text {. } 0 / 250 & \mathrm{~mA}\end{array}$ 49/8. P. \& P. 2/6

MODEL AS-100D 100K $\Omega$ / VOLT bin., mirror scale. Built-in meter
protection. $0 / 3 / 12 / 60 / 120$ 1300/600/1,200 v. D.C 0/6/30/120/300/600 v 12 Amp. $0 / 2 \mathrm{~K} / 200 \mathrm{~K} / 2 \mathrm{M}$ $12 \mathrm{Amp} .0 / 2 \mathrm{~K} / 200 \mathrm{~K} / 2 \mathrm{M}$ \&12.10.0. P. \& P. $3 / 6$.



NEW MODEL $500 \quad 30,000$ MODEL PT 34 1,000 $500 / 1,000 \mathrm{v}$. A.C. D. $0.011 / 100 / 500 \mathrm{~mA}$ D.C. $0 / 100 \mathrm{~K} \Omega 39 / \mathrm{t}$.
 P. \&. P. 1/6.


MODEL TE-10A. 200k $\Omega$ MODEL TE-10A, 200k $\Omega$
Volt $5 / 25 / 50 / 250 / 500 / 2,500 \mathrm{v}$ Volt $5 / 25 / 50 / 250 / 500 / 2,500$
D.C. $10 / 50 / 100 / 600 / 1,000$ D.C. $10 / 50 / 100 / 600 / 1,000$
A.C. $0 / 50 \mu \mathrm{~A} / 2 \cdot 5 \mathrm{~mA} / 250 \mathrm{~mA}$ D.C. $0 / 6 \mathrm{~K} / 6$ meg. ohm. -20 to +22 dB . $10 \cdot 0,100 \mathrm{mFd} .0 \cdot 100-0 \cdot 1 \mathrm{mFd}$. 69/6. P. \& P. $2 / 6$.

## LAFAYETTE LA-224T TRANSISTOR STEREO AMPLIFIER <br> 

LAFAYETTE LR-500T

 4, 8 or 16 ohms plus convenient output for tor direct stereo taping. 9 verastile controls. Responge $22-22,000$ cpe $\pm 1 \mathrm{~dB}$. H.D. less than $1 \%$. Brushed sluminium, gold anodised extruded front panel. Simulated operation. 247.10.0. Carr. 10\%.


## BAKELITE PANEL METERS

| A | Type MR.65. 3in. square Ironts. |  |  |
| :---: | :---: | :---: | :---: |
|  | ${ }^{2} 5 \mu \mathrm{~A}$. . . . . . . 6776 | 500mA . . . . . . $32 / 6$ | 30V. A.C.* . . $32 / 6$ |
|  | $50 \mu \mathrm{~A}$. . . . . . . $45 /-$ | $1 \mathrm{amp} . . . . . . . .32 / 8$ | 50V. A.C.* . . $32 / 6$ |
|  | $50-0-50 \mu \mathrm{~A}$. . . $42 / 8$ | 5 amp . . . . . . . $82 / 6$ | $150 \mathrm{~V} . \mathrm{A}, \mathrm{C} \cdot$ - . 32,6 |
|  | 100 | $15 \mathrm{amp} . . . . . . . .32 / 6$ | 300V. A.C.* . $82 / 6$ |
|  | $100-0-100 \mu \mathrm{LA}$. $42 / 6$ | 30 amp. . . . . . $32 / 6$ | 1 amp . A.C.* . $82 / 6$ |
|  | 500 LA . . . . . . 39818 | $50 \mathrm{amp} . . . . . . .32 / 6$ |  |
|  | 1 mA . . . . . . . . $82 / 6$ | 6V. D.C. . . . . $32 / 6$ | 10 amp. A.C.*.32/6 |
|  | 1-0-1mA .....32/6 | 10V. I.C. - . . $32 / 6$ | 20 mmp . A.C.* $32 / 6$ |
|  | $5 \mathrm{~mA} . . . . . . . . .32 / 6$ | 20V. D.C. ....32/6 | 30 amp A.C.*.32/6 |
|  | $10 \mathrm{~mA} . . . . . . .82 / 8$ | 50V, D.C. ....32/6 | 50 amp A.C. ${ }^{-} .82 / 6$ |
| *Moving iron, all | 50 mA . . . . . . . $32 / 6$ | 150 V . D.C. - . $32 / 8$ | VU meter. . . . $59 / 6$ |
| other moving ooil. | 100ma ..... . $32 / 6$ | 300V. D.C. ...32/8 |  |

NEW RANGE OF "SEW" EDGEWISE METERS


MODEL, PE70. Dimensions $317 / 32 \times 111 / 32 \times 2$ in deep overall. Available as follows
50 microamp. ...... $57 / 8 \quad 500$ microamp. . . . . $49 / 8$
$50-0-50$ microamp....57/ $\quad 500$ microamp. . . . . $49 / 8$ $\begin{array}{ll}100 \text { microamp......55/- } & 300 \text { volt A.C. ........45/- } \\ 1000-100 \text { microamp } 52 / 6 & \text { VU meter } . . . . . . . .62 / 2 ~\end{array}$ 200 microamp......52/6

Post extra


COMMUNICATION RECEIVER BHoring for CW' Kc/s-30 Mc/s. Incorporates variable phune jack. Metal cabinet. Operation $240 / 240 \mathrm{~V}$. A. | Supplied brand new, guaranteed with |
| :--- |
| instructions. |

LAFAYETTE MODEL HA-700 AM/CW/SSB AMATEUR COMMUNICATION RECEIVER FILTERS for exceptional selectivity and genaitivity Frequency coverage on 5 bands $150-400 \mathrm{Kc} / \mathrm{s}$, $550 /$ $1,600 \mathrm{Kc} / \mathrm{s}, 1 \cdot 6-4 \cdot 0 \mathrm{Mc} / \mathrm{a}, 4-8-14 \cdot 5 \mathrm{Mc} / \mathrm{s}, 10 \cdot 5-30 \mathrm{Mc} / \mathrm{s}$. limiter, B.F.O. product detector, electrical hand spread, \& meter, slide rule dial. Output for phones, low to $2 \mathrm{k} \Omega$ or speaker 4 or $8 \Omega$. Operation $220 / 240 \mathrm{~V}$
$\mathrm{~A} . \mathrm{C}$. Size $79 \times 15 \times 10 \mathrm{in}$ \& A.C. Size $71 \times 15 \times 10 \mathrm{in}$. Supplied brand new and
 g.A.E. for leaflet.
-


GARRARD DEGKS
Brand New and Guars Brand New and Guaranteed
1025 with cartriage 87.10 .0 1025 with cartrilge 87.10 .0
A70 Mk II less cart. $\mathbf{2 1 2 . 1 2 . 0}$. LA B 80 Mk II léss cart. 223.10. LAB 80 Mk . II with bawe. £27.10.0. 401 Transcription lesh cart. 287.6.0. Carr. $7 / 6$.
WOODEN PI, WOODEN PLINTH fir diarrard Series $1000,2000,3000$ ete. with perspex
24.io.c. P. \& P. $4 / 6$.

DE LUXE PLAYYRS pordable To it standard $69 / 6$ RCS AMPLIFIER 3 WATL Ready made and tested with UCL82 triode pentode valve and loud- 59/6 speazerion
AMPLIIIER.
Built and teated. Eetter sonnd.
Trandormer 3 watt ECL8 8 triode pentod Volnre and tone controis with knobs. Quality 89/6 Loudmpeszer.
SINGLE PLAYERS MONO AUTOCHANGERS MONO 8tarar (6 volt) 22.19.6 Garrard 8RPE2 $\quad 8.19 .6$ $\begin{array}{lr}\text { Garrard 8P25 } & \text { els.19.6 }\end{array}$ Philips AG1016 811.18 .6 $\begin{array}{ll}\text { Garrard LAB80 } & \text { 2E4.10.6 } \\ \text { Garrard } 401 & 20.19 .8\end{array}$ All fitted LP/78 atylii and piokup orystal complete. GARRARD TEAK WOOD BASE W.B.1. Ready 65/= outonitormonnting 1000, GAR

SANGAMO 3 inch SCALE METER 45/-ea Varions calibrationg and movements, 100 Mioroamp 1. Milliamp; 50-0-60 Mieroamp, ete. S.A.E. Ior list.


RETURN OF POST DESPATCH
RADIO COMPONENT

THF E.A.R. RECORD PLAYER CABINET 53/6 strongly built wooden cabinet oovered in Blae and Grey leathercloth. Size $16 \times 17 \times 8$ in. Motor Board $14 \pm \times 12$ in. deoks. Amplifier space sire $14 \times 7 \times 8 \mathrm{in}$. The baifle is out out lor a $6 \nmid \mathrm{in}$. dia. speaker.

NEW TUBULAR ELECTROLYTTCS CAN TYPES 2/850 \%. 2/3 100/25 \%. $2 /-\quad 8 / 600$ ₹. TYPE8 $4 / 850$ ₹. . $\quad 2 / 3$ 250/25 $7 . . .2 / 6 ~ 16 / 600$ ₹. $\begin{array}{lllllllll}8 / 450 & \nabla . & 2 / 3 & 500 / 25 & \nabla . . & 4 /- & 16+16 / 500 & \% & 9 /- \\ 18 / 450 & \nabla . & 8 /- & 8+8 / 450 & \nabla . & 8 / 6 & 32+32 / 850 & \nabla . & 3 / 6\end{array}$ | $18 / 450$ |  |  |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $92 / 450$ |  |  |  |
| $\nabla$ | $\cdots$ | $3 / 9$ | $8+16 / 450$ | $25 / 25$ ₹. .. $\quad 1 / 9 \quad 16+18 / 450$ ₹. $4 / 8,60+100 / 850$ ₹. $11 / 6$ $50 / 50$ ₹. . $2 /-32+32 / 850$ F. $4 / 8100+200 / 875$ ₹. $12 / 0$

 CERAMIC. 500 v .1 pF , to 0.01 mld , 9 d . Dises $1 /-$.
$350 \mathrm{v} .-0.19 \mathrm{~d} ., 0.52 / 8 ; 1 \mathrm{mid} .8 /-; 2 \mathrm{mid} .150 \mathrm{v} .8 /-$.
1,000 च. $-0.001 .0 .0022 .0 .0047,0.01,0.02,1 / 6 ; 0.047,0.1,2 / 6$. E.H.T. CONDENSERS. 0.001 mid., $7 \mathrm{kV} ., 6 / 6 ; 20 \mathrm{kV} ., 10 / 6$. SILVER MICA. Close toleranoe $1 \% .5-500 \mathrm{pF} 1 /-560-2200 \mathrm{pF}$ 2/-: $2,700-5,600 \mathrm{pF} \quad 3 / 8 ; 6,800 \mathrm{pF}-0.01 \mathrm{mld} 6 /-$ eaoh. TWIN GANG. "0-0" $208 \mathrm{pF} .+178 \mathrm{DF} ., 10 / 6 ; 365 \mathrm{pF}$., miniature $10 /-; 500 \mathrm{pF}$ standard with trimmers, $9 / 6 ; 500 \mathrm{pF}$. midget less trimmers, 7/6; 500 pF . slow motion, standard 9/-;
 $100 \mathrm{pF} ., 160 \mathrm{pF} ., 5 / 6$ each. Can be ganzed. Couplers 9 d , each, TUNING. 8 olid dielectric. 100 pF ., $300 \mathrm{pF} ., 500 \mathrm{pF} ., 5 /-$ each. TRIMMERS. Compression oeramic $30,{ }^{1} 50,70 \mathrm{pF}, 1 /-$
 850v. RECTIFIERS.8eleninm $\frac{1}{1}$ wave 100mA5/-; BY100 10/CONTACT COOLED $\frac{1}{2}$ Wave $60 \mathrm{~mA} 7 / 6 ; 85 \mathrm{~mA} 9 / 6$. CONTACT COOLED $\frac{1}{2}$ WAVE $60 \mathrm{~mA} 7 / 6 ; 85 \mathrm{~mA} 9 / 6$.
Full wave $75 \mathrm{~mA} 10 /-$; $150 \mathrm{~mA} 19 / 6 ; \mathrm{T} . \mathrm{V}$. reote. from $10 /-$.
'SONOCOLOUR' CINE RECORDING TAPE $5^{\prime \prime}$ reel, $900^{\prime}$ with $L P$ strobe markings also cine light de-
fiector-mirror for aynohranisation.
$14 /-$ each. JACK 8OGKET std. open-cirenli 2/6, closed cirouit 4/6; Chrome Lead Socket 7/6. DIN 3-pin 1/8, 5 -pin $1 / 6 ;$ Lead 3/6 Phono Plugs 1/-. 8ooket 1/-. JACK PLUGS Std. Chrome 8/
 2 p .2 -way, or 8 p. 6-way, or 8 p .4 -way $4 / 6$ es ch.


 PICK-DP ARM Complete with ACOS LP-78 Turnover GP67 and 8tylli 25/-; ACOS GP67 15/-; Stereo 85/-.

## BAKER MAJOR £8



30-14,500 e.p.s., Ietest double cone, wooler and tweeter cone together with a speoisl B A K ER magnet assembly having a fux density of 14,000 gauss and a total fux of 145.000 Marwells. Bass resonance 45 a,p.1, Reted 20 watts. Voive coils available 8 or 8 or 16 ohms. Prioe 28, or Module an illus. $80-17,000$ o.p.s. with tweeter, crossover, baffe and instruotions s10.18.6. "BONDACOUST" CABINET WADDING 18in. wide, $2 / 6 \mathrm{tt}$. BAKER "GROUP SOUND" SPEAKERS-POST FREE 'Group 25' 'Group 35' 'Group 50'

E.M.I. Cone Tweeter $31^{\prime \prime}$ qquare, $3-20 \mathrm{ke} / \mathrm{s} .10 \mathrm{w} .17 / 6$ Quality Horn Tweeters 2-18ke/s. 10w. 29/6. Crossover $16 / 6$. LOUDSFEAKERS P.M. 3 OHM8. $2 \frac{1}{1 i n}$. $31 \mathrm{in.} ,4 \mathrm{in}$. , 5in.,
 Double cone 3 or $15 \mathrm{ohm} 85 /-; 10 \times 6 i n .30 /-; 8 \times 6 i n . ~ 21 /-$



## MINETTE

 AMPLIFIERFor Hi-Fikecord Players


Chassis ive $7 \times 81+4$ in. high. Valves ECL82, E280 Two stage negative loedbsok. Quslity outpat 8 ohm matobing. Bargain offer complete with engraved control panel, valvan knobs, volume and tone controls,
wired and tested.
Post $5 / 6$. wired and tested.

CALLERS WELCOME
VEST CROYDON 337 WHITEHORSE ROAD. WEST CROYDON

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SAME DAY SERVICE
NEW! TESTED! GUARANTEED!


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You can do so much with MARTIN kits. The system of using pre-fabricated transistorised units which can be interlinked in a variety of ways enables you to assemble the combination of your choice and then extend it unit by unit until you possess a full stereo gramophone and radio assembly. When new units are produced, they can be added to existing equipment very easily with the advantage that you can continue to use equipment you already have,
so that your installation is always up to date. Most important of all is the power and quality which MARTIN Audiokits give you. Their sturdy construction assures compactness without sacrifice to quality or efficiency. They offer excellent value, are very easily installed and will give years of unfailing service. That is why people prefer MARTIN - it's simple to install, good to listen to, and looks completely professional.

## AMPLIFIER SYSTEMS • TUNERS • RECORDERS

ONLY FROM MARTIN MARTIN AUDIOKITS are available for Mono, and can be doubled up for stereo, or as complete stereo units. 3 ohm and 15 ohm systems are available. There is a special pre-amp for low output pick-ups and escutcheon panels to suit the arrangement you choose. The tuner is styled to match.
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UNITS INCLUDE:
$\square$-stage input selector
$\square$ Pre-amp/tone controls
10 watt amp. (3 ohms)
10 watt amp. ( 15 ohms )
$\square$ Mains power supply
F.M. Tuner

Trade enquiries invited

## MARTIN ELECTRONICS

154 High Street, Brentford, Middlesex
Please send Recordakit/F.M. Tuner/Audiokit Hi-Fi Leaflets. (Strike out items not wanted)

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Address $\qquad$

P.W. 8/68

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You'll find it easy to learn with this outstandingly successful NEW PICTORIAL METHOD-the essential facts are explained in the simplest language, one at a time, and each is illustrated by an accurate, cartoontype drawing. The books are based on the latest research into simplified learning tech-
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STEREO AMPLIFIER (2 are required for Stereo). The X101 is a brilliant new addition to our highly successful range of products. Its professional performance and advanced solid-state cir-
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R, M,S, I'ovver output: 13 W (music power), 10 W (Sine Wave). Sinsilivity: for rated output 1 mV into 3 K ohms load. roquency fesponse: minus 3 dB points are 20 Hz and 40 KHz .
Ontpur impudance: 3 ohms ( $3-15$ ohms may be used)
Sulply Voh1age: 24 V D.C. at 800 mA ( $6-24 \mathrm{~V}$ may be used) output at Size:2 14 - X C. Supply with 3 ohms speaker. 7 watts.
Size. ${ }^{2}$,
The fully comprehensive instruction manual does not only show the basics, such as circuit diagram and connections, but also gives practical easy-to-understand detailed information about the X101. ventional inputs. They include: Tape Head, Mag. P U X X P . P . Tuner, Mic, etc. $\mathbf{4 9} / 6+2 / 6$ p. \& p .

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## Bi (I)/LI AHIGH qualITY MONAURAL

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Sensitivities for 200 mV output at 1 KHz .
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Mar. IPU: 2 mV
Iux.: $\quad 100 \mathrm{mV}$
Cer. IPU.: 80 mV Tive/Ree. Out put: 100 mV
Tape/Ree, Outiput: 100 mV
Equalisation for each input is correct to within $\pm 2 \mathrm{~dB}$ (R.I.A.A.)
Tone Control Kange: Bass $\pm 13 \mathrm{~dB}$ at 60 Hz
Total Distortion : (for 200 mV output) $<0.02 \%$
Signal Noise: > -60dB
Supply Voltage: 24 V D.
79/6 plus $2 / 6 \mathrm{D} . \& \mathrm{~d}$.
A STEREO VERSION (PR101/S) WILL BE ANNOUNCED SHORTLY

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## SPECIFICATMON

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Sensitivity: M. Wi at Mc/s 10 microvolts plus or minus 1 als

- Fligh (internal ferrite rod aerial on
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## TOPIC OF THE MONTH

## Impressed but unperturbed

THE recent Electronics and Automation Exhibition at Olympia has been called "the greatest technical show on earth", and with justification. Let us sprout a few figures...

It attracted more than 112,000 visitors, including 9,000 from 80 different countries. Equipment worth more than $£ 50 \mathrm{M}$ was displayed by the near- 1,000 exhibitors from 15 countries in the 12 acres of floor space. The industries supporting the exhibition had a turnover of $£ 2,420 \mathrm{M}$ last year, of which $£ 430 \mathrm{M}$ came from exports (averaging no less than $£ 1 \cdot 75 \mathrm{M}$ exports every day). There are 900,000 people employed in the industry, meaning that at least 2.5 M people rely on the electrical, electronics and allied trades to live.

These are cold, hard facts-impressive but impersonal. Yet they spotlight the way in which the industry is now in many ways affecting, controlling and fashioning our lives and environment; making its impact industrially, economically and socially.

Without electronic aids to support production and commercial activities, our industrialists would face a bleak future in this competitive world, for without modern scientific methods they are doomed. On the domestic and industrial front, TV and radio communications continue to progress. Techniques developed in space research are finding industrial and domestic applications; techniques devised for industry are being adapted for medicine and surgery. So it goes on-a great interplay and flexibility.

It is remarkable how the garden-shed set-ups of the early days of wireless have ballooned into one of our greatest growth industries, and one which will exert an ever-increasing influence in many spheres as the years go by. Yet one fringe activity seems to have been content to maintain a dignified aloofness to this headlong acceleration.

In the "cottage industry" days, enthusiasts were building their own radio sets. And today, even amidst all the technical magnificence of modern electronics, enthusiasts are still building their own radio sets. Which goes to show, if it shows anything at all, that it's a splendid hobby!
W. N. STEVENS—Editor.

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[^0]... AND SO AD INFINITUM!


The vanishing species? Will they get so small in the end that they'll disappear altogether ? Nobody knows, but they're certainly having a jolly good try. The "they" are the integrated circuits. You can see (just about) one in the photograph being poked through the proverbial eye of a needle. This one is a Mullard unencapsulated TTL decade counter performing its special trick of jumping through the eye of a number 5 sewing needle; the circuit contains over 120 components, and the "rope" is 40 gauge sewing cotton.

## GRUNDIG MUSICOLOR



The Music Boy de luxe is now available in leatherstyled padded finish and a choice of four colours. This portable receiver covers long, medium, short and v.h.f. wavebands, and runs from a PP9 battery from which 150 hours' life is expected. It contains 15 semiconductors, has telescopic aerial for v.h.f. and s.w., and a ferrite aerial for the other wave bands. Price is $29 \frac{1}{2}$ gns.

## TON-UP TAPPERS

sometmes appeare to deceive the ear, too. That is, wo correctly understand the latast piece of potty niggling by the GPo.

The Radio Services Department of that august Poos
bat lataly been mailing letters of complaint to licensed amateurs who are sending their callsigns faster than the specified 12 w.p.m. (it usect to be 20 w.p.m.). Why it should suddenly become necessary to throw the boek at operators is beyond understanding. yutess the GPO momtorstmue so declined inai hay can only copy dead slow morse, It comes to somathing when the professionals ask the amateus to slow down!
We did it-or did we ? Either way it does seem a coincidence that no sooner does our Leader raise an evebrow at the GPO's attitude to c.w. speeds on the amateur bands (page 817. March 1968) than that very same government body announce that the speed restriction is raised to 20 w.p.m. Whoever it was who used super red tape solvent to get this one through-your very good health Sir, and to all you amateurs-whip those weights off the bug keys lads, we're having a c.w. ball.

## VANISHING SPECIES



Things in the electronic world are getting smaller and smaller. With integrated circuits coming in one wonders whether the days of the common transistor are numbered. But even transistors
 themselves are shrinking.
The larger photograph shows the Motorola Quad transistor 2 N5146 which houses four transistors in a 14 pin TO-86 flat package measuring $0.25 \times 0.25 \times 0.07 \mathrm{in}$. exclusive of leads. Typical electrical characteristics for each of the four transistors are: $\mathrm{h}_{\mathrm{FE}} 40$ at $\mathrm{I}_{\mathrm{C}}=1 \mathrm{~A}$ d.c.; $\mathrm{V}_{\mathrm{CE}}$ (sat) 0.7 V d.c. at 1 A d.c.; $\mathrm{f}_{\mathrm{T}} 250 \mathrm{Mc} / \mathrm{s}$ at $\mathrm{Ic}=50 \mathrm{~mA}$ d.c.

A low-level, high-speed switch and an r.f. amplifier have been added to Motorola's new Micro-T transistor line. These are only $0.08 \times 0.058 \mathrm{in}$. as the small photograph indicates. This is about one-tenth the size of a TO-18 can. For a v.h.f./u.h.f. amplifier mixer, or oscillator application, the MMT918 offers a high current gainbandwidth product of $600 \mathrm{Mc} / \mathrm{s} \mathrm{min}$. measured at $100 \mathrm{Mc} / \mathrm{s}$; output capacitance of $1.7 \mathrm{pF}(0.1-1 \mathrm{Mc} / \mathrm{s})$, and a collector-emitter breakdown voltage of 15 V d.c. min.

Further details of both these units from Motorola Semiconductors Ltd., York House, Empire Way, Wembley.

FACE-LIFT FOR AVO


The AVO Digital System is completely new. It comprises a main display unit which is designed to accept a number of plug-in modules. The measured value is automatically presented in digital form by four in-line neon indicators having a numeral height of 14 mm . The polarity and over-range indication is also presented automatically and the decimal point is automatic with range switching.

A built-in Weston reference cell provides a reference voltage which enables the calibration of the lower ranges to be corrected to the initial accuracy. The stability of the cell is $0.01 \%$ per year and the temperature co-efficient over the range $10^{\circ} \mathrm{C}$ to $40^{\circ} \mathrm{C}$ is less than $\pm 5 \mu \mathrm{~V} /{ }^{\circ} \mathrm{C}\left( \pm 0.0005 \% /{ }^{\circ} \mathrm{C}\right)$.

The specifications are impressive: d.c. voltage from 0.1999 to $1.999 \mathrm{~V} \pm 0.05 \%$ of indication $\pm 0.05 \%$ of full range at $20^{\circ} \mathrm{C}$. The input impedance on the higher ranges is $10 \mathrm{M} \Omega$ and greater than $1.000 \mathrm{M} \Omega$ on the two lower ones. D.C. current from 0.1999 to 1.999 mA ; resistance from 0.1999 to $1,999 \mathrm{k} \Omega$ with similar coverage for the a.c. voltage and current ranges.

The unit has other ranges and applications. Further details may be obtained from the makers.

## INVISIBLE MOTORS



Well, not quite but darned near. High output efficiency and low weight combined with extreme miniaturisation are the features of two new groups of d.c. electric motors in the revised and expanded Micromotors range from $B \& R$ Relays Ltd. There are three models in each groupdesignated 050 and 030 -but all have a common configuration. These really are small, for instance, those in
the 050 range have a diameter of 15 mm and a casing length of 16 mm . By employing skew-winding with three rectangular coils and an ironless bell-shaped armature, the starting time can be speeded and the spindle diameter can be very small. This helps reduce friction losses at the commutator and gives low contact resistance between the precisely matched gold alloy bushes and the $95 \%$ silver alloy collector. The 050/0055 motor has a no-load running speed of 19.100 r.p.m. which can be reduced by slip-on gear-boxes in the ratios $3 \cdot 45: 1,11 \cdot 8: 1,141: 1$, and 5.750:1. With an armature resistance of $5 \Omega$ and a measuring voltage of 3 V , the $030 / 010$ motor develops a specific torque of $16.90 \mathrm{cmp} / \mathrm{A}$.

## RADIONETTE MULTICORDER



This tape recorder is claimed to be the first in the world to use only one single reel. It has two speeds and gives up to 12 hours' playing time-enough for 18 big L.P. records. It will also accept pre-recorded tapes and tapes recorded on conventional tape recorders, with tracks in the opposite direction.

The Multicorder is fully portable and transistorised, and a companion battery eliminator is a vailable too. Another accessory is the vinyl carrying case which also accommodates the microphone. The mike is a dynamic type, and can be used as a "pillow phone".

Outlets are provided for extension speaker, earphone and radio. It has an output/recording/battery meter and a tape-position indicator. There are four tracks, any one of which is instantly selectable by the track selector control thus obviating the need to turn the reel over.

Power required is 9 V obtained from six U2 cells. Current consumption is $80-100 \mathrm{~mA}$ at low volume rising to $200-250 \mathrm{~mA}$ at 1 watt output. Circuitry uses seven transistors and two diodes; wow and flutter less than $0.2 \%$; tape speeds $1 \frac{7}{8}$ and $3 \frac{3}{4}$ i.p.s.; reel size 5in.; microphone input $700 \Omega$ with a sensitivity of 1 2 mV ; radio input is $470 \Omega$ with a sensitivity of 20 mV ; amplifier outlet $20 \mathrm{k} \Omega, 50-100 \mathrm{mV}$. Price with mike is 49 gns , case to suit costs an extra 5 gnn .

## A SIMPLE SIGNAL GENERATOR James Hossack

THE signal generator described here uses a conventional twin-triode oscillator circuit for both the r.f. and a.f. sections, and has a frequency coverage of $120 \mathrm{kc} / \mathrm{s}$ to $50 \mathrm{Mc} / \mathrm{s}$, thus enabling tests to be carried out on most domestic radio and television apparatus (with the exception of u.h.f. receivers), harmonics being used to cover up to $200 \mathrm{Mc} / \mathrm{s}$. The method of construction is somewhat unusual in that it employs the "Cir-kit" technique, enabling an extremely satisfactory printed circuit board to be made without the use of chemicals or other etching medium.

## CIRCUITRY

The theoretical circuit is shown in Fig. 1, and apart from resistor and capacitor values, both halves of the signal generator are identical. Briefly, damped oscillations set up in the grid inductance of the lefthand triode of each valve are maintained by feedback of the correct phase supplied from the righthand anode via the appropriate coupling capacitor. In the case of the a.f. section, a tightly-coupled coil, actually the primary of the a.f. transformer T1, whose secondary comprises the audio oscillator coil, picks up the oscillation and employs it to modulate the anode of the r.f. section when a modulated output is required. Final calibration of the generator is simplified if a second, calibrated,

generator can be borrowed, although an alternative, but less accurate, procedure is described later.

## THE CASE

Although a suitable die-cast metal box can be purchased for a reasonable cost, it was decided to press into service a discarded metal container measuring $8 \times 6 \frac{1}{2} \times 4 \frac{1}{2} \mathrm{in}$., replacing the ebonite base with an aluminium sheet $8 \frac{1}{2} \times 6 \frac{1}{2} \mathrm{in}$. which then becomes the front panel. Drilling details for the latter are shown in Fig. 2.

A small metal sub-frame $6 \times 4 i n$. constructed of angle aluminium and bolted to this panel at XX carries the printed circuit board, the coils being bolted directly to the lower part of the front panel, or else supported on a small strip of Bakelite, as in Fig. 3. Coil-winding details are given in Table 1. Figure 3 also indicates a convenient method for mounting the coils. The three lowest-frequency coils are supported on a length of $\frac{3}{8} \mathrm{in}$. ferrite rod bolted to the front panel, while coils 4 and 5 can be wound on a suitable short-wave coil former from which the core has been removed. The coil for the highest range, which is self-supporting, is best inserted after


Fig. 1: Circuit diagram of the simple signal generator.


Fig. 2 (above): Drilling details of the front panel.
Fig. 3 (below): Suggested method of mounting the ferrite coils.

the generator has been set up and calibrated on the lower ranges as in this way it can be checked that the coverage is complete without excessive overlap. Since two-terminal coils are used, coverages for all coils may in any case be altered fairly easily, after construction has been completed, owing to the "open", nature of the printed circuit layout. For example, if a more conventional type of mounting is desired for the l.f. coils in preference to the ferrite rod method, the turns for coils $1-3$ should be increased by about $30 \%$, and adjusted finally, by removal of turns, to give the desired coverage.

After mounting coils, range switch, and output terminals, the remaining front panel components, consisting of on/off and modulation switches, output control, and indicator lamp, are bolted in position. The lamp, though not essential, is a desirable addition, since it has been found, in practice, that test equipment may be inadvertently left switched


Fig. 4: Wiring diagram of the underside of the "chassis" using Cir-kit copper strip.
on for long periods, with possible overheating. As a further precaution in this respect, due to the poor ventilation consequent upon nearly complete screening, it was considered desirable to include the $1 \Omega$ dropping resistor, R7, which reduces the heater voltage to a safe 5.8 V .

## CONSTRUCTION

The next step is to cut and drill the paxolin "Cir-kit" board to take valve holders (B9G, printed circuit type), tuning capacitor, mains transformer, and all fixed capacitors and resistors, including the silicon diode, D1, but excluding C8 and C9, which are mounted on the back of the sub-chassis. C3 and C4 are soldered respectively across the primary and secondary of the modulation transformer, which is also bolted directly to this chassis. Make sure that the tuning capacitor is efficiently earthed with a piece of heavy gauge wire do not rely on the "Cir-kit" strip for this purpose, since oscillation may be impaired on the highest-frequency range.

Now, lay the copper strip on the underside of the board, following the layout of Fig. 4, and taking care to leave sufficient overlap at corners to facilitate subsequent soldering. Finally, the "Cir-kit" strips are pierced with a pin where they underlie the component holes, and all resistors, capacitors, etc. can be threaded through and soldered into position. R5 and the silicon rectifier should be spaced about $\frac{1}{2} \mathrm{in}$. above the paxolin board to assist heat dissipation. At the same time, solder the valveholder pins to the appropriate strips, insert and

| Range | Coverage | No. of turns | Wire gauge s.w.g. | Former |
| :---: | :---: | :---: | :---: | :---: |
| 1 | $120-300 \mathrm{kc} / \mathrm{s}$ | 250 | 32 | $\}\}^{\frac{3}{8} \text { in. ferrite }} \begin{aligned} & \text { rod } \end{aligned}$ |
| 2 | $300-650 \mathrm{kc} / \mathrm{s}$ | 120 | 32 |  |
| 3 | 600-2000kc/s | 64 | 32 |  |
| 4 | $1.9-6.0 \mathrm{Mc} / \mathrm{s}$ | 50 | 32 | $\begin{aligned} & \text { pile wound } \\ & \text { on } \frac{1}{4} \text { in. } \\ & \text { former } \end{aligned}$ |
| 5 | $5 \cdot 1-22 \mathrm{Mc} / \mathrm{s}$ | 14 | 28 |  |
| 6 | 20-50Mc/s | 4 | 16 | self-supporting |

Table 1. Winding details for the coils.
solder the mains transformer leads, and place a spot of solder at each strip junction, as previously mentioned.

The flying leads connecting the p.c. board to the under chassis components (coil, range switch, modulation transformer, and smoothing capacitors) and to those above chassis (modulation switch, indicator lamp, and other controls), can also be soldered on at this stage, leaving sufficient lengths to reach the appropriate connections on the front panel (compare Fig. 4).

## ASSEMBLY

The completed circuit board is now screwed on to the sub-chassis frame, the latter bolted to the front panel, and all flying leads soldered into position. Figure 5 is a top view of the completed assembly. Unless a separate signal source is available and it is desired to use the heterodyne method of calibration, with headphones, it will probably be better to leave the generator out of its cabinet meantime, since this will enable sufficient output to be picked up on
a nearby receiver without the necessity for a coupling lead or dummy aerial．

Initial calibration is best carried out with the modulation off．Switch to the lowest frequency range （range 1），and tune the generator for zero beat with the long－wave light programme on the adjacent receiver．This enables the $200 \mathrm{kc} / \mathrm{s}$ point to be accur－ ately marked．Leaving the generator set to this point，tune in the harmonics of $200 \mathrm{kc} / \mathrm{s}$ on the receiver at 600,800 ，and $1,000 \mathrm{kc} / \mathrm{s}$ ．Leaving the receiver set to the latter frequency，switch on the internal modulation，and tune the generator，on range 3 ，for maximum response from the receiver


Fig．5：Top view of the completed unit． at this new frequency．Mark this point $1 \mathrm{Mc} / \mathrm{s}$ ．Har－ monics will now be available at 2，3， 4 etc． $\mathrm{Mc} / \mathrm{s}$ ， and the receiver can be tuned to detect any or all of these frequencies，depending on its short－wave coverage．After each setting has been found on the receiver，leave the latter untouched，and retune the generator for maximum response on the

## ＊components list

| Resistors： |  |  |  |
| :---: | :---: | :---: | :---: |
| R1 | $1 \cdot 5 \mathrm{k} \boldsymbol{\Omega} \frac{1}{2}$ watt | R5 | $3 \cdot 5 \mathrm{k} \Omega 5$ watt |
| R2 | $22 \mathrm{k} \Omega 1$ watt | R6 | $45 \Omega 1$ watt |
| R3 | $2 \cdot 2 \mathrm{k} \Omega \frac{1}{2}$ watt | R7 | $1 \Omega 1$ watt |
| R4 | $47 \mathrm{k} \Omega 1$ watt | VR1 | $10 \mathrm{k} \Omega$ pot． |
| Capacitors： |  |  |  |
| C1 | 20pF | C7 | 0．0047pF |
| C2 | $0 \cdot 0047 \mu \mathrm{~F}$ | C8 | $16 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic |
| C3 | 100pF | C9 | $8 \mu \mathrm{~F} 350 \mathrm{~V}$ electrolytic |
| C4 | $0.01 \mu \mathrm{~F}$ | C10 | $0 \cdot 1 \mu \mathrm{~F} 650 \mathrm{~V}$ |
| C5 | 10pF | C11 | $0.01 \mu \mathrm{~F}$ |
| C6 | $0.01 \mu \mathrm{~F}$ | VC1 | 300 pF variable |
| Valves： |  |  |  |
| V1 | ECC83 | V2 | ECC83 |
| Inductors： |  |  |  |
| L1－L6 see table |  |  |  |
| T1 3：1 or 5：1 intervalve transformer |  |  |  |
| T2 | $0-250 \mathrm{~V}$ at 25 m | ， 6.3 V | at $1 \cdot 2 \mathrm{~A}$ |
| Switches： |  |  |  |
| S1 1 pole 6 way |  |  |  |
| S2 2 pole 3 way |  |  |  |
| S3 SPST mains toggle |  |  |  |
| Miscellaneous： |  |  |  |
| Silic coil two chas | on rectifier type ormers and wire co－ax sockets； sis and case；$n$ | 3Y600 | dial bulb and holder； two B9A valve holders； pper strip；materials for olts；solder etc． |

receiver，this representing the fundamental of the frequency to which the receiver is tuned．

Although this procedure will not produce accuracy comparable with the use of a second（calibrated） generator，nevertheless，it should be sufficiently accurate for general testing purposes．A useful check can be made by graphing frequency against dial reading for each range，and this will also ensure that spurious responses－particularly troublesome when the receiver used is a small transistor type－ are not confused with the fundamentals or main harmonics．

## T⿴⿱冂一⿰丨丨丁口内 DODKS

三 AMATEUR RADIO CIRCUITS BOOK
Compiled by G．R．Jessop，G6JP．Published by Radio Society of Great Britain， 28 Little Russell Street，London，W．C．1． 119 pages．Size $8 \frac{3}{4} \times 5 \frac{1}{2} \mathrm{in}$ ．Price 10 s 6 d ．

THIS second edition is packed with circuits for the Ham．It does not give full details of how to build each project，but supplies the circuit and sufficient information for most amateurs to con－ struct the units described．Just about every aspect of amateur radio is catered for and circuits are given for a．t．u．＇s；front ends；speech amplifiers；oscillators； transistor transmitters；test gear etc．A large number of the circuits are transistorised and one depicts a 70 and $144 \mathrm{Mc} / \mathrm{s}$ converter using field effect tran－ sistors．
This edition is a decided improvement on its pre－ decessor in that it appears to contain even more detailed information．For the amateur enthusiast or ham who likes all those useful circuits in one place this is a good ten－and－sixpence worth，and can be confidently recommended．－DLG．

## 三 WORLD AT THEIR FINGERTIPS <br> 产 By John Claricoats，G6CL．Published by Radio Society of 

DEFINITELY a must for the Historians，the curious and for those radio enthusiasts who like to read an interesting book which is devoid of maths and other such features which makes some works rather heavy going．This book is the story of Amateur Radio in the United Kingdom and a history of the Radio Society of Great Britain．John Clari－ coats is certainly to be congratulated on producing some interesting and informative reading，coupled with a huge number of facts many of which are quite an eye－opener．

Scene 1 commences with the very first meeting of a group of enthusiasts with their＂coherer＂＿－＂．．a a $\frac{1}{2}$－inch diameter glass tube，I inch long，filled with iron filings．Corks were pressed into the ends of the tube and copper wires were passed through into the iron filings so that they did not quite meet＂．Finally， after chapters of interesting facts and photographs， the book arrives at the present－day．

One is often surprised by the odd snippits of information which come out，for instance the various people who have held membership in the Society－ Sir Oliver Lodge，Senatore Guglielmo Marconi to name just two．
Just who were the first amateurs and what did they get up to．Well，there was．．．no，you buy the book and read for yourself．$-D L G$ ．

# I.E.A. EXHIBITION 1968 

THE Seventh International Instruments, Electronics and. Automation Exhibition held at Olympia, London, from May 13 to 18 was one of the greatest technical exhibitions of its kind ever staged. A thousand companies from 15 different countries occupied the 695 stands spread over 250,000 square feet (around 12 acres!).

The equipment shown ranged from homely connectors to highly complex factory automation systems and much of it was on show to the public for the first time, some having only arrived from the development departments just in time for the exhibition.

Obviously it is impossible to deal with this exhibition in detail in the space available but we have selected some of the more interesting items touching on aspects of appeal to readers of Practical Wireless.

## FREQUENCY CONTROL

An interesting frequency-controlled oscillator was shown by Pedoka Ltd.; consisting of a small encapsulated unit, capable of printed circuit mounting, housing a miniature tuning fork to which piezoelectric elements are strapped. The crystals are energised at a low voltage, transferring energy to the fork which vibrates at its natural frequency. The oscillations are then passed on to built-in amplifying circuits. Frequency accuracy, in the range 300 to $3,000 \mathrm{c} / \mathrm{s}$, is normally better than $0 \cdot 1$ of a cycle. They can be built as oscillators or filters.

## PRECISION MEASUREMENT

A displacement transducer and digital display giving reading accurate to one part per million was featured by Automatic Systems Laboratories.

The firm also showed a number of displacement transducers possessing a resolution of 0.25 micron and an accuracy of 0.5 micron. These are digitised sequentially, the measurements printed out on tape.

## CHEQUE CHECK

Verification of cheques which need to be examined at more than one location in banks is speeded up by the Epsylon Telecheque system, operating with closed circuit television. The unit is so designed that the camera not only views the surface of the cheque but also sees through it to give warning of attempts to forge either signature or the amount payable. When the authorising officer at the remote station has approved the cheque, he presses a button which activates electromagnetic equipment at the bank counter to emboss the cheque with a mark indicating that it is approved.

## LONG LIFE RELAY

Astralux Dynamics Ltd. featured their Reedac reed relay which can switch up to 15 A at 250 V a.c. with a life expectancy of 500 million operations (approx. 16 years of once-a-second operation). It is controlled by $6-24 \mathrm{~V}$ d.c. and the control circuit requires a power of only 125 mW .

## FLAMEPROOF FLASH

An electronic flash unit which is flameproof and allows conventional photography to be carried out in explosive atmospheres (mines, oil refineries, etc.) was exhibited by Ernest Turner Ltd.

## TAPE WOUND CORES

Ross \& Catherall Ltd. showed for the first time cut tape wound transformer cores, epoxy resin covered but not impregnated to preserve the electrical properties. The new process is claimed to give an improved core with no increase in cost.

## VIBRATING C

The type XL7900 shown by Mullard Ltd. is a vibrating capacitor with which extremely small voltages can be measured. Electrometers using this capacitor have measured currents as small as $8 \times 10^{-17}$ Amp., the equivalent of the flow of 500 electrons per second.

It contains four metal plates in parallel, the outer ones fixed, the inner ones mechanically linked to preserve constant spacing but able to vibrate as a pair with respect to the fixed plates. A.C. is applied between one vibratory and one fixed plate. The voltage to be measured is applied to the other two plates.

## ELECTRONICS FOR CARS

A. B. Electronic Components Ltd. showed microcircuits for use in the electric systems of cars, designed as part of the Lucas alternator equipment which will ultimately replace the conventional d.c. generator. Thick film resistive and conductive elements are fired to a refractory base and then Lucas "hybridise" the circuit by fitting semiconductors of their own manufacture.

## LONG LIFE BITS

Harrison Clark Ltd. showed a new type of soldering bit with a 500 micron electrolytic coating within the diameter and a protective nickel coating over the top. Cost is high but it is estimated that their life is 75 times that of a standard copper bit. One specimen has been in use for six months and completed 600,000 joints and is still operating. The c!aim is for up to $4,000,000$ joints without undue wear.

## MINI COMPUTERS

Muldivo Ltd. displayed a range of desk-top computers. The most sophisticated was the IME86S featuring seven registers all with check-back factors after calculation. Cost, £740. The most compact weighed only 28.51 b . and had an average speed of calculation of 0.2 seconds, or 2.5 mS for an elementary addition.

## MINIATURE MAINS SWITCH

A. F. Bulgin \& Co. Ltd. exhibited a mains switch needing only a $1 / 32 \mathrm{in}$. $\times \cdot 0 \cdot 512 \mathrm{in}$. panel cut out and projects only 0.2 in . It weighs 17 gm . and carries an illuminated legend with a brilliant-glow neon lamp.

## C) What TRANSISTOR



## 3 RECEIVERS <br> FOR <br> Beginners

NUMBER THREE . . . is the last in this series and describes the construction and alignment of a three transistor five stage receiver covering the medium waveband.

T$\rceil$ HE final receiver in this short series, especially for the beginner, differs from the other two. The previous designs have been t.r.f. receivers standing for tuned radio frequency-whereas this receiver is called a super heterodyne or superhet.

## The T.R.F

What is the difference between the two types? Well, let us look at Fig. 1. The radio frequency signal (r.f.) comes into the set via the aerial to the r.f. amplifier stage. Here it is amplified and passed to the detector where it is converted to audio frequency (a.f.) and from here passes to the a.f. amplifier for further amplification.

If we drew a similar block diagram of the first receiver in the series it would look like Fig. 2. The first stage amplifies the signal at r.f., passes it to the


Fig. 1: Block diagram of a t.r.f. receiver.

Fig. 2: A reflexed t.r.f., note the signal passes through the first stage twice.

## by T. Simon

detector stage which converts it to a.f., and it is then fed back to the first stage again for further amplification. Note that the first time it passed through the first stage it was amplified at r.f. and the second time at a.f. We say that the stage is reflexed or that it is a reflex stage. Figures 1 and 2 depict t.r.f. receivers since the signal is amplified at the frequency it is received at, i.e. it is not changed or converted to a different r.f. frequency.

## The Superhet

Now look at Fig. 3. This is a block diagram of a superhet receiver. Note that the last two blocks marked DET and AF are the same as the last two in Fig. 1. But what about the first three marked MIX, IF and OSC? This is the difference between the simple t.r.f. and the superhet.

The signal is again received via the aerial and fed to the mixer-which might be thought of as an ordinary r.f. amplifier stage, just like the first box in Fig. 1. Let us suppose that the signal received is at a frequency of $2,000 \mathrm{kc} / \mathrm{s}$. The box marked OSC is an oscillator-a tiny transmitter which emits a signaland this also is fed with the aerial signal to the mixer. Just as its name implies, the mixer mixes the two signals together and at the output of the mixer there will be two main signals, the sum and the difference of the two signals fed in.

Let's take an example to clarify matters. We are receiving a signal from the aerial at $2,000 \mathrm{kc} / \mathrm{s}$ (say) and our oscillator is tuned to give a signal of $2,460 \mathrm{kc} / \mathrm{s}$. Therefore, at its output, there will be two signals, $2,000 \mathrm{kc} / \mathrm{s}$ plus $2,460 \mathrm{kc} / \mathrm{s}=4,460 \mathrm{kc} / \mathrm{s}$, and 2,460 minus $2,000 \mathrm{kc} / \mathrm{s}=460 \mathrm{kc} / \mathrm{s}$. If we put a tuned circuit in the output and tune it to $460 \mathrm{kc} / \mathrm{s}$ it will pass the $460 \mathrm{kc} / \mathrm{s}$ signal and reject the $2,460 \mathrm{kc} / \mathrm{s}$ signal.

Suppose that we couple the tuning of our aerial circuits and those of our oscillator so that the oscillator is always tuned to a frequency $460 \mathrm{kc} / \mathrm{s}$ above the frequency to which the aerial circuit is tuned to. Then, no matter where we tune in the band, there will always be a signal of $460 \mathrm{kc} / \mathrm{s}$ at the output of the mixer. This is just exactly what happens in the superhet.
The i.f. stage is nothing more than an r.f. amplifier tuned to amplify at the i.f. (intermediate frequency) which in this case is $460 \mathrm{kc} / \mathrm{s}$. From here the signal is detected and the resultant audio is amplified by the a.f. amplifier just as it was in the t.r.f.

## Reflex Circuit

Figure 4 shows a block diagram of the receiver described here. The first transistor is arranged to function as both mixer and oscillator. The second stage is reflexed, and the i.f. signal at $460 \mathrm{kc} / \mathrm{s}$ is first amplified at this frequency and then passes to the detector where it is converted to a.f. The a.f. signal is now passed back again to the i.f. stage which this time amplifies a signal at audio frequencies and passes it to the a.f. audio output stage to feed the speaker or headphones.

## The Receiver

The complete circuit for the receiver is shown in Fig. 5. The signal is fed to the small coupling coil between pins 8 and 9 on L1. The tuned circuit $\mathrm{VC1} / \mathrm{L} 1$ tunes in the station and this is then coupled to the base of Tr 1 by the second coupling coil, pins 5 and 7. Coil L2 also has three windings. The two sets between pins 8 and 9 , and 5 and 7 cause the circuit to oscillate by feeding back some of the r.f. energy, while the tuned circuit VC2/L2 governs the exact frequency at which the stage will oscillate. We arrange this oscillator frequency to be $460 \mathrm{kc} / \mathrm{s}$ above the incoming signal frequency, and since $\mathrm{VC1}$ and VC2 are ganged together, they will alter the tuned


Fig. 5: Circuit diagram of the reflexed superhet receiver.


Fig. 3 (above): Block diagram of a simple superhet.
Fig. 4 (below): Superhet with a reflexed i.f. stage.
circuits by the same amount thus ensuring that the oscillating frequency is always $460 \mathrm{kc} / \mathrm{s}$ above the incoming signal.

The tuned circuit marked i.f.t. 1 is tuned to the intermediate frequency ( $460 \mathrm{kc} / \mathrm{s}$ ) in order to select this difference signal and reject all others. Note that the lead from pin 8 of L2 is connected to pin 2 of the i.f.t., i.e. the signal is tapped into the coil. If it were taken to pin 1 of the i.f.t. there would be a mismatch between the collector and the i.f.t. tuned circuit which would make the circuit tune very broadly. In this case it would be very undesirable since we only want our i.f.t. to tune sharply to $460 \mathrm{kc} / \mathrm{s}$.

The coupling winding on i.f.t. 1 (which is not tuned) couples the signal to base of the i.f. stage Tr2. Here it is amplified at $460 \mathrm{kc} / \mathrm{s}$ and appears at the collector of $\operatorname{Tr} 2$ which is again tapped into the tuned load formed by i.f.t.2. The small untuned coupling winding feeds the signal to the diode detector which in turn feeds the resultant audio signal to the volume control VR1. Capacitor C4 couples this (now audio) signal back again to the base of Tr2 which now acts as an audio amplifier. The amplified audio appears across the $1 \mathrm{k} \Omega$ resistor R8, the tuned circuit of i.f.f. 2 will not affect this audio signal since it is tuned to $460 \mathrm{kc} / \mathrm{s}$ which is well outside the audio range. From R8 the audio signal is fed, via C6, to the base of Tr 3 , which amplifies the signal and feeds it to the miniature loudspeaker or headphones.

The dial was made from a small scrap of scraper board, obtainable from most good art shops, a small packet
costing 2 s . 6d. Alternatively, a piece of white card marked with Indian ink etc., would prove equally suitable.

## Construction

First, take a piece of aluminium $4 \frac{5}{8} \times 4 \frac{1}{2}$ in. and cut out, bend and drill as indicated in Fig. 7. Either 18 or 20 gauge aluminium will suit, 20 gauge being used in the prototype. The lighter gauge makes cutting and drilling a little easier and is quite good enough since the chassis does not have to bear any great weight.

Next, mark out and drill the front panel. The larger holes may be first drilled with the largest drill to hand, usually a $\frac{1}{4}$ or $\frac{3}{8}$ in., and then enlarged carefully with a half-round file. Any plastic material will do but extra care is needed since plastics, especially Perspex, is easily cracked and chipped.

Take the veroboard and drill the four 6BA mounting holes, again exercising care. Now, fix together the front panel and chassis. Mount the three items on the front panel-VC1/VC2, VR1/on-off and the "speaker".

Wiring of the veroboard is the next job, so first insert pins into the board as indicated. Carefully drill the board and mount the coils and i.f.t's. The

## * components list

## Resistors:

| R1 | $56 \mathrm{k} \Omega$ | R5 | $82 \mathrm{k} \Omega$ | R9 $47 \mathrm{k} \Omega$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| R2 | $10 \mathrm{k} \Omega$ | R6 | $10 \mathrm{k} \Omega$ | $\mathrm{R} 10 \quad 1 \mathrm{k} \Omega$ |
| R3 | $1 \mathrm{k} \Omega$ | R 7 | $1 \mathrm{k} \Omega$ | $\mathrm{VR1} 5 \mathrm{k} \Omega$ |
| R4 | $1 \mathrm{k} \Omega$ | R8 | $1 \mathrm{k} \Omega$ | edgewise pot. |
|  |  |  |  | with switch |

## Capacitors:

| C1 | $0 \cdot 1 \mu \mathrm{~F}$ |
| :---: | :---: |
| C2 | $0.01 \mu \mathrm{~F}$ |
| C3 | $0.1 \mu \mathrm{~F}$ |
| C4 | $10 \mu \mathrm{~F} 16 \mathrm{~V}$ electrolytic |
| C5 | $10 \mu \mathrm{~F} 16 \mathrm{~V}$ electrolytic |
| C6 | $10 \mu \mathrm{~F} 16 \mathrm{~V}$ electrolytic |
| C7 | $10 \mu \mathrm{~F} 16 \mathrm{~V}$ electrolytic |
| $\left.\begin{array}{l} \mathrm{TC} 1 \\ \mathrm{TC} 2 \end{array}\right\}$ | 30 pF miniature ceramic trimmers |
| vC1 $\}$ |  |
| VC2 3 | $300+300 \mathrm{pF}$ twin gang variable |

$\mathrm{CP} \quad 350 \mathrm{pF}$ padder $(300+50 \mathrm{pF}$ in parallel)

## Semiconductors:

| Tr1 | AF115 Mullard | Tr3 | OC71 Mullard |
| :--- | :--- | :--- | :--- | :--- |
| Tr2 | AF115 Mullard | D1 | OA81 Mullard |

## Inductors:

\(\left.\begin{array}{ll}L1 \& Miniature transistor Type 2T Blue <br>
L2 \& Miniature transistor Type 2T Red <br>
IF1 \& Type IFT 14 <br>

IFT2 \& Type IFT 14\end{array}\right\}\)| Denco |
| :---: |
| (Clacton) |
| Ltd. |

## Miscellaneous:

Veroboard $3 \frac{3}{4} \times 2 \frac{1}{2}$ in.; material for front panel $4 \frac{3}{4} \times$ $2 \frac{3}{4}$ in.; aluminium $4 \frac{1}{2} \times 4 \frac{5}{8}$ in.; dynamic mike insert (L.S.) $2 \mathrm{k} \Omega$ impedance, model MM2 (Henrys Radio); nine 6BA and two 8BA nuts and bolts; dial to suit; white pointer knob; solder tags; screened leadabout 6in.; wire; solder, wire for aerial and earth; 9 volt battery (PP3); battery terminal clip; strip of aluminium to hold battery $2 \frac{3}{4} \times \frac{5}{8} \mathrm{in}$.


Fig. 6 (above): Drilling details of the front panel and battery clip.
Fig. 7 (below): Chassis drilling and under-chassis wiring.
cut-outs for the i.f.t's are made by drilling a number of small holes with a $3 / 32 \mathrm{in}$. drill, and then filing to the final size with a small thin file. The i.f.t's are held in place by bending over the lugs connected to the metal screening cans. Make sure to earth these lugs or the screening will be ineffective and instability could easily result.

Wire in the transistors and diode last of all and use a heat shunt for the purpose. The finished wiring should be carefully checked against the circuit and layout diagrams, Figs. 5, 7 and 8. Note that the coils are held in position by a small plastic nut which should be only finger tight since it is easy to crack the nut or even sheer off the thread if too much force is applied.

Finally, wire in the battery but do not connect the terminal clips until you have checked the completed wiring against Fig. 5. Check carefully the connections to the transistors and the diode. Now connect the battery and the set is ready for alignment.

## Alignment

If you have a signal generator and know how to use it then you should experience no difficulty in alignment. If not, and you do not have any experience in aligning superhet receivers, it would be wise to enlist the aid of the local radio dealer who might do this for you at a small fee. It is possible to align the receiver by ear and for this purpose you will need an insulated trimming tool plus, of course, an ear! A plastic knitting needle filed to the shape of a screwdriver will do. A metal screwdriver is no use since the metal would de-tune the circuitry.

With a suitable aerial and earth connected, the core of the oscillator coil (L2) is adjusted until a station is heard at the low frequency end of the dial i.e., with the vanes of VC1/VC2 almost completely enmeshed. When a signal has been located, the core of the blue coil (LI) is adjusted for maximum volume.

VC1/VC2 are now tuned to the other end of the band so that you should seek a signal which comes in when the vanes are now almost fully open. Now, gently adjust the oscillator trimmer (TC2) for maximum volume after which the other trimmer (TC1) is also gently adjusted for a further possible increase in output. Now return to the first station with the vanies of the gang more enmeshed, and again slightly adjust the cores of the coils for any slight increase in volume. After this the other station is returned to and the trimmers again adjusted. These adjustments will get smaller and smaller until no further improvement can be realised. At this point you should turn the set over and very carefully adjust the cores in the tops of the i.f.t's starting with i.f.t.2. The adjustment will be extremely small since these are aligned before dispatch, so it may be that very little improvement will be effected. This adjustment will, in any case, be very slight and it would probably be in order to leave the cores of the i.f.t's alone.

The small "speaker" should give reasonable volume for bedtime listening; however, with the prototype, a pair or $2,000 \Omega$ headphones connected


Fig. 8: Layout and wiring of components above chassis.
in its place worked extremely well if not as good as the speaker.

Aerials from 30 to 150 ft . were tried and all gave good results, several foreign stations coming through very well after dark including Radio Luxembourg. A case would be easy to make, and this is left to individual constructors. Any plastic, wood, or even aluminium would suit and should present no problems. It would be in order to fit a headphone jack for late night headphone listening.

Although this receiver is the most complicated of the three in this series, if you think of it as three separate one-transistor circuits, then the wiring is not really so difficult. The circuit, as it stands, is not considered suitable for conversion to other wavebands.

## SOUND LIGHT \& COLOUR

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JULY ISSUE
on sale JULY 12th

## PRACTICAL TELEVISION <br> TRANSISTORISED U.H.F./V.H.F. AERIAL DISTRIBUTION SYSTEM

Constructional details of a wideband u.h.f./v.h.f. amplifier system for driving a number of receivers from a common aerial system.

## VIDICONS

A practical account of the camera tube most used by amateur enthusiasts with setting up details and tips on buying rejects.

## TIME-DELAY FAULTS

How to diagnose those puzzling faults that develop some time after the set is switched on.

AUGUST issue on sale JULY 19th.

# Preamplifier for 'RADIO2' on 1500 metres 

AS a result of the recent reorganisation of BBC programmes and in particular the allocation of the 247 metres wavelength to transmitters radiating the new "Pop Music" programme "Radio 1", listeners in many parts of the country who formerly enjoyed good reception of the Light Programme on 247 metres from their local medium waveband transmitter, are now faced with reception of the "Radio 2 " programme on 1500 metres, unless of course they are fortunate enough to possess a v.h.f. receiver, in which case Radio 2, 3, and 4 are readily available (but an a.m. receiver is still necessary for reception of Radio 1 !).

Whilst the Radio 2 transmitter on 1500 metres is an extremely powerful one, being rated at 400 kW radiated power, its situation at Droitwich inevitably means that some parts of Great Britain are situated at a considerable distance therefrom, and as a result, listeners in these areas are finding that reception of Radio 2 on 1500 metres compares very unfavourably with their former reception of the Light Programme on 247 metres. Not everyone is prepared, or financially able, to face the expense of purchasing a combined f.m. a.m. receiver to ensure reception of all four BBC radio programmes; this problem is particularly acute in the case of elderly persons, frequently pensioners of modest means, to whom radio is a great boon. Equally understandably, this section of the community tends to rely on radio receivers which have seen many years of service and which do not possess v.h.f. facilities.

## Aerial systems

However, before going to the expense of installing a preamplifier such as is described later in this article, it is advisable to first of all ensure that as good an aerial system as possible is in use. The proverbial piece of flex dangling at the rear of the set, or hooked to the nearby picture rail, which sufficed for reception of the local 247 metres transmitter, just will not do to provide a reasonable signal from Radio 2 at a range of 150 miles or more.

The days when practically every house boasted an "L" type aerial reaching from chimney stack to a pole (or convenient tree) in the back garden are long past, but if an outdoor aerial of this type can be erected, using good quality aerial wire and porcelain insulators, it is amazing the degree of improvement in reception which results. A good second best is a vertical rod aerial, mounted on a chimney stack, or on a stand-off bracket from the wall of the house as high above the ground as possible. Suitable copper aerial rods and fixing brackets can be obtained from suppliers advertising in this magazine. Another effective alternative is an aerial mounted in the loft, using the maximum feasible length of good quality aerial wire and proper porcelain or glass insulators. The downlead should


Underside view of the preamplifier.
be taken out at the base of the roof, and carried down the side of the house (separated as widely as possible from any metal rainwater pipes etc.).

None of the abovementioned suggestions can be readily used by people living in flats, bed sitting rooms etc. Modern blocks of flats frequently have a communal TV aerial system, with an outlet in the living room of each flat. This outlet forms a reasonably satisfactory aerial connection for radio purposes, but it is absolutely essential to ensure that the radio receiver to be used has no direct connection between the mains supply and the aerial and earth sockets, i.e., the power supplies to the receiver should be by means of a fully isolating mains transformer, or, if a.c./d.c. techniques are used, both the aerial and earth sockets must be isolated by means of high voltage working capacitors, otherwise there is danger of mains voltage finding its way into the TV aerial distribution system, with possibly costly, and dangerous, results. If no TV aerial outlet is available, one can only "make do" with a picture rail aerial;


Fig. 1: Circuit of the preamplifier.

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this should be confined to the length of not more than two walls of the room, extending the wire to completely circuit the room usually provides a weaker rather than a stronger signal.

If after everything possible has been done to improve the aerial system (attempts to provide a more efficient "earth" connection seem to have little beneficial results in the case of mains operated receivers, at any rate, on Long and Medium wavebands), the 1500 metres programme is still weak, and suffers from excessive background hiss and hoise, consideration should be given to the provision of a preamplifier, which for cheapness and simplicity, can be designed to provide r.f. amplification ahead of the main receiver at the predetermined frequency of $200 \mathrm{kc} / \mathrm{s}$ ( 1500 metres), being switched out of action when any other frequency is desired. Such a unit was constructed by the author, firstly using valves, and then later a transistorised version was built; both have given excellent results in two difficult reception areas in which they have been tried out. It is the latter, the transistorised unit, which will probably appeal to most constructors, and full details of this unit are accordingly given.

## Preamplifier circuitry

The circuit was designed around an AF117 transistor, which is capable of a high level of gain at radio frequencies, yet has a commendably low noise level, and has been found inherently stable in use. After a number of trial and error adjustments to the breadboard prototype, the circuit values shown in Fig. 1 were adopted, and the entire unit re-constructed in a plastic box, with removable lid, measuring approximately $4 \frac{1}{2} \times 2 \times 2$ in. A metal container should not be used, as this could seriously lower the "Q" of the coil L1, quite apart from possible insulation problems.

The circuit (see Fig. 1) operates as follows. Signals from the aerial are fed to section (a) of the changeover switch; with this switch in the "off" position, signals are bypassed, via section (b) of the switch, direct to the coaxial link feeding into the radio receiver's aerial and earth sockets. With the switch in the "on" position however, signals are fed to the aerial coupling winding of L1, this being a Denco Transistor Coil, Type Blue, Range 1, specifically designed to cover the Long Waveband. Signals are induced in the tuned winding (between pins 6 and 7), where, as only a frequency of $200 \mathrm{kc} / \mathrm{s}$ is required to be tuned in, the more usual variable capacitor is replaced by a fixed capacitor Cl connected across the winding.

Denco Ltd., in their data sheet, indicate that a fixed capacity of about 260 pF is required to tune to the Radio 2 frequency, but in the prototype the author


Fig. 2: Lavout of main components. Fig. 3 (right): AF117 connections.
found that a value of 180 pF provided resonance at a midway setting of the coil core. This may possibly have been due to excessive external capacity in the rest of the circuit, constructors should therefore be prepared to experiment with the value of Cl to find the most suitable value. The coupling winding (between pins 5 and 6) provides the necessary low impedance coupling link to the base of TrI, whose correct working conditions for r.f. amplification are set by the values of R1, R2 and R3 in conjunction with their respective bypass capacitors. The amplified r.f. signal appears at the collector of Trl, and the choke/capacity coupling provided by L2 (an r.f. choke of approx. 10 mH ) and $\mathrm{C} 4(0 \cdot 1 \mu \mathrm{~F})$ is used to couple the output to the radio receiver via the aforementioned section (b) of the changeover switch.


Fig. 4: Wiring and component layout of the tagboard.
Output is via the shortest convenient length of standard coaxial cable, terminated at the receiver end by suitable plugs to fit the aerial and earth sockets. The inner conductor is of course connected to the aerial plug, and the screening braid to the earth plug.

It will be noticed that sections (c) and (d) of the changeover switch provide a double pole, on/off switch

## * components list

Resistors:


Capacitors:

$$
\begin{aligned}
& \text { C1 see text (silver mica) } \quad \text { C3 } 0.05 \mu \mathrm{~F} 150 \mathrm{~V} \\
& \text { C2 } \\
& \text { C } \\
& \text { atl } \\
& \text { all } \\
& \text { miniature foil, unless otherwise stated. }
\end{aligned}
$$

Transistor:
Tr1 AF117 Mullard

## Miscellaneous:

Plastic container (with lid) approx. $4 \frac{1}{2} \times 2 \times 2$ in.; 4 pole-2 wayswitch; Denco Blue, Range 1 (transistor) type coit L1; PP3 battery and connector clip; aerial socket; pointer type control knob; 9 -way miniature group panel; r.f. choke approx. 10 mH ; connecting wire; coaxial cable.
The following additional components would be required for the mains supply system in Fig. 7:
$6 \cdot 3 \mathrm{~V}$ pilot bulb and holder; 2-OA81 diodes; $3-25 \mu \mathrm{~F} 25 \mathrm{~V}$ capacitors; $1-2 \cdot 2 \mathrm{k} \Omega \frac{1}{2} \mathrm{~W}$ resistor (see text); twisted flexible wire; tagboard to mount the aforementioned components.
for the battery supply, so that in the "off" position, the battery is completely disconnected, and simultaneously, any signal received by the aerial is bypassed around the preamplifier direct to the radio receiver.
Current consumption was found to be 2.5 mA , so that a PP3 battery, which fits snugly into the space available, will give many hours of useful life. It is a simple matter to remove the lid of the container to replace the battery when necessary.
All the capacitors, resistors, and the transistor, are mounted on a standard miniature 9 -way group panel, only 8 ways being used, the 9 th pair of tags being either bent flat or removed, thus providing a space for the PP3 battery to stand in an upright position. Wiring of the group panel is clearly shown in Fig. 4, whilst Fig. 5 gives wiring details of the changeover switch. In conjunction with Fig. 1, and the layout indicated in Fig. 2 which was used in the prototype, the intending constructor should have no difficulty in assembling this unit.

Connect approx. 6in. of insulated wire, or coaxial cable where applicable, to the changeover switch tag as shown in Fig. 5 before mounting this component through a $\frac{8}{8} \mathrm{in}$. hole in the front of the plastic container. These leads are subsequently shortened as required, to connect to the group panel, battery etc. Smaller holes, $\frac{1}{2} \mathrm{in}$. dia, are drilled in the rear of the container to accommodate the aerial socket and the exit of the coaxial output cable, and a OBA hole is required in the side to allow for fixing of L1. Mount all resistors, capacitors and Tr1 on the group panel (do not shorten the leads of Tr1, and do not forget to use a heat shunt when soldering these leads). Place the completed group panel on the "floor" of the container, and make all external connections from the panel as shown. Lastly, mount L1, and make the necessary connections to its pins, referring to the coding shown in Fig. 1. Cl is soldered directly across pins 1 and 6 . Note that both pins 1 and 9 are connected to the positive "earth" line of the unit, using tag J of the group panel for this purpose. It was not found necessary to secure the group panel to the plastic case in the prototype, as stiffness of the external wiring retained it firmly in position. The fact that the battery stands upon the unused end provides additional anchoring; the battery can be wedged securely in position with scraps of plastic foam pressed down between it and the walls of the container.

## Testing

When assembly has been completed, and all wiring checked, set the changeover switch to the "off" (anticlockwise) position. Insert battery, and connect battery clip. Take great care that polarity is correctly observed (a reversed battery will almost certainly cause instant destruction of Trl). Replace lid of container. Remove aerial from socket of receiver, and re-insert in aerial socket at rear of preamplifier.
Connect the preamplifier coaxial output lead to the aerial and earth sockets of the receiver. Switch on the radio receiver, and tune to "Radio 2 " on 1500 metres, which should be received exactly as before the preamp was placed in circuit. Now turn the switch to "on", and adjust core of L 1 , as resonance is neared, a very distinct improvement in reception will take place. The increase in volume will be partly masked by the a.v.c. action, but a big drop in background noise will be noticed. Adjust L1 for best possible reception. Return switch to "off", and the dramatic diminution


Fig. 5 (left): Connections to SW1. Fig. 6 (right): View of the complete unit.
in performance will be immediately apparent. The preamplifier is left connected at all times, but is of course only switched "on" when listening to "Radio 2". There is only one drawback to the unit, namely that it is possible to inadvertently switch off the main receiver, yet leave the preamplifier switched "on", with consequent unwanted drain on the internal battery. A small pilot lamp could be fitted to show when the preamplifier was "on", but the consumption of even the smallest pilot lamp would be almost ten times that of the unit itself!

## Mains power unit

It is possible to obtain a suitable supply for the preamplifier from the radio receiver, provided this is of the fully isolated a.c. mains type (with double wound mains transformer) using 6.3 V heater supply to the valves. The theoretical circuit of such a supply is shown in Fig. 7. As one side of the receiver's heater supply is normally connected to chassis, as shown in Fig. 7, it will be necessary to insert a $0.1 \mu \mathrm{~F} 150 \mathrm{~V}$ capacitor in the "earth" lead from the preamp. (point X Fig. 2). Switching off the main receiver would of course automatically remove the power supply to the preamplifier. The author has not tried out this modification, but there is no reason why it should not be satisfactory. Some adjustment of the value of the $2 \cdot 2 \mathrm{k} \Omega$ smoothing resistor (in the negative supply lead) might be required to ensure a supply as near as possible to 9 V "on load".


Fig. 7: Circuit of the mains power unit.
However, in view of the low price and long life of a PP3 battery, many constructors may feel it would not be worth while to go to the added expense of a mains power supply for the unit. On no account should any attempt be made to supply the unit from an a.c/ d.c. receiver with series heaters and a live chassis.

## 

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THE Society, formed in January 1960 by 6 stalwarts living in the district, now holds its regular weekly meetings on Thursdays at the Beauchamp Lodge Settlement, 2 Warwick Crescent, London W.2. The meetings cater for all interests commencing with c.w. tuition from 7 to 7.45, and then follows a meeting consisting of lectures, quizzes. film and slide shows, junk sales etc.

The club is on the air most Thursday nights with its own callsign-G3PAD which it also uses regularly in contests, field days, demonstrations at local events etc. The equipment includes a 160 metre home-brew transmitter for phone and c.w.; the "Buccaneer" multiband h.f. transmitter (as described in Practical Wireless, September 1964 (jolly good show-Ed.) for all bands 80 to 10 metres; an HRO receiver; 4 and 2 metre transmitters with complimentary crystal-controlled converters working into a common 10 to $12 \mathrm{Mc} / \mathrm{s}$ i.f. strip.

Antennas include a 400 ft . long wire for 160 and 80 metres; a T2FD (terminated tilted folded dipole) for the h.f. bands; fully rotatable six element yagi for 2 metres mounted on the roof approximately 80ft. up; while a 3 element beam for 4 metres with a 14 element 70 cm beam are to be mounted shortly. The club also possesses a 300 watt generator for portable use.

Membership includes a wide variety of types from topband addicts to DX operators. There is also a v.h.f. section. All these are in addition to the manv


Lorry (G8AZX) operating the 2 metre station.
keen s.w.l's who attend the club. Many of the s.w.l's have benefited, from practical experience gained at the club, in their careers. There is also an active group of G8 plus 3 's on $432 \mathrm{Mc} / \mathrm{s}$, and $1296 \mathrm{Mc} / \mathrm{s}$ equipment is at present under construction.

Being situated in the centre of the town, many overseas visitors find their way to the club and are often persuaded to give impromptu talks on amateur radio operation from their own country. Due to the large number of members who live in flats and are thus deprived of constructional facilities, the club holds a constructional evening on Wednesdays at 8 p.m. with a workbench and test


Eric (G3MHQ) and Alan (G8AOO) at the 1966 Club Field Day. equipment provided.
The club gave a demonstration on amateur radio to the Hackney group Queen's Scouts at Gilwell Park last year, and also intends to enter for the 70 cm contests to be held this year, and v.h.f. n.f.d., also to hold its own h.f. field day.

The club has its own quarterly news letter Key Klix edited by Alex Summers, G3AWS. Each year the Beauchamp Award is presented to the member who has served the club best in the past year. This year it was awarded to s.w. 1 Terry Collins.

Visitors are always welcome and full details are available from the Hon. Secretary, M. A. Pawley, G8AWV, who is known to lurk at 52 Sumatra Road, West Hampstead, London, N.W.6. Why not drop in and see us?

## PART FOUR ...... LOUDSPEAKERS

## IAIN SMITH

SO far in this series I have given some general notes on pick-ups and amplifiers, two links upon which lie a great deal of responsibility for the performance of the whole system. Together, of course, with the turntable drive. These links, however, besides giving a good flat, distortion free, overall response have little else about them to determine the final sound, the tonal balance, of the system. This is the job of the loudspeaker. The quality of the loudspeaker and its enclosure is of the utmost importance. The loudspeaker is the second weakest link in the reproducing chain but whereas one pick-up can sound the same as another, loudspeakers can sound as different as Beethoven and The Beatles. Let us now examine why choice of a loudspeaker is so important. Remember that at one time the loudspeaker was the weakest link. This does not mean that pick-ups have degenerated, rather that loudspeaker design has advanced in leaps and bounds. Research has concentrated on the past weaknesses of loudspeakers and made discoveries and improvements.

## Principles

A loudspeaker works on the motor principle. It consists of a frame with a magnet assembly attached. Within this frame is a wax paper cone with a coil wound on impregnated paper. This coil is suspended in the magnet air gap and the a.c. signal is fed to the coil. This causes the coil to move in and out at varying distances and speeds depending on the signal.


Fig. 5: Cross - section of a typical loudspeaker assembly.

The paper cone, being attached to the coil, moves in sympathy and displaces similar airwaves around the speaker. A cross-section of a loudspeaker assembly is shown in Fig. 5.

## Response

Generally speaking, loudspeakers vary in size according to the job they have to do. Smaller units, 5 in . diameter or less, are usually designed to handle higher frequencies above $3,000 \mathrm{c} / \mathrm{s}$ because these frequencies require smaller mechanical masses to reproduce with minimum distortion. Larger units; of 10 and 12 in . diameter, are better for lower frequencies in the middle and bass register, because these frequencies require larger volumes of air to be moved due to the longer wavelengths involved. Specially designed high frequency units can handle frequencies from $3,000 \mathrm{c} / \mathrm{s}$ to $20,000 \mathrm{c} / \mathrm{s}$ quite efficiently. The same applies to low frequency units in the $20 \mathrm{c} / \mathrm{s}$ to $3,000 \mathrm{c} / \mathrm{s}$ region.

So we have two individual units which if used together can reproduce the whole audio spectrum. How, then do we connect them? We cannot just connect both units in parallel across one signal source. This is because the high frequency unit output will be distorted by the fact that it is being fed by low frequency signals and vice versa for the low frequency unit. Obviously, then, a frequency selective circuit is required and this brings us to the L-C Crossover Filter network.

Figure 6 shows a schematic diagram of a network. Speaker LS1 is the low frequency unit, LS2 is the high frequency unit. High frequencies cause capacitors to present a low reactance and inductors a high reactance and vice versa for low frequencies. Use is made of these reactive properties in this network. High frequencies are easily passed by C2 into speaker LS2 while L2 shunts off the low frequencies. Meanwhile low frequencies are easily passed by L1 into speaker LSI while Cl shunts off the high frequencies. By careful choice of capacitors and inductors the response of LS2 can be made to fall off at the same point as the response of LS2 rises, say, $3,000 \mathrm{c} / \mathrm{s}$. This point is known as the crossover frequency or point, hence the name of the circuit.

A unit becoming increasingly popular is the dual cone unit. This is a low frequency type cone with a small high frequency unit attached to the centre. Although more efficient, as far as power consumption is concerned, than a crossover system, the frequency range does not extend as far, either end of the spectrum. However, development goes on and in the future the crossover network may disappear.

Two main drawbacks of conventional loudspeakers are "cone break-up" and "Doppler distortion". Let us deal first with cone break-up. This occurs due to movement of the cone distorting its shape and hence distorting the waveform produced. Aluminium cones help overcome this problem, being stiffer, and one manufacturer sandwiches aluminium between two layers of conventional cone material, a development which has met with success.

Most readers will be familiar with the Doppler effect, when a moving object emitting sound, shortens the wavelengths in front of it and lengthens those at the rear. The effect is to make, say, the engine note of an approaching car appear to rise in frequency and suddenly decrease as the car passes the listening point. Now imagine a loudspeaker cone emitting two frequencies $100 \mathrm{c} / \mathrm{s}$ and $6,000 \mathrm{c} / \mathrm{s}$. During one cycle of the low note, sixty cycles of the higher note occur, half of them with the cone approaching the listener, the other half with the cone receding. From the explanation of the Doppler effect it can be seen that this is a form of f.m. distortion that can only be produced by the loudspeaker in any sound system.


Fig. 6: A simple crossover filter network.
Cone break-up can be overcome, Doppler distortion is a little more difficult but one new development which should help both is the Electrostatic speaker. In this type of speaker an electrostatic charge is applied to two diaphragms. Application of the signal between the two diaphragms alters the stress between them and hence produces an audio note. At the moment these speakers are mainly used for treble units.

Returning to the conventional type speaker, some points to remember when making a choice. It should be large enough, both in power handling capacity and diameter, to satisfy your needs. Its impedance should be matched to the output impedance of your amplifier. The low frequency resonance should be between $30 \mathrm{c} / \mathrm{s}$ and $45 \mathrm{c} / \mathrm{s}$ for a good low frequency response. The magnet should be a high flux magnet, say 15,000 lines. The cone surround should be flexible but not too sloppy.

No matter how good your speaker is it will only be as good as the enclosure which houses it. For small enclosures the infinite baffle or IB enclosure is the best. The only opening is the speaker aperture and the enclosure must be carefully designed to be tuned to a reasonably low frequency. An enclosure for the home constructor is the bass reflex enclosure. This type of enclosure relies on the fact that most of the bass notes come from the rear of the speaker. Below the speaker is another aperture or port through which the bass notes are reflected to appear in front of the speaker with the treble notes.

The area of this port should be approximately equal to the working area of the speaker cone.

What size should the cabinet be? Approximately $2 \frac{1}{2}$ to $3 \mathrm{cu} . \mathrm{ft}$. minimum for a 10 in . speaker and 5 to 6 cu . ft. minimum for a 12 in . speaker. An ideal material is $\frac{3}{4} \mathrm{in}$. thick chipboard because of the high density and sound absorbent properties. A speaker cabinet should not resonate or reverberate. This adds "coloration" to the sound and can alter the resonant frequency of the enclosure, usually making it higher. An ideological example is a cabinet of concrete but most wives would strongly object to this purely from an appearance point of view!

Internal damping of the cabinet to prevent resonance can be done with acoustic wadding but the amount must be determined by trial and error. Glasswool lin. thick is another good material and in a small unit I have used $\frac{1}{2}$ in. thick foam rubber sheeting with some success. To prevent the speaker aperture being seen through the speaker fabric, paint the board, under the fabric, matt black. To ensure that the speaker fabric is taut use a synthetic material known as Tygan. This can be tightened after the glue has dried by holding an electric fire in front of it for half a minute or so.

Remembering that a good speaker and cabinet is worth the expense, I would summarise as follows:

1. If using a dual cone unit choose one with the widest frequency response.
2. For a good low frequency response the cone resonance should be $30 \mathrm{c} / \mathrm{s}$ to $45 \mathrm{c} / \mathrm{s}$.
3. The magnet should be high flux around 15,000 lines.
4. The impedance should be matched to the amplifier.
5. The power rating should be matched to the amplifier.
6. With separate units for bass and treble a crossover filter network will be required.

## To be continued

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## 1 WATI INT

A.J. MCEVOY, B.SC.

RECENTLY we read in P.W. of the RCA CA3020. This is a neat little product, providing 500 mW in a single-ended push-pull circuit. The unit appears in a transistor style TO-5 twelve lead container, and is quoted as being capable of operation from $-55^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$. In consumer and industrial products, however, the ruggedness specified for military applications is unnecessary, but a little more power would be appreciated, and it is at this point that the General Electric Corp. makes a challenge with its PA222, now available in the UK at 42 s . It can provide up to 1.2 watts into a load of not less than $15 \Omega$. As in most things, however, the result is reached by a compromise, and it should not be concluded that the CA3020 amplifier, described some time ago in these pages by $L$. McNamara, is superseded by the design which follows. The earlier circuit operated from a 9 volt battery, and therefore was compatible with portable transistorised apparatus, whereas the G.E. unit requires a 22 volt supply for full output. Similarly, some form of heatsink proves essential, as a result of the greater power dissipated in the circuit, and the extremes of temperature which the CA3020 can tolerate would endanger the PA222. None the less, it is an example of competent semiconductor engineering, and the manufacturer is justified in recommending it for record players, radio sets and intercoms. In the circuit to be described, the power supply is not included on the circuit board, as some constructors may wish to use the unit on batteries, e.g. two PP9's in series; a suitable power unit could consist of a transformer with a $15-18 \mathrm{~V}$ secondary, plus 0.5 A bridge rectifier and a $5000 \mu \mathrm{~F}$ smoothing capacitor.

## Circuit operation

Now to examine the circuit itself. It is somewhat larger than the integrated circuits the constructor may already be familiar with, being a full 0.77 in . long! This epoxy moulded shell is a G.E. modification of the 14-pin "dual in-line" package, introduced in the USA for more economical integrated circuits not subjected to environmental extremes. The modification consists in the reduced pin requirement, and the provision of a heatsink tab at the end of the unit. In fact, this tab extends right to the centre of the moulding, and the chip of silicon, into which all the components of the circuit are integrated, is
mounted on it. In use, the tab is soldered to an area of copper foil, which should be as extensive as is convenient for better heat dispersal. However, even with a good thermal contact, at full rating it is still possible for the tab to reach $50^{\circ} \mathrm{C}$.

Electrically, the circuit follows established IC practice, being a monolithic epitaxial silicon unit with a preference for $\mathrm{N}-\mathrm{P}-\mathrm{N}$ transistor configurations. Seven active elements are integrated into the chip-six transistors and a diode, as well as six resistive areas.

As can be seen in Fig. 1, the signal is first applied to the base of Tr 1 , a conventional common emitter amplifier stage. Here provision is made for an external load resistor, and due to the spread of characteristics between individual units, no definite value for this resistor is specified in the components list. Instead, as part of the test programme at the factory, a suitable value is determined by the manufacturer, and this is stamped on the plastics moulding of each IC. The resistor will be $68 \mathrm{k} \Omega, 100 \mathrm{k} \Omega$, or $150 \mathrm{k} \Omega$, so the moulding will be marked $R 68 \mathrm{k}, \mathrm{R} 100 \mathrm{k}$, or R150k. The amplified signal developed across this resistor, R 7 in the circuit diagram, then enters the base of Tr2, a split load phase splitter. It may be objected that the resistive elements serving as emitter and collector loads here are unequal; but then, so also are the impedances into which the signals developed across them are fed, and signal equality is thus maintained.

It is now possible to regard $\operatorname{Tr} 4$ and $\operatorname{Tr} 5$, and Tr3 and Tr6, as super alpha pairs in series connected single ended push pull. Since a low output impedance is a characteristic of this type of circuit,


Fig. 1: Diagram of the G.E. PA222 integrated circuit.
a good match to a 15 to $25 \Omega$ loudspeaker will be obtained. The diode D1 operates as a latching diode in the negative half of the output signal cycle, maintaining full drive.

The performance of the unit in a practical amplifier is in great measure controlled by the external elements used with the IC, and in the circuit to be described, two separate feedback loops are used. First there is a d.c. feedback through $\mathbf{R 8}$; this is in fact the base bias supply for Trl, which due to the internal circuitry of the IC, is dependent on the currents in the emitters of Tr 2 and Tr 3 . Should these increase, the base bias will increase; since then the current in RI will increase, the base voltage on Tr 2 will drop, tending to restore the original situation. The effect on the overall d.c. stability of the amplifier is obvious. Further, the reader will now realise the importance of the correct choice of R7; if it is too low, the power dissipated in the circuit will be unnecessarily large, whereas if it is too high, the output stages are starved, resulting in distortion.

The question of a.c. stability should also be considered. As is well known, the epitaxial transistor excels at high frequencies, and in a direct coupled amplifier such as this, there is no inherent frequency limitation. An r.f. suppressor C4 is therefore added across the input terminals, and together with the impedance of the signal source, it introduces a time constant limiting high frequency performance. (If necessary, with a very high impedance source, a $27 \mathrm{k} \Omega$ resistor may be placed across the input terminals.) To this high frequency cut-off eliminating r.f. instability there is added an a.c. feedback loop to correct the performance of the unit for audio frequencies. R9 and R11 form a potential divider across the audio output of the unit, and the signal developed across R11 is returned to pin 1 of the IC, the emitter of Tr1. This transistor acts as a common base amplifier towards this feedback signal, and therefore the performance of the circuit over the audio range is linearised. Other r.f. suppression components are C 7 in the collector circuit of Trl , and R10-C6 across the audio output.

## Construction

With this understanding of the operation of the circuit, construction can begin. The regular reader will be familiar with the procedure for preparing printed circuit boards, using lacquer paint to protect the conductor areas of copper foil on a sheet of laminated paxolin while removing the unwanted areas with a concentrated $\mathrm{FeCl}_{3}$ solution. Remembering the function of part of the copper foil as a heatsink as well as an electrical conductor, it will be realised that veroboard is unsuited to this application, unless a separate square of copper, lin. square, is soldered to the reverse side of the board, bridging several of the conducting strips, close to the tab of the IC.

## $\star$ components list

## Resistors:

| R7 | see text | R10 | $22 \Omega$ |
| :--- | :--- | :--- | :--- |
| R8 | $22 \mathrm{k} \Omega$ | R11 | $10 \Omega$ |
| R9 | $470 \Omega$ |  |  |

(R1-R6 are contained within the integrated circuit).

## Capacitors:

| C 1 | $0.1 \mu \mathrm{~F}$ | C 5 | $10 \mu \mathrm{~F} 25 \mathrm{~V}$ |
| :--- | :--- | :--- | :--- |
| C 2 | $200 \mu \mathrm{~F} 25 \mathrm{~V}$ | C 6 | $0.001 \mu \mathrm{~F}$ |
| C 3 | $10 \mu \mathrm{~F} 25 \mathrm{~V}$ | C 7 | 350 pF |
| C 4 | $0.001 \mu \mathrm{~F}$ |  |  |

Integrated circuit type G.E. PA222, Jermyn Industries, Vestry Estate, Sevenoaks, Kent.
Price is $42 /-$ plus p. \& p.


Fig. 2: Circuit diagram of the complete amplifier, suitable for use with a medium impedance microphone or pick-up.


Fig. 3: Layout of the printed circuit board (copper side). Only the PA222 is mounted on this side.

Actual assembly of the unit on the circuit board follows standard methods. It might be well to mount
the IC last, to avoid damage due to overheatıng. The soldering of the tab should be done with special care as it is to be a thermal and electrical conductor, so that a generous amount of solder, on the tab and the surrounding copper, is worth while. This area should be pretinned, so that the solder will be in place when the IC is inserted, and only the proximate area will require remelting to adhere to the tab. Then the rest of the solder will rapidly dissipate the heat in the melted zone.

## Testing

All will now be ready for test, and a signal source, power supply and loudspeaker can be connected. As already mentioned, the speaker should be of at least $15 \Omega$, and there should be vigilance to prevent accidental short circuits of the loudspeaker connections; should these be allowed to persist for more than a very short time, there will be excessive dissipation in the chip, with the possibility of damage. When switching on for the first time, it would be wise to insert a milliammeter in the power supply line; the current drawn should be approximately 25 mA . with no signal. This will rise immediately any audio output is drawn from the circuit, a characteristic of all class $B$ push-pull amplifiers, reaching a maximum of 115 mA at full output. This figure, for 1 watt output, indicates an overall efficiency for the amplifier of almost $50 \%$, a quite creditable performance.


Underside view of the complete amplifier showing layout of components, other than the I.C.

As most of the assembly of electronic elements in the circuit is completed in the manufacturing of the IC, it is unlikely that any troubleshooting will be necessary. The following points are, however, worth noting. Provided the correct value for R 7 is used, the most probable cause of excessive dissipation, or high quiescent current, is a leaky capacitor C3 changing the base bias applied to Tri. Should distortion occur, suspect the capacitor C5, which is intended to ensure full drive during the positive half of the output signal. (Diode Dl has this function for the negative half.)

The applications of the amplifier are left to the initiative of the reader; it is hoped that successful assembly and operation of this IC amplifier will inspire the same enthusiasm for these components in the constructor as it has in the writer of this article.


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# practically Wireless commentary by IENTI 

LAST month's venture into the hurly-burly of wireless politics may be expected to give Henry-and the Editor-a few bruises. So, while the liniment is still out, let's look at the parallel problem of wired systems.

Problem it is, for the Radio and Television Retailers' Association is still, at the time of writing, having a bitter wrangle with the Greater London Council over an award of a contract to Rediffusion that involves a cool $£ 600,000$. This was a 15 year contract awarded early in the year for wiring a v.h.f. distribution system for television and sound to 9,000 council dwellings and 8,000 homes by private developers.

Let me block in a few details. By 1970 all three existing television programmes should be radiated on 625 lines u.h.f., and duplicated (BBC and ITA) on 405-lines v.h.f. This means that all dual-standard receiver owners will be able to receive the broadcast programmes, provided that they have an adequate aerial installation and live within the 99.5 per cent coverage area. For those that don't, and for many others that receive unacceptable quality of picture or sound, the various relay systems will be a necessity.


An adequate aerial installation

But-and it is a big butrelay systems are formidably costly when translating u.h.f. signals, and relaying u.h.f. is out of the question because of cable losses. And whereas the BBC is battling hard for better u.h.f. coverage, and has evinced an optimism about future developments which members of the Royal Television Society regarded with some scepticism at a recent forum, the ITA appears to be thinking along different lines.

The radio retailer wants to be able to sell a set that satisfies his customer aesthetically, as well as being capable of picking up the programmes in any given area, whether these are broadcast or piped. Which argues that v.h.f. wired systems are the answer. The normal dualstandard television receiver will pick up the radiated u.h.f. and v.h.f. signals, plus any piped signal from a relay company on an unused v.h.f. channel. A relay network should work with normal sets, they say.

But Rediffusion are battling hard for h.f. systems. At an earlier Royal Television Society meeting, R. P. Gabriel, technical director of Rediffusion Research, brought up some impressive arguments for h.f. systems. Even on grounds of costs in rural areas, he asserted that wired sound-and-vision could hold its own. A feasibility study at Wooler showed that transmitter costs could be up to $£ 50$ per home, while the network cost, based on three-core cable, reed switches and diode logic, and even assuming new cable posts for all remote areas, could be reduced to $£ 32$ per home. He forecast that purely broadcast reception would eventually nullify any of the advantages at present enjoyed by the higher frequency bands and lead to the
sort of chaos we are all familiar with on the medium waves.

Moreover, he argued, the wired systems eliminated the real weak spot of the average receiver, the tuner unit, if h.f. relay rather than v.h.f. wired systems were employed.

Which is where we came in, for it was a v.h.f. system that was agreed in principle by the G.L.C. for the Thamesmead contract. Five firms tendered for this (including Rediffusion,


There are hot words flying
we should add), and then the committee decided to extend the invitation to h.f. systems, and Rediffusion collared the award.

Mr. Michael Keegan, director of RTRA, is understandably up in arms. H.F. systems rule out Woolwich and District Traders TV Relay Ltd., and prevent the ordinary dealer from selling any set 'from the shelf'. But Rediffiusion argue that normal sets are simplified front ends can always be used, and that special sets are available from a number of firms, and can be installed by local dealers.

Altogether, there are hot words flying. Henry has tried to be objective, and feels sure that readers with a vested interest in wireless reception will have a few opinions to offer.

The floor is yours, gentlemen.

# repairing radio sets 

## PART 5


#### Abstract

We have now arrived at the stage where we will examine, step by step, the servicing of a six transistor domestic receiver.




NOW that we have a reasonable grounding in the elementary theory of semiconductor diodes and transistors and a fair knowledge of the static and dynamic conditions under which "circuit blocks" in transistorised equipment operate, we are in a good position to concentrate more on the servicing angle, based on the popular transistor radio.

It has already been intimated that general servicing resolves to three basic actions. These are (i) locating the faulty stage or section (fault diagnosis), (ii) finding the faulty part or wiring in the located stage and (iii) making the repair (such as clearing the shortor open-circuit or replacing the component). Sometimes action (i) will reveal some maladjustment, like misalignment of the tuned circuits, in which case the "repair" will be to restore the tuning by realignment and so forth.

Mr. Hellyer, in his parts, is telling about making the actual repair, soldering and the mechanical aspects of the exercise, so this final article dealing mostly with the electronics of radio will focus most attention on actions (i) and (ii).

A block diagram of a typical "domestic" transistor set is given in Fig. 22. Recapitulation on the process involved will not be amiss: the aerial, which is a ferrite rod, abstracts the electromagnetic component of the passing radio wave and produces an r.f. signal voltage across its appropriate winding(s). This is fed to the frequency changer to produce the i.f. signal by heterodyning with the local oscillator signal. The oscillator is tuned "in gang" with the aerial tuning to maintain a frequency-difference equal to the i.f., and this signal is then amplified by the i.f. stage.

The detector rectifies the modulated i.f. signal and delivers an a.f. signal corresponding in nature to the envelope of the modulation. It also produces a d.c. voltage from the i.f. carrier-wave, which is fed back to the i.f. stage as a.g.c. bias.

The a.f. signal is applied to the a.f. stage and thence to the output stage which drives the loudspeaker. In other words, the output stage converts the a.f. signal to power required by the loudspeaker. Power for the transistors is usually given by a battery or series of cells, although some sets have mains power packs.

## FIRST CHECK— TOTAL CURRENT

Now, if we are presented with a "dead" set, the first move is to discover where the discontinuity exists. However, before this trend is commenced, it is just as well to make sure that the battery or power supply is "energising" the circuits. The quickest action here is to break the supply positive lead and introduce a current meter in series, as shown in Fig. 23. An average transistor set passes about 14 mA when there is no output from the loudspeaker. This is called the quiescent current, and when delivering about 250 mW (about maximum for a small set) the current can rise to almost 50 mA .

Since the set is "dead", we should not get a reading anything like 50 mA . Indeed, the reading could be below the quiescent current value as a result of the fault. On the other hand, it could be well above the quiescent value even with zero loudspeaker output if the fault is caused by a bad electrical leak or short in component, transistor or circuit

If the current is substantially above the quiescent value, the battery should be disconnected and an attempt made to locate where the extra current is being dissipated. Large current means that something must be getting pretty warm, and this might be a transistor. A transistor warm to the touch when the set is quiescent is a fair indication either
that the transistor is faulty or that its biasing is seriously incorrect.

This is where our grounding in the static conditions of transistor circuits will pay dividends, and it is not intended here to repeat what has already been said on this subject.

If there is a zero current, check the battery voltage under load conditions. This requires the connection of a resistor across the battery, as shown in Fig. 24, for open-circuit voltage measurement with a high resistance voltmeter means nothing! The resistor should have a value to pass about 50 mA , but do not leave it connected across the battery too long. Calculation is easy, calling for the application of Ohm's law. That is, dividing the battery voltage by the current in amperes. The resistance value is then in ohms. A value of 180 ohms will thus pass 50 mA at 9 V . Use the nearest preferred value. If the battery then measures more than 1 V below its nominally rated voltage, its resistance is rising; but it would still work. If the voltage falls by 25 per cent or more the battery should be replaced.


Fig. 23: Showing how the total current of a transistor set is measured.


Fig. 24: A transistor battery should be checked under load, as this diagram shows.

Assuming now that the quiescent current is reasonable we can start hunting for the faulty stage. There are two basic ways of doing this: (i) using the loudspeaker as an indicator of signal and (ii) using a separate indicator which can be moved from stage to stage. Let us take (i) first.

## STAGE-BY-STAGE TESTING

The plan is to apply suitable signal to each stage in turn until (a) we get an output from the loudspeaker or (b) until the output ceases; (a) and (b) depend on whether the test signal is applied at the front working towards the loudspeaker or at the loudspeaker working back towards the aerial. If we use (a) we would (1) apply modulated r.f. signal to aerial circuit, (2) to the frequency change, (3) modulated i.f. signal to the i.f. stage, (4) audio signal to the a.f. stage, (5) audio signal to the output stage and, finally, (6) audio signal (power) to the loudspeaker. At some point along the line we would get a response from the loudspeaker. Say there was no response with input at (1) or (2) but response with input at (3), the trouble would obviously lie in the frequency changer or coupling to the i.f. stage.

By using scheme (b) we would apply the audio first to the loudspeaker and then work back towards the aerial until the response ceases. If, for instance, we get a response with the input at point (5) but not at point (4), the discontinuity would exist in the a.f. stage or coupling to the output stage. The signal injection point numbers used above are indicated on the block diagram in Fig. 22.

Whether scheme (a) or (b) is used is essentially a matter of preference. One is not particularly quicker than the other, for if we use scheme (a) and find that the loudspeaker is open-circuit we would not have used any more time than if (b) were used and the aerial was found to be open-circuit. Many technicians, including H.M. Forces, prefer scheme (b). The practising service technician is used to employing both schemes. If one is measuring the performance of the equipment, stage by stage, then by establishing a calibrated output meter in place of the loudspeaker, the level of test signal required to give a "standard" output can quickly be determined at each stage.

## SIGNAL TRACING

Method (ii), involving the use of a signal detector, or signal tracer as it is called, has much in its favour from the domestic transistor set point of view. In many cases the signal as picked up by the set's aerial can be used, and the idea is to tap the probe, stage by stage, from the aerial towards the loudspeaker, listening for the signal at each point.

Very sensitive probe-type detectors use headphones or earpieces, and the signal actually at the ferrite rod aerial winding can be heard on some of them. This equipment consists of a simple rectifier followed by a stage or two of a.f. amplification, terminating across the 'phones or earpiece.

The plan, then, is to tap along the circuit until the signals cease, at which point the break exists. If we use Fig. 22 for illustration again, signal at (1), (2) and (3) but not at (4) would indicate discontinuity somewhere between the i.f. and a.f. inputs. A signal tracer can also be used to "test" the detector stage more conveniently than the schemes previously outlined. This is because this sort of instrument is designed for switching straight into its audio stages, thereby permitting amplification of any audio present across the set's detector load.

For example, if i.f. signal is "heard" at the detector input, while no signal can be heard across the load, the detector diode is probably shorting or opencircuit.

In practice, it is rarely necessary to run through the whole sequence of signal tracing or stage-by-stage testing because the set itself, even in its "dead" condition, often yields clues. Most sets give a "thump" from the loudspeaker when switched on due to the output transistors passing a current pulse through the loudspeaker. If this occurs on the faulty set, one can be sure that the loudspeaker and output transistors are passing current, at least; also, of course, that the power supply is active.
The first move in this event, therefore, would be establishing that the rest of the audio section is active. This can be done by applying an audio signal to point (4) in Fig. 22. If this signal gets through to the loudspeaker, then one would signal-trace or stage-by-stage test in the r.f. and i.f. stages.

A quick test for audio "liveliness" in valved sets is to touch the control grid of the a.f. valve with a finger or with the blade of a screwdriver with a finger resting on the blade. A very loud hum is produced by the loudspeaker if all is well. This same test does not work so well in transistor sets or amplifiers because there is no mains input, and the hum that is heard is mains hum. Nevertheless, a weak hum is often present when the set is being serviced in mains-
wired environments, and when a finger-connected screwdriver blade is used very loud crackles (if not hum) should emanate from the loudspeaker when the blade is scraped on the a.f. transistor base.

Complementary to the signal tracer is the "signal injector". This is a small transistorised testing probe or box containing a multivibrator. This is rich in harmonics of the fundamental frequency, and wherever applied to a transistor signal circuit will give an output from the loudspeaker. Thus, it is a simple matter to work to and fro' along the stages until the point where the signal appears or ceases is located. More detailed testing might then be needed to reveal the actual component responsible for the defect.

One disadvantage of this instrument is that it can give an output when applied to the aerial circuit, even though the set is otherwise dead. This is when the trouble is due to failure of the local oscillator; so really the instrument could be used indirectly to tell whether the local oscillator section is at fault !

## TRANSISTOR SET CIRCUIT

So much for stage-by-stage testing and signal tracing in transistor sets. Let us now try to tie this in with the circuit. Figure 25 shows a circuit of a fairly recent transistor portable, and this is divided into the stages shown in Fig. 22.
The ferrite rod aerial contains two main sets of windings, one tuning the medium-waves and the other the long-waves. The top winding allows the connection of a car-type aerial.

The signals are tuned by the aerial section of the gang, C3, and applied to the base of the frequency changer transistor Tr . The collector/emitter circuit
of this transistor is also arranged in the form of an oscillator in conjunction with the oscillator coils, and tuning here is by C8, ganged to C3.

The i.f. signal developed in the collector circuit of Tr 1 is tuned by the first i.f. transformer (i.f.t.1) and thence coupled to the base of the i.f. transistor $\operatorname{Tr} 2$. The second i.f. transformer (i.f.t.2) tunes the signal again in the collector and couples it to the detector diode D2. R11, in conjunction with the volume control R12, forms the detector load, with C16 acting as the i.f. bypass.

The a.f. section consists of the complementary transistors $\operatorname{Tr} 3$ and $\operatorname{Tr} 4$, the collector of the former in d.c. connection with the base of the latter. $\operatorname{Tr} 5$ and $\operatorname{Tr} 6$ are the output transistors, also in complementary mode. These complementary circuits were considered in Part 3.

The loudspeaker is coupled to the junction of Tr5 and Tr6 emitters through the electrolytic capacitor C23. The jack socket for headphones or tape recorder coupling disconnects the loudspeaker when a jack plug is inserted.

Tr1-Tr4 are in the common-base emitter (signalwise), $\operatorname{Tr} 1$ having R4 and R5 to set the base bias and Tr3 having R13 and R14. Base bias for Tr4 is achieved by the d.c. coupling, as explained in Part 3, while the bias for the i.f. transistor $\operatorname{Tr} 2$ is obtained by the potential-divider effect (across the supply) of R8 in the upper leg and the series combination of R10, R11 and R12 in the lower leg.
This is where a.g.c. is applied, for across the detector load (R11 and R12) develops a positive potential of magnitude depending on the strength of the i.f. signal applied to the detector diode D2. This potential counters the negative position at Tr 2


Fig. 25: Circuit diagram of a commercial transistor set, showing the stages detailed in Fig. 1.
base fixed by the potential-divider, and the stronger the i.f. signal (i.e., signal picked up by the aerial), the greater the counteracting effect. This reduces the gain of the i.f. stage accordingly, and thus sets the gain to suit the strength of the input signal.

This is called reverse a.g.c. Sometimes forward a.g.c. is applied. In this case the a.g.c. potential adds to the potential at the base supplied by the potential-divider. This causes an increase in collector current, and a resistor in series with the "cold" side of the collector load produces a greater, volts drop, which is reflected as a decrease in collector voltage. Special transistors are also available for optimum forward a.g.c. effect.

Diode D1 assists the a.g.c. action by damping the tuned circuits when the input signal is very strong. This diode is biased from the emitter of Tr2, and the circuit is arranged so that the damping increases when the diode conduction increases, as happens when Tr2 collector (and hence emitter) current falls due to the a.g.c. action earlier described.

The transistors in Fig. 25 circuit are alloy-diffused type, and the high gain possible from the i.f. stage satisfies the requirements for a small set. Some sets, especially earlier models using alloy-junction transistors, feature two i.f. stages. The line-up would then be OC44 frequency changer followed by two OC45 stages.

The low value of feedback capacitance of the alloy-diffused AF117 makes i.f. neutralisation unnecessary, but some earlier models will be found to have neutralised i.f. stages. These were illustrated in Part 3.

So far, we have investigated the action necessary with a "dead" set. In practice, the connection of instruments and test probes is nowhere near as easy as verbal description implies! Most sets are built upon printed circuit boards, making it very difficult to establish connection to the required circuit. Fortunately, the components are numbered on the printed circuit boards (in many sets, anyway!), so it is really essential to have to hand a circuit diagram on which the components carry the same reference numbers. It is then relatively simple to locate the circuit to which instrument or test connection has to be made.

## CONNECTING-IN

It is virtually impossible to clip on to a conductor, or even component wire, of a printed circuit board assembly, so once the required circuit has been located it saves a great deal of time to solder on a short length of 22 s.w.g. tinned copper wire as a "test point". This facilitates the connection of test equipment.

Signal from a generator can easily be coupled to the aerial from the "car aerial" socket if fitted. Alternatively, a loop of three or four turns of wire placed near the ferrite rod should be connected across the generator output lead. On no account should the generator be connected direct to the aerial coils themselves, as this practice heavily damps the tuned circuits and makes alignment and tuning tests virtually impossible.
Tests in the i.f. stages can be at either base or collector, depending on the requirements. But it is best to feed the generator signal to points such as these through a capacitor of about $0.01 \mu \mathrm{~F}$ (a higher
value is needed to couple-in and extract audio signal).

There should be no problem in identifying the positions marked on the block diagram in Fig. 22 with the actual circuit positions in Fig. 25. All sets follow the general pattern outlined.
So much, then, for the "dead" set; let us now investigate other faults that occur in transistor sets.

## LOW SENSITIVITY

This is a fairly common symptom, and the most common cause is a battery nearing exhaustion. This should be the first test, as shown in Fig. 23. Transistors, unlike valves, rarely lose "conductivity" (emission, so to speak), so while it is desirable to check valves on a tester or by substitution, this should not be one of the initial actions when testing a transistor set for low sensitivity. Indeed, it is often a watchmaker's job extracting transistors from small sets.
D.C. testing, as explained in Part 1, will generally bring to light a defunct transistor without having to remove it from circuit. Open-circuit bypass capacitors in the base or emitter circuit will cut sensitivity without affecting the d.c. conditions. The best check is by shunting each suspect in turn with a test capacitor of about $0.5 \mu \mathrm{~F}$.

The stage gain of a section can be measured, if one has the equipment, by applying a signal of known level to the input and measuring the signal on a valve-type voltmeter (or transistor-type voltmeter) at the output. The gain, of course, is given by dividing the output signal by the input signal. and this can be converted to decibels if required. Input and output impedance is important with this kind of test, especially when decibels are used to express the gain.
If the gain appears to be low in a stage or stages containing a tuned circuit, misalignment could well be responsible, and this may come about by alteration in value of a fixed tuning capacitor as well as by unskilled tampering with the tuning cores. For example, C6, C10 or C12 in Fig. 25 (across the i.f. transformer windings) could have altered in value. This is shown up, however, by the associated core failing to bring the circuit into proper tune. A word of warning here: it is bad practice simply to "peak" the i.f. tuning to improve sensitivity, for in some sets the tuning is staggered and peaking could encourage instability.

When realignment of transistor sets becomes necessary (or if it has to be checked), it is bighly desirable to refer to the maker's manual or to a service sheet for the correct procedure, as this differs between sets. Remember, though, that the sensitivity of the aerial is adjusted by sliding the coils along the ferrite rod (in addition to the trimming of the aerial coils). This action changes the inductance, being maximum with the coils in the middle of the rod and decreasing as they are slid towards either end.

A broken ferrite rod will impair the sensitivity considerably. The best action here is to replace the rod. If a replacement is not available, however, it is possible to cement the broken pieces together, using a commercially produced cement that adheres without heat treatment. The broken section or sections should be pushed very tight together and it is important that the rod remains straight when repaired.

## INSTABILITY

Open-circuit decoupling capacitors can cause this symptom, especially in the audio stages. (Such effects are given on Bands 6 and 7 of the fault symptoms record).

Open-circuit C18 or C24 in Fig. 25 are a common source of instability, especially noticeable as the internal resistance of the battery rises.

Peaking i.f. transformers which are designed for "stagger tuning" is another cause in which the amateur becomes involved. Sets with neutralising of the i.f. stages are particularly prone to instabilty if the i.f.'s. are maladjusted or if the neutralising capacitor changes in value. When replacing i.f. transistors in sets of this kind, it may be necessary to re-neutralise, depending on the stability of the basic design.

It is often necessary to replace older transistors with more recent ones of higher gain. This can encourage instability, and to overcome this the base potential-divider values should be altered to reduce the base bias (i.e., increase the value of the top arm). When a higher-gain frequency changer transistor is used, the set may burst into oscillation towards the high-frequency end of the medium wave band. Again, reduce the base bias; but if this does not cure the trouble, the value of the emitter capacitor should be reduced. This is C7 in Fig. 25. Incidentally, this capacitor controls the amplitude of local oscillator signal, and when a lower gain transistor is used, the value may have to be increased to sustain oscillation over the bands.

Lack of oscillation is a common fault, particularly with older sets. The oscillator coils are sometimes responsible, but in some. cases the older type frequency changer transistor has a reluctance to oscillate. Oscillation can be checked by connecting a voltmeter across the emitter resistor and shorting out the oscillator tuning capacitor (C8 in Fig. 25). If the stage is oscillating, a change in meter reading should occur when the oscillator tuning is shorted (see Test 1 in Fig. 25).

## DISTORTION

Distortion (Symptom 9) mostly results from unbalance or incorrect biasing in the audio sections. Low-level distortion is often caused by unbalance of the two output transistors. This causes secondharmonic distortion at low as well as high levels.

Another common distortion, explained in Part 3, is crossover distortion due to the quiescent current of the output transistors being too low. Crossover distortion is also present at low levels, and can be seen by monitoring the signal across the loudspeaker on an oscilloscope when a sinewave signal is applied to the driver stage.

Remember, also, that low battery voltage greatly encourages distortion, and the first action, therefore, should be to test the battery or replace that in use with one known to be in good condition.

Other causes of distortion have already been given in Part 3.

We have now covered almost all aspects of transistor radio servicing, but it is essential for the amateur and student to read this final electronics article in conjunction with Parts 1 and 3 , which deal with d.c. and signal operating conditions.

TO BE CONTINUED

## Youn

QUESTIONS ANSWVERED

## Audio Thump!

Is there any way of eliminating the "thump" in the loudspeaker when switching on a mainsenergised transistor amplifier?

This appears to be due to the smoothing capacitor in the power supply being uncharged at the moment of switching on and therefore momentarily inoperative.
If, having switched on, the amplifier is then switched off and then immediately on again, there is no thump. However, if a few seconds are allowed to elapse before switching on again, the thump returns.-S. Pinder (Weston-super-Mare).

If the thump is due to the charging action of the capacitors in the power supply, then we suggest that you check that these capacitors are in good condition. You might also try the effect of including a small resistor of suitable wattage rating between the output of the rectifier and the reservoir capacitor which will limit the charging current. The value of this resistor might prove fairly critical and perhaps a value of $47 \Omega$ would be a suitable value to start.

You should also investigate the possibility of employing a suitable Thermistor in series with the feed to the capacitors. This would give a high series resistance until current was drawn from the power supply. Suitable Thermistors are made by firms such as Standard Telephones and Cables Limited, Footscray, Sidcup, Kent.

## Technical Terms

Could you please send me a complete list of the technical terms in use in wireless and electronics today as I am a comparative newcomer to the world of electronics?-J. Edwards (Anglesey, N. Wales).

It is far beyond the scope of our query service to supply a complete list of technical terms. We suggest, however, that you obtain a copy of our Practical Wireless Radio and Television Reference Data from your local bookseller. A nother useful book is Dictionary of Radio and Television which is also published by this company.

## S.W. Converters

I am hoping to build a shortwave converter but I am not sure of the principle involved. Each time the tuning capacitor in the converter is altered to cover a different frequency its output frequency will alter and therefore the broadcast receiver, which it is feeding, will need to be re-tuned for each station received. Is this so?-C. Reading (Ruislip).

Converters for use with broadcast receivers, in effect, enable the broadcast receiver to be used as an i.f. amplifier. All of the incoming signals are converted, and appear at the output of the converter at one single frequency-often $1: 6 \mathrm{Mc} / \mathrm{s}$. In effect, a converter is the front-end of a normal superhet receiver, in which the role of the i.f. amplifier is played by the broadcast receiver which remains tuned to the unvarying i.f. of the output of the converter. Thus the output of the converter remains constant.

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## THE BROADCAST BANDS

by CHRISTOPHER
DANPURE

T\HE year is certainly on the move, with July upon us and with good conditions, especially during night hours those log books should be full of interesting entries. So to help you even further here are this month's propagation predictions.
West Africa: $1000-1600,25,21,17$ and $15 \mathrm{Mc} / \mathrm{s}$; $1600-1800,25,21,17,15$ and $11 \mathrm{Mc} / \mathrm{s} ; 1800-2000,25$, $21,17,15,11,9,7,6$ and $5 \mathrm{Mc} / \mathrm{s} ; 2000-2400,21,17,15$, $11,9,7,6$ and $5 \mathrm{Mc} / \mathrm{s} ; 2400-0200,17,15,11,9,7,6$ and $5 \mathrm{Mc} / \mathrm{s} ; 0200-0600,17,15,11,9,7,6,5$ and $4 \mathrm{Mc} / \mathrm{s}$; $0600-0800,21,17,15,11$ and $9 \mathrm{Mc} / \mathrm{s} ; 0800-1000,2117$ and $15 \mathrm{Mc} / \mathrm{s}$.
South Africa: 0800-1400, 25 and $21 \mathrm{Mc} / \mathrm{s} ; 1400-1600$, 25,21 and $17 \mathrm{Mc} / \mathrm{s}$; $1600-1800,25,21,17$ and $15 \mathrm{Mc} / \mathrm{s}$; 1800-2000, 21, 17, 15, 11 and $9 \mathrm{Mc} / \mathrm{s} ; 2000-2200,21,17$, $15,11,9,7,6$ and $5 \mathrm{Mc} / \mathrm{s} ; 2200-2400,17,15,11,9,7$ and $6 \mathrm{Mc} / \mathrm{s} 2400-0400,11,9,7$ and $6 \mathrm{Mc} / \mathrm{s}$; $0400-0600$, 11 and $9 \mathrm{Mc} / \mathrm{s} ; 0600-0800,21,17$ and $15 \mathrm{Mc} / \mathrm{s}$.
East Africa: $0800-1400,25,21$ and $17 \mathrm{Mc} / \mathrm{s} ; 1400-$ $1600,25,21,17$ and $15 \mathrm{Mc} / \mathrm{s} ; 1600-1800,25,21,17,15$ and $11 \mathrm{Mc} / \mathrm{s} ; 1800-2000,17,15,11,9,7$ and $6 \mathrm{Mc} / \mathrm{s}$; $2000-0200,15,11,9,7,6$ and $5 \mathrm{Mc} / \mathrm{s} ; 0200-0400,15,11$ and $9 \mathrm{Mc} / \mathrm{s} ; 0400-0600,17,15$ and $11 \mathrm{Mc} / \mathrm{s} ; 0600-0800$, 21,17 and $15 \mathrm{Mc} / \mathrm{s}$.
South Asia: $0600-1400,21,17$ and $15 \mathrm{Mc} / \mathrm{s}$; $1400-$ $1600,21,17,15$ and $11 \mathrm{Mc} / \mathrm{s} ; 1600-1800,21,17,15,11$, 9 and $7 \mathrm{Mc} / \mathrm{s}$; $1800-2200,17,15,11,9,7,7,6,5$ and $4 \mathrm{Mc} / \mathrm{s}$; $2200-2400,15,11,9,7,6$ and $5 \mathrm{Mc} / \mathrm{s} ; 2400-0200,15$, 11,9 and $7 \mathrm{Mc} / \mathrm{s} ; 0200-0400,15,11$ and $9 \mathrm{Mc} / \mathrm{s} ; 0400-$ $0600,17,15$ and $11 \mathrm{Mc} / \mathrm{s}$.
South East Asia: $0600-1000,21 \mathrm{Mc} / \mathrm{s}$ only; 1000-1200, 21 and $17 \mathrm{Mc} / \mathrm{s} ; 1200-1400,21,17$ and $15 \mathrm{Mc} / \mathrm{s} ; 1400-$ 1600, 21, 17, 15 and $11 \mathrm{Mc} / \mathrm{s}$; 1600-1800, 17, 15, 11 and $9 \mathrm{Mc} / \mathrm{s} ; 1800-2200,17,15,11,9,7,6$ and $5 \mathrm{Mc} / \mathrm{s} ; 2200-$ $2400,15,11,9$ and $7 \mathrm{Mc} / \mathrm{s} ; 2400-0200,15$ and $11 \mathrm{Mc} / \mathrm{s}$; 0200-0600, 17 and $15 \mathrm{Mc} / \mathrm{s}$.
North East Asia: 0600-2000, 17 and $15 \mathrm{Mc} / \mathrm{s}$; 20002200,15 and $11 \mathrm{Mc} / \mathrm{s} ; 2200-0600,15 \mathrm{Mc} / \mathrm{s}$.
Australia via Asia: $0600-1000,21 \mathrm{Mc} / \mathrm{s} ; 1000-1200$, $17 \mathrm{Mc} / \mathrm{s} ; 1200-1400,15 \mathrm{Mc} / \mathrm{s} ; 1400-1800,11 \mathrm{Mc} / \mathrm{s} ; 1800-$ $2200,11,9,7$ and $6 \mathrm{Mc} / \mathrm{s} ; 2200-2400$, 15 and $11 \mathrm{Mc} / \mathrm{s}$; $2400-0200,15 \mathrm{Mc} / \mathrm{s} ; 0200-0400$, Circuit closed to BC bands, $0400-0600,17 \mathrm{Mc} / \mathrm{s}$.

South America (North of the Amazon): 1200-1800, $21 \mathrm{Mc} / \mathrm{s} ; 1800-2000,21$ and $17 \mathrm{Mc} / \mathrm{s} ; 2000-2200,21,17$ and $15 \mathrm{Mc} / \mathrm{s} ; 2200-2400,17,15$ and $11 \mathrm{Mc} / \mathrm{s} ; 2400-0400$, $17,15,11,9,7$ and $6 \mathrm{Mc} / \mathrm{s} ; 0400-0800,15,11,9,7$ and $6 \mathrm{Mc} / \mathrm{s} ; 0800-1000,17,15$ and $11 \mathrm{Mc} / \mathrm{s} ; 1000-1200,17$ and $15 \mathrm{Mc} / \mathrm{s}$.
Those were propagation conditions from various parts of the world to the UK for July 1968. Now on to this month's DX-tips.

## EUROPE

Belgium: Radio Belgium, Brussels, is now giving very strong signals from 2115-2300 on 6,010 daily.

Denmark: R. Denmark, Copenhagen, is now on the following schedule--Danish only daily: 1130-1155, 1330-1345, 1730-1815 all on 15,165. Danish daily and English for last 30 mins on weekdays only: 0730-0845, $1200-1315,1400-1515$, and 1830-1945 all on 15,165, $0100-0215$ on 9,520 . Danish daily and Spanish for last 30 mins on weekdays only: $2200-2315$ on 15,165 . On Saturdays and Sundays only for the UK and Europe in English on 9,520.

Monaco: Trans-World Radio, Monte Carlo, is now using 7,260 in its English transmissions on Sunday afternoons from 1415-1530.

Poland: Polish Radio, Warsaw, is now on the following schedule for its transmissions to the UK and W. Europe in English-0730-0800, 11,840, 11,725, 9,675 and 9,$525 ; 1830-1857,11,815$ and 7,$125 ; 1930-$ 2000, 11,815, 9,570 and 7,125 ; 2030-2100, 11,815, 9,570 and 9,$540 ; 2130-2155,11,815$ and 7,125; 2230$2300,9,540,7,285,6,005$ and $1502 \mathrm{Kc} / \mathrm{s}$; 2303-2330, $818 \mathrm{Kc} / \mathrm{s}$. Daily classical music concerts: $1500-1600$ on $7,285,6,005$ and $1502 \mathrm{Kc} / \mathrm{s} ; 1900-2000$ on $7,285,6,005$ and $1502 \mathrm{Kc} / \mathrm{s}$. Music by Chopin daily: $0630-0700$ on $7,125,6,005$ and $1502 \mathrm{Kc} / \mathrm{s} ; 1600-1630$ on $7,285,6,005$ and $1502 \mathrm{Kc} / \mathrm{s}$. Light and popular music programmes: $1230-1400$ on $11,955,6,005$ and $1502 \mathrm{Kc} / \mathrm{s} ; 2330-0100$ on $9,540,7,125$ and $1502 \mathrm{Kc} / \mathrm{s}$.

Sweden: Radio Sweden is now operating as follows: 0445-0615 on 17,845; 0630-0715 on 6,065; 0830-0900 on 17,800 and 15,$240 ; 0930-1030$ on 21,690 and 9,625 ; 1030-1100 on 9,$625 ; 1100-1215$ on 15,240 and 9,625 ; 1230-1330 on 21,675 and 15,310; 1400-1530 on 21,585 and 17,$760 ; 1600-1700$ on 21,585 and 15,$310 ; 1730-$ 1800 on 15,240 and 6,$065 ; 1800-1830$ on 15,240 ; 18301930 on 21,690 and 15,$240 ; 1945-2015$ on 6,$065 ; 2015-$ 2115 on 11,915 and 6,$065 ; 2130-2230$ on 11,705 and 6,$065 ; 2245-2345$ on 15,445 and 11,$705 ; 2400-0230$ on 15,275 and 11,$705 ; 0300-0430$ on 11,705. English programmes are transmitted for 30 minutes daily at $1100,1230,1400,1600,1900,2045,2245,0030,0200$ and at 0330 .

## AUSTRALASIA

Australia: R. Australia has more alterations to its transmission schedule: $1800-2115$ now on 9,600 and 9,540 to the Pacific Isles in English; English to S.E. Asia now on 17,870 from 2245-0930; English to N.E. Asia now on 11,765 from 0900-1400; English to MidPacific from $0030-0830$ on 15,240, 0830-1215 on 7,190; New transmission in English from 0200-0800 to South Pacific on 15,180; The North American Service from $0100-0300$ is now on $21,740,17,840$ and 15,320 .

Many thanks for the Polish Radio schedule to A. Golics, and to others who have sent in items for use in the column. Deadline this month is the 15 th, so good listening.

# THE AMATEUR BANDS by DAVID GIBSON, G3JDG 

BIT of a mixed bag this month, some heard quite a lot of DX while others fished around at the wrong times. Never mind, reel in the antenna and stick another worm on. Stephen Herod (Suffolk) says that ten is best at weekends. Philip Batt (Lancs), informs of great doings on $21 \mathrm{Mc} / \mathrm{s}$ from 2115 to 2245 but says he can't often take advantage because he has to be up for school in the mornings. D. Spooner overheard 5H3JS saying that there are only eleven amateurs in Tanzania and only five of those are active.

Jim Baker has been given the go-ahead to arrange skeds between $G$ stations and JAlPFU in Yokohama on $21 \mathrm{Mc} / \mathrm{s}$ A.M. ONLY. (Down, you s.s.b. devils.) Any G's interested should drop Jim a line, his address is- 86 Max Road, Liverpool 14, Lancs. How about trying it with the club station?

## 10

S. Herod (Suffolk), R1O9A, 50ft. end-fed indoors plus an R.A.P. broadcast s/het logged these on $28 \mathrm{Mc} / \mathrm{s}-\mathrm{CN} 8 \mathrm{BG}, \quad$ CR4BL, CR7CI, ET3REL, LU1DAB, KV4DC, PY4KL, ZSIAX.
M. Pasek (Notts), QP-166 into an HRO, 150 ft . end-fed, detected the following hoard on tenCR6KK, CR7GH, LU6DRB, PY2ERS, VR6EBE (Pitcairn Island), VU2FN, VU2ER, ZC4RAF, ZC4RB, ZD8Z, ZEICCF, ZE1TX, ZSIXX, 4UITTU, 5Z4JH, 9J2WR, 9J2RA.
R. Dinning (Ayrshire), HA-350 + PR 30, 252 ft . endfed b.f.o'd these s.s.b. types into intelligibility on ten-ET3FMA, KP4CRD, LUIDAB, LZ2KKZ, OD5BA, UF6CR, VP8JC, XW8BS, ZE1WPC, 5Z4LG, 9J2BC, WI-W $\varnothing$.
P. Baker (S. Wales), HE30, 150 ft . end-fed, says $98 \%$ of these were s.s.b-CR6BF, ET3REL, HR1JMF, IT7GAL, K6PXQ/MM, K $\varnothing V P X / M M$, OD5-BA, BZ, CN, EP, FB, PZ1AW, SV1AN, SVøWL, TI3ALV, UF6CK, VOIAI, W9IOV/MM, YV5ADI, ZC4RB, ZC4RM, ZE2JA, ZS1FH, 5Z4LG, 9 J 2 DT , and all on $28 \mathrm{Mc} / \mathrm{s}$ too.

## 20/15

Still the favourite for most DX chasers, probably because it is the most consistent band of the lot.
R. Pusey (London, N.2), KW201 (I just went all green), 40 ft . inverted L at 15 ft . suffers from local QRM from underground trains and a factory. At times, this beautiful QRM was almost completely spoilt due to interference from-CN8BB, CP1HB, CR6DO, HB $\varnothing$ AG, HC5DR, HK6AWX, HL9KR, KH6FIL, OH6NS, PJ2CE, VE8ML, VK3IP, VK5HV VK5WD, W9ISN/MM, XE $\varnothing R Z W$, 9Q5HF, 9X5SP. Cor, wish I got QRM like that. It doesn't even keep to twenty, on fifteen he got savage bursts fromJA1DJL, KP4CRD, KV4AD, OD5BZ, OD5FG, PY2ARS, PY4DLH, ST4MO, SVØWM, VK9LR VK9WD, W4CQC/MM, ZE1AA, ZL1AIX, ZL1TU, 5H3JL, 6W8DY, 9M2NS, 9M2PO, 9Q5TR, 9V1MS, 9X5SP.
B. Bashford (Sussex), C52 set, 45 ft . end-fed, queries QQ7A heard in QSO with LA5YJ and claiming to be on Ganzo Island. Any comments? Brian also
sends in the following $\log$ for twenty s.s.b.-AP2SG, CM5AFF, CR6CN, CT2AP, F9HP/M, FC2CD, FK8AU, HM1AJ, HV3SJ, IØART, UA9WJ, UB5KMS, UI8AG, UO5AM, VP2KBE, UV3TQ, VE1DW, VE7TD, VK2DI, VK6SM, VU2HL, ZE2HW, ZL1AJ, ZS1JM, ZS3HX, 4X4HQ.
D. Higgins (Lanarkshire), KT340, 40ft. end-fed indoors, is having a crack at the RAE-hope you passed OM. Meanwhile, he's been keeping his hand in on twenty and fifteen. His $\log$ for 20 readsCE3AEV, CN8AAW, CR6BX, CT2AS, CX7AP, EA6ITU, EL4WI, EP3AM, ET3USA, HB4FE, HBøLL, HC8BY, HI3ELJ, HK7YA, HP!AA, HR1DB, HV3SJ, IZ6KDB (Ponza Island), LU4DEG, LU6AH1, OA4O, OY5NF, PI8LS, PJ2CB, PY9AI, PZ1BW, SK6AB, TF2WKM, TG9EP, UAØNM, UG6AW, UJ8AC, UL7LA, UV9OP, VK2NN, VK3XO, VK4SD, VK5HV, VK6FD, VK7RX. VP2AL, VP7NF, VP8HZ, 9H1T, 9K2AG, 9K2AM, 9M2XX, 9Q5HF, 9VINV, 9X5CG.

On fifteen metres-CR6GM, CR6LF, EA6ITU, EA8FG, EAØAH, EL2AL, ET3NPV, FG7XT, GB2SM, HL9TG, HP1LB, IZ6KDB, K3MFJ/MM, KC4CKW, LU1VH, MP4TCE, OD5FB, PY2BGL, SVICD, UD6BD, UF6FE, VK3AMK, VS9MB, VU2JM, WIPYM/P/KP4, WA4NMA/AM, XE3PI, XW8AX, ZD8RB, ZEICX, ZL1JN, ZL1TU, ZP5JB. ZS4IO, ZS6AO, 4 S7PB, $4 Z 4 \mathrm{HF}, 5 \mathrm{~A} 4 \mathrm{TZ}$, 5 W 1 AS , $5 Z 4 \mathrm{KK}, 9 \mathrm{G} 1 \mathrm{DY}, 9 \mathrm{H} 1 \mathrm{BD}, 9 \mathrm{~K} 2 \mathrm{BV}, 9 \mathrm{M} 2 \mathrm{DW}, 9 \mathrm{M} 2 \mathrm{PO}$, 9VICN, 9U5SK, 9X5AA, 9X5SP.

## 40

Yep, on its lil ol' own, coz only one person sent in a log I could put in.
F. McVerry (Lanarkshire), RF24 into an R1155, 40 ft . end-fed indoors, did a "lone ranger" on $7 \mathrm{Mc} / \mathrm{s}$. His catch included-CN8AW, CTIRR, EA8EZ, K3LLR, K5DJH/4, WøNEU/P/LA, PY1TX, PY2EGA, PY6NG, PY7APS, PY7ARP, PY7GAI, PY7VNY, TF3TF, UA9KPO, W1RGB, W2DIR, W2BHK, WA2JLJ, W3NNX, W4TLI, WA4WKM, WB4DGT, W4URR/MM, ZB2AP, ZS1JA, ZS2H.

## NEWS

July is a good month for contests and rallies. July 6th-7th, Topband Contest; 6th-7th, Cheltenham Festival Rally; 7th, South Shields Mobile Rally; 13th -14th, Field Day-High power h.f., this is a new contest. It is c.w. only from 3.5 to $28 \mathrm{Mc} / \mathrm{s}$ and the power limit is 150 watts; 14th, Worcester Mobile Rally; 21st, $70 \mathrm{Mc} / \mathrm{s}$ contest (portables); 21st, Cornish Mobile Rally at Newquay; August 3rd-4th, $144 \mathrm{Mc} / \mathrm{s}$ contest.
Letter from Fred (G3SVK) with all the gen on his DX-peditions ( tnx OM ) to the Channel Is. Pens ready? Sark:-28-31 July; Alderney:-August 1-4; Guernsey:-5-6; Jersey:-7-9. All c.w./s.s.b. $1 \cdot 8$ to $28 \mathrm{Mc} / \mathrm{s}$ with calls GC3SVK, GC3TTN, GC3LDH, GC3KNZ. QSL's via bureau or s.a.e. to home QTH except GC3SVK via G3TZZ.

Isles of Scilly, callsign to listen for-G3SVK/P August 31 -September $2,1.8$ to $28 \mathrm{Mc} / \mathrm{s}$ c.w./s.s.b. QSL's to G3TZZ with s.a.e. or via bureau.

T)
PP3 Eliminator. Play your pocket radio from the mains! save \&s. Cormplete component kit comprises 4 smoothing condenser and instrucsmoothing condenser and
tions. only $6 / 8$ plus $1 /$ - post.

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Pamous war-tme "cat's eye" used for seeing in the dark. This is an
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verter cell with a verter cell with a
silvercaesiumscrean which lights up (like a cathode ray tube) When the electrons released by the infra-red strike it. A golden opportunity for some will be supplied with cells, if requested.

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-continued from the July issue

IIATERIALS required for the Plate Contact Board are the piece of exterior quality hardboard $18 \times 5 \frac{1}{2} \mathrm{in}$. also $2 \times 18 \mathrm{in}$. lengths of $\frac{1}{2} \mathrm{in}$. square wood (ramin is ideal), 37 half-inch 6BA round head screws and nuts, 37 half-inch 6BA cheese head screws and nuts. The latter are for fixing the contact plates, and the cheese heads will be of assistance in holding a crocodile clip, while tuning that particular note. Thirty-seven double-ended tags will also be needed for the tuning resistance strip. The $\frac{1}{4} \mathrm{in}$. square strips of wood are fixed along the back and front edges of the board underneath flush with the edges. Glue and screw with countersunk heads, these act as stiffeners.
Place the resistance strip on the board as positioned in Fig. 5. Hold firmly in position. and choosing a hole near the centre, pencil mark a small circle through the hole on to the board. With a block of wood underneath, punch in the centre and drill through and bolt together, correctly align the strip and mark similarly, about quarter way along from each end, drill through and bolt up, and similarly deal with the first and last holes. With strip securely bolted up drill the remainder of the holes, using the tops ones as a guide.

Unbolt and remove the strip, and place aside, clean level if necessary with a flat file, where the board has been drilled. We now follow on with fitting the plates. This is a prominent part of the instrument, and is well worth doing neatly. First mark a pencil line $1 \frac{13}{16} \mathrm{in}$. from the front edge of the board, and parallel to it, a piece of hardboard, or wood about 1 in . wide and 1 ft .5 in . long is required as a straight-edge, and should be temporarily fixed, with edge along this line, and covering where the sharps will come later. It could be fixed with a screw at each end or between where the plates will come, the coloured felt to be fixed later would hide any holes. Measure along the pencil line, from the bass end edge mark at $9 \frac{5}{\text { IT }} \mathrm{in}$. with a set square, draw a vertical line, from front edge up to this mark.

Place plate $F$ No. 18 on this line, so that it passes up under the middle of the plate. The hole in the middle of the plate should now be on this line.

# portable KEYLESS ORGAN 

Draw a small circle through the hole to confirm. Punch and drill, and place a cheese head bolt through the two holes, put a single-headed tag and nut underneath and screw up finger tight. Should there be a gap between plate and straight-edge, or perhaps too tight, unbolt and elongate the hole in the board in the required direction to rectify the fault, using a small rat-tail file or wire file. When the plate is positioned correctly, bolt up securely. Now we need some thin cardboard spacing pieces, say $\frac{1}{8} \mathrm{in}$. wide strips of visiting card $1 \frac{1}{2}$ in. long and a few $2 \frac{1}{2} \mathrm{in}$. long, preferably cut off with a sharp knife, any spare phosphor bronze strip might serve. Take No. 17 plate and place on the left of No. 18, with a spacing piece in between and touching the straight-edge, mark centre hole as before and drill. Bolt up finger tight and correct as before if necessary. Keep proceeding in this manner, until all naturals are fixed. Tighten up with a screwdriver when satisfied all are straight and neat, remove the straight-edge.

Fix sharps as follows: Looking at D No. 3 Fig. 5 it will be noticed that the "crack" between C and D sharp is in line with a screw place a spacing strip against the top of 1,3 and 5 . The lower edges of 2 and 4 are now placed on the other side of the spacing piece and touching it, and in the correct position with a spacing piece in between them. Mark and drill as before. Looking at sharps 7, 9 and 11, it will be noticed that the "crack" between 6 and 8 is in line with the screw of No. 7, similarly with 8 and 10 , and 10 and 12 . Follow on in this way throughout.

Elongate any holes in board to shift position of plate where necessary. It is important that the finished job looks regular and neat, and with no shorts between plates.

All the plates are now removed and placed aside in order, and piece of felt laid as indicated in Fig. 5. The author used some scarlet felt as used at the back of piano keys. Use adhesive sparingly, just sufficient to hold the felt in place while fixing plates, overlap edges and trim off for a neat finish.

Commence refixing the plates with No. 18 F. Pierce through the felt into the hole, and fit up as before, keeping the felt flat and smooth, proceed until completed. The 37 holes for connecting wires are marked off in line with the plate screws, as shown in Fig. 5 and drilled with a $1 / 16 \mathrm{in}$. drill.

Now the resistance strip can be fitted on the board. Lay the strip with the holes corresponding, and start from the middle by placing a double ended tag on a screw and pushing through the two holes, place a nut on the screw under the board, and make finger tight. Soldering tags are usually stamped out on a machine, thus leaving a rounded finish on one side, and a sharp edge on the other. The rounded side should be presented to the graphite track, as the other side could cut it. Work from the centre each way, until all are in place and just finger tight.

Still working outwards from centre, tighten up with slight pressure, at same time placing the double ended tags astride the strip. Now the back part of the tags where projecting are bent down firmly over the back edge. The front part of the tags are left for later soldering a wire which will go through a $1 / 16 \mathrm{in}$. hole and then underneath to tags, on the bolts which hold the plates. Proceed to tighten up all screws securely on the resistance strip. The success of this idea relies upon rigidity and firmness of contact with the graphite surface. The author does not claim any originality in use of a lead pencil as a resistance, old hands will recollect its use as a grid leak with early detector valves.

To assist in tuning, a paper strip should be prepared with letters aligned with the spaces between the screws, and stuck down in position as in Fig. 5.

Drill a hole at the treble end to take the tuning preset control VR3. In the prototype there was just room to fit a simple on/off switch in this position. The vibrato switch is fitted towards the bass end in the position indicated. It only now remains to wire up the resistance strip tags to their respective plates. Keep wires taut for neatness.

Wiring to VR3 and tuning switch should be followed from Fig. 7. Finally drill a hole about a $\frac{1}{4} \mathrm{in}$. from each end of the board, for two fixing screws.

## Making the case

Starting with the bottom of the case, we require $1 \mathrm{ft} .7 \frac{1}{4} \mathrm{in} . \times 12 \frac{1}{2} \mathrm{in}$. of $\frac{1}{8} \mathrm{in}$. plywood. The back is made with a piece of wood $\frac{1}{2} \mathrm{in} . \times 3 \mathrm{in}$. $x 1 \mathrm{ft} .7 \frac{1}{4} \mathrm{in}$. long. The two sides are 3 in . wide x 12 in . $\mathrm{x} \frac{1}{2} \mathrm{in}$. We also need some $\frac{3}{4}$ in. panel pins.

The long 3 in . wide piece is placed along the back, and flush with edge of the bottom board, and pinned together. The two side pieces are placed flush with the sides of the bottom board, and butted against
the backboard, fix with panel pins to back and bottom. This makes a shallow box with the long front piece omitted. Inside on the back piece of wood, make a pencil line $\frac{3}{3} \mathrm{in}$. down from the top, repeat each side for about 5in. from the back. A 1 ft . 6 in . length of $\frac{1}{2} \mathrm{in}$. square wood is fixed inside on the back, just below this line. Two short pieces continue round on each side. These will support the baffle board.

On the bottom board, inside the case, measure 5 in . and mark at each end and middle, parallel with the open front edge of the case. Fix across the case a piece of wood 1 ft . 6 in . long, $1 \frac{3}{4} \mathrm{in}$. wide, and $\frac{1}{2}$ in. thick along these marks with the $\frac{1}{2}$ in. edge downwards, and leaving marks just visible. Fix on the back of this piece of wood another of same thickness and length, but $1 \frac{1}{2} \mathrm{in}$. wide, so that the uppermost edge is level with the two side fillets, and thus completing the support for baffle board all round. A carrying handle should now be fitted to the right-hand side of case.

For the baffle board, a piece of $\frac{1}{8}$ in. plywood is cut to fit on these fillets and approximately 1 ft . 6 in . $x 6 \frac{5}{8}$ in., check for exact size. The aperture for the loudspeaker should next be cut out. The baffle does not need to be fixed, as the top will be screwed down and will secure it. The material for covering the speaker is later fixed on the outside of the baffle, as there will be a corresponding hole cut in the top. Measurements allow for'thickness up to $\frac{1}{8} \mathrm{in}$. for the material. The top and cover are made in three pieces. The back part is fixed to the back and sides of case with round head screws and is 1 ft . $7 \frac{1}{4} \mathrm{in}$. x 7 in . approximately. The front half is about $5 \frac{1}{8} \mathrm{in}$. wide, exact size is best arrived at by first fixing the back half, and then measuring to front of case. Similarly with the front flap. Three fancy surface fitting hinges secure the back half to the front, and another three secure the flap to the front half. These are obtainable from D.I.Y. shops, as well as the carrying handle. The front flap needs to be held down, and a simple method is to fix a small screw eye in the centre of the $\frac{1}{4} \mathrm{in}$. square wood, as described later, to be fixed along and level with the front edge of the bottom board. Where this screw eye marks the inside of the flap cut a corresponding slot to receive it, and it will then only need a turn to secure the flap.
To complete the front compartment, a small panel of aluminium is made up from a piece bent up at right angles, and large enough to take the toggle switch (mellow/bright tone), and just on its right


Fig. 5: Constructional details of the contact plate board and tuning strip.


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the expression (volume) control. The panel is recessed inside the compartment, so that knobs do not project out of line with the front of the case. A short piece of $\frac{1}{2} \mathrm{in}$. square wood is fixed along the bottom edge of the small piece of plywood, and when pinned to it, is placed behind the expression control and fixed to bottom board with a couple of screws through the $\frac{1}{2} \mathrm{in}$. square wood. On the right hand side a similar panel is fitted up with the main on and off toggle switch, and also enclosed with a small piece of plywood. A 1 ft . 6in. length of $\frac{1}{4} \mathrm{in}$. square wood is fixed flush with the front edge of the bottom board. Bostik No. 1 will hold it well without pins. The compartment now left will later house the two wands etc.

A cover for the resistance strip is made with a piece of matching coloured plastic, similar to formica, purchased as an off-cut. Cut a length to just cover the length of the resistance strip, and wide enough to cover it and the tags with their wires and also allow for fixing two strips of $\frac{1}{4} i n$. square wood along and level with the two edges, and to rest on the hardboard. Attach the wood to the plastic with Bostik No. 1. This cover needs to be easily removed for tuning, and the method used by the author works quite well. About 4in. from each end of the front strip of wood, screw in a small brass screw from underneath. Snip off the head, file clean and slightly round. Fit the two spigots thus left into two corresponding holes of a close fit drilled in the hardboard.

## Finishing the case

The author removed all the components and glasspapered all over the exterior, making a slight radius on all edges and corners. File down any protruding pins or screws, fill in as required with Polyfilla. After this has hardened and been glass-papered level, remove all dust and give two coats of emulsion paint all over. The colour should be as near as possible to the finishing colour which was cream in the author's case. With fine glass-paper, give all exterior a gentle rub down and good dusting, and the job will be ready for a finishing coat of any good enamel or paint. Refix the carrying handle.
It is advised that a small square of thick felt be placed and fixed with Bostik at each corner on the bottom of the case. The front half of the top with flap attached will need a support to keep it from closing up the loudspeaker aperture. A narrow strip of leather about 6 in . long should be fixed to the front half with a small screw and washer and the other end similarly fixed to the contact board, say at the extreme bass end. When fixed the front half should be held up at an angle similar to a music desk, leaving the loudspeaker well clear. When closed the leather should fold in half, out of the way.

Two more square pieces of felt should be fixed, one at each end, just inside the front compartment. These should receive an occasional rub with the wands to clean the contacts at the ends.

## Making the wands

Two are recommended, and their use will be gone into fully later. Two strips of wood about $5 / 16 \mathrm{in}$. wide and $3 / 16 \mathrm{in}$. thick of ramin or hardwood, are required, both 9 in. long. A $\frac{1}{4} \mathrm{in}$. from one end, in the centre of the widest side, drill a
hole to take a $\frac{1}{8} \mathrm{in}$. aluminium rivet, held firmly. A piece of wood, end grain uppermost is fixed in a vice. A $\frac{1}{8} \mathrm{in}$. round head rivet is placed head down, held in small pliers and tapped firmly with a hammer to form a depression to match in the wood. Place the rivet head held in the wand to fit into this depression, place a soldering tag on the stem, pointing down the wand. Push down on the tag firmly with a pointed awl, snip off the stem all but $1 / 16 \mathrm{in}$., this should now be gently tapped with a hammer all round to form a burr to hold the assembly firmly together. This end of the wand is now tapered and filed around the end and close to the rivet head. Drill a $1 / 16 \mathrm{in}$. hole $\frac{1}{2} \mathrm{in}$. from the end of the tag. The fine plastic-covered stranded wire from the tag will go through the hole to the underside of the wand and along its length, to be Sellotaped the other end where it is soldered on to the miniature twin cored and screened cable.

Wand 2 is made in the same way, but this one has a simple on and off switch connected to the control circuit on the output panel, so that the preamp can be controlled to give a gradual decay of the sound, as required. Normal playing will be done with the switch closed with the forefinger.

To make the switch, measure $3 \frac{1}{2} \mathrm{in}$. and $4 \frac{5}{8} \mathrm{in}$. from the rivet and mark the wood. At each mark drill through the wood to take an 8 or 6BA screw, preferably round head. At the $4 \frac{5}{8} \mathrm{in}$. marked hole, put a round head screw through from the top of the wand, and place a soldering tag on underneath and nut, with the tag pointing away from the rivet. Prepare a piece of $\mathrm{p} / \mathrm{b}$ bonze or spring brass $1 \frac{3}{4} \mathrm{in}$. long $x \frac{1}{4} \mathrm{in}$. wide, drill two holes, one at $3 / 16 \mathrm{in}$. and another at $\frac{1}{2}$ in. from one end. The latter should have a round head screw pushed through the spring and the hole in the wood ( $3 \frac{1}{2}$ in. from the rivet), put a soldering tag on underneath also pointing from the rivet and fit the nut.

The remaining hole in the spring metal only needs a small round head wood screw to be driven into the wood after the spring metal has been correctly aligned down the wand and resting on the head of the first R.H. screw. The spring metal is now lightly bent upwards so that it is easy to make and break


View of the organ with the loudspeaker panel removed.
contact with the latter screw head. To complete wand 1, as this only requires one conductor, the two cores and screening are soldered together and joined to the thin stranded conductor from the rivet contact, in a neat bundle near the end of the wood farthest from the rivet contact.

Wand 2 should have a length of thin stranded connecting wire soldered to the tag on the rivet contact, and cut off at the other end of the wand. We now need two-core screened wire, one yard for each wand, which must be plastic covered. Solder the screening to the wire from the rivet and the two cores to the two tags underneath the switch. Make a neat bundle and bind tightly down on the wood, with coloured Sellotape and along the length of the wand leaving the switch and contact rivet clear.

## Testing panels and wiring up to controls

The note generator panel should be tested by inserting a meter in the negative battery lead that goes to the panel. A connection from the positive tag on panel is taken to battery positive. Reading should be about 2 mA . The vibrato circuit is similarly tested in a similar fashion. Vibrato switch should be closed, or the terminal tags on the panel shorted temporarily. Reading should also be about 2 mA and if oscillating the needle should fluctuate. If all is in order connect up to the output panel, and to loudspeaker as shown in Figs. 2 and 4. The two tags which will later take wand 2 switch should be temporarily shorted. 4.5 V negative goes to the tag provided. The positive potential should be provided through the interpanel connection. Before a note will sound it is necessary to connect a wire from 4.5 V negative on the generator panel to tag connected to R7 where VR3 will ultimately be connected.

Assuming that the two panels are working all right we can proceed with the wiring up of batteries and controls. The two panels and batteries are all fitted into the back compartment under the baffle board. The note generator panel to the right against the back, and the output panel to the right and against the back. The loudspeaker magnet should occupy the space between the panels. Batteries are held in position with the three aluminium clips, fixed to the top of the dividing board which should have recesses cut into it, and clips fixed


Fig. 6: Details of battery connection.
with countersunk screws, so as not to interfere with the bedding down of the baffle board.

The first battery clip to hold the two 4.5 V batteries will need to be about 6 in . long by about $\frac{3}{4} \mathrm{in}$. wide. One end will be screwed down on the dividing board at about 3in. from the bass end. The two batteries are laid on their sides, Sellotaped together. The clip can then be pushed down and over them and bent out at the other end to rest on the bottom board to which it can eventually be screwed.

The second clip should be placed about halfway along the dividing board, a $\frac{1}{2}$ in. wide strip $3 \frac{1}{2}$ in. long will be needed and after fixing as before is bent down and over a 4.5 V battery lying on its side. Only the one fixing should be necessary for one battery. The third clip is fitted same as the second one and the 4.5 V battery is positioned at the treble end with the clip about 3 in. from the end.


Fig. 7: Wiring of the tuning switch and pre-set tuning control.
Proceed with the wiring up of the expression control as detailed in Fig. 4. It will be necessary to cut a slot in the dividing board to take the cable. The vibrato switch will also need a small slot cut out to take two leads which go to the tags provided on the panel. See Fig. 7 for details of wiring to tuning switch and preset control, more slots or holes will be needed in the dividing board to take the wires. The two wands will need holes drilled at each end of the front stowage compartment, through the dividing board. A hole will also be necessary for the wires to the main switch.

All that now remains is to connect up the batteries to the panels. Commence with the two separate 4.5 V batteries, by connecting their positives together and taking to one pole of the main switch, the positive of the 9 V battery goes to the other pole of the double-pole switch. While proceeding with the negative connections to panels, see that the main switch is off. It is necessary to have a double-pole switch in this position, as with a single-pole one there would be a difference of potential between the 4.5 V and the 9 V batteries, causing a continuous slight leak, in spite of the switch being off. The other two connections on the switch are joined together and the wire is taken direct to the positive tag on the output panel, this is detailed in Fig. 6. It only now remains to bring out two wires from the tags marked "to VR3" with an extra one from the tag marked "to top C plate", these can be stranded bell wire, and all three twisted together and brought

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out through a hole in the dividing board at the treble end and connected up as indicated. Finish with the connections to the tuning switch, see Fig. 7.

## Tuning

It is assumed the constructor has arrived at the stage where the top $C$ sounds when tuning switch is on, and vibrato and wands working OK. The next step is to get the resistance strip tuned. With top C sounding, check with a tuning fork. The fork should be struck on the knee, while holding by the stem, and then placed near the ear and tuning control slowly rotated until beats are at zero. The result should be perfect unison, both sounding together as one. If the constructor has access to a piano tuned to pitch, or a piano accordion for this first tuning, all will be straightforward. Tuning must always start from the top note, working down in half-tone stages. It must be explained that the system recommended for this first or rough tuning, in which the strip has been completely covered with graphite, means that they will mostly have to be flattened. From experience this has been found to be the easiest way, for the initial set-up of the tuning strip.

A crocodile clip should be connected to a 2 ft . length of flex, and the other end to 4.5 V negative (B1) on the note generator panel, and clip placed on the cheese head of the second plate down from the top $C$. Tuning switch and vibrato should be switched off, now note $B$ should be sounding, tune with $B$ on the piano by rubbing off some of the graphite between the two top screws with a soft pencil rubber. This will flatten the note; if required to be sharpened, use a HB pencil and rub the lead from one tag to the next by the screw round heads, if necessary work outwards each side to the edge of strip. When roughly in tune proceed with the next note $A$ sharp in the same way. When finished start again, check the $C$ is still correct and proceed again downward, this time it will go much quicker, some notes hardly requiring attention. After a recommended break we can tackle the third and last tuning, taking particular care that each note is well in tune with the piano, that is with complete absence of beats.

It is possible that occasionally a case may arise when it is impossible to raise the pitch of a note beyond a certain limit short of that required, this can be the result of a poor contact under the tags
on either side, try the left-hand one first by undoing the screw, lifting tag and rubbing the pencil lead well all around the hole and just beyond the area covered by the tag, and replacing the nut very tightly. Make sure that plate screw is still tight. The note will now probably be too high, flatten with the rubber until correctly in tune. Once this tuning has been done, it will require only occasional attention afterwards. The author checks through the tuning with the piano just after that has had its periodical tuning. This takes only a few minutes, and is very pleasurable to play afterwards, when really correctly in tune.

We will now consider the case of a constructor who has no piano or is unable to have the use of one for the first tuning. A tuning fork or pitch pipe is essential, and with the top C tuning switch on, adjust the tuning control as before. Switch off the tuning switch and place the crocodile clip to B cheese head when it should be obvious if that note requires to be sharpened or flattened. Attend to this accordingly as before. It must be mentioned that it is no use humming the notes of the natural scale Doh Te Lah Soh Fah Me Ray Doh because tuning of the sharps afterwards will alter the tuning of these. If the constructor has a good ear and can hum the chromatic scale carry on tuning for a complete octave. Concentrate on this octave until satisfied that it is reasonably in tune. A musical programme from the radio might help in checking. Assuming the octave is reasonably in tune, now place the clip on C one octave below top C and using wand 2 with its switch closed, and top $C$ switched off, touch top $C$ plate, if this is quickly taken off and on the octave notes will sound in a rapid alternating sequence and give a fair indication of in tune-ness, flatten or sharpen as before while doing this. Proceed with the next note $B$ (24) place a clip on this, now use Wand 2 as before, but on the octave higher $B$ (36) proceed as before, until bottom $C$ is reached and tuned.

It is possible to obtain a complete set of tuning forks for one octave, but these would cost a few pounds. A complete octave of pitch pipes would be a cheaper proposition. These use reeds similar to a mouth organ. A chromatic mouth organ would also serve but is fairly expensive. Your local music store might help. These are all tuned to standard pitch, but should be confirmed if one is purchased.

## TO BE CONCLUDED NEXT MONTH

## IMPORTANT

DON'T BU̇Y PRACTICAL WIRELESS and then allow it to become torn and dirty. Don't search frantically through your back issues for that particular article either.

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## WIRELESS INDEX

The index to Volume 43 of Practical Wireless is now available from the Post Sales Department, George Newnes Ltd., Tower House, Southampton Street, London, W.C.2.

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## Shocking affair

I wish to draw your attention to the practice of some advertisers who advise that " 50 volts is easily obtainable between the 200 and 250 volt taps of a mains transformer".

- This is extremely hazardous practice, since if the user comes into contact with an earth or negative terminal a violent shock will be experienced which may be fatal under certain circumstances.

Should a 50 -volt supply be required, for example with surplus ex-GPO equipment or servo-systems, a suitable double-wound mains transformer should be used to safeguard the user.- $\mathbf{P}$. White (Freckleton, near Preston, Lancs.).

## P.O's and solder

This letter is intended as a warning to be careful when sending a postal order for something to be sent by mail.
I sent a P.O. for 3s. 6d. to a firm in London for a service sheet. The same P.O. was returned to me, which, I should have added, was crossed. I am still stuck with it after two weeks, so make it a s.a.e. every time men.

Also, to Mr. Parkinson of Grimsby (see letters May), a good way to remove solder without expensive gear is to give the object being soldered a quick flick and the hot solder will fly off usually on to your trousers. This is culled from a Practical Wireless from way back which I once read and never forgot.-J. Martin (Southowram, Halifax, Yorks.).

## Instant silence

With reference to the comments on "instant silence" by S. G. Hill (PW, March) I feel I must point out to him that these headset assemblies for W.S. 19 are available from several of the advertisers in P.W., catalogued often as Headset Assembly No. 10, complete with mic. but I know from experience that the No. 10 does not ensure silence when there is nothing being played in the phones, merely reducing it to an inaudible level when a signal is being received. The headset, furthermore, looks so ungainly as to make many fellow train passengers
doubt the sanity of your correspondent - so I would like to dissuade him from the use of such an assembly.-R. Davenport (address supplied).

## Death of a diode

On Wednesday, 3 April my crystal set suddenly died out and although I tried changing all the components it did not help. However, when I tried it today it was working all right. Could you possibly tell me why this should happen?C. Richmond (Hants.).
[Readers' post-mortems gratefully received-Editor.]

## Finale

Your correspondents Finn and Moult have torn me to pieces in your June issue and quite rightly so, under the circumstances they were very polite. I had based my assumption on the fact that I use a BY 100 in series with my soldering iron to reduce bit wear when the iron is idling for long periods. My iron is, of course, a 240 volt one running from 240 volt mains.
I now realise that I should have done my "sums" before committing pen to paper and I apologise most sincerely to anyone who has been misled by my letter in your March issue.-Mark Francis (Gloucs.).

## 30-line television

If by any chance a reader has one of the old 30 -line mechanical television receivers from the 1930s, we would very much appreciate details, as we are forming a wireless museum in connection with our local amateur radio society.
We would particularly like one of these vintage sets in time for our exhibition of old wireless receivers at our Mobile Rally, to be held on the banks of the River Nene at Peterborough on September 2D. Byrne (Peterborough Amateur Radio Society, Jersey House, Eye, Peterborough).

## Radio club-Yorkshire

Would any readers in the Morley area who would be interested in forming a local radio club please contact me. Members of all ages and all radio interests would be
extremely welcome.-B. Mellor (15 South View, Churwell, Morley, Yorks.).

## 19 set information

I appeal to any 19 set owners who could tell me the basic procedures of how to handle the receiver. I am having one for my 12th birthday and would be very grateful.M. Pickard (9 Robincross, Borrowwash, Derbyshire).

## Turn again Whittington

One has every sympathy with Mr. McLaren who did not receive the information he requested and paid for. (Letters, May issue.)
I recognise the firm from his description, and 1 do ask him to get in touch with them again even though I know the necessity should not have arisen. I think there must be a genuine mistake because I have dealt with this firm several times recently and have found the service quick and efficient by post, and on the two occasions I have called personally I was treated with the greatest patience and courtesy by the young lads in the shop.

I am a newcomer to the hobby and cannot be the easiest of customers to help. Their time-consuming advice has been quite invaluable to me in completing my relatively simple project.—J. Hackwood (London, S.E.9).

## Time Gentlemen please

Reference "MW Column" page 57 of the May 1968 issue of Practical Wireless. Alistair Woodland states: "The fact that GMT has now disappeared completely, etc., etc.". I must point out that this statement is erroneous and can be very misleading to a beginner.

It is only for an experimental period of three years that we are on British Standard Time, and it will then be decided one way or another what we finally do. However, GMT will always remain for reporting, and it is certain to remain where shipping is concerned, especially for navigation.

Further, on a point of interest, GMT is now more widely known as "Universal Time".-Lt.-Com. F. Behenna (London, S.W.1).


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(continued on next page)

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| $18 / 6$ |  |  |  |  |  |
| $1 W$ | $5 \%$ | $4 \cdot 7 \Omega$ | to $10 \mathrm{M} \Omega$ | E24 | $2 \uparrow$ |
| 10 | $17 /-$ |  |  |  |  |
| $10 \%$ | $4.7 \Omega$ | to $10 \mathrm{M} \Omega$ | E12 | $3 / 3$ | $25 / 10$ | 1/6 leas per 100 in 100 's of one ohmic value. PLEASE atate your choice of values. <br> QUALITY CARBON SKELETON PRE-8ETS: $100 \Omega, 250 \Omega, 500 \Omega, 1 \mathrm{k} \Omega, 2 \mathrm{k} \Omega, 2 \cdot 5 \mathrm{k} \Omega, 5 \mathrm{k} \Omega, 10 \mathrm{k} \Omega$, $2 \mathrm{M} \Omega, 2 \cdot 5 \mathrm{M} \Omega, 5 \mathrm{M} \Omega, 10 \mathrm{M} \Omega$. <br> A vailable in horizontal or vertical mounting 1/-each. LOW COST VOLUME CONTROLS: $100 \Omega$ to $10 \mathrm{M} \Omega$ $\operatorname{lin} 2 / 3$ each. $5 \mathrm{k} \Omega$ to $5 \mathrm{M} \Omega \log 2 / 8$ each. <br> CERAMICS: $100,220,170,1000,2200,4700 \mathrm{pF}$. $500 \mathrm{~V} 5 \mathrm{~d} .0 \cdot 005,0 \cdot 01,0 \cdot 02,0 \cdot 05 \mu \mathrm{~F} 50 \mathrm{~V}$ ' d . ELECTROLYTICS: $5,10,25,50 \mu \mathrm{~F} 10 \mathrm{~F}, 15$, Sub-min Mullard C426 range: all values in stock. Large or small orders despatched same day. <br> EVERYTHING BRAND NEW . NO 'SURPLUS' <br> SEND 1 /- for our catalogue containing data on 200 up-to-date semiconductors avallable from stock, as ents lable. Invalualie to every serious experimenter and designer. <br> DISCOUNT8: $10 \%$ over $£ 3,15 \%$ over 210 . <br> ELECTROVALUE <br> 6 MANSFIELD PLACE ASCOT BERKSHIRE}

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Duxford, Cambs. (Sawston 3031)
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$0.01,0.015,0.022 \mu \mathrm{~F}, 7 \mathrm{~d}$.
$0.033 \mu \mathrm{~F}, 8 \mathrm{a}$
$0.047 \mu \mathrm{~F}, 8 \mathrm{~d}$.
 $2 / 3.0 .47 \mu \mathrm{~F}, 2 / 8$.
Modular, metalised, P.C. mounting, $20 \%$, $250 \mathrm{~V}: 0.01$, $0.015,0 \cdot 022 \mu \mathrm{~F}, 7 \mathrm{~d} .0 \cdot 033,0.047 \mu \mathrm{~F}, 8 \mathrm{~d} .0 \cdot 068,0 \cdot 1 \mu \mathrm{~F}, 9 \mathrm{~g}$, $\begin{array}{ll}0 \cdot 15 \mu \mathrm{~F}, & 11 \mathrm{~d}, \\ 0 \cdot 68 \mu \mathrm{~F}, 22 \mu \mathrm{~F}, 1 / \\ 2 / 3 . & 1 \mu \mathrm{~F}, 2 / 9 .\end{array}$
POLISTXRENE CAPACITORS: $5 \%$ 160V (nnencapsulated): $10,12,15,18,22,27,33,39,47,56,68,82,100$, $120,150,180,220,270,330,390,470,560,680,820 \mathrm{pF}$. $6,800,8,200,10,000 \mathrm{pF}, 8 \mathrm{~d} .15,000,22,000 \mathrm{pF}, 9 \mathrm{~d}$. $6,800,8,200,10,000 \mathrm{pF}, 8 \mathrm{~s}$
$1 \%, 100 \mathrm{~V}$ (encapsulated) $=100,129,150,180,220,270$, $330,390,470,660,680,820 \mathrm{pF}, 1 /-1,000,1,200,1,500$ $1,800,2,200,2,700,3,300,4,700 \mathrm{pF}, 1 / 3,5,600,6,800$,
$8,200,10,000,12,000,15,000 \mathrm{pF}, 1 / 6.18,000,28,000$, $8,200,10,000,12,000,15,000 \mathrm{pF}, 1 / 6,18,000,22,000$,
$27,000,33,000,39,000 \mathrm{pF}, 1 / 9.0047,0.056 \mu \mathrm{~F}, 2 /-$ $27,000,33,000,39,000 \mathrm{pF}, 1 / 2.0 .047,0 \cdot 006 \mu \mathrm{~L}, 2 /-$
$0 \cdot 068,0 \cdot 082,0 \cdot 1 \mu \mathrm{~F}, 2 / 8,0 \cdot 12 \mu \mathrm{~F}, 2 / 9,0 \cdot 15,0 \cdot 18 \mu \mathrm{~F}, 8 /-$ $0 \cdot 22 \mu \mathrm{~F}, 4 /-, 0 \cdot 27,0 \cdot 33 \mu \mathrm{~F}, 5 /-0 \cdot 39 \mu \mathrm{~F}, 5 / 9,0 \cdot 47 \mu \mathrm{~L}, 6 / 8$. POTENTIOMETERS (Carbon), miniature, Itn. $\times$ gpindle. Lin. $100 \Omega$ to $10 \mathrm{M} \Omega$, Log $5 k \Omega$ to $5 M \Omega, 8 / 3$.
SKELETON PRE-SET POTENTIOMETER
(Carbon): Lin. $100 \Omega$ to $5 \mathrm{M} \Omega$. Horizontal and vertical P.C. mounting. Miniature $(0.3 \mathrm{~W}), 1 /-$. Submin. $(0 \cdot 1 \mathrm{~W})$, 10 d .
RESISTORS (Carbon film), very low noise. Range: $5 \%, 47 \Omega$ to $1 \mathrm{M} \Omega ; 10 \%, 10 \Omega$ to $10 \mathrm{M} \Omega$. W ( $5 \%$ ), 8d (over 99,1 d 1 d), 100 of per value $18 / 9$. IW ( $10 \%$ ), 2 d (over $99,1 \frac{18}{} \mathrm{~d}$ ), 100 off per value $13 / 9$. if ( $5 \%$ ), $2 t \mathrm{~d}$ (over $99,2 \mathrm{~d}$ ), 100 off per value $15 / 6$.

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## Send S.A.E. for May, 1968 Catalogue

(continued on facing page)

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EBF8
EBE8
EBF8
EBL1
EBL2



$5 / 6$
$6 /-$
$7 /-$
$8 /-$
$11 / 3$
$8 / 6$
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$13 / 6$
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## TRANSISTORS

| 16 | 201- | 0 C 203 | 1016 | AsY73 101- | JTX4A | 8/6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| OC23 | 12/6 | OC204 | 12/6 | AsY74 16/- | Mati01 | 1816 |
| OC.24 | 15/- | Oc205 | 15/- | A8Z17 151- | Mati20 | 7/9 |
| 0 C 25 | 7/6 | OC206 | 22/6 | AsZ18 151- | Mati21 | $18 / 6$ |
| $00^{026}$ | ${ }^{6 /-}$ | AC107 | 10/- | ${ }^{\text {Asz20 }}{ }^{7 / 8}$ | V30/30 P |  |
| $0 \mathrm{OC28}$ | 12/6 | AC125 | 3/6 | AsZ21 $12 / 6$ | - |  |
| O029 | 14/9 | ACl2 6 | 8/6 | AUY10 $201-$ | 2G309 |  |
| 0035 | 131- | AC127 | $7 / 6$ | ${ }_{\text {BC107 }}{ }^{7 / 6}$ | 2 C 371 A |  |
| C36 | 12/6 | AC128 | 6/8 | BC108 ${ }_{\text {BCY }}$ 6/8 | or | 31- |
| - | 91- | AC176 | $7 / 6$ |  | 2 C 381 | 8/6 |
| OC43 | 9/- | ACY17 | $8 / 8$ $5 / 6$ | BCZ33 $10 \%$ | ${ }^{2} \mathbf{N} 410$ | $3 / 6$ $3 / 6$ |
| $0{ }_{0}$ | ${ }^{3 / 8}$ | ${ }_{\text {ACY }}$ A 9 | ${ }_{6} / 6$ | ${ }^{\text {BF167 }} 818$ | ${ }_{2}^{2 N 412}$ | /6 |
| 0058 0.70 0 | 12/8 4 | ACY20 | 51- |  |  | 6/6 |
| 0.070 00671 | $4 /-$ $3 / 6$ | ACY21 | ${ }_{3}^{6 / 8}$ | BF184 BF194 7/6 | ${ }_{2}^{2 N 697}$ | $7 / 18$ |
| $\mathrm{OCO}^{\text {O }}$ | $5 /-$ | ACY22 | 18/8 | BFY10 $7 / 8$ | 2N706 | 8/6 |
| 0073 00675 | $7 / 8$ | AD149 | 16/- |  | 2N763 | 87/- |
| 0.775 0.76 | ${ }_{6 /}^{61}$ | AF102 | 18/- | $\begin{array}{lll}\text { BFY17 } \\ \text { BFY18 } & 8 / 8 \\ 5 /-\end{array}$ | ${ }_{2}^{2 N 11321}$ | 87/- |
| $0 \mathrm{OCF}_{7}$ | 81- | AF114 | 8/8 | BFY19 5/- | ${ }^{2} \mathrm{~N} 1304$ |  |
| 0 Ocis | 5)- | AF115 | 6/- | BFY50 8/6 | 2N1756 | 15/- |
| Cis | 51- | AF116 | 6/6 | BFY51 4/- | 2 N 2068 | 20/- |
| ${ }_{0} \mathrm{OC81}$ | $51-$ | $\mathrm{AFP17}^{\text {AF17 }}$ |  | BFY5 ${ }^{\text {B/6 }}$ | ${ }_{2}^{2 N} 232968$ |  |
| 0081 D $0 \cdot 83$ | $3 /-$ $5 /-$ | ${ }_{\text {AF112 }}$ | 10/- | $\begin{array}{ll}\text { BSY26 } \\ \text { B8Y28 } & 51 \\ 51\end{array}$ | 2N2926 | $\begin{gathered} 5 / 8 \\ 13 /- \end{gathered}$ |
| 0684 | $5 /-$ | AF125 | 8/6 | B8Y65 51- | 2 S 002 | 201- |
| 0 Cl 122 | 12/6 | AF126 | 6)- | GET103 5j- | 28003 | 20/- |
| ${ }_{0} \mathrm{OCl}_{139}$ | $7 / 6$ | AF127 | 6/- | GET104 8- | 28004 | 151- |
| OCl40 | 9/6 | AF178 | 12/6 | GET113 4/- | 28005 | 501- |
| OCl41 | $12 / 6$ | AF186 | 17/8 | GET114 4/- | 28006 | $201-$ |
| OC170 | $5{ }^{5}$ - | AFY19 | 22/6 | GET115 8/6 | 2801214 | 140) |
| $0 \mathrm{Cl71}$ | 6/- | AFZ11 | 171- | GET11610/- | 28018 | 601- |
| OC200 | 776 | AFZ12 | 10/- | GET872 61 - | 2S102 | 22/- |
| OC:201 | 10/- | AsY26 | 6/8 | GET875 6/- | 28103 | 25/- |
| OC202 | 13/- | A8Y28 | 6/6 | GET880 91 | 28104 | 15/- |

## I.C. AUDIO AMPLIFIERS Type CA3020 <br> Integrated Circuit Audio Amplifier in TOS encapsulation

 (size of a small transistor), equivalent to seven n-p-n 550 mW . Total harmonic distortion $1 \%$. Will operate on voltage from 3 to 9 volts.80/- plus 2/-p.p.

## DETECTOR DIODES

Germanium Point Contact:
OA5 $8 /=;$ OA6 $4 /-$ OA7 $4 /-;$ OA47 2/6; OA70 2/-; OA79 2/8; OA81 2/-; 0 A85 2/6; OA86 3/6. Subminiature: ©A90 2/f; OA91 2/-; 0A95 2/-
Silicon Function, subminiature:
OA200 2/6; OA202 3/6.

## SILICON POWER RECTIFIERS

BY100, 700 p.i.v., 450 mA , W.E.
BYZ10, 800 p.i.v., 5 Amps, S.M.
PYZ12, 400 p.i.v., 6 Amps, 8.M.
BYZ19, as BYZ13 but stud negai
DD000, 50 pii.v., 500 mA , W.E.
DD006, 400 p.i.v., 500 mA . W.E.
DD058, 800 p.W., 500 mA , W.E...................
Note: W.E.-Wire Ended; S.M.-stud Mounted.'.

## THYRISTORS

$3 / 40,400$ p.i.v. 3 amp stud mounted. Gate voltage 3.0v. at 20mA max. ...............................
BLUE SPOT, 200 p.i.v. 5 amp, stud mounted.
 Gate voltage $3 \cdot 25 \mathrm{v}$. at 120 mA max. .

## SPECIAL OFFER OF TRANSISTORS

AM/FM and SW KIT comprising two AF125 (mixer/ oscillator), two AF126 (1F), one ACl26 (audio) and two AC128 (push/puil output). 81/-post paid.
GERMANUM GENERAL PURPOSE. 2G371A or B, 2G813. 25/- per doz. sssorted.

COMPLEMENTARY PAIRS (PNP/NPN)
ACI28/AC176 (Germanium) 13/-; 2N697/2N1132 (silicon) 27/-; ASY26/ASY28 (Germanium) 12/-.

## 25 WATT SOLDERING IRONS

200-250 watt exceptionally well made lightweight soldering irons with polished wooden handles and chromium plated body. Angle bit of sufficient length for long Hife. No breakable plastics used in construction. PRICE 16/-
(P.P. 2/-).

## AVALANCHE SILICON RECTIFIERS

Type RAs508AF, 960 p.i.v. at 6 amps. max., stud 10/6

## DRY REED INSERTS

Glasa dry reed inserts approx. $\ddagger$ in. dis $x$ lin long with axial lads one make contact of 100 ma capacity at Amp.turns relay coils. PRICE 18/- per doz. post iree.

TEXAS SLLICON FULLLWAVE BRIDGE RECTIFIERS $1 \mathrm{B20K} 10100 \mathrm{piv}$, 2 amps , dimensions $1 \cdot 4 \times 1 \cdot 4 \mathrm{x} \cdot 6 \mathrm{in}$. $95 /-$ 1B100M10 $100 \mathrm{piv}, 10 \mathrm{amps}$, dimensions $2 \times 24 \mathrm{zlin} .85 /-$ Postage $1 / 6$ per rectifier.

## CATHODE RAY TUBES FOR OSCILLOSCOPES

$2 A P 1-2 \mathrm{in}$. screen. EHT 500 to 1000 V . Typical sen-
sitivity at $500 \mathrm{~V}, \mathrm{X}-220 \mathrm{~mm} / \mathrm{V} ; \mathrm{Y}-260 \mathrm{~mm} / \mathrm{V}$. USM11 sitivity at 500 V . X-220mm/V; Y-'260mm/V. USM11 Base. Oversil length 7 in . 1500 V . typical sensitivity
$3 \mathrm{BPl}-3 \mathrm{in}$. screen, EHT $3 \mathrm{BPl}-3 \mathrm{in}$, screen, EHT 1500 . $\mathrm{X}-150 \mathrm{mmV} ; \mathrm{Y}-200 \mathrm{~mm} / \mathrm{V}$. B14A Base.
$\qquad$
Both the above types are from current manufacture, not surplus or second hand.

## 10-watts STUD MOUNTED ZENER DIODES

$4.7 \mathrm{~V}, 5 \mathrm{~V}, 5.6 \mathrm{~V}, 6.2 \mathrm{~V}, 6.8 \mathrm{~V}, 75 \mathrm{~V}, 8.2 \mathrm{~V}, 9.1 \mathrm{~V}, 30.0 \mathrm{~V}$ $12 \cdot 0 \mathrm{~V}, 15 \cdot 0 \mathrm{~V}, 16.0 \mathrm{~V}, 18.0 \mathrm{~V}, 20.0 \mathrm{~V}, 24.0 \mathrm{~V}$,
$33.0 \mathrm{~V}, 36.0 \mathrm{~V}, 43 \cdot 0 \mathrm{~V}, 47 \cdot 0 \mathrm{~V}-$ al at $7 / 6$.

## MOVING COIL VOLTMETERS

Type 120DA: flange size 120 mm ( 4 sin) square:


The following blueprints are available from stock. Descriptive text is not available but the date of issue is shown for each blueprint. Send, preferably, a postal order to cover cost of the blueprint (stamps over 6d. unacceptable) to Blueprint Department, Practical Wireless, George Newnes Ltd., Tower House, Southampton Street, London, W.C.2.


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(b) We cannot undertake to supply detailed information for converting war surplus equipment, or to supply circuitry.
(c) It is usually impossible to supply information on imported domestic equipment owing to the lack of details available.
(d) We regret we are unable to answer technical queries over the telephone.
(e) It helps us if queries are clear and concise.
(f) We cannot guarantee to answer any query not accompanied by the current query coupon and a stamped addressed envelope.

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    New 12in. Speakers with Built-in Tweeter, 3 or 15 ohm, 28/6. Post paid.
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    Short wave TX Chassis. Two valve battery model, 8/6. P. \& P. paid. Model Makers Motor 26 volt will run from 12 or 6 volt. 7/6. P. \& P. paid.
    Motors removed from Washing Machines $\frac{7}{2}$ h.p. 1400 revs $250-200$ volt A/C complete with pulley, 26/-. P. \& P. $10 /=$
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